

PRELIMINARY DRAINAGE REPORT

for
HAVEN VALLEY

El Paso County, Colorado

August 2021

EL PASO COUNTY PCD FILE NO. PUDSP-21-007

Prepared for:

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PRELIMINARY DRAINAGE REPORT

for
HAVEN VALLEY
Security, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E. Date
Colorado P.E. License No. 33797
For and on Behalf of Drexel, Barrell & Co.

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name: Richmond American Homes

By: Date

Title: Matthew Jenkins
Director, Land Acquisition
Address: 4350 S. Monaco Street
Denver, CO 80237

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. Date
County Engineer/ECM Administrator
CONDITIONS:

PRELIMINARY DRAINAGE REPORT

for
HAVEN VALLEY
Security, Colorado

2.0 PURPOSE

This report is prepared by Drexel, Barrell & Co in support of the Haven Valley in Security, CO. The purpose of this report is to identify onsite and offsite drainage patterns, storm sewer, inlet locations, and areas tributary to the site, and to safely route developed storm water runoff to adequate outfall facilities.

3.0 GENERAL SITE DESCRIPTION

Location

Haven Valley is a 11.768 acre subdivision within the northwest quarter of Section 12, Township 15 South, Range 66 West of the 6th Principle Meridian in El Paso County, Colorado. The site is located southwest of Cable Ln and west of Hunters Run. The site is bounded on the north by Calvary Fellowship Fountain Valley church and Cable Ln, the west by Good Shepherd United Methodist church, and the south and the east by residential subdivision Pheasant Run Ranch Filing No. 1. See Vicinity Map in Appendix.

Existing Site Conditions

The site is approximately 11.768 acres in size surrounded by existing development. There are no existing structures on the site, only native grasses, a few trees and shrubs. There are no existing irrigation facilities on the project site. The project site slopes moderately from the northeast to southwest at approximately 5-7%. Existing drainage flows to the southwest where it drains overland between two houses to Pecos Drive, then south on Widefield Drive. Severe flooding has been observed between these two houses and one of the houses has experienced mold issues in the past.

Proposed Site Conditions

Haven Valley is a small lot single-family development, consisting of approximately 98 lots, streets, landscape areas and open space. A proposed full-spectrum detention pond is proposed to be constructed in an existing off-site drainage easement adjacent to the west side of the site. The flows will be released from the detention pond and be carried by pipe between the two houses and outlet via a bubbler in Widefield Drive. There is an existing drainage and utility easement located between the two houses.

Soils

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S.

Department of Agriculture Soil Conservation Service, the site is underlain by the Blakeland loamy sand (Soil No. 8). This soil is a type 'A' hydrologic soil group. This type of soil typically exhibits rapid infiltration rates and slow runoff characteristics with moderate erosion potential. See appendix for Soil Map.

Climate

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel 08041C0763G (December 7, 2018), the site does not lie within a designated 100-year floodplain. The site is in Zone X, an area of minimal flood hazard. See Appendix for FIRMette map.

Previous Drainage Studies

The site is located within the Security Drainage Basin, as studied in the Little Johnson/Security Drainage Basin Planning Study, prepared by Simons Li & Associates, Inc., 1987.

4.0 EXISTING CONDITION HYDROLOGY SUMMARY

Basin OS1 is an offsite basin to the north. This basin drains the Elm Grove Subdivision (town homes, age restricted) and several commercial buildings on the east side of Main St. and the Wilson Elementary School on the west side of Main St. The runoff path begins on Main Street near the intersection of Bradley Road, then flows southerly down Main Street via curb and gutter. The runoff at this intersection is collected by a storm sewer constructed as part of the 1993 Main Street reconstruction by El Paso County. The storm drain system conveys runoff east underground via storm sewer and discharges in to a valley gutter within the Elm Grove Subdivision. The valley gutter drains south to an existing detention pond (roughly 3-4' deep) where it is detained slightly. The pond discharges via a 24" CMP to the south. The 24" CMP is undersized for the 100-year which overtops the pond and drains into a swale which in turn drains south overland between two houses in the Security Colorado Addition 4, then south to the curb and gutter in Pecos Drive and Widefield Drive. The runoff generated by Basin OS1 is calculated to be 46.0 cfs and 88.8 cfs for the 5-year and 100-year storm respectively into the detention pond. After detention, the pond outflows are 18.1 cfs and 52.3 cfs respectively for the 5-year and 100-year storms.

Basin OS2 is an offsite basin to the north of the site. Runoff from this basin is primarily generated from roof, parking lot and vacant land. The runoff path begins on Cable Lane and generally flows southerly along the west property line until it reaches Design Point A. Design Point A collects the flow from Basin OS2 and the release from the detention pond

in Basin OS1. This flow is routed southerly through a small swale that divides Basins OS3 and H1. The calculated runoff from Basin OS2 is 11.8 cfs and 21.5 cfs for the 5-year and 100-year storm respectively.

Design Point A. The drainage swale previously mentioned conveys the flow from Design Point A to Design Point B. The calculated flow at Design Point A is 29.9 cfs and 73.8 cfs for the 5-year and 100-year storm respectively. This flow includes detained flow from the Elm Grove pond and from Basin OS-2 which is conveyed south in an existing swale to a historic low point just north of Security Colorado Addn. No. 4 (Des. Pt. B).

Basin OS3 is an offsite basin to the west of the site. Runoff from this basin is generated from roof, street, parking lot and vacant land. The runoff path flows southerly down Main Street via curb and gutter and then easterly onto Leta Drive. The flow then continues south through a parking lot until it empties onto vacant land, then travels to the southeast to Design Point B. Design Point B collects the flow from all basins; OS1, OS2, OS3 and H1 and drains them overland between two houses in the Security Colorado Addition 4, then south to the curb and gutter in Pecos Drive and Widefield Drive. Severe flooding between these houses has been observed on numerous occasions in the past. The calculated runoff from Basin OS3 is 15.6 cfs and 37.4 cfs for the 5-year and 100-year storm respectively.

Basin H1 is an onsite basin which drains the site plus street runoff from Alturas Drive and Cable Lane. The east half of Alturas Drive drains is not included in this basin which drains overland eastward into the Windmill Creek Subdivision per the approved drainage report by Jefferies Engineering, October 10, 2001. Runoff from the undeveloped lot west of Alturas Drive is currently collected in a swale west of the ROW and directed south into a detention pond which outlets into the FMIC superditch. Future conditions for this undeveloped lot will need to remain the same as existing since additional runoff down Alturas would severely affect downstream properties. Runoff from Alturas Drive is included in this basin per existing conditions. The runoff path for Basin H1 begins near the intersection of Alturas Drive and Bradley Road (west half), and then flows southwesterly via an asphalt curb southward and over the top of the FMIC superditch. The flow then crosses Cable Lane and generally flows southwesterly through vacant land to Design Point B. The calculated runoff for Basin H1 is 6.9 cfs and 30.4 cfs for the 5 year and 100 year storm respectively.

Please detail which side(s) of these roads the flow is directed to so it can be compared to the proposed condition.

Design Point B includes flow from Design Point A, Basin OS-3, and H1. Design Point B discharges through the Security Colorado Addition No. 4 Refile Subdivision overland between two houses, then south to curb and gutter Pecos Drive and Widefield Drive. The total flow at Design Point B is 46.1 cfs and 129.0 cfs for the 5-year and 100-year storm respectively between the two houses. Both of these two homeowners have indicated that they have experienced severe flooding of the backyard and crawl spaces of their homes.

Basin OS4 is an offsite basin to the west of the site including Main Street and a portion of land west of Main Street. Runoff from this basin is generated from roof, street, and parking lot. The runoff path flows southerly down Main Street via curb and gutter to the intersection of Pecos Drive. An existing storm sewer system was constructed in 1993 as part of the 1993 Main Street reconstruction project by El Paso County. The storm system picks up street flow and discharges it to a 15' bubbler located just east of the intersection of Pecos Drive and

Please detail which side(s) of these roads the flow is directed to so it can be compared to the proposed condition.

Main Street. From the bubbler, all runoff is carried overland east to Widefield Drive (Design Pt C), then south on Widefield Drive via curb and gutter. There is no existing storm sewer system within Pecos or Widefield Drive. The calculated runoff from Basin OS4 is 39.6 cfs and 82.3 cfs for the 5-year and 100-year storm respectively. The existing street capacity of Widefield Drive (0.54% street slope) as it flows south from Pecos Drive is 12 cfs and 54 cfs for the 5-year and 100-year storm respectively. As shown, the flow from this basin alone exceeds the street capacity of Widefield Drive.

Design Point C is located at the intersection of Pecos Drive and Widefield Drive and includes flow from Design Point B and Basin OS-4. At Design Point C the existing flow with detention from the Elm Grove pond is 80.3 cfs and 200.0 cfs for the 5-year and 100-year storm respectively, which is all overland flow. The existing street capacity of Widefield Drive as it flows south (0.54% street slope) from Pecos Drive is 12 cfs and 54 cfs for the 5-year and 100-year storm events. As shown, the existing street capacity is severely exceeded in existing conditions which is echoed by the residents in this area experiencing chronic flooding at this intersection. This development is proposing to reduce the flooding issues in this area which will be discussed later in this report.

5.0 PROPOSED HYDROLOGY (RATIONAL METHOD) & HYDRAULIC SUMMARY

The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals. Urban Drainage UD-Detention and Flowmaster were used to determine pond and storm system sizing. UD-Inlet and UD-Sewer were also used to identify pond and storm system sizing (see appendix for calculations). See below for a summary runoff table of the basins and for descriptions of each design point. See appendix for Proposed Drainage Map showing the proposed drainage basin locations.

Rational Method Runoff Summary

BASIN	AREA (AC)	Q5 (cfs)	Q100 (cfs)
A	0.44	0.5	1.5
OS-1	16.90	46.0	88.8
OS-2	2.85	11.8	21.5
B	1.42	3.2	6.6
C	3.43	6.4	14.0
D	0.98	1.2	3.5
E	1.59	3.1	6.7
F	3.29	6.9	15.3
G	0.83	1.0	3.0
OS-3	9.74	15.6	37.4
H	1.77	2.4	6.1
OS-4	20.04	39.6	82.3

Design Point 1 (DP-1) represents flows generated from existing Elm Grove pond release in

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offsite basin OS-1, as well as flows from offsite basin OS-2 and onsite Basin A. The flows are conveyed via a swale and are then captured by a proposed public Double Type D area inlet. The flows leave this inlet via a proposed public 36" RCP storm pipe and are conveyed to the proposed Extended Detention Basin to the south. The total flow at DP-1 is 28.1 cfs and 71.0 cfs for the 5-year and 100-year storm respectively. The Double Type D area inlet can capture all of the DP-1 flows.

Design Point 2 (DP-2) represents flows generated from onsite Basin B. The flows are captured by a proposed private at-grade 5' Type R inlet in Basin B. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried south to DP-J1. The total flow at DP-2 is 3.2 cfs and 6.6 cfs for the 5-year and 100-year storm respectively.

Design Point 3 (DP-3) represents flows generated from Basin C. The flows are captured by a proposed private at-grade 15' Type R inlet in Basin C. The flows leave this inlet via a proposed private 24" RCP storm pipe and are carried west to DP-J1. The total flow at DP-3 is 6.4 cfs and 14.0 cfs for the 5-year and 100-year storm respectively.

Design Point J1 (DP-J1) represents flows generated from Basins B and C. This design point is located at a proposed junction with a Type II manhole in Basin C. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried south to DP-J3. The total flow at DP-J1 is 9.5 cfs and 20.3 cfs for the 5-year and 100-year storm respectively.

Design Point 4 (DP-4) represents flows generated from Basin D. The flows are conveyed via a swale and are then captured by a proposed private sump condition Type C area inlet in Basin D. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried west to DP-J2. The total flow at DP-4 is 1.2 cfs and 3.5 cfs for the 5-year and 100-year storm respectively.

Design Point 5 (DP-5) represents flows generated from Basin E, which includes a portion of Cable Ln as shown on the proposed drainage map in the Appendix. The flows are captured by a proposed private at-grade 5' Type R inlet in Basin E. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried south to DP-J2. The total flow at DP-5 is 3.1 cfs and 6.7 cfs for the 5-year and 100-year storm respectively. Cable Lane is an existing public two-lane paved roadway. As part of this project, the roadway will be widened and curb and gutter added. Basin E will collect runoff from a portion the existing and proposed Cable Lane. The remainder of the roadway drainage will follow historic patterns.

Design Point J2 (DP-J2) represents flows generated from Basins D and E. This design point is located at a proposed junction with a Type II manhole in Basin E. The flows leave this manhole via a proposed private 18" RCP storm pipe and are carried west to DP-J3. The total flow at DP-J2 is 4.3 cfs and 10.0 cfs for the 5-year and 100-year storm respectively.

Design Point J3 (DP-J3) represents flows generated from Basins B, C, D and E. This design point is located at a proposed junction with a Type II manhole in Basin F. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried west to DP-6. The total flow at DP-J3 is 13.5 cfs and 29.8 cfs for the 5-year and 100-year storm respectively.

Design Point 6 (DP-6) represents flows generated from Basins B, C, D, E and F. The flows are captured by a proposed private sump 15' Type R inlet in Basin F. The flows leave this inlet via a proposed private 24" RCP storm pipe and are carried west to the proposed Extended Detention Basin. The total flow at DP-6 is 19.2 cfs and 42.4 cfs for the 5-year and 100-year storm respectively.

Calcs and drainage plan indicate 20.1 cfs and 44.4 cfs, revise accordingly

Design Point 7 (DP-7) represents flows generated from Basin G only. The flows from the existing Elm Grove pond release are captured by the area inlet in Basin A as discussed under DP-1. The flows are captured by a proposed swale and are carried to the proposed Extended Detention Basin. The total flow at DP-7 is 1.0 cfs and 3.0 cfs for the 5-year and 100-year storm respectively.

revise to private

Design Point P1 (DP-P1) represents all of the flows generated from Basins OS-1, Exist. Elm Pond release and Basins A through G. These are all of the flows that are captured by the proposed Extended Detention Basin. Further detail is provided on the EDB in the following section of this report. The total flows at DP-P1 is 63.1 cfs and 152.1 cfs for the 5-year and 100-year storm respectively.

Design Point 8 (DP-8) represents flows generated from Basin H, OS-5 and OS-6 combined with the released flows from the proposed EDB. The flows are conveyed via a swale and are then captured by a proposed public sump condition Type C area inlet in Basin H. The flows leave this inlet via a proposed public 24" RCP storm pipe and are carried south to DP-J4. By piping these flows between the two houses, flooding for these two existing residences will be eliminated in this area. In the event of a storm event that overtops the EDB spillway, a concrete channel is proposed between the two existing residences to help prevent flooding. The concrete channel is to be 2.5' high x 6.5' wide and is directly over the 24" RCP pipe below. The total flow at DP-8 is 2.3 cfs and 21.5 cfs for the 5-year and 100-year storm respectively.

