

# FINAL DRAINAGE REPORT FOR BRADLEY POINT FILING NO. 1

## EL PASO COUNTY, COLORADO

DECEMBER 2022

**PCD-ENGINEERING REVIEW COMMENTS  
IN BLUE BOXES WITH BLUE TEXT**

Prepared for:

**Stephen J. Schnurr  
Bradley Point, LLC  
2010 Fox Mountain Point  
Colorado Springs, CO 80906  
(719) 491-3101**

Prepared by:



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Colorado Springs, CO 80903  
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Project #70-074  
PCD Project # MS-21-002

Remove "Preliminary" and update accordingly on all pages.

**PRELIMINARY/FINAL DRAINAGE REPORT FOR  
BRADLEY POINT FILING NO. 1**

**DRAINAGE PLAN STATEMENTS**

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin.

[Redacted signature]

\_\_\_\_\_  
Virgil A. Sanchez, P.E. #37160  
For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

[Redacted signature]

BY: \_\_\_\_\_  
Stephen J. Schnurr

TITLE: \_\_\_\_\_  
DATE: \_\_\_\_\_

ADDRESS: Stephen J. Schnurr  
2010 Fox Mountain Point  
Colorado Springs, CO 80906

EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
Jennifer Irvine, P.E.  
County Engineer / ECM Administrator

At time of final submittal replace "Jennifer Irvine, P.E." with "Joshua Palmer, P.E.". Include signatures and stamps from engineer and developer.

**PRELIMINARY/FINAL DRAINAGE REPORT FOR  
BRADLEY POINT FILING NO. 1**

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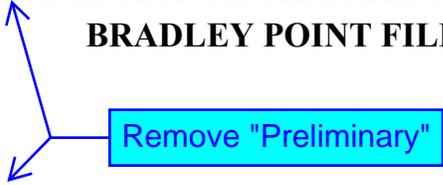
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# PRELIMINARY/FINAL DRAINAGE REPORT FOR BRADLEY POINT FILING NO. 1

## PURPOSE



This document is the Preliminary/Final Drainage Report for Bradley Point Filing No. 1. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual.

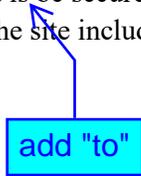
## GENERAL LOCATION AND DESCRIPTION

“Bradley Point Filing No. 1” refers to the subdivision of two parcels, 6503-40-0038 and 6503-40-0040. Bradley Point Filing No. 1 is located within the southeast and northwest quarters of the southeast quarter of Section 3, Township 15 south, Range 66 West, of the 6th Principal Meridian, El Paso County, Colorado. The site boundary is defined by Highway 85/87 on the southwestern boundary, Parcel 1 of the Rocky Mountain Materials and Asphalt Exemption Plat Map – Rec. No. 211713132 on the northwestern boundary, A.T. & S.F. Railroad Right of Way on the northeastern boundary, and unplatted land – Book 2780, Page 119, Schedule No. 65112-00-001 on the southeastern boundary. Bradley Point Filing No. 1 lies within the Little Johnson Drainage Basin. Flows from this site are tributary the US 85-87 corridor and ultimately tributary to Fountain Creek.

Bradley Point Filing No. 1 consists of 9.736 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Approximately 23.5% of the site is covered in an aggregate base coarse material. Existing site terrain generally slopes from northwest to southeast at grade rates that vary between 0.7% and 10.4%. An existing dirt access road runs along the southwestern edge of the railroad. One end terminates at the fence along the northwestern boundary of the project site, while the other end terminates as it meets the asphalt road of the project site.

Bradley Point Filing No. 1 is currently zoned M for industrial use. The purpose of development is to provide secure materials storage and parking. The development is to be secured via a perimeter fence and controlled access gate. Additional improvements proposed for the site include paving for an internal access entrance and storm drainage improvements for both lots.

## SOILS



Soils for this project are delineated by the Soils Map in the appendix as Blakeland Loamy Sand (8) and Nunn Clay Loam (59). Blakeland Loamy Sand is characterized as Hydrologic Soil Type "A", and comprises approximately 99.3% of the site. The remaining 0.7% on the southern corner of the site consists of the Nunn Clay Loam, which is characterized as Hydrologic Soil Group C. Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". Natural vegetation is sparse, consisting of native grasses and weeds over a majority of the site. Approximately one quarter of the site is covered with an aggregate base material.

## HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

## HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

## FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0744 G, effective date December 7<sup>th</sup>, 2018. A copy of this panel can be found in the appendix.

## DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the ECM, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates). Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method.

## EXISTING DRAINAGE CONDITIONS

The Bradley Point Filing No. 1 site consists of 9.736 Drainage Basin. This area was previously studied in the "Little Johnson/Security Creek Drainage Basin Planning Study" (DBPS), dated April 1988, and prepared by Simons, LLI & Associates, Inc., in cooperation with Kiowa Engineering Corporation.

### Design Point 1

**Basin A** consists of 4.65 undeveloped acres of moderately sparse natural grasses and vegetation, and is comprised of the northwestern half of the overall site. Runoff produced within **Basin A** is anticipated to reach peak runoff rates of  $Q_5=6.0$  cfs and  $Q_{100}=15.5$  cfs, and will flow east towards the **DP1**, where it collects in a localized depression. Runoff reaching **DP1**, continues east and discharges into Lot 2 (**Basin B**). Any delays in routing potentially caused by intermittent ponding are not considered by this analysis.

### **Design Point 2**

**Basin B** consists of 1.27 undeveloped acres of extremely sparse vegetation growing through a semi-compacted base material, located near the center of the site. Runoff produced within **Basin B** is anticipated to reach peak runoff rates of Q5=2.1 cfs and Q100=4.9 cfs, which will collect with runoff from **Design Point 1** to reach combined peak flow rates of Q5=6.7 and Q100=16.8 cfs. This flow naturally continues south towards the design point, where it collects in the roadside ditch and is redirected southeast towards downstream infrastructure.

### **Design Point 3**

**Basin C** consists of 1.39 undeveloped acres, approximately 60% of which is extremely sparse vegetation growing through an aggregate base material, while the rest of the basin consists of moderately sparse natural grasses and vegetation. This basin is situated near the center of the site. Runoff produced within **Basin C** is anticipated to reach peak runoff rates of Q5=1.8 cfs and Q100=4.7 cfs, and will flow south towards the **DP3**, where it will be redirected south east via the roadside ditch.

### **Design Point 4**

**Basin D** consists of 1.82 undeveloped acres, approximately 30% of which is extremely sparse vegetation growing through an aggregate base material, while the rest of the basin consists of sparse natural grasses and vegetation. This basin is situated on the southeastern side of the site. Runoff produced within **Basin D** flows from north to south, collecting in a localized depression at the design point, and is anticipated to reach peak runoff rates of Q5=2.4 cfs and Q100=6.1 cfs.

### **Design Point 5**

Offsite **Basin E** consists of 5.53 acres, which is located to the northwest of the site, consisting of a portion of sparse natural grasses and vegetation within the borrow ditch and northern half of the existing asphalt paved US Highway 85/87. Peak runoff rates from **Basin E** reach Q5=6.5 cfs and Q100=16.2 cfs. **Basin E2** consists of approximately 1.08 acres of the northern half of existing Highway 85/87, located immediately adjacent to the southwest of the site. Approximately half of **Basin E2** consists of an asphalt paved roadway surface, and the other half consists of sparse natural grasses and vegetation, reaching peak runoff rates of Q5=1.8 cfs and Q100=4.2 cfs. Runoff produced within **Basin E** and **Basin E2** will combine and flow east towards **Design Point 5**. Runoff at **DP5** is anticipated to reach peak runoff rates of Q5=6.7 cfs and Q100=16.5 cfs.

### **Design Point 6**

**Basin F** consists of approximately 0.45 acres of the northern half of existing Highway 85/87, and is located on the south end of the site. A majority of this basin consists of an asphalt paved roadway surface, while a small portion consists of sparse natural grasses and vegetation. Runoff produced within **Basin F** is anticipated to reach peak runoff rates of Q5=1.4 cfs and Q100=2.6 cfs. Runoff from **DP2** and **DP5** combine with runoff from **Basin F** at **DP6**. This cumulative flow is expected to reach peak flow rates of Q5=13.1 and Q100=32.0 cfs.

### **Design Point 7**

**Basin G** consists of approximately 0.65 acres of the northern half of existing Highway 85/87, located along the southwest of the site. Approximately half of this basin consists of an asphalt paved roadway surface, and the other half consists of sparse natural grasses and vegetation. Runoff produced

within **Basin G** is anticipated to reach peak runoff rates of Q5=1.7 cfs and Q100=3.4 cfs. This runoff will discharge into the existing roadside ditch. At **DP7**, runoff from **Basin G** will combine with flows from **Design Point 3** and **Design Point 6**, and shall continue within the existing roadside ditch. The cumulative flow is expected to reach rates of Q5=13.5 and Q100=32.7 cfs. A cross section of the existing ditch with 100 year event flows can be viewed on the Existing Drainage Map.

## FOUR STEP PROCESS

**Step 1 Reduce runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable.** An aggregate base material is proposed as the ground cover to minimize directly connected impervious areas from the proposed paved road. This material also serves the purpose of eliminating unnecessary impervious area (pavement) and encouraging infiltration.

Delete or revise regarding 100-year volume

**Step 2 Treat and Slowly Release the WQCV.** – Two infiltration detention facilities are planned collect and slowly discharge runoff by infiltration. The water quality capture volume is intended to slowly drain in approximately 12 hours within 97% of the 100 year event to drain in less than 120 hours.

State the types of BMP

Porous Landscape Detention (PLDs) or Sand Filter Basins (SFBs)?

**Step 3 Stabilize Stream Channels.** – With implementation of the two detention facilities, the runoff from the proposed industrial development will be significantly reduced to below predevelopment conditions. The developed discharge on and off the site is less than existing and, therefore, is not anticipated to have negative effects on downstream drainageways.

PLD/SFB??

**Step 4 Implement Source Controls.** – The proposed project will use silt fences, vehicle tracking control pads, straw bale barriers, outlet protection, temporary sediment basins, erosion control blankets, and reseeded to mitigate the potential for erosion across the site and protect downstream waters.

## PROPOSED DRAINAGE CHARACTERISTICS

### General Concept Drainage Discussion

The following is a description of the onsite basins, offsite flows and the overall drainage characteristics for the development of Bradley Point Filing No. 1. The development of Bradley Point Filing No. 1 consists converting the two existing undeveloped lots into two distinct storage parking areas, one with a paved entrance. A shared access easement will be provided from the primary access, within Lot 1 to the southern second lot. At the request of the developer, the internal surface runoff from each lot will be routed its own onsite infiltration pond. This type of treatment has proved a suitable solution for the parcel located upstream from this subject site.

Specifically surface runoff will be collected and conveyed by swales located along the perimeter of the parcels and ponds. Flows conveyed by the swales which will direct runoff to low points and proposed 24" RCP culverts which will convey runoff to the bottom of the ponds. Riprap stilling basins will be provided at the outfall of the system as would be constructed in a sand filter pond. These facilities will be detailed and designed within the subsequent drainage report update to accompany the final plat submittal.

Designed in this report?

The following detailed drainage discussion provides an overview of the proposed development. Surface flow is designated as Design Points (DP). Captured flow within the storm sewer system is designated as Pipe Runs (PR).

## Detailed Drainage Discussion

### Design Point 1

**Basin A** consists of 4.47 acres of gravel parking lot/storage area, including a portion of a proposed paved road and is comprised of the northeastern half of this site. Runoff produced within **Basin A** is anticipated to reach peak runoff rates of  $Q_5=9.9$  cfs and  $Q_{100}=19.7$  cfs, and will flow from north to south towards the design point as sheet flow over lot and following a proposed swale. The proposed swale to the western boundary of the basin conveys runoff to a forebay with a rip rap level spreader structure, to dissipate energy and approximate existing flow conditions, and the runoff continues east into a proposed infiltration **Pond 1** through a 24" PVC storm pipe.

verify material

### Design Point 2

**Basin B** consists of 4.17 acres of gravel parking lot/storage area. This basin is located within the southeastern half of the site. Runoff will be conveyed as sheet flow over lot and following a proposed swale. The proposed swale to the southern boundary of the basin conveys runoff to a forebay with a rip rap level spreader structure, to dissipate energy and approximate existing flow conditions, and the runoff continues east into a proposed infiltration **Pond 2** through a 24" PVC storm pipe. Runoff produced within **Basin B** generally flows north to south and is anticipated to reach peak runoff rates of  $Q_5=9.0$  cfs and  $Q_{100}=18.0$  cfs at the proposed infiltration **Pond 2**. Runoff rates are less than existing flows.

### Design Point 3

**Basin E** consists of 5.53 acres which is located to the northwest of the site, consisting of a portion of sparse natural grasses and vegetation within the borrow ditch and northern half of the existing asphalt paved US Highway 85/87. This basin is situated on the northwestern portion of the site. Runoff from this basin flows north to south onsite. See existing **Basin E** conditions. Runoff produced within **Basin E** is anticipated to reach peak runoff rates of  $Q_5=6.5$  cfs and  $Q_{100}=16.2$  cfs, and will combine with flows from **Basin F**. **Basin F** consists of 0.72 acres of the northern half of existing Highway 85/87, located to the southwest of the site. Approximately half of this basin consists of an asphalt paved roadway surface, and the other half consists of sparse natural grasses and vegetation. Runoff produced within **Basin F** is anticipated to reach peak runoff rates of  $Q_5=1.4$  and  $Q_{100}=3.0$  cfs, and will flow east from the crown of the road where it discharges into the existing roadside ditch and combines with runoff from **Basin E**. The flows are redirected southeast towards the design point at peak runoff rates of  $Q_5=6.6$  and  $Q_{100}=16.0$  cfs. From here, the runoff will continue southeast to downstream infrastructure

### Design Point 4

**Basin G** consists of approximately 2.28 acres of the northern half of existing Highway 85/87, located to the southwest of the site. Approximately half of this basin consists of an asphalt paved roadway surface, and the other half consists of sparse natural grasses and vegetation. Runoff produced within **Basin G** is anticipated to reach peak runoff rates of  $Q_5=4.0$  cfs and  $Q_{100}=8.8$  cfs. At this point, the runoff will combine with flows from **Design Point 3** and will continue southeast. This flow will run east from the crown of the road in order to discharge into the existing roadside ditch. A cross section of the roadside

ditch at this point can be viewed on the Proposed Drainage Map, depicting what is experienced during the 100 year event. This cumulative flow is expected to reach rates of Q5=7.4 and Q100=17.5 cfs. Flows to the ditch have been reduced by not quite half from that of the existing condition (Q5=13.5 and Q100=32.7 cfs). As the roadside ditch flattens out near the corner of the subject site, the collected runoff will dissipate into sheet flow and be directed east towards an offsite 18” ADS culvert that drains into the existing railroad ditch. This conveyance process can be seen on the Roadside Ditch Conveyance Exhibit in the Appendix.

**WATER QUALITY AND DETENTION**

Please clarify type of pond. Previous section mentioned a sand filter basin.

Two **Private Infiltration Ponds** are proposed for this site in order to reduce the fully developed flows from the site to pre-development levels and address water quality. The ponds have been sized utilizing the StormShed 4G program with the outlet being infiltration only. The ponds have been sized to store the WQCV, EURV, and the flood control volumes for the 2, 5, 10, 25, 50, and 100 year storm events. Based upon contributing area of 4.47 acres and watershed imperviousness is 82% for Pond 1 and a contributing area of 4.17 acres and 80% imperviousness for Pond 2. The WQCV for both ponds will be slowly released over approximately 12-12.5 hours. The 100 year storm events will drain fully in less than 120 hours. The maximum 100-Yr storage volume is 0.626 acre-feet (27,287.79 cf) for Pond 1 and 0.578 acre-feet (25,163.86 cf) for Pond 2, resulting in maximum ponding depths of 4.880 feet and 4.615 feet respectively. Each pond has a minimum of 2’ of freeboard and is capable of storing the 500 year storm event. Print outs of the model are included in the appendix. It is important to note that the parcel to the northwest is currently utilizing a similarly constructed facility to detain onsite runoff.

**EROSION CONTROL**

Address infiltration test results.

How do these compare to MHFD calculations (SDI sheets)?

It is the policy of the El Paso County that M&S Civil Consultants, Inc submits an erosion control plan with the drainage report. Proposed straw bale barriers, silt fence, vehicle traffic control, a temporary sediment basin, permanent erosion control fabric, and reseeding are proposed as erosion control measures. The proposed development will not adversely impact the existing surrounding industrial infrastructure.

**CONSTRUCTION COST OPINION – BRADLEY POINT FILING NO. 1**

State the total land disturbance. Discuss Appendix I requirements and applicable permits.

**Private Drainage Facilities:**

Item	Description	Quantity	Unit Cost	Cost
1.	24" RCP	80 LF	\$125 /LF	\$10,000
2.	Infiltration Pond	2 EA	\$8,000 /EA	\$16,000
3.	Forebay	2 EA	\$5,000 /EA	\$10,000
<b>Total \$</b>				<b>\$36,000</b>

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2021.

**DRAINAGE & BRIDGE FEES – BRADLEY POINT FILING NO. 1**

This site is within the Little Johnson Drainage Basin. The 2021 Drainage and Bridge Fees per El Paso County for the Bradley Point Filing No. 1 site are as follows:

Per Bradley Point Filing No. 1 Site Boundary – **Total Area** **9.74 Acres**

**BRADLEY POINT FILING NO. 1 FEES:**

<b>Drainage Fees:</b>	9.736	x	81.0%	x	\$12,048	=	\$	<u>95,012.46</u>
							<b>Total</b>	<b>\$ 95,012.46</b>

It should be noted that these fees are provided in this Final Drainage Report for informational purposes only. ↖ The fees are due with plat recording, not information only.

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2021.

**SUMMARY**

Development of this site will not adversely affect the surrounding developments per this final drainage report. The proposed drainage facilities will adequately convey, detain and route runoff from tributary and onsite flows to the Fountain Creek Drainage Channel via proposed onsite improvements. A Full Spectrum Detention pond will be used to discharge developed flows that approximate historic conditions onto the adjoining, vacant Rio Grande property to the southeast. This property discharges into the railroad ditch to the east, which eventually discharges into Fountain Creek. Proposed Flow rates are lower than existing. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. Overall, the development of the Bradley Point Filing No. 1 project shall not adversely affect adjacent or downstream property.

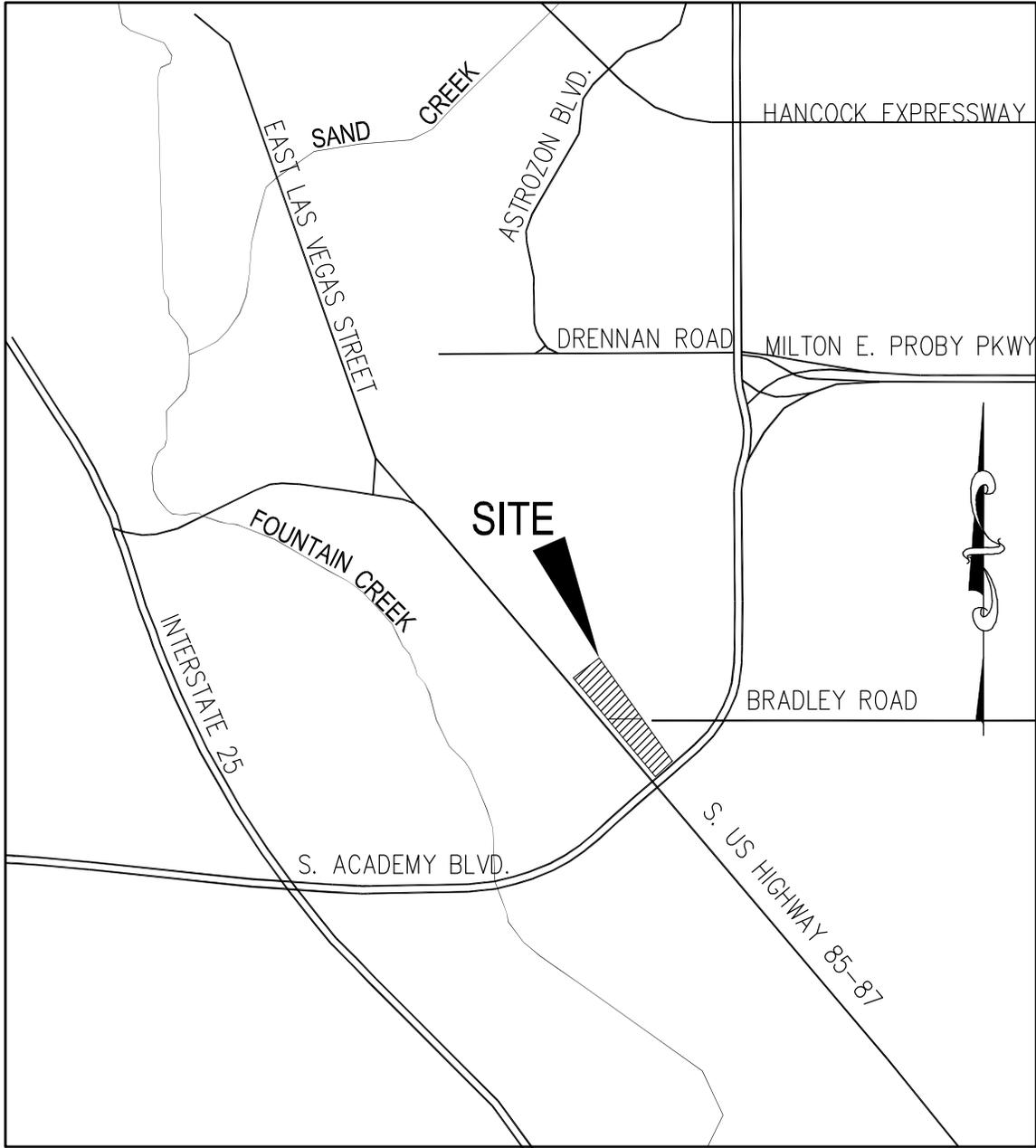
↖ adjoining property?

