PRELIMINARY DRAINAGE REPORT for HAVEN VALLEY

El Paso County, Colorado

February 2022

EL PASO COUNTY PCD FILE NO. PUDSP-21-007

Prepared for:

Richmond American Homes

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Prepared by:

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PRELIMINARY DRAINAGE REPORT

for HAVEN VALLEY

Security, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E. Colorado P.E. License No. 33797 For and on Behalf of Drexel, Barrell & Co.

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name:

Richmond American Homes

By:

Title: Address: Matthew Jenkins Director, Land Acquisition 4350 S. Monaco Street Denver, CO 80237 Date

Date

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. County Engineer/ECM Administrator CONDITIONS: Date

PRELIMINARY DRAINAGE REPORT

for HAVEN VALLEY Security, Colorado

2.0 PURPOSE

This report is prepared by Drexel, Barrell & Co in support of the Haven Valley in Security, CO. The purpose of this report is to identify onsite and offsite drainage patterns, storm sewer, inlet locations, and areas tributary to the site, and to safely route developed storm water runoff to adequate outfall facilities.

3.0 GENERAL SITE DESCRIPTION

<u>Location</u>

Haven Valley is a 11.768 acre subdivision within the northwest quarter of Section 12, Township 15 South, Range 66 West of the 6th Principle Meridian in El Paso County, Colorado. The site is located southwest of Cable Ln and west of Hunters Run. The site is bounded on the north by Calvary Fellowship Fountain Valley church and Cable Ln, the west by Good Shepherd United Methodist church, and the south and the east by residential subdivision Pheasant Run Ranch Filing No. 1. See Vicinity Map in Appendix.

Existing Site Conditions

The site is approximately 11.768 acres in size surrounded by existing development. There are no existing structures on the site, only native grasses, a few invasive trees and shrubs. There are no existing irrigation facilities on the project site. The project site slopes moderately from the northeast to southwest at approximately 5-7%. Existing drainage flows to the southwest where it drains overland between two houses to Pecos Drive, then south on Widefield Drive. Severe flooding has been observed between these two houses and one of the houses has experienced mold issues in the past.

Proposed Site Conditions

Haven Valley is a small lot single-family development, consisting of approximately 98 lots, streets, landscape areas and open space. A proposed full-spectrum detention pond is proposed to be constructed in an existing off-site drainage easement adjacent to the west side of the site. The flows will be released from the detention pond and be carried by pipe between the two houses and outlet via a bubbler in Widefield Drive. There is an existing drainage and utility easement located between the two houses.

<u>Soils</u>

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S. Department of Agriculture Soil Conservation Service, the site is underlain by the Blakeland loamy sand (Soil No. 8). This soil is a type 'A' hydrologic soil group. This type of soil

typically exhibits rapid infiltration rates and slow runoff characteristics with moderate erosion potential. See appendix for Soil Map.

<u>Climate</u>

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel 08041C0763G (December 7, 2018), the site does not lie within a designated 100-year floodplain. The site is in Zone X, an area of minimal flood hazard. See Appendix for FIRMette map.

Previous Drainage Studies

The site is located within the Security Drainage Basin, as studied in the Little Johnson/Security Drainage Basin Planning Study, prepared by Simons Li & Associates, Inc., 1987.

4.0 EXISTING CONDITIONS HYDROLOGY SUMMARY

Basin OS-1 is an offsite basin to the north. This basin drains the Elm Grove Subdivision (town homes, age restricted) and several commercial buildings on the east side of Main St. and the Wilson Elementary School on the west side of Main St. The runoff path begins on Main Street near the intersection of Bradley Road, then flows southerly down Main Street via curb and gutter. The runoff at this intersection is collected by a storm sewer constructed as part of the 1993 Main Street reconstruction by El Paso County. The storm drain system conveys runoff east underground via storm sewer and discharges in to a valley gutter within the Elm Grove Subdivision. The valley gutter drains south to an existing detention pond (roughly 3-4' deep) where it is detained slightly. The pond discharges via a 24" CMP to the south. The 24" CMP is undersized for the 100-year which overtops the pond and drains into a swale which in turn drains south overland between two houses in the Security Colorado Addition 4, then south to the curb and gutter in Pecos Drive and Widefield Drive. The runoff generated by Basin OS1 is calculated to be 46.0 cfs and 88.8 cfs for the 5-year and 100-year storm respectively into the detention pond. After detention, the pond outflows are 18.1 cfs and 52.3 cfs respectively for the 5-year and 100year storms.

Basin OS-2 is an offsite basin to the north of the site. Runoff from this basin is primarily generated from roof, parking lot and vacant land. The runoff path begins on Cable Lane and generally flows southerly along the west property line until it reaches Design Point A. Design Point A collects the flow from Basin OS2 and the release from the detention pond in Basin OS1. This flow is routed southerly through a small swale that divides Basins OS3

and H1. The calculated runoff from Basin OS2 is 11.8 cfs and 21.5 cfs for the 5-year and 100-year storm respectively.

Design Point A. The drainage swale previously mentioned conveys the flow from Design Point A to Design Point B. The calculated flow at Design Point A is 29.9 cfs and 73.8 cfs for the 5-year and 100-year storm respectively. This flow includes detained flow from the Elm Grove pond and from Basin OS-2 which is conveyed south in an existing swale to a historic low point just north of Security Colorado Addn. No. 4 (Des. Pt. B).

Basin OS-3 is an offsite basin to the west of the site. Runoff from this basin is generated from roof, street, parking lot and vacant land. The runoff path flows southerly down Main Street via curb and gutter and then easterly onto Leta Drive. The flow then continues south through a parking lot until it empties onto vacant land, then travels to the southeast to Design Point B. Design Point B collects the flow from all basins; OS1, OS2, OS3 and H1 and drains them overland between two houses in the Security Colorado Addition 4, then south to the curb and gutter in Pecos Drive and Widefield Drive. Severe flooding between these houses has been observed on numerous occasions in the past. The calculated runoff from Basin OS3 is 15.6 cfs and 37.4 cfs for the 5-year and 100-year storm respectively.

Basin H-1 is an onsite basin which drains the site plus street runoff from Alturas Drive and Cable Lane. The east half of Alturas Drive drains is not included in this basin which drains overland eastward into the Windmill Creek Subdivision per the approved drainage report by Jefferies Engineering, October 10, 2001. Runoff from the undeveloped lot west of Alturas Drive is currently collected in a swale west of the ROW and directed south into a detention pond which outlets into the FMIC superditch. Future conditions for this undeveloped lot will need to remain the same as existing since additional runoff down Alturas would severely affect downstream properties. Runoff from Alturas Drive is included in this basin per existing conditions. The runoff path for Basin H1 begins near the intersection of Alturas Drive and Bradley Road (west half), and then flows southwesterly via an asphalt curb southward and over the top of the FMIC superditch. The flow then crosses Cable Lane and generally flows southwesterly through vacant land to Design Point B. The calculated runoff for Basin H1 is 6.9 cfs and 30.4 cfs for the 5-year and 100-year storm respectively.

Design Point B includes flow from Design Point A, Basin OS-3, and H-1. Design Point B discharges through the Security Colorado Addition No. 4 Refile Subdivision overland between two houses, then to the curb and gutter on the north side of Pecos Drive and the east side of Widefield Drive. The total flow at Design Point B is 46.1 cfs and 129.0 cfs for the 5-year and 100-year storm respectively between the two houses. Both of these two homeowners have indicated that they have experienced severe flooding of the backyard and crawl spaces of their homes.

Basin OS-4 is an offsite basin to the west of the site including Main Street and a portion of land west of Main Street. Runoff from this basin is generated from roof, street, and parking lot. The runoff path flows southerly down Main Street via curb and gutter to the intersection of Pecos Drive. An existing storm sewer system was constructed in 1993 as part of the 1993 Main Street reconstruction project by El Paso County. The storm system picks up street flow and discharges it to a 15' bubbler located just east of the intersection of Pecos Drive and Main Street. From the bubbler, all runoff is carried overland east to Widefield Drive (Design Pt C), then south on Widefield Drive via curb and gutter. There is no existing storm sewer system within Pecos or Widefield Drive. None of the storm infrastructure east of this bubbler or within Widefield Dr. shown on the DBPS were ever installed. The existing bubbler was not proposed in the DBPS. The calculated runoff from Basin OS4 is 39.6 cfs and 82.3 cfs for the 5-year and 100-year storm respectively. The existing street capacity of Widefield Drive as it flows south from Pecos Drive is 7 cfs and 41 cfs for the 5-year and 100-year storm respectively. As shown, the flow from this basin alone exceeds the street capacity of Widefield Drive. Therefore, the flows from Basin OS-4 are split between the curb and gutter on each side of the street.

Design Point C is located at the intersection of Pecos Drive and Widefield Drive and includes flow from Design Point B and Basin OS-4. At Design Point C the existing flow with detention from the Elm Grove pond is 80.3 cfs and 200.0 cfs for the 5-year and 100-year storms respectively, which is all overland flow. The existing street capacity of Widefield Drive as it flows south from Pecos Drive is approximately 7 cfs and 41 cfs for the 5-year and 100-year storm events respectively. As shown, the existing street capacity is severely exceeded in existing conditions which is echoed by the residents in this area experiencing chronic flooding at this intersection. This development is proposing to reduce the flooding issues in this area which will be discussed later in this report. Since street capacity is being exceeded, the flows at DP-C are split evenly on each side of the street. Each side of the street carries 40.1 cfs and 100.0 cfs for the 5-year and 100-year

storm respectively.

The way this is written, it seems like the street has the capacity for the listed flows. But in reality, I think you are trying to say that that is how much flow will go down each side of the street (but the street capacity will be exceeded). So clarify this by revising to something like: "The following flows will be conveyed to each side of the street...40.1 and 100.0....which will still exceed the capacity of the existing streets by XX cfs for 5-year and XX cfs for 100-yr." And then per the text I highlighted on Pg 11, discuss where/how these excess flows 5.0 PROPOSED HYDROLO will be conveyed. Via sidewalks and yards? I know the proposed flows are less than existing, but it's worth

documenting and accounting for all flows originating from the proposed site (and the other tributary basins) The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals. Urban Drainage UD-Detention and Flowmaster were used to determine pond and storm system sizing. UD-Inlet and UD-Sewer were also used to identify pond and storm system sizing (see appendix for calculations). See below for a summary runoff table of the basins and for descriptions of each design point. See appendix for Proposed Drainage Map showing the proposed drainage basin locations.

BASIN	AREA (AC)	Q5 (cfs)	Q100 (cfs)
А	0.44	0.5	1.5
OS-1	16.90	46.0	88.8
OS-2	2.85	11.8	21.5
В	1.42	3.2	6.6
С	3.43	6.4	14.0
D	0.98	1.2	3.5
E	3.09	6.4	14.0
F	0.69	1.4	3.1
G	1.61	2.8	6.2

Rational Method Runoff Summary

OS-3	9.74	15.6	37.4
Н	0.84	1.0	2.9
OS-4	20.04	39.6	82.3
OS-5	0.15	0.3	0.7
OS-6	0.41	0.9	2.0
I	0.69	0.6	2.2

Design Point 1 (DP-1) represents flows generated from existing Elm Grove pond release in offsite basin OS-1, as well as flows from offsite basin OS-2 and onsite Basin A. The flows are conveyed via a swale and are then captured by a proposed private Double Type D area inlet. The flows leave this inlet via a proposed private 36" RCP storm pipe and are conveyed to the proposed Extended Detention Basin to the south. The total flow at DP-1 is 28.1 cfs and 71.0 cfs for the 5-year and 100-year storm respectively. The Double Type D area inlet can capture all of the DP-1 flows.

Design Point 2 (DP-2) represents flows generated from onsite Basin B. The flows are captured by a proposed private at-grade 5' Type R inlet in Basin B. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried south to DP-J1. The total flow at DP-2 is 3.2 cfs and 6.6 cfs for the 5-year and 100-year storm respectively.

Design Point 3 (DP-3) represents flows generated from Basin C. The flows are captured by a proposed private at-grade 15' Type R inlet in Basin C. The flows leave this inlet via a proposed private 24" RCP storm pipe and are carried west to DP-J1. The total flow at DP-3 is 6.4 cfs and 14.0 cfs for the 5-year and 100-year storm respectively.

Design Point J1 (DP-J1) represents flows generated from Basins B and C. This design point is located at a proposed junction with a Type II manhole in Basin C. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried south to DP-J2. The total flow at DP-J1 is 9.5 cfs and 20.3 cfs for the 5-year and 100-year storm respectively.

