

Grandview Reserve Master Development Drainage Plan

April 2020

HR Green Project No: 191850

Prepared For:

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Engineer's Statement

This report and plan for the drainage design of the development , Grandview Reserve, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *El Paso County Drainage Criteria Manual* and is in conformity with the master plan of the drainage basin. I understand that El Paso County does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Chris McFarland, PE Date

State of Colorado No. 44947

For and on behalf of HR Green Development, LLC

Developer's Statement

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

4 Site Investments LLC

By: _____

Title: _____

Address: _____

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.

County Engineer/ECM Administrator

Date

Master Development Drainage Plan – Grandview Reserve

I. General Purpose, Location and Description

a. Purpose and Scope of study

The Purpose of this Master Development Drainage Plan (MDDP) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, areas tributary to the site and the planned storm water management for Grandview Reserve 2 development. The items discussed in this report are preliminary in nature and final drainage calculations and design will be required as development proceeds. This report provides a general drainage concept and guidance for future development of Grandview Reserve.

b. DBPS Investigations

The Gieck Ranch Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by Drexel, Barrell was reviewed to determine existing plans and constraints that would influence the design of Grandview Reserve. The proposed plans for Grandview Reserve are in general conformance with the DBPS.

The DBPS shows 4 reaches through Grandview Reserve. The Main Stem (MS) in the south western portion of the site, the Main Stem Tributary #2 (MST2) to the north and east of the Main Stem, the East Fork Tributary (EFT) in the middle of the site north and east of MST2, and the East Fork Upper (EF) at the north east side of the site. These drainageways have been reviewed in the following reports and further analysis will be completed of these major drainageways in future planning documents.

- Unnamed Tributary Black Squirrel Creek, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004
- Haegler and Gieck Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004
- Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006
- Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)

c. Agency Jurisdictions

Listed below are the jurisdictions that this project will conform to:

El Paso County

Falcon Colorado Municipal Code (where applicable)

Federal Emergency Management Agency

d. General Project Description

Grandview Reserve is located in Falcon, Colorado within El Paso County and contains approximately 765 acres within the south half of section 21 and 22 and the north half of section 27 and 28, Township 12 South, and Range 66 West of the Sixth Principal Meridian in El Paso County, Colorado. See below for approximate site location.



Figure 1 - Site Map

e. Data Sources

Listed Below are the technical resources reviewed in the preparation of this MDDP:

- City of Colorado Springs Drainage Criteria Manual (DCM), Volumes 1 and 2
- Mile High Flood District
- NOAA Atlas 14
- NRCS Soil Survey for El Paso County Area, Colorado
- FEMA FIRM 08041C0556G and FIRM 08041C0552G (eff. 12/7/2018)
- El Paso County Assessor Property Records

f. Applicable Criteria and Standards

Per the DBPS, flows from the proposed site will be limited to historic flows in an effort to maintain the stability and of the existing channels with the drainage basin. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended.

II. Project Characteristics

a. Location in Drainage Basin, offsite flows, size

Grandview Reserve is located within the Gieck Ranch Drainage Basin which covers approximately 22 square miles. This drainage basin is tributary to Black Squirrel Creek and joins said creek just to the south of Elicott, CO about 18 miles to the south. Black Squirrel Creek eventually drains to the Arkansas River in Pueblo Colorado. The majority of the Gieck Ranch Drainage basin is undeveloped consisting of rural farmland. The Geick Ranch Drainage basin is also recognized as the Haegler Ranch drainage basin.

lies north of ?

As part of the Fourway LOMR discussed above, the study reviewed the hydrology and hydraulics for the Main Stem Tributaries, however only a small portion of the site within Grandview was analyzed. The peak flows rates for the Main Stem fo " 100 year event was 413 cfs and for the Main Stem Tributary was 280 cfs.

revised

For the East Fork tributaries (EF and EFT), the DBPS established 100 year flow rates of 595 cfs for the East Fork (EF) and 217 cfs for the East Fork Tributary (EFT)

Generally offsite flows are conveyed through the site via the 4 tributaries. Minor offsite basins may sheet flow onto the site. These flows will be routed through the site via the tributaries.

b. Compliance with DBPS

This MDDP is in general conformance with the guidelines outlined in the Gieck Ranch DBPS. Grandview Reserve will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

c. Site Characteristic

Per the NRCS web soil survey, the site is made up entirely of Type A and B soils. The majority of which are Type A soils. The predominate soils are Blakeland loamy sand, Columbine gravelly sandy loam, and Stapleton sandy loam. The first two soils are Type A soil and cover approximately 55.1% of the site and the later soil is a Type B soil and covers the remaining 44.9% of the site. See Appendix A for the NRCS soil map.

Current ground cover is predominantly short- to mid-grass prairie grasslands and former farmland which consists of nonnative weeds and grasses. The site has very few, if any, trees and a minimal number of shrubs are found on the site.

d. Major drainage ways and structures

As mentioned previously, 4 major drainage ways exist on the site. These convey existing on and off-site flows and current on site flows through the site in a southeasterly direction. The drainageways eventually cross Highway 24 via culverts and other structures; further survey will be conducted to determine their effectiveness as the development of the site progresses.

A breached stock pond is located along the Main Stem and the effects of the existing breached dam are unknown at this time. As development occurs, this dam will be completely removed and improvements will be constructed along the channels to become high functioning low maintenance drainageway corridors.

e. Existing and proposed land uses

The existing site is open rangeland and farmland with no visible structures. The proposed development will consist of low, medium, and high density residential, along with two institutional sites, multiple pocket park sites, a large community park and a commercial area adjacent to Highway 24. The current land plan assumes approximately 3,261 dwelling units will be constructed on the site.

Provide description or table of proposed lot sizes as applicable in the density categories (high, medium, low...) used below.

III. Hydrologic Analysis

a. Major Basins and subbasins

Major Basins Table Added

- Previous basin study. Creek Ranch Drainage Basin Planning Study
- Per FEMA FIRM 08041C0556G and 08041C0552G (eff. 12/7/2018), Grandview Reserve has four mapped channels within its boundaries.
- Per aerial imaging, no major irrigation is in the vicinity that would affect Grandview Reserve.

The site has been divided into 8 major drainage basins per where each basin is tributary to a full spectrum detention pond facility. These basins and as assumed a reference for previous comment

Subbasin Description

The entire site drains in a south easterly direction and is divided into 18 subbasins together as described below.

assumed a reference for previous comment

- Subbasin A1 is located in the southwestern corner of the site, to the south and west of MS. The basin drains towards the southeast to proposed detention pond A. Current planning documents call for medium density dwelling units and a small pocket park. The basin is 37.00 acres, with a composite impervious value of 35.22% and runoff rates for the 5 and 100 year of 30.72 cfs and 100.64 cfs respectively. The pond will discharge at predevelopment rates and into MS via the ponds outlet structure.
- Subbasin B1 is located between MS and MST2 to the east of subbasin A1. The basin drains towards the southeast and towards subbasin B2. Current planning documents call for medium density dwelling units and a small pocket park. The basin is 10.00 acres, with a composite impervious value of 35.22% and runoff rates for the 5 and 100 year of 12.36 cfs and 40.08 cfs respectively. The pond will discharge at predevelopment rates and into MS via the ponds outlet structure.

density dwelling units and some parkland area. The basin is 37.00 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 29.46 cfs and 97.08 cfs respectively.

- Subbasin B² is located between MS and MST2 to the northeast of subbasin A1. The basin is Detention Pond B. Current planning documents call for medium density dwelling units and a pocket park. The basin is 24.89 acres, with a composite impervious value of 43.26% and runoff rates for the 5 and 100 year of 12.02 cfs and 42.26 cfs respectively.
calculations reviewed and 42.26 verified. **Please refer to**
calculations in appendix
- Subbasin C is located through the existing MS towards Detention Pond C. The basin drains towards the southeast and towards the south of basin B1 and the existing MST2 tributary runs through an institutional parcel, medium and high density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 51.20% and runoff rates for the 5 and 100 year of 77.99 cfs and 238.03 cfs respectively.
- Subbasin D1 is located between MS and MST2 to the east of Basin B3 and adjacent to the MST2 channel. The basin drains towards the southeast and towards drainage basin D2. Current planning documents call for medium density dwelling units along with a pocket park. The basin is 24.33 acres, with a composite impervious value of 53.89% and runoff rates for the 5 and 100 year of 24.15 cfs and 70.07 cfs respectively.
- Subbasin D2 is located between MS and MST2 to the south of basins D1 and B3. The basin drains towards the southwest and towards detention pond D. Current planning documents call for high density dwelling units along with a pocket park and a commercial parcel. The basin is 77.90 acres, with a composite impervious value of 62.10% and runoff rates for the 5 and 100 year of 98.47 cfs and 252.18 cfs respectively.
- Subbasin E1 is located just east of EFT along the northern portion of the site. The basin drains towards the southeast and towards basins F3 and F4. Current planning documents call for low density dwelling units. The basin is 88.60 acres, with a composite impervious value of 19.54% and runoff rates for the 5 and 100 year of 46.88 cfs and 178.04 cfs respectively.
- Subbasin F1 is located east of basin E1 and between EFT and EF along the northern portion of the site. The basin drains towards the southeast and towards basin F3 and F4. Current planning documents call for a large community park, high density dwelling units, commercial site and an institution parcel. The basin is 33.73 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 16.28 cfs and 58.95 cfs respectively.
- Subbasin F2 is located east of the existing drainage channel EFT. The basin drains towards the southwest and towards basin F4 and to the EFT drainage channel which runs parallel to the north east with Highway 24. Current planning documents call for high density dwelling units and

seems low

commercial space. The basin is 67.64 acres, with a composite impervious value of 51.39% and runoff rates for the 5 and 100 year of 60.11 cfs and 170.90 cfs respectively.

- Subbasin F3 is located west of the existing drainage channel EF. The basin drains towards the ge channel EF but will be conveyed south towards subbasin F4. nts call for medium density dwelling units. The basin is 12.84 acres, bus value of 45.00% and runoff rates for the 5 and 100 year of 11.36 cfs /.

est of the existing drainage channel EF and south of subbasins F1 and ards the southeast towards detention pond F. Current planning n and medium-high density dwelling units. The basin is 51.81 acres, bus value of 49.54% and runoff rates for the 5 and 100 year of 42.32 cfs ly.

- Subbasin E4 is located east of the existing drainage channel EFT along the northern property ns towards the southeast towards detention pond G. Current planning documents call for medium density dwelling units and a park. The basin is 20.13 acres, with a composite impervious value of 36.52% and runoff rates for the 5 and 100 year of 13.78 cfs and 43.95 cfs respectively.

• Subbasin G2 is located east of the existing drainage channel EFT along the northern property boundary. The basin drains towards the southeast towards detention pond G. Current planning documents call for low density dwelling units. The basin is 15.14 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 6.55 cfs and 23.95 cfs respectively.

- Subbasin H1 is located in the northeast corner of the site and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for low density dwelling units and smallpark. The basin is 20.71 acres, with a composite impervious value of 24.49% and runoff rates for the 5 and 100 year of 5.68 cfs and 27.62 cfs respectively.

• Subbasin H2 is located south of basin G2 and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for medium density dwelling units and smallpark. The basin is 18.55 acres, with a composite impervious value of 46.68% and runoff rates for the 5 and 100 year of 16.24 cfs and 47.62 cfs respectively.

- Subbasin H3 is located south of basin H2 and east of the existing drainage channel EFT. The basin drains towards the southeast towards subbasin H4. Current planning documents call for medium density dwelling units and smallpark. The basin is 6.01 acres, with a composite impervious value of 40.57% and runoff rates for the 5 and 100 year of 5.21 cfs and 15.60 cfs respectively.

- Subbasin H4 is located south of basin H2 and east of the existing drainage channel EFT and basin H3. The basin drains towards the south towards detention pond H. Current planning documents call for medium density dwelling units and park/open space area. The basin is 27.65

seems low

acres, with a composite impervious value of 38.24% and runoff rates for the 5 and 100 year of 20.93 cfs and 64.71 cfs respectively.

The above mentioned basins are large planning area basins and as drainage reports are developed for the individual developed parcels additional drainage reports and calculations will be required. It is expected that storm drainage infrastructure consisting of inlets, storm sewer and open drainage channels will be constructed as the property develops.

b. Methodology

Design rainfall was determined utilizing figures from the NOAA Atlas 14, Volume 8, Version 2 to determine the 5-year and 100-year rainfall values for 1, 6 and 24-hour events. The 1-hour rainfall depths are 1.22 and 2.50 in/hr respectively, 6 hour 1.79 and 3.87 in/hr respectively and 2.36 and 4.90 in/hr for the 24 hour event. The rainfall values were then used as inputs into the Colorado Urban Hydrograph Procedure (CUHP) spreadsheets to determine runoff values for both pre-development and post-development site.

CUHP is an evolution of the Snyder unit hydrograph and is calibrated for use along the Colorado Front Range. 1 Hour rainfall amounts are input into the program to produce a storm hyetograph that is then used to calculate a storm hydrograph for each basin depending on the subbasins properties including slope, length, shape, impervious area, pervious depression storage area, and various infiltration rates. Tabular hydrographs are then computed and can be used in EPA SWMM. The CUHP results are included within Appendix B.

EPA SWMM was used to determine flow routing via the kinematic wave method. Subbasins were routed to their respective design points and detention ponds for both the developed and predeveloped condition to determine peak runoff amounts for the 5-year and 100-year storm events. Information from these models along with information and calculations performed in the Colorado Springs BMP spreadsheets was used to determine pond sizing calculations and release rates.

c. Basin Hydrology

A summary of the flows for both the predeveloped and developed cases for each basin, subbasin and Pond are found on next page along with the full computation found in Appendix B.

SWMM Basin and Pond Summary						
Basin Description	Basin Area (ac)	% Impervious	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)	5 Year Pond Volume (ac-ft)	100 Year Pond Volume (ac-ft)
A1	45.38	35.22%	30.72	100.64		
			Pond A		1.83	3.50
B1	37.00	45.00%	29.46	97.08		
B2	24.89	43.26%	12.02	42.26		
B3	118.90	49.42%	92.76	295.27		
			Pond B		5.90	19.00
C1	77.83	51.20%	77.99	238.03		
			Pond C		3.91	6.87
D1	24.33	44.14%	24.15	70.07		
D2	77.90	62.10%	98.47	252.18		
			Pond D		6.61	10.19
E1	88.60	19.54%	46.88	178.04		
			Pond E		1.96	2.44
F1	33.73	25.00%	16.28	58.95		
F2	67.64	51.39%	60.11	170.90		
F3	12.84	45.00%	11.36	32.93		
F4	51.81	46.54%	42.32	124.89		
			Pond F		7.38	12.62
G1	20.13	36.52%	13.78	43.95		
G2	15.14	25.00%	6.55	23.95		
			Pond G		0.72	2.03
H1	20.71	24.49%	5.68	27.62		
H2	18.55	43.68%	16.24	47.62		
H3	6.01	40.57%	5.21	15.60		
H4	27.65	38.24%	20.93	64.71		
			Pond H		2.93	6.17

IV. Hydraulic Analysis

a. Major Drainageways

In general the site runoff runs into the 4 major drainageways and in a southeasterly direction. These basins are described in more detail below:

The Main Stem (MS) in the south western portion of the site, the Main Stem Tributary #2 (MST2) to the north and east of the Main Stem, the East Fork Tributary (EFT) in the middle of the site north and east of MST2, and the East Fork Upper (EF)

Include approximate culvert sizes if known.

The Main Stem (MS) is in the southwestern portion of the site. Offsite flows collect and are conveyed under Easto **sizes** vert. MS travels in a southeasterly direction and combines with the Main Stem Tributary **unknown** site and then is conveyed past Highway 24 via a culvert. Jurisdictional wetlands exist and the area is within a Zone A floodplain towards the southern portion of the site. This channel sees only intermittent flows at this time however once development occurs there may be a more constant baseflow.

MST2 crosses Eastonville road via an existing culvert and flows through the site in a southeasterly direction. An existing breached stock pond exists in the approximate center point of the channel within the site. Portions of this channel are within a mapped floodplain as shown in the existing FIRM Panel. Per a July email from the USACE this drainage channel was determined to be a non-jurisdictional waters/wetland.

The East Fork tributary (EFT) crosses the north property line and are conveyed through the site via a natural channel. The channel has been mapped as a Zone A floodplain per the existing FIRM panel. There is no existing crossing for this section of the drainage channel below Highway 24 and instead the flows are conveyed to the north east towards the East Fork Upper (EF). Per a July email from the USACE this drainage channel was determined to be a non-jurisdictional waters/wetland.

The EF crosses the north property line approximately 1500' east of the EFT crossing. The flow through the site is via a **Note added** Zone A floodplain. The channel is mapped as a Highway 24 via an existing shallow bridge. The EF and EFT eventually merge approximately 1750 southeast of the site, however as mentioned above Highway 24 blocks the flow of the EFT and flows are conveyed northeast to the EF bridge crossing.

These drainageways will require further analysis and design which will be completed as the project progresses.

Does FEMA modeling show velocities that may require channel stabilization? Mention types of stabilization that may be required.

V. Environmental Evaluations

a. Significant existing or potential wetland and riparian areas impacts

As part of this work, the developer has engaged Ecosystem Services, LLC (ECOS) to perform environmental studies of the site that will be submitted with the planning documents. Major information from these report related to the wetlands shows that two of the tributaries through the site, the Main Stem and the East Fork contain jurisdictional wetlands and the other two tributaries, the East Fork Tributary and the Main Stem Tributary #2 are non-jurisdictional wetlands.

At this time, only minor improvements to the jurisdictional channels are proposed. These stream improvements will be made with keeping the natural habitat intact and the natural function of these channels as it is to maintain the wetland habitat. The non-jurisdictional channels will be modified and the design of those channels is forthcoming.

b. Stormwater quality considerations and proposed practices

As part of the development, full spectrum detention facilities will be installed to provide water quality for the development. The facilities will be designed using El Paso County criteria and provide stormwater quality by slowing the release of stormwater captured by the ponds and allowing solids to settle out. Additionally when possible the revised drainage channels, which were not jurisdictional wetlands, will be

used to convey stormwater via a natural channel. The natural channel will provide an pervious means to transport stormwater and provide some water quality benefits as well.

On site practices for schools, churches and other buildings should use means such that impervious areas drain across pervious area to allow for infiltration during the minor events. This would include discharge of the gutters onto landscape areas vs. directly connecting to storm sewer and using natural ditches and swales where it is logical and makes sense to convey stormwater inlieu of storm sewer piping.

c. Permitting requirements

When work infringes upon the wetlands or floodplain a 404 Permit will be required. If the work within the waterways is minimal, it will likely be covered under a nationwide 404 permit; it is however possible that an individual permits will be required.

The Colorado Department of Public **statements** will require permits for any disturbance that exceed 1 acre of land. Should gr**added** a dewatering permit will also be required.

EI Paso County will require an Erosion and Stormwater Quality Control Permit and any other construction permits required to complete the construction of the site.

Add FEMA LOMR requirements and Floodplain Development permits.

VI. Selected Plan

a. Plan Hydrology

This MDDP schematically addressed on-site and off-site drainage patterns using the existing topography and proposed land use plan for the overall drainage design. Individual preliminary and final drainage reports will better define the planning areas as the site is developed. These reports will include inlet design, storm sewer hydraulics, street design and other requirements typical of more detailed drainage reports.

The overall site is divided into 8 separate major basins, basins A-H and contribute to individual detention ponds for each major basin. Basin sizes range from 35 acres to 181 acres in size. Basins A, B, C and D drain and eventually discharge into the Main Stem and Main Stream Tributary #2. Basins E, F, G, and H drain towards the East Fork Drainage channel.

The sub-basins are described in additional detail above.

b. Detention Ponds

The site plans propose the construction of 8 separate full spectrum detention facilities.

- Pond A is located in the southwest corner of the site and discharges into the Main Stem drainageway. The pond is planned to store a maximum of 4.05 ac-ft during the 100 year event and have a peak outflow of 55.9 cfs which is slightly below the pre development peak outflow of 57.1 cfs. The 5 year storage volume is 2.46 ac-ft with a peak outflow of 3.7 cfs.
- Pond B is located to the east of Pond A and the Main Stem and discharges into the Main Stem Tributary #2. The pond is planned to store a maximum of 16.60 ac-ft during the 100 year event

and have a peak outflow of 165.4 cfs which is slightly above the pre development peak outflow of 164.2 cfs. The 5 year storage volume is 8.44 ac-ft with a peak outflow of 2.6 cfs.

- Pond C is located near the center of the western portion of the site near the existing Main Stem Tributary #2. The pond discharges into a revised open channel to be designed and discharges to the Main Stem Tributary #2 which merges with the Main Stem Tributary just off site. The pond is planned to store a maximum of 6.91 ac-ft during the 100 year event and have a peak outflow of 119.2 cfs which is slightly below the pre development peak outflow of 120.2 cfs. The 5 year storage volume is 4.07 ac-ft with a peak outflow of 1.5 cfs.
- Pond D is located near the southern portion of the site adjacent to Highway 24. The pond discharges into the Main Stem right after the Main Stem and Main Stem Tributary #2 merge. The pond is planned to store a maximum of 9.41 ac-ft during the 100 year event and have a peak outflow of 154.4 cfs which equals the predevelopment peak flow rate. The 5 year storage volume is 6.28 ac-ft with a peak outflow of 2.0 cfs.
- Pond E is located in the middle of the site just east of the East Fork drainage way. The pond discharges into the East Fork drainageway. The pond is planned to store a maximum of 2.40 ac-ft during the 100 year event and have a peak outflow of 163.4 cfs which is greater than the pre development peak outflow of 157.99 cfs. The 5 year storage volume is 1.70 ac-ft with a peak outflow of 18.8 cfs.
- Pond F is located near the south east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 12.40 ac-ft during the 100 year event and have a peak outflow of 235.5 cfs which is greater than the pre development peak outflow of 221.11 cfs. The 5 year storage volume is 8.07 ac-ft with a peak outflow of 14.5 cfs.
- Pond G is located near the north east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway at an upstream location within the site. The pond is planned to store a maximum of 2.54 ac-ft during the 100 year event and have a peak outflow of 50.7 cfs which is slightly greater than the pre development peak outflow of 48.48 cfs. The 5 year storage volume is 1.69 ac-ft with a peak outflow of 9.1 cfs.
- Pond H is located near the south east corner of the site just east of the East Fork Tributary drainageway and adjacent to Highway 24. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 6.60 ac-ft during the 100 year event and have a peak outflow of 99.1 cfs which matches the pre development peak outflow. The 5 year storage volume is 4.03 ac-ft with a peak outflow of 1.3 cfs.

summary

table added

Overall runoff from the site will by and large match the predevelopment peak flows. The volume of water will increase however as the drainage channels are designs, continuous simulation models will be done to see the effects of prolonged runoff rates.

Provide a table listing pre-development and proposed detained release rates at each design point discharging offsite.

VII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

VIII. Summary

Grandview Reserve is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development increased runoff will occur. In order to mitigate downstream impacts 8 large full spectrum detention facilities will be built to reduce the runoff rate to near historic levels. These detention facilities will provide water quality enhancements in order to account for the increased urbanization of the upstream catchment areas. Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and be included in future submittals.

Add a "no adverse impact" statement regarding the proposed design to downstream properties.

IX. References

El Paso County – Drainage Criteria Manual, 2014

City of Colorado Springs – Drainage Criteria Manual, May 2014

Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

Unnamed Tributary Black Squirrel Creek, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004

Haegler and Gieck Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004

Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006

Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)

EPC Engineering Criteria Manual (Appendix I updated July, 2019)

Meridian Ranch MDDP, January 2018

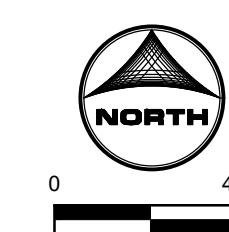
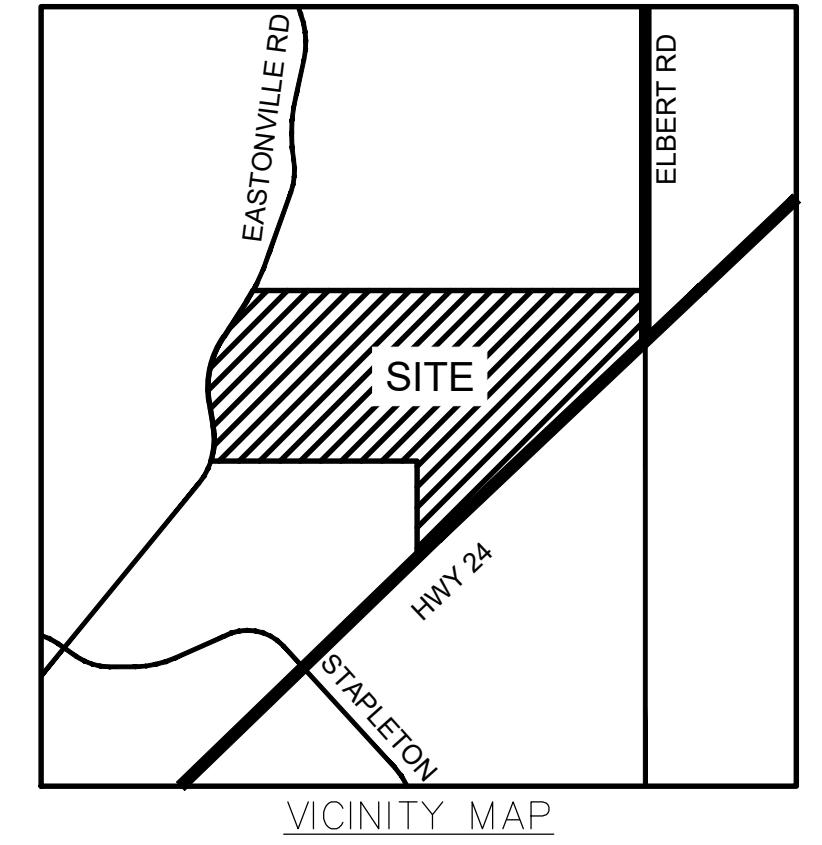
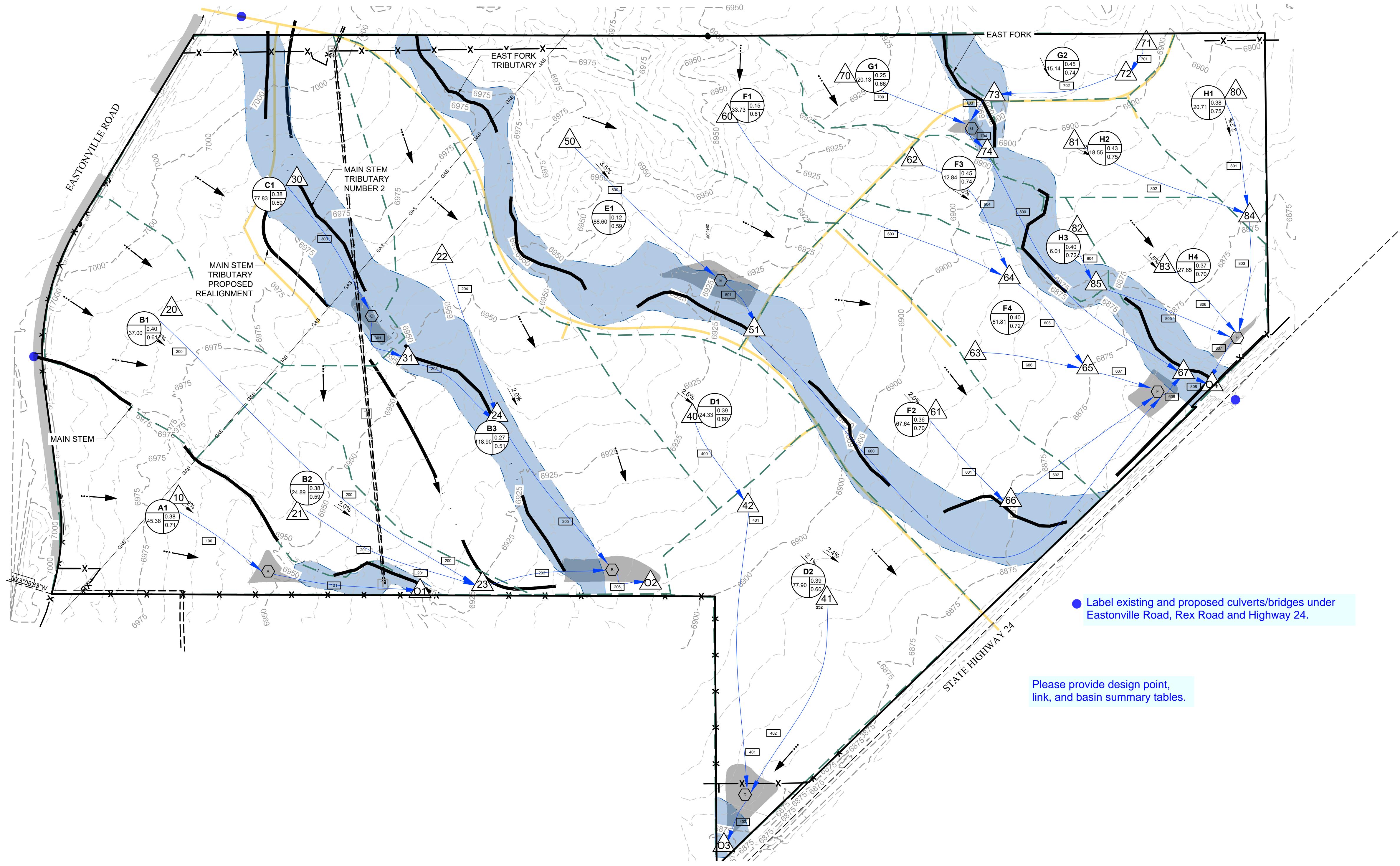
statement added

References added

Appendix A

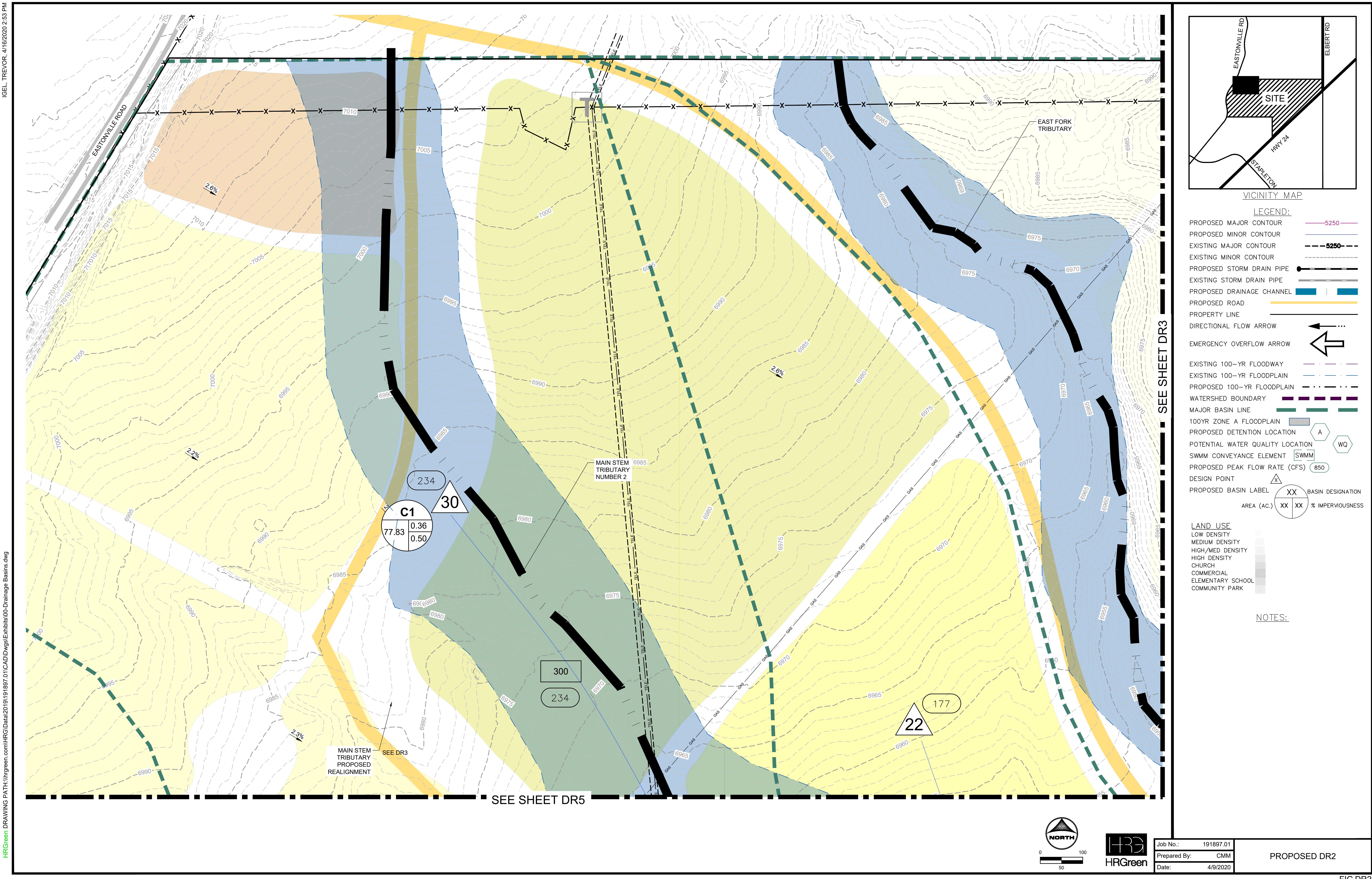
Please move pdf sheets 20-31 (drainage plans) to the end of the pdf.

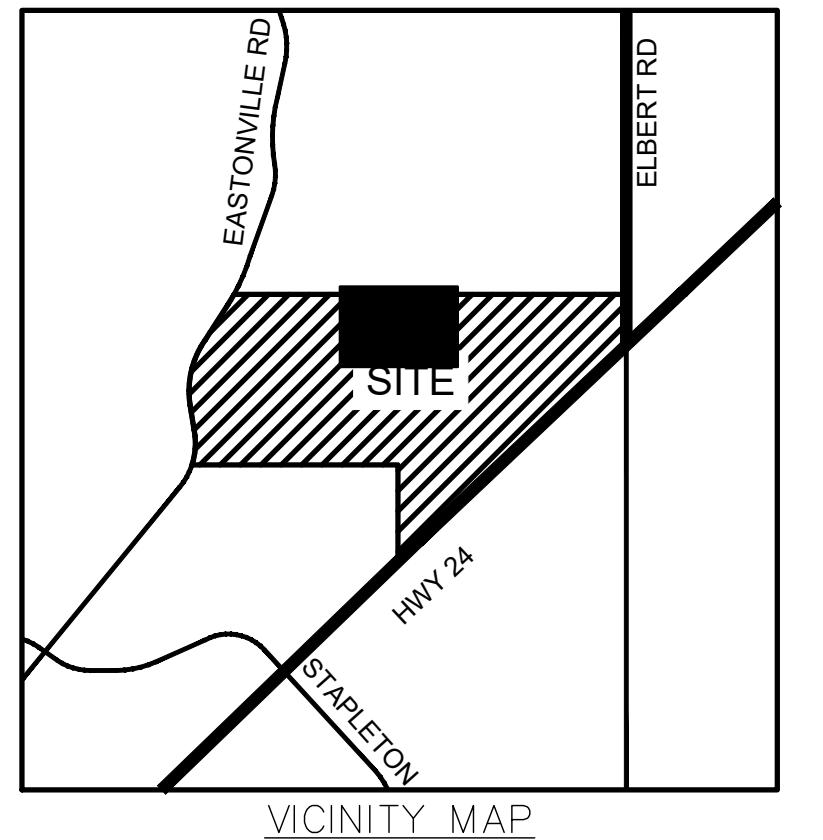
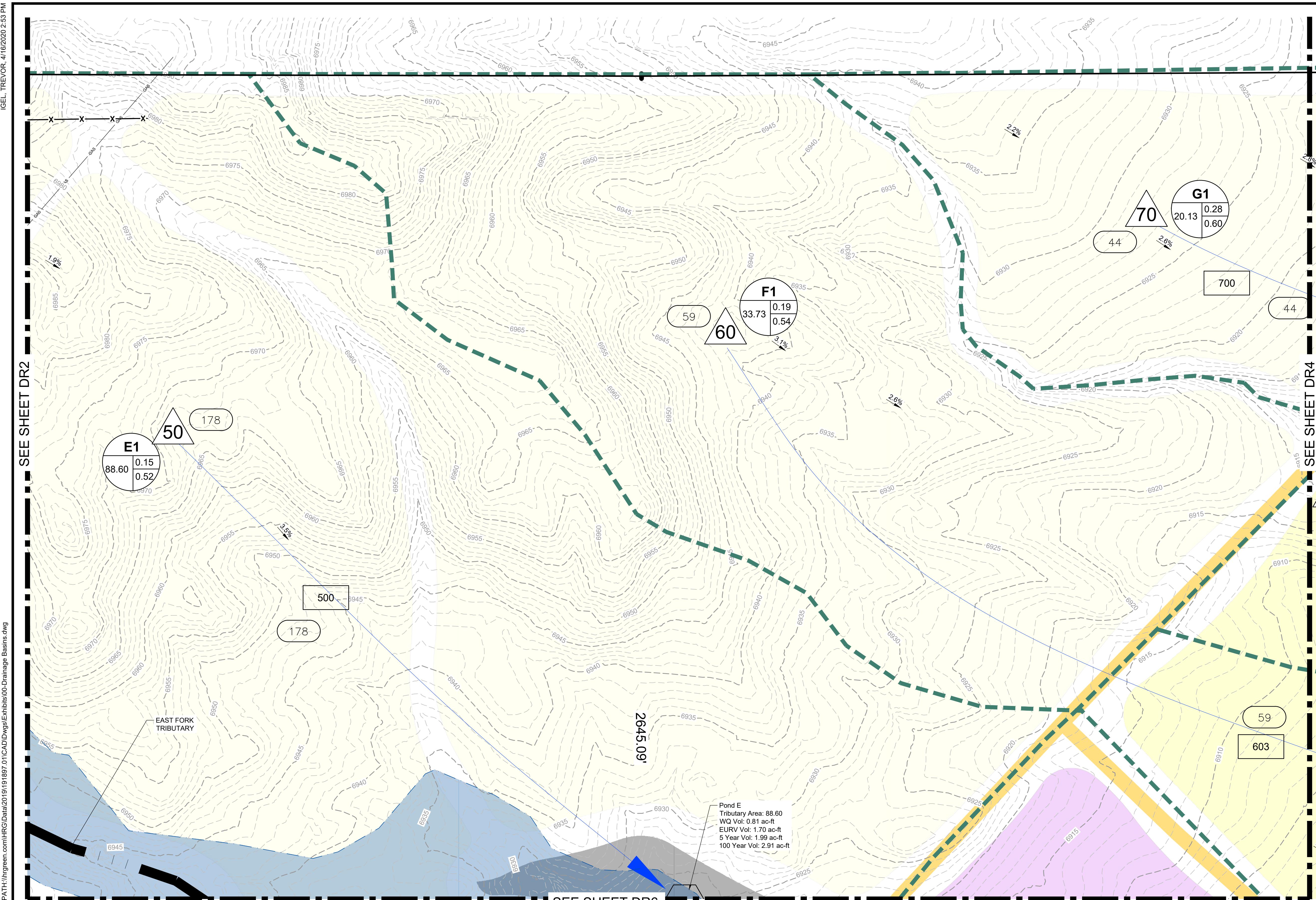
Label the entire contributing basins.