## REFERENCES

- 1.) "City of Colorado Springs Drainage Criteria Manual", Volumes 1 & 2, City of Colorado May 2014.
- 2.) Mile High Flood District (2021). Criteria Manual. "Urban Storm Drainage Criteria Manuals, Volumes 1-3". Retrieved from <https://mhfd.org/resources/criteria-manual/>
- 3.) NRSC Web Soil Survey Map for El Paso County. <http://websoilsurvey.nrcs.usda.gov>
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date December 7<sup>th</sup>, 2018.
- 5.) Simons, LLI & Associates, Inc., in cooperation with Kiowa Engineering Corporation (April 1988). "Little Johnson/Security Creek Drainage Basin Planning Study". Retrieved from <https://coloradosprings.gov/dbps>
- 6.) Colorado Aggregate Recycling (2021). Colorado Springs: Products. Retrieved From <https://www.coloradoaggregaterecycling.com/colorado-springs/>
- 7.) "El Paso County Drainage Criteria Manual", Volumes 1 & 2, Municode 2021.

## **APPENDIX**

**VICINITY MAP**

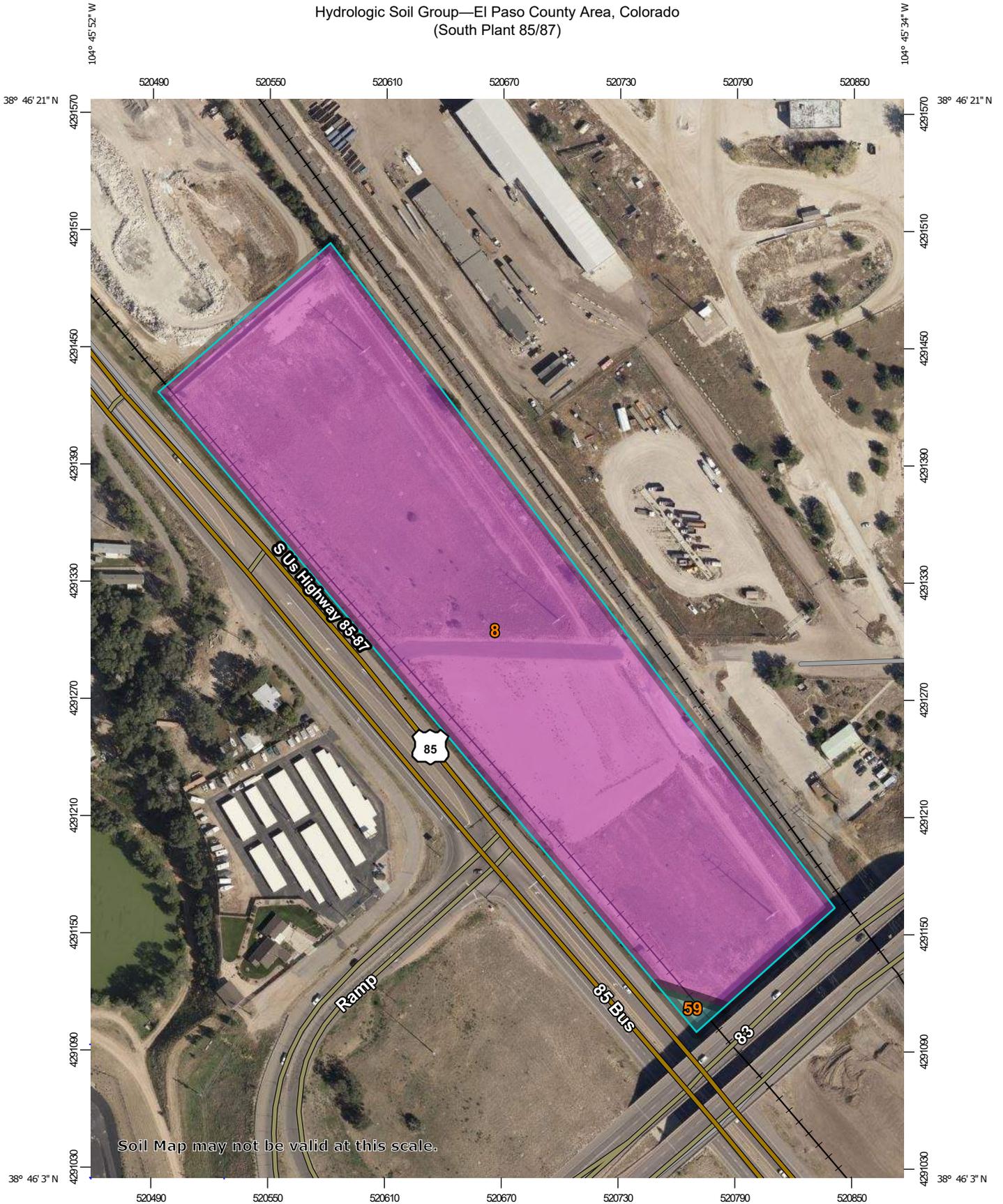


# VICINITY MAP

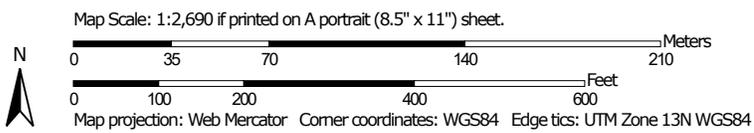
N.T.S.

## **SOILS MAP**

Hydrologic Soil Group—El Paso County Area, Colorado  
(South Plant 85/87)



Soil Map may not be valid at this scale.



## MAP LEGEND

### Area of Interest (AOI)

Area of Interest (AOI)

### Soils

#### Soil Rating Polygons

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

#### Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

#### Soil Rating Points

-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

### Water Features

 Streams and Canals

### Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	11.2	99.3%
59	Nunn clay loam, 0 to 3 percent slopes	C	0.1	0.7%
<b>Totals for Area of Interest</b>			<b>11.3</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### Rating Options

*Aggregation Method:* Dominant Condition

**FIRM PANEL**



## **HYDROLOGIC CALCULATIONS**

**BRADLEY POINT FILING NO. 1**  
**EXISTING CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Runoff Coefficient Summary)**

BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	STREETS/DEVELOPED			AGGREGATE BASE MATERIAL			UNDEVELOPED/LANDSCAPE			RUNOFF COEFFICIENT	
			AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
<i>A</i>	202348.4143	4.65	0.07	0.90	0.96	4.58	0.35	0.54	0.00	0.08	0.35	<b>0.36</b>	<b>0.55</b>
<i>B</i>	55366.9622	1.27	0.20	0.90	0.96	1.07	0.35	0.54	0.00	0.08	0.35	<b>0.44</b>	<b>0.61</b>
<i>C</i>	60455.3113	1.39	0.00	0.90	0.96	1.39	0.35	0.54	0.00	0.08	0.35	<b>0.35</b>	<b>0.54</b>
<i>D</i>	79161.6725	1.82	0.00	0.90	0.96	1.82	0.35	0.54	0.00	0.08	0.35	<b>0.35</b>	<b>0.54</b>
<i>E</i>	240799.7172	5.53	2.12	0.90	0.96	0.00	0.35	0.54	3.41	0.08	0.35	<b>0.39</b>	<b>0.58</b>
<i>E2</i>	46914.4055	1.08	0.50	0.90	0.96	0.00	0.35	0.54	0.58	0.08	0.35	<b>0.46</b>	<b>0.63</b>
<i>F</i>	19702.8045	0.45	0.35	0.90	0.96	0.00	0.35	0.54	0.10	0.08	0.35	<b>0.71</b>	<b>0.82</b>
<i>G</i>	28387.025	0.65	0.49	0.90	0.96	0.00	0.35	0.54	0.16	0.08	0.35	<b>0.70</b>	<b>0.81</b>

Calculated by: CVW  
Date: 12/7/2022  
Checked by: DLM

**BRADLEY POINT FILING NO. 1**  
**EXISTING CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Drainage Summary)**

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>STREET / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>		<b>INTENSITY *</b>		<b>TOTAL FLOWS</b>	
<b>BASIN</b>	<b>AREA TOTAL (Acres)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>C<sub>5</sub></b>	<b>Length (ft)</b>	<b>Height (ft)</b>	<b>T<sub>c</sub> (min)</b>	<b>Length (ft)</b>	<b>Slope (%)</b>	<b>Velocity (fps)</b>	<b>T<sub>t</sub> (min)</b>	<b>TOTAL (min)</b>	<b>CHECK (min)</b>	<b>I<sub>5</sub> (in/hr)</b>	<b>I<sub>100</sub> (in/hr)</b>	<b>Q<sub>5</sub> (c.f.s.)</b>	<b>Q<sub>100</sub> (c.f.s.)</b>
		<i>From DCM Table 5-1</i>															
<b>A</b>	4.65	0.36	0.55	0.36	100	2.75	9.6	613	0.9%	0.7	15.1	24.7	14.0	3.6	6.1	6.0	15.5
<b>B</b>	1.27	0.44	0.61	0.44	100	1.6	10.3	316	0.9%	1.0	5.5	15.8	12.3	3.8	6.4	2.1	4.9
<b>C</b>	1.39	0.35	0.54	0.35	100	1.4	12.1	417	1.1%	1.1	6.6	18.7	12.9	3.8	6.3	1.8	4.7
<b>D</b>	1.82	0.35	0.54	0.35	100	1.98	10.8	470	1.3%	0.8	9.7	20.5	13.2	3.7	6.2	2.4	6.1
<b>E</b>	5.53	0.39	0.58	0.39	30	0.6	5.6	2000	1.5%	0.9	38.7	44.2	21.3	3.0	5.0	6.5	16.2
<b>E2</b>	1.08	0.46	0.63	0.46	100	0.96	11.7	525	0.3%	0.8	10.8	22.5	13.5	3.7	6.2	1.8	4.2
<b>F</b>	0.45	0.71	0.82	0.71	75	1.06	5.4	298	0.7%	1.3	4.0	9.3	12.1	4.2	7.1	1.4	2.6
<b>G</b>	0.65	0.70	0.81	0.70	100	1.34	6.6	406	0.6%	1.1	5.9	12.5	12.8	3.8	6.4	1.7	3.4

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW \_\_\_\_\_

Date: 12/7/2022 \_\_\_\_\_

Checked by: DLM \_\_\_\_\_

please be sure and check intensity formula if you expand and add columns!!!

**BRADLEY POINT FILING NO. 1**  
**EXISTING CONDITIONS DRAINAGE CALCULATIONS**  
**(Basin Routing Summary)**

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>PIPE / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>		<b>INTENSITY*</b>		<b>TOTAL FLOWS</b>		COMMENTS
DESIGN POINT	CONTRIBUTING BASINS/PIPES	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>s</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)		
1	Basin A	1.66	2.54				14.0					14.0	3.6	6.1	6.0	15.5	LOCALIZED DEPRESSION	
					Basin A Tc was used													
2	Basin B Design Point 1	0.55 1.66	0.77 2.54				14.0	406	0.7%	1.1	7.0	20.9	3.0	5.1	6.7	16.8	EXITS SITE TO ROADSIDE DITCH	
		2.22	3.31		Design Pt 1 Tc was used													
3	Basin C	0.49	0.75				12.9					12.9	3.8	6.3	1.8	4.7	EXITS SITE TO ROADSIDE DITCH	
					Basin C Tc was used													
4	Basin D	0.64	0.98				13.2					13.2	3.7	6.2	2.4	6.1	LOCALIZED DEPRESSION	
					Basin D Tc was used													
5	Basin E2 Basin E	0.50 2.18	0.68 3.23				21.3	525	0.3%	1.1	8.1	29.4	2.5	4.2	6.7	16.5	EXISTING ROADSIDE DITCH	
		2.67	3.91		Basin E Tc was used													
6	Basin F Design Point 5 Design Point 2	0.32 2.67 2.22	0.37 3.91 3.31				29.4					29.4	2.5	4.2	13.1	32.0	EXISTING ROADSIDE DITCH	
		5.22	7.59		Design Point 5 Tc was used													
7	Basin G Design Point 6 Design Point 3	0.45 5.22 0.49	0.53 7.59 0.75				29.4	452	0.5%	1.1	7.0	36.3	2.2	3.7	13.5	32.7	EXISTING ROADSIDE DITCH	
		6.16	8.87		Design Pt 6 Tc was used													

Use the total Time of Travel, T<sub>t</sub>, from pg. 23 for existing conditions calculation not the T<sub>t</sub> check..

<b>Time of Travel (T<sub>t</sub>)</b>	
TOTAL (min)	CHECK (min)
24.7	14.0
15.8	12.3
18.7	12.9
20.5	13.2
44.2	21.3
22.5	13.5
9.3	12.1
12.5	12.8

**BRADLEY POINT FILING NO. 1**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Runoff Coefficient Summary)**

BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	STREETS/DEVELOPED			AGGREGATE BASE MATERIAL			UNDEVELOPED/LANDSCAPE			RUNOFF COEFFICIENT	
			AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
<i>A</i>	194500.7466	4.47	0.12	0.90	0.96	4.34	0.59	0.70	0.00	0.08	0.35	<b>0.60</b>	<b>0.71</b>
<i>B</i>	181766.1572	4.17	0.00	0.90	0.96	4.17	0.59	0.70	0.00	0.08	0.35	<b>0.59</b>	<b>0.70</b>
<i>E</i>	240799.7172	5.53	2.12	0.90	0.96	0.00	0.35	0.54	3.41	0.08	0.35	<b>0.39</b>	<b>0.58</b>
<i>F</i>	31224.2092	0.72	0.38	0.90	0.96	0.00	0.35	0.54	0.33	0.08	0.35	<b>0.52</b>	<b>0.68</b>
<i>G</i>	99495.0053	2.28	1.19	0.90	0.96	0.00	0.35	0.54	1.09	0.08	0.35	<b>0.51</b>	<b>0.67</b>

Calculated by: CVW  
Date: 12/7/2022  
Checked by: DLM

**BRADLEY POINT FILING NO. 1**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Drainage Summary)**

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>STREET / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>		<b>INTENSITY *</b>		<b>TOTAL FLOWS</b>	
<b>BASIN</b>	<b>AREA TOTAL (Acres)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>C<sub>5</sub></b>	<b>Length (ft)</b>	<b>Height (ft)</b>	<b>T<sub>c</sub> (min)</b>	<b>Length (ft)</b>	<b>Slope (%)</b>	<b>Velocity (fps)</b>	<b>T<sub>t</sub> (min)</b>	<b>TOTAL (min)</b>	<b>CHECK (min)</b>	<b>I<sub>5</sub> (in/hr)</b>	<b>I<sub>100</sub> (in/hr)</b>	<b>Q<sub>5</sub> (c.f.s.)</b>	<b>Q<sub>100</sub> (c.f.s.)</b>
		<i>From DCM Table 5-1</i>															
<b>A</b>	4.47	0.60	0.71	0.60	100	0.6	10.7	460	0.5%	1.5	5.2	15.9	13.1	3.7	6.2	9.9	19.7
<b>B</b>	4.17	0.59	0.70	0.59	100	0.6	10.9	540	1.1%	1.0	8.7	19.6	13.6	3.7	6.2	9.0	18.0
<b>E</b>	5.53	0.39	0.58	0.39	30	0.6	5.6	2000	1.5%	1.8	18.1	23.6	21.3	3.0	5.0	6.5	16.2
<b>F</b>	0.72	0.52	0.68	0.52	60	0.8	7.4	525	0.3%	0.8	11.3	18.7	13.3	3.7	6.2	1.4	3.0
<b>G</b>	2.28	0.51	0.67	0.51	60	1	7.0	985	0.4%	0.9	17.8	24.8	15.8	3.4	5.8	4.0	8.8

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW  
Date: 12/7/2022

Checked by: DLM

please be sure and check intensity formula if you expand and add columns!!!

**BRADLEY POINT FILING NO. 1**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Basin Routing Summary)**

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>PIPE / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>	<b>INTENSITY*</b>		<b>TOTAL FLOWS</b>		COMMENTS	
DESIGN POINT	CONTRIBUTING BASINS/PIPES	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>s</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)		
<b>1</b>	<b>Basin A</b>	2.67	3.16				13.1					13.1	3.7	6.2	<b>9.9</b>	<b>19.7</b>		PROPOSED CULVERT
					Basin A Tc was used													
<b>2</b>	<b>Basin B</b>	2.46	2.92				13.6					13.6	3.7	6.2	<b>9.0</b>	<b>18.0</b>	PROPOSED CULVERT	
					Basin B Tc was used													
<b>3</b>	<b>Basin E</b> <b>Basin F</b>	2.18 0.37	3.23 0.49				21.3	525	0.4%	1.3	6.9	28.2	2.6	4.3	<b>6.6</b>	<b>16.0</b>	ROADSIDE DITCH	
		2.55	3.71		Basin E Tc was used													
<b>4</b>	<b>Design Pt 3</b> <b>Basin G</b>	2.55 1.16	3.71 1.53				28.2	985	0.4%	1.2	13.3	41.5	2.0	3.3	<b>7.4</b>	<b>17.5</b>	ROADSIDE DITCH	
		3.71	5.24		Design Pt 3 Tc was used													

**BRADLEY POINT FILING NO. 1**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Storm Sewer Routing Summary)**

<i>PIPE RUN</i>	<i>Contributing Pipes/Design</i>	<i>Equivalent CA<sub>5</sub></i>	<i>Equivalent CA<sub>100</sub></i>	<i>Maximum T<sub>C</sub></i>	<i>Intensity*</i>		<i>Flow</i>	
					<i>I<sub>5</sub></i>	<i>I<sub>100</sub></i>	<i>Q<sub>5</sub></i>	<i>Q<sub>100</sub></i>
<b>PR 1</b>	<b>DESIGN POINT 1</b>	2.67	3.16	13.1	3.7	6.2	<b>9.9</b>	<b>19.7</b>
<b>PR 2</b>	<b>DESIGN POINT 2</b>	2.46	2.92	13.6	3.7	6.2	<b>9.0</b>	<b>18.0</b>

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 12/7/2022

Checked by: VAS

## **HYDRAULIC CALCULATIONS**

<b><i>Weighted Percent Imperviousness of Site to Pond 1</i></b>				
<b><i>Contributing Basins</i></b>	<b><i>Area (Acres)</i></b>	<b><i>C<sub>s</sub></i></b>	<b><i>*Impervious % (I)</i></b>	<b><i>(Acres)*(I)</i></b>
<b><i>A</i></b>	<b><i>4.47</i></b>	<b><i>0.60</i></b>	<b><i>82</i></b>	<b><i>366.14</i></b>
<b><i>Totals</i></b>	<b><i>4.47</i></b>			<b><i>366.14</i></b>
<b><i>Imperviousness to Infiltration Pond 1</i></b>	<b><i>82.0</i></b>			

**BRADLEY POINT FILING NO. 1**  
**DRAINAGE REPORT DRAINAGE CALCULATIONS**  
**(Pond Volume Calculation)**

**POND 1**

Elevation	SF	CF	Storage	
			AF	Sum
5777.00	3,863.00			0
5778.00	4,846.00	4,354.50	0.10	0.10
5779.00	5,885.00	5,365.50	0.12	0.22
5780.00	6,980.00	6,432.50	0.15	0.37
5781.00	8,133.00	7,556.50	0.17	0.54
5782.00	9,343.00	8,738.00	0.20	0.74
5783.00	10,650.00	9,996.50	0.23	0.97
5784.00	55,435.00	33,042.50	0.76	1.73
Total =		<u>75,486</u> CF		
			Total =	<u>1.733</u> Ac-ft

Calculated by: DLM  
Date: 5/3/2022  
Checked by: \_\_\_\_\_

<b>Weighted Percent Imperviousness of FSD Pond 1</b>				
<b>Contributing Basins</b>	<b>Area (Acres)</b>	<b>C<sub>s</sub></b>	<b>*Impervious % (I)</b>	<b>(Acres)*(I)</b>
<b>B</b>	4.17	0.59	80	333.82
<b>Totals</b>	<b>4.17</b>			<b>333.82</b>
<b>Imperviousness to Infiltration Pond 2</b>	<b>80.0</b>			

	1	2	1*2
<b>Total Site Imperviousness</b>	Ac	Imp	
Area 1	4.47	0.82	3.67 A
Area 2	4.17	0.8	3.34 B
Area 3			
Total	8.64		7.00 A+B
Site Imperviousness		7.00 / 8.64	0.81

**BRADLEY POINT FILING NO. 1**  
**DRAINAGE REPORT DRAINAGE CALCULATIONS**  
**(Pond Volume Calculation)**

**POND 2**

Elevation	SF	CF	Storage	
			AF	Sum
5772.00	3,316.00			0
5773.00	4,278.00	3,797.00	0.09	0.09
5774.00	5,299.00	4,788.50	0.11	0.20
5775.00	6,373.00	5,836.00	0.13	0.33
5776.00	7,505.00	6,939.00	0.16	0.49
5777.00	8,692.00	8,098.50	0.19	0.68
5778.00	9,954.00	9,323.00	0.21	0.89
5779.00	24,989.00	17,471.50	0.40	1.29
		Total =	<u>56,254</u> CF	
			Total =	<u>1.3</u> Ac-ft
#NUM!				
#NUM!				