Design Point 4 (DP-4) represents flows generated from Basin D. The flows are conveyed via a swale and are then captured by a proposed private sump condition Type C area inlet in Basin D. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried west to DP-J2. The total flow at DP-4 is 1.2 cfs and 3.5 cfs for the 5-year and 100-year storm respectively.

Design Point 5 (DP-5) represents flows generated from Basin E, which includes a portion of Cable Ln as shown on the proposed drainage map in the Appendix. This design point represents the flows at the intersection of New Haven Point and Hawk Haven View. The street capacity is sufficient at this point for these flows as can be seen in the street capacity charts included in the Appendix. These flows continue to the west where they are captured by the proposed inlet at DP-6. The total flow at DP-5 is 6.4 cfs and 14.0 cfs for the 5-year and 100-year storm respectively. Cable Lane is an existing public two-lane paved roadway. As part of this project, the roadway will be widened and curb and gutter added. Basin E will collect runoff from a portion the existing and proposed Cable Lane. The remainder of the roadway drainage will follow historic

patterns.

Design Point J2 (DP-J2) represents flows generated from Basins B, C and D. This design point is located at a proposed junction with a Type II manhole in Basin E. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried west to DP-J3. The total flow at DP-J2 is 10.6 cfs and 23.4 cfs for the 5-year and 100-year storm respectively.

Design Point 6 (DP-6) represents flows generated from Basin F. The flows are captured by a proposed private at-grade 15' Type R inlet in Basin F. The flows leave this inlet via a proposed private 24" RCP storm pipe and are carried south to DP-J3. The total flow at DP-6 is 7.7 cfs and 17.0 cfs for the 5-year and 100-year storm respectively.

Design Point J3 (DP-J3) represents flows generated from Basins B, C, D, E and F. This design point is located at a proposed junction with a Type II manhole in Basin G. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried west to DP-J4. The total flow at DP-J3 is 17.4 cfs and 38.4 cfs for the 5-year and 100-year storm respectively.

Design Point 7 (DP-7) represents flows generated from Basin G. The flows are captured by a proposed private sump 5' Type R inlet in Basin G. The flows leave this inlet via a proposed private 18" RCP storm pipe and are carried north to DP-J4. The total flow at DP-7 is 2.8 cfs and 6.2 cfs for the 5-year and 100-year storm respectively.

Design Point J4 (DP-J4) represents flows generated from Basins B, C, D, E, F and G. This design point is located at a proposed junction with a Type II manhole in Basin G. The flows leave this manhole via a proposed private 24" RCP storm pipe and are carried west to the proposed private full-spectrum Extended Detention Basin. The total flow at DP-J4 is 20.0 cfs and 44.1 cfs for the 5-year and 1 Label if inlet is public ely.

or private

Design Point 8 (DP-8) represents flows generated from Basin H only. The flows from the existing Elm Grove pond release are captured by the area inlet it Basin A as discussed under DP-1. The flows from Basin H are captured by a proposed swale and are carried to the proposed Extended Detention Basin. The total flow at DP-8 is 1.0 cfs and 2.9 cfs for the 5-year and 100-year storm respectively.

Design Point P1 (DP-P1) represents all of the flows generated from Basins OS-1, Exist. Elm Pond release and Basins A through G. These are all of the flows that are captured by the proposed Extended Detention Basin. Further detail is provided on the EDB in the following section of this report. The total flows at DP-P1 is 63.9 cfs and 153.8 cfs for the 5year and 100-year storm respectively.

Design Point 9 (DP-9) represents flows generated from Basin I, OS-5 and OS-6 combined with the released flows from the proposed EDB. The flows are conveyed via a swale and are then captured by a proposed private sump condition Type C area inlet in Basin I. The flows leave this inlet via a proposed public 24" RCP storm pipe and are carried south to DP-J5. This pipe system is identified as a public reimbursable facility in the DBPS. By piping these flows between the two houses, flooding for these two existing residences will be eliminated in this area. In the event of a storm event that overtops

Revise to "Basin I," to clarify that this statement is not including OS-5, and OS-6. But then add a statement saying that runoff from OS-5 and OS-6 is also will not be captured in the EDB, but is unnessary because they are offsite basins that will not mix with runoff that needs to be treated.

the EDB spillway, a concrete channel is proposed between the two existing residences to help prevent flooding. The concrete channel is to be 2.5' high x 6.5' wide and is directly over the 24" RCP pipe below. The total flow at DP-9 is 2.6 cfs and 22.6 cfs for the 5-year and 100-year storm respectively. This basin is not being captured for water quality control, however it is under 1 acre, which is acceptable per ECM Appendix 1.7.1.C.1.

Design Point O4 (DP-O4) represents flows generated from Basin OS-4. A proposed public at-grade 15' Type R inlet is to be installed on existing Pecos Dr/Widefield Dr. knuckle. This inlet will not be able to capture all of the flows generated from the existing basin but will capture some of the street flows and relieve some of the flooding experienced by the residents in this area. The total flow at DP-O4 is 39.6 cfs and 82.3 cfs for the 5-year and 100-year storms respectively. These flows are split between the curb and gutter on each side of the street due to the existing street capacity of Pecos Dr. and Widefield Dr., so the flows on the north side of Pecos Dr. approaching the proposed inlet are 19.8 cfs and 41.1 cfs for the 5-year and 100-year storm respectively. The proposed 15' Type R inlet can capture approximately 20 cfs of the 100-yr storm flows. The remaining approximate 21.1 cfs will continue to the south along the east curb and gutter of Widefield Drive along historic drainage routes as outlined in the DBPS. Per the 1/2 street section street capacity chart Figure 7-9, the street capacity of Pecos Dr. and Widefield Dr. is 7 cfs for the 5-year storm, and 41 cfs for the 100-yr storm. Therefore, the street capacity can handle the 100-yr flows, but not the 5-yr flows (the streets already cannot not handle the flows in the existing condition but we are reducing the total flows as noted below as well). The depth of gutter flow for the remaining 21.1 cfs is 0.44'. See street capacity charts and flow de Use MHFD UD-Inlet Version 5.01 to Appendix. determine street capacity only. Per

Design Point J5 (DP-J5) represents flows generated from Basins proposed inlet), OS-5, OS-6 and the flows released from the proposed inlet.

point is located at a proposed junction with a Type I manhole in Basin OS-4. The total flow at DP-J5 is 9.6 cfs and 42.6 cfs for the 5-year and 100-year storm respectively. The flows leave this manhole via a proposed public 36" RCP storm pipe (or equivalent elliptical pipe - this pipe system was also identified in the DBPS as public and reimbursable) and are carried south where they will outlet via a proposed 25' Type R inlet to be used as a bubbler in Widefield Drive and continue to the south along historic drainage routes as outlined in the DBPS. The bubbler inlet will serve to release the developed upstream flows into Widefield Drive as street flow at the end of the storm sewer system. The inlet will fill and overtop/exit the inlet throat into the street. A small pipe will be provided at the bottom of the inlet to release nuisance flows and allow the inlet to drain after filling. The small pipe to drain the bubbler inlet is planned to be designed similar to a grease interceptor to avoid clogging issues experienced by the county on other similar facilities. Design detail will be provided with the construction Note that the small pipe will daylight documents. N

downstream and release flows to the curb

The flows that bypass and gutter in Widefield Dr. of Widefield Dr. is approximately 21.1 cfs for the 100-yr storm. The flows being conveyed via the 36" RCP storm pipe exiting the manhole at DP-J5 is 42.6 cfs for the 100-yr storm. Therefore, the combined flows just past the bubbler are 63.7 cfs for the 100-yr storm. The existing flows at this point are 100.0 cfs for the 100-yr storm. The development of

It looks like DP-J5 does not account for the intercepted flow from DP-04. Be sure that intercepted flow at the inlet from DP-04 is accounted for in the pipe flow to the bubbler. All note that not all of the pipe flow will be released

Haven Valley will not increase but decrease the flows and flooding issues in the area and downstream on Widefield Drive due to the proposed detention facility which has been sized to not just handle the development of Haven Valley, but all surrounding areas that had no detention required of them in the DBPS. None of the storm infrastructure along Pecos Dr. or Widefield Dr. shown on the DBPS was ever installed. To our knowledge, the homes along the east side of Widefield Dr. do not currently experience flooding and since the proposed flows will be less than the existing flows, no new flooding issues will be created but alleviated if there are any. Also, since the proposed flows are being decreased from the existing flows, there will be no negative impact to the outfall of the existing County pond (in Pheasant Run Ranch Filing No. 1) south of the proposed bubbler. This existing pond does not get backed up under current conditions and therefore will not be backed up in the future with the lower proposed flow amounts in Widefield Drive. Based on what evidence? Please quantify and discussed both statements a little more.

None of the proposed streets exceed capacity, see Appendix for Street Capacity Charts. See also inlet capacity charts for inlet sizing in the Appendix.

A portion of Cable Ln. will be reconstructed and its drainage patterns shall remain the same as existing. The runoff from much of Cable Lane adjacent to the Haven Valley site (with the exception of flows captured by Basins B, C & E) will not be captured by the project's detention facility. This roadway redevelopment falls under the exclusions listed in the ECM I.7.1.B.2 & 3. The total added paved area will be 0.10 acres, which is under the 1 acre of added paved area per 1 mile of roadway. The average width of the existing paved roadway is 22'+, the proposed mat width is 30', which is also less than the 8.25' added width requirement. The roadway width is also not being increased by 2 times or more of the original roadway.

Width does not match street section s
 on Preliminary Development plan.
 Coordinate between plan and report o
 actual paved width.

6.0 PROPOSED DETENTION/WATER QUALITY FACILITIES

The proposed private full spectrum Extended Detention Basin (EDB) is located southwest of the project site within a 1.29 acre drainage easement. This detention pond will fulfill on-site detention needs as well as providing detention for upstream properties, since there is a lack up detention facilities upstream which has caused chronic flooding issues between the two residences that the flows currently pass between on their way to Widefield Dr. The 1.29 acre easement is proposed to be a private drainage/detention easement and the pond to be maintained by Homeowners Association. The Security DBPS does not address the need for a pond in this area, rather it shows roughly 188 cfs (100-year storm) passing between the two houses with only a 24" storm sewer and no swale to convey the flow. The developed peak 100-year flow calculated in this report is 152.1 cfs at this location. The difference in flow is attributed to the DBPS bypassing Elm Grove Pond. The proposal shown in the DBPS does not work and will flood the two residences. Even though the DBPS does not adequately address flooding issues in this area, we are proposing to construct a facility nearly three times the size of a facility necessary to detain runoff from our project site alone.

The proposed detention facility has been designed to capture flows from Basins OS-1, OS-2, OS-3, OS-4, OS-5 and Basins A through H. A total of 41.47 acres is tributary to this EDB with a composite imperviousness of 57.8%. The required pond volume for 100-year

detention is 4.409 acre-feet. The actual pond volume will be 4.542 acre-feet. Concrete forebays with energy dissipaters will be placed where the flows enter the pond on the northeast and the east sides of the pond. The combined volume of the two forebays will be 3% of the WQCV volume for the pond and will be divided proportionally. The flows will exit the forebays through a notch and into the concrete trickle channel at the bottom of the pond that conveys the flows to the micropool. It will capture then release the flows at a reduced flow rate with the use of a plate with orifice holes into a proposed 18" pipe with a restrictor plate. This pipe connects to an area inlet, then a 24" pipe continues to the south, between the two existing residences, and outfalls into a bubbler in Widefield Dr. where the Per UD-detention spreadsheet

spillway width is 40'. Please revise. In accordance with El Paso County criteria, the moaified Type C outlet structure with a permanent micropool will release the WQCV over a 40-hour period. The outlet structure will result in release rates of 0.9 cfs and 17.6 cfs for the 5-year and 100-year storm respectively.

A 30-ft wide riprap emergency spillway will be located on the south side of the pond. In the event that water overtops the spillway, flow will discharge into a 2.5' high x 6.5' wide concrete channel between the two residences before discharging into Widefield Dr. curb and gutter and continuing to the south. Riprap or concrete will be installed between the end of the channel and the back of the sidewalk. In order to design the concrete channel conservatively, the flows from existing DP-B were used, which is 129.0 cfs. The depth of this flow would be 1.3', as can be seen in the colculations included in the Appendix.

Pond calculations are provided in the appendix as well as forebay volumes, micropool sizing, outlet structure design, discharge pipe and spillway design.

