FINAL DRAINAGE REPORT FOR SCHMIDT PARCEL EARLY GRADING

Prepared For:

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> SEPTEMBER 2022 Project No. 25188.13

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> PCD Filing No.: CDR-22-007



FINAL DRAINAGE REPORT FOR SCHMIDT PARCEL

SEPTEMBER 2022

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Muh Touli

Mike Bramlett, Colorado P.E. 32314 For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Turkey Canon Quarry, LLC

By:

Title: Address:

V.P. 20 Boulder Crescent, Suite 200

20 Boulder Crescent, Suite 200 Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

APPROVED Engineering Department 12/07/2022 4:07:18 PM dsdnijkamp EPC Planning & Community Development Department

Date

Joshua Palmer, P.E. County Engineer/ ECM Administrator

Conditions:



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PURPOSE

This document is the Final Drainage Report for the Schmidt Parcel. The purpose of this report is to identify on-site and off-site drainage patterns, areas tributary to the site, and to safely route storm water to adequate outfall facilities.

GENERAL SITE DESCRIPTION

GENERAL LOCATION

The Schmidt Parcel (hereby referred to as the "site") is a proposed development with a total area of approximately 97 acres.

The site is located in the southwest quarter of Section 32, Township 12 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located between Black Forest Road and Vollmer Road. The site is bounded by the Trails at Forest Meadows Fillings 3 and 4 to the south, by Silver Pond subdivision and Holiday Hills Filing No.1 to the north, by Black Forest Road to the West and by Vollmer Road to the East. The parcel is planned to be platted after approval of the Preliminary Plan. Refer to the vicinity map in Appendix A for additional information.

DESCRIPTION OF PROPERTY

The site is currently being designed to partly fill in the large pit in the middle of the site. Eventually the parcel will be platted as single and multi-family residential lots and associated development. The site is comprised of variable sloping grasslands that generally slope(s) downward to the west at 2 to 25% towards the Cottonwood Creek tributary basin.

Per a NRCS web soil survey, the site is made up of Type A and B soils. Type A soils have a high infiltration rate when thoroughly wet, while Type B soils have a moderate infiltration when thoroughly wet. Refer to the soil survey map in Appendix A for additional information.

Cottonwood Creek is within the western portion of the site. However there is no proposed disturbance within the creek.

There are no known irrigation facilities located on the project site.

FLOODPLAIN STATEMENT

Based on the FEMA Firm Maps Number 08041C0529G revised December 7, 2018, the vast majority of the development is located within Zone X, or areas area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. A portion of the site is within Zone AE directly adjacent to Cottonwood Creek. The area of disturbance



for site grading is located outside of the delineated floodway within Zone X. The FEMA map containing the site has been presented in Appendix A.

EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek and Cottonwood Creek Drainage Basins. Approximately 16 acres on the sites eastern property line is in the Sand Creek Drainage Basin, while the remainder of the site lies within the Cottonwood Creek Drainage Basin.

Cottonwood Creek transverse the site on the west side of the property running north to south. The reach that runs through the site was studied in the "Cottonwood Creek Drainage Basin Planning Study" (Cottonwood DBPS) completed by Matrix Design Group in July 2019. According to the Cottonwood Creek DBPS reach RUC160 runs through the site, and has been identified as being in stable condition.

The Sand Creek Basin was studied by the City of Colorado Springs in "Sand Creek Drainage Basin Planning Study" (Sand DBPS) completed by Stantec in January 2021. The Sand Creek DBPS assumed the Schmidt Parcel property to have an "Open Space" use for the majority of the site, which is consistent with the proposed development at this time. However, the Cottonwood Creek DBPS assumed a 2.5 Acre Rural Residential Land use for the majority of the site. The site generally drains from northeast to southwest consisting of slopes that range from 2 to 25 %. Currently, the site is undeveloped and a large pit exists in the middle.

EXISTING SUB-BASIN DRAINAGE

The existing condition consists of nine onsite basins and four offsite basins. Values for Basins OSI4 and OSB4 came from "Silver Ponds Subdivision Filing No.1 Final Drainage Report", by M.V.E Inc. revised May 5th 1996.

Basin OSI4 (Q5 = 19.0 cfs, Q100 = 44.2 cfs) is 27.16 acres of an existing developed subdivision know as Silver Ponds Subdivision Filing 1.Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report", by M.V.E Inc. revised May 5th 1996. Runoff from this basin flows south and enters the site across the northern property line at DPI4. Flow from this basin is routed through Basin EX3 to DP3.1 (Q5 = 17.0 cfs, Q100 = 40.0 cfs) where flow enters Cottonwood Creek.

Basin OSB4 (Q5 = 39.1 cfs, Q100 = 89.8 cfs) is 52.02 acres of an existing developed subdivision know as Silver Ponds Subdivision Filing 1.Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report", by M.V.E Inc. revised May 5^{th} 1996. Runoff from this basin flows south and enters the site across the northern property line at DPB4. Flow from this



basin is routed through Basin EX7 to DP7.1 (Q5 = 43.1, Q100 = 97.9 cfs) where flow enters the adjacent property.

Basin OS1 (Q5 = 0.2 cfs, Q100 = 1.5 cfs) is 0.61 acres of dirt roadway. Runoff from this basin flows south and enters the site across the northern property line at DP10. Flow from this basin is routed through Basins EX2 and EX4 to DP4.1 (Q5 = 7.6cfs, Q100 = 50.9 cfs) where flow remains in the existing pit until it evaporates or infiltrates.

Basin OS2 (Q5 = 0.1 cfs, Q100 = 0.6 cfs) is 0.22 acres of dirt roadway. Runoff from this basin flows south and enters the site across the northern property line at DP11. Flow from this basin is routed through Basin EX1 to DP1.1 (Q5 = 2.8 cfs, Q100 = 19.0 cfs) where flow enters Vollmer Road right of way.

Basin EX1 (Q5 = 2.8 cfs, Q100 = 18.8 cfs) is 15.6 acres of undeveloped land at the eastern portion of the site. Runoff from this basin drains to Vollmer Road right of way at DP1. Flows from Basin OS2 is routed through Basin EX1, and exists the site at DP1.1 (Q5 = 2.8 cfs, Q100 = 19.0 cfs). Flow continues southwest along Vollmer Road right of way and follows existing drainage patterns. There is no drainage infrastructure at DP1.1 in the existing condition. Runoff that enters Vollmer Road right of way is assumed to overtop the crown of Vollmer Road and continues to flow southeast towards Sand Creek.

Basin EX2 (Q5 = 3.1 cfs, Q100 = 20.6 cfs) is 22.9 acres of undeveloped land. Runoff from this basin overland flows south where it meets the bottom of an existing berm along the southern boundary. Flow is directed into the existing pit at DP2. Flow enters the basin at DP10 from basin OS1 and is routed through basin EX2 to DP2.1 (Q5 = 3.2 cfs, Q100 = 21.1 cfs). Flows from DP2.1 continue to flow to DP4.1 (Q5 = 7.6cfs, Q100 = 50.9 cfs) where runoff remains in the pit.

Basin EX3 (Q5 = 0.5 cfs, Q100 = 3.1 cfs) is 2.50 acres of undeveloped land adjacent to the northern property line. Runoff from this basin flows north down slope of the existing berm and is routed along the base of the berm to DP3. Off-site runoff enters the basin along the northern property line from Basin OSI4. Flows are routed together at DP3.1 (Q5 = 17.0 cfs, Q100 = 40.0 cfs) and then flow west and enter Cottonwood Creek.

Basin EX4 (Q5 = 7.6 cfs, Q100 = 51.0 cfs) is 33.1 acres of undeveloped land that mainly consists of an existing pit that is approximately 31 acres in area and 15 feet deep. Runoff from this basin flows south to DP4. Flow enters the basin at DP 2.1 (Q5 = 3.2 cfs, Q100 = 21.1 cfs) and is routed to DP4.1 (Q5 = 7.6 cfs, Q100 = 50.9 cfs). Currently there is no outlet for the pit and runoff remains in the pit and either evaporates or infiltrates over time.



Basin EX5 (Q5 = 2.2 cfs, Q100 = 14.7 cfs) is 8.0 acres of undeveloped land that drains to the west, directly into Cottonwood Creek. Flows from DP5 and DP6 combine at DP6.1 (Q5 = 3.1 cfs, Q100 = 21.0 cfs). Flow leaves the site at DP6.1 and continues to flow in Cottonwood Creek to the southwest.

Basin EX6 (Q5 = 0.9 cfs, Q100 = 6.3 cfs) is 3.4 acres of undeveloped land that drains to the east, directly into Cottonwood Creek. Flows from DP5 and DP6 combine at DP6.1 (Q5 = 3.1 cfs, Q100 = 21.0 cfs). Flow leaves the site at DP6.1 and continues to flow in Cottonwood Creek to the southwest.

Basin EX7 (Q5 = 0.9, Q100 = 5.7 cfs) is 2.9 acres of undeveloped land that drains southwest to DP7. Off-site flows enter the site at DPB4 (Q5 = 39.1, Q100 = 89.8 cfs). Flows from OSB4 are routed through the basin via overland flow to DP7.1 (Q5 = 43.1, Q100 = 97.9 cfs) where flow leaves the site and enters the adjacent property.

Basin EX8 (Q5 = 1.3 cfs, Q100 = 8.5 cfs) is 6.40 acres of undeveloped land that drains to the south via overland flow to DP8. Flow exists the site at DP8 and continues to flow onto the adjacent property to the south known as the Trails at Forest Meadows Filing 4.

Basin EX9 (Q5 = 0.9 cfs, Q100 = 6.0 cfs) is 2.4 acres of undeveloped land that drains south down slope of the existing berm via overland flow. Runoff from this basin leaves the site across the southern boundary and enters the subdivision to the south at DP9.

PROPOSED DRAINAGE CONDITIONS

PROPOSED SUB-BASIN DRAINAGE

The proposed basin (and sub-basin) delineation is shown on the drainage basin map within Appendix D and is described as follows.

Basin A ($Q_5=1.9$ cfs, $Q_{100}=13.0$ cfs) is 11.7 acres of native and stabilized vegetation. Runoff from this basin drains south east and enters purposed swale B1-B1. Flow for Basin A enters Basin B at design point 1. Flow from DP1 is routed through Basins B and F where flow is ultimately routed to the proposed sediment basin at DP6.1 ($Q_5=10.1$ cfs, $Q_{100}=68.7$ cfs).

Basin B ($Q_5=3.5$ cfs, $Q_{100}=23.8$ cfs) is 22.0 acres of native and stabilized vegetation. Runoff from this basin drains south west and enters purposed swale B1-B1. Flow for Basin B enters Basin F at design point 2. Flow is routed through Basin F to the purposed sediment basin at DP6.1 ($Q_5=10.1$ cfs, $Q_{100}=68.7$ cfs).



Basin C ($Q_5=0.8$ cfs, $Q_{100}=5.5$ cfs) is 4.0 acres of undeveloped land with native vegetation. Runoff from this basin drains south east to DP3, where flow enters Vollmer Road right of way. There is no drainage infrastructure at DP3. Runoff that enters Vollmer Road right of way flows existing drainage patterns and is assumed to overtop the crown of Vollmer Road and continues to flow southeast towards Sand Creek. Total runoff entering the right of way has decreased from ($Q_5=2.8$ cfs, $Q_{100}=19.0$ cfs) in the existing condition to ($Q_5=0.8$ cfs, $Q_{100}=5.5$ cfs) in the proposed condition.

Basin D ($Q_5=0.6$ cfs, $Q_{100}=4.3$ cfs) is 2.6 acres of native and stabilized vegetation. Runoff from this basin drains south to DP4. Flow from Basin D overland flows to the adjacent site to the south known as Trails at Forest Meadows Filings 3. Runoff from the site was accounted for in "Trails at Forest Meadows Filing No. 3 Final Drainage Report" (Trails No. 3 FDR) completed by M&S Civil Consultants in August 2015. In the Trails No. 3 FDR flows from the Schmidt parcel were accounted for in Basins OS2 and OS3. The basins total 1.56 acres and send a total flow of $Q_5=1.0$ cfs and $Q_{100}=$ 3.6 cfs. Proposed condition flows remain reasonable consistent with accounted for flows from the Trails No. 3 FDR. There are no expected negative downstream impacts expected from basin D.

Basin E ($Q_5=0.2$ cfs, $Q_{100}=1.5$ cfs) is 1.6 acres of stabilized earthen channel known as Swale B2-B2. Runoff from this basin drains west to DP5. Off-site flow enters the basin at DP14 from the neighboring site the north known as Silver Ponds Subdivision Filing No. 1. Flows from Basin E and OSI4 combine and enter Cottonwood Creek at DP5.1 ($Q_5=13.2$ cfs, $Q_{100}=30.5$ cfs).

Basin F ($Q_5=5.7$ cfs, $Q_{100}=42.6$ cfs) is 36.6 acres of native and stabilized vegetation. Grading efforts in this basin are to provide a sediment basin to provide water quality and detention for the parcel as well as providing a smooth ~2.0% plane to convey runoff to the sediment basin. Runoff from this basin drains southwest to DP6. Flow enters the basin at DP2.1 ($Q_5=5.3$ cfs, $Q_{100}=36.2$ cfs) from Basins A and B. Flow combines in the proposed sediment basin at DP6.1 ($Q_5=10.1$ cfs, $Q_{100}=68.7$ cfs).