Job No.: 191897.01
Prepared By: TBI
Date: 04/14/2020

PROPOSED DR1



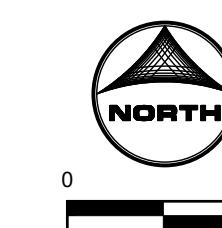


LEGEND:

- PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- PROPOSED STORM DRAIN PIPE
- EXISTING STORM DRAIN PIPE
- PROPOSED DRAINAGE CHANNEL
- PROPOSED ROAD
- PROPERTY LINE
- DIRECTIONAL FLOW ARROW
- EMERGENCY OVERFLOW ARROW
- EXISTING 100-YR FLOODWAY
- EXISTING 100-YR FLOODPLAIN
- PROPOSED 100-YR FLOODPLAIN
- WATERSHED BOUNDARY
- MAJOR BASIN LINE
- 100YR ZONE A FLOODPLAIN
- PROPOSED DETENTION LOCATION
- POTENTIAL WATER QUALITY LOCATION
- SWMM CONVEYANCE ELEMENT
- PROPOSED PEAK FLOW RATE (CFS) 850
- DESIGN POINT
- PROPOSED BASIN LABEL
- AREA (AC.) XX % IMPERVIOUSNESS

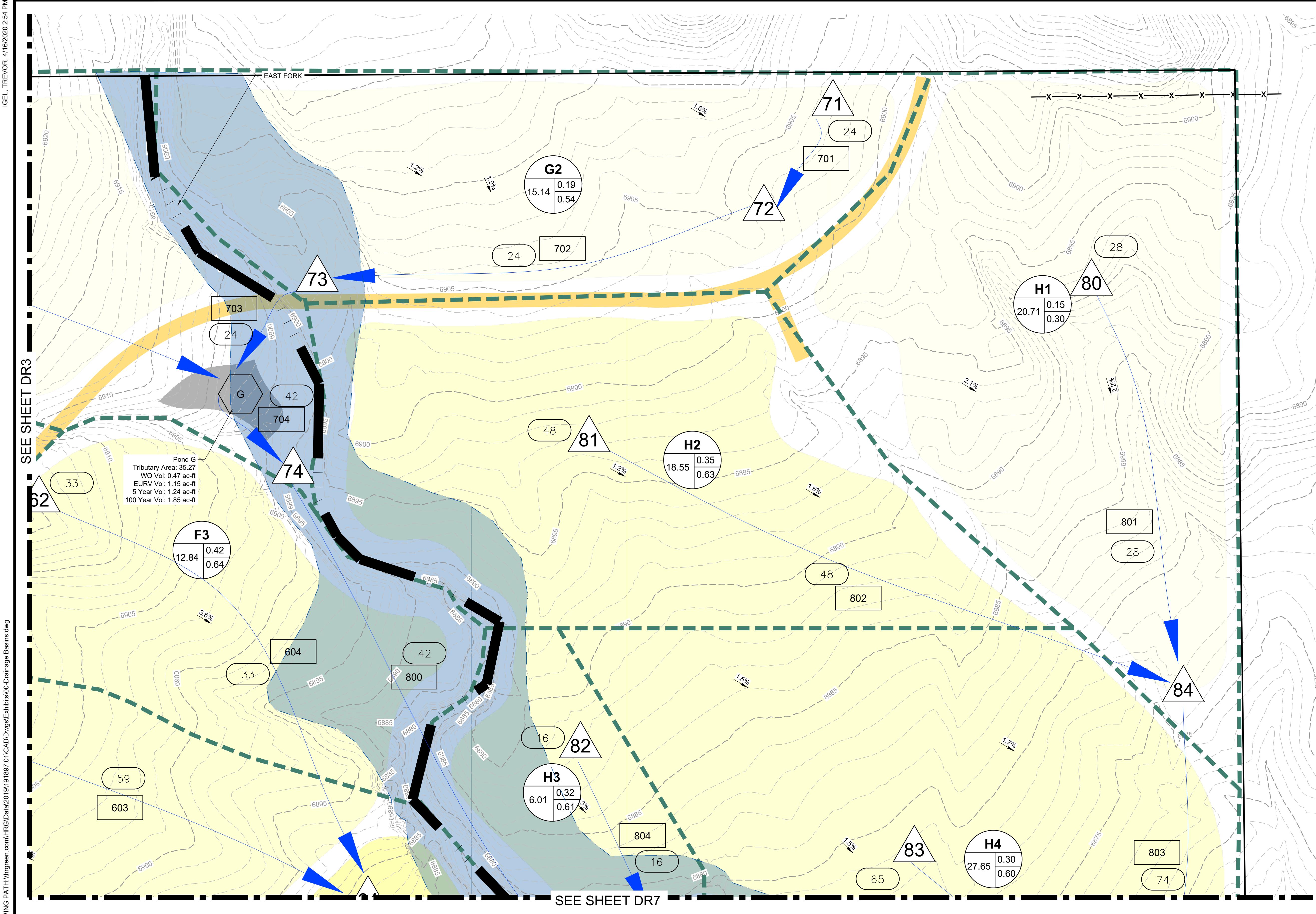
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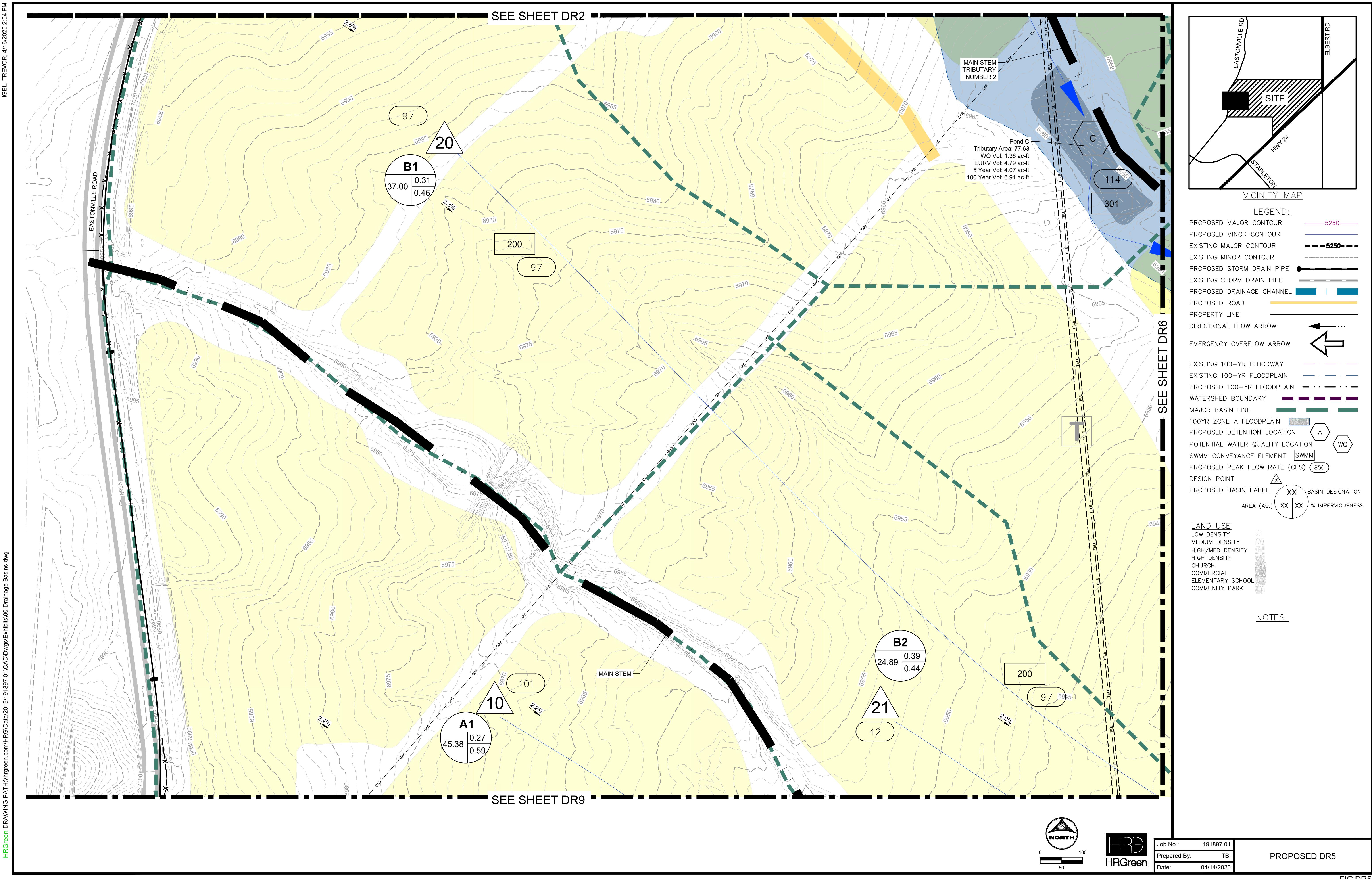
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- MEDIUM DENSITY
- HIGH/MED DENSITY
- HIGH DENSITY
- CHURCH
- COMMERCIAL
- ELEMENTARY SCHOOL
- COMMUNITY PARK

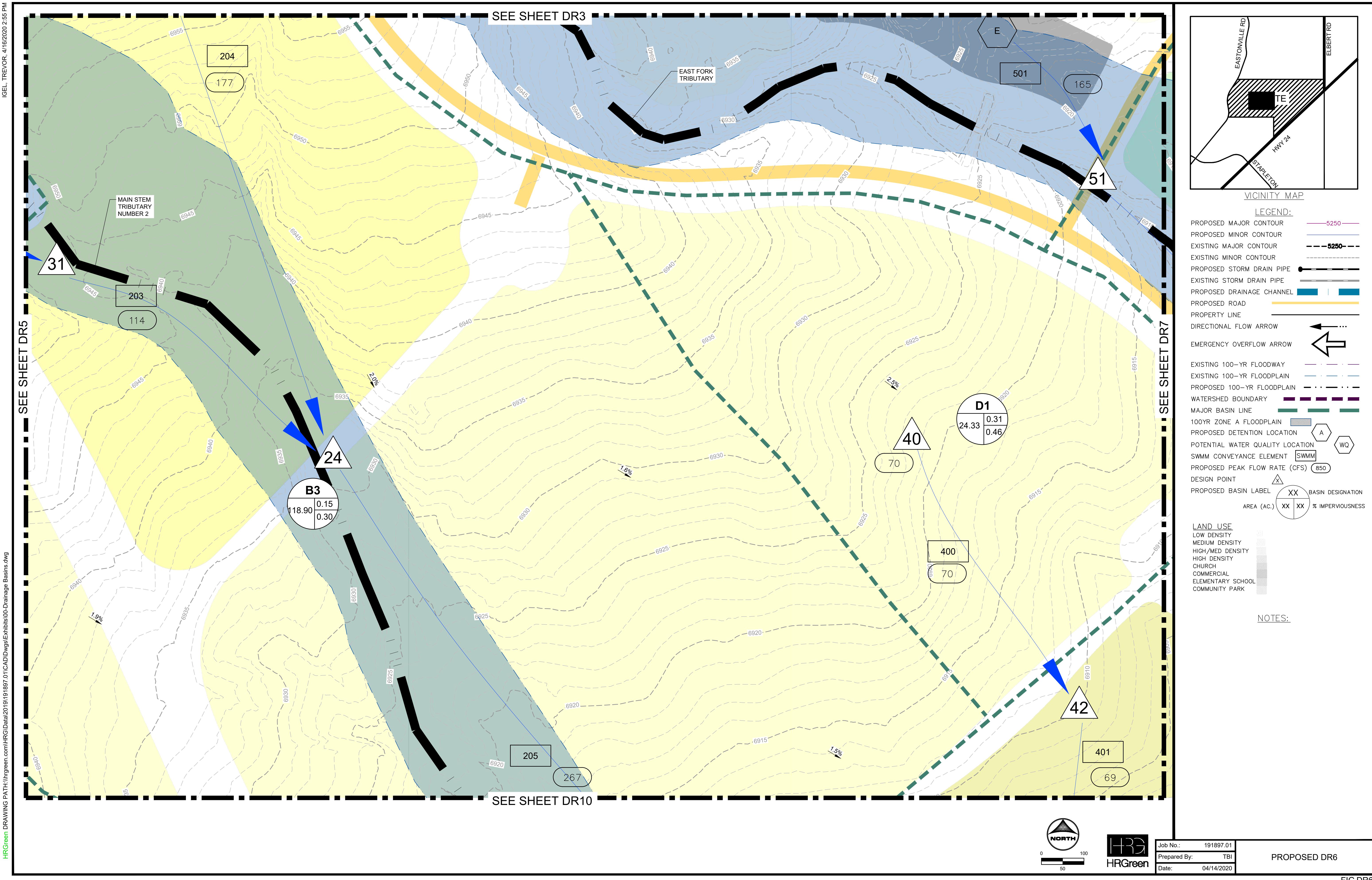
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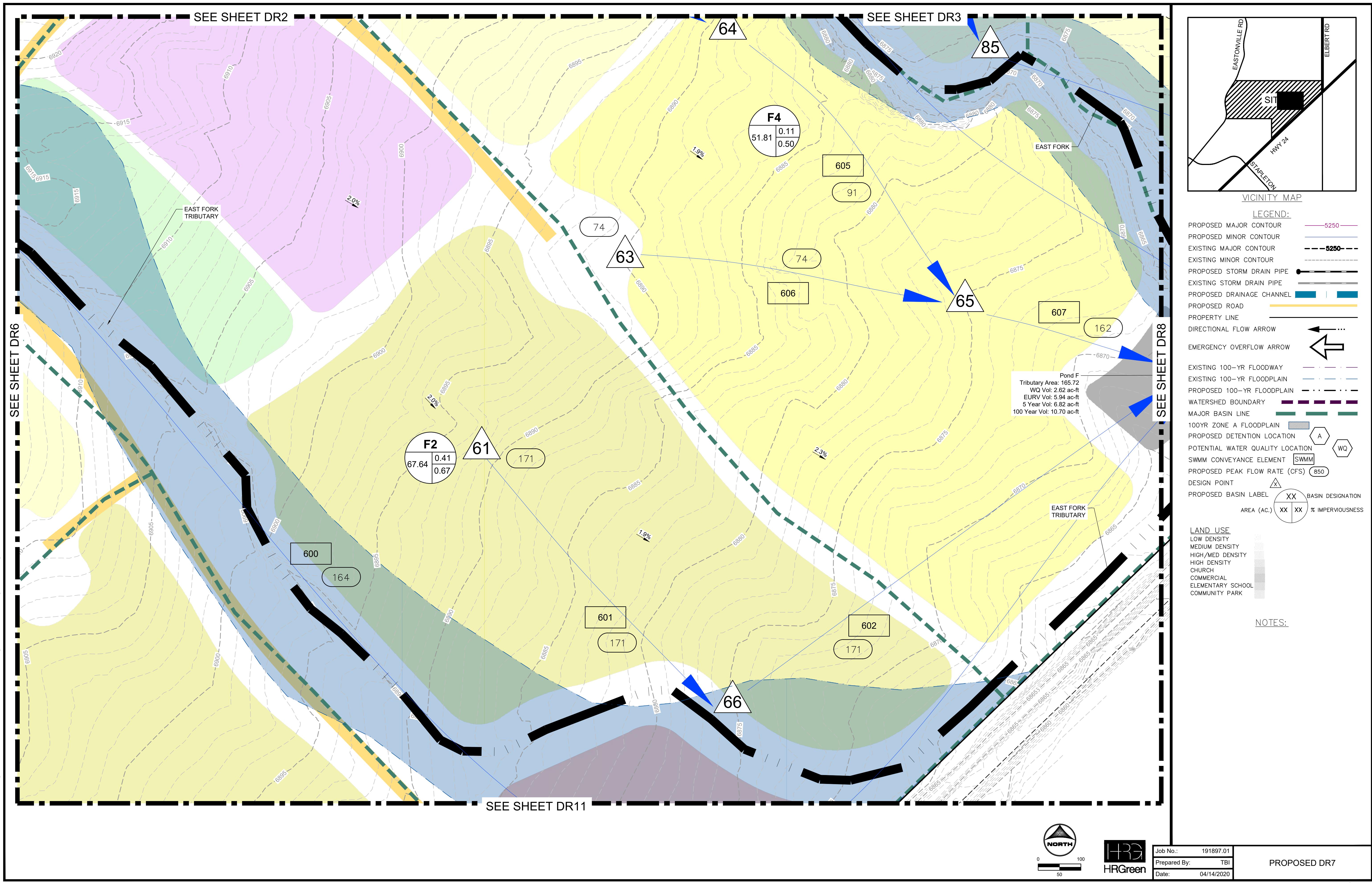
Job No.: 191897.01
Prepared By: TBI
Date: 04/14/2020

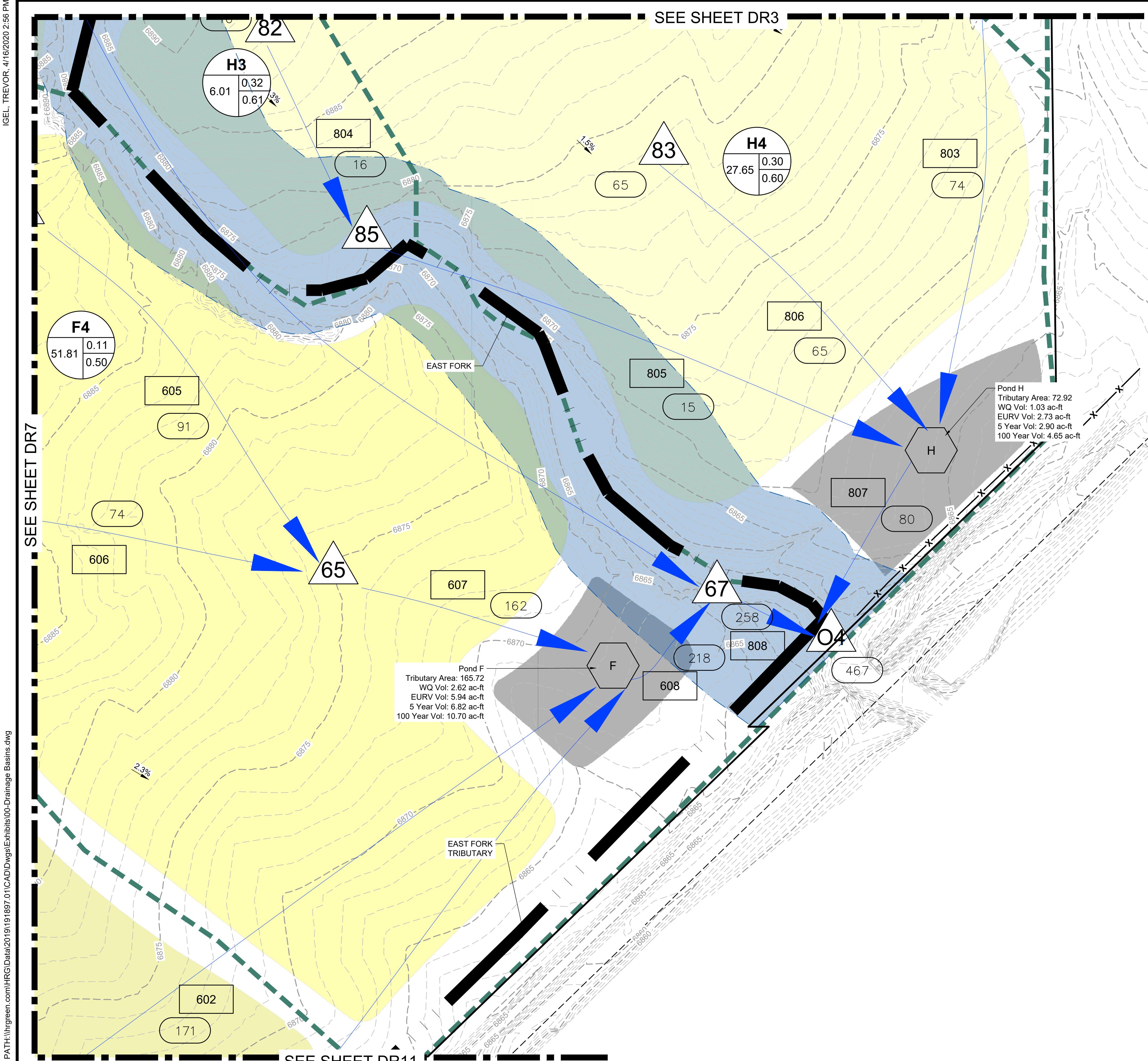
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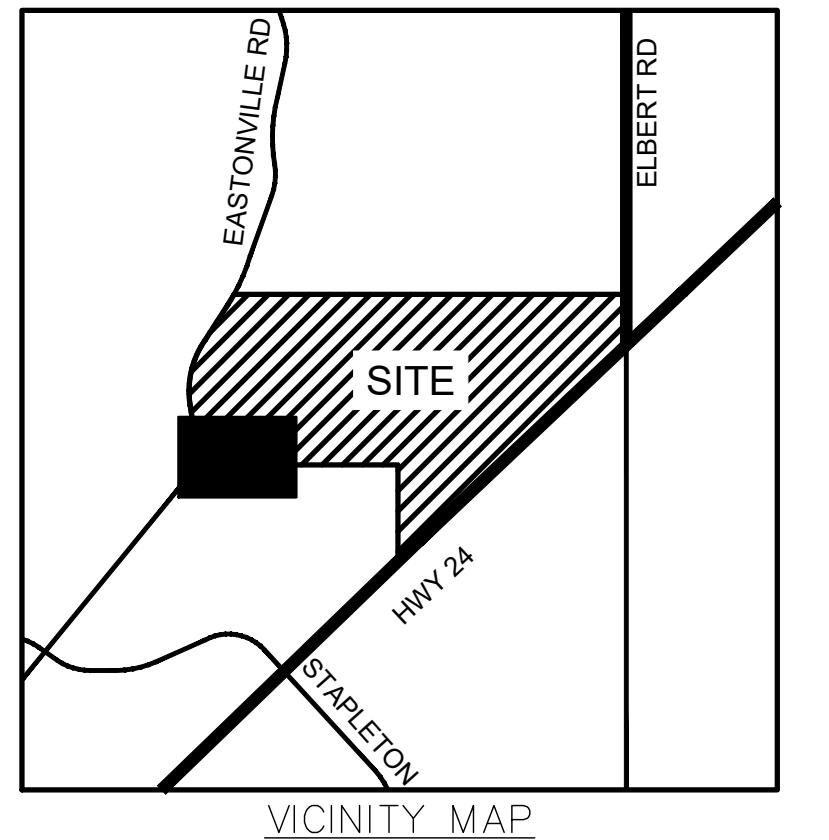
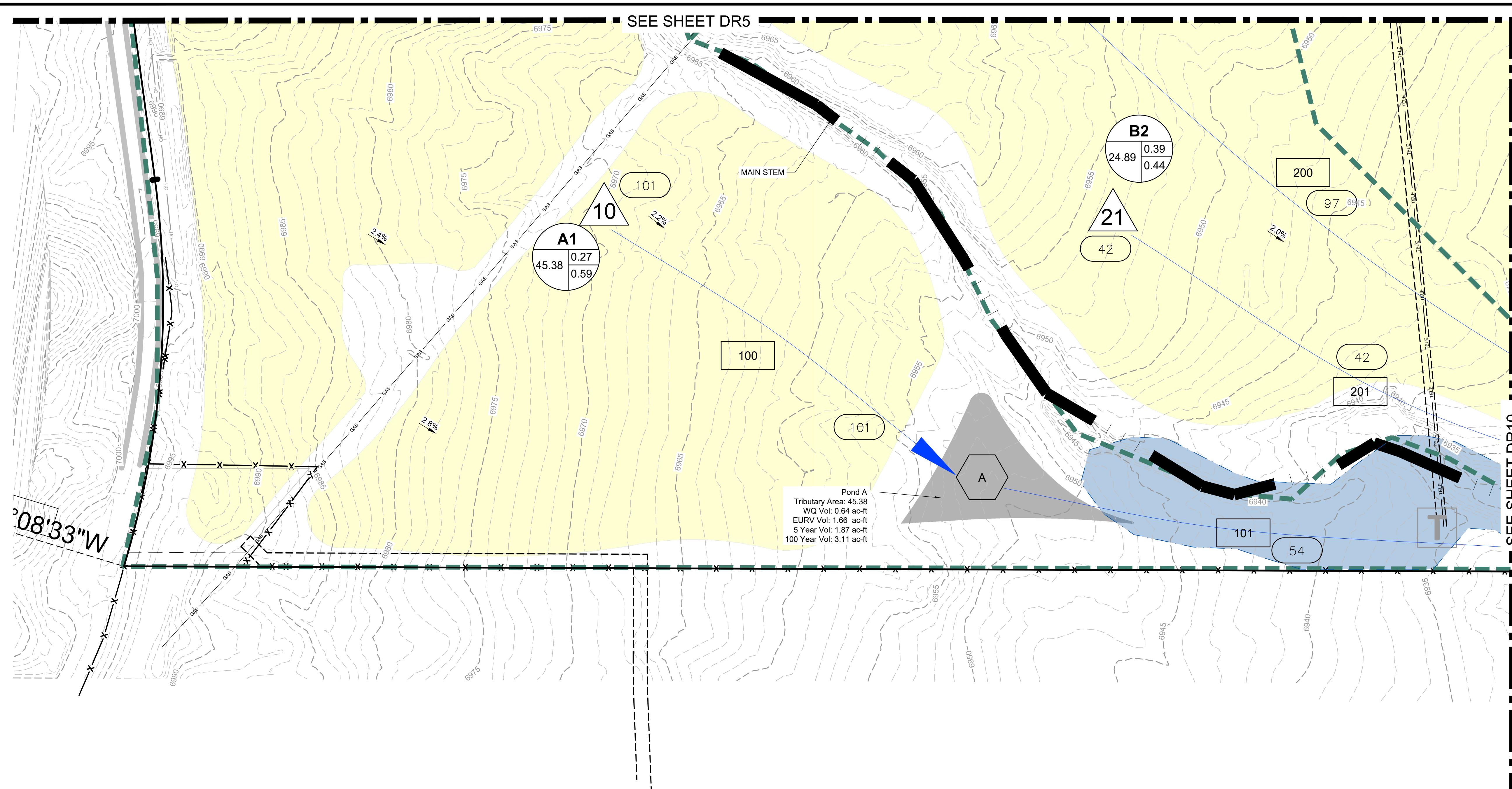










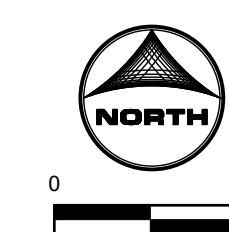


LEGEND:

- PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- PROPOSED STORM DRAIN PIPE
- EXISTING STORM DRAIN PIPE
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- EXISTING 100-YR FLOODWAY
- EXISTING 100-YR FLOODPLAIN
- PROPOSED 100-YR FLOODPLAIN
- WATERSHED BOUNDARY
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- 100YR ZONE A FLOODPLAIN
- PROPOSED DETENTION LOCATION
- POTENTIAL WATER QUALITY LOCATION
- SWMM CONVEYANCE ELEMENT
- PROPOSED PEAK FLOW RATE (CFS) 850
- DESIGN POINT
- PROPOSED BASIN LABEL
- AREA (AC.) XX % IMPERVIOUSNESS

NOTES:

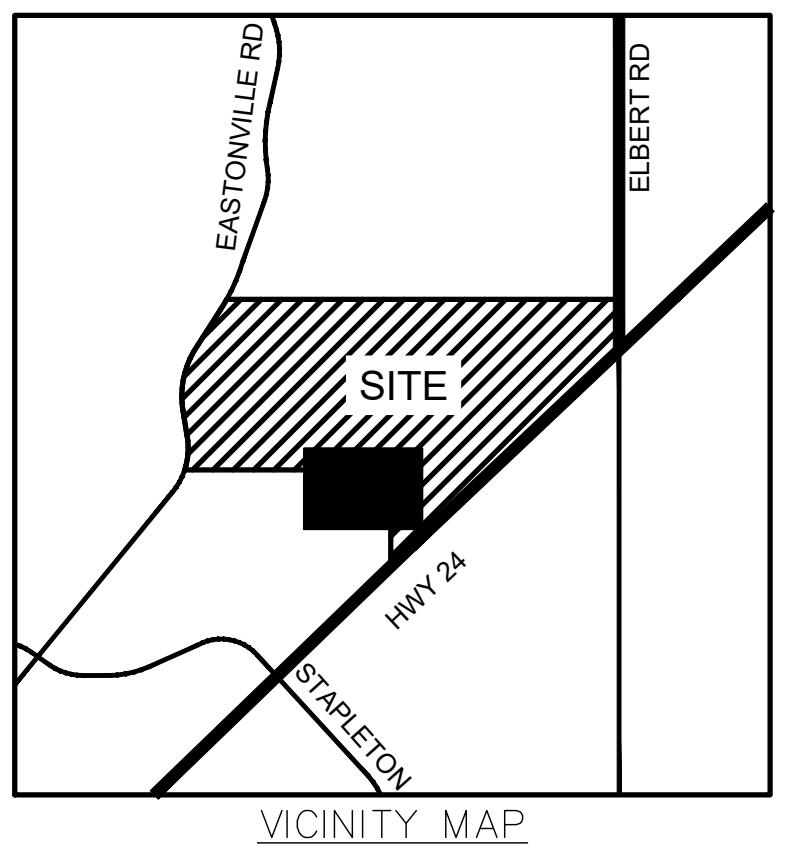
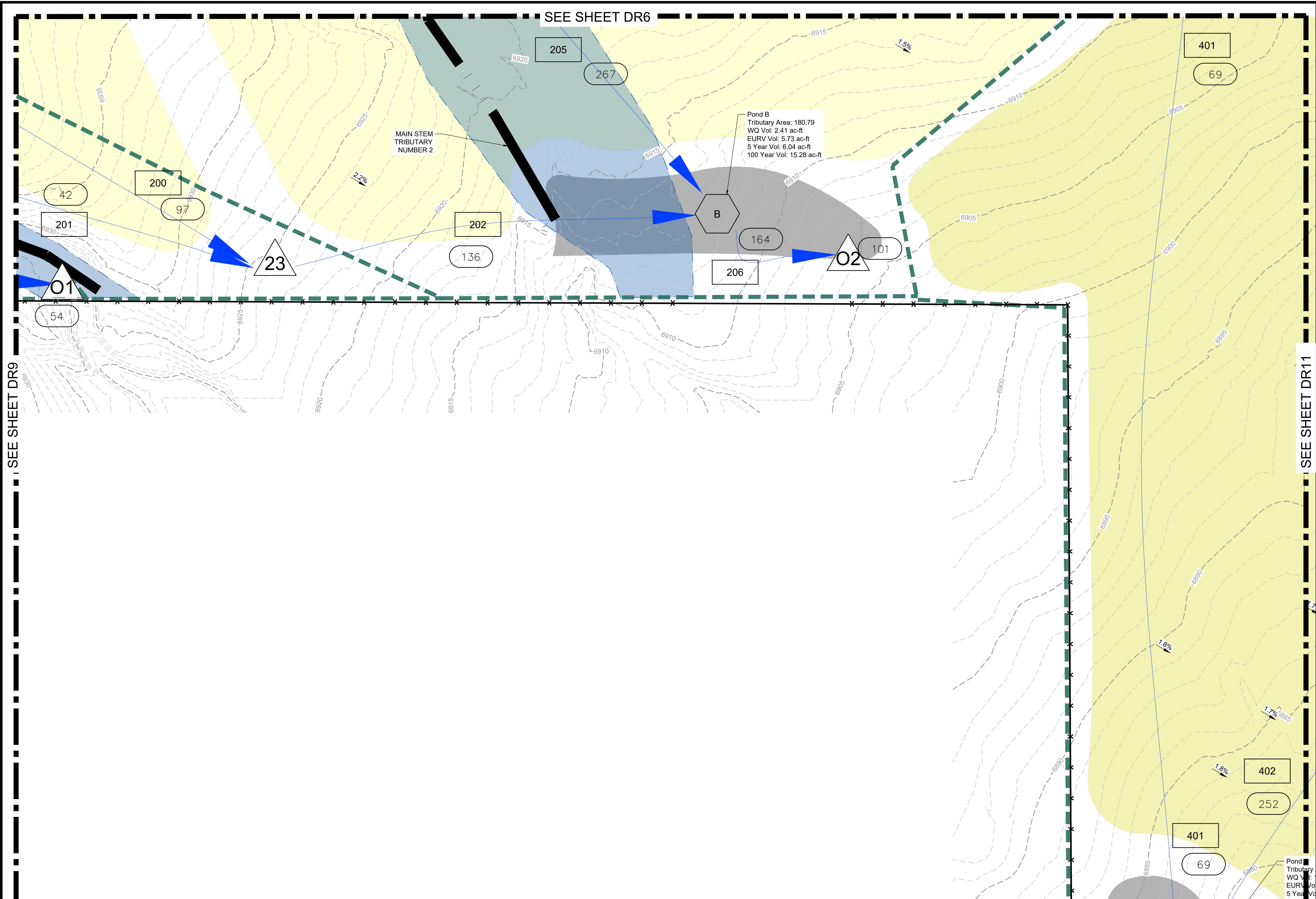
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- MEDIUM DENSITY
- HIGH/MED DENSITY
- HIGH DENSITY
- CHURCH
- COMMERCIAL
- ELEMENTARY SCHOOL
- COMMUNITY PARK