Page 5 above indicates the street capacity as 54 cfs (100yr) yet the flow going south is 62 cfs. It does not appear that the roadway can handle the 100yr flows. Please revise accordingly

Design Point O4 (DP-O4) represents flows generated from Basin OS-4. A proposed public at-grade 15' Type R inlet is to be installed on existing Pecos Dr. This inlet will not be able to capture all of the flows but will capture some and improve the flooding in this area. The total flow at DP-O4 is 39.6 cfs and 82.3 cfs for the 5-year and 100-year storm respectively. The proposed 15' Type R inlet can capture approximately 20 cfs. The remaining approximate 62 cfs will continue to the south along Widefield Drive along historic drainage routes as outlined in the DBPS. The street capacity of Pecos Dr. and Widefield Dr. can handle the 100-yr flows, but not the 5-yr flows.

Identify the depth of flow along widefield drive

Design Point J4 (DP-J4) represents flows generated from Basins H, OS-4, OS-5, OS-6 and the flows released from the proposed EDB. This design point is located at a proposed junction with a Type I manhole in Basin OS-4. The total flow at DP-J4 is 41.9 cfs and 103.8 cfs for the 5-year and 100-year storm respectively. The flows leave this manhole via a proposed public 34"x 53" elliptical RCP storm pipe and are carried south where they will outlet via a proposed 25' Type R inlet to be used as a bubbler in Widefield Drive and continue to the south along historic drainage routes as outlined in the DBPS. The bubbler inlet will serve to release the developed upstream flows into Widefield Drive as street flow at the end of the storm sewer system. The inlet will fill and overtop/exit the inlet throat into

Review 1: Please also provide the flow being conveyed by Widefield drive and the flow that is being piped to the proposed 25' bubbler.

Review 2: Per the information provided above it appears that 62 cfs is conveyed by Widefield drive and 41.8 cfs is conveyed by the 34x53" RCP. Please confirm and indicate the flow that is being conveyed by the pipe and the flow conveyed by Widefield drive in your narrative.

Describe plan to keep this small pipe from clogging. The upstream bubbler at Pecos and Main is a constant maintenance issue, always clogging with the sediment/muck that settles out in the inlet/bubbler. That amount of maintenance is unacceptable.

flows and allow the inlet to drain after filling.

None of the proposed streets exceed capacity, see Appendix for Street Capacity Charts. See also inlet capacity charts for inlet sizing in the Appendix.

Please be sure to identify whether or not any of the storm infrastructure within Widefield drive shown on the DBPS was ever installed.

6.0 PROPOSED DETENTION/WATER QUALITY FACILITIES

The proposed private full spectrum Extended Detention Basin (EDB) is located southwest of the project site within a 1.29 acre drainage easement. This detention pond will fulfill on-site detention needs as well as providing detention for upstream properties, since there is a lack up detention facilities upstream which has caused chronic flooding issues between the two residences that the flows currently pass between on their way to Widefield Dr. The 1.29 acre easement is proposed to be a private drainage/detention easement and the pond to be maintained by Homeowners Association. The Security DBPS does not address the need for a pond in this area, rather it shows roughly 188 cfs (100-year storm) passing between the two houses with only a 24" storm sewer and no swale to convey the flow. The developed peak 100-year flow calculated in this report is 152.1 cfs at this location. The difference in flow is attributed to the DBPS bypassing Elm Grove Pond. The proposal shown in the DBPS does not work and will flood the two residences. Even though the DBPS does not adequately address flooding issues in this area, we are proposing to construct a facility necessary to detain runoff from our project site

Per the revised design the 18" pipe connects to an inlet and then is piped between the houses via a 24" pipe. Please revise accordingly

The proposed detention facility has been designed to capture flows from Basins OS-1, OS-2, OS-3 and Basins A through G. A total of 41.47 acres is tributary to this EDB with a composite imperviousness of 57.8%. The required pond volume for 100-year detention is 4.409 acre-feet. The actual pond volume will be 4.542 acre-feet. Concrete forebays with energy dissipaters will be placed where the flows enter the pond on the northeast and the east sides of the pond. The combined volume of the two forebays will be 3% of the WQCV volume for the pond and will be divided proportionally. The flows will exit the forebays through a notch and into the concrete trickle channel at the bottom of the pond that conveys the flows to the micropool. It will capture then release the flows at a reduced flow rate with the use of a plate with orifice holes into a proposed 18" pipe with a restrictor plate. The 18" pipe continues to the south, between the two existing residences, and outfalls into a bubbler in Widefield Dr. where they continue in historic patterns to the south.

In accordance with El Paso County criteria, the modified Type C outlet structure with a permanent micropool will release the WQCV over a 40-hour period. The outlet structure will result in release rates of 0.9 cfs and 17.6 cfs for the 5-year and 100-year storm respectively.

A 30-ft wide riprap emergency spillway will be located on the south side of the pond. In the event that water overtops the spillway, flow will discharge into a 2.5' high x 6.5' wide concrete channel between the two residences before discharging into Widefield Dr. curb and gutter and continuing to the south.

Provide calculation of this channel conveying the 100yr flow. Staff has to ensure that the 100yr undetained flow overtopping the spillway will be conveyed to this channel and contained within this channel before approving this design. Additionally, how is the discharge from the channel addressed? is riprap proposed from the channel to the back of the sidewalk?

bay volumes, micropool

Stabilized access ramp shall be a minimum of 15ft wide and no greater than 12% slope, in accordance with DCMv1, Chap 11.2.2

sizing, outlet structure design, discharge pipe and spillway design.

The pond will have a 10' wide maintenance access that will provide access to the pond bottom. Private maintenance agreements and O&M manuals will be established for this pond as required by the County.

7.0 FOUR-STEP PROCESS

This project conforms to the City of Colorado Springs/El Paso County Four Step Process. The process focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

1. **Employ Runoff Reduction Practices:** Proposed impervious areas on this site (roofs, asphalt/sidewalk) will sheet flow across landscaped ground as much as possible to slow runoff and increase time of concentration prior to being conveyed to the proposed public streets and storm sewer system. This will minimize directly connected impervious areas within the project site.
2. **Implement BMP's that provide a Water Quality Capture Volume with slow release:** Runoff from this project will be treated through capture and slow release of the WQCV in a permanent Extended Detention Basin facility designed per current City of Colorado Springs/El Paso County drainage criteria.
3. **Stabilize Drainage Ways:** Flows from the pond are released into Widefield Dr. curb and gutter and no stabilization will be necessary.
4. **Implement Site Specific and Other Source Control BMP's:** The site is proposed as a residential development, and as such standard household source control will be utilized in order to minimize potential pollutants entering the storm system. Example source control measures consist of: garages for storage of household chemicals, trash receptacles for individual households and in common areas for pet waste. The need for Industrial and Commercial BMP's was considered, however per ECM 1.7.2.A the need for industrial and commercial BMPs are not applicable for this project.

8.0 GEOTECHNICAL HAZARDS

In accordance with geotechnical recommendations, the project design is intended to direct runoff away from structures at a minimum slope of six inches over ten feet, and into the receiving water quality basin. This will be accomplished by a variety of means, i.e. curb and gutter and storm sewer.

9.0 DRAINAGE & BRIDGE FEES

Drainage and Bridge Fees

The project lies within the Security Drainage Basin and is previously un-platted. The following fees are required at time of plat recordation:

Impervious area = 11.768 acres x 58.1% = 6.84 acres

Drainage Fees

\$19,752 x 6.84 Impervious Acres = \$135,103.68

Bridge Fees

None

Reimbursement for construction of some of the drainage facilities for Haven Valley and the storm sewer outfall in accordance with DCM Section 3.3, is anticipated as identified by the Little Johnson/Security Drainage Basin Planning Study. See Appendix for Sheet 22 of this DBPS for the reimbursable facilities. Construction costs are listed below and the drainage fee is requested to be adjusted accordingly.

10.0 CONSTRUCTION COST ESTIMATE

Private (Non-Reimbursable)

Description	Quantity	Unit Cost	Cost
Type C Area Inlet	1 EA	\$4,800/EA	\$4,800
5' Type R Inlet	2 EA	\$5,700/EA	\$11,400
15' Type R Inlet	2 EA	\$10,300/EA	\$20,600
Type II Manhole	3 EA	\$5,000/EA	\$15,000
18" RCP storm	865 LF	\$67/LF	\$57,955
24" RCP storm	180 LF	\$81/LF	\$14,580
		Subtotal	\$124,335
		Engineering & Contingency (10%)	<u>\$12,434</u>
		TOTAL	\$136,769

Public/Private (Reimbursable)

Description	Quantity	Unit Cost	Cost
Type C Area Inlet	1 EA	\$4,800/EA	\$4,800
Double Type D Area Inlet	1 EA	\$11,800/EA	\$11,800
15' Type R Inlet	1 EA	\$10,300/EA	\$10,300
25' Type R Inlet	1 EA	\$15,000/EA	\$15,000
Type I Manhole	3 EA	\$7,000/EA	\$21,000
18" RCP storm	65 LF	\$67/LF	\$4,355
24" RCP storm	105 LF	\$81/LF	\$8,505
36" RCP storm	385 LF	\$124/LF	\$47,740
48" RCP storm	15 LF	\$184/LF	\$2,760
34"x53" elliptical RCP	330 LF	\$184/LF	\$60,720
Water Quality/Detention Pond	1 EA	\$50,000/LS	\$50,000
		Subtotal	\$236,980
		Engineering & Contingency (10%)	<u>\$23,698</u>
		TOTAL	\$260,678

Only items identified in the DBPS would be reimbursable. Please revise the list accordingly. Alternatively it may be identified that the extent of reimbursable storm infrastructure will be determined at the final plat stage but please revise the title so that it does not imply that all items are reimbursable.

11.0 CONCLUSIONS

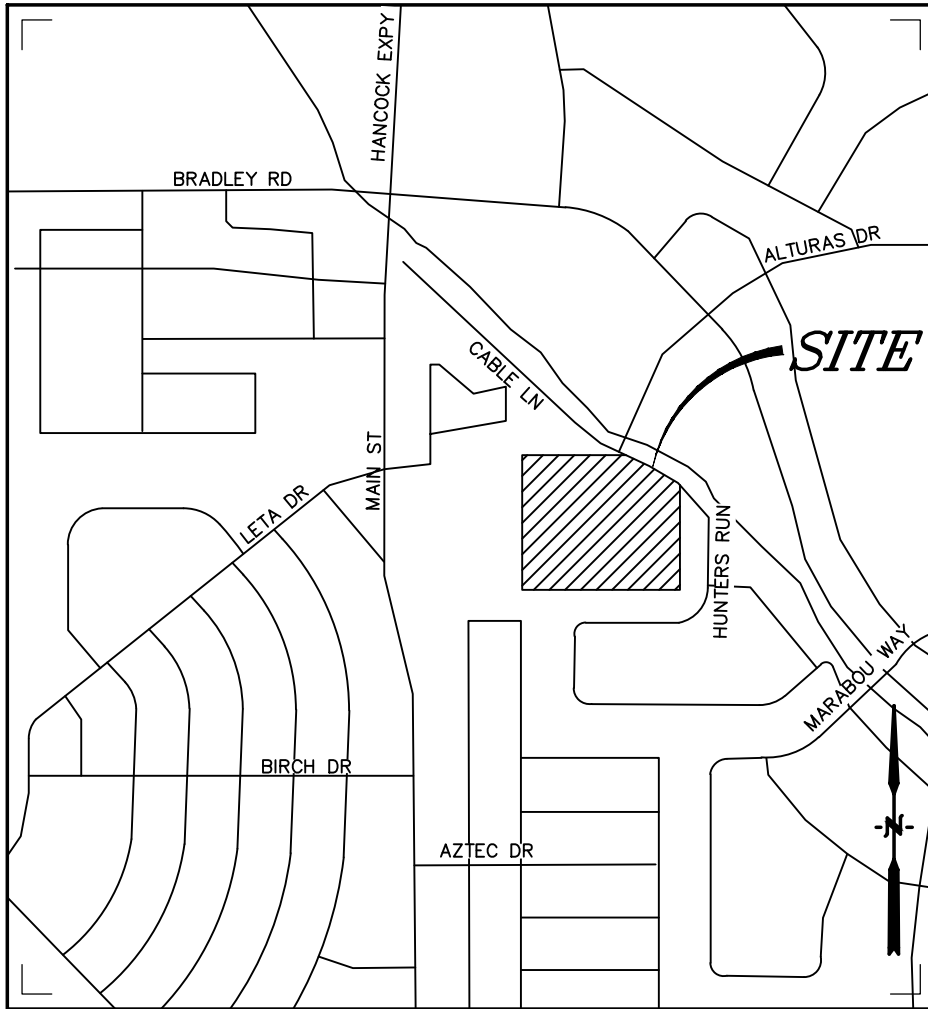
The Haven Valley project has been designed in accordance with El Paso County criteria. The detention pond and water quality basin have been designed to limit the release of storm runoff to historic flows. This development will not negatively impact the downstream facilities.

12.0 REFERENCES

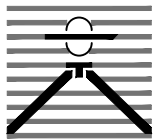
The sources of information used in the development of this study are listed below:

1. City of Colorado Springs/El Paso County Drainage Criteria Manual, May 2014.
2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised April 2008.
3. Preliminary & Final Drainage Report for Patriot Village. Prepared by Core Engineering Group, LLC, December 2013.
4. Natural Resources Conservation Service (NRCS) Web Soil Survey
5. Federal Emergency Management Agency, Flood Insurance Rate Map, El Paso County, Colorado and Unincorporated Areas, Map Number 08041C0763G, Effective Date December 7, 2018
6. EL Paso County Board Resolution No 15-042: El Paso County adoption of Chapter 6 and Section 3.2.1, Chapter 13 of the City of Colorado Springs Drainage Criteria Manual, May 2014.
7. Little Johnson/Security Drainage Basin Planning Study. Prepared by Simons Li & Associates, Inc., 1988.
8. Soil Investigation Report for Patriot Village. Prepared by Colorado Engineering & Geotechnical Group, Inc., November 15, 2004.