Basin G ($Q_5=1.0$ cfs, $Q_{100}=7.0$ cfs) is 4.3 acres of undeveloped land that drains to the south at DP7. Runoff from this basin overland flow to DP7 and continues to flow onto the adjacent property to the south known as the Trails at Forest Meadows Filing 4. This basin was studied in "Trails at Forest Meadows Filing No. 4 Final Drainage Report" (Trails No. 4 FDR) completed by M&S Civil Consultants in April 2016, as basin OS5. Basin OS5 from the Trails No. 4 FDR had an area of 4.46 acres with flows of $Q_5 = 2.1$ cfs and $Q_{100}= 9.0$ cfs. Developed runoff remains relatively consistent with expected flows for the Trails No. 4 FDR. There are no expected negative downstream impacts expected from this basin.

Basin H ($Q_5=1.9$ cfs, $Q_{100}=12.7$ cfs) is 10.2 acres of undeveloped land that drains to the west, directly into Cottonwood Creek at DP8. Flows from DP8 and DP9 combine at DP9.1 ($Q_5=2.6$ cfs,



 Q_{100} = 18.7 cfs) where flow leaves the site and continues to flow in Cottonwood Creek to the southwest.

Basin I ($Q_5=0.6$ cfs, $Q_{100}=4.2$ cfs) is 3.4 acres of undeveloped land that drains to the east, directly into Cottonwood Creek at DP9. Flows from DP8, DP9 and outflow from the Sediment Basin combine at DP9.1 ($Q_5=2.6$ cfs, $Q_{100}=18.7$ cfs) where flow leaves the site and continues to flow in Cottonwood Creek to the southwest.

Basin J ($Q_5=0.7$ cfs, $Q_{100}=4.7$ cfs) is 2.9 of undeveloped land that drains southwest to DP10. Offsite flows enter the site at DPB4 ($Q_5=39.1$ cfs, $Q_{100}=89.8$ cfs). Flows from OSB4 are routed through the basin via overland flow to DP10.1 ($Q_5=43.1$ cfs, $Q_{100}=97.9$ cfs) where flow leaves the site and enters the adjacent property.

Basin OSI4 (Q5 = 19.0 cfs, Q100 = 44.2 cfs) is 27.16 acres of an existing developed subdivision know as Silver Ponds Subdivision Filing 1.Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report", by M.V.E Inc. revised May 5th 1996. Runoff from this basin flows south and enters the site across the northern property line at DPI4. Flow from this basin is routed through Basin E to DP5.1 (Q5 = 13.2 cfs, Q100 = 30.5 cfs) where flow enters Cottonwood Creek. There is no significant change in flows going to Cottonwood Creek in the proposed condition than there was in the existing condition, as the flows were already concentrated towards the creek.

Basin OSB4 (Q5 = 39.1 cfs, Q100 = 89.8 cfs) is 52.02 acres of an existing developed subdivision know as Silver Ponds Subdivision Filing 1.Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report", by M.V.E Inc. revised May 5th 1996. Runoff from this basin flows south and enters the site across the northern property line at DPB4. Flow from this basin is routed through Basin J to DP10.1 (Q5 = 43.1 cfs, Q100 = 97.9 cfs) where flow enters the adjacent property. Since there is no proposed changes made in basin J, flows remain the same as in the proposed condition as the existing condition.

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.



HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Table 1 - 1-hr Point Rainfall Data

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD MHFD-Detention v4.05 spreadsheet was utilized for evaluating the proposed sediment basin. Hydraflow Express was used to model swale capacity calculations as shown in Appendix C. Proposed swales B1, B2, and C have been designed to meet El Paso County criteria for velocity, freeboard, and stability. All proposed swales will be temporary until the time of construction for the proposed single and multi-family developments proposed for this site.

DRAINAGE FACILITY DESIGN

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Flow from the site enters Cottonwood Creek in two locations. At the northwestern corner of the property known as DP3.1 (Q5 = 17.0 cfs, Q100 = 40.0 cfs) in existing condition & DP5.1 (Q₅= 13.2 cfs, Q₁₀₀= 30.5 cfs) in proposed condition. Flow also enters Cottonwood Creek at the western boundary known a DP 6.1 (Q5 = 3.1 cfs, Q100 = 21.0 cfs) in existing condition & DP9.1 (Q₅=2.6 cfs, Q₁₀₀= 18.7 cfs) in proposed condition. Flow entering Cottonwood Creek has slightly decreased in the



proposed condition at both locations. There is no expected changes in water surface elevations in Cottonwood Creek with the development of this site.

Step 1 – Reducing Runoff Volumes: The Schmidt Parcel development project does not consists of any proposed hardscape or roofs and therefor all runoffs associated with this development are routed via overland flow or through grass lined swales.

Step 2 – Stabilize Drainageways: The majority of the site lies within the Cottonwood Creek Drainage Basin, while the eastern most portion on the property is within the Sand Creek Drainage Basin. Cottonwood Creek transvers the western portion of the site. Basin and bridge fees will be due at time of platting. There are no proposed improvements with the 100-year flood plain. According "Cottonwood Creek Drainage Basin Planning Study" (Cottonwood DBPS) completed by Matrix Design Group in July 2019, the creek reach that transvers the site is known as RUC160. This reach has been categorized as having no know or future expected erosion issues according to the Cottonwood DBPS Figure 4-7. Proposed outfalls will be analysis in the final design stage for stability. Applicable excerpts from Cottonwood DBPS can be found in Appendix D.

Step 3 – Treat the WQCV: The sites water quality will be provided by a temporary sediment basin. Long term water quality for the site will be provided by on site full spectrum water quality and detention ponds that will be designed at the time of construction documents associated with the single and multi-family developments planed for the site. The runoff from this site will be routed to the proposed sediment basin via overland flow and grassed lined swales. The proposed sediment basin has been designed to promote settlement of suspended solids. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 72 hours per Mile High Flood District guidelines. All flows released from the sediment basin and future ponds will be reduced to less than historic rates.

Step 4 – Consider Need for Industrial and Commercial BMPs: There are no commercial or industrial components to this development; therefore no BMPs of this nature are required. BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The site is not a high-risk site per Figure I-1 in ECM Appendix I, therefore specialized BMPs do not need to be considered. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include permanent vegetation, permanent swale, and sediment basin.

WATER QUALITY

The sites water quality will be provided by a temporary sediment basin. Long term water quality for the site will be provided by on site full spectrum water quality and detention ponds that will be designed at the time of construction documents associated with the single and multi-family



developments planed for the site. The proposed sediment basin was designed per Urban Drainage and Flood Control District guidelines. Flow shall be released per detail per Mile High Flood District detail SC-7. The riser pipe shall be 12" in diameter to be connected to a 12" outfall pipe that will direct flow to swale C-C. An emergency overflow spillway is provided for the sediment basin that is directed into Cottonwood Creek from swale C-C. For this drainage report the design points are discussed in the Proposed Drainage Conditions section of this report. The corresponding design points and basin are shown within the Proposed Drainage Map within Appendix E. For additional information on the proposed sediment basin and outlet characteristics see the MHFD sheets within Appendix C.

EROSION CONTROL PLAN

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. We respectfully request that the Operation & Maintenance Manual be submitted in conjunction with the construction documents, prior to obtaining a grading permit.

DRAINAGE AND BRIDGE FEES

The site lies within the Cottonwood Creek and Sand Creek Drainage Basins. Anticipated drainage and bridge fees will be provided at time of platting.

SUMMARY

The proposed Schmidt Parcel drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainage ways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements.



REFERENCES

- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2. El Paso County ECM, 2019
- 3. El Paso County DCM Vol. 1 Update, 2015
- 4. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- 5. <u>Final Drainage Report For Silver Ponds Subdivision Filing No. 1</u>, M.V.E. Inc., Febuary 2, 1995, Revised May 5, 1996.
- 6. Sand Creek Drainage Basin Planning Study, Stantec, January 2021
- 7. <u>Cottonwood Creek Drainage Basin Planning Study</u>, Matrix Design Group, July 2019
- 8. <u>Trails at Forest Meadows Filing No. 3 Final Drainage Report M&S Civil Consultants Inc.</u>, August 2015
- 9. <u>Trails at Forest Meadows Filing No. 4 Final Drainage Report M&S Civil Consultants Inc.</u>, April 2016



Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map







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National Cooperative Soil Survey

Conservation Service



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.3	19.5%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	64.2	56.2%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	12.1	10.6%
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	В	15.6	13.6%
Totals for Area of Intere	st		114.1	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



NOTES TO USERS

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.



Appendix B Hydrologic Calculations



COMPOSITE % IMPERVIOUS CALCULATIONS - EXISTING CONDITIONS

Subdivision:

Location: El Paso County

Project Name: Schmidt Parcel

Project No.: 25188.13

Calculated By: <u>APL</u>

Checked By:

Date: <u>9/2/22</u>

		PAS	STURE/MEA	DOW (2% Ir	np.)	Basin	s Total	Basins Total
Basin ID	Total Area	C.	Com	Area (ac)	Weighted	Weig	nted C	Weighted %
Dasin iD	(ac)	C 5	C 100	Alca (ac)	% Imp.	C ₅	C ₁₀₀	Imp.
EX1	15.60	0.09	0.36	15.60	2.0%	0.09	0.36	2.0%
EX2	22.90	0.09	0.36	22.90	2.0%	0.09	0.36	2.0%
EX3	2.50	0.09	0.36	2.50	2.0%	0.09	0.36	2.0%
EX4	33.10	0.09	0.36	33.10	2.0%	0.09	0.36	2.0%
EX5	8.00	0.09	0.36	8.00	2.0%	0.09	0.36	2.0%
EX6	3.40	0.09	0.36	3.40	2.0%	0.09	0.36	2.0%
EX7	2.90	0.09	0.36	2.90	2.0%	0.09	0.36	2.0%
EX8	6.40	0.09	0.36	6.40	2.0%	0.09	0.36	2.0%
EX9	2.40	0.09	0.36	2.40	2.0%	0.09	0.36	2.0%
OS1	0.61	0.09	0.36	0.61	2.0%	0.09	0.36	2.0%
OS2	0.22	0.09	0.36	0.22	2.0%	0.09	0.36	2.0%
TOTAL	98.03							2.0%

STANDARD FORM SF-2 - EXISTING CONDITIONS TIME OF CONCENTRATION

Subdivision:

Location: El Paso County

Project Name: Schmidt Parcel

Project No.: 25188.13

Calculated By: APL

Checked By:

Date: 9/2/22

		SUB-	BASIN			INITI	AL/OVER	LAND		т	RAVEL TIM	IE				í	
		D/	ATA				(T _i)				(T _t)			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C₅	C ₁₀₀	L	S _o	t i	L _t	S _t	к	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t _c	t _c
ID	(ac)	Soils Group	(%)		<u> </u>	(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
EX1	15.60	А	2%	0.09	0.36	300.0	2.5%	23.2	872	2.5%	5.0	0.8	18.4	41.6	1172.3	35.6	41.6
EX2	22.90	A	2%	0.09	0.36	300.0	2.3%	23.9	1412	1.9%	5.0	0.7	34.1	58.1	1712.0	44.1	58.1
EX3	2.50	A	2%	0.09	0.36	38.0	18.1%	4.3	1278	1.4%	5.0	0.6	36.2	40.6	1315.5	45.2	40.6
EX4	33.10	А	2%	0.09	0.36	300.0	5.4%	18.1	945	2.2%	10.0	1.5	10.6	28.7	1244.7	37.0	28.7
EX5	8.00	В	2%	0.09	0.36	227.0	11.0%	12.5	1054	2.1%	15.0	2.2	8.1	20.5	1281.0	38.7	20.5
EX6	3.40	В	2%	0.09	0.36	202.0	10.4%	12.0	1054	2.1%	15.0	2.2	8.1	20.0	1256.0	38.7	20.0
EX7	2.90	В	2%	0.09	0.36	175.0	2.6%	17.6	0	0.0%	5.0	0.0	0.0	17.6	175.0	25.7	17.6
EX8	6.40	А	2%	0.09	0.36	300.0	2.0%	25.3	453	2.0%	5.0	0.7	10.7	36.0	753.0	31.4	36.0
EX9	2.40	А	2%	0.09	0.36	53	9.0%	6.4	0	0.0%	5.0	0.0	0.0	6.4	53.0	25.7	10.0
OS1	0.61	A	2%	0.09	0.36	30.1	1.8%	8.2	0	0.0%	10.0	0.0	0.0	8.2	30.1	25.7	10.0
OS2	0.22	А	2%	0.09	0.36	34.7	1.8%	8.8	0	0.0%	10.0	0.0	0.0	8.8	34.7	25.7	10.0

NOTES:

$t = t_1 + t_2$	Equation	$6-2$ $0.395(1.1-C_5)\sqrt{L_i}$	F (63	Table 6-2. NRCS Conveyance factors, K					
· c · 1 · · f	Equation	$t_i = \frac{1}{S_0^{0.33}}$	Equation 0-3	Type of Land Surface	Conveyance Factor, K				
Where:				Heavy meadow	2.5				
$t_c = \text{computed time of concentration (minutes)}$		Where:		Tillage/field	5				
		t_i = overland (initial) flow time (minutes)		Short pasture and lawns	7				
t_i = overland (initial) flow time (minutes)		C_5 = runoff coefficient for 5-year frequency (from Table 6-4) L_1 = length of overland flow (ft)		Nearly bare ground	10				
t_t = channelized flow time (minutes).		$S_o =$ average slope along the overland flow path (ft/ft).		Grassed waterway	15				
L. L.				Paved areas and shallow paved swales	20				
$t_t = \frac{1}{60K\sqrt{S_o}} = \frac{1}{60V_t}$	Equation 6-4	$t_c = (26 - 1/t) + \frac{1}{60(14i + 9)\sqrt{S_t}}$	Equation 6-5						
Where:		Where:							
t_t = channelized flow time (travel time, min) L_t = waterway length (ft)		t_c = minimum time of concentration for first design point when less	than t_c from Equation 6-1.						