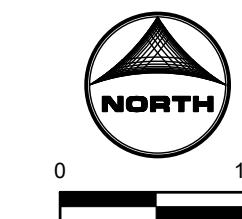
HRG
HRGreen

Job No.: 191897.01
Prepared By: TBI
Date: 04/14/2020

PROPOSED DR9

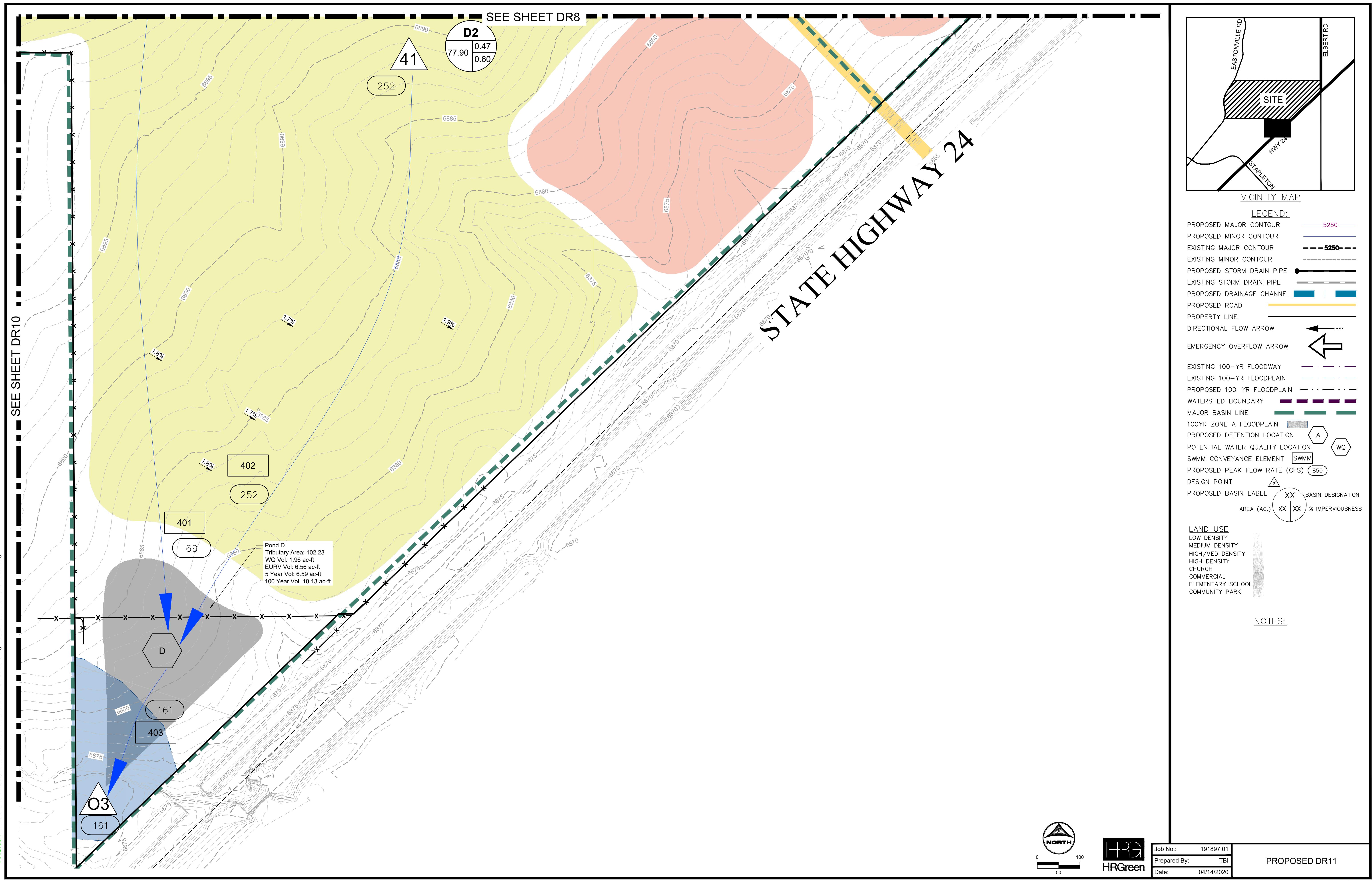


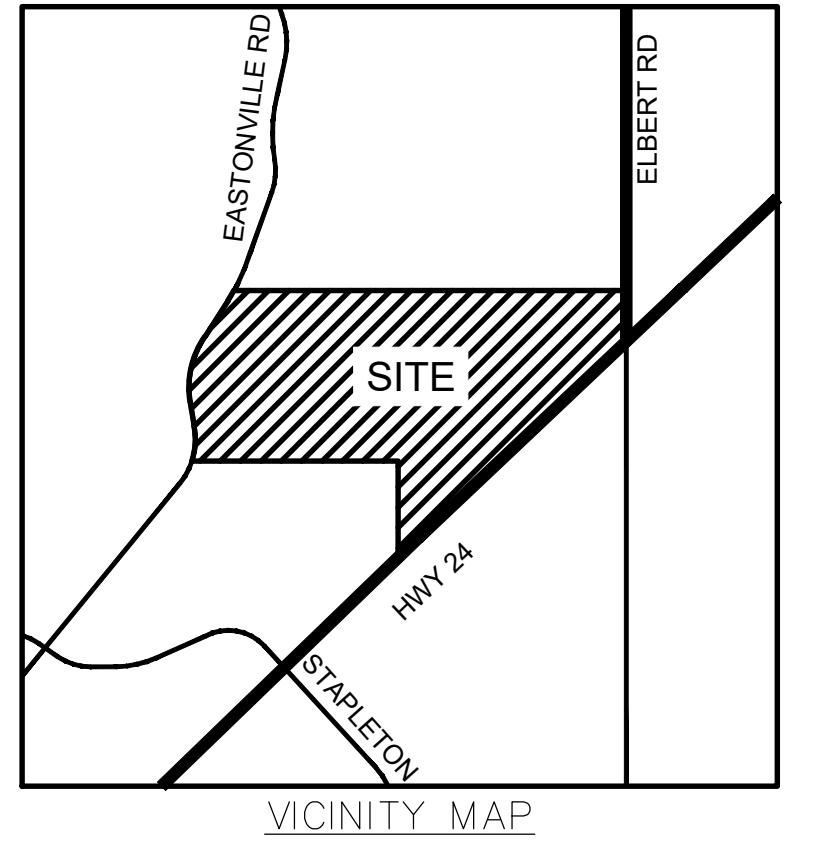
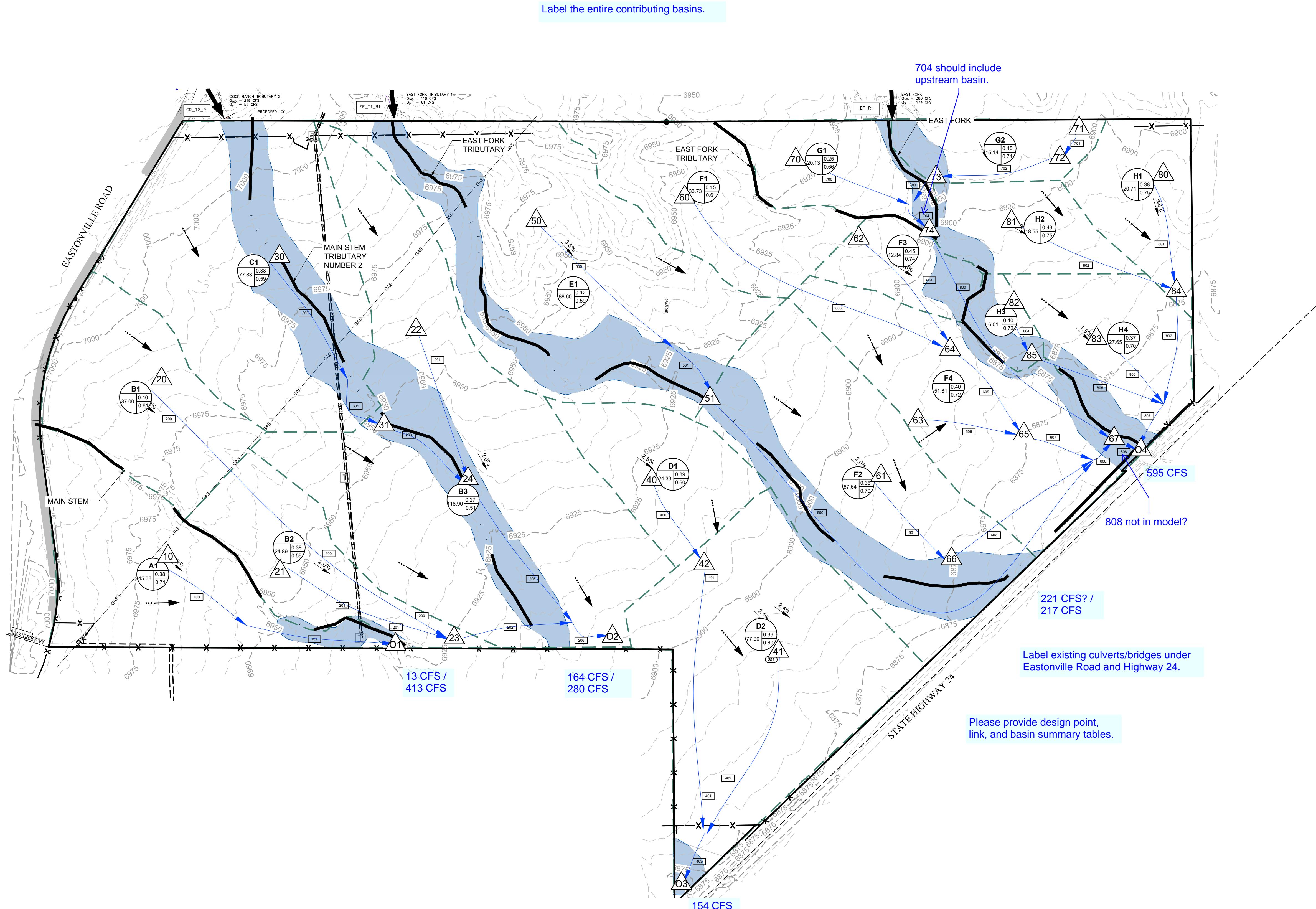
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PROPOSED MINOR CONTOUR
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PROPOSED STORM DRAIN PIPE
EXISTING STORM DRAIN PIPE
PROPOSED DRAINAGE CHANNEL
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PROPOSED BASIN LABEL
AREA (AC.) XX % IMPERVIOUSNESS
LAND USE
LOW DENSITY
MEDIUM DENSITY
HIGH/MED DENSITY
HIGH DENSITY
CHURCH
COMMERCIAL
ELEMENTARY SCHOOL
COMMUNITY PARK

NOTES:

Job No.: 191897.01
Prepared By: TBI
Date: 04/14/2020

PROPOSED DR10





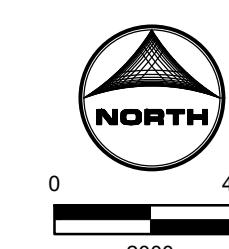
LEGEND:

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- PROPOSED MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- PROPOSED STORM DRAIN PIPE
- EXISTING STORM DRAIN PIPE
- PROPOSED DRAINAGE CHANNEL
- PROPOSED ROAD
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- DIRECTIONAL FLOW ARROW
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- EXISTING 100-YR FLOODPLAIN
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- POTENTIAL WATER QUALITY LOCATION
- SWMM CONVEYANCE ELEMENT
- PROPOSED PEAK FLOW RATE (CFS)
- DESIGN POINT
- PROPOSED BASIN LABEL
- AREA (AC.)
- BASIN DESIGNATION
- % IMPERVIOUSNESS

LAND USE

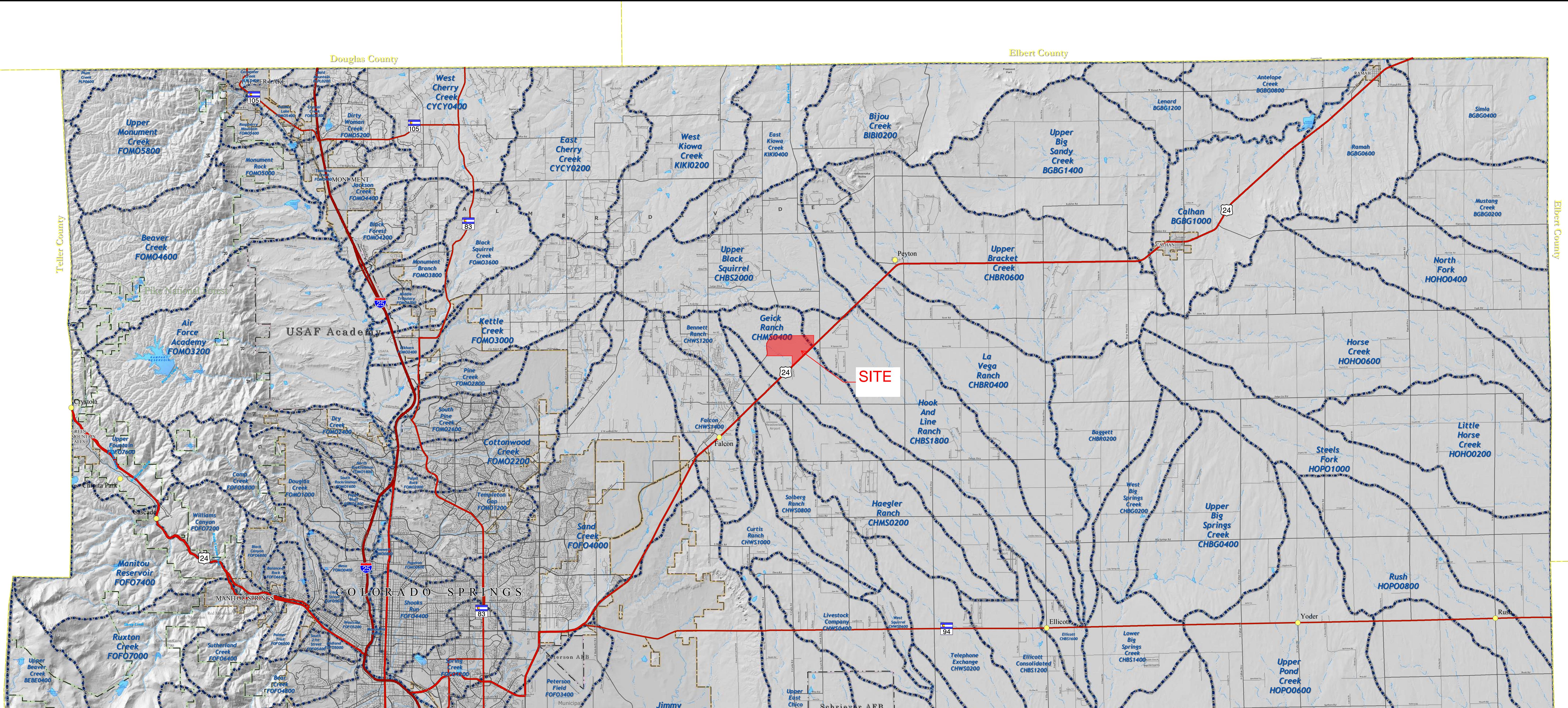
- LOW DENSITY
- MEDIUM DENSITY
- HIGH/MED DENSITY
- HIGH DENSITY
- CHURCH
- COMMERCIAL
- ELEMENTARY SCHOOL
- COMMUNITY PARK

NOTES:



Job No.: 191897.01
Prepared By: TBI
Date: 04/14/2020

EXISTING EX1



Drainage Basins

El Paso County Colorado

Legend

Drainage Basins Source: Muller Engineering Company (1988)

US Interstate Highways

US Highways

Colorado State Highways

Major Roadways

Local Streets & Roads

Creeks

Perennial

Intermittent

Lakes & Reservoirs

Summits

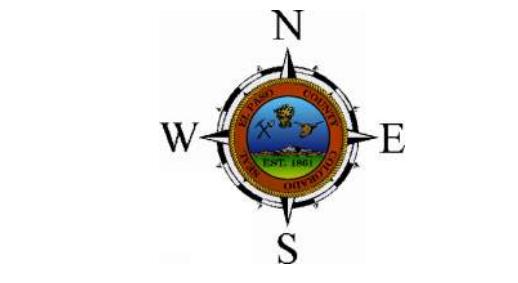
Unincorporated Urban Areas

Incorporated Cities

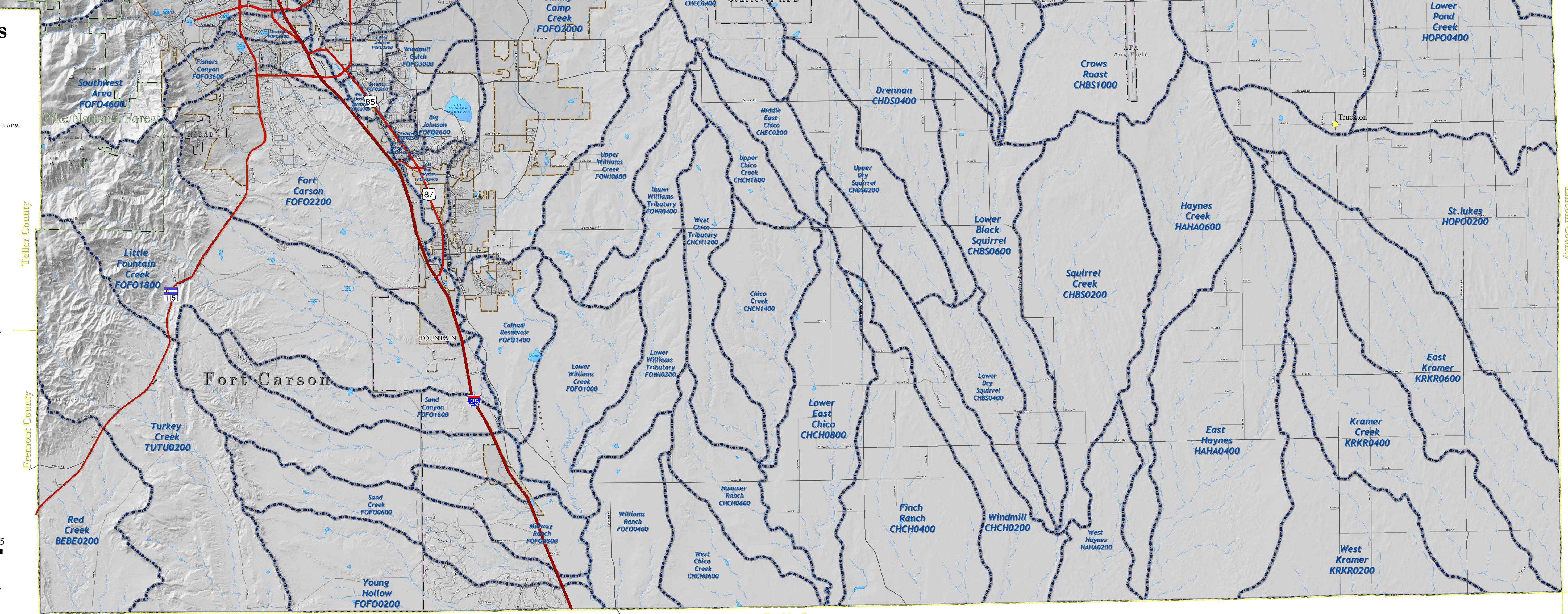
Military

Forest

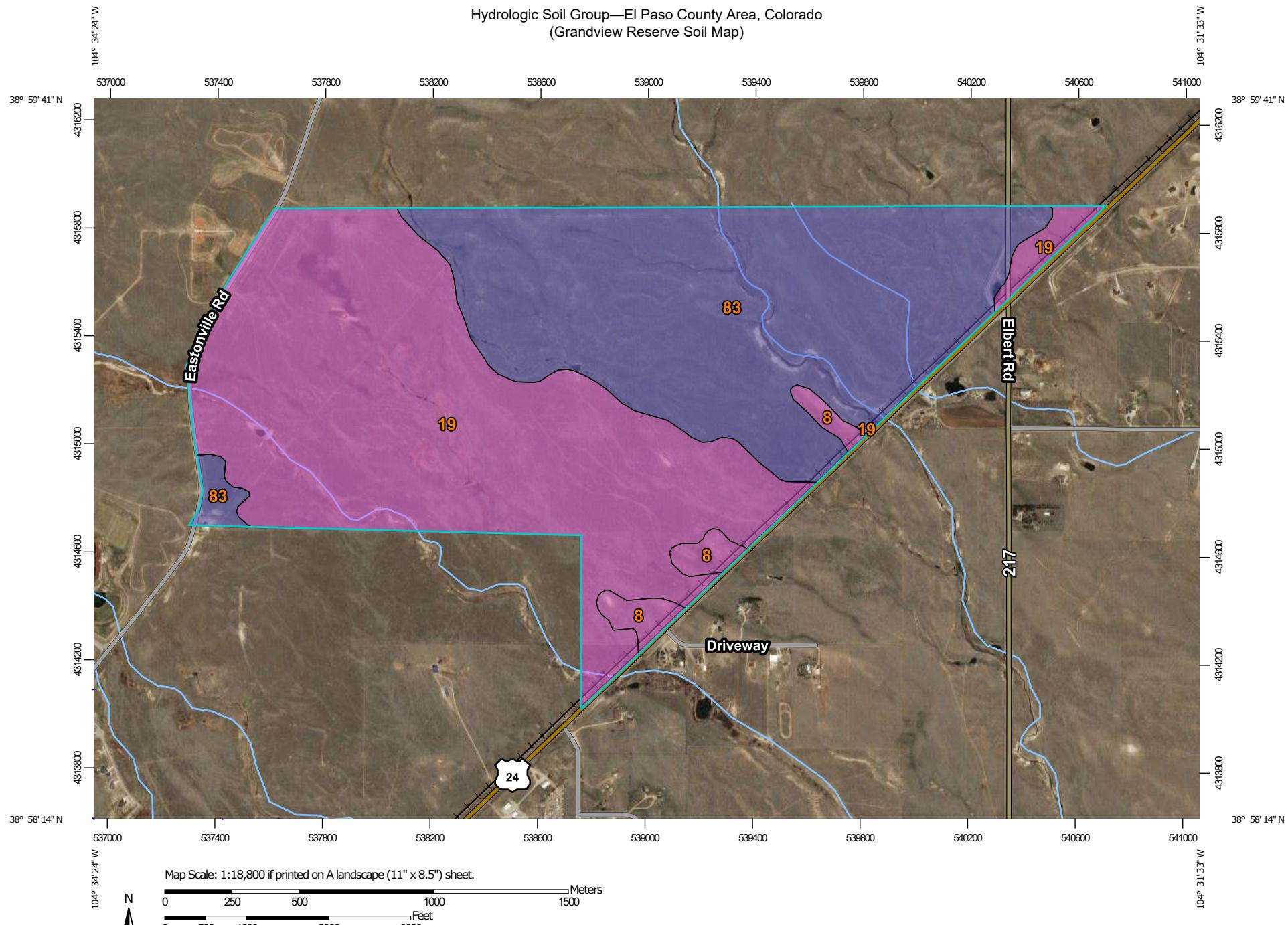
County Lines



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Hydrologic Soil Group—El Paso County Area, Colorado
(Grandview Reserve Soil Map)



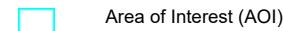
Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

4/6/2020
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)



Soils

Soil Rating Polygons

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Lines

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Points

	A
	A/D
	B
	B/D

	C
	C/D
	D
	Not rated or not available

Water Features



Streams and Canals

Transportation

	Rails
	Interstate Highways
	US Routes
	Major Roads
	Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 8, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.4	2.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	450.7	52.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	B	385.4	44.9%
Totals for Area of Interest			858.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Appendix B

Basin Description	Park/Open Space	High Density/Schools	Med/High Density	Med Density	Low Density	Commercial	Total Impervious	Total Acreage	Composite Percent Impervious	Predominant Soil Group	5 Year C Factor	100 Year C Factor
Impervious Percentage	10%	65%	55%	45%	25%	75%						
A1	12.68	0.00	0.00	32.70	0.00	0.00	15.98	45.38	35.22%	B	0.38	0.71
						Pond A			45.38	35.22%		
B1	0.00	0.00	0.00	37.00	0.00	0.00	16.65	37.00	45.00%	A	0.4	0.61
B2	1.24	0.00	0.00	23.65	0.00	0.00	10.77	24.89	43.26%	A	0.38	0.59
B3	7.42	12.64	53.20	45.64	0.00	0.00	58.76	118.90	49.42%	A	0.36	0.5
						Pond B			180.79	47.66%		
C1	4.19	30.61	1.70	41.33	0.00	0.00	39.85	77.83	51.20%	A	0.38	0.59
						Pond C			77.83	51.20%		
D1	0.60	0.00	0.00	23.73	0.00	0.00	10.74	24.33	44.14%	A	0.39	0.6
D2	5.60	64.10	0.00	0.00	0.00	8.20	48.38	77.90	62.10%	A	0.39	0.6
						Pond D			102.23	57.82%		
E1	32.26	0.00	0.00	0.00	56.34	0.00	17.31	88.60	19.54%	B	0.12	0.59
						Pond E			88.60	19.54%		
F1	0.00	0.00	0.00	0.00	33.73	0.00	8.43	33.73	25.00%	B	0.15	0.61
F2	18.34	40.50	0.00	0.00	0.00	8.80	34.76	67.64	51.39%	B	0.36	0.7
F3	0.00	0.00	0.00	12.84	0.00	0.00	5.78	12.84	45.00%	B	0.45	0.74
F4	6.24	0.00	29.80	15.77	0.00	0.00	24.11	51.81	46.54%	B	0.37	0.64
						Pond F			166.02	44.02%		
G1	4.88	0.00	0.00	15.25	0.00	0.00	7.35	20.13	36.52%	B	0.25	0.66
G2	0.00	0.00	0.00	0.00	15.14	0.00	3.79	15.14	25.00%	B	0.45	0.74
						Pond G			35.27	31.57%		
H1	0.70	0.00	0.00	0.00	20.01	0.00	5.07	20.71	24.49%	A	0.38	0.75
H2	0.70	0.00	0.00	17.85	0.00	0.00	8.10	18.55	43.68%	B	0.43	0.75
H3	0.76	0.00	0.00	5.25	0.00	0.00	2.44	6.01	40.57%	B	0.4	0.72
H4	5.34	0.00	0.00	22.31	0.00	0.00	10.57	27.65	38.24%	B	0.37	0.7
						Pond H			72.92	35.91%		

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results								Excess Precip.		Storm Hydrograph				
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.157	0.143	37.3	5.59	19.4	3.95	9.3	57	164,729	0.25	40,666	35.0	13	40,592	0.29
B1		0.158	0.131	33.0	4.82	17.2	3.41	8.0	53	134,310	0.08	11,390	35.0	4	11,363	0.12
B2		0.158	0.109	58.5	6.42	30.4	4.54	10.7	20	90,351	0.08	7,662	40.0	2	7,665	0.07
B3		0.158	0.221	39.1	8.15	20.3	5.76	13.6	142	431,607	0.08	36,602	40.0	12	36,572	0.10
C1		0.158	0.183	30.3	5.75	15.7	4.06	9.6	120	281,797	0.08	23,898	35.0	10	23,870	0.13
D1		0.157	0.108	31.5	4.11	16.4	2.91	6.9	36	88,318	0.25	21,803	35.0	8	21,721	0.33
D2		0.157	0.182	37.7	6.77	19.6	4.78	11.3	97	282,777	0.25	69,809	40.0	22	69,820	0.29
E1		0.157	0.193	28.9	5.77	15.0	4.08	9.6	144	321,618	0.25	79,397	35.0	32	79,287	0.37
F1		0.157	0.125	37.2	5.07	19.4	3.58	8.5	42	122,440	0.25	30,227	35.0	10	30,151	0.29
F2		0.157	0.171	45.1	7.42	23.5	5.24	12.4	70	245,533	0.25	60,614	40.0	16	60,563	0.24
F3		0.157	0.081	37.8	3.84	19.6	2.72	6.4	16	46,609	0.25	11,506	35.0	4	11,472	0.28
F4		0.157	0.151	43.2	6.52	22.5	4.61	10.9	56	186,981	0.25	46,160	40.0	13	46,174	0.25
G1		0.157	0.099	38.8	4.45	20.2	3.14	7.4	24	73,072	0.25	18,039	35.0	6	17,996	0.28
G2		0.157	0.087	42.3	4.33	22.0	3.06	7.2	17	54,958	0.25	13,567	35.0	4	13,536	0.26
H1		0.158	0.101	43.7	4.89	22.7	3.45	8.1	22	75,177	0.08	6,375	35.0	2	6,365	0.09
H2		0.157	0.095	37.0	4.21	19.2	2.97	7.0	24	67,337	0.25	16,623	35.0	5	16,581	0.29
H3		0.157	0.057	32.6	2.94	16.9	2.08	4.9	9	21,816	0.25	5,384	35.0	2	5,324	0.32
H4		0.157	0.114	36.7	4.72	19.1	3.33	7.9	35	100,370	0.25	24,778	35.0	8	24,718	0.29

Printouts for Storm Hydrographs

flow in

Printouts for Unit Hydrographs

flow in cfs

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results								Excess Precip.		Storm Hydrograph				
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.156	0.142	37.3	5.57	19.4	3.93	9.3	57	164,729	1.56	257,605	45.0	67	257,125	1.47
B1		0.157	0.130	33.0	4.80	17.2	3.39	8.0	53	134,310	1.17	157,714	40.0	49	157,336	1.32
B2		0.157	0.109	58.5	6.39	30.4	4.52	10.6	20	90,351	1.17	106,094	50.0	21	106,130	0.83
B3		0.157	0.220	39.1	8.11	20.3	5.73	13.5	142	431,607	1.17	506,815	45.0	140	506,418	1.18
C1		0.157	0.182	30.3	5.72	15.7	4.04	9.5	120	281,797	1.17	330,900	40.0	111	330,490	1.43
D1		0.156	0.107	31.5	4.10	16.4	2.90	6.8	36	88,318	1.56	138,112	40.0	40	137,590	1.64
D2		0.156	0.181	37.7	6.75	19.6	4.77	11.2	97	282,777	1.56	442,208	45.0	115	442,279	1.47
E1		0.156	0.192	28.8	5.76	15.0	4.07	9.6	144	321,618	1.56	502,948	40.0	158	502,220	1.78
F1		0.156	0.124	37.2	5.06	19.4	3.57	8.4	42	122,440	1.56	191,472	45.0	49	190,993	1.47
F2		0.156	0.170	45.1	7.40	23.5	5.23	12.3	70	245,533	1.56	383,966	50.0	87	383,641	1.28
F3		0.156	0.081	37.7	3.83	19.6	2.71	6.4	16	46,609	1.56	72,888	45.0	18	72,670	1.43
F4		0.156	0.150	43.2	6.50	22.5	4.59	10.8	56	186,981	1.56	292,403	45.0	68	292,494	1.32
G1		0.156	0.099	38.8	4.44	20.2	3.14	7.4	24	73,072	1.56	114,270	45.0	28	113,996	1.41
G2		0.156	0.087	42.3	4.31	22.0	3.05	7.2	17	54,958	1.56	85,944	45.0	20	85,743	1.32
H1		0.157	0.100	43.7	4.86	22.7	3.44	8.1	22	75,177	1.17	88,277	45.0	22	88,139	1.06
H2		0.156	0.095	37.0	4.20	19.2	2.97	7.0	24	67,337	1.56	105,301	45.0	27	105,031	1.46
H3		0.156	0.057	32.6	2.93	16.9	2.07	4.9	9	21,816	1.56	34,116	40.0	10	33,729	1.58
H4		0.156	0.114	36.7	4.70	19.1	3.32	7.8	35	100,370	1.56	156,958	45.0	41	156,578	1.48

Printouts for Storm Hydrographs

flow in cfs

time in minutes	A1	B1	B2	B3	C1	D1	D2	E1	F1	F2	F3	F4	G1	G2	H1	H2	H3	H4
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
20	0.19	0.10	0.03	0.16	0.20	0.16	0.27	0.47	0.16	0.17	0.07	0.16	0.10	0.07	0.04	0.10	0.04	0.14
25	8.12	3.13	0.92	4.86	6.18	6.49	11.23	19.84	6.56	7.27	2.97	6.77	4.15	2.92	1.31	4.16	1.72	5.78
30	34.59	26.76	8.08	44.30	53.77	25.80	50.87	85.32	27.24	33.89	11.70	30.29	16.76	11.74	11.22	16.64	6.64	23.63
35	55.93	43.27	15.49	97.67	95.72	36.82	90.40	139.23	42.28	63.07	16.51	52.88	24.75	17.20	18.33	24.08	8.94	35.59
40	64.93	48.76	18.92	129.21	110.70	40.00	109.38	157.99	48.34	79.01	18.22	63.75	27.87	19.43	21.16	26.79	9.51	40.19
45	66.80	48.19	20.36	140.35	108.85	39.34	114.87	155.63	49.45	85.76	18.42	67.82	28.46	20.06	21.89	27.12	9.32	40.86
50	64.59	44.98	20.74	138.21	100.81	37.49	112.26	146.93	47.76	86.73	17.78	67.62	27.55	19.63	21.22	26.14	8.91	39.39
55	61.26	40.75	20.19	127.94	90.29	34.77	106.51	135.02	45.25	83.59	16.83	64.71	26.19	18.75	19.74	24.71	8.30	37.23
60	57.64	36.45	19.11	117.17	79.70	32.18	100.16	123.69	42.57	79.90	15.87	61.71	24.78	17.90	18.34	23.24	7.72	34.96
65	54.17	32.98	18.06	106.73	71.53	30.21	94.06	114.66	40.04	76.47	14.98	58.85	23.43	17.05	17.02	21.88	7.28	32.86
70	49.50	29.39	16.95	95.83	63.09	26.87	86.32	101.69	36.49	71.24	13.57	54.41	21.31	15.53	15.43	19.83	6.47	29.87
75	44.49	25.88	15.77	86.25	54.40	23.41	77.73	86.59	32.81	64.76	12.22	49.38	19.24	14.13	13.98	17.82	5.68	26.80
80	39.66	22.48	14.61	77.59	45.94	20.04	69.44	72.09	29.24	59.04	10.92	44.90	17.27	12.84	12.74	15.86	4.91	23.82
85	35.05	19.22	13.48	69.37	38.02	16.98	61.48	60.25	25.85	53.80	9.69	40.70	15.40	11.62	11.61	14.01	4.19	20.99
90	30.75	16.13	12.47	61.54	32.28	14.46	54.04	51.51	22.66	48.89	8.53	36.78	13.66	10.48	10.54	12.25	3.57	18.32
95	26.60	13.89	11.62	54.03	28.03	12.58	46.90	44.50	19.60	44.35	7.40	33.11	11.95	9.39	9.51	10.59	3.11	15.80
100	22.94	12.24	10.86	46.67	24.54	11.06	40.40	38.42	16.94	39.99	6.40	29.55	10.37	8.32	8.50	9.19	2.75	13.72
105	20.31	10.86	10.14	40.05	21.41	9.70	35.55	32.88	15.01	35.72	5.68	26.07	9.12	7.30	7.50	8.16	2.43	12.18
110	18.18	9.62	9.45	35.53	18.50	8.47	31.77	27.72	13.44	31.55	5.10	22.87	8.17	6.44	6.54	7.31	2.14	10.90
115	16.30	8.47	8.77	32.01	15.60	7.31	28.48	22.84	12.06	27.80	4.58	20.38	7.35	5.79	5.80	6.55	1.87	9.75
120	14.59	7.37	8.10	28.94	12.97	6.22	25.53	18.25	10.79	24.99	4.12	18.44	6.63	5.26	5.26	5.86	1.61	8.71
125	13.00	6.29	7.44	26.14	10.33	5.18	22.79	13.83	9.62	22.73	3.68	16.78	5.96	4.78	4.81	5.22	1.37	7.73
130	11.49	5.24	6.78	23.51	7.70	4.19	20.20	9.50	8.50	20.76	3.27	15.27	5.33	4.35	4.41	4.61	1.14	6.80
135	10.07	4.20	6.11	20.95	5.08	3.19	17.76	5.87	7.45	18.98	2.89	13.89	4.74	3.94	4.05	4.03	0.92	5.93
140	8.73	3.16	5.48	18.46	2.69	2.20	15.47	3.75	6.46	17.33	2.52	12.59	4.18	3.56	3.69	3.48	0.69	5.09
145	7.39	2.12	5.01	16.03	1.47	1.36	13.20	2.42	5.47	15.78	2.16	11.37	3.64	3.20	3.35	2.93	0.47	4.26
150	6.05	1.15	4.66	13.61	0.84	0.87	10.94	1.51	4.47	14.31	1.79	10.21	3.10	2.86	3.02	2.38	0.29	3.42
155	4.72	0.63	4.37	11.19	0.46	0.56	8.68	0.88	3.48	12.94	1.43	9.09	2.55	2.51	2.69	1.83	0.18	2.58
160	3.38	0.36	4.11	8.77	0.25	0.35	6.42	0.45	2.49	11.57	1.06	7.96	2.01	2.17	2.36	1.28	0.12	1.77
165	2.17	0.20	3.86	6.35	0.13	0.20	4.29	0.17	1.60	10.20	0.72	6.83	1.47	1.83	2.03	0.80	0.07	1.09
170	1.37	0.11	3.63	3.98	0.05	0.11	2.67	0.04	1.00	8.84	0.44	5.70	0.97	1.49	1.70	0.51	0.04	0.70
175	0.88	0.05	3.40	2.12	0.01	0.04	1.71	0.03	0.65	7.48	0.28	4.58	0.60	1.15	1.37	0.33	0.02	0.45
180	0.56	0.02	3.18	1.17	0.00	0.01	1.09	0.02	0.41	6.11	0.18	3.45	0.39	0.80	1.05	0.20	0.01	0.28
185	0.33	0.00	2.96	0.66	0.00	0.01	0.67	0.02	0.25	4.75	0.11	2.36	0.25	0.50	0.72	0.12	0.00	0.16
190	0.18	0.00	2.74	0.36	0.00	0.01	0.38	0.01	0.13	3.39	0.06	1.46	0.15	0.32	0.41	0.06	0.00	0.08
195	0.08	0.00	2.52	0.19	0.00	0.00	0.19	0.01	0.06	2.17	0.03	0.93	0.08	0.21	0.22	0.03	0.00	0.03
200	0.02	0.00	2.30	0.09	0.00	0.00	0.07	0.01	0.02	1.36	0.01	0.60	0.04	0.13	0.12	0.01	0.00	0.01
205	0.01	0.00	2.07	0.03	0.00	0.00	0.02	0.00	0.01	0.88	0.00	0.37	0.01	0.08	0.07	0.00	0.00	0.01
210	0.01	0.00	1.85	0.00	0.00	0.00	0.01	0.00	0.01	0.56	0.00	0.22	0.00	0.04	0.04	0.00	0.00	0.00
215	0.01	0.00	1.63	0.00	0.00	0.00	0.01	0.00	0.00	0.33	0.00	0.11	0.00	0.02	0.02	0.00	0.00	0.00
220	0.00	0.00	1.41	0.00	0.00	0.00	0.01	0.00	0.00	0.18	0.00	0.04	0.00	0.01	0.00	0.00	0.00	0.00
225	0.00	0.00	1.19	0.00	0.00	0.01	0.00	0.00	0.08	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
230	0.00	0.00	0.97	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
235	0.00	0.00	0.75	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
240	0.00	0.00	0.53	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
245	0.00	0.00	0.32	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
250	0.00	0.00	0.17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
255	0.00	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
260	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
265	0.00	0.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
270	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
275	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
280	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
285	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
290	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
295	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
300	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
305	0.00	0.00	0.00	0.00	0.0													