APPENDIX



Vicinity Map
Not to scale



**HAVEN HILLS
COLORADO SPRINGS, CO
VICINITY MAP**

Drexel, Barrell & Co.
Engineers • Surveyors

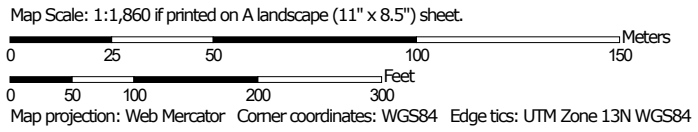
DATE:
JOB NO:
21085-03CSCV

DWG. NO.
VMAP
SHEET 1 OF 1

Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	12.7	100.0%
Totals for Area of Interest			12.7	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

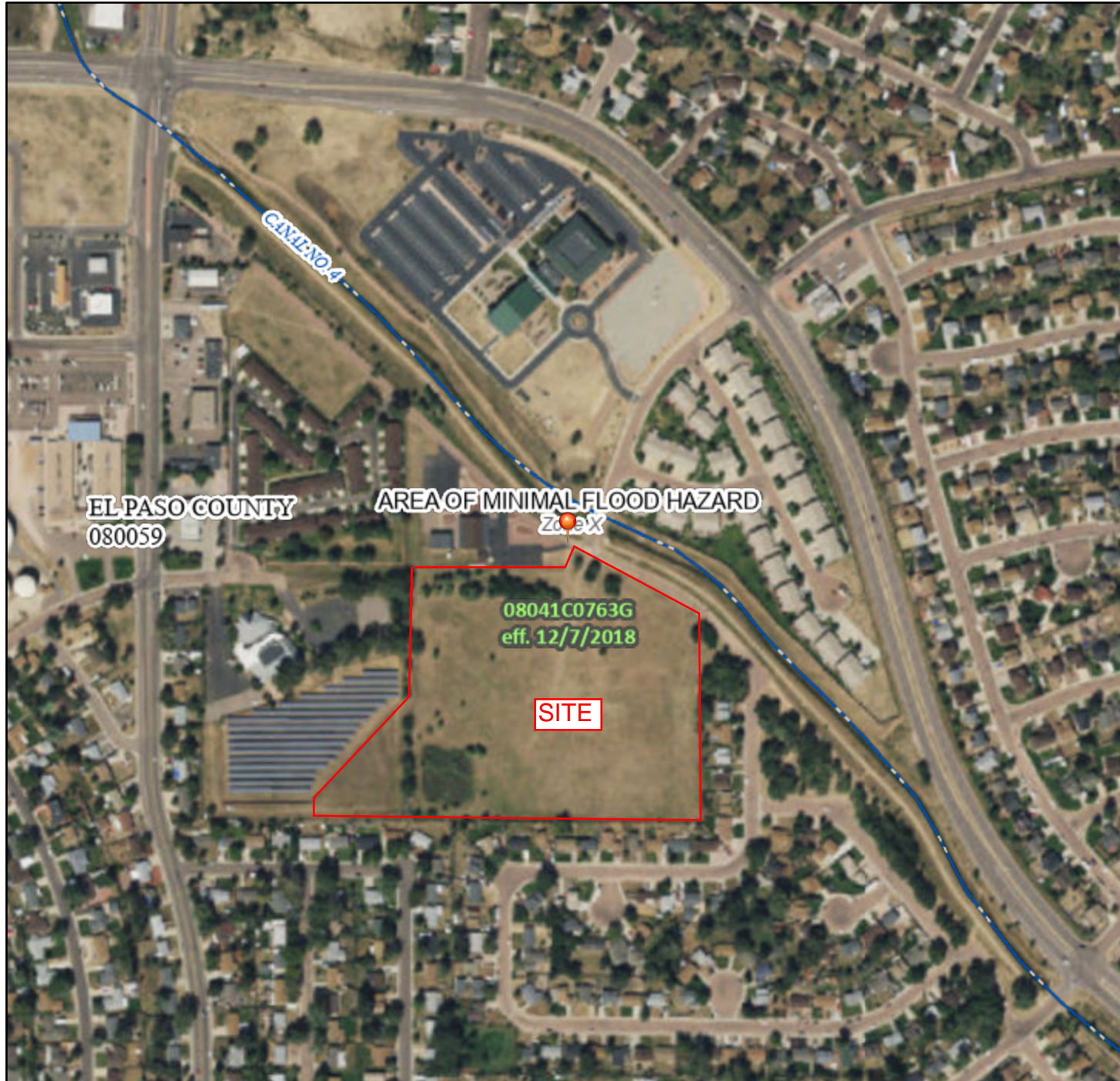
Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

National Flood Hazard Layer FIRMette



104°44'26"W 38°46'14"N



104°43'49"W 38°45'46"N

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) <i>Zone A, V, A99</i>
		With BFE or Depth <i>Zone AE, AO, AH, VE, AR</i> Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile <i>Zone X</i>
		Future Conditions 1% Annual Chance Flood Hazard <i>Zone X</i>
		Area with Reduced Flood Risk due to Levee. See Notes. <i>Zone X</i>
		Area with Flood Risk due to Levee <i>Zone D</i>
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard <i>Zone X</i> Effective LOMRs
		Area of Undetermined Flood Hazard <i>Zone D</i>
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped

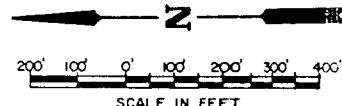
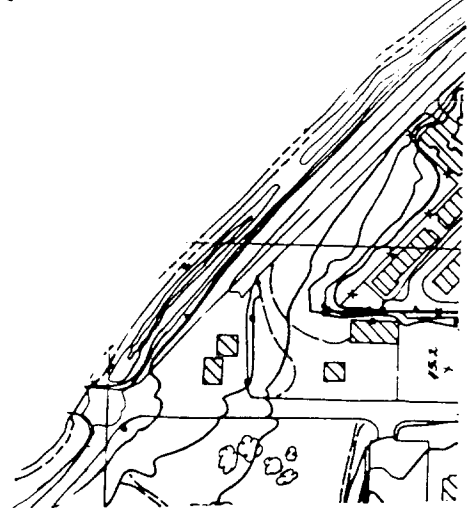
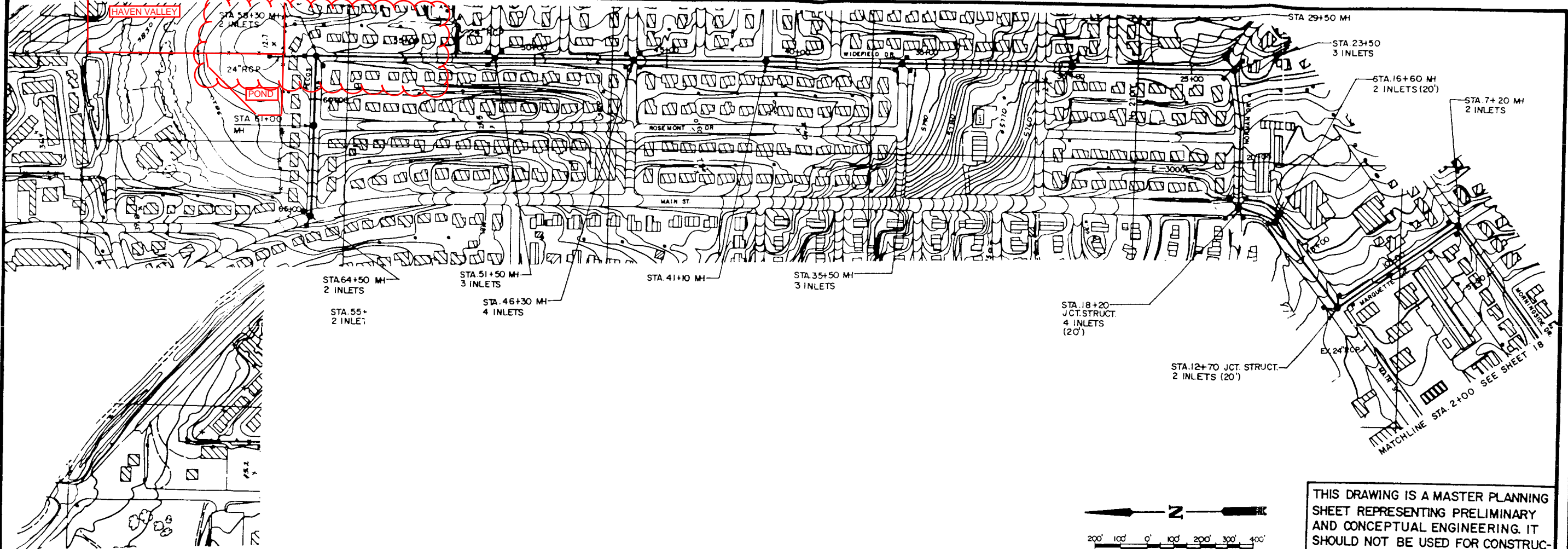
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.



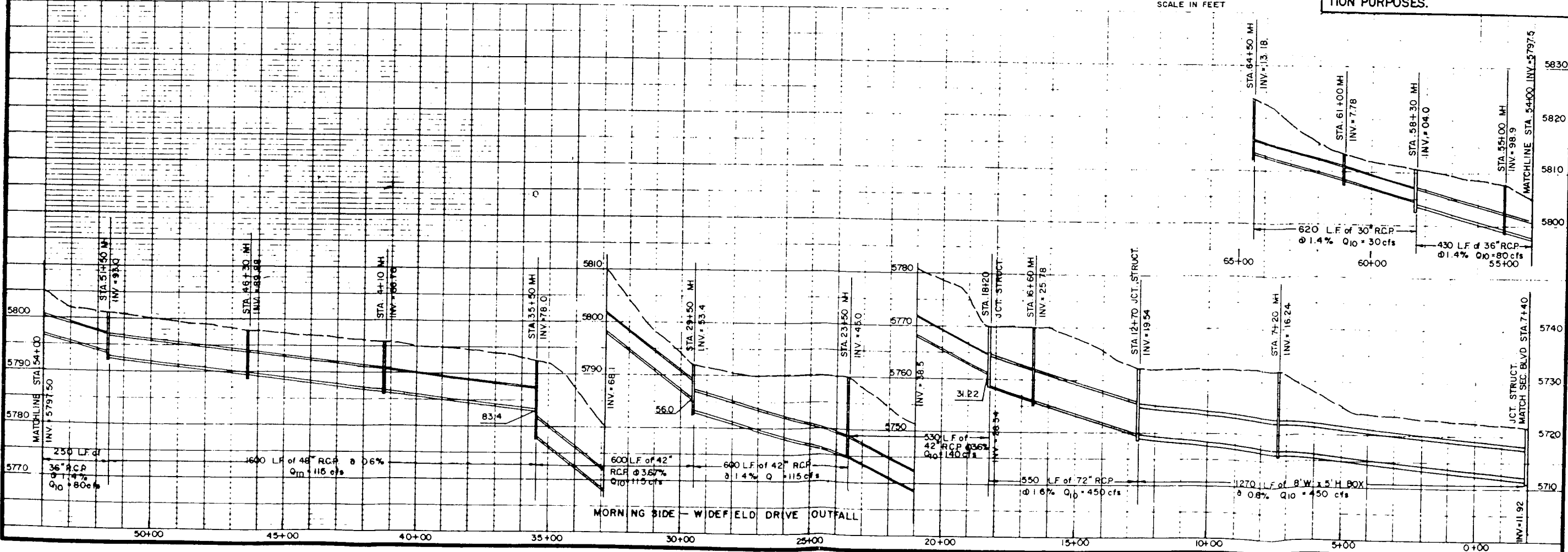
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **4/8/2021 at 1:19 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.



SIB Simons, Li & Associates, Inc.
 410 West 8th Ave., Colorado Springs, Colorado 80907 Phone 303-539-7742

LITTLE JOHNSON / SECURITY CREEK
 DRAINAGE BASIN PLANNING STUDY
 PRELIMINARY DESIGN
 PLAN & PROFILE: MORNINGSIDE - WIDEFIELD DRIVE OUTFALL

Project No.	PCOEPC-01
Date:	10/87
Design:	TCF
Drawn:	EAK
Checked:	TCF
Revisions:	

Review 1 comment: El Paso County.

Revise accordingly throughout
Review 2: unresolved



Review 1 comment: Table 6-6 of CH 6 should be referenced. It appears that the coefficients shown in the table match those shown on table 6-6
Review 2: Unresolved

PROJECT INFORMATION

PROJECT: Haven Valley
 PROJECT NO: 21085-03
 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: City of Colorado Springs
 REPORT TYPE: Final
 DATE: 4/29/2021
 Soil Type: A

	C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow		0.08		0.35	0
Commercial		0.81		0.88	95
1/8 Acre Residential		0.45		0.59	65
Asphalt/Sidewalk		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 5-1, City of Colorado Springs "Drainage Criteria Manual"

EXISTING

SUB-BASIN	SURFACE DESIGNATION	AREA ACRE	COMPOSITE RUNOFF COEFFICIENTS				% IMPERV
			C2	C5	C10	C100	
OS-1	Pasture/Meadow	0.00		0.08		0.35	0
	Commercial	8.10		0.81		0.88	95
	1/8 Acre Residential	7.20		0.45		0.59	65
	Asphalt/Sidewalk	1.60		0.90		0.96	100
	WEIGHTED AVERAGE			0.67		0.76	83%
TOTAL OS-1		16.90					
OS-2	Pasture/Meadow	0.00		0.08		0.35	0
	Commercial	2.85		0.81		0.88	95
	1/8 Acre Residential	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.81		0.88	95%
TOTAL OS-2		2.85					
OS-3	Pasture/Meadow	4.93		0.08		0.35	0
	Commercial	4.05		0.81		0.88	95
	1/8 Acre Residential	0.76		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.41		0.59	45%
TOTAL OS-3		9.74					
OS-4	Pasture/Meadow	0.00		0.08		0.35	0
	Commercial	4.20		0.81		0.88	95
	1/8 Acre Residential	15.84		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.53		0.65	71%
TOTAL OS-4		20.04					
H-1	Pasture/Meadow	12.03		0.08		0.35	0
	Commercial	0.00		0.81		0.88	95
	1/8 Acre Residential	0.39		0.45		0.59	65
	Asphalt/Sidewalk	1.02		0.90		0.96	100
	WEIGHTED AVERAGE			0.15		0.40	9%
TOTAL H-1		13.44					
TOTAL SITE		62.97		0.48		0.63	58.1%

PROJECT INFORMATION

PROJECT: Haven Valley
 PROJECT NO: 21085-03
 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: City of Colorado Springs
 REPORT TYPE: Final
 DATE: 4/29/2021



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING TIME OF CONCENTRATION STANDARD FORM SF-2

SUB-BASIN DATA					INITIAL/OVERLAND TIME (t _i)				TRAVEL TIME (t _t)					TIME OF CONC. t _c		FINAL t _c
BASIN	DESIGN PT.	C _s	C ₁₀₀	AREA	LENGTH	HT	SLOPE	t _i	LENGTH	HT	SLOPE	VEL.	t _t	COMP. t _c	MINIMUM t _c	Min
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	t _c	t _c	Min
OS-1		0.67	0.76	16.90	100	2	2.0	6.5	1600	26	1.6	7.4	3.6	10.1	5	10.1
OS-2		0.81	0.88	2.85	100	2	2.0	4.3	400	13	3.3	10.6	0.6	4.9	5	5.0
	A	0.69	0.78	19.75										10.1	5	10.1
OS-3		0.41	0.59	9.74	100	2.5	2.5	9.5	1200	34	2.8	9.8	2.0	11.5	5	11.5
H-1		0.15	0.40	13.44	100	2	2.0	14.1	1600	73	4.6	12.5	2.1	16.2	5	16.2
	B	0.32	0.52	26.03					700	20	2.9	5.28	2.2	16.2	5	16.2
OS-4		0.53	0.65	20.04	100	2	2.0	8.5	2000	41	2.1	8.48	3.9	12.5	5	12.5
	C	0.41	0.58	46.07					100	1	1	3.10	0.5	16.7	5	16.7



Drexel, Barrell & Co.