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

 L_t = waterway length (ft) $L_t = \text{waterway regim (ii)}$ $S_0 = \text{waterway slope (ft/ft)}$ $V_t = \text{travel time velocity (ft/sec)} = K\sqrt{S_0}$ K = NRCS conveyance factor (see Table 6-2).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3 - EXISITNG CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Project Name: Schmidt Parcel Project No.: 25188.13 Calculated By: APL

Sub	division:	

Location: El Paso County

Design Storm: 5-Year													Checked By: Date: 9/2/22										
		DIRECT RUNOFF TOTAL RUN										F	1	STREE	т	I	Р	IPE		TRA	AVEL 1	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _r (min)	REMARKS
	1	1 EX1 15.60 0.09 41.6 1.40 1.99 2.8																		Runoff overland flows across exisitng field to DP1 where flow enters Vollmer ROW			
	1.1	1 1.41 1.40 1.55 2.8 1.1 41.6 1.42 1.99								2.8											Flow for Basin EX1 and OS2 combine at DP 1.1 and enters Vollmer ROW		
	2	EX2	22.90	0.09	58.1	2.06	1.49	3.1															contiues into Basin EX2, overland hows across existing field to DP 2 where how
	2.1								58.1	2.12	1.49	3.2											Flows Form Basin EX2 and OS1 combine at DP2.1 and enters Basin EX4
	3	EX3	2.50	0.09	40.6	0.23	2.03	0.5															Runoff from Basin EX3 overland flows down berm and flows along bottom of berm to DP3 .
	3.1								40.6	8.37	2.03	17.0											Flows from Basin EX3 and DP I4 combine at DP3.1 and enters Cottonwood Creek
	4	EX4	33.10	0.09	28.7	2.98	2.55	7.6															Runoff form basin EX4 overland flows across steep side slopes into the exisitng pit, flow contuies to travel south and remains in the pit at DP4
	4.1								58.1	5.09	1.49	7.6											Flow for Basin EX4 and desing point DP2.1 combine at DP 4.1
	5	EX5	8.00	0.09	20.5	0.72	3.05	2.2															Runoff from Basin EX5 overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	6	EX6	3.40	0.09	20.0	0.31	3.09	0.9															slopes & contuies to flow along the thalweg axis of the creek
	6.1								20.5	1.03	3.05	3.1											Cottonwood Creek to the Southwest
	7	EX7	2.90	0.09	17.6	0.26	3.28	0.9															Runoff from Basin EX7, overland flows southwest to the adjacent property at DP7
	7.1								28.7	16.91	2.55	43.1											Flows from Basin EX7 and DP B4 combine at DP7.1 and flow contuines on to neighboring property
	8	EX8	6.40	0.09	36.0	0.58	2.21	1.3															Runoff from Basin EX8, overland flows south to DP8 where flow leaves the site and enters the subdivision to the south
	9	EX9	2.40	0.09	10.0	0.22	4.13	0.9															Runoff from Basin EX9, overland flows south and enters the adjacent property to the south
	10	OS1	0.61	0.09	10.0	0.05	4.13	0.2															Runoff from Basin OS1, overland flows south and enters the site at DP10
	11 OS2 0.22 0.09 10.0 0.02 4.13 0.1															Runoff from Basin OS2, overland flows south and enters the site at DP11							
	B4	OSB4	52.02	0.32	28.7	16.65	2.35	39.1															Off-site basin OSB4 Values from Sliver Pond FDR (Bains OS1- B4 & DP8)
	14	OSI4	27.16	0.30	29.2	8.15	2.33	19.0															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - EXISITNG CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	El Pas 100-Ye	o Cour ear	unty															ame: t No.: d By: d By: Date:	Schm 25188 APL 9/2/2	idt Pa 8.13	rcel		
		1		DIRE		NOFE			Т					TDEE	r		DI	DE	-	ΤΡΑΙ		F	
		-		DIRE		IOFF								TINEL			FI	F L	(INAV		L	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	EX1	15.60	0.36	41.6	5.62	3.34	18.8															Runoff overland flows across exisitng field to DP1 where flow enters Vollmer ROW
	1.1								41.6	5.70	3.34	19.0											Flow for Basin EX1 and OS2 combine at DP 1.1 and enters Vollmer ROW
	2	EX2	22.90	0.36	58.1	8.24	2.50	20.6															Runoff from Basin EX2, overland flows across exsiting field to DP 2 where flow contiues into Basin EX4
	2.1								58.1	8.46	2.50	21.1											Flows Form Basin EX2 and OS1 combine at DP2.1 and enters Basin EX4
	3	EX3	2.50	0.36	40.6	0.90	3.40	3.1															Runoff from Basin EX3 overland flows down berm and flows along bottom of berm to DP3 .
	3.1								40.6	11.76	3.40	40.0											Flows from Basin EX3 and DP I4 combine at DP3.1 and enters Cottonwood Creek
	4	EX4	33.10	0.36	28.7	11.92	4.28	51.0															Runoff form basin EX4 overland flows across steep side slopes into the exisitng pit, flow contuies to travel south and remains in the pit at DP4
	4.1								58.1	20.38	2.50	50.9											Flow for Basin EX4 and desing point DP2.1 combine at DP 4.1
	5	EX5	8.00	0.36	20.5	2.88	5.12	14.7															Runoff from Basin EX5 overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	6	EX6	3.40	0.36	20.0	1.22	5.18	6.3															Runoff from Basin EX6 overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	6.1								20.5	4.10	5.12	21.0											Flow from basin EX5 and EX6 combine at DP6.1 and contuines to flow in Cottonwood Creek to the Southwest
	7	FX7	2 90	0.36	17.6	1 04	5 51	57			-												Runoff from Basin EX7, overland flows southwest to the adjacent property at DP7
	71	2,07	2.00	0.00		1.0 1	5.51	517	28.7	22.80	1 28	97.9											Flows from Basin EX7 and DP B4 combine at DP7.1 and flow contuines on to
	0	EVO	6 40	0.26	26.0	2 20	2 70	0 5	20.7	22.05	4.20	57.5											Runoff from Basin EX8, overland flows south to DP8 where flow leaves the site
	0	EVO	2.40	0.30	10.0	2.30	6.02	6.5															Runoff from Basin EX9, overland flows south and enters the adjacent property to
	9	0.51	2.40	0.30	10.0	0.00	0.95	0.0															the south Runoff from Basin OS1, overland flows south and enters the site at DP10
	10	051	0.01	0.30	10.0	0.22	0.95	1.5															Runoff from Basin OS2, overland flows south and enters the site at DP11
														Off-site basin OSB4 Values from Sliver Pond FDR (Bains OS1- B4 & DP8)									
	D4	OSI4	27.16	0.42	28.7	10.86	4.11	44.2															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

COMPOSITE % IMPERVIOUS CALCULATIONS - PROPOSED CONDITIONS

Subdivision:

Location: El Paso County

Project Name: Schimidt Parcel

Project No.: 25188.13

Calculated By: APL

Checked By:

Date: 9/2/22

			Gravlel (80% Imp.)		PAS	STURE/MEA	DOW (0% Ir	np.)	Basins	s Total	Basins Total
Basin ID	Total Area	C₅	C ₁₀₀	Area (ac)	Weighted	C₅	C ₁₀₀	Area (ac)	Weighted	Weigl	nted C	Weighted %
	(ac)	5			% Imp.	C ₅ C ₁₀₀		. ,	% Imp.	C ₅	C ₁₀₀	Imp.
А	11.70	0.59	0.70	0.00	0.0%	0.09	0.36	11.70	2.0%	0.09	0.36	2.0%
В	22.00	0.59	0.70	0.45	1.6%	0.09	0.36	21.55	2.0%	0.10	0.37	3.6%
С	4.00	0.59	0.70	0.00	0.0%	0.09	0.36	4.00	2.0%	0.09	0.36	2.0%
D	2.60	0.59	0.70	0.00	0.0%	0.09	0.36	2.60	2.0%	0.09	0.36	2.0%
E	1.60	0.59	0.70	0.00	0.0%	0.09	0.36	1.60	2.0%	0.09	0.36	2.0%
F	36.60	0.59	0.70	0.36	0.8%	0.09	0.36	36.24	2.0%	0.09	0.36	2.8%
G	4.30	0.59	0.70	0.00	0.0%	0.09	0.36	4.30	2.0%	0.09	0.36	2.0%
н	10.20	0.59	0.70	0.00	0.0%	0.09	0.36	10.20	2.0%	0.09	0.36	2.0%
I.	3.40	0.59	0.70	0.00	0.0%	0.09	0.36	3.40	2.0%	0.09	0.36	2.0%
J	2.90	0.59	0.70	0.00	0.0%	0.09	0.36	2.90	2.0%	0.09	0.36	2.0%
TOTAL	99.30											2.6%

SB TOTAL 70.30

2.90%

STANDARD FORM SF-2 - PROPOSED CONDITIONS TIME OF CONCENTRATION

Subdivision:

Location: El Paso County

Project Name: Schimidt Parcel

Project No.: 25188.13

Calculated By: APL

Checked By:

9/2/22 Date:

		SUB-	BASIN			INITI	AL/OVER	LAND		Т	RAVEL TIM	E					
		D/	ATA				(T _i)				(T _t)			(L	FINAL		
BASIN	D.A.	Hydrologic	Impervious	C₅	C ₁₀₀	L	S _o	ti	L _t	S _t	к	VEL.	t _t	COMP. t c	TOTAL	Urbanized t _c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
А	11.70	А	2.0%	0.09	0.36	300.0	2.8%	22.6	1324	1.8%	7.0	0.9	23.6	46.2	1623.7	43.5	46.2
В	22.00	А	3.6%	0.10	0.37	300.0	2.3%	23.8	1402	1.8%	7.0	0.9	24.9	48.6	1701.7	43.7	48.6
С	4.00	А	2.0%	0.09	0.36	300.0	2.1%	24.8	423	2.1%	5.0	0.7	9.8	34.6	722.7	30.9	34.6
D	2.60	А	2.0%	0.09	0.36	231.8	2.6%	20.3	0	0.0%	5.0	0.0	0.0	20.3	231.8	25.7	25.7
E	1.60	А	2.0%	0.09	0.36	35.0	2.9%	7.6	1372	0.8%	7.0	0.6	36.5	44.1	1406.5	53.2	53.2
F	36.60	А	2.8%	0.09	0.36	300.0	2.8%	22.3	1554	2.7%	5.0	0.8	31.6	53.9	1853.8	42.4	53.9
G	4.30	В	2.0%	0.09	0.36	300.0	2.0%	25.1	0	0.0%	5.0	0.0	0.0	25.1	300.0	25.7	25.7
Н	10.20	В	2.0%	0.09	0.36	227.0	11.0%	12.5	1054	2.1%	15.0	2.2	8.1	20.6	1281.0	38.8	38.8
I	3.40	В	2.0%	0.09	0.36	202	10.4%	12.0	1054	2.1%	15.0	2.2	8.1	20.1	1256.0	38.7	38.7
J	2.90	В	2.0%	0.09	0.36	175	2.6%	17.7	0	0.0%	5.0	0.0	0.0	17.7	175.0	25.7	25.7

NOTES:

	$t_1 = t_1 + t_2$	Equation 6	$0.395(1.1-C_5)\sqrt{L_i}$	Equation 6.2	Table 6
	C 1 1	Equation o	$T_i = \frac{S_e^{0.33}}{S_e^{0.33}}$	Equation 0-5	Type of Land S
Wher	e:				Heavy mead
	$t_c = \text{computed time of concentration (minutes)}$		Where:		Tillage/fiel
			t_i = overland (initial) flow time (minutes)		Short pasture and
	t_i = overland (initial) flow time (minutes)		$C_5 =$ runoff coefficient for 5-year frequency (from Table 6-4) $L_2 =$ length of overland flow (ft)		Nearly bare gr
	$t_t =$ channelized flow time (minutes).		S_0 = average slope along the overland flow path (ft/ft).		Grassed water
	L. L.				Paved areas and shallow
	$t_t = \frac{1}{60K\sqrt{S_o}} = \frac{1}{60V_t}$	Equation 6-4	$t_c = (26 - 1/i) + \frac{1}{60(14i + 9)\sqrt{S_t}}$	Equation 6-5	
When	e:		Where:		

Where:

 t_t = channelized flow time (travel time, min) L_t = waterway length (ft) $\begin{array}{l} \mathcal{U}_{1} = \forall \mathsf{act}(\mathsf{ray}) \in \mathsf{Righ}(\mathsf{at}) \\ \mathcal{V}_{5} = \forall \mathsf{act}(\mathsf{ray}) \in \mathsf{fr}/\mathsf{f}) \\ \mathcal{V}_{t} = \mathsf{travel time velocity}(\mathsf{ft/sec}) = \mathsf{K} \sqrt{\mathsf{S}_{\circ}} \\ \mathcal{K} = \mathsf{NRCS conveyance factor (see Table 6-2).} \end{array}$

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1. L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Table 0-2. TAKCS CONV	eyance factors, K
Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Payed areas and shallow payed swales	20

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STANDARD FORM SF-3 - PROPOSED CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Date: 9/2/22

	Project Name: Schimidt Parcel
Subdivision:	Project No.: 25188.13
Location: El Paso County	Calculated By: APL
Design Storm: 5-Year	Checked By:

Design Storm: 5-Year

				DIF	RECT RU	NOFF			T	OTAL I	RUNO	FF		STREE	Г		PI	PE		TRA	AVEL TI	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	А	11.70	0.09	46.2	1.05	1.83	1.9															Runoff overland flows to proposed swale and contuies into Basin B at DP1
	2	В	22.00	0.09	48.6	1.98	1.76	3.5															Runoff from Basin B, overland flows to proposed swale and contuies into Basin F at DP2
	2.1								48.6	3.03	1.76	5.3											Flows Form Basin A and B combine at DP2.1 and enters Basin F
	3	С	4.00	0.09	34.6	0.36	2.27	0.8															Runoff overland flows across exisitng field to DP3 where flow enters Vollmer ROW
	4	D	2.60	0.09	25.7	0.23	2.72	0.6															Runoff form basin D overland flows south and enters the adjacent property to the south
	5	E	1.60	0.09	53.2	0.14	1.62	0.2															Runoff from Basin E is collected in the proposed swale and routed west to Cottonwood Creek
	5.1								53.2	8.29	1.62	13.4											Flows from Basins E and DP 14 combine at DP-3.1 and contunie into Cottonwood Creek Rupoff form basin E overland flows across steen side slopes into the nit flow.
	6	F	36.60	0.09	53.9	3.29	1.60	5.3															contuies to travel south and remains in the pit at DP6
	6.1								53.9	6.33	1.60	10.1											Flow from Basin F and DP2.1 combine at DP6.1 and remain in the pit at DP6.1
	7	G	4.30	0.09	25.7	0.39	2.72	1.1															Runoff from Basin G, overland flows southwest to the adjacent property at DP7
	8	н	10.20	0.09	38.8	0.92	2.10	1.9															Runoff from Basin H overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	9	Ι	3.40	0.09	38.7	0.31	2.10	0.6															Runoff from Basin I overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	9.1								38.8	1.22	2.10	2.7											Flow from Basins H and I combine at DP9.1 and contunie to flow in Cottonwood creek offsite, Emergany Spillway Flows are accouned for in 9.1
	10	J	2.90	0.09	25.7	0.26	2.72	0.7															Runoff from Basin J, overland flows south and enters the site at DP10
	10.1								28.7	16.91	2.55	43.1											Flows from Basins J and DP B4 combine at DP10.1 and enters the adjacent proporerty
	B4	OSB4	52.02	0.32	28.7	16.65	2.35	39.1															Off-site basin OSB4 Values from Sliver Pond FDR (Bains OS1- B4 & DP8)
	14	OSI4	27.16	0.30	29.2	8.15	2.33	19.0															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - PROPOSED CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

																Pro	ject N	ame:	Schin	nidt Pa	arcel		
Subdivision:	EL D															0.1	Projec	t No.:	2518	8.13			
Location:	EI Pase	o Cour	ity													Cal	culate	d By:	APL				
Design Storm.	100 10	201														C	[Date:	9/2/2	22			
																				u			
				DIRE	CT RU	NOFF			T	OTAL R	UNOF	F	S	TREET	-		PI	PE		TRAV	EL TIN	ИE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	А	11.70	0.36	46.2	4.21	3.08	13.0															Runoff overland flows to proposed swale and contuies into Basin B at DP1
	2	В	22.00	0.37	48.6	8.07	2.95	23.8															Runoff from Basin B, overland flows to proposed swale and contuies into Basin F at DP2
	2.1								48.6	12.28	2.95	36.2											Flows Form Basin A and B combine at DP2.1 and enters Basin F
	3	с	4.00	0.36	34.6	1.44	3.80	5.5															Runoff overland flows across exisitng field to DP3 where flow enters Vollmer ROW
	4	D	2.60	0.36	25.7	0.94	4.56	4.3															Runoff form basin D overland flows south and enters the adjacent property to the south
	5	E	1.60	0.36	53.2	0.58	2.72	1.6															Runoff from Basin E is collected in the proposed swale and routed west to Cottonwood Creek
	5.1								53.2	11.44	2.72	31.1											Flows from Basins E and DP I4 combine at DP5.1 and contunie into Cottonwood Creek
	6	F	36.60	0.36	53.9	13.30	2.69	35.7															Runoff form basin F overland flows across steep side slopes into the pit, flow contuies to travel south and remains in the pit at DP6
	6.1								53.9	25.58	2.69	68.7											Flow from Basin F and DP2.1 combine at DP6.1 and remain in the pit at DP6.1
	7	G	4.30	0.36	25.7	1.55	4.56	7.1															Runoff from Basin G, overland flows southwest to the adjacent property at DP7
	8	н	10.20	0.36	38.8	3.67	3.52	12.9															Runoff from Basin H overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	9	I	3.40	0.36	38.7	1.22	3.52	4.3															Runoff from Basin I overland flows down the Cottonwood Creek enbankment slopes & contuies to flow along the thalweg axis of the creek
	9.1								38.8	4.89	3.52	18.9											Flow from Basins H and I combine at DP9.1 and contunie to flow in Cottonwood creek, Emergancy Spillway flows are accouted for in 9.1
	10	J	2.90	0.36	25.7	1.04	4.56	4.7															Runoff from Basin J, overland flows south and enters the site at DP10
	10.1								28.7	22.89	4.28	97.9											Flows from Basins J and DP B4 combine at DP10.1 and enters the adjacent proporerty
	B4	OSB4	52.02	0.42	28.7	21.85	4.11	89.8															Off-site basin OSB4 Values from Sliver Pond FDR (Bains OS1- B4 & DP8)
	14	OSI4	27.16	0.40	29.2	10.86	4.07	44.2															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

