### LAND AREA:

55,024 SQ. FT. OR 1.263 ACRES MORE OR LESS

### **BASIS OF BEARING:**

BEARINGS ARE BASED ON THE NORTH LINE OF TRACT D, CARRIAGE MEADOWS NORTH FILING NO. 1, BEARING N 89°48'24" E, A DISTANCE OF 699.24 FEET, AS MONUMENTED AT BOTH ENDS BY A FOUND 1-1/4" YELLOW PLASTIC CAP STAMPED "FWS PLS 38226".

### **BENCHMARK:**

BASIS OF ELEVATIONS: ELEVATIONS ARE BASED UPON A FOUND 2" ALUMINUM CAP STAMPED "FARNSWORTH GROUP INC. PLS 38053" ON THE WEST LINE OF TRACT B (ELEVATION = 5724.52)

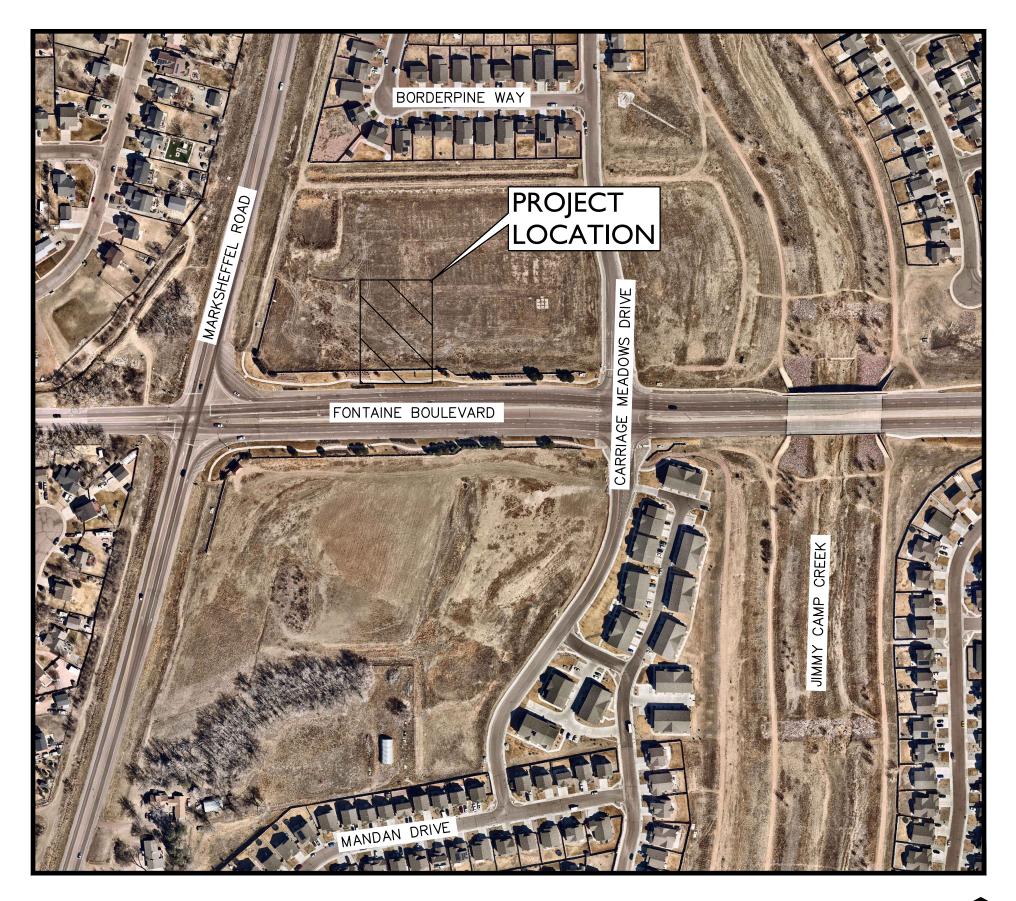
### LEGAL DESCRIPTION

VILLAGE AT LORSON RANCH FILING NO.1, LOT 2

### **GENERAL NOTES:**

- THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATIONS AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE.
- 2. THE OWNER IS AWARE THAT THE ACCESS PERMITS (AP211569, AP211570) ARE SUBJECT TO CONDITIONS OF APPROVAL.

# MCDONALD'S LOT 2 OF VILLAGE AT LORSON RANCH FILING 1 UTILITY CONSTRUCTION PLANS



### VICINITY MAP

NOT TO SCALE

VORTH

	UTILITY CONSTRUCTION PLANS
SHEET NUMBER	SHEET TITLE
3.0	COVER
3.1	NOTES
3.2	UTILITY PLAN
3.3	DETAILS

### CONTACTS:

<u>DEVELOPER:</u> MCDONALD'S USA, LLC 110 N. CARPENTER STREET CHICAGO, IL 60607 TEL: (206) 348–4374 CONTACT: ROBERT YAGUSESKY EMAIL: ROBERT.YAGUSESKY@US.MCD.COM

ENGINEER KIMLEY-HORN AND ASSOCIATES, INC. 2 NORTH NEVADA AVE., SUITE 900 COLORADO SPRINGS, CO 80903 TEL: (719) 453-0180 CONTACT: JESSICA MCCALLUM, P.E. EMAIL: JESSICA.MCCALLUM@KIMLEY-HORN.COM

LANDSCAPE ARCHITECT: KIMLEY-HORN AND ASSOCIATES, INC. 2 NEVADA NORTH AVE., SUITE 900 COLORADO SPRINGS, CO 80903 TEL: (719) 453-0180 CONTACT: JEREMY POWELL, P.L.A. EMAIL: JEREMY.POWELL@KIMLEY-HORN.COM TEL: (303) 228–2300 CONTACT: DARREN WOLTERSTORFF, P.L.S. EMAIL: DARREN.WOLTERSTORFF@KIMLEY-HORN.COM <u>OWNER:</u> CRADLAN, LLC 212 N. WAHSATCH AVE, SUITE 301 COLORADO SPRINGS, CO 80903

ARCHITECT: CORESTATES GROUP

NAPERVILLE, IL 60540

135 WATER STREET, SUITE 201

TEL: (224) 585-4591 CONTACT: JOY VRCHOTA EMAIL: JOY.VRCHOTA@CORE-STATES.COM

<u>SURVEYOR:</u> KIMLEY-HORN AND ASSOCIATES, INC.

6200 S. SYRACUSE WAY, SUITE 300

GREENWOOD VILLAGE, CO 80111

DISTRICT APPROVAL (WATER)

WIDEFIELD WATER AND SANITATION DISTRICT RECOGNIZES THE DESIGN ENGINEER AS HAVING RESPONSIBILITY FOR THE DESIGN AND HAS LIMITED ITS SCOPE OF REVIEW ACCORDINGLY. WIDEFIELD WATER AND SANITATION DISTRICT WATER DESIGN APPROVAL

DATE: BY:

PROJECT NO:\_\_\_\_\_

IN CASE OF ERRORS OR OMISSIONS WITH THE WATER DESIGN AS SHOWN ON THIS DOCUMENT THE STANDARDS AS DEFINED IN THE "RULES AND REGULATIONS FOR INSTALLATION OF WATER MAINS AND SERVICES" SHALL RULE.

APPROVALS EXPIRES 180 DAYS FROM DESIGN APPROVAL

### DISTRICT APPROVAL (WASTEWATER)

WIDEFIELD WATER AND SANITATION DISTRICT RECOGNIZES THE DESIGN ENGINEER AS HAVING RESPONSIBILITY FOR THE DESIGN AND HAS LIMITED ITS SCOPE OF REVIEW ACCORDINGLY. WIDEFIELD WATER AND SANITATION DISTRICT

WATER DESIGN APPROVAL

DATE: \_\_\_\_\_ BY:\_\_\_\_

PROJECT NO:\_\_\_\_

IN CASE OF ERRORS OR OMISSIONS WITH THE WATER DESIGN AS SHOWN ON THIS DOCUMENT THE STANDARDS AS DEFINED IN THE "RULES AND REGULATIONS FOR INSTALLATION OF WASTEWATER MAINS AND SERVICES" SHALL RULE.

APPROVALS EXPIRES 180 DAYS FROM DESIGN APPROVAL



now what's **below. Call** before you dig.

1									DESCRIPTION
									REV DATE
	Kimley » Horn								
	PREPARED BY:								
	Prepared For:	McDonald's USA. LLC	cations are the confidential and pr	property of McDonald's USA, LLC and shall not be copied or reproduced	without written authorization. The contract accuments were prepared for use on this specific site in conjunction with its issue date and are	not suitable for use on a different site or at a later time. Use of	urese arawings for reference or example on another project requires the services of properly licensed architects and engineers. Reproduction of	the contract documents for reuse on another project is not authorized.	
	DRAWN BY P		7/30/2024	REVIEWED BY	MUL	0	7/30/2024		
	TITLE	IITII ITV PI ANS		DESCRIPTION		COVER		SITE ID SITE ADDRESS	51028 NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO 51028 SPRINGS, CO
·	<u>.</u> -		-	3		<u>)</u>			

### PRIVATE ENGINEER'S NOTICE TO CONTRACTORS:

- THE FOLLOWING NOTES ARE PROVIDED TO GIVE DIRECTIONS TO THE CONTRACTOR BY THE ENGINEER OF THE PLANS.
- 1. THE APPROVAL OF THIS PLAN OR ISSUANCE OF A PERMIT BY WIDEFIELD WATER AND SANITATION DISTRICT DOES NOT AUTHORIZE THE SUBDIVIDER AND OWNER TO VIOLATE ANY FEDERAL, STATE OR COUNTY LAWS, ORDINANCES, REGULATIONS, OR POLICIES.
- 2. NEITHER THE OWNER, NOR THE ENGINEER OF WORK WILL ENFORCE SAFETY MEASURES OR REGULATIONS. THE CONTRACTOR SHALL DESIGN, CONSTRUCT, AND MAINTAIN ALL SAFETY DEVICES, INCLUDING SHORING, AND SHALL BE SOLELY RESPONSIBLE FOR CONFORMING TO ALL LOCAL, STATE AND FEDERAL SAFETY AND HEALTH STANDARDS, LAWS, AND REGULATIONS.
- 3. CONTRACTOR AGREES THAT HE/SHE SHALL ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOBSITE CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THIS PROJECT, INCLUDING: SAFETY OF ALL PERSONS AND PROPERTY, AND THIS REQUIREMENT SHALL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS; AND THAT THE CONTRACTOR SHALL DEFEND, INDEMNIFY, AND HOLD THE OWNER AND ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT EXCEPT LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF THE OWNER OR THE ENGINEER.
- 4. THE CONTRACTOR SHALL BE RESPONSIBLE TO INSURE THAT ALL SLOPES, STREETS, UTILITIES, AND STORM SEWERS ARE BUILT IN ACCORDANCE WITH THESE PLANS. IF THERE IS ANY QUESTION REGARDING THESE PLANS OR FIELD STAKES, THE CONTRACTOR SHALL REQUEST AN INTERPRETATION BEFORE DOING ANY WORK BY CALLING THE ENGINEER OF RECORD AT 719-453-0180. THE CONTRACTOR SHALL ALSO TAKE THE NECESSARY STEPS TO PROTECT THE PROJECT AND ADJACENT PROPERTY FROM ANY EROSION AND SILTATION THAT RESULT FROM HIS OPERATIONS BY APPROPRIATE MEANS (SAND BAGS, HAY BALES, TEMPORARY DESILTING BASINS, DIKES, SHORING, ETC.) UNTIL SUCH TIME THAT THE PROJECT IS COMPLETED AND ACCEPTED FOR MAINTENANCE BY WHATEVER OWNER, AGENCY, OR ASSOCIATION IS TO BE ULTIMATELY RESPONSIBLE FOR MAINTENANCE.
- 5. EXCEPT AS NOTED HEREON ALL UTILITY SERVICES WITHIN THIS DEVELOPMENT ARE UNDERGROUND INSTALLATIONS. THE CONTRACTOR SHALL NOTIFY ALL UTILITY COMPANIES PRIOR TO STARTING WORK NEAR THEIR FACILITIES, AND SHALL COORDINATE HIS WORK WITH COMPANY REPRESENTATIVES. FOR UTILITY MARK-OUT SERVICE, CALL 811.
- 6. THE EXISTENCE AND LOCATION OF UNDERGROUND UTILITIES OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED FROM A SEARCH OF THE AVAILABLE RECORDS. TO THE BEST OF OUR KNOWLEDGE THERE ARE NO OTHER EXISTING UTILITIES EXCEPT AS SHOWN ON THESE PLANS. NO REPRESENTATION IS MADE AS TO THE ACCURACY OR COMPLETENESS OF SAID UTILITY INFORMATION. THE CONTRACTOR IS REQUIRED TO TAKE PRECAUTIONARY MEASURES TO PROTECT THE UTILITY LINES SHOWN HEREON AND ANY OTHERS NOT OF RECORD OR NOT SHOWN ON THESE PLANS. ALL DAMAGES THERETO CAUSED BY THE CONTRACTOR SHALL BE REPAIRED TO THE APPROPRIATE SPECIFICATIONS AND STANDARDS AT THE EXPENSE OF THE CONTRACTOR.
- 7. LOCATION AND ELEVATION OF EXISTING IMPROVEMENTS SHALL BE CONFIRMED BY FIELD MEASUREMENTS PRIOR TO CONSTRUCTION OF NEW WORK.
- 8. CONTRACTOR SHALL MAKE EXPLORATORY EXCAVATIONS AND LOCATE EXISTING UNDERGROUND FACILITIES SUFFICIENTLY AHEAD OF CONSTRUCTION TO PERMIT REVISIONS TO PLANS IF REVISIONS ARE NECESSARY BECAUSE OF ACTUAL LOCATION OF EXISTING FACILITIES.
- 9. FOR ALL UTILITY TRENCHES, SOILS REPORTS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD BY A QUALIFIED SOILS ENGINEER WHICH CERTIFY THAT TRENCH BACKFILL WAS COMPACTED AS DIRECTED BY THE SOILS ENGINEER IN ACCORDANCE WITH THE ON-SITE EARTHWORK SPECIFICATIONS.
- 10. ANY WORK DONE WITHOUT INSPECTION OR MATERIALS TESTING IS SUBJECT TO REMOVAL OR CORRECTION.
- 11. CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVAL OF ANY DAMAGE TO THE EXISTING IMPROVEMENTS AND REPLACEMENT TO THE SATISFACTION OF THE FIELD ENGINEER.
- 12. PRIOR TO COMMENCING CONSTRUCTION, THE CONTRACTOR SHALL VERIFY ALL JOIN CONDITIONS FOR GRADING, DRAINAGE AND UNDERGROUND FACILITIES, INCLUDING LOCATION AND ELEVATION OF EXISTING UNDERGROUND FACILITIES AT CROSSINGS WITH PROPOSED UNDERGROUND FACILITIES. IF CONDITIONS DIFFER FROM THOSE SHOWN ON THE PLANS THE CONTRACTOR SHALL NOTIFY THE ENGINEER AND SHALL NOT BEGIN CONSTRUCTION UNTIL THE CHANGED CONDITIONS HAVE BEEN EVALUATED.
- 13. THE CONTRACTOR SHALL FAMILIARIZE HIMSELF/HERSELF WITH THE PLANS, THE SOILS AND/OR GEOLOGY REPORTS, AND THE SITE CONDITIONS PRIOR TO COMMENCING WORK.
- 14. SHOULD CONFLICTING INFORMATION BE FOUND ON THE PLANS OR IN THE FIELD, THE CONTRACTOR SHALL NOTIFY THE PROJECT ENGINEER AT KIMLEY-HORN BEFORE PROCEEDING WITH THE WORK IN QUESTION.
- 15. THE CONTRACTOR SHALL BE RESPONSIBLE FOR SURVEY MONUMENTS AND/OR VERTICAL CONTROL BENCHMARKS WHICH ARE DISTURBED OR DESTROYED BY CONSTRUCTION. CONTRACTOR'S LAND SURVEYOR MUST FIELD LOCATE, REFERENCE, AND/OR PRESERVE ALL HISTORICAL OR CONTROLLING MONUMENTS PRIOR TO ANY EARTHWORK. IF DESTROYED, CONTRACTOR'S LAND SURVEYOR SHALL REPLACE SUCH MONUMENTS WITH APPROPRIATE MONUMENTS. A CORNER RECORD OR RECORD OF SURVEY, AS APPROPRIATE, SHALL BE FILED AS REQUIRED BY THE PROFESSIONAL LAND SURVEYORS ACT. IF ANY VERTICAL CONTROL IS TO BE DISTURBED OR DESTROYED, THE COLORADO SPRINGS (EL PASO COUNTY) FIELD SURVEY SECTION MUST BE NOTIFIED, IN WRITING, AT LEAST 3 DAYS PRIOR TO THE CONSTRUCTION. THE CONTRACTOR WILL BE RESPONSIBLE FOR THE COST OF REPLACING ANY VERTICAL CONTROL BENCHMARKS DESTROYED BY THE CONSTRUCTION.
- 16. DEVIATIONS FROM THESE SIGNED PLANS WILL NOT BE ALLOWED UNLESS THE COUNTY OR DISTRICT ENGINEER APPROVES A CONSTRUCTION CHANGE OR THE COUNTY/AGENCY INSPECTOR REQUIRES THE CHANGE.
- 17. AS-BUILT DRAWINGS MUST BE SUBMITTED BY THE CONTRACTOR TO THE ENGINEER PRIOR TO ACCEPTANCE OF THIS PROJECT.
- 18. THE AREA WHICH IS DEFINED AS A NON GRADING AREA AND WHICH IS NOT TO BE DISTURBED SHALL BE STAKED PRIOR TO START OF THE WORK. THE PERMIT APPLICANT AND ALL OF THEIR REPRESENTATIVES OR CONTRACTORS SHALL COMPLY WITH THE REQUIREMENTS FOR PROTECTION OF THIS AREA AS REQUIRED BY ANY APPLICABLE AGENCY. ISSUANCE OF THE CITY'S GRADING PERMIT SHALL NOT RELIEVE THE APPLICANT OR ANY OF THEIR REPRESENTATIVES OR CONTRACTORS FROM COMPLYING WITH ANY STATE OR FEDERAL REQUIREMENTS BY AGENCIES INCLUDING BUT NOT LIMITED TO COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT OR COLORADO DIVISION OF WILDLIFE. COMPLIANCE MAY INCLUDE OBTAINING PERMITS, OTHER AUTHORIZATIONS, OR COMPLIANCE WITH MANDATES BY ANY APPLICABLE STATE OR FEDERAL AGENCY.
- 19. NOTES AND DETAILS DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS. WHERE NO DETAILS ARE GIVEN, CONSTRUCTION SHALL BE AS SHOWN FOR SIMILAR WORK.
- 20. IF AT ANY TIME DURING THE GRADING OPERATION, ANY UNFAVORABLE GEOLOGICAL CONDITIONS ARE ENCOUNTERED, GRADING IN THAT AREA SHALL STOP UNTIL APPROVED CORRECTIVE MEASURES ARE OBTAINED.
- 21. STRAIGHT GRADE SHALL BE MAINTAINED BETWEEN CONTOUR LINES AND SPOT ELEVATIONS UNLESS OTHERWISE SHOWN ON THE PLANS. THE CONTRACTOR SHALL TAKE ADDITIONAL CARE TO ENSURE POSITIVE DRAINAGE AWAY FROM THE STRUCTURE WHILE MEETING MINIMUM AND MAXIMUM PAVEMENT SLOPES AS DEFINED IN THE CRITERIA.
- 22. ALL DEBRIS AND FOREIGN MATERIAL SHALL BE REMOVED FROM THE SITE AND DISPOSED OF AT APPROVED DISPOSAL SITES. THE CONTRACTOR SHALL OBTAIN NECESSARY PERMITS FOR THE TRANSPORTATION OF MATERIAL TO AND FROM THE SITE.
- 23. DIMENSIONS TO PIPELINES ARE TO CENTERLINE UNLESS OTHERWISE NOTED.24. CONSTRUCTION STAKING FOR IMPROVEMENTS SHOWN IN THESE PLANS SHALL BE PERFORMED BY CONTRACTOR'S LICENSED LAND SURVEYOR.
- 25. ALL DIMENSIONS ARE IN FEET OR DECIMALS THEREOF.
- 26. SPOT GRADES ARE TO FLOWLINE OR FINISH PAVEMENT GRADE UNLESS OTHERWISE NOTED.
- 27. CONTRACTOR TO BE AWARE OF ALL OVERHEAD LINES AT ALL TIMES, SO AS NOT TO DISTURB THEM.
- 28. WATER SHALL BE PROVIDED ONSITE AND USED TO CONTROL DUST DURING DEMOLITION AND CONSTRUCTION OPERATIONS.
- 29. STORM DRAINAGE SYSTEMS SHOWN ON THESE PLANS HAVE BEEN DESIGNED FOR THE FINAL SITE CONDITION AT COMPLETION OF THE PROJECT. THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ADEQUATE DRAINAGE OF THE SITE, DURING INTERIM CONDITIONS OF CONSTRUCTION.
- 30. RETAINING WALLS LOCATED CLOSER TO THE PROPERTY LINE THAN THE HEIGHT OF THE WALL SHALL BE BACKFILLED NOT LATER THAN 10 DAYS AFTER CONSTRUCTION OF THE WALL AND NECESSARY STRUCTURAL SUPPORTING MEMBERS UNLESS RECOMMENDED OTHERWISE BY RESPONSIBLE ENGINEER.
- 31. THE CONTRACTOR IS RESPONSIBLE FOR APPLYING FOR AND OBTAINING A STATE STORMWATER DISCHARGE PERMIT FROM COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT (CDPHE) AT MINIMUM 10 BUSINESS DAYS PRIOR TO THE START OF GRADING ACTIVITIES ONSITE. 10 BUSINESS DAYS IS THE MINIMUM TIME REQUIRED BY THE STATE TO PROCESS THE APPLICATION. IT IS HIGHLY RECOMMENDED THAT THE CONTRACTOR APPLY FOR THE PERMIT AT LEAST 20 BUSINESS DAYS PRIOR TO THE START OF GRADING ACTIVITIES.

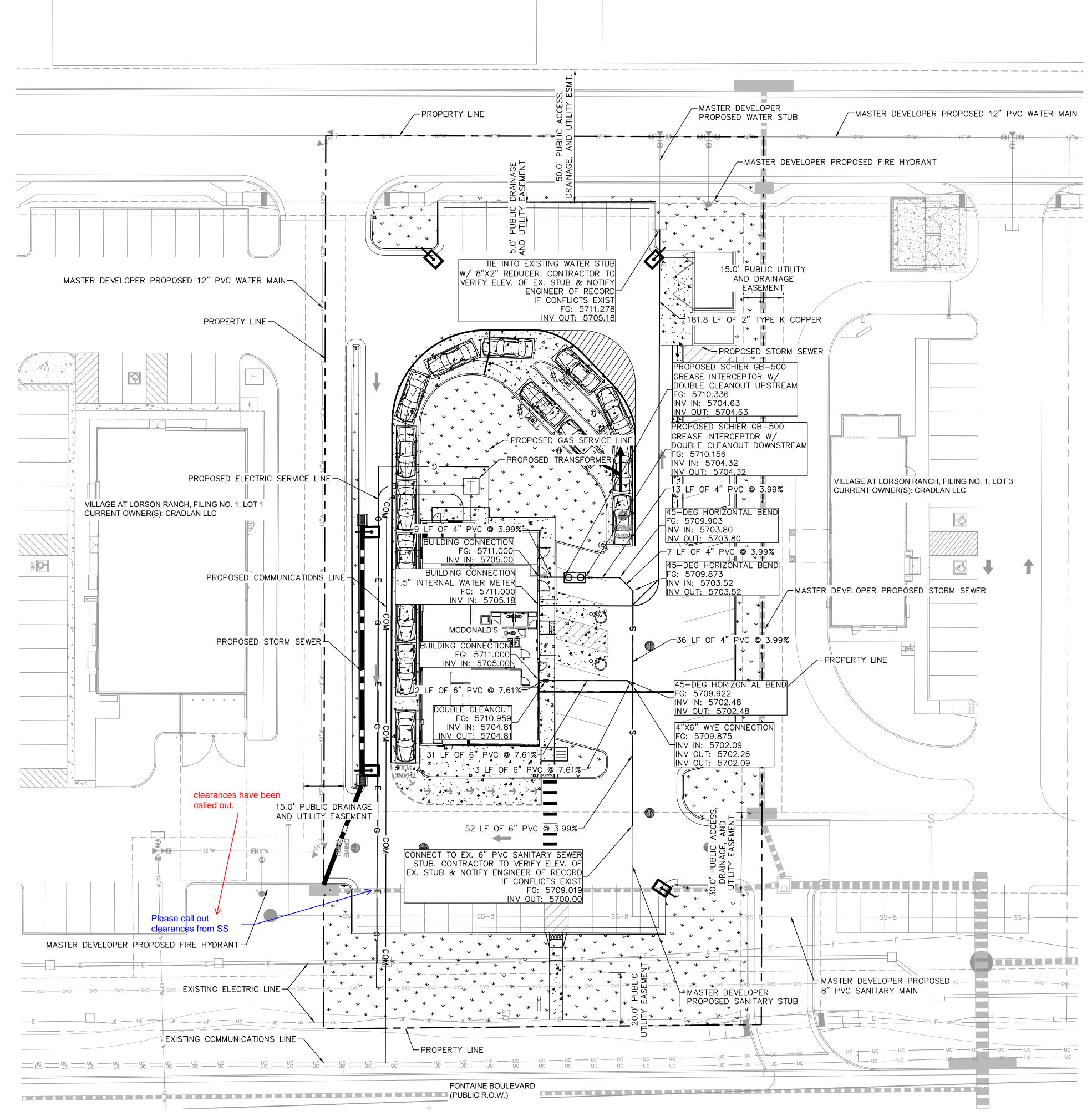
### WIDEFIELD WATER AND SANITATION DISTRICT GENERAL NOTES:

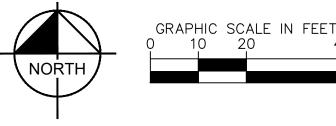
- ALL UTILITY CONSTRUCTION TO BE CONDUCTED IN CONFORMANCE WITH THE CURRENT WIDEFIELD WATER AND SANITATION DISTRICT SPECIFICATIONS. COMPACTION REQUIREMENTS SHALL BE 95% STANDARD PROCTOR AS DETERMINED BY ASTM D698, UNLESS OTHERWISE APPROVED BY THE WIDEFIELD WATER AND SANITATION DISTRICT OR A HIGHER STANDARD IS IMPOSED BY ANOTHER AGENCY HAVING RIGHT-OF-WAY JURISDICTION.
- 2. ALL MATERIALS AND WORKMANSHIP SHALL BE SUBJECT TO INSPECTION BY THE WIDEFIELD WATER AND SANITATION DISTRICT. THE WIDEFIELD WATER AND SANITATION DISTRICT RESERVES THE RIGHT TO ACCEPT OR REJECT ANY SUCH MATERIALS AND WORKMANSHIP THAT DOES NOT CONFORM TO ITS STANDARDS AND SPECIFICATIONS.
- 3. THE DEVELOPER OR HIS ENGINEER HAS LOCATED ALL FIRE HYDRANTS AND FUTURE SERVICE STUBS. ANY REQUIRED REALIGNMENT, EITHER HORIZONTAL OR VERTICAL, SHALL BE AT THE EXPENSE OF THE DEVELOPER.
- 4. ALL DUCTILE IRON PIPE, TO INCLUDE FITTINGS, VALVES AND FIRE HYDRANTS WILL BE WRAPPED WITH POLYETHYLENE TUBING, AND ELECTRICALLY ISOLATED.
  5. ALL DUCTILE IRON PIPE AND FITTINGS SHALL BE DOUBLE BONDED. SPECIFICATIONS FOR CATHODIC PROTECTION ON BOTH DIP
- MAINS AND PVC MAINS IS SPECIFIED IN THE STANDARDS AND SPECIFICATIONS. 6. PVC MAIN LINES SHALL BE INSTALLED WITH COATED NO. 12 TRACER WIRE.
- 7. THE CONTRACTOR IS REQUIRED TO NOTIFY THE WIDEFIELD WATER AND SANITATION DISTRICT (390–7111) A MINIMUM OF 48 HOURS AND A MAXIMUM OF 96 HOURS PRIOR TO THE START OF CONSTRUCTION. THE CONTRACTOR SHALL ALSO NOTIFY AFFECTED UTILITY COMPANIES 48 HOURS PRIOR TO CONSTRUCTION ADJACENT TO THE KNOWN UTILITY LINES.
- 8. THE LOCATION OF ALL UTILITIES AS SHOWN ON THESE DRAWINGS ARE APPROXIMATE ONLY. THE LOCATION OF ALL UTILITIES SHALL BE VERIFIED PRIOR TO CONSTRUCTION BY THE CONTRACTOR.
- 9. THE CONTRACTOR SHALL FIELD EXCAVATE AND VERIFY THE VERTICAL AND HORIZONTAL LOCATION OF ALL TIE-INS. CONTRACTOR SHALL NOTIFY THE WIDEFIELD WATER AND SANITATION DISTRICT AND THE ENGINEER OF THE FIELD VERIFIED INFORMATION PRIOR TO CONSTRUCTION.
- 10. ALL BENDS SHALL BE FIELD STAKED PRIOR TO CONSTRUCTION.
- 11. ANY WATER UTILITY MATERIAL REMOVED AND NOT REUSED SHALL BE RETURNED TO THE WIDEFIELD WATER AND SANITATION DISTRICT IF THE DISTRICT SO REQUESTS.
- 12. THE CONTRACTOR SHALL AT HIS EXPENSE SUPPORT AND PROTECT ALL UTILITY MAINS SO THAT THEY WILL FUNCTION CONTINUOUSLY DURING CONSTRUCTION. SHOULD A UTILITY MAIN FAIL AS A RESULT OF THE CONTRACTOR'S OPERATION, IT WILL BE REPLACED IMMEDIATELY BY EITHER THE CONTRACTOR OR THE WIDEFIELD WATER AND SANITATION DISTRICT AT FULL COST OF LABOR AND MATERIALS TO THE CONTRACTOR.
- ANY PUMPING OR BYPASS OPERATIONS MUST BE REVIEWED AND APPROVED PRIOR TO EXECUTION BY BOTH THE WIDEFIELD WATER AND SANITATION DISTRICT AND THE ENGINEER.
   CONTRACTOR MUST REPLACE OR REPAIR ANY DAMAGE TO ALL SURFACE IMPROVEMENTS, INCLUDING BUT NOT LIMITED TO
- FENCES, CURB AND GUTTER AND/OR ASPHALT THAT MAY BE CAUSED DURING CONSTRUCTION. 15. ALL WATER LINES 6" AND LARGER, AND ALL SEWER LINES 8" AND LARGER, SHALL HAVE AS "AS-BUILT" PLANS PREPARED
- AND APPROVED PRIOR TO FINAL ACCEPTANCE BY THE WIDEFIELD WATER AND SANITATION DISTRICT.
  16. PRIOR TO CONSTRUCTION, A PRE-CONSTRUCTION CONFERENCE IS REQUIRED A MINIMUM OF 72 HOURS IN ADVANCE OF COMMENCEMENT OF WORK. TO SET THE PRE-CONSTRUCTION CONFERENCE, CONTRACT BRANDON BERNARD-WATER DIVISION MANAGER AND/OR JASON DREESSEN, WASTEWATER DIVISION MANAGER AT (719) 955-0548 OF THE WIDEFIELD WATER AND SANITATION DISTRICT FOR A TIME. NO PRE-CONSTRUCTION CONFERENCE TIMES WILL BE SET UNTIL 4 SETS OF SIGNED DRAWINGS ARE RECEIVED BY THE WIDEFIELD W&S DISTRICT.

					BY
					DESCRIPTION
					DATE
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PREPARED BY:					
	McDonald's USA, LLC	These drawings and specifications are the confidential and proprietary property of McDonald's USA, LLC and shall not be copied or reproduced	for use on this specific site in conjunction with its issue date and are not suitable for use on a different site or at a later time. Use of	these drawings for reference or example on another project requires the services of property licensed architects and enaineers. Reproduction of	the contract documents for reuse on another project is not authorized.
DRAWN BY F	STD ISSUE DATE 7/30/2024	REVIEWED BY	DATE ISSUED	7/30/2024	
	UTILITY PLANS	NOIL		)	SITE ADDRESS NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO B SPRINGS, CO
TITLE	UTILI'	DESCRIPTION	L NOTES		SITE ID 51028

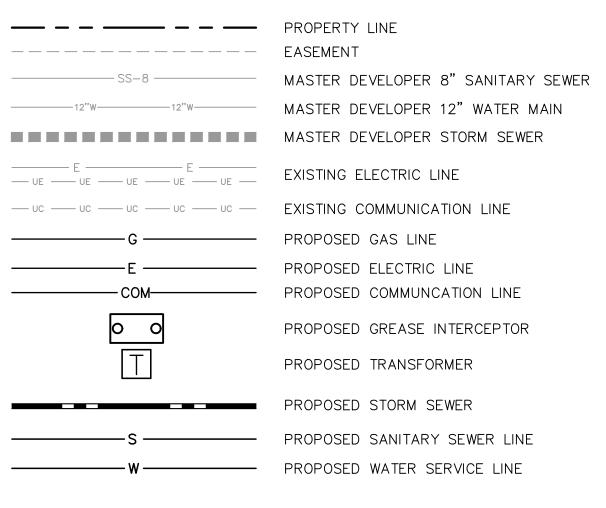


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## LEGEND



### <u>NOTES</u>

- 1. ALL CONDITIONS SHOWN TO BE "EXISTING" OR "MASTER DEVELOPER PROPOSED" SHALL BE VERIFIED IN THE FIELD BY THE GENERAL CONTRACTOR PRIOR TO START OF CONSTRUCTION INCLUDING BUT NOT LIMITED TO POTHOLING OF EXISTING UTILITY ELEVATIONS AT CROSSINGS AND TIE-IN LOCATIONS. ANY DISCREPANCIES SHALL BE NOTED AND SUBMITTED TO THE OWNER AND THE ENGINEER OF RECORD FOR REVIEW. CHANGES TO THE ORIGINAL DESIGN OF THIS PROJECT DUE TO EXISTING SITE CONDITIONS MUST BE APPROVED BY BOTH THE ENGINEER AND OWNER PRIOR TO MAKING ANY CHANGES.
- ALL WATER SERVICE LINES SHALL MAINTAIN A BURY DEPTH OF 5'-6'.

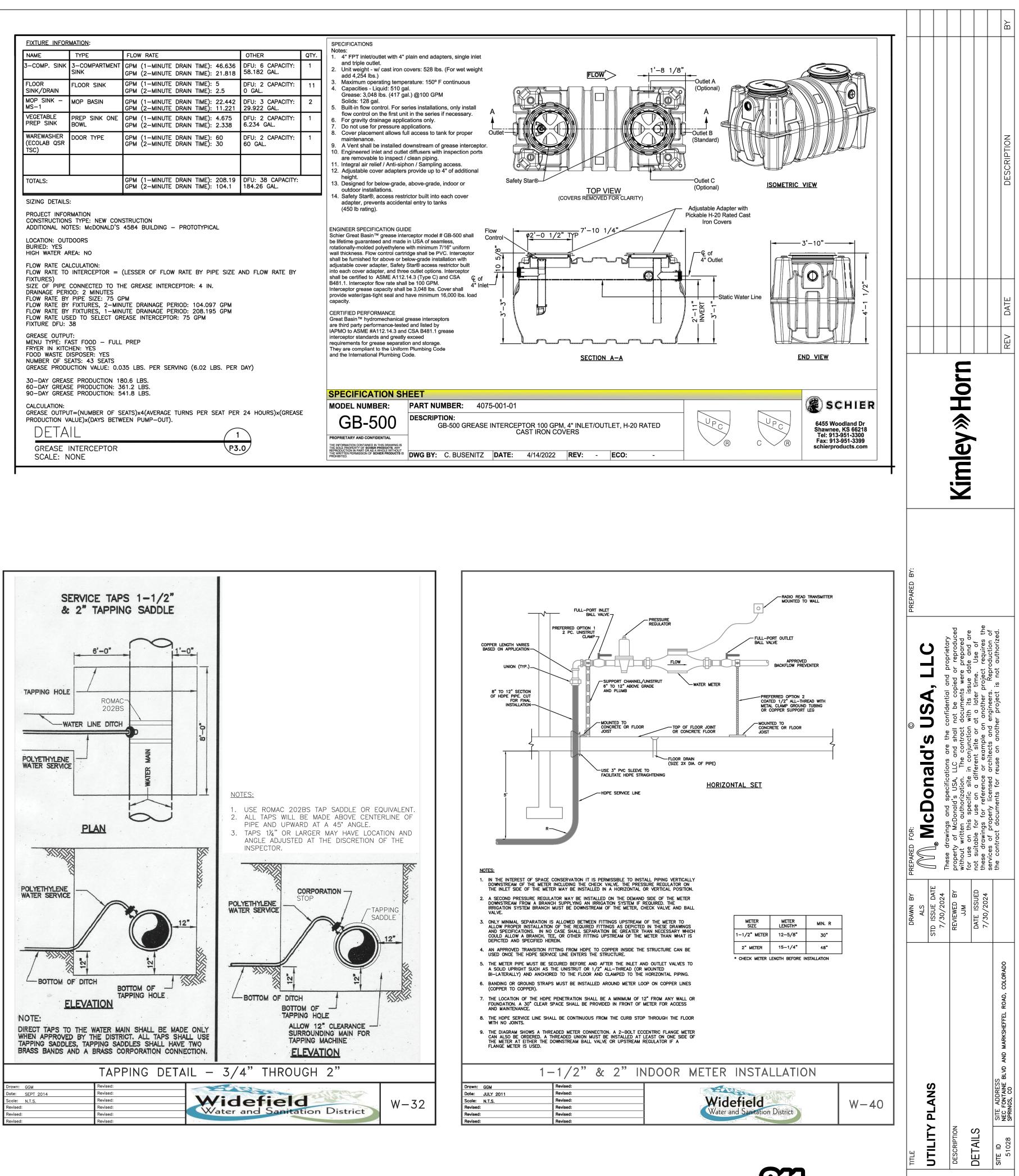
### <u>Cautionary note</u>

1. CONTRACTOR SHALL MAINTAIN 1.5' OF VERTICAL SEPARATION AT ALL WET UTILITY CROSSING AND 1' OF VERTICAL SEPARATION AT ALL DRY UTILITY CROSSINGS. CONTRACTOR SHALL POTHOLE ALL EXISTING UTILITY CROSSINGS TO VERIFY DEPTH AND COORDINATE WITH ENGINEER OF RECORD.

PREPARED BY:				Jse of equires the	Juction of	
<pre>     PREPARED FOR:</pre>	McDonald's USA, LLC		Ъ	DATE ISSUED   not suitable for use on a different site or at a later time. Use 7/30/2004   these drawings for reference or example on another project requ	ervices of properly licensed architects and engineers. Reproduction of the contract documents for reuse on another project is not authorized.	
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FIXTURE INFOR	<u>MATION</u> :				SPECIFICATIONS	
NAME	TYPE	FLOW RATE	OTHER	QTY.	Notes: 1. 4" FPT inlet/outlet with 4	" plain end adapters, si
3-COMP. SINK	3-COMPARTMENT SINK	GPM (1—MINUTE DRAIN TIME): 46.636 GPM (2—MINUTE DRAIN TIME): 21.818	DFU: 6 CAPACITY: 58.182 GAL.	1	and triple outlet. 2. Unit weight - w/ cast iron add 4,254 lbs.)	
Floor Sink/drain	FLOOR SINK	GPM (1–MINUTE DRAIN TIME): 5 GPM (2–MINUTE DRAIN TIME): 2.5	DFU: 2 CAPACITY: 0 GAL.	11	<ol> <li>Maximum operating tem</li> <li>Capacities - Liquid: 510 Grease: 3,048 lbs. (417</li> </ol>	gal.
MOP SINK - MS-1	MOP BASIN	GPM (1–MINUTE DRAIN TIME): 22.442 GPM (2–MINUTE DRAIN TIME): 11.221	DFU: 3 CAPACITY: 29.922 GAL.	2	Solids: 128 gal. 5. Built-in flow control. For flow control on the first u	series installations, only
VEGETABLE PREP SINK	PREP SINK ONE BOWL	GPM (1–MINUTE DRAIN TIME): 4.675 GPM (2–MINUTE DRAIN TIME): 2.338	DFU: 2 CAPACITY: 6.234 GAL.	1	6. For gravity drainage app 7. Do not use for pressure	lications only. applications.
WAREWASHER (ECOLAB QSR TSC)	DOOR TYPE	GPM (1—MINUTE DRAIN TIME): 60 GPM (2—MINUTE DRAIN TIME): 30	DFU: 2 CAPACITY: 60 GAL.	1	<ol> <li>Cover placement allows maintenance.</li> <li>A Vent shall be installed</li> <li>Engineered inlet and out</li> </ol>	downstream of grease let diffusers with inspec
					are removable to inspec 11. Integral air relief / Anti-si 12. Adjustable cover adapte	phon / Sampling access
TOTALS:		GPM (1–MINUTE DRAIN TIME): 208.19 GPM (2–MINUTE DRAIN TIME): 104.1	DFU: 38 CAPACITY: 184.26 GAL.		height. 13. Designed for below-grad outdoor installations.	-
SIZING DETAILS	:		-		14. Safety Star®, access res adapter, prevents accide (450 lb rating).	
FIXTURES) SIZE OF PIPE DRAINAGE PERI FLOW RATE BY FLOW RATE BY FLOW RATE BY FLOW RATE US FIXTURE DFU: GREASE OUTPU MENU TYPE: FI FRYER IN KITCI FOOD WASTE D NUMBER OF SI GREASE PRODU 30-DAY GREAS 60-DAY GREAS	REA: NO LCULATION: INTERCEPTOR = CONNECTED TO TH OD: 2 MINUTES PIPE SIZE: 75 GI FIXTURES, 2-MIN FIXTURES, 1-MIN ED TO SELECT GR 38 IT: AST FOOD - FULL HEN: YES ISPOSER: YES EATS: 43 SEATS	UTE DRAINAGE PERIOD: 104.097 GPM UTE DRAINAGE PERIOD: 208.195 GPM EASE INTERCEPTOR: 75 GPM PREP 35 LBS. PER SERVING (6.02 LBS. PER 30.6 LBS. 61.2 LBS.			ENGINEER SPECIFICATION G Schier Great Basin™ grease in be lifetime guaranteed and mac rotationally-molded polyethylen wall thickness. Flow control can shall be furnished for above or adjustable cover adapter, Safe into each cover adapter, and th shall be certified to ASME A11 B481.1. Interceptor flow rate sh Interceptor grease capacity sha provide water/gas-tight seal an capacity. CERTIFIED PERFORMANCE Great Basin™ hydromechanicc are third party performance-tes IAPMO to ASME #A112.14.3 al interceptor standards and great requirements for grease separa They are compliant to the Unifc and the International Plumbing	terceptor model # GB-50 be in USA of seamless, e with minimum 7/16" un tridge shall be PVC. Inte below-grade installation ty Star® access restrictor ree outlet options. Interco 2.14.3 (Type C) and CS/ all be 100 GPM. all be 3,048 lbs. Cover sh d have minimum 16,000 al grease interceptors ted and listed by nd CSA B481.1 grease tity exceed titon and storage. form Plumbing Code Code.
PRODUCTION V	ALUE)×(DAYS BETW	EATS)x4(AVERAGE TURNS PER SEAT PER EEN PUMP-OUT).	R 24 HOURS)x(GREAS	E	GB-500	PART NUMBER DESCRIPTION: GB-500
DETA					PROPRIETARY AND CONFIDENTIAL THE INFORMATION CONTAINED IN THIS DRAWING IS THEFOSDE FORTOR SHARE RECOLUTION AND THEFOSDE FORTOR SHARE RECOLUTION AND THE WINTTEN PERMISSION OF SCHIER PRODUCTS PROHIBITED	
	INTERCEPTOR	\P3			THE SOLE PROPERTY OF SCHIER PRODUCTS. ANY	



Know what's **below. Call** before you dig.

3.3

### **OWNER'S SIGNATURE BLOCK**

I, THE OWNER/DEVELOPER HAVE READ AND WILL COMPLY WITH THE REQUIREMENTS OF THE GRADING AND EROSION CONTROL PLAN.

NAME

DATE

### ENGINEER'S SIGNATURE BLOCK

THIS GRADING AND EROSION CONTROL PLAN WAS PREPARED UNDER MY DIRECTION AND SUPERVISION AND IS CORRECT TO THE BEST OF MY KNOWLDGE AND BELIEF. SAID PLAN HAS BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR GRADING AND EROSION CONTROL PLANS. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARING THIS PLAN.

JESSICA MCCALLUM, PE KIMLEY-HORN AND ASSOCIATES, INC. DATE

### EL PASO COUNTY REVIEW STATEMENT

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSION, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONIBILITY FOR COMPLETENESS AND / OR ACCURACY OF THIS DOCUMENT. FILED IN ACCORDANCE WITH THE REQUIREMENTS OF THE EL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA MANUAL VOLUMES 1 AND 2, AND ENGINEERING CRITERIA MANUAL ÀS AMENDED.

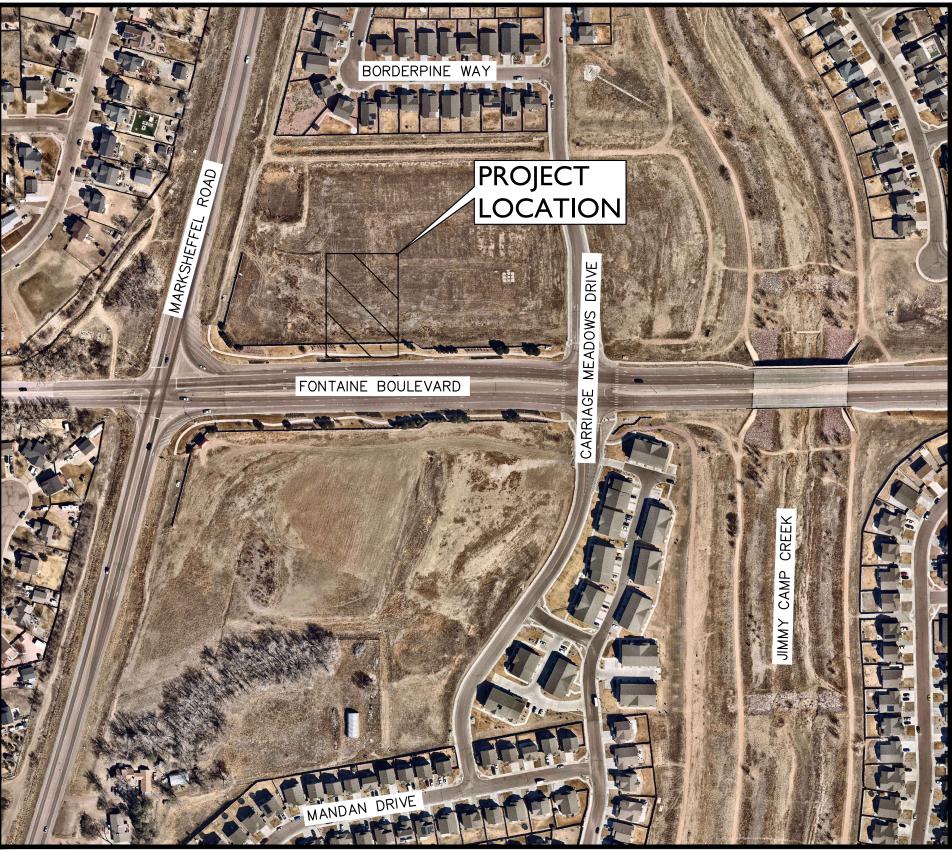
IN ACCORDANCE WITH FCM SECTION 1.12 THESE CONSTRUCTION DOCUMENTS WILL BE VALID FOR A CONSTRUCTION FOR A PERIOD OF 2 YEARS FROM THE DATE SIGNED BY THE EL PASO COUNTY ENGINEER. IF THE CONSTRUCTION HAS NOT STARTED WITHIN THOSE 2 YEARS, THE PLANS WILL NEED TO BE RESUBMITTED FOR APPROVAL, INCLUDING PAYMENT OF REVIEW FEES AT THE PLANNING AND COMMUNITY DEVELOPMENT DIRECTOR'S DISCRETION.

JOSHUA PALMER, P.E. COUNTY ENGINEER / ECM ADMINISTRATOR

DATE

# MCDONALD'S AT FONTAINE AND MARKSHEFFEL GRADING AND EROSION CONTROL VILLAGE AT LORSON RANCH FILING NO.1 LOT 2

 $S_2^{\frac{1}{2}}$  of section 15, township 15s, range 65 west of the 6th p.m., COUNTY OF EL PASO, STATE OF COLORADO



VICINITY MAP

NOT TO SCALE

GRA	DING AND EROSION CONTROL PLAN
SHEET NUMBER	SHEET TITLE
C2.1	COVER
C2.2	NOTES
C2.3	INITIAL EC
C2.4	FINAL EC
C2.5	CUT FILL PLAN
C2.6	EROSION CONTROL DETAILS
C2.7	EROSION CONTROL DETAILS
C2.8	EROSION CONTROL DETAILS
C2.9	EROSION CONTROL DETAILS
C2.10	EROSION CONTROL DETAILS

### LAND AREA:

55,101 SQ. FT. OR 1.265 ACRES MORE OR LESS

BASIS OF BEARING:

### **BENCHMARK**:

ELEVATIONS ARE BASED UPON A FOUND 2" ALUMINUM CAP STAMPED "FARNSWORTH GROUP INC. PLS 38053" ON THE WEST LINE OF TRACT B AS SHOWN AS HEREON (ELEVATION = 5724.52) LEGAL DESCRIPTION VILLAGE AT LORSON RANCH FILING NO.1, LOT 2

### GENERAL NOTES:

- JUSTICE.
- APPROVAL.