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PROJECT: Haven Valley
 PROJECT NO: 21085-03
 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: City of Colorado Springs
 REPORT TYPE: Final
 DATE: 4/29/2021

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING RUNOFF 5 YR STORM P1= **1.50**

BASIN (S)	DESIGN POINT	AREA (AC)	DIRECT RUNOFF		C * A	I (IN/HR)	Q (CFS)
			RUNOFF COEFF	t _c (MIN)			
OS-1		16.90	0.67	10.1	11.24	4.09	46.0
Exist. Elm Grove Pond Release							18.1
OS-2		2.85	0.81	5.0	2.31	5.10	11.8
	A						29.9
OS-3		9.74	0.41	11.5	4.02	3.88	15.6
H-1		13.44	0.15	16.2	2.06	3.34	6.9
	B	26.03	0.32	16.2	8.38	3.34	46.1
OS-4		20.04	0.53	12.5	10.53	3.76	39.6
	C	46.07	0.41	16.7	18.91	3.29	80.3

PROJECT INFORMATION

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 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: City of Colorado Springs
 REPORT TYPE: Final
 DATE: 4/29/2021



Drexel, Barrell & Co.

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING RUNOFF 100 YR STORM P1= **2.52**

BASIN (S)	DESIGN POINT	AREA (AC)	DIRECT RUNOFF		C * A	I (IN/HR)	Q (CFS)
			RUNOFF COEFF	t _c (MIN)			
OS-1		16.90	0.76	10.1	12.91	6.88	88.8
Exist. Elm Grove Pond Release							52.3
OS-2		2.85	0.88	5.0	2.51	8.58	21.5
	A						73.8
OS-3		9.74	0.59	11.5	5.74	6.52	37.4
H-1		13.44	0.40	16.2	5.42	5.62	30.4
	B	26.03	0.52	16.2	13.67	5.62	129.0
OS-4		20.04	0.65	12.5	13.04	6.31	82.3
	C	46.07	0.58	16.7	26.71	5.53	200.0

PROJECT INFORMATION

PROJECT: Haven Valley
 PROJECT NO: 21085-03
 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: El Paso County
 REPORT TYPE: Final
 DATE: 8/19/2021
 Soil Type: A



Drexel, Barrell & Co.

	C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow		0.08		0.35	0
1/8 acre Residential		0.45		0.59	65
Asphalt/Sidewalk		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 6-6, El Paso County "Drainage Criteria Manual"

PROPOSED							
SUB-BASIN	SURFACE DESIGNATION	AREA ACRE	COMPOSITE RUNOFF COEFFICIENTS				% IMPERV
			C2	C5	C10	C100	
A	Pasture/Meadow	0.20		0.08		0.35	0
	1/8 acre Residential	0.24		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.28		0.48	35%
TOTAL A		0.44					
B	Pasture/Meadow	0.00		0.08		0.35	0
	1/8 acre Residential	1.11		0.45		0.59	65
	Asphalt/Sidewalk	0.31		0.90		0.96	100
	WEIGHTED AVERAGE			0.55		0.67	73%
TOTAL B		1.42					
C	Pasture/Meadow	0.32		0.08		0.35	0
	1/8 acre Residential	2.69		0.45		0.59	65
	Asphalt/Sidewalk	0.42		0.90		0.96	100
	WEIGHTED AVERAGE			0.47		0.61	63%
TOTAL C		3.43					
D	Pasture/Meadow	0.43		0.08		0.35	0
	1/8 acre Residential	0.55		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.29		0.48	36%
TOTAL D		0.98					
E	Pasture/Meadow	0.12		0.08		0.35	0
	1/8 acre Residential	1.27		0.45		0.59	65
	Asphalt/Sidewalk	0.20		0.90		0.96	100
	WEIGHTED AVERAGE			0.48		0.62	64%
TOTAL E		1.59					
F	Pasture/Meadow	0.00		0.08		0.35	0
	1/8 acre Residential	3.81		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL F		3.81					
G	Pasture/Meadow	0.40		0.08		0.35	0
	1/8 acre Residential	0.44		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.27		0.48	34%
TOTAL G		0.84					
H	Pasture/Meadow	0.47		0.08		0.35	0
	1/8 acre Residential	0.22		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.20		0.43	21%
TOTAL H		0.69					
TOTAL		13.20		0.43		0.58	57.9%
TOTAL POND TRIBUTARY		25.10		0.47		0.62	58.0%

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 DATE: 8/19/2021



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF
 PROPOSED TIME OF CONCENTRATION STANDARD FORM SF-2

SUB-BASIN DATA					INITIAL/OVERLAND TIME (t _i)				TRAVEL TIME (t _t)					PIPE TRAVEL TIME (t _p)				TIME OF CONC. t _c		FINAL t _c
BASIN	DESIGN PT.	C ₅	C ₁₀₀	AREA	LENGTH	HT	SLOPE	t _i	LENGTH	HT	SLOPE	VEL.	t _t	LENGTH	SLOPE	VEL.	t _t	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	Ft	%	FPS	Min	t _c	t _c	Min
A	1	0.28	0.48	0.44	100	8	8.0	7.7	350	14	4.0	6.2	0.9					8.6	5	8.6
OS-1		0.67	0.76	16.90	100	2	2	6.5	1600	26	1.6	7.4	3.6					10.1	5	10.1
OS-2		0.81	0.88	2.85	100	2	2	4.3	400	13	3.3	10.6	0.6					4.9	5	5.0
B	2	0.55	0.67	1.42	100	2	2.0	8.2	1300	57.0	4.4	12.3	1.8					10.0	5	10.0
C	3	0.47	0.61	3.43	100	2	2.0	9.3	250	11	4.4	6.5	0.6	600	3.3	10.6	0.9	10.9	5	10.9
	J1	0.49	0.63	4.85										5	0.5	3.4	0.0	10.9	5	10.9
D	4	0.29	0.48	0.98	100	7	7.0	7.9	250	9	3.6	5.9	0.7					8.6	5	8.6
E	5	0.48	0.62	1.59	100	2	2.0	9.2	600	22	3.7	11.3	0.9					10.1	5	10.1
	J2	0.41	0.57	2.57										5	0.5	3.4	0.0	10.1	5	10.1
	J3	0.46	0.61	7.42										450	2.2	7.2	1.0	11.2	5	11.2
F		0.45	0.59	3.81	100	10	10.0	5.6	600	14	2.3	8.9	1.1					6.8	5	6.8
	6	0.46	0.60	11.23										110	2.7	12.6	0.1	11.3	5	11.3
G	7	0.27	0.48	0.84	100	9	9.0	7.4										7.4	5	7.4
OS-3		0.41	0.59	9.74	100	2.5	2.5	9.5	1200	34	2.8	9.8	2.0					11.5	5	11.5
	P1	0.47	0.62	25.10														11.5	5	11.5
H	8	0.20	0.43	0.69	100	5	5.0	9.9	800	16	2.0	4.4	3.0					12.9	5	12.9
OS-4	O4	0.53	0.65	20.04	100	2	2	8.5	2000	41	2.1	8.5	3.9					12.5	5	12.5

PROJECT INFORMATION

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 DATE: 8/19/2021



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED RUNOFF 5 YR STORM P1= 1.50

BASIN (S)	DESIGN POINT	AREA (AC)	DIRECT RUNOFF		C * A	I (IN/HR)	Q (CFS)
			RUNOFF COEFF	t _c (MIN)			
A		0.44	0.28	8.6	0.12	4.34	0.5
OS-1		16.90	0.67	10.1	11.24	4.09	46.0
Exist. Elm Grove Pond Release							18.1
OS-2		2.85	0.81	5.0	2.31	5.10	11.8
	1	3.29	0.74	10.1	2.43	4.09	28.1
B	2	1.42	0.55	10.0	0.78	4.11	3.2
C	3	3.43	0.47	10.9	1.61	3.96	6.4
	J1	4.85	0.49	10.9	2.39	3.96	9.5
D	4	0.98	0.29	8.6	0.28	4.33	1.2
E	5	1.59	0.48	10.1	0.76	4.08	3.1
	J2	2.57	0.41	10.1	1.04	4.08	4.3
	J3	7.42	0.46	11.2	3.44	3.93	13.5
F		3.81	0.45	6.8	1.71	4.69	8.0
	6	11.23	0.46	11.3	5.15	3.91	20.1
G	7	0.84	0.27	7.4	0.23	4.55	1.0
OS-3		9.74	0.41	11.5	4.02	3.88	15.6
	P1	25.10	0.47	11.5	11.83	3.88	64.0
POND RELEASE							0.9
H		0.69	0.20	12.9	0.14	3.70	0.5
OS-5		0.15	0.45	12.9	0.07	3.70	0.2
OS-6		0.41	0.45	12.9	0.18	3.70	0.7
	8						2.3
OS-4	O4	20.04	0.53	12.5	10.53	3.76	39.6
	J4						41.9

PROJECT INFORMATION

PROJECT: Haven Valley
 PROJECT NO: 21085-03
 DESIGN BY: SBN
 REV. BY: TDM
 AGENCY: El Paso County
 REPORT TYPE: Final
 DATE: 8/19/2021



Drexel, Barrell & Co.

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED

RUNOFF 100 YR STORM

P1= 2.52

BASIN (S)	DESIGN POINT	AREA (AC)	DIRECT RUNOFF			I (IN/HR)	Q (CFS)	PIPE SIZING		
			RUNOFF COEFF	t _c (MIN)	C * A			n	Slope (ft/ft)	Pipe Diameter (in)
A		0.44	0.48	8.6	0.21	7.29	1.5			
OS-1		16.90	0.76	10.1	12.91	6.88	88.8			
Exist. Elm Grove Pond Release							52.3			
OS-2		2.85	0.88	5.0	2.51	8.58	21.5			
	1	3.29	0.83	10.1	2.72	6.88	71.0	0.016	0.038	36
B	2	1.42	0.67	10.0	0.95	6.90	6.6	0.016	0.035	18
C	3	3.43	0.61	10.9	2.10	6.66	14.0	0.016	0.005	24
	J1	4.85	0.63	10.9	3.05	6.65	20.3	0.016	0.035	24
D	4	0.98	0.48	8.6	0.48	7.27	3.5	0.016	0.023	18
E	5	1.59	0.62	10.1	0.98	6.86	6.7	0.016	0.005	18
	J2	2.57	0.57	10.1	1.46	6.86	10.0	0.016	0.023	18
	J3	7.42	0.61	11.2	4.51	6.60	29.8	0.016	0.023	24
F		3.81	0.59	6.8	2.25	7.88	17.7			
	6	11.23	0.60	11.3	6.76	6.56	44.4	0.016	0.125	24
G	7	0.84	0.48	7.4	0.40	7.65	3.1			
OS-3		9.74	0.59	11.5	5.74	6.52	37.4			
	P1	25.10	0.62	11.5	15.62	6.52	154.1			
POND RELEASE							17.6	0.016	0.006	18
H		0.69	0.43	12.9	0.29	6.22	1.8			
OS-5		0.15	0.59	12.9	0.09	6.22	0.6			
OS-6		0.41	0.59	12.9	0.24	6.22	1.5			
	8						21.5	0.016	0.029	24
OS-4	O4	20.04	0.65	12.5	13.04	6.31	82.3	0.016	0.005	48
	J4						103.8	0.016	0.006	34"x53" elpt

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	North Swale
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Slope	040000 ft/ft
Left Side Slope	0.25 V : H
Right Side Slope	10.00 V : H
Bottom Width	4.00 ft
Discharge	23.00 cfs

Results

Depth	0.69 ft
Flow Area	3.7 ft ²
Wetted Perim	7.52 ft
Top Width	6.82 ft
Critical Depth	0.86 ft
Critical Slope	0.017463 ft/ft
Velocity	6.19 ft/s
Velocity Head	0.60 ft
Specific Enerç	1.28 ft
Froude Numb	1.48
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	East Swale
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Slope	030000 ft/ft
Left Side Slope	0.25 V : H
Right Side Slope	0.25 V : H
Bottom Width	2.00 ft
Discharge	3.50 cfs

Results

Depth	0.33 ft
Flow Area	1.1 ft ²
Wetted Perim	4.70 ft
Top Width	4.62 ft
Critical Depth	0.36 ft
Critical Slope	0.021252 ft/ft
Velocity	3.23 ft/s
Velocity Head	0.16 ft
Specific Enerç	0.49 ft
Froude Numb	1.17
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	South Swale
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

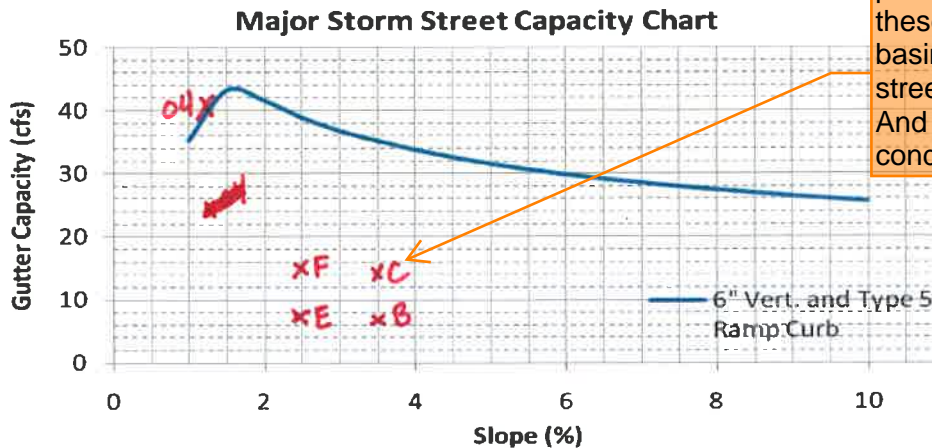
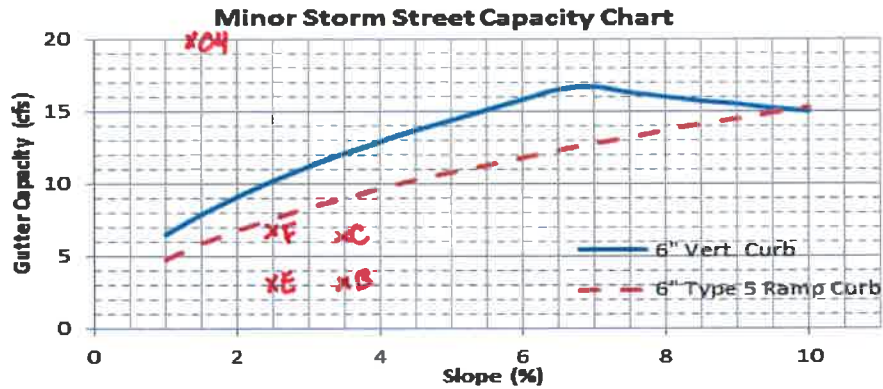
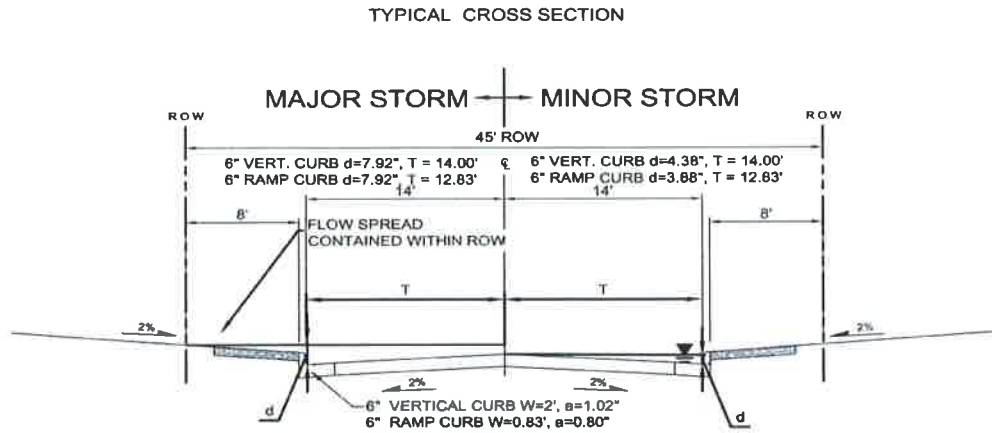
Input Data