Printouts for Unit Hydrographs

flow in cfs

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results								Excess Precip.		Storm Hydrograph				
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs) (c.f.)	Volume	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.097	0.131	25.0	4.03	13.0	2.84	6.7	85	164,729	0.57	94,676	35.0	31	94,308	0.68
B1		0.092	0.139	18.2	3.44	9.5	2.43	5.7	95	134,310	0.58	77,837	30.0	29	77,220	0.80
B2		0.093	0.113	33.3	4.40	17.3	3.11	7.3	35	90,351	0.56	50,405	35.0	12	50,284	0.48
B3		0.109	0.171	35.1	6.09	18.2	4.30	10.2	159	431,607	0.31	135,184	35.0	37	135,109	0.31
C1		0.089	0.205	15.3	3.91	7.9	2.76	6.5	238	281,797	0.64	181,072	30.0	76	180,336	0.97
D1		0.092	0.115	17.3	3.03	9.0	2.14	5.1	66	88,318	0.67	59,557	30.0	24	58,560	0.99
D2		0.084	0.229	15.9	4.30	8.3	3.04	7.2	229	282,777	0.87	246,138	30.0	98	245,292	1.26
E1		0.114	0.151	26.8	4.61	13.9	3.25	7.7	155	321,618	0.41	131,675	35.0	47	131,227	0.53
F1		0.107	0.097	32.8	3.94	17.1	2.78	6.6	48	122,440	0.47	56,968	35.0	16	56,751	0.48
F2		0.088	0.198	21.9	4.83	11.4	3.41	8.1	145	245,533	0.75	184,862	35.0	60	183,986	0.89
F3		0.092	0.087	20.4	2.87	10.6	2.03	4.8	30	46,609	0.68	31,862	30.0	11	31,302	0.88
F4		0.121	0.121	41.5	5.37	21.6	3.79	8.9	58	186,981	0.36	67,763	35.0	17	67,675	0.34
G1		0.096	0.093	25.2	3.31	13.1	2.34	5.5	37	73,072	0.59	43,083	30.0	14	42,758	0.68
G2		0.107	0.067	37.3	3.43	19.4	2.42	5.7	19	54,958	0.47	25,571	35.0	7	25,468	0.43
H1		0.109	0.078	39.3	3.85	20.4	2.72	6.4	25	75,177	0.31	23,258	35.0	6	23,195	0.27
H2		0.092	0.101	20.5	3.09	10.6	2.18	5.2	42	67,337	0.67	45,076	30.0	16	44,528	0.88
H3		0.094	0.058	19.2	2.36	10.0	1.67	3.9	15	21,816	0.64	13,878	30.0	5	13,432	0.87
H4		0.095	0.111	22.8	3.45	11.9	2.44	5.7	57	100,370	0.61	61,173	30.0	21	60,592	0.76

5-Year Post Development CUHP Output

Printouts for Unit Hydrographs

flow in cfs

time in minutes	A1	B1	B2	B3	C1	D1	D2	E1	F1	F2	F3	F4	G1	G2	H1	H2	H3	H4
5	77.33	93.25	30.09	102.59	220.53	65.84	199.90	128.93	44.36	115.64	29.50	42.62	37.03	18.62	23.03	42.42	14.61	55.54
10	82.78	86.57	34.71	158.92	211.37	57.29	212.53	153.31	47.44	142.37	26.77	58.18	35.84	18.73	24.44	38.99	12.72	53.96
15	70.87	64.60	32.47	154.15	146.87	42.55	148.71	136.86	43.94	117.23	20.78	56.54	30.18	17.61	23.25	30.20	9.82	43.13
20	57.63	49.16	28.07	139.10	107.74	32.08	108.63	110.77	37.50	92.72	16.66	52.59	24.96	15.66	21.07	24.25	7.67	35.72
25	47.82	39.67	24.21	116.79	80.83	25.68	83.75	93.90	32.69	72.89	13.46	46.34	20.75	13.62	18.22	19.53	6.26	28.56
30	39.89	30.81	21.23	103.58	53.91	19.28	58.88	77.26	28.57	61.39	11.05	41.06	17.44	12.21	16.48	16.06	5.00	24.34
35	34.20	21.94	18.25	90.37	40.79	13.08	41.89	67.52	24.45	50.16	8.64	37.09	14.97	10.80	14.74	12.59	3.73	20.17
40	28.51	17.08	16.20	78.14	31.82	10.94	33.60	57.77	21.87	38.93	6.23	33.12	12.50	9.45	13.00	9.12	2.78	16.00
45	22.81	14.12	14.45	70.52	22.85	8.81	25.30	48.03	19.44	28.50	5.21	29.15	10.02	8.61	11.70	7.55	2.35	11.83
50	17.12	11.17	12.70	62.89	13.88	6.68	17.01	38.28	17.01	24.76	4.40	26.80	7.55	7.77	10.67	6.39	1.93	10.13
55	15.14	8.21	10.96	55.26	4.91	4.55	8.72	30.20	14.58	21.02	3.60	24.47	6.69	6.93	9.63	5.24	1.51	8.74
60	13.25	5.26	9.21	47.63	0.00	2.41	0.43	26.95	12.15	17.28	2.80	22.14	5.86	6.09	8.60	4.08	1.09	7.35
65	11.35	2.30	7.46	40.01		0.28	0.00	23.70	9.73	13.53	1.99	19.80	5.04	5.25	7.56	2.92	0.66	5.96
70	9.45	0.00	6.57	32.38		0.00		20.45	8.85	9.79	1.19	17.47	4.21	4.41	6.53	1.77	0.24	4.57
75	7.55		5.99	29.45				17.20	8.04	6.05	0.39	15.14	3.39	3.73	5.49	0.61	0.00	3.18
80	5.65		5.41	26.90				13.96	7.23	2.30	0.00	12.80	2.56	3.45	4.78	0.00		1.79
85	3.76		4.83	24.36				10.71	6.42	0.00		11.25	1.74	3.17	4.43			0.40
90	1.86		4.24	21.82				7.46	5.61			10.48	0.92	2.89	4.09			0.00
95	0.00		3.66	19.28				4.21	4.80			9.70	0.09	2.61	3.74			
100			3.08	16.73				0.96	3.99			8.92	0.00	2.33	3.40			
105			2.50	14.19				0.00	3.18			8.14		2.05	3.05			
110			1.91	11.65					2.37			7.37		1.77	2.71			
115			1.33	9.11					1.57			6.59		1.49	2.36			
120			0.75	6.57					0.76			5.81		1.21	2.02			
125			0.16	4.02					0.00			5.03		0.93	1.67			
130			0.00	1.48								4.25		0.65	1.33			
135				0.00								3.48		0.37	0.98			
140												2.70		0.09	0.64			
145												1.92		0.00	0.29			
150												1.14		0.00				
155												0.37						
160												0.00						

Printouts for Storm Hydrographs

flow in cfs

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results								Excess Precip.		Storm Hydrograph				
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.096	0.134	24.4	4.01	12.7	2.83	6.7	87	164,729	1.93	317,756	40.0	101	316,720	2.22
B1		0.091	0.141	17.8	3.42	9.2	2.42	5.7	98	134,310	1.82	243,813	35.0	97	241,630	2.62
B2		0.092	0.115	32.5	4.38	16.9	3.09	7.3	36	90,351	1.79	161,555	40.0	42	161,041	1.70
B3		0.089	0.250	19.5	5.26	10.2	3.72	8.8	285	431,607	1.88	813,554	40.0	295	807,930	2.48
C1		0.088	0.210	14.7	3.88	7.6	2.74	6.5	247	281,797	1.91	539,141	35.0	238	535,192	3.07
D1		0.092	0.116	17.1	3.02	8.9	2.14	5.0	67	88,318	2.03	179,570	35.0	70	176,587	2.88
D2		0.083	0.230	15.8	4.30	8.2	3.04	7.2	231	282,777	2.25	634,968	35.0	252	632,818	3.24
E1		0.113	0.150	26.5	4.56	13.8	3.23	7.6	157	321,618	1.75	563,176	40.0	178	561,356	2.01
F1		0.106	0.096	32.4	3.90	16.9	2.76	6.5	49	122,440	1.81	221,916	40.0	59	221,037	1.75
F2		0.088	0.199	21.7	4.82	11.3	3.40	8.0	146	245,533	2.12	520,116	40.0	171	517,601	2.53
F3		0.091	0.088	20.1	2.86	10.5	2.02	4.8	30	46,609	2.04	95,234	35.0	33	93,473	2.56
F4		0.090	0.168	22.4	4.39	11.7	3.10	7.3	108	186,981	2.06	385,413	40.0	125	383,174	2.42
G1		0.095	0.095	24.6	3.29	12.8	2.33	5.5	38	73,072	1.94	142,048	40.0	44	140,977	2.18
G2		0.106	0.067	36.8	3.40	19.2	2.41	5.7	19	54,958	1.81	99,609	45.0	24	99,196	1.58
H1		0.107	0.078	38.6	3.80	20.1	2.69	6.3	25	75,177	1.49	111,730	45.0	28	111,424	1.33
H2		0.092	0.102	20.2	3.08	10.5	2.18	5.1	43	67,337	2.03	136,549	35.0	48	134,796	2.57
H3		0.093	0.059	18.9	2.36	9.8	1.66	3.9	15	21,816	1.99	43,454	35.0	16	42,019	2.60
H4		0.094	0.113	22.3	3.44	11.6	2.43	5.7	58	100,370	1.96	197,106	35.0	65	195,054	2.34

Printouts for Storm Hydrographs

flow in cf

Printouts for Unit Hydrographs

flow in cfs

time in minutes	A1	B1	B2	B3	C1	D1	D2	E1	F1	F2	F3	F4	G1	G2	H1	H2	H3	H4
5	79.48	95.51	30.93	212.33	229.82	66.81	201.50	131.02	45.09	117.17	29.92	92.63	37.90	18.89	23.57	43.06	14.85	56.70
10	84.67	87.92	35.54	282.68	215.27	57.76	213.46	154.59	47.98	143.83	27.05	104.96	36.56	18.95	24.84	39.42	12.85	54.86
15	71.63	65.18	33.09	218.45	147.65	42.75	148.95	137.43	44.32	117.53	20.92	85.95	30.43	17.77	23.57	30.43	9.89	43.38
20	58.21	48.97	28.30	170.33	107.98	32.20	108.75	111.17	37.59	92.99	16.68	69.02	25.18	15.74	21.25	24.29	7.66	35.92
25	47.87	39.61	24.48	132.75	78.94	25.61	83.53	93.98	32.85	72.85	13.48	54.84	20.77	13.71	18.39	19.57	6.27	28.68
30	40.08	30.32	21.34	107.50	49.89	19.02	58.31	77.43	28.63	61.37	11.00	46.28	17.51	12.26	16.59	16.00	4.96	24.34
35	34.09	21.04	18.21	82.24	39.94	13.05	41.79	67.50	24.41	49.89	8.52	38.16	14.92	10.82	14.79	12.42	3.65	20.00
40	28.10	16.93	16.26	57.04	30.26	10.85	33.38	57.58	21.90	38.40	6.04	30.04	12.33	9.48	12.98	8.85	2.77	15.66
45	22.11	13.83	14.43	48.62	20.58	8.66	24.98	47.65	19.41	28.45	5.18	21.93	9.74	8.62	11.74	7.51	2.33	11.51
50	16.99	10.74	12.59	40.20	10.90	6.46	16.57	37.72	16.92	24.63	4.35	18.95	7.50	7.76	10.67	6.32	1.89	10.06
55	15.00	7.64	10.76	31.78	1.22	4.26	8.16	30.14	14.43	20.80	3.52	16.25	6.63	6.90	9.60	5.12	1.46	8.61
60	13.00	4.55	8.92	23.36	0.00	2.07	0.00	26.83	11.95	16.97	2.70	13.54	5.77	6.04	8.53	3.93	1.02	7.17
65	11.00	1.45	7.15	14.94		0.00		23.53	9.65	13.14	1.87	10.83	4.91	5.18	7.46	2.74	0.58	5.72
70	9.01	0.00	6.53	6.53				20.22	8.82	9.32	1.04	8.13	4.04	4.32	6.39	1.55	0.15	4.27
75	7.01		5.92	0.00				16.91	7.99	5.49	0.22	5.42	3.18	3.72	5.32	0.36	0.00	2.82
80	5.01		5.31					13.60	7.16	1.66	0.00	2.72	2.31	3.43	4.76	0.00		1.38
85	3.02		4.70					10.29	6.33	0.00		0.01	1.45	3.15	4.41			0.00
90	1.02		4.09					6.98	5.50			0.00	0.59	2.86	4.05			
95	0.00		3.47					3.67	4.67				0.00	2.57	3.69			
100			2.86					0.36	3.84					2.29	3.34			
105			2.25					0.00	3.01					2.00	2.98			
110			1.64						2.18					1.71	2.62			
115			1.03						1.35					1.43	2.27			
120			0.41						0.52					1.14	1.91			
125			0.00						0.00					0.85	1.55			
130														0.57	1.19			
135														0.28	0.84			
140														0.00	0.48			
145														0.12				
150														0.00				

Appendix C

SWMM Model Pre Development 5 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

SWMM Pre Development 5 Year

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff NO
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00

Ending Date 01/01/2005 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:05:00

Routing Time Step 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	12.024	3.918
External Outflow	12.024	3.918
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.000	0.000
Continuity Error (%)	-0.002	

SWMM Model Pre Development 5 Year

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step	:	30.00 sec
Average Time Step	:	30.00 sec
Maximum Time Step	:	30.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	1.00
Percent Not Converging	:	0.00

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.08	0.31	6945.31	0 00:35	0.30
24	JUNCTION	0.10	0.44	6934.44	0 00:40	0.44
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.10	0.48	6911.48	0 00:35	0.48
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.11	0.48	6900.48	0 00:35	0.48
65	JUNCTION	0.17	0.69	6880.69	0 00:36	0.69
66	JUNCTION	0.24	0.89	6868.89	0 00:40	0.89
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0 00:00	0.00
73	JUNCTION	0.11	0.43	6902.43	0 00:35	0.42

			SWMM Model	Pre Development	5 Year		
80		JUNCTION	0.00	0.00	6890.00	0 00:00	0.00
81		JUNCTION	0.00	0.00	6896.00	0 00:00	0.00
82		JUNCTION	0.00	0.00	6886.00	0 00:00	0.00
83		JUNCTION	0.00	0.00	6878.00	0 00:00	0.00
84		JUNCTION	0.11	0.48	6872.48	0 00:35	0.47
85		JUNCTION	0.06	0.30	6874.30	0 00:35	0.30
PondC		JUNCTION	0.00	0.00	6956.00	0 00:00	0.00
PondA		JUNCTION	0.00	0.00	6949.00	0 00:00	0.00
PondB		JUNCTION	0.11	0.44	6911.44	0 00:41	0.43
PondE		JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
PondG		JUNCTION	0.11	0.42	6900.42	0 00:36	0.42
PondH		JUNCTION	0.11	0.47	6866.47	0 00:36	0.47
PondF		JUNCTION	0.24	0.89	6866.89	0 00:41	0.88
PondD		JUNCTION	0.10	0.48	6881.48	0 00:37	0.47
Outfall2		OUTFALL	0.00	0.00	6910.00	0 00:00	0.00
Outfall11		OUTFALL	0.00	0.00	6947.00	0 00:00	0.00
Outfall4		OUTFALL	0.00	0.00	6865.00	0 00:00	0.00
Outfall3		OUTFALL	0.00	0.00	6880.00	0 00:00	0.00
31		OUTFALL	0.00	0.00	6953.00	0 00:00	0.00
51		OUTFALL	0.00	0.00	6920.00	0 00:00	0.00
74		OUTFALL	0.00	0.00	6897.00	0 00:00	0.00
67		OUTFALL	0.00	0.00	6865.50	0 00:00	0.00

Node Inflow Summary

Total Inflow Volume Node gal	Flow Balance Error Percent	Type	Maximum Lateral	Maximum Total	Time of Max	Lateral	
			Inflow	Inflow	Occurrence	Inflow	
			CFS	CFS	days hr:min	10^6 gal	10^6
10 0.304	0.000	JUNCTION	13.03	13.03	0 00:35	0.304	
20 0.085	0.000	JUNCTION	4.33	4.33	0 00:35	0.085	
21 0.0573	0.000	JUNCTION	1.66	1.66	0 00:40	0.0573	

			SWMM Model	Pre Development	5 Year		
22		JUNCTION		11.85	11.85	0 00:40	0.274
0.274	0.000						
23		JUNCTION		0.00	5.99	0 00:35	0
0.142	0.000						
24		JUNCTION		0.00	11.85	0 00:40	0
0.274	0.000						
30		JUNCTION		9.95	9.95	0 00:35	0.179
0.179	0.000						
40		JUNCTION		8.12	8.12	0 00:35	0.162
0.162	0.000						
41		JUNCTION		22.23	22.23	0 00:40	0.522
0.522	0.000						
42		JUNCTION		0.00	8.12	0 00:35	0
0.162	0.000						
50		JUNCTION		32.34	32.34	0 00:35	0.593
0.593	0.000						
60		JUNCTION		9.70	9.70	0 00:35	0.226
0.226	0.000						
61		JUNCTION		16.46	16.46	0 00:40	0.453
0.453	0.000						
62		JUNCTION		3.65	3.65	0 00:35	0.0858
0.0858	0.000						
63		JUNCTION		12.98	12.98	0 00:40	0.345
0.345	0.000						
64		JUNCTION		0.00	13.35	0 00:35	0
0.311	0.000						
65		JUNCTION		0.00	26.04	0 00:36	0
0.657	0.000						
66		JUNCTION		0.00	16.46	0 00:40	0
0.453	0.000						
70		JUNCTION		5.57	5.57	0 00:35	0.135
0.135	0.000						
71		JUNCTION		3.87	3.87	0 00:35	0.101
0.101	0.000						
72		JUNCTION		0.00	3.87	0 00:35	0
0.101	0.000						
73		JUNCTION		0.00	3.87	0 00:35	0
0.101	0.000						
80		JUNCTION		1.85	1.85	0 00:35	0.0476
0.0476	0.000						
81		JUNCTION		5.37	5.37	0 00:35	0.124
0.124	0.000						
82		JUNCTION		1.92	1.92	0 00:35	0.0398
0.0398	0.000						
83		JUNCTION		8.07	8.07	0 00:35	0.185
0.185	0.000						
84		JUNCTION		0.00	7.22	0 00:35	0
0.172	0.000						

		SWMM Model	Pre Development	5 Year			
85		JUNCTION	0.00	1.92	0	00:35	0
0.0398	0.000	JUNCTION	0.00	9.95	0	00:35	0
PondC		JUNCTION	0.00	13.03	0	00:35	0
0.179	0.000	JUNCTION	0.00	17.56	0	00:41	0
PondA		JUNCTION	0.00	32.34	0	00:35	0
0.304	0.000	JUNCTION	0.00	9.42	0	00:36	0
PondB		JUNCTION	0.00	17.11	0	00:36	0
0.416	0.000	JUNCTION	0.00	42.32	0	00:41	0
PondE		JUNCTION	0.00	30.00	0	00:38	0
0.593	0.000	JUNCTION	0.00	17.56	0	00:41	0
PondG		JUNCTION	0.00	13.03	0	00:35	0
0.236	0.000	JUNCTION	0.00	17.11	0	00:36	0
PondH		JUNCTION	0.00	32.34	0	00:35	0
0.397	0.000	JUNCTION	0.00	9.42	0	00:36	0
PondF		JUNCTION	0.00	42.32	0	00:41	0
1.11	0.000	JUNCTION	0.00	30.00	0	00:38	0
PondD		JUNCTION	0.00	17.56	0	00:41	0
0.685	0.000	OUTFALL	0.00	13.03	0	00:35	0
Outfall2		OUTFALL	0.00	17.11	0	00:36	0
0.416	0.000	OUTFALL	0.00	30.00	0	00:38	0
Outfall1		OUTFALL	0.00	9.42	0	00:35	0
0.304	0.000	OUTFALL	0.00	17.11	0	00:36	0
Outfall14		OUTFALL	0.00	32.34	0	00:35	0
0.397	0.000	OUTFALL	0.00	42.32	0	00:41	0
Outfall13		OUTFALL	0.00	30.00	0	00:38	0
0.685	0.000	OUTFALL	0.00	9.95	0	00:35	0
31		OUTFALL	0.00	32.34	0	00:35	0
0.179	0.000	OUTFALL	0.00	42.32	0	00:41	0
51		OUTFALL	0.00	13.03	0	00:35	0
0.593	0.000	OUTFALL	0.00	17.11	0	00:36	0
74		OUTFALL	0.00	9.42	0	00:36	0
0.236	0.000	OUTFALL	0.00	30.00	0	00:38	0
67		OUTFALL	0.00	17.56	0	00:41	0
1.11	0.000	OUTFALL	0.00	13.03	0	00:35	0

Node Flooding Summary

No nodes were flooded.

Outfall Loading Summary

Outfall Node	SWMM Model Pre Development 5 Year			
	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal

Outfall2	67.36	3.82	17.56	0.416
Outfall11	55.28	3.40	13.03	0.304
Outfall14	59.31	4.14	17.11	0.397
Outfall13	60.56	7.00	30.00	0.685
31	50.97	2.17	9.95	0.179
51	51.53	7.12	32.34	0.593
74	58.61	2.49	9.42	0.236
67	65.97	10.41	42.32	1.110
System	58.70	40.55	169.75	3.918

Link Flow Summary

Link	Type	Maximum	Time of Max	Maximum	Max/	Max/
		Flow	Occurrence	Veloc	Full	Full
		CFS	days hr:min	ft/sec	Flow	Depth
100	DUMMY	13.03	0 00:35			
200	DUMMY	4.33	0 00:35			
201	DUMMY	1.66	0 00:40			
202	CONDUIT	5.95	0 00:36	10.09	0.00	0.04
204	DUMMY	11.85	0 00:40			
205	CONDUIT	11.83	0 00:41	11.82	0.01	0.06
300	DUMMY	9.95	0 00:35			
400	DUMMY	8.12	0 00:35			
401	CONDUIT	8.03	0 00:37	8.38	0.02	0.10
402	DUMMY	22.23	0 00:40			
500	DUMMY	32.34	0 00:35			
601	DUMMY	16.46	0 00:40			
602	CONDUIT	16.42	0 00:41	6.99	0.07	0.18
603	DUMMY	9.70	0 00:35			
604	DUMMY	3.65	0 00:35			
605	CONDUIT	13.32	0 00:36	11.62	0.01	0.07
606	DUMMY	12.98	0 00:40			
607	CONDUIT	26.04	0 00:36	12.42	0.02	0.09
700	DUMMY	5.57	0 00:35			
701	DUMMY	3.87	0 00:35			
702	DUMMY	3.87	0 00:35			
703	CONDUIT	3.86	0 00:36	4.80	0.01	0.08
801	DUMMY	1.85	0 00:35			

		SWMM Model	Pre Development	5 Year			
802	DUMMY	5.37	0	00:35			
803	CONDUIT	7.18	0	00:36	6.34	0.01	0.07
804	DUMMY	1.92	0	00:35			
806	DUMMY	8.07	0	00:35			
805	CONDUIT	1.91	0	00:37	4.00	0.01	0.06
301	DUMMY	9.95	0	00:35			
101	DUMMY	13.03	0	00:35			
206	DUMMY	17.56	0	00:41			
501	DUMMY	32.34	0	00:35			
704	DUMMY	9.42	0	00:36			
807	DUMMY	17.11	0	00:36			
608	DUMMY	42.32	0	00:41			
403	DUMMY	30.00	0	00:38			

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Fri Apr 10 17:42:01 2020

Analysis ended on: Fri Apr 10 17:42:01 2020

Total elapsed time: < 1 sec

SWMM Model Pre Development 100 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

SWMM 100 Year Pre Development

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff NO
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00

Ending Date 01/01/2005 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:05:00

Routing Time Step 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	82.644	26.931
External Outflow	82.609	26.919
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.000	0.000
Continuity Error (%)	0.043	

SWMM Model Pre Development 100 Year

Highest Flow Instability Indexes

Link 608 (1)

Routing Time Step Summary

Minimum Time Step : 30.00 sec
Average Time Step : 30.00 sec
Maximum Time Step : 30.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.04
Percent Not Converging : 0.00

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.21	0.59	6945.59	0 00:45	0.58
24	JUNCTION	0.36	1.43	6935.43	0 00:45	1.42
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.24	1.05	6912.05	0 00:40	1.05
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.27	1.04	6901.04	0 00:45	1.03
65	JUNCTION	0.43	1.52	6881.52	0 00:45	1.52
66	JUNCTION	0.61	2.08	6870.08	0 00:50	2.08
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0 00:00	0.00
73	JUNCTION	0.27	0.94	6902.94	0 00:45	0.94

		SWMM Model	Pre Development	100 Year			
80		JUNCTION	0.00	0.00	6890.00	0 00:00	0.00
81		JUNCTION	0.00	0.00	6896.00	0 00:00	0.00
82		JUNCTION	0.00	0.00	6886.00	0 00:00	0.00
83		JUNCTION	0.00	0.00	6878.00	0 00:00	0.00
84		JUNCTION	0.32	1.19	6873.19	0 00:45	1.18
85		JUNCTION	0.15	0.64	6874.64	0 00:40	0.64
PondC		JUNCTION	0.00	0.00	6956.00	0 00:00	0.00
PondA		JUNCTION	0.00	0.00	6949.00	0 00:00	0.00
PondB		JUNCTION	0.39	1.43	6912.43	0 00:46	1.42
PondE		JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
PondG		JUNCTION	0.27	0.94	6900.94	0 00:46	0.94
PondH		JUNCTION	0.32	1.18	6867.18	0 00:46	1.18
PondF		JUNCTION	0.61	2.08	6868.08	0 00:51	2.08
PondD		JUNCTION	0.25	1.05	6882.05	0 00:42	1.05
Outfall2		OUTFALL	0.00	0.00	6910.00	0 00:00	0.00
Outfall11		OUTFALL	0.00	0.00	6947.00	0 00:00	0.00
Outfall4		OUTFALL	0.00	0.00	6865.00	0 00:00	0.00
Outfall3		OUTFALL	0.00	0.00	6880.00	0 00:00	0.00
31		OUTFALL	0.00	0.00	6953.00	0 00:00	0.00
51		OUTFALL	0.00	0.00	6920.00	0 00:00	0.00
74		OUTFALL	0.00	0.00	6897.00	0 00:00	0.00
67		OUTFALL	0.00	0.00	6865.50	0 00:00	0.00

Node Inflow Summary

Total Inflow Volume Node gal	Flow Balance Error Percent	Type	Maximum Lateral	Maximum Total	Time of Max	Lateral
			Inflow	Inflow	Occurrence	Inflow
		CFS	CFS	days hr:min	10^6 gal	10^6
10 0.304	0.000	JUNCTION	13.03	13.03	0 00:35	0.304
20 0.085	0.000	JUNCTION	4.33	4.33	0 00:35	0.085
21 0.794	0.000	JUNCTION	20.74	20.74	0 00:50	0.794

		SWMM Model	Pre Development	100 Year		
22		JUNCTION	140.35	140.35	0	00:45
3.79	0.000					3.79
23		JUNCTION	0.00	23.90	0	00:45
0.879	0.000					0
24		JUNCTION	0.00	140.35	0	00:45
3.79	0.000					0
30		JUNCTION	110.70	110.70	0	00:40
2.47	0.000					2.47
40		JUNCTION	40.00	40.00	0	00:40
1.03	0.000					1.03
41		JUNCTION	114.87	114.87	0	00:45
3.31	0.000					3.31
42		JUNCTION	0.00	40.00	0	00:40
1.03	0.000					0
50		JUNCTION	157.99	157.99	0	00:40
3.76	0.000					3.76
60		JUNCTION	49.45	49.45	0	00:45
1.43	0.000					1.43
61		JUNCTION	86.73	86.73	0	00:50
2.87	0.000					2.87
62		JUNCTION	18.42	18.42	0	00:45
0.544	0.000					0.544
63		JUNCTION	67.82	67.82	0	00:45
2.19	0.000					2.19
64		JUNCTION	0.00	67.87	0	00:45
1.97	0.000					0
65		JUNCTION	0.00	135.62	0	00:45
4.16	0.000					0
66		JUNCTION	0.00	86.73	0	00:50
2.87	0.000					0
70		JUNCTION	28.46	28.46	0	00:45
0.853	0.000					0.853
71		JUNCTION	20.06	20.06	0	00:45
0.641	0.000					0.641
72		JUNCTION	0.00	20.06	0	00:45
0.641	0.000					0
73		JUNCTION	0.00	20.06	0	00:45
0.641	0.000					0
80		JUNCTION	21.89	21.89	0	00:45
0.659	0.000					0.659
81		JUNCTION	27.12	27.12	0	00:45
0.786	0.000					0.786
82		JUNCTION	9.51	9.51	0	00:40
0.252	0.000					0.252
83		JUNCTION	40.86	40.86	0	00:45
1.17	0.000					1.17
84		JUNCTION	0.00	49.01	0	00:45
1.44	0.000					0

		SWMM Model	Pre Development	100 Year			
85		JUNCTION	0.00	9.51	0	00:40	0
0.252	0.000	JUNCTION	0.00	110.70	0	00:40	0
PondC		JUNCTION	0.00	13.03	0	00:35	0
2.47	0.000	JUNCTION	0.00	164.21	0	00:46	0
PondA		JUNCTION	0.00	157.99	0	00:40	0
0.304	0.000	JUNCTION	0.00	48.48	0	00:45	0
PondB		JUNCTION	0.00	99.16	0	00:45	0
4.66	0.000	JUNCTION	0.00	221.11	0	00:46	0
PondE		JUNCTION	0.00	154.35	0	00:45	0
3.76	0.000	JUNCTION	0.00	164.21	0	00:46	0
PondG		JUNCTION	0.00	13.03	0	00:35	0
1.49	0.000	JUNCTION	0.00	99.16	0	00:45	0
PondH		JUNCTION	0.00	48.48	0	00:45	0
2.87	0.000	JUNCTION	0.00	154.35	0	00:45	0
PondF		JUNCTION	0.00	110.70	0	00:40	0
7.02	0.000	JUNCTION	0.00	221.11	0	00:46	0
PondD		JUNCTION	0.00	157.99	0	00:40	0
4.34	0.000	OUTFALL	0.00	0.00	0	00:46	0
Outfall2		OUTFALL	0.00	164.21	0	00:46	0
4.66	0.000	OUTFALL	0.00	13.03	0	00:35	0
Outfall1		OUTFALL	0.00	99.16	0	00:45	0
0.304	0.000	OUTFALL	0.00	48.48	0	00:45	0
Outfall4		OUTFALL	0.00	154.35	0	00:45	0
2.87	0.000	OUTFALL	0.00	110.70	0	00:40	0
Outfall3		OUTFALL	0.00	221.11	0	00:46	0
4.34	0.000	OUTFALL	0.00	157.99	0	00:40	0
31		OUTFALL	0.00	0.00	0	00:40	0
2.47	0.000	OUTFALL	0.00	164.21	0	00:46	0
51		OUTFALL	0.00	13.03	0	00:35	0
3.76	0.000	OUTFALL	0.00	99.16	0	00:45	0
74		OUTFALL	0.00	48.48	0	00:45	0
1.49	0.000	OUTFALL	0.00	154.35	0	00:45	0
67		OUTFALL	0.00	110.70	0	00:40	0
7.02	0.000	OUTFALL	0.00	221.11	0	00:46	0

Node Flooding Summary

No nodes were flooded.

