

### Grandview Reserve Master Development Drainage Plan

November 2020 HR Green Project No: 191850

#### **Prepared For:**

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Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

### Engineer's Statement

This report and plan for the drainage design of the development, Grandview Reserve, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *El Paso County Drainage Criteria* Manual and is in conformity with the master plan of the drainage basin. I understand that El Paso County does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Greg Panza, PE

State of Colorado No. 37081

For and on behalf of HR Green Development, LLC



### Developer's Statement

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

**4 Site Investments LLC** By: ANAGE Title: Address:

Date

1271 KELLS JOHNSON BUD, COLORADO SPRENKS, CO 80920

# El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.

Date

County Engineer/ECM Administrator



# Master Development Drainage Plan – Grandview Reserve

# I. General Purpose, Location and Description

### a. Purpose and Scope of study

The Purpose of this Master Development Drainage Plan (MDDP) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, areas tributary to the site and the planned storm water management for Grandview Reserve 2 development. The items discussed in this report are preliminary in nature and final drainage calculations and design will be required as development proceeds. This reports provides a general drainage concept and guidance for future development of Grandview Reserve.

#### b. DBPS Investigations

The Gieck Ranch Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by Drexel, Barrell was reviewed to determine existing plans and constraints that would influence the design of Grandview Reserve. The proposed plans for Grandview Reserve are in general conformance with the DBPS.

The DBPS shows 4 reaches through Grandview Reserve. The Main Stem (MS) in the south western portion of the site, the Main Stem Tributary #2 (MST2) to the north and east of the Main Stem, the East Fork Tributary (EFT) in the middle of the site north and east of MST2, and the East Fork Upper (EF) at the north east side of the site. These drainageways have been reviewed in the following reports and further analysis will be completed of these major drainageways in future planning documents.

- Unnamed Tributary Black Squirrel Creek, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004
- Haegler and Gieck Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004
- Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006
- Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)
- Meridian Ranch Master Development Drainage Plan (MDDP), Tech Contractors, January 2018

### c. Agency Jurisdictions

Listed below are the jurisdictions that this project will conform to:

El Paso County

Falcon Colorado Municipal Code (where applicable)

Federal Emergency Management Agency



### d. General Project Description

Grandview Reserve is located in Falcon, Colorado within El Paso County and contains approximately 765 acres within the south half of section 21 and 22 and the north half of section 27 and 28, Township 12 South, and Range 66 West of the Sixth Principal Meridian in Ela Paso County, Colorado. See below for approximate site location.



Figure 1 - Site Map

#### e. Data Sources

Listed Below are the technical resources reviewed in the preparation of this MDDP:

City of Colorado Springs Drainage Criteria Manual (DCM), Volumes 1 and 2 Mile High Flood District NOAA Atlas 14 NRCS Soil Survey for El Paso County Area, Colorado FEMA FIRM 08041C0556G and FIRM 08041C0552G (eff. 12/7/2018) El Paso County Assessor Property Records



### f. Applicable Criteria and Standards

Per the DBPS, flows from the proposed site will be limited to historic flows in an effort to maintain the stability and of the existing channels with the drainage basin. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended.

# **II. Project Characteristics**

### a. Location in Drainage Basin, offsite flows, size

Grandview Reserve is located within the Gieck Ranch Drainage Basin which covers approximately 22 square miles. This drainage basin is tributary to Black Squirrel Creek and joins said creek just to the south of Elicott, CO about 18 miles to the south. Black Squirrel Creek eventually drains to the Arkansas River in Pueblo Colorado. The majority of the Gieck Ranch Drainage basin is undeveloped consisting of rural farmland. The Geick Ranch Drainage basin lies north of the Haegler Ranch drainage basin.

As part of the Fourway LOMR discussed above, the study reviewed the hydrology and hydraulics for the Main Stem Tributaries, however only a small portion of the site within Grandview was analyzed. The peak flows rates for the Main Stem for the 100 year event was 413 cfs and for the Main Stem Tributary was 280 cfs.