Mannings Coeffic	0.030
Slope	020000 ft/ft
Left Side Slope	0.15 V : H
Right Side Slope	0.25 V : H
Bottom Width	4.00 ft
Discharge	3.90 cfs

Results

Depth	0.28 ft
Flow Area	1.5 ft ²
Wetted Perim	7.04 ft
Top Width	6.98 ft
Critical Depth	0.27 ft
Critical Slope	0.022123 ft/ft
Velocity	2.54 ft/s
Velocity Head	0.10 ft
Specific Enerç	0.38 ft
Froude Numb	0.95
Flow Type	Subcritical

Figure 7-9. Street Capacity Charts Minor Residential (Attached Sidewalk)



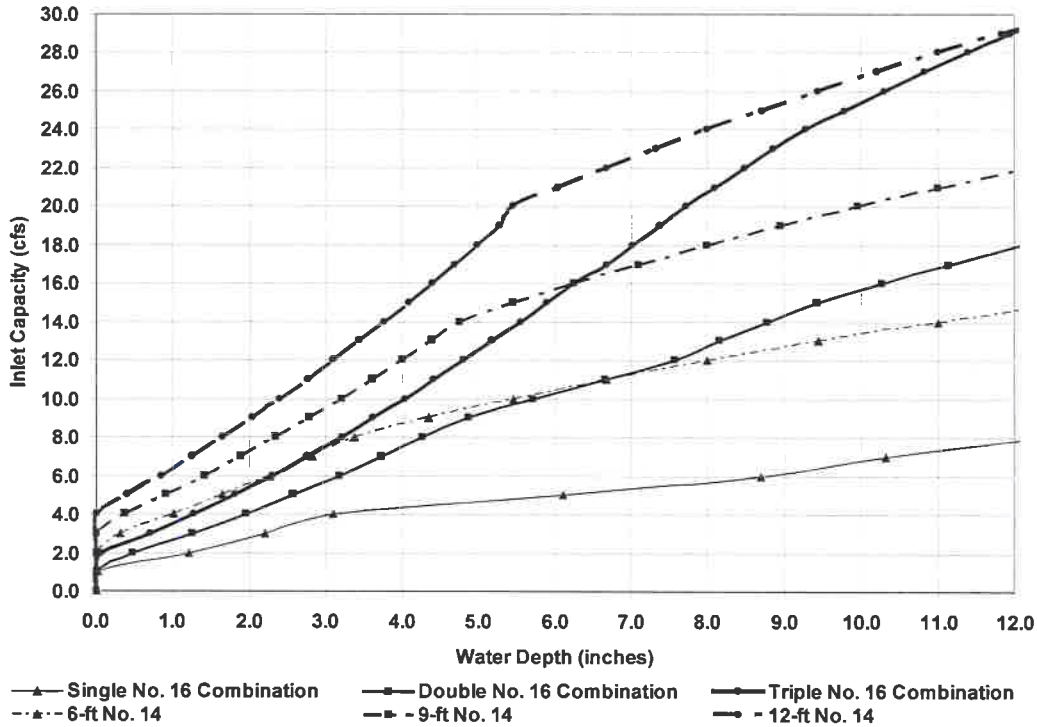
provide key/legend for these. Do they represent basins, DP's, or specific streets? And is this existing conditions or proposed?

These charts shall only be used for the standard street sections as shown. The capacity shown is based on 1/2 the street section as calculated by the UD-Inlet spreadsheets. Minor storm capacities are based on no crown overtopping, curb height or maximum allowable spread widths. Major storm capacities are based on flow being contained within the public right-of-way, including conveyance capacity behind the curb. The UDFCD Safety Reduction Factor was applied. An 'n_{STREET}' of 0.016 and 'n_{BACK}' of 0.020 was used. Calculations were done using UD-Inlet 3.00.xls, March, 2011.

Figure 8.1. Allowable Inlet Capacity— Sump Conditions

Note: See Section 8.3.2 for assumptions.

Type 16 and Type 14 Inlets for Sump Conditions



DL-1: Q₁₀₀ = 71.0 cfs → Double Type D inlet

Allowable Inlet Capacity for Type C and D Inlets for Sump Conditions

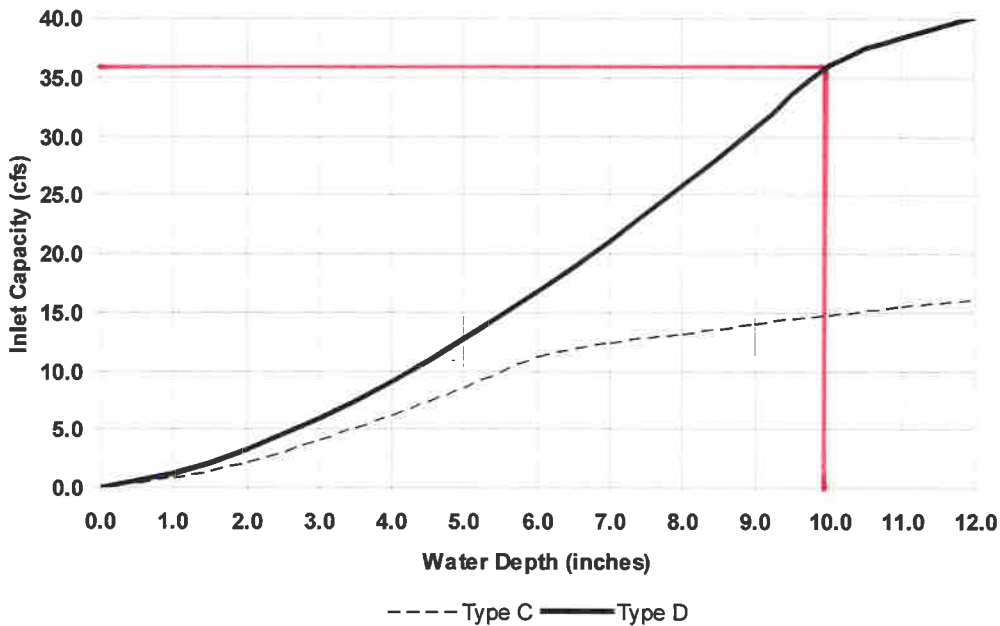
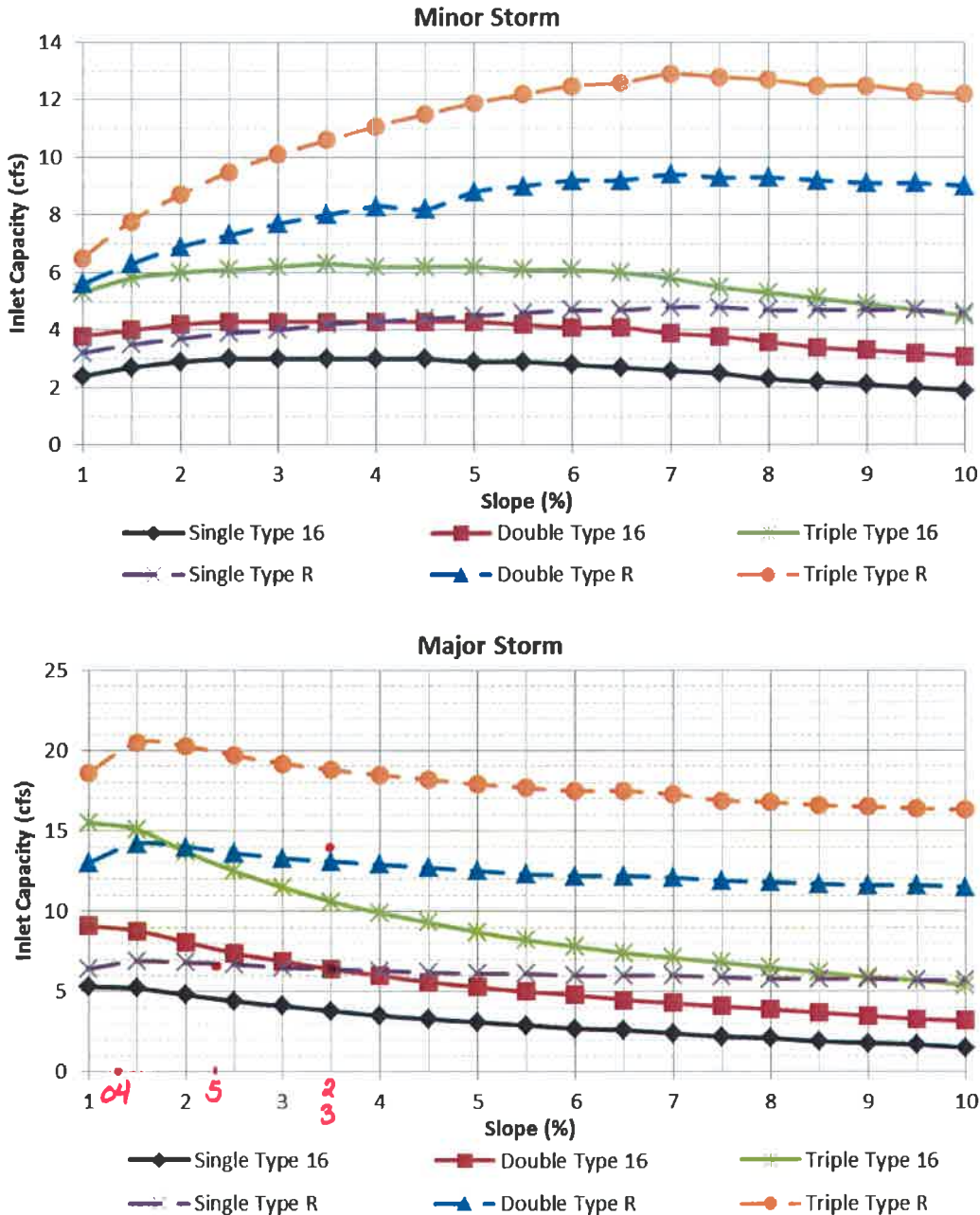


Figure 8-9. Inlet Capacity Chart Continuous Grade Conditions, Minor Residential (Local) (Attached Sidewalk)

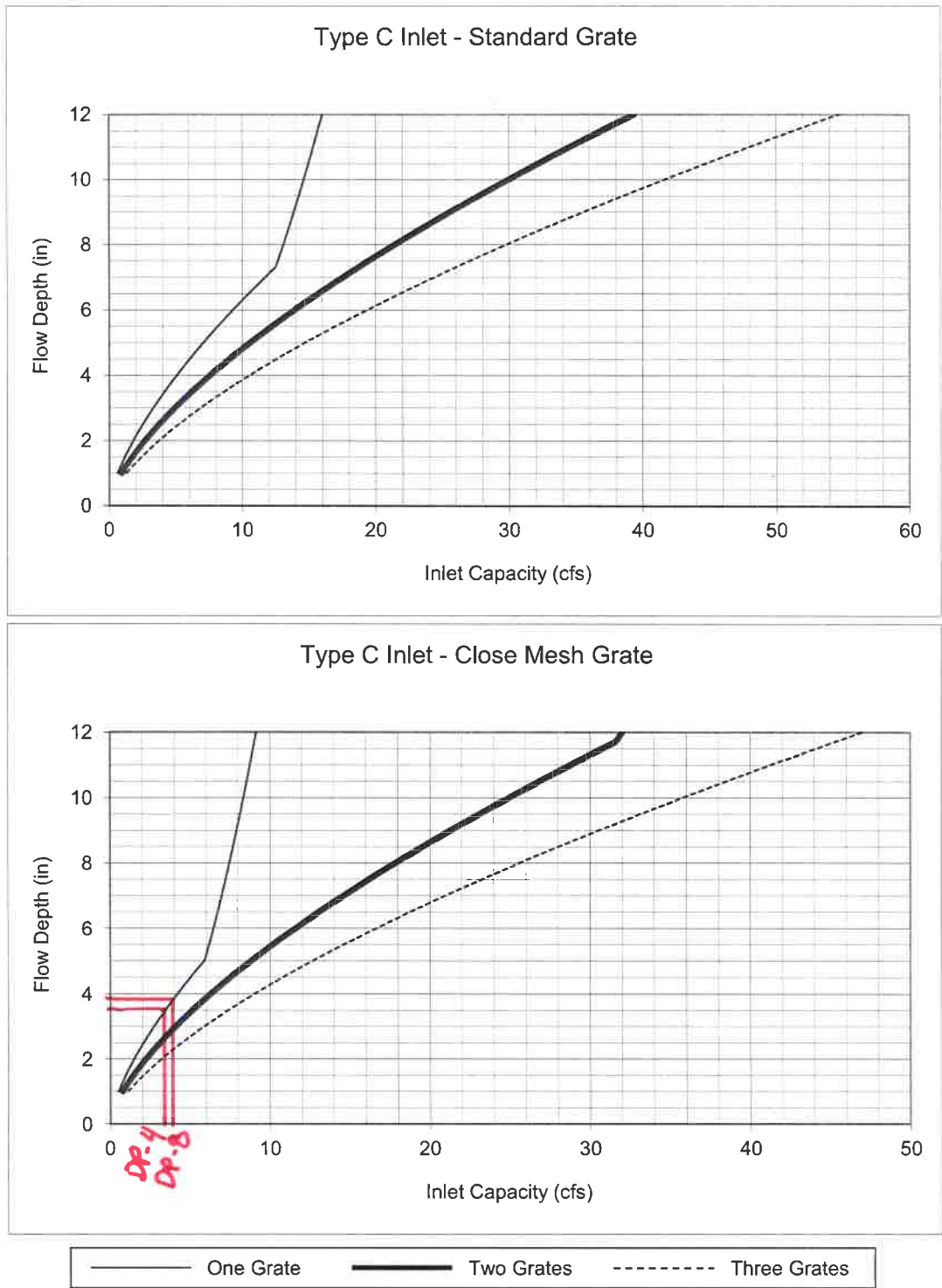
Street Section Data: Street Width Flowline to Flowline = 28'
Type of Curb and Gutter = 6" vertical



DL-2: Q₁₀₀ = 6.6 cfs → Single Type R
 DL-3: Q₁₀₀ = 14.0 cfs → Triple Type R
 DL-5: Q₁₀₀ = 6.7 cfs → Single Type R
 DP-04: Q₁₀₀ = 41.1 cfs → Triple Type R

The standard street section parameters as defined in Chapter 7 must apply to use these charts. For non-standard sections, the inlet capacity shall be calculated using the UDFCD spreadsheets. The maximum spread width is limited by the curb height based on no curb overtopping during a minor storm and flow being contained within the public right-of-way during the major storm. Calculations were done using UD-Inlet 3.00.xls, Mar., 2011 with the default clogging factors.