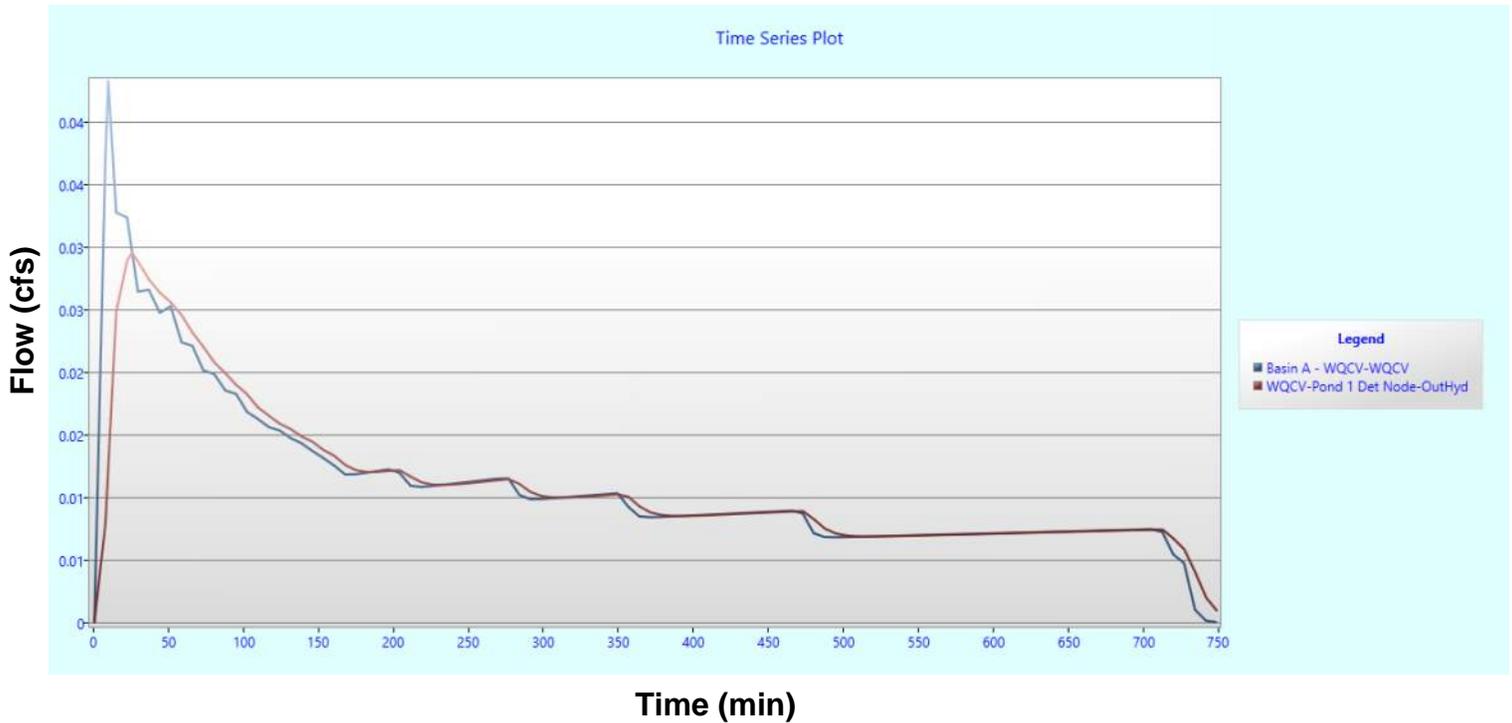
Calculated by: GT  
Date: 9/15/2020  
Checked by: \_\_\_\_\_

# StormSHED 4G Analyses

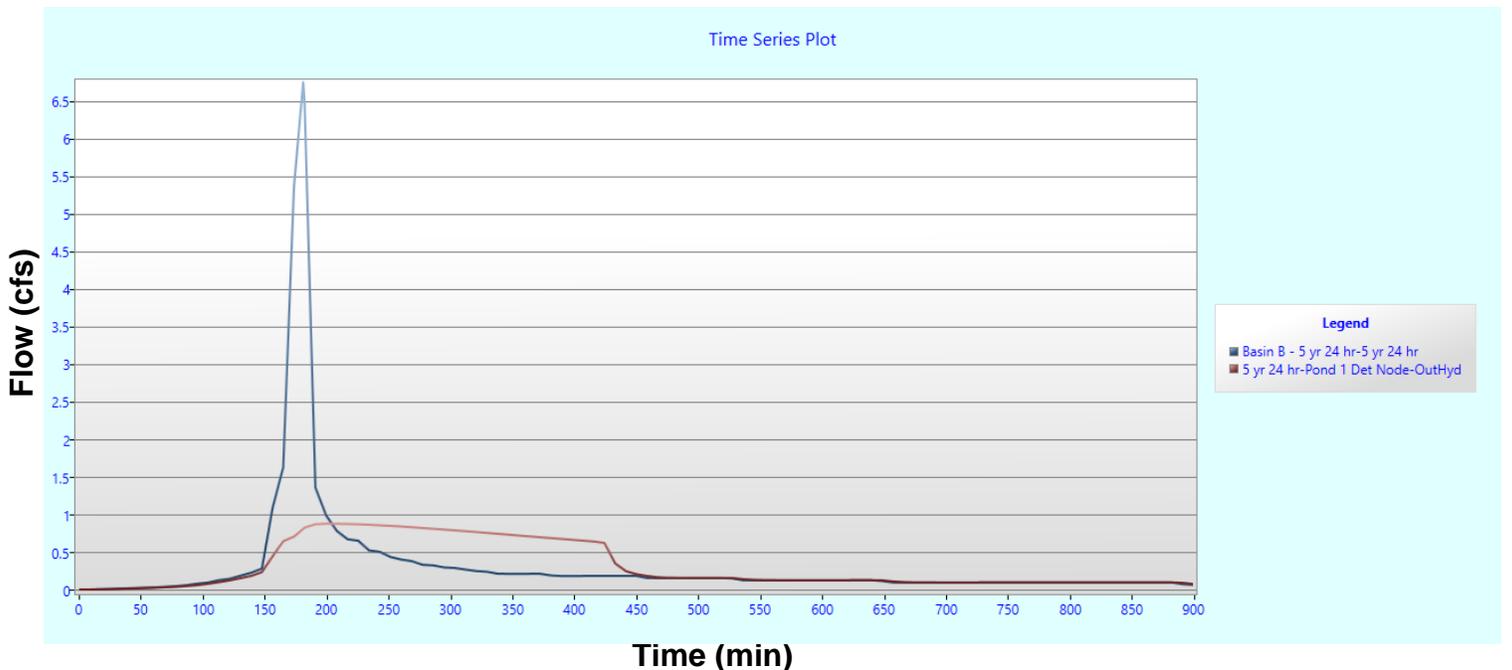
## North Pond Summary Table (POND 1)

Design Event	Match Flows (cfs)	Peak Q (cfs)	Max Depth (ft)	Vol (cf)	HtoE	% Vol
WQCV	0.0432	0.0295	0.0047	15.7203	0.01	99.92
5 yr 24 hr	6.7560	0.8970	1.6587	6,668.4623	0.01	99.99
100 yr 24 hr	20.4919	1.5600	4.8800	27,287.7935	0.12	99.95

## North Pond: WQCV Inflow and Outflow Hydrographs

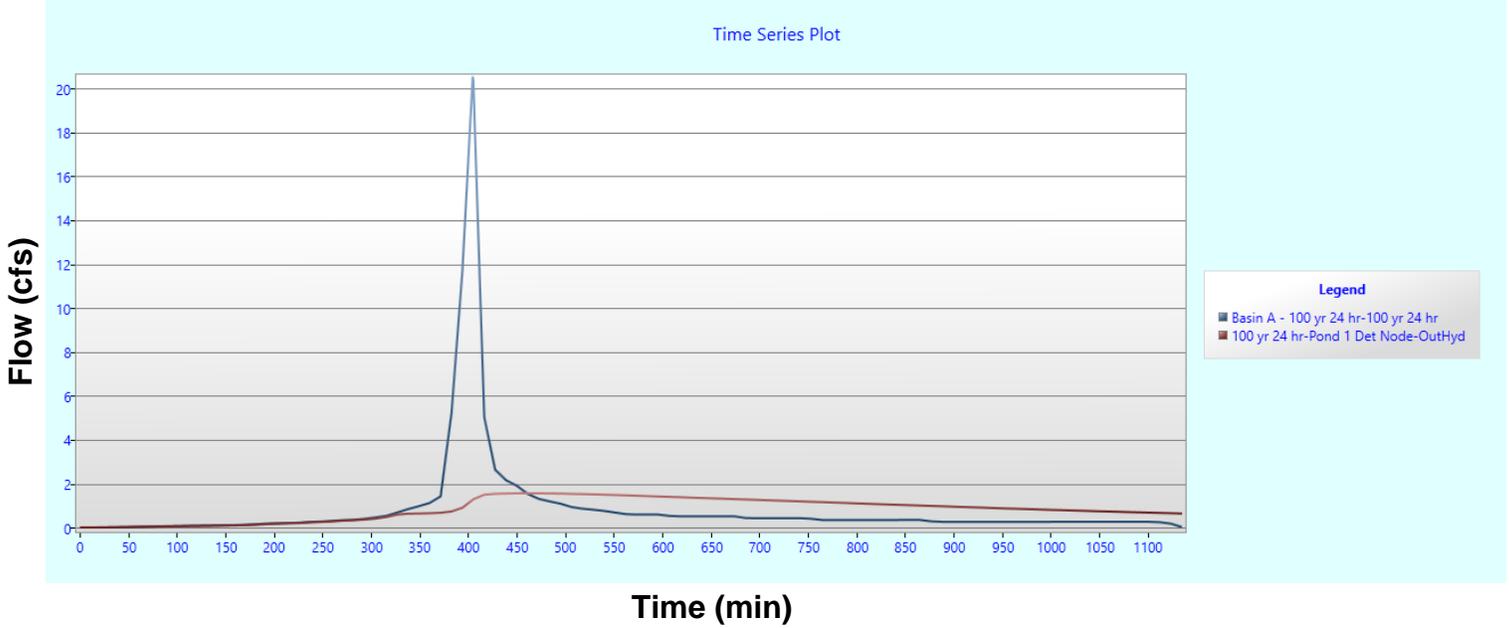


## North Pond: 5 YR Inflow and Outflow Hydrographs

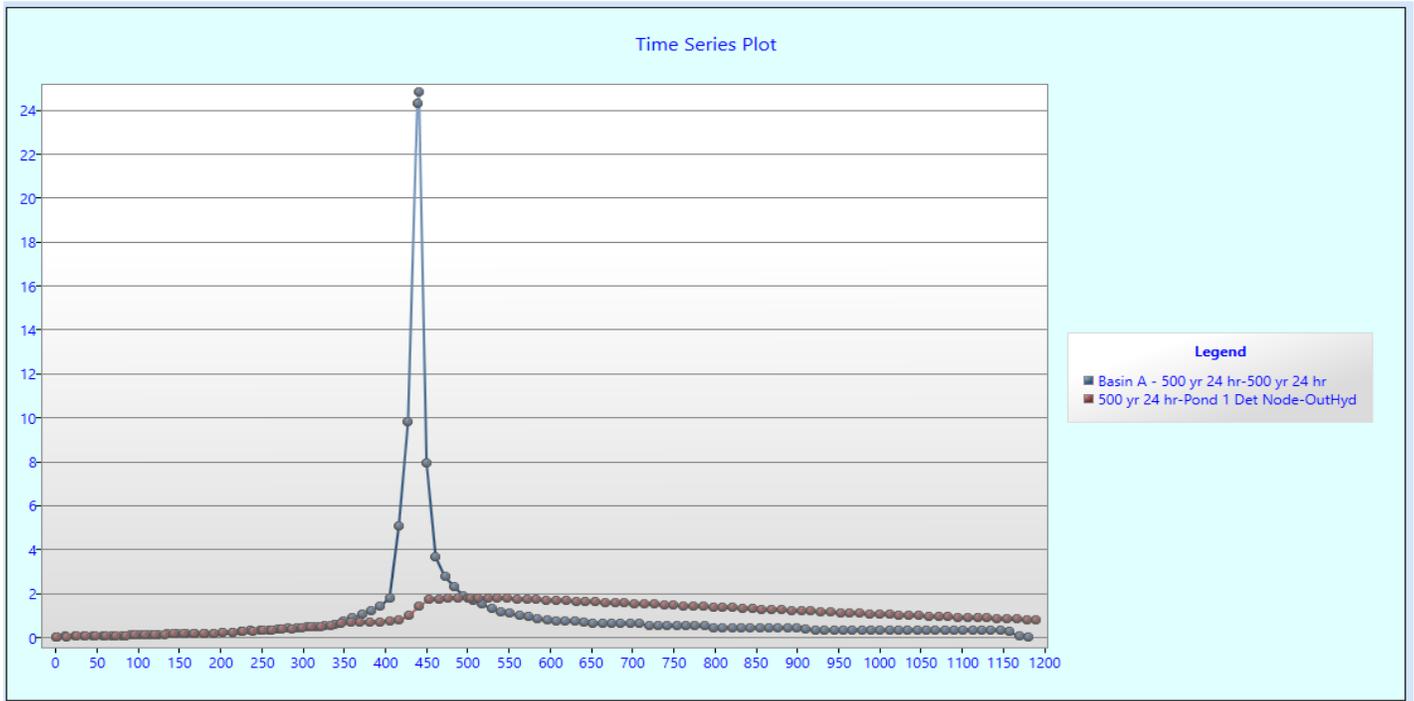


Address flows going through the spillway (overtopping) and flows being infiltrated. (See comment letter)

### North Pond: 100 YR Inflow and Outflow Hydrographs



### North Pond: 500 YR Inflow and Outflow Hydrograph and Summary Table

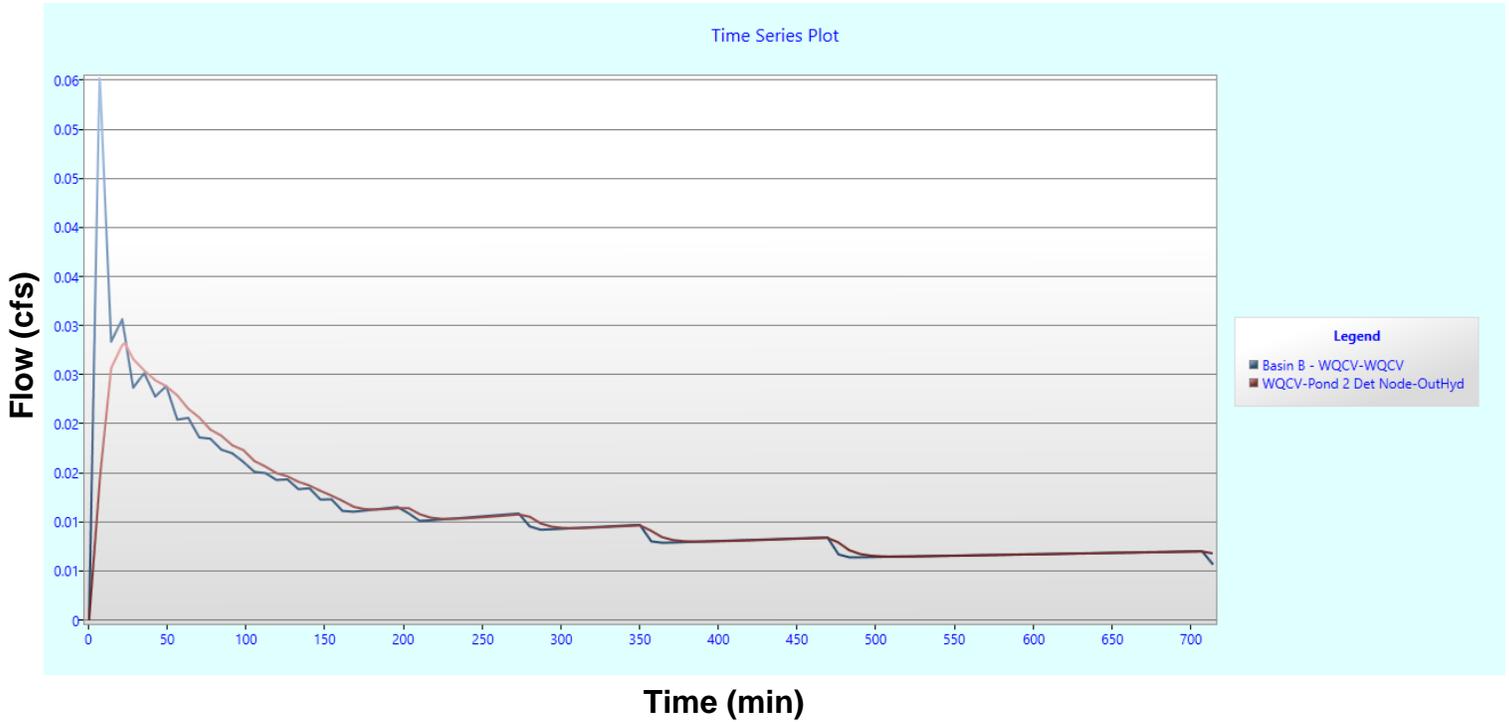


Design Event	Match Flows (cfs)	Peak Q (cfs)	Max Depth (ft)	Vol (cf)	HtoE	% Vol
500 yr 24 hr	24.7740	1.7555	5.7144	34,511.9753	1.42	99.96