## FEMA CLASSIFICATION

THE FLOOD INSURANCE RATE MAP (FIRM) PANEL NO. 08041C0957G EFFECTIVE DATE DECEMBER 7, 2018, HAS BEEN EXAMINED AS IT RELATES TO THE PROPERTY BEING PLATTED. THE PROPERTY LIES WITHIN ZONE X, AREA OF MINIMAL FLOOD HAZARD.

## ONSITE DISTURBANCE:

OFFSITE DISTURBANCE: TOTAL:

### CONTACTS:

**DEVELOPER:** 

MCDONALD'S USA, LLC 110 N. CARPENTER STREET CHICAGO, IL 60607 TEL: (206) 348-4374 CONTÀCT: ROBERT YAGUSESKY NORTH EMAIL: ROBERT.YAGUSESKY@US.MCD.COM

> <u>ENGINEER</u> KIMLEY-HORN AND ASSOCIATES, INC. 2 NORTH NEVADA AVE., SUITE 900 COLORADO SPRINGS, CO 80903 TEL: (719) 284-7275 CONTÀCT: JESSICA MCCALLUM, P.E.

LANDSCAPE ARCHITECT: KIMLEY-HORN AND ASSOCIATES, INC. 2 NEVADA NORTH AVE., SUITE 300 COLORADO SPRINGS, CO 80903 TEL: (719) 453-0180 CONTACT: JEREMY POWELL, P.L.A. EMAIL: JEREMY.POWELL@KIMLEY-HORN.COM

BEARINGS ARE BASED ON THE NORTH LINE OF TRACT D, CARRIAGE MEADOWS NORTH FILING NO. 1, BEARING N89°48'24" E, A DISTANCE OF 699.24 FEET, AS MONUMENTED AT BOTH ENDS BY A FOUND YELLOW PLASTIC CAP STAMPED "FWS PLS 38226".

1. THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATIONS AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF

2. THE OWNER IS AWARE THAT THE ACCESS PERMITS (AP211569, AP211570) ARE SUBJECT TO CONDITIONS OF

### LIMITS OF CONSTRUCTION

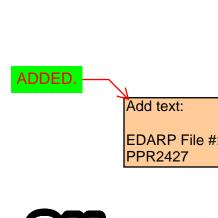
=	±1.11	ACRES

- $= \pm 0.00$  ACRES
- $= \pm 1.11$  ACRES

<u>ARCHITECT:</u> CORE STATES GROUP 135 WATER STREET, SUITE 201 NAPERVILLE, IL 60540 TEL: (224) 585-4591 CONTACT: JOY VRCHOTA EMAIL: JVRCHOTA@CORE-STATES.COM

SURVEYOR: KIMLEY-HORN AND ASSOCIATES, INC. 6200 S. SYRACUSE WAY, SUITE 300 GREENWOOD VILLAGE, CO 80111 TEL: (303) 228-2300 CONTACT: DARREN WOLTERSTORFF, P.L.S. EMAIL: JESSICA.MCCALLUM@KIMLEY-HORN.COM EMAIL: DARREN.WOLTERSTORFF@KIMLEY-HORN.COM

> OWNER: CRADLAN COMMERCIAL, LLLP 212 N. WAHSATCH AVE, SUITE 301 COLORADO SPRINGS, CO 80903 TEL: (719)-635-3200 CONTÀCT: JEFF MARK EMAIL: JMARK@LANDHUISCO.COM





Know what's **below**. Call before you di

								BΥ
								DESCRIPTION
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				Vimboy NU.		•		
	PREPARED BY:							
	PREPARED FOR:	McDonald's USA. LLC	These Arowings and specifications are the confidential and providentiation	property of McDonald's USA, LLC and shall not be copied or reproduced	ut written authorization. The contract accuments were prepared se on this specific site in conjunction with its issue date and are	not suitable for use on a different site or at a later time. Use of these drawings for reference or example on another project requires the	services of properly licensed architects and engineers. Reproduction of the contract documents for reuse on another project is not authorized.	
	BY PR	ALS ALS ALS		REVIEWED BY prope	JJM WITNOL D	DATE ISSUED   not s 7/30/2024   these		
	ШТЕ			DESCRIPTION		COVER	SITE ID   SITE ADDRESS	51028 NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO 51028 SPRINGS, CO
g.				C	2		,	

### ENGINEERING CONSTRUCTION NOTES

- 1. ALL EXISTING UTILITIES SHOWN ARE LOCATED ACCORDING TO THE INFORMATION AVAILABLE TO THE ENGINEER AT THE TIME THE DRAWINGS WERE PREPARED AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR THE ENGINEER. GUARANTEE IS NOT MADE THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN OR THAT THE LOCATION OF THOSE SHOWN ARE ENTIRELY ACCURATE. THE LOCATIONS SHOWN ARE FOR BIDDING PURPOSES ONLY. FINDING THE ACTUAL LOCATION OF ANY EXISTING UTILITIES IS THE CONTRACTORS RESPONSIBILITY AND SHALL BE DONE BEFORE HE COMMENCES ANY WORK IN THE VICINITY. FURTHERMORE, THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES DUE TO THE CONTRACTORS FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. THE OWNER OR ENGINEER WILL ASSUME NO LIABILITY FOR ANY DAMAGES SUSTAINED OR COST INCURRED BECAUSE OF THE OPERATIONS IN THE VICINITY OF EXISTING UTILITIES OR STRUCTURES, NOR FOR TEMPORARY BRACING AND SHORING OF SAME. IF IT IS NECESSARY TO SHORE, BRACE, SWING OR RELOCATE A UTILITY, THE UTILITY COMPANY OR DEPARTMENT AFFECTED SHALL BE CONTACTED AND THEIR PERMISSION OBTAINED REGARDING THE METHOD TO USE FOR SUCH WORK.
- 2. CONTRACTOR AGREES THAT HE/SHE SHALL ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOBSITE CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THIS PROJECT, INCLUDING: SAFETY OF ALL PERSONS AND PROPERTY, AND THIS REQUIREMENT SHALL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS; AND THAT THE CONTRACTOR SHALL DEFEND, INDEMNIFY, AND HOLD THE OWNER AND ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT.
- 3. IT IS THE CONTRACTOR'S RESPONSIBILITY TO CONTACT THE VARIOUS UTILITY COMPANIES WHICH MAY HAVE BURIED OR AERIAL UTILITIES WITHIN OR NEAR THE CONSTRUCTION AREA BEFORE COMMENCING WORK. THE CONTRACTOR SHALL PROVIDE 48 HOURS MINIMUM NOTICE TO ALL UTILITY COMPANIES PRIOR TO BEGINNING CONSTRUCTION.
- 4. CONTRACTOR SHALL CONTACT UTILITY NOTIFICATION CENTER FOR THE LOCATION OF UNDERGROUND UTILITIES AT LEAST 48 HOURS PRIOR TO COMMENCEMENT OF CONSTRUCTION (1-800-922-1987).
- 5. CONSTRUCTION SHALL COMPLY WITH ALL GOVERNING CODES AND BE CONSTRUCTED TO SAME.
- 6. THE CONTRACTOR SHALL BE RESPONSIBLE TO OBTAIN ALL REQUIRED CONSTRUCTION PERMITS AND BONDS PRIOR TO CONSTRUCTION.
- 7. THE CONTRACTOR SHALL RESTORE ALL DISTURBED VEGETATION IN KIND, UNLESS SHOWN OTHERWISE
- 8. ALL PAVING. CONSTRUCTION. MATERIALS. AND WORKMANSHIP WITHIN THE PUBLIC RIGHT-OF-WAY OR EASEMENT SHALL CONFORM TO THE CITY OF COLORADO SPRINGS'S SPECIFICATIONS AND STANDARDS. (LATEST EDITION)

9. CONTRACTOR SHALL PROVIDE ALL LIGHTS, SIGNS, BARRICADES, FLAGGERS, AND ALL OTHER DEVICES NECESSARY TO PROVIDE FOR PUBLIC SAFETY IN ACCORDANCE WITH MUTCD CONSTRUCTION AREA TRAFFIC CONTROL. ENGINEERING DEMOLITION NOTES

- ALL DEMOLITION SHALL BE CARRIED OUT IN A SAFE MANNER AND IN STRICT ACCORDANCE WITH OSHA REGULATIONS.
- 2. ALL CONDITIONS SHOWN TO BE "EXISTING" SHALL BE VERIFIED IN THE FIELD BY THE GENERAL CONTRACTOR PRIOR TO START OF CONSTRUCTION. ANY DISCREPANCIES SHALL BE NOTED AND SUBMITTED TO THE OWNER AND THE ENGINEER FOR REVIEW. CHANGES TO THE ORIGINAL DESIGN OF THIS PROJECT DUE TO EXISTING SITE CONDITIONS MUST BE APPROVED BY BOTH THE OWNER AND THE ENGINEER PRIOR TO MAKING ANY CHANGES.
- 3. THE CONTRACTOR SHALL FIELD VERIFY THE EXTENT OF DEMOLITION.
- 4. WHEN UTILITIES ARE REMOVED, CAP AND SEAL A MINIMUM OF 8" BELOW FINISH GRADE

### **ENGINEERING SITE NOTES**

- 1. CONTRACTOR IS RESPONSIBLE FOR PROTECTION OF ALL PROPERTY CORNERS.
- 2. CONTRACTOR SHALL MATCH PROPOSED CURB AND GUTTER, CONCRETE, AND PAVEMENT TO EXISTING GRADE AT ALL TIE IN LOCATIONS.
- 3. CONTRACTOR SHALL REMOVE PAVEMENT AND CONCRETE IN ACCORDANCE WITH SPECIFICATIONS OF EL PASO COUNTY AND/OR THE COLORADO STATE DEPARTMENT OF TRANSPORTATION.
- 4. THE EARTHWORK FOR ALL BUILDING FOUNDATIONS AND SLABS SHALL BE IN ACCORDANCE WITH GEOTECHNICAL RECOMMENDATIONS AND ARCHITECTURAL BUILDING PLANS AND SPECIFICATIONS.
- 5. CONTRACTOR SHALL REFER TO BUILDING PLANS AND SPECIFICATIONS FOR ACTUAL LOCATION OF ALL UTILITY ENTRANCES, TO INCLUDE, SANITARY SEWER LATERALS, DOMESTIC AND FIRE PROTECTION WATER SERVICE, ELECTRICAL, AND TELEPHONE SERVICE. CONTRACTOR SHALL COORDINATE INSTALLATION OF UTILITIES IN SUCH A MANNER AS TO AVOID CONFLICTS AND ASSURE PROPER DEPTHS ARE ACHIEVED, AS WELL AS, COORDINATE WITH ANY UTILITY COMPANIES FOR APPROVED LOCATIONS AND SCHEDULING OF TIE-INS/CONNECTIONS TO THEIR FACILITIES.
- 6. CONTRACTOR IS RESPONSIBLE FOR REPAIRING THE DAMAGE DONE TO ANY EXISTING ITEM DURING CONSTRUCTION, SUCH AS, BUT NOT LIMITED TO, DRAINAGE, UTILITIES, PAVEMENT, STRIPING, CURB, ETC. REPAIRS SHALL BE EQUAL TO, OR BETTER THAN, EXISTING CONDITIONS. CONTRACTOR IS RESPONSIBLE TO DOCUMENT ALL EXISTING DAMAGE AND NOTIFY CONSTRUCTION MANAGER PRIOR TO CONSTRUCTION START.
- 7. CONTRACTOR TO REMOVE OR RELOCATE, WHEN APPLICABLE, ALL EXISTING BUILDINGS, FOUNDATIONS, BASEMENTS, CONNECTING IMPROVEMENTS, DRAIN PIPES, SANITARY SEWER PIPES, POWER POLES, AND GUY WIRES, WATER METERS AND WATER LINES, WELLS, SIDEWALKS, SIGN POLES, UNDERGROUND GAS, SEPTIC TANKS, AND ASPHALT, SHOWN AND NOT SHOWN, WITHIN CONSTRUCTION LIMITS AND WHERE NEEDED, TO ALLOW FOR NEW CONSTRUCTION AS SHOWN.

### ENGINEERING PAVING NOTES

- 1. CONTRACTOR SHALL ADJUST AND/OR CUT EXISTING PAVEMENT AS NECESSARY TO ASSURE A SMOOTH FIT AND CONTINUOUS GRADE.
- 2. ALL CONCRETE SIDEWALKS SHALL HAVE CONTROL JOINTS CUT ON 5' CENTERS AND EXPANSION JOINTS PLACED ON 20' CENTERS. CONCRETE PAVEMENT JOINTS SHALL BE SPACED AT 12' CENTERS MAXIMUM.
- 3. ALL AREAS INDICATED AS PAVEMENT SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE TYPICAL PAVEMENT SECTIONS.
- 4. WHERE NEW PAVEMENT MEETS THE EXISTING PAVEMENT, THE CONTRACTOR SHALL SAW CUT THE EXISTING PAVEMENT A MINIMUM 2" DEEP FOR A SMOOTH AND STRAIGHT JOINT AND MATCH THE EXISTING PAVEMENT ELEVATION WITH THE PROPOSED PAVEMENT UNLESS OTHERWISE INDICATED.

### **ENGINEERING GRADING NOTES**

- 1. CONTOURS ON SIDEWALKS AND PRIVATE/PUBLIC ROADWAYS ARE TO FINISH GRADE.
- 2. FOR GROUND TREATMENT OF ALL DISTURBED AREAS WITHIN THE PROJECT SITE, REFER TO LANDSCAPE PLANS
- 3. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE CONTROL OF DUST AND DIRT RISING AND SCATTERING IN THE AIR DURING CONSTRUCTION AND SHALL PROVIDE WATER SPRINKLING OR OTHER SUITABLE METHODS OF CONTROL THE CONTRACTOR SHALL COMPLY WITH ALL GOVERNING REGULATIONS PERTAINING TO ENVIRONMENTAL PROTECTION.
- 4. THE CONTRACTOR SHALL GRADE THE SITE TO THE ELEVATIONS INDICATED AND SHALL RE-GRADE WASHOUTS WHERE THEY OCCUR AFTER EVERY RAINFALL UNTIL A GRASS STAND OR OTHER FINAL LANDSCAPE PLANTING IS WELL ESTABLISHED.

### ENGINEERING DRAINAGE AND STORM WATER NOTES

- 1. ON-SITE STORM SEWER SYSTEM HAS BEEN PROVIDED TO MAINTAIN THE EXISTING DRAINAGE PATTERNS.
- 2. ALL ON-SITE STORM SEWER IS PRIVATE, UNLESS OTHERWISE NOTED.
- 3. EXISTING DRAINAGE STRUCTURES TO BE INSPECTED AND REPAIRED AS NEEDED. EXISTING PIPES TO BE CLEANED OUT TO REMOVE ALL SILT AND DEBRIS.
- 4. THE CONTRACTOR SHALL DE-SILT ALL DRAINAGE STRUCTURES AS REQUIRED DURING AND AT THE END OF CONSTRUCTION TO PROVIDE POSITIVE DRAINAGE FLOWS.
- 5. IF DEWATERING IS REQUIRED, THE CONTRACTOR SHALL OBTAIN ANY APPLICABLE REQUIRED PERMITS. THE CONTRACTOR IS TO COORDINATE WITH THE OWNER PRIOR TO EXCAVATION.

## ENGINEERING GENERAL NOTES FOR CONTRACTOR

17. THE CONTRACTOR SHALL BE RESPONSIBLE FOR SURVEY MONUMENTS AND/OR VERTICAL CONTROL BENCHMARKS WHICH ARE DISTURBED OR DESTROYED BY CONSTRUCTION. A LAND SURVEYOR MUST FIELD LOCATE, REFERENCE, AND/OR PRESERVE ALL HISTORICAL OR CONTROLLING MONUMENTS PRIOR TO ANY EARTHWORK. IF DESTROYED, A LAND SURVEYOR SHALL REPLACE SUCH MONUMENTS WITH APPROPRIATE MONUMENTS. A CORNER RECORD OR RECORD OF SURVEY, AS APPROPRIATE, SHALL BE FILED AS REQUIRED BY THE PROFESSIONAL LAND SURVEYORS ACT. IF ANY VERTICAL CONTROL IS TO BE DISTURBED OR DESTROYED, THE EL PASO COUNTY FIELD SURVEY SECTION MUST BE NOTIFIED, IN WRITING, AT LEAST 3 DAYS PRIOR TO THE CONSTRUCTION. THE CONTRACTOR WILL BE RESPONSIBLE FOR THE COST OF REPLACING ANY VERTICAL CONTROL BENCHMARKS DESTROYED BY THE CONSTRUCTION.

19. AS-BUILT DRAWINGS MUST BE SUBMITTED TO THE ENGINEER OF RECORD PRIOR TO ACCEPTANCE OF THIS PROJECT.

PRIOR TO START OF THE WORK. THE PERMIT APPLICANT AND ALL OF THEIR REPRESENTATIVES OR CONTRACTORS SHALL COMPLY WITH THE REQUIREMENTS FOR PROTECTION OF THIS AREA AS REQUIRED BY ANY APPLICABLE AGENCY. ISSUANCE OF THE CITY/COUNTY'S GRADING PERMIT SHALL NOT RELIEVE THE APPLICANT OR ANY OF THEIR REPRESENTATIVES OR CONTRACTORS FROM COMPLYING WITH ANY STATE OR FEDERAL REQUIREMENTS BY AGENCIES INCLUDING BUT NOT LIMITED TO COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT OR COLORADO DIVISION OF WILDLIFE. COMPLIANCE MAY INCLUDE OBTAINING PERMITS, OTHER AUTHORIZATIONS, OR COMPLIANCE WITH MANDATES BY ANY APPLICABLE STATE OR FEDERAL AGENCY.

20. THE AREA WHICH IS DEFINED AS A NON-GRADING AREA AND WHICH IS NOT TO BE DISTURBED SHALL BE STAKED

22. IF AT ANY TIME DURING THE GRADING OPERATION, ANY UNFAVORABLE GEOLOGICAL CONDITIONS ARE ENCOUNTERED, GRADING IN THAT AREA SHALL STOP UNTIL APPROVED CORRECTIVE MEASURES ARE OBTAINED.

23. STRAIGHT GRADE SHALL BE MAINTAINED BETWEEN CONTOUR LINES AND SPOT ELEVATIONS UNLESS OTHERWISE SHOWN ON THE PLANS. THE CONTRACTOR SHALL TAKE ADDITIONAL CARE TO ENSURE POSITIVE DRAINAGE AWAY FROM THE STRUCTURE WHILE MEETING MINIMUM AND MAXIMUM PAVEMENT SLOPES AS DEFINED IN THE CRITERIA.

24. ALL DEBRIS AND FOREIGN MATERIAL SHALL BE REMOVED FROM THE SITE AND DISPOSED OF AT APPROVED DISPOSAL SITES. THE CONTRACTOR SHALL OBTAIN NECESSARY PERMITS FOR THE TRANSPORTATION OF MATERIAL TO AND FROM THE SITE.

26. CONSTRUCTION STAKING FOR IMPROVEMENTS SHOWN IN THESE PLANS SHALL BE PERFORMED BY A LICENSED LAND SURVEYOR.

THE FOLLOWING NOTES ARE PROVIDED TO GIVE DIRECTIONS TO THE CONTRACTOR BY THE ENGINEER OF THE PLANS. THE CITY OR COUNTY ENGINEER'S SIGNATURE ON THESE PLANS DOES NOT CONSTITUTE APPROVAL OF ANY OF THESE NOTES AND THE CITY WILL NOT BE HELD RESPONSIBLE FOR THEIR ENFORCEMENT.

APPROVAL OF THESE PLANS BY THE CITY/COUNTY DOES NOT AUTHORIZE ANY WORK TO BE PERFORMED UNTIL A PERMIT HAS BEEN ISSUED.

THE APPROVAL OF THIS PLAN OR ISSUANCE OF A PERMIT BY EL PASO COUNTY DOES NOT AUTHORIZE THE SUBDIVIDER AND OWNER TO VIOLATE ANY FEDERAL, STATE OR COUNTY LAWS, ORDINANCES, REGULATIONS, OR POLICIES.

NEITHER THE OWNER, NOR THE ENGINEER OF WORK WILL ENFORCE SAFETY MEASURES OR REGULATIONS. THE CONTRACTOR SHALL DESIGN, CONSTRUCT, AND MAINTAIN ALL SAFETY DEVICES, INCLUDING SHORING, AND SHALL BE SOLELY RESPONSIBLE FOR CONFORMING TO ALL LOCAL, STATE AND FEDERAL SAFETY AND HEALTH STANDARDS, LAWS, AND REGULATIONS.

CONTRACTOR AGREES THAT HE/SHE SHALL ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOBSITI CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THIS PROJECT, INCLUDING: SAFETY OF ALL PERSONS AND PROPERTY, AND THIS REQUIREMENT SHALL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS; AND THAT THE CONTRACTOR SHALL DEFEND, INDEMNIFY, AND HOLD THE OWNER AND ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT EXCEPT LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF THE OWNER OR THE ENGINEER.

THE CONTRACTOR SHALL BE RESPONSIBLE TO INSURE THAT ALL SLOPES, STREETS, UTILITIES, AND STORM SEWERS ARE BUILT IN ACCORDANCE WITH THESE PLANS. IF THERE IS ANY QUESTION REGARDING THESE PLANS OR FIELD STAKES, THE CONTRACTOR SHALL REQUEST AN INTERPRETATION BEFORE DOING ANY WORK BY CALLING THE ENGINEER OF WORK AT 719-453-0180. THE CONTRACTOR SHALL ALSO TAKE THE NECESSARY STEPS TO PROTECT THE PROJECT AND ADJACENT PROPERTY FROM ANY EROSION AND SILTATION THAT RESULT FROM HIS OPERATIONS BY APPROPRIATE MEANS (SAND BAGS, TEMPORARY DESILTING BASINS, DIKES, SHORING, ETC.) UNTIL SUCH TIME THAT THE PROJECT IS COMPLETED AND ACCEPTED FOR MAINTENANCE BY WHATEVER OWNER, AGENCY, OR ASSOCIATION IS TO BE ULTIMATELY RESPONSIBLE FOR MAINTENANCE.

7. EXCEPT AS NOTED HEREON ALL UTILITY SERVICES WITHIN THIS DEVELOPMENT ARE UNDERGROUND INSTALLATIONS. THE CONTRACTOR SHALL NOTIFY ALL UTILITY COMPANIES PRIOR TO STARTING WORK NEAR THEIR FACILITIES, AND SHALL COORDINATE HIS WORK WITH COMPANY REPRESENTATIVES. FOR UTILITY MARK-OUT SERVICE, CALL 811.

THE EXISTENCE AND LOCATION OF UNDERGROUND UTILITIES OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED FROM A SEARCH OF THE AVAILABLE RECORDS. TO THE BEST OF OUR KNOWLEDGE THERE ARE NO OTHER EXISTING UTILITIES EXCEPT AS SHOWN ON THESE PLANS. NO REPRESENTATION IS MADE AS TO THE ACCURACY OR COMPLETENESS OF SAID UTILITY INFORMATION. THE CONTRACTOR IS REQUIRED TO TAKE PRECAUTIONARY MEASURES TO PROTECT THE UTILITY LINES SHOWN HEREON AND ANY OTHERS NOT OF RECORD OR NOT SHOWN ON THESE PLANS. ALL DAMAGES THERETO CAUSED BY THE CONTRACTOR SHALL BE REPAIRED TO THE APPROPRIATE SPECIFICATIONS AND STANDARDS AT THE EXPENSE OF THE CONTRACTOR.

9. LOCATION AND ELEVATION OF EXISTING IMPROVEMENTS SHALL BE CONFIRMED BY FIELD MEASUREMENTS PRIOR TO CONSTRUCTION OF NEW WORK.

10. CONTRACTOR SHALL MAKE EXPLORATORY EXCAVATIONS AND LOCATE EXISTING UNDERGROUND FACILITIES SUFFICIENTLY AHEAD OF CONSTRUCTION TO PERMIT REVISIONS TO PLANS IF REVISIONS ARE NECESSARY BECAUSE OF ACTUAL LOCATION OF EXISTING FACILITIES.

11. FOR ALL UTILITY TRENCHES, SOILS REPORTS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD BY A QUALIFIED SOILS ENGINEER WHICH CERTIFY THAT TRENCH BACKFILL WAS COMPACTED AS DIRECTED BY THE SOILS ENGINEER IN ACCORDANCE WITH THE ON-SITE EARTHWORK SPECIFICATIONS.

12. ANY WORK DONE WITHOUT INSPECTION OR MATERIALS TESTING IS SUBJECT TO REMOVAL OR CORRECTION.

13. CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVAL OF ANY DAMAGE TO THE EXISTING IMPROVEMENTS AND REPLACEMENT TO THE SATISFACTION OF THE FIELD ENGINEER.

14. PRIOR TO COMMENCING CONSTRUCTION, THE CONTRACTOR SHALL VERIFY ALL JOIN CONDITIONS FOR GRADING, DRAINAGE AND UNDERGROUND FACILITIES, INCLUDING LOCATION AND ELEVATION OF EXISTING UNDERGROUND FACILITIES AT CROSSINGS WITH PROPOSED UNDERGROUND FACILITIES. IF CONDITIONS DIFFER FROM THOSE SHOWN ON THE PLANS THE CONTRACTOR SHALL NOTIFY THE ENGINEER AND SHALL NOT BEGIN CONSTRUCTION UNTIL THE CHANGED CONDITIONS HAVE BEEN EVALUATED

15. THE CONTRACTOR SHALL FAMILIARIZE HIMSELF/HERSELF WITH THE PLANS, THE SOILS AND/OR GEOLOGY REPORTS AND THE SITE CONDITIONS PRIOR TO COMMENCING WORK.

16. SHOULD CONFLICTING INFORMATION BE FOUND ON THE PLANS OR IN THE FIELD, THE CONTRACTOR SHALL NOTIFY THE PROJECT ENGINEER AT KIMLEY-HORN BEFORE PROCEEDING WITH THE WORK IN QUESTION.

18. DEVIATIONS FROM THESE SIGNED PLANS WILL NOT BE ALLOWED UNLESS THE COUNTY ENGINEER APPROVES A CONSTRUCTION CHANGE OR THE COUNTY/AGENCY INSPECTOR REQUIRES THE CHANGE.

21. NOTES AND DETAILS DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS. WHERE NO DETAILS ARE GIVEN, CONSTRUCTION SHALL BE AS SHOWN FOR SIMILAR WORK.

25. DIMENSIONS TO PIPELINES ARE TO CENTERLINE UNLESS OTHERWISE NOTED.

27. ALL DIMENSIONS ARE IN FEET OR DECIMALS THEREOF.

28. SPOT GRADES ARE TO FLOWLINE OR FINISH PAVEMENT GRADE UNLESS OTHERWISE NOTED.

29. CONTRACTOR TO BE AWARE OF ALL OVERHEAD LINES AT ALL TIMES, SO AS NOT TO DISTURB THEM. 30. WATER SHALL BE PROVIDED ONSITE AND USED TO CONTROL DUST DURING DEMOLITION AND CONSTRUCTION OPERATIONS.

31. STORM DRAINAGE SYSTEMS SHOWN ON THESE PLANS HAVE BEEN DESIGNED FOR THE FINAL SITE CONDITION AT COMPLETION OF THE PROJECT. THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ADEQUATE DRAINAGE OF THE SITE, DURING INTERIM CONDITIONS OF CONSTRUCTION.

32. RETAINING WALLS LOCATED CLOSER TO THE PROPERTY LINE THAN THE HEIGHT OF THE WALL SHALL BE BACKFILLED NOT LATER THAN 10 DAYS AFTER CONSTRUCTION OF THE WALL AND NECESSARY STRUCTURAL SUPPORTING MEMBERS UNLESS RECOMMENDED OTHERWISE BY RESPONSIBLE ENGINEER.

### STANDARD NOTES FOR EL PASO COUNTY GRADING AND EROSION CONTROL PLANS

- ON-SITE WATERS, INCLUDING WETLANDS.

- TO COORDINATE THE MEETING TIME AND PLACE WITH COUNTY STAFF.
- COMPLETION OF THE DISTURBANCE.

- PERMIT CLOSURE.
- ECM ADMINISTRATOR PRIOR TO IMPLEMENTATION.
- AND APPROVED.
- OF THE CONTROL MEASURE(S).
- SEDIMENT OFF SITE.
- SURFACE WATER BODY, CREEK, OR STREAM.

- AND PROPERLY DISPOSED OF IMMEDIATELY.
- APPURTENANCES AS A RESULT OF SITE DEVELOPMENT.
- THEIR ORIGINAL CONTAINERS, WITH ORIGINAL MANUFACTURER'S LABELS.
- CHEMICAL(S). SPECIAL CONDITIONS AND MONITORING MAY BE REQUIRED.
- CONTROL MEASURES.
- APPLY.
- 26. PRIOR TO CONSTRUCTION THE PERMITTEE SHALL VERIFY THE LOCATION OF EXISTING UTILITIES.
- FROM EARTHWORK EQUIPMENT AND WIND.
- THESE PLANS.
- INFORMATION OR APPLICATION MATERIALS CONTACT:

COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT WATER QUALITY CONTROL DIVISION WQCD - PERMITS 4300 CHERRY CREEK DRIVE SOUTH DENVER, CO 80246-1530 ATTN: PERMITS UNIT

STORMWATER DISCHARGES FROM CONSTRUCTION SITES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLUTION, CONTAMINATION, OR DEGRADATION OF STATE WATERS. ALL WORK AND EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY

2. NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED IN WRITING

A SEPARATE STORMWATER MANAGEMENT PLAN (SWMP) FOR THIS PROJECT SHALL BE COMPLETED AND AN EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP) ISSUED PRIOR TO COMMENCING CONSTRUCTION. MANAGEMENT OF THE SWMP DURING CONSTRUCTION IS THE RESPONSIBILITY OF THE DESIGNATED QUALIFIED STORMWATER MANAGER OR CERTIFIED EROSION CONTROL INSPECTOR. THE SWMP SHALL BE LOCATED ON SITE AT ALL TIMES DURING CONSTRUCTION AND SHALL BE KEPT UP TO DATE WITH WORK PROGRESS IN THE FIELD. 4. ONCE THE ESQCP IS APPROVED AND A "NOTICE TO PROCEED" HAS BEEN ISSUES, THE CONTRACTOR MAY INSTALL THE INITIAL STAGE EROSION AND SEDIMENT CONTROL MEASURES AS INDICATED ON THE APPROVED GEC. A PRE-CONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, AND EL PASO COUNTY WILL BE HELD PRIOR TO ANY CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE APPLICANT 5. CONTROL MEASURES MUST BE INSTALLED PRIOR TO COMMENCEMENT OF ACTIVITIES THAT COULD CONTRIBUTE POLLUTANTS TO STORMWATER.

CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES AND DISTURBED LAND AREAS SHALL BE INSTALLED IMMEDIATELY UPON

ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE MAINTAINED AND REMAIN IN EFFECTIVE OPERATING CONDITION UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED AND FINAL STABILIZATION IS ESTABLISHED. ALL PERSONS ENGAGED IN LAND DISTURBANCE ACTIVITIES SHALL ASSESS THE ADEQUACY OF CONTROL MEASURES AT THE SITE AND IDENTIFY IF CHANGES TO THOSE CONTROL MEASURES ARE NEEDED TO ENSURE THE CONTINUED EFFECTIVE PERFORMANCE OF THE CONTROL MEASURES. ALL CHANGES TO TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES MUST BE INCORPORATED INTO THE STORMWATER MANAGEMENT PLAN. TEMPORARY STABILIZATION SHALL BE IMPLEMENTED ON DISTURBED AREAS AND STOCKPILES WHERE GROUND DISTURBING CONSTRUCTION ACTIVITY HAS PERMANENTLY CEASED OR TEMPORARILY CEASED FOR LONGER THAN 14 DAYS.

FINAL STABILIZATION MUST BE IMPLEMENTED AT ALL APPLICABLE CONSTRUCTION SITES. FINAL STABILIZATION IS ACHIEVED WHEN ALL GROUND DISTURBING ACTIVITIES ARE COMPLETE AND ALL DISTURBED AREAS EITHER HAVE A UNIFORM VEGETATIVE COVER WITH INDIVIDUAL PLAN DENSITY OF 70% OF PRE-DISTURBED LEVELS ESTABLISHED OR EQUIVALENT PERMANENT ALTERNATIVE STABILIZATION METHOD IS IMPLEMENTED. ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED UPON FINAL STABILIZATION AND BEFORE

ALL PERMANENT STORMWATER MANAGEMENT FACILITIES SHALL BE INSTALLED AS DESIGNED IN THE APPROVED PLANS. ANY PROPOSED CHANGES THAT EFFECT THE DESIGN OR FUNCTION OF PERMANENT STORMWATER MANAGEMENT STRUCTURES MUST BE APPROVED BE THE

10. EARTH DISTURBANCES SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY MINIMIZE ACCELERATED SOIL EROSION AND RESULTING SEDIMENTATION. ALL DISTURBANCES SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME. PRE-EXISTING VEGETATION SHALL BE PROTECTED AND MAINTAINED WITHIN 50 HORIZONTAL FEET OF A WATERS OF THE STATE UNLESS SHOWN TO BE INFEASIBLE AND SPECIFICALLY REQUESTED

COMPACTION OF SOIL MUST BE PREVENTED IN AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES OR WHERE FINAL STABILIZATION WILL BE ACHIEVED BY VEGETATIVE COVER. AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES SHALL ALSO BE PROTECTED FROM SEDIMENTATION DURING CONSTRUCTION UNTIL FINAL STABILIZATION IS ACHIEVED. IF COMPACTION PREVENTION IS NOT FEASIBLE DUE TO SITE CONSTRAINTS, ALL AREAS DESIGNATED FOR INFILTRATION AND VEGETATION CONTROL MEASURES MUST BE LOOSENED PRIOR TO INSTALLATION

12. ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORMWATER AROUND, THROUGH, OR FROM THE EARTH DISTURBANCE AREA SHALL BE A STABILIZED CONVEYANCE DESIGNED TO MINIMIZE EROSION AND THE DISCHARGE OF

13. CONCRETE WASH WATER SHALL BE CONTAINED AND DISPOSED OF IN ACCORDANCE WITH THE SWMP. NO WASH WATER SHALL BE DISCHARGED TO OR ALLOWED TO ENTER STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES. CONCRETE WASHOUTS SHALL NOT BE LOCATED IN AN AREA WHERE SHALLOW GROUNDWATER MAY BE PRESENT, OR WITHIN 50 FEET OF A

14. DURING DEWATERING OPERATIONS OF UNCONTAMINATED GROUND WATER MAY BE DISCHARGED ON SITE, BUT SHALL NOT LEAVE THE SITE IN THE FORM OF SURFACE RUNOFF UNLESS AN APPROVED STATE DEWATERING PERMIT IS IN PLACE. 15. EROSION CONTROL BLANKETING OR OTHER PROTECTIVE COVERING SHALL BE USED ON SLOPES STEEPER THAN 3:1.

16. CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL WASTES FROM THE CONSTRUCTION SITE FOR DISPOSAL IN ACCORDANCE WITH LOCAL AND STATE REGULATORY REQUIREMENTS. NO CONSTRUCTION DEBRIS, TREE SLASH, BUILDING MATERIAL WASTES OR UNUSED BUILDING MATERIALS SHALL BE BURIED, DUMPED, OR DISCHARGED AT THE SITE.

17. WASTE MATERIALS SHALL NOT BE TEMPORARILY PLACED OR STORED IN THE STREET, ALLEY, OR OTHER PUBLIC WAY, UNLESS IN ACCORDANCE WITH AN APPROVED TRAFFIC CONTROL PLAN. CONTROL MEASURES MAY BE REQUIRED BY EL PASO COUNTY ENGINEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES.

18. TRACKING OF SOILS AND CONSTRUCTION DEBRIS OFF-SITE SHALL BE MINIMIZED. MATERIALS TRACKED OFF-SITE SHALL BE CLEANED UP

19. THE OWNER/DEVELOPER SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS, DIRT, TRASH, ROCK, SEDIMENT, SOIL AND SAND THAT MAY ACCUMULATE IN ROADS, STORM DRAINS, AND OTHER DRAINAGE CONVEYANCE SYSTEMS AND STORMWATER

20. THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE SHALL BE LIMITED, AS MUCH AS PRACTICAL, TO THAT QUANTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE. ALL MATERIALS STORED ON-SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER, IN

21. NO CHEMICAL(S) HAVING THE POTENTIAL TO BE RELEASED IN STORMWATER ARE TO BE STORED OR USED ONSITE UNLESS PERMISSION FOR THE USE OF SUCH CHEMICAL(S) IS GRANTED IN WRITING BY THE ECM ADMINISTRATOR. IN GRANTING APPROVAL FOR THE USE OF SUCH

22. BULK STORAGE OF ALLOWED PETROLEUM PRODUCTS OR OTHER ALLOWED LIQUID CHEMICALS IN EXCESS OF 55 GALLONS SHALL REQUIRE ADEQUATE SECONDARY CONTAINMENT PROTECTION TO CONTAIN ALL SPILLS ONSITE AND TO PREVENT ANY SPILLED MATERIALS FROM ENTERING STATE WATERS, ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR OTHER FACILITIES. 23. NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER FLOW IN THE CURB AND GUTTER OR DITCH EXCEPT WITH APPROVED SEDIMENT

24. OWNER/DEVELOPER AND THEIR AGENTS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33 USC 1344), IN ADDITION TO THE REQUIREMENTS OF THE LAND DEVELOPMENT CODE, DCM VOLUME II AND THE ECM APPENDIX I. ALL APPROPRIATE PERMITS MUST BE OBTAINED BY THE CONTRACTOR PRIOR TO CONSTRUCTION (1041, NPDES, FLOODPLAIN, 404, FUGITIVE DUST, ETC.). IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS AND OTHER LAWS, RULES, OR REGULATIONS OF OTHER FEDERAL, STATE, LOCAL OR COUNTY AGENCIES, THE MOST RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL

25. ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE ONLY AT APPROVED CONSTRUCTION ACCESS POINTS.

27. A WATER SOURCE SHALL BE AVAILABLE ON SITE DURING EARTHWORK OPERATIONS AND SHALL BE UTILIZED AS REQUIRED TO MINIMIZE DUST 28. THE GEOTECHNICAL EVALUATION FOR THIS SITE HAS BEEN PREPARED BY CTL THOMPSON, INC AND SHALL BE CONSIDERED A PART OF

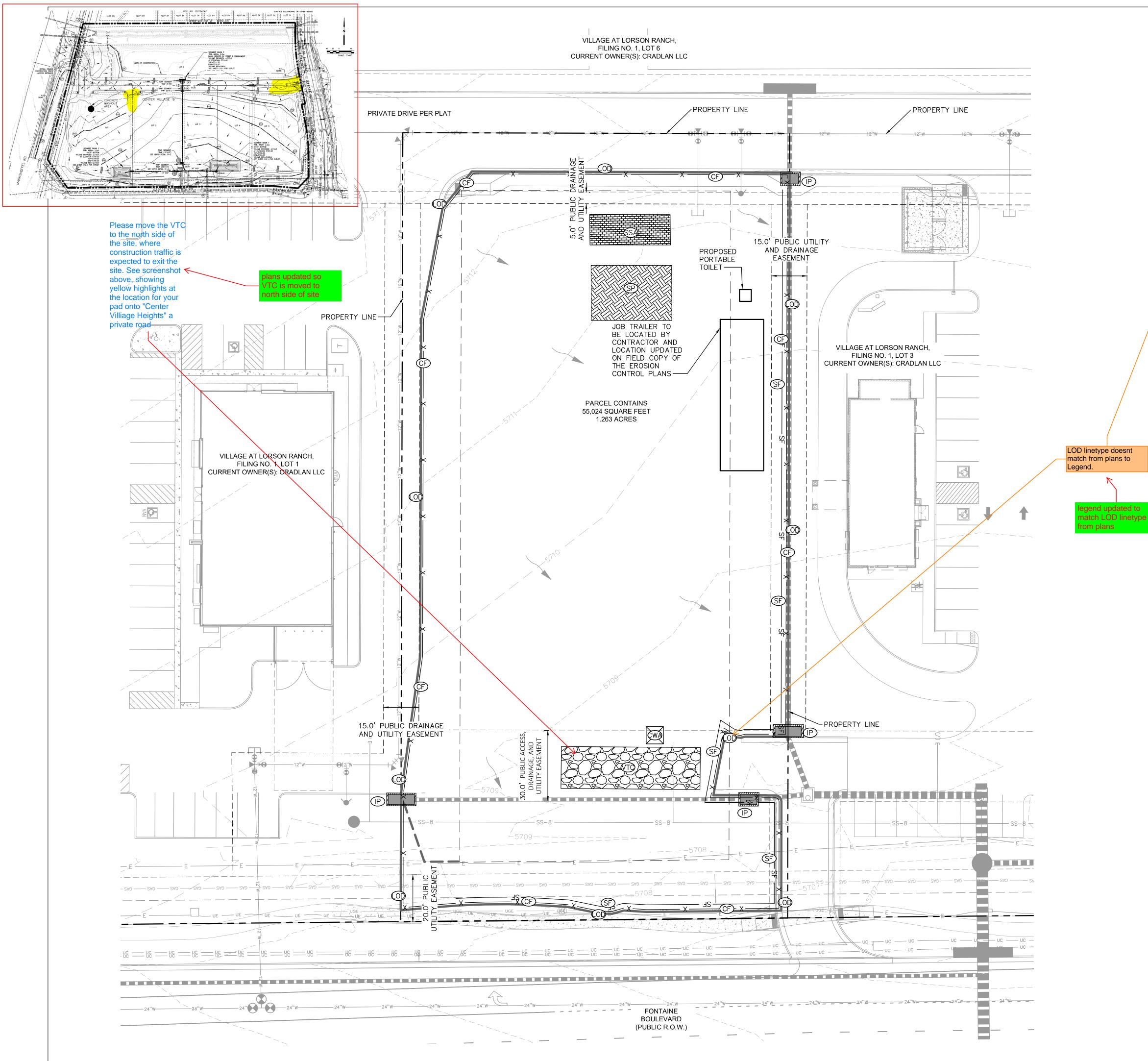
29. AT LEAST TEN (10) DAYS PRIOR TO THE ANTICIPATED START OF CONSTRUCTION, FOR PROJECTS THAT WILL DISTURB ONE (1) ACRE OF MORE, THE OWNER OR OPERATOR OF CONSTRUCTION ACTIVITY SHALL SUBMIT A PERMIT APPLICATION FOR STORMWATER DISCHARGE TO THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT, WATER QUALITY DIVISION, THE APPLICATION CONTAINS CERTIFICATION OF COMPLETION OF A STORMWATER MANAGEMENT PLAN (SWMP), OF WHICH THIS GRADING AND EROSION CONTROL PLAN MAY BE A PART. FOR

https://cdphe.colorado.gov/cor400000-stormwater-discharge

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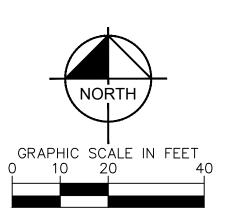
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SOIL STOCKPILE

INLET PROTECTION EXISTING ELECTRIC LINE EXISTING UNDERGROUND COMMUNICATION LINE

### NOTES

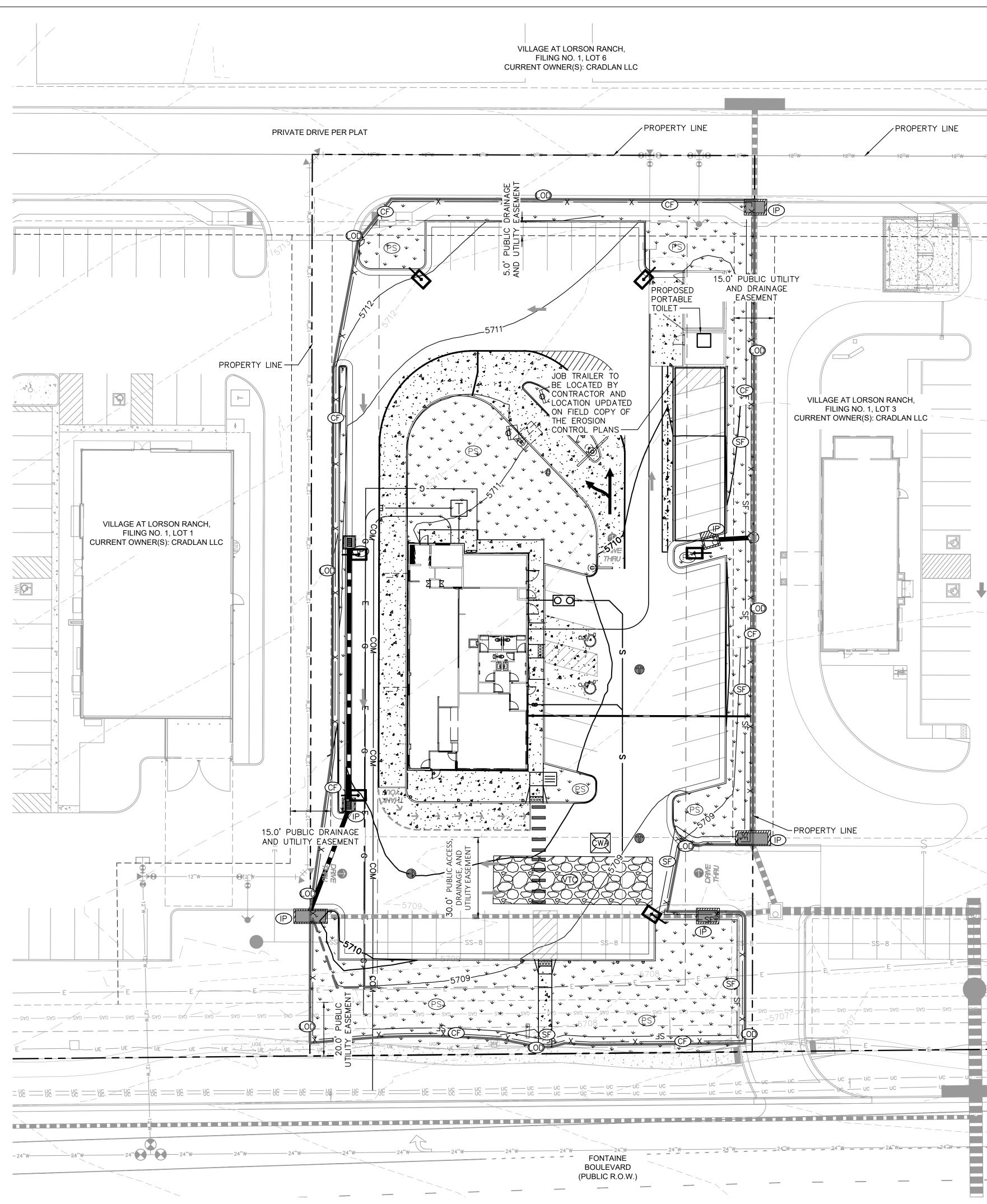
- 1. THE INTENT OF THIS PLAN IS TO IDENTIFY THE EROSION CONTROL PRACTICES RECOMMENDED. THE CONTRACTOR SHALL REFERENCE ADDITIONAL CONSTRUCTION PLANS FOR DEMOLITION OF EXISTING AND CONSTRUCTION OF PROPOSED IMPROVEMENTS.
- 2. ADJACENT STREETS AND SIDEWALK SHALL BE KEPT CLEAN AND FREE OF SEDIMENT AND/OR DEBRIS AT ALL TIMES. CONTRACTOR SHALL PERFORM STREET SWEEPING AT ALL TIMES DURING ACTIVE TRACKING AND AT A MINIMUM ON A DAILY BASIS AT THE END OF EACH CONSTRUCTION DAY.
- 3. TEMPORARY STABILIZATION (TS) SHALL BE IMPLEMENTED WITHIN THE DISTURBED PORTIONS OF THE PROJECT SITE NO LATER THAN 14 DAYS FOLLOWING THE CEASE OF CONSTRUCTION ACTIVITIES WITHIN THE DISTURBED AREAS.
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- 7. ALL WORK IN THE FONTAINE BOULEVARD ROW REQUIRES A ROW PERMIT FROM COLORADO SPRINGS. CONTRACTOR IS RESPONSIBLE FOR APPLYING FOR AND OBTAINING ALL NECESSARY ROW PERMITS.
- 8. CONTRACTOR SHALL REFER TO THE APPROVED GEOTECHNICAL REPORT FOR OVEREXCAVATION REQUIREMENTS AND ADDITIONAL INFORMATION.
- 9. SILT FENCE TO BE INSTALLED PRIOR TO COMMENCEMENT OF ONSITE GRADING AND CONSTRUCTION ACTIVITIES.
- 10. DEMOLITION, REMOVAL AND SOIL TREATMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER RECOMMENDATIONS AS NOTED IN THE APPROVED PROJECT GEOTECHNICAL REPORT.
- 11. CONTRACTOR TO NOTE PROXIMITY OF EXISTING IMPROVEMENTS ADJACENT TO THE SITE AND PROVIDE NECESSARY MEASURES TO PROTECT ALL FACILITIES AND STRUCTURES IN PLACE.
- 12. CONTRACTOR SHALL MAINTAIN STABILIZED STAGING AREA (SSA), VEHICLE TRACKING CONTROL (VTC), AND CONCRETE WASHOUT AREA (CWA) AT THE CONSTRUCTION ENTRANCE AT ALL TIMES. CONTRACTOR SHALL UPDATE THE EROSION CONTROL PLAN IN THE FIELD TO INDICATE THE LOCATION OF THE SSA, VTC, AND CWA BMPS AS EXCAVATION SEQUENCING DICTATES.
- 13. CONTRACTOR MAY SUBSTITUTE SEDIMENT CONTROL LOGS (SCL) FOR SILT FENCE (SF) AS PERIMETER CONTROL, DEPENDING UPON SITE CONDITIONS. SCL, AND SF MAY BE INTERCHANGED DEPENDING ON SITE CONDITIONS. 14. CONTRACTOR SHALL OBTAIN R.O.W. PERMITS FOR ANY R.O.W. CLOSURES.
- 15. SEE FINAL LANDSCAPING PLAN IN THE SITE DEVELOPMENT PLAN FOR FINAL STABILIZATION MEASURES.