Outfall Loading Summary

Outfall Node	SWMM Model Pre Development 100 Year			
	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal

Outfall2	76.53	37.73	164.21	4.665
Outfall11	55.28	3.40	13.03	0.304
Outfall14	67.08	26.46	99.16	2.867
Outfall13	67.92	39.52	154.35	4.336
31	53.89	28.39	110.70	2.472
51	58.47	39.76	157.99	3.757
74	67.08	13.78	48.48	1.494
67	74.31	58.49	221.11	7.022
System	65.07	247.53	962.28	26.917

Link Flow Summary

Link	Type	Maximum	Time of Max	Maximum	Max/	Max/
		Flow	Occurrence	Veloc	Full	Full
		CFS	days hr:min	ft/sec	Flow	Depth
100	DUMMY	13.03	0 00:35			
200	DUMMY	4.33	0 00:35			
201	DUMMY	20.74	0 00:50			
202	CONDUIT	23.89	0 00:46	15.49	0.01	0.08
204	DUMMY	140.35	0 00:45			
205	CONDUIT	140.32	0 00:46	24.86	0.09	0.20
300	DUMMY	110.70	0 00:40			
400	DUMMY	40.00	0 00:40			
401	CONDUIT	39.84	0 00:42	13.30	0.10	0.21
402	DUMMY	114.87	0 00:45			
500	DUMMY	157.99	0 00:40			
601	DUMMY	86.73	0 00:50			
602	CONDUIT	86.65	0 00:51	11.22	0.36	0.42
603	DUMMY	49.45	0 00:45			
604	DUMMY	18.42	0 00:45			
605	CONDUIT	67.80	0 00:45	19.12	0.05	0.15
606	DUMMY	67.82	0 00:45			
607	CONDUIT	135.63	0 00:46	20.33	0.08	0.19
700	DUMMY	28.46	0 00:45			
701	DUMMY	20.06	0 00:45			
702	DUMMY	20.06	0 00:45			
703	CONDUIT	20.04	0 00:46	7.87	0.08	0.19
801	DUMMY	21.89	0 00:45			

		SWMM Model Pre Development 100 Year		
802	DUMMY	27.12	0	00:45
803	CONDUIT	48.96	0	00:46
804	DUMMY	9.51	0	00:40
806	DUMMY	40.86	0	00:45
805	CONDUIT	9.46	0	00:42
301	DUMMY	110.70	0	00:40
101	DUMMY	13.03	0	00:35
206	DUMMY	164.21	0	00:46
501	DUMMY	157.99	0	00:40
704	DUMMY	48.48	0	00:45
807	DUMMY	99.16	0	00:45
608	DUMMY	221.11	0	00:46
403	DUMMY	154.35	0	00:45

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Fri Apr 10 13:11:18 2020

Analysis ended on: Fri Apr 10 13:11:18 2020

Total elapsed time: < 1 sec

SWMM 5 Year Post Development

SWMM 5 Year Output

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff NO

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00

Ending Date 01/02/2005 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:05:00

Routing Time Step 30.00 sec

Flow Routing Continuity	Volume acre-feet	Volume 10^6 gal
-------------------------	---------------------	----------------------

Dry Weather Inflow	0.000	0.000
--------------------------	-------	-------

Wet Weather Inflow	0.000	0.000
--------------------------	-------	-------

Groundwater Inflow	0.000	0.000
--------------------------	-------	-------

RDII Inflow	0.000	0.000
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External Inflow	39.629	12.914
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External Outflow	23.957	7.807
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Flooding Loss	0.000	0.000
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Evaporation Loss	0.000	0.000
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Exfiltration Loss	0.000	0.000
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Initial Stored Volume	0.000	0.000
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Final Stored Volume	15.654	5.101
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Continuity Error (%)	0.045	
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SWMM 5 Year Output

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step	:	30.00 sec
Average Time Step	:	30.00 sec
Maximum Time Step	:	30.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	1.01
Percent Not Converging	:	0.00

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.04	0.75	6945.75	0 00:30	0.74
24	JUNCTION	0.21	1.17	6935.17	0 00:30	1.16
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.17	0.20	6953.20	0 02:23	0.20
67	JUNCTION	0.16	0.59	6866.09	0 01:57	0.59
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.03	0.82	6911.82	0 00:30	0.81
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	0.03	0.21	6920.21	0 01:12	0.21
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.03	0.66	6900.66	0 00:35	0.66
65	JUNCTION	0.05	1.10	6881.10	0 00:35	1.10
66	JUNCTION	0.08	1.71	6869.71	0 00:35	1.71

SWMM 5 Year Output

70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.03	0.55	6902.55	0	00:35	0.54
74	JUNCTION	0.02	0.24	6897.24	0	01:15	0.24
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.04	0.80	6872.80	0	00:30	0.79
85	JUNCTION	0.02	0.48	6874.48	0	00:30	0.47
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.16	0.59	6865.59	0	01:57	0.59
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	5.89	6.37	6917.37	0	01:30	6.37
PondC	STORAGE	4.70	5.56	6961.56	0	02:23	5.56
PondA	STORAGE	4.01	4.67	6953.67	0	01:46	4.67
PondD	STORAGE	5.54	6.51	6887.51	0	02:25	6.51
PondE	STORAGE	4.04	4.77	6927.77	0	01:12	4.77
PondF	STORAGE	5.76	6.73	6872.73	0	02:02	6.73
PondG	STORAGE	0.11	1.20	6901.20	0	01:15	1.20
PondH	STORAGE	4.49	5.12	6871.12	0	02:09	5.12

Node Inflow Summary

Total	Flow		Maximum Lateral	Maximum Total	Time of Max	Lateral
Inflow	Balance		Lateral	Total	Occurrence	Inflow
Volume	Error		Inflow	Inflow		Volume
Node		Type	CFS	CFS	days hr:min	10^6 gal
gal	Percent					10^6
10		JUNCTION	30.72	30.72	0 00:35	0.705
0.705	0.000					
20		JUNCTION	29.46	29.46	0 00:30	0.578
0.578	0.000					
21		JUNCTION	12.02	12.02	0 00:35	0.376

SWMM 5 Year Output						
0.376	0.000	JUNCTION	92.76	92.76	0	00:30
22						2.04
2.04	0.000	JUNCTION	0.00	40.92	0	00:30
23						0
0.954	0.000	JUNCTION	0.00	93.26	0	00:30
24						0
2.96	0.000	JUNCTION	77.99	77.99	0	00:30
30						1.38
1.38	0.000	JUNCTION	0.00	1.52	0	02:23
31						0
0.925	0.000	JUNCTION	0.00	23.06	0	01:57
67						0
2.4	-0.000	JUNCTION	24.15	24.15	0	00:30
40						0.438
0.438	0.000	JUNCTION	98.47	98.47	0	00:30
41						1.83
1.83	0.000	JUNCTION	0.00	24.15	0	00:30
42						0
0.438	-0.000	JUNCTION	46.88	46.88	0	00:35
50						0.982
0.982	0.000	JUNCTION	0.00	18.70	0	01:12
51						0
0.69	0.000	JUNCTION	16.28	16.28	0	00:35
60						0.424
0.424	0.000	JUNCTION	60.11	60.11	0	00:35
61						1.38
1.38	0.000	JUNCTION	11.36	11.36	0	00:30
62						0.234
0.234	0.000	JUNCTION	42.32	42.32	0	00:30
63						0.975
0.975	0.000	JUNCTION	0.00	26.88	0	00:35
64						0
0.659	0.000	JUNCTION	0.00	69.12	0	00:35
65						0
1.63	0.000	JUNCTION	0.00	60.11	0	00:35
66						0
1.38	0.000	JUNCTION	13.78	13.78	0	00:30
70						0.32
0.32	0.000	JUNCTION	6.55	6.55	0	00:35
71						0.191
0.191	0.000	JUNCTION	0.00	6.55	0	00:35
72						0
0.191	0.000	JUNCTION	0.00	6.55	0	00:35
73						0
0.191	0.000	JUNCTION	0.00	9.05	0	01:15
74						0
0.51	-0.000	JUNCTION	5.68	5.68	0	00:35
80						0.173

SWMM 5 Year Output

0.173	0.000						
81		JUNCTION	16.24	16.24	0	00:30	0.333
0.333	0.000						
82		JUNCTION	5.21	5.21	0	00:30	0.1
0.1	0.000						
83		JUNCTION	20.93	20.93	0	00:30	0.453
0.453	0.000						
84		JUNCTION	0.00	21.67	0	00:30	0
0.507	0.000						
85		JUNCTION	0.00	5.21	0	00:30	0
0.1	0.000						
Outfall2		OUTFALL	0.00	34.45	0	01:30	0
2.22	0.000						
Outfall1		OUTFALL	0.00	5.43	0	01:46	0
0.441	0.000						
Outfall4		OUTFALL	0.00	35.27	0	01:51	0
3.71	0.000						
Outfall3		OUTFALL	0.00	2.52	0	02:25	0
1.43	0.000						
PondB		STORAGE	0.00	134.27	0	00:31	0
3.91	0.047						
PondC		STORAGE	0.00	77.99	0	00:30	0
1.38	0.005						
PondA		STORAGE	0.00	30.72	0	00:35	0
0.705	0.012						
PondD		STORAGE	0.00	120.96	0	00:30	0
2.27	0.003						
PondE		STORAGE	0.00	46.88	0	00:35	0
0.982	0.118						
PondF		STORAGE	0.00	129.20	0	00:35	0
3.01	0.014						
PondG		STORAGE	0.00	20.07	0	00:35	0
0.51	0.116						
PondH		STORAGE	0.00	47.25	0	00:32	0
1.06	0.001						

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

SWMM 5 Year Output

of Max Occurrence	Maximum Storage hr:min	Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB			241.825	30	0	0	296.729	37	0
01:30	34.45								
PondC			111.256	19	0	0	174.130	30	0
02:23	1.52								
PondA			53.736	15	0	0	79.797	22	0
01:46	5.43								
PondD			192.634	28	0	0	287.984	41	0
02:24	2.52								
PondE			56.473	16	0	0	85.437	24	0
01:11	18.70								
PondF			235.289	29	0	0	351.325	44	0
02:02	16.38								
PondG			2.647	0	0	0	31.290	6	0
01:15	9.05								
PondH			88.617	17	0	0	127.653	25	0
02:09	4.21								

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall2	99.64	2.76	34.45	2.223
Outfall1	99.67	0.55	5.43	0.441
Outfall4	99.67	4.61	35.27	3.709
Outfall3	99.69	1.78	2.52	1.434
System	99.67	9.70	73.13	7.806

SWMM 5 Year Output

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	30.72	0 00:35			
200	DUMMY	29.46	0 00:30			
201	DUMMY	12.02	0 00:35			
202	CONDUIT	40.84	0 00:31	18.27	0.02	0.11
203	CONDUIT	1.52	0 02:24	6.34	0.00	0.05
204	DUMMY	92.76	0 00:30			
205	CONDUIT	93.43	0 00:31	22.09	0.06	0.17
300	DUMMY	77.99	0 00:30			
400	DUMMY	24.15	0 00:30			
401	CONDUIT	23.53	0 00:32	11.46	0.06	0.16
402	DUMMY	98.47	0 00:30			
500	DUMMY	46.88	0 00:35			
601	DUMMY	60.11	0 00:35			
602	CONDUIT	60.09	0 00:35	10.17	0.25	0.34
603	DUMMY	16.28	0 00:35			
604	DUMMY	11.36	0 00:30			
605	CONDUIT	26.88	0 00:35	14.61	0.02	0.09
606	DUMMY	42.32	0 00:30			
607	CONDUIT	69.12	0 00:31	16.65	0.04	0.14
700	DUMMY	13.78	0 00:30			
701	DUMMY	6.55	0 00:35			
702	DUMMY	6.55	0 00:35			
703	CONDUIT	6.54	0 00:36	5.62	0.03	0.11
801	DUMMY	5.68	0 00:35			
802	DUMMY	16.24	0 00:30			
803	CONDUIT	21.49	0 00:32	8.87	0.03	0.11
804	DUMMY	5.21	0 00:30			
806	DUMMY	20.93	0 00:30			
805	CONDUIT	5.08	0 00:32	5.42	0.02	0.09
808	CONDUIT	23.06	0 01:57	2.25	0.00	0.06
800	CONDUIT	8.95	0 01:25	2.34	0.00	0.02
600	CONDUIT	18.26	0 01:17	5.75	0.00	0.03
101	DUMMY	5.43	0 01:46			
206	DUMMY	34.45	0 01:30			
301	DUMMY	1.52	0 02:23			
501	DUMMY	18.70	0 01:12			
704	DUMMY	9.05	0 01:15			
807	DUMMY	4.21	0 02:09			
608	DUMMY	16.38	0 02:02			
403	DUMMY	2.52	0 02:25			

SWMM 5 Year Output

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Mon Apr 13 19:10:46 2020
Analysis ended on: Mon Apr 13 19:10:46 2020
Total elapsed time: < 1 sec

SWMM 100 Year Output

SWMM 100 Year Post Development

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff NO
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00

Ending Date 01/02/2005 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:05:00

Routing Time Step 30.00 sec

Flow Routing Continuity	Volume acre-feet	Volume 10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	123.320	40.186
External Outflow	105.086	34.244
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	18.084	5.893
Continuity Error (%)	0.122	

SWMM 100 Year Output

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step : 30.00 sec
Average Time Step : 30.00 sec
Maximum Time Step : 30.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.02
Percent Not Converging : 0.00

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.06	1.35	6946.35	0 00:35	1.34
24	JUNCTION	0.27	2.22	6936.22	0 00:51	2.22
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.24	1.68	6954.68	0 00:59	1.68
67	JUNCTION	0.24	2.30	6867.80	0 01:13	2.30
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.05	1.40	6912.40	0 00:35	1.38
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	0.04	0.74	6920.74	0 00:49	0.74
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.06	1.19	6901.19	0 00:40	1.19
65	JUNCTION	0.09	1.92	6881.92	0 00:40	1.92

SWMM 100 Year Output

66	JUNCTION	0.13	3.12	6871.12	0	00:40	3.12
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.06	1.02	6903.02	0	00:45	1.02
74	JUNCTION	0.05	0.60	6897.60	0	01:12	0.60
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.07	1.45	6873.45	0	00:40	1.45
85	JUNCTION	0.03	0.82	6874.82	0	00:35	0.81
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.24	2.30	6867.30	0	01:13	2.30
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.72	9.85	6920.85	0	01:16	9.85
PondC	STORAGE	5.17	7.08	6963.08	0	00:59	7.08
PondA	STORAGE	5.81	8.60	6957.60	0	01:13	8.59
PondD	STORAGE	5.66	8.08	6889.08	0	01:04	8.08
PondE	STORAGE	4.04	5.84	6928.84	0	00:49	5.84
PondF	STORAGE	5.86	8.17	6874.17	0	01:09	8.17
PondG	STORAGE	0.20	2.69	6902.69	0	01:12	2.68
PondH	STORAGE	4.95	6.51	6872.51	0	01:12	6.51

Node Inflow Summary

Total Inflow Volume Node gal	Flow Balance Error Percent	Type	Maximum Lateral	Maximum Total	Time of Max	Lateral
			Inflow	Inflow	Occurrence	Inflow
10 2.37	0.000	JUNCTION	100.64	100.64	0 00:40	2.37
20 1.81	0.000	JUNCTION	97.08	97.08	0 00:35	1.81

SWMM 100 Year Output						
		JUNCTION	42.26	42.26	0 00:40	1.2
21	0.000	JUNCTION	295.27	295.27	0 00:40	6.04
1.2	0.000	JUNCTION	0.00	136.17	0 00:35	0
22	0.000	JUNCTION	0.00	334.84	0 00:51	0
6.04	0.000	JUNCTION	238.03	238.03	0 00:35	4
23	0.000	JUNCTION	0.00	115.75	0 00:59	0
3.01	0.000	JUNCTION	0.00	270.41	0 01:13	0
24	-0.000	JUNCTION	70.07	70.07	0 00:35	1.32
9.43	0.000	JUNCTION	252.18	252.18	0 00:35	4.73
30	0.000	JUNCTION	0.00	70.07	0 00:35	0
4	0.000	JUNCTION	178.04	178.04	0 00:40	4.2
31	0.000	JUNCTION	0.00	164.75	0 00:49	0
3.39	0.000	JUNCTION	58.95	58.95	0 00:40	1.65
67	-0.000	JUNCTION	170.90	170.90	0 00:40	3.87
9.72	0.000	JUNCTION	32.93	32.93	0 00:35	0.699
40	0.000	JUNCTION	124.89	124.89	0 00:40	2.87
1.32	0.000	JUNCTION	0.00	90.88	0 00:40	0
41	0.000	JUNCTION	0.00	215.63	0 00:40	0
4.73	0.000	JUNCTION	0.00	170.90	0 00:40	0
42	0.000	JUNCTION	43.95	43.95	0 00:40	1.05
1.32	0.000	JUNCTION	23.95	23.95	0 00:45	0.742
50	0.000	JUNCTION	0.00	23.95	0 00:45	0
4.2	0.000	JUNCTION	0.00	23.95	0 00:45	0
51	0.000	JUNCTION	0.00	42.13	0 01:12	0
3.95	0.000	JUNCTION	0.00	23.95	0 00:45	0
60	0.000	JUNCTION	0.00	23.95	0 00:45	0
1.65	0.000	JUNCTION	0.00	23.95	0 00:45	0
61	0.000	JUNCTION	0.00	23.95	0 00:45	0
3.87	0.000	JUNCTION	0.00	23.95	0 00:45	0
62	0.000	JUNCTION	0.00	23.95	0 00:45	0
0.699	0.000	JUNCTION	0.00	23.95	0 00:45	0
63	0.000	JUNCTION	0.00	23.95	0 00:45	0
2.87	0.000	JUNCTION	0.00	23.95	0 00:45	0
64	0.000	JUNCTION	0.00	23.95	0 00:45	0
2.35	0.000	JUNCTION	0.00	23.95	0 00:45	0
65	0.000	JUNCTION	0.00	23.95	0 00:45	0
5.22	0.000	JUNCTION	0.00	23.95	0 00:45	0
66	0.000	JUNCTION	0.00	23.95	0 00:45	0
3.87	0.000	JUNCTION	0.00	23.95	0 00:45	0
70	0.000	JUNCTION	0.00	23.95	0 00:45	0
1.05	0.000	JUNCTION	0.00	23.95	0 00:45	0
71	0.000	JUNCTION	0.00	23.95	0 00:45	0
0.742	0.000	JUNCTION	0.00	23.95	0 00:45	0
72	0.000	JUNCTION	0.00	23.95	0 00:45	0
0.742	0.000	JUNCTION	0.00	23.95	0 00:45	0
73	0.000	JUNCTION	0.00	23.95	0 00:45	0
0.742	0.000	JUNCTION	0.00	23.95	0 00:45	0
74	-0.000	JUNCTION	0.00	42.13	0 01:12	0
1.79	-0.000					

			SWMM 100 Year Output				
80		JUNCTION	27.62	27.62	0	00:45	0.833
0.833	0.000	JUNCTION	47.62	47.62	0	00:35	1.01
81		JUNCTION	15.60	15.60	0	00:35	0.314
1.01	0.000	JUNCTION	64.71	64.71	0	00:35	1.46
82		JUNCTION	0.00	73.73	0	00:40	0
0.314	0.000	JUNCTION	0.00	15.60	0	00:35	0
83		JUNCTION	0.00	256.11	0	01:16	0
1.46	0.000	OUTFALL	0.00	53.95	0	01:13	0
84		OUTFALL	0.00	478.86	0	01:05	0
1.84	0.000	OUTFALL	0.00	160.70	0	01:04	0
85		OUTFALL	0.00	447.00	0	00:49	0
0.314	0.000	STORAGE	0.00	238.03	0	00:35	0
Outfall2		STORAGE	0.00	100.64	0	00:40	0
10.3	0.000	STORAGE	0.00	320.21	0	00:35	0
Outfall1		STORAGE	0.00	178.04	0	00:40	0
2.03	0.000	STORAGE	0.00	385.87	0	00:41	0
Outfall4		STORAGE	0.00	67.73	0	00:40	0
16.7	0.000	STORAGE	0.00	153.03	0	00:38	0
Outfall3		STORAGE	0.00	153.03	0	00:38	0
5.21	0.000	PondB					
12.4	0.062	PondC					
4	0.130	PondA					
2.37	0.096	PondD					
6.05	0.105	PondE					
4.2	0.178	PondF					
9.08	0.109	PondG					
1.8	0.079	PondH					
3.61	0.143						

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

SWMM 100 Year Output

of Occurrence	Max Storage hr:min	Maximum Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB		363.135	43	0	0		827.701	97	0
01:15	256.11								
PondC		146.763	26	0	0		299.338	52	0
00:58	115.75								
PondA		75.030	37	0	0		152.554	76	0
01:12	53.95								
PondD		192.591	31	0	0		418.291	67	0
01:04	160.70								
PondE		48.028	17	0	0		106.230	37	0
00:48	164.75								
PondF		250.108	31	0	0		549.589	67	0
01:09	229.20								
PondG		5.811	1	0	0		88.594	16	0
01:11	42.13								
PondH		131.315	21	0	0		268.983	42	0
01:12	80.17								

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall12	99.64	12.77	256.11	10.280
Outfall11	99.69	2.53	53.95	2.035
Outfall14	99.67	20.76	478.86	16.717
Outfall13	99.69	6.47	160.70	5.209
System	99.67	42.53	924.48	34.241

SWMM 100 Year Output

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	100.64	0 00:40			
200	DUMMY	97.08	0 00:35			
201	DUMMY	42.26	0 00:40			
202	CONDUIT	136.36	0 00:36	26.17	0.08	0.19
203	CONDUIT	115.74	0 00:59	23.03	0.37	0.42
204	DUMMY	295.27	0 00:40			
205	CONDUIT	334.86	0 00:51	31.89	0.22	0.32
300	DUMMY	238.03	0 00:35			
400	DUMMY	70.07	0 00:35			
401	CONDUIT	69.37	0 00:36	15.63	0.17	0.28
402	DUMMY	252.18	0 00:35			
500	DUMMY	178.04	0 00:40			
601	DUMMY	170.90	0 00:40			
602	CONDUIT	170.58	0 00:41	13.26	0.71	0.62
603	DUMMY	58.95	0 00:40			
604	DUMMY	32.93	0 00:35			
605	CONDUIT	90.74	0 00:41	20.83	0.06	0.17
606	DUMMY	124.89	0 00:40			
607	CONDUIT	215.42	0 00:40	23.26	0.13	0.24
700	DUMMY	43.95	0 00:40			
701	DUMMY	23.95	0 00:45			
702	DUMMY	23.95	0 00:45			
703	CONDUIT	23.94	0 00:45	8.29	0.09	0.20
801	DUMMY	27.62	0 00:45			
802	DUMMY	47.62	0 00:35			
803	CONDUIT	73.66	0 00:40	12.80	0.09	0.21
804	DUMMY	15.60	0 00:35			
806	DUMMY	64.71	0 00:35			
805	CONDUIT	15.43	0 00:37	7.47	0.06	0.16
808	CONDUIT	270.40	0 01:13	4.87	0.04	0.23
800	CONDUIT	41.98	0 01:17	4.06	0.00	0.06
600	CONDUIT	164.38	0 00:51	12.48	0.01	0.09
101	DUMMY	53.95	0 01:13			
206	DUMMY	256.11	0 01:16			
301	DUMMY	115.75	0 00:59			
501	DUMMY	164.75	0 00:49			
704	DUMMY	42.13	0 01:12			
807	DUMMY	80.17	0 01:12			
608	DUMMY	229.20	0 01:09			

403 SWMM 100 Year Output
DUMMY 160.70 0 01:04

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Mon Apr 13 19:00:38 2020
Analysis ended on: Mon Apr 13 19:00:38 2020
Total elapsed time: < 1 sec

Appendix D

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type: Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.	Extended Detention Basin (EDB) <input type="button" value="▼"/>																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
2. WQCV/EURV Outlet Details A) Average Infiltration Rate of WQCV B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface C) Underdrain Outlet Orifice Area D) Number of WQCV Orifice Rows E) Vertical Spacing between WQCV Orifice Rows F) WQCV Orifice Area (A_o) per Row G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth) H) EURV Orifice Area (A_o) in Single Row I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth) J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)	<table border="1"> <thead> <tr> <th colspan="2">Input Parameters</th> </tr> <tr> <th>User Input</th> <th>COS DCM</th> </tr> </thead> <tbody> <tr> <td>i = N/A</td> <td>N/A in / hr</td> </tr> <tr> <td>y₁ = N/A</td> <td>N/A inches</td> </tr> <tr> <td>y₂ = N/A</td> <td>N/A sq in</td> </tr> <tr> <td>Underdrain Ao = 10</td> <td>10 ft</td> </tr> <tr> <td># WQCV rows = 4.0</td> <td>4.0 inches</td> </tr> <tr> <td>Orifice Spacing = 0.61</td> <td>0.61 sq in</td> </tr> <tr> <td>WQCV Ao = 3.40</td> <td>3.40 ft</td> </tr> <tr> <td>Max Stage wqcv = 2.96</td> <td>2.96 sq in</td> </tr> <tr> <td>EURV Ao = 4.50</td> <td>4.50 ft</td> </tr> <tr> <td>Max Stage eurv = 0.60</td> <td>0.60</td> </tr> <tr> <td>Cd = 0.60</td> <td>0.60</td> </tr> </tbody> </table>	Input Parameters		User Input	COS DCM	i = N/A	N/A in / hr	y ₁ = N/A	N/A inches	y ₂ = N/A	N/A sq in	Underdrain Ao = 10	10 ft	# WQCV rows = 4.0	4.0 inches	Orifice Spacing = 0.61	0.61 sq in	WQCV Ao = 3.40	3.40 ft	Max Stage wqcv = 2.96	2.96 sq in	EURV Ao = 4.50	4.50 ft	Max Stage eurv = 0.60	0.60	Cd = 0.60	0.60																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench. A) Length of Basin at Top of EURV B) Width of Basin at Top of EURV C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge) D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge) E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge) F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)	<table border="1"> <thead> <tr> <th colspan="2">Input Parameters</th> </tr> <tr> <th>User Input</th> <th>COS DCM</th> </tr> </thead> <tbody> <tr> <td>L_{PCM} = 370.3</td> <td>370.3 ft</td> </tr> <tr> <td>W_{PCM} = 113.6</td> <td>113.6 ft</td> </tr> <tr> <td>Stage at Top of Bench = 4.60</td> <td>4.60 ft</td> </tr> <tr> <td>L_{Bench} = 371.1</td> <td>371.1 ft</td> </tr> <tr> <td>W_{Bench} = 114.4</td> <td>114.4 ft</td> </tr> <tr> <td>Z_{Surcharge} = 4.00</td> <td>4.00 ft / ft</td> </tr> </tbody> </table> <p>User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.</p> <p>Bench Slope is 4H:1V in length direction Bench Slope is 4H:1V in width direction</p>	Input Parameters		User Input	COS DCM	L _{PCM} = 370.3	370.3 ft	W _{PCM} = 113.6	113.6 ft	Stage at Top of Bench = 4.60	4.60 ft	L _{Bench} = 371.1	371.1 ft	W _{Bench} = 114.4	114.4 ft	Z _{Surcharge} = 4.00	4.00 ft / ft																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
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Tributary Watershed Hydrology A) Input hydrology data (copy/paste) from model runs B) Adjust "Time Interval" to match hydrograph data 5-yr and 100-yr Hydrology Required (Other Storms are Optional)	<table border="1"> <thead> <tr> <th colspan="7">Pre-Development Peak Flow (cfs)</th> </tr> <tr> <th></th> <th>2 Year</th> <th>5 Year</th> <th>10 Year</th> <th>25 Year</th> <th>50 Year</th> <th>100 Year</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>13.03</td> <td></td> <td></td> <td></td> <td>57.08</td> </tr> </tbody> </table> <p>Time Interval 5.0 minutes</p> <table border="1"> <thead> <tr> <th colspan="7">Post-Development Storm Inflow Hydrographs (cfs)</th> </tr> <tr> <th>Time (min)</th> <th>2 Year</th> <th>5 Year</th> <th>10 Year</th> <th>25 Year</th> <th>50 Year</th> <th>100 Year</th> </tr> </thead> <tbody> <tr><td>0:00</td><td>0.00</td><td></td><td></td><td></td><td>0.00</td><td></td></tr> <tr><td>0:05</td><td>0.32</td><td></td><td></td><td></td><td>0.84</td><td></td></tr> 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Year	0:00	0.00				0.00		0:05	0.32				0.84		0:10	2.12				2.93		0:15	6.24				8.14		0:20	19.45				26.66		0:25	29.43				70.19		0:30	30.68				95.65		0:35	28.10				100.37		0:40	24.84				96.25		0:45	22.05				89.32		0:50	19.61				81.43		0:55	17.40				74.41		1:00	15.33				68.04		1:05	13.43				58.60		1:10	11.93				49.54		1:15	10.74				42.06		1:20	9.68				35.93		1:25	8.69				30.71		1:30	7.74				26.07		1:35	6.69				21.81		1:40	5.63				17.82		1:45	4.64				14.14		1:50	3.79				10.94		1:55	3.24				8.55		2:00	2.68				6.51		2:05	2.16				4.89		2:10	1.73				3.64		2:15	1.39				2.70		2:20	1.11				1.98		2:25	0.88				1.45		2:30	0.68				1.07		2:35	0.53				0.82		2:40	0.41				0.64		2:45	0.32				0.50		2:50	0.24				0.39		2:55	0.17				0.29		3:00	0.12				0.20		3:05	0.08				0.13		3:10	0.05				0.07		3:15	0.02				0.03		3:20	0.01				0.01		3:25	0.00				0.00		3:30							3:35							3:40							3:45							3:50							3:55							4:00							4:05							4:10							4:15							4:20							4:25							4:30							4:35							4:40							4:45							4:50							4:55							5:00							5:05							5:10							5:15							5:20							5:25							5:30							5:35						
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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

Last Edited: April 13, 2020

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters	
User Input	COS DCM
H _{weir front} =	4.50 ft
L _{weir front} =	8.00 9.00 ft
S _{weir sides} =	0.00 ft / ft
Horizontal L _{weir sides} =	8.00 5.00 ft
Grate Open Area =	70% 70% %
Debris Clogging =	50% 50% %
H _{grate top} =	4.50 4.50 ft
Slope L _{weir sides} =	8.00 5.00 ft
Open Area (No Clogging) =	44.80 31.50 sq ft
Open Area (clogged) =	22.40 15.75 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters	
User Input	COS DCM
Pipe Invert Depth =	1.50 ft
Pipe Diameter =	36.00 inches
Plate Height =	22.42 28.11 inches
Theta =	1.82 2.63 radians
Outlet Ao =	4.63 4.78 sq ft
Outlet centroid =	1.06 1.22 ft
Open Area Ratio =	9.68 6.59

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters	
User Input	COS DCM
H _{spillway invert} =	5.90 ft
L _{spillway crest} =	42.00 33.00 ft
S _{spillway ends} =	4.00 4.00 ft / ft
Freeboard Depth =	1.00 1.00 ft
Flow Depth _{spillway} =	0.80 1.00 ft
Freeboard Top Stage =	7.70 8.00 ft
Max Basin Area =	1.27 1.29 acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.64	1.66	2.16				7.27	
Predevelopment Peak Q (cfs) =	N/A	N/A	13.0				57.1	
Peak Inflow (cfs) =	N/A	N/A	30.7				100.4	
Peak Outflow (cfs) =	0.3	0.5	4.6				56.3	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.4				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.1				1.2	
Time to Drain 97% of Volume (hr) =	39	69	73				61	
Time to Drain 99% of Volume (hr) =	41	72	77				72	
Maximum Ponding Depth (ft) =	3.40	4.50	4.70				5.90	
Area at Max Ponding Depth (ac) =	0.80	0.97	0.98				1.09	
Maximum Volume Stored (ac-ft) =	0.64	1.66	1.87				3.11	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.64	1.66	2.16				7.27	
Predevelopment Peak Q (cfs) =	N/A	N/A	13.0				57.1	
Peak Inflow (cfs) =	N/A	N/A	30.7				100.4	
Peak Outflow (cfs) =	0.3	0.5	4.3				57.5	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.3				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.2				1.8	
Time to Drain 97% of Volume (hr) =	39	69	73				61	
Time to Drain 99% of Volume (hr) =	41	72	77				72	
Maximum Ponding Depth (ft) =	3.40	4.50	4.70				5.90	
Area at Max Ponding Depth (ac) =	0.80	0.97	0.98				1.09	
Maximum Volume Stored (ac-ft) =	0.64	1.66	1.87				3.11	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

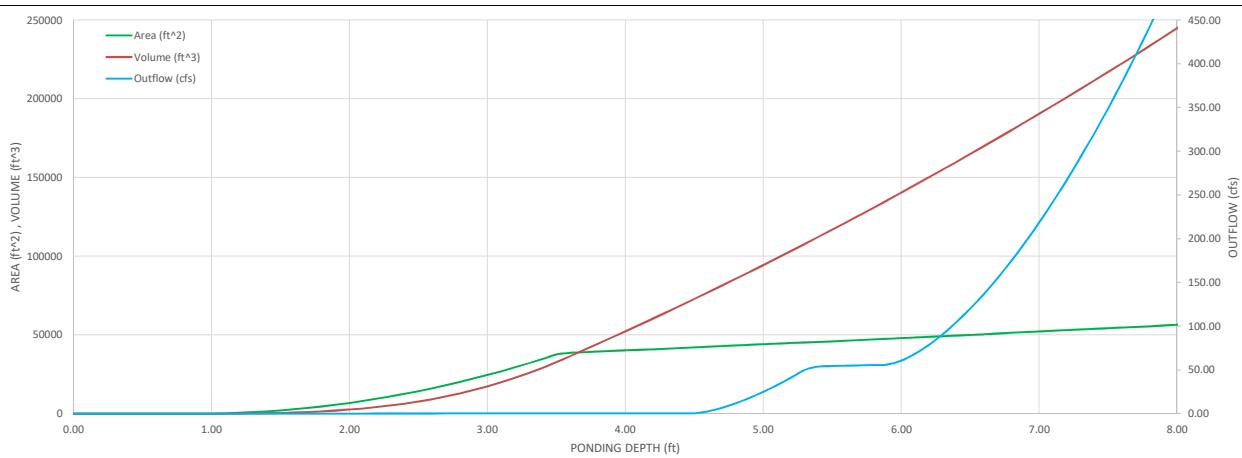
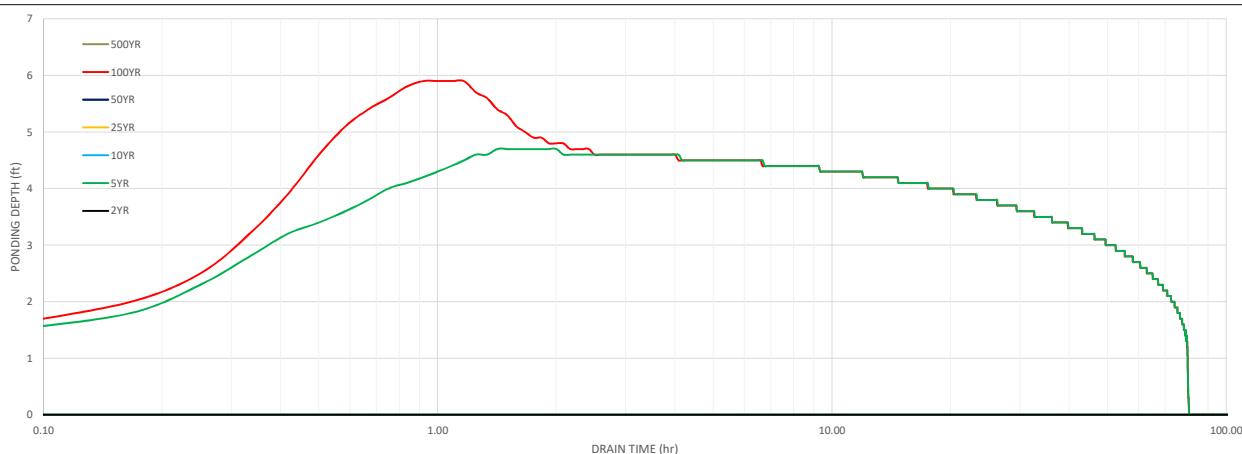
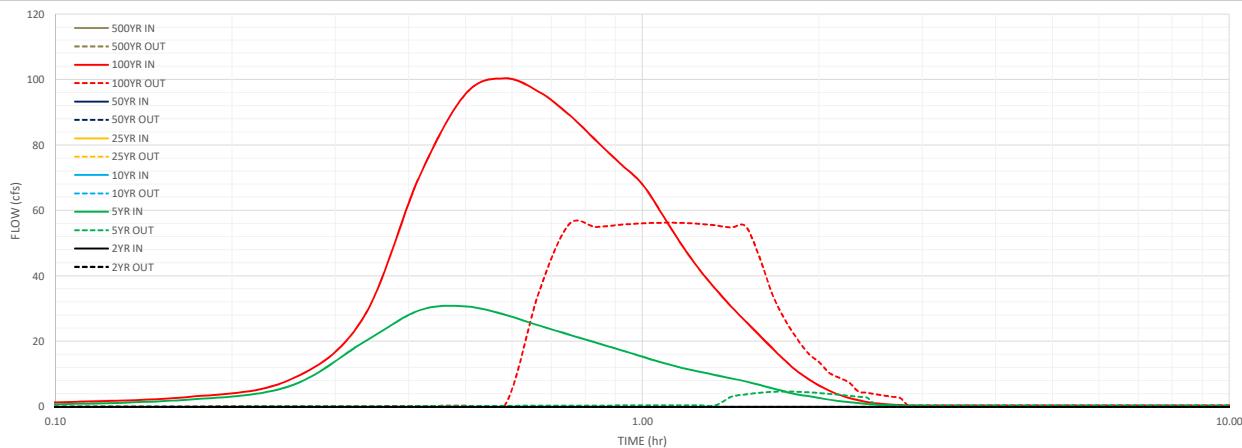


Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

Last Edited: April 13, 2020



Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
C) Underdrain Outlet Orifice Area
D) Number of WQCV Orifice Rows
E) Vertical Spacing between WQCV Orifice Rows
F) WQCV Orifice Area (A_o) per Row
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
H) EURV Orifice Area (A_o) in Single Row
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	i = N/A in / hr
y ₁ = N/A	y ₁ = N/A inches
y ₂ = N/A	y ₂ = N/A sq in
Underdrain Ao = 14	Underdrain Ao = 14 sq in
# WQCV rows = 4.0	Orifice Spacing = 4.0 inches
WQCV Ao = 1.49	WQCV Ao = 1.49 sq in
Max Stage wqcv = 4.70	Max Stage wqcv = 4.70 ft
EURV Ao = 1.49	EURV Ao = 1.49 sq in
Max Stage eurv = 6.00	Max Stage eurv = 6.00 ft
Cd = 0.60	Cd = 0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
B) Width of Basin at Top of EURV
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 644.7	L PCM = 644.7 ft
W PCM = 191.2	W PCM = 191.2 ft
Stage at Top of Bench = 6.10	L Bench = 6.10 ft
Z Surcharge = 4.00	W Bench = 645.5 ft
	Z Surcharge = 4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