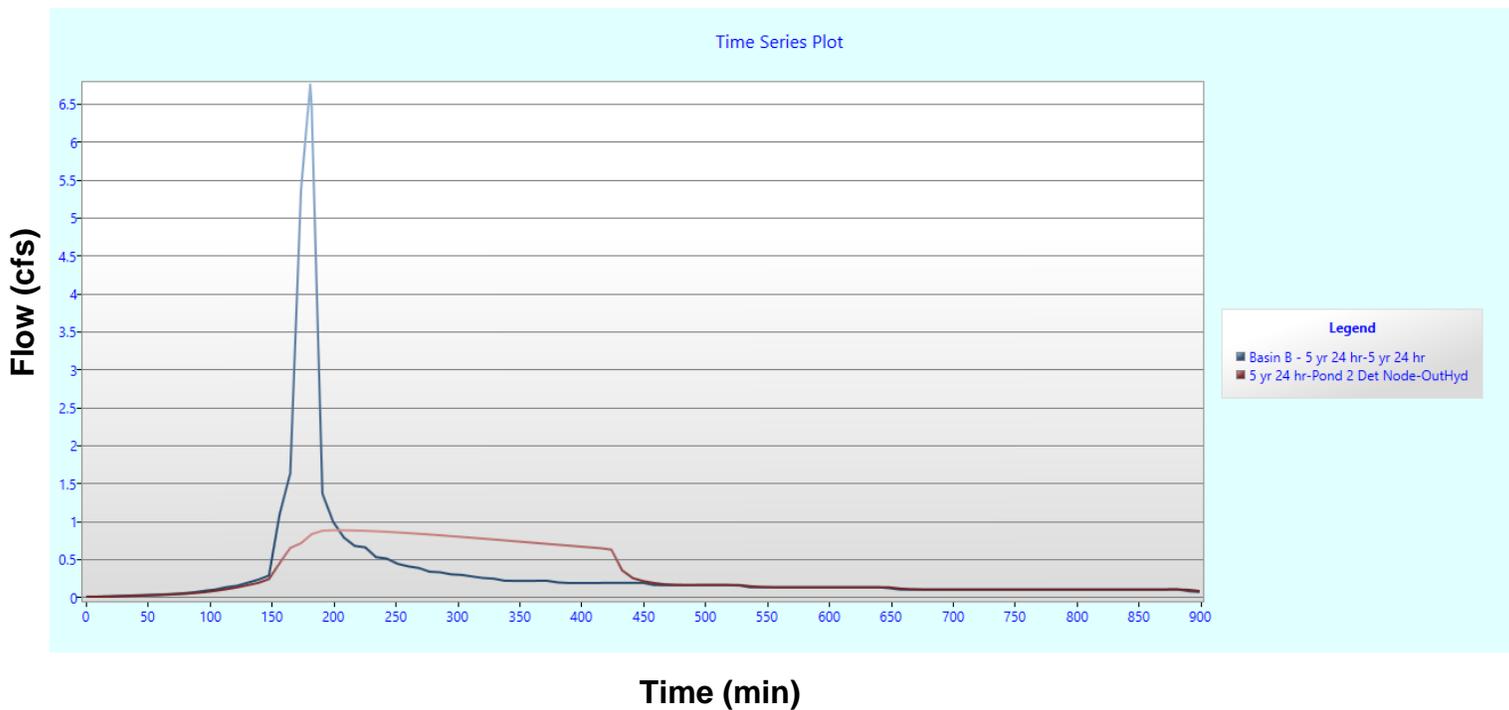
## South Pond Summary Table (POND 2)

Design Event	Match Flows (cfs)	Peak Q (cfs)	Max Depth (ft)	Vol (cf)	HtoE	% Vol
WQCV	0.0551	0.0281	0.0045	14,9835	0.01	99.95
5 yr 24 hr	6.7430	0.8767	1.5473	6,143.8109	0.01	99.97
100 yr 24 hr	19.9827	1.4999	4.6147	25,163.8586	0.01	99.96

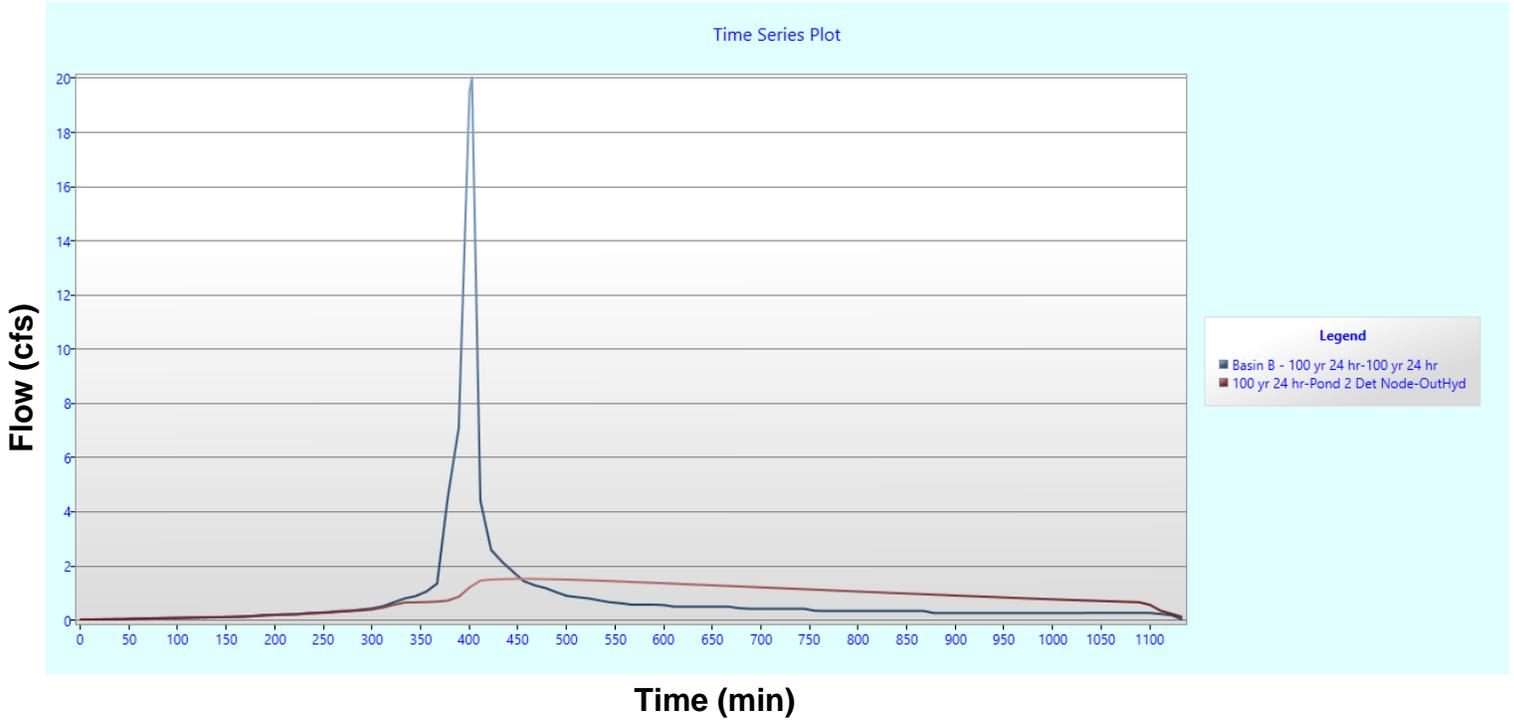
## South Pond: WQCV Inflow and Outflow Hydrographs



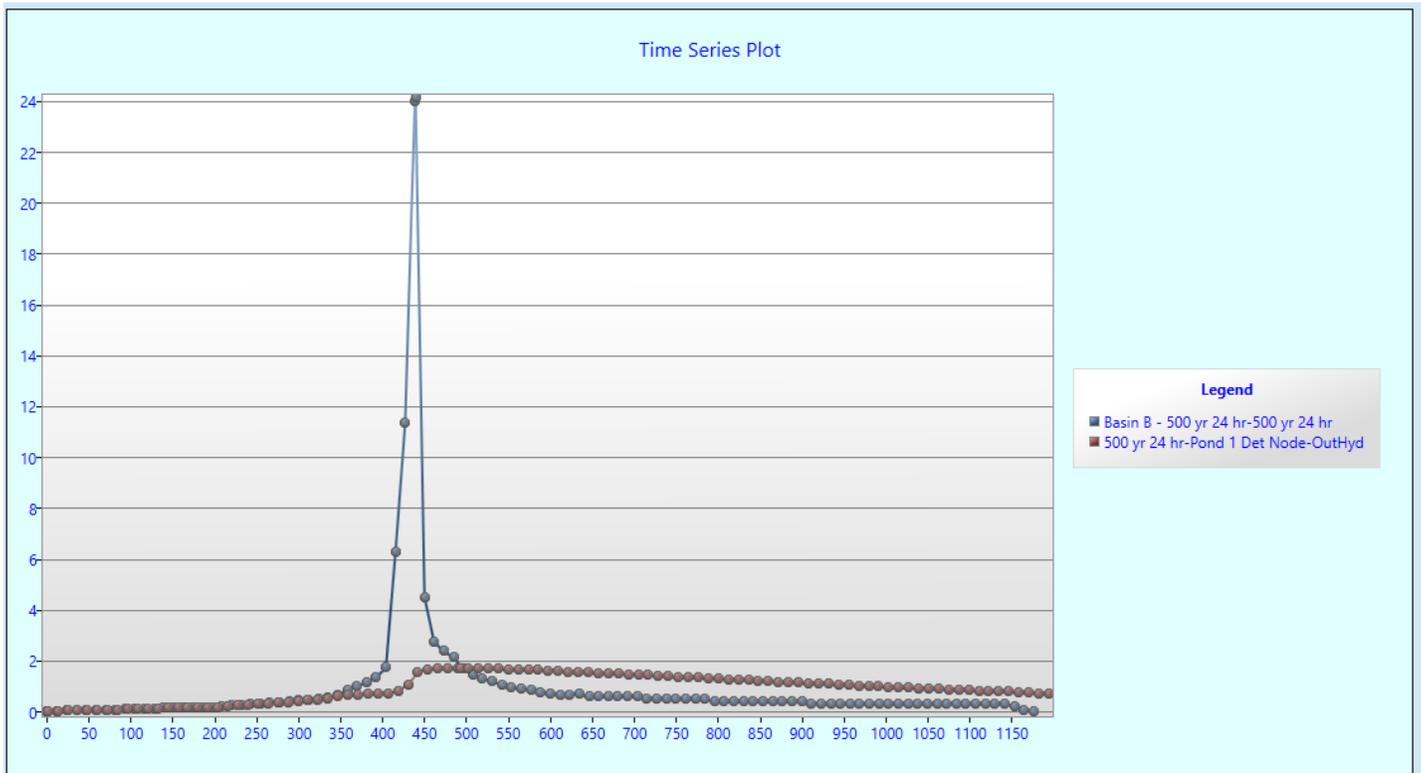
## South Pond: 5 YR Inflow and Outflow Hydrographs



## South Pond: 100 YR Inflow and Outflow Hydrographs



## South Pond: 500 YR Inflow and Outflow Hydrograph and Summary Table



Design Event	Match Flows (cfs)	Peak Q (cfs)	Max Depth (ft)	Vol (cf)	HtoE	% Vol
500 yr 24 hr	24.0984	1.6845	5.4160	31,832.7139	1.05	99.95

provide entire report including calculations, boring logs, field notes, figure with boring locations.



**ENTECH**  
ENGINEERING, INC.

505 ELKTON DRIVE  
COLORADO SPRINGS, CO 80907  
PHONE (719) 531-5599  
FAX (719) 531-5238

August 4, 2021  
Revised October 19, 2021

Highway 85/87 Properties, LLC  
2010 Fox Mountain Point  
Colorado Springs, CO 80906

Attn: Steve Schnurr

Re: Infiltration Rates (Percolation Test Method)  
Bradley Point, Filing No. 1  
Parcel Nos. 65034-00-038 and 65034-00-040  
Colorado Springs, Colorado

Dear Mr. Schnurr:

As requested, personnel of Entech Engineering, Inc. have performed percolation testing at the above referenced site to evaluate the site soils to determine the infiltration rate for the proposed detention ponds.

The testing was performed on July 22 and 26, 2021 and on August 20, 2021. The test locations are shown in Figure 1. The Test Boring Logs, Percolation Test results, Infiltration Rates, and Laboratory Test results are included with this report. Laboratory results are summarized in Table 1. Soils encountered in the profile and percolation holes consisted of clayey sand, clayey-silty sand, and silty sand. Very clean sand was encountered at 4 to 5 feet in the test pits. The percent passing the No. 200 sieve in the Test Pit Samples was 1.8 and 4.1 percent. Bedrock and groundwater were not encountered in the test borings which were drilled to 20 feet. Based on the soils encountered in the test borings, the pond locations tested will have good infiltration characteristics, if the granular soils are exposed. The test boring logs and laboratory testing (grain size) are included with this report.

#### Southern Pond

The percolation rates were 10 minutes/inch for P1 (TB-1A), and 3 minutes/inch for P2 (TB-1A). The percolation rates correspond to adjusted average Infiltration Rate of 1 inch/hour (TB-1A). An additional test pit (TP 2) was excavated to evaluate the sands and gravel encountered at depth. A percolation rate less than 1 min/in, which corresponds to an infiltration rate of 8.1 inches/hour was measured.

#### Northern Pond

The percolation rates were 8 minutes/inch for P3 (TB-2A), and 10 minutes/inch for P4 (TB-2A). The percolation rates correspond to adjusted average Infiltration Rate of 0.35 inches/hour (TB-2A). An additional test pit (TP 1) was excavated to evaluate the sands and gravel encountered at depth. A percolation rate less than 1 min/in, which corresponds to an infiltration rate of 8.1 inches/hour was measured in the field. TB 3 was drilled in the northern site. A percolation rate of 4 minutes/inch, which corresponds to an infiltration rate of 1.7 inches/hour was measured.

Results of the percolation testing/infiltration testing is included in this report. If the proposed detention ponds penetrate into the sand and gravels, infiltration rates of 8.0 inches/hour can be used. The pond excavation should be observed to verify that suitable soils are encountered. The pond surfaces will require periodic cleaning to maintain the high infiltration rates. The ponds should be installed to El Paso County standards/specifications.

Address in O&M  
Manual

Highway 85-87 Properties  
Infiltration Rates (Percolation Test Method) - Revised  
Bradley Point, Filing No. 1  
Parcel Nos. 65034-00-038 and 65034-00-040  
El Paso County, Colorado  
Page 2

We trust that this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

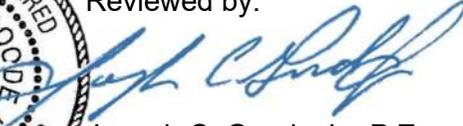
ENTECH ENGINEERING, INC.



Logan L. Langford, P.G.  
Geologist



Reviewed by:



Joseph C. Goode Jr., P.E.  
President

LLL

Encl.

Entech Job No. 210082  
AAprojects/2021/210082 Infiltration Rate

## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** dlm  
**Company:** M&S Civil Consultants  
**Date:** December 8, 2022  
**Project:** Bradley Point Filing No. 1  
**Location:** US Hwy 85-87 / Bradley Road

(POND 1)

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a/100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	<p><math>I_a = </math> <input type="text" value="82.0"/> %</p> <p><math>i = </math> <input type="text" value="0.820"/></p> <p>WQCV = <input type="text" value="0.27"/> watershed inches</p> <p>Area = <input type="text" value="194,501"/> sq ft</p> <p><math>V_{WQCV} = </math> <input type="text" value=""/> cu ft</p> <p><math>d_e = </math> <input type="text" value="0.60"/> in</p> <p><math>V_{WQCV OTHER} = </math> <input type="text" value="6,173"/> cu ft</p> <p><math>V_{WQCV USER} = </math> <input type="text" value=""/> cu ft</p>
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	<p><math>D_{WQCV} = </math> <input type="text" value="0.1"/> ft</p> <p><math>Z = </math> <input type="text" value="3.00"/> ft / ft <b>DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE</b></p> <p><math>A_{Min} = </math> <input type="text" value="1994"/> sq ft</p> <p><math>A_{Actual} = </math> <input type="text" value="3863"/> sq ft</p> <p><math>V_T = </math> <input type="text" value=""/> cu ft</p>
<p>3. Filter Material</p> <div style="border: 2px solid cyan; padding: 5px; display: inline-block; margin-top: 20px;"> <p style="color: cyan; font-weight: bold; font-size: 1.2em;">Fill in filter material used.</p> </div>	<p>Choose One _____</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;"> <p><input type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input checked="" type="radio"/> Other (Explain):</p> </div> <p>_____</p> <p>_____</p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p style="margin-left: 20px;">i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p style="margin-left: 20px;">ii) Volume to Drain in 12 Hours</p> <p style="margin-left: 20px;">iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One _____</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;"> <p><input type="radio"/> YES</p> <p><input checked="" type="radio"/> NO</p> </div> <p><math>y = </math> <input type="text" value="N/A"/> ft</p> <p><math>Vol_{12} = </math> <input type="text" value="N/A"/> cu ft</p> <p><math>D_o = </math> <input type="text" value="N/A"/> in</p>

**Design Procedure Form: Sand Filter (SF)**

Sheet 2 of 2

**Designer:** dlm  
**Company:** M&S Civil Consultants  
**Date:** December 8, 2022  
**Project:** Bradley Point Filing No. 1  
**Location:** US Hwy 85-87 / Bradley Road

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One \_\_\_\_\_  
 YES     NO

6. Inlet / Outlet Works

A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Notes: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** dlm  
**Company:** M&S Civil Consultants  
**Date:** December 8, 2022  
**Project:** \_\_\_\_\_  
**Location:** \_\_\_\_\_

(POND 2)

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a/100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	<p><math>I_a = </math> <input style="width: 50px;" type="text" value="80.0"/> %</p> <p><math>i = </math> <input style="width: 50px;" type="text" value="0.800"/></p> <p><math>WQCV = </math> <input style="width: 50px;" type="text" value="0.26"/> watershed inches</p> <p><math>Area = </math> <input style="width: 50px;" type="text" value="181,766"/> sq ft</p> <p><math>V_{WQCV} = </math> <input style="width: 50px;" type="text" value=""/></p> <p><math>d_b = </math> <input style="width: 50px;" type="text" value="0.60"/> in</p> <p><math>V_{WQCV\ OTHER} = </math> <input style="width: 50px;" type="text" value="5,551"/> cu ft</p> <p><math>V_{WQCV\ USER} = </math> <input style="width: 50px;" type="text" value=""/> cu ft</p>
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	<p><math>D_{WQCV} = </math> <input style="width: 50px;" type="text" value="0.0"/> ft</p> <p><math>Z = </math> <input style="width: 50px;" type="text" value="3.00"/> ft / ft <span style="color: red; font-weight: bold;">DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE</span></p> <p><math>A_{Min} = </math> <input style="width: 50px;" type="text" value="1818"/> sq ft</p> <p><math>A_{Actual} = </math> <input style="width: 50px;" type="text" value="3316"/> sq ft</p> <p><math>V_T = </math> <input style="width: 50px;" type="text" value=""/> cu ft</p>
<p>3. Filter Material</p>	<p>Choose One _____</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;"> <input type="radio"/> 18" CDOT Class B or C Filter Material  <input checked="" type="radio"/> Other (Explain):         </div> <p style="margin-left: 40px;">_____</p> <p style="margin-left: 40px;">In situ eathern materials</p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p style="margin-left: 40px;">i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p style="margin-left: 40px;">ii) Volume to Drain in 12 Hours</p> <p style="margin-left: 40px;">iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One _____</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;"> <input type="radio"/> YES  <input checked="" type="radio"/> NO         </div> <p><math>y = </math> <input style="width: 50px;" type="text" value="N/A"/> ft</p> <p><math>Vol_{12} = </math> <input style="width: 50px;" type="text" value="N/A"/> cu ft</p> <p><math>D_o = </math> <input style="width: 50px;" type="text" value="N/A"/> in</p>

**Design Procedure Form: Sand Filter (SF)**

Sheet 2 of 2

**Designer:** dlm  
**Company:** M&S Civil Consultants  
**Date:** December 8, 2022  
**Project:**  
**Location:**

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES     NO

6. Inlet / Outlet Works

A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Notes: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

## Worksheet for Irregular Swale Section - A-A

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.004 ft/ft
Discharge	16.00 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	5,785.60
0+33	5,785.00
0+54	5,784.50
0+65	5,785.00
0+83	5,785.80

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5,785.60)	(0+65, 5,785.00)	0.030
(0+65, 5,785.00)	(0+83, 5,785.80)	0.016

Options	
Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results	
Normal Depth	7.1 in
Roughness Coefficient	0.029
Elevation	5,785.09 ft
Elevation Range	5,784.5 to 5,785.8 ft
Flow Area	11.2 ft <sup>2</sup>
Wetted Perimeter	39.0 ft
Hydraulic Radius	3.4 in
Top Width	39.03 ft
Normal Depth	7.1 in
Critical Depth	5.2 in
Critical Slope	0.021 ft/ft
Velocity	1.43 ft/s
Velocity Head	0.03 ft
Specific Energy	0.62 ft
Froude Number	0.469

## Worksheet for Irregular Swale Section - A-A

Results	
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	7.1 in
Critical Depth	5.2 in
Channel Slope	0.004 ft/ft
Critical Slope	0.021 ft/ft

## Worksheet for Irregular Swale Section - B-B

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.003 ft/ft
Discharge	16.00 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	5,785.20
0+50	5,784.00
0+57	5,783.70
0+62	5,784.00
0+86	5,784.90

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5,785.20)	(0+62, 5,784.00)	0.030
(0+62, 5,784.00)	(0+86, 5,784.90)	0.016

Options	
Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results	
Normal Depth	8.2 in
Roughness Coefficient	0.027
Elevation	5,784.39 ft
Elevation Range	5,783.7 to 5,785.2 ft
Flow Area	11.6 ft <sup>2</sup>
Wetted Perimeter	38.5 ft
Hydraulic Radius	3.6 in
Top Width	38.50 ft
Normal Depth	8.2 in
Critical Depth	6.2 in
Critical Slope	0.017 ft/ft
Velocity	1.38 ft/s
Velocity Head	0.03 ft
Specific Energy	0.71 ft
Froude Number	0.443