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								DESCRIPTION
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	Kimley » Horn							
PREPARED BY:								
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DRAWN BY	ALS STD ISSUE DATE	7/30/2024	REVIEWED BY	JJM	DATE ISSUED	7/30/2024		
ШПЕ	CONSTRUCTION DRAWINGS		DESCRIPTION				SITE ID SITE ADDRESS	51028 NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO 51028 SPRINGS, CO



\_\_\_\_\_\_ PROPERTY LINE PROPERTY LINE  $+\!\!+-\!\!--\!\!--$ . . 15.0' PUBLIC UTILITY AND DRAINAGE PROPOSED EASEMENT PORTABLE TOILET ------· • • JOB TRAILER TO BE LOCATED BY CONTRACTOR AND VILLAGE AT LORSON RANCH, LOCATION UPDATED FILING NO. 1, LOT 3 ON FIELD COPY OF CURRENT OWNER(S): CRADLAN LLC THE EROSION CONTROL PLANS-B Ð | 二字二| " (PS)" -PROPERTY LINE \_\_\_\_ - 573 -. \_\_\_\_ uc \_\_\_\_\_ uc \_\_\_\_ – UC – — UC — UC — \_ -24''W - 24''W - 24'FONTAINE BOULEVARD (PUBLIC R.O.W.)

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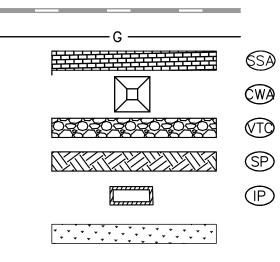
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FILING NO. 1, LOT 6

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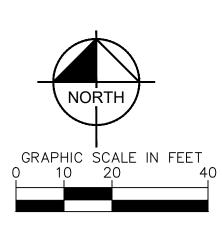
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PROPOSED GAS LINE
STABILIZED STAGING AREA
CONCRETE WASHOUT
VEHICLE TRACKING CONTROL
SOIL STOCKPILE
INLET PROTECTION
FINAL STABILIZATION. (REFERENCE FINAL LANDSCAPING PLANS)

### NOTES

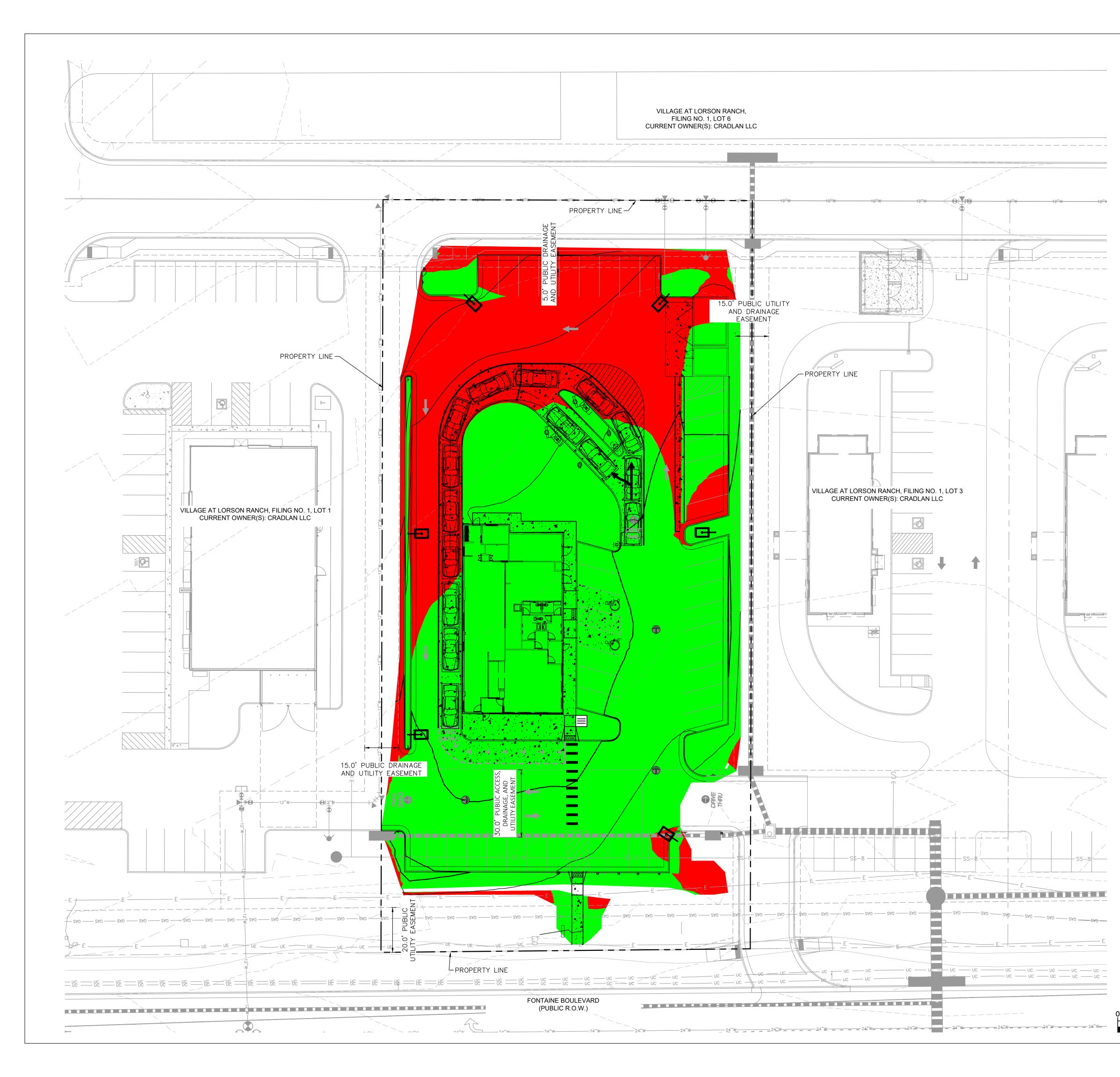
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ППСЕ	CONSTRUCTION DRAWINGS		DESCRIPTION			SITE ADDRESS	51028 NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO
	DRAWN BY PREPARED FOR:	WINGS STIF PATE FOR: © MCDONALD'S USA. LLC	NSTRUCTION DRAWINGS 7/30/2024 These dravings and specifications are the confidential and provision	WINGS ALS ALS ALS T/30/2024 REVIEWE BY REVIEWE BY PREPARED FOR: () MCDONAId'S USA, LLC These drawings and specifications are the confidential and proprietary REVIEWE BY PREPARED BY: PREPARED BY: PRE	DRAWN BY       DRAWN BY       PREPARED FOR:       ©         ALS       ALS       ALS       T/30/2024         7/30/2024       T/30/2024       These drawings and specifications are the confidential and proprietary property of MCDonald's USA, LLC and shall not be copied or reproduced without written authorization. The contract documents were prepared for use on this specific site in conjunction with its issue date and are	DRAWN BY       PREPARED FOR:       Image: Construction of the construction with its issue date and are not suitable for use on a different site or at a later time. Use of these drawings for reference or example on another project requires the construction of the contract drawings for reference or example on another project requires the construct or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawings for reference or example on another project requires the contract drawing for the contract drawings for reference or example on another project requires the contract drawing for reference or example on another project requires the contract drawing for the contract drawing for the contract drawing for reference or example on another project requires the contract drawing for the con	DRAWN BY       DRAWN BY       REPARED FOR:       Image       Image </th



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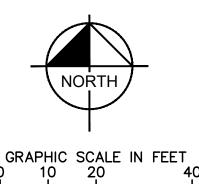
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## CUT FILL SUMMARY

PROPOSED CUT = 128 CY
PROPOSED FILL = $698$ CY
NET = 570 CY

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	Kimlev»		
McDonald's USA, L	property of McDonald's USA, LLC and shall not be conjugation und proprietary property of McDonald's USA, LLC and shall not be copied or reproduced without written authorization. The contract documents were prepared for use on this specific site in conjunction with its issue date and are	not suitable for use on a different site or at a later time. Use of these drawings for reference or example on another project requires the services of properly licensed architects and engineers. Reproduction of	the contract documents for reuse on another project is not authorized.
STD ISSUE DATE 7/30/2024	REVIEWED BY JJM	DATE ISSUED 7/30/2024	L ROAD, COLORADO
		CUT FILL PLAN	SITE ID SITE ADDRESS 51028 SPRINGS, CO
	CONSTRUCTION DRAWINGS 7/30/2024 THIS CONSTRUCTION DRAWINGS	CONSTRUCTION DRAWINGS       ALS       ALS       MCDOnald's USA, LLC         7/30/2024       7/30/2024       These drawings and specifications are the confidential and proprietary property of McDonald's USA, LLC and shall not be copied or reproduced without written authorization. The contract documents were prepared for use on this secific site in conjunction with its issue date and ore	ALS     ALS     ALS       CONSTRUCTION DRAWINGS     STD ISSUE DATE     MCDONAId'S USA, L       7/30/2024     T/30/2024     These drawings and specifications are the confidential and post       DESCRIPTION     REVIEWED BY     These drawings and specifications are the confidential and post       UN     JUM     Property of McDonald's USA, LLC and shall not be copied or JUM       DESCRIPTION     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIM     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIM     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIM     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIM     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIM     DIM     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA, LLC and shall not be copied or JUM       DIA     DIA     Property of McDonald's USA





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### **Concrete Washout Area (CWA)**

#### Description

Concrete waste management involves designating and properly managing a specific area of the construction site as a concrete washout area. A concrete washout area can be created using one of several approaches designed to receive wash water from washing of tools and concrete mixer chutes, liquid concrete waste from dump trucks, mobile batch mixers, or pump trucks. Three basic approaches are available: excavation of a pit in the ground, use of an above ground storage area, or use of prefabricated haulaway concrete washout containers. Surface discharges of concrete washout



**MM-1** 

water from construction sites are prohibited. Photograph CWA-1. Example of concrete washout area. Note gravel tracking pad for access and sign.

#### Appropriate Uses

Concrete washout areas must be designated on all sites that will generate concrete wash water or liquid concrete waste from onsite concrete mixing or concrete delivery.

Because pH is a pollutant of concern for washout activities, when unlined pits are used for concrete washout, the soil must have adequate buffering capacity to result in protection of state groundwater standards; otherwise, a liner/containment must be used. The following management practices are recommended to prevent an impact from unlined pits to groundwater:

- The use of the washout site should be temporary (less than 1 year), and
- The washout site should be not be located in an area where shallow groundwater may be present, such as near natural drainages, springs, or wetlands.

#### **Design and Installation**

Concrete washout activities must be conducted in a manner that does not contribute pollutants to surface waters or stormwater runoff. Concrete washout areas may be lined or unlined excavated pits in the ground, commercially manufactured prefabricated washout containers, or aboveground holding areas constructed of berms, sandbags or straw bales with a plastic liner.

Although unlined washout areas may be used, lined pits may be required to protect groundwater under certain conditions.

Urban Drainage and Flood Control District

Urban Storm Drainage Criteria Manual Volume 3

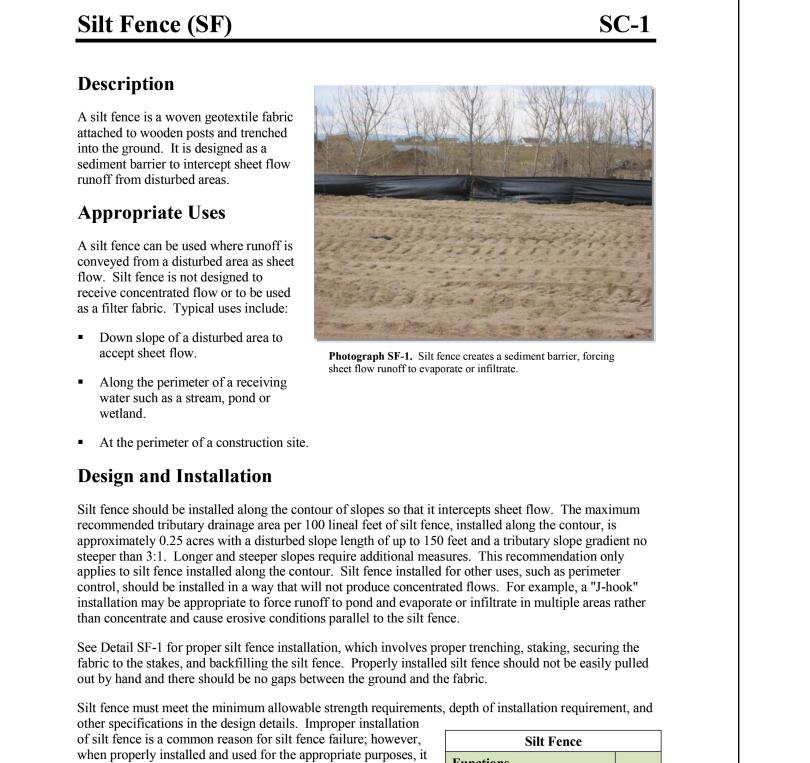
Do not locate an unlined washout area within 400 feet of any natural drainage pathway or waterbody or within 1,000 feet of any wells or drinking water sources. Even for lined concrete washouts, it is advisable to locate the facility away from waterbodies and drainage paths. If site constraints make these

November 2010

can be highly effective.

<b>Concrete Washout Area</b>					
Functions					
Erosion Control	No				
Sediment Control	No				
Site/Material Management	Yes				

CWA-1



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	Urban Storm Drainage Criteria Manual Volume 3	

Functions

Erosion Control

Sediment Control

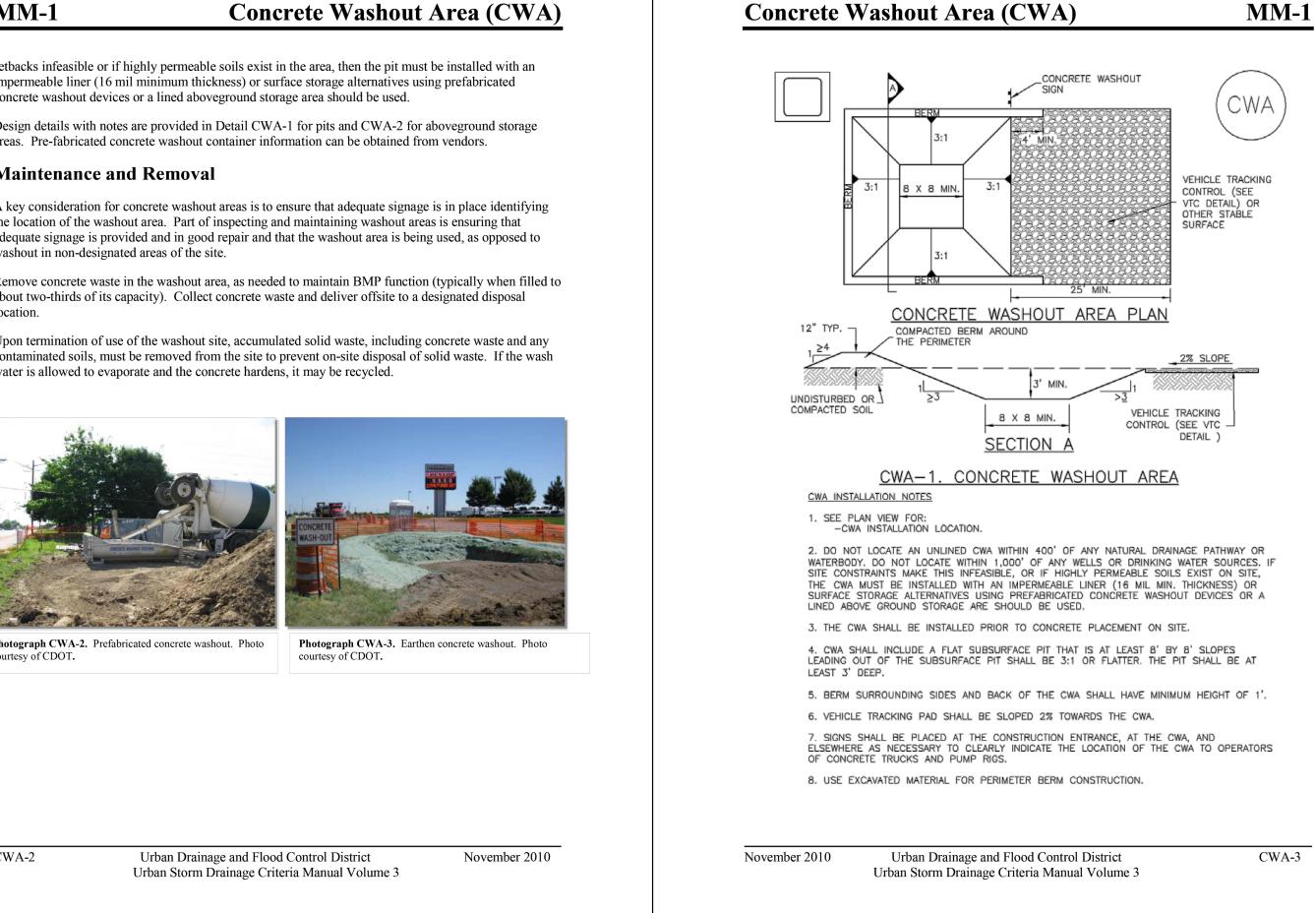
Site/Material Management

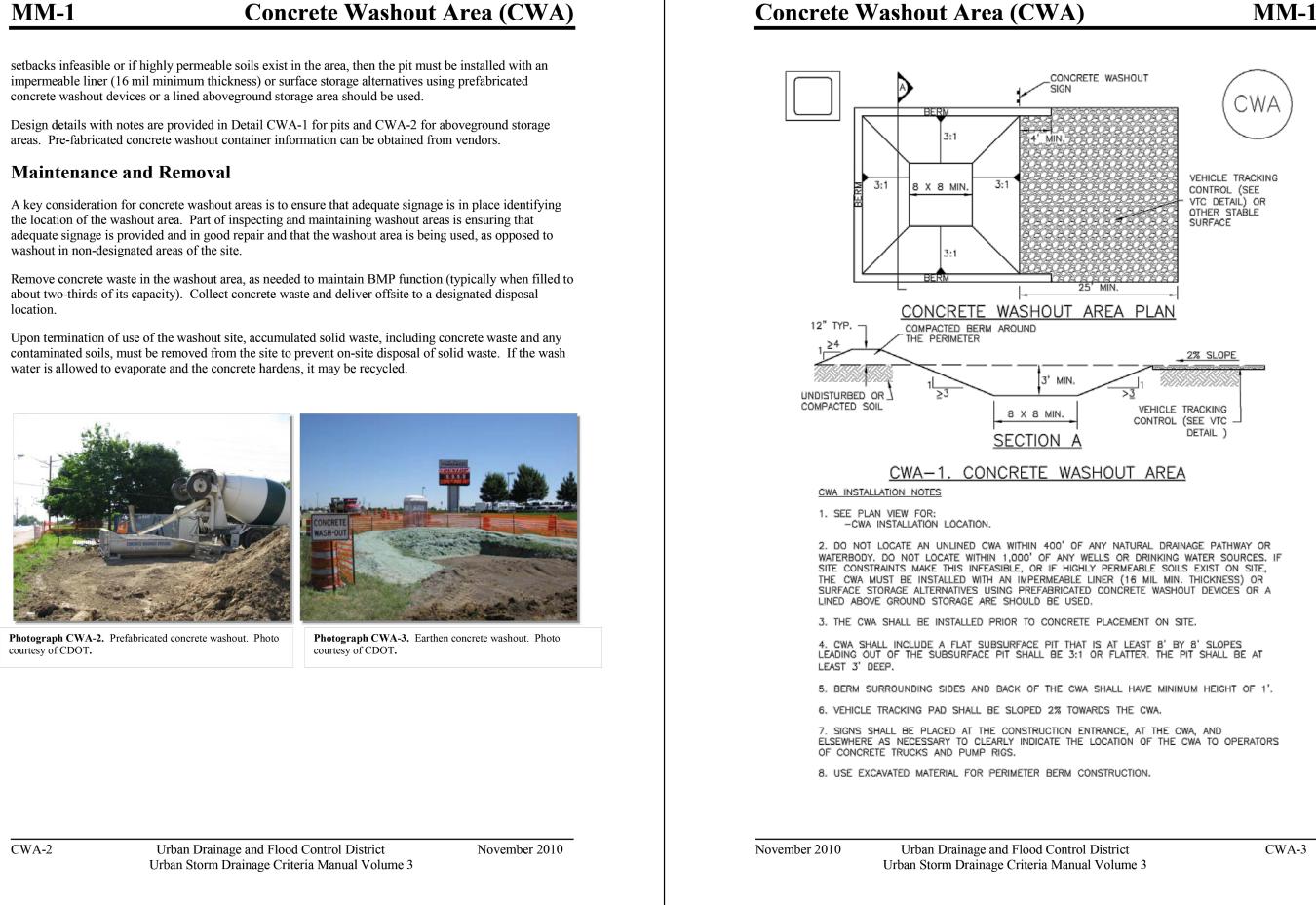
No

Yes

No

#### Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3





**SC-1** 

### Maintenance and Removal

Inspection of silt fence includes observing the material for tears or holes and checking for slumping fence and undercut areas bypassing flows. Repair of silt fence typically involves replacing the damaged section with a new section. Sediment accumulated behind silt fence should be removed, as needed to maintain BMP effectiveness, typically before it reaches a depth of 6 inches.

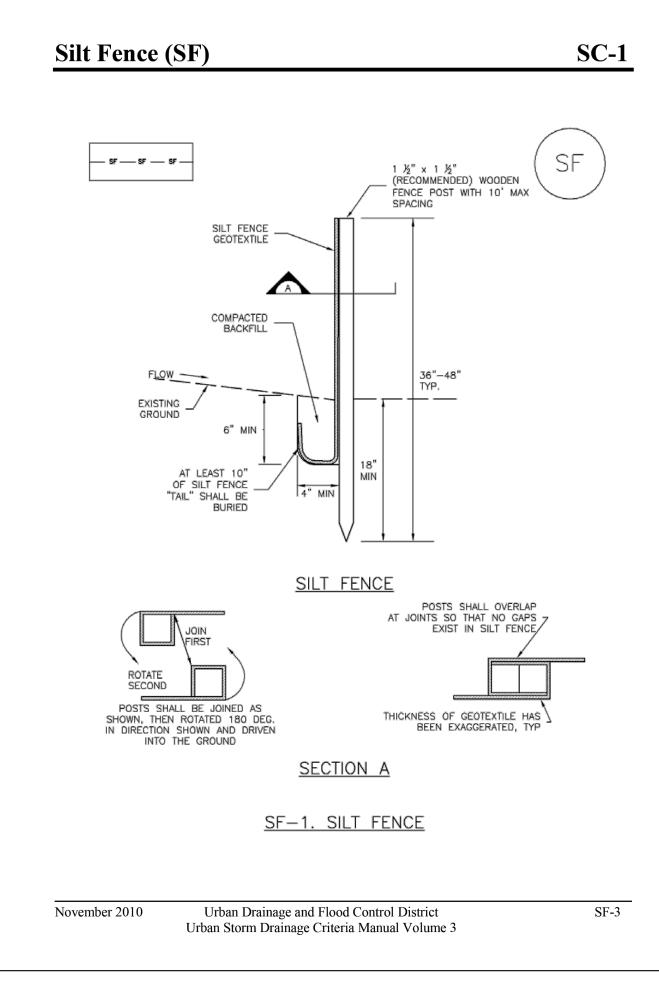
Silt fence may be removed when the upstream area has reached final stabilization.





Photograph SF-2. When silt fence is not installed along the contour, a "J-hook" installation may be appropriate to ensure that the BMP does not create concentrated flow parallel to the silt fence. Photo courtesy of Tom

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MM-	1 Concrete Washout Area (CWA)	
<u>MM-</u>	<ol> <li>Concrete Washout Area (CWA)</li> <li>INSPECT BMPS EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPS SHOULD BE PROACTIVE, NOT REACTIVE, INSPECT BMPS AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE ERGSION, AND PERFORM NECESSARY MAINTENANCE.</li> <li>REQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPS IN EFFECTIVE OPERATING CONDITION, INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.</li> <li>HERRE BMPS HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.</li> <li>HERRE MAYS HAUE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.</li> <li>CONCRETE WASTE, CONCRETE MATERIALS, ACCUMULATED IN PIT, SHALL BE REMOVED ONCE THE MATERIALS HAVE REACHED A DEPH OF 2'.</li> <li>CONCRETE WASTE, CONCRETE MATERIALS, ACCUMULATED IN PIT, SHALL BE REMOVED ONCE THE MATERIALS HAVE REACHED A DEPH OF 2'.</li> <li>CONCRETE WASTE, UNTER, WASTED PIECES OF CONCRETE AND ALL OTHER DEBRIS IN THE SUBSURFACE PIT SHALL BE TRANSPORTED FROM THE JOB SITE IN A WATER-TIGHT.</li> <li>MEINT BAUSURFACE PIT SHALL BE TRANSPORTED FROM THE JOB SITE IN A WATER-TIGHT.</li> <li>THE CWA SHALL REMAIN IN PLACE UNTIL ALL CONCRETE FOR THE PROJECT IS PLACED.</li> <li>THE CWA SHALL REMAIN IN PLACE UNTIL ALL CONCRETE FOR THE PROJECT IS PLACED.</li> <li>MEINT BAUSURFACE PIT SHALL BE TRANSPORTE APPROVED BY THE LOCAL JURISDICTION.</li> <li>MEINT BAUSURFACE MATERIALS HAVE REACHED A DEPH PARKER, COLORADO, NOT AMAINEL IN AUTOR.</li> <li>MEINT BAUSURFACE PIT SHALL BE TRANSPORTE APPROVED BY THE LOCAL JURISDICTION.</li> <li>MEINT BAUSURFACE PIT SHALL BE TRANSPORTE APPROVED BY THE LOCAL JURISDICTION.</li> <li>MEINT BAUSURFACE PIT SHALL BE TRANSPORTE APPROVED BY THE LOCAL JURISDICTION.</li> <li>MEINT BAUSURFACE PIT A MAINTER APPROVED BY THE LOCAL JURISDICTION.</li> <li>MEINT DO THERWINSE STABLIZZED IN A MAINTER APPROVED BY THE LOC</li></ol>	
		Kimley »Horn
CWA-4	Urban Drainage and Flood Control District November 2010 Urban Storm Drainage Criteria Manual Volume 3	PREPARED BY:
	SULT FENCE INSTALLATION NOTES SULT FENCE INSTALLATION NOTES I. SILT FENCE INSTALLATION NOTES I. SILT FENCE MUST BE PLACED AWAY FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING, SILT FENCE AT THE TOE OF A SLOPE SHOULD BE INSTALLED IN A FLAT LOCATION AT LEAST SEVERAL FEET (2-5 FT) FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING, SILT FENCE, AT THE TOE OF A SLOPE SHOULD BE INSTALLED IN A FLAT LOCATION AT LEAST SEVERAL FEET (2-5 FT) FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING, SILT FENCE, AT THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING, AND DEPOSITION. 2. A UNFORM 6° X 4° ANCHOR TRENCH SHALL BE EXCAVATED USING TRENCHER OR SILT FENCE INSTALLATION DEVICE. NO ROAD GRADERS, BACKHOES, OR SIMILAR EQUIPMENT SHALL E USED. 3. COMPACT ANCHOR TRENCH BY HAND WITH A "JUMPING JACK" OR BY WHEEL ROLLING, COMPACTON SHALL BE SUCH THAT SILT FENCE RESISTS BEING PULLED OUT OF ANCHOR E ON ONTOCRABLE SANG BETWEEN STARES AFTER IT HAS BEEN ANCHORED TO THE STAKES. THERE SHOULD E E NO NOTICEABLE SANG BETWEEN STARES AFTER IT HAS BEEN ANCHORED TO THE STAKES. THERE SHOULD ES INT FENCE FABRIC SHALL BE ANCHORED TO THE STAKES USING 1° HEAVY DUTY STAPLES OR NALLS WITH 1° HEADS. STAPLES AND NAILS SHOULD BE PLACED 3° ALONG THE FABRIC SOUNT THE STAKE. 5. SILT FENCE FABRIC SHALL BE ANCHORED TO THE STAKES USING 1° HEAVY DUTY STAPLES OR NALLS WITH 1° HEADS. STAPLES AND NAILS SHOULD BE PLACED 3° ALONG THE FABRIC DOWN THE STAKE.	FOR: © MCDDDAJd'S USA, LLC MCDDDAJd'S USA, LLC MCDDDAJd'S USA, LLC of McDonald's USA, LLC and shall not be copied or reproduced written authorization. The contract documents were prepared written authorization. The contract documents were prepared on this specific site in conjunction with its issue date and are been appendent of the or the order of the order
CWA-4	SILT FENCE INSTALLATION NOTES  SILT FENCE INSTALLATION NOTES  SILT FENCE INSTALLATION NOTES  SILT FENCE INSTALLATION NOTES  SILT FENCE MUST BE PLACED AWAY FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING, SILT FENCE AT THE TOE OF A SLOPE SHOULD BE INSTALLED IN A FLAT LOCATION AT LEAST SEVERAL FEET (2–5 FT) FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING SILT FENCE ATTHE TOE OF A SLOPE SHOULD BE INSTALLED IN A FLAT LOCATION AT LEAST SEVERAL FEET (2–5 FT) FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING STALLATION DEVICE. NO ROAD GRADERS, BACKHOES, OR SIMILAR EQUIPMENT SHALL BE SUCH THAT SILT FENCE RESISTS BEING PULLED OUT OF ANCHOR COMPACTION SHALL BE SUCH THAT SILT FENCE RESISTS BEING PULLED OUT OF ANCHOR ECONFACTION SHALL BE PULLED TIGHT AS IT IS ANCHORED TO THE STAKES. THERE SHOULD BE NO NOTICEABLE SAG BETWEEN STAKES AFTER IT HAS BEEN ANCHORED TO THE STAKES. S. SILT FENCE SHALL BE PULLED TIGHT AS IT IS ANCHORED TO THE STAKES. THERE SHOULD BE NO NOTICEABLE SAG BETWEEN STAKES AFTER IT HAS BEEN ANCHORED TO THE STAKES. S. SILT FENCE FABRIC SHALL BE ANCHORED TO THE STAKES USING 1" HEAVY DUTY STAFLES OR NALISWITH 1" HEADS, STAPLES AND NAILS SHOULD BE PLACED 3" ALONG THE FABRIC DOWN THE STAKE. S. AT THE END OF A RUN OF SILT FENCE ALONG A CONTOUR, THE SILT FENCE SHOULD BE TURNED PERPENDICULUAR TO THE COLOUR TO CREATE A "U-HOOK"."	FOR: © MCDDDAJd'S USA, LLC MCDDDAJd'S USA, LLC MCDDDAJd'S USA, LLC of McDonald's USA, LLC and shall not be copied or reproduced written authorization. The contract documents were prepared on this specific site in conjunction with its sisue date and are provided of the contract of the time of the

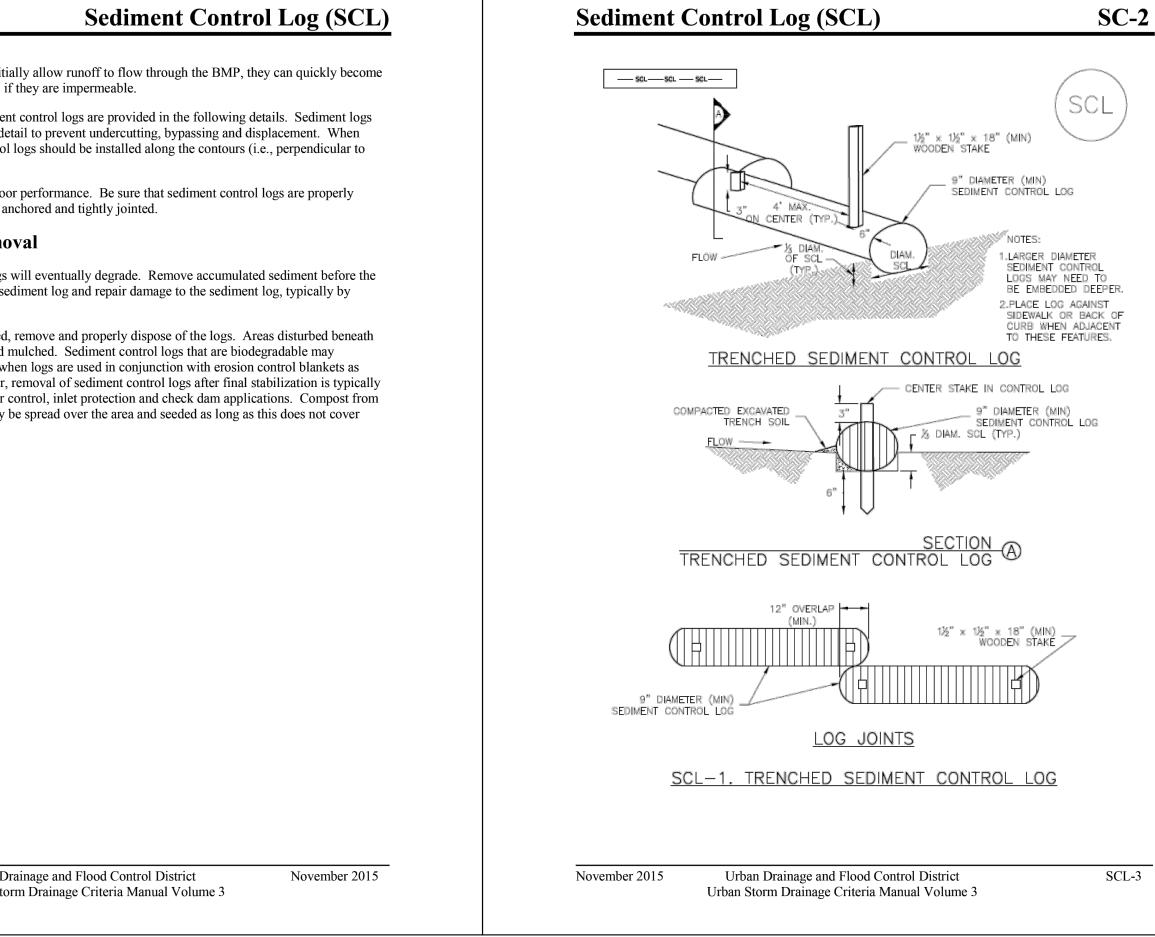


Know what's **below**. Call before you dig.

C2.6

Sediment Control Lo	g (SCL)	SC-2	<b>SC-2</b>
<ul> <li>Description</li> <li>A sediment control log is a linear roll made of natural materials such as straw, coconut fiber, or compost. The most common type of sediment control log has straw filling and is often referred to as a "straw wattle." All sediment control logs are used as a sediment barrier to intercept sheet flow runoff from disturbed areas.</li> <li>Appropriate Uses</li> <li>Sediment control logs can be used in the following applications to trap sediment:</li> <li>As perimeter control for stockpiles and the site.</li> <li>As part of inlet protection designs.</li> </ul>	<image/>		Although sediment contr a barrier and should be in Design details and notes must be properly installe installed on slopes, sedin flow). Improper installation car trenched (if lighter than a <b>Maintenance an</b> Be aware that sediment of depth is one-half the heig replacing the damaged se Once the upstream area i the logs may need to be a occasionally be left in pl permanent slope breaks) appropriate when used ir compost sediment contro
<ul> <li>As check dams in small drainage ditches. (Sediment control logs are not intended for use in channels with high flow velocities.)</li> <li>On disturbed slopes to shorten flow lengths (as an erosion control).</li> <li>As part of multi-layered perimeter conserved sediment control logs work well in combe <b>Design and Installation</b></li> <li>Sediment control logs should be installed allowable tributary drainage area per 100 approximately 0.25 acres with a disturbed steeper than 3:1. Longer and steeper slop applies to sediment control logs installed perimeter control logs. For examplinistallation may be appropriate to force revaporate or infiltrate in multiple areas ra and cause erosive conditions parallel to the stalled to the stalled of the stalled in the stalled of the stalled force of the stalled</li></ul>	along the contour to avoid concentratin lineal feet of sediment control log, insta l slope length of up to 150 feet and a tri es require additional measures. This rec along the contour. When installed for c a way that will not e, a "J-hook" moff to pond and ther than concentrate	and, 2) as a "J-hook" extron site. stream, pond or wetland. sediment controls. ang flows. The maximum alled along the contour, is butary slope gradient no commendation only other uses, such as the control Log rol Moderate ttrol Yes	
	ge and Flood Control District	SCL-1	SCL-2
	inage Criteria Manual Volume 3		502-2
Sediment Control Lo	inage Criteria Manual Volume 3	SC-2	<u>SC-2</u>
Sediment Control Lo	g (SCL)	SC-2	SC-2 SEDIMENT CONTROL 1. SEE PLAN VIEW 2. SEDIMENT CONT TO ANY UPGRADIED 3. SEDIMENT CONT FIBER, AND SHALL HOLES AND OBVIOU 4. SEDIMENT CONT HOWEVER, THEY SU 5. IT IS RECOMMEN A DEPTH OF APPR DEPTH IS NOT FEA DAMAGE LANDSCAP STAKING. COMPOST 6. THE UPHILL SID FILTER MATERIAL T COMPACTED INTO ROLLER OR BLOWN 7. FOLLOW MANUF DO NOT SPECIFY SI MINIMUM OF 6" IN THE LOG. STAKES LOGS SHOULD BE SEDIMENT CONTROL 1. INSPECT BMPS MAINTENANCE OF E POSSIBLE (AND ALL EROSION, AND PEI 2. FREQUENT OBSI EFFECTIVE OPERATIO DOCUMENTED THOP 3. WHERE BMPS H DISCOVERY OF THE 4. SEDIMENT ACCU
Sediment Control Lo	g (SCL)	SC-2	SC-2 SEDIMENT CONTRO 1. SEE PLAN VIEW 2. SEDIMENT CON TO ANY UPGRADIE 3. SEDIMENT CON FIBER, AND SHALL HOLES AND OBVIO 4. SEDIMENT CON FIBER, AND SHALL HOLES AND OBVIO 4. SEDIMENT CON FIBER, AND SHALL HOLES AND OBVIO 5. IT IS RECOMME A DEPTH OF APP DEPTH IS NOT FE DAMAGE LANDSCAI STAKING. COMPOS 6. THE UPHILL SI FILTER MATERIAL COMPACTED INTO ROLLER OR BLOW 7. FOLLOW MANUE DO NOT SPECIFY MINIMUM OF 6" IN THE LOG. STAKES LOGS SHOULD BE SEDIMENT CONTRO 1. INSPECT BMPs MAINTENANCE OF POSSIBLE (AND A EROSION, AND PE 2. FREQUENT OBS EFFECTIVE OPERAT DOCUMENTED THO 3. WHERE BMPs I

Urban Storm Drainage Criteria Manual Volume 3



## Sediment Control Log (SCL)

ALLATION NOTES

TION AND LENGTH OF SEDIMENT CONTROL LOGS.

THAT ACT AS A PERIMETER CONTROL SHALL BE INSTALLED PRIOR ISTURBING ACTIVITIES.

SHALL CONSIST OF STRAW, COMPOST, EXCELSIOR OR COCONUT OF ANY NOXIOUS WEED SEEDS OR DEFECTS INCLUDING RIPS,

MAY BE USED AS SMALL CHECK DAMS IN DITCHES AND SWALES. BE USED IN PERENNIAL STREAMS.

SEDIMENT CONTROL LOGS BE TRENCHED INTO THE GROUND TO & OF THE DIAMETER OF THE LOG. IF TRENCHING TO THIS 'OR DESIRABLE (SHORT TERM INSTALLATION WITH DESIRE NOT TO R TRENCHING DEPTH MAY BE ACCEPTABLE WITH MORE ROBUST T ARE 8 LB/FT DO NOT NEED TO BE TRENCHED.

SEDIMENT CONTROL LOG SHALL BE BACKFILLED WITH SOIL OR E OF ROCKS AND DEBRIS. THE SOIL SHALL BE TIGHTLY OF A RIGHT TRIANGLE USING A SHOVEL OR WEIGHTED LAWN

GUIDANCE FOR STAKING. IF MANUFACTURERS' INSTRUCTIONS AKES SHALL BE PLACED ON 4" CENTERS AND EMBEDDED A DUND. 3" OF THE STAKE SHALL PROTRUDE FROM THE TOP OF BROKEN PRIOR TO INSTALLATION SHALL BE REPLACED. COMPOST ' ON CENTER.

TENANCE NOTES DAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. LD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS N 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE ESSARY MAINTENANCE.

AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN ON. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE

REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON

PSTREAM OF SEDIMENT CONTROL LOG SHALL BE REMOVED AS NALITY OF THE BMP, TYPICALLY WHEN DEPTH OF ACCUMULATED  $\frac{1}{2}$  OF THE HEIGHT OF THE SEDIMENT CONTROL LOG.

#### HALL BE REMOVED AT THE END OF CONSTRUCTION.COMPOST LEFT IN PLACE AS LONG AS BAGS ARE REMOVED AND THE AREAS EXIST AFTER REMOVAL, THEY SHALL BE COVERED WITH CHED OR OTHERWISE STABILIZED IN A MANNER APPROVED BY

KER, COLORADO, JEFFERSON COUNTY, COLORADO, DOUGLAS COUNTY, COLORADO, AVAILABLE IN AUTOCAD) AVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN

November 2015

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### Inlet Protection (IP)

### Description

Inlet protection consists of permeable barriers installed around an inlet to filter runoff and remove sediment prior to entering a storm drain inlet. Inlet protection can be constructed from rock socks, sediment control logs, silt fence, block and rock socks, or other materials approved by the local jurisdiction. Area inlets can also be protected by over-excavating around the inlet to form a sediment trap.

### **Appropriate Uses**

Install protection at storm sewer inlets that are operable during construction.

Consider the potential for tracked-out sediment or temporary stockpile areas to contribute sediment to inlets when determining which inlets must be protected. This may include inlets in the general proximity of the construction area, not limited to downgradient inlets. Inlet protection is <u>not</u> a stand-alone BMP and should be used in conjunction with other upgradient BMPs.

Photograph IP-1. Inlet protection for a curb opening inlet.

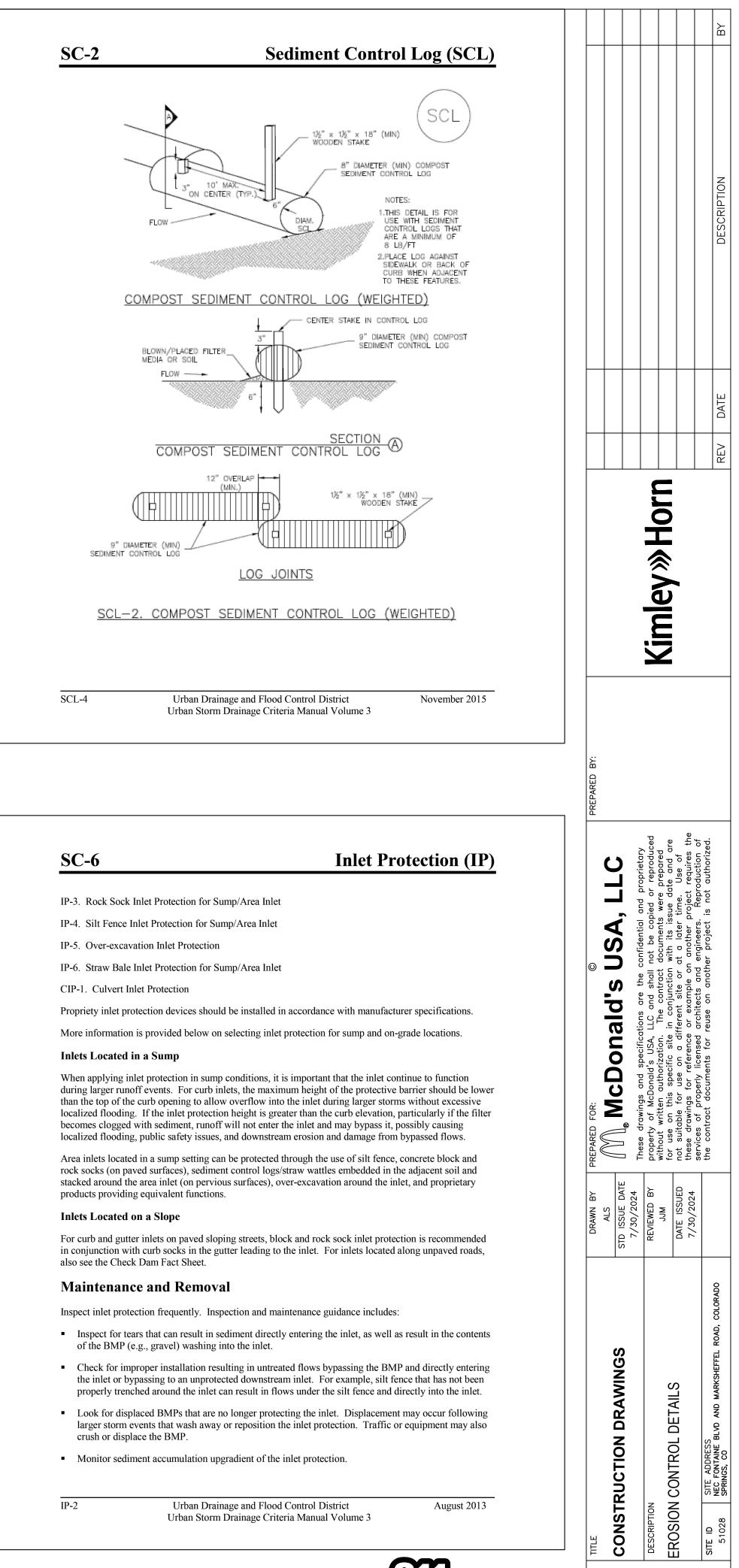
### **Design and Installation**

To function effectively, inlet protection measures must be installed to ensure that flows do not bypass the inlet protection and enter the storm drain without treatment. However, designs must also enable the inlet to function without completely blocking flows into the inlet in a manner that causes localized flooding. When selecting the type of inlet protection, consider factors such as type of inlet (e.g., curb or area, sump or on-grade conditions), traffic, anticipated flows, ability to secure the BMP properly, safety and other site-specific conditions. For example, block and rock socks will be better suited to a curb and gutter along a roadway, as opposed to silt fence or sediment control logs, which cannot be properly secured in a curb and gutter setting, but are effective area inlet protection measures.

Several inlet protection designs are provided in the Design Details. Additionally, a variety of proprietary products are available for inlet protection that may be approved for use by local governments. If proprietary products are used, design details and installation procedures from the manufacturer must be followed. Regardless of the type of inlet protection selected, inlet protection is most effective when combined with other BMPs such as curb socks and check dams. Inlet protection is often the last barrier before runoff enters the storm sewer or receiving water.