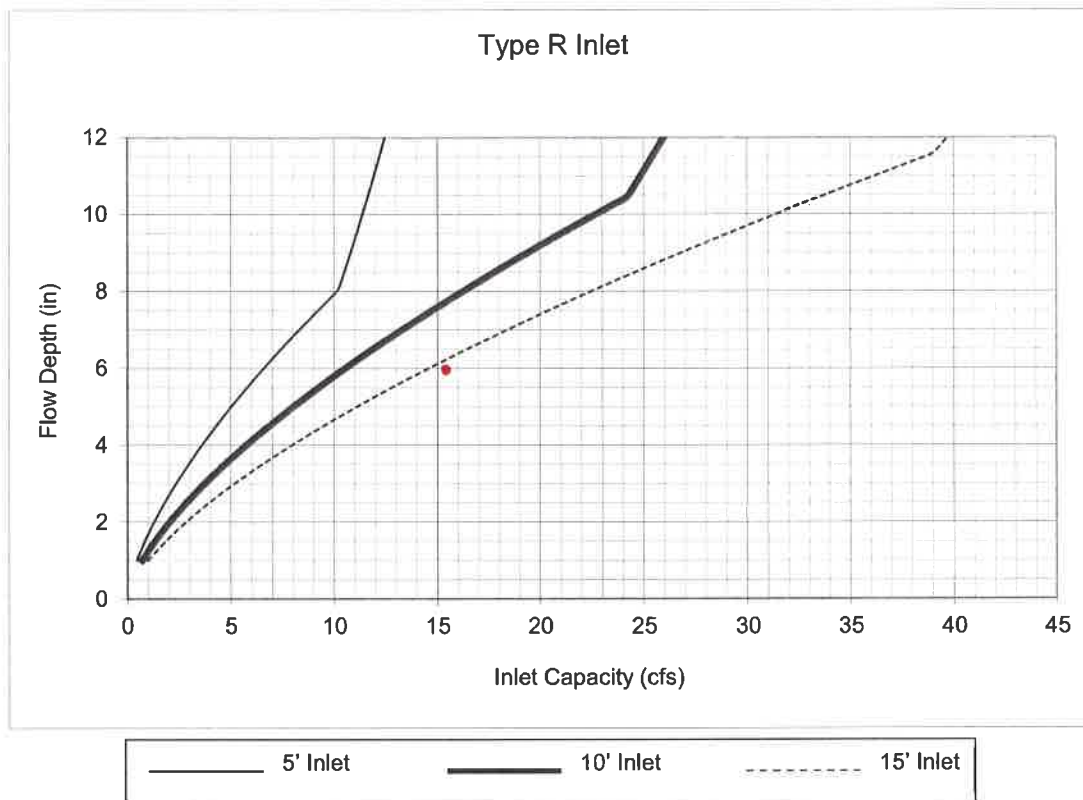
Figure 8-10. Inlet Capacity Chart Sump Conditions, Area (Type C) Inlet



Notes:

1. The standard inlet parameters must apply to use these charts.

Figure 8-11. Inlet Capacity Chart Sump Conditions , Curb Opening (Type R) Inlet



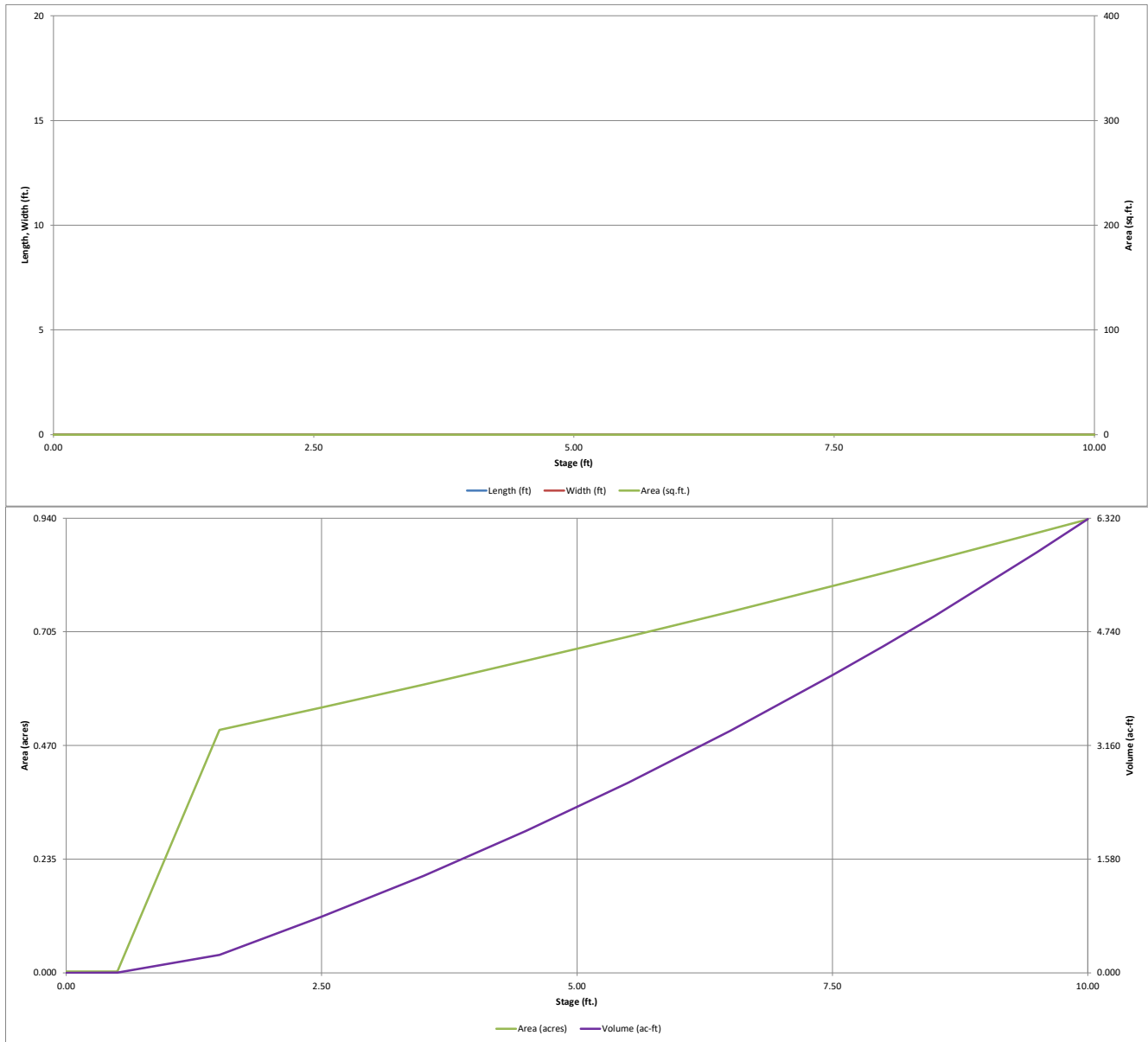
DP-6: $Q_{100} = 15.3 \text{ cfs} \rightarrow 15' \text{ inlet}$

Notes:

1. The standard inlet parameters must apply to use this chart.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

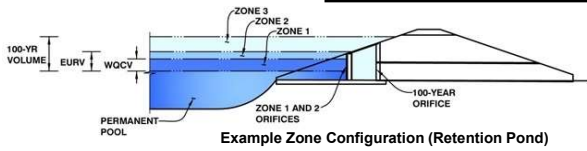


Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Haven Valley**

Basin ID: _____



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.53	0.791	Orifice Plate
Zone 2 (EURV)	5.84	2.087	Orifice Plate
Zone 3 (100-year)	7.84	1.531	Weir&Pipe (Restrict)
		4.409	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	6.00	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	27.00	inches
Orifice Plate: Orifice Area per Row =	5.22	sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row =	3.625E-02	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.00	4.00					
Orifice Area (sq. inches)	5.22	5.22	5.22					
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice

	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft ²
Vertical Orifice Centroid =	N/A	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	% , grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H _c =	6.90	N/A	feet
Over Flow Weir Slope Length =	4.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	9.69	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	11.20	N/A	ft ²
Overflow Grate Open Area w/ Debris =	5.60	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	11.20		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.16	N/A	ft ²
Outlet Orifice Centroid =	0.53	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.82	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	8.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	30.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.94	feet
Stage at Top of Freeboard =	9.94	feet
Basin Area at Top of Freeboard =	0.93	acres

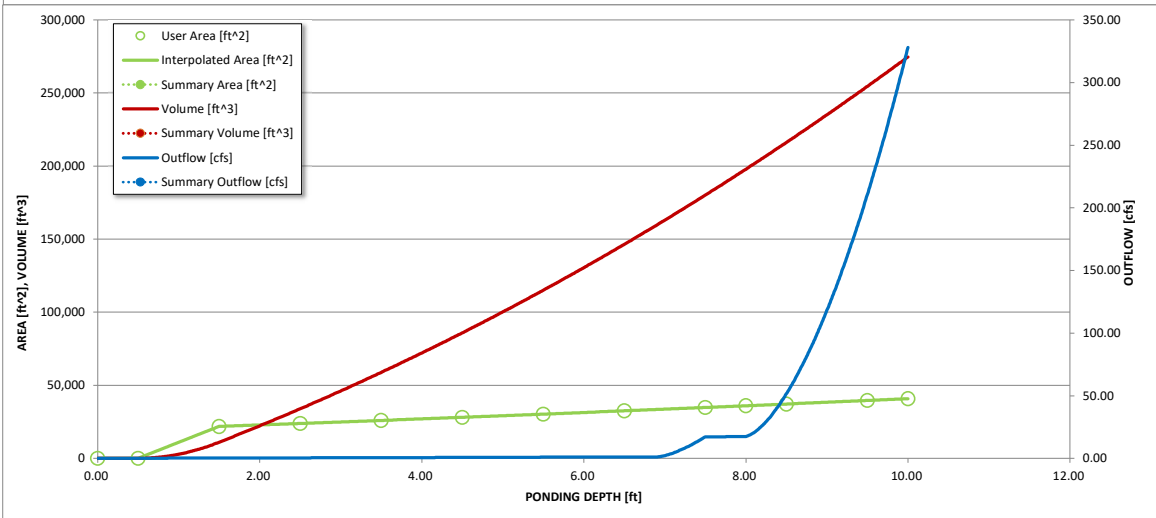
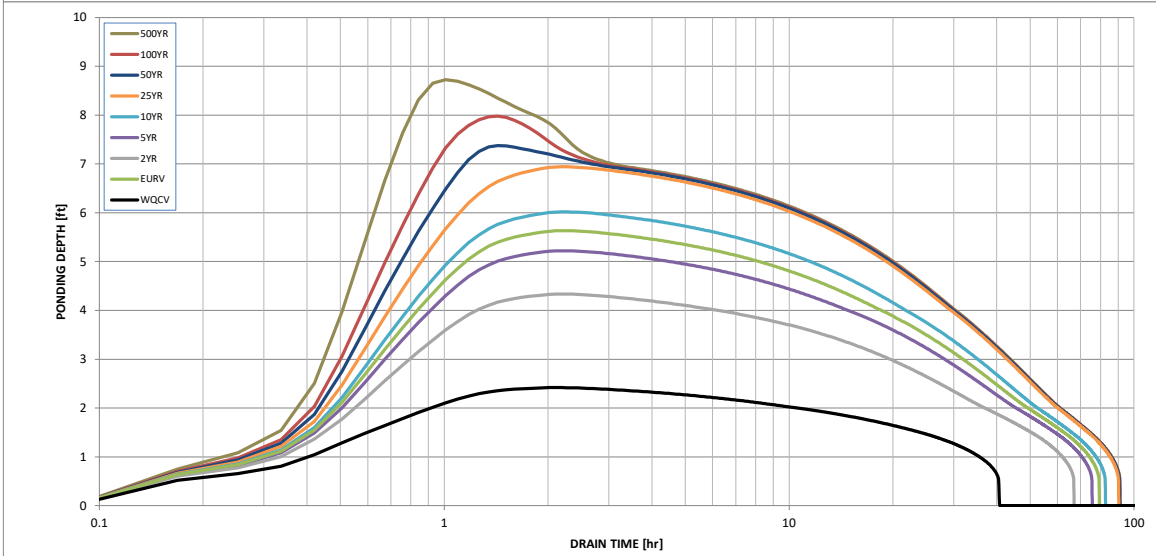
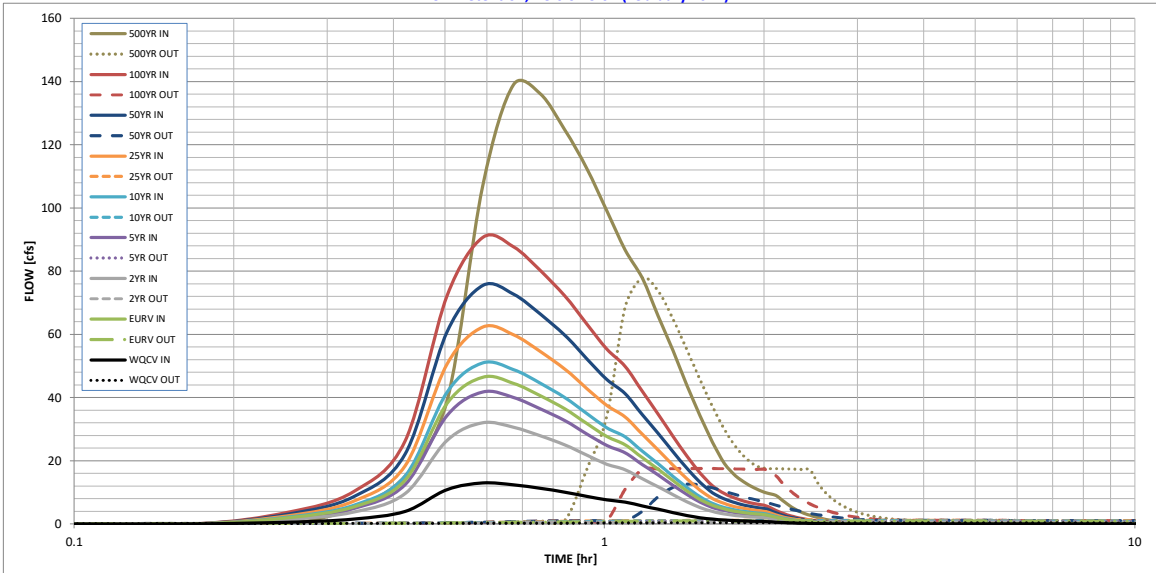
Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.49
Calculated Runoff Volume (acre-ft) =	0.791	2.878	1.972	2.583	3.161	3.877	4.717	5.696	8.827
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.791	2.877	1.971	2.582	3.161	3.876	4.716	5.691	8.825
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.00	0.01	0.01	0.03	0.19	0.47	1.18
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.2	0.5	1.1	8.0	19.5	49.0
Peak Inflow Q (cfs) =	13.0	46.4	32.0	41.7	50.3	64.3	75.5	90.7	139.0
Peak Outflow Q (cfs) =	0.4	1.0	0.7	0.9	1.0	1.4	12.6	17.6	77.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	4.3	2.1	1.3	1.6	0.9	1.6
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Overflow Gate 1	Overflow Gate 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.0	1.0	1.5	1.5
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	73	63	70	76	82	81	79	74
Time to Drain 99% of Inflow Volume (hours) =	40	77	65	74	80	87	87	87	85
Maximum Ponding Depth (ft) =	2.42	5.63	4.34	5.22	6.02	6.94	7.38	7.98	8.72
Maximum Volume Storage (acre-ft) =	0.730	2.732	0.64	0.68	0.72	0.77	0.79	0.82	0.87
Maximum Volume Storage (acre-ft) =	0.730	2.732	1.863	2.449	3.003	3.696	4.032	4.517	5.151

The small decimal differences may be acceptable but the 50yr storm should be adjusted. At this preliminary plan stage this can move forward but shall be revisited at the final drainage report stage. Consider using the latest UD detention sheet as I have heard it may yield better results.