Appendix C Hydraulic Calculations



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

	ent Basin not an ED	VIT WOOV PERMANENT PROCESSION PRO	2 SONE 1 1 AND 2 CES e Configura		an												
	weinwer_a <u>Watershed</u> ent Basin not an ED Perr	VI WOCY PERMANENT POR Example Zone Information Selected BMP Iver	1 AND 2 ces e Configura														
Number of the second	vouwej_a <u>Watershed</u> ent Basin not an ED ₽err	PERMANENT POOL Example Zone Information Selected BMP Type	1 AND 2 CES e Configura	100-YE	-												
	Watershed ent Basin not an ED	PERMANENT Example Zone Pool Example Zone Information Selected BMP Type	1 AND 2 CES e Configura	100-YE					1								
Number of the state o	Watershed ent Basin not an ED Perr	Information Selected BMP Type	e Configura		EAR		Depth Increment =		ft				Ontional		1		
Numerical Internation Description Description <thdescription< <="" td=""><td>Watersher ent Basin not an ED</td><td>Information Selected BMP Type</td><td></td><td>ation (Rete</td><td>ntion Pond)</td><td></td><td>Stage - Storage</td><td>Stage</td><td>Override</td><td>Length</td><td>Width</td><td>Area</td><td>Override</td><td>Area</td><td>Volume</td><td>Volume</td><td></td></thdescription<>	Watersher ent Basin not an ED	Information Selected BMP Type		ation (Rete	ntion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume	
Turbuse Turbuse <t< td=""><td>ent Basin not an ED</td><td>Selected BMP Type</td><td></td><td></td><td></td><td></td><td>Description</td><td>(ft)</td><td>Stage (ft)</td><td>(ft)</td><td>(ft)</td><td>(ft²)</td><td>Area (ft ²)</td><td>(acre)</td><td>(ft 3)</td><td>(ac-ft)</td><td></td></t<>	ent Basin not an ED	Selected BMP Type					Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)	
Sediment Basin not an EDB Wether Mark 333 prove Wether Mark 333 prove 400 - - 4500 100	ent Basin not an ED	D Sciecced Divit Territ	FDR	1		6982	6983		1.00			-	16 813	0.090	10.400	0.741	
Witchel Laght, Witchel Stand, Witchel Stand	Per	B Watershed Area =	70.20	acres			6984		2.00				37,163	0.853	37,487	0.861	
Viewended length to Certado Liddl h H - - - - <th< td=""><td>Perr</td><td>Watershed Length =</td><td>3,434</td><td>ft</td><td></td><td></td><td>6985</td><td></td><td>3.00</td><td></td><td></td><td>-</td><td>64,907</td><td>1.490</td><td>88,522</td><td>2.032</td><td></td></th<>	Perr	Watershed Length =	3,434	ft			6985		3.00			-	64,907	1.490	88,522	2.032	
Waterhel Boys 0.04 mm Mm 0000 mm <	Perc	Watershed Length to Centroid =	1,103	ft			6986		4.00			-	84,578	1.942	163,265	3.748	
Weithed improvances 2000 Processory Processory Methods (bin Model Services) 2000 Processory Processory Methods (bin Model Services) 2000 Processory Procesory Processory Processory Processory Procesory Processory	Perc	Watershed Slope =	0.014	ft/ft			6987		5.00	-		-	96,770	2.222	253,939	5.830	
The drain time, pro Target WOX Data Ire 4 Target WOX Data Ire	Per	Watershed Imperviousness =	2.90%	percent			6988		6.00			-	108,418	2.489	356,533	8.185	
Thr drain time, per MHED SC-07 Image: Stress of the stress o	E E L	entage Hydrologic Soil Group A =	100.0%	percent			6989		7.00			-	121,28/	2.784	4/1,385	10.822	
The drain time, per MHED SC-07 max works works in the schedule law sc	Percent	age Hydrologic Soil Groups C/D =	0.0%	percent						-		-					
Arr model with the stand Dotts - User products MHED SC-07 Memory products Absence from thydrograd with the products and thydrograd with the products and the interproducts and and the interproduct and the int	rain time per	Target WQCV Drain Time =	72.0	hours	Drain Time	Too Long				-							
Mint D S-C-07 Anter provider recarding holds abore secting 1-10 with hydrogen housing. Image: Control of the hydrogen housing hydrogen hydrogen housing hydrogen housing hydrogen housing hydrogen housing hydrogen hydro		.oration for 1-hr Rainfall Depths =	User Input	_						-		1					
Logendaria Characterize Characterize <td>SC-07 After</td> <td>providing required inputs above inc</td> <td>luding 1-hou</td> <td>rainfall</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td>	SC-07 After	providing required inputs above inc	luding 1-hou	rainfall						-		-					
Water Quality Captors: Volume (VIQC) B800 Encode to the function of th	depths	, click 'Run CUHP' to generate rung e embedded Colorado Urban Hydrc	off hydrograp Igraph Procec	hs using lure.	Ontinenal Uni												
Lares Buts Road Volume (2180) Source feet Image: Source feet Image	Water ()uality Canture Volume (WOCV) =	5 800	acre-feet	5 800	acre-feet				-							
2-yr Rundt Volume (P1 = 1.19) 0.05 ser-fett 1.19 order - <t< td=""><td>Excer</td><td>s Urban Runoff Volume (EURV) =</td><td>6.000</td><td>acre-feet</td><td>6.000</td><td>acre-feet</td><td>K</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	Excer	s Urban Runoff Volume (EURV) =	6.000	acre-feet	6.000	acre-feet	K										
Syr Rundf Volume (P1 = 15,n) = 0.00 screfed 150 notes Syr Rundf Volume (P1 = 25, n) = 0.05 screfed 20 notes Story Rundf Volume (P1 = 25, n) = 0.06 screfed 20 notes Story Rundf Volume (P1 = 25, n) = 0.06 screfed 20 notes Story Rundf Volume (P1 = 4, n) = 10.07 screfed 20 notes Story Rundf Volume (P1 = 4, n) = 10.02 screfed 20 notes Approximate Syr Detertivol Volume = 0.06 screfed <td< td=""><td>2-y</td><td>r Runoff Volume (P1 = 1.19 in.) =</td><td>0.055</td><td>acre-feet</td><td>1.19</td><td>inches</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	2-y	r Runoff Volume (P1 = 1.19 in.) =	0.055	acre-feet	1.19	inches											
10 yr Rundf Volance (P1 = 17, 5in) = 1.17 inches 25 yr Rundf Volance (P1 = 22, 5in) = 1.800 acc-feet 10 yr Rundf Volance (P1 = 22, 5in) = 1.800 acc-feet 300 yr Rundf Volance (P1 = 22, 5in) = 1.800 acc-feet 300 yr Rundf Volance (P1 = 22, 5in) = 1.800 acc-feet 300 yr Rundf Volance (P1 = 22, 5in) = 1.800 acc-feet Approximate Syr Deternion Volance = 0.085 acc-feet Approximate Syr Deternion Volance = 0.119 acc-feet Approximate Syr Deternion Volance = 0.333 acc-feet Define Zones and Basin Geometry 200 arc-feet - - - - Stelet Zone 3 Songe Volance (Dtron) = acc-feet - - - - - Stelet Zone 3 Songe Volance (Dtron) = acc-feet - - - - - - - Stelet Zone 3 Songe Volance (Dtron) = acc-feet -	5-	yr Runoff Volume (P1 = 1.5 in.) =	0.104	acre-feet	1.50	inches											
$ \begin{array}{c} \Delta y r kuon voume (r1 = 2.h) = 0.951 \\ 0.97 Rund Voume (r1 = 2.52.h) = 0.951 \\ 0.97 Rund Voum (r1 = 2.52.h) = 0.951 \\ 0.97 Rund Voum (r1 = 2.52.h) = 0.951 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.524 \\ 0.97 Rund Voum (r1 = 1.h) = 0.528 \\ 0.97 Rund $	10-y	r Runoff Volume (P1 = 1.75 in.) =	0.147	acre-feet	1.75	inches			Per	MHF) SC-(07, 3,6	500 CI	F of vo	olume	per ad	cre:
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	2	s-yr KUNOTT VOLUME (P1 = 2 in.) =	0.951	acre-feet	2.00	inches			70.2	2 AC*	3.6000	CF* (1	acre-	ft/435	59.9 C	CF)= 5	.80 Aci
300-yr Rundf Volume (P1 = 4 in, P Aproximate 2-yr Detertion Volume Approximate 3-yr Detertion Volume Approximate 1-yr Detertion Volume Approximate 12-yr Detertion Volume Approximate 12-yr Detertion Volume Approximate 10-yr Detert	50-y 100-v	r Runoff Volume (P1 = 2.25 in.) =	3.087	acre-feet	2.25	inches			- <u></u>		_,	(2010			, - 3	
Approximate Syre Detention Volume 0.067 serv-feet $ -$	50	0-yr Runoff Volume (P1 = 4 in.) =	10.624	acre-feet	4.00	inches											
Approximate 5 yr Detertion Volume 0.085 acre-fect	Арр	oximate 2-yr Detention Volume =	0.060	acre-feet		-						-					
Approximate 19yr Detertion Volume 0.174 acre-fect	Appr	oximate 5-yr Detention Volume =	0.085	acre-feet													
Approximate 5-yr utertion volume 0.373 acce-feet	Appro-	ximate 10-yr Detention Volume =	0.119	acre-feet								-					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Appro	ximate 25-yr Detention Volume =	0.1/4	acre-feet													
Define Zones and Basin Geometry Image: Constant of the second secon	Appro	imate 100-yr Detention Volume =	0.873	acre-feet			-										
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			· · · ·														
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Define Zor	es and Basin Geometry	r	-								-					
Select Zone 3 Storage Volume (Optional) = acre-feet <		Zone 1 Volume (WQCV) =	5.800	acre-feet								-					
Selet Zole 3 storage Volume (Uption)) = Table Volume (Dipon)) = Table Volume (Dipon)) = Contract $act-fect$ $-a$ a <	Select Zo	ne 2 Storage Volume (Optional) =		acre-feet								-					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Select Zo	Total Detention Basin Volume -	5 800	acre-feet						-		-					
Initial Surcharge Depth (H_{QD}) user th		Initial Surcharge Volume (ISV) =	User	# 3						-		-					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		Initial Surcharge Depth (ISD) =	user	ft								-					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Total Av	vailable Detention Depth (H _{total}) =	user	ft						-							
		Depth of Trickle Channel $(H_{TC}) =$	user	ft						-		-					
Slopes of Main Basin Sloge (Suah) = user user HV		Slope of Trickle Channel (S_{TC}) =	user	ft/ft						-		-					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Sic	pes of Main Basin Sides (S _{main}) =	user	H:V								-					
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		Initial Surcharge Area (A _{ISV}) =	user	ft 2						-							
	5	surcharge Volume Length $(L_{ISV}) =$	user	ft								-					
Depth of Basin Floor (H_{FLOOR}) user ft	5	Surcharge Volume Width $(W_{ISV}) =$	user	ft								-					
Length or basin Horo (L_{LOOR}) = user tr <td< td=""><td></td><td>Depth of Basin Floor (H_{FLOOR}) =</td><td>user</td><td>ft</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></td<>		Depth of Basin Floor (H _{FLOOR}) =	user	ft								-					
Area of Basin Flor (V_{FLOR})userft²Volume of Basin Flor (V_{FLOR})userft²		Width of Basin Floor (L _{FLOOR}) =	user	π.						-		-					
Volume of Basin Floor (V_{FLOOR}) = user ft ³		Area of Basin Floor (AFLOOR) =	user	ft ²													
		Volume of Basin Floor (V _{FLOOR}) =	user	ft ³						-							
Depth of Main Basin (H_{MAIN}) = User π		Depth of Main Basin $(H_{MAIN}) =$	user	ft						-		-					
Length of Main Basin (Lyauy) = user ft		Length of Main Basin (L _{MAIN}) =	user	ft						-		-					
Width of Main Basin (W _{MAD}) = user tt		Width of Main Basin (W _{MAIN}) =	user	ft + 2						-		-		-			
A rea or main basin (A _{MAM}) = User (t ⁻ Volume of Main Basin (A _{MAM}) = User (t ⁻		Area or Main Basin (A _{MAIN}) =	user	nt - ft 3													
Calculated Total Basin Volume (Viguar) = user a carefect	Calcul:	ated Total Basin Volume (Vtotal) =	user	acre-feet										-			
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Project:	SCHMIDT PARCEL								
Basin ID:	Custom Sediment	Basin							
				Estimated	Estimated	Outlet Time			
100-YR VOLUME EURY WOOV			7	Stage (ft)	volume (ac-rt)		1		
T T Mach			Zone I (WQCV)	4.99	5.800	Orifice Plate			
ZONE 1 AND 2	ORIFICE		Zone 2						
PERMANENT ORIFICES POOL Example Zone	Configuration (R	etention Pond)	Zone 3	T-+-! (-!!)	F 000		l		
Licer Input: Orifice at Linderdrain Outlet (typica	lly used to drain W(O(V in a Eiltration F	MD)	i otal (all zones)	5.800	J	Calculated Parame	tors for Underdrain	
Underdrain Orifice Invert Denth =	N/A	ft (distance below	the filtration media	surface)	Underd	rain Orifice Area =	N/A		<u>I</u>
Underdrain Orifice Diameter =	N/A	inches		Surface)	Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifi	ces or Elliptical Slot	Weir (typically use	d to drain WQCV a	nd/or EURV in a se	dimentation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basin	n bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	4.215E-02	ft ²	
Depth at top of Zone using Orifice Plate =	5.61	ft (relative to basin	n bottom at Stage =	= 0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	tangular oponings)		Ellipti	cal Slot Centrold =	N/A	reet	
Office Plate. Office Area per Row =	0.07	sq. inches (use red	langular openings)		L		N/A	it.	
User Input: Stage and Total Area of Each Orific	ce Row (numbered	from lowest to high	nest)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	1.25	1.55	1.85	2.15	2.45			
Orifice Area (sq. inches)	6.07	6.07	6.07	6.07	6.07	6.07			
	<u> </u>	[[1
Change of Onifine Combined (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orlince Centrold (ft)									
Office Area (34. incres)									1
User Input: Vertical Orifice (Circular or Rectand	gular)						Calculated Parame	ters for Vertical Or	ifice
	Not Selected	Not Selected					Not Selected	Not Selected	
Invert of Vertical Orifice =			ft (relative to basir	bottom at Stage =	= 0 ft) Ver	tical Orifice Area =			ft ²
Depth at top of Zone using Vertical Orifice =			ft (relative to basir	bottom at Stage =	= 0 ft) Vertical	Orifice Centroid =			feet
Vertical Orifice Diameter =			inches						
User Input: Overflow Weir (Dropbox with Flat	or Sloped Grate and	d Outlet Pipe OR Re	ctangular/Trapezoi	dal Weir and No O	utlet Pipe)		Calculated Parame	ters for Overflow V	Veir
	Not Selected	Not Selected					Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =			ft (relative to basin b	oottom at Stage = 0	ft) Height of Grate	e Upper Edge, H_t =			feet
Overflow Weir Front Edge Length =			feet		Overflow W	eir Slope Length =			feet
Overflow Weir Grate Slope =			H:V	Gra	ate Open Area / 10	0-yr Orifice Area =			
Horiz. Length of Weir Sides =			feet	Ov	erflow Grate Open	Area w/o Debris =			ft ²
Overflow Grate Type =			%	0	vernow Grate Oper	1 Area w/ Debris =			π
			<i>7</i> 0						
User Input: Outlet Pipe w/ Flow Restriction Plat	e (Circular Orifice, !	Restrictor Plate, or	Rectangular Orifice)	Ca	culated Parameters	s for Outlet Pipe w/	Flow Restriction P	late
	Not Selected	Not Selected					Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =			ft (distance below ba	asin bottom at Stage	= 0 ft) Ot	utlet Orifice Area =			ft ²
Circular Orifice Diameter =			inches		Outlet	Orifice Centroid =			feet
				Half-Cent	ral Angle of Restric	tor Plate on Pipe =	N/A	N/A	radians
Licer Input: Emergency Spillway (Bestangular e							Calculated Barama	tors for Spillwov	
Snillway Invert Stage	5 10	ft (relative to basin	hottom at Stage -	= 0 ft)	Snillway D	esian Flow Denth-	0.43	feet	
Spillway Crest Length =	40.00	feet	- bottom at stage -	010)	Stage at T	op of Freeboard =	6.53	feet	
Spillway End Slopes =	4.00	H:V			Basin Area at T	op of Freeboard =	2.64	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at T	op of Freeboard =	9.52	acre-ft	
Developed the due wards Develope									
Routed Hydrodraph Results	The user can over	ride the default CU	HP hydrographs an	d runoff volumes b	ov entering new val	ues in the Inflow H	vdrographs table ((Columns W through	AF).
Routed Hydrograph Results Design Storm Return Period =	The user can over WQCV	<i>ride the default CU</i> EURV	<i>HP hydrographs an</i> 2 Year	<i>d runoff volumes b</i> 5 Year	<i>ay entering new val</i> 10 Year	ues in the Inflow H 25 Year	<i>ydrographs table (C</i> 50 Year	Columns W through 100 Year	<i>AF).</i> 500 Year
<u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) =	The user can over WQCV N/A	<i>ride the default CU</i> EURV	HP hydrographs and 2 Year	d runoff volumes b 5 Year	<i>y entering new val</i> 10 Year	ues in the Inflow H 25 Year	<i>ydrographs table (0</i> 50 Year	<i>Columns W through</i> 100 Year	500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acce-ft) =	The user can over WQCV N/A 5.800 N/A	ride the default CU EURV 6.00	HP hydrographs an 2 Year	<i>d runoff volumes b</i> 5 Year	<i>ny entering new val.</i> 10 Year	ues in the Inflow H 25 Year	ydrographs table (C 50 Year	Columns W through 100 Year	500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	WQCV N/A 5.800 N/A	ride the default CU EURV 6.00	HP hydrographs an 2 Year	d runoff volumes b 5 Year	<i>ny entering new val</i> 10 Year	ues in the Inflow H 25 Year	vdrographs table (U 50 Year	Columns W through 100 Year	500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CHHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	The user can over WQCV N/A 5.800 N/A N/A N/A	ride the default CU EURV 6.00	HP hydrographs and 2 Year	d runoff volumes b 5 Year	ny entering new val 10 Year	ues in the Inflow H 25 Year	vdrographs table (u 50 Year	Columns W through 100 Year	500 Year
Kouted Hydrograph Kesults Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Rendevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Flow, q (cfs/acre) =	WQCV N/A 5.800 N/A N/A N/A N/A N/A	ride the default CU EURV 6.00	HP hydrographs and 2 Year	d runoff volumes b 5 Year	ny entering new val 10 Year	ues in the Inflow H	vdrographs table (0 50 Year	Columns W through 100 Year	500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	WQCV N/A 5.800 N/A N/A N/A N/A N/A N/A 2.2	6.00	HP hydrographs an 2 Year	d runoff volumes b 5 Year	y entering new val 10 Year	ues in the Inflow H 25 Year	ydrographs table ((50 Year	Columns W through	500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q =	WQCV N/A 5.800 N/A	nide the default CU EURV 6.00 N/A	HP hydrographs an 2 Year N/A	d runoff volumes b 5 Year	y entering new val 10 Year	ues in the Inflow H 25 Year	ydrographs table ((50 Year	Columns W through	<i>AF).</i> 500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velority through Grate 1 (frec) =	N/A N/A 5.800 N/A	N/A	HP hydrographs an 2 Year N/A	d runoff volumes b 5 Year	y entering new val 10 Year N/A	ues in the Inflow H	ydrographs table (t	Columns W through 100 Year	AF). 500 Year
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Riow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	WQCV N/A 5.800 N/A	N/A N/A N/A	HP hydrographs an 2 Year N/A N/A N/A	A runoff volumes b 5 Year N/A N/A	y entering new val 10 Year N/A N/A	ues in the Inflow H 25 Year N/A N/A	ydrographs table (d 50 Year N/A	Columns W through 100 Year N/A N/A	N/A N/A
Routed Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Rlow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	WQCV N/A 5.800 N/A	N/A N/A N/A	HP hydrographs an 2 Year N/A N/A N/A	N/A N/A	y entering new val 10 Year N/A N/A N/A	ves in the Inflow H 25 Year N/A N/A	ydrographs table (C 50 Year N/A N/A	Columns W through 100 Year N/A N/A	N/A N/A N/A
Routed Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Rlow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Nufflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	N/A N/A 5.800 N/A 63 72 4 99	N/A N/A N/A	HP hydrographs an 2 Year N/A N/A N/A	A runoff volumes b 5 Year N/A N/A N/A	y entering new val 10 Year N/A N/A N/A	ves in the Inflow H 25 Year N/A N/A	vdrographs table (d 50 Year N/A N/A N/A	Columns W through 100 Year N/A N/A	N/A N/A
Kouted Hydrograph Kesuits Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Rlow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Area at Maximum Ponding Depth (facres) =	N/A N/A 5.800 N/A Plate N/A 63 72 4.99 2.22	N/A N/A	HP hydrographs an 2 Year N/A N/A N/A	V/A N/A N/A	y entering new val 10 Year N/A N/A N/A	Les in the Inflow H 25 Year N/A N/A N/A	vdrographs table (d 50 Year N/A N/A N/A	Columns W through 100 Year	N/A N/A