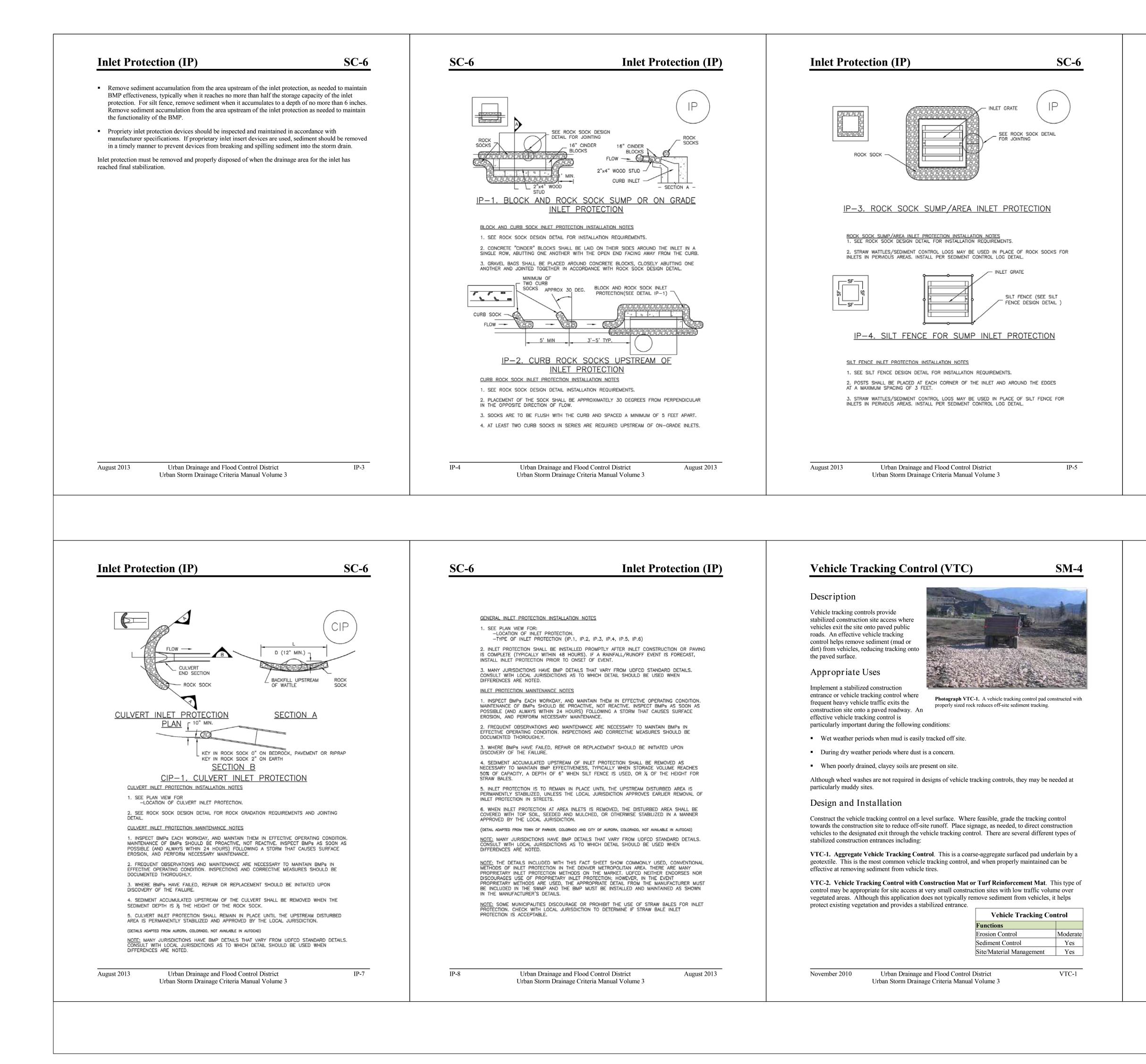
Design details with protection:	notes are provided for these forms of inlet	Inlet Protection (various forms)		
		Functions		
IP-1. Block and Ro Inlets	ock Sock Inlet Protection for Sump or On-grade	Erosion Control	No	
mets		Sediment Control	Yes	
IP-2. Curb (Rock)	Socks Upstream of Inlet Protection, On-grade	Site/Material Management	No	
Inlets				
August 2013	Urban Drainage and Flood Control Distri	ct	IP-1	
-	Urban Storm Drainage Criteria Manual Volu	ime 3		

**SC-6** 

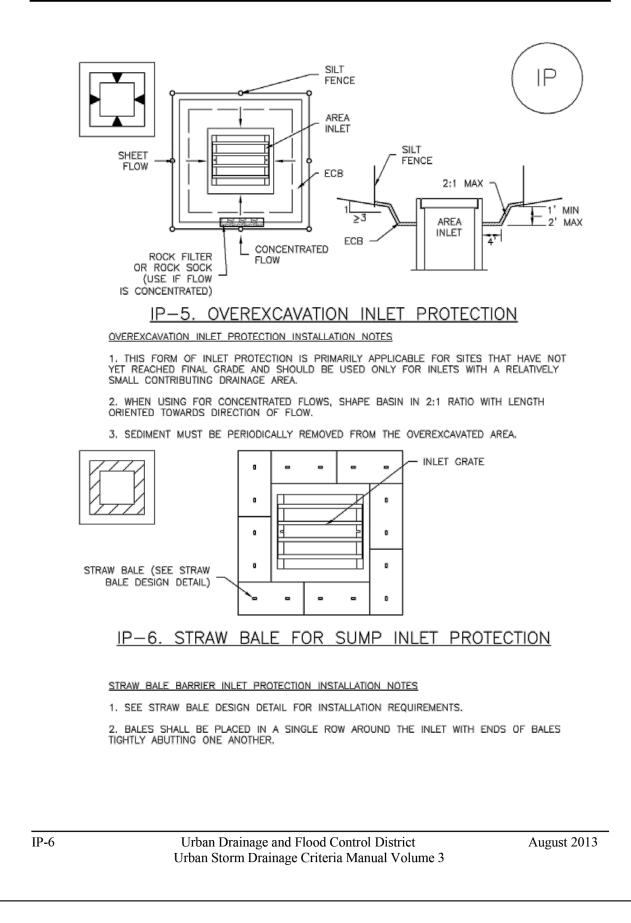


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C2.7







### **SM-4**

### Vehicle Tracking Control (VTC)

Photograph VTC-2. A vehicle tracking control pad with wheel wash

**VTC-3.** Stabilized Construction Entrance/Exit with Wheel Wash. This is an aggregate pad, similar to VTC-1, but includes equipment for tire washing. The wheel wash equipment may be as simple as hand-held power washing equipment to more advance proprietary systems. When a wheel wash is provided, it is important to direct wash water to a sediment trap prior to discharge from the site.

Vehicle tracking controls are sometimes installed in combination with a sediment trap to treat runoff.

Maintenance and Removal

Inspect the area for degradation and replace aggregate or material used for a stabilized entrance/exit as needed. If the area becomes clogged and ponds water, remove and dispose of excess sediment or replace material with a fresh layer of aggregate as necessary.

With aggregate vehicle tracking controls, ensure rock and debris from this area do not enter the public right-of-way.

Remove sediment that is tracked onto the public right of way daily or more frequently as needed. Excess sediment in the roadway indicates that the stabilized construction entrance needs maintenance.

Ensure that drainage ditches at the entrance/exit area remain clear.

A stabilized entrance should be removed only when there is no longer the potential for vehicle tracking to occur. This is typically after the site has been stabilized.

facility. Photo courtesy of Tom Gore.

When wheel wash equipment is used, be sure that the wash water is discharged to a sediment trap prior to discharge. Also inspect channels conveying the water from the wash area to the sediment trap and stabilize areas that may be eroding.

When a construction entrance/exit is removed, excess sediment from the aggregate should be removed and disposed of appropriately. The entrance should be promptly stabilized with a permanent surface following removal, typically by paving.

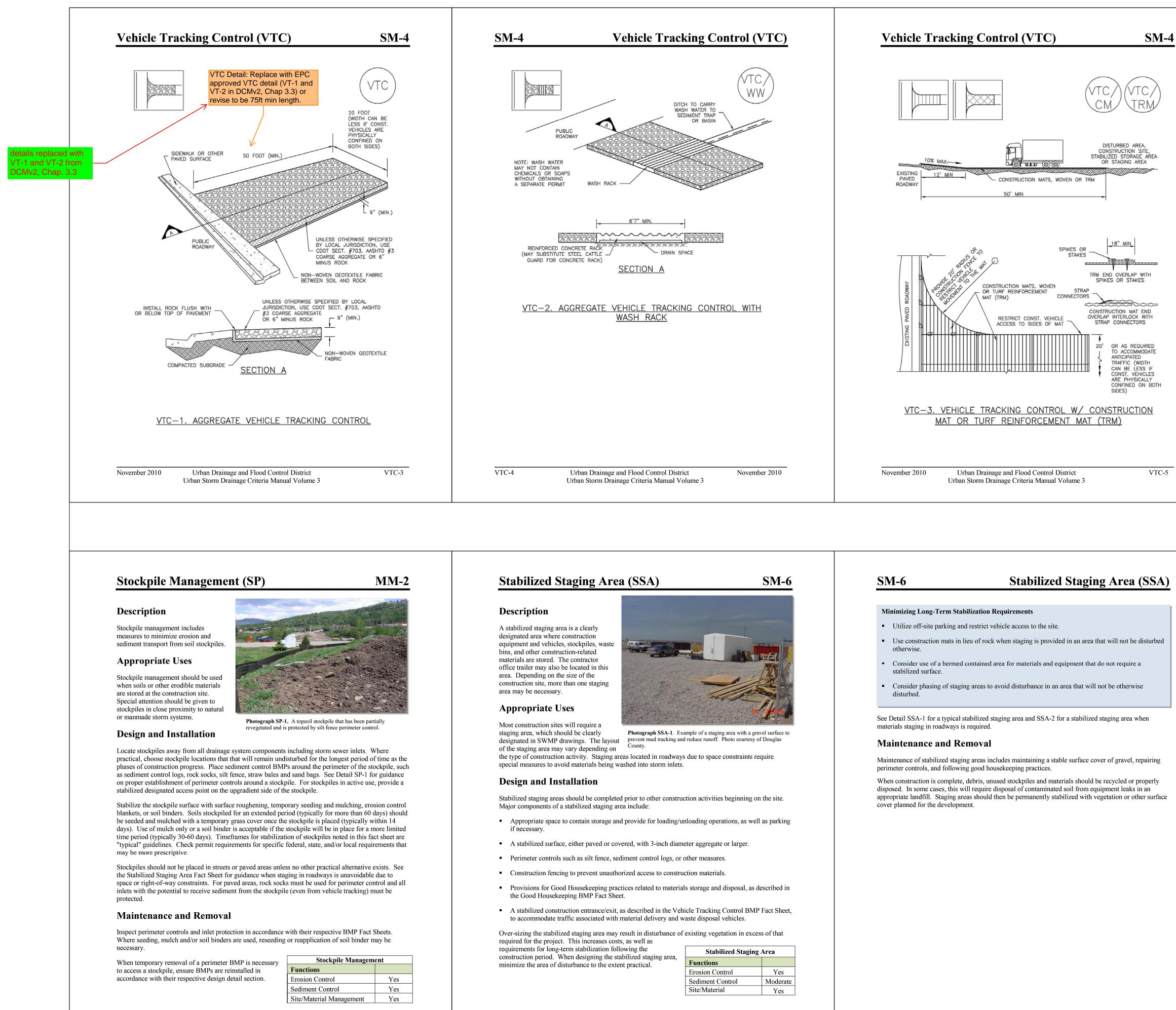


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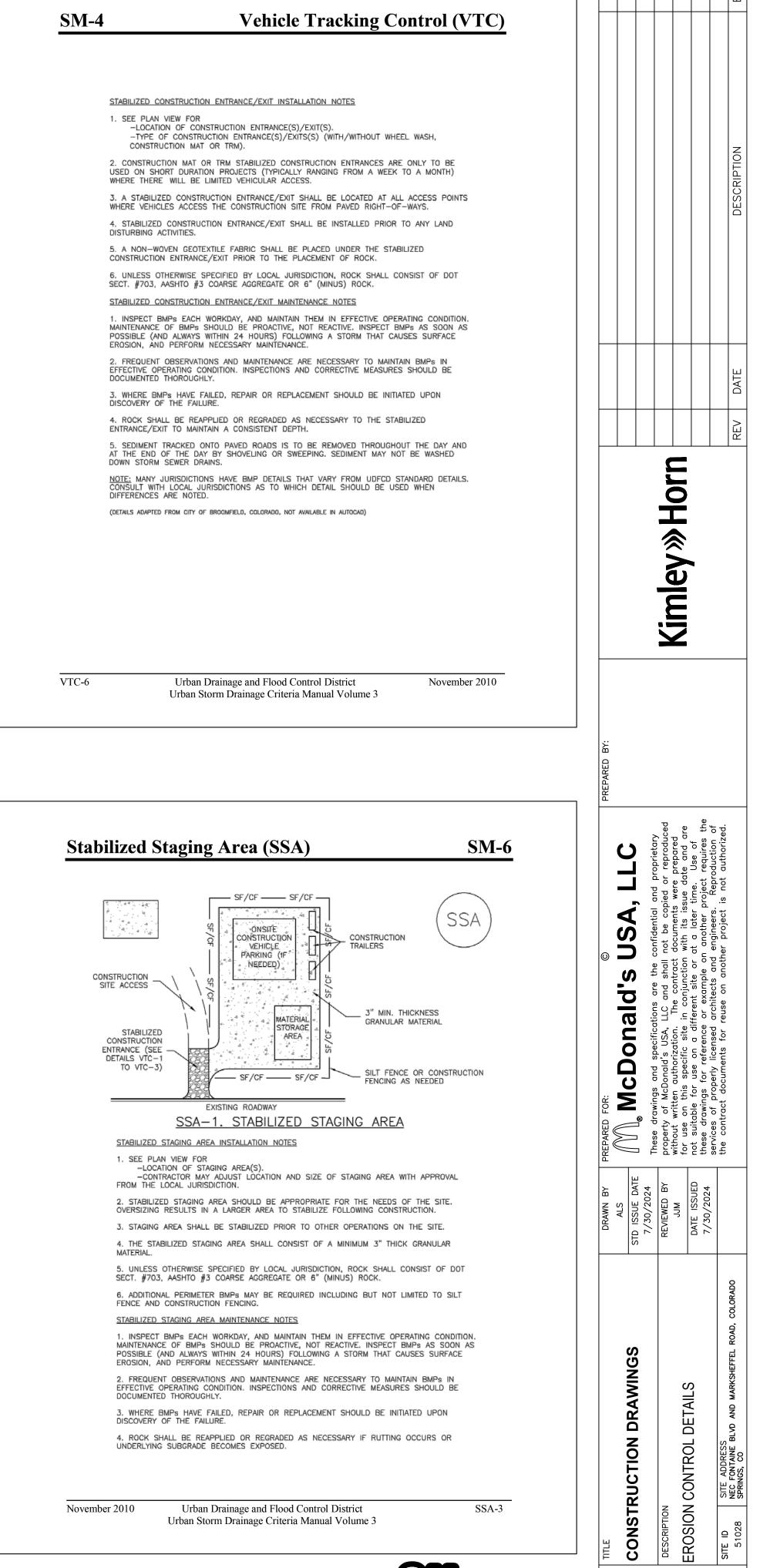
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PREPARED BY:					0			
PREPARED FOR:	M McDonald's USA. LLC		property of McDonald's USA, LLC and shall not be copied or reproduced	without written authorization. The contract documents were prepared for use on this specific site in conjunction with its issue date and are	not suitable for use on a different site or at a later time. Use of these drawings for reference or example on another project requires the	services of properly licensed architects and engineers. Reproduction of	the contract documents for reuse on another project is not authorized.	
BY	ALS STD ISSLIF DATE	7/30/2024	REVIEWED BY	MUL	DATE ISSUED	1 202 /00 / 1		
ците	CONSTRUCTION DRAWINGS		DESCRIPTION				SITE ID   SITE ADDRESS	51028 NEC FONTAINE BLVD AND MARKSHEFFEL ROAD, COLORADO



November 2010	Urban Drainage and Flood Control District	
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SP-1

November 2010 Urbaı Urban S





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C2.9

### **SM-6**

### Stabilized Staging Area (SSA)

STABILIZED STAGING AREA MAINTENANCE NOTES

5. STABILIZED STAGING AREA SHALL BE ENLARGED IF NECESSARY TO CONTAIN PARKING, STORAGE, AND UNLOADING/LOADING OPERATIONS.

6. THE STABILIZED STAGING AREA SHALL BE REMOVED AT THE END OF CONSTRUCTION. THE GRANULAR MATERIAL SHALL BE REMOVED OR, IF APPROVED BY THE LOCAL JURISDICTION, USED ON SITE, AND THE AREA COVERED WITH TOPSOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED IN A MANNER APPROVED BY LOCAL JURISDICTION. NOTE: MANY MUNICIPALITIES PROHIBIT THE USE OF RECYCLED CONCRETE AS GRANULAR MATERIAL FOR STABILIZED STAGING AREAS DUE TO DIFFICULTIES WITH RE-ESTABLISHMENT OF

VEGETATION IN AREAS WHERE RECYCLED CONCRETE WAS PLACED. NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

(DETAILS ADAPTED FROM DOUGLAS COUNTY, COLORADO, NOT AVAILABLE IN AUTOCAD)

SSA-4

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Sediment Basin (SB)

### Description

A sediment basin is a temporary pond built on a construction site to capture eroded or disturbed soil transported in storm runoff prior to discharge from the site. Sediment basins are designed to capture site runoff and slowly release it to allow time for settling of sediment prior to discharge. Sediment basins are often constructed in locations that will later be modified to serve as post-construction stormwater basins.

### Appropriate Uses

Most large construction sites (typically greater than 2 acres) will require one or more sediment basins for effective

Sediment basins should not be used as stand-alone sediment controls. Erosion and other sediment controls should also be implemented upstream. When feasible, the sediment basin should be installed in the same location where a permanent post-

### construction detention pond will be located.

### **Design and Installation**

- achieved because of site space constraints, baffling may be required to extend the effective inflow point(s) and the outlet to
- **Dam Embankment**: It is recom embankment slopes be 4:1 (H:V than 3:1 (H:V) in any location.

August 2013

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**SC-7** 

courtesy of WWE.

management of construction site runoff. On linear construction projects, sediment basins may be impractical; instead, sediment traps or other combinations of BMPs may be more appropriate.

The design procedure for a sediment basin includes these steps: • **Basin Storage Volume**: Provide a storage volume of at least 3,600 cubic feet per acre of drainage

area. To the extent practical, undisturbed and/or off-site areas should be diverted around sediment basins to prevent "clean" runoff from mixing with runoff from disturbed areas. For undisturbed areas (both on-site and off-site) that cannot be diverted around the sediment basin, provide a minimum of 500 ft<sup>3</sup>/acre of storage for undeveloped (but stable) off-site areas in addition to the 3,600 ft<sup>3</sup>/acre for disturbed areas. For stable, developed areas that cannot be diverted around the sediment basin, storage volume requirements are summarized in Table SB-1.

Basin Geometry: Design basin with a minimum length-to-width ratio of 2:1 (L:W). If this cannot be

tive distance between the o minimize short-circuiting.	Sediment Basins						
ommended that	Functions						
V) or flatter and no steeper	Erosion Control	No					
	Sediment Control	Yes					
	Site/Material Management	No					
		- 10					

SB-1

## **SC-7**

SB-4

### Sediment Basin (SB)

### Maintenance and Removal

Maintenance activities include the following:

- Dredge sediment from the basin, as needed to maintain BMP effectiveness, typically when the design storage volume is no more than one-third filled with sediment.
- Inspect the sediment basin embankments for stability and seepage.
- Inspect the inlet and outlet of the basin, repair damage, and remove debris. Remove, clean and replace the gravel around the outlet on a regular basis to remove the accumulated sediment within it and keep the outlet functioning.
- Be aware that removal of a sediment basin may require dewatering and associated permit requirements.
- Do not remove a sediment basin until the upstream area has been stabilized with vegetation.

Final disposition of the sediment basin depends on whether the basin will be converted to a permanent post-construction stormwater basin or whether the basin area will be returned to grade. For basins being converted to permanent detention basins, remove accumulated sediment and reconfigure the basin and outlet to meet the requirements of the final design for the detention facility. If the sediment basin is not to be used as a permanent detention facility, fill the excavated area with soil and stabilize with vegetation.

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### Sediment Basin (SB)

### **SC-7**

SEDIMENT BASIN MAINTENANCE NOTES 1. INSPECT BMPS EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.

 FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY. 3. WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.

4. SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN BMP EFFECTIVENESS, TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT (I.E., TWO FEET BELOW THE SPILLWAY CREST).

5. SEDIMENT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS STABILIZED AND GRASS COVER IS ACCEPTED BY THE LOCAL JURISDICTION. 6. WHEN SEDIMENT BASINS ARE REMOVED, ALL DISTURBED AREAS SHALL BE COVERED WITH TOPSOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED AS APPROVED BY LOCAL JURISDICTION.

(DETAILS ADAPTED FROM DOUGLAS COUNTY, COLORADO) NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

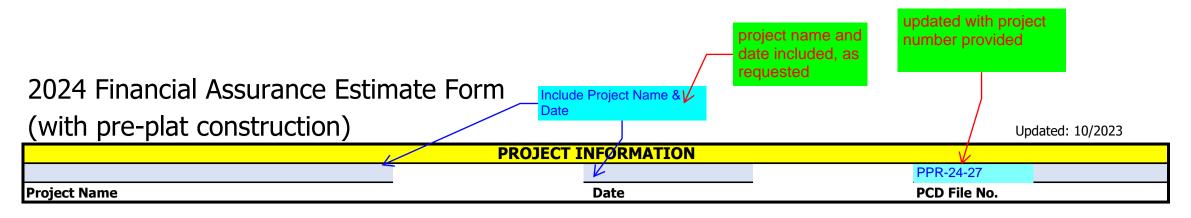
August 2013

Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 **SB-7** 



Call before you dig

			Vimburn					REV DATE	
PREPARED BY:					0				
PREPARED FOR:	McDonald's USA. LLC	These drawings and specifications are the confidential and proprietary	property of McDonald's USA, LLC and shall not be copied or reproduced	without written authorization. The contract accuments were prepared for use on this specific site in conjunction with its issue date and are	not suitable for use on a different site or at a later time. Use of these drawings for reference or example on another project requires the	services of properly licensed architects and engineers. Reproduction of	the contract documents for reuse on another project is not authorized.		
DRAWN BY PI	ALS CTD ISSUIT DATE	7/30/2024	REVIEWED BY	MUL	DATE ISSUED				
TITLE	SONSTRICTION DRAWINGS		DESCRIPTION						
		(		)	1 C	)			



				Unit				(with Pre-Plat Construction)		
Description	Quantity	Units		Cost			Total	% Complete		Remaining
<b>SECTION 1 - GRADING AND EROSION CONTRO</b>	<b>)L (Constructior</b>	and Perm	ane	ent BMPs)						
Earthwork										
less than 1,000; \$5,300 min	569.	CY	\$	8.00	=	\$	5,300.00		\$	5,300.0
1,000-5,000; \$8,000 min		CY	\$	6.00	=	\$	-		\$	-
5,001-20,000; \$30,000 min		CY	\$	5.00	=	\$	-		\$	-
20,001-50,000; \$100,000 min		CY	\$	3.50	=	\$	-		\$	-
50,001-200,000; \$175,000 min		CY	\$	2.50	=	\$	-		\$	-
greater than 200,000; \$500,000 min		CY	\$	2.00	=	\$	-		\$	-
Permanent Erosion Control Blanket		SY	\$	9.00	=	\$	-		\$	-
Permanent Seeding (inc. noxious weed mgmnt.) & Mulching	.28	AC	\$	2,018.00	=	\$	573.11		\$	573.1
Permanent Pond/BMP (provide engineer's estimate)		EA			=	\$	-		\$	-
Concrete Washout Basin	1.	EA	\$	1,172.00	=	\$	1,172.00		\$	1,172.0
Inlet Protection	7.	EA	\$	217.00	=	\$	1,519.00		\$	1,519.0
Rock Check Dam		EA	\$	651.00	=	\$	-		\$	-
Safety Fence	982.34	LF	\$	3.00	=	\$	2,947.03		\$	2,947.03
Sediment Basin		EA	\$	2,294.00	=	\$	-		\$	-
Sediment Trap		EA	\$	538.00	=	\$	-		\$	-
Silt Fence	500.55	LF	\$	3.00	=	\$	1,501.65		\$	1,501.6
Slope Drain		LF	\$	43.00		\$	_,		\$	
Straw Bale		EA	\$	33.00	=	\$	-		\$	-
Straw Wattle/Rock Sock		LF	\$	8.00	=	\$	-		\$	-
Surface Roughening		AC	\$	269.00		\$	-		\$	-
Temporary Erosion Control Blanket		SY	\$	3.00	=	\$	-		\$	-
Temporary Seeding and Mulching		AC	\$	1,793.00	=	\$	-		\$	-
Vehicle Tracking Control	1.	EA	\$		=	\$	3,085.00		\$	3,085.0
		=, ,	Ť	0,000.00	=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
	NTENANCE (35%	of Constr	ucti	on BMPs)	=	\$	3,168.44		\$	3,168.4
- Subject to defect warranty financial assurance. A minimum of 20% shall	(			<b>,</b>		Ŧ			т	
e retained until final acceptance (MAXIMUM OF 80% COMPLETE		Sectio	տ 1	Subtotal	=	\$	19,266.24		\$	19,266.24
LLOWED) SECTION 2 - PUBLIC IMPROVEMENTS *										
ROADWAY IMPROVEMENTS										
Construction Traffic Control										
		LS			=	\$	-		\$	
Addredate Base Course (135 lbs/ct)		LS Tons	Ś	37.00	=	\$	-		\$	-
Aggregate Base Course     (135 lbs/cf)       Aggregate Base Course     (135 lbs/cf)		Tons	\$	37.00 66.00	=	\$	- - -		\$ \$ \$	-
Aggregate Base Course (135 lbs/cf)		Tons CY	\$ \$ \$	66.00		\$ \$ \$	- - - -		\$ \$ \$	
Aggregate Base Course       (135 lbs/cf)         Asphalt Pavement (3" thick)       (135 lbs/cf)		Tons CY SY		66.00 18.00		\$ \$ \$ \$	- - - - -		\$ \$ \$ \$	-
Aggregate Base Course(135 lbs/cf)Asphalt Pavement (3" thick)Asphalt Pavement (4" thick)		Tons CY SY SY		66.00 18.00 25.00		\$ \$ \$ \$ \$	- - - - - -		\$ \$ \$ \$ \$	-
Aggregate Base Course(135 lbs/cf)Asphalt Pavement (3" thick)Asphalt Pavement (4" thick)Asphalt Pavement (6" thick)		Tons CY SY SY SY		66.00 18.00 25.00 38.00	=	\$ \$ \$ \$ \$ \$	- - - - - - -		\$ \$ \$ \$ \$ \$ \$	-
Aggregate Base Course       (135 lbs/cf)         Asphalt Pavement (3" thick)         Asphalt Pavement (4" thick)         Asphalt Pavement (6" thick)         Asphalt Pavement         (147 lbs/cf)		Tons CY SY SY SY Tons		66.00 18.00 25.00 38.00 114.00	=	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
Aggregate Base Course(135 lbs/cf)Asphalt Pavement (3" thick)Asphalt Pavement (4" thick)Asphalt Pavement (6" thick)Asphalt Pavement (6" thick)Asphalt Pavement(147 lbs/cf) thickRaised Median, Paved		Tons CY SY SY SY Tons SF		66.00 18.00 25.00 38.00 114.00 11.00	=	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign		Tons CY SY SY SY Tons SF EA		66.00 18.00 25.00 38.00 114.00	=	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - -
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign		Tons CY SY SY SY Tons SF EA EA	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	66.00 18.00 25.00 38.00 114.00 11.00 392.00	=	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking		Tons CY SY SY SY Tons SF EA EA EA	<ul> <li>\$</li> <li>\$&lt;</li></ul>	66.00 18.00 25.00 38.00 114.00 11.00 392.00 17.00	= = = = = = =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking		Tons CY SY SY Tons SF EA EA EA SF SF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	66.00 18.00 25.00 38.00 114.00 11.00 392.00 17.00 30.00	=	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - -
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3		Tons CY SY SY Tons SF EA EA SF SF EA	<ul> <li>\$</li> <li>\$&lt;</li></ul>	66.00 18.00 25.00 38.00 114.00 392.00 17.00 30.00 259.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I		Tons CY SY SY Tons SF EA EA SF SF EA EA EA	<ul> <li>\$</li> <li>\$&lt;</li></ul>	66.00         18.00         25.00         38.00         114.00         392.00         17.00         30.00         259.00         31.00		\$       \$         \$	- - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - -
Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3		Tons CY SY SY Tons SF EA EA SF SF EA	<ul> <li>\$</li> <li>\$&lt;</li></ul>	66.00 18.00 25.00 38.00 114.00 392.00 17.00 30.00 259.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- - - - - - - - - - - - -

Curb and Gutter, Type C (Ramp)	LF	\$ 38.00	=	\$ -	\$	- '
4" Sidewalk (common areas only)	SY	\$ 62.00	=	\$ -	\$.	- ,
5" Sidewalk	SY	\$ 77.00	=	\$ -	\$.	- ,
6" Sidewalk	SY	\$ 94.00	=	\$ -	\$	- ,
8" Sidewalk	SY	\$ 125.00		\$ -	\$	- ''
Pedestrian Ramp	EA	\$ 1,496.00	=	\$ -	\$	- ,
Cross Pan, local (8" thick, 6' wide to include return)	LF	\$ 79.00	=	\$ -	\$	- ,
Cross Pan, collector (9" thick, 8' wide to include return)	LF	\$ 119.00		\$ -	\$.	- ''
Curb Opening with Drainage Chase	EA	\$ 1,926.00	=	\$ -	\$	- ,
Guardrail Type 3 (W-Beam)	LF	\$ 65.00	=	\$ -	\$.	- ''
Guardrail Type 7 (Concrete)	LF	\$ 94.00	=	\$ -	\$.	
Guardrail End Anchorage	EA	\$ 2,731.00	=	\$ -	\$	- ''
Guardrail Impact Attenuator	EA	\$ 4,902.00	=	\$ -	\$	- ,
Sound Barrier Fence (CMU block, 6' high)	LF	\$ 102.00		\$ -	\$	- ,
Sound Barrier Fence (panels, 6' high)	LF	\$ 104.00	=	\$ -	\$	- ,
Electrical Conduit, Size =	LF	\$ 22.00	=	\$ -	\$.	- 2
Traffic Signal, (provide engineer's estimate)	EA		=	\$ -	\$.	- >

PROJECT INFORMATION										
Project Name		Date		PCD File No.						

			Unit			•	-Plat Construction)
Description	Quantity	Units	Cost		Total	% Complete	Remaining
				=	\$ -		\$-
[insert items not listed but part of construction plans]				=	\$-		\$ -
STORM DRAIN IMPROVEMENTS							
Concrete Box Culvert (M Standard), Size (W x H)		LF		=			\$-
18" Reinforced Concrete Pipe		LF	\$ 82.00	=	\$-		\$
24" Reinforced Concrete Pipe		LF	\$ 98.00	=	\$ -		\$-
30" Reinforced Concrete Pipe		LF	\$ 123.00	=	\$-		\$-
36" Reinforced Concrete Pipe		LF	\$ 151.00	=	\$-		\$-
42" Reinforced Concrete Pipe		LF	\$ 201.00	=	\$ -		\$-
48" Reinforced Concrete Pipe		LF	\$ 245.00	=	\$ -		\$
54" Reinforced Concrete Pipe		LF	\$ 320.00	=	\$ -		\$-
60" Reinforced Concrete Pipe		LF	\$ 374.00	=	\$-		\$
66" Reinforced Concrete Pipe		LF	\$ 433.00	=	\$ -		\$-
72" Reinforced Concrete Pipe		LF	\$ 495.00	=	\$-		\$
18" Corrugated Steel Pipe		LF	\$ 105.00	=	\$ -		\$-
24" Corrugated Steel Pipe		LF	\$ 121.00	=	\$-		\$
30" Corrugated Steel Pipe		LF	\$ 154.00	=	\$ -		\$
36" Corrugated Steel Pipe		LF	\$ 184.00	=	\$ -		\$
42" Corrugated Steel Pipe		LF	\$ 212.00	=	\$ -		\$ -
48" Corrugated Steel Pipe		LF	\$ 223.00	=	\$ -		\$-
54" Corrugated Steel Pipe		LF	\$ 327.00	=	\$ -		\$-
60" Corrugated Steel Pipe		LF	\$ 353.00	=	\$ -		\$-
66" Corrugated Steel Pipe		LF	\$ 427.00	=	\$ -		\$-
72" Corrugated Steel Pipe		LF	\$ 502.00	=	\$ -		\$ -
78" Corrugated Steel Pipe		LF	\$ 578.00	=	\$ -		\$ -
84" Corrugated Steel Pipe		LF	\$ 691.00	=	\$ -		\$
Flared End Section (FES) RCP Size =							т ф
(unit cost = 6x pipe unit cost)		EA		=	\$ -		\$
Flared End Section (FES) CSP Size =		<b>F</b> A		=	\$ -		\$
(unit cost = 6x pipe unit cost)		EA					т _
End Treatment- Headwall		EA		=	\$-		\$-
End Treatment- Wingwall		EA		=	\$ -		\$
End Treatment - Cutoff Wall		EA	<b>. . . . . . . . . .</b>	=	\$ -		\$ -
Curb Inlet (Type R) L=5', Depth < 5'		EA	\$ 7,212.00	=	\$ -		\$ -
Curb Inlet (Type R) L=5', 5' ≤ Depth < 10'		EA	\$ 9,377.00	=	<b>\$</b> -		\$ -
Curb Inlet (Type R) L =5', 10' ≤ Depth < 15'		EA	\$ 10,859.00	=	\$ -		\$ ·
Curb Inlet (Type R) L =10', Depth $< 5'$		EA	\$ 9,925.00	=	\$ -		\$-
Curb Inlet (Type R) L =10', 5' ≤ Depth < 10'		EA	\$ 10,230.00	=	<b>\$</b> -		<b>\$</b> -
Curb Inlet (Type R) L =10', 10' ≤ Depth < 15'		EA	\$ 12,805.00	=	<b>\$</b> -		<b>\$</b> -
Curb Inlet (Type R) L =15', Depth < 5'		EA	\$ 12,907.00	=	<b>\$</b> -		\$-
Curb Inlet (Type R) L =15', $5' \le \text{Depth} < 10'$		EA	\$ 13,835.00	=	<b>\$</b> -		\$-
Curb Inlet (Type R) L =15', $10' \leq \text{Depth} < 15'$		EA	\$ 15,130.00	=	\$-		\$-
Curb Inlet (Type R) L =20', $Depth < 5'$		EA	\$ 13,755.00	=	\$-		\$-
Curb Inlet (Type R) L =20', $5' \leq \text{Depth} < 10'$		EA	\$ 15,181.00	=	\$-		\$-
Grated Inlet (Type C), Depth < 5'		EA	\$ 6,037.00	=	\$-		\$
Grated Inlet (Type D), Depth < 5'		EA	\$ 7,458.00	=	\$-		\$
Storm Sewer Manhole, Box Base		EA	\$ 15,130.00	=	\$ -		\$
Storm Sewer Manhole, Slab Base		EA	\$ 8,322.00	=	\$-		\$
Geotextile (Erosion Control)		SY	\$ 9.00	=	\$ -		\$
Rip Rap, d50 size from 6" to 24"		Tons	\$ 104.00	=	\$-		\$
Rip Rap, Grouted		Tons	\$ 124.00	=	\$-		\$
Drainage Channel Construction, Size (W x H)		LF		=	\$ -		\$
Drainage Channel Lining, Concrete		CY	\$ 741.00	=	\$ -		\$
Drainage Channel Lining, Rip Rap		CY	\$ 145.00	=	\$ -		\$

* - Subject to defect warranty financial assurance. A minimum of 20% shall be retained until final acceptance (MAXIMUM OF 80% COMPLETE ALLOWED)	Section	a 2 Subtotal	=	\$	-	\$	-	
[insert items not listed but part of construction plans]			=	\$	-	\$	-	
			=	\$	-	\$	-	
Drainage Channel Lining, Other Stabilization			=	\$	-	\$	-	*
Brainage Gharmer Eining, Grass	7.0	φ 1,511.00	—	Ψ		Ψ		

PROJECT INFORMATION									
Project Name	Date		P	CD File No.					

				Unit			(with Pre	-Plat Construction)
Description	Quantity	Units		Cost		Total	% Complete	Remaining
<b>SECTION 3 - COMMON DEVELOPMENT IMPRO</b>	VEMENTS (Pr	ivate or Di	stri	ict and N	<b>OT Maint</b>	ained by EPC)**		
ROADWAY IMPROVEMENTS								
This section should include any					=	\$-		\$-
road and storm water facilities					=	\$-		\$-
which are being built for the overall Disregard					=	\$-		\$-
common development, such as the comment shared access along the west					=	\$-		\$-
property line.					=	\$-		\$-
					=	\$-		\$-
STORM DRAIN IMPROVEMENTS (Exception	on: Permanent Por	nd/BMP shall b	be ite	emized unde	er Section 1)			
					=	\$-		\$-
					=	\$-		\$-
					=	\$-		\$-
					=	\$-		\$-
					=	\$-		\$-
					=	\$-		\$-
WATER SYSTEM IMPROVEMENTS								
Water Main Pipe (PVC), Size 8"		LF	\$	84.00	=	\$-		\$-
Water Main Pipe (Ductile Iron), Size 8"		LF	\$	98.00	=	\$-		\$-
Gate Valves, 8"		EA	\$	2,418.00	=	\$-		\$-
Fire Hydrant Assembly, w/ all valves		EA	\$	8,584.00	=	\$-		\$-
Water Service Line Installation, inc. tap and valves		EA	\$	1,723.00	=	\$-		\$-
Fire Cistern Installation, complete		EA			=	\$-		\$-
					=	\$-		\$-
[insert items not listed but part of construction plans]					=	\$-		\$-
SANITARY SEWER IMPROVEMENTS								
Sewer Main Pipe (PVC), Size 8"		LF	\$	84.00	=	\$-		\$-
Sanitary Sewer Manhole, Depth < 15 feet		EA	\$	5,708.00	=	\$-		\$-
Sanitary Service Line Installation, complete		EA	\$	1,825.00	=	\$-		\$-
Sanitary Sewer Lift Station, complete		EA			=	\$-		\$-
					=	\$-		\$-
[insert items not listed but part of construction plans]					=	\$-		\$-
LANDSCAPING IMPROVEMENTS (I	For subdivision spe		of a	approval, or	PUD)			
		EA			=	\$-		\$-
		EA			=	\$-		\$-
		EA			=	\$-		\$-
		EA			=	\$-		\$-
		EA			=	\$-		\$-
** - Section 3 is not subject to defect warranty requirements		Sectio	า 3	Subtotal	=	\$		\$-

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		PROJECT 1	INFORMATI	ON				
Project Name			Date				PCD File No.	
Description	Quantity	Units	Unit Cost			Total	(with Pre- % Complete	onstruction) Remaining
AS-BUILT PLANS (Public Improveme	ents inc. Permanent WQCV BMPs)			=	\$	-	:	\$ -
POND/BMP CERTIFICATION (inc. elevations and volume calculations)		LS		=	\$	-	:	\$ -
			(Sum of all se			<b>iction Financia</b> -builts and pond/Bl		\$ 19,266.24
		•			-	vith Pre-Plat C -builts and pond/Bl	·	\$ <u>19,266.2</u> 4
				Total D	efect War	ranty Financia	I Assurance	\$ 1,174.6
	(2	20% of all item	is identified as (	*). To be co	ollateralized	at time of prelimin	ary acceptance)	

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McDonald's at Fontaine and Marksheffel Village at Lorson Ranch Filing No. 1, Lot 2 El Paso County, CO

Prepared for:

McDonald's USA, LLC. 110 North Carpenter Street Chicago, IL 60607-2101 (206) 348-4374 Contact: Robert Yagusesky

Prepared by:

Kimley-Horn and Associates, Inc. 2 North Nevada Avenue, Suite 900 Colorado Springs, Colorado 80903 (719) 284-7275 Contact: Jessica McCallum, P.E.

Project #: 096806032

Prepared: July 30, 2024

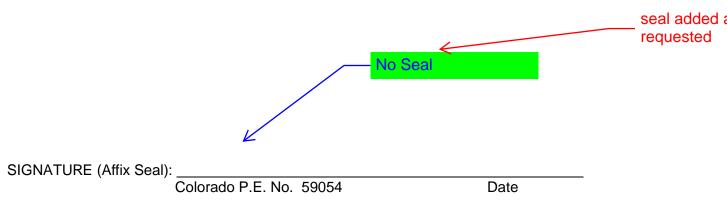




#### CERTIFICATION

#### ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



### DEVELOPER'S STATEMENT

I, McDonald's USA, LLC, the developer has read and will comply with all of the requirements specified in this drainage report and plan.

Business Name

Authorized Signature

Date

Printed Name

Title

Address:

### EL PASO COUNTY

Filed in accordance with Section 51.1 of the El Paso Land Development Code as amended.

Director of Public Works

Date

Conditions:

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Please Segment Appendices (A, B, C etc). Update TOC.

table of update

### INTRODUCTION

### PURPOSE AND SCOPE OF STUDY

The purpose of this report is to outline the Final Drainage Report for Lot 2 of the Village at Lorson Ranch Filing No. 1 subdivision, located near the northeast corner of Marksheffel Road and Fontaine Boulevard (the "Property"), El Paso County, Colorado (the "County"). This Final Drainage Report identifies on-site and offsite drainage patterns, storm sewer and inlet locations, and areas tributary to the site and proposes to safely route developed storm water to adequate outfalls. The Property is approximately 1.263 acres in size.

The Property is located within the Jimmy Camp Creek Drainage Basin and is part of the subject area of the *Final Drainage Plan for Village at Lorson Ranch* dated June 2024, prepared by Core Engineering Group, LLC (the "FDP"). The FDP is in conformance with the *Lorson Ranch MDDP1* by Pentacor Engineering (approved November 7, 2006) and *Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1* (approved September 7, 2017).

### GENERAL PROJECT DESCRIPTION

The proposed improvements consist of the construction of an approximately 3,694-gross square-foot McDonald's, fast-food restaurant building with a dual drive-thru, parking lot, and landscaping (the "Project") within the Property (the "Site"). The Project will be processed through El Paso County. Additional outside agency review or processing is not anticipated as part of the Project.

The Project is located within a portion of the south half of the southeast quarter of Section 15, Township 15 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, County of El Paso, State of Colorado (see Vicinity Map). The Property is bounded by Lot 1 of Village at Lorson Ranch Filing No. 1 to the west, private road and Lot 6 of Village at Lorson Ranch Filing No. 1 to the north, Lot 3 of Village at Lorson Ranch Filing No. 1 to the east, and Fontaine Boulevard to the south. The Property is currently undeveloped and native vegetation (grass with no shrubs). The Property generally slopes from northwest to southeast with the existing stormwater outfall being the existing 34"x53" HERCP south of the Site, routing flow under existing Fontaine Boulevard. Per the FDP, the anticipated ultimate outfall for this Property is the existing Pond G1/G2 south of the Site, ultimately tributary to Jimmy Camp Creek.

An ALTA and topographic field survey were completed for the Project by Kimley-Horn and Associates, Inc. dated September 6, 2024 and is the basis for design for the drainage improvements in conjunction with the Master Development design documents.



VICINITY MAP NOT TO SCALE

and accompanying infrastructure

### **PROJECT CHARACTERISTICS**

The Project Site is 1.263 acres in size. The Project involves the construction of an approximately 3,694 square foot McDonald's eating restaurant with a dual drive-thru.

The proposed building, parking lot, paved drives, and other impervious surfaces comprise 74.8 percent (55,034 square feet) of the overall Project Site. Landscape areas internal and on the perimeter of the site consist of landscape islands within the parking lot, and landscape zones adjacent to the building and landscape setback areas. The proposed internal landscaping areas make up 24.5 percent (13,486 square feet) of the Project Site.

Generally, the existing site slopes approximately 1-3% from the northwest to the southeast. This historic runoff pattern will generally be maintained and unaffected with the proposed Project.

There are no major irrigation facilities within the Site. The Project does not provide on-site water quality or detention for the Project area, but per the FDP, existing offsite full spectrum detention pond, Pond G1/G2 (the "EDB"), provides water quality and detention for the Site. The existing land use is undeveloped vacant land. The proposed land use is a fast food restaurant with drive-thru.



### SOILS CONDITIONS

NRCS soil data is available for this Site (see Appendix) and the onsite soils are USCS Hydrologic Soil Group C. Group C soils have a slow infiltration rate and possess a slow rate of water transmission. This site specifically is predominately comprised of Manzanst clay loam.

### DRAINAGE DESIGN CRITERIA

### REGULATIONS

water

The proposed development does not propose any deviations from the Drainage Criteria Manual County of El Paso, Colorado, dated October 31, 2018.

#### DEVELOPMENT DESIGN CRITERIA REFERENCE AND CONSTRAINTS

constraints such as

The proposed storm facilities follow the Drainage Criteria Manual County of El Paso, Colorado (the "CRITERIA"), El Paso County Engineering Criteria Manual (the "ECM"), and the Urban Storm Drainage Criteria Manual (the "MANUAL"). Site drainage is not significantly impacted by such constraints as utilities or existing development. Further detail regarding onsite drainage patterns is provided in the Proposed Drainage Conditions Section.

### HYDROLOGIC CRITERIA

updated to include language from comment

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per Section 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site basin. The 100-year detention and water quality capture volume are provided in the EDB. Based upon this approach, we feel that the drainage design provided for the Site is conservative and in keeping with the zoning and historic drainage concept for the area.

### HYDRAULIC CRITERIA

The proposed drainage facilities are designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using FIRM panels by FEMA and information provided in the CRITERIA. Results of the hydraulic calculations are summarized in the Appendix.

### VARIANCES FROM CRITERIA

Due to existing grades and to match the historical flows presented at the Site, some drainage will be directed back to the County ROW. This is an existing condition. Besides this condition, no variances from the CRITERIA have been proposed for this development.

This paragraph is - confusing. Please clarify. updated to language to "Appendix C"

**Kimley**»Horn

Which one?



#### **EXISTING DRAINAGE CONDITIONS**

#### EXISTING DRAINAGE BASIN

The FDP defines 14 basins on the developed conditions drainage map. The Project lies within sub-basins PR3, PR4, PR5, and PR6. The sub-basins have 5-year and 100-year runoff coefficients of 0.83 and 0.90, respectively. The runoff for all sub-basins flows south towards the master developer-proposed 34"x53" HERCP. This historic surface runoff pattern will generally be maintained with the proposed Project. Per the FDP, the ultimate discharge from the Site is the master developer-proposed 34"x53" HERCP south of the Site.

#### MAJOR DRAINAGE BASIN DESCRIPTION

The Project is within the Jimmy Camp Creek Drainage Basin. The major drainage basin is mostly undeveloped land. Drainage facilities downstream of this Project are to be constructed per the master development. There are no known major irrigation facilities within 100 feet of the property.

The proposed drainage facilities for the Project are designed to generally follow the historic flow patterns of the Property as well as the intent of the original storm water design for the overall development. Please refer to the FDP for a full discussion of the original design for the subdivision. Applicable portions of the FDP are included in the Appendix for reference.

As documented within the FDP, this proposed Project lies within sub-basins PR3, PR4, PR5, and PR6. Drainage within sub-basin PR3 on the north side of the Site was designed to flow east to an inlet within the private drive. Drainage within sub-basin PR4 in the southwest corner of the Site was designed to flow southwest to an inlet within the drive aisle. Drainage within sub-basin PR5 on the west and south sides of the Site was designed to flow southeast to an inlet within the drive aisle. Drainage within sub-basin PR6, the majority of the site, on the north and east sides of the Site was designed to flow southwest to an inlet within the shared drive aisle. All sub-basins ultimately discharge to the master developer-proposed 34"x53" HERCP south of the Site which outfalls to the existing EDB south of the Site. The FDP states that both water quality capture volume ("WQCV") and 100-year detention would be provided within the EDB.

FDP Sub-Basin	Sub-Basin Area (acres)	FDP Develop (Entire Sub-E		DP Description	Ultimate Outfall
		5-year (CFS)	100-year (CFS)	-	
PR3	0.11	0.50	0.90	5' Type R, SUMP	Existing EDB
PR4	1.68	7.20	13.1	10' Type R on- grade curb inlet	Existing EDB
PR5	0.39	1.70	3.00	5' Type R, SUMP	Existing EDB
PR6	0.72	3.10	5.60	10' Type R on- grade curb inlet	Existing EDB

#### Table 1: Developed Drainage Conditions per the FDP

#### **PROPOSED DRAINAGE CONDITIONS**

The developed runoff from the Project will generally be collected by means of private roof drains and storm sewer inlets located in the paved driveways within each delineated basin area. The runoff collected from each basin and the roof system of the proposed building will be conveyed to the private storm sewer system and outfall to the master developer-proposed 34"x53" HERCP south of the Project. The master developer-proposed 34"x53" HERCP ultimately outfalls to the EDB south of the project. The storm sewer infrastructure connecting to the master developer-proposed 34"x53" HERCP is anticipated to be constructed in fourth quarter of 2024 or first quarter of 2025. The ultimate outfall per the FDP is to the EDB south of the Site and Jimmy Camp Creek.

The Property has been divided into 8 sub-basins, A1-A3, R1, EX1A, EX4, EX5, and OS1. The runoff generated on the building roof area, sub-basin R1, is collected and conveyed via a private roof drain system which outfalls to the master developer-proposed private storm sewer. Sub-basins A1-A3 are all internal areas within the parking lot, sidewalk, and landscaping areas. Sub-basins A1-A3 drain to inlets within the parking lot and drive aisles and are routed to the private storm sewer system. Sub-basin EX1A consists mostly of master development proposed private road and sidewalk and drains to master developer-proposed inlet within the private road. Sub-basins EX4 and EX5 consist of site area but drain to master developer-proposed inlets on-site that were sized to accommodate site flows. Sub-basin OS1 consists of landscape area that drains to the Fontaine Boulevard public right-of-way. A proposed conditions map is provided in the Appendix. No offsite flow will affect the site under proposed conditions.

	SUMM	ARY - PRO	POSED RUNC	OFF TABLE	
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)*	DIRECT 100- YR RUNOFF (CFS)	BASIN IMP. (%)
A1	A1	0.38	1.28	2.50	73.9%
A2	A2	0.15	0.65	1.19	91.9%
A3	A3	0.03	0.15	0.27	98.8%
R1	R1	0.09	0.32	0.68	90.0%
EX1A	EX1A	0.08	0.36	0.66	94.1%
EX4	EX4	0.09	0.39	0.71	94.6%
EX5	EX5	0.30	1.15	2.19	80.3%
OS1	OS1	0.15	0.16	0.58	12.1%

Table 2: Peak Stormwater Runoff Calculation Summary

DESIGN POINT (DP)/BASIN	CONVEYANCE TO DP	DP OUTFALL	OUTFALL DESCRIPTION <sup>(1)</sup>	OUTFALL CONDITION	ULTIMATE OUTFALL	TREATMENT METHOD
A1	SHEET FLOW/ C&G	STRC A1	5' CDOT TYPE R	IN SUMP	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
A2	SHEET FLOW/ C&G	STRC A2	COMBINATION DEN. NO. 13 GRATE INLET	IN SUMP	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
A3	SHEET FLOW/ C&G	STRC A3	COMBINATION DEN. NO. 13 GRATE INLET	ON GRADE	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
R1	ROOF DRAIN	R1	6" PVC ROOF DRAIN TO EX. 24" RCP		EXISTING EDB, JIMMY CAMP CREEK	EXISTING PONDS G1/G2
EX1A	SHEET FLOW/ C&G	STRC EX1A	EX. 5' CDOT TYPE R	IN SUMP	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
EX4	SHEET FLOW/ C&G	STRC EX4	EX. 10' CDOT TYPE R	ON GRADE	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
EX5	SHEET FLOW/ C&G	STRC EX5	EX. 5' CDOT TYPE R	IN SUMP	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2
OS1	SHEET FLOW	FONTAINE BLVD ROW	EX. 25' CDOT TYPE R	IN SUMP	EXISTING EDB, JIMMY CAMP CREEK	EXISTING POND G1/G2

Table 3: Proposed Sub-basin Outfall Descriptions

#### EMERGENCY OVERFLOW ROUTING

Emergency overflow routing for onsite clogged inlets is from northwest to southeast towards the existing 25' Type R sump inlet within the Fontaine Blvd ROW.