- A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
17.56					164.21	

- B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	Post-Development Storm Inflow Hydrographs (cfs)					
(min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0:00	0.00				0.00	
0:05	0.69				2.08	
0:10	5.80				8.30	
0:15	16.64				20.58	
0:20	42.42				58.80	
0:25	68.16				179.82	
0:30	75.65				276.49	
0:35	71.78				307.62	
0:40	64.91				331.81	
0:45	58.24				366.22	
0:50	52.24				365.58	
0:55	47.02				346.26	
1:00	42.99				321.76	
1:05	39.68				290.00	
1:10	36.25				252.97	
1:15	32.60				216.52	
1:20	29.09				182.15	
1:25	26.07				152.09	
1:30	23.97				127.70	
1:35	22.28				109.78	
1:40	20.74				96.42	
1:45	19.35				85.46	
1:50	18.07				76.27	
1:55	16.77				68.63	
2:00	14.81				60.20	
2:05	12.66				51.42	
2:10	10.67				42.95	
2:15	8.88				35.32	
2:20	7.28				28.18	
2:25	5.90				21.64	
2:30	4.82				15.96	
2:35	4.08				11.69	
2:40	3.58				9.39	
2:45	3.19				7.53	
2:50	2.86				6.09	
2:55	2.60				4.98	
3:00	2.39				4.12	
3:05	2.22				3.47	
3:10	2.09				2.97	
3:15	1.97				2.55	
3:20	1.86				2.21	
3:25	1.77				2.08	
3:30	1.70				1.98	
3:35	1.63				1.88	
3:40	1.58				1.81	
3:45	1.54				1.75	
3:50	1.51				1.70	
3:55	1.49				1.67	
4:00	1.47				1.65	
4:05	1.46				1.64	
4:10	1.46				1.64	
4:15	1.46				1.64	
4:20	1.46				1.64	
4:25	1.45				1.64	
4:30	1.45				1.63	
4:35	1.45				1.63	
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4:45	1.45				1.63	
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5:25	1.43				1.61	
5:30	1.43				1.61	
5:35	1.43				1.61	

5:40		1.42			1.61	
5:45		1.42			1.61	
5:50		1.42			1.60	
5:55		1.42			1.60	
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

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5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
H _{weir front} =	6.00	5.00 ft
L _{weir front} =	17.00	17.00 ft
S _{weir sides} =	0.00	0.00 ft / ft
Horizontal L _{weir sides} =	17.00	7.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	6.00	6.00 ft
Slope L _{weir sides} =	17.00	7.00 ft
Open Area (No Clogging) =	202.30	83.30 sq ft
Open Area (clogged) =	101.15	41.65 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	54.00	48.00 inches
Plate Height =	37.00	42.00 inches
Theta =	1.95	2.42 radians
Outlet Ao =	11.61	11.66 sq ft
Outlet centroid =	1.73	1.87 ft
Open Area Ratio =	17.42	7.14

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
H _{spillway invert} =	9.50	9.30 ft
L _{spillway crest} =	136.00	122.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	0.90	1.00 ft
Freeboard Top Stage =	11.40	11.30 ft
Max Basin Area =	3.70	3.68 acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73	6.67				31.72	
Predevelopment Peak Q (cfs) =	N/A	N/A	17.6				164.2	
Peak Inflow (cfs) =	N/A	N/A	75.7				366.2	
Peak Outflow (cfs) =	1.1	1.4	1.4				166.4	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.0				0.8	
Time to Drain 97% of Volume (hr) =	40	68	76				61	
Time to Drain 99% of Volume (hr) =	42	72	80				73	
Maximum Ponding Depth (ft) =	4.70	6.00	6.10				9.10	
Area at Max Ponding Depth (ac) =	1.92	2.83	2.85				3.32	
Maximum Volume Stored (ac-ft) =	2.41	5.73	6.04				15.28	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73	6.67				31.72	
Predevelopment Peak Q (cfs) =	N/A	N/A	17.6				164.2	
Peak Inflow (cfs) =	N/A	N/A	75.7				366.2	
Peak Outflow (cfs) =	1.1	1.4	1.4				166.5	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.0				2.0	
Time to Drain 97% of Volume (hr) =	40	68	76				61	
Time to Drain 99% of Volume (hr) =	42	72	80				73	
Maximum Ponding Depth (ft) =	4.70	6.00	6.10				9.20	
Area at Max Ponding Depth (ac) =	1.92	2.83	2.85				3.34	
Maximum Volume Stored (ac-ft) =	2.41	5.73	6.04				15.62	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

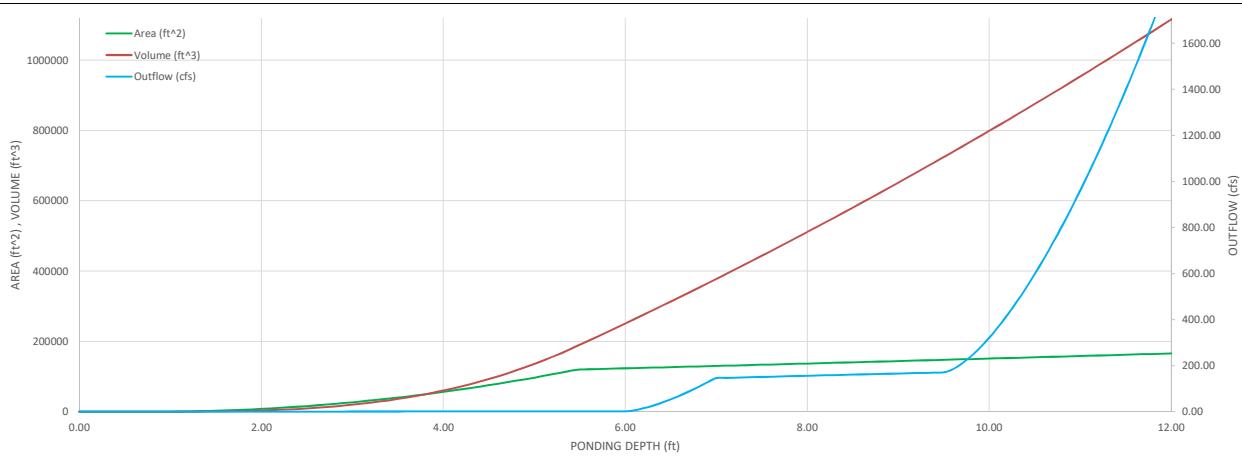
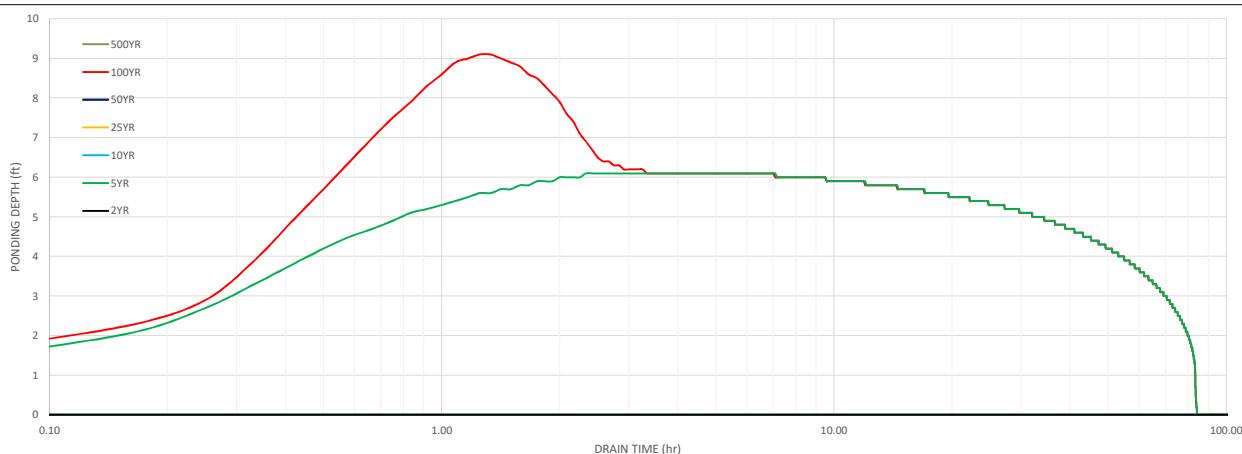
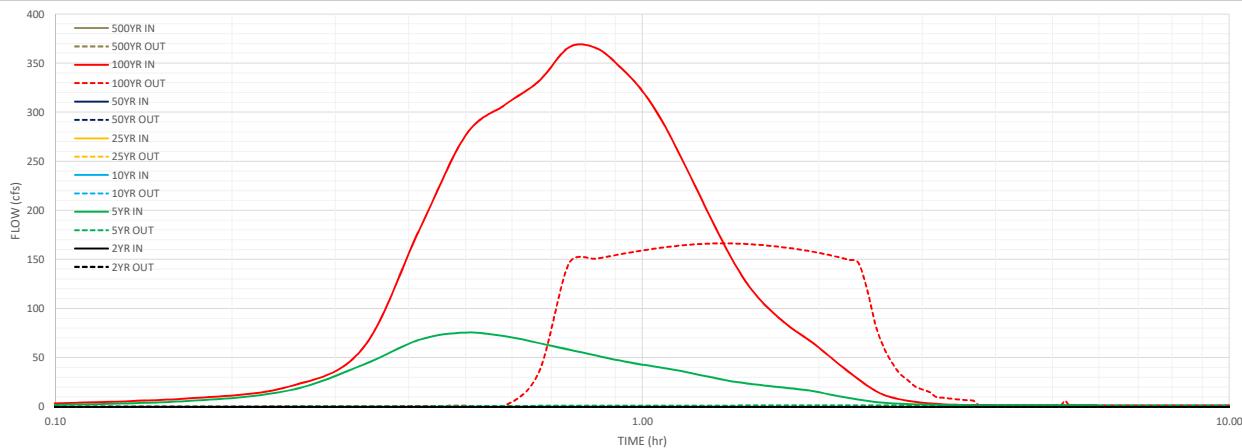


Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond C

Date: April 6, 2020

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1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A_o) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A_o) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	i = N/A in / hr
y = N/A	y = N/A inches
Underdrain Ao = N/A	Underdrain Ao = N/A sq in
# WQCV rows = 12	# WQCV rows = 12
Orifice Spacing = 4.0	Orifice Spacing = 4.0 inches
WQCV Ao = 1.05	WQCV Ao = 1.05 sq in
Max Stage wqcv = 4.00	Max Stage wqcv = 4.00 ft
EURV Ao = 17.07	EURV Ao = 17.07 sq in
Max Stage eurv = 6.00	Max Stage eurv = 6.00 ft
Cd = 0.60	Cd = 0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 453.3	L PCM = 453.3 ft
W PCM = 177.8	W PCM = 177.8 ft
Stage at Top of Bench = 6.10	Stage at Top of Bench = 6.10 ft
L Bench = 454.1	L Bench = 454.1 ft
W Bench = 178.6	W Bench = 178.6 ft
Z Surcharge = 4.00	Z Surcharge = 4.00 ft / ft

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

- A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	9.95				120.21	

- B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	5.0 minutes	Post-Development Storm Inflow Hydrographs (cfs)					
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00	0.00				0.00		
0:05		1.75				4.56	
0:10		11.33				15.20	
0:15		27.93				32.42	
0:20		61.14				76.70	
0:25		78.99				190.43	
0:30		71.29				238.04	
0:35		58.22				222.59	
0:40		47.28				193.29	
0:45		38.58				162.70	
0:50		32.22				131.89	
0:55		27.64				110.47	
1:00		23.60				95.05	
1:05		20.00				74.37	
1:10		16.49				54.92	
1:15		14.05				38.35	
1:20		12.80				27.93	
1:25		12.09				21.76	
1:30		11.62				18.07	
1:35		10.55				15.64	
1:40		9.56				14.06	
1:45		8.84				12.98	
1:50		8.33				12.35	
1:55		7.74				12.15	
2:00		5.88				9.32	
2:05		4.08				6.49	
2:10		2.79				4.48	
2:15		1.86				3.04	
2:20		1.21				1.99	
2:25		0.80				1.32	
2:30		0.49				0.80	
2:35		0.25				0.40	
2:40		0.09				0.14	
2:45		0.01				0.01	
2:50		0.00				0.00	
2:55							
3:00							
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5:35							

5:40						
5:45						
5:50						
5:55						
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond C

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Last Edited: April 08, 2020

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
H _{weir front} =	6.00	5.00 ft
L _{weir front} =	12.00	11.00 ft
S _{weir sides} =	0.00	0.00 ft / ft
Horizontal L _{weir sides} =	12.00	11.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	6.00	6.00 ft
Slope L _{weir sides} =	12.00	11.00 ft
Open Area (No Clogging) =	100.80	84.70 sq ft
Open Area (clogged) =	50.40	42.35 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	48.00	42.00 inches
Plate Height =	33.13	39.36 inches
Theta =	1.96	2.63 radians
Outlet Ao =	9.25	9.37 sq ft
Outlet _{centroid} =	1.54	1.71 ft
Open Area Ratio =	10.90	9.04

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
H _{spillway invert} =	8.00	999.00 ft
L _{spillway crest} =	79.00	42.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	1.00	1.00 ft
Freeboard Top Stage =	10.00	ft
Max Basin Area =	2.34	acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79	4.34				12.42	
Predevelopment Peak Q (cfs) =	N/A	N/A	10.0				120.2	
Peak Inflow (cfs) =	N/A	N/A	79.0				238.0	
Peak Outflow (cfs) =	0.6	1.7	1.5				119.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Orifice Plate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	N/A				1.2	
Time to Drain 97% of Volume (hr) =	39	67	65				63	
Time to Drain 99% of Volume (hr) =	41	72	69				72	
Maximum Ponding Depth (ft) =	4.00	6.00	5.60				7.10	
Area at Max Ponding Depth (ac) =	1.32	1.85	1.80				1.98	
Maximum Volume Stored (ac-ft) =	1.36	4.79	4.07				6.91	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79	4.34				12.42	
Predevelopment Peak Q (cfs) =	N/A	N/A	10.0				120.2	
Peak Inflow (cfs) =	N/A	N/A	79.0				238.0	
Peak Outflow (cfs) =	0.6	1.7	1.5				116.8	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Orifice Plate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A	N/A				1.3	
Time to Drain 97% of Volume (hr) =	39	67	65				63	
Time to Drain 99% of Volume (hr) =	41	72	69				72	
Maximum Ponding Depth (ft) =	4.00	6.00	5.60				7.10	
Area at Max Ponding Depth (ac) =	1.32	1.85	1.80				1.98	
Maximum Volume Stored (ac-ft) =	1.36	4.79	4.07				6.91	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

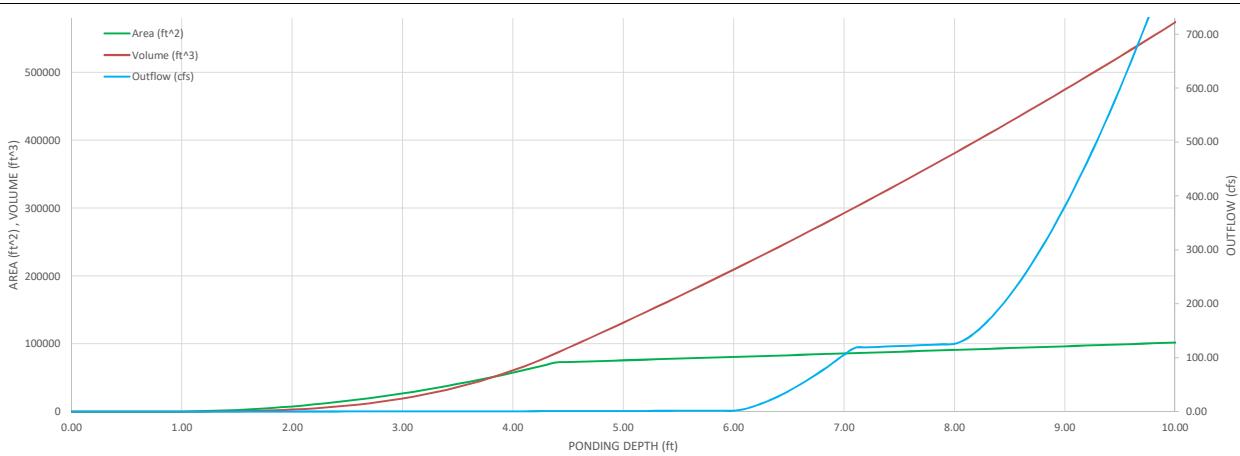
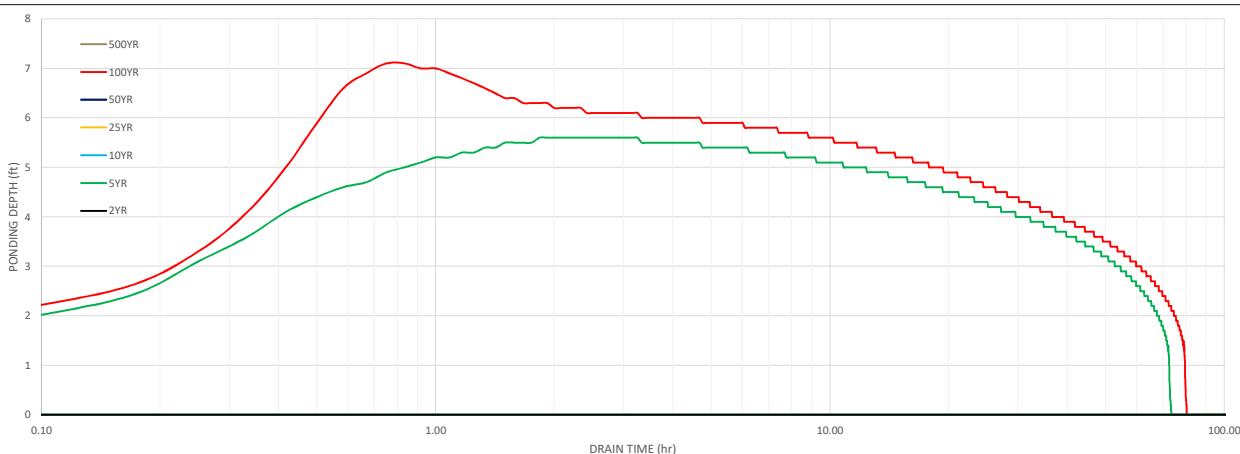
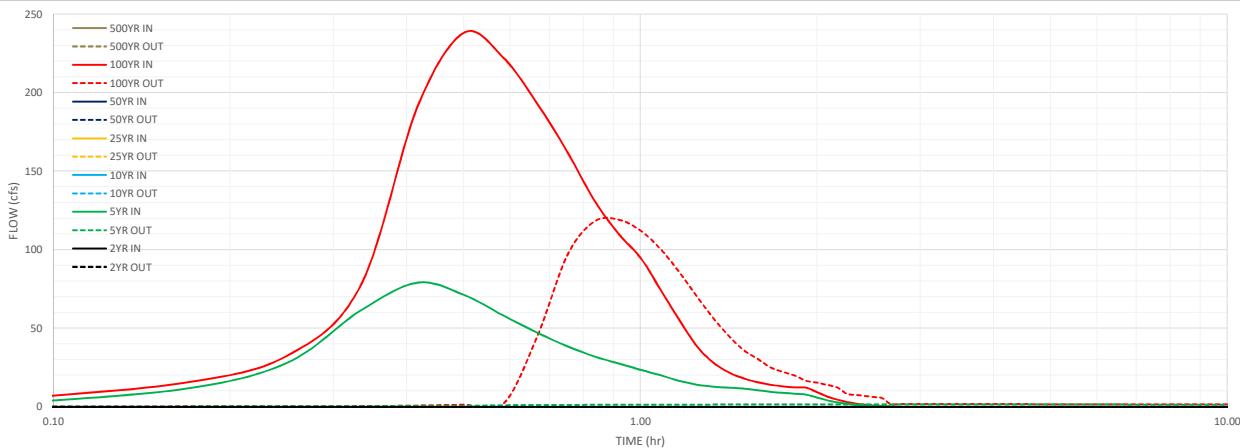


Designer: Chris McFarland

Project: Grandview Reserve Pond C

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond D

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details
A) Average Infiltration Rate of WQCV
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
C) Underdrain Outlet Orifice Area
D) Number of WQCV Orifice Rows
E) Vertical Spacing between WQCV Orifice Rows
F) WQCV Orifice Area (A_o) per Row
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
H) EURV Orifice Area (A_o) in Single Row
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	i = N/A in / hr
y = N/A	y = N/A inches
Underdrain Ao = N/A	Underdrain Ao = N/A sq in
# WQCV rows = 13	# WQCV rows = 13
Orifice Spacing = 4.0	Orifice Spacing = 4.0 inches
WQCV Ao = 1.34	WQCV Ao = 1.34 sq in
Max Stage wqcv = 4.50	Max Stage wqcv = 4.50 ft
EURV Ao = 20.83	EURV Ao = 20.83 sq in
Max Stage eurv = 6.50	Max Stage eurv = 6.50 ft
Cd = 0.60	Cd = 0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.
A) Length of Basin at Top of EURV
B) Width of Basin at Top of EURV
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 588.5	L PCM = 588.5 ft
W PCM = 180.1	W PCM = 180.1 ft
Stage at Top of Bench = 6.60	Stage at Top of Bench = 6.60 ft
L Bench = 589.3	L Bench = 589.3 ft
W Bench = 180.9	W Bench = 180.9 ft
Z Surcharge = 4.00	Z Surcharge = 4.00 ft / ft

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
30.00					154.35	

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	Post-Development Storm Inflow Hydrographs (cfs)					
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0:00	0.00				0.00	
0:05		1.91				5.05
0:10		13.55				18.88
0:15		36.44				44.44
0:20		87.25				108.47
0:25		118.48				244.10
0:30		113.01				314.40
0:35		95.70				305.49
0:40		80.03				273.09
0:45		67.12				239.63
0:50		56.09				204.40
0:55		48.05				175.96
1:00		41.91				156.02
1:05		36.47				129.55
1:10		30.68				102.47
1:15		25.11				77.55
1:20		21.41				56.75
1:25		19.34				42.46
1:30		18.14				33.79
1:35		16.52				28.16
1:40		14.92				24.40
1:45		13.77				21.80
1:50		12.92				19.98
1:55		12.02				18.83
2:00		9.58				15.10
2:05		6.95				10.86
2:10		4.98				7.82
2:15		3.53				5.61
2:20		2.44				3.93
2:25		1.66				2.73
2:30		1.13				1.86
2:35		0.72				1.18
2:40		0.41				0.67
2:45		0.20				0.31
2:50		0.08				0.11
2:55		0.04				0.05
3:00		0.02				0.02
3:05		0.01				0.01
3:10		0.01				0.01
3:15		0.00				0.00
3:20						0.00
3:25						
3:30						
3:35						
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5:40						
5:45						
5:50						
5:55						
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond D

Date: April 6, 2020

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5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS	DCM
H _{weir front} =	6.50	6.50 ft
L _{weir front} =	11.00	9.00 ft
S _{weir sides} =	0.00	ft / ft
Horizontal L _{weir sides} =	11.00	9.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	6.50	6.50 ft
Slope L _{weir sides} =	11.00	9.00 ft
Open Area (No Clogging) =	84.70	56.70 sq ft
Open Area (clogged) =	42.35	28.35 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS	DCM
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	48.00	48.00 inches
Plate Height =	44.00	44.00 inches
Theta =	2.56	2.56 radians
Outlet Ao =	12.07	12.07 sq ft
Outlet centroid =	1.93	1.93 ft
Open Area Ratio =	7.02	4.70

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS	DCM
H _{spillway invert} =	8.00	999.00 ft
L _{spillway crest} =	105.00	42.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	1.00	1.00 ft
Freeboard Top Stage =	10.00	ft
Max Basin Area =	2.95	acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.96	6.56	6.97				18.57	
Predevelopment Peak Q (cfs) =	N/A	N/A	30.0				154.4	
Peak Inflow (cfs) =	N/A	N/A	118.5				314.4	
Peak Outflow (cfs) =	0.9	2.2	2.2				161.7	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Orifice Plate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	N/A				1.8	
Time to Drain 97% of Volume (hr) =	40	67	70				62	
Time to Drain 99% of Volume (hr) =	42	72	75				72	
Maximum Ponding Depth (ft) =	4.50	6.50	6.50				7.90	
Area at Max Ponding Depth (ac) =	1.71	2.43	2.43				2.63	
Maximum Volume Stored (ac-ft) =	1.96	6.56	6.59				10.13	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.96	6.56	6.97				18.57	
Predevelopment Peak Q (cfs) =	N/A	N/A	30.0				154.4	
Peak Inflow (cfs) =	N/A	N/A	118.5				314.4	
Peak Outflow (cfs) =	0.8	2.2	2.2				153.1	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Orifice Plate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A	N/A				2.8	
Time to Drain 97% of Volume (hr) =	40	67	70				63	
Time to Drain 99% of Volume (hr) =	42	72	75				72	
Maximum Ponding Depth (ft) =	4.50	6.50	6.50				8.10	
Area at Max Ponding Depth (ac) =	1.71	2.43	2.43				2.66	
Maximum Volume Stored (ac-ft) =	1.96	6.56	6.59				10.66	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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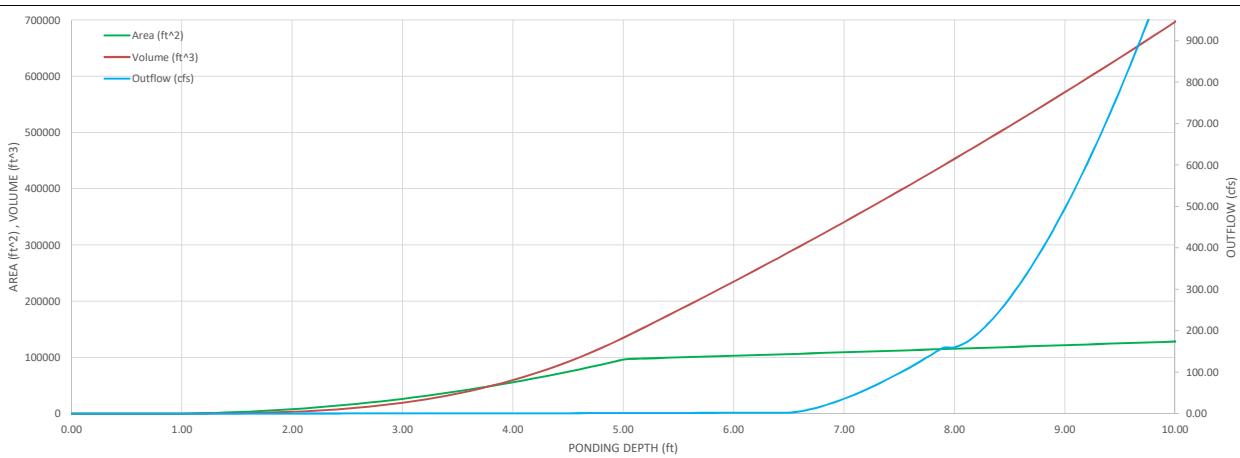
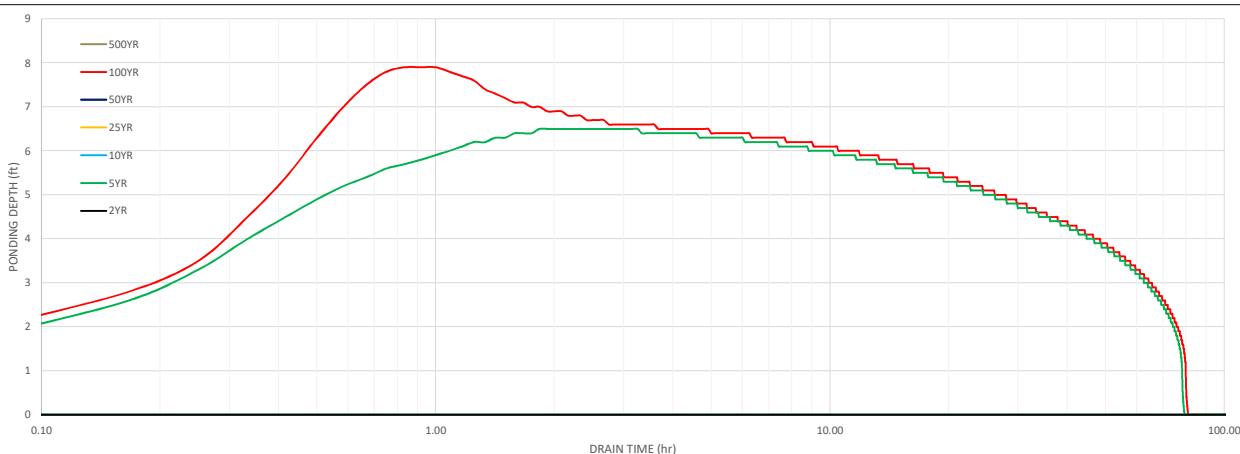
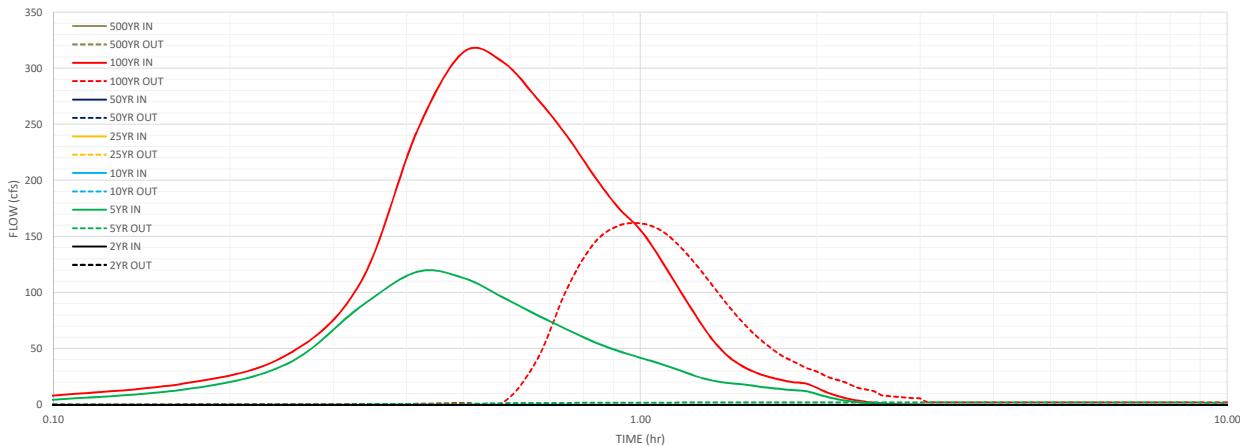


Designer: Chris McFarland

Project: Grandview Reserve Pond D

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond E

Date: April 6, 2020

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1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
C) Underdrain Outlet Orifice Area
D) Number of WQCV Orifice Rows
E) Vertical Spacing between WQCV Orifice Rows
F) WQCV Orifice Area (A_o) per Row
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
H) EURV Orifice Area (A_o) in Single Row
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	i = N/A in / hr
y ₁ = N/A	y ₁ = N/A inches
y ₂ = N/A	y ₂ = N/A sq in
Underdrain Ao = 10	Underdrain Ao = 10 sq in
# WQCV rows = 4.0	Orifice Spacing = 4.0 inches
WQCV Ao = 0.67	WQCV Ao = 0.67 sq in
Max Stage wqcv = 3.60	Max Stage wqcv = 3.60 ft
EURV Ao = 0.67	EURV Ao = 0.67 sq in
Max Stage eurv = 4.50	Max Stage eurv = 4.50 ft
Cd = 0.60	Cd = 0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
B) Width of Basin at Top of EURV
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 327.0	L PCM = 327.0 ft
W PCM = 127.7	W PCM = 127.7 ft
Stage at Top of Bench = 4.60	L Bench = 4.60 ft
Z Surcharge = 4.00	W Bench = 327.8 ft
	Z Surcharge = 4.00 ft / ft

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

- A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
32.34					157.99	

- B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	Post-Development Storm Inflow Hydrographs (cfs)					
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0:00	0.00				0.00	
0:05		0.16				0.43
0:10		1.11				1.54
0:15		5.07				7.00
0:20		23.64				35.29
0:25		41.87				110.52
0:30		46.56				162.17
0:35		43.13				176.94
0:40		37.83				172.03
0:45		33.03				161.08
0:50		29.04				147.26
0:55		25.75				135.35
1:00		22.65				124.96
1:05		19.67				109.31
1:10		16.82				92.46
1:15		14.63				77.36
1:20		13.01				65.86
1:25		11.61				56.57
1:30		10.30				48.68
1:35		8.90				41.54
1:40		7.47				34.92
1:45		6.08				28.67
1:50		4.75				22.81
1:55		3.50				17.32
2:00		2.49				12.10
2:05		1.86				8.45
2:10		1.45				6.02
2:15		1.16				4.29
2:20		0.92				3.03
2:25		0.73				2.11
2:30		0.57				1.42
2:35		0.44				0.96
2:40		0.34				0.71
2:45		0.26				0.55
2:50		0.20				0.44
2:55		0.15				0.34
3:00		0.11				0.26
3:05		0.07				0.19
3:10		0.05				0.13
3:15		0.03				0.08
3:20		0.02				0.04
3:25		0.01				0.02
3:30		0.00				0.00
3:35		0.00				0.00
3:40		0.00				0.00
3:45		0.00				0.00
3:50		0.00				0.00
3:55		0.00				0.00
4:00		0.00				0.00
4:05		0.00				0.00
4:10		0.00				0.00
4:15						
4:20						
4:25						
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5:35						

5:40						
5:45						
5:50						
5:55						
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond E

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5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
$H_{weir\ front}$ =	4.50	ft
$L_{weir\ front}$ =	15.00	9.00
$S_{weir\ sides}$ =	0.00	ft / ft
Horizontal $L_{weir\ sides}$ =	15.00	9.00
Grate Open Area =	70%	%
Debris Clogging =	50%	%
$H_{grate\ top}$ =	4.50	ft
Slope $L_{weir\ sides}$ =	15.00	9.00
Open Area (No Clogging) =	157.50	sq ft
Open Area (clogged) =	78.75	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	ft
Pipe Diameter =	60.00	inches
Plate Height =	43.00	50.00
Theta =	2.02	radians
Outlet Ao =	15.06	15.37
Outlet centroid =	1.99	ft
Open Area Ratio =	10.46	3.69