The pond will have a 15' wide maintenance road that will provide access to the pond bottom. The maintenance road can be accessed at the west end of New Haven Point. It then ramps down at 12% to the bottom of the pond and around its perimeter. Private maintenance agreements and O&M manuals will be established for this pond as required by the County.

7.0 FOUR-STEP PROCESS

This project conforms to the City of Colorado Springs/El Paso County Four Step Process. The process focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

- 1. **Employ Runoff Reduction Practices:** Proposed impervious areas on this site (roofs, asphalt/sidewalk) will sheet flow across landscaped ground as much as possible to slow runoff and increase time of concentration prior to being conveyed to the proposed public streets and storm sewer system. This will minimize directly connected impervious areas within the project site.
- 2. Implement BMP's that provide a Water Quality Capture Volume with slow release: Runoff from this project will be treated through capture and slow release of the

WQCV in a permanent Extended Detention Basin facility designed per current City of Colorado Springs/El Paso County drainage criteria.

- 3. **Stabilize Drainage Ways:** Flows from the pond are released into Widefield Dr. curb and gutter and no stabilization will be necessary.
- 4. Implement Site Specific and Other Source Control BMP's: The site is proposed as a residential development, and as such standard household source control will be utilized in order to minimize potential pollutants entering the storm system. Example source control measures consist of: garages for storage of household chemicals, trash receptacles for individual households and in common areas for pet waste. The need for Industrial and Commercial BMP's was considered, however per ECM 1.7.2.A the need for industrial and commercial BMPs are not applicable for this project.

8.0 GEOTECHNICAL HAZARDS

In accordance with geotechnical recommendations, the project design is intended to direct runoff away from structures at a minimum slope of six inches over ten feet, and into the receiving water quality basin. This will be accomplished by a variety of means, i.e. curb and gutter and storm sewer.

9.0 DRAINAGE & BRIDGE FEES

2022 Drainage and Bridge Fees

The project lies within the Security Drainage Basin and is previously un-platted. The following fees are required at time of plat recordation:

Impervious area = 11.768 acres x 58.1% = 6.84 acres

Drainage Fees

\$21,134 x 6.84 Impervious Acres = \$144,556.56

Bridge Fees

None

Reimbursement for construction of some of the drainage facilities for Haven Valley and the storm sewer outfall in accordance with DCM Section 3.3, is anticipated as identified by the Little Johnson/Security Drainage Basin Planning Study. See Appendix for Sheet 22 of this DBPS for the reimbursable facilities. Construction costs are listed below and the drainage fee is requested to be adjusted accordingly.

10.0 CONSTRUCTION COST ESTIMATE

Private (Non-Reimbursable) Description	Quantity	Unit Cost	Cost
Type C Area Inlet	2 FA	\$4,800/EA	<u>\$9,600</u>
Double Type D Area Inlet	1 EA	\$11,800/EA	\$11,800
5' Type R Inlet	2 EA	\$5,700/EA	\$11,400
15' Type R Inlet	2 EA	\$10,300/EA	\$20,600
Type I Manhole	1 EA	\$7,000/EA	\$7,000
Type II Manhole	5 EA	\$5,000/EA	\$25,000
18" RCP storm	930 LF	\$67/LF	\$62,310
24" RCP storm	200 LF	\$81/LF	\$16,200
36'' RCP storm	385 LF	\$124/LF	\$47,740
Extended Detention Basin	0.5 EA	\$100,000/EA	\$50,000
		Subtotal	\$261,650
	Engineering	& Contingency (10%)	<u>\$26,165</u>
		TOTAL	\$287,815

Public (Reimbursable) – Facilit	ies identified in the	DBPS					
Description	Quantity	Unit Cost	Cost_				
15' Type R Inlet	1 EA	\$20,600/EA	\$20,600				
25' Type R Inlet	1 EA	\$30,000/EA	\$30,000				
Type I Manhole	2 EA	\$14,000/EA	\$28,000				
24" RCP storm	105 LF	\$162/LF	\$17,010				
30" RCP storm	15 LF	\$200/LF	\$3,000				
36" RCP storm	335 LF	\$248/LF	\$83,080				
	Engineering	Subtotal & Contingency (10%)	\$181,690 <u>\$18,169</u>				
		TOTAL	\$199,859				
Private (Reimbursable) – per ECM Appendix L (see below) Description Quantity Unit Cost Cost							
Extended Detention Basin	0.5 EA	\$100,000/EA	\$50,000				
	Engineering	Subtotal & Contingency (10%)	\$50,000 <u>\$5,000</u>				

TOTAL \$55,000

Per ECM Appendix L 3.10.4a, the proposed detention facility qualifies for a 50% reimbursement. The following requirements for the reimbursement have been met:

- 1. Allowed only where regional system is not yet in place.
- 2. The pond is less than 15 acre-feet in volume from the lowest outlet structure to the crest of the emergency spillway.

- 3. The on-site pond is not part of the regional plan.
- 4. The outlet of the pond must be designed to release at historical levels for all precipitation events from the 2-year storm to the 100-year storm. A smaller outlet may be required by the County if adequate downstream channel improvements are not in place to protect residents from the 2-year storm flows.
- 5. County approved design and construction.
- 6. Landowners assume responsibility for maintenance.

11.0 CONCLUSIONS

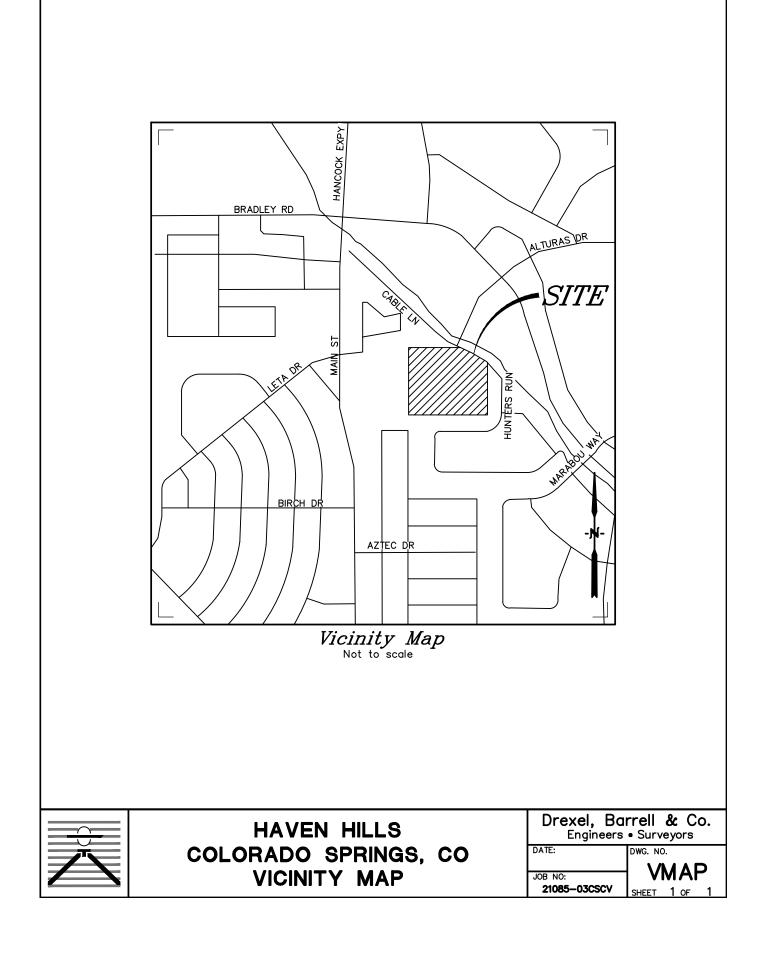
The Haven Valley project has been designed in accordance with El Paso County criteria. The detention pond and water quality basin have been designed to limit the release of storm runoff to less than historic flows. This development will not negatively impact the downstream facilities. This development will improve the downstream conditions by lessening the flows where there are currently flooding issues.

12.0 REFERENCES

The sources of information used in the development of this study are listed below:

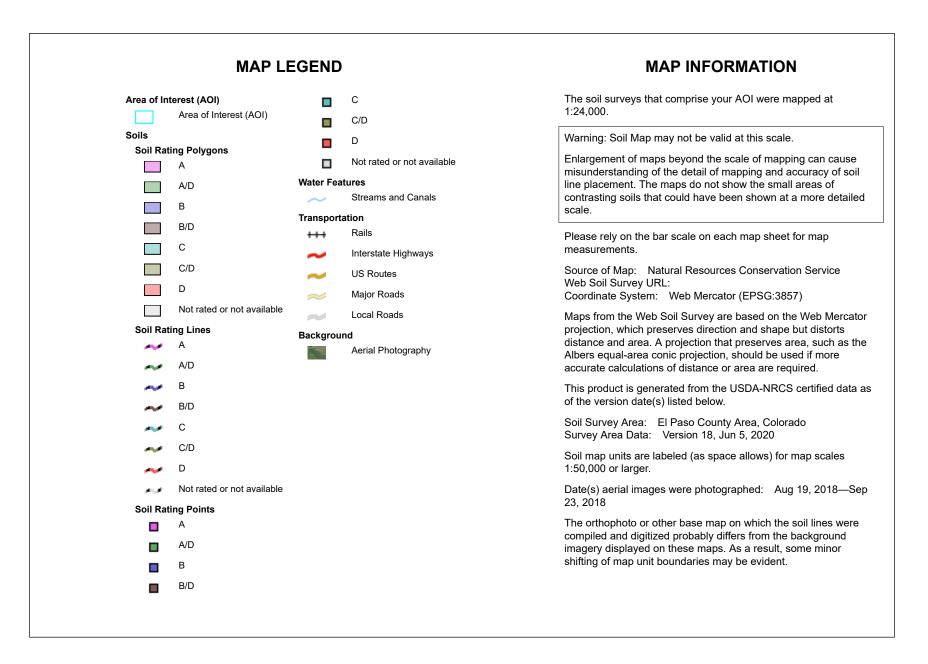
- 1. City of Colorado Springs/El Paso County Drainage Criteria Manual, May 2014.
- 2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised April 2008.
- 3. Preliminary & Final Drainage Report for Patriot Village. Prepared by Core Engineering Group, LLC, December 2013.
- 4. Natural Resources Conservation Service (NRCS) Web Soil Survey
- 5. Federal Emergency Management Agency, Flood Insurance Rate Map, El Paso County, Colorado and Unincorporated Areas, Map Number 08041C0763G, Effective Date December 7, 2018
- 6. EL Paso County Board Resolution No 15-042: El Paso County adoption of Chapter 6 and Section 3.2.1, Chapter 13 of the City of Colorado Springs Drainage Criteria Manual, May 2014.
- 7. Little Johnson/Security Drainage Basin Planning Study. Prepared by Simons Li & Associates, Inc., 1988.
- 8. Soil Investigation Report for Patriot Village. Prepared by Colorado Enginering & Geotechnical Group, Inc., November 15, 2004.