#### MAJOR DRAINAGEWAYS

There are no major drainageways on site or near the site.

#### HYDRAULIC ANALYSIS METHODOLOGY

The proposed drainage facilities will be designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using FIRM panels by FEMA and information provided in the CRITERIA. Hydraulic calculations were computed using STORMCAD, which makes use of the Standard Step method to compute the hydraulic profile. Results of the hydraulic calculations are provided in the Appendix. There will be no additional provisions selected or deviations from the CRITERIA.

Inlet capacity calculations are provided in the Appendix for the calculated 5-year and 100-year flows routed to the Type R curb inlets and private area drains on site. The capacity of each inlet is adequate for the 100 year developed flows for each sub-basin.

#### **Storm Sewer Requirements**

Proposed pipe sizes are 18" RCP.

#### DETENTION AND WATER QUALITY REQUIREMENTS

Detention and water quality for the proposed major and minor events is provided within the existing extended full spectrum detention Pond G1/G2. This pond was constructed with Carriage Meadows South at Lorson Ranch Filing No. 1 subdivision.

Pond G1/G2 provides 2.301 acre feet of water quality storage and 12.881 acre feet of storage for the 100-year event. The outlet structure was designed to release the WQCV in at least 40 hours per County requirements.

#### Four-Step Process

Please include the EURV Capacity as well.

The four-step process per the CRITERIA provides guidance and requirements for the selection of siting of structural Best Management Practices (BMPs) for new development and significant redevelopment.

#### Step 1: Employ Runoff Reduction Practices

Currently the site is vacant land. Development of the site will increase current runoff conditions due to the site being vacant. However, implementation of landscaping throughout the site and the proposed storm sewer infrastructure will help slow runoff and encourage infiltration.

#### Step 2: Stabilize Drainageways

Jimmy Camp Creek is the adjacent drainageway to the development. Jimmy Camp Creek was reconstructed and stabilized in 2006.

#### Step 3: Provide Water Quality Capture Volume (WQCV)

The water quality capture volume will be provided by the regional detention Pond G1/G2.



#### Step 4: Consider Need for Industrial and Commercial BMPs

Erosion control BMPs for both the initial and final stages of the Project were designed to reduce contamination. Source control BMPs will include the use of vehicle tracking control, inlet protection, silt fences, concrete washout areas, stockpile management, and stabilized staging areas. The Grading and Erosion Control Plans will be submitted as a separate construction document set. There are no Covering of Storage/Handling Areas or Spill Containment and Control BMP's anticipated with this development.

#### **EROSION CONTROL PLAN**

Erosion Control Plans will be submitted separately as a standalone construction document.

#### FLOODPLAIN STATEMENT

The Flood Insurance Rate Maps (FIRM) 08041C0543G effective date December 7, 2018, by FEMA, indicates that the Site is located in Zone X (outside of the 500-year flood plain). This panel is included in the Appendix.

#### COMPLIANCE WITH FDP

The FDP provides final drainage calculations for the Village at Lorson Ranch master development. This report shows compliance with the FDP. From the FDP Report, this is from 3a,

Sub-Basins PR3, PR5, and PR6 in the FDP have assumed 5-year runoff coefficient of 0.90. The proposed Project has a 5-year runoff coefficient of 0.71 and a 100-year runoff coefficient of 0.83. The 5-year and 100-year runoff events from the FDP for Sub-Basins PR3-PR6 total to 12.5 and 22.8 cfs, respectively. The proposed 5-year and 100-year runoff events calculated by this report are 4.30 and 8.2 cfs, respectively. Therefore, the proposed Project Site is generally in compliance with the FDF

The proposed Project Site drainage basins are captured by a private storm sewer network and routed to the existing full spectrum extended detention Pond G1'G2. Therefore, the proposed Project Site is in general compliance with the FDP.

Reference Appendix for applicable FDP sections.

#### FEES DEVELOPMENT

### DRAINAGE AND BRIDGE FEES

Lorson Ranch initiated the closure of Jimmy Camp Creek drainage basin for drainage/bridge fees and is awaiting a recorded closure agreement with El Paso County. There is an interim agreement with El Paso County that no fees are required at this time. Therefore, not drainage and bridge fees are required for this Project.

these flow rates came

from (basins).

### PRIVATE DRAINAGE FACILITY COST (NON-REIMBURSABLE)

Fee	QUANTITY	UNIT	\$/UNIT	Fee Total
18" RCP	160	LF	82.00	\$13,120
5' CDOT TYPE R	6	EA	7,212.00	\$43,272
TOTAL				\$56,392

.ine do drainage map.

#### **GROUNDWATER CONSIDERATIONS**

Per the Geotechnical Engineering Report prepared by Universal Engineering Sciences (UES), Inc on August 18, 2023 for McDonald's, groundwater was encountered within the top three feet of one boring at the time of field exploration. However, seasonal fluctuations in groundwater elevations and above average precipitation levels prior to the collection of boring samples may have influenced groundwater levels. Therefore, the shallow spread footing foundation and shallow excavations proposed for the Project are not anticipated to be affected by groundwater.

A perimeter drain system will not be provided for this Project.

#### **SUMMARY**

### COMPLIANCE WITH STANDARDS

The drainage design presented within this report for Lot 2 of the Village at Lorson Ranch Filing No. 1 subdivision, conforms to the El Paso County Storm Drainage Criteria and the Mile High Flood District Manual. Additionally, the Site runoff and storm drain facilities is not anticipated to adversely affect the downstream and surrounding developments. This report and its findings are consistent with the drainage requirements documented in the FDP.

### REFERENCES

- 1. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994
- 2. Mile High Flood District Drainage Criteria Manual (MHFD), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 3. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0543G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).
- 4. Lorson Ranch MDDP 1, November 7, 2006 by Pentacor.
- 5. Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 prepared by Core Engineering Group, approved September 7, 2017
- 6. Master Development Drainage Plan for Village at Lorson Ranch Filing No. 1 and Final Drainage Report for Village at Lorson Ranch Filing No. 1 Initial Infrastructure. Prepared by Core Engineering Group, LLC., April 2024. ("FDP")



- 7. Custom Soil Resource Report for El Paso County Area, Colorado. Prepared by NRCS, July 2024.
- 8. Final Plat for Village at Lorson Ranch Filing No. 1. Prepared by Civil Consultants, Inc., April 2024.

### APPENDIX

SOILS MAP AND FEMA FIRM PANEL



United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

## Custom Soil Resource Report for El Paso County Area, Colorado



## Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND	)	MAP INFORMATION
Area of Int	terest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils	Soil Map Unit Polygons	00 12	Very Stony Spot Wet Spot	Warning: Soil Map may not be valid at this scale.
~	Soil Map Unit Lines Soil Map Unit Points	∆ V	Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
Special (19)	Point Features Blowout	Water Fea		line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.
X X	Borrow Pit Clay Spot	Transport	Streams and Canals ation Rails	Please rely on the bar scale on each map sheet for map measurements.
\$	Closed Depression Gravel Pit	~	Interstate Highways	Source of Map: Natural Resources Conservation Service
*	Gravelly Spot	~	US Routes Major Roads	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
@ 	Landfill Lava Flow	Backgrou	Local Roads Ind	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the
<u>له</u> ج	Marsh or swamp Mine or Quarry	The second	Aerial Photography	Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
0	Miscellaneous Water Perennial Water			This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
~	Rock Outcrop			Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 21, Aug 24, 2023
+	Saline Spot Sandy Spot			Soil map units are labeled (as space allows) for map scales
<b>⊕</b> ◊	Severely Eroded Spot Sinkhole			1:50,000 or larger. Date(s) aerial images were photographed: Aug 14, 2018—Sep
3 10 10	Slide or Slip Sodic Spot			23, 2018
<u>(</u>				The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
52	Manzanst clay loam, 0 to 3 percent slopes	1.3	100.0%
Totals for Area of Interest		1.3	100.0%

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## El Paso County Area, Colorado

### 52—Manzanst clay loam, 0 to 3 percent slopes

### **Map Unit Setting**

National map unit symbol: 2w4nr Elevation: 4,060 to 6,660 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 50 to 54 degrees F Frost-free period: 130 to 170 days Farmland classification: Prime farmland if irrigated

### **Map Unit Composition**

Manzanst and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Manzanst**

#### Setting

Landform: Terraces, drainageways Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear, concave Parent material: Clayey alluvium derived from shale

### **Typical profile**

A - 0 to 3 inches: clay loam Bt - 3 to 12 inches: clay Btk - 12 to 37 inches: clay Bk1 - 37 to 52 inches: clay Bk2 - 52 to 79 inches: clay

### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Gypsum, maximum content: 3 percent
Maximum salinity: Slightly saline (4.0 to 7.0 mmhos/cm)
Sodium adsorption ratio, maximum: 10.0
Available water supply, 0 to 60 inches: High (about 9.0 inches)

### Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4c Hydrologic Soil Group: C Ecological site: R067BY037CO - Saline Overflow Hydric soil rating: No

#### **Minor Components**

#### Ritoazul

Percent of map unit: 7 percent Landform: Drainageways, interfluves Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY042CO - Clayey Plains Hydric soil rating: No

### Arvada

Percent of map unit: 6 percent Landform: Drainageways, interfluves Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY033CO - Salt Flat Hydric soil rating: No

#### Wiley

Percent of map unit: 2 percent Landform: Interfluves Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY002CO - Loamy Plains Hydric soil rating: No

# Soil Information for All Uses

# **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

# **Soil Erosion Factors**

Soil Erosion Factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

## Wind Erodibility Index

The wind erodibility index is a numerical value indicating the susceptibility of soil to wind erosion, or the tons per acre per year that can be expected to be lost to wind erosion. There is a close correlation between wind erosion and the texture of the surface layer, the size and durability of surface clods, rock fragments, organic matter, and a calcareous reaction. Soil moisture and frozen soil layers also influence wind erosion.



	MAP LEGEND	1	MAP INFORMATION
Area of Interest	(AOI) 🛹	250	The soil surveys that comprise your AOI were mapped at
	of Interest (AOI)	310	1:24,000.
Soils Soil Rating Po	lvgons	Not rated or not available	Warning: Soil Map may not be valid at this scale.
0		ting Points	
38		0	Enlargement of maps beyond the scale of mapping can cause
48		38	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of
56		48	contrasting soils that could have been shown at a more detailed scale.
		56	
86		86	Please rely on the bar scale on each map sheet for map
134		134	measurements.
180		160	Source of Map: Natural Resources Conservation Service
220		180	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
		220	
250		250	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts
	ated or not available	310	distance and area. A projection that preserves area, such as the
Soil Rating Lir		Not rated or not available	Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
	Water Fea	atures	
	~	Streams and Canals	This product is generated from the USDA-NRCS certified data as
	Transport	ation	of the version date(s) listed below.
<b>~~</b> 48	+++	Rails	Soil Survey Area: El Paso County Area, Colorado
<b>~~</b> 56	~	Interstate Highways	Survey Area Data: Version 21, Aug 24, 2023
<b>~~</b> 86	~	US Routes	Soil map units are labeled (as space allows) for map scales
<b>~</b> 134	~	Major Roads	1:50,000 or larger.
160	~	Local Roads	Date(s) aerial images were photographed: Aug 14, 2018—Sep
<b>***</b> 180	Backgrou	nd	23, 2018
<b>~~</b> 220		Aerial Photography	The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Table—Wind Erodibility Index

Map unit symbol	Map unit name	Rating (tons per acre per year)	Acres in AOI	Percent of AOI
52	Manzanst clay loam, 0 to 3 percent slopes	86	1.3	100.0%
Totals for Area of Interes	st		1.3	100.0%

## **Rating Options—Wind Erodibility Index**

Units of Measure: tons per acre per year Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

# K Factor, Whole Soil

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Factor K does not apply to organic horizons and is not reported for those layers.



MAP INFORMATION

rea of In	terest (AOI)	~	.24	$\sim$	Streams and Canals	The soil surveys that comprise your AOI were mapped at 1:24,000.
	Area of Interest (AOI)	~	.28	Transpor	tation	1.24,000.
oils Soil Bat	ing Polygons	~~	.32	+++	Rails	Warning: Soil Map may not be valid at this scale.
	.02	~~	.37	~	Interstate Highways	
	.05	~	.43	~	US Routes	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
	.10	~	.49	$\sim$	Major Roads	line placement. The maps do not show the small areas of
	.15	~	.55	$\sim$	Local Roads	contrasting soils that could have been shown at a more detailed scale.
	.17	~	.64	Backgro	and Aerial Photography	
	.20		Not rated or not available	20	Achar Hotography	Please rely on the bar scale on each map sheet for map measurements.
	.24	Soil Rati	ng Points			modolionono.
	.28		.02			Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
	.32		.05			Coordinate System: Web Mercator (EPSG:3857)
	.37		.10			Maps from the Web Soil Survey are based on the Web Mercator
	.43		.15			projection, which preserves direction and shape but distorts
	.49		.17			distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more
	.55		.20			accurate calculations of distance or area are required.
	.64		.24			This product is generated from the USDA-NRCS certified data
	Not rated or not available		.28			as of the version date(s) listed below.
Soil Rat	ing Lines		.32			Soil Survey Area: El Paso County Area, Colorado
~	.02		.37			Survey Area Data: Version 21, Aug 24, 2023
~	.05		.43			Soil map units are labeled (as space allows) for map scales
~	.10		.49			1:50,000 or larger.
~	.15		.55			Deta(a) social images were abstagraphed. Aug 14,0040 . Co
~	.17		.64			Date(s) aerial images were photographed: Aug 14, 2018—Sep 23, 2018
	.20		Not rated or not available			<b>-</b>
		Water Feat	tures			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Table—K Factor, Whole Soil

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
52	Manzanst clay loam, 0 to 3 percent slopes	.32	1.3	100.0%
Totals for Area of Interes	st		1.3	100.0%

## Rating Options—K Factor, Whole Soil

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)

# **Soil Qualities and Features**

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

# Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

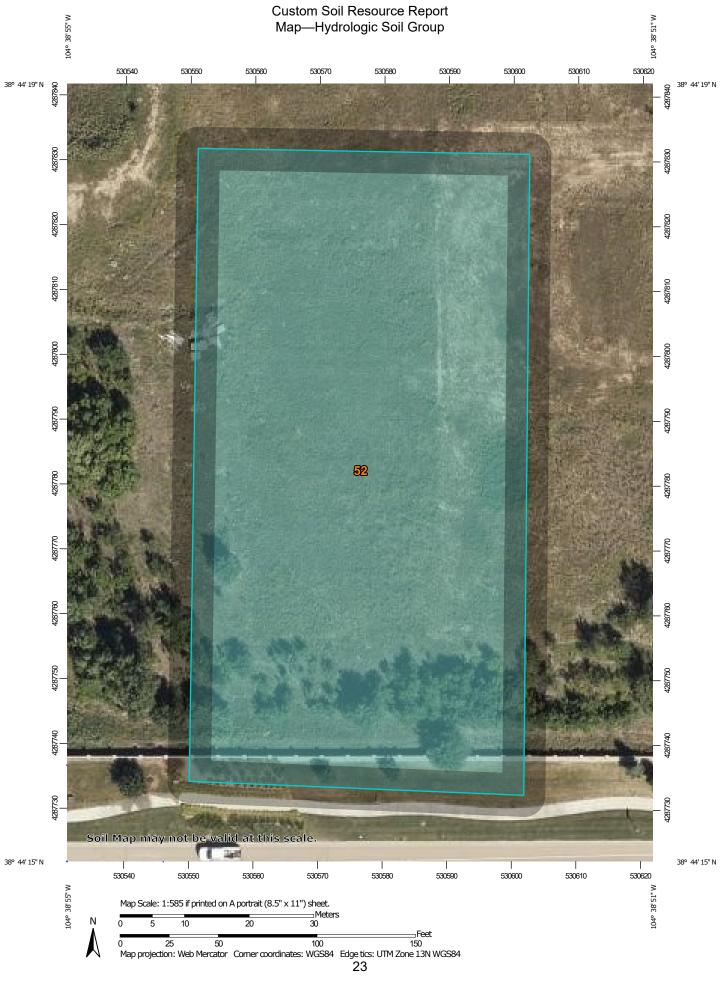
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

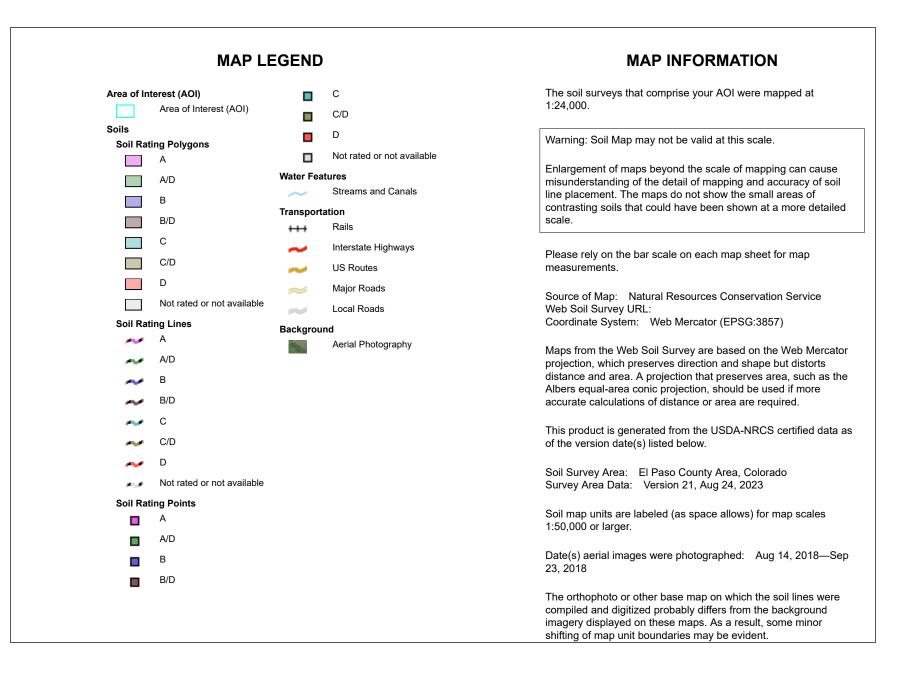
Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
52	Manzanst clay loam, 0 to 3 percent slopes	С	1.3	100.0%
Totals for Area of Interes	st		1.3	100.0%

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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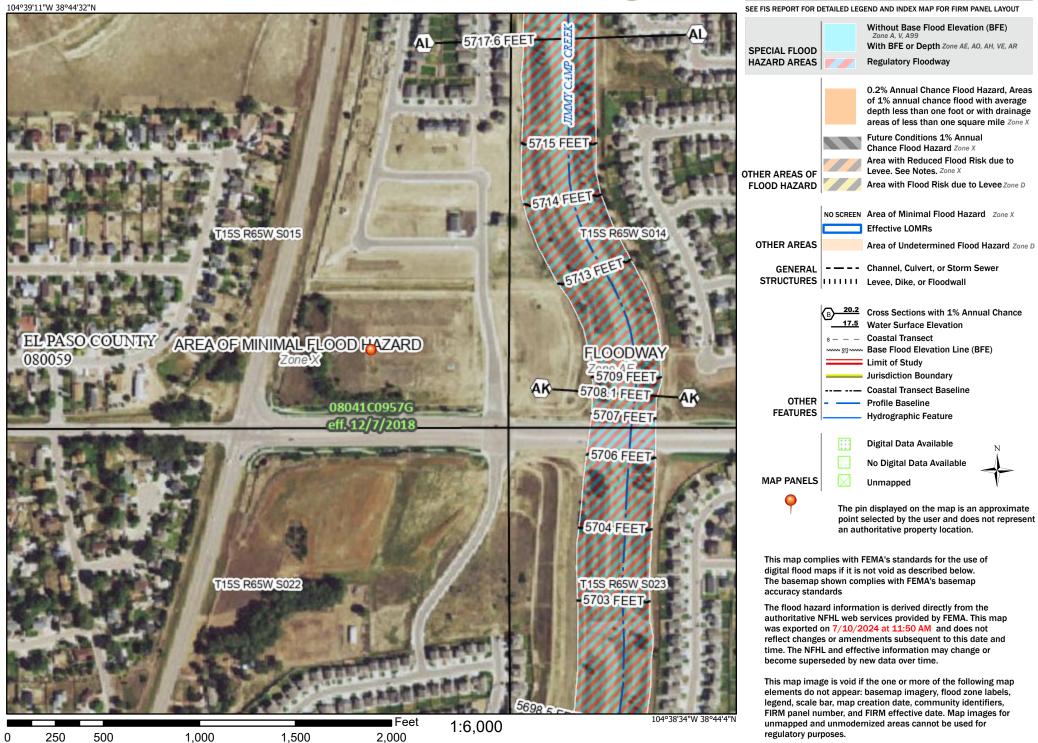
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# National Flood Hazard Layer FIRMette



### Legend



Basemap Imagery Source: USGS National Map 2023

HYDROLOGIC CALCULATIONS

IDF Equations:

$I_{100} = -2.52 \ln(D) + 12.735$
l₅₀ = -2.25ln(D) + 11.375
l <sub>25</sub> -2.00ln(D) + 10.111
l₁₀ -1.75ln(D) + 8.847
l₅ -1.50ln(D) + 7.583
l₂ -1.19ln(D) + 6.035

Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
<b>P</b> <sub>1</sub> =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulatio
------------------------------------

			/ /	,		
Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

\*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

McDonal	ld's - Draina	ge Report								Watercou	ırse Coeffic	ient				
Proposed	l Runoff Cal	culations			Forest	& Meadow	2.50	Short G	ass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of C	Concentratio	n			Fallow or	Cultivation	5.00		Nearly Ba	re Ground	10.00		Paveo	d Area & Sh	allow Gutter	20.00
		SUB-BASIN			INIT	IAL / OVERL	AND	Т	RAVEL TIM	IE				T(c) CHECk		FINAL
		DATA				TIME			T(t)				(URE	BANIZED BA	SINS)	T(c)
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
A1	A1	16,437	0.38	0.70	100	2.1%	5.7	91	1.3%	20.00	2.3	0.7	6.4	191	11.1	6.4
A2	A2	6,545	0.15	0.84	100	1.6%	4.1	64	1.1%	20.00	2.1	0.5	5.0	164	10.9	5.0
A3	A3	1,451	0.03	0.89	25	2.8%	1.4	51	1.1%	20.00	2.1	0.4	5.0	76	10.4	5.0
R1	R1	3,719	0.09	0.75	80	1.0%	5.7			20.00	0.0	0.0	5.7	80	10.4	5.7
EX1A	EX1A	3,589	0.08	0.86	37	2.0%	2.2	131	1.4%	20.00	2.3	0.9	5.0	168	10.9	5.0
EX4	EX4	3,855	0.09	0.86	0	0.0%		205	1.2%	20.00	2.2	1.6	5.0	205	11.1	5.0
EX5	EX5	12,991	0.30	0.75	77	2.0%	4.5	94	1.6%	20.00	2.6	0.6	5.1	171	11.0	5.1
OS1	OS1	6,447	0.15	0.24	37	2.2%	7.3	28	4.2%	20.00	4.1	0.1	7.4	65	10.4	7.4

	s - Drainage Re											
Proposed R	unoff Calculati	ions			Desi	gn Storm	5 Year					
(Rational Met	hod Procedure)											
D						RUNOFF				VE RUNO		Γ
DESIGN	ASIN INFORMATIC DRAIN	AREA	RUNOFF	T(c)	CxA	I	Q	T(c)	CxA		Q	NOTES
POINT	BASIN	ac.	COEFF	min	•	in/hr	cfs	min	•	in/hr	cfs	
A1	A1	0.38	0.70	6.4	0.27	4.81	1.28					
A2	A2	0.15	0.84	5.0	0.13	5.17	0.65					
A3	A3	0.03	0.89	5.0	0.03	5.17	0.15					
R1	R1	0.09	0.75	5.7	0.06	4.97	0.32					
EX1A	EX1A	0.08	0.86	5.0	0.07	5.17	0.36					
EX4	EX4	0.09	0.86	5.0	0.08	5.17	0.39					
EX5	EX5	0.30	0.75	5.1	0.22	5.14	1.15					
OS1	OS1	0.15	0.24	7.4	0.04	4.58	0.16					

Proposed	<b>ld's - Drainage R d Runoff Calcula</b> Aethod Procedure)	-			Des	ign Storm	100 Year					
E	BASIN INFORMATIO	N		DIF	RECT RUN	OFF			CUMULATI	VE RUNOF	F	
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	ا in/hr	Q cfs	NOTES
A1	A1	0.38	0.82	6.4	0.31	8.07	2.50					
A2	A2	0.15	0.91	5.0	0.14	8.68	1.19					
A3	A3	0.03	0.94	5.0	0.03	8.68	0.27					
R1	R1	0.09	0.95	5.7	0.08	8.35	0.68					
EX1A	EX1A	0.08	0.92	5.0	0.08	8.68	0.66					
EX4	EX4	0.09	0.92	5.0	0.08	8.68	0.71					
EX5	EX5	0.30	0.85	5.1	0.25	8.62	2.19					
OS1	OS1	0.15	0.51	7.4	0.08	7.69	0.58					

### 096806032

# Weighted Imperviousness Calculations

	AREA	AREA	ROOF	ROOF		RO	OF		LANDSCAPE	LANDSCAPE		LAND	SCAPE		PAVEMENT	PAVEMENT		PAVE	MENT		WEIGHTED		WEIGHTED	COEFFICIEN	ITS
SUB-BASIN	(SF)	(Acres)	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	IMPERVIOUSNESS	C2	C5	C10	C100
A1	16,437	0.38	0	90%	0.73	0.75	0.90	0.95	4,286	0%	0.04	0.15	0.30	0.45	12,151	100%	0.89	0.90	0.90	0.95	73.9%	0.67	0.70	0.74	0.82
A2	6,545	0.15	0	90%	0.73	0.75	0.90	0.95	530	0%	0.04	0.15	0.30	0.45	6,015	<b>100%</b>	0.89	0.90	0.90	0.95	91.9%	0.82	0.84	0.85	0.91
A3	1,451	0.03	0	90%	0.73	0.75	0.90	0.95	18	0%	0.04	0.15	0.30	0.45	1,433	100%	0.89	0.90	0.90	0.95	98.8%	0.88	0.89	0.89	0.94
R1	3,719	0.09	3,719	90%	0.73	0.75	0.90	0.95	0	0%	0.04	0.15	0.30	0.45	0	100%	0.89	0.90	0.90	0.95	90.0%	0.73	0.75	0.90	0.95
EX1A	3,589	0.08	0	90%	0.73	0.75	0.90	0.95	212	0%	0.04	0.15	0.30	0.45	3,377	100%	0.89	0.90	0.90	0.95	94.1%	0.84	0.86	0.86	0.92
EX4	3,855	0.09	0	90%	0.73	0.75	0.90	0.95	207	0%	0.04	0.15	0.30	0.45	3,648	100%	0.89	0.90	0.90	0.95	94.6%	0.84	0.86	0.87	0.92
EX5	12,991	0.30	0	90%	0.73	0.75	0.90	0.95	2,564	0%	0.04	0.15	0.30	0.45	10,427	100%	0.89	0.90	0.90	0.95	80.3%	0.72	0.75	0.78	0.85
OS1	6,447	0.15	0	90%	0.73	0.75	0.90	0.95	5,669	0%	0.04	0.15	0.30	0.45	778	100%	0.89	0.90	0.90	0.95	12.1%	0.14	0.24	0.37	0.51
TOTAL	55,034	1.26	3,719	90%	0.73	0.75	0.90	0.95	13,486	0%	0.04	0.15	0.30	0.45	37,829	100%	0.89	0.90	0.90	0.95	74.8%	0.67	0.71	0.75	0.83

	SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMMULATIVE 5-YR RUNOFF (CFS)	CUMMULATIVE 100- YR RUNOFF (CFS)						
A1	A1	0.38	1.28	2.50	1.28	2.50						
A2	A2	0.15	0.65	1.19	0.65	1.19						
A3	A3	0.03	0.15	0.27	0.81	1.46						
R1	R1	0.09	0.32	0.68	0.32	0.68						
EX1A	EX1A	0.08	0.36	0.66	0.36	0.66						
EX4	EX4	0.09	0.39	0.71	1.20	2.17						
EX5	EX5	0.30	1.15	2.19	2.35	4.36						
OS1	OS1	0.15	0.16	0.58	0.16	0.58						
TOTAL		1.26	4.47	8.77								

HYDRAULIC CALCULATIONS

## MHFD-Inlet, Version 5.03 (August 2023)

# INLET MANAGEMENT

Worksheet Protected

NLET NAME	Inlet A1	Inlet A2	Inlet A3
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT/Denver 13 Combination	CDOT/Denver 13 Combination
ER-DEFINED INPUT			
User-Defined Design Flows			
Vinor Q <sub>Known</sub> (cfs)	1.3	0.7	0.2
Major Q <sub>Known</sub> (cfs)	2.5	1.2	0.3
Bypass (Carry-Over) Flow from Upstream	<u> </u>	am (left) to downstream (right) in order for	
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Watershed Characteristics			
Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			
Watershed Profile			
Overland Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input			
Dverland Slope (ft/ft)         Dverland Length (ft)         Channel Slope (ft/ft)         Channel Length (ft)         Winor Storm Rainfall Input         Design Storm Return Period, Tr (years)			
Dverland Slope (ft/ft)         Dverland Length (ft)         Channel Slope (ft/ft)         Channel Length (ft)         Winor Storm Rainfall Input         Design Storm Return Period, Tr (years)			
Dverland Slope (ft/ft)         Dverland Length (ft)         Channel Slope (ft/ft)         Channel Length (ft)         Minor Storm Rainfall Input         Design Storm Return Period, Tr (years)         Dne-Hour Precipitation, P1 (inches)			

#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	1.3	0.7	0.2
Major Total Design Peak Flow, Q (cfs)	2.5	1.2	0.3
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	0.0
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	0.0

## MHFD-Inlet, Version 5.03 (August 2023)

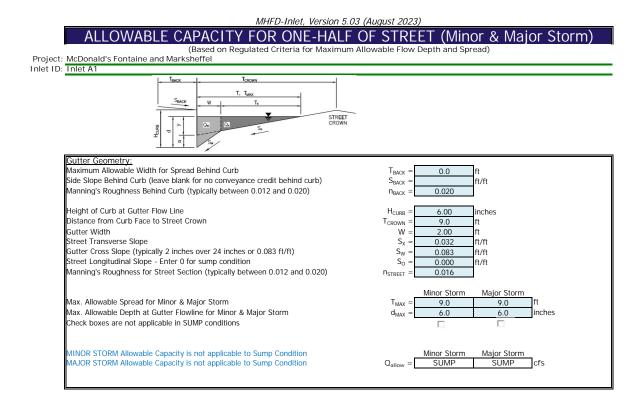
# INLET MANAGEMENT

Worksheet Protected

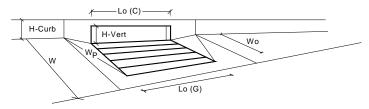
INLET NAME	Inlet EX1A	Inlet EX4	Inlet EX5
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening
ER-DEFINED INPUT			
User-Defined Design Flows			
Minor Q <sub>Known</sub> (cfs)	0.4	0.4	1.2
Major Q <sub>Known</sub> (cfs)	0.7	0.7	2.2
Bypass (Carry-Over) Flow from Upstream	0		
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Subcatchment Area (acres) Percent Impervious			
Subcatchment Area (acres)			
NRCS Soil Type			
Watershed Profile			
Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			
	-	•	
Minor Storm Rainfall Input			
Design Storm Return Period, Tr (years)			
One-Hour Precipitation, P <sub>1</sub> (inches)			
Major Storm Rainfall Input			
Design Storm Return Period, T <sub>r</sub> (years)			

#### CALCULATED OUTPUT

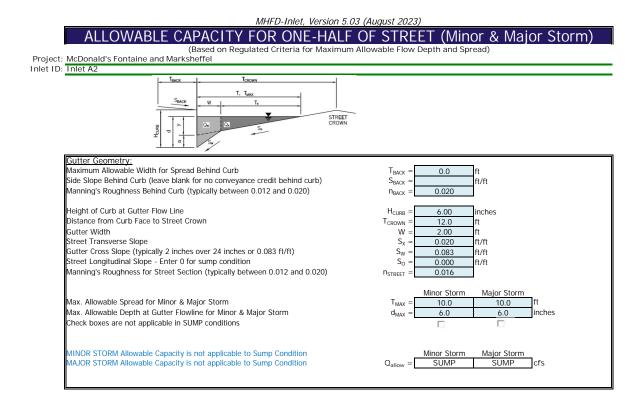
Minor Total Design Peak Flow, Q (cfs)	0.4	0.4	1.2
Major Total Design Peak Flow, Q (cfs)	0.7	0.7	2.2
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	N/A



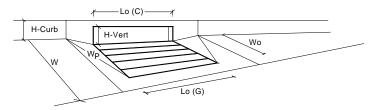




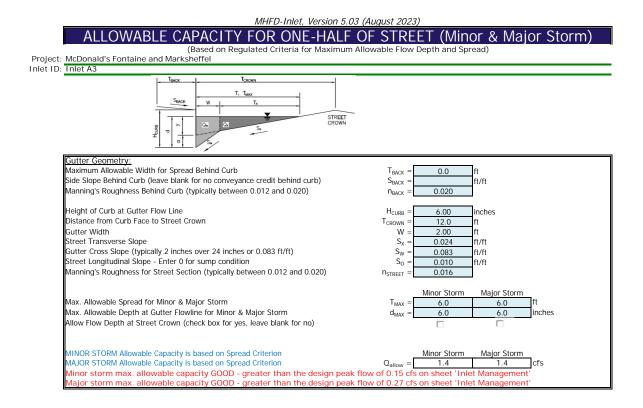
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	7
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	incrics
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.7	4.7	inches
Grate Information	Fonding Depth =	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	Ifeet
Width of a Unit Grate	$W_0 =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	-
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_0(G) =$	N/A	N/A	
Curb Opening Information	-0 (-)	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>n</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	1
	_			
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	Π.
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.22	0.22	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	1
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	2.9	2.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	1.3	2.5	cfs
				•



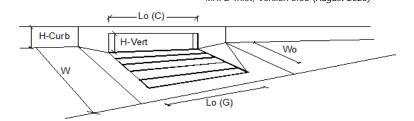




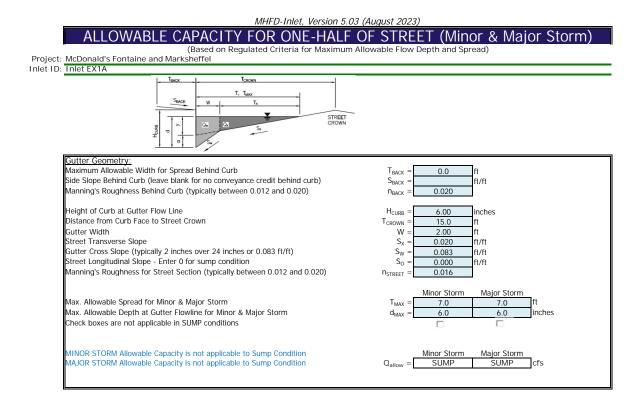
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		13 Combination	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	3.9	3.9	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	3.00	3.00	feet
Width of a Unit Grate	W <sub>o</sub> =	1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	0.60	0.60	
Curb Opening Information	•	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) =$	3.00	3.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.70	3.70	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.66	0.66	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	0.35	0.35	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.16	0.16	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	0.61	0.61	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.61	0.61	
	-			-
		MINOR	MAJOR	1
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	1.4	1.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	0.7	1.2	cfs



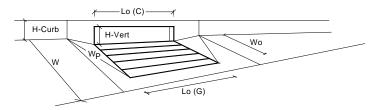
#### INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.03 (August 2023)



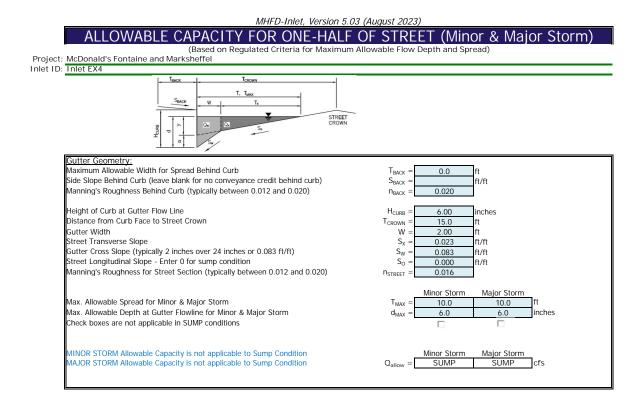
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT/Denver 2	13 Combination	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.2	0.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o$	C% =	100	100	%



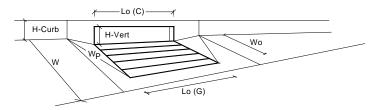




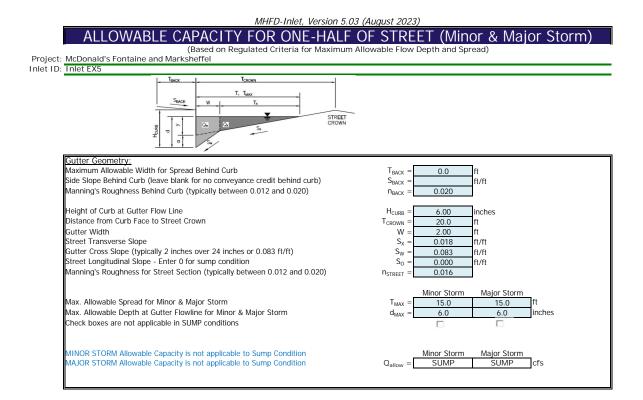
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	3.2	3.2	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.10	0.10	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.96	0.96	-
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>combination</sub> =	N/A	N/A	
, i i i i i i i i i i i i i i i i i i i				-
		MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	0.8	0.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	0.4	0.7	cfs



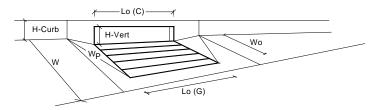




Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.2	4.2	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>n</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.19	0.19	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.81	0.81	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	Combination			4
	_	MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	3.0	3.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	0.4	0.7	cfs

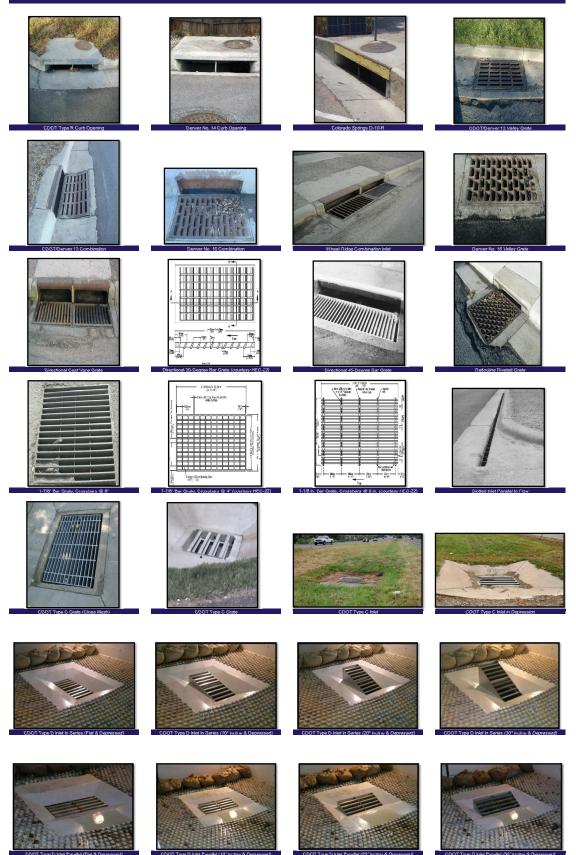




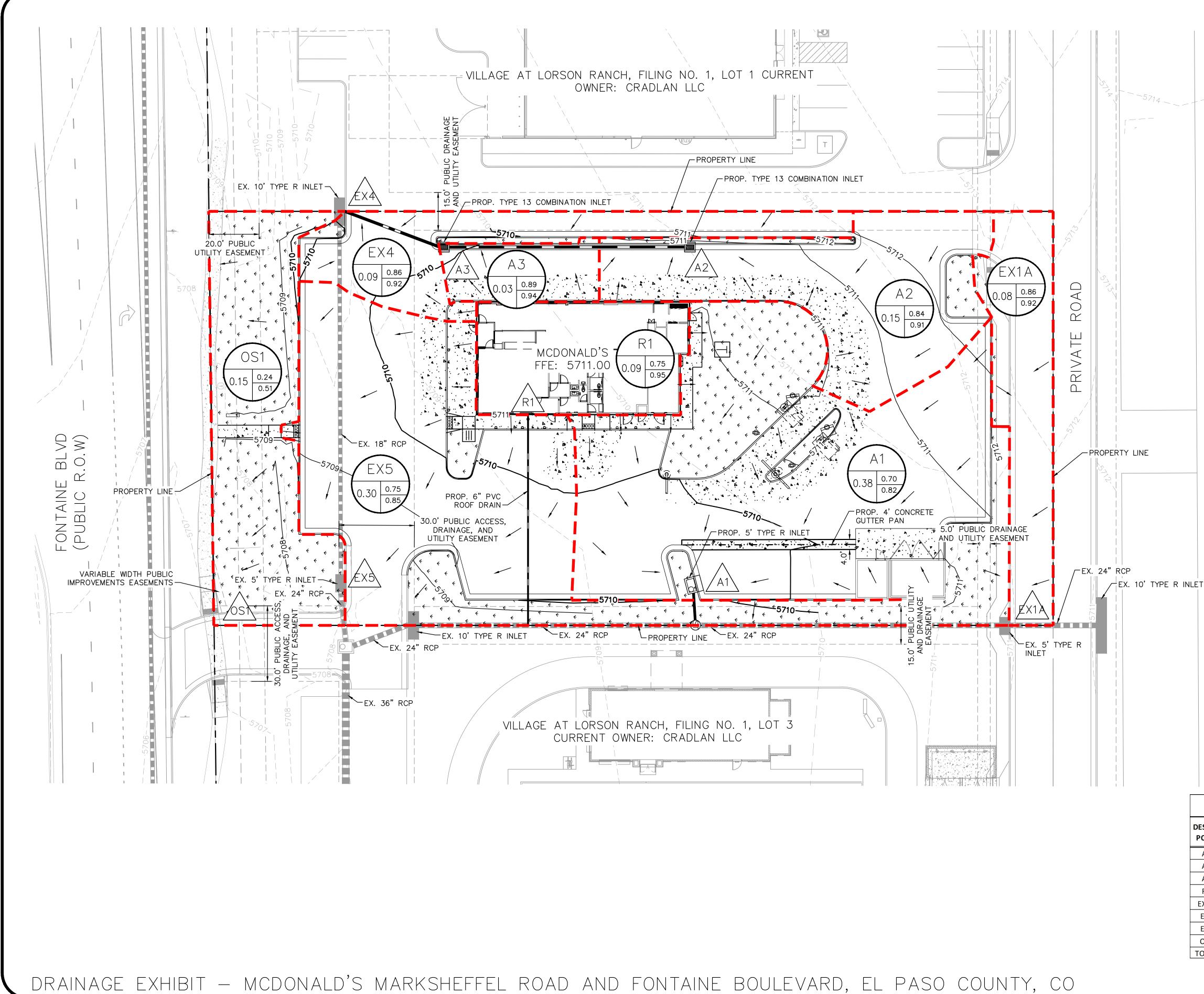


CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	4.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_0$ (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_0$ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>n</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.23	0.23	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	o _[	3.2	3.2	cfs
Inter Interception Capacity (assumes clogged condition)	$Q_a = Q_{PEAK REQUIRED} =$	3.2 1.2	2.2	cfs
Intel Capacity 15 GOOD for Minor and Major Storms (>Q Peak)		1.2	2.2	013

#### INLET PICTURES

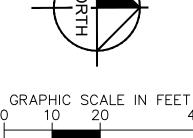


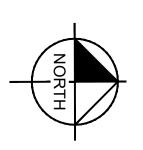
DRAINAGE EXHIBIT

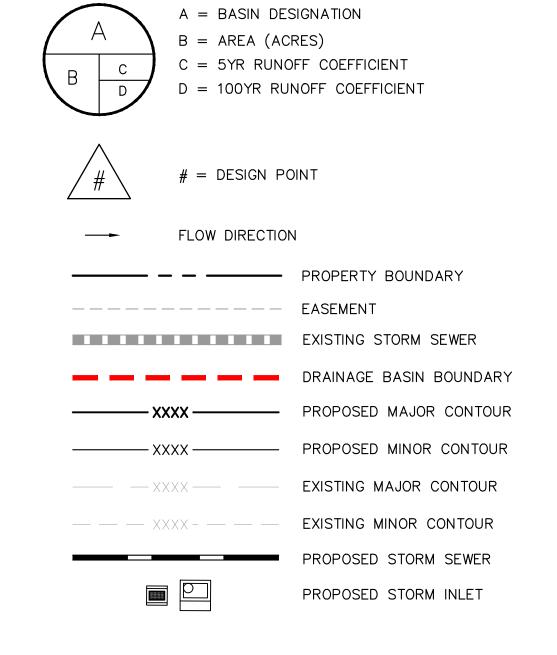


# **Kimley**»Horn

SUMMARY - PROPOSED RUNOFF TABLE							
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMMULATIVE 5-YR RUNOFF (CFS)	CUMMULATIVE 100- YR RUNOFF (CFS)	
<mark>A1</mark>	A1	0.38	1.28	2.50	1.28	2.50	
A2	A2	0.15	0.65	1.19	0.65	1.19	
A3	A3	0.03	0.15	0.27	0.81	1.46	
R1	R1	0.09	0.32	0.68	0.32	0.68	
EX1A	EX1A	0.08	0.36	0.66	0.36	0.66	
EX4	EX4	0.09	0.39	0.71	1.20	2.17	
EX5	EX5	0.30	1.15	2.19	2.35	4.36	
OS1	OS1	0.15	0.16	0.58	0.16	0.58	
TOTAL		1.26	4.47	8.77			







LEGEND

MASTER DRAINAGE STUDIES

## FINAL DRAINAGE PLAN SF 248

## **VILLAGE AT LORSON RANCH**

## JUNE, 2024

Prepared for:

Lorson, LLC 212 N. Wahsatch Ave, Suite 301 Colorado Springs, Colorado 80903 (719) 635-3200

#### Prepared by:

Core Engineering Group, LLC 15004 1<sup>ST</sup> Avenue South Burnsville, MN 55306 (719) 570-1100

Project No. 100.070



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#### ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Richard L. Schindler, P.E. #33997 For and on Behalf of Core Engineering Group, LLC

#### **OWNER'S STATEMENT**

I, the Owner, have read and will comply with all the requirements specified in the drainage report and plan.

Lorson, LLC

By Jeff Mark

Title

Manager

Address

212 N. Wahsatch Avenue, Suite 301, Colorado Springs, CO 80903

#### FLOODPLAIN STATEMENT

To the best of my knowledge and belief, this development is not located within a designated floodplain as shown on Flood Insurance Rate Map Panel No. and 08041C0957 G, dated December 7, 2018. (See Appendix A, FEMA FIRM Exhibit)

Richard L. Schindler, #33997

Date

#### EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volume 1 and 2, and Engineering Criteria Manual, As Amended.

Joshua Palmer, P.E. County Engineer/ECM Administrator

Date

#### Conditions:

Date

Date

#### 1.0 LOCATION and DESCRIPTION

**Village at Lorson Ranch** is located west of Jimmy Camp Creek. The site is located on approximately 9.722 acres of vacant land. This project will develop this site into a commercial development. The land for the commercial lots is currently owned by Cradlan, LLC.

The site is located in the Southeast 1/4 of Section 15, Township 15 South and Range 65 West of the 6<sup>th</sup> Principal Meridian. The site is bounded on the north by Carriage Meadows North Filing No. 1, on the west by Marksheffel Road, on the east by Carriage Meadows Drive, and the south by Fontaine Boulevard. For reference, a vicinity map is included in Appendix A of this report.

#### Conformance with applicable Drainage Basin Planning Studies

There is an existing (unapproved) DBPS for Jimmy Camp Creek prepared by Wilson & Company in 1987, and is referenced in this report. The only major drainage improvements for this study area according to the 1987 Wilson study was the reconstruction of the main stem of Jimmy Camp Creek. In 2006 the main stem of Jimmy Camp Creek was reconstructed in accordance with the 1987 study. There are no further improvements to be made on Jimmy Camp Creek.

Conformance with Lorson Ranch MDDP1 by Pentacor Engineering (approved November 7, 2006) and Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 (approved September 7, 2017)

Core Engineering Group has an approved MDDP for Lorson Ranch, which covers this study area for major infrastructure. The major infrastructure in the MDDP includes storm sewer in Fontaine Boulevard and relocation of the FMIC irrigation ditch which was constructed in 2006 conforming to the MDDP for Lorson Ranch. Other major infrastructure improvements constructed to serve this site include Pond G1/G2 constructed as part of Carriage Meadows South at Lorson Ranch Filing No. 1. Pond G1/G2 is an offsite full spectrum detention pond constructed in 2017 and included detention and water quality provisions that serve Village at Lorson Ranch.