For the East Fork tributaries (EF and EFT), the DBPS established 100 year flow rates of 595 cfs for the East Fork (EF) and 217 cfs for the East Fork Tributary (EFT)

Generally offsite flows are conveyed through the site via the 4 tributaries. Minor offsite basins may sheet flow onto the site. These flows will be routed through the site via the tributaries.

#### b. Compliance with DBPS

This MDDP is in general conformance with the guidelines outlined in the Gieck Ranch DBPS. Grandview Reserve will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

Existing downstream infrastructure is currently the historic drainage channels and minimal downstream improvements exist. As such, the site follows the DBPS and limits offsite flow rates to at or below historic rates. Outfalls out of the site will generally be along the same historic tributaries. Although outfall rates will be at or below historic, volume of runoff will increase and therefore downstream facilities may see additional flow volume than historic. This may provide a net benefit to the downstream facilities by providing more water to assist with vegetation however it should be noted that increased volume may also lead to more erosion or channel movement.

#### c. Site Characteristic

Per the NRCS web soil survey, the site is made up entirely of Type A and B soils. The majority of which are Type A soils. The predominate soils are Blakeland loamy sand, Columbine gravelly sandy loam, and Stapleton sandy loam. The first two soils are Type A soil and cover approximately 55.1% of the site and



the later soil is a Type B soil and covers the remaining 44.9% of the site. See Appendix A for the NRCS soil map.

Current ground cover is predominantly short- to mid-grass prairie grasslands and former farmland which consists of nonnative weeds and grasses. The site has very few, if any, trees and a minimal number of shrubs are found on the site.

#### d. Major drainage ways and structures

As mentioned previously, 4 major drainage ways exist on the site. These convey existing on and off-site flows and current on site flows through the site in a southeasterly direction. The drainageways eventually cross Highway 24 via culverts and other structures; further survey will be conducted to determine their effectiveness as the development of the site progresses.

A breached stock pond is located along the Main Stem and the effects of the existing breached dam are unknown at this time. As development occurs, this dam will be completely removed and improvements will be constructed along the channels to become high functioning low maintenance drainageway corridors.

#### e. Existing and proposed land uses

The existing site is open rangeland and farmland with no visible structures. The proposed development will consist of low, medium, and high density residential, along with two institutional sites, multiple pocket park sites, a large community park and a commercial area adjacent to Highway 24. The current land plan assumes approximately 3,261 dwelling units will be constructed on the site.

Land Use	MAX DU/AC
Low	2
Medium	4
Medium – High	8
High	12

### III. Hydrologic Analysis

### a. Major Basins and subbasins

#### Major Basin Description

- Previous basin study: Gieck Ranch Drainage Basin Planning Study
- Per FEMA FIRM 08041C0556G and 08041C0552G (eff. 12/7/2018), Grandview Reserve has four mapped channels within its boundaries.
- Per aerial imaging, no major irrigation is in the vicinity that would affect Grandview Reserve.

The site has been divided into 8 major drainage basins per where each basin is tributary to a full spectrum detention pond facility. These basins and associated sub basins are described in more detail in the next section of this report.

#### **Subbasin Description**

The entire site drains in a south easterly direction and is divided into 8 major drainage basins and a total of 18 subbasins together as described below.