APPENDIX





USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	12.7	100.0%
Totals for Area of Intere	st	12.7	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

USDA

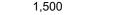
National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation **AREAOF MINIMAL FLOOD HAZARD** EL PASO COUNTY **Coastal Transect** Mase Flood Elevation Line (BFE) Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER **Profile Baseline** 08041C0763G FEATURES Hydrographic Feature eff. 12/7/2018 **Digital Data Available** No Digital Data Available SITE MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/8/2021 at 1:19 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Feet 1:6,000 2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

104°43'49"W 38°45'46"N

n

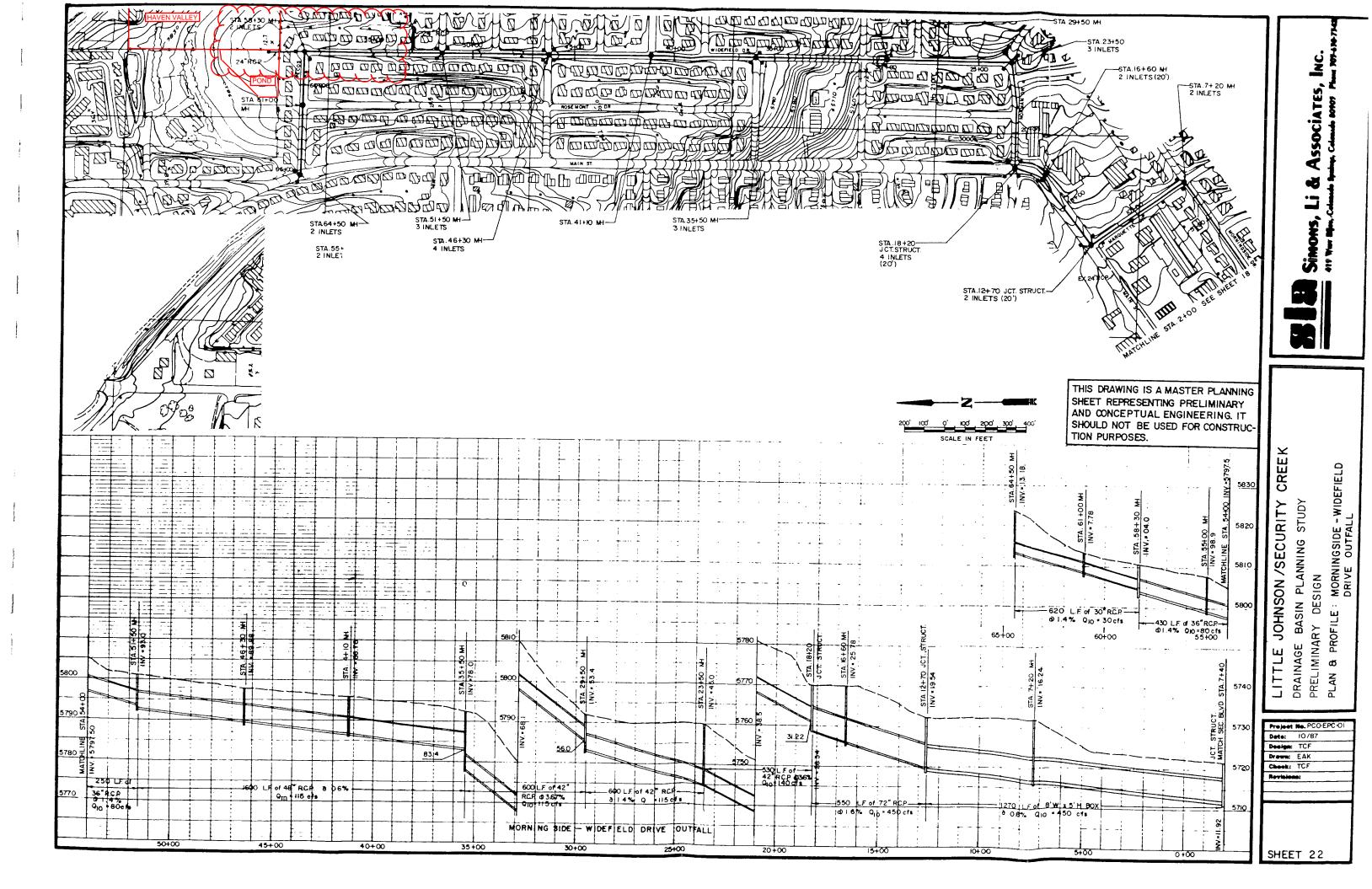
250

500

104°44'26"W 38°46'14"N

080059

1,000



PROJECT IN	FORMATION						
PROJECT:	Haven Valley						
PROJECT NO:	21085-03						
DESIGN BY:	SBN					Drex	el, Barrell & Co.
REV. BY:	TDM						
AGENCY:	El Paso County						
REPORT TYPE:	Final						
DATE:	2/3/2022						
Soil Type: A							
• •			C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadov	v			0.08		0.35	0
Commercial				0.81		0.88	95
1/8 Acre Reside	ntial			0.45		0.59	65
Asphalt/Sidewal	k			0.90		0.96	100
*C-Values and Basin Im	nperviousness based on Table 6-6, El Pase	o County "Draina	ge Criteria Manual"				
EXISTING							
SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSITE	RUNOFF CO	DEFFICIENTS		% IMPERV
		ACRE	C2	C5	C10	C100	
OS-1	Pasture/Meadow	0.00		0.08		0.35	0
	Commercial	8.10		0.81		0.88	95
	1/8 Acre Residential	7.20		0.45		0.59	65
	Asphalt/Sidewalk	1.60		0.90		0.96	100
	WEIGHTED AVERAGE			0.67		0.76	83%
TOTAL OS-1		16.90					
OS-2	Pasture/Meadow	0.00		0.08		0.35	0
03-2	Commercial	2.85	-	0.00		0.35	95
	1/8 Acre Residential	0.00		0.81		0.88	65
	Asphalt/Sidewalk	0.00	-	0.45		0.59	100
	WEIGHTED AVERAGE	0.00		0.90		0.90	95%
TOTAL OS-2	WEIGHTED AVERAGE	2.85		0.01		0.00	9570
OS-3	Pasture/Meadow	4.93		0.08		0.35	0
	Commercial	4.05		0.81		0.88	95
	1/8 Acre Residential	0.76		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.41		0.59	45%
TOTAL OS-3		9.74					
OS-4	Pasture/Meadow	0.00		0.08		0.35	0
~ √- 7	Commercial	4.20		0.00		0.35	95
	1/8 Acre Residential	15.84		0.01		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE	0.00		0.53		0.65	71%
TOTAL OS-4		20.04		0.00		0.00	
H-1	Pasture/Meadow	12.03		0.08		0.35	0
	Commercial	0.00		0.81		0.88	95
	1/8 Acre Residential	0.39		0.45		0.59	65
	Asphalt/Sidewalk	1.02		0.90		0.96	100
	WEIGHTED AVERAGE			0.15	ļ	0.40	9%
TOTAL H-1		13.44					
TOTAL SITE		62.97		0.48		0.63	58.1%

PROJECT INFORMATION

Haven Valley
21085-03
SBN
TDM
El Paso County
Final
2/3/2022



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF EXISTING TIME OF CONCENTRATION STANDARD FORM SF-2

EXISTING TIME OF CONCENTRATION STANDARD FORM ST-2																
SUB-BASIN					INITIAL/OVERLAND			TRAVEL TIME				TIME OF CONC.		FINAL		
		DATA			TIME (t _i)			(t _t)					tc		t _c	
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	LENGTH	HT	SLOPE	ti	LENGTH	HT	SLOPE	VEL.	t	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	t _c	t _c	Min
OS-1		0.67	0.76	16.90	100	2	2.0	6.5	1600	26	1.6	7.4	3.6	10.1	5	10.1
OS-2		0.81	0.88	2.85	100	2	2.0	4.3	400	13	3.3	10.6	0.6	4.9	5	5.0
	A	0.69	0.78	19.75										10.1	5	10.1
OS-3		0.41	0.59	9.74	100	2.5	2.5	9.5	1200	34	2.8	9.8	2.0	11.5	5	11.5
H-1		0.15	0.40	13.44	100	2	2.0	14.1	1600	73	4.6	12.5	2.1	16.2	5	16.2
	В	0.32	0.52	26.03					700	20	2.9	5.28	2.2	16.2	5	16.2
OS-4		0.53	0.65	20.04	100	2	2.0	8.5	2000	41	2.1	8.48	3.9	12.5	5	12.5
	С	0.41	0.58	46.07					100	1	1	3.10	0.5	16.7	5	16.7

PROJECT INFORMATION	
PROJECT:	Haven Valley
PROJECT NO:	21085-03
DESIGN BY:	SBN
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Final
DATE:	2/3/2022

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING	RUNOFF	Ę	5 YR STORM			P1=	1.50
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
OS-1		16.90	0.67	10.1	11.24	4.09	46.0
Exist. Elm Grove Pond Release							18.1
OS-2		2.85	0.81	5.0	2.31	5.10	11.8
	A						29.9
OS-3		9.74	0.41	11.5	4.02	3.88	15.6
H-1		13.44	0.15	16.2	2.06	3.34	6.9
	В	26.03	0.32	16.2	8.38	3.34	46.1
OS-4		20.04	0.53	12.5	10.53	3.76	39.6
	С	46.07	0.41	16.7	18.91	3.29	80.3



Drexel, Barrell & Co.

PROJECT INFORMATION

PROJECT:	Haven Valley
PROJECT NO:	21085-03
DESIGN BY:	SBN
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Final
DATE:	2/3/2022



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING	RUNOFF	10	00 YR STOF	RM		P1=	2.52
			DIRECT RUNG	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
OS-1		16.90	0.76	10.1	12.91	6.88	88.8
Exist. Elm Grove Pond Release							52.3
OS-2		2.85	0.88	5.0	2.51	8.58	21.5
	Α						73.8
OS-3		9.74	0.59	11.5	5.74	6.52	37.4
H-1		13.44	0.40	16.2	5.42	5.62	30.4
	В	26.03	0.52	16.2	13.67	5.62	129.0
OS-4		20.04	0.65	12.5	13.04	6.31	82.3
	С	46.07	0.58	16.7	26.71	5.53	200.0

PROJECT IN	FORMATION						-0-
PROJECT:	Haven Valley						×.
PROJECT NO:	21085-03						
DESIGN BY:	SBN					Drexe	, Barrell & Co.
REV. BY:	TDM						
AGENCY:	El Paso County						
REPORT TYPE:	Final						
DATE:	2/3/2022						
Soil Type: A							
			C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow				0.08		0.35	0
1/8 acre Residen	tial			0.45		0.59	65
Asphalt/Sidewall	k			0.90		0.96	100
*C-Values and Basin Imp	perviousness based on Table 6-6, El Pas	o County "Drainag	ge Criteria Manual"				
PROPOSED							
SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSITE	RUNOFF CO	EFFICIENTS		% IMPERV
		ACRE	C2	C5	C10	C100	
A	Pasture/Meadow	0.20		0.08		0.35	0
	1/8 acre Residential	0.24		0.45		0.59	65
	Asphalt/Sidewalk			0.43		0.96	100
		0.00					
	WEIGHTED AVERAGE	ļ		0.28		0.48	35%
TOTAL A		0.44					
В	Pasture/Meadow	0.00		0.08		0.35	0
	1/8 acre Residential	1.11		0.45		0.59	65
	Asphalt/Sidewalk	0.31		0.90		0.96	100
	WEIGHTED AVERAGE			0.55		0.67	73%
TOTAL B		1.42					
C	Pasture/Meadow	0.32		0.08		0.35	0
	1/8 acre Residential	2.69		0.45		0.59	65
	Asphalt/Sidewalk	0.42		0.90		0.96	100
	WEIGHTED AVERAGE		_	0.47		0.61	63%
TOTAL C		3.43					
D	Pasture/Meadow	0.43		0.08		0.35	0
	1/8 acre Residential	0.55	-	0.45		0.59	65
	Asphalt/Sidewalk WEIGHTED AVERAGE	0.00	-	0.90		0.96	100
	WEIGHTED AVERAGE	0.00		0.29		0.48	36%
TOTAL D E	Pasture/Meadow	0.98		0.08		0.35	0
E	1/8 acre Residential	2.72	-	0.08		0.55	65
	Asphalt/Sidewalk	0.21		0.45		0.39	100
	WEIGHTED AVERAGE	0.21		0.90		0.90	64%
TOTAL E		3.09		0.40		0.00	0-7/0
F	Pasture/Meadow	0.00		0.08		0.35	0
-	1/8 acre Residential	0.69		0.00		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE	0.00		0.45		0.59	65%
TOTAL F		0.69	1				
G	PROPOSED	0.00		0.00		0.00	0
	1/8 acre Residential	1.61		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL G		1.61					
Н	Pasture/Meadow	0.40		0.08		0.35	0
	1/8 acre Residential	0.44		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.27		0.48	34%
TOTAL H		0.84					
1	Pasture/Meadow	0.47		0.08		0.35	0
	1/8 acre Residential	0.22		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
TOTAL	WEIGHTED AVERAGE	0.00		0.20		0.43	21%
TOTAL I		0.69					
		40.40		0.40		0.50	E7 70/
TOTAL		13.19		0.43		0.58	57.7%
TOTAL DOND TO		44.00		Λ E F		0.60	57 00/
TOTAL POND TR		41.99	1	0.55		0.68	57.8%

PROJECT INFORMATION

PROJECT:	Haven Valley
PROJECT NO:	21085-03
DESIGN BY:	SBN
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Final
DATE:	2/3/2022



Drexel, Barrell & Co.