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program SOURCE CUHP CUHP CUHP CUHP CUHP CUHP CUHP CUHP CUHP Time Interval TIME WQCV [cfs] EURV [cfs] 2 Year [cfs] 5 Year [cfs] 10 Year [cfs] 25 Year [cfs] 50 Year [cfs] 100 Year [cfs] 500 Year [cfs] 0:00:00 5 00 min 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0:05:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0:10:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0:15:00 0.00 0.00 0.02 0.00 0.01 0.01 0.01 0.01 0.01 0:20:00 0.00 0.00 0.02 0.03 0.03 0.02 0.02 0.02 0.14 0:25:00 0.00 0.00 0.18 0.42 0.63 0.13 0.25 0.32 3.71 0:30:00 0.00 0.00 0.46 0.97 1.37 2.68 6.52 9.69 37.01 0:35:00 1.66 7.65 0.00 0.00 0.61 1.19 15.76 24.64 78.24 0:40:00 0.00 0.00 0.61 1.19 1.66 10.74 20.88 33.49 99.70 0:45:00 0.00 0.00 0.58 1.12 1.56 11.23 21.85 35.86 107.80 0:50:00 0.00 0.53 1.40 34.85 0.00 1.00 10.79 20.86 108.26 0:55:00 0.00 0.00 0.47 0.90 1.26 9.83 18.89 31.81 102.61 1:00:00 0.00 0.00 0.43 0.82 1.15 8.79 16.99 28.72 96.77 1:05:00 0.00 0.00 0.40 0.75 1.04 7.98 15.41 26.14 91.95 1:10:00 0.00 0.00 0.36 0.67 0.94 7.23 13.95 23.68 85.45 1:15:00 0.00 0.00 0.33 0.62 0.88 6.48 12.49 21.23 77.41 1:20:00 0.00 0.00 0.31 0.57 0.82 5.86 11.35 19.25 70.62 1:25:00 0.00 0.00 0.28 0 53 0.76 5.39 10.41 17 64 64 45 1:30:00 0.00 0.00 0.26 0.48 0.70 4.94 9.54 16.14 58.62 1:35:00 0.00 0.00 0.24 0.44 0.63 4.50 8.67 14.68 53.21 1:40:00 0.00 0.00 0.21 0.39 0 56 4 06 7 81 13 24 47 98 1:45:00 0.00 0.00 0.19 0.35 0.50 3.62 6.95 11.80 42.84 1:50:00 37.81 0.00 0.00 0.17 0.30 0.43 3.18 6.09 10.36 1:55:00 0.00 0.00 0.15 0.28 0.39 2.74 5.25 8.94 33.04 2:00:00 0.00 0.00 0.14 0.26 0.37 2.42 4.68 7.94 29.68 2:05:00 0.24 0.34 27.08 0.00 0.00 0.13 2.24 4.31 7.29 2:10:00 0.00 0.00 0.12 0.22 0.32 2.08 4.00 6.74 24.79 2:15:00 0.00 0.00 0.11 0.20 0.29 1.92 3.70 6.24 22.72 2:20:00 5.75 20.78 0.00 0.00 0.10 0.19 0.27 1.77 3.41 2:25:00 0.00 0.00 0.09 0.17 0.24 1.62 3.12 5.26 18.93 2:30:00 0.00 0.08 1.47 17.17 0.00 0.15 0.21 2.83 4.77 2:35:00 0.00 0.00 0.07 0.13 0.19 1.32 2.54 4.29 15.51 2:40:00 0.00 0.00 0.07 0.12 0.17 1.17 2.25 3.82 13.85 2:45:00 0.00 0.00 0.06 0.10 0.14 1.03 1.96 3.34 12.20 2:50:00 0.00 0.00 0.05 0.08 0.12 0.88 1.67 2.86 10.55 2:55:00 0.00 0.00 0.04 0.07 0.09 0.73 1.39 2.38 8.90 3:00:00 0.00 0.00 0.03 0.05 0.07 0.58 1.10 1.90 7.25 3:05:00 0.00 0.81 1.42 0.00 0.02 0.03 0.05 0.43 5.61 3:10:00 0.00 0.00 0.01 0.02 0.03 0.29 0.53 0.94 3.96 3:15:00 0.00 0.00 0.01 0.01 0.01 0.14 0.24 0.47 2.38 3:20:00 0.00 0.00 0.01 0.01 0.01 0.05 0.08 0.18 1.43 3:25:00 0.00 0.00 0.00 0.01 0.01 0.02 0.03 0.07 0.90 3:30:00 0.00 0.00 0.00 0.01 0.01 0.01 0.02 0.03 0 57 3:35:00 0.00 0.00 0.00 0.00 0.01 0.01 0.01 0.02 0.34 3:40:00 0.00 0.00 0.00 0.00 0.01 0.01 0.19 0.01 0.01 3:45:00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.01 0.09 3:50:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.02 3:55:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 4:00:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 4:05:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 4:10:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 4:15:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:20:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:25:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:30:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:35:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:40:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:45:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:50:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 4:55:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:00:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:05:00 5:10:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:15:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:20:00 5:25:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:30:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:35:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:40:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:45:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:50:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 5:55:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

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ummary Stage-Area-Volu ne user can create a summ ne user should graphically o	Ime-Discharge ary S-A-V-D by e compare the sum	Relationships ntering the desi mary S-A-V-D t	red stage increr able to the full S	nents and the re G-A-V-D table in	emainder of the the chart to cor	table will popul	ate automatically. all key transition points.
Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floo
							from the S-A-V table on
							Sheet basin.
							Also include the inverts of outlets (e.g. vertical orifice
							overflow grate, and spillwa
							where applicable).
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MHFD-Detention_v4-05.xlsm, Outlet Structure

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Sediment Basin Outlet Pipe

Circular		Highlighted	
Diameter (ft)	= 1.00	Depth (ft)	= 0.67
		Q (cfs)	= 2.840
		Area (sqft)	= 0.56
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 5.07
Slope (%)	= 0.50	Wetted Perim (ft)	= 1.92
N-Value	= 0.009	Crit Depth, Yc (ft)	= 0.73
		Top Width (ft)	= 0.94
Calculations		EGL (ft)	= 1.07
Compute by:	Known Q		
Known Q (cfs)	= 2.84		





Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Apr 28 2022

EAST SWALE B-B (B1)

Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 6.00	Depth (ft) =	0.93
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	38.50
Total Depth (ft)	= 2.25	Area (sqft) =	9.04
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	4.26
Slope (%)	= 1.80	Wetted Perim (ft) =	13.67
N-Value	= 0.035	Crit Depth, Yc (ft) =	0.89
		Top Width (ft) =	13.44
Calculations		EGL (ft) =	1.21
Compute by:	Known Q		
Known Q (cfs)	= 38.50		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

NORTH SWALE B-B (B2)

Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 6.00	Depth (ft) =	= 1.25
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 36.40
Total Depth (ft)	= 2.25	Area (sqft)	= 13.75
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 2.65
Slope (%)	= 0.50	Wetted Perim (ft)	= 16.31
N-Value	= 0.035	Crit Depth, Yc (ft)	= 0.86
		Top Width (ft)	= 16.00
Calculations		EGL (ft)	= 1.36
Compute by:	Known Q		
Known Q (cfs)	= 36.40		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Jul 19 2022

Spillway C-C

Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 40.00	Depth (ft)	= 0.43
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 56.56
Total Depth (ft)	= 1.90	Area (sqft)	= 17.94
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.15
Slope (%)	= 1.80	Wetted Perim (ft)	= 43.55
N-Value	= 0.035	Crit Depth, Yc (ft)	= 0.40
		Top Width (ft)	= 43.44
Calculations		EGL (ft)	= 0.58
Compute by:	Known Depth	ζ,	
Known Depth (ft)	= 0.43		



Appendix D Reference Material



RECEIVED

MAY 10 1996

Planning Dapla

SILVER PONDS SUBDIVISION FILING NO. 1

FINAL DRAINAGE REPORT

February 2, 1995 Revised May 5, 1996 Project No. 60572

PREPARED FOR:

The Campbell Corporation 4975 Austin Bluffs Parkway Colorado Springs, CO 80918

PREPARED BY:

M.V.E., Inc. 1911 Lelaray St. Colorado Springs, CO 80909

60572fdr.wp6-d49

Design	Included Basins	Cumulative	5-yr	100-yr
Point		Drainage Area	Discharge	Discharge
		(Ac)	(cfs)	(cfs)
1	OSA1	18.14	13.1	30.4
2	OSA2	8.72	7.0	16.3
3	OSA1 thru A3	29.05	20.5	47.7
4	OSA1 thru A4	31.04	24.3	53.6
5	OSB1	39.26	29.8	69.3
6	OSB1 thru B2	44.66	25.9	60.3
7	OSB1 thru B3	50.03	35.7	83.1
8	OSB1 thru B4	52.02	39.2	89.8
9	OSD1	8.26	7.9	18.4
10	OSD1 thru D2	19.95	24.1	52.9
11	D3	3.41	4.5	9.9
12	E1	4.24	5.5	12.1
13	F1	4.26	6.6	14.4
14	OSG1	6.66	7.0	16.4
15	OSG1 thru G2	9.22	10.5	24.0
16	OSH1	17.22	17.5	38.4
17	OSH1 thru H2	28.28	27.9	61.3
18	OSI1	3.67	3.3	7.8
19	OSI1 thru I2	11.05	7.9	18.4
20	I3	8.01	6.3	14.6
21	OSI1 thru I4	27.16	19.0	44.2
22	J1	4.19	3.0	6.9

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Table 3.1 - Developed Condition Hydrologic Data

5-year and 100-Year

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M.V.E., Inc. Colorado Springs, Colorado

Proj. No.: 60572 Project: SILVER PONDS

DEVELOPED DISCHARGES RAINFALL/RUNOFF ANALYSIS - RATIONAL METHOD i100 Q100 Design Area CS C100 Tc i5 05 Point (Ac) (min) (in/hr) (in/hr)(cfs) (cfs) ______ _____ 30.4 1 18.14 0.30 0.40 27.7 2.40 4.20 13.1 16.3 2 8.72 0.30 0.40 22.9 2.68 4.68 7.0 25.4 4.41 29.8 69.3 5 39.26 0.30 0.40 2.53 0.40 3.19 5.57 7.9 18.4 9 8.26 0.30 16.5 0.40 3.52 6.15 7.0 16.4 14 6.66 0.30 13.5 38.4 17.22 0.39 0.49 24.1 2.60 4.55 17.5 16 7.8 18 3.67 0.30 0.40 18.2 3.03 5.30 3.3 47.7 0.30 0.40 28.7 2.35 4.11 20.5 3 29.05 0.34 0.43 29.8 2.30 4.02 24.3 53.6 4 31.04 60.3 3.38 25.9 0.30 0.40 39.5 1.93 6 44.66 4.29 4.0 9.2 33 5.37 0.30 0.40 26.7 2.45 7 50.03 0.30 0.40 28.2 2.38 4.15 35.7 83.1 4.11 39.2 89.8 0.42 28.7 2.35 52.02 0.32 8 0.39 0.49 17.6 3.09 5.39 14.1 30.9 D2 11.69 52.9 24.1 10 19.95 0.39 0.49 17.5 3.10 5.41 0.39 11 3.41 0.49 14.5 3.40 5.94 4.5 9.9 5.85 0.49 15.0 3.35 5.5 12.1 12 4.24 0.39 3.94 6.89 6.6 14.4 13 4.26 0.39 0.49 10.5 7.8 6.24 3.6 G2 2.56 0.39 0.49 13.1 3.57 24.0 0.43 14.0 3.46 6.04. 10.5 15 9.22 0.33 H2 11.06 0.39 0.49 17.5 3.10 5.41 13.4 29.3 0.39 0.49 25.3 2.53 4.42 27.9 61.3 28.28 17 18.4 11.05 0.30 0.40 28.0 2.39 4.17 7.9 19 6.3 14.6 0.40 23.9 4.57 20 8.01 0.30 2.62 0.40 23.1 2.67 4.66 6.5 15.1 14 8.10 0.30 44.2 0.30 0.40 29.2 2.33 4.07 19.0 21 27.16 22 4.19 0.30 0.40 28.8 2.35 4.10 3.0 6.9

Date: 1-31-96



TRAILS AT FOREST MEADOWS FILING NO. 3 FINAL DRAINAGE REPORT

AMENDMENT TO: MASTER DEVELOPMENT DRAINAGE PLAN UPDATE FOR WOODMEN HEIGHTS AND FINAL DRAINAGE REPORT FOR FOREST MEADOWS FILING NO.1AND NO.4

August 2015

Prepared for:

Rivers Development, Inc. 13530 Northgate Estates Drive, Suite 200 Colorado Springs, CO 80921





CIVIL CONSULTANTS, INC. 20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

Project #08-029



Basin U is located in the easterly portion of the site and contains 1.23 acres of Vollmer Road asphalt and curb and gutter. Basin U has proposed design flows of 4.3 cfs for the minor storm event (5-Year) and 8.1 cfs for the major storm event (100-Year). Runoff from Basin U will flow, via curb and gutter to Design Point E3, an existing 20' D-10-R inlet, in an at-grade condition. The inlet at Design Point E3 has been sized to accept flows from Basin T, U and portions of historic flows from Basins EX1 and EX2 (capacity of \sim 30 cfs). Collected flows from Design Point E3 will be conveyed in an existing 30" RCP (pipe 10) to pipe 11, an existing 48" RCP. Combined flows in 9, 10 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2. Additional discussion the runoff reaching Design Point 3 is discussed in upcoming paragraphs.