- Subbasin A1 is located in the southwestern corner of the site, to the south and west of MS. The
  basin drains towards the southeast to proposed detention pond A. Current planning documents
  call for medium density dwelling units and a small pocket park. The basin is 37.00 acres, with a
  composite impervious value of 35.22% and runoff rates for the 5 and 100 year of 30.72 cfs and
  100.64 cfs respectively. The pond will discharge at predevelopment rates and into MS via the
  ponds outlet structure.
- Subbasin B1 is located between MS and MST2 to the east of subbasin A1. The basin drains towards the southeast and towards subbasin B2. Current planning documents call for medium density dwelling units and some parkland area. The basin is 37.00 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 29.46 cfs and 97.08 cfs respectively.
- Subbasin B2 is located between MS and MST2 to the northeast of subbasin A1. The basin drains towards the southeast and towards Detention Pond B. Current planning documents call for medium density dwelling units. The basin is 24.89 acres, with a composite impervious value of 43.26% and runoff rates for the 5 and 100 year of 12.02 cfs and 42.26 cfs respectively.
- Subbasin B3 is located between MS and EF and to the northeast of east of basin B2. The existing MST2 tributary runs through the basin. The site drains towards the southeast and towards Detention Pond B. Current planning documents call for high, medium-high, and medium density dwelling units along with a pocket park. The basin is 118.90 acres, with a composite impervious value of 49.42% and runoff rates for the 5 and 100 year of 92.76 cfs and 295.27 cfs respectively.
- Subbasin C1 is located to the northeast of east of basin B1 and the existing MST2 tributary runs through the middle of the basin. The basin drains towards the southeast and towards Detention Pond C. Current planning documents call for an institutional parcel, medium and high density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 51.20% and runoff rates for the 5 and 100 year of 77.99 cfs and 238.03 cfs respectively.
- Subbasin D1 is located between MS and MST2 to the east of Basin B3 and adjacent to the MST2 channel. The basin drains towards the southeast and towards drainage basin D2. Current planning documents call for medium density dwelling units along with a pocket park. The basin is 24.33 acres, with a composite impervious value of 53.89% and runoff rates for the 5 and 100 year of 24.15 cfs and 70.07 cfs respectively.
- Subbasin D2 is located between MS and MST2 to the south of basins D1 and B3. The basin drains towards the southwest and towards detention pond D. Current planning documents call for high density dwelling units along with a pocket park and a commercial parcel. The basin is 77.90 acres, with a composite impervious value of 62.10% and runoff rates for the 5 and 100 year of 98.47 cfs and 252.18 cfs respectively.
- Subbasin E1 is located just east of EFT along the northern portion of the site. The basin drains towards the southeast and towards basins F3 and F4. Current planning documents call for low density dwelling units. The basin is 88.60 acres, with a composite impervious value of 19.54% and runoff rates for the 5 and 100 year of 46.88 cfs and 178.04 cfs respectively.



- Subbasin F1 is located east of basin E1 and between EFT and EF along the northern portion of the site. The basin drains towards the southeast and towards basin F3 and F4. Current planning documents call for a large community park, high density dwelling units, commercial site and an institution parcel. The basin is 33.73 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 16.28 cfs and 58.95 cfs respectively.
- Subbasin F2 is located east of the existing drainage channel EFT. The basin drains towards the southwest and towards basin F4 and to the EFT drainage channel which runs parallel to the north east with Highway 24. Current planning documents call for high density dwelling units and commercial space. The basin is 67.64 acres, with a composite impervious value of 51.39% and runoff rates for the 5 and 100 year of 60.11 cfs and 170.90 cfs respectively.
- Subbasin F3 is located west of the existing drainage channel EF. The basin drains towards the southeast towards drainage channel EF but will be conveyed south towards subbasin F4. Current planning documents call for medium density dwelling units. The basin is 12.84 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 11.36 cfs and 32.93 cfs respectively.
- Subbasin F4 is located west of the existing drainage channel EF and south of subbasins F1 and F3. The basin drains towards the southeast towards detention pond F. Current planning documents call for medium and medium-high density dwelling units. The basin is 51.81 acres, with a composite impervious value of 49.54% and runoff rates for the 5 and 100 year of 42.32 cfs and 124.89 cfs respectively.
- Subbasin G1 is located west of the existing drainage channel EFT along the northern property boundary. The basin drains towards the southeast towards detention pond G. Current planning documents call for medium density dwelling units and a park. The basin is 20.13 acres, with a composite impervious value of 36.52% and runoff rates for the 5 and 100 year of 13.78 cfs and 43.95 cfs respectively.
- Subbasin G2 is located east of the existing drainage channel EFT along the northern property boundary. The basin drains towards the southeast towards detention pond G. Current planning documents call for low density dwelling units. The basin is 15.14 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 6.55 cfs and 23.95 cfs respectively.
- Subbasin H1 is located in the northeast corner of the site and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for low density dwelling units and smallpark. The basin is 20.71 acres, with a composite impervious value of 24.49% and runoff rates for the 5 and 100 year of 5.68 cfs and 27.62 cfs respectively.
- Subbasin H2 is located south of basin G2 and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for medium density dwelling units and smallpark. The basin is 18.55 acres, with a composite impervious value of 46.68% and runoff rates for the 5 and 100 year of 16.24 cfs and 47.62 cfs respectively.