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
$H_{spillway\ invert}$ =	5.80	ft
$L_{spillway\ crest}$ =	100.00	42.00
$S_{spillway\ ends}$ =	4.00	4.00
Freeboard Depth =	1.00	1.00
Flow Depth _{spillway} =	0.70	ft
Freeboard Top Stage =	7.50	ft
Max Basin Area =	1.22	acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.81	1.70	3.01				12.89	
Predevelopment Peak Q (cfs) =	N/A	N/A	32.3				158.0	
Peak Inflow (cfs) =	N/A	N/A	46.6				176.9	
Peak Outflow (cfs) =	0.3	0.4	18.0				164.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.6				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.1				1.0	
Time to Drain 97% of Volume (hr) =	44	69	71				54	
Time to Drain 99% of Volume (hr) =	46	72	76				69	
Maximum Ponding Depth (ft) =	3.60	4.50	4.80				5.70	
Area at Max Ponding Depth (ac) =	0.88	0.96	0.98				1.06	
Maximum Volume Stored (ac-ft) =	0.81	1.70	1.99				2.91	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.81	1.70	3.01				12.89	
Predevelopment Peak Q (cfs) =	N/A	N/A	32.3				158.0	
Peak Inflow (cfs) =	N/A	N/A	46.6				176.9	
Peak Outflow (cfs) =	0.3	0.4	16.3				153.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.5				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A	0.3				2.8	
Time to Drain 97% of Volume (hr) =	44	69	71				54	
Time to Drain 99% of Volume (hr) =	46	72	76				69	
Maximum Ponding Depth (ft) =	3.60	4.50	4.90				6.10	
Area at Max Ponding Depth (ac) =	0.88	0.96	0.99				1.10	
Maximum Volume Stored (ac-ft) =	0.81	1.70	2.09				3.34	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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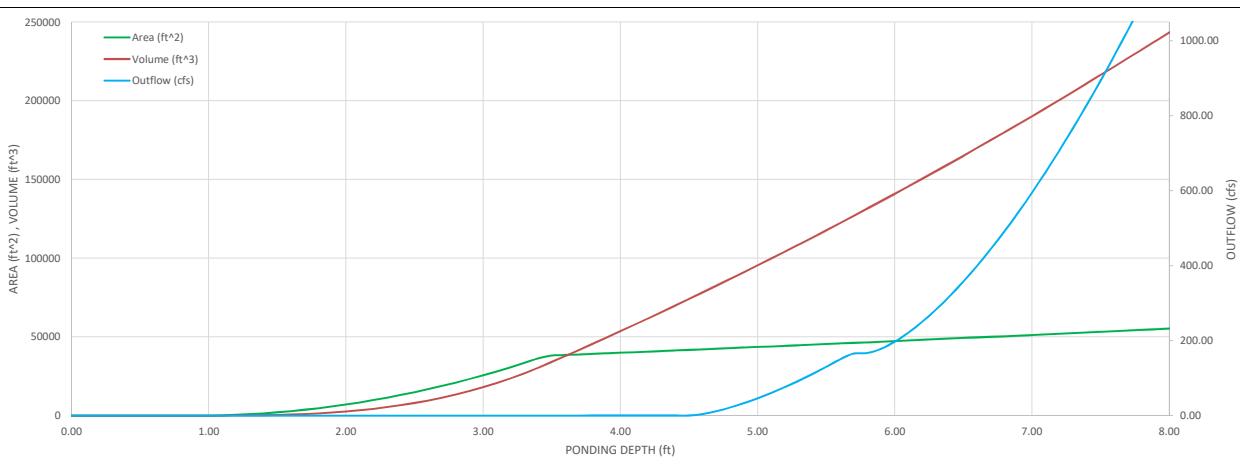
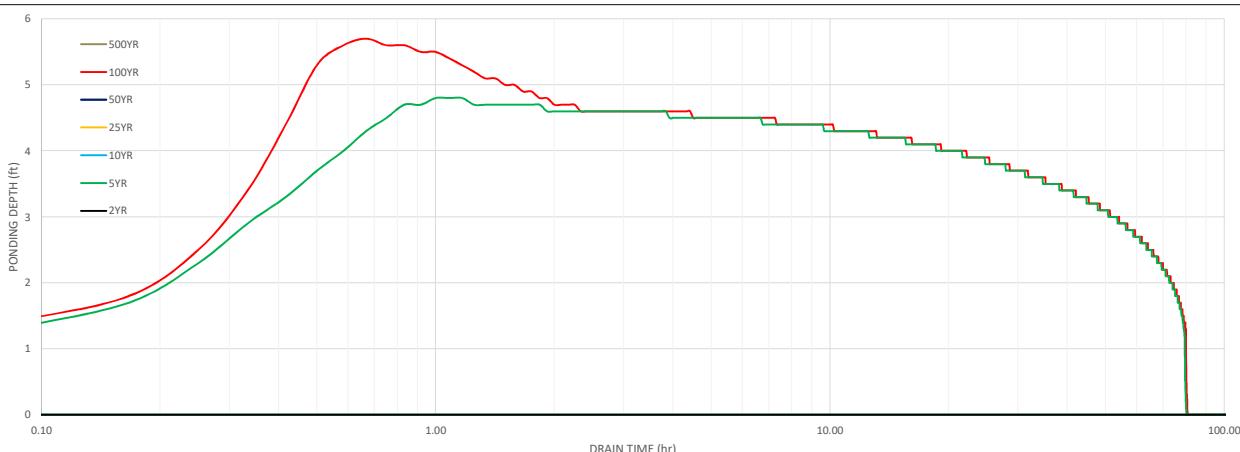
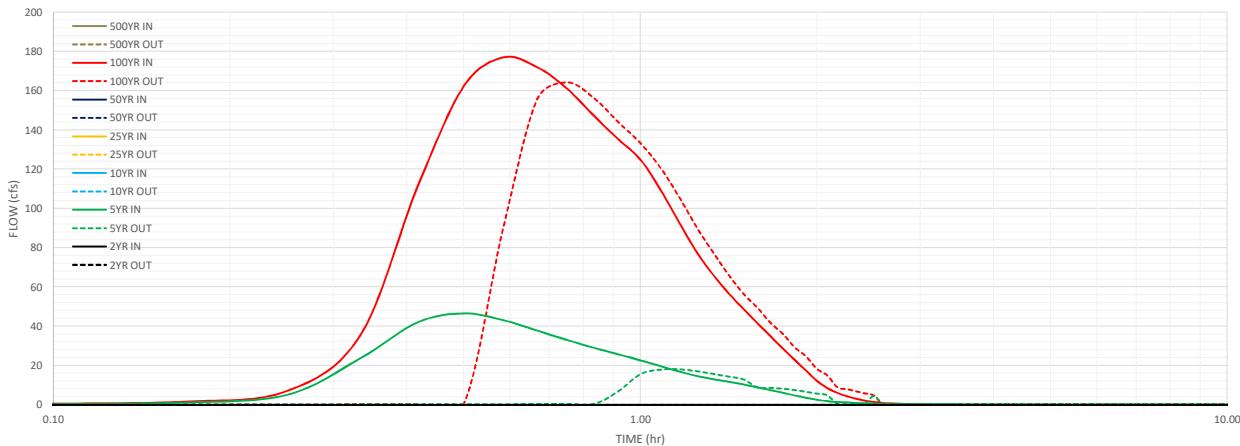


Designer: Chris McFarland

Project: Grandview Reserve Pond E

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond F

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1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
C) Underdrain Outlet Orifice Area
D) Number of WQCV Orifice Rows
E) Vertical Spacing between WQCV Orifice Rows
F) WQCV Orifice Area (A_o) per Row
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
H) EURV Orifice Area (A_o) in Single Row
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	N/A
y = N/A	N/A
Underdrain Ao = N/A	N/A
# WQCV rows = 14	13
Orifice Spacing = 4.0	4.0
WQCV Ao = 1.55	1.47
Max Stage wqcv = 4.80	4.50
EURV Ao = 1.55	7.84
Max Stage eurv = 6.00	6.00
Cd = 0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
B) Width of Basin at Top of EURV
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 570.9	570.9
W PCM = 217.0	217.0
Stage at Top of Bench = 6.10	6.10
L Bench = 571.7	571.7
W Bench = 217.8	217.8
Z Surcharge = 4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

- A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
42.34					221.11	

- B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	Post-Development Storm Inflow Hydrographs (cfs)					
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0:00	0.00				0.00	
0:05	0.52				1.80	
0:10	5.98				8.99	
0:15	19.71				25.32	
0:20	58.79				77.64	
0:25	94.74				207.48	
0:30	103.82				301.83	
0:35	97.47				329.97	
0:40	87.23				323.46	
0:45	77.84				304.34	
0:50	69.34				281.05	
0:55	61.26				257.82	
1:00	54.52				237.51	
1:05	49.46				211.11	
1:10	45.22				185.26	
1:15	40.70				161.15	
1:20	36.24				139.03	
1:25	32.06				119.17	
1:30	28.34				101.90	
1:35	24.61				86.26	
1:40	21.24				72.79	
1:45	19.05				62.33	
1:50	17.44				54.79	
1:55	16.04				48.91	
2:00	13.99				42.35	
2:05	11.69				35.81	
2:10	9.57				29.96	
2:15	7.79				24.91	
2:20	6.28				20.57	
2:25	5.03				16.95	
2:30	4.03				13.95	
2:35	3.21				11.42	
2:40	2.52				9.20	
2:45	1.92				7.18	
2:50	1.38				5.32	
2:55	0.95				3.69	
3:00	0.65				2.49	
3:05	0.46				1.70	
3:10	0.33				1.17	
3:15	0.24				0.81	
3:20	0.18				0.56	
3:25	0.14				0.38	
3:30	0.11				0.26	
3:35	0.08				0.18	
3:40	0.06				0.13	
3:45	0.05				0.10	
3:50	0.03				0.07	
3:55	0.02				0.05	
4:00	0.02				0.04	
4:05	0.01				0.03	
4:10	0.01				0.02	
4:15	0.00				0.01	
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4:25					0.00	
4:30						
4:35						
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5:00						
5:05						
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5:40						
5:45						
5:50						
5:55						
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond F

Date: April 6, 2020

Last Edited: April 13, 2020

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
H _{weir front} =	6.00	5.00 ft
L _{weir front} =	13.00	10.00 ft
S _{weir sides} =	0.00	0.00 ft / ft
Horizontal L _{weir sides} =	13.00	10.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	6.00	6.00 ft
Slope L _{weir sides} =	13.00	10.00 ft
Open Area (No Clogging) =	118.30	70.00 sq ft
Open Area (clogged) =	59.15	35.00 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	66.00	60.00 inches
Plate Height =	46.05	54.00 inches
Theta =	1.98	2.50 radians
Outlet Ao =	17.70	18.61 sq ft
Outlet centroid =	2.14	2.38 ft
Open Area Ratio =	6.68	3.76

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
H _{spillway invert} =	7.60	999.00 ft
L _{spillway crest} =	126.00	42.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	0.90	ft
Freeboard Top Stage =	9.50	ft
Max Basin Area =	3.37	acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	2.62	5.94	7.80				26.37	
Predevelopment Peak Q (cfs) =	N/A	N/A	42.3				221.1	
Peak Inflow (cfs) =	N/A	N/A	103.8				330.0	
Peak Outflow (cfs) =	1.1	1.5	15.1				227.3	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.4				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.2				1.9	
Time to Drain 97% of Volume (hr) =	42	68	72				61	
Time to Drain 99% of Volume (hr) =	45	72	77				72	
Maximum Ponding Depth (ft) =	4.80	6.00	6.30				7.60	
Area at Max Ponding Depth (ac) =	2.12	2.84	2.89				3.08	
Maximum Volume Stored (ac-ft) =	2.62	5.94	6.82				10.70	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	2.21	5.94	7.80				26.37	
Predevelopment Peak Q (cfs) =	N/A	N/A	42.3				221.1	
Peak Inflow (cfs) =	N/A	N/A	103.8				330.0	
Peak Outflow (cfs) =	1.1	1.4	13.2				214.5	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.3				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A	0.2				3.0	
Time to Drain 97% of Volume (hr) =	36	69	74				63	
Time to Drain 99% of Volume (hr) =	38	73	78				73	
Maximum Ponding Depth (ft) =	4.50	6.00	6.30				7.80	
Area at Max Ponding Depth (ac) =	1.81	2.84	2.89				3.11	
Maximum Volume Stored (ac-ft) =	2.21	5.94	6.82				11.32	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

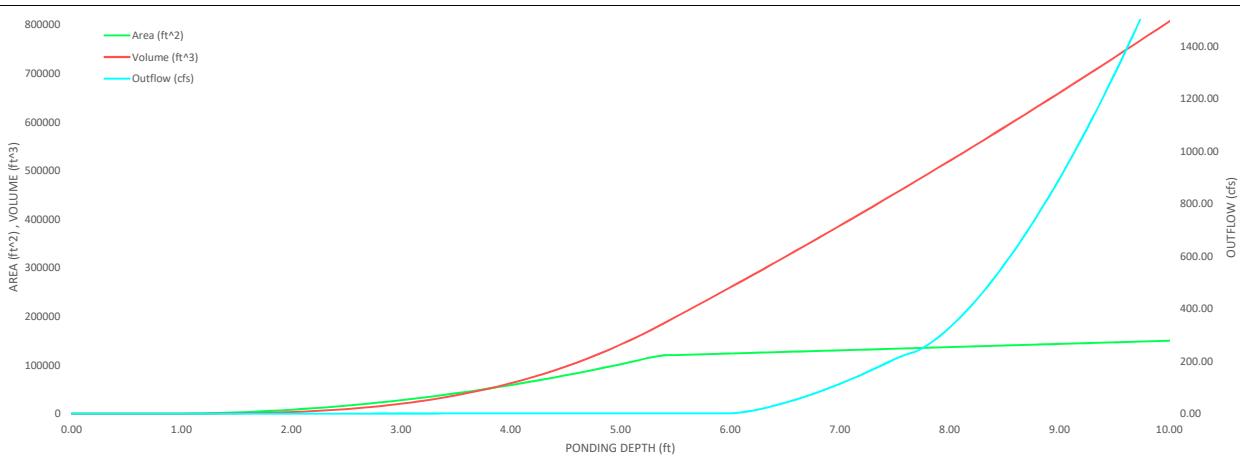
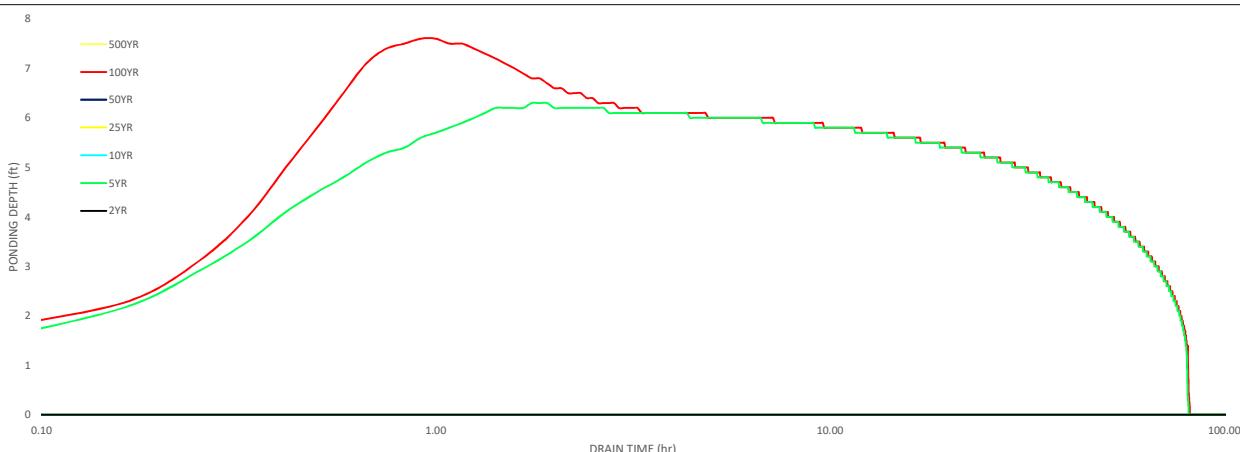
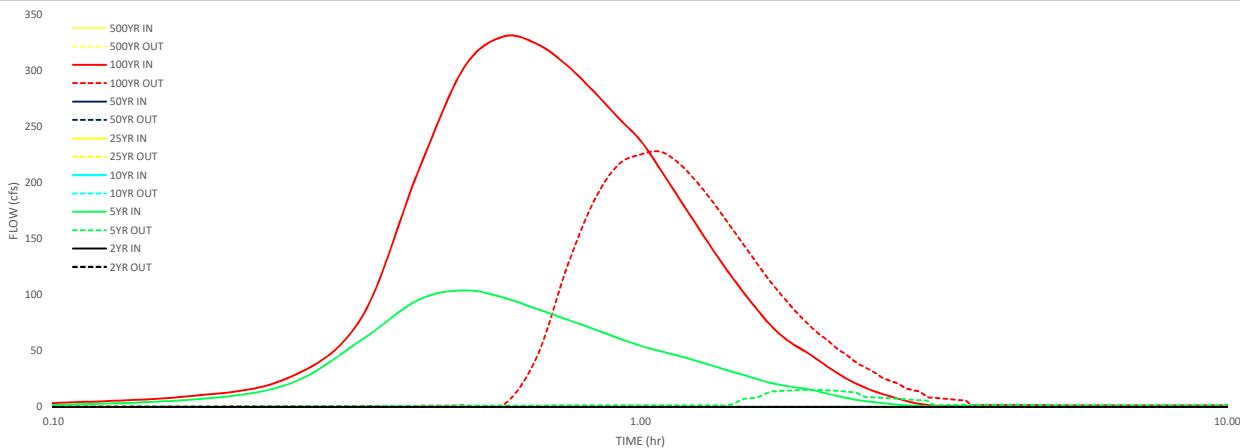


Designer: Chris McFarland

Project: Grandview Reserve Pond F

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond G

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
C) Underdrain Outlet Orifice Area
D) Number of WQCV Orifice Rows
E) Vertical Spacing between WQCV Orifice Rows
F) WQCV Orifice Area (A_o) per Row
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
H) EURV Orifice Area (A_o) in Single Row
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters	
User Input	COS DCM
i = N/A	i = N/A in / hr
y ₁ = N/A	y ₁ = N/A inches
y ₂ = N/A	y ₂ = N/A sq in
Underdrain Ao = 9	Underdrain Ao = 9 sq in
# WQCV rows = 4.0	Orifice Spacing = 4.0 inches
WQCV Ao = 0.49	WQCV Ao = 0.49 sq in
Max Stage wqcv = 3.20	Max Stage wqcv = 3.20 ft
EURV Ao = 1.94	EURV Ao = 1.94 sq in
Max Stage eurv = 4.00	Max Stage eurv = 4.00 ft
Cd = 0.60	Cd = 0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
B) Width of Basin at Top of EURV
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
F) Average Side Slopes of Flood Control Surcharge above Transition Bench
(Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters	
User Input	COS DCM
L PCM = 349.7	349.7 ft
W PCM = 105.4	105.4 ft
Stage at Top of Bench = 4.10	4.10 ft
L Bench = 350.5	350.5 ft
W Bench = 106.2	106.2 ft
Z Surcharge = 4.00	4.00 ft / ft

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

- A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	9.42				48.48	

- B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required
(Other Storms are Optional)

Time Interval	5.0 minutes	Post-Development Storm Inflow Hydrographs (cfs)					
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00	0.00				0.00		
0:05	0.18				0.49		
0:10	1.27				1.75		
0:15	3.86				5.05		
0:20	12.69				17.55		
0:25	19.21				47.38		
0:30	20.06				63.86		
0:35	18.72				67.51		
0:40	16.88				66.01		
0:45	15.24				62.38		
0:50	13.74				57.86		
0:55	12.37				53.71		
1:00	11.12				49.93		
1:05	10.01				44.10		
1:10	9.05				38.52		
1:15	8.20				33.58		
1:20	7.42				29.30		
1:25	6.67				25.48		
1:30	5.98				22.03		
1:35	5.28				18.97		
1:40	4.64				16.31		
1:45	4.05				13.93		
1:50	3.52				11.83		
1:55	3.12				10.10		
2:00	2.67				8.48		
2:05	2.26				7.10		
2:10	1.90				5.93		
2:15	1.58				4.93		
2:20	1.30				4.04		
2:25	1.05				3.25		
2:30	0.82				2.54		
2:35	0.62				1.90		
2:40	0.46				1.36		
2:45	0.35				0.99		
2:50	0.28				0.73		
2:55	0.22				0.54		
3:00	0.17				0.39		
3:05	0.13				0.28		
3:10	0.10				0.19		
3:15	0.07				0.13		
3:20	0.05				0.09		
3:25	0.04				0.07		
3:30	0.03				0.06		
3:35	0.02				0.04		
3:40	0.02				0.03		
3:45	0.01				0.03		
3:50	0.01				0.02		
3:55	0.01				0.01		
4:00	0.00				0.01		
4:05					0.00		
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5:40						
5:45						
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5:55						
6:00						

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond G

Date: April 6, 2020

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5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
H _{weir front} =	4.00	4.00 ft
L _{weir front} =	26.00	26.00 ft
S _{weir sides} =	0.00	0.00 ft / ft
Horizontal L _{weir sides} =	26.00	26.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	4.00	4.00 ft
Slope L _{weir sides} =	26.00	26.00 ft
Open Area (No Clogging) =	473.20	473.20 sq ft
Open Area (clogged) =	236.60	236.60 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	30.00	27.00 inches
Plate Height =	22.22	26.24 inches
Theta =	2.07	2.80 radians
Outlet Ao =	3.90	3.94 sq ft
Outlet _{centroid} =	1.03	1.12 ft
Open Area Ratio =	121.39	119.97

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
H _{spillway invert} =	5.40	4.90 ft
L _{spillway crest} =	136.00	23.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	0.30	0.90 ft
Freeboard Top Stage =	6.70	6.80 ft
Max Basin Area =	1.08	1.09 acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.47	1.15	1.57				5.51	
Predevelopment Peak Q (cfs) =	N/A	N/A	9.4				48.5	
Peak Inflow (cfs) =	N/A	N/A	20.1				67.5	
Peak Outflow (cfs) =	0.2	0.3	9.4				47.1	
Ratio (Outflow/Predevelopment) =	N/A	N/A	1.0				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.0				0.1	
Time to Drain 97% of Volume (hr) =	41	69	73				63	
Time to Drain 99% of Volume (hr) =	43	72	78				74	
Maximum Ponding Depth (ft) =	3.20	4.00	4.10				4.80	
Area at Max Ponding Depth (ac) =	0.67	0.85	0.85				0.91	
Maximum Volume Stored (ac-ft) =	0.47	1.15	1.24				1.85	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	0.47	1.15	1.57				5.51	
Predevelopment Peak Q (cfs) =	N/A	N/A	9.4				48.5	
Peak Inflow (cfs) =	N/A	N/A	20.1				67.5	
Peak Outflow (cfs) =	0.2	0.3	8.4				47.1	
Ratio (Outflow/Predevelopment) =	N/A	N/A	1.0				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.0				0.1	
Time to Drain 97% of Volume (hr) =	41	69	73				63	
Time to Drain 99% of Volume (hr) =	43	72	78				74	
Maximum Ponding Depth (ft) =	3.20	4.00	4.10				4.80	
Area at Max Ponding Depth (ac) =	0.67	0.85	0.85				0.91	
Maximum Volume Stored (ac-ft) =	0.47	1.15	1.24				1.85	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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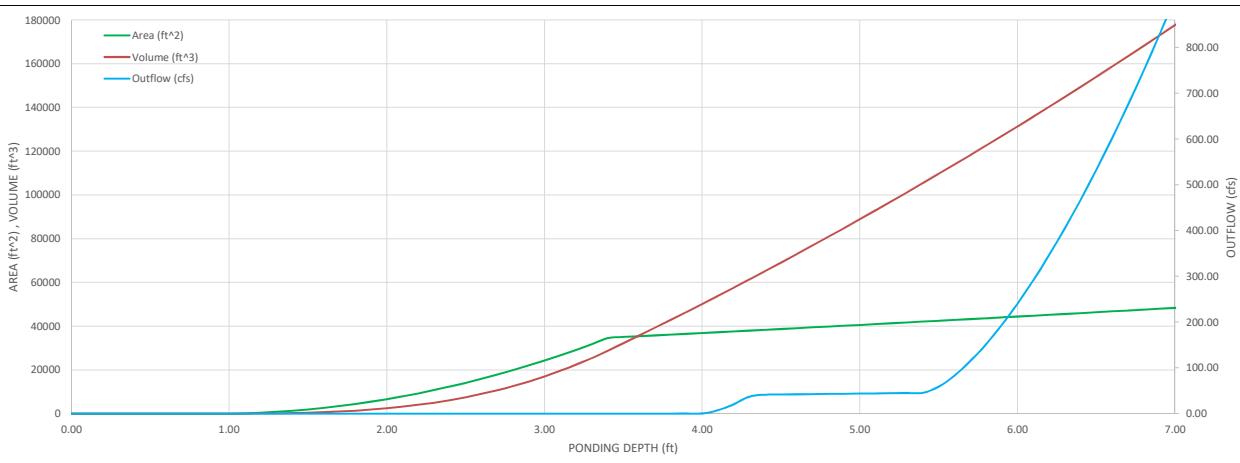
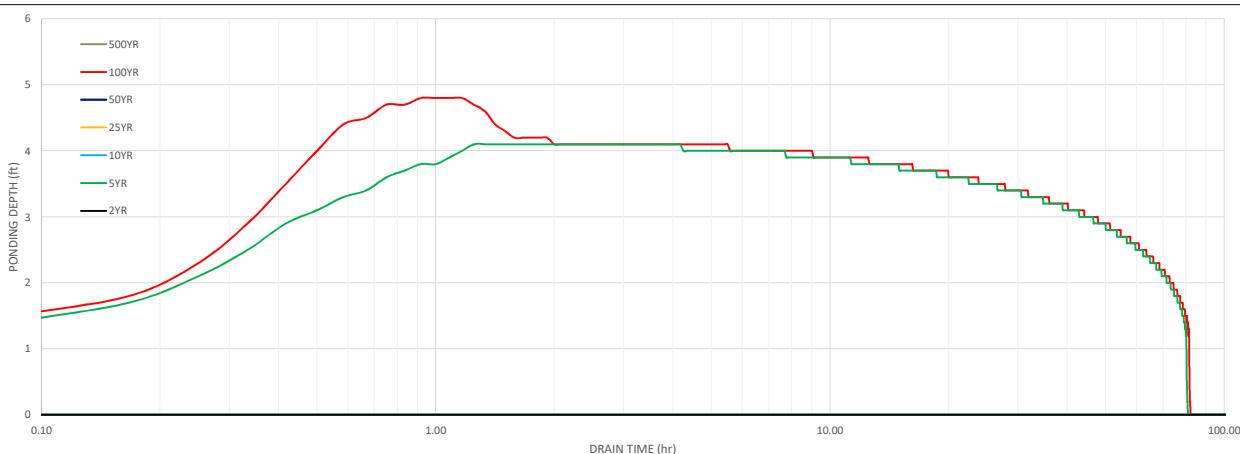
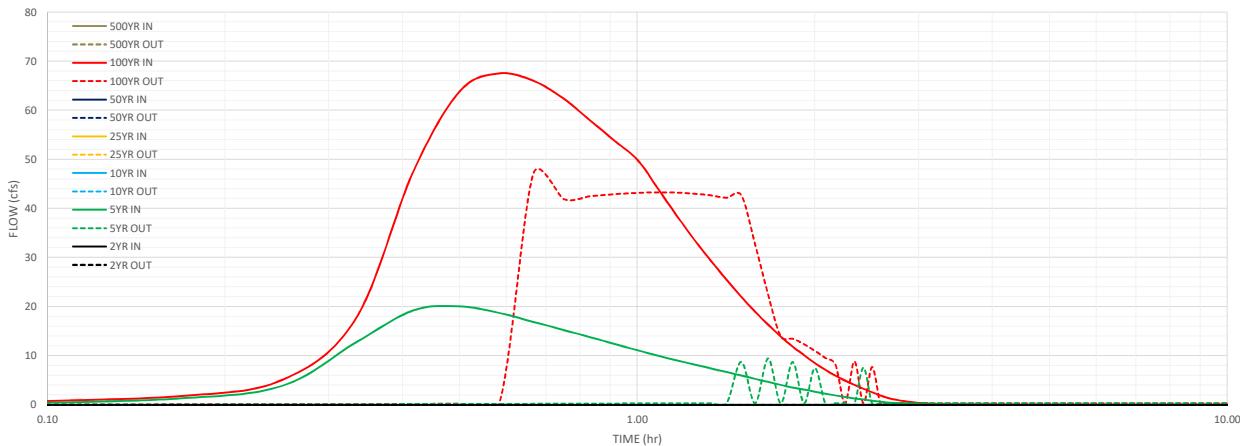


Designer: Chris McFarland

Project: Grandview Reserve Pond G

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond G

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type: Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.	Extended Detention Basin (EDB)																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
2. WQCV/EURV Outlet Details A) Average Infiltration Rate of WQCV B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface C) Underdrain Outlet Orifice Area D) Number of WQCV Orifice Rows E) Vertical Spacing between WQCV Orifice Rows F) WQCV Orifice Area (A_o) per Row G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth) H) EURV Orifice Area (A_o) in Single Row I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth) J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)	<table border="1"> <thead> <tr> <th colspan="2">Input Parameters</th> </tr> <tr> <th>User Input</th> <th>COS DCM</th> </tr> </thead> <tbody> <tr> <td>i = N/A</td> <td>N/A in / hr</td> </tr> <tr> <td>y = N/A</td> <td>N/A inches</td> </tr> <tr> <td>Underdrain Ao = N/A</td> <td>N/A sq in</td> </tr> <tr> <td># WQCV rows = 11</td> <td>11</td> </tr> <tr> <td>Orifice Spacing = 4.0</td> <td>4.0 inches</td> </tr> <tr> <td>WQCV Ao = 0.86</td> <td>0.86 sq in</td> </tr> <tr> <td>Max Stage wqcv = 3.80</td> <td>3.80 ft</td> </tr> <tr> <td>EURV Ao = 4.73</td> <td>4.73 sq in</td> </tr> <tr> <td>Max Stage eurv = 5.00</td> <td>5.00 ft</td> </tr> <tr> <td>Cd = 0.60</td> <td>0.60</td> </tr> </tbody> </table>	Input Parameters		User Input	COS DCM	i = N/A	N/A in / hr	y = N/A	N/A inches	Underdrain Ao = N/A	N/A sq in	# WQCV rows = 11	11	Orifice Spacing = 4.0	4.0 inches	WQCV Ao = 0.86	0.86 sq in	Max Stage wqcv = 3.80	3.80 ft	EURV Ao = 4.73	4.73 sq in	Max Stage eurv = 5.00	5.00 ft	Cd = 0.60	0.60																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
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3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench. A) Length of Basin at Top of EURV B) Width of Basin at Top of EURV C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge) D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge) E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge) F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)	<table border="1"> <thead> <tr> <th colspan="2">Input Parameters</th> </tr> <tr> <th>User Input</th> <th>COS DCM</th> </tr> </thead> <tbody> <tr> <td>L PCM = 468.4</td> <td>468.4 ft</td> </tr> <tr> <td>W PCM = 141.1</td> <td>141.1 ft</td> </tr> <tr> <td>Stage at Top of Bench = 5.10</td> <td>5.10 ft</td> </tr> <tr> <td>L Bench = 469.2</td> <td>469.2 ft</td> </tr> <tr> <td>W Bench = 141.9</td> <td>141.9 ft</td> </tr> <tr> <td>Z Surcharge = 4.00</td> <td>4.00 ft / ft</td> </tr> </tbody> </table> <p>User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.</p> <p>Bench Slope is 4H:1V in length direction Bench Slope is 4H:1V in width direction</p>	Input Parameters		User Input	COS DCM	L PCM = 468.4	468.4 ft	W PCM = 141.1	141.1 ft	Stage at Top of Bench = 5.10	5.10 ft	L Bench = 469.2	469.2 ft	W Bench = 141.9	141.9 ft	Z Surcharge = 4.00	4.00 ft / ft																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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4. Tributary Watershed Hydrology A) Input hydrology data (copy/paste) from model runs B) Adjust "Time Interval" to match hydrograph data 5-yr and 100-yr Hydrology Required (Other Storms are Optional)	<table border="1"> <thead> <tr> <th colspan="7">Pre-Development Peak Flow (cfs)</th> </tr> <tr> <th></th> <th>2 Year</th> <th>5 Year</th> <th>10 Year</th> <th>25 Year</th> <th>50 Year</th> <th>100 Year</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>17.11</td> <td></td> <td></td> <td></td> <td>99.16</td> </tr> </tbody> </table> <table border="1"> <thead> <tr> <th>Time Interval</th> <th>5.0 minutes</th> <th colspan="6">Post-Development Storm Inflow Hydrographs (cfs)</th> </tr> <tr> <th>Time (min)</th> <th>2 Year</th> <th>5 Year</th> <th>10 Year</th> <th>25 Year</th> <th>50 Year</th> <th>100 Year</th> <th>500 Year</th> </tr> </thead> <tbody> <tr><td>0:00</td><td>0.00</td><td></td><td></td><td></td><td></td><td>0.00</td><td></td></tr> 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Year	0:00	0.00					0.00		0:05	0.41					1.20		0:10	3.42					4.91		0:15	10.22					13.16		0:20	29.97					40.46		0:25	45.35					109.08		0:30	46.22					147.68		0:35	41.85					152.97		0:40	36.79					145.92		0:45	32.51					134.77		0:50	28.57					122.07		0:55	24.90					110.10		1:00	21.86					99.42		1:05	19.69					85.33		1:10	17.78					73.97		1:15	15.86					63.12		1:20	14.00					53.39		1:25	12.24					44.73		1:30	10.61					36.81		1:35	9.00					29.80		1:40	7.68					24.16		1:45	6.80					19.99		1:50	6.25					17.20		1:55	5.79					15.20		2:00	4.96					12.77		2:05	4.07					10.46		2:10	3.32					8.57		2:15	2.70					7.04		2:20	2.18					5.80		2:25	1.75					4.76		2:30	1.37					3.85		2:35	1.07					3.04		2:40	0.81					2.31		2:45	0.60					1.65		2:50	0.43					1.12		2:55	0.31					0.76		3:00	0.23					0.51		3:05	0.17					0.34		3:10	0.12					0.23		3:15	0.09					0.16		3:20	0.07					0.12		3:25	0.06					0.09		3:30	0.05					0.07		3:35	0.04					0.06		3:40	0.03					0.05		3:45	0.03					0.04		3:50	0.02					0.03		3:55	0.01					0.02		4:00	0.01					0.01		4:05	0.01					0.01		4:10	0.00					0.01		4:15						0.00		4:20								4:25								4:30								4:35								4:40								4:45								4:50								4:55								5:00								5:05								5:10								5:15								5:20								5:25								5:30								5:35							
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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond G

Date: April 6, 2020

Last Edited: April 13, 2020

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
User Input	COS DCM	
H _{weir front} =	5.00	5.00 ft
L _{weir front} =	9.00	7.00 ft
S _{weir sides} =	0.00	0.00 ft / ft
Horizontal L _{weir sides} =	9.00	7.00 ft
Grate Open Area =	70%	70% %
Debris Clogging =	50%	50% %
H _{grate top} =	5.00	5.00 ft
Slope L _{weir sides} =	9.00	7.00 ft
Open Area (No Clogging) =	56.70	34.30 sq ft
Open Area (clogged) =	28.35	17.15 sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50 ft
Pipe Diameter =	42.00	42.00 inches
Plate Height =	34.00	34.00 inches
Theta =	2.24	2.24 radians
Outlet Ao =	8.34	8.34 sq ft
Outlet _{centroid} =	1.54	1.54 ft
Open Area Ratio =	6.80	4.11

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
User Input	COS DCM	
H _{spillway invert} =	6.70	999.00 ft
L _{spillway crest} =	136.00	27.00 ft
S _{spillway ends} =	4.00	4.00 ft / ft
Freeboard Depth =	1.00	1.00 ft
Flow Depth _{spillway} =	0.50	ft
Freeboard Top Stage =	8.20	ft
Max Basin Area =	1.89	acres

9. Routed Hydrograph Results

Results based on User Input

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.03	2.73	3.25				11.08	
Predevelopment Peak Q (cfs) =	N/A	N/A	17.1				99.2	
Peak Inflow (cfs) =	N/A	N/A	46.2				153.0	
Peak Outflow (cfs) =	0.4	0.7	4.2				101.9	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A	0.0				1.7	
Time to Drain 97% of Volume (hr) =	39	68	73				62	
Time to Drain 99% of Volume (hr) =	41	72	77				72	
Maximum Ponding Depth (ft) =	3.80	5.00	5.10				6.20	
Area at Max Ponding Depth (ac) =	1.09	1.52	1.53				1.65	
Maximum Volume Stored (ac-ft) =	1.03	2.73	2.90				4.65	

Results based on COS DCM Inputs

WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =								
Inflow Hydrograph Volume (ac-ft) =	1.03	2.73	3.25				11.08	
Predevelopment Peak Q (cfs) =	N/A	N/A	17.1				99.2	
Peak Inflow (cfs) =	N/A	N/A	46.2				153.0	
Peak Outflow (cfs) =	0.4	0.7	3.6				98.1	
Ratio (Outflow/Predevelopment) =	N/A	N/A	0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate	Overflow Grate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A	0.2				2.8	
Time to Drain 97% of Volume (hr) =	39	68	73				62	
Time to Drain 99% of Volume (hr) =	41	72	77				73	
Maximum Ponding Depth (ft) =	3.80	5.00	5.20				6.40	
Area at Max Ponding Depth (ac) =	1.09	1.52	1.54				1.68	
Maximum Volume Stored (ac-ft) =	1.03	2.73	3.05				4.98	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