Basin OS2 is located off-site, in the northerly portion of the site and contains 1.22 acres of undeveloped land. Basin OS2 has undeveloped flows of 0.8 cfs for the minor storm event (5-Year) and 3.6 cfs for the major storm event (100-Year). Runoff from Basin OS2 will be directed around Basin Q, via the proposed perimeter berm to Design Point 9 (accumulated flows 10.2 cfs-5 year, 22.4 cfs-100 year) and a proposed diversion swale. The diversion swale will route flows to an existing 48" RCP (pipe 14). Pipe 14 and 3 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2. *Any increase in flows due to future development of Basin OS1/OS2 will require the construction of a proposed detention facility*, as per the Sand Creek DBPS.

Basin OS3 is located off-site, in the northerly portion of the site and contains 0.34 acres of undeveloped land. Basin OS3 has undeveloped flows of 0.2 cfs for the minor storm event (5-Year) and 1.0 cfs for the major storm event (100-Year). Runoff from Basin OS3 will be directed westward via the proposed perimeter berm to Design Point 9 (accumulated flows 10.2 cfs-5 year, 22.4 cfs-100 year) and a proposed diversion swale. The aforementioned diversion swale will route flows to an existing 48" RCP (pipe 14).

Flows reaching **Design Point E3** are historic and tributary to Vollmer Road (EX1, EX2 and EX3, see Historic drainage map DP-1). A portion of these Historic (EX1 and EX2) and proposed flows (Basin T and U), will be routed into the existing Vollmer Road infrastructure at the north end of the Dry Needle Place/Vollmer Road intersection and the northerly boundary of Filing No. 2. If sufficient conveyance capacity were to exist within the Vollmer ROW to convey runoff from the historic upstream watersheds, flows rates as high as 87.8 cfs for the minor storm event (5- Year) and 388.7 cfs for the major storm event (100-Year) could be expected to reach Design Point E3. These calculated flows differ by 2 cfs in the 5-year event and 1 cfs in the 100- year event from those estimated within the FDR2 report. A field inspection of the existing roadside ditch and roadway was conducted by M&S Civil Consultants in the Early Summer of 2015 and the estimated conveyance capacity was determined using Bentley's FlowMaster program. Based upon the observed longitudinal slope and geometry, the capacity of the street/ditch section at the northern boundary was found to be as high as approximately 135 cfs, thereby limiting the maximum amount of upstream runoff which is able to reach the subject site and Design Point 3. Runoff upstream of the site, in excess of ditch capacity, is believed to intermittently overtop Vollmer Road continue east toward Sand Creek. Recent storms during the summer months of 2015 (June & July) have aided in additional sediment transport in the area, thus likely further decreasing the available conveyance capacity. In the proposed condition grading will occur along portions of the west side of Vollmer Road to add width to the existing roadway and a vertical curb and gutter section along the west side of the street. A proposed cross section was analyzed upstream of Design Point 3 which indicates an estimated street conveyance capacity of 131 cfs for the west side of Vollmer Road when ponding reaches a depth of 1' at the flowline.

A temporary radial asphalt curb with a riprap transition will be constructed at the confluence of the roadway section and the existing ditch, at the north end of the subdivision, to aid in directing runoff from the existing ditch to the proposed curb and guttered street section. The proposed improvements will be detailed in the street improvement plans for Trails at Forest Meadows Filing No. 3. The proposed improvements will be constructed within the right of way in a manner so that they do not impact lots or offsite property.

It should be noted that based upon the Preliminary Drainage Report of Sterling Ranch Phase 1, dated March 2015 by M&S Consultants, the construction of the Sterling Ranch Subdivision and Marksheffel Road will

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FINAL DRAINAGE REPORT																			
						(A)	rea l	Draiı	nage	Sun	mar	V)							
Prote Compasite Russoff Conflictent Summary OVERLAND STREET / CHANNEL FLOW Time of Travel (T,) INTENSITY * TOTAL FLOWS													FLOWS	4					
BASIN	TOTAL	C ₆	C180	4	Length	Height	Tc	Length	Slope	Velocity	T,	TOTAL	ų	I300	Q,	Qim	CA,	Basin	CA100
F2-F FILING 2	2.95	0.57	0.67	0.25	117	5	10.6	842	1.8%	4.7	(min) 3.0	(min) 13.7	(in/hr) 3.6	(im/hr) 6.4	(c.f.s.) 6.1	(c.f.s.) 12.8	1.69	F2-F	1.99
F2-I FILING 2	1.72	0.57	0.67	0.25	194	3.2	18.8	714	1.9%	4.9	2.4	21.2	2.9	5.2	2.9 .	6.0	0.99	F2-1	1,16
F2-J FILING 2	3.12	0.57	0.67	0.25	164	4	15,2	623	1.9%	4.3	2.2	17.3	3.2	5.8	5.8	12.0	1.78	F2-J	2.09
K	0.92	0.57	0.67	0.25	131	2.6	14.5	0	1.0%	3.5	0.0	14.5	3.5	6.3	1.8	3.9	0,52	ĸ	0.62
L	0.55	0.57	0.67	0.25	80	1.5	II.6	0	1.0%	3.5	0.0	11,6	3.9	6.9	1.2	2.5	0.31	L	0.37
М	2.62	0.57	0.67	0.25	76	1,5	11,1	843	2.5%	5.5	2.6	13.6	3.6	6.4	5.4	11.3	1.49	м	1.76
<u>M-1</u>	0.65	0.57	0.67	0.25	118	2.4	13.7	170	1.0%	3.5	0.8	14,5	3.5	6.3	1.3	2.7	0.37	M-1	0.44
0	0.70	0.57	0.67	0.25	155	10	10,7 [.]	0	2.5%	5.6	0.0	10.7	4.0	7.1	1.6	. 3.3	0.40	0	0.47
P	2.14	0.57	0.67	0.25	76	1.5	11,1	920	1.1%	3.7	4,2	15.2	3.4	6.1	4.2	8.8	1.22	P	1.43
Q	3.66	0.57	0.67	0.25	170	3.4	16.5	1016	1.3%	3.7	4.6	21.1	2.9	5.2	6.1	12.8	2.09	Q	2.45
R	2.37	0.57	0.67	0.25	112	2.2	13.5	369	1.9%	4.8	1.3	14.7	3.5	6.2	4.7	9.9	1.35	R	1.59
S	3.09	0.57	0.67	0.25	298	6	21.8	1015	2.5%	5.5	3.1	24.8	2.7	4.8	4.7	9.9	1.76	5	2.07
T	1.73	0.57	0.67	0.2,5	62	1.2	10.1	0	2.5%	5.6	0.0	10.1	4.1	7.3	4.0	8.4	0.99	T.	1.16
U	1.23	0.90	0.95	0.25	34	0.7	7.3	1284	2.3%	5.3	4.0	11.3	3.9	7.0	4.3	8.1	1.11	U	1.17
OS2	1,22	0.13	0.33	0.13	52	8	5.3	0	2.5%	5.6	0.0	53	5.0	8.9	<i>0.8</i>	3.6	0.16	OS2	6,40
OS3	0.34	0.13	0.33	0.13	40	8	43	0	2.5%	5.6	0.0	5.0	5,1	9.1	<i>0.2</i>	1.0	0.04	053	0.13

* Into 11C & 110 m travel time of 5 m Calculated by: ET Date: 5/26/2015

Checked by:

MS CivilTrails at FM Filing No. 3 Drainage Calcs

Page 1 of 1



distant distant

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TRAILS AT FOREST MEADOWS FILING NO. 4 FINAL DRAINAGE REPORT

AMENDMENT TO: MASTER DEVELOPMENT DRAINAGE PLAN UPDATE FOR WOODMEN HEIGHTS AND FINAL DRAINAGE REPORT FOR FOREST MEADOWS FILING NO.1AND NO.4

April 2016

Prepared for:

Challenger Homes, Inc. 13530 Northgate Estates Drive, Suite 200 Colorado Springs, CO 80921 (719) 598-5192

Prepared by:



CIVIL CONSULTANTS, INC. 20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

Project #08-032

Filing No.3 - Basins **OS2, **P, **Q are located to the northeast of the subject site, in the north portions of the Filing 3 site. The flows from these basins were previously analyzed as part of "The Trails at Forest Meadows Filing No. 3 Preliminary/Final Drainage Report" (TRM 3 FDR). Runoff produced within Basins **OS2 (0.8 cfs/3.6 cfs), **P (4.2 cfs/8.8 cfs), and **Q (6.1 cfs/12.8 cfs) flows have been accounted for and are included in this Final Drainage Report.

Basin V is located in the northerly portion of the site, north of Vanderwood Road, and contains 2.48 acres of single family residential lots and streets. Basin V has proposed design flows of 3.2 cfs for the minor storm event (5-Year) and 7.6 cfs for the major storm event (100-Year). Runoff from Basin V will flow, overland via side lot swales, to the curb and gutter of proposed Vanderwood Road. These flows will combine with flows from Basin ******Q and be conveyed west via curb and gutter to Design Point 11 (11.0 cfs/25.2 cfs), a proposed 8' D-10-R inlet in a sump condition. Design Point 11 (11.0 cfs/25.2 cfs) cumulative flows include Basin X. The inlet at Design Point 11 has been sized to accept flows in the developed condition. Collected flows from Design Point 11 will be conveyed in a 48" RCP (Pipe 2) to Design Point 12, a proposed 10' D-10-R inlet in the sump condition. In the event of clogging or total inlet failure, flows from Design Point 11 will overtop crown/curb and flow southeast over Tract I to a temporary sediment basin located in the Trails at Forest Meadows Filing No. 1.

Basin W is located in the northerly portion of the site, south of Vanderwood Road, and contains 2.2 acres of single family residential lots and streets. Basin W has proposed design flows of 3.1 cfs for the minor storm event (5-Year) and 7.1 cfs for the major storm event (100-Year). Runoff from Basin W will flow, overland via side lot swales, to the curb and gutter of proposed Vanderwood Road. These flows will combine with flows from Basin ******P and be conveyed west via curb and gutter to Design Point 12 (7.5 cfs/16.8 cfs), a proposed 10' D-10-R inlet in a sump condition. Design Point 12 (7.5 cfs/16.8 cfs) cumulative flows include Basin Y. The inlet at Design Point 12 has been sized to accept flows in the developed condition. Collected flows from Design Point 12 will be conveyed in an existing 48" RCP (Pipe 3). In the event of clogging or total inlet failure, flows from Design Point 12 will overtop curb and flow southeast over Tract I to a temporary sediment basin located in the Trails at Forest Meadows Filing No. 1.

Basin X is located in the northerly portion of the site, north of Vanderwood Road, and contains 2.03 acres of single family residential lots and streets. Basin X has proposed design flows of 2.7 cfs for the minor storm event (5-Year) and 6.4 cfs for the major storm event (100-Year). Runoff from Basin X will flow, overland via side lot swales, to the curb and gutter of proposed Vanderwood Road. These flows will be conveyed east via curb and gutter and be combined with flows from Basin ******Q and Basin V to Design Point 11 (11.0 cfs/25.2 cfs), a proposed 8' D-10-R inlet in a sump condition. The inlet at Design Point 11 has been sized to accept flows in the developed condition. Collected flows from Design Point 11 will be conveyed in a 48" RCP (Pipe 2) to Design Point 12, a proposed 10' D-10-R inlet in the sump condition. In the event of clogging or total inlet failure, flows from Design Point 11 will overtop crown/curb and flow southeast over Tract I to a temporary sediment basin located in the Trails at Forest Meadows Filing No. 1.

Basin Y is located in the northerly portion of the site, south of Vanderwood Road, and contains 0.78 acres of single family residential lots and streets. Basin Y has proposed design flows of 1.2 cfs for the minor storm event (5-Year) and 2.8 cfs for the major storm event (100-Year). Runoff from Basin Y will flow, overland via side lot swales, to the curb and gutter of proposed Vanderwood Road. These flows will be conveyed east via curb and gutter and be combined with flows from Basin ******P and Basin W to Design Point 12 (7.5 cfs/16.8 cfs), a proposed 10' D-10-R inlet in a sump condition. The inlet at Design Point 12 has been sized to accept flows in the developed condition. Collected flows from Design Point 12 will be conveyed in an existing 48" RCP (Pipe 3). In the event of clogging or total inlet failure, flows from Design Point 12 will overtop curb and flow southeast over Tract I to a temporary sediment basin located in the Trails at Forest Meadows Filing No. 1.

Basin Z is located in the northerly portion of the site, south of Leaf Wood Court, and contains 1.2 acres of

(30.5 cfs/63.9 cfs). Hence flows to this Design Point are less and will not adversely affect the existing subdivision or storm infrastructure.

Basin OS4 is located north of the site and contains 0.83 acres of offsite undeveloped land. In the interim, Basin OS4 has existing design flows of 0.4 cfs for the minor storm event (5-Year) and 1.8 cfs for the major storm event (100-Year). Runoff from Basin OS4 will sheet flow overland to a proposed swale/berm along the north property line. These flows will be conveyed west and combine with flows from Basins ******OS2 (0.8 cfs/3.6 cfs) to Design Point 10 (1.0 cfs/4.7 cfs). These flows will be routed to a riprap lined depression and a 48" PP storm sewer with FES (Pipe Run 1). Pipe 1, 2 and 3 have been sized to accept these developed flows and do not exceed the pipe design flows in the Trails at Forest Meadows Filing No. 2 Final Drainage Report. In the event of clogging and/or failure, an overflow route will be graded in between lots 39 and 40 to design point 11 and will be limited to historic flows (Q100=84 cfs). Any increase in flows due to future development of Basin OS1 MDDP will require the construction of a proposed detention facility, as per the Sand Creek DBPS. Upon development of Basin OS1 the riprap depression will be filled in and the storm sewer system will be routed to the north to collect the developed flows.