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF PROPOSED TIME OF CONCENTRATION STANDARD FORM SF-2

SUB-BASIN INITIAL/OVERLAND						TRAVEL TIME				PIPE TRAVEL TIME			TIME OF CONC.		FINAL					
		DATA				TIME (t _i)				(t _t)					(t _p)			t	;	tc
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	LENGTH	HT	SLOPE	ti	LENGTH	HT	SLOPE	VEL.	t	LENGTH	SLOPE	VEL.	t	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	Ft	%	FPS	Min	t _c	t _c	Min
A	1	0.28	0.48	0.44	100	8	8.0	7.7	350	14	4.0	6.2	0.9					8.6	5	8.6
OS-1		0.67	0.76	16.90	100	2	2	6.5	1600	26	1.6	7.4	3.6					10.1	5	10.1
OS-2		0.81	0.88	2.85	100	2	2	4.3	400	13	3.3	10.6	0.6					4.9	5	5.0
В	2	0.55	0.67	1.42	100	2	2.0	8.2	1300	57.0	4.4	12.3	1.8					10.0	5	10.0
С	3	0.47	0.61	3.43	100	2	2.0	9.3	250	11	4.4	6.5	0.6	600	3.3	10.6	0.9	10.9	5	10.9
	J1	0.49	0.63	4.85										5	0.5	3.4	0.0	10.9	5	10.9
D	4	0.29	0.48	0.98	100	7	7.0	7.9	250	9	3.6	5.9	0.7					8.6	5	8.6
Е	5	0.46	0.60	3.09	55	1.5	2.7	6.3	915	28	3.1	10.3	1.5					7.8	5	7.8
	J2	0.46	0.61	5.83										40	2.0	8.3	0.1	11.0	5	11.0
F		0.45	0.59	0.69	50	1	2.0	6.8	470	16	3.4	10.8	0.7					7.5	5	7.5
	6	0.46	0.60	3.78										50	3.1	10.3	0.1	7.9	5	7.9
	J3	0.46	0.60	9.61										40	2.5	9.3	0.1	11.1	5	11.1
G	7	0.45	0.59	1.61	80	1	1.3	10.1	720	17	2.4	9.1	1.3					11.4	5	11.4
	J4	0.46	0.60	11.22										20	1.0	5.9	0.1	11.5	5	11.5
OS-3		0.41	0.59	9.74	100	2.5	2.5	9.5	1200	34	2.8	9.8	2.0					11.5	5	11.5
Н	8	0.27	0.48	0.84	100	7	7.0	8.1	350	17	4.9	6.9	0.8					8.9	5	8.9
	P1	0.55	0.68	41.99														11.5	5	11.5
OS-5		0.45	0.59	0.15	50	2	4.0	5.4										5.4	5	5.4
OS-6		0.45	0.59	0.41	70	4	5.7	5.7										5.7	5	5.7
I		0.20	0.43	0.69	20	1	5.0	4.4	850	18	2.1	4.5	3.2					7.6	5	7.6
	9	0.31	0.50	1.25														13.3	5	13.3
OS-4	04	0.53	0.65	20.04	100	2	2	8.5	2000	41	2.1	8.5	3.9					12.5	5	12.5

PROJECT INFORMATION	
PROJECT:	Haven Valley
PROJECT NO:	21085-03
DESIGN BY:	SBN
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Final
DATE:	2/3/2022



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED RUNOFF 5			5 YR STORI	М	P1=	1.50	
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
A		0.44	0.28	8.6	0.12	4.34	0.5
OS-1		16.90	0.67	10.1	11.24	4.09	46.0
Exist. Elm Grove Pond Release							18.1
OS-2		2.85	0.81	5.0	2.31	5.10	11.8
	1	3.29	0.74	10.1	2.43	4.09	28.1
В	2	1.42	0.55	10.0	0.78	4.11	3.2
С	3	3.43	0.47	10.9	1.61	3.96	6.4
	J1	4.85	0.49	10.9	2.39	3.96	9.5
D	4	0.98	0.29	8.6	0.28	4.33	1.2
E	5	3.09	0.46	7.8	1.43	4.48	6.4
	J2	5.83	0.46	11.0	2.67	3.95	10.6
F		0.69	0.45	7.5	0.31	4.53	1.4
	6	3.78	0.46	7.9	1.74	4.46	7.7
	J3	9.61	0.46	11.1	4.41	3.94	17.4
G	7	1.61	0.45	11.4	0.72	3.89	2.8
	J4	11.22	0.46	11.5	5.14	3.89	20.0
OS-3		9.74	0.41	11.5	4.02	3.88	15.6
Н	8	0.84	0.27	8.9	0.23	4.28	1.0
	P1	25.10	0.47	11.5	11.80	3.88	63.9
POND RELEASE							0.7
OS-5		0.15	0.45	5.4	0.07	5.00	0.3
OS-6		0.41	0.45	5.7	0.18	4.93	0.9
I		0.69	0.20	7.6	0.14	4.53	0.6
	9						2.6
OS-4	04	20.04	0.53	12.5	10.53	3.76	39.6
	J5						9.6

PROJECT INFORMATION

PROJECT:	Haven Valley
PROJECT NO:	21085-03
DESIGN BY:	SBN
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Final
DATE:	2/3/2022



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

OPOSED	RUNOFF	10	0 YR STOF	RM					P1=	2.5
			DIRECT RUNC)FF					PIPE SIZ	NG
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	n	Slope (ft/ft)	Pipe Diameter (in
A		0.44	0.48	8.6	0.21	7.29	1.5			
OS-1		16.90	0.76	10.1	12.91	6.88	88.8			
Exist. Elm Grove Pond Release							52.3			
OS-2		2.85	0.88	5.0	2.51	8.58	21.5			
	1	3.29	0.83	10.1	2.72	6.88	71.0	0.016	0.038	36
В	2	1.42	0.67	10.0	0.95	6.90	6.6	0.016	0.035	18
С	3	3.43	0.61	10.9	2.10	6.66	14.0	0.016	0.005	24
	J1	4.85	0.63	10.9	3.05	6.65	20.3	0.016	0.035	24
D	4	0.98	0.48	8.6	0.48	7.27	3.5	0.016	0.023	18
E	5	3.09	0.60	7.8	1.86	7.52	14.0			
	J2	5.83	0.61	11.0	3.53	6.63	23.4	0.016	0.023	24
F		0.69	0.59	7.5	0.41	7.61	3.1			
	6	3.78	0.60	7.9	2.27	7.50	17.0	0.016	0.005	24
	J3	9.61	0.60	11.1	5.80	6.62	38.4	0.016	0.023	24
G	7	1.61	0.59	11.4	0.95	6.54	6.2	0.016	0.005	18
	J4	11.22	0.60	11.5	6.75	6.53	44.1	0.016	0.125	24
OS-3		9.74	0.59	11.5	5.74	6.52	37.4			
Н	8	0.84	0.48	8.9	0.40	7.19	2.9			
	P1	25.10	0.62	11.5	15.56	6.52	153.8			
POND RELEASE							17.6	0.016	0.006	18
OS-5		0.15	0.59	5.4	0.09	8.40	0.7			
OS-6		0.41	0.59	5.7	0.24	8.29	2.0			
I		0.69	0.43	7.6	0.29	7.61	2.2			
	9						22.6	0.016	0.029	24
OS-4	O4	20.04	0.65	12.5	13.04	6.31	82.3	0.016	0.005	30
	J5						42.6	0.016	0.006	36 or elp. ed

Worksheet Worksheet for Trapezoidal Channel

	otion	
Worksheet	North	<mark>swale</mark>
Flow Element	Trape	ezoidal Cha
Method	Mann	ning's Form
Solve For	Chan	nel Depth
Input Data		
Mannings Coe	effic 0.030	
Slope	040000 f	t/ft
Left Side Slop	e 0.25 \	/ : H
Right Side Slo	•	
Bottom Width	4.00 f	
Discharge	23.00 c	
Results		
-		ft
Depth	0.69	
Flow Area	3.7	ft²
Flow Area Wetted Perime	3.7 7.52	ft² ft
Flow Area Wetted Perime Top Width	3.7 7.52 6.82	ft ² ft ft
Flow Area Wetted Perime Top Width Critical Depth	3.7 7.52 6.82 0.86	ft ² ft ft ft
Flow Area Wetted Perime Top Width Critical Depth Critical Slope	3.7 7.52 6.82 0.86 0.017463	ft ² ft ft ft ft/ft
Flow Area Wetted Perime Top Width Critical Depth Critical Slope Velocity	3.7 7.52 6.82 0.86 0.017463 6.19	ft ² ft ft ft ft/ft ft/ft
Flow Area Wetted Perime Top Width Critical Depth Critical Slope Velocity Velocity Head	3.7 7.52 6.82 0.86 0.017463 6.19 0.60	ft ² ft ft ft ft/ft ft/s ft
Flow Area Wetted Perime Top Width Critical Depth Critical Slope Velocity Velocity Head Specific Energy	3.7 7.52 6.82 0.86 0.017463 6.19 0.60 1.28	ft ² ft ft ft ft/ft ft/s ft
Flow Area Wetted Perime Top Width Critical Depth Critical Slope Velocity Velocity Head	3.7 7.52 6.82 0.86 0.017463 6.19 0.60 1.28	ft ² ft ft ft ft/ft ft/s ft

Worksheet Worksheet for Trapezoidal Channel

Method Solve ForManning's For Channel DepthInput Data	
Flow ElementTrapezoidal CłMethodManning's ForSolve ForChannel DepthInput DataMannings Coeffic0.030Slope030000 ft/ftLeft Side Slope0.25 V : HRight Side Slope0.25 V : HBottom Width2.00 ftDischarge3.50 cfsResultsDepth0.33 ftFlow Area1.1 ft²Wetted Perimi4.70 ftTop Width4.62 ftCritical Depth0.36 ft	otion
MethodManning's For Channel DepthInput Data	East Swale
Solve For Channel Depth Input Data Input Data Mannings Coeffic 0.030 Slope 030000 ft/ft Left Side Slope 0.25 V : H Right Side Slope 0.25 V : H Bottom Width 2.00 ft Discharge 3.50 cfs Results Depth 0.33 ft Flow Area 1.1 ft² Wetted Perim 4.70 ft Top Width 4.62 ft Critical Depth 0.36 ft	Trapezoidal Cha
Input DataMannings Coeffic0.030Slope030000ft/ftLeft Side Slope0.25V : HRight Side Slope0.25V : HBottom Width2.00Discharge3.50CfsResultsDepth0.33Flow Area1.11.1ft²Wetted Perimi4.70Top Width4.62Critical Depth0.36ft	Manning's Form
Mannings Coeffic0.030Slope030000ft/ftLeft Side Slope0.25V : HRight Side Slope0.25V : HBottom Width2.00ftDischarge3.50cfsResultsDepth0.33ftFlow Area1.1ft²Wetted Perim4.70ftTop Width4.62ftCritical Depth0.36ft	Channel Depth
Mannings Coeffic0.030Slope030000ft/ftLeft Side Slope0.25V : HRight Side Slope0.25V : HBottom Width2.00ftDischarge3.50cfsResultsDepth0.33ftFlow Area1.1ft²Wetted Perim4.70ftTop Width4.62ftCritical Depth0.36ft	
Slope030000ft/ftLeft Side Slope0.25V : HRight Side Slope0.25V : HBottom Width2.00ftDischarge3.50cfsResultsDepth0.33Flow Area1.1ft²Wetted Perim4.70ftTop Width4.62ftCritical Depth0.36ft	
Left Side Slope0.25 V : HRight Side Slope0.25 V : HBottom Width2.00 ftDischarge3.50 cfsResultsDepth0.33 ftFlow Area1.1 ft²Wetted Perimit4.70 ftTop Width4.62 ftCritical Depth0.36 ft	effic 0.030
Right Side Slope0.25 V : HBottom Width2.00 ftDischarge3.50 cfsResultsDepth0.33 ftFlow Area1.1 ft²Wetted Perimt4.70 ftTop Width4.62 ftCritical Depth0.36 ft	030000 ft/ft
Bottom Width Discharge2.00 ft 3.50 cfsResultsDepth0.33 ft 1.1 ft²Wetted Perim Top Width4.70 ft 4.62 ft 0.36 ft	e 0.25 V:H
Discharge3.50 cfsResultsDepth0.33 ftFlow Area1.1 ft²Wetted Perim4.70 ftTop Width4.62 ftCritical Depth0.36 ft	pe 0.25 V : H
ResultsDepth0.33 ftFlow Area1.1 ft²Wetted Perim4.70 ftTop Width4.62 ftCritical Depth0.36 ft	2.00 ft
Depth0.33 ftFlow Area1.1 ft²Wetted Perime4.70 ftTop Width4.62 ftCritical Depth0.36 ft	3.50 cfs
Depth0.33 ftFlow Area1.1 ft²Wetted Perime4.70 ftTop Width4.62 ftCritical Depth0.36 ft	
Flow Area1.1ft²Wetted Perime4.70ftTop Width4.62ftCritical Depth0.36ft	
Wetted Perime4.70ftTop Width4.62ftCritical Depth0.36ft	0.33 ft
Top Width4.62 ftCritical Depth0.36 ft	1.1 ft ²
Critical Depth 0.36 ft	4.70 ft
	4.62 ft
Critical Slope 0.021252 ft/ft	0.36 ft
	0.021252 ft/ft
Velocity 3.23 ft/s	3.23 ft/s
Velocity Head 0.16 ft	0.16 ft
Specific Energ 0.49 ft	0.49 ft
Froude Numb 1.17	1.17
Flow Type Supercritical	Supercritical

Fr # larger than allowable (DCM 6.5.2) Swale will need to be lined.