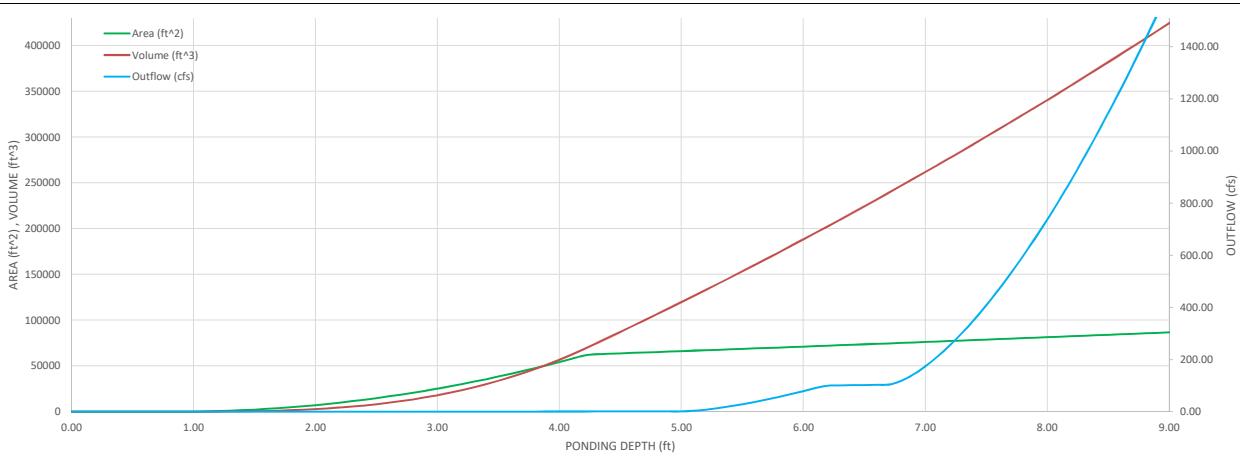
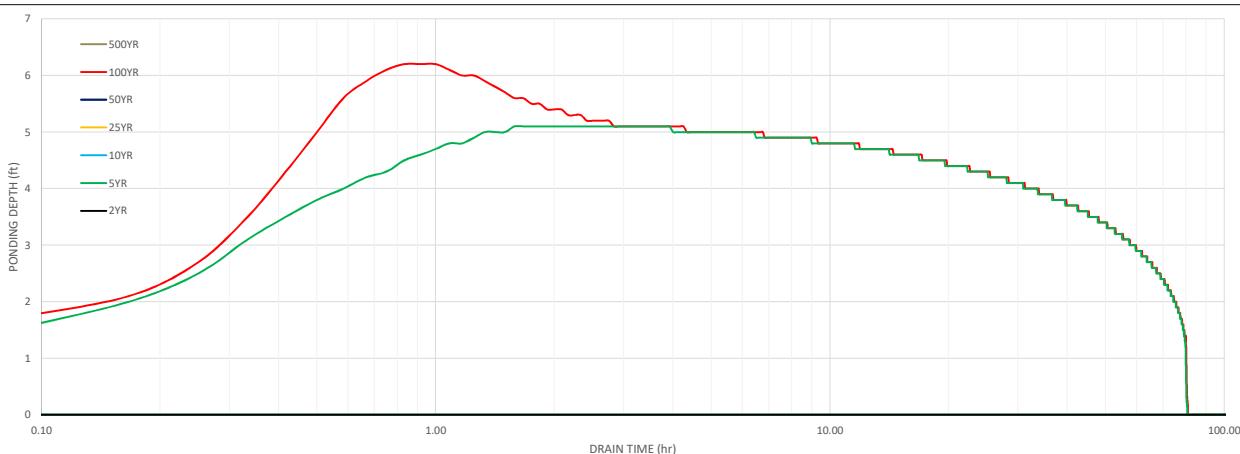
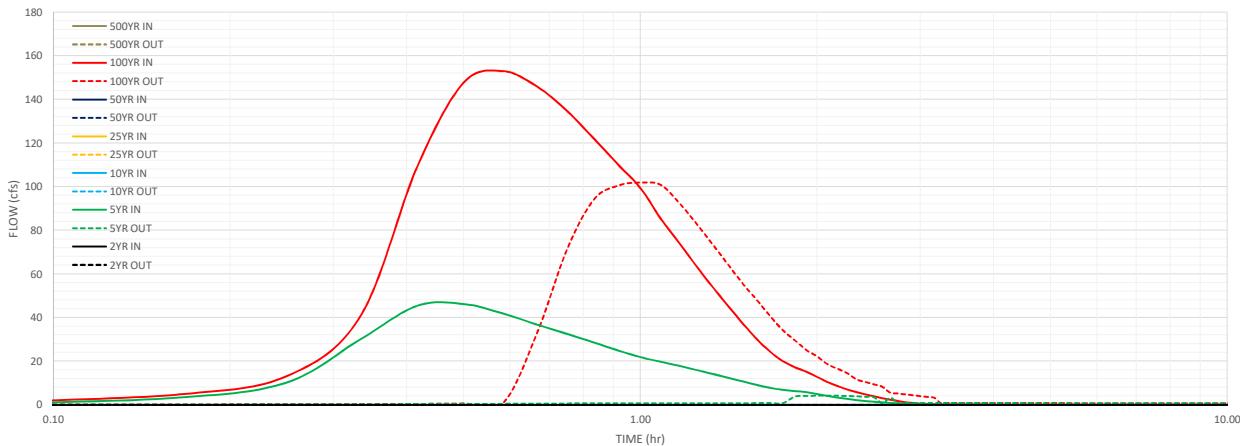


Designer: Chris McFarland

Project: Grandview Reserve Pond G

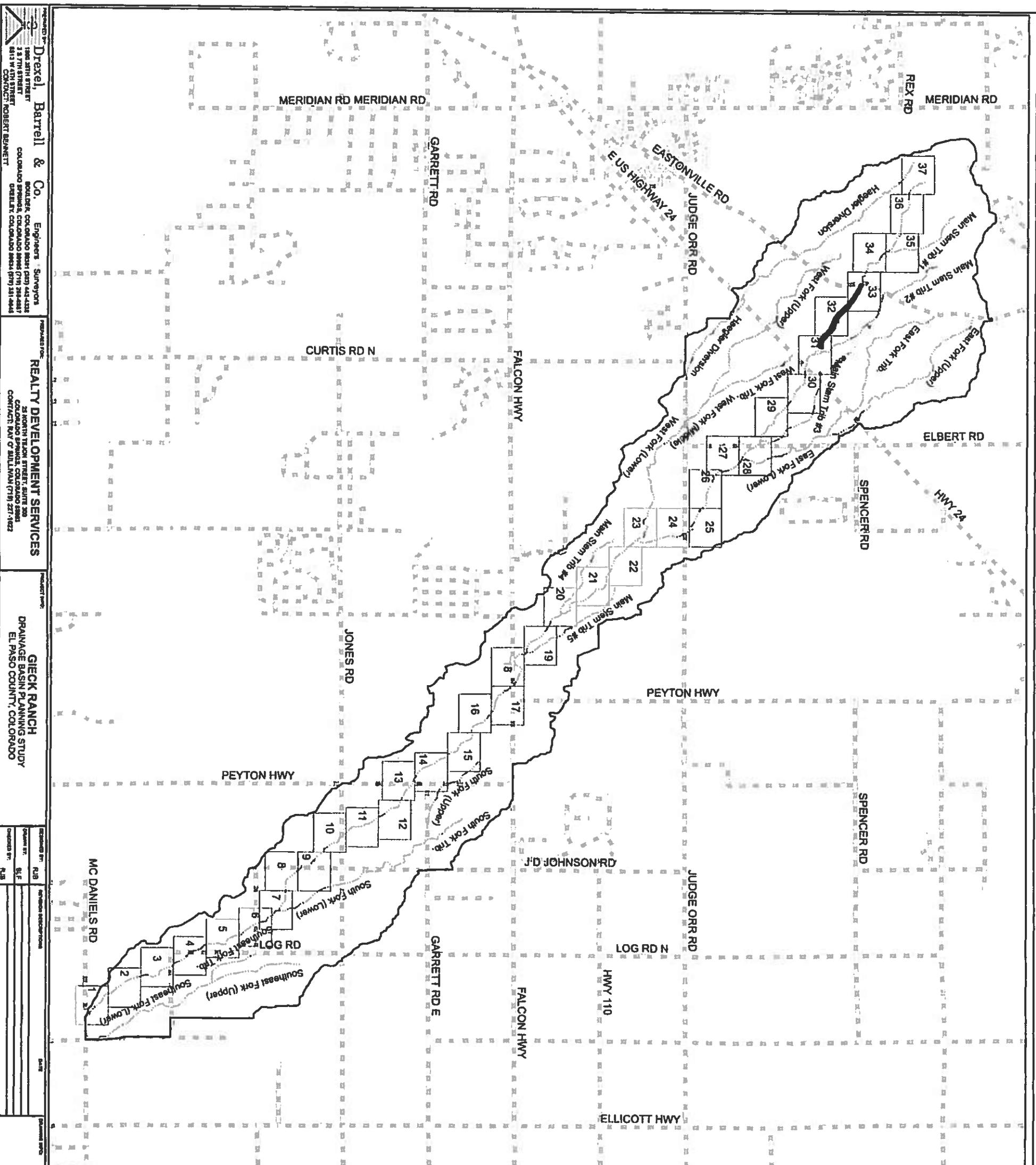
Date: April 6, 2020

Last Edited: April 13, 2020



Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Appendix E



THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOTS DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.



Legend

	Roads
	Streams
	Matchlines
	Basin Boundary

GIECK RANCH KEY MAP MAIN STEM

AUGUST 2007 **C7706-1** **PL**

Scale: 1" = 600' **6D 038** **K1**

7025

MST2-R2

6005

6198

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

Legend



MST2-R2

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours

0

100 200 Feet

0

100 200 Feet

	Ponds
	Riparian: Good

	Proposed Future Conditions 100-yr Flood Limits
	Streams

	Reaches
	Reach Breaklines
	Roads
	Cross-sections
	Structures
	Section Lines
	5-ft contours
	2-ft contours



Legend

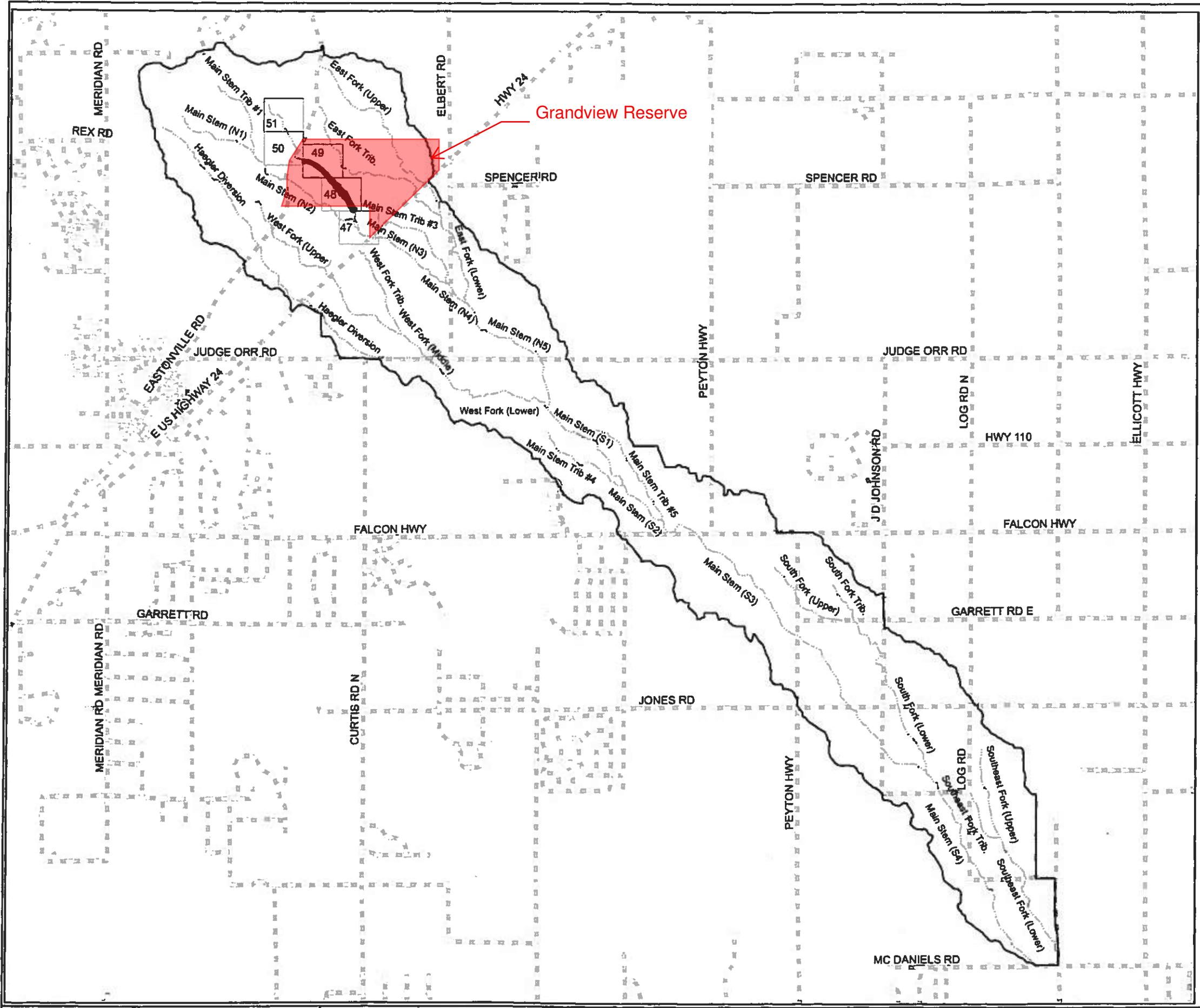
Streams

Roads

Basin Boundary

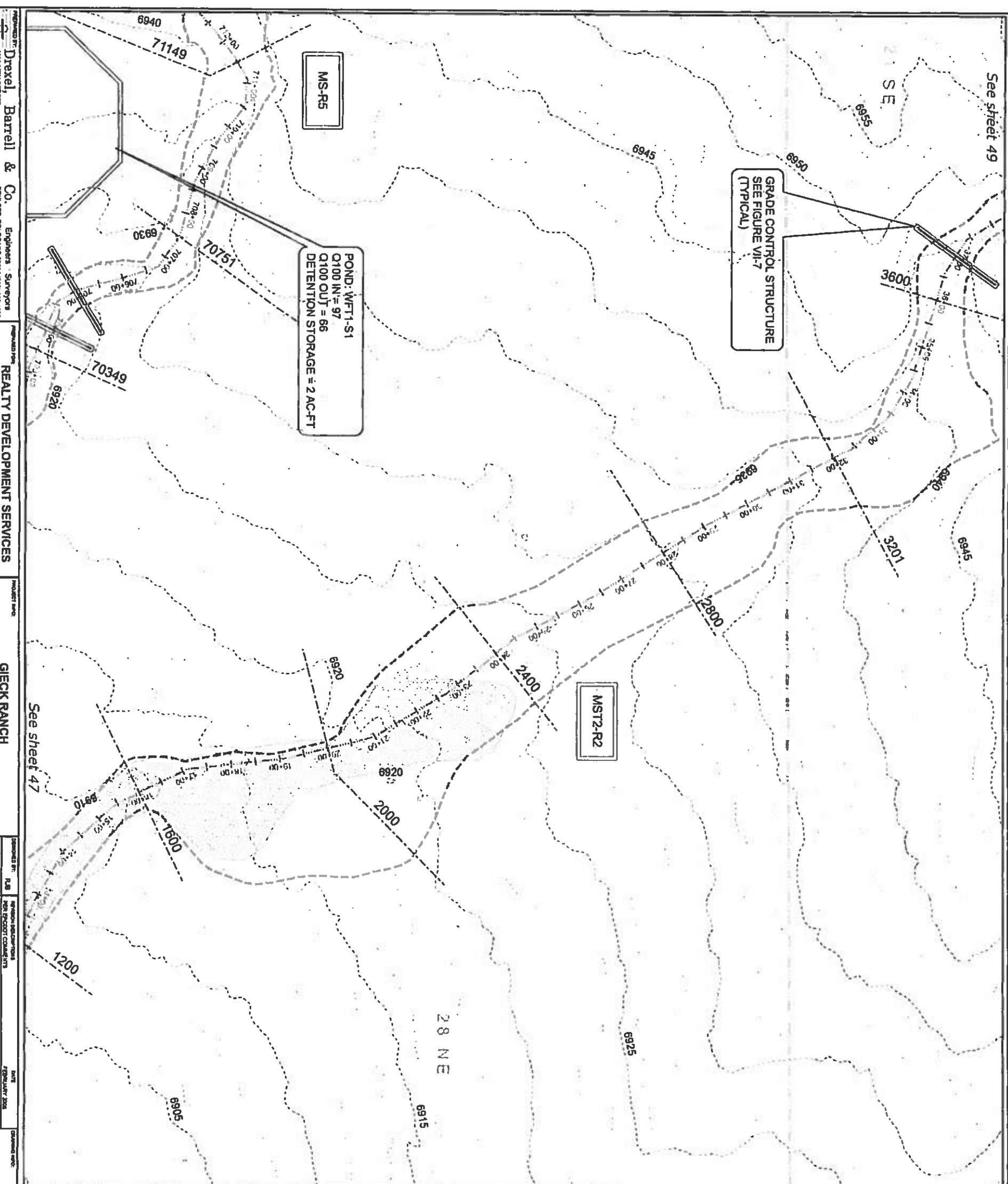
Matchlines

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0 1 2 Miles

See sheet 49



Environmental Key

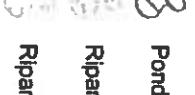


Ponds

Riparian: Good

Flood Limits

Streams



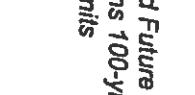
Riparian: Poor



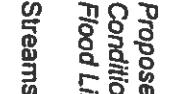
Proposed Future Conditions 100-yr Flood Limits



Reaches



Cross-sections



Structures



Section Lines



Roads

Reach Breaklines

5-ft contours

0

100

200

Feet



Reach	Slope (%)	Q_{100} (cfs)	V_{100} (ft/s)
MST2-R2	1.93	271	3.16

RECOMMENDED PLAN IMPROVEMENTS			
Reach		Vegetation Augmentation	
MST2-R2			

Note:
See Technical Addenda for grade control data.

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Drexell, Barrell & Co., Engineers Surveyors
100 EAST 16TH STREET
DENVER, COLORADO 80202
303-295-1100
FAX: 303-295-1101
E-MAIL: DBC@AOL.COM
CONTACT: ROBERT BENNETT, P.E., GCM

REALTY DEVELOPMENT SERVICES
DRAINAGE BASIN PLANNING STUDY
COLOMBO, COLORADO
CONTACT: PAT O'BRIEN (303) 277-4622

GIECK RANCH
DRAINAGE BASIN PLANNING STUDY
EL PASO COUNTY, COLORADO

GIECK RANCH DBPS
PLAN VIEW
MAIN STEM TRIBUTARY-2 #2

AUGUST 2007 C7706-2 PL
1" = 200' 6D 038 48
NONE

Drexel, Barrell & Co., Engineers & Surveyors
1000 14TH STREET
307 17TH STREET
APT. 2W
CONTACT: ROBERT BENNETT
BOULDER, COLORADO 80302 (303) 442-3233
COLORADO SPRINGS, COLORADO 80903 (719) 592-0587
GOLDEN, COLORADO 80401 (303) 251-4645

REALTY DEVELOPMENT SERVICES
 24 NORTH TEJON STREET, SUITE 300
 COLORADO SPRINGS, COLO. 80903
 CONTRACT: RAY OR SULLIVAN (719) 227-4822

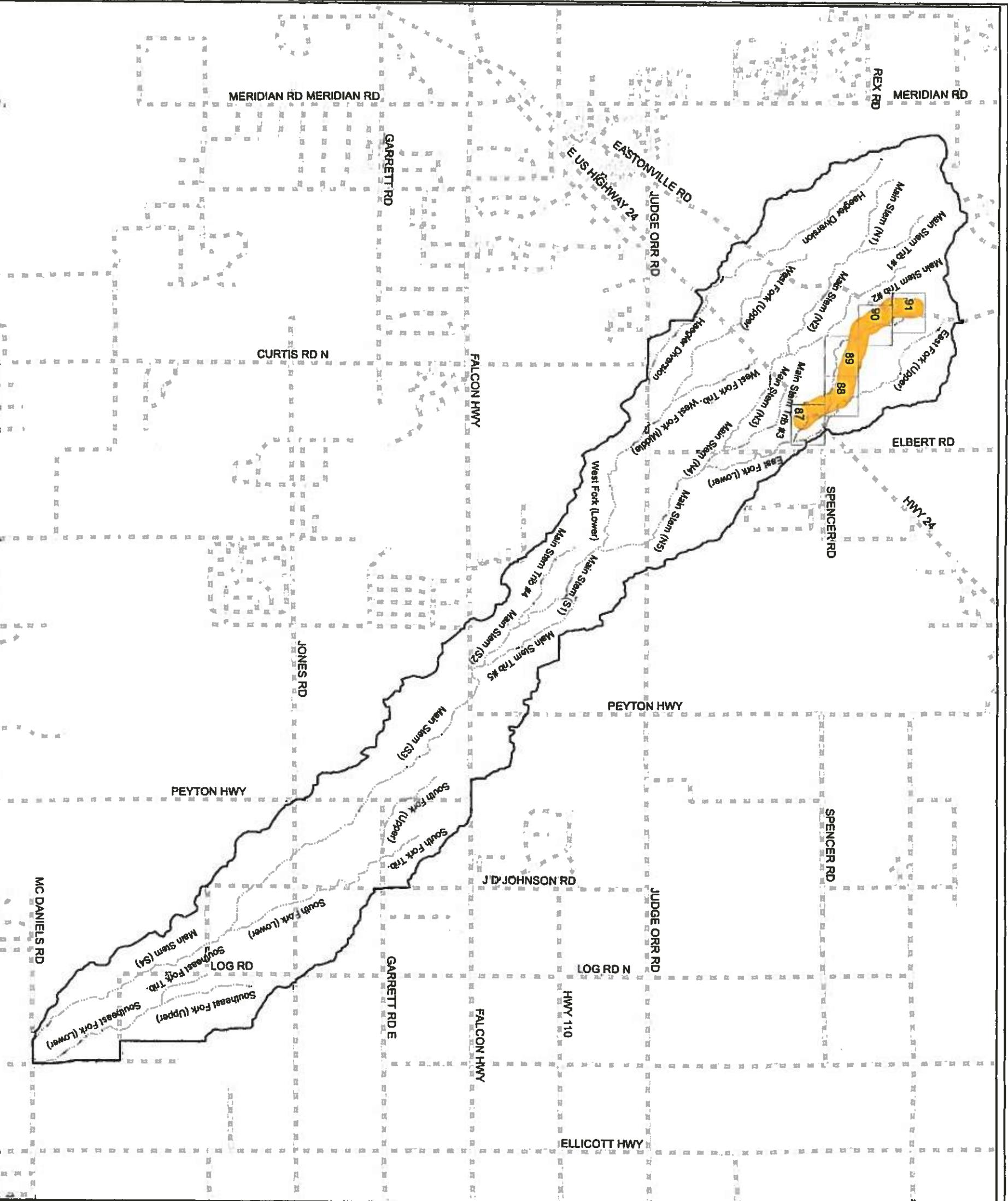
PROPERTY NAME: **GIECK RANCH**

DRAINAGE BASIN PLANNING STUDY
 EL PASO COUNTY, COLORADO

प्राप्ति	प्राप्ति	प्राप्ति
१८५	१८६	१८७
१८८	१८९	१९०
१९१	१९२	१९३
१९४	१९५	१९६

**GIECK RANCH
KEY MAP
EAST FORK TRIBUTARY**

DATE: AUGUST 2007
ITEM NO: C7706-1
PLATE: PL



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DIRECTION SHOULD
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DECISIONS.



Legend

Streams

Roads

Basin Boundary

Environmental Key

Ponds

Riparian: Good

Riparian: Poor

Streams

Reaches

Cross-sections

Roads

Structures

Section Lines

5-ft contours

Reach Breaklines

Proposed Future Conditions 100-yr Flood Limits

Potential Wetlands

The channel is considered dry unless shown as one of the above environmental categories.

0 100 200 Feet

2-ft contours



RECOMMENDED PLAN IMPROVEMENTS

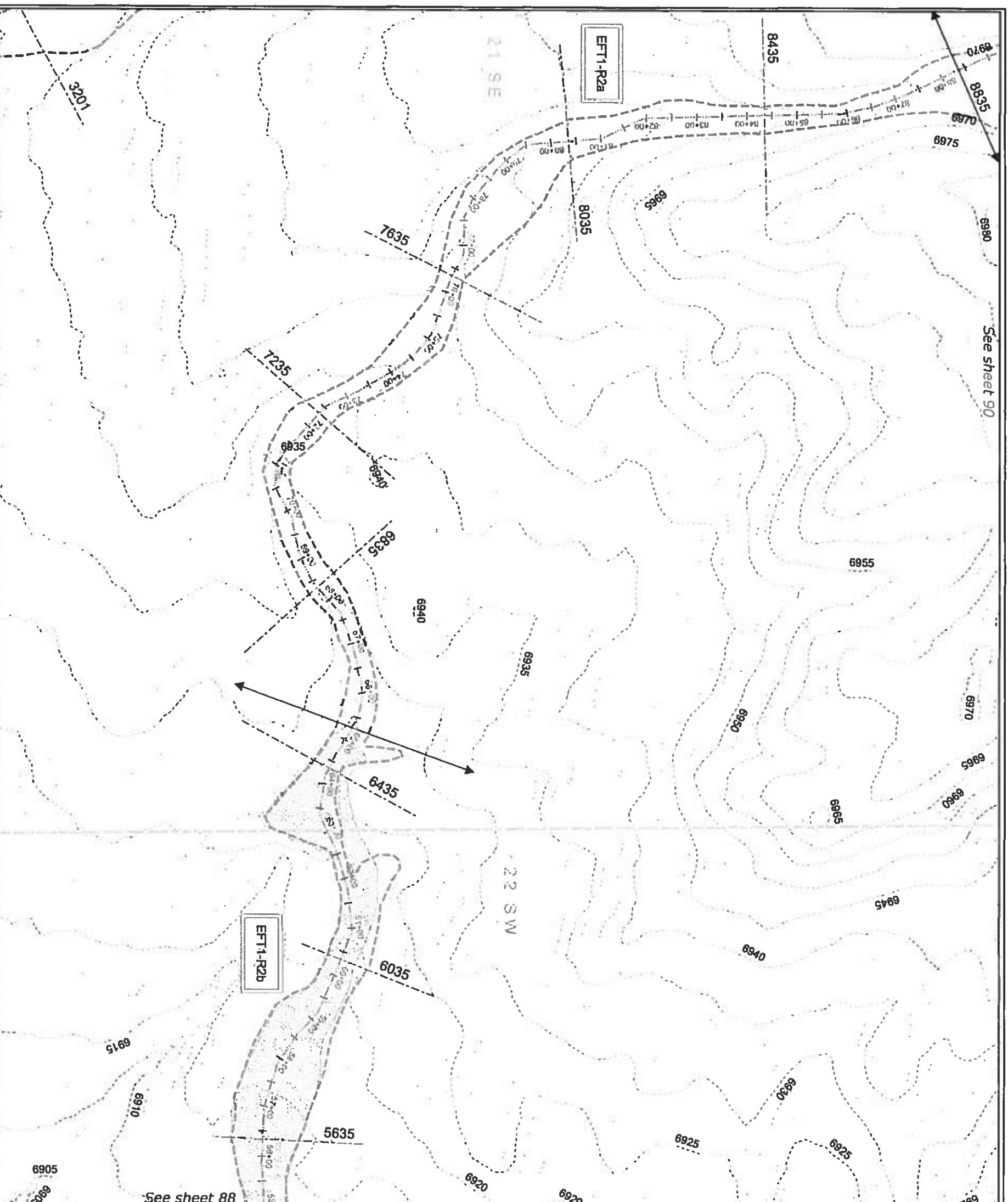
Reach

Reach	Slope (%)	Q ₁₀₀ (cfs)	V ₁₀₀ (ft/s)
EFT1-R2a	1.83	217	3.73
EFT1-R2b	1.60	217	2.68

As-needed Improvements

EFT1-R2a	As-needed Improvements
EFT1-R2b	As-needed Improvements

See sheet 88



Legend

Proposed Future Conditions 100-yr Flood Limits

Streams

Reaches

Cross-sections

Roads

Structures

Section Lines

5-ft contours

Reach Breaklines

Proposed Future Conditions 100-yr Flood Limits

Potential Wetlands

Ponds

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Streams

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5-ft contours

Reach Breaklines

Proposed Future Conditions 100-yr Flood Limits

Potential Wetlands

Ponds

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Streams

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Roads

Structures

Section Lines

5-ft contours

Reach Breaklines

Proposed Future Conditions 100-yr Flood Limits

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Prepared by: Drexel, Barrell & Co. Engineers Surveyors
1001 17th Street, Suite 1000, Denver, CO 80202
1-800-333-1000
Attn: Project Manager
Colorado Office: Colorado River 1000-2000
Contact Ray O'Sullivan (719) 271-4622

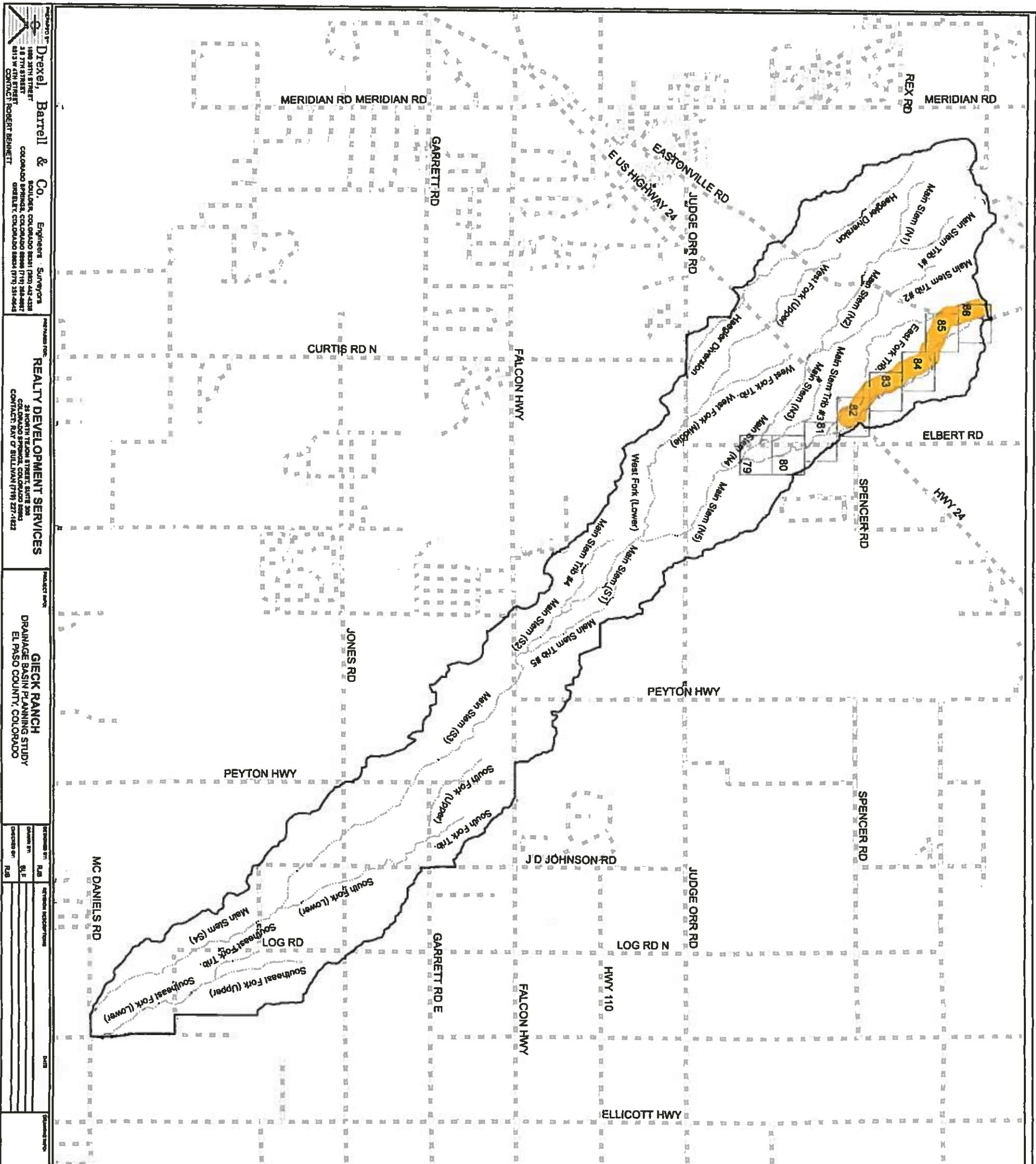
REALLY DEVELOPMENT SERVICES
24 MONTH TEAM, APRIL 2006 - APRIL 2008
24 MONTH TEAM, COLORADO RIVER 1000-2000
DRAINAGE BASIN PLANNING STUDY
EL PASO COUNTY, COLORADO

GIECK RANCH
DRAINAGE BASIN PLANNING STUDY
EL PASO COUNTY, COLORADO

Prepared by: GIECK RANCH
1001 17th Street, Suite 1000, Denver, CO 80202
1-800-333-1000
Attn: Project Manager
Colorado Office: Colorado River 1000-2000
Contact Ray O'Sullivan (719) 271-4622

EAST FORK DBPS
PLAN VIEW
EAST FORK TRIBUTARY #3

AUGUST 2007 C7706-2 PL
1' = 200' 6D 038 89



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Legend

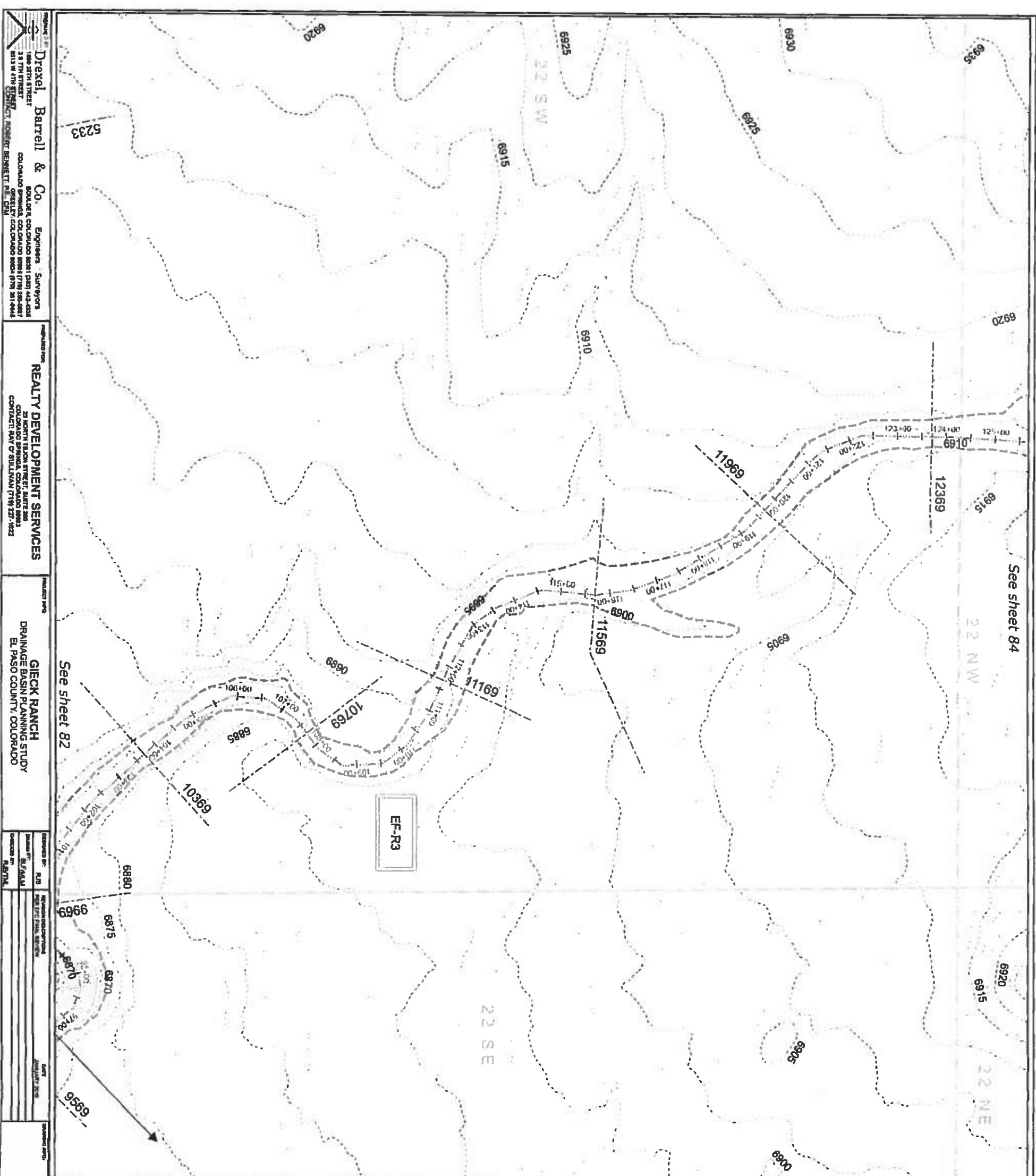
Streams

Roads

Basin Boundary

Matchlines

0
1
2 Miles



Reach	Slope (%)	Q ₁₀₀ (cfs)	V ₁₀₀ (ft/s)
EF-R3	1.53	595	5.09
RECOMMENDED PLAN IMPROVEMENTS			
Reach	As-needed Improvements		
EF-R3	As-needed Improvements		
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GIECK RANCH DBPS PLAN VIEW EAST FORK #5	DATE: AUGUST 2007 SCALE: 1" = 200' MATERIAL: NONE	JOB NO.: C7706-2 INSTRUMENT #: 6D 038 NET SURVEY: 83	PL

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Environmental Key

Legend

The channel is considered dry unless shown as one of the above environmental categories.

Riparian: Good

Proposed Future
Conditions 100-yr
Flood Limits



Structures
Section Lines
5-ft contours
2-ft contours