Basin OS5 is located to the north of the site and contains 4.46 acres of offsite undeveloped land. In the interim, Basin OS5 has existing design flows of 2.1 cfs for the minor storm event (5-Year) and 9.0 cfs for the major storm event (100-Year). Runoff from Basin OS5 will sheet flow overland to a proposed swale/berm along the north property line and existing Black Forest Road. These flows will be conveyed south and combine with flows from Basins DD and OS6 to Design Point 17 (4.2 cfs/14.5 cfs). These flows donot exceed the 100 year flows at Design Point EX1 (3.7 cfs/16.7 cfs), see Existing Drainage Plan DP-1. Any increase in flows due to future development of Basin OS5 will require the construction of a proposed detention facility.

Basin OS6 is located to the north of the site and contains 0.45 acres of offsite undeveloped land. In the interim, Basin OS6 has existing design flows of 0.1 cfs for the minor storm event (5-Year) and 0.6 cfs for the major storm event (100-Year). Runoff from Basin OS6 will sheet flow overland to a proposed swale/berm along the north property line and existing Black Forest Road. These flows will be conveyed south and combine with flows from Basins DD and OS5 to Design Point 17 (4.2 cfs/14.5 cfs). These flows donot exceed the 100 year flows at Design Point EX1 (3.7 cfs/16.7 cfs), see Existing Drainage Plan DP-1. Basin OS6 (see Existing Drainage Plan DP-1) is tributary to the Cottonwood Creek Basin. In the interim, conveyance of flows from OS6 will be tributary to the Sand Creek Basin. Upon future development of Basin OS6 all runoff will required to be routed to the Cottonwood Creek Basin.

Basin OS1 MDDP is located off-site, in the northerly portion of the site and contains 78.0 acres of undeveloped land. Basin OS1 is composed of Basins OS2, OS4, OS5 and OS6. Upon development of Basin OS1, flows of 34.4 cfs for the minor storm event (5-Year) and 84.1 cfs for the major storm event (100-Year) will be routed, via a storm sewer, to the proposed 48" RCP (Pipe Run 1(34.4 cfs/84.1 cfs)) storm sewer within the property site. Pipe Run 1 will route flows to and combine with flows at Pipe Run 2 (41.3 cfs/100.0 cfs), a proposed 48" RCP storm sewer. Pipe Run 2 will route flows to and combine with flows at Pipe Run 3 (45.8 cfs/110.0 cfs), an existing 48" RCP storm sewer. These flows donot exceed the flows designed for the north future filings (48.8 cfs/118.2 cfs), as noted in the Trails at Forest Meadows Filing No. 2 report. Basin OS1 will be conveyed through and combined with the flows of Trails at Forest Meadows Filing No.2 for historic drainage map and calculations. Any increase in flows due to future development of Basin OS1 will require the construction of a proposed detention facility, as per the Sand Creek DBPS.

EROSION CONTROL

It is the policy of the City of Colorado Springs that we submit an erosion control plan with the drainage report. At this time we respectfully request that the erosion control plan be submitted in conjunction with the final grading plan. Proposed straw bale check dams, silt fence, vehicle traffic control, and reseeding are proposed as erosion control measures. The proposed 90 single family lots will not adversely impact the existing surrounding residential infrastructure. The proposed BMP's in the plan and report shall be installed and maintained to accomplish this task.

TRAILS AT FOREST MEADOWS FILING NO. 4 PRELIMINARY DRAINAGE REPORT

(Area Drainage Summary)

From Area Runoff Coefficient Summary					OVER	LAND		STR	EET / CH	IANNEL	FLOW	of Travel	INTEN	SITY *	TOTAL	FLOWS	#REFI		#REF!
BASIN	AREA TOTAL	Cs	C ₁₀₀	C ₅	Length	Height	Tc	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q5	Q100	CA ₅	Basin	CA ₁₀
	(Acres)	From DC	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(mín)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)			
Existing Area Drainage Summary																			
#OS1 Historic	78	0.24	0.33				1					47.6			34.4	84,1	18.72	#OS1 Historic	25.74
**0S2	1.22	0.13	0.33	1	-			E.				5.3			0.8	- 3.6	0.16	**OS2	0.40
OS4	0,83	0.13	0.33	0.13	48	12	4.5	950	1.3%	2.3	7,0	11.4	3.9	6.6	0.4	1.8	0.11	OS4	0.27
OS5	4.46	0.13	0.33	0.13	64	12	5.7	1138	1.9%	2.3	8.3	14.0	3.6	6.1	2.1	9.0	0.58	OS5	1.47
OS6	0.45	0,13	0.33	0.13	200	2	28.1	232	4.3%	3.0	1.3	29.4	- 2.5	4.2	0.1	0.6	0.06	OS6	0.15
EX5	6.47	0.13	0.33	0.13	26	2	5.2	1545	1.3%	0.8	34.0	39.1	2.1	3.5	1.8	7.5	0.84	EX5	2.14
EX6	0.38	0.13	0.33	0.13	95	1	19.0	91	11.0%	1.1	1.4	20.5	3.1	5.1	0.2	0.6	0.05	EX6	0.13
EX7	0.72	0.13	0.33	0.13	127	2	19.3	215	1.9%	0.8	4.7	24.0	2.8	4.7	0.3	1.1	0.09	EX7	0.24
EX8	9.1	0.13	0.33	0.13	128	4	15.4	530	2.6%	0.8	11.6	27.1	2,6	4.4	3.1	13.3	1.18	EX8	3.00
EX9	6.3	0.13	0.33	0.13	165	7	15.8	1017	2,1%	0.8	22.4	38.2	2.1	3.6	1.7	7.4	0.82	EX9	2,08
EX10	4.9	0.13	0.33	0.13	216	4	23.8	382	2.1%	0.8	8.4	32.2	2.4	4.0	1.5	6.4	0.64	EX10	1.62
EX11	6.8	0.13	0.33	0.13	204	4	22.7	1310	2.0%	0.8	28.8	51.5	1.7	2.8	1.5	6.3	0.88	EXII	2.24
**P	2.14	0.57	0.67			and survey the						15.2			4.2	8.8	1.22	**p	1.43
**Q	3.66	0.57	0.67			2						21.1	1		6.1	12.8	2.09	++0	2.45
#B	2.89	0.57	0.67									11.4			6.4	13.4	1.65	#B	1.94
#D	1.36	0.58	0.68			_						9.2			3.3	7.0	0.79	#D	0.92
#F	1.28	0.58	0.68									10.2			3.0	6.3	0.74	#F	0.87
#8	1.32	0.58	0.68									10.2			3.1	6.5	0.77	#H	0.90
#J	1.37	0.58	0.68			5			- Mar for 1. Cally and			10.1			3.2	6.8	0.79	#J	0.93
#L	1.46	0.57	0.67									10.3	nie – Photosofi – – John – –		3.4	7.0	0.83	#L	0.98
#0	1.63	0.56	0.66									10.7			3.6	7.6	0.91	#O	1.08
				1	Proposed	Area	Drainag	e Sumn	narv					<u> </u>	and the second second				
V	2.48	0.38	0.54	0.38	139	2.78	73.1	604	1.5%	3.0	3.3	16.4	3.4	57	3.2	7.6	0.94	v	1 34
W	22	0.40	0.54	0.40	112	2.24	11.2	604	1.5%	3.0	3.3	14.6	3.6	6.0	3.1	21	0.88	w	1 19
X	2.03	0.38	0.53	0.38	128	2.56	12.5	427	1.3%	3.0	2.3	14.8	3.5	5.9	2.7	6.0	0.77	x	1.07
Y	0.78	0.43	0.57	0.43	115	2.3	10.9	427	13%	3.0	2.3	13.3	3.7	6.2	7.2	2.8	0.34	v	0.44
Z	0.63	0.40	0.54	0.40	56	2.2	6.4	0	1.3%	2.3	0.0	6.4	4.8	8.1	1.2	2.7	0.25	7	0.34
AA	47	0.43	0.57	0.43	111	2.2	10.8	732	2.0%	3.0	4.0	14.8	3.5	5.9	7.2	15.9	2.02	ĂĂ	2.68
BB	1.56	0.43	0.57	0.43	107	2.1	10.6	732	2.0%	3.0	4,0	14.6	3.6	6.0	2.4	5.3	0.67	BB	0.89
CC	3.12	0.43	0.57	0.43	118	2.36	11.1	261	4.0%	3.0	1.4	12.5	3.8	6.4	5.1	11.3	1.34	cc	1.78
DD	1,61	0.40	0.54	0.40	83	4.9	6.8	590	1.1%	2.3	4.3	14.1	4.0	6.7	2.6	5.8	0.64	DD	0.87
EE	1,29	0.40	0.54	0.40	68	2.7	7.0	111	2,0%	23	0.3	7.8	45	7.6	23	5.3	0.52	EE	0.70

* Intensity equations assume a minimum travel time of 5 minutes.

** Data from Trails at Forest Meadows Filing No. 3 Final Drainage Report (TFM 3 FDR).

Data from Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No.1 & No.4 (MDDP)

Calculated by: ET Date: 12/9/2015 Checked by: VAS





City of Colorado Springs 30 S. Nevada Ave Colorado Springs, CO 80903

COTTONWOOD CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JULY 2019

C. TOR

Department of Public Works Water Resources Engineering

10 104 102.2

Prepared by:













	0.12 mi ²	
UC050 0.27 mi ²		+
	UC100	
	0.34 mi ²	
UC060	0.24 mi ²	A Line
0.23 mi ²		
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mi ²		
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0.05 mi ²		
	0.10 mi ²	R.C.
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		- S. B. B.
		2 Martin Barris
		1
BRIARGATE PKWY		A Company
		18 States
0.19 mi ²		1
0.23 mi ²	Future Land Use - Cottonwood	Creek
	Land Use	% of Basin Area
	0-1.99 du/ac	5.3%
UC165	12.0-24.99 du/ac	1.7%
N.22 III		0.3%
	2.5 AGRE RURAL RESIDENTIAL	7.0%
<u>UC150</u> 0.09 mi ²	3 5-7 99 du/ac	21.4%
	35 ACRE TRACT	1.4%
	5 ACRE RURAL RESIDENTIAL	8.7%
	8.0-11.99 du/ac	2.8%
	CIVIC	4.7%
UC160	COMMERCIAL	8.7%
		1.3%
		1.8%
The second se	NATURAL OPEN SPACE (PAIR CONDITION)	0.0%
	PARK/OPEN SPACE (FAIR CONDITION)	1.6%
A DEPENDENCE OF THE OWNER	PARK/OPEN SPACE (GOOD CONDITION)	0.9%
a Marine and and	ROW	13.5%
ure Development	WOODS (FAIR CONDITION)	2.9%
Planned		
The second	Future Land Use - South Pine	Creek
	land lise	% of Basin Area
A CONTRACTOR OF A CONTRACT		0.7%
Part / Barriston	12.0-24.99 du/ac	1.9%
And Annual Michael Constant Annual	2.0-3.49 du/ac	4.2%
	25+ du/ac	0.0%
	3.5-7.99 du/ac	29.4%
ALL DATE OF A STRAT	8.0-11.99 du/ac	2.3%
		6.2%
		18.1%
		4.2%
TOTAL STATES AND	NATURAL OPEN SPACE (FAIR CONDITION)	1.6%
G Contractor of Contractor	PARK/OPEN SPACE (FAIR CONDITION)	5.4%
	PARK/OPEN SPACE (GOOD CONDITION)	1.1%
	ROW	20.8%
And		

FIGURE 3-6 FUTURE CITY & COUNTY LAND USE COTTONWOOD CREEK & SOUTH PINE CREEK DBPS COLORADO SPRINGS, CO



1,000 2,000 3,000









SAND CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JANUARY 2021

Prepared for:





Prepared by:

Stantec





SAND CREEK - SAND CREEK DRAINAGE BASIN PLANNING STUDY

Basin Characteristics and Environmental Resources



Disclaiment his document has appended based on into matching powled by others as cles in the Notes section. General werked the accuracy analytic completeness of this information and chall not be responsible for any ensuing an encoder of the incorporated herein as a result. Little document or powled by others as cles in the Notes section. General and the required accuracy analytic regionability for vertiging the accuracy and completeness of the data.

Figure 2-7: NWI Wetlands Located in Sand Creek Drainage Basin (Page 4)

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SAND CREEK - SAND CREEK DRAINAGE BASIN PLANNING STUDY

Hydrology

Figure 3-15. Future Land Use MapFuture Condition Model Results Appendix E Maps

LEGEND:

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-- -6000- -- EXISTING MAJOR CONTOUR ---- EXISTING MINOR CONTOUR DRAINAGE BASIN MAJOR DRAINAGE BASIN

> A = BASIN DESIGNATIONB = AREA IN ACRES

DESIGN POINT EXISTING DRAINAGE ARROW

SCHIMIDT PARCEL EXISTING DRAINAGE MAP

PCD FILE NO: CDR-22-007

EXISTING DRAINAGE MAP SCHMIDT PARCEL JOB NO. 25188.13 09/02/2022 SHEET 1 OF 1

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ORIGINAL SCALE: 1" = 150'

SCHMIDT PARCEL PROPOSED DRAINAGE MAP