The Village at Lorson Ranch is located within the *"Jimmy Camp Creek Drainage Basin"*, which is a fee basin in El Paso County. Jimmy Camp Drainage Basin will be a closed basin within Lorson Ranch within a few months and drainage fees will not be administered per agreements with the county.

#### 2.0 DRAINAGE CRITERIA

The supporting drainage design and calculations were performed in accordance with the City of Colorado Springs and El Paso County "Drainage Criteria Manual (DCM)", dated November, 1991, the El Paso County "Engineering Criteria Manual", Chapter 6 and Section 3.2.1 Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014, and the UDFCD "Urban Storm Drainage Criteria Manual" Volumes 1, 2 and 3 for inlet sizing and full spectrum ponds. No deviations from these published criteria are requested for this site.

The Rational Method as outlined in Section 6.3.0 of the May 2014 "Drainage Criteria Manual" and in Section 3.2.8.F of the El Paso County "Engineering Criteria Manual" was used for basins less than 130 acres to determine the rainfall and runoff conditions for the proposed development of the site. The runoff rates for the 5-year initial storm and 100-year major design storm were calculated.

Current updates to the Drainage Criteria manual for El Paso County states the if detention is necessary, Full Spectrum Detention will be included in the design, based on this criteria, Full Spectrum Detention will not be required for this development.

#### 3.0 EXISTING HYDROLOGICAL CONDITIONS

This site is currently undeveloped with native vegetation (grass with no shrubs) and gentle slopes in a southerly direction to the north side of Fontaine Boulevard.

The Soil Conservation Service (SCS) classifies the soils within the Village at Lorson Ranch property as Manzanst clay loam and Ellicot loamy coarse sand. The clay loam is considered to be hydrologic soil group C and the sandy loams are considered hydrologic soil group A (see table 3.1 below). The clay loams are difficult to vegetate and comprise of the majority of the study area. These soils can be mitigated easily by limiting their use as topsoil since they this is a commercial site and most areas will be paved or landscaped with rock bedding.

Soil No.	Soil	Hydro. Group	Shrink/Swell Potential	Permeability	Surface Runoff Potential	Erosion Hazard
28	Ellicott Loamy Coarse Sand (0.8%)	А	Low	Moderate	Medium	Moderate
52	Manzanst Clay Loam (2.2%)	С	High	Slow	Medium	Moderate

#### Table 3.1: SCS Soils Survey for the Study Area

Excerpts from the SCS "Soil Survey of El Paso County Area, Colorado" are provided in *Appendix A* for further reference.

For the purpose of preparing hydrologic calculations for this report, the soils of each basin are assumed to be wholly comprised of the majority soil hydrologic group.

This site is not located within the delineated 100-year floodplain of the East Tributary of Jimmy Camp Creek per the Federal Emergency Management Agency (FEMA) Flood Rate Insurance Map (FIRM) number 08041C10957 G, effective December 7, 2018.

#### <u>Basin EX1</u>

This existing basin consists primarily of flows from the existing FMIC channel, a majority of these flows are from the offsite area west of the channel. Runoff from basin EX1 flows to the existing FMIC channel, then continues west toward Carriage Meadows Drive. The existing runoff from this 0.95 acre basin is 0.3cfs and 1.6cfs for the 5-year and 100-year events. No other runoff is directed to this basin.

The FMIC historically consisted of an open channel from Cottonwood Meadows to Jimmy Camp Creek (culvert under Marksheffel). Upon development of Lorson Ranch in 2007, a 48" pipe was installed from Cottonwood Meadows west and under Marksheffel Road. The 48" pipe carries FMIC water (50cfs) and stormwater to the east side of Marksheffel Road where a reconstructed open channel directs water east to Carriage Meadows Drive. In addition, this open channel section is designed to handle runoff from the full buildout of Marksheffel Road which is carried in a 30" RCP under Marksheffel Road. The 30" RCP is located directly north of the 48" FMIC pipe. Stormwater and FMIC water (113cfs & 214cfs in 5/100 year storm) travels east to Carriage Meadows Drive where a diversion structure and a box culvert effectively separate stormwater from FMIC water. The diversion structure is a 25' D-10-R inlet with a 1.5' opening and the box culvert is a 3x4 culvert with a gate to regulate or shut off flow. During times of FMIC operation, the gate is adjusted so that only the FMIC water is allowed to pass east in the FMIC channel. Additional runoff at this gate will pond up and flow into the 25' diversion structure. During times the FMIC is not operating, the gate is closed which forces all runoff into the 25' diversion structure. The outlet structure is drained by a 48" RCP that flows east under Carriage Meadows Drive. A 60" RCP at 0.95% slope continues east and outlets directly into Jimmy Camp Creek with a capacity of 270cfs. Just north of the 60" RCP, a 36" stub has been constructed to accept flows from a WQ basin in the Carriage

Meadows residential areas. This entire system is in place and has been fully operational since August, 2006.

#### Basin EX2

This existing basin consists of on-site undeveloped basin located approximately 100' east of Marksheffel Road, south of and adjacent to the existing FMIC channel, and north of Fontaine Boulevard. This basin has moderate slopes and flows overland south downstream to Fontaine Boulevard, then to an existing 34"x53" HERCP storm sewer that routes runoff southerly under Fontaine Boulevard. The total pre-developed flow from this 8.44 acre basin is 3.4cfs and 19.0cfs in the 5 and 100-year storm events.

#### Basin EX3

Basin EX3 is a self-contained basin and does not accept any offsite flows. Surface flows are FROM Marksheffel Road and are directed to an existing drainage swale that flows in a southerly-southwesterly direction to an existing 18" RCP, these flows are then routed within this existing 18" RCP to the aforementioned existing 34"x53" HERCP that flows southerly under Fountain Boulevard. The existing runoff from this 0.73 acre site is 0.4cfs and 2.4cfs for the 5-year and 100-year events. The drainage area and flows have not changed from the previous reports when the inlets/storm was designed.

#### Basin EX4

Basin EX4 consists of the west half of Carriage Meadows Drive, a developed north-south road. Flow is directed westerly to the existing curb and gutter, then continues southerly to an existing 5' Type "R" inlet. This inlet is located on west side of Carriage Meadows Drive, at the northwest corner of Fountaine Boulevard and Carriage Meadows Drive. Flow is routed westerly from this inlet to the aforementioned 34"x53" HERCP via an existing 30" RCP. The existing runoff from this 0.57 acre site is 2.6cfs and 4.7cfs for the 5-year and 100-year events.

#### 4.0 DEVELOPED HYDROLOGICAL CONDITIONS

Hydrology for **Village at Lorson Ranch** drainage report was based on the City of Colorado Springs/El Paso County Drainage Criteria. Sub-basins that lie within this project were determined and the 5-year and 100-year peak discharges for the developed conditions have been presented in this report. Based on these flows, storm inlets will be added when the street capacity is exceeded.

Soil types A/B & C/D have been assumed for the developed hydrologic conditions. See Appendix A for SCS Soils Map.

The time of concentration for each basin and sub-basin was developed using an overland, ditch, street and pipe flow components. The maximum overland flow length for developed conditions was limited to 100 feet. Travel time velocities ranged from 2 to 6 feet per second. The travel time calculations are included in the back of this report.

Runoff coefficients for the various land uses were obtained from Table 6-6 dated May 2014 from the updated City of Colorado Springs/El Paso County Drainage Criteria Manual. See Appendix B.

Drainage for the site was divided into 8 proposed basins and 3 existing basins. Runoff coefficients for the 5/100-year events are 0.83 and 0.90 respectively. This is a commercial site, and most areas will be paved or landscaped with rock bedding. Analysis for each of the basins are briefly discussed as follows:

#### Basins EX1, EX3 & EX4

These offsite basins have been discussed in the existing Hydrological Conditions portion of this report, any additional discussion is not required.

#### <u>Basin PR1</u>

This basin consists of a commercial area, surface runoff will be directed to a future 10' Type "R" inlet in a sump condition at the southwest corner of this basin. Runoff from this inlet, (design point #7) will be conveyed westerly via future 18" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 1.24 acre basin is 5.3cfs for the 5-year storm event and 9.7cfs for the 100-year storm event. See the appendix for detailed calculations. Interim flows from this area (non-developed) will be conveyed south overland to a temporary sediment basin which flows into Inlet DP8 (5' Type R).

#### Basin PR2

This basin consists of a commercial area, surface runoff will be directed to a proposed 20' Type "R" inlet in a sump condition at the south-center part of this basin. Runoff from this inlet, (design point #1) will be conveyed southerly by a proposed 24" RCP, then easterly via proposed 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 2.41 acre basin is 9.4cfs for the 5-year storm event and 17.0cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin PR3

This basin consists of a commercial area and street, surface runoff will be directed to a proposed 5' Type "R" inlet in a sump condition at the south-center portion of this basin. Runoff from this inlet, (design point #1a) will be conveyed southerly by a proposed 24" RCP, then easterly via proposed 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 0.11 acre basin is 0.5cfs for the 5-year storm event and 0.9cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin PR4

This basin consists of a commercial area, surface runoff will be directed to a proposed continuous ongrade 10' Type "R" inlet at the southeast corner of this basin. Runoff from this inlet, (design point #4) will be conveyed easterly via proposed 18", 24", & 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 1.68 acre basin is 7.2cfs for the 5-year storm event and 13.1cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin PR5

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed southerly, then easterly to a proposed 5' Type "R" inlet in a sump condition at the southeast corner of this basin. Runoff from this inlet, (design point #5) is routed by a proposed 24" RCP to the previously discussed proposed 36" RCP then continues easterly to the previously mentioned existing 34"x53" HERCP. Developed flow from this 0.39 acre basin is 1.7cfs for the 5-year storm event and 3.0cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin PR6

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed easterly and southerly to a proposed 10' Type "R" inlet in a sump condition at the southeast corner of this basin. Runoff from this inlet, (design point #3) is routed southeasterly by a proposed 24" RCP to the previously discussed proposed 36" RCP then continues easterly to the existing 34"x53" HERCP. Developed flow from this 0.72 acre basin is 3.1cfs for the 5-year storm event and 5.6cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin PR7

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed southerly to a future 10' Type "R" inlet in a sump condition at the south-center portion of this basin. Runoff from this inlet, (design point #8a) is routed by proposed 18" & 24" RCP's southwesterly and westerly to the existing 34"x53" HERCP. Developed flow from this 1.41 acre basin is 6.0cfs for the 5-year storm event and 11.0cfs for the 100-year storm event. See the appendix for detailed calculations.

Interim flows from this area (non-developed) will be conveyed south overland to a temporary sediment basin which flows into Inlet DP8 (5' Type R).

#### Basin PR8

This basin consists of parking for a future fast-food type of commercial area, surface flow from this basin is directed northerly to a proposed 5' Type "R" inlet in a sump condition at the north-center portion of this basin. This inlet will be constructed as part of the first phase of construction and stubs will be provided for future inlets for Basins PR1 and PR7. Runoff from this inlet, (design point #8) is routed westerly by proposed 24" RCP to the existing 34"x53" HERCP. Developed flow from this 0.22 acre basin is 0.9cfs for the 5-year storm event and 1.7cfs for the 100-year storm event. See the appendix for detailed calculations. Interim flows from this area (non-developed) will be conveyed directly to a temporary sediment basin which flows into Inlet DP8 (5' Type R).

See the Developed Conditions Hydrology Calculations in the back of this report and the Developed Conditions Drainage Map (Map Pocket) for the 5-year and 100-year storm event amounts.

#### 5.0 HYDRAULIC SUMMARY

The sizing of the hydraulic structures was prepared by using the *StormSewers* software programs developed by Intellisolve, which conforms to the methods outlined in the "City of Colorado Springs/El Paso County Drainage Criteria Manual". Street capacities and Inlets were sized by Denver Urban Drainage's xcel spreadsheet UD-Inlet.

It is the intent of this drainage report to use the proposed parking area curb/gutter and storm sewer to convey runoff to an existing storm sewer system, then to the existing detention and water quality pond G1/G2 located in Carriage Meadows South. This pond has been adequately sized to accept the developed flow from this development. See Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 prepared by Core Engineering Group, Reference SF1711, approved September 7, 2017. Flows will then outlet to the East Tributary of Jimmy Camp Creek. Inlet size and location are shown on the storm sewer layout in the appendix. See the appendix for detailed calculations and the storm sewer model.

	Residential Local		Residentia	I Collector	Principal Arterial	
Street Slope	5-year	100-year	5-year	100-year	5-year	100-year
0.5%	6.3	26.4	9.7	29.3	9.5	28.5
0.6%	6.9	28.9	10.6	32.1	10.4	31.2
0.7%	7.5	31.2	11.5	34.6	11.2	33.7
0.8%	8.0	33.4	12.3	37.0	12.0	36.0
0.9%	8.5	35.4	13.0	39.3	12.7	38.2
1.0%	9.0	37.3	13.7	41.4	13.4	40.2
1.4%	10.5	44.1	16.2	49.0	15.9	47.6
1.8%	12.0	45.4	18.4	50.4	18.0	50.4
2.2%	13.3	42.8	19.4	47.5	19.5	47.5
2.6%	14.4	40.7	18.5	45.1	18.5	45.1
2.7%	14.7	40.6	18.4	45.0	18.4	45.0
3.0%	15.5	39.0	17.7	43.2	17.8	43.2
3.5%	16.7	37.2	16.9	41.3	17.0	41.3
4.0%	17.9	35.7	16.2	39.7	16.3	39.7
4.5%	19.0	34.5	15.7	38.3	15.7	38.3
5.0%	19.9	33.4	15.2	37.1	15.2	37.1

Table 1: Street Capacities (100-year capacity is only <sup>1</sup>/<sub>2</sub> of street)

Note: all flows are in cfs (cubic feet per second).

Design Point 1 is located on the north side of Center Village and accepts developed flows from Basin PR2. The runoff will be conveyed to Design Point 1 via curb/gutter. The street capacity of Street B (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

( <u>5-year storm)</u> Tributary Basins: PR2 Upstream flowby:	Inlet/MH Number: Inlet DP1 Total Street Flow: 9.4cfs
Flow Intercepted: 9.4cfs Inlet Size: 20' type R, sump	Flow Bypassed: 0.0cfs
<b>Street Capacity:</b> Street slope = 0.9%, cap	acity = 8.0cfs, okay half flow from each side
<u>(100-year storm)</u> Tributary Basins: PR2 Upstream flowby:	Inlet/MH Number: Inlet DP1 Total Street Flow: 17.0cfs
Flow Intercepted: 17.0cfs Inlet Size: 20' type R, SUMP	Flow Bypassed: 0.0cfs
<b>Street Capacity:</b> Street slope = 0.9%, cap	acity = 35.4cfs (half street) is okay

#### Design Point 1a

Design Point 1a is located on the south side of Center Village and accepts developed flows from Basin PR3. The runoff will be conveyed to Design Point 1a via curb/gutter. The street capacity of Street B (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR3 Upstream flowby:	Inlet/MH Number: Inlet DP1a Total Street Flow: 0.5cfs			
Flow Intercepted: 0.5cfs Inlet Size: 5' type R, sump	Flow Bypassed: 0.0cfs			
<b>Street Capacity:</b> Street slope = 0.9%, cap	acity = 8.0cfs, okay half flow from each side			
<u>(100-year storm)</u> Tributary Basins: PR3 Upstream flowby:	Inlet/MH Number: Inlet DP1a Total Street Flow: 0.9cfs			
Flow Intercepted: 0.9cfs Inlet Size: 5' type R, SUMP	Flow Bypassed: 0.0cfs			
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay				

#### Design Point 2

Design Point 2 is located on the south side of Center Village and is the total pipe flow from Des. Pts 1 & 1a. The runoff will be conveyed to Design Point 3 via a 24" storm sewer. The total pipe flow is 9.8cfs/17.8cfs in the 5/100-year storm events.

Design Point 3 is located on the north side of an access street and accepts developed flows from Basin PR6. The runoff will be conveyed to Design Point 3 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR6 Upstream flowby:	Inlet/MH Number: Inlet DP3 Total Street Flow: 3.1cfs	
Flow Intercepted: 3.1cfs Inlet Size: 10' type R, sump	Flow Bypassed: 0.0cfs	
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 8.0cfs, okay		
<u>(100-year storm)</u> Tributary Basins: PR6 Upstream flowby:	Inlet/MH Number: Inlet DP3 Total Street Flow: 5.6cfs	
Flow Intercepted: 5.6cfs Inlet Size: 10' type R, SUMP	Flow Bypassed: 0.0cfs	
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay		

#### <u>Design Point 3a</u>

Design Point 3a is located on the north side of an access street and is the total pipe flow from Des. Pts 2 & 3. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 12.5cfs/22.8cfs in the 5/100-year storm events.

#### Design Point 4

Design Point 4 is located on the south side of an access street and accepts developed flows from Basin PR4. The runoff will be conveyed to Design Point 4 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR4 Upstream flowby:	Inlet/MH Number: Inlet DP4 Total Street Flow: 7.2cfs	
Flow Intercepted: 5.9cfs Inlet Size: 10' type R, on-grade	Flow Bypassed: 1.3cfs to DP5	
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 8.0cfs, okay		
<u>(100-year storm)</u> Tributary Basins: PR4 Upstream flowby:	Inlet/MH Number: Inlet DP4 Total Street Flow: 13.1cfs	
Flow Intercepted: 8.1cfs Inlet Size: 10' type R, on-grade	Flow Bypassed: 5.0cfs to DP5	
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay		

Design Point 5 is located on the south side of an access street and accepts developed flows from Basin PR5. The runoff will be conveyed to Design Point 5 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

	PR5 1.3cfs from DP4	Inlet/MH Number: Inlet DP5 Total Street Flow: 1.7+1.3=3.0cfs		
Flow Intercepted:3.0cfsFlow Bypassed:0.0cfsInlet Size:5' type R, sump				
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 8.0cfs, okay				
<u>(100-year storm)</u> Tributary Basins: Upstream flowby:		Inlet/MH Number: Inlet DP5 Total Street Flow: 5.0+3.0=8.0cfs		
Flow Intercepted: Inlet Size: 5' type R	8.0cfs 8, sump	Flow Bypassed: 0.0cfs		
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay				

#### <u>Design Point 5a</u>

Design Point 5a is located on the south side of an access street and is the total pipe flow from Des. Pts 4 & 5. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 8.9cfs/16.1cfs in the 5/100-year storm events.

#### Design Point 6

Design Point 6 is located on the south side of an access street and is the total pipe flow from Des. Pts 3a & 5a. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 20.5cfs/37.3cfs in the 5/100-year storm events.

Design Point 7 is located on the east end of an access street and accepts developed flows from Basin PR1 which will be developed in the future. The runoff will be conveyed to Design Point 7 via future curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded. A future inlet will be designed and the size verified before construction at this design point when the adjacent lot is developed. Interim flows from this area (non-developed) will be conveyed south overland to a temporary sediment basin which flows into Inlet DP8 (5' Type R).

<u>(5-year storm)</u> Tributary Basins: PR1 Upstream flowby:	Inlet/MH Number: future Inlet DP7 Total Street Flow: 5.3cfs		
Flow Intercepted:5.3cfsFlow Bypassed:0.0cfsInlet Size:future 10' type R, sump			
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 8.0cfs, okay			
<u>(100-year storm)</u> Tributary Basins: PR1 Upstream flowby:	Inlet/MH Number: future Inlet DP7 Total Street Flow: 9.7cfs		
Flow Intercepted: 9.7cfs Inlet Size: future 10' type R, SUMP	Flow Bypassed: 0.0cfs		
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay			

#### Design Point 8

Design Point 8 is located on the east end of an access street and accepts developed flows from Basin PR8 which will be developed in the future. The runoff will be conveyed to Design Point 8 via future curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded. Interim flows from this area (non-developed) will be conveyed overland directly to a temporary sediment basin which flows into Inlet DP8 (5' Type R).

(5-year storm) Tributary Basins: PR8 Upstream flowby:	Inlet/MH Number: Inlet DP8 Total Street Flow: 0.9cfs		
Flow Intercepted:0.9cfsFlow Bypassed:0.0cfsInlet Size:5' type R, sump			
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 8.0cfs, okay			
<u>(100-year storm)</u> Tributary Basins: PR8 Upstream flowby:	Inlet/MH Number: Inlet DP8 Total Street Flow: 1.7cfs		
Flow Intercepted: 1.7cfs Inlet Size: 5' type R, SUMP	Flow Bypassed: 0.0cfs		
<b>Street Capacity:</b> Street slope = 0.9%, capacity = 35.4cfs (half street) is okay			

#### <u>Design Point 8a</u>

Design Point 8a is located on the east end of an access street and accepts developed flows from Basin PR7 which will be developed in the future. The runoff will be conveyed to Design Point 8a via future curb/gutter. The total surface flow is 6.0cfs/11.0cfs in the 5/100-year storm events. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded. A future inlet will be designed and the size verified before construction at this design point when the adjacent lot is developed.

#### Design Point 9

Design Point 9 is located on the south side of an access street and is the total pipe flow from Des. Pts 7, 8 & 8a. The runoff will be conveyed to Design Point 10 via a 24" storm sewer. The total pipe flow is 12.2cfs/22.4cfs in the 5/100-year storm events.

#### Design Point 10

Design Point 10 is located on the south side of an access street and is the total pipe flow from Des. Pts 6 & 9. The runoff will be conveyed to an existing 34"x53" HERCP. The total pipe flow is 31.5cfs/57.3cfs in the 5/100-year storm events. The allowable flow into the existing HERCP is 32.2cfs/59.0cfs per the Fontaine Blvd. Phase 1 FDR which designed the existing system.

#### 6.0 DETENTION AND WATER QUALITY PONDS

Detention and Storm Water Quality for Village at Lorson Ranch will be provided for in existing Pond G1/G2 located south of Fontaine Boulevard. Pond G1/G2 is an existing full spectrum detention pond constructed in 2017 as part of the Carriage Meadows South at Lorson Ranch Filing No. 1 subdivision (SF 1711) per El Paso County criteria. Pond G1/G2 was as-builted and certified on June 27, 2023 by Core Engineering Group. A copy of the certification letter, as-builts, and a pond drainage area map are located in the appendix of this report.

For additional information, see the approved Final Drainage Report and Plan for "Carriage Meadows South at Lorson Ranch Filing No. 1, SF 1711, dated 08/10/2017.

The following text was taken from the Carriage Meadows South final drainage report:

#### Detention Pond G1/G2 (Full Spectrum Design), (District Facility, SF1711)

This is an on-site permanent full spectrum detention pond that includes water quality. Pond G1/G2 is designed as a single pond in the UDCF Full Spectrum spreadsheets. The full spectrum print outs are in the appendix of this report. See map in appendix for watershed areas. This pond is sized to provide full spectrum and water quality for the Brownsville Subdivision No. 2 should it become a part of Lorson Ranch.

- Watershed Ares: 96 acres
- Watershed Imperviousness: 79%
- Hydrologic Soils Group A, B, C/D
- Zone 1 WQCV: 2.301 ac-ft, WSEL: 5683.93
- Zone 2 EURV: 8.104 ac-ft, WSEL: 5686.29
- Zone 3 (100-yr): 12.881ac-ft, WSEL: 5687.93
- Pipe Outlet: 36" RCP at 0.4%
- 5-yr outflow = 4.2cfs, 100-yr outflow = 55.6cfs

#### 7.0 DRAINAGE AND BRIDGE FEES

Village at Lorson Ranch is located within the Jimmy Camp Creek drainage basin which is currently a fee basin in El Paso County. Current El Paso County regulations require drainage and bridge fees to be paid for platting of land as part of the plat recordation process. Lorson Ranch initiated the closure of Jimmy Camp Creek drainage basin for drainage/bridge fees a few years ago and will be approved by El Paso County and the Pikes Peak Drainage Board before this plat is recorded. In the event the basin isn't closed Lorson Ranch has interim agreements with the county that no fees are required at this time. Therefore, no drainage fees or bridge fees are required to be paid at this time. A copy of the drainage board meeting minutes is in the appendix of this report.

Item	Quantity	Unit	Unit Cost	Item Total
5' Inlet	3	EA	\$5,000/EA	\$15,000
10' Inlet	4	EA	\$8,000/EA	\$32,000
20' Inlet	1	EA	\$12,000/EA	\$12,000
18" Storm	206	LF	\$180	\$37,080
24" Storm	351	LF	\$240	\$84,240
36" Storm	73	LF	\$360	\$26,280
Manholes	2	EA	\$10,000	\$20,000
			Subtotal	\$226,600
			Eng/Cont (10%)	\$22,660
		Total Est. Cost	\$249,260	

Table 7.1:	Private Drainage Facility	Costs	(non-reimbursable)
	I III ato Brainago I aoint		

#### 8.0 FOUR STEP PROCESS

The site has been developed to minimize wherever possible the rate of developed runoff that will leave the site and to provide water quality management for the runoff produced by the site as proposed on the development plan. The following four step process should be considered and incorporated into the storm water collection system and storage facilities where applicable.

#### Step 1: Employ Runoff Reduction Practices

Village at Lorson Ranch has employed several methods of reducing runoff.

- The street configuration was laid out to minimize the length of streets. Many streets are straight and perpendicular resulting in lots with less wasted space. Landscape buffers are provided for adjacent residential development
- Utilize existing Full Spectrum Detention Outlet Structure (Pond G1/G2) which has been previously constructed and sized for runoff from this development. The full spectrum detention mimics existing storm discharges and includes water quality.

#### Step 2: Stabilize Drainageways

Jimmy Camp Creek is a major drainageway located east of this site. In 2006 Jimmy Camp Creek was reconstructed and stabilized per county criteria. The design included a natural sand bottom and armored sides.

#### Step 3: Provide Water Quality Capture Volume

Treatment of the water quality capture volume (WQCV) is required for all new developments. Village at Lorson Ranch utilizes an existing full spectrum stormwater extended detention basin outlet structure within existing Pond G1/G2 which include Water Quality Volumes and WQ outlet structures.

#### Step 4: Consider Need for Industrial and Commercial BMP's

There are no industrial areas within this site. This site is commercial but will be mostly light use commercial areas such as restaurants, gas station, mini storage, etc which does not need specific BMP's.

#### 9.0 CONCLUSIONS

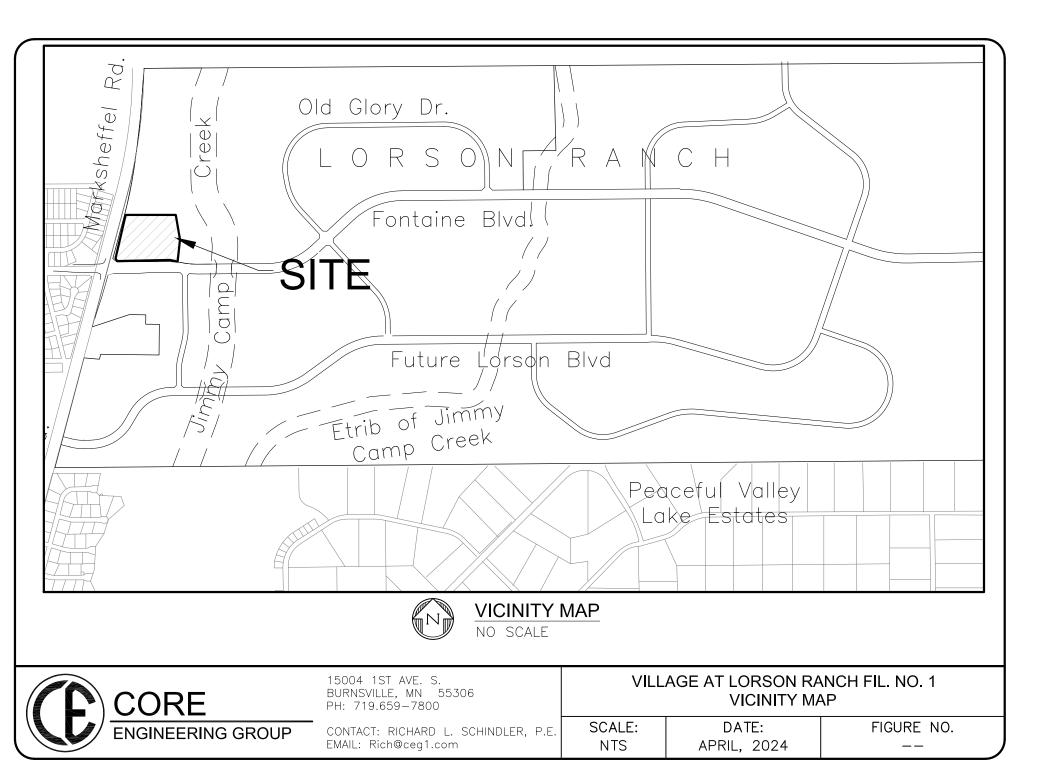
This drainage report has been prepared in accordance with the City of Colorado Springs/El Paso County Drainage Criteria Manual. The proposed development and drainage infrastructure will not cause adverse impacts to adjacent properties or properties located downstream. Several key aspects of the development discussed above are summarized as follows:

- Developed runoff will be conveyed via curb/gutter and storm sewer facilities
- Jimmy Camp Creek has been reconstructed east of this study area
- Detention and water quality for this site will be provided in Pond G1/G2 constructed as part of Carriage Meadows South (SF1711)

#### 10.0 REFERENCES

- 1. City of Colorado Springs/El Paso County Drainage Criteria Manual DCM, dated November, 1991
- 2. Soil Survey of El Paso County Area, Colorado by USDA, SCS
- 3. Jimmy Camp Creek Drainage Basin Planning Study, Dated March 9, 2015, by Kiowa Engineering Corporation
- 4. City of Colorado Springs "Drainage Criteria Manual, Volume 2
- 5. El Paso County "Engineering Criteria Manual"
- 6. Lorson Ranch MDDP 1, November 7, 2006 by Pentacor.
- 7. El Paso County Resolution #15-042, El Paso County adoption of Chapter 6 and Section 3.2.1 of the City of Colorado Springs Drainage Criteria Manual dated May, 2014.
- 8. Final Drainage Report for Fontaine Boulevard Phase 1 Improvements prepared by Pentacor, dated November, 2006
- 9. Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 prepared by Core Engineering Group, Reference SF1711, approved September 7, 2017
- 10. Final Drainage Report for Carriage Meadows North prepared by Core Engineering Group, Reference SF1723, approved April 12, 2018

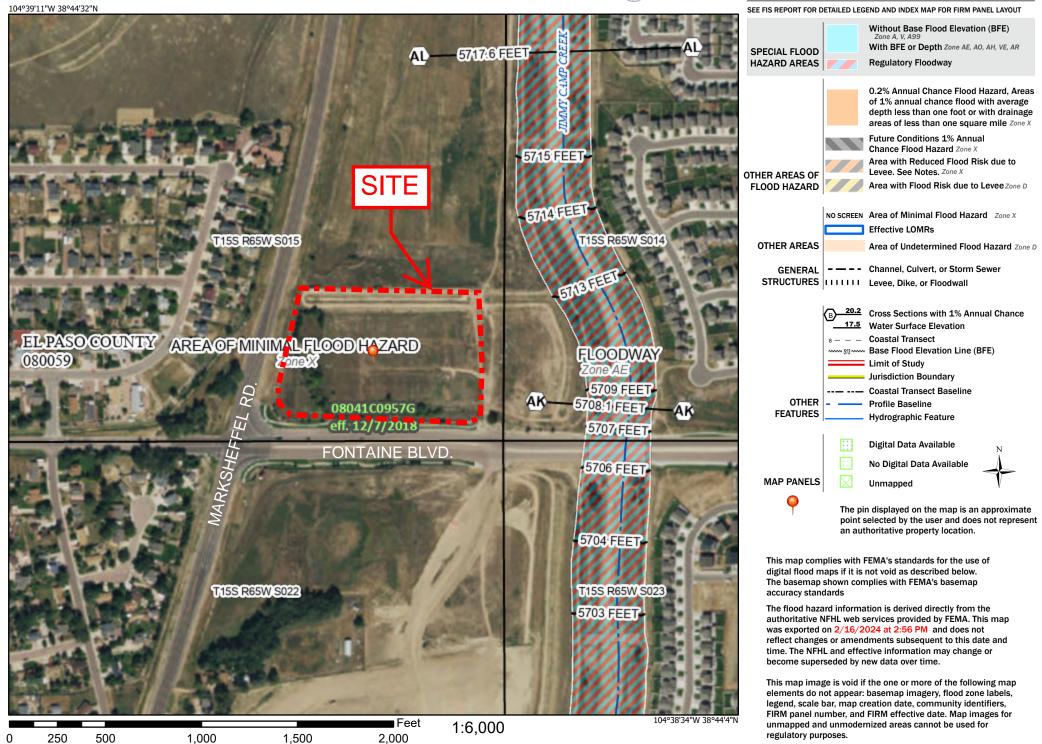
#### APPENDIX A – VICINTIY MAP, SOILS MAP, FEMA MAP



## National Flood Hazard Layer FIRMette



#### Legend



Basemap Imagery Source: USGS National Map 2023



Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

### El Paso County Area, Colorado

#### 28—Ellicott loamy coarse sand, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 3680 Elevation: 5,500 to 6,500 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 47 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Ellicott and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Ellicott**

#### Setting

Landform: Stream terraces, flood plains Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium

#### **Typical profile**

A - 0 to 4 inches: loamy coarse sand C - 4 to 60 inches: stratified coarse sand to sandy loam

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: NoneFrequent
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A Ecological site: R069XY031CO - Sandy Bottomland Other vegetative classification: SANDY BOTTOMLAND (069AY031CO) Hydric soil rating: No

USDA

#### **Minor Components**

#### Fluvaquentic haplaquoll

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

#### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

#### **Data Source Information**

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022



## El Paso County Area, Colorado

## 52—Manzanst clay loam, 0 to 3 percent slopes

## Map Unit Setting

National map unit symbol: 2w4nr Elevation: 4,060 to 6,660 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 50 to 54 degrees F Frost-free period: 130 to 170 days Farmland classification: Prime farmland if irrigated

## **Map Unit Composition**

Manzanst and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Manzanst**

## Setting

Landform: Drainageways, terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave, linear Parent material: Clayey alluvium derived from shale

## **Typical profile**

A - 0 to 3 inches: clay loam Bt - 3 to 12 inches: clay Btk - 12 to 37 inches: clay Bk1 - 37 to 52 inches: clay Bk2 - 52 to 79 inches: clay

## **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Gypsum, maximum content: 3 percent
Maximum salinity: Slightly saline (4.0 to 7.0 mmhos/cm)
Sodium adsorption ratio, maximum: 10.0
Available water supply, 0 to 60 inches: High (about 9.0 inches)

## Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4c

USDA

*Hydrologic Soil Group:* C *Ecological site:* R067BY037CO - Saline Overflow *Hydric soil rating:* No

### **Minor Components**

#### Ritoazul

Percent of map unit: 7 percent Landform: Interfluves, drainageways Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY042CO - Clayey Plains Hydric soil rating: No

### Arvada

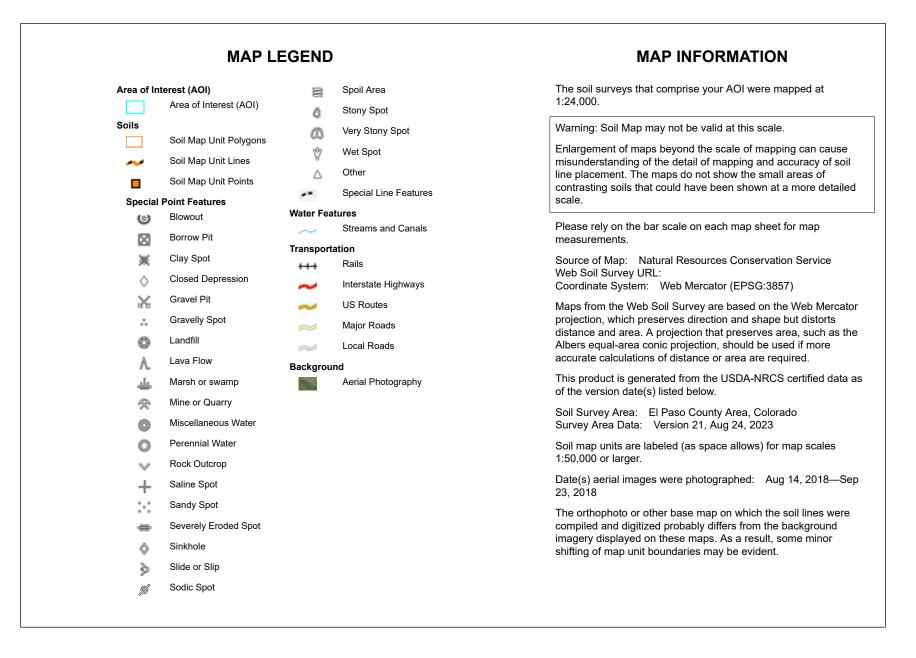
Percent of map unit: 6 percent Landform: Interfluves, drainageways Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY033CO - Salt Flat Hydric soil rating: No

## Wiley

Percent of map unit: 2 percent Landform: Interfluves Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY002CO - Loamy Plains Hydric soil rating: No

## **Data Source Information**

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022





## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	0.1	1.2%
52	Manzanst clay loam, 0 to 3 percent slopes	8.5	98.8%
Totals for Area of Interest		8.6	100.0%



CORE
ENGINEERING GROUP

## Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

	1		UP	Date: A	April, 20	: <u>Leonar</u> <u>24</u> _eonard off			1	Total	Runoff		Project Design	o: <u>100.0</u> t: Village <u>i Storm:</u> reet	70 e at Lors <u>5 - Yea</u>	on Ran <u>r Event</u> Pipe	nch FDR t <b>(Curre</b>	ent)	ravel Tir	ne	
Street or Basin	Design Point	Area Design	Area (A)	Runoff Coeff. (C)	tc	CA		Ø	tc	Σ (CA)		a	Slope	Street Flow		Slope	Pipe Size	Length	Velocity	tt	Remarks
		Ā	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX1			0.95	0.15	40.3	0.14	2.04	0.3													
EX2			8.44	0.15	26.4	1.27	2.68	3.4													
EX3			0.73	0.15	11.1	0.11	3.98	0.4													
EX4			0.57	0.90	5.0	0.51	5.17	2.6													
													-								
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### Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

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				Checke	ed By: <u>L</u> ect Run	eonard. off	Beasley	<u> </u>		Total R	unoff		Desigr	n <u>Storm</u> eet	: <u>100-Y</u>	Pipe	ent (Cu	urrent) ⊤r	avel Tir	ne l	
Street or Basin	Design Point	Area Design	Area (A)	Runoff Coeff. (C)	to to	CA		Ø	tc	Σ (CA)		Ø	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	tt	Remarks
		Ar	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX1			0.95	0.50	40.3	0.48	3.42	1.6													
EX2			8.44	0.50	26.4	4.22	4.49	19.0													
EX3			0.73	0.50	11.1	0.37	6.68	2.4													
EX4			0.57	0.96	5.0	0.55	8.68	4.7													
														1					<u> </u>		

						13	PROJECT NA PROJECT NL ENGINEER: 1	ME: Village at 1 IMBER: 100.07 LAB 2024	Lorson Ranch '0	FDR		20
	15004 1st A Burnsville, M						DATE: April, 2	2024				
		<i>lopment Drain</i> CONDITION Hydro	IS COEFFICIE	NT "C" CALCUL								
BASIN	Soil No.	Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Impervious	Type of Cover
EX1	52	С	0.95	100.00%	0.15		0.50		51		0%	Pasture/Meadow
EX0	50	0	0.44	100.000/	0.45		0.50		<b>F</b> 1		00/	Desture (Messieur
EX2	52	С	8.44	100.00%	0.15		0.50		51		0%	Pasture/Meadow
EX3	52	С	0.76	100.00%	0.15		0.50		51		0%	Pasture/Meadow
LAG	52	0	0.70	100.0070	0.10		0.00		51		070	T astarc/weadow
EX4	52	С	0.66	100.00%	0.90		0.96		51		100%	Paved Road

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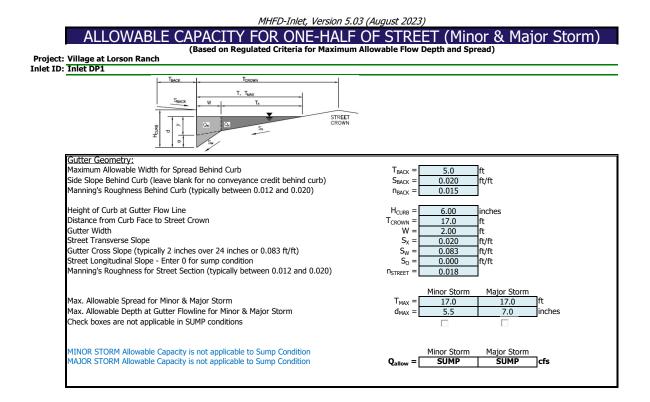
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	ENGI	NEERIN	ig grou	IP	Date: Feb. Checked B	15, 2024				Project: Villa		Ranch FDR	
	Sub-Ba	asin Data		Ir	nitial Overla	-	-		7	Travel Time (t	t)		Final tc
BASIN or DESIGN	C₅	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	Ti minutes	LENGTH (L) feet	Computed tC Minutes	USDCM Recommended tc=ti+tt (min)			
EX1	0.15	0.95	15.0	51.00	10.78%	0.15	5.59	1398.00	0.20%	0.67	34.73	40.32	40.32
EX2	0.15	8.44	7.0	226.00	3.10%	0.21	17.81	229.00	1.31%	0.80	4.76		
			15.0					284.00	0.70%	1.25	3.77	26.35	26.35
EX3	0.15	0.73	15.0	37.00	4.05%	0.09	6.58	442.00	1.20%	1.64	4.48	11.06	11.06
EX4	0.90	0.66	20.0	22.00	2.00%	0.27	1.35	462.00	1.75%	2.65	2.91	4.26	4.26

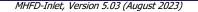
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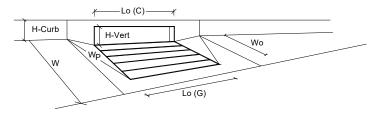
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		NG GROU	JP	Date: A	April <u>, 20</u>	<u>Leonar</u> 24 .eonard		-					Project	: <u>100.0</u> : Village Storm:	at Lor	son Rar I <b>r Even</b> t	nch FDR t <b>(Devel</b>	(oped)			
	it			Dire	ect Run	off	r.	r		Total I	Runoff			Str	eet				Pipe		
Street or Basin	Design Point	Area Design	Area (A)	Runoff Coeff. (C)	t t	CA	. <u> </u>	Ø	t t	Σ (CA)	. <u> </u>	Ø	Slope / Pipe Slope	Full Street Max Flow	Max Allow street flow	Street Velocity	Design Pipe Flow	Slope	Pipe Size	Min Pipe Flow	Pipe Velocity
		<	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	min	cfs	%	in	cfs	fps
EX1			0.95	0.15	40.3	0.14	2.04	0.3													
EX3			0.73	0.15	11.1	0.11	3.98	0.4													
EX4			0.57	0.90	5.0	0.51	5.17	2.6													
PR1	7		1.24	0.83	5.0	1.03	5.17	5.3													
PR2	1		2.41	0.83	6.9	2.00	4.68	9.4													
PR3	1a		0.11	0.83	5.0	0.09	5.17	0.5													
(PR2-PR3)	2	2.52		0.83					6.9	2.09	4.68	9.8									
PR4	4		1.68	0.83	5.0	1.39	5.17	7.2													
PR5			0.39	0.83	5.0	0.32	5.17	1.7													
(PR4-PR5)	5a	2.07		0.83					5.0	1.72	5.17	8.9									
PR6 (PR2,PR3&PR6)	3a		0.72	0.83	5.0	0.60	5.17	3.1	7.0	2.69	4.66	12.5									
(PR2-PR6)	6	5.31		0.83					7.1	4.41	4.65	20.5									
PR7	8a		1.41	0.83	5.0	1.17	5.17	6.0													
PR8	8		0.22	0.83	5.0	0.18	5.17	0.9													
(PR1,PR7&PR8)	9	2.87							5.1	2.38	5.14	12.2									
(PR1-PR8)	10	8.18							7.1	6.79	4.64	31.5									

Or Basin EX1	RIN	G GROL	JP	Calcula Date: A		Leonar	d Reasl														
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		Design	(A)							(CA)			e / Iope			et city	gn -Iow	e		v v	e city
	5	Area De	Area (A)	Runoff Coeff. (C)	tc	CA		Ø	tc	Σ (C		Ø	Slope / Pipe Slope	Full Street Max Flow	Max Allow street flow	Street Velocity	Design Pipe Flow	Slope	Pipe Size	Min Pipe Flow	Pipe Velocity
EX1		A	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	min	cfs	%	ft	cfs	fps
I			0.95	0.50	40.3	0.48	3.42	1.6													
EX3			0.73	0.50	11.1	0.37	6.68	2.4													
EX4			0.57	0.96	5.0	0.55	8.68	4.7													
PR1 7			1.24	0.90	5.0	1.12	8.68	9.7													
PR2 1			2.41	0.90	6.9	2.17	7.85	17.0													
PR3 1a	a		0.11	0.90	5.0	0.10	8.68	0.9													
(PR2-PR3) <b>2</b>		2.52		0.90					7.0	2.27	7.83	17.8									
PR4 4			1.68	0.90	5.0	1.51	8.68	13.1													
PR5			0.39	0.90	5.0	0.35	8.68	3.0													
(PR4-PR5) 5a	a	2.07		0.90					5.0	1.86	8.66	16.1									
PR6 3a	a		0.72	0.90	5.0	0.65	8.68	5.6	7.0	2.92	7.83	22.8									
(PR2-PR6) <b>6</b>	;	5.31		0.90					7.1	4.78	7.81	37.3									
PR7 8a	a		1.41	0.90	5.0	1.27	8.68	11.0													
PR8 8			0.22	0.90	5.0	0.20	8.68	1.7													
(PR1,PR7&PR8) 9		2.87							5.0	2.58	8.68	22.4									
(PR1-PR8) <b>10</b>	D	8.18	8.18	0.90	7.1	7.36	7.79	57.3	7.1	7.36	7.79	57.3									

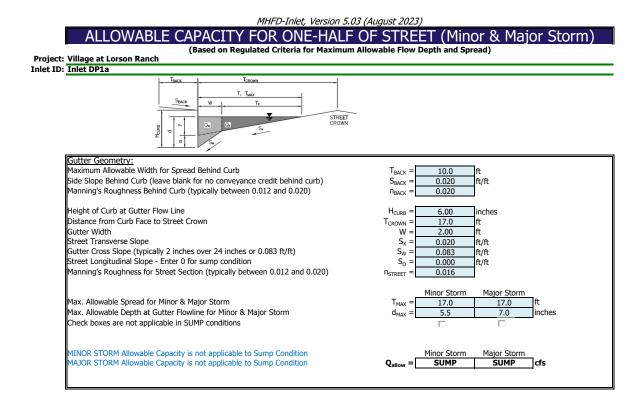
Œ	) <u>CC</u>	DRE						of Concen	tration-Pr	<u>roposed</u>		00.070			
	ENG	INEER	ING GR		Calculated Date: <u>Apri</u> Checked I	il <u>, 2024</u>					Job No: <u>1</u> Project: <u>V</u>		rson Ranch		
:	Sub-Ba	sin Data		Ini	tial Overla	nd Time (†	ti)		Tr	avel Time	(tt)			(urbanized sins)	Final tc
BASIN or DESIGN	C₅	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	(S) (V) Ti (L) (S) (V) Tt							TOTAL LENGTH (L) feet	Regional tc tc=(L/180)+10 minutes	USDCM Recommended Tc=Tı+Tt (mın)
EX1	0.15	0.95	15.0	51.00	10.78%	0.15	5.59	1398.00	0.20%	0.67	34.73	40.32			40.32
EX3	0.15	0.73	15.0	37.00	4.05%         0.09         6.58         442.00         1.20%         1.64         4.48         11.06										11.06
EX4	0.90	0.66	20.0	22.00	2.00%	0.27	1.35	462.00	1.75%	2.65	2.91	4.26			4.26
PR1	0.90	1.24	20.0	15.00	2.00%	0.22	1.12	410.00	1.22%	2.21	3.09	4.21	425.00	12.36	4.21
PR2	0.90	2.41	7.0	36.00	2.00%	0.35	1.73	114.00	1.00%	0.70	2.71				
			20.0					300.00	1.00%	2.00	2.50	6.94	450.00	12.50	6.94
PR3	0.90	0.11	20.0	22.00	2.00%	0.27	1.35	128.00	1.00%	2.00	1.07	2.42	150.00	10.83	2.42
PR4	0.90	1.68	20.0	10.00	2.00%	0.18	0.91	597.00	1.60%	2.53	3.93	4.85	607.00	13.37	4.85
PR5	0.90	0.39	20.0	10.00	1.96%	0.18	0.92	353.00	1.60%	2.53	2.33	3.24	363.00	12.02	3.24
PR6	0.90	0.72	20.0	10.00	2.00%	0.18	0.91	368.00	1.34%	2.32	2.65	3.56	378.00	12.10	3.56
PR7	0.90	1.41	20.0	15.00	2.20%	0.23	1.08	320.00	1.56%	2.50	2.14	3.22	335.00	11.86	3.22
PR8	0.90	0.22	20.0	25.00	2.00%	0.29	1.44	108.00	1.56%	2.50	0.72	2.16	133.00	10.74	2.16