## Worksheet for Irregular Swale Section - B-B

Results	
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	8.2 in
Critical Depth	6.2 in
Channel Slope	0.003 ft/ft
Critical Slope	0.017 ft/ft

## Worksheet for Irregular Swale Section - C-C

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.004 ft/ft
Discharge	16.00 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	5,784.20
0+60	5,783.00
0+65	5,782.80
0+70	5,783.00
0+96	5,784.10

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5,784.20)	(0+70, 5,783.00)	0.030
(0+70, 5,783.00)	(0+96, 5,784.10)	0.016

#### Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

#### Results

Normal Depth	7.1 in
Roughness Coefficient	0.027
Elevation	5,783.40 ft
Elevation Range	5,782.8 to 5,784.2 ft
Flow Area	11.0 ft <sup>2</sup>
Wetted Perimeter	39.5 ft
Hydraulic Radius	3.3 in
Top Width	39.47 ft
Normal Depth	7.1 in
Critical Depth	5.5 in
Critical Slope	0.018 ft/ft
Velocity	1.46 ft/s
Velocity Head	0.03 ft
Specific Energy	0.63 ft
Froude Number	0.489

## Worksheet for Irregular Swale Section - C-C

Results	
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	7.1 in
Critical Depth	5.5 in
Channel Slope	0.004 ft/ft
Critical Slope	0.018 ft/ft

## Worksheet for Irregular Swale Section - D-D

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.005 ft/ft
Discharge	17.50 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	5,782.50
0+52	5,782.00
0+65	5,781.60
0+78	5,782.00
0+96	5,782.90

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5,782.50)	(0+78, 5,782.00)	0.030
(0+78, 5,782.00)	(0+96, 5,782.90)	0.016

#### Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

#### Results

Normal Depth	7.0 in
Roughness Coefficient	0.029
Elevation	5,782.19 ft
Elevation Range	5,781.6 to 5,782.9 ft
Flow Area	12.1 ft <sup>2</sup>
Wetted Perimeter	48.9 ft
Hydraulic Radius	3.0 in
Top Width	48.90 ft
Normal Depth	7.0 in
Critical Depth	5.5 in
Critical Slope	0.021 ft/ft
Velocity	1.45 ft/s
Velocity Head	0.03 ft
Specific Energy	0.62 ft
Froude Number	0.513

## Worksheet for Irregular Swale Section - D-D

Results	
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	7.0 in
Critical Depth	5.5 in
Channel Slope	0.005 ft/ft
Critical Slope	0.021 ft/ft

## Worksheet for Irregular Swale Section - E-E

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.020 ft/ft
Discharge	17.50 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	5,780.80
0+43	5,780.00
0+56	5,779.20
0+62	5,780.00
0+79	5,781.00

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5,780.80)	(0+62, 5,780.00)	0.030
(0+62, 5,780.00)	(0+79, 5,781.00)	0.016

Options	
Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results	
Normal Depth	8.0 in
Roughness Coefficient	0.030
Elevation	5,779.86 ft
Elevation Range	5,779.2 to 5,781.0 ft
Flow Area	5.2 ft <sup>2</sup>
Wetted Perimeter	15.8 ft
Hydraulic Radius	4.0 in
Top Width	15.76 ft
Normal Depth	8.0 in
Critical Depth	8.0 in
Critical Slope	0.019 ft/ft
Velocity	3.35 ft/s
Velocity Head	0.17 ft
Specific Energy	0.84 ft
Froude Number	1.025

## Worksheet for Irregular Swale Section - E-E

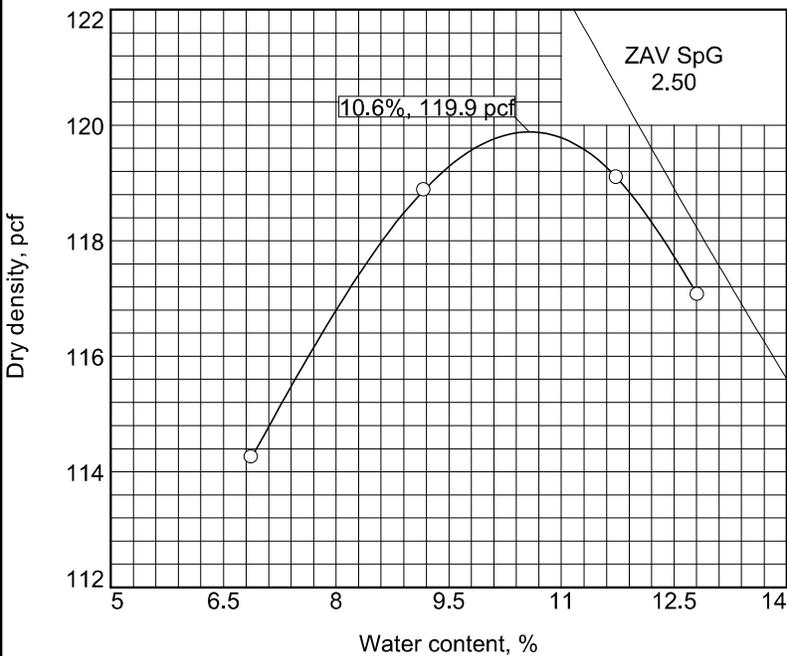
Results	
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	8.0 in
Critical Depth	8.0 in
Channel Slope	0.020 ft/ft
Critical Slope	0.019 ft/ft

**AGGREGATE BASE EXHIBIT**

These test results apply only to the samples which were tested. the testing report shall not be reproduced, except in full, without the written approval of K & A, Inc

# COMPACTION TEST REPORT

Curve No. 1217



Preparation Method _____	
Rammer: Wt. <u>10 lb.</u>	Drop <u>18 in.</u>
Type <u>Manual</u>	
Layers: No. <u>five</u>	Blows per <u>56</u>
Mold Size <u>0.075 cu. ft.</u>	
Test Performed on Material	
Passing <u>3/4 in.</u> Sieve	
%>3/4 in. <u>1</u>	%<No.200 <u>6.8</u>
Atterberg (D 4318): LL <u>NV</u>	PI <u>NP</u>
NM (D 2216) _____	Sp.G. (D 854) <u>2.5</u>
USCS (D 2487) <u>GP-GM</u>	
AASHTO (M 145) <u>A-1-a</u>	
Date: Sampled <u>3-25-2021</u>	
Received <u>3-25-2021</u>	
Tested <u>4-6-2021</u>	
Tested By <u>KP</u>	

### COMPACTION TESTING DATA ASTM D 1557-12 Method C Modified

	1	2	3	4	5	6
<b>WM + WS</b>	10658.0	10919.0	11031.0	10997.0		
<b>WM</b>	6504.0	6504.0	6504.0	6504.0		
<b>WW + T #1</b>	730.1	718.7	669.0	786.8		
<b>WD + T #1</b>	692.6	670.9	615.7	723.4		
<b>TARE #1</b>	147.1	149.6	161.5	228.7		
<b>WW + T #2</b>						
<b>WD + T #2</b>						
<b>TARE #2</b>						
<b>MOIST.</b>	6.9	9.2	11.7	12.8		
<b>DRY DENS.</b>	114.3	118.9	119.1	117.1		

### SIEVE TEST RESULTS ASTM D-422 ASTM D-1140

Opening Size	% Passing	Specs.
1"	100	100
3/4"	99	95 - 100
3/8"	68	
#4	48	30 - 65
#8	31	25 - 55
#16	21	
#30	16	
#50	12	
#100	9	
#200	6.8	3.0 - 12

### TEST RESULTS

Maximum dry density = 119.9 pcf  
Optimum moisture = 10.6 %

**Project No.** 21-1-235    **Client:**  
**Project:** Colorado Aggregate Recycling

○ **Location:** Import, South Yard    **Sample Number:** 1217

**Kumar & Associates, Inc.**

**Denver, Colorado**

### Material Description

Recycled Concrete/ Class 6 ABC/ poorly graded gravel with silt and sand

### Remarks:

**Checked by:** \_\_\_\_\_ DS

**Title:** Lab Manager

**Figure**

**BRADLEY POINT FILING NO. 1**  
**AGGREGATE BASE RUNOFF COEFFICIENT CALCULATION**

		<i>PASSING #4 SIEVE</i>			<i>LARGER THAN #4 SIEVE</i>			<i>RUNOFF COEFFICIENT</i>	
<b>ITEM</b>	<b>ITEM DESCRIPTION</b>	<b>PERCENT (%)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>PERCENT (%)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>
<b>3/4" Minus, CDOT CL6 Road Base</b>	Recycled Concrete/ Class 6 ABC/ poorly graded gravel with silt and sand	0.48	0.09	0.36	0.52	0.59	0.70	<b>0.35</b>	<b>0.54</b>

Calculated by: CVW \_\_\_\_\_  
 Date: 5/5/2021



Missing MHFD-Detention Worksheet for Sand Filter

include riprap sizing calcs for spillway, forebay, and if there is a culvert crossing at entrance.

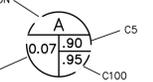
Drainage maps should be the last pages of the report. Move drainage maps to the end of the report.

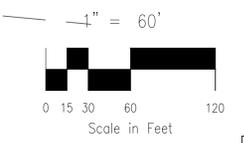
#### **EXISTING DRAINAGE MAP**

# BRADLEY POINT FILING NO. 1 - EXISTING DRAINAGE MAP

AP NO. 65034-00-038 AND AP NO. 65034-00-040 ON HIGHWAY 85/87 (EAST LAS VEGAS STREET)  
IN SECTION 3, T15S R66W, 6th P.M., EL PASO COUNTY, COLORADO

## LEGEND

- BASIN DESIGNATION  A C5
- ACRES 
-  SURFACE DESIGN POINT
-  BASIN BOUNDARY
-  EXIST MAJ CONT (5')
-  EXIST MIN CONT (1')
-  EX OR EXIST
-  EXISTING
-  ADJ. PROPERTY BOUNDARY
-  OVERHEAD ELECTRIC
-  EXISTING FLOW DIRECTION ARROW
-  EXISTING TREE

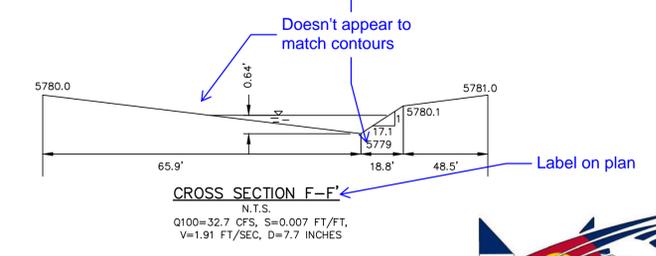
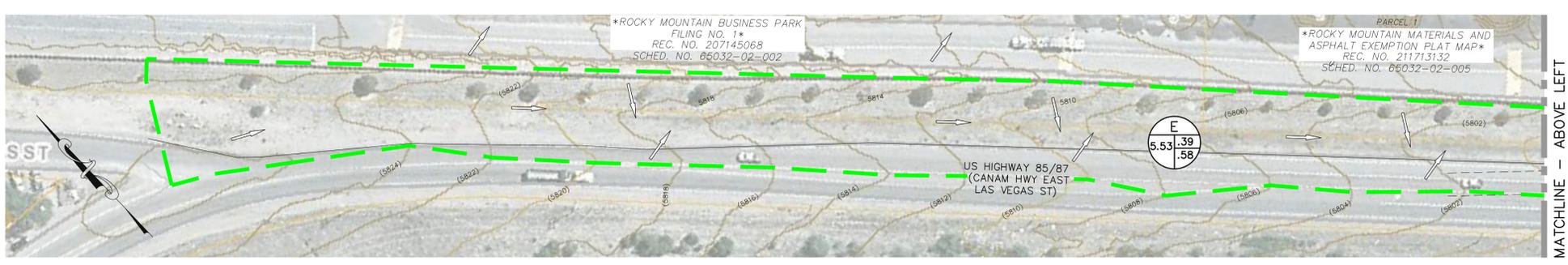
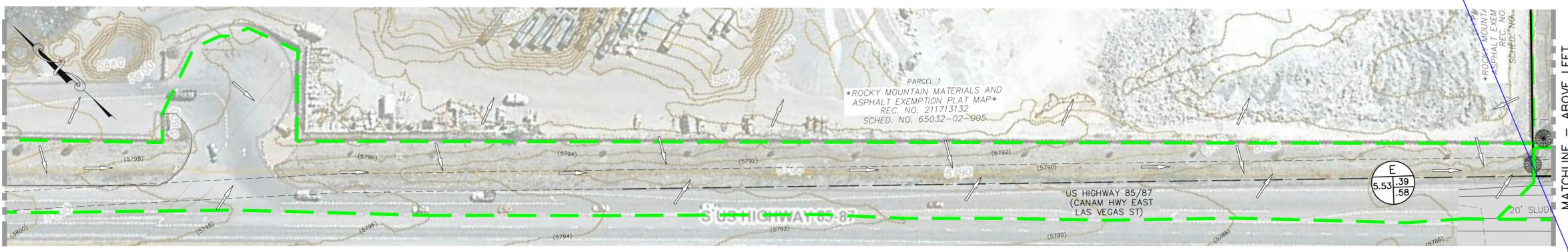
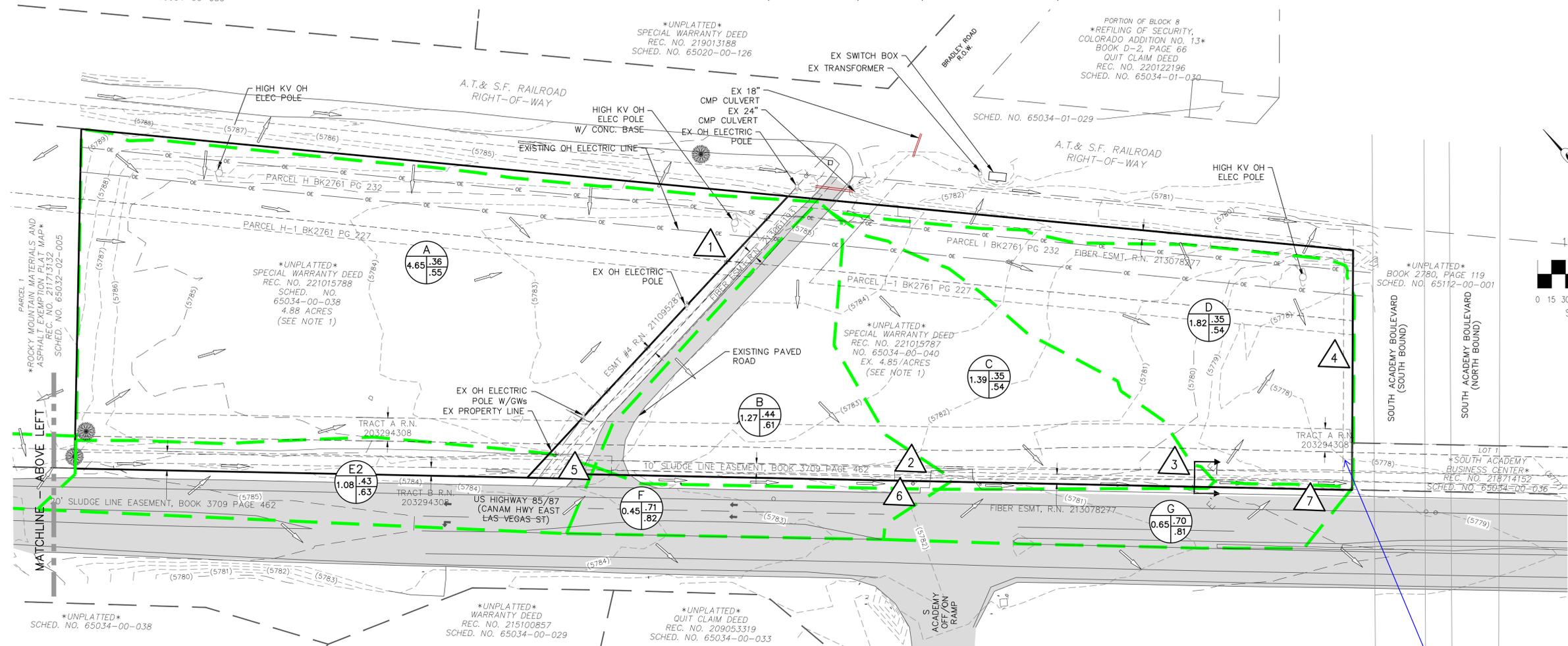


BASIN SUMMARY			
BASIN	AREA (ACRES)	Q <sub>5</sub>	Q <sub>100</sub>
A	4.65	6.0	15.5
B	1.27	2.1	4.9
C	1.39	1.8	4.7
D	1.82	2.4	6.1
E	5.53	6.5	16.2
E2	1.08	1.8	4.2
F	0.45	1.4	2.6
G	0.65	1.7	3.4

DESIGN POINT SUMMARY				
DESIGN POINT	Q <sub>5</sub>	Q <sub>100</sub>	CONTRIBUTING BASIN/DESIGN POINT	STRUCTURE
1	6.0	15.5	A	LOCALIZED DEPRESSION
2	6.7	16.8	B, DP 1	EXISTS TO ROADSIDE DITCH
3	1.8	4.7	C	EXISTS TO ROADSIDE DITCH
4	2.4	6.1	D	LOCALIZED DEPRESSION
5	6.7	16.5	E, E2	EXISTING ROADSIDE DITCH
6	13.1	32.0	F, DP 2, DP 5	EXISTING ROADSIDE DITCH
7	13.5	32.7	G, DP 3, DP 6	EXISTING ROADSIDE DITCH

BRADLEY POINT FILING NO. 1  
EXISTING DRAINAGE MAP  
DATE SUBMITTED: 9/30/22  
SHEET 1 OF 1

**NOTE 1:**  
PARCELS ARE UNDER THE SAME OWNERSHIP



**PROPOSED DRAINAGE MAP**



**ROADSIDE DITCH CONVEYANCE EXHIBIT**



SITE MAP  
N.T.S.

**LEGEND**



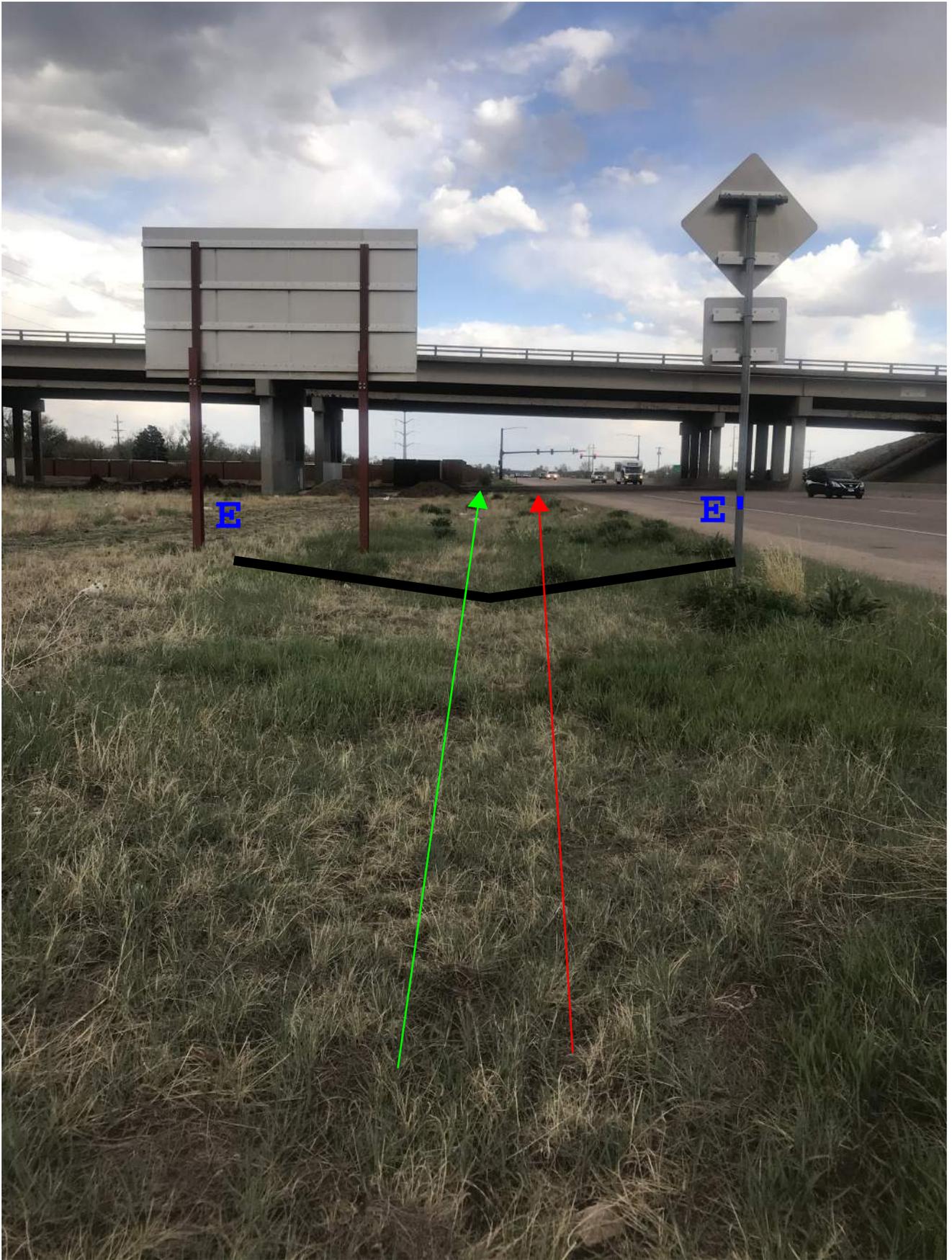
**ACTUAL FLOWPATH**



**LOGICAL FLOWPATH**

















18" ADS  
CULVERT



Remove GEC Plans and submit as a separate document.