Worksheet Worksheet for Trapezoidal Channel

Project Description	
Worksheet S	South Swale
Flow Element T	rapezoidal Cha
Method N	lanning's Form
Solve For C	Channel Depth
Input Data	
Mannings Coeffic 0.03	30
Slope 02000	00 ft/ft
Left Side Slope 0.1	15 V:H
Right Side Slope 0.2	25 V:H
Bottom Width 4.0	DO ft
Discharge 3.9	90 cfs
Results	
Depth 0.2	8 ft
Flow Area 1.	5 ft ²
Wetted Perime 7.0	4 ft
Top Width 6.9	8 ft
Critical Depth 0.2	7 ft
Critical Slope 0.02212	3 ft/ft
Velocity 2.5	4 ft/s
Velocity Head 0.1	0 ft
Specific Enerç 0.3	8 ft
Froude Numb 0.9	5 🔨
Flow Type Subcritica	al

Fr # larger than allowable (DCM 6.5.2) Swale will need to be lined.

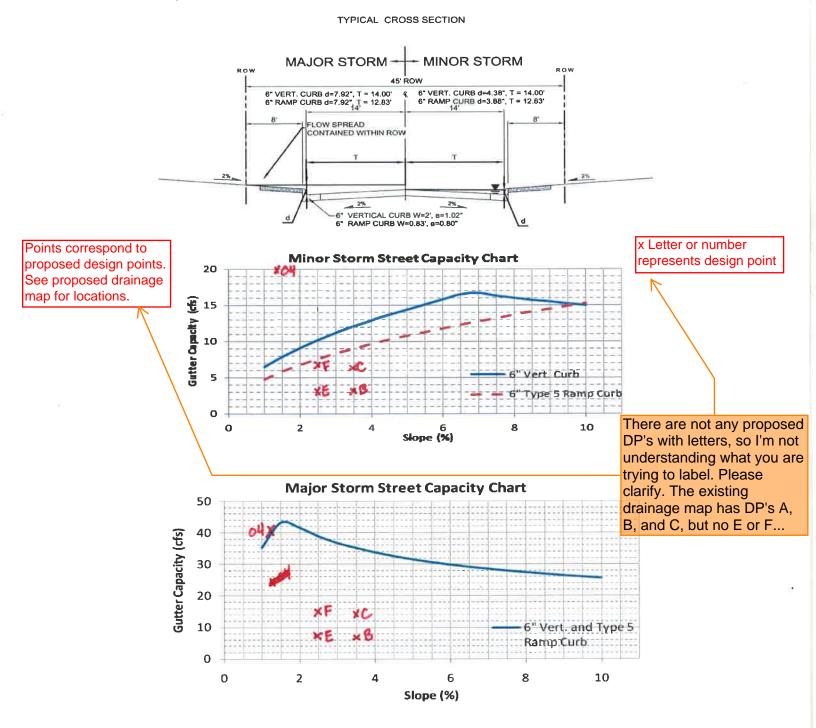
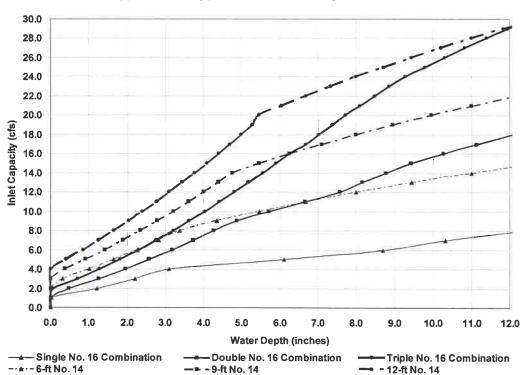
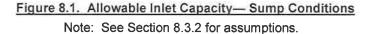


Figure 7-9. Street Capacity Charts Minor Residential (Attached Sidewalk)

These charts shall only be used for the standard street sections as shown. The capacity shown is based on $\frac{1}{2}$ the street section as calculated by the UD-Inlet spreadsheets. Minor storm capacities are based on no crown overtopping, curb height or maximum allowable spread widths. Major storm capacities are based on flow being containing within the public right-of-way, including conveyance capacity behind the curb. The UDFCD Safety Reduction Factor was applied. An 'INSTREET' of 0.016 and 'N_{BACK}' of 0.020 was used. Calculations were done using UD-Inlet 3.00.xls, March, 2011.

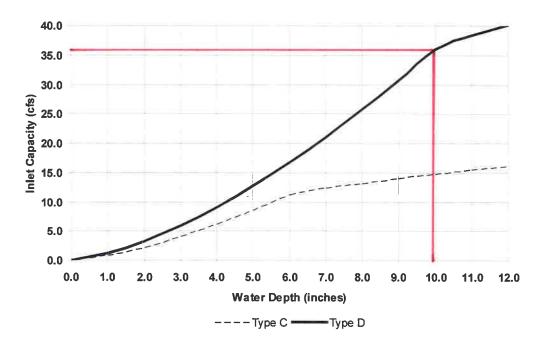
City of Colorado Springs Drainage Criteria Manual, Volume 1





Type 16 and Type 14 Inlets for Sump Conditions





01/2006 City and County of Denver

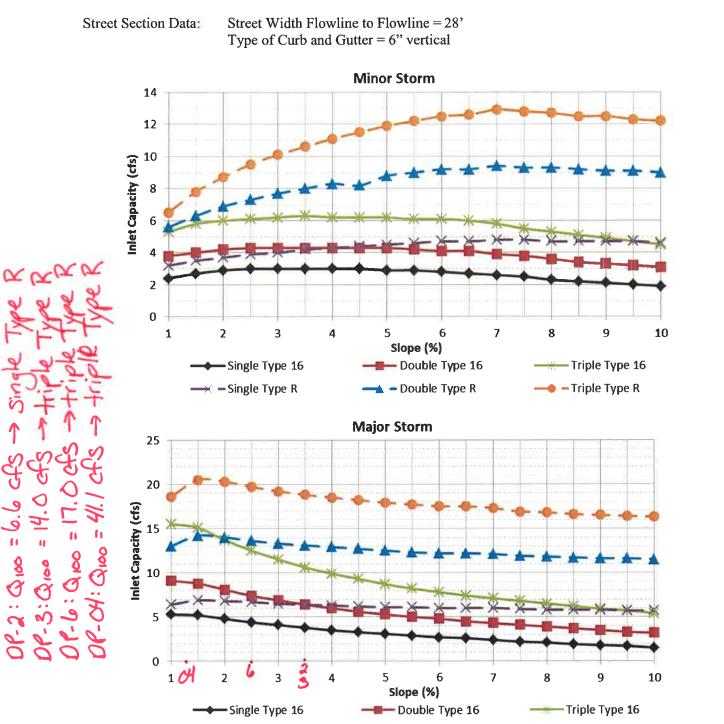


Figure 8-9. Inlet Capacity Chart Continuous Grade Conditions, Minor Residential (Local) (Attached Sidewalk)

The standard street section parameters as defined in Chapter 7 must apply to use these charts. For non-standard sections, the inlet capacity shall be calculated using the UDFCD spreadsheets. The maximum spread width is limited by the curb height based on no curb overtopping during a minor storm and flow being contained within the public right-of-way during the major storm. Calculations were done using UD-Inlet 3.00.xls, Mar., 2011 with the default clogging factors.

- Double Type R

- Single Type R

- Triple Type R

11

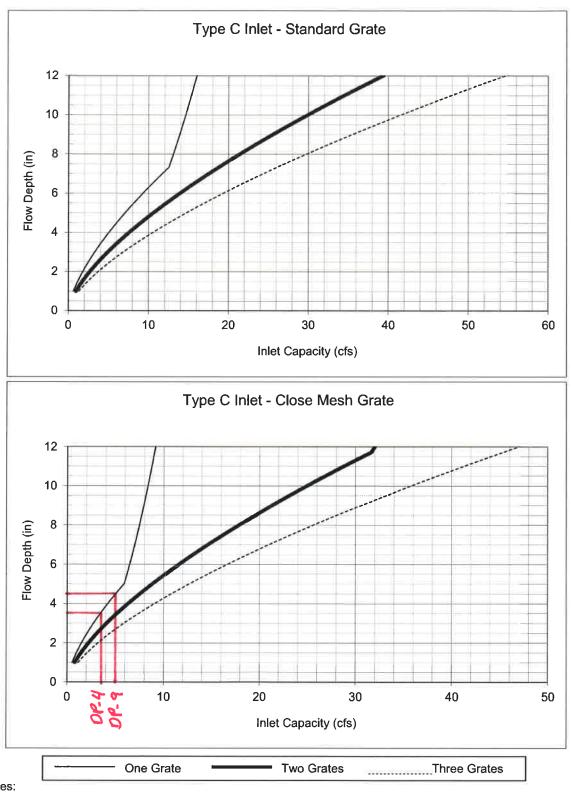


Figure 8-10. Inlet Capacity Chart Sump Conditions, Area (Type C) Inlet

Notes:

DP-4: Q100 = 3.5 cf

1. The standard inlet parameters must apply to use these charts.

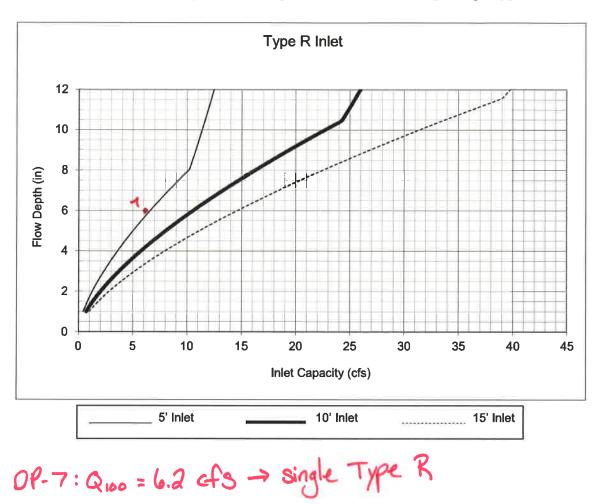


Figure 8-11. Inlet Capacity Chart Sump Conditions, Curb Opening (Type R) Inlet

Notes:

1. The standard inlet parameters must apply to use this chart.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project: Haven Valley
Basin ID:
POOL Example Zone Configuration (Retention Pond)

Watershed Information

tersned information		
Selected BMP Type =	EDB	
Watershed Area =	41.99	acres
Watershed Length =	2,000	ft
Watershed Length to Centroid =	500	ft
Watershed Slope =	0.023	ft/ft
Watershed Imperviousness =	57.80%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

are embedded colorado orban nyaro	graphinioceau		Optional U
Water Quality Capture Volume (WQCV) =	0.801	acre-feet	
Excess Urban Runoff Volume (EURV) =	2.914	acre-feet	
2-yr Runoff Volume (P1 = 1.19 in.) =	2.123	acre-feet	1.19
5-yr Runoff Volume (P1 = 1.5 in.) =	2.801	acre-feet	1.50
10-yr Runoff Volume (P1 = 1.75 in.) =	3.345	acre-feet	1.75
25-yr Runoff Volume (P1 = 2 in.) =	4.111	acre-feet	2.00
50-yr Runoff Volume (P1 = 2.25 in.) =	4.864	acre-feet	2.25
100-yr Runoff Volume (P1 = 2.52 in.) =	5.798	acre-feet	2.52
500-yr Runoff Volume (P1 = 3.49 in.) =	9.040	acre-feet	3.49
Approximate 2-yr Detention Volume =	1.886	acre-feet	
Approximate 5-yr Detention Volume =	2.473	acre-feet	
Approximate 10-yr Detention Volume =	2.998	acre-feet	
Approximate 25-yr Detention Volume =	3.634	acre-feet	
Approximate 50-yr Detention Volume =	4.026	acre-feet	
Approximate 100-yr Detention Volume =	4.464	acre-feet	