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override

	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

TOTAL FOREBAY VOLUME

$$V = 3\% \times WQCV$$

$$WQCV = 0.92 \text{ ac-ft}$$

$$V = 0.0276 \text{ ac-ft}$$

$$Q_{in \text{ NE}} = 75.3 \text{ cfs}$$

$$Q_{in \text{ E}} = 42.4 \text{ cfs}$$

$$Q_{total} = 117.7 \text{ cfs}$$

NORTHEAST FOREBAY VOLUME

$$\frac{75.3 \text{ cfs}}{117.7 \text{ cfs}} = \frac{x \text{ ac-ft}}{0.0276 \text{ ac-ft}}$$

$$x = 0.0177 \text{ ac-ft}$$

$$= 769.2 \text{ ft}^3$$

FOREBAY RELEASE NOTCH WIDTH

$$Q = CLH^{2/3}$$

$$Q_{100} = 75.3 \text{ cfs}$$

$$2\% \text{ of } Q = 1.51 \text{ cfs}$$

$$C = 2.6$$

$$H \text{ (height of forebay wall)} = 1 \text{ ft}$$

$$L = 7.0 \text{ in}$$

EAST FOREBAY VOLUME

$$\frac{42.4 \text{ cfs}}{117.7 \text{ cfs}} = \frac{x \text{ ac-ft}}{0.0276 \text{ ac-ft}}$$

$$x = 0.0099 \text{ ac-ft}$$

$$= 433.1 \text{ ft}^3$$

FOREBAY RELEASE NOTCH WIDTH

$$Q = CLH^{2/3}$$

$$Q_{100} = 42.4 \text{ cfs}$$

$$2\% \text{ of } Q = 0.85 \text{ cfs}$$

$$C = 2.6$$

$$H \text{ (height of forebay wall)} = 1 \text{ ft}$$

$$L = 4 \text{ in}$$

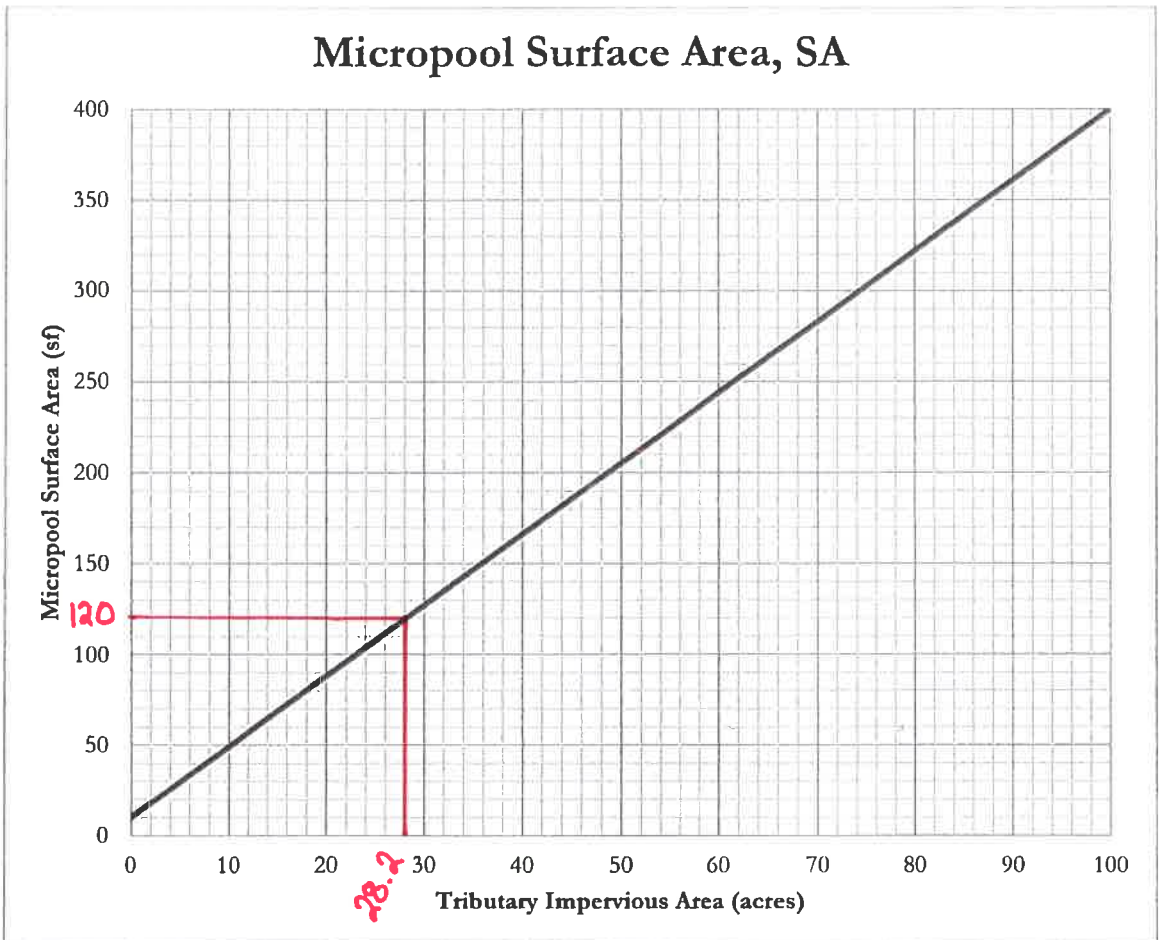


Figure 1 – Micropool surface area (SA) determination chart

The tributary impervious area is the effective number of impervious acres that will be treated by the extended detention basin (EDB). It is calculated by multiplying the tributary area to be treated by the impervious fraction of that area.

$$TIA = I \times A$$

$\frac{68}{100} \times 41.47 = 28.2 \text{ ac}$

TIA = Tributary impervious area (acres)
I = Imperviousness (fraction)
A = Tributary catchment area upstream (acres)

For EDBs with tributary impervious areas greater than 100 acres, the micropool surface area is 400 sf. The initial surcharge depth (ISD) is defined as the depth of the initial surcharge volume (ISV). The surface area determined using Figure 1 assumes an ISD of 4 inches. The initial surcharge volume is thus calculated by multiplying the micropool surface area by 4 inches.

$$ISV = SA \times 4 \text{ inches}$$

ISV = Initial surcharge volume (cf)
SA = Surface area (from Figure 1, sf)

PREPARED BY:



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(719)260-0887
BOULDER • COLORADO SPRINGS • GREELEY

CLIENT:



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DENVER, CO 80237
CONTACT: MATTHEW JENKINS
(720) 977-3686

DRAINAGE PLANS FOR:

HAVEN VALLEY

(LETA DR.) BRADLEY RD/ALTURAS DR.
SECURITY, EL PASO COUNTY, COLORADO

ISSUE DATE

INITIAL ISSUE 4/29/21
LATEST ISSUE 8/19/21

DESIGNED BY: TDM

DRAWN BY: GES

CHECKED BY: TDM

FILE NAME: 21085-03DR01

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO.

DRAWING SCALE:
HORIZONTAL: 1" = 100'
VERTICAL: N/A

EXISTING CONDITIONS
DRAINAGE PLAN

PROJECT NO. 21085-03CSCV
DRAWING NO.

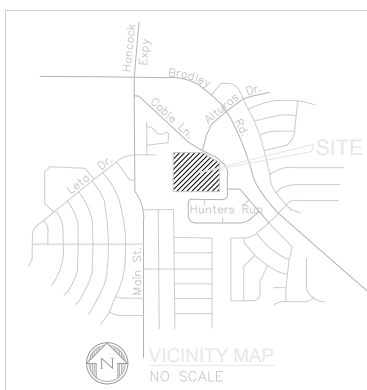
DR01

SHEET: 1 OF 3

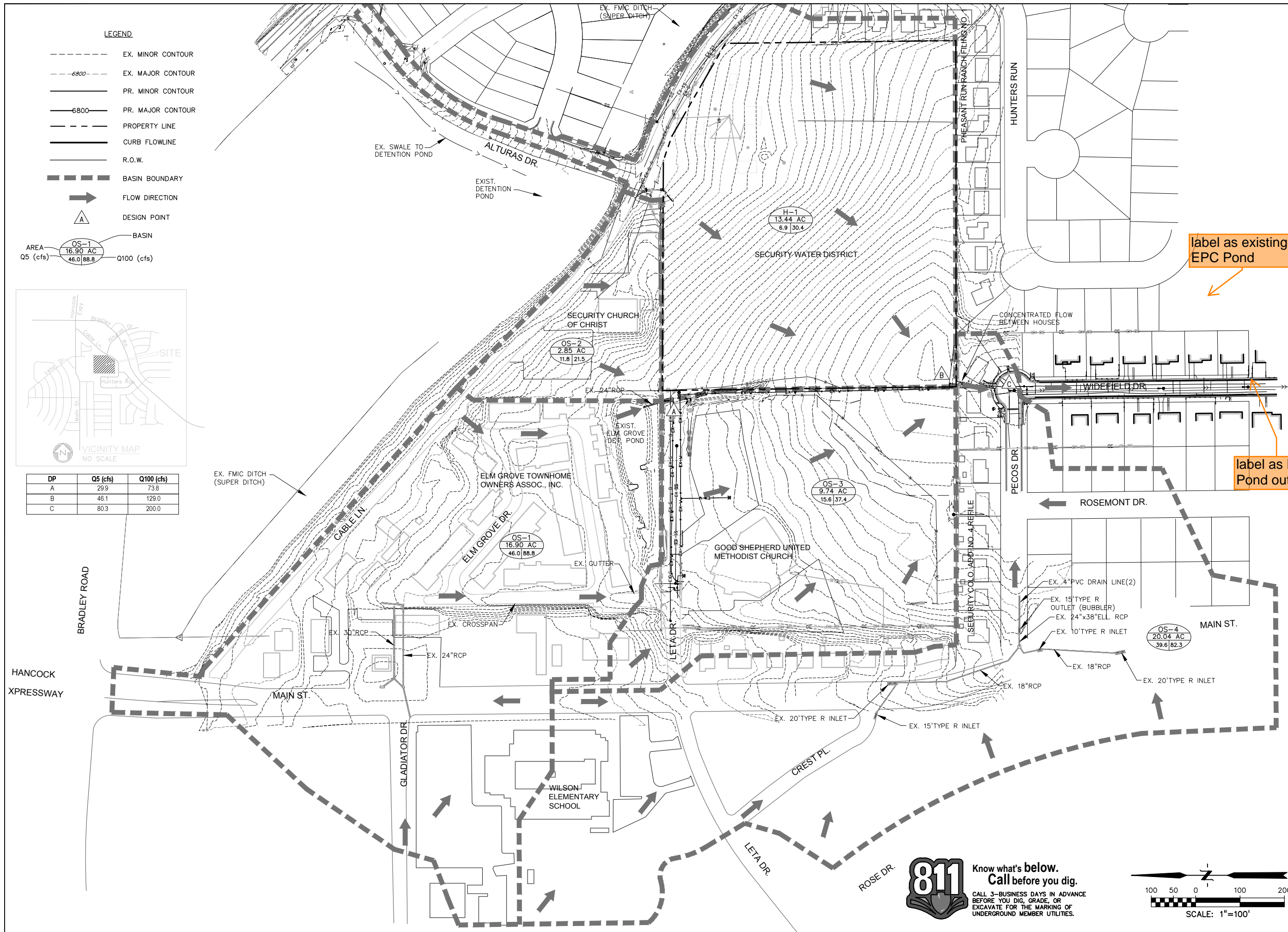
LEGEND

- EX. MINOR CONTOUR
- - - - - EX. MAJOR CONTOUR
- PR. MINOR CONTOUR
- - - - - PR. MAJOR CONTOUR
- PROPERTY LINE
- CURB FLOWLINE
- R.O.W.
- BASIN BOUNDARY
- FLOW DIRECTION
- ▲ DESIGN POINT

BASIN
AREA OS-1
Q5 (cfs) 16.90 AC 46.0 | 88.8
Q100 (cfs)