## **GRADING AND EROSION CONTROL PLANS**

**STANDARD CONSTRUCTION NOTES:**

- ALL DRAINAGE AND ROADWAY CONSTRUCTION SHALL MEET THE STANDARDS AND SPECIFICATIONS OF THE CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL VOLUMES 1 AND 2, AND THE EL PASO COUNTY ENGINEERING CRITERIA MANUAL.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE NOTIFICATION AND FIELD LOCATION OF ALL EXISTING UTILITIES, WHETHER SHOWN ON THE PLANS OR NOT, BEFORE BEGINNING CONSTRUCTION. LOCATION OF EXISTING UTILITIES SHALL BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. CALL 811 TO CONTACT THE UTILITY NOTIFICATION CENTER OF COLORADO SPRINGS.
- CONTRACTOR SHALL KEEP A COPY OF THESE APPROVED PLANS, THE GRADING AND EROSION CONTROL PLAN, THE STORMWATER MANAGEMENT PLAN (SWMP), THE SOILS AND GEOTECHNICAL REPORT AND THE APPROPRIATE DESIGN AND CONSTRUCTION STANDARDS AND SPECIFICATIONS AT THE JOB SITE AT ALL TIME INCLUDING THE FOLLOWING:
  - EL PASO COUNTY ENGINEERING CRITERIA MANUAL (ECM)
  - CITY OF COLORADO SPRINGS/EL PASO COUNTY ENGINEERING CRITERIA MANUAL VOLUMES 1 AND 2.
  - COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) STANDARDS SPECIFICATION FOR ROAD AND BRIDGE CONSTRUCTION.
  - CDOT M&S STANDARDS.
- IT IS THE DESIGN ENGINEER'S RESPONSIBILITY TO ACCURACY SHOW EXISTING CONDITION BOTH ONSITE AND OFFSITE ON THE CONSTRUCTION PLANS. ANY MODIFICATION OR NECESSARY DUE TO CONFLICT OMISSIONS OR CHANGED CONDITIONS WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- ONCE THE ESQCP HAS BEEN ISSUED, THE CONTRACTOR MAY INSTALL THE INITIAL STAGE EROSION AND SEDIMENT CONTROL BMPS AS INDICATED ON THE GEC. A PRECONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, AND EL PASO COUNTY WILL BE HELD PRIOR TO ANY CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE APPLICANT TO COORDINATE THE MEETING TIME AND PLACE WITH COUNTY PCD INSPECTIONS STAFF.
- IT IS THE CONTRACTORS RESPONSIBILITY TO UNDERSTAND THE REQUIREMENTS OF ALL JURISDICTIONAL AGENCIES AND TO OBTAIN ALL REQUIRED PERMITS, INCLUDING BUT NOT LIMITED TO EL PASO COUNTY EROSION AND STORM WATER QUALITY CONTROL PERMIT (ESQCP), US ARMY CORPS OF ENGINEER ISSUED 401 AND/OR 404 PERMITS AND COUNTY AND STATE FUGITIVE DUST PERMITS.
- ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE CONSTRUCTION SITE AT APPROVED CONSTRUCTION ACCESS POINTS.
- ANY TEMPORARY SIGNAGE AND STRIPING SHALL COMPLY WITH EL PASO COUNTY DOW AND MUTCD CRITERIA.
- CONTRACTOR SHALL OBTAIN ANY PERMITS REQUIRE BY EL PASO COUNTY DOT INCLUDING WORK WITHIN THE RIGHT-OF-WAY AND SPECIAL TRANSPORT PERMITS.
- THE LIMITS OF CONSTRUCTION SHALL REMAIN WITHIN THE PROPERTY LINE UNLESS OTHERWISE NOTED. THE OWNER/DEVELOPER SHALL OBTAIN WRITTEN PERMISSION AND EASEMENTS, WHERE REQUIRED, FROM ADJOINING PROPERTY OWNER(S) PRIOR TO ANY OFFSITE DISTURBANCE GRADING, OR CONSTRUCTION.

**GRADING AND EROSION CONTROL NOTES:**

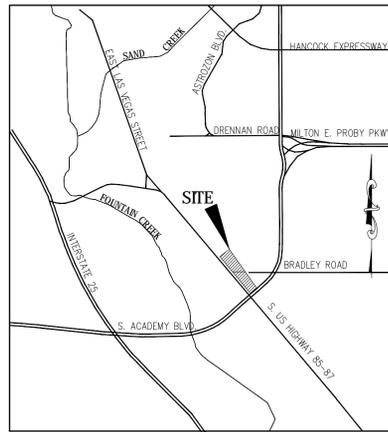
- STORMWATER DISCHARGES FROM CONSTRUCTION SITES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLUTION, CONTAMINATION, OR DEGRADATION OF STATE WATERS. ALL WORK AND EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE WATERS, INCLUDING WETLANDS.
- NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING.
- A SEPARATE STORMWATER MANAGEMENT PLAN (SWMP) FOR THIS PROJECT SHALL BE COMPLETED AND AN EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP) ISSUED PRIOR TO COMMENCING CONSTRUCTION. MANAGEMENT OF THE SWMP DURING CONSTRUCTION IS THE RESPONSIBILITY OF THE DESIGNATED QUALIFIED STORMWATER MANAGER OR CERTIFIED EROSION CONTROL INSPECTOR. THE SWMP SHALL BE LOCATED ON SITE AT ALL TIMES DURING CONSTRUCTION AND SHALL BE KEPT UP TO DATE WITH WORK PROGRESS AND CHANGES IN THE FIELD.
- ONCE THE ESQCP IS APPROVED AND A "NOTICE TO PROCEED" HAS BEEN ISSUED, THE CONTRACTOR MAY INSTALL THE INITIAL STAGE EROSION AND SEDIMENT CONTROL MEASURES AS INDICATED ON THE APPROVED GEC. A PRECONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, AND EL PASO COUNTY WILL BE HELD PRIOR TO ANY CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE APPLICANT TO COORDINATE THE MEETING TIME AND PLACE WITH COUNTY STAFF.
- CONTROL MEASURES MUST BE INSTALLED PRIOR TO COMMENCEMENT OF ACTIVITIES THAT COULD CONTRIBUTE POLLUTANTS TO STORMWATER. CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, AND DISTURBED LAND AREAS SHALL BE INSTALLED IMMEDIATELY UPON COMPLETION OF THE DISTURBANCE.
- ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE MAINTAINED AND REMAIN IN EFFECTIVE OPERATING CONDITION UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED AND FINAL STABILIZATION IS ESTABLISHED. ALL PERSONS ENGAGED IN LAND DISTURBANCE ACTIVITIES SHALL ASSESS THE ADEQUACY OF CONTROL MEASURES AT THE SITE AND IDENTIFY IF CHANGES TO THOSE CONTROL MEASURES ARE NEEDED TO ENSURE THE CONTINUED EFFECTIVE PERFORMANCE OF THE CONTROL MEASURES. ALL CHANGES TO TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES MUST BE INCORPORATED INTO THE STORMWATER MANAGEMENT PLAN.
- TEMPORARY STABILIZATION SHALL BE IMPLEMENTED ON DISTURBED AREAS AND STOCKPILES WHERE GROUND DISTURBING CONSTRUCTION ACTIVITY HAS PERMANENTLY CEASED OR TEMPORARILY CEASED FOR LONGER THAN 14 DAYS.
- FINAL STABILIZATION MUST BE IMPLEMENTED AT ALL APPLICABLE CONSTRUCTION SITES. FINAL STABILIZATION IS ACHIEVED WHEN ALL GROUND DISTURBING ACTIVITIES ARE COMPLETE AND ALL DISTURBED AREAS EITHER HAVE A UNIFORM VEGETATIVE COVER WITH INDIVIDUAL PLANT DENSITY OF 70 PERCENT OF PRE-DISTURBANCE LEVELS ESTABLISHED OR EQUIVALENT PERMANENT ALTERNATIVE STABILIZATION METHOD IS IMPLEMENTED. ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED UPON FINAL STABILIZATION AND BEFORE PERMIT CLOSURE.
- ALL PERMANENT STORMWATER MANAGEMENT FACILITIES SHALL BE INSTALLED AS DESIGNED IN THE APPROVED PLANS. ANY PROPOSED CHANGES THAT EFFECT THE DESIGN OR FUNCTION OF PERMANENT STORMWATER MANAGEMENT STRUCTURES MUST BE APPROVED BY THE ECM ADMINISTRATOR PRIOR TO IMPLEMENTATION.
- EARTH DISTURBANCES SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY MINIMIZE ACCELERATED SOIL EROSION AND RESULTING SEDIMENTATION. ALL DISTURBANCES SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME. PRE-EXISTING VEGETATION SHALL BE PROTECTED AND MAINTAINED WITHIN 50 HORIZONTAL FEET OF A WATERS OF THE STATE UNLESS SHOWN TO BE INFEASIBLE AND SPECIFICALLY REQUESTED AND APPROVED.
- COMPACTION OF SOIL MUST BE PREVENTED IN AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES OR WHERE FINAL STABILIZATION WILL BE ACHIEVED BY VEGETATIVE COVER. AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES SHALL ALSO BE PROTECTED FROM SEDIMENTATION DURING CONSTRUCTION UNTIL FINAL STABILIZATION IS ACHIEVED. IF COMPACTION PREVENTION IS NOT FEASIBLE DUE TO SITE CONSTRAINTS, ALL AREAS DESIGNATED FOR INFILTRATION AND VEGETATION CONTROL MEASURES MUST BE LOOSENEED PRIOR TO INSTALLATION OF THE CONTROL MEASURE(S).
- ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORMWATER AROUND, THROUGH, OR FROM THE EARTH DISTURBANCE AREA SHALL BE A STABILIZED CONVEYANCE DESIGNED TO MINIMIZE EROSION AND THE DISCHARGE OF SEDIMENT OFF SITE.
- CONCRETE WASH WATER SHALL BE CONTAINED AND DISPOSED OF IN ACCORDANCE WITH THE SWMP. NO WASH WATER SHALL BE DISCHARGED TO OR ALLOWED TO ENTER STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEMS OR FACILITIES. CONCRETE WASHOUTS SHALL NOT BE LOCATED IN AN AREA WHERE SHALLOW GROUNDWATER MAY BE PRESENT, OR WITHIN 50 FEET OF A SURFACE WATER BODY, CREEK OR STREAM.
- DURING DEWATERING OPERATIONS OF UNCONTAMINATED GROUND WATER MAY BE DISCHARGED ON SITE, BUT SHALL NOT LEAVE THE SITE IN THE FORM OF SURFACE RUNOFF UNLESS AN APPROVED STATE DEWATERING PERMIT IS IN PLACE.
- EROSION CONTROL BLANKETING OR OTHER PROTECTIVE COVERING SHALL BE USED ON SLOPES STEEPER THAN 3:1.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL WASTES FROM THE CONSTRUCTION SITE FOR DISPOSAL IN ACCORDANCE WITH LOCAL AND STATE REGULATORY REQUIREMENTS. NO CONSTRUCTION DEBRIS, TREE SLASH, BUILDING MATERIAL WASTES OR UNUSED BUILDING MATERIALS SHALL BE BURIED, DUMPED, OR DISCHARGED AT THE SITE.
- WASTE MATERIALS SHALL NOT BE TEMPORARILY PLACED OR STORED IN THE STREET, ALLEY, OR OTHER PUBLIC WAY, UNLESS IN ACCORDANCE WITH AN APPROVED TRAFFIC CONTROL PLAN. CONSTRUCTION CONTROL MEASURES MAY BE REQUIRED BY EL PASO COUNTY ENGINEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES.
- TRACKING OF SOILS AND CONSTRUCTION DEBRIS OFF-SITE SHALL BE MINIMIZED. MATERIALS TRACKED OFF-SITE SHALL BE CLEANED UP AND PROPERLY DISPOSED OF IMMEDIATELY.
- THE OWNER/DEVELOPER SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS, DIRT, TRASH, ROCK, SEDIMENT, SOIL, AND SAND THAT MAY ACCUMULATE IN ROADS, STORM DRAINS AND OTHER DRAINAGE CONVEYANCE SYSTEMS AND STORMWATER APPURTENANCES AS A RESULT OF SITE DEVELOPMENT.
- THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE SHALL BE LIMITED, AS MUCH AS PRACTICAL, TO THAT QUANTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE. ALL MATERIALS STORED ON-SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER, IN THEIR ORIGINAL CONTAINERS, WITH ORIGINAL MANUFACTURER'S LABELS.
- NO CHEMICAL(S) HAVING THE POTENTIAL TO BE RELEASED IN STORMWATER ARE TO BE STORED OR USED ONSITE UNLESS PERMISSION FOR THE USE OF SUCH CHEMICAL(S) IS GRANTED IN WRITING BY THE ECM ADMINISTRATOR. IN GRANTING APPROVAL FOR THE USE OF SUCH CHEMICAL(S), SPECIAL CONDITIONS AND MONITORING MAY BE REQUIRED.
- BULK STORAGE OF ALLOWED PETROLEUM PRODUCTS OR OTHER ALLOWED LIQUID CHEMICALS IN EXCESS OF 55 GALLONS SHALL REQUIRE ADEQUATE SECONDARY CONTAINMENT PROTECTION TO CONTAIN ALL SPILLS ONSITE AND TO PREVENT ANY SPILLED MATERIALS FROM ENTERING STATE WATERS, ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR OTHER FACILITIES.
- NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER FLOW IN THE CURB AND GUTTER OR DITCH EXCEPT WITH APPROVED SEDIMENT CONTROL MEASURES.
- OWNER/DEVELOPER AND THEIR AGENTS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33 USC 1344), IN ADDITION TO THE REQUIREMENTS OF THE LAND DEVELOPMENT CODE, DOM VOLUME 1 AND THE ECM APPENDIX 1. ALL APPROPRIATE PERMITS MUST BE OBTAINED BY THE CONTRACTOR PRIOR TO CONSTRUCTION (1041, NPDES, FLOODPLAIN, 404, FUGITIVE DUST, ETC.). IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS AND OTHER LAWS, RULES, OR REGULATIONS OF OTHER FEDERAL, STATE, LOCAL, OR COUNTY AGENCIES, THE MOST RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL APPLY.
- ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE ONLY AT APPROVED CONSTRUCTION ACCESS POINTS.
- PRIOR TO CONSTRUCTION THE PERMITTEE SHALL VERIFY THE LOCATION OF EXISTING UTILITIES.
- A WATER SOURCE SHALL BE AVAILABLE ON SITE DURING EARTHWORK OPERATIONS AND SHALL BE UTILIZED AS REQUIRED TO MINIMIZE DUST FROM EARTHWORK EQUIPMENT AND WIND.
- THE SOILS REPORT FOR THIS SITE HAS BEEN PREPARED BY ENTECH ENGINEERS, ENTITLED "SOILS, GEOLOGY, AND GEOLOGIC HAZARD STUDY", DATED JANUARY 22ND, 2021, AND SHALL BE CONSIDERED A PART OF THESE PLANS.
- AT LEAST TEN (10) DAYS PRIOR TO THE ANTICIPATED START OF CONSTRUCTION, FOR PROJECTS THAT WILL DISTURB ONE (1) ACRE OR MORE, THE OWNER OR OPERATOR OF CONSTRUCTION ACTIVITY SHALL SUBMIT A PERMIT APPLICATION FOR STORMWATER DISCHARGE TO THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT, WATER QUALITY DIVISION. THE APPLICATION CONTAINS CERTIFICATION OF COMPLETION OF A STORMWATER MANAGEMENT PLAN (SWMP), OF WHICH THIS GRADING AND EROSION CONTROL PLAN MAY BE A PART. FOR INFORMATION OR APPLICATION MATERIALS CONTACT:  
 COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT  
 WATER QUALITY CONTROL DIVISION  
 WQCD - PERMITS  
 4300 CHERRY CREEK DRIVE SOUTH  
 DENVER, CO 80246-1530  
 ATTN: PERMITS UNIT

# BRADLEY POINT FILING NO. 1

## COUNTY OF EL PASO, STATE OF COLORADO

# GRADING/EROSION CONTROL PLANS

DECEMBER 2022



VICINITY MAP  
N.T.S.



SITE MAP  
N.T.S.

**ADDITIONAL NOTES:**

STAGING AREA TO BE DETERMINED BY CONTRACTOR IN THE FIELD. THE LOCATIONS SHALL BE DELINEATED ON THIS PLAN BY THE CONTRACTOR.

**SHEET INDEX**

SHEET 1	TITLE SHEET
SHEET 2	GRADING & EROSION CONTROL PLAN
SHEET 3	GRADING & EROSION CONTROL DETAILS
SHEET 4	GRADING & EROSION CONTROL DETAILS
SHEET 5	GRADING & EROSION CONTROL DETAILS

EXISTING SITE TERRAIN GENERALLY SLOPES FROM NORTH TO SOUTHEAST AT GRADE RATES THAT VARY BETWEEN 0.7% TO 10%.

THERE ARE NO BATCH PLANTS ON SITE.

AREAS LEFT OPEN FOR 30 DAYS OR MORE, OTHER THAN FOR UTILITY AND DRAINAGE CONSTRUCTION SHALL BE SEEDED AND/OR MULCHED.

**BENCHMARKS**

- CONTROL DISK SET IN ABUTMENT OF BRIDGE  
 N: 1341598.37  
 E: 3210918.78  
 ELEV.: 5782.74'

NO PORTION OF THIS PROPERTY IS LOCATED WITHIN A DESIGNATED FEMA FLOODPLAIN IN ACCORDANCE WITH FLOOD INSURANCE RATE MAPS (FIRM) 08041C0744 G, EFFECTIVE DATE DECEMBER 7, 2018.

**AGENCIES**

OWNER/DEVELOPER:	STEPHEN J. SCHNURR 2010 FOX MOUNTAIN POINT COLORADO SPRINGS, CO 80906 STEPHEN J. SCHNURR (719) 491-3101
CIVIL ENGINEER:	M & S CIVIL CONSULTANTS, INC. 212 N. WAHSATCH AVE, SUITE 305 COLORADO SPRINGS, CO 80903 VIRGIL A. SANCHEZ P.E. (719) 955-5485
WATER RESOURCES:	SECURITY WATER AND SANITATION DISTRICT 231 SECURITY BOULEVARD COLORADO SPRINGS, CO 80911 ROY HEALD (719) 392-3475
COUNTY ENGINEERING:	EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT 2880 INTERNATIONAL CIRCLE, SUITE 110 COLORADO SPRINGS, CO 80910 GILBERT LAFORCE (719) 520-7945
TRAFFIC ENGINEERING:	EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS 3275 AKERS DRIVE COLORADO SPRINGS, CO 80922 JENNIFER IRVINE, P.E. (719) 520-6460
FIRE DISTRICT:	SECURITY FIRE DEPARTMENT 400 SECURITY BOULEVARD SECURITY, CO 80911 BRANDON SULLIVAN (719) 392-7121
GAS DEPARTMENT:	COLORADO SPRINGS UTILITIES 1521 HANCOCK EXPRESSWAY COLORADO SPRINGS, CO 80903 (719) 668-7640
ELECTRIC DEPARTMENT:	COLORADO SPRINGS UTILITIES 1521 HANCOCK EXPRESSWAY COLORADO SPRINGS, CO 80903 (719) 668-7640
COMMUNICATIONS:	TBD (U.N.C.C. LOCATORS) (800) 922-1987 AT&T (LOCATORS) (719) 635-3674

**ENGINEER'S STATEMENT:**

THIS GRADING AND EROSION CONTROL PLAN WAS PREPARED UNDER MY DIRECTION AND SUPERVISION AND IS CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. SAID PLAN HAS BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR GRADING AND EROSION CONTROL PLANS. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARING THIS PLAN.