Define Zones and Basin Geometry

0.801	acre-feet
2.113	acre-feet
1.550	acre-feet
4.464	acre-feet
user	ft ³
user	ft
user	ft
user	ft
user	ft/ft
user	H:V
user	
user	ft ²
user	ft
user	ft ²
user	ft ³
user	ft
user	ft
	2.113 1.550 4.464 user user user user user user user user

Width of Main Basin (W_{MAIN}) =

Volume of Main Basin (V_{MAIN}) =

Area of Main Basin (A_{MAIN}) =

Calculated Total Basin Volume (V_{total}) = user

user ft

user ft 3

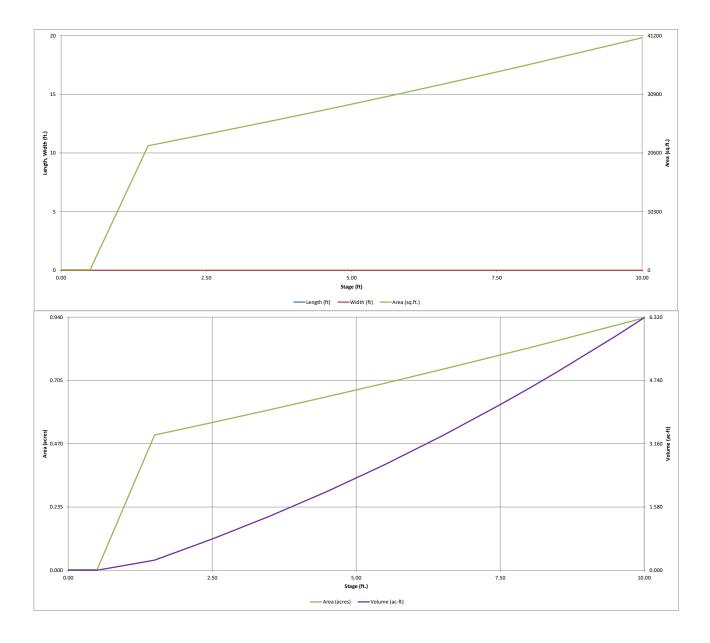
user ft²

acre-feet

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	.,	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)		
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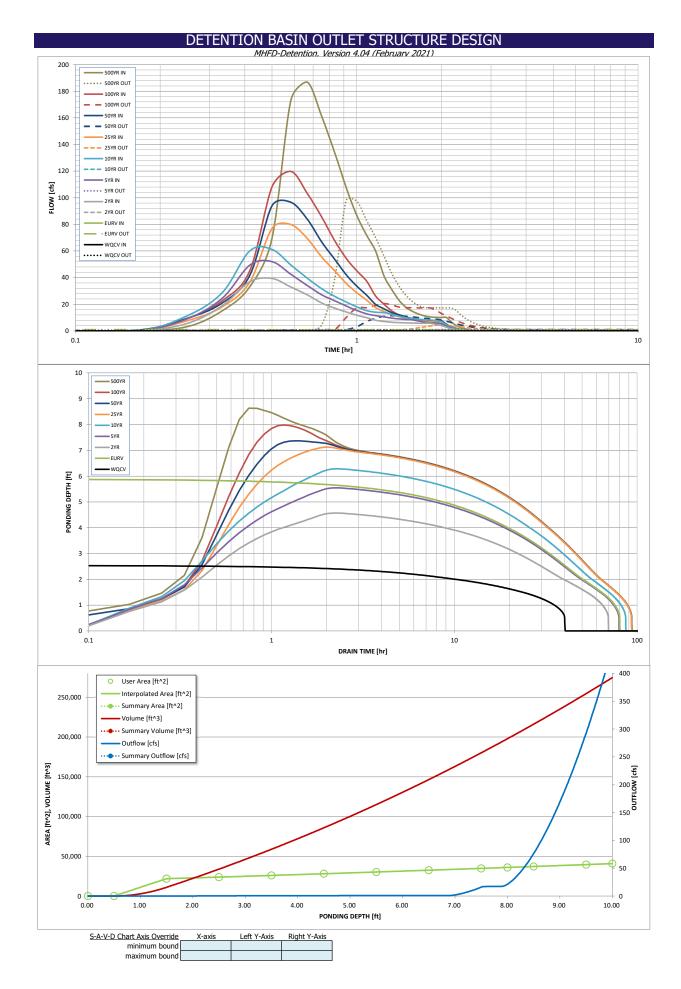
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Basin ID:	N/A N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	the filtration media	Estimated Stage (ft) 2.55 5.89 7.91 Total (all zones) surface)	Underd	Irain Orifice Area =		ters for Underdrain	
VOLUME EURV WOCV VOLUME EURV WOCV PERMANENT POOL EURV WOCV PERMANENT POOL Example Zone 0 User Input: Orifice at Underdrain Outlet (typically Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	onifice Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	Zone 2 (EURV) Zone 3 (100-year) <u>MP)</u> the filtration media	Stage (ft) 2.55 5.89 7.91 Total (all zones)	Volume (ac-ft) 0.801 2.113 1.550 4.464 Underd	Orifice Plate Orifice Plate Weir&Pipe (Restrict) Irain Orifice Area =			
User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	onifice Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	Zone 2 (EURV) Zone 3 (100-year) <u>MP)</u> the filtration media	Stage (ft) 2.55 5.89 7.91 Total (all zones)	Volume (ac-ft) 0.801 2.113 1.550 4.464 Underd	Orifice Plate Orifice Plate Weir&Pipe (Restrict) Irain Orifice Area =			L
VOLUME_ EURY VOCY ZONE 1 AND 2 POOL ZONE 1 AND 2 POOL CONE 1 AND 2 POOL CONE 1 AND 2 OMFICES POOL Example Zone C User Input: Orifice at Underdrain Outlet (typically Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	onifice Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	Zone 2 (EURV) Zone 3 (100-year) <u>MP)</u> the filtration media	2.55 5.89 7.91 Total (all zones)	0.801 2.113 1.550 4.464 Underd	Orifice Plate Orifice Plate Weir&Pipe (Restrict) Irain Orifice Area =			L
User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice Plate with one or more orifice Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Area per Row =	onifice Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	Zone 2 (EURV) Zone 3 (100-year) <u>MP)</u> the filtration media	5.89 7.91 Total (all zones)	2.113 1.550 4.464 Underd	Orifice Plate Weir&Pipe (Restrict) Irain Orifice Area =			L
DESTINATE OFFICES DESTINATE OFFICES DOL DESTINATION DESTI	onifice Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	Zone 3 (100-year)	7.91 Total (all zones)	1.550 4.464 Underd	Weir&Pipe (Restrict)			L
DESTINAMENT OWFICES Example Zone O User Input: Orifice at Underdrain Outlet (typically Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = Underdrain Orifice Diameter = Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	Configuration (Re used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	tention Pond) CV in a Filtration Bf ft (distance below inches Weir (typically used ft (relative to basin	MP) the filtration media	Total (all zones)	4.464 Underd	Irain Orifice Area =			L
User Input: Orifice at Underdrain Outlet (typically Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	used to drain WQ N/A N/A s or Elliptical Slot ' 0.00 5.89 N/A	CV in a Filtration BI ft (distance below inches Weir (typically used ft (relative to basin	the filtration media		Underd	Irain Orifice Area =			L
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	N/A N/A s or Elliptical Slot 0.00 5.89 N/A	ft (distance below inches <u>Weir (typically used</u> ft (relative to basin	the filtration media		Underd	Irain Orifice Area =			L
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	N/A N/A s or Elliptical Slot 0.00 5.89 N/A	ft (distance below inches <u>Weir (typically used</u> ft (relative to basin	the filtration media	surface)		Irain Orifice Area =			
Underdrain Orifice Diameter = User Input: Orifice Plate with one or more orifice Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	N/A s or Elliptical Slot 0.00 5.89 N/A	inches <u>Weir (typically used</u> ft (relative to basin		,	Underdrain				
Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	0.00 5.89 N/A	ft (relative to basin	to drain WOCV and			Orifice Centroid =	N/A	feet	
Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	0.00 5.89 N/A	ft (relative to basin	to drain WOCV and						
Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	5.89 N/A	•	unu n you unu	d/or EURV in a sed	imentation BMP)		Calculated Parame	ters for Plate	
Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	N/A	ft (rolative to be -!-	n bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	N/A	ft ²	
Orifice Plate: Orifice Area per Row =		it (relative to pasin	n bottom at Stage =	= 0 ft)	Ellir	ptical Half-Width =	N/A	feet	
·	N/A	inches			Ellipti	cal Slot Centroid =	N/A	feet	
		inches			E	lliptical Slot Area =	N/A	ft ²	
User Input: Stage and Total Area of Each Orifice	Row (numbered f	rom lowest to high	<u>est)</u>						_
[Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	2.00	4.00						
Orifice Area (sq. inches)	5.22	5.22	3.00						
-			· · · · · · · · · · · · · · · · · · ·		.				1
-	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
User Input: Vertical Orifice (Circular or Rectangu			1					ters for Vertical Ori	fice
	Not Selected	Not Selected	1				Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	,	ft (relative to basin	5	,	tical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A		ft (relative to basin	bottom at Stage =	= 0 ft) Vertical	Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat or			tangular/Trapezoid	al Weir (and No Ou	<u>itlet Pipe)</u>		Calculated Parame	ters for Overflow W	<u>/eir</u>
_	Zone 3 Weir	Not Selected	1				Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.90		ft (relative to basin b	oottom at Stage = 0 f		e Upper Edge, $H_t =$	6.90	N/A	feet
Overflow Weir Front Edge Length =	5.00	,	feet		Overflow W	eir Slope Length =	5.00	N/A	feet
Overflow Weir Grate Slope =	0.00	,	H:V	Gr	rate Open Area / 10	0-yr Orifice Area =	15.05	N/A	
Horiz. Length of Weir Sides =	5.00	N/A	feet	0\	verflow Grate Open	Area w/o Debris =	17.40	N/A	ft ²
Overflow Grate Type =	Type C Grate	N/A	1	C	Overflow Grate Oper	n Area w/ Debris =	8.70	N/A	ft ²
Debris Clogging % =	50%	N/A	%						
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, R	estrictor Plate, or R	ectangular Orifice)		Ca	Iculated Parameters	for Outlet Pipe w/	Flow Restriction Pl	ate
	Zone 3 Restrictor	Not Selected	1				Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below ba	asin bottom at Stage	= 0 ft) Oi	utlet Orifice Area =	1.16	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches		Outlet	: Orifice Centroid =	0.53	N/A	feet
Restrictor Plate Height Above Pipe Invert =	11.20		inches	Half-Cent	tral Angle of Restrict	tor Plate on Pipe =	1.82	N/A	radians
User Input: Emergency Spillway (Rectangular or 1		I.					Calculated Parame	1	
Spillway Invert Stage=	7.90	1 ·	bottom at Stage =	= 0 ft)		esign Flow Depth=	0.95	feet	
Spillway Crest Length =	40.00	feet			5	op of Freeboard =	9.85	feet	
Spillway End Slopes =	4.00	H:V				op of Freeboard =	0.93	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at T	op of Freeboard =	6.17	acre-ft	
Routed Hydrograph Results	The user can over	ride the default CU	HP hydrographs and	d runoff volumos b	v entering now valu	es in the Inflow Her	drographs table (C	humne M/ through	AF)
Design Storm Return Period =	WOCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
UCSUU SIGUI REULU PERA = IP	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.49
		2.914	2.123	2.801	3.345	4.111	4.864	5.798	9.040
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	0.801		2.123	2.801	3.345	4.111	4.864	5.798	9.040
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	N/A	N/A						32.7	74.0
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	N/A N/A	N/A	0.4	0.8	1.1	10.1	19.9	52.7	71.0
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A N/A N/A	N/A N/A	0.4	0.8					
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A N/A N/A N/A	N/A N/A N/A	0.4	0.8	0.03	0.24	0.47	0.78	1.76
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A N/A N/A	N/A N/A	0.4	0.8					
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	N/A N/A N/A N/A N/A 0.4 N/A	N/A N/A N/A 0.9 N/A	0.4 0.01 39.4 0.7 N/A	0.8 0.02 52.0 0.9 1.1	0.03 61.2 1.0 0.9	0.24 79.9 4.5 0.4	0.47 96.6 11.4 0.6	0.78 119.8 20.5 0.6	1.76 186.8 97.9 1.3
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow 2 (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow =	N/A N/A N/A N/A 0.4 N/A Plate	N/A N/A N/A 0.9 N/A Plate	0.4 0.01 39.4 0.7 N/A Plate	0.8 0.02 52.0 0.9 1.1 Plate	0.03 61.2 1.0 0.9 Plate	0.24 79.9 4.5 0.4 Overflow Weir 1	0.47 96.6 11.4 0.6 Overflow Weir 1	0.78 119.8 20.5 0.6 Spillway	1.76 186.8 97.9 1.3 Spillway
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	N/A N/A N/A N/A 0.4 N/A Plate N/A	N/A N/A N/A 0.9 N/A Plate N/A	0.4 0.01 39.4 0.7 N/A Plate N/A	0.8 0.02 52.0 0.9 1.1 Plate N/A	0.03 61.2 1.0 0.9 Plate N/A	0.24 79.9 4.5 0.4 Overflow Weir 1 0.2	0.47 96.6 11.4 0.6 Overflow Weir 1 0.6	0.78 119.8 20.5 0.6 Spillway 0.9	1.76 186.8 97.9 1.3 Spillway 1.0
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A N/A N/A N/A 0.4 N/A Plate N/A N/A	N/A N/A N/A 0.9 N/A Plate N/A N/A	0.4 0.01 39.4 0.7 N/A Plate N/A N/A	0.8 0.02 52.0 0.9 1.1 Plate N/A N/A	0.03 61.2 1.0 0.9 Plate N/A N/A	0.24 79.9 4.5 0.4 Overflow Weir 1 0.2 N/A	0.47 96.6 11.4 0.6 Overflow Weir 1 0.6 N/A	0.78 119.8 20.5 0.6 Spillway 0.9 N/A	1.76 186.8 97.9 1.3 Spillway 1.0 N/A
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	N/A N/A N/A N/A 0.4 N/A Plate N/A N/A 38	N/A N/A N/A 0.9 N/A Plate N/A N/A 74	0.4 0.01 39.4 0.7 N/A Plate N/A N/A 65	0.8 0.02 52.0 0.9 1.1 Plate N/A N/A 73	0.03 61.2 1.0 0.9 Plate N/A N/A 79	0.24 79.9 4.5 0.4 Overflow Weir 1 0.2 N/A 84	0.47 96.6 11.4 0.6 Overflow Weir 1 0.6 N/A 83	0.78 119.8 20.5 0.6 Spillway 0.9 N/A 82	1.76 186.8 97.9 1.3 Spillway 1.0 N/A 76
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	N/A N/A N/A N/A 0.4 N/A Plate N/A N/A N/A 38 40	N/A N/A N/A 0.9 N/A Plate N/A N/A 74 78	0.4 0.01 39.4 0.7 N/A Plate N/A N/A 65 68	0.8 0.02 52.0 0.9 1.1 Plate N/A N/A 73 77	0.03 61.2 1.0 0.9 Plate N/A N/A 79 84	0.24 79.9 4.5 0.4 Overflow Weir 1 0.2 N/A	0.47 96.6 11.4 0.6 Overflow Weir 1 0.6 N/A	0.78 119.8 20.5 0.6 Spillway 0.9 N/A	1.76 186.8 97.9 1.3 Spillway 1.0 N/A 76 87
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Auflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	N/A N/A N/A N/A 0.4 N/A Plate N/A N/A 38	N/A N/A N/A 0.9 N/A Plate N/A N/A 74	0.4 0.01 39.4 0.7 N/A Plate N/A N/A 65	0.8 0.02 52.0 0.9 1.1 Plate N/A N/A 73	0.03 61.2 1.0 0.9 Plate N/A N/A 79	0.24 79.9 4.5 0.4 Overflow Weir 1 0.2 N/A 84 90	0.47 96.6 11.4 0.6 Overflow Weir 1 0.6 N/A 83 90	0.78 119.8 20.5 0.6 Spillway 0.9 N/A 82 89	1.76 186.8 97.9 1.3 Spillway 1.0 N/A 76