- Subbasin H3 is located south of basin H2 and east of the existing drainage channel EFT. The basin drains towards the southeast towards subbasin H4. Current planning documents call for medium density dwelling units and smallpark. The basin is 6.01 acres, with a composite impervious value of 40.57% and runoff rates for the 5 and 100 year of 5.21 cfs and 15.60 cfs respectively.
- Subbasin H4 is located south of basin H2 and east of the existing drainage channel EFT and basin H3. The basin drains towards the south towards detention pond H. Current planning documents call for medium density dwelling units and park/open space area. The basin is 27.65 acres, with a composite impervious value of 38.24% and runoff rates for the 5 and 100 year of 20.93 cfs and 64.71 cfs respectively.

The above mentioned basins are large planning area basins and as drainage reports are developed for the individual developed parcels additional drainage reports and calculations will be required. It is expected that storm drainage infrastructure consisting of inlets, storm sewer and open drainage channels will be constructed as the property develops.

 Offsite Basins as shown in the Meridian Ranch MDDP include basins HG4, HG5, HG6A, HG6B, HG13, and HG14. Flow contributing to the site from these basins will be routed through the existing tributaries. Flow rates as shown in the MDDP Ranch report include the following flows and associated tributary areas.

	Offsite Flow Summary													
Basin Description	Ultimate Design Point	Basin Area (ac)	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)										
HG4	G6	57	Main Stem	2	42									
HG5	G6	72	Main Stem	3	52									
HG6A	G6	88	Main Stem	3	51									
HG6B	G6	66	Main Stem	2	35									
HG13	G08	54	Main Stem Tributary 2	4	59									
			Main Stem Tributary	-										
HG14	G08	147	2	5	83									

Offsite Flow Summary											
Design Point	Basin Area (ac)	Receiving Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)							
G6	760	Main Stem	36	628							
<u> </u>		Main Stem	_								

These basins along with the offsite basins which lie east of Eastoneville Road contribute flows onto the site through the major tributaries. Estimate oncoming flows for each tributary are as follows:



Offsite Flow Summary												
Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)										
Main Stem	36	628										
Main Stem Tributary 2	8	122										
East Fork Tributary*	56	116										
East Fork*	175	357										
*Flows from Gieck Ranch												

DBPS, Oct 2010

As hydraulic analysis continues for the channels, these offsite flows will be used to size the channels for proper conveyance of the flow however it should be noted that the flows mentioned for the Main Stem and Main Stem Tributary 2 assume proper conveyance of the flow through (below or above) Eastonville Road. Due to the unknown nature of these conditions at the time of buildout, a probable scenario of the split flows will require analysis and agreed upon flow rates to each channel will be required. Currently some of the flow shown going to the Main Stem Tributary 2 may be diverted into the Main Stem Tributary. Previous analysis done by JR Engineering assumed approximately 160 additional cfs going to the Main Stem Tributary #2 during the 100 year event and as such it is recommended the following flows be used for analysis of the oncoming offsite flows:

Revised Offsite Flow Summary											
5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)										
67	413										
59	280										
61	217										
180	595										
	ffsite Flow Sum 5 Year Peak Runoff (cfs) 67 59 61 180										

\*Flows from Gieck Ranch

DBPS, Oct 2010

\*\*Flows from 4 Way Ranch LOMR, Mar 2004

Please note that the preliminary drainage reports will be required to reconcile any differences between the various reports done for these channels.