DP	Q5 (cfs)	Q100 (cfs)
A	29.9	73.8
B	46.1	129.0
C	80.3	200.0

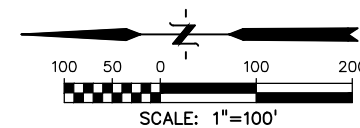


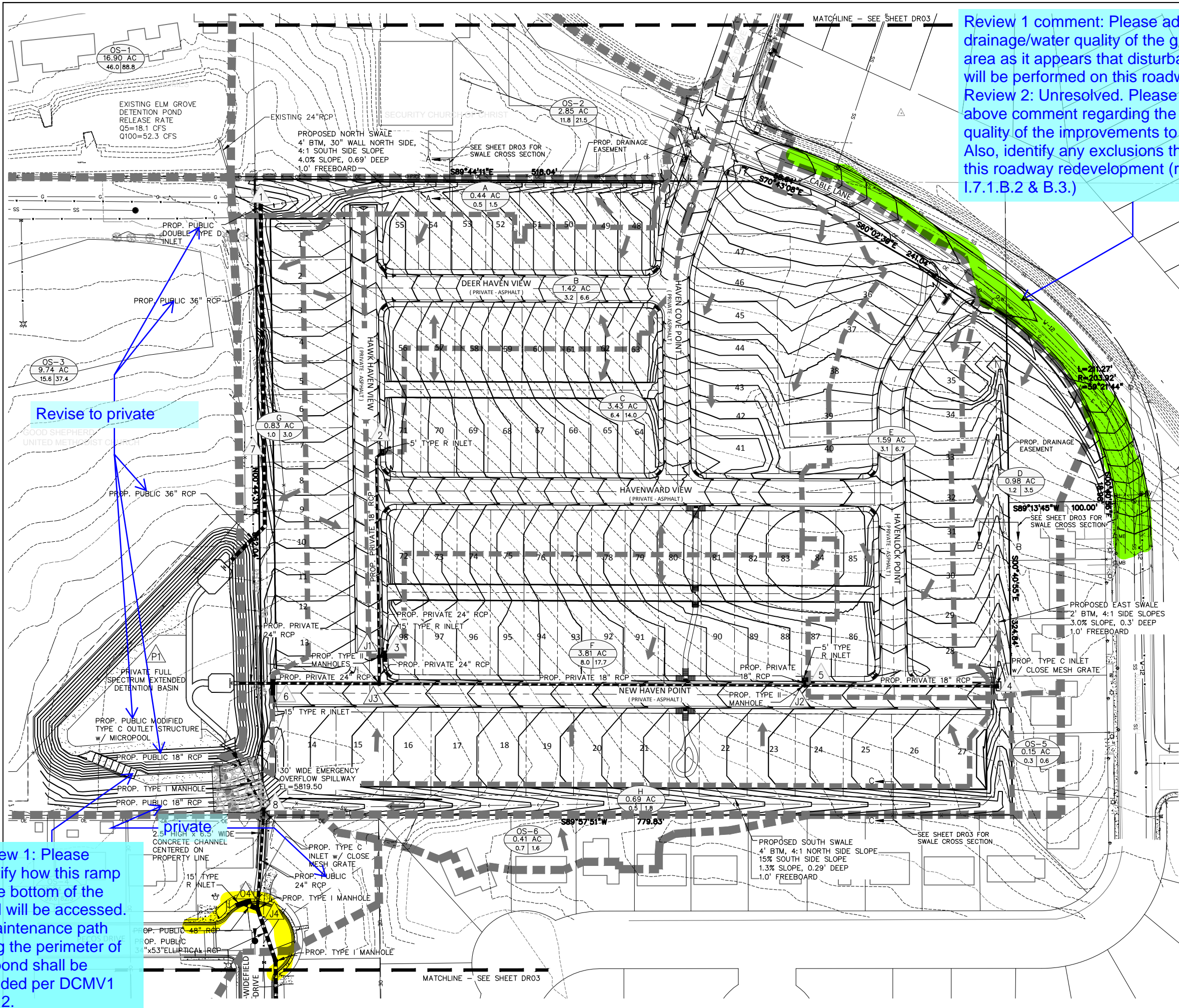
label as existing EPC Pond

label as EPC Pond outfall



Know what's below.
Call before you dig.
CALL 3-BUSINESS DAYS IN ADVANCE BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND MEMBER UTILITIES.



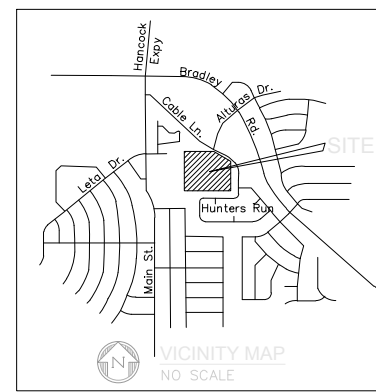
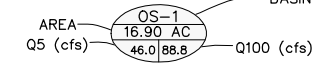


Review 1 comment: Please address the drainage/water quality of the green highlighted area as it appears that disturbance/construction will be performed on this roadway.
 Review 2: Unresolved. Please address the above comment regarding the drainage/water quality of the improvements to Cable Ln.
 Also, identify any exclusions that may apply to this roadway redevelopment (refer to ECM I.7.1.B.2 & B.3.)

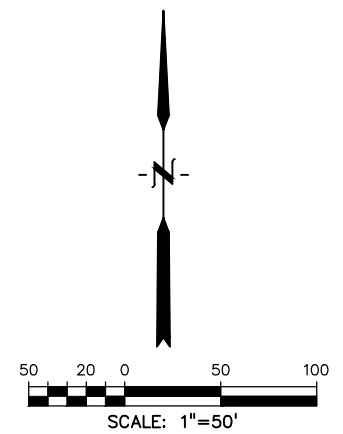
Revise to private

Review 1: Please identify how this ramp to the bottom of the pond will be accessed. A maintenance path along the perimeter of the pond shall be provided per DCMV1 11.2.2.
 Review 2: Unresolved.

- LEGEND
- EX. MINOR CONTOUR
 - EX. MAJOR CONTOUR
 - PR. MINOR CONTOUR
 - PR. MAJOR CONTOUR
 - PROPERTY LINE
 - CURB FLOWLINE
 - R.O.W.
 - BASIN BOUNDARY
 - FLOW DIRECTION
 - DESIGN POINT
 - BASIN



DP	Q5 (cfs)	Q100 (cfs)
1	28.1	71.0
2	3.2	6.6
3	6.4	14.0
J1	9.5	20.3
4	1.2	3.5
5	3.1	6.7
J2	4.3	10.0
J3	13.5	29.8
6	20.1	44.4
7	1.0	3.1
P1	64.0	154.1
8	2.3	21.5
O4	39.6	82.3
J4	41.9	103.8



811 Know what's below. Call before you dig.
 CALL 3-BUSINESS DAYS IN ADVANCE BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND MEMBER UTILITIES.

PREPARED BY:

 DREXEL, BARRELL & CO.
 Engineers-Surveyors
 3 SOUTH 7TH STREET
 COLORADO SPGS, COLORADO 80905
 CONTACT: TIM D. MCCONNELL, P.E. (719)260-0887
 BOULDER • COLORADO SPRINGS • GREELEY

CLIENT:

 RICHMOND AMERICAN HOMES
 4350 S. MONACO ST.
 DENVER, CO 80237
 CONTACT: MATTHEW JENKINS (720) 977-3686

DRAINAGE PLANS FOR:
HAVEN VALLEY
 (LETA DR.) BRADLEY RD/ALTURAS DR.
 SECURITY, EL PASO COUNTY, COLORADO

ISSUE	DATE
INITIAL ISSUE	4/29/21
LATEST ISSUE	8/19/21

DESIGNED BY: TDM
 DRAWN BY: SBN
 CHECKED BY: TDM
 FILE NAME: 21085-03DR02

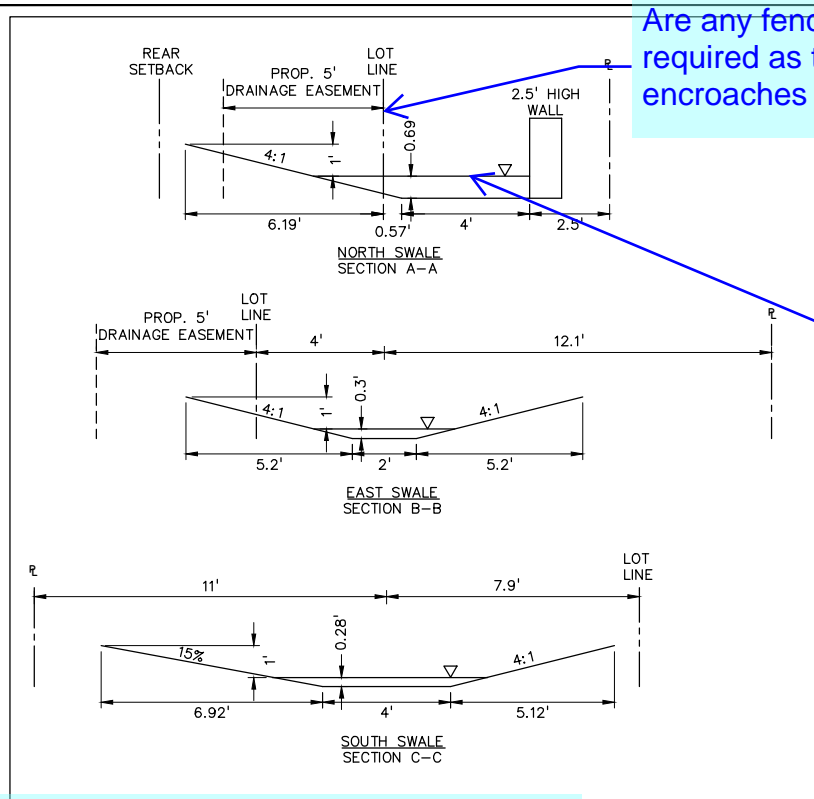
PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO.
 DRAWING SCALE:
 HORIZONTAL: 1" = 50'
 VERTICAL: N/A

PROPOSED CONDITIONS
 DRAINAGE PLAN

PROJECT NO. 21085-03CSCV
 DRAWING NO.

DR02

SHEET: 2 OF 3



Are any fence restrictions required as the 100yr wse encroaches into the lots?

Please label the 100 yr water surface elevation on these sections

After discussion with staff (including the County Engineer) there are concerns that the increase in stormwater volume due to this development may further exacerbate the drainage problems downstream of the site. Please analyze to the next man-made outfall which appears to be at the intersection of Main St and Marquette (Please verify).

label basins and show flow arrows

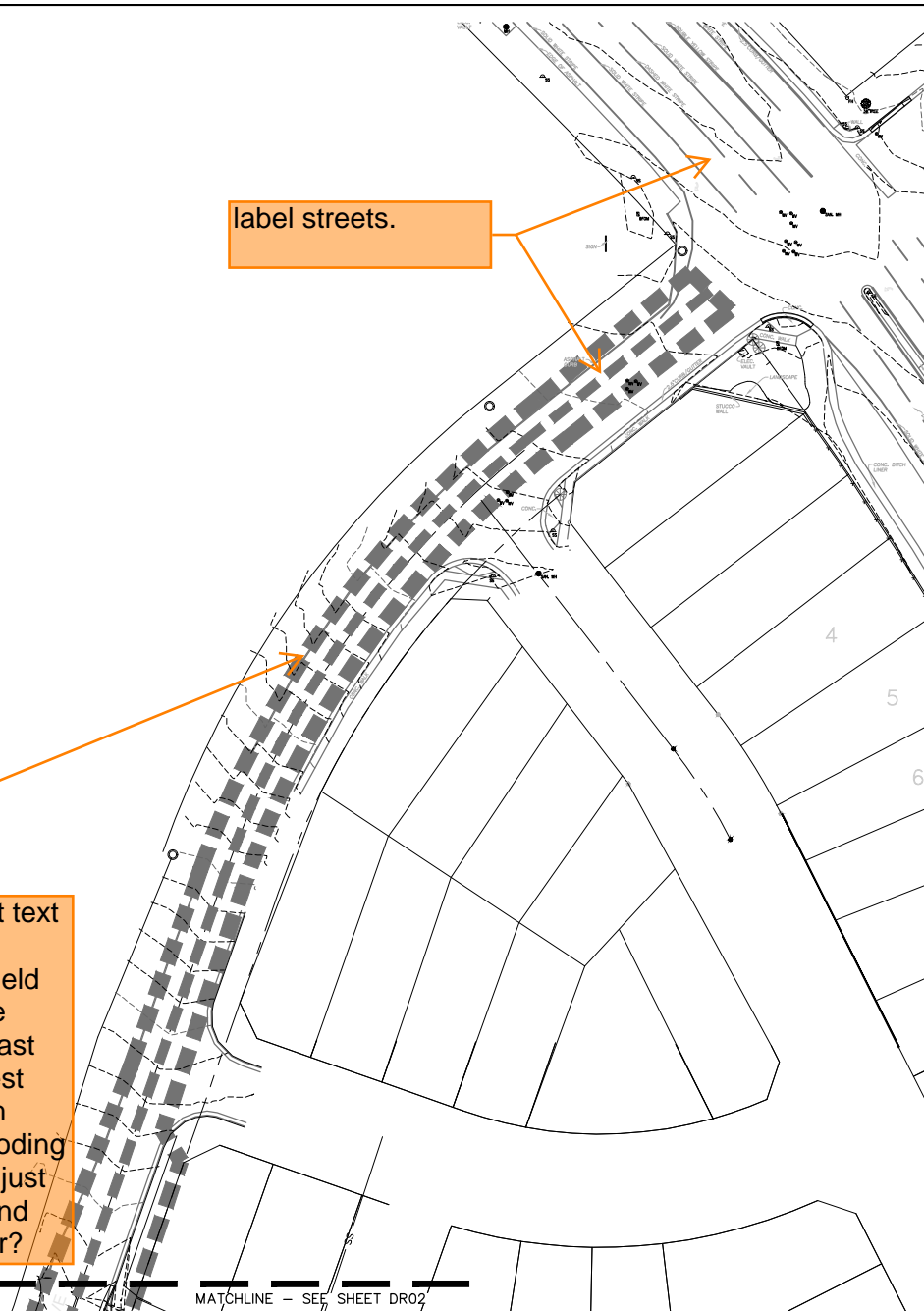
Please also address in the report text the possibility of flooding at the homes on the east side of Widefield Dr, adjacent to the bubbler, since there will be more flows on the east side of the street, than on the west side. Do the homes have enough elevation such that instead of flooding the homes, the excess flows will just overtop the crown of the street and continue down the western gutter?

label street.

Does the outfall from Haven Valley area currently only convey down the east side of Widefield? Because if not, this could effect the outfall of the EPC pond if there is now more water on the east side than before. See my comment in the report above on pages 4 and 5. Discuss in Section 5.0 above.

label as existing EPC pond

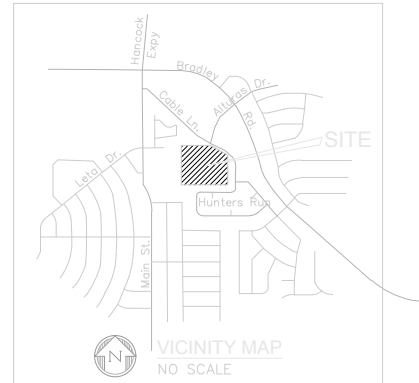
Show existing outlet from EPC pond and discuss effects of the proposed conditions on this outlet. We do not want the pond backing up. In the report text above, address this potential issue and how impacts have been mitigated. This is part of showing that there is a suitable outfall for this site.



label streets.

LEGEND

- - - - - EX. MINOR CONTOUR
- 6800--- EX. MAJOR CONTOUR
- PR. MINOR CONTOUR
- 6800———— PR. MAJOR CONTOUR
- PROPERTY LINE
- CURB FLOWLINE
- R.O.W.
- BASIN BOUNDARY
- ➔ FLOW DIRECTION
- △ DESIGN POINT
- BASIN
- OS-1 16.90 AC
- Q5 (cfs) 46.0
- Q100 (cfs) 88.8



PREPARED BY:

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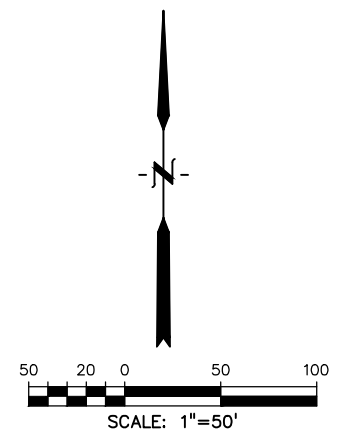
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DRAWING SCALE:
HORIZONTAL: 1" = 50'
VERTICAL: N/A

PROPOSED
CONDITIONS
DRAINAGE PLAN
PROJECT NO. 21085-03CSCV
DRAWING NO.

DR03

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