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate progra

г		verride the calcu								
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.64	0.06	3.20
-	0:15:00	0.00	0.00	5.66	9.19	11.41	7.68	9.48	9.37	15.23
-	0:20:00	0.00	0.00	19.11	24.72	29.00	18.23	21.11	22.81	33.20
-	0:25:00	0.00	0.00	37.00	49.38	60.10	36.67	41.73	45.18	69.52
	0:30:00	0.00	0.00	39.40	52.03	61.16	76.89	94.01	108.19	173.19
-	0:40:00	0.00	0.00	32.97 27.10	42.49 34.15	49.49 39.65	79.88 69.44	96.63 84.01	119.78 103.39	186.79 161.36
-	0:45:00	0.00	0.00	21.04	27.13	31.70	55.59	66.87	85.63	134.48
-	0:50:00	0.00	0.00	17.15	22.76	26.07	45.35	54.02	68.14	107.93
·	0:55:00	0.00	0.00	14.28	18.76	21.73	35.78	42.31	54.61	86.75
	1:00:00	0.00	0.00	11.78	15.36	18.03	28.72	33.64	45.15	71.94
-	1:05:00	0.00	0.00	9.95	12.80	15.20	23.18	26.91	37.49	60.07
_	1:10:00	0.00	0.00	8.10	11.54	14.02	17.52	19.99	26.37	41.37
	1:15:00	0.00	0.00	7.10	10.53	13.66	14.62	16.58	20.06	31.05
-	1:20:00	0.00	0.00	6.54	9.58	12.55	12.19	13.76	15.05	22.85
-	1:25:00	0.00	0.00	6.21	8.96	10.97	10.74	12.09	11.87	17.59
-	1:30:00 1:35:00	0.00	0.00	6.02	8.55	9.91	9.22	10.37	10.04	14.57
	1:40:00	0.00	0.00	5.88 5.78	8.31 7.32	9.19 8.72	8.25 7.63	9.28 8.58	8.80 8.01	12.53 11.21
-	1:45:00	0.00	0.00	5.73	6.61	8.41	7.03	8.11	7.53	10.42
-	1:50:00	0.00	0.00	5.72	6.15	8.19	6.98	7.85	7.36	10.42
-	1:55:00	0.00	0.00	4.78	5.84	7.78	6.84	7.69	7.28	10.08
ľ	2:00:00	0.00	0.00	4.11	5.44	6.97	6.77	7.62	7.28	10.08
-	2:05:00	0.00	0.00	2.72	3.60	4.63	4.50	5.05	4.84	6.69
	2:10:00	0.00	0.00	1.73	2.30	2.98	2.91	3.27	3.13	4.31
-	2:15:00	0.00	0.00	1.10	1.44	1.89	1.85	2.08	1.98	2.72
-	2:20:00	0.00	0.00	0.64	0.87	1.13	1.12	1.25	1.19	1.63
-	2:25:00	0.00	0.00	0.36	0.53	0.67	0.68	0.76	0.72	0.98
-	2:30:00 2:35:00	0.00	0.00	0.16	0.27	0.33	0.35	0.39	0.36	0.49
-	2:40:00	0.00	0.00	0.06	0.10	0.11 0.01	0.13 0.01	0.14 0.01	0.13	0.16
-	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00 3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5.55.00									

TOTAL FOREBAY VOLUME

V=3% x WQCV

WQCV=	0.801 ac-ft	_
V=	0.0240 ac-ft	

Qin NE=	71 cfs
Qin E=	44.1 cfs
Qtotal=	115.1 cfs

NORTHEAST FOREBAY VOLUME

71	cfs	=	x	ac-ft
115.1	cfs		0.0240	ac-ft

x =	0.0148	ac-ft
=	645.7	ft ³

EAST FOREBAY VOLUME

44.1	cfs	=	x	ac-ft
115.1	cfs		0.0240	ac-ft
x =	0.0	0092	ac-ft	
=	4	01.1	ft ³	

FOREBAY RELEASE NOTCH WIDTH

Q=CLH^{2/3}

Q ₁₀₀ =	71 cfs
2% of Q=	1.42 cfs
C=	2.6
H (height of forebay wall)=	1 ft
L=	7 in

FOREBAY RELEASE NOTCH WIDTH

Q=CLH^{2/3}

L=

Q ₁₀₀ =	44.1 cfs
2% of Q=	0.88 cfs
C=	2.6
H (height of forebay wall)=	1 ft

4 in

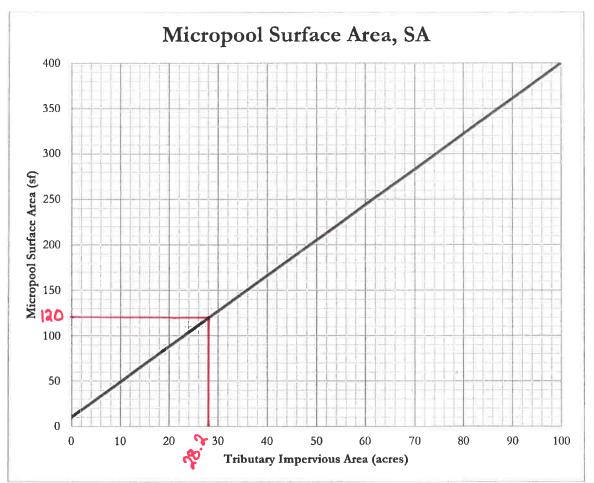


Figure 1 – Micropool surface area (SA) determination chart

The tributary impervious area is the effective number of impervious acres that will be treated by the extended detention basin (EDB). It is calculated by multiplying the tributary area to be treated by the $\frac{68}{100} \times 41.47 = 28.2$ ac impervious fraction of that area.

$$TIA = I \times A$$

- TIA = Tributary impervious area (acres)
- = Imperviousness (fraction) 1
- Α = Tributary catchment area upstream (acres)

For EDBs with tributary impervious areas greater than 100 acres, the micropool surface area is 400 sf. The initial surcharge depth (ISD) is defined as the depth of the initial surcharge volume (ISV). The surface area determined using Figure 1 assumes an ISD of 4 inches. The initial surcharge volume is thus calculated by multiplying the micropool surface area by 4 inches.

$$ISV = SA \times 4$$
 inches

= Surface area (from Figure 1, sf) SA

Worksheet Worksheet for Rectangular Channel

Concrete channel between existing homes

Project Description

-,	
Worksheet	Rectangular Chann
Flow Element	Rectangular Chann
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.016	
Slope	030000	ft/ft
Bottom Width	6.50	ft
Discharge	129.00	cfs

Results		
Depth	1.30	ft
Flow Area	8.4	ft²
Wetted Perime	9.09	ft
Top Width	6.50	ft
Critical Depth	2.30	ft
Critical Slope	0.005771	ft/ft
Velocity	15.30	ft/s
Velocity Head	3.64	ft
Specific Enerç	4.93	ft
Froude Numb	2.37	
Flow Type	upercritical	

Cross Section Cross Section for Irregular Channel

Depth of flow just past DP-O4

Project Description	
Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formul
Solve For	Channel Depth
Section Data	
Mannings Coefficier	0.016
Slope	0.012500 ft/ft

0.44 ft

21.1 cfs

.00 to 0.66

Water Surface Eleva

Elevation Range

Discharge

0.70		<u></u>			
0.00 -0+10	-0+05	0+00	0+05	0+10	0+15
					V:1 H:1 NTS

Worksheet Worksheet for Irregular Channel

Project Description	
Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formul
Solve For	Channel Depth

Input Data

Slope 012500 ft/ft Discharg 21.1 cfs

Options

Current Roughness Methoved Lotter's Method Open Channel Weighting vved Lotter's Method Closed Channel Weighting Horton's Method

Results		
Mannings Coefficie	0.016	
Water Surface Elev	0.44	ft
Elevation Range).00 to 0.66	
Flow Area	4.4	ft²
Wetted Perimeter	14.79	ft
Top Width	14.44	ft
Actual Depth	0.44	ft
Critical Elevation	0.55	ft
Critical Slope	0.005493	ft/ft
Velocity	4.59	ft/s
Velocity Head	0.33	ft
Specific Energy	0.77	ft
Froude Number	1.48	
Flow Type	Supercritical	

Calculation Messages:

Water elevation exceeds lowest end station by 0.16394137 ft.

Roughness Segments				
Start Station	End Station	Mannings Coefficient		
-0+09	-0+01	0.020		
-0+01	0+14	0.016		
		_		
Natural Ch	annel Poin	ts		
Station (ft)	Elevation (ft)			
-0+09	0.6	6		
-0+01	0.5	0		
0+00	0.0	0		
0+14	0.2	8		