#### b. Methodology

Design rainfall was determined utilizing figures from the NOAA Atlas 14, Volume 8, Version 2 to determine the 5-year and 100-year rainfall values for 1, 6 and 24-hour events. The 1-hour rainfall depths are 1.22 and 2.50 in/hr respectively, 6 hour 1.79 and 3.87 in/hr respectively and 2.36 and 4.90 in/hr for the 24 hour event. The rainfall values were then used as inputs into the Colorado Urban Hydrograph Procedure (CUHP) spreadsheets to determine runoff values for both pre-development and post-development site.

CUHP is an evolution of the Snyder unit hydrograph and is calibrated for use along the Colorado Front Range. 1 Hour rainfall amounts are input into the program to produce a storm hyetograph that is then uses to calculate a storm hydrograph for each basin depending on the subbasins properties including slope, length, shape, impervious area, pervious depression storage area, and various infiltration rates. Tabular hydrographs are then computed and can be used in EPA SWMM. The CUHP results are included within Appendix B.



EPA SWMM was used to determine flow routing via the kinematic wave method. Subbasins were routed to their respective design points and detention ponds for both the developed and predeveloped condition to determine peak runoff amounts for the 5-year and 100-year storm events. Information from these models along with information and calculations performed in the Colorado Springs BMP spreadsheets was used to determine pond sizing calculations and release rates.

#### c. Basin Hydrology

A summary of the flows for both the predeveloped and developed cases for each basin, subbasin and Pond are found on next page along with the full computation found in Appendix B.

SWMM Basin and Pond Summary												
	Basin		100 Year	5 Year Pond	100 Year Pond							
Basin	Area	%	Runoff	Peak Runoff	Volume (ac-	Volume (ac-						
Description	(ac)	Impervious	(cfs)	(cfs)	ft)	ft)						
A1	45.38	35.22%	30.72	100.64		•						
			Po	ond A	1.83	3.50						
B1	37.00	45.00%	29.46	97.08								
B2	24.89	43.26%	12.02	42.26								
B3	118.90	49.42%	92.76	295.27								
			Po	ond B	5.90	19.00						
C1	77.83	51.20%	77.99	238.03								
			Po	ond C	3.91	6.87						
D1	24.33	44.14%	24.15	70.07								
D2	77.90	62.10%	98.47	252.18								
			Po	ond D	6.61	10.19						
E1	88.60	19.54%	46.88	178.04								
			Po	ond E	1.96	2.44						
F1	33.73	25.00%	16.28	58.95								
F2	67.64	51.39%	60.11	170.90								
F3	12.84	45.00%	11.36	32.93								
F4	51.81	46.54%	42.32	124.89								
			Po	ond F	7.38	12.62						
G1	20.13	36.52%	13.78	43.95								
G2	15.14	25.00%	6.55	23.95								
			Po	ond G	0.72	2.03						
H1	20.71	24.49%	5.68	27.62								
H2	18.55	43.68%	16.24	47.62								
H3	6.01	40.57%	5.21	15.60								
H4	27.65	38.24%	20.93	64.71								
			Po	ond H	2.93	6.17						



# IV. Hydraulic Analysis

#### a. Major Drainageways

In general the site runoff runs into the 4 major drainageways and in a southeasterly direction. These basins are described in more detail below:

The Main Stem (MS) in the south western portion of the site, the Main Stem Tributary #2 (MST2) to the north and east of the Main Stem, the East Fork Tributary (EFT) in the middle of the site north and east of MST2, and the East Fork Upper (EF)

The Main Stem (MS) is in the southwestern portion of the site. Offsite flows collect and are conveyed under Eastonville Road via a culvert. MS travels in a southeasterly direction and combines with the Main Stem Tributary #2 (MST2) just off site and then is conveyed past Highway 24 via a culvert. Jurisdictional wetlands exist within this channel and the area is within a Zone A floodplain towards the southern portion of the site. This channel sees only intermittent flows at this time however once development occurs there may be a more constant baseflow.