\_\_\_\_\_  
 VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160  
 FOR AND ON BEHALF OF M&S CIVIL CONSULTANTS, INC. DATE

**DEVELOPER'S STATEMENT:**

I, THE OWNER/DEVELOPER HAVE READ AND WILL COMPLY WITH THE REQUIREMENTS OF THE GRADING AND EROSION CONTROL PLAN.

\_\_\_\_\_  
 STEPHEN J. SHNURR DATE

**EL PASO COUNTY:**

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

FILED IN ACCORDANCE WITH THE REQUIREMENTS OF THE EL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA MANUAL VOLUMES 1 AND 2, AND ENGINEERING CRITERIA MANUAL AS AMENDED.

IN ACCORDANCE WITH ECM SECTION 1.12, THESE CONSTRUCTION DOCUMENTS WILL BE VALID FOR CONSTRUCTION FOR A PERIOD OF 2 YEARS FROM THE DATE SIGNED BY THE EL PASO COUNTY ENGINEER. IF CONSTRUCTION HAS NOT STARTED WITHIN THOSE 2 YEARS, THE PLANS WILL NEED TO BE RESUBMITTED FOR APPROVAL, INCLUDING PAYMENT OF REVIEW FEES AT THE PLANNING AND COMMUNITY DEVELOPMENT DIRECTOR'S DISCRETION.

\_\_\_\_\_  
 JENNIFER IRVINE, P.E.  
 COUNTY ENGINEER/ECM ADMINISTRATOR DATE

6.) MAINTENANCE OF CONTROL MEASURES CAN BE FOUND IN CONSTRUCTION DETAILS SECTION

7.) INFORMATION REGARDING DETAILED INSTALLATION OF BMP'S AND ALL OTHER IMPORTANT ASPECTS OF THESE PROCEDURES SHOULD BE REFERRED TO IN STORM WATER MANAGEMENT PLAN

EL PASO COUNTY FILE NO. MS-21-002

BRADLEY POINT FILING NO. 1	
GRADING & EROSION CONTROL PLAN	DATE: 12/07/22
PROJECT NO: 70-074	SCALE: HORIZONTAL: N/A VERTICAL: N/A
DESIGNED BY: VAS	CHECKED BY: DLN
DRAWN BY: CWV	SHEET 1 OF 5
	GR01

212 N. WAHSATCH AVE, STE 305  
 COLORADO SPRINGS, CO 80903  
 PHONE: 719.955.5485



FOR AND ON BEHALF OF  
 M&S CIVIL CONSULTANTS, INC.

VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160

NO.	DATE	DESCRIPTION

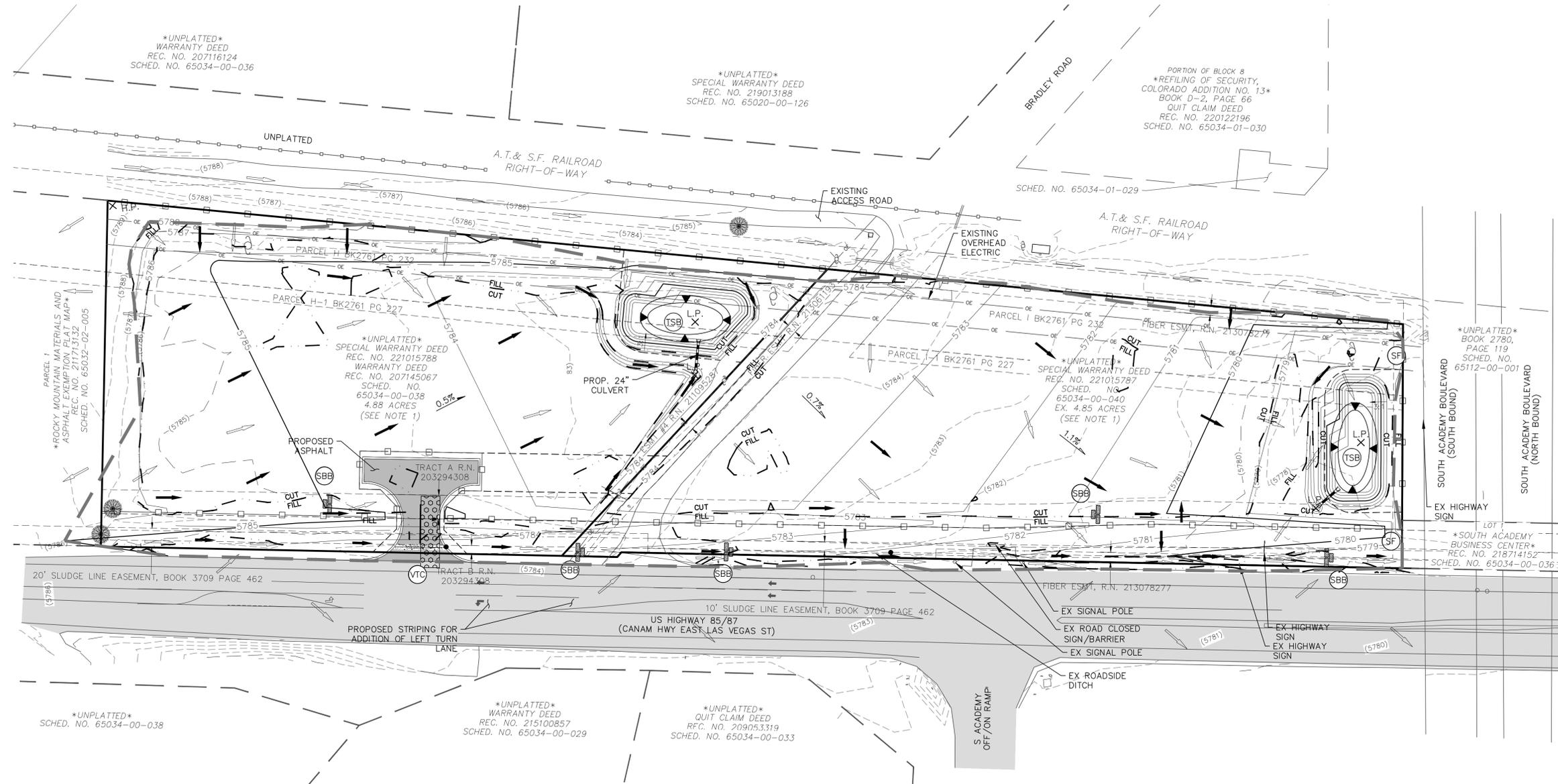


CAUTION

# BRADLEY POINT FILING NO. 1

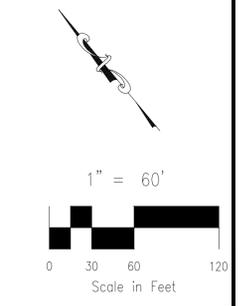
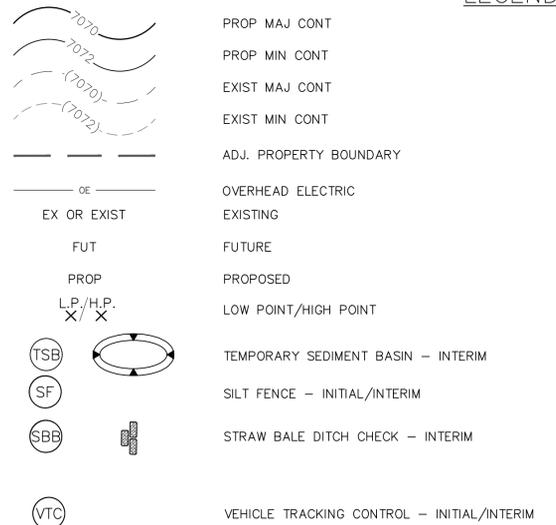
## GRADING AND EROSION CONTROL PLAN

### DECEMBER 2022



#### ADDITIONAL NOTES:

1. STAGING AND STOCKPILES AREA TO BE DETERMINED BY CONTRACTOR IN THE FIELD. THE LOCATIONS SHALL BE DELINEATED ON THIS PLAN BY THE CONTRACTOR.
2. THE EROSION CONTROL DELINEATED ON THIS PLAN SHALL BE REGULARLY UPDATED BY THE CONTRACTOR.
3. PROPOSED SLOPES SHALL BE 4:1 OR LESS.
4. THE CONTRACTOR SHALL OBTAIN A COPY OF THE GEOTECHNICAL ENGINEERING REPORT AND KEEP A COPY ONSITE DURING ALL EARTHWORK OPERATIONS.
5. THE CONTRACTOR SHALL PROVIDE SUFFICIENT BUFFER BETWEEN THE LIMITS OF DISTURBANCE AND AREAS IN WHICH NO GRADING SHALL OCCUR TO MAKE SUFFICIENT TIE IN BETWEEN THE PROPOSED GRADE AND EXISTING GRADE WHICH MAY NOT BE CLEARLY ILLUSTRATED ON THIS PLAN.
6. EXISTING VEGETATION CONSISTS OF SPARSE, NATIVE GRASSES; APPROXIMATELY 23.5% OF THE SITE IS COVERED IN AN AGGREGATE BASE MATERIAL IN THE EXISTING CONDITION.
7. FINAL STABILIZATION SHALL BE COMPLETED AT THE END OF THE CONSTRUCTION ACTIVITIES. ALL AREAS DISTURBED WITHIN THE CONSTRUCTION BOUNDARY/LIMITS OF DISTURBANCE AREA SHALL BE RESEEDED WITH NATIVE SEEDING.
8. NO PORTION OF THE PROPOSED CROSSROADS MIXED USE SITE LIES WITHIN A FEMA EFFECTIVE 100-YR FLOODPLAIN.
9. EROSION CONTROL BLANKET SHALL BE USED ON SLOPES GREATER THAN 4:1.
10. FENCE AND SIGNAGE ADDED TO KEEP ON-SITE STORED MATERIALS OUT OF THE PONDS.



FOR LOCATING & MARKING GAS, ELECTRIC, WATER & TELEPHONE LINES

FOR BURIED UTILITY INFORMATION  
48 HRS BEFORE YOU DIG  
CALL 1-800-922-1987

BRADLEY POINT FILING NO. 1
DATE: 12/07/22

GRADING & EROSION CONTROL PLAN
SCALE: HORIZONTAL: 1" = 60' VERTICAL: N/A

PROJECT NO. 70-074
DESIGNED BY: CWM

212 N. WARSATCH AVE., STE 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.955.5465
SHEET 2 OF 5

FOR AND ON BEHALF OF M&S CIVIL CONSULTANTS, INC.
CIVIL CONSULTANTS, INC.

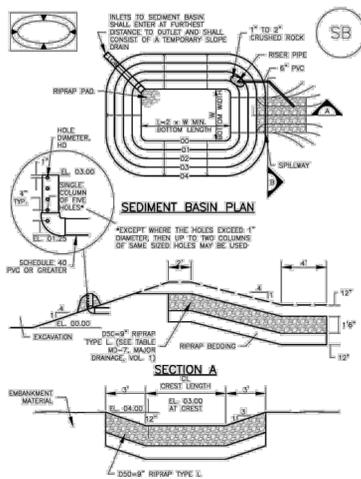
APPROVED BY:
NO. DATE: DESCRIPTION:

IRGUL A. SANCHEZ, COLORADO P.E. NO. 37160
THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.

CAUTION



**Sediment Basin (SB) SC-7**



August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 SB-5

**SC-7 Sediment Basin (SB)**

Upstream Drainage Area (Acres)	Basin Bottom Width (ft)	Spillway Crest Length (ft)	High Stormwater Depth (ft)
1	12.8	2	1/2
2	28	3	3/4
3	33.3	4	1
4	38.7	5	1 1/4
5	44.1	6	1 1/2
6	49.5	7	1 3/4
7	54.9	8	2
8	60.3	9	2 1/4
9	65.7	10	2 1/2
10	71.1	11	2 3/4
11	76.5	12	3
12	81.9	13	3 1/4
13	87.3	14	3 1/2
14	92.7	15	3 3/4
15	98.1	16	4

- SEDIMENT BASIN INSTALLATION NOTES**
- SEE PLAN VIEW FOR:
    - LOCATION OF SEDIMENT BASIN
    - TYPE OF BASIN (STANDARD BASIN OR NONSTANDARD BASIN)
    - FOR STANDARD BASIN, BOTTOM WIDTH W, CREST LENGTH CL, AND HOLE DIAMETER, HD.
    - FOR NONSTANDARD BASIN, SEE CONSTRUCTION DRAWINGS FOR DESIGN OF BASIN INCLUDING RISER HEIGHT H, NUMBER OF COLLARS N, HOLE DIAMETER HD AND PIPE DIAMETER D.
  - FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED.
  - SEDIMENT BASINS SHALL BE INSTALLED PRIOR TO ANY OTHER LAND-DISTURBING ACTIVITY THAT RELIES ON BASINS AS A EROSION CONTROL.
  - EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE NO. 200 SIEVE.
  - EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D698.
  - PIPE SCH 40 OR GREATER SHALL BE USED.
  - THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASINS FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR ANY SEDIMENT BASINS THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES.

SB-6 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 August 2013

**Sediment Basin (SB) SC-7**

- SEDIMENT BASIN MAINTENANCE NOTES**
- INSPECT BMPs EACH WINTER, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 48 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.
  - FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
  - WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON OCCURRENCE OF THE FAILURE.
  - SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN BMP EFFECTIVENESS. TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT O.E., TWO FEET BELOW THE SPILLWAY CREST.
  - SEDIMENT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS STABILIZED AND GRASS COVER IS ACCEPTED BY THE LOCAL JURISDICTION.
  - WHEN SEDIMENT BASINS ARE REMOVED, ALL DISTURBED AREAS SHALL BE COVERED WITH TOPSOIL, SEEDING AND MULCHED OR OTHERWISE STABILIZED AS APPROVED BY LOCAL JURISDICTION.
- NOTES ADAPTED FROM SOILS (404) (0.0000)
- NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM USDC STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 SB-7

**EC-2 Temporary and Permanent Seeding (TS/PS)**

soil amendments and rototill them into the soil to a depth of 6 inches or more.

Topsoil should be salvaged during grading operations for use and spread on areas to be revegetated later. Topsoil should be viewed as an important resource to be utilized for vegetation establishment, due to its water-holding capacity, structure, texture, organic matter content, biological activity, and nutrient content. The rooting depth of most native grasses in the semi-arid Denver metropolitan area is 6 to 18 inches. At a minimum, the upper 6 inches of topsoil should be stripped, stockpiled, and ultimately respread across areas that will be revegetated.

Where topsoil is not available, subsoils should be amended to provide an appropriate plant-growth medium. Organic matter, such as well-digested compost, can be added to improve soil characteristics conducive to plant growth. Other treatments can be used to adjust soil pH conditions when needed. Soil testing, which is typically inexpensive, should be completed to determine and optimize the types and amounts of amendments that are required.

If the disturbed ground surface is compacted, rip or rototill the surface prior to placing topsoil. If adding compost to the existing soil surface, rototilling is necessary. Surface roughening will assist in placement of a stable topsoil layer on steeper slopes, and allow infiltration and root penetration to greater depth.

Prior to seeding, the soil surface should be rough and the seedbed should be firm, but neither too loose nor compacted. The upper layer of soil should be in a condition suitable for seeding at the proper depth and conducive to plant growth. Seed-to-soil contact is the key to good germination.

- Seed Mix for Temporary Vegetation**
- To provide temporary vegetative cover on disturbed areas which will not be paved, built upon, or fully landscaped or worked for an extended period (typically 30 days or more), plant an annual grass appropriate for the time of planting and mulch the planted areas. Annual grasses suitable for the Denver metropolitan area are listed in Table TS/PS-1. These are to be considered only as general recommendations when specific design guidance for a particular site is not available. Local governments typically specify seed mixes appropriate for their jurisdiction.
- Seed Mix for Permanent Revegetation**
- To provide vegetative cover on disturbed areas that have reached final grade, a perennial grass mix should be established. Permanent seeding should be performed promptly (typically within 14 days) after reaching final grade. Each site will have different characteristics and a landscape professional or the local jurisdiction should be contacted to determine the most suitable seed mix for a specific site. In lieu of a specific recommendation, one of the perennial grass mixes appropriate for site conditions and growth season listed in Table TS/PS-2 can be used. The pure live seed (PLS) rates of application recommended in these tables are considered to be absolute minimum rates for seed applied using proper drill-seeding equipment.
- If desired for wildlife habitat or landscape diversity, shrubs such as rubber rabbitbrush (*Chrysothamnus nauseosus*), fourwing saltbush (*Atriplex canescens*) and skullbush sumac (*Rhus trilobata*) could be added to the upland seedmixes at 0.25, 0.5 and 1 pound PLS/acre, respectively. In riparian zones, planting stock of such species as American plum (*Prunus americana*), woods rose (*Rosa woodsii*), plains cottonwood (*Populus sargentii*), and willow (*Populus spp.*) may be considered. On non-topsoiled upland sites, a legume such as Ladak alfalfa at 1 pound PLS/acre can be included as a source of nitrogen for perennial grasses.

TS/PS-2 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 June 2012

**Temporary and Permanent Seeding (TS/PS) EC-2**

Seeding dates for the highest success probability of perennial species along the Front Range are generally in the spring from April through early May and in the fall after the first of September until the ground freezes. If the area is irrigated, seeding may occur in summer months, as well. See Table TS/PS-3 for appropriate seeding dates.

**Table TS/PS-1. Minimum Drill Seeding Rates for Various Temporary Annual Grasses**

Species* (Common name)	Growth Season	Pounds of Pure Live Seed (PLS)/acre	Planting Depth (inches)
1. Oats	Cool	35 - 50	1 - 2
2. Spring wheat	Cool	25 - 35	1 - 2
3. Spring barley	Cool	25 - 35	1 - 2
4. Annual ryegrass	Cool	10 - 15	1/2
5. Millet	Warm	3 - 15	1/2 - 3/4
6. Sudangrass	Warm	5 - 10	1/2 - 3/4
7. Sorghum	Warm	5 - 10	1/2 - 3/4
8. Winter wheat	Cool	20 - 35	1 - 2
9. Winter barley	Cool	20 - 35	1 - 2
10. Winter rye	Cool	20 - 35	1 - 2
11. Triticale	Cool	25 - 40	1 - 2

\* Successful seeding of annual grass resulting in adequate plant growth will usually produce enough dead-plant residue to provide protection from wind and water erosion for an additional year. This assumes that the cover is not disturbed or mowed closer than 8 inches.

Hydraulic seeding may be substituted for drilling only where slopes are steeper than 3:1 or where access limitations exist. When hydraulic seeding is used, hydraulic mulching should be applied as a separate operation, when practical, to prevent the seeds from being encapsulated in the mulch.

See Table TS/PS-3 for seeding dates. Irrigation, if consistently applied, may extend the use of cool season species during the summer months.

Seeding rates should be doubled if seed is broadcast, or increased by 50 percent if done using a Brillion Drill or by hydraulic seeding.

June 2012 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 TS/PS-3

**Temporary and Permanent Seeding (TS/PS) EC-2**

Seeding dates for the highest success probability of perennial species along the Front Range are generally in the spring from April through early May and in the fall after the first of September until the ground freezes. If the area is irrigated, seeding may occur in summer months, as well. See Table TS/PS-3 for appropriate seeding dates.

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5. Millet	Warm	3 - 15	1/2 - 3/4
6. Sudangrass	Warm	5 - 10	1/2 - 3/4
7. Sorghum	Warm	5 - 10	1/2 - 3/4
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9. Winter barley	Cool	20 - 35	1 - 2
10. Winter rye	Cool	20 - 35	1 - 2
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\* Successful seeding of annual grass resulting in adequate plant growth will usually produce enough dead-plant residue to provide protection from wind and water erosion for an additional year. This assumes that the cover is not disturbed or mowed closer than 8 inches.