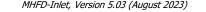


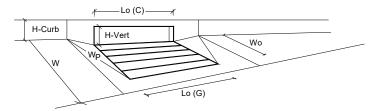




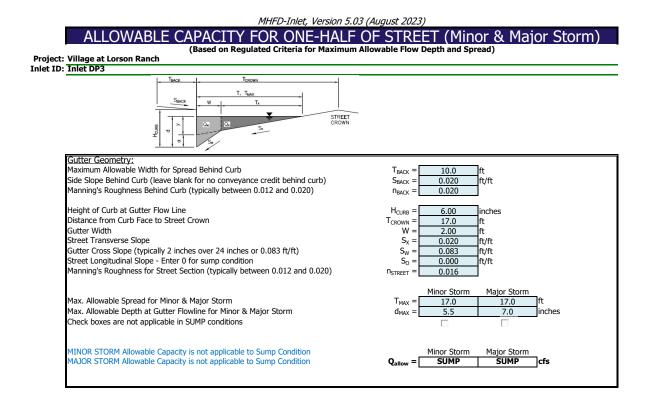
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	6.9	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Grate</sub> =	0.29	0.41	ft
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.75	0.84	-
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{Combination} =$	N/A	N/A	-
combination milet renormance reduction ractor for Long milets	Combination =	11/74	N/A	_
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	9.8	18.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	9.4	17.0	cfs

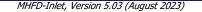


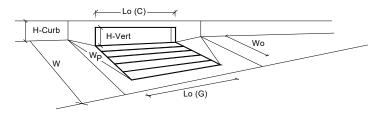




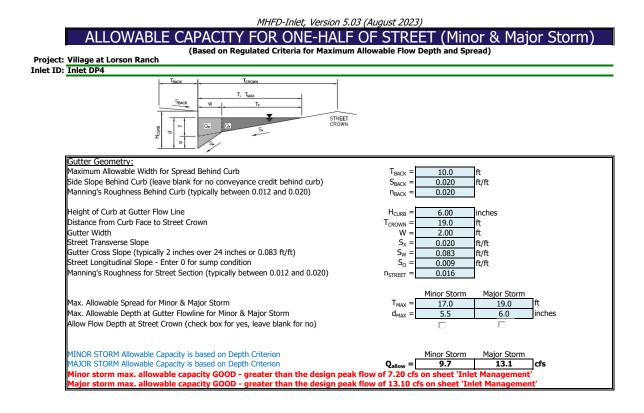
CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	1
	_			
	<b>c</b> 5	MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	<b>4.4</b> 0.5	<b>4.6</b> 0.9	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	0.5	0.9	us



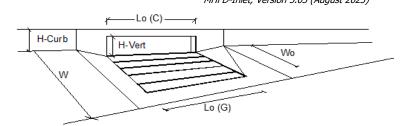




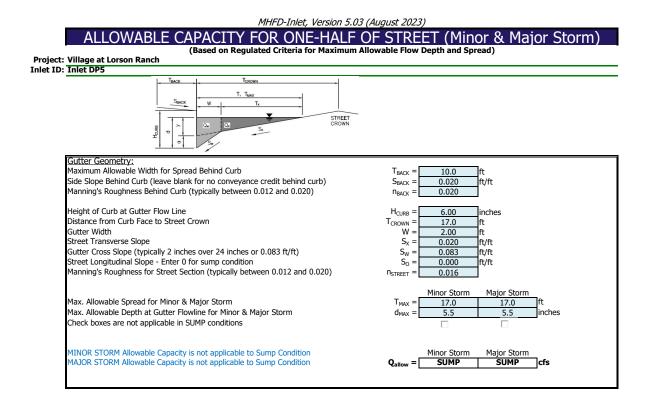
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{0}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.90	0.91	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	6.6	6.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{\text{PEAK REQUIRED}} =$	3.1	5.6	cfs

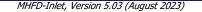


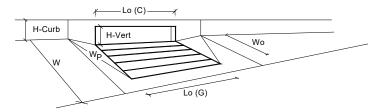
## INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.03 (August 2023)



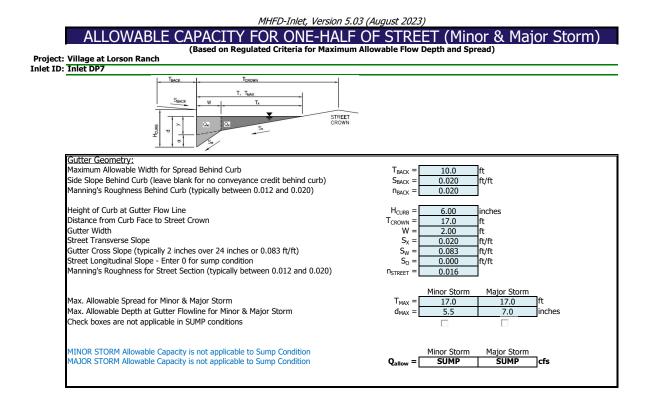
Design Information (Input)	-	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10	10.10	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	-	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.9	8.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	1.3	5.0	cfs
Capture Percentage = $Q_a/Q_o$	C% =	81	61	%

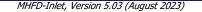


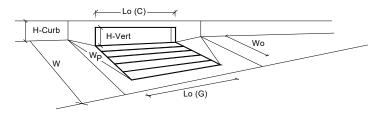




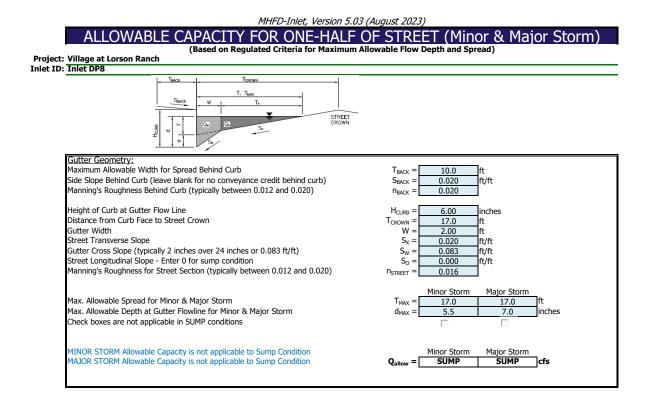
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	-	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	linches
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	7.2	inches
Grate Information	Ponding Depth =	MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_0 =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	icet
Clogging Factor for a Single Grate (typical values 0.15-0.50)	$A_{ratio} = C_f(G) =$	N/A N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{f}(G) = C_{w}(G) $	N/A	N/A	-
Grate Orifice Coefficient (typical value 2.15 - 5.00)	$C_{0}(G) = C_{0}(G) = C_{0}(G)$	N/A N/A	N/A	-
Curb Opening Information	C <sub>0</sub> (O) =	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	leet
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) = C_{w}(C) = C_{w}(C)$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 2.5 5.7)	$C_{0}(C) = C_{0}(C) = C_{0}(C)$	0.67	0.67	-
	-0 (-)	0.07	0107	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.29	0.43	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
				-
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	4.4	8.0	cfs
WARNING: Inlet Capacity < Q Peak for Major Storm	$Q_{PEAK REQUIRED} =$	3.0	8.0	cfs

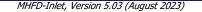


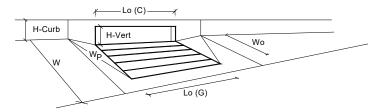




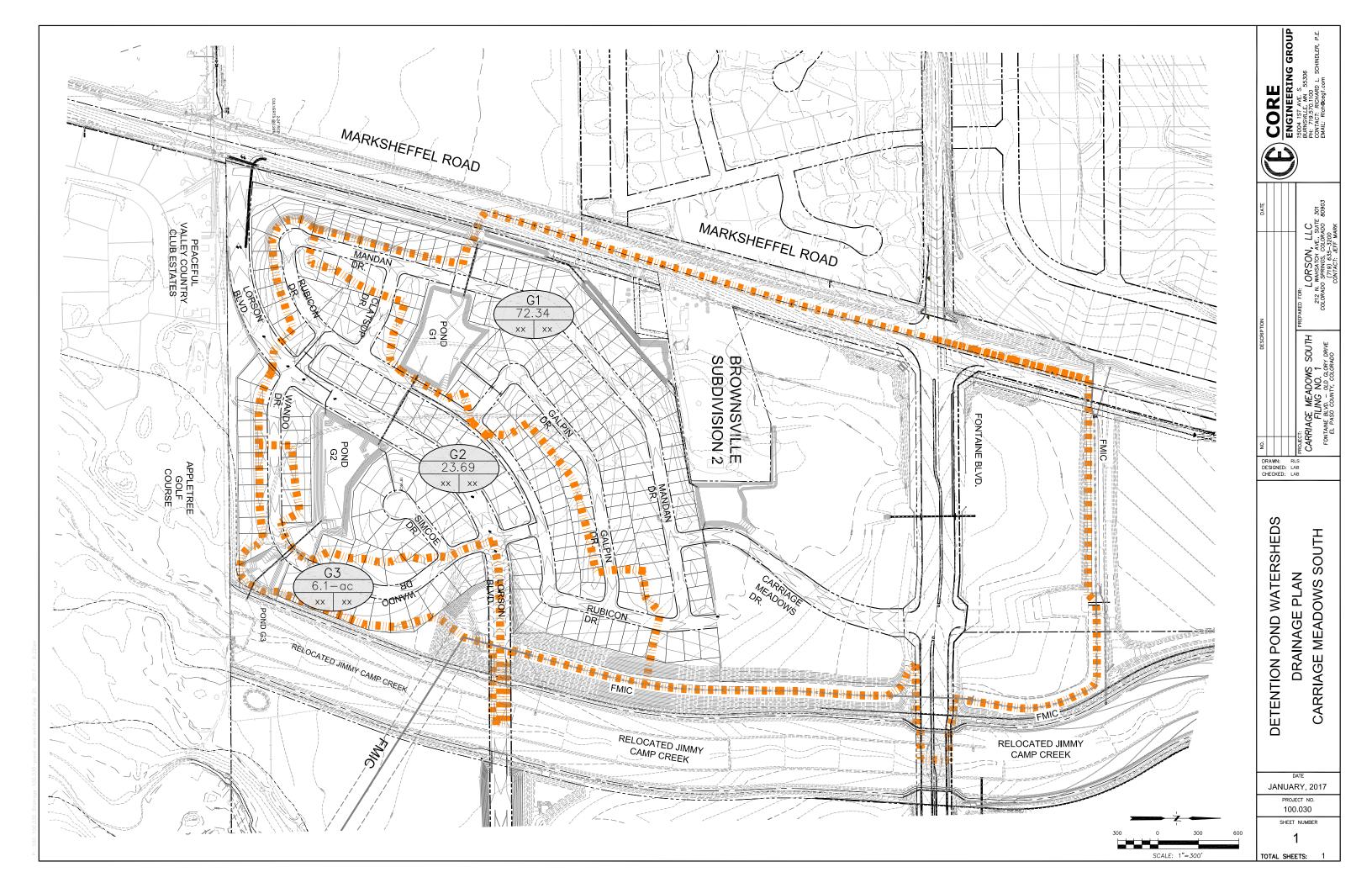
CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	6.5	inches
Grate Information		MINOR	MAJOR	<ul> <li>Override Depths</li> </ul>
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}$ (G) =		N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.29	0.38	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	-
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.90	0.96	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	_	MINOR	MA100	
	o _1	MINOR 6.6	MAJOR 10.2	-fe
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	<b>5.</b> 3	9.7	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	5.5	9.7	us







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	-	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information	r onding bepar	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>0</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	compandon	,		-
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	4.4	4.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	0.9	1.7	cfs





June 27, 2023

El Paso County Planning and Community Development 2880 International Circle, Suite 110 Colorado Springs, CO 80910

RE: Carriage Meadows South Filing No. 1 (SF 17-011) Certification Letter

Dear El Paso County PCD,

Based upon information gathered from as-built surveys and periodic visits to the project, Core Engineering Group is of the opinion that the subdivision improvements have been constructed in general conformance with the approved design plans as filed with El Paso County.

The site and adjacent properties (as affected by work performed under the County permit) appear to be stable with respect to settlement and subsidence, sloughing of cut and fill slopes, revegetation or other ground cover, and the improvements (public improvements, common development improvements, site grading and paving) visually appear to meet or exceed the minimum design requirements. There have been some service line utility trench settlements but that is currently being addressed as part of the punchlist process.

The sanitary and watermain located in the public ROW has also been completed in accordance with Widefield Water and Sanitation Districts criteria.

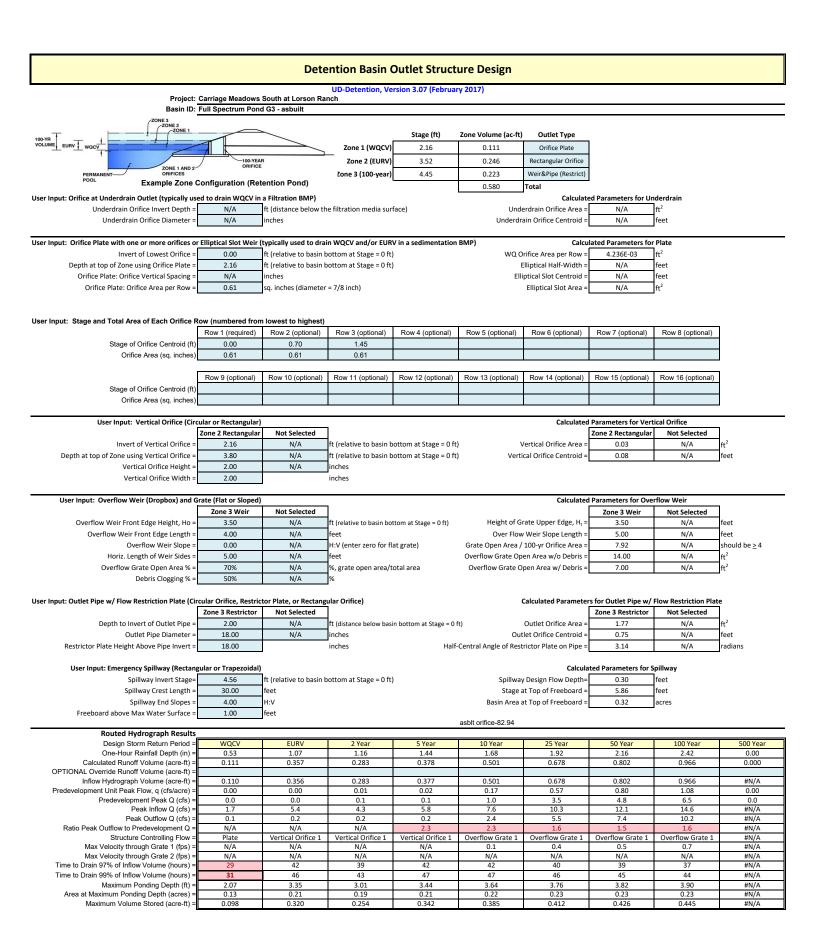
In addition, Core Engineering Group has verified that the Extended Detention Basin/WQ Pond G1, G2, and G3 have been constructed and certified and meet the volume and elevation requirements and have been constructed in general compliance with the approved construction plans. The outlet structure for Pond G3 did change slightly from the design so the full spectrum spreadsheet was updated for this pond and it meets the design output as shown in the approved final drainage report.

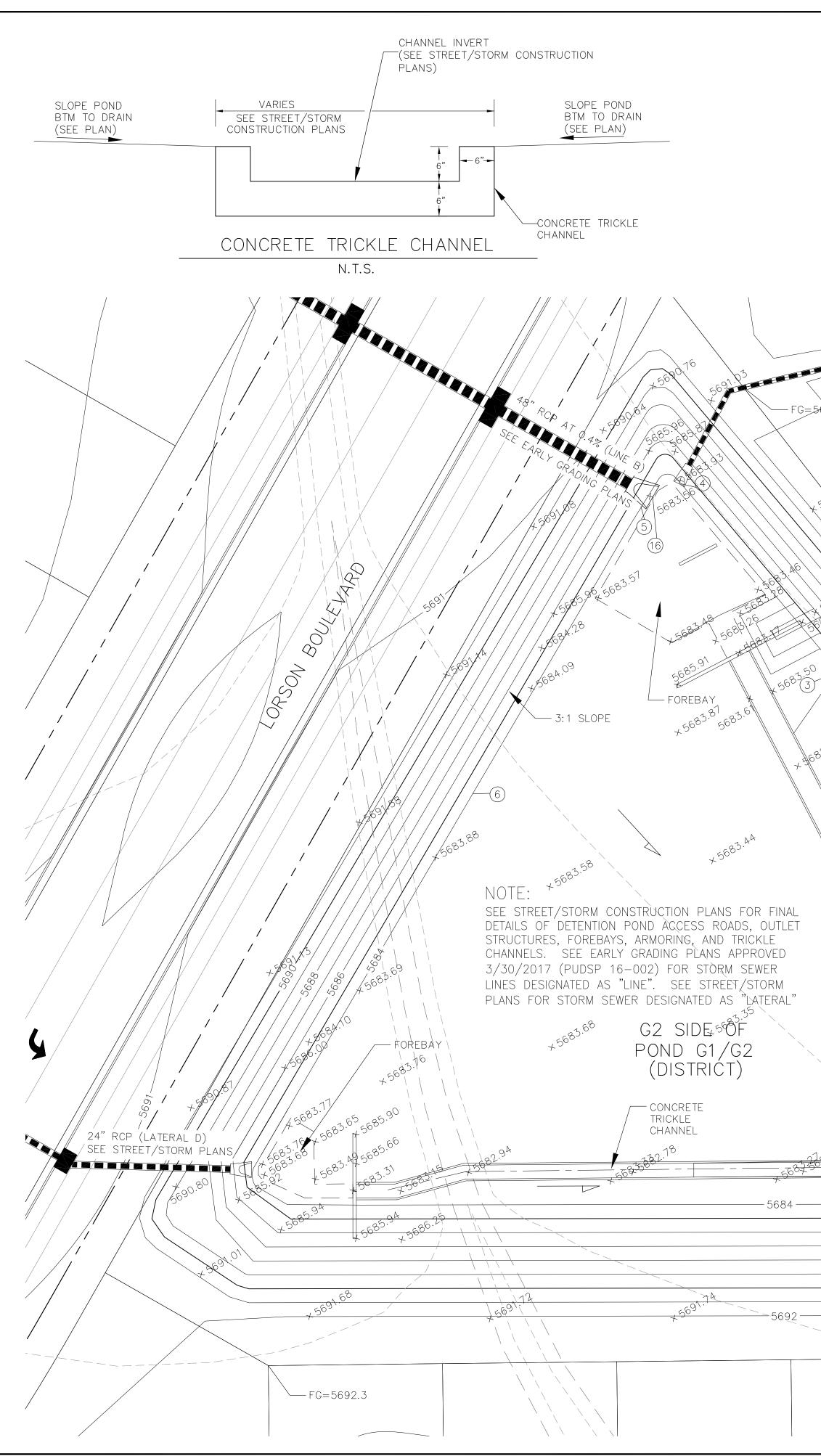
Based on information gathered during construction and post-construction, Core Engineering Group is of the opinion that the public streets and storm sewer have been constructed in general accordance with the approved construction documents.



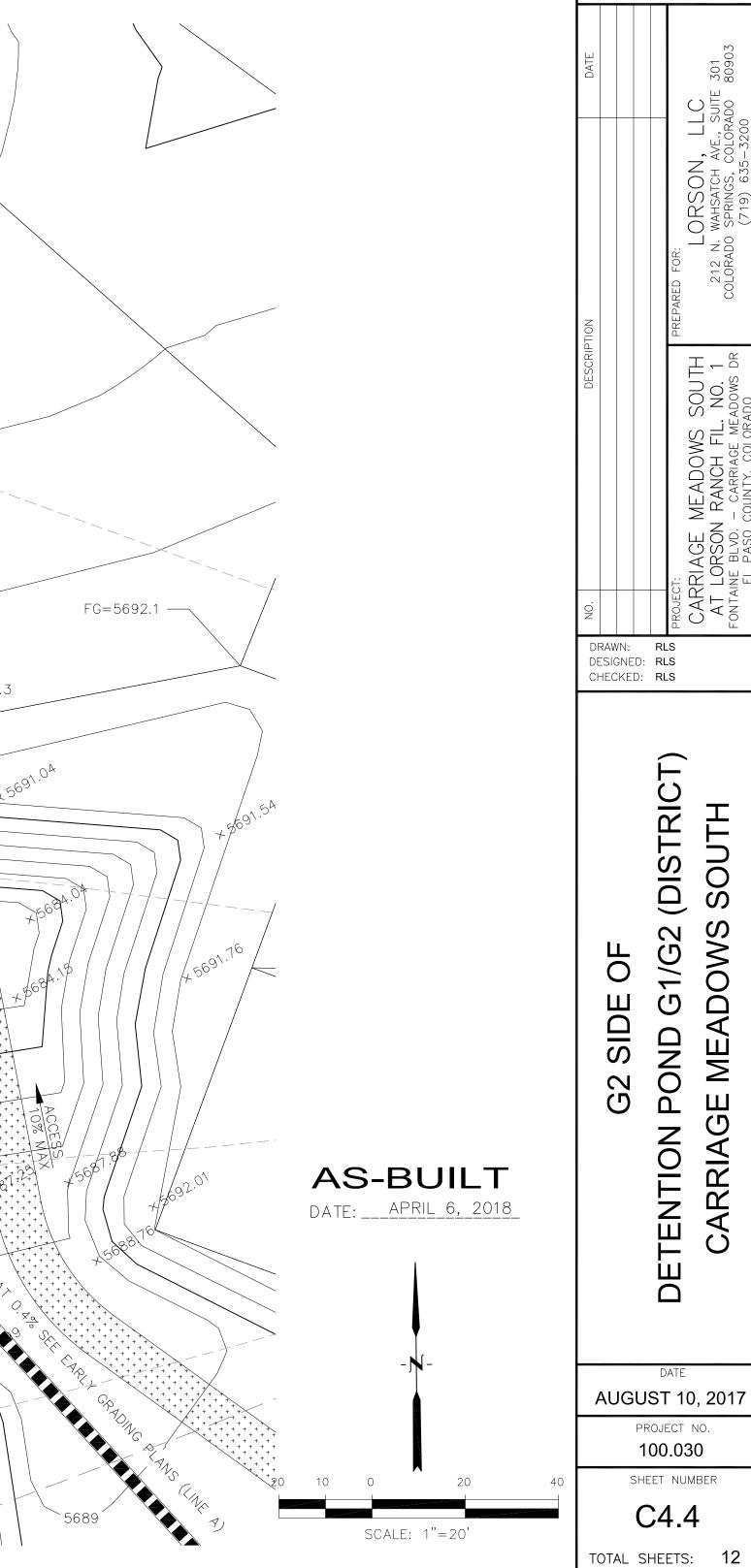
Pond G1/G2, G3 As-builts Street/storm As-builts

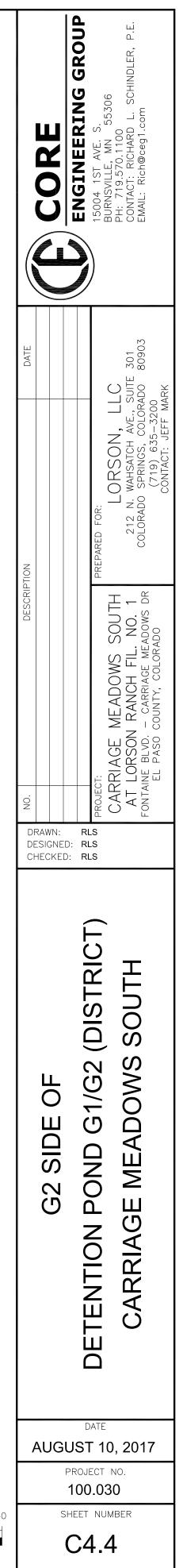
UD-Detention, Version 3.07 (February 2017)           Project: Carriage Meadows South at Loron Ranch           Basin ID: Full Spectrum Pond G3 - abuilt           Secure Configuration (Retention Pond)           Required Volume Calculation           Solected BPP Type         Colspan="2">Colspan="2"Colspa=""2"Colspan="2"Colspan="2"Colspan="2"Colspan="2"C	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	Volume (ft*3) 694 4,269 11,477	Volum (ac-ft)
Note of the second se	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	(ft*3) 694 4,269	(ac-ft)
asbt orffice=82.4           Depth forement         Optional           squired Volume Calculation           Selected BMP Type - Watershed Area = Watershed Area = 55.00%         Selected BMP Type - E2000         Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan= Colspan="2">Colspan="2">Colspan= Colspan="2">Colspan="2">Colspan="2">Colspan= Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan= Colspan="2">Colspan="2"Colspan="	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	(ft*3) 694 4,269	(ac-ft
Deck investige         Deck investige         Deck investige         Optional         Optional           Process         Example Zone Configuration (Retention Pond)         Stage - Storage	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	(ft*3) 694 4,269	(ac-ft
Depth Increment         0.1         1           Proc.         Example Zone Configuration (Retention Pond)         Stage - Skrage         Stage - Skrage         Stage - Skrage         Optional         (n)	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	(ft*3) 694 4,269	(ac-ft
Proc.         Example Zone Configuration (Retention Pond)         Stage - Strage Stage Stage Stage (Net Net Net Net Net Net Net Net Net Net	de         Area (acre)           0.001         0.029           0.134         0.134           0.197         0.242           1         0.251	(ft*3) 694 4,269	(ac-ft
Description         (i)         (ii)         (iii)         (iiii)         (iii)	0.001 0.029 0.134 0.134 0.197 9 0.242 1 0.251	694 4,269	
Solectod DMP Type = Watershed Area = Watershed Area = Watershed Stope = Watersh	0.029           0.134           0.197           9           0.242           1           0.251	4,269	
Watershed Area = Watershed Lingh =         6.02         acres         5685         -         2.05         -         -         -         6.84           Watershed Lingh =         730         h         5695         -         3.06         -         -         8.85           Watershed Singh =         0.016         ht         5697         -         4.06         -         -         10.5           Watershed Singh =         560%         percent         597=5677.22         -         4.28         -         -         -         10.9           Parcentage Phytotogic Sol Convert         597=5677.81         -         4.28         -         -         -         10.9	0.134 0.197 0.242 1 0.251	4,269	
Watershed Stope =         0.016         htt         5687         -         4.06         -         -         1         10.5           Watershed snope =         55.00%         percent         59/r=5687.22         -         4.28         -         -         10.0           Percentage Mydiodpic Sci Groups Acody         0.01%         percent         100/r=5687.81         -         4.27         -         -         10.9	9 0.242 1 0.251	11.477	0.098
Watershed Imperviousness         55.00%         percent         9yr=5687.22         -         4.28         -         -         10,9           Percentage Hydrologic Sol Group A =         0.0%         percent         100yr=5687.81         -         4.87         -         -         11,9	1 0.251		0.263
Percentage Hydrologic Soil Group A = 0.0% percent 100yr=5687.81 4.87 11,9		21,034	0.483
		23,395 30,141	0.537
Percentage Hydrologic Soil Group B = 100.0% percent 5688 5.06 12,2		32,443	0.745
Percentage Hydrologic Soil Groups C/D = 0.0% percent 5689 - 6.06 14,1	0 0.324	45,632	1.048
Desired WQCV Drain Time = 40.0         hours                Location for 1-hr Rainfail Depths = User hput			
Location or nin rainstance pepers - Geen space               Water Quality C sphure Volume (WQCV) = 0.111         acre-feet         Optional User Override			
Excess Urban Runoff Volume (EURV) = 0.357 acre-feet 1-hr Precipitation			
2-yr Runoff Volume (P1 = 1.16 in.) = 0.283 acre-feet 1.16 inches			
5-yr Runoff Volume (P1 = 1.44 in.) = 0.378 acre-feet 1.44 inches		-	
25-yr Runoff Volume (P1 = 1.92 in.) = 0.678 acre-feet 1.92 inches			
50-yr Runoff Volume (P1 = 2.16 in.) = 0.802 acre-feet 2.16 inches		-	
100-yr Runoff Volume (P1 = 2.42 in.) =         0.966         acre-feet         2.42         inches               500-yr Runoff Volume (P1 = 0 in.) =         0.000         acre-feet         inches			
Approximate 2-yr Detention Volume = 0.265 acre-feet			
Approximate 5-yr Detention Volume = 0.355 acre-feet			
Approximate 10-yr Detention Volume =         0.463         acre-feet <th< td=""><td></td><td></td><td></td></th<>			
Approximate 2b-yr Delenition Volume = 0.525 acre-feet			
Approximate 100-yr Detention Votume = 0.580 acre-feet			
tage-Storage Calculation  -			
Zone 1 Volume (WQCV) =         0.111         acre-feet			
Zone 3 Volume (100-year - Zones 1 & 2) = 0.223 acre-feet			
Total Detention Basin Volume =         0.580         acre-feet <td></td> <td></td> <td></td>			
Initial Surcharge Volume (ISV) =         user         #*3			
Total Available Detention Depth (H <sub>ctabl</sub> ) = user ft			
Depth of Trickle Channel (H <sub>TC</sub> ) = user nt			
Slope of Trickle Channel (Sr <sub>17</sub> ) =         user         trift <td></td> <td></td> <td></td>			
Basin Length-to-Width Ratio (R <sub>w</sub> ) = user			
Initial Surcharge Area (A <sub>10</sub> )         user         ft*2			
Surcharge Volume Length (L <sub>SV</sub> ) = user ft Surcharge Volume Width (W <sub>SV</sub> ) = user ft			
Depth of Basin Floor (H <sub>R.cont</sub> ) = user tt			
Length of Basin Floor (H <sub>1000</sub> ) = user ft			
Width of Basin Floor (M <sub>RCOD</sub> ) =         user         ft			
Volume of Basin Floor (V <sub>1000</sub> ) user #1/3			
Depth of Main Basin (H <sub>MAIN</sub> ) = user ft			
Length of Main Basin (L <sub>MAM</sub> ) =         user         tt		+	
Area of Main Basin (A <sub>ndAN</sub> ) = user tt <sup>A</sup> 2			
Volume of Main Basin (V <sub>LUM</sub> ) = user (P3			
Calculated Total Basin Volume (V <sub>total</sub> ) = user acre-feet		<u> </u>	
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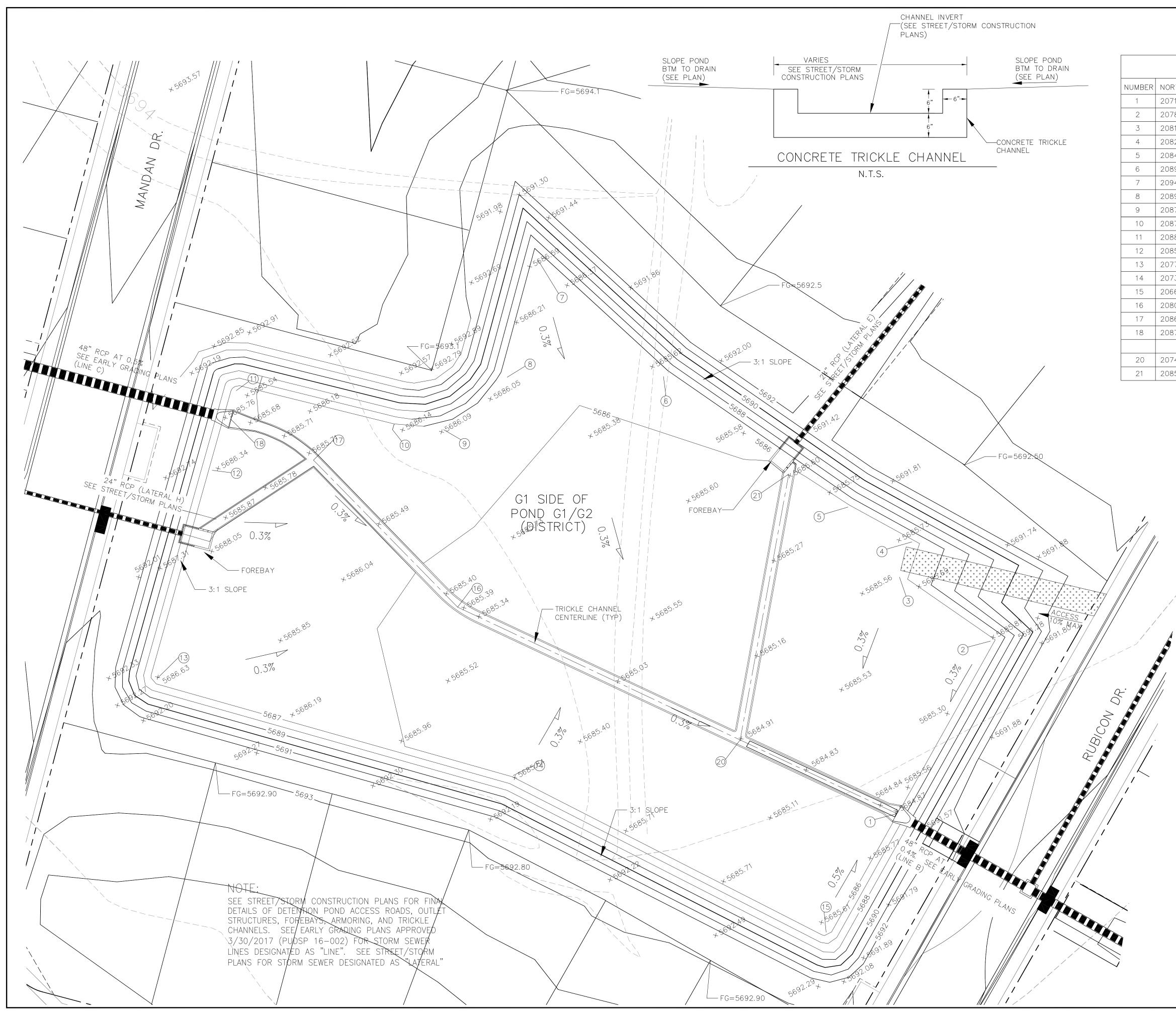




		POINT	TABLE					POINT	TABLE			
	NUMBER N		EASTING	ELEVATION	NOTES		NUMBER		EASTING	ELEVATION	NOTES	
		20426.91	20695.07	5683.00	POND BOTTOM			20358.26	20684.49	5683.00	POND BOTTOM	
		20435.42	20580.07	5683.19	POND BOTTOM							
	3 2	20508.55	20484.61	5683.80	POND BOTTOM							
		20562.75	20440.18	5684.00	POND BOTTOM							
		20556.24	20428.64	5684.00	POND BOTTOM							
	6 2	20473.78	20380.35	5684.00	POND BOTTOM		16	20558.92	20432.02	5683.55	INVERT 48" RCP	
								20000102	20102.02			
	9 2	20360.30	20583.01	5683.00	POND BOTTOM							
l					\ \			<b> </b>     /	1	\ \		
							17		/			
		(C, C)					2.3 <sup>3</sup> DE DR.					
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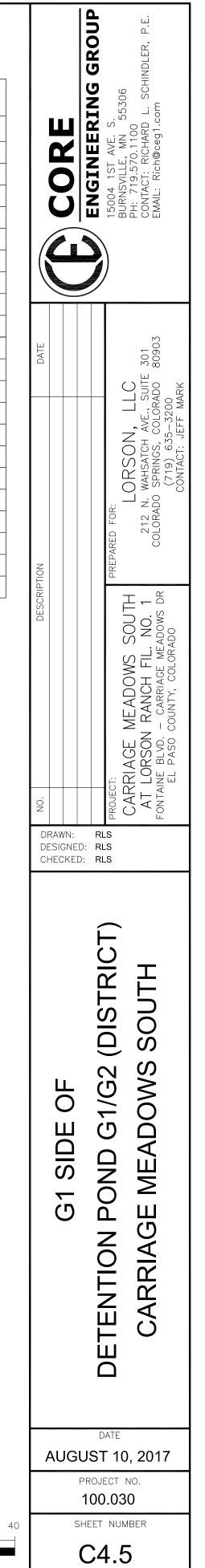






## DOINT TADIE

POINT	TABLE		
RTHING	EASTING	ELEVATION	NOTES
714.71	20158.47	5684.80	INV 48" RCP (LINE B)
786.15	20197.19	5685.54	POND BOTTOM
812.62	20159.51	5685.65	POND BOTTOM
827.21	20164.67	5685.70	POND BOTTOM
841.64	20138.20	5685.74	POND BOTTOM
895.71	20061.76	5686.10	POND BOTTOM
943.87	20009.80	5686.20	POND BOTTOM
895.38	19997.02	5686.11	POND BOTTOM
873.70	19970.67	5686.17	POND BOTTOM
873.69	19949.53	5686.21	POND BOTTOM
889.83	19884.81	5686.30	POND BOTTOM
856.85	19874.86	5686.55	POND BOTTOM
770.85	19852.26	5686.28	POND BOTTOM
730.51	19999.53	5685.88	POND BOTTOM
665.63	20129.13	5685.60	POND BOTTOM
800.21	19976.50	5685.40	TRICKLE CHANNEL INVERT
861.06	19916.81	5685.66	TRICKLE CHANNEL INVERT
878.04	19882.51	5685.80	INV 48" RCP (LINE C)
745.23	20093.52	568501	TRICKLE CHANNEL INVERT
855.30	20113.66	5685.45	TRICKLE CHANNEL INVERT

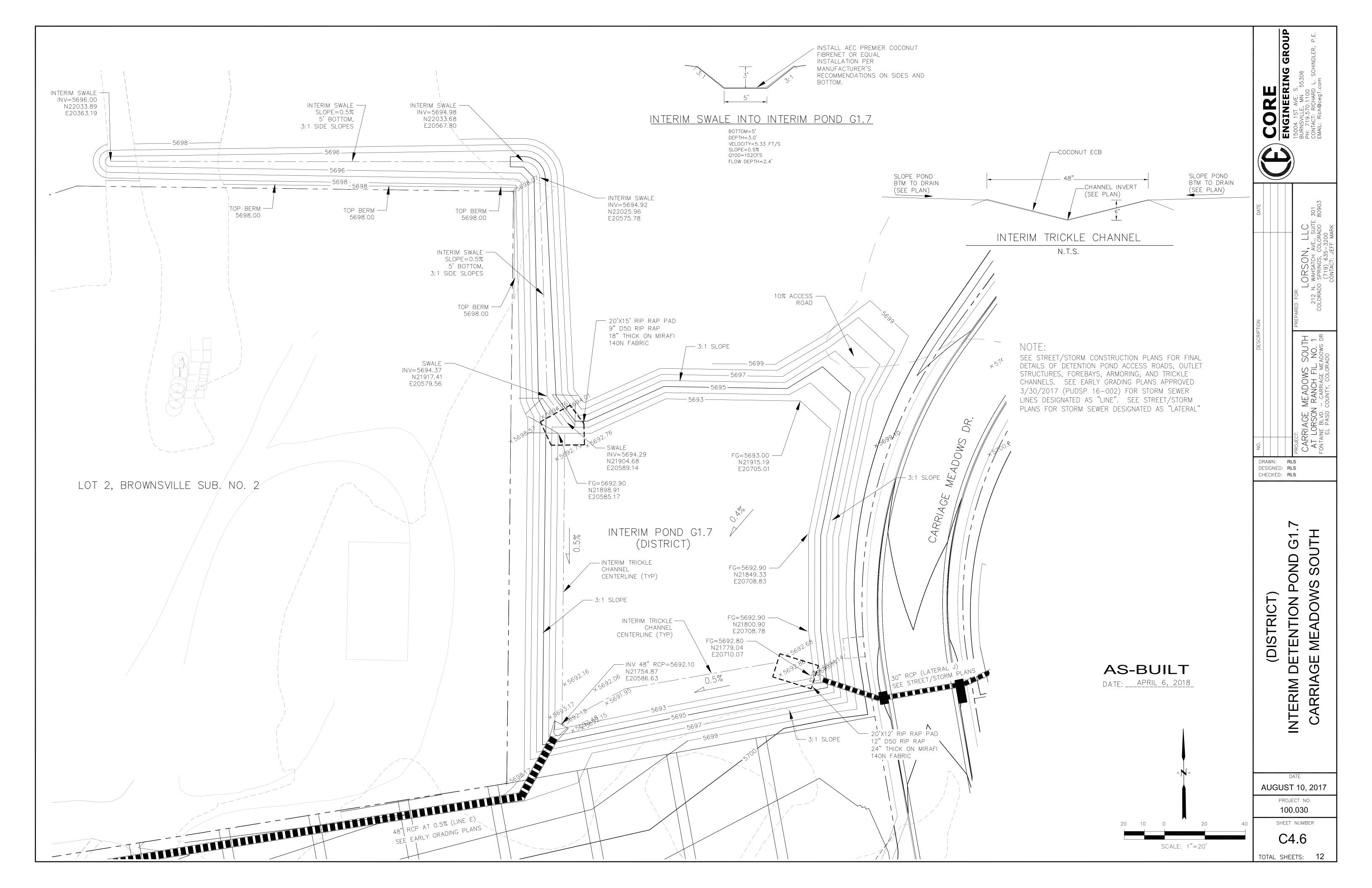


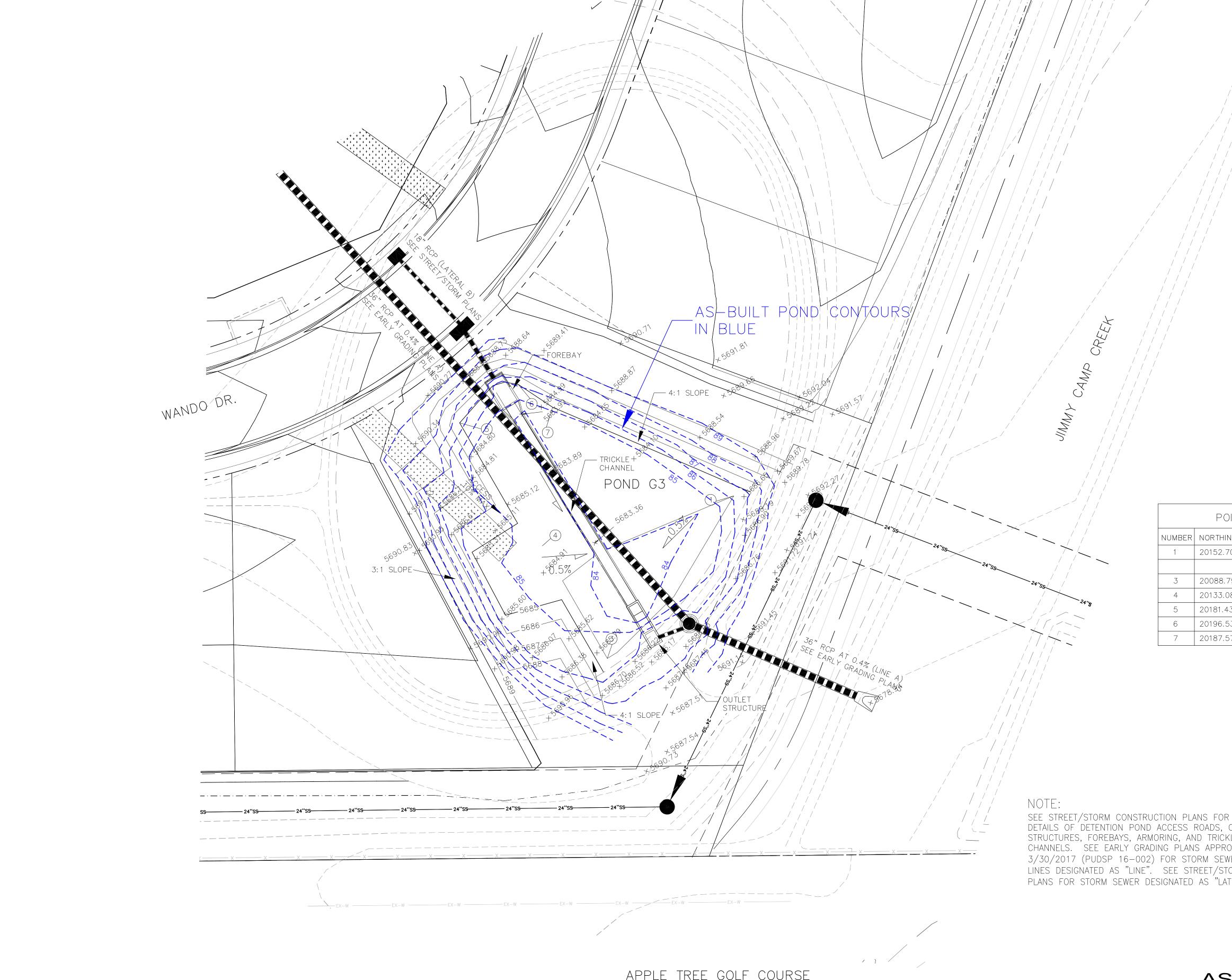
TOTAL SHEETS: 12

SCALE: 1"=20'

**AS-BUILT** 

DATE: <u>APRIL 6, 2018</u>

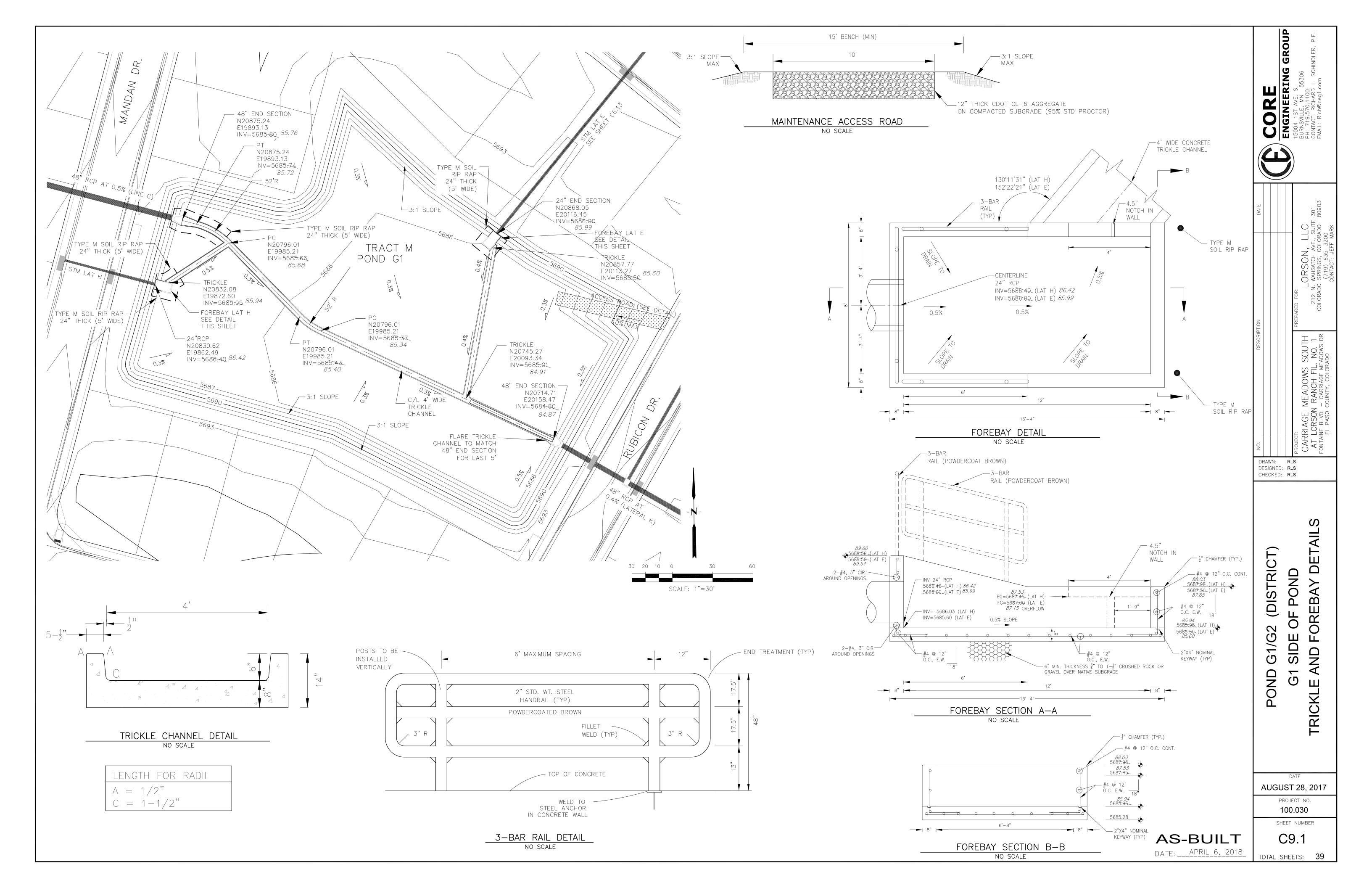


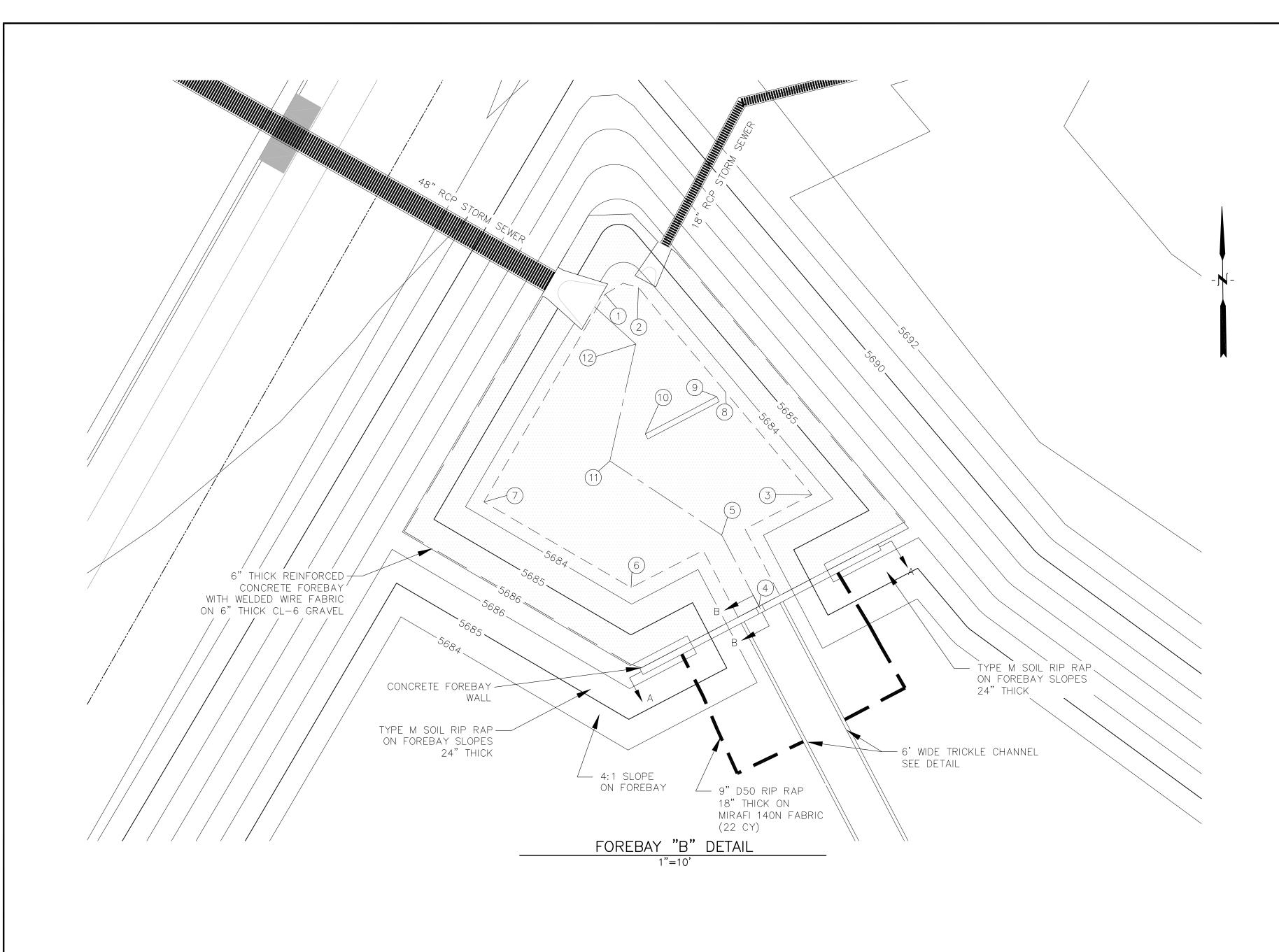


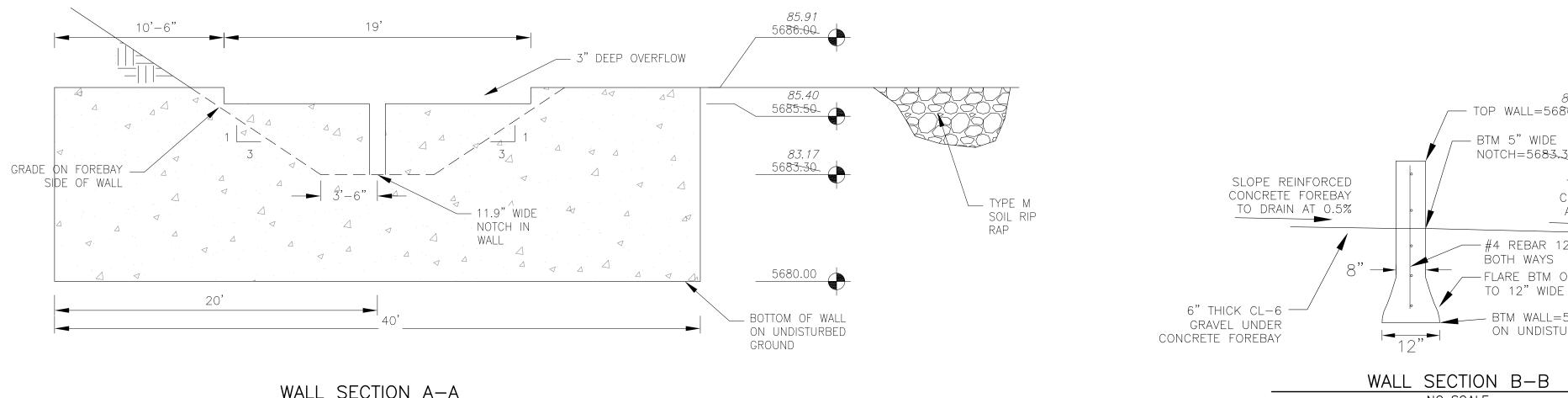
APPLE TREE GOLF COURSE

AS DATE:

					CORE	ENGINEERING GROUP 15004 1ST AVE. S. BURNSVILLE, MN 55306 PH: 719.570.1100 CONTACT: RICHARD L. SCHINDLER, P.E. EMAIL: Rich@ceg1.com
					DESCRIPTION DATE	MEADOWS SOUTH I RANCH FIL. NO. 1 - CARRIAGE MEADOWS DR county, colorado
POINT [hing 2.70	TABLE EASTING 20951.65	ELEVATION 5684	NOTES POND BOTTOM		DRAWN: DESIGNED: CHECKED:	
88.79 3.08 1.43 6.53 7.57	20901.93 20876.39 20843.88 20866.94 20880.42	5684 5684.20 5685 5685 5685	POND BOTTOM POND BOTTOM POND BOTTOM POND BOTTOM POND BOTTOM			(DISTRICT) S SOUTH
OR FIN S, OUTL ICKLE PROVED SEWER STORM LATERA	_ET					DETENTION POND G3 CARRIAGE MEADOW
	<b>3UIL</b> April 6, 20		- N - 20 10 0 SCALE: 1"	20 40 = 20'	PI 1 SH	DATE IST 10, 2017 ROJECT NO. 00.030 EET NUMBER C4.8 SHEETS: 12

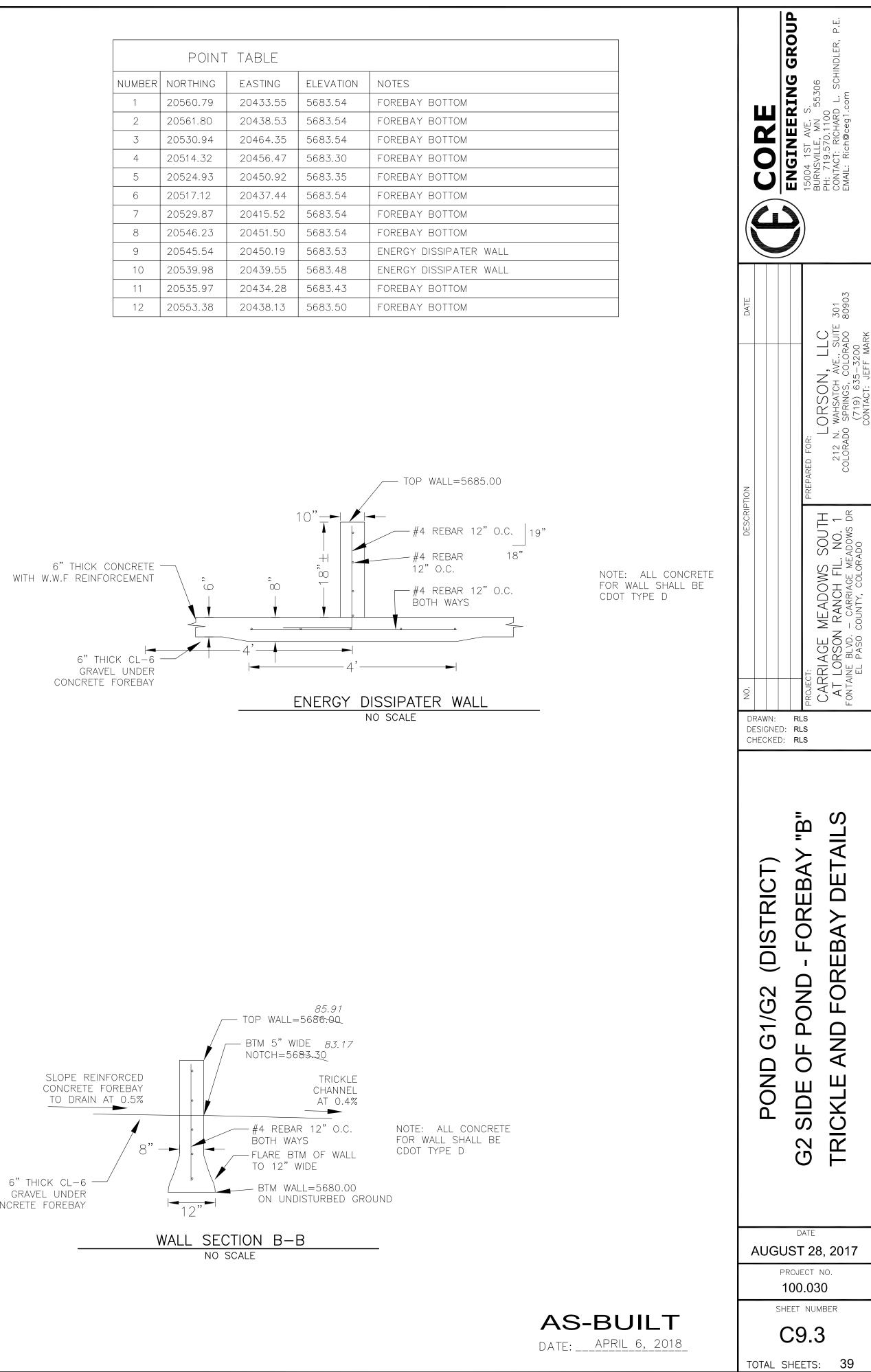


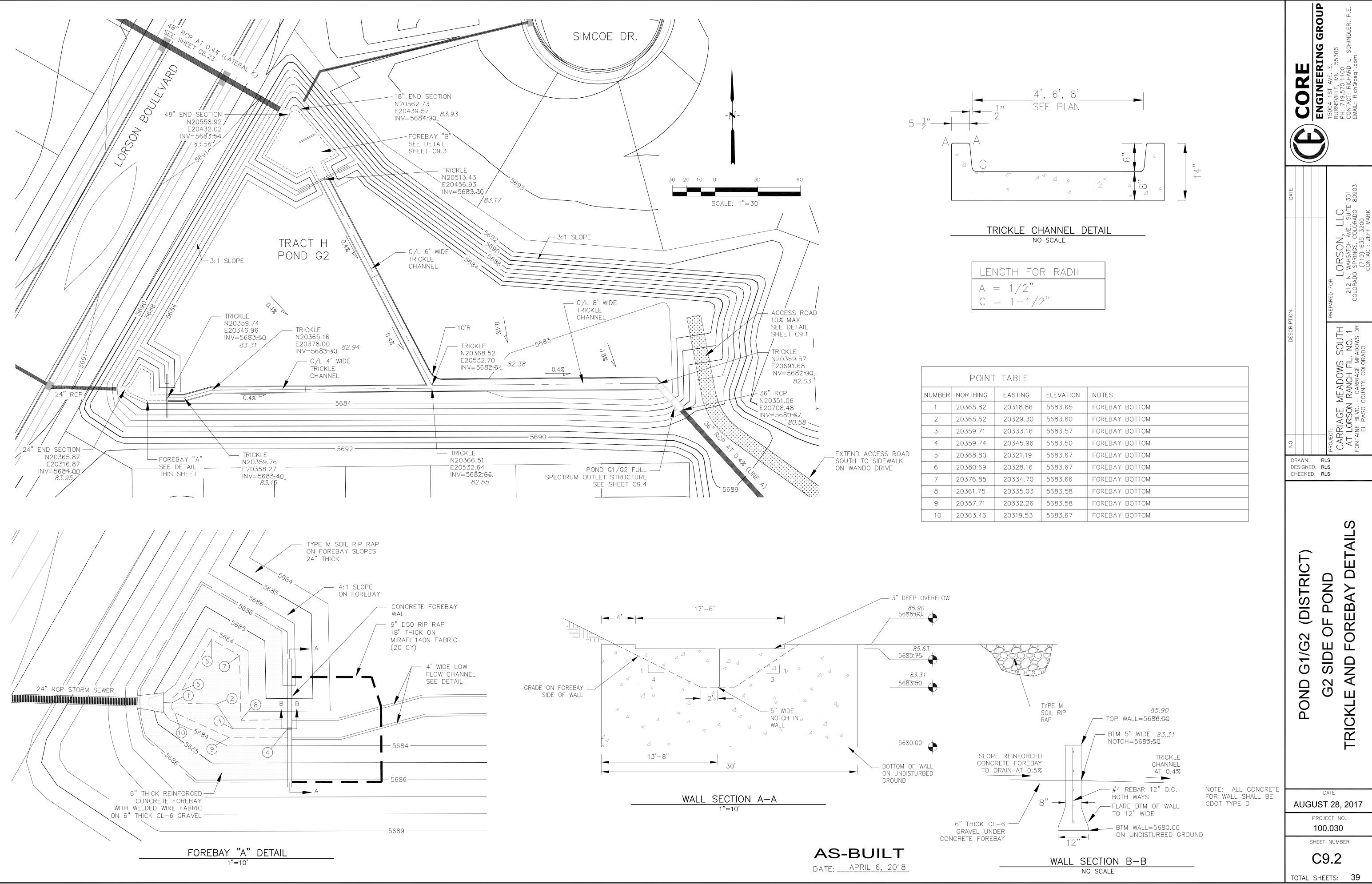


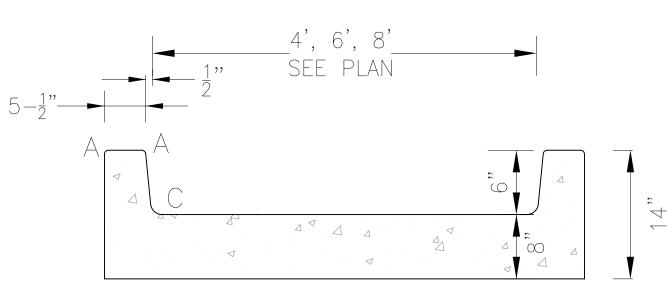


WALL SECTION A-A 1"=10'

	POINT	TABLE	
NUMBER	NORTHING	EASTING	ELEVAT
1	20560.79	20433.55	5683.5
2	20561.80	20438.53	5683.5
3	20530.94	20464.35	5683.5
4	20514.32	20456.47	5683.3
5	20524.93	20450.92	5683.3
6	20517.12	20437.44	5683.5
7	20529.87	20415.52	5683.5
8	20546.23	20451.50	5683.5
9	20545.54	20450.19	5683.5
10	20539.98	20439.55	5683.4
11	20535.97	20434.28	5683.4
12	20553.38	20438.13	5683.5



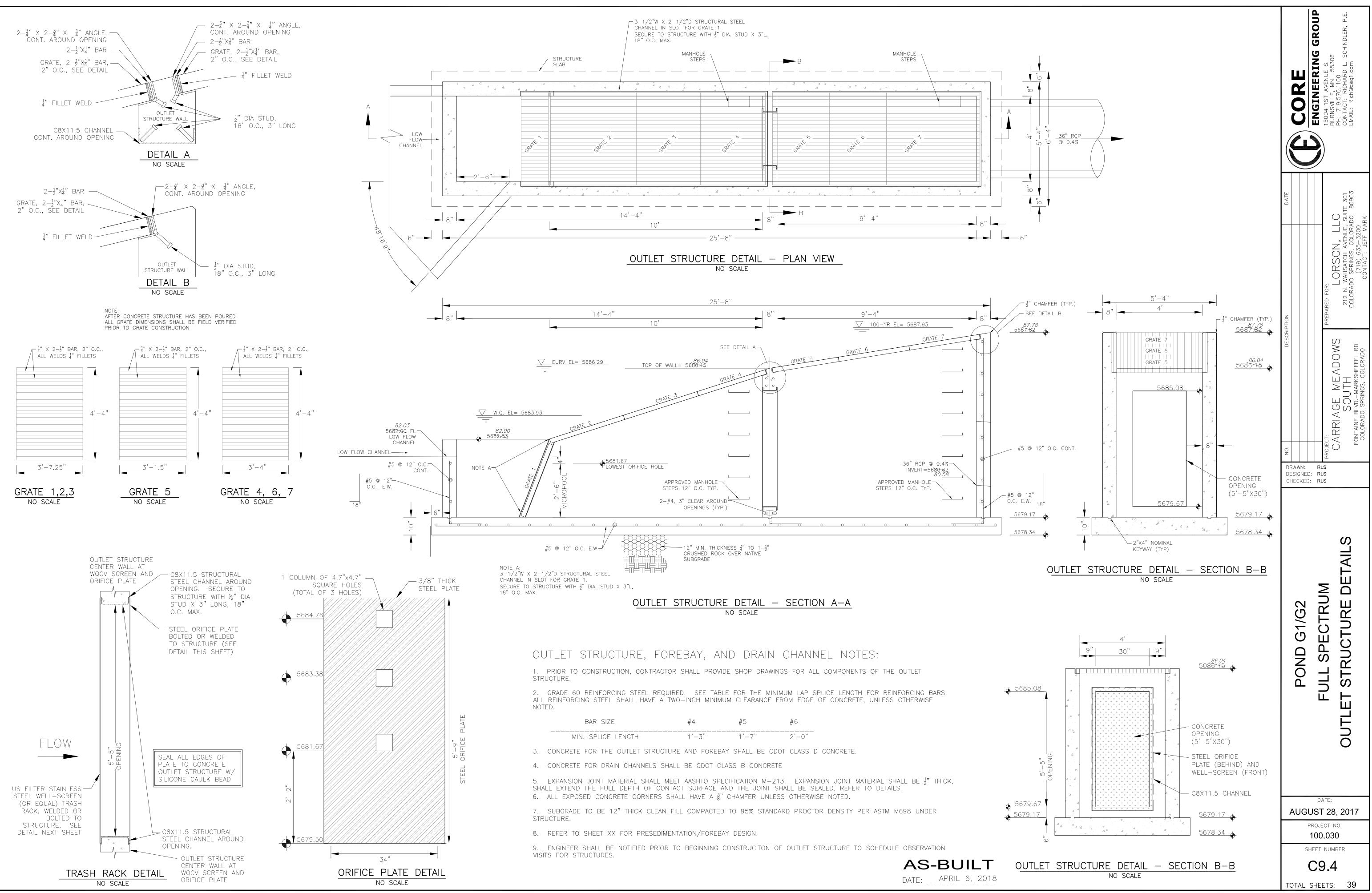




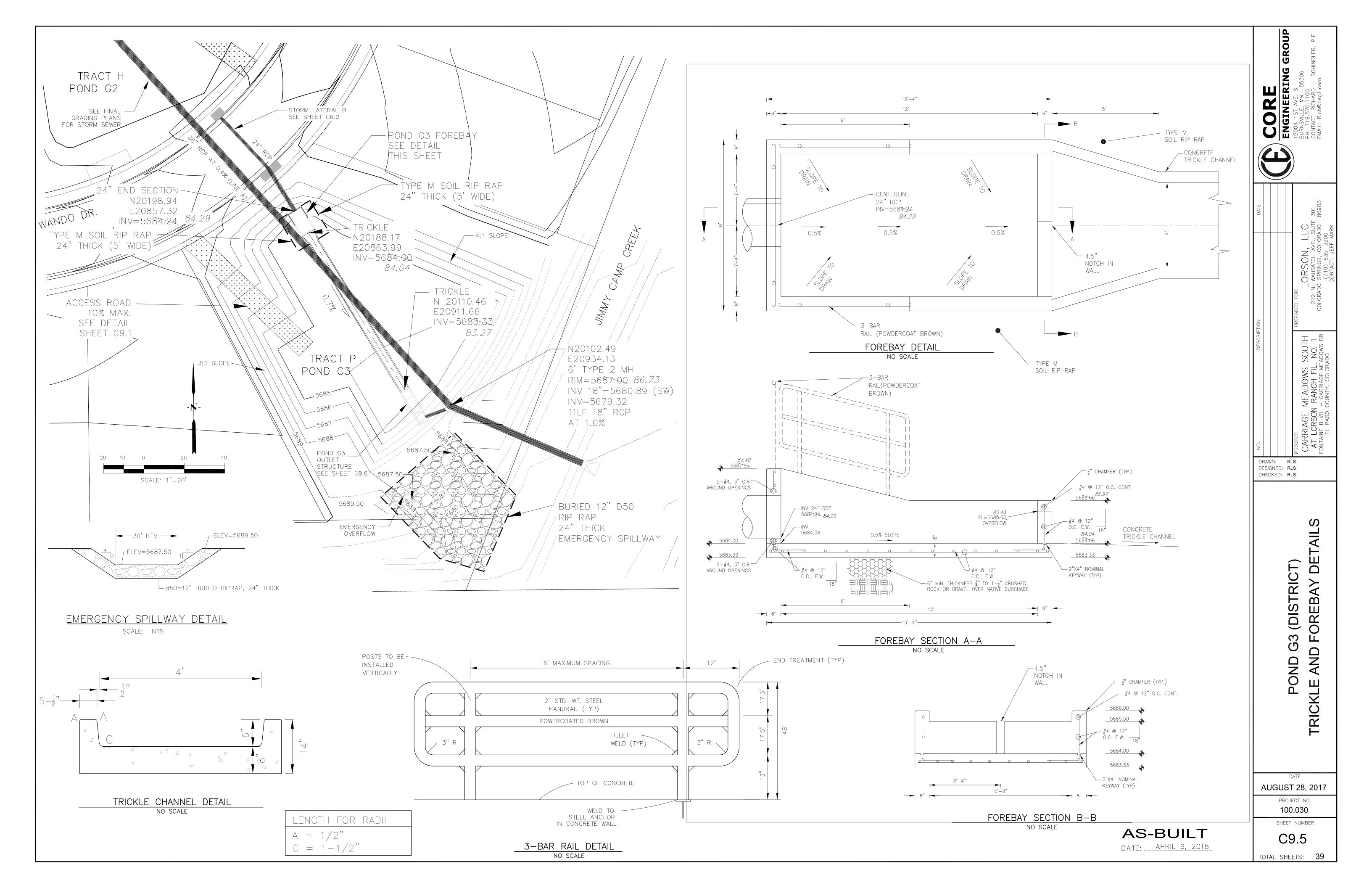
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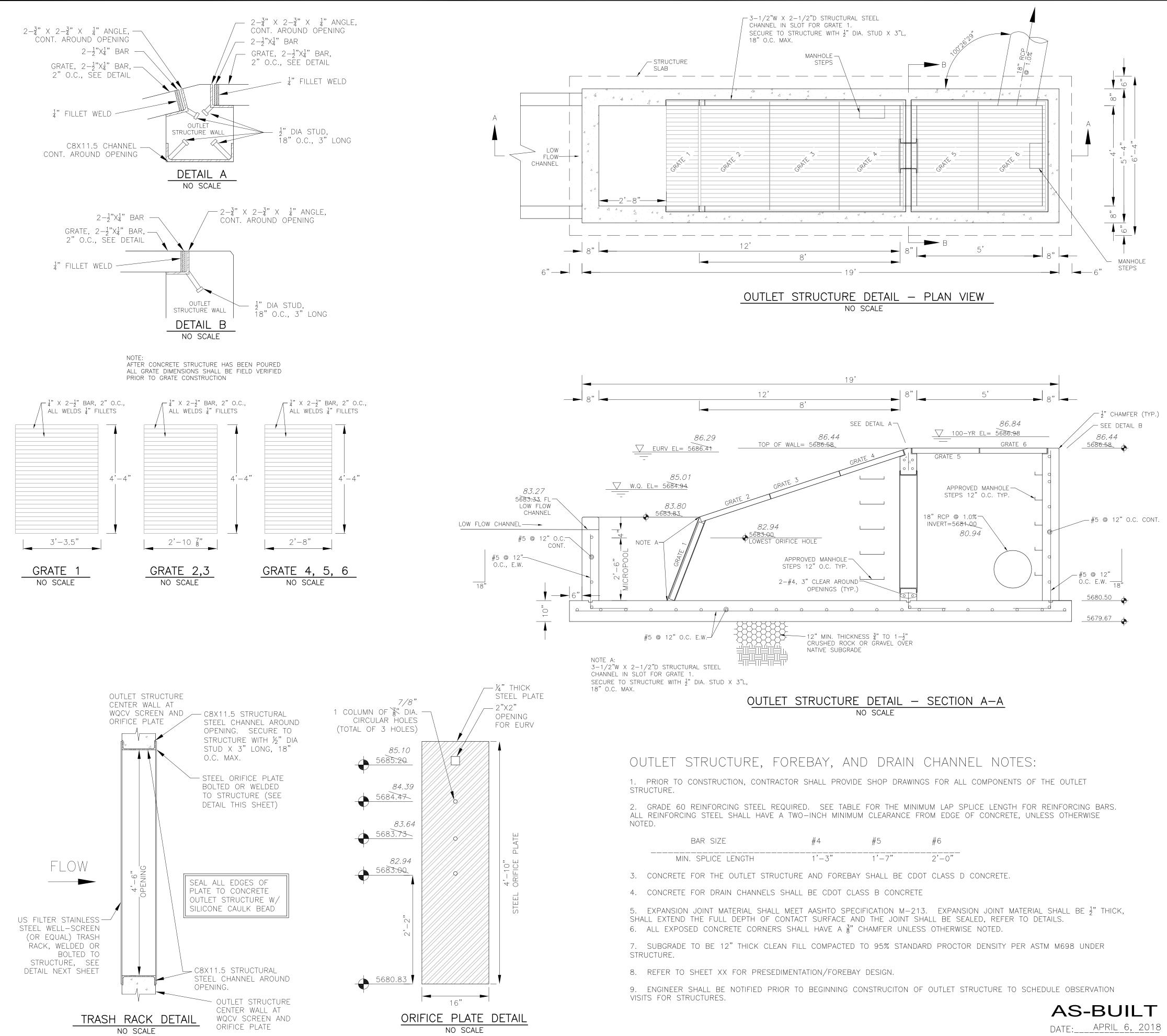
	POINT	TABLE		
NUMBER	NORTHING	EASTING	ELEVATION	NOTES
1	20365.82	20318.86	5683.65	FOREBAY BOTTOM
2	20365.52	20329.30	5683.60	FOREBAY BOTTOM
3	20359.71	20333.16	5683.57	FOREBAY BOTTOM
4	20359.74	20345.96	5683.50	FOREBAY BOTTOM
5	20368.80	20321.19	5683.67	FOREBAY BOTTOM
6	20380.69	20328.16	5683.67	FOREBAY BOTTOM
7	20376.85	20334.70	5683.66	FOREBAY BOTTOM
8	20361.75	20335.03	5683.58	FOREBAY BOTTOM
9	20357.71	20332.26	5683.58	FOREBAY BOTTOM
10	20363.46	20319.53	5683.67	FOREBAY BOTTOM

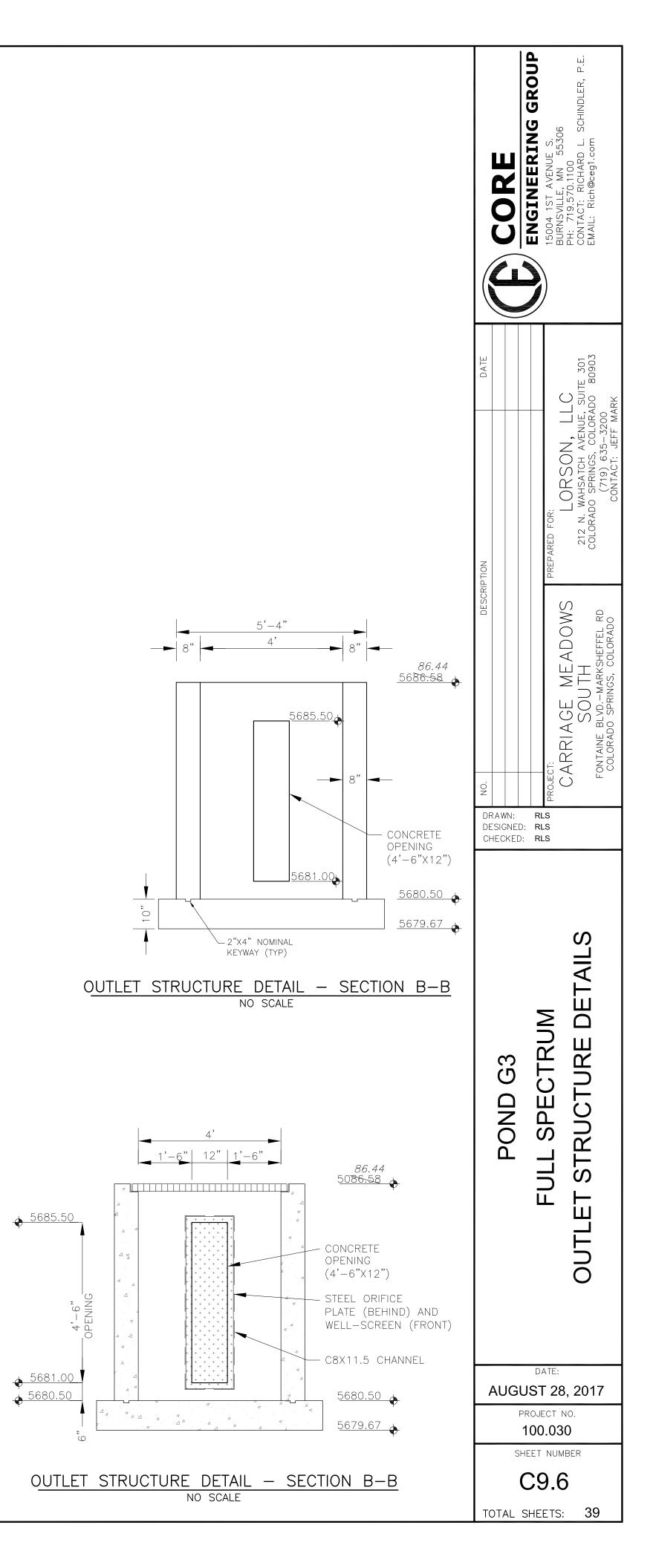
	CORENT ENGINEERING GROUP 15004 1ST AVE. S. BURNSVILLE, MN 55306 PH: 719.570.1100 CONTACT: RICHARD L. SCHINDLER, P.E. EMAIL: Rich@ceg1.com
	NO.     DESCRIPTION     DATE       AT LORSON RANCH FIL. NO. 1     DATE     DATE       AT LORSON RANCH FIL. NO. 1     PREPARED FOR:     LORSON, LLC       AT LORSON RANCH FIL. NO. 1     212 N. WAHSATCH AVE., SUITE 301     2013       FONTAINE BLVD CARRIAGE MEADOWS DR     212 N. WAHSATCH AVE., SUITE 301     2013       FONTAINE BLVD CARRIAGE MEADOWS DR     212 N. WAHSATCH AVE., SUITE 301     212 N. WAHSATCH AVE., SUITE 301
	POND G1/G2 (DISTRICT) G2 SIDE OF POND TRICKLE AND FOREBAY DETAILS
Ē	DATE AUGUST 28, 2017 PROJECT NO. 100.030



BAR SIZE	#4	#5	#6
MIN. SPLICE LENGTH	1'-3"	1'7"	2'-0"







## APPENDIX E- DRAINAGE BOARD MINUTES, STORM SEWER SCHEMATIC AND HYDRAFLOW STORM SEWER CALCS

## Minutes City of Colorado Springs/ El Paso County Drainage Board Meeting Summary January 23, 2024

The City of Colorado Springs/ El Paso County Drainage Board held its meeting at 1:30 PM, Tuesday, January 23, 2024, at Pikes Peak Regional Building in the Pikes Peak Hearing Room.

**MEMBERS PRESENT:** Tim McConnell (Chair), Marc Whorton (Vice Chair), Grant Petik, Brett Louk, Mark Sherwood, Scott Smith

OTHERS PRESENT: Christina Aragon (City), Erin Powers (City), Erica Schmitz (City), Amy Tuten (City), Rebecca Greenberg (City), Daniel Torres (El Paso County), Carlos Hernandez (El Paso County), Jeff Rice (El Paso County), Greg Shaner (Matrix), Jesse Sullivan (Matrix), Tina Buschar (View Homes), JM Turley (View Homes), Jeff Mark (Landhuis), Rich Wray (Kiowa), Dave Gorman (MVE)

Item 1: Meeting called to order by *Tim McConnell* at 1:31 PM.

## Item 2:

a) Approval of the November 14, 2023, Drainage Board minutes

Approval of the minutes from the November 14, 2023, Drainage Board Meeting. Motion was made by *Scott Smith* to approve the minutes of November 14, 2023, *with the amendment to remove Marc Whorton's duplicate naming in the "Members Present"*. Motion was seconded by *Mark Sherwood*.

## **Motion Passed 6-0**

Item 3: Old Business - None.

## Item 4: New Business

# a) Partial Closure of Jimmy Camp Creek for Bull Hill/Rolling Meadows (County) – presented by Jeff Rice (County), Jeff Mark (Landhuis), and Rich Wray (Kiowa)

Jeff Rice introduces the request for the closure of a portion of Jimmy Camp Creek Basin for Bull Hill, Rolling Meadows, and the remaining unplatted portions of Lorson Ranch development in unincorporated El Paso County. El Paso County supports the approval of the partial closure, but they are still reviewing to ensure this action will not significantly increase the drainage fee for the remaining parcels in the basin. *Tim McConnell* asks if this item will need to come back to Drainage Board once the determinations are made, or will it be approved administratively. *Jeff Rice* responds that could be decided by the Board whether or not they would like to have the item come back to the Board. *Jeff Mark* then states it would be preferred if the Item could be settled administratively, but agrees it is the Board's decision. *Jeff Rice* displays the map of Lorson Ranch to show the area of concern for this Item. *Jeff Mark* continues to describe the area in question and explain the background of the improvements already installed and future installments. Jeff explains this request is being brought to the Board because the cost of the improvements is anticipated to far exceed what the basin fees would be based on the analysis. Mark Sherwood asks if they are fairly confident about the required improvements to be installed in the area. Jeff Rice answers that they are confident about the final design and associated fees. Rich Wray arrives and offers further details on the calculations of the drainage fees for the area. He then continues to explain justifications to support this request. Scott Smith asks Jeff Mark about the current status of this portion of Lorson Ranch in terms of the fees and reimbursable cost and if it's in balance. Jeff Rice responds by explaining the current status of this portion of Lorson Ranch discussing the fees and credits for the basin. Marc Whorton asks if the channel improvements have been accepted by the County. Jeff Rice confirms that the channels have been completed and accepted, and the metro district maintains it. Marc Whorton then asks when the updated DBPS will be completed, and Jeff Rice responds that it is anticipated to be completed within the year.

*Marc Whorton* asks if Jeff Mark would be ok with splitting up the request to close the portion of the basin with completed improvements while the County finishes their review and completes the updated DBPS. Jeff agrees the would be acceptable if the Board agrees.

*Marc Whorton* moves to approve the partial closure of Jimmy Camp Creek just for the remaining Lorson developments, pending confirmation that this action will not significantly raise the resulting drainage fees for the remaining parcels in the basin with the expectation that the applicant will bring the same request back to the Board for Rolling Meadows/ Bull Hill. *Scott Smith* seconds the motion.

#### **Motion Passed 6-0**

## b) Sand Creek Channel Stabilization Reimbursement Request (City) – presented by Erica Schmitz (City) and Gregory Shaner (Matrix)

*Erica Schmitz* introduces the request for reimbursement for Sand Creek channel improvements. Erica continues providing a bit of background for the request and states that City staff is remaining neutral on this request because the reimbursement request is greater than the 10% allotted by code. *Gregory Shaner* is introduced and continues to provide background on the project and history of the site. Gregory describes the difficulties and obstacles with the project, which helps to justify why they are requesting a larger reimbursement. Grant Petik asks for clarification on some of the additional costs shown in their analysis. Gregory explains the costs depicted and discusses more details about the project. Board members and applicant discuss the cost breakdown, and Tim McConnell mentions an analysis to determine whether a fee increase is warranted. There is further discussion amongst the Board.

*Tim McConnell* moves to approve the \$553,188.31 channel improvements reimbursement request. *Mark Sherwood* seconds the motion.

#### **Motion Passed 6-0**

## c) Sand Creek Request to Designate Reimbursable Infrastructure (City) – presented by Erica Schmitz (City)

*Erica Schmitz* introduces the request for channel improvements associated with the Final Plat for The Crossing at Palmer Park Filing No. 5 be designated as reimbursable. Erica adds that City staff is remaining neutral on this request but offers options for possible motions. Erica introduces *Dave Gorman*, who takes the stand to explain the background of their improvements and the reason for their request. Dave explains there has been no improved or stabilization of the channel in this area previously. *Mike Turley* asks about drainage fees in association with platting the area. *Erin Powers* 

addresses Mike's question with City policy. *Scott Smith* then asks if these improvements are installed already, and Dave responds that they have not. Dave explains that plans have been reviewed by the City and this is just an estimated cost for the improvements. *Scott Smith* confirms that this is a request to improvement costs to be considered reimbursable and Dave confirms. There is further discussion between the Board and applicant describing the project and development for The Crossing at Palmer Park Filing No. 5.

*Scott Smith* moves to approve the request to add this reimbursable amount to the Sand Creek Drainage Basin with a request for a fee analysis of the Sand Creek Basin upon request for reimbursement. *Marc Whorton* seconds the motion.

#### **Motion Passed 6-0**

#### e) Housekeeping

## a. February meeting cancellation

*Mark Sherwood* moves to approve the cancellation of the schedule meeting in February 2024. *Marc Whorton* seconds the motion.

#### **Motion Passed 6-0**

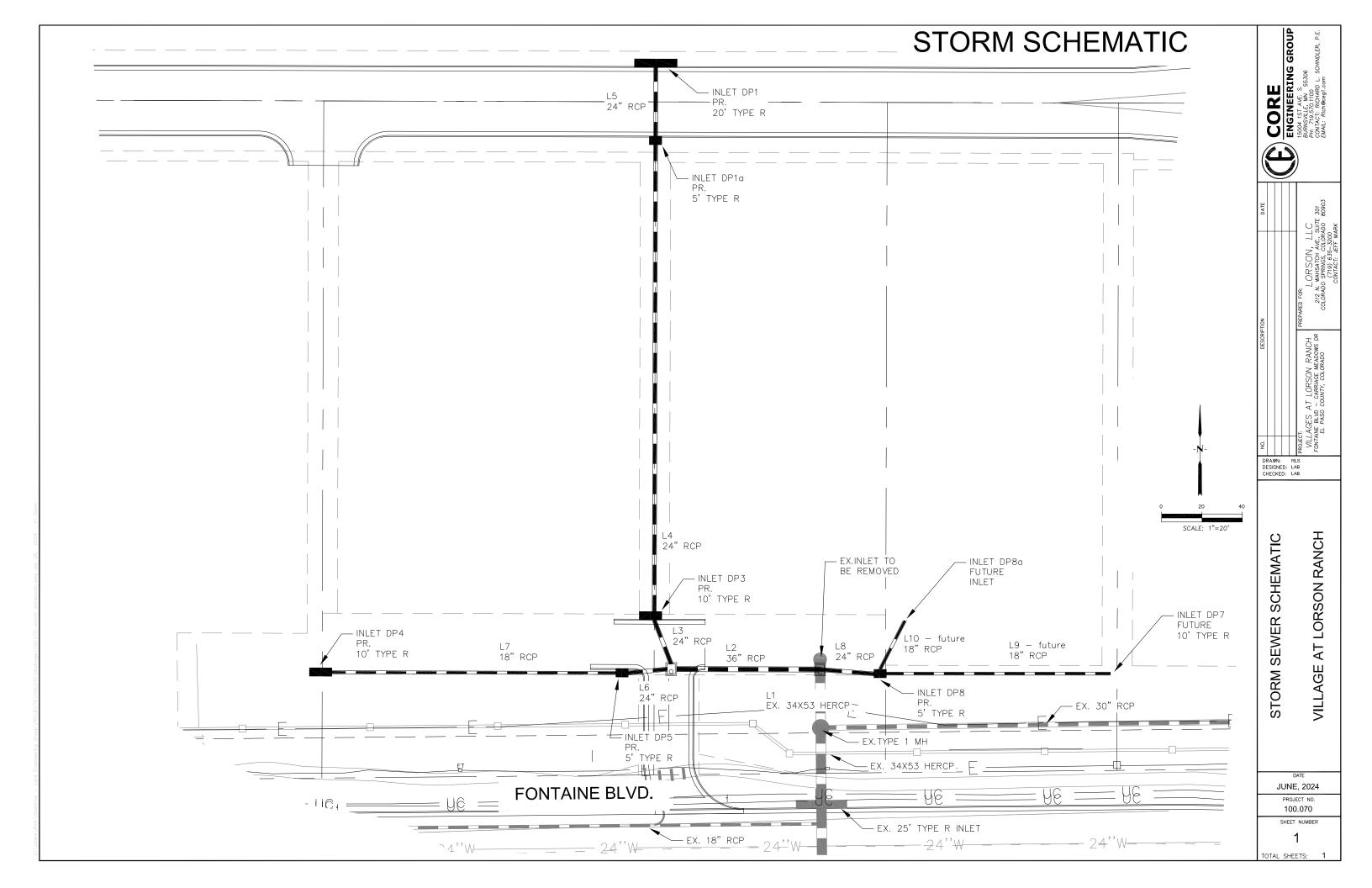
## f) Open Discussion

*Tim McConnell* asks about Gary's vacancy and the upcoming vacancies when his and Marc's terms expire in May 2024. *Erin Powers* responds explaining that the vacancies are posted and reviews the process for hiring.

*Tim McConnell* then asks about the financial update from the County and requests they could provide an update at the next meeting.

*Tim McConnell* asked about Amy's financial update and the unclaimed reimbursements, wanting more details on where the additional unclaimed funds were reallocated to. *Erin Powers* responds that she will speak with Amy to find out if the unclaimed funds will be reallocated to each individual basin versus the Interest fund.

Item 5: Tim McConnell - Meeting adjourned at 3:43 PM.



# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	1	31.50	34x53	EII	28.90	5701.86	5702.05	0.657	5704.47	5703.75	0.38	5703.75	End	Manhole
2	2	20.50	36	Cir	72.76	5702.15	5702.51	0.495	5703.75	5703.96	n/a	5703.96	1	Manhole
3	3	12.50	24	Cir	26.00	5703.26	5703.52	1.001	5704.32	5704.79	0.23	5704.79	2	Manhole
4	4	9.80	24	Cir	239.29	5703.62	5706.01	0.999	5704.79	5707.13	n/a	5707.13 j	3	Manhole
5	5	9.40	24	Cir	35.00	5706.11	5706.46	1.000	5707.13	5707.56	0.44	5707.56	4	Manhole
6	6	8.90	24	Cir	22.46	5703.26	5703.38	0.535	5704.31	5704.44	n/a	5704.44	2	Manhole
7	7	5.90	18	Cir	151.60	5703.88	5704.63	0.495	5704.89	5705.64	0.34	5705.98	6	Manhole
8	8	12.20	24	Cir	28.65	5702.90	5703.19	1.012	5703.94	5704.44	0.51	5704.44	1	Manhole
9	9	5.30	18	Cir	125.20	5703.69	5704.94	0.998	5704.44	5705.83	n/a	5705.83	8	None
10	10	6.00	18	Cir	29.57	5703.69	5703.99	1.016	5704.50	5704.94	0.41	5704.94	8	None
Village	5yr						4	J	Number o	f lines: 10	_]	Run [	Date: 3/28/	2024
	: Return period = 5 Yrs. ; j - Line o	antaine ku	d iuman									L		

# **Storm Sewer Tabulation**

statio	ı	Len	Drng A	rea	Rnoff	Area x	C	Tc				Cap full	Vel	Pipe		Invert Ele	9V	HGL Ele	v	Grnd / Rim Elev		Line ID
.ine		-	Incr	Total	-coeff	Incr	Total	Inlet	Syst	(1)	tiow	Tull		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
4	<b>F</b> in al	20,000	0.00	0.00	0.00	0.00	0.00	0.0	2.0		24 50	00.44	0.05	24	0.00	5704.90	E702 0E	EZ04 47	E702 7E	E707.94	E707 E0	1
1 2		28.899 72.756		0.00	0.00	0.00	0.00	0.0	2.0 1.6	0.0	31.50 20.50	89.44 47.54	6.35 5.70	34 x 53 e 36	0.66					5707.84 5707.59		
3		26.003		0.00	0.00	0.00	0.00	0.0	1.5	0.0	12.50	22.63		24	1.00					5707.92		
, I		239.285		0.00	0.00	0.00	0.00	0.0	0.2	0.0	9.80	22.60		24	1.00					5708.05		
5		35.000		0.00	0.00	0.00	0.00	0.0	0.0	0.0	9.40	22.62		24	1.00					5712.13		
5		22.463		0.00	0.00	0.00	0.00	0.0	0.8	0.0	8.90	16.54		24	0.53					5707.92		
7		151.599		0.00	0.00	0.00	0.00	0.0	0.0	0.0	5.90	7.43	4.67	18	0.50					5707.94		
3		28.652		0.00	0.00	0.00	0.00	0.0	0.7	0.0	12.20	22.76		24	1.01					5707.59		
9		125.197		0.00	0.00	0.00	0.00	0.0	0.0	0.0	5.30	10.49		18	1.00					5707.55		
10	8	29.568	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	6.00	10.58	5.64	18	1.02	5703.69	5703.99	5704.50	5704.94	5707.55	5707.54	10
Villaç	ge 5yr	I	l	1	1		1		1	1	1	1	1	I		Number	of lines: 1	0	1	Run Dat	te: 6/9/202	24
	=S·Into	neity – F	01 75 / /	(Inlet tim	a + 28 2	0) ^ 1 21	l. Retur	n neriod	=Yrs. 5		نالم = م	h = hc				1				1		

# **Storm Sewer Summary Report**

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	1	57.30	34x53	EII	29.00	5701.86	5702.05	0.655	5704.41	5704.32	n/a	5704.32	End	Manhole
2	2	37.30	36	Cir	72.76	5702.15	5702.51	0.495	5704.32	5704.52	0.81	5705.32	1	Manhole
3	3	22.80	24	Cir	26.00	5703.26	5703.52	1.001	5705.32*	5705.59*	0.34	5705.93	2	Manhole
4	4	17.80	24	Cir	239.29	5703.62	5706.01	0.999	5705.93	5707.53	n/a	5707.53 j	3	Manhole
5	5	17.00	24	Cir	35.00	5706.11	5706.46	1.000	5707.53	5707.95	0.72	5707.95	4	Manhole
6	6	16.10	24	Cir	22.46	5703.26	5703.38	0.535	5705.32*	5705.44*	0.06	5705.50	2	Manhole
7	7	8.10	18	Cir	151.60	5703.88	5704.63	0.495	5705.50*	5706.40*	0.33	5706.73	6	Manhole
8	8	22.40	24	Cir	29.00	5702.90	5703.19	1.000	5704.52	5704.88	0.92	5704.88	1	Manhole
9	9	9.70	18	Cir	125.20	5703.69	5704.94	0.998	5704.88	5706.14	0.64	5706.14	8	None
10	10	11.00	18	Cir	29.57	5703.69	5703.99	1.016	5704.98	5705.28	0.72	5706.00	8	None
Village	100yr	_1		1		1			Number o	f lines: 10	2	Run I	Date: 3/28/	2024
NOTES:	Return period = 100 Yrs.;*Surch	narged (HG	L above crow	/n).; i - Lin	e contains	hyd. jump.			1			k		

# **Storm Sewer Tabulation**

Statio	ı	Len	Drng A	j Area	Rnoff	Area x	C	Tc			Total	Сар	Vel	Pipe		Invert Ele	θV	HGL Ele	v	Grnd / Ri	m Elev	Line ID
.ine			Incr	Total	-coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	-
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	hr) (cfs) (cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft) (ft)	(ft)	(ft)	(ft)	
	End	29.000	0.00	0.00	0.00	0.00	0.00	0.0	1.1	0.0	57.30	89.28	7.87	34	0.65	5701.86	5702.05	5704.41	5704.32	5707.84	5708.48	1
2	1	72.756	0.00	0.00	0.00	0.00	0.00	0.0	0.9	0.0	37.30	47.54	7.15	x 53 e 36	0.51	5702.15	5702.52	5704.32	5704.51	5708.48	5708.48	2
3	2	26.003	0.00	0.00	0.00	0.00	0.00	0.0	0.8	0.0	22.80	22.63	7.26	24	1.00	5703.26	5703.52	5705.33	5705.60	5708.48	5708.71	3
ŀ	3	239.285	0.00	0.00	0.00	0.00	0.00	0.0	0.1	0.0	17.80	22.60	6.31	24	1.00	5703.62	5706.01	5705.94	5707.53	5708.71	5712.17	4
5	4	35.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	17.00	22.62	6.96	24	1.00	5706.11	5706.46	5707.53	5707.95	5712.17	5711.79	5
6	2	22.463	0.00	0.00	0.00	0.00	0.00	0.0	0.6	0.0	16.10	16.54	5.13	24	0.53	5703.26	5703.38	5705.33	5705.45	5708.48	5707.92	6
7	6	151.599	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	8.10	7.43	4.58	18	0.50	5703.88	5704.64	5705.51	5706.41	5707.92	5709.01	7
3	1	29.000	0.00	0.00	0.00	0.00	0.00	0.0	0.4	0.0	22.40	22.62	8.07	24	1.00	5702.90	5703.19	5704.52	5704.88	5708.48	5708.74	8
9	8	125.197	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	9.70	10.49	6.43	18	1.00	5703.69	5704.94	5704.88	5706.14	5708.74	5706.75	9
10	8	29.568	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	11.00	10.58	6.80	18	1.02	5703.69	5703.99	5704.98	5705.28	5708.74	5705.79	10
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# MAP POCKET