MST2 crosses Eastonville road via an existing culvert and flows through the site in a southeasterly direction. An existing breached stock pond exists in the approximate center point of the channel within the site. Portions of this channel are within a mapped floodplain as shown in the existing FIRM Panel. Per a July email from the USACE this drainage channel was determined to be a non-jurisdictional waters/wetland.

The East Fork tributary (EFT) crosses the north property line and are conveyed through the site via a natural channel. The channel has been mapped as a Zone A floodplain per the existing FIRM panel. There is no existing crossing for this section of the drainage channel below Highway 24 and instead the flows are conveyed to the north east towards the East Fork Upper (EF). Per a July email from the USACE this drainage channel was determined to be a non-jurisdictional waters/wetland.

The EF crosses the north property line approximately 1500' east of the EFT crossing. The flow through the site is via a natural channel and travels in a southeasterly direction. The channel is mapped as a Zone A floodplain, and the channel crosses Highway 24 via an existing shallow bridge. The EF and EFT eventually merge approximately 1750 southeast of the site, however as mentioned above Highway 24 blocks the flow of the EFT and flows are conveyed northeast to the EF bridge crossing.

Per SWMM modeling the current velocities will require channel stabilization. The channels are to be engineered later in the design which will likely include a combination of channel widening, lowering of slope facilitated by the implementation of drop structures to meet non erosive velocity requirements. Bank stabilization, should it be necessary, may include coir rolls, erosion control blankets, live willow staking, soil lifts and/or other measures to ensure successful bank stabilization. These drainageways will require further analysis and design which will be completed as the project progresses.

# V. Environmental Evaluations

### a. Significant existing or potential wetland and riparian areas impacts

As part of this work, the developer has engaged Ecosystem Services, LLC (ECOS) to perform environmental studies of the site that will be submitted with the planning documents. Major information from these report related to the wetlands shows that two of the tributaries trough the site, the Main Stem





and the East Fork contain jurisdictional wetlands and the other two tributaries, the East Fork Tributary and the Main Stem Tributary #2 are non-jurisdictional wetlands.

At this time, only minor improvements to the jurisdictional channels are proposed. These stream improvements will be made with keeping the natural habitat intact and the natural function of these channels as it is to maintain the wetland habitat. The non-jurisdictional channels will be modified and the design of those channels is forthcoming.

#### b. Stormwater quality considerations and proposed practices

As part of the development, full spectrum detention facilities will be installed to provide water quality for the development. The facilities will be designed using El Paso County criteria and provide stormwater quality by slowing the release of stormwater captured by the ponds and allowing solids to settle out. Additionally when possible the revised drainage channels, which were not jurisdictional wetlands, will be used to convey stormwater via a natural channel. Stormwater must be treated before entering the natural channels. The natural channel will provide an pervious means to transport stormwater and provide some water quality benefits as well.

On site practices for the homes, schools, churches and other buildings should use means such that impervious areas drain across pervious area to allow for infiltration during the minor events. This would include discharge of the gutters onto landscape areas vs. directly connecting to storm sewer and using natural ditches and swales where it is logical and makes sense to convey stormwater inlieu of storm sewer piping.

#### c. Permitting requirements

When work infringes upon the wetlands or floodplain a 404 Permit will be required. If the work within the waterways is minimal, it will likely be covered under a nationwide 404 permit; it is however possible that an individual permits will be required.