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June 2012 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 TS/PS-3

**EC-2 Temporary and Permanent Seeding (TS/PS)**

**Table TS/PS-2. Minimum Drill Seeding Rates for Perennial Grasses**

Common Name	Botanical Name	Growth Season*	Growth Form	Seeds/Pound	Pounds of PLS/acre
<b>Alkali Soil Seed Mix</b>					
Alkali sacaton	<i>Sporobolus airoides</i>	Cool	Bunch	1,750,000	0.25
Basin wildrye	<i>Elymus cinereus</i>	Cool	Bunch	165,000	2.5
Solar streambank wheatgrass	<i>Agropyron riparium</i> 'Sodar'	Cool	Sod	170,000	2.5
Jose tall wheatgrass	<i>Agropyron elongatum</i> 'Jose'	Cool	Bunch	79,000	7.0
Arriba western wheatgrass	<i>Agropyron smithii</i> 'Arriba'	Cool	Sod	110,000	5.5
<b>Total</b>					<b>17.5</b>
<b>Fertile Loamy Soil Seed Mix</b>					
Ephraim crested wheatgrass	<i>Agropyron cristatum</i> 'Ephraim'	Cool	Sod	175,000	2.0
Darwin hard fescue	<i>Festuca ovina</i> 'Darwinia'	Cool	Bunch	545,000	1.0
Lincoln smooth brome	<i>Bromus inermis</i> 'Lynx'	Cool	Sod	130,000	3.0
Solar streambank wheatgrass	<i>Agropyron riparium</i> 'Sodar'	Cool	Sod	170,000	2.5
Arriba western wheatgrass	<i>Agropyron smithii</i> 'Arriba'	Cool	Sod	110,000	7.0
<b>Total</b>					<b>15.5</b>
<b>High Water Table Soil Seed Mix</b>					
Meadow foxtail	<i>Alopecurus pratensis</i>	Cool	Sod	900,000	0.5
Rushley	<i>Agrostis alba</i>	Warm	Open sod	5,000,000	0.25
Road cutgrass	<i>Poa compressa</i> 'Raben'	Cool	Sod	400,000	0.5
Lincoln smooth brome	<i>Bromus inermis</i> 'Lynx'	Cool	Sod	130,000	3.0
Pathfinder switchgrass	<i>Panicum oligosperum</i> 'Pathfinder'	Warm	Sod	389,000	1.0
Altair tall wheatgrass	<i>Agropyron elongatum</i> 'Altair'	Cool	Bunch	79,000	5.5
<b>Total</b>					<b>16.75</b>
<b>Transition Turf Seed Mix<sup>1</sup></b>					
Rueben Canadian bluegrass	<i>Poa compressa</i> 'Raben'	Cool	Sod	2,500,000	0.5
Darwin hard fescue	<i>Festuca ovina</i> 'Darwinia'	Cool	Bunch	545,000	1.0
Clinton perennial ryegrass	<i>Lolium perenne</i> 'Clinton'	Cool	Sod	247,000	3.0
Lincoln smooth brome	<i>Bromus inermis</i> 'Lynx'	Cool	Sod	130,000	3.0
<b>Total</b>					<b>7.5</b>

\* All of the above seeding mixes and rates are based on drill seeding followed by crimped straw mulch. These rates should be doubled if seed is broadcast and should be increased by 50 percent if the seeding is done using a Brillion Drill or is applied through hydraulic seeding. Hydraulic seeding may be substituted for drilling only where slopes are steeper than 3:1. If hydraulic seeding is used, hydraulic mulching should be done as a separate operation.

<sup>1</sup> See Table TS/PS-3 for seeding dates.

<sup>2</sup> If rate is to be applied, the transition turf seed rates should be doubled.

<sup>3</sup> Control wheatgrass should not be used on slopes steeper than 6:1 to 1:1.

<sup>4</sup> Can substitute 0.5 lbs PLS of blue grass for the 2.0 lbs PLS of Vaughn sidetown grass.

TS/PS-4 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 June 2012

**Temporary and Permanent Seeding (TS/PS) EC-2**

**Table TS/PS-2. Minimum Drill Seeding Rates for Perennial Grasses (cont.)**

Common Name	Botanical Name	Growth Season*	Growth Form	Seeds/Pound	Pounds of PLS/acre
<b>Sandy Soil Seed Mix</b>					
Blue grass	<i>Bouteloua gracilis</i>	Warm	Sod-forming bunchgrass	825,000	0.5
Campier little bluestem	<i>Schizachyrium scoparium</i> 'Campier'	Warm	Bunch	240,000	1.0
Prairie sandreed	<i>Calamagrostis longifolia</i>	Warm	Open sod	274,000	1.0
Sand dropseed	<i>Sporobolus vaginatus</i>	Cool	Bunch	5,298,000	0.25
Vaughn sidetown grass	<i>Bouteloua curtipendula</i> 'Vaughn'	Warm	Sod	191,000	2.0
Arriba western wheatgrass	<i>Agropyron smithii</i> 'Arriba'	Cool	Sod	110,000	5.5
<b>Total</b>					<b>10.25</b>
<b>Heavy Clay, Rocky, Poorhill Seed Mix</b>					
Ephraim crested wheatgrass <sup>1</sup>	<i>Agropyron cristatum</i> 'Ephraim'	Cool	Sod	175,000	1.5
Oahu intermediate wheatgrass	<i>Agropyron intermedium</i> 'Oahu'	Cool	Sod	115,000	5.5
Vaughn sidetown grass <sup>2</sup>	<i>Bouteloua curtipendula</i> 'Vaughn'	Warm	Sod	191,000	2.0
Lincoln smooth brome	<i>Bromus inermis</i> 'Lynx'	Cool	Sod	130,000	3.0
Arriba western wheatgrass	<i>Agropyron smithii</i> 'Arriba'	Cool	Sod	110,000	5.5
<b>Total</b>					<b>17.5</b>

<sup>1</sup> All of the above seeding mixes and rates are based on drill seeding followed by crimped straw mulch. These rates should be doubled if seed is broadcast and should be increased by 50 percent if the seeding is done using a Brillion Drill or is applied through hydraulic seeding. Hydraulic seeding may be substituted for drilling only where slopes are steeper than 3:1. If hydraulic seeding is used, hydraulic mulching should be done as a separate operation.

<sup>2</sup> See Table TS/PS-3 for seeding dates.

<sup>3</sup> If rate is to be applied, the transition turf seed rates should be doubled.

<sup>4</sup> Control wheatgrass should not be used on slopes steeper than 6:1 to 1:1.

<sup>5</sup> Can substitute 0.5 lbs PLS of blue grass for the 2.0 lbs PLS of Vaughn sidetown grass.

June 2012 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 TS/PS-5

**EC-2 Temporary and Permanent Seeding (TS/PS)**

**Table TS/PS-3. Seeding Dates for Annual and Perennial Grasses**

Seeding Dates	Annual Grasses (Numbers in table reference species in Table TS/PS-1)		Perennial Grasses	
	Warm	Cool	Warm	Cool
January 1-March 15	✓		✓	✓
March 16-April 30	4	1,2,3	✓	✓
May 1-May 15	4		✓	
May 16-June 30	4,5,6,7			
July 1-July 15	5,6,7			
July 16-August 31				
September 1-September 30		8,9,10,11		
October 1-December 31			✓	✓

**Mulch**

Cover seeded areas with mulch or an appropriate rolled erosion control product to promote establishment of vegetation. Anchor mulch by crimping, netting or use of a non-toxic tackifier. See the Mulching BMP Fact Sheet for additional guidance.

**Maintenance and Removal**

Monitor and observe seeded areas to identify areas of poor growth or areas that fail to germinate. Reseed and mulch these areas, as needed.

An area that has been permanently seeded should have a good stand of vegetation within one growing season if irrigated and within three growing seasons without irrigation in Colorado. Reseed portions of the site that fail to germinate or remain bare after the first growing season.

Seeded areas may require irrigation, particularly during extended dry periods. Targeted weed control may also be necessary.

Protect seeded areas from construction equipment and vehicle access.

TS/PS-6 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 June 2012

**Rolled Erosion Control Products (RECP) EC-6**

**Table RECP-1. ECTC Standard Specification for Temporary Rolled Erosion Control Products**  
(Adapted from Erosion Control Technology Council 2005)

Product Description	Slope Applications*	Channel Applications*	Minimum Tensile Strength <sup>1</sup>	Expected Longevity
Mulch Control Nets	5:1 (HV)	≤0.10 @ 5:1 0.25 lbs/ft <sup>2</sup> (12 Pa)	5 lbs/ft (0.073 kN/m)	
Netless Rolled Erosion Control Blankets	4:1 (HV)	≤0.10 @ 4:1 0.5 lbs/ft <sup>2</sup> (24 Pa)	5 lbs/ft (0.073 kN/m)	Up to 12 months
Single-net Erosion Control Blankets & Open Weave Textiles	3:1 (HV)	≤0.15 @ 3:1 1.5 lbs/ft <sup>2</sup> (72 Pa)	50 lbs/ft (0.73 kN/m)	
Double-net Erosion Control Blankets	2:1 (HV)	≤0.20 @ 2:1 2.1 lbs/ft <sup>2</sup> (84 Pa)	75 lbs/ft (1.09 kN/m)	
Mulch Control Nets	5:1 (HV)	≤0.10 @ 5:1 0.25 lbs/ft <sup>2</sup> (12 Pa)	25 lbs/ft (0.36 kN/m)	24 months
Erosion Control Blankets & Open Weave Textiles (slowly degrading)	1.5:1 (HV)	≤0.25 @ 1.5:1 2.00 lbs/ft <sup>2</sup> (96 Pa)	100 lbs/ft (1.45 kN/m)	24 months
Erosion Control Blankets & Open Weave Textiles	1:1 (HV)	≤0.25 @ 1:1 2.25 lbs/ft <sup>2</sup> (108 Pa)	125 lbs/ft (1.82 kN/m)	36 months

\* C Factor and shear stress for mulch control nettings must be obtained with netting used in conjunction with pre-applied mulch material. (See Section 3.3 of Chapter 7 Construction BMPs for more information on the C Factor).

<sup>1</sup> Minimum Average Roll Values, Machine direction using ECTC Mod. ASTM D 5035.

<sup>2</sup> C Factor calculated as ratio of soil loss from RECP protected slope (tested at specified or greater gradient, HV) to ratio of soil loss from unprotected (control) plot in large-scale testing.

<sup>3</sup> Required minimum shear stress RECP (unvegetated) can sustain without physical damage or excess erosion (> 12.7 mm (0.5 in) soil loss) during a 30-minute flow event in large-scale testing.

<sup>4</sup> The permissible shear stress levels established for each performance category are based on historical experience with products characterized by Manning's roughness coefficients in the range of 0.01 - 0.05.

<sup>5</sup> Acceptable large-scale test methods may include ASTM D 6459, or other independent testing deemed acceptable by the engineer.

<sup>6</sup> Per the engineer's discretion. Recommended acceptable large-scale testing protocol may include ASTM D 6460, or other independent testing deemed acceptable by the engineer.

November 2010 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 RECP-3

BRADLEY POINT FILING NO. 1

GRADING & EROSION CONTROL DETAILS

PROJECT NO. 70-074

DATE: 5/27/21

SCALE: HORIZONTAL: N/A VERTICAL: N/A

DESIGNED BY: CW DRAWN BY: CW CHECKED BY: DLM

212 N. WABASH AVE., STE. 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.553.3463

WIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160

FOR AND ON BEHALF OF CIVIL CONSULTANTS, INC.

NO.	DATE	ARR'D. BY:	DESCRIPTION:

THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR UNAUTHORIZED CHANGES TO OR ALTERATIONS OF THESE PLANS. ALL CHANGES TO BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.

CAUTION

**EC-6 Rolled Erosion Control Products (RECP)**

**Table RECP-2. ECTC Standard Specification for Permanent<sup>1</sup> Rolled Erosion Control Products**  
(Adapted from: Erosion Control Technology Council 2005)

Product Type	Slope Applications	Channel Applications	
		Maximum Shear Stress <sup>2</sup>	Minimum Tensile Strength <sup>3</sup>
TRMs with a minimum thickness of 0.25 inches (6.35 mm) per ASTM D 6525 and UV stability of 90% per ASTM D 4355 (500 hours exposure).	0.5:1 (H:V)	6.0 lbs/ft <sup>2</sup> (288 Pa)	125 lbs/ft (1.82 kN/m)
	0.5:1 (H:V)	8.0 lbs/ft <sup>2</sup> (384 Pa)	150 lbs/ft (2.19 kN/m)
	0.5:1 (H:V)	10.0 lbs/ft <sup>2</sup> (480 Pa)	175 lbs/ft (2.55 kN/m)

<sup>1</sup> For TRMs containing degradable components, all property values must be obtained on the non-degradable portion of the matting alone.  
<sup>2</sup> Minimum Average Roll Values, machine direction only for tensile strength determination using ASTM D 6818 (Supersede Mod. ASTM D 5033 for RECPs)  
<sup>3</sup> Field conditions with high loading and/or high survivability requirements may warrant the use of a TRM with a tensile strength of 44 kN/m (3,000 lb/ft) or greater.  
<sup>4</sup> Required minimum shear stress TRM (fully vegetated) can sustain without physical damage or excess erosion (> 12.7 mm (0.5 in.) soil loss) during a 30-minute flow event in large scale testing.  
<sup>5</sup> Acceptable large-scale testing protocols may include ASTM D 6460, or other independent testing deemed acceptable by the engineer.

**Design and Installation**

RECPs should be installed according to manufacturer's specifications and guidelines. Regardless of the type of product used, it is important to ensure no gaps or voids exist under the material and that all corners of the material are secured using stakes and trenching. Continuous contact between the product and the soil is necessary to avoid failure. Never use metal stakes to secure temporary erosion control products. Often wooden stakes are used to anchor RECPs; however, wood stakes may present installation and maintenance challenges and generally take a long time to biodegrade. Some local jurisdictions have had favorable experiences using biodegradable stakes.

This BMP Fact Sheet provides design details for several commonly used ECB applications, including:

- ECB-1 Pipe Outlet to Drainage
- ECB-2 Small Ditch or Drainage
- ECB-3 Outside of Drainage

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**Rolled Erosion Control Products (RECP) EC-6**

Staking patterns are also provided in the design details according to these factors:

- ECB type
- Slope or channel type

For other types of RECPs including TRMs, these design details are intended to serve as general guidelines for design and installation; however, engineers should adhere to manufacturer's installation recommendations.

**Maintenance and Removal**

Inspection of erosion control blankets and other RECPs includes:

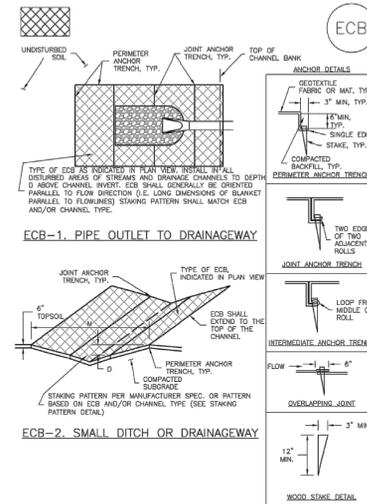
- Check for general signs of erosion, including voids beneath the mat. If voids are apparent, fill the void with suitable soil and replace the erosion control blanket, following the appropriate staking pattern.
- Check for damaged or loose stakes and secure loose portions of the blanket.

Erosion control blankets and other RECPs that are biodegradable typically do not need to be removed after construction. If they must be removed, then an alternate soil stabilization method should be installed promptly following removal.

Turf reinforcement mats, although generally resistant to biodegradation, are typically left in place as a dense vegetated cover grows in through the mat matrix. The turf reinforcement mat provides long-term stability and helps the established vegetation resist erosive forces.

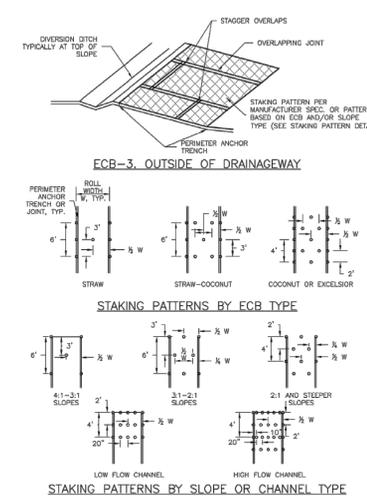
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**EC-6 Rolled Erosion Control Products (RECP)**



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**Rolled Erosion Control Products (RECP) EC-6**



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**EC-6 Rolled Erosion Control Products (RECP)**

**EROSION CONTROL BLANKET INSTALLATION NOTES**

- SEE PLAN VIEW FOR:
  - LOCATION OF ECB.
  - TYPE OF ECB (STRAW, STRAW-COCONUT, COCONUT, OR EXCELSIOR).
  - AREA, IN SQUARE YARDS OF EACH TYPE OF ECB.
- 100% NATURAL AND BIODEGRADABLE MATERIALS ARE PREFERRED FOR RECPs, ALTHOUGH SOME JURISDICTIONS MAY ALLOW OTHER MATERIALS IN SOME APPLICATIONS.
- IN AREAS WHERE ECBs ARE SHOWN ON THE PLAN, THE PERIMETER SHALL PLACE TOPSOIL AND PERFORM FINAL GRADING, SURFACE PREPARATION, AND SEEDING AND MULCHING. SURFACE SHALL BE SMOOTH AND MOIST PRIOR TO ECB INSTALLATION AND THE ECB SHALL BE IN FULL CONTACT WITH SUBGRADE. NO GAPS OR VOIDS SHALL EXIST UNDER THE BLANKET.
- PERIMETER ANCHOR TRENCH SHALL BE USED ALONG THE OUTSIDE PERIMETER OF ALL BLANKET AREAS.
- JOINT ANCHOR TRENCH SHALL BE USED TO JOIN ROLLS OF ECBs TOGETHER (LONGITUDINALLY AND TRANSVERSELY) FOR ALL ECBs EXCEPT STRAW WHICH MAY USE AN OVERLAPPING JOINT.
- INTERMEDIATE ANCHOR TRENCH SHALL BE USED AT SPACING OF ONE-HALF ROLL LENGTH FOR COCONUT AND EXCELSIOR ECBs.
- OVERLAPPING JOINT DETAIL SHALL BE USED TO JOIN ROLLS OF ECBs TOGETHER FOR ECBs ON SLOPES.
- MATERIAL SPECIFICATIONS OF ECBs SHALL CONFORM TO TABLE ECB-1.
- ANY AREAS OF SEEDING AND MULCHING DISTURBED IN THE PROCESS OF INSTALLING ECBs SHALL BE RESEED AND MULCHED.
- DETAILS ON DESIGN PLANS FOR MAJOR DRAINAGEWAY STABILIZATION WILL GOVERN IF DIFFERENT FROM THOSE SHOWN HERE.

TYPE	COCONUT CONTENT	STRAW CONTENT	EXCELSIOR CONTENT	RECOMMENDED "NETTING"
STRAW	-	100%	-	DOUBLE/NATURAL
STRAW-COCONUT	30% MIN	70% MAX	-	DOUBLE/NATURAL
COCONUT	100%	-	-	DOUBLE/NATURAL
EXCELSIOR	-	-	100%	DOUBLE/NATURAL

NOTE: FOR USE ONLY IN AREAS SUBJECT TO EROSION AND DRAINAGE CHANNELS. MATERIALS NOTED MAY BE RESEEDED IN SOME JURISDICTIONS.

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**Rolled Erosion Control Products (RECP) EC-6**

**EROSION CONTROL BLANKET MAINTENANCE NOTES**

- INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.
- FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
- WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.
- ECBs SHALL BE LEFT IN PLACE TO EVENTUALLY BIODEGRADE, UNLESS REQUESTED TO BE REMOVED BY THE LOCAL JURISDICTION.
- ANY ECB PULLED OUT, TORN, OR OTHERWISE DAMAGED SHALL BE REPAIRED OR REPLACED. ANY SUBGRADE AREAS BELOW THE GEOTEXTILE THAT HAVE ERODED TO CREATE A VOID UNDER THE BLANKET, OR THAT REMAIN DEVOID OF GRASS SHALL BE REPAIRED, RESEEDED AND MULCHED AND THE ECB REINSTALLED.

NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM USDC STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

(DETAILS ADAPTED FROM DOUGLAS COUNTY, COLORADO AND TOWN OF PARKER, COLORADO, NOT AVAILABLE IN AUTOCAD)

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BRADLEY POINT FILING NO. 1  
 GRADING & EROSION CONTROL DETAILS  
 PROJECT NO. 70-074  
 SCALE: HORIZONTAL: N/A  
 VERTICAL: N/A  
 DATE: 5/27/21  
 SHEET 5 OF 5  
 GR05

212 N. WABASH AVE, STE 305  
 COLORADO SPRINGS, CO 80903  
 PHONE: 719.555.3463

CIVIL CONSULTANTS, INC.

VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160

FOR AND ON BEHALF OF CIVIL CONSULTANTS, INC.

REVISIONS:

NO.	DATE	DESCRIPTION	ARR'D. BY	DATE

THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR UNAUTHORIZED CHANGES TO OR ALTERATIONS OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.

CAUTION

FOR LOCATING & MARKING GAS, ELECTRIC, WATER & TELEPHONE LINES

FOR BURIED UTILITY INFORMATION CALL 1-800-922-1987