The Colorado Department of Public Health and Environment will require permits for any disturbance that exceed 1 acre of land. Should groundwater be encountered, a dewatering permit will also be required.

El Paso County will require an Erosion and Stormwater Quality Control Permit and any other construction permits required to complete the construction of the site.

FEMA will require a permit for floodplain development prior to the commencement of any construction or development within any special flood hazard area (SFHA).

FEMA will require a letter of map revision (LOMR) should work alter the base flood elevation (BFE) of any area falling withing the floodplain as shown in FEMA FIRM 08041C0556G and FIRM 08041C0552G (eff. 12/7/2018).

#### d. 4-Step Process

In accordance with the Engineering Criteria Manual I.7.2.A and DCM V2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume, and considering the need for Industrial Commercial BMPs.



Step 1 – Reducing Runoff Volumes: The development of the project site includes a variety of land uses including open and vegetated areas interspersed to help disconnect imperious areas and reduce runoff volumes.

Step 2 – Stabilize Drainageways: Altered channels will be designed in a manner that provides water quality benefits through infiltration and the removal of pollutants via phytoremediation. Vegetation will also be selected to stabilize the channel by reducing the velocity of flows and decreasing any scour. Should the final channel require, grade control structures may be implemented to further reduce flow velocities and protect against erosion. These improvements will help stabilize drainageways.

Step 3 – Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

Step 4 – Consider the need for Industrial and Commercial BMP's: A site specific storm water quality and erosion control plan and narrative will be prepared with subsequent land use approvals prepared in conjunction with the report prior to any construction. Site specific temporary source control BMPs as well as permanent BMPs are detailed in this plan and narrative. Guidelines detailed in the El Paso DCM V2 4.2 pertaining to the covering and storage handline and spill containment and control shall be followed as necessary.

### VI. Selected Plan

### a. Plan Hydrology

This MDDP schematically addressed on-site and off-site drainage patterns using the existing topography and proposed land use plan for the overall drainage design. Individual preliminary and final drainage reports will better define the planning areas as the site is developed. These reports will include inlet design, storm sewer hydraulics, street design and other requirements typical of more detailed drainage reports.

The overall site is divided into 8 separate major basins, basins A-H and contribute to individual detention ponds for each major basin. Basin sizes range from 35 acres to 181 acres in size. Basins A, B, C and D drain and eventually discharge into the Main Stem and Main Strem Tributary #2. Basins E, F, G, and H drain towards the East Fork Drainage channel.

The sub-basins are described in additional detail above.

#### **b.** Detention Ponds

The site plans propose the construction of 8 separate full spectrum detention facilities.

- Pond A is located in the southwest corner of the site and discharges into the Main Stem drainageway. The pond is planned to store a maximum of 4.05 ac-ft during the 100 year event and have a peak outflow of 55.9 cfs which is slightly below the pre development peak outflow of 57.1 cfs. The 5 year storage volume is 2.46 ac-ft with a peak outflow of 3.7 cfs.
- Pond B is located to the east of Pond A and the Main Stem and discharges into the Main Stem Tributary #2. The pond is planned to store a maximum of 16.60 ac-ft during the 100 year event and have a peak outflow of 165.4 cfs which is slightly above the pre development peak outflow of 164.2 cfs. The 5 year storage volume is 8.44 ac-ft with a peak outflow of 2.6 cfs.



- Pond C is located near the center of the western portion of the site near the existing Main Stem Tributary #2. The pond discharges into a revised open channel to be designed and discharges to the Main Stem Tributary #2 which merges with the Main Stem Tributary just off site. The pond is planned to store a maximum of 6.91 ac-ft during the 100 year event and have a peak outflow of 119.2 cfs which is slightly below the pre development peak outflow of 120.2 cfs. The 5 year storage volume is 4.07 ac-ft with a peak outflow of 1.5 cfs.
- Pond D is located near the southern portion of the site adjacent to Highway 24. The pond discharges into the Main Stem right after the Main Stem and Main Stem Tributary #2 merge. The pond is planned to store a maximum of 9.41 ac-ft during the 100 year event and have a peak outflow of 154.4 cfs which equals the predevelopment peak flow rate. The 5 year storage volume is 6.28 ac-ft with a peak outflow of 2.0 cfs.
- Pond E is located in the middle of the site just east of the East Fork drainage way. The pond discharges into the East Fork drainageway. The pond is planned to store a maximum of 2.40 acft during the 100 year event and have a peak outflow of 163.4 cfs which is greater than the pre development peak outflow of 157.99 cfs. The 5 year storage volume is 1.70 ac-ft with a peak outflow of 18.8 cfs.
- Pond F is located near the south east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 12.40 ac-ft during the 100 year event and have a peak outflow of 235.5 cfs which is greater than the pre development peak outflow of 221.11 cfs. The 5 year storage volume is 8.07 ac-ft with a peak outflow of 14.5 cfs.
- Pond G is located near the north east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway at an upstream location within the site. The pond is planned to store a maximum of 2.54 ac-ft during the 100 year event and have a peak outflow of 50.7 cfs which is slightly greater than the pre development peak outflow of 48.48 cfs. The 5 year storage volume is 1.69 ac-ft with a peak outflow of 9.1 cfs.
- Pond H is located near the south east corner of the site just east of the East Fork Tributary drainageway and adjacent to Highway 24. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 6.60 ac-ft during the 100 year event and have a peak outflow of 99.1 cfs which matches the pred development peak outflow. The 5 year storage volume is 4.03 ac-ft with a peak outflow of 1.3 cfs.

Overall runoff from the site will by and large match the predevelopment peak flows. The volume of water will increase however as the drainage channels are designs, continuous simulation models will be done to see the effects of prolonged runoff rates. Predevelopment and post development flows for the 5-year and 100-year events are summarized in the following table for the 4 site outfalls.



OUTFALL	Predev	elopment	Postdevelopment*					
OUTFALL	5 year	100 year	5 year	100 year				
1	80.03	479.80	67.69	466.95				
2	85.96	597.41	61.68	536.11				
3	30.00	154.35	8.58	160.70				
4	341.05	1335.77	276.10	1291.25				

\*Values to be refined with Preliminary and Final Drainage Reports for each filing

### VII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

### VIII. Summary

Grandview Reserve is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development increased runoff will occur. In order to mitigate downstream impacts 8 large full spectrum detention facilities will be built to reduce the runoff rate to near historic levels. These detention facilities will provide water quality enhancements in order to account for the increased urbanization of the upstream catchment areas.

Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and be included in future submittals. The proposed design, as described in this report, is not anticipated to cause any adverse impact to downstream properties however as noted previously due to the increased volume of water, downstream tributaries will see increases in the volume of flow. It is advised that low impact design be taken into account when designing and developing each filing. This shall include those items listed in the four step process above and any additional measures that are within reason to disconnect impervious areas and increase infiltration. This will alleviate the additional volume of water due to development. Although the rate will remain at or below historic levels, the amount of time the channels will see water will increase which may cause more channel movement than historic. Downstream planning efforts should allow for the natural migration and movement of the channel by continuing to provide large floodplain areas to allow movement of the channel.



### IX. References

El Paso County - Drainage Criteria Manual, 2014

City of Colorado Springs - Drainage Criteria Manual, May 2014

Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

Unnamed Tributary Black Squirrel Cree, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004

Haegler and Gieck Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004

Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006

Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)

EPC Engineering Criteria Manual (Appendix I updated July, 2019)

Meridian Ranch MDDP, January 2018



Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix A





the task as it's drance of heap qualed or exceeded in any envirow. The special flood hearand Area is the area subject. In flooring by the 1% annual charce flood. Areas of Special flood hazard include Zones, A.E. AH, AO, AO, AO, AO, V and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual charce flood. ZONE A. No Base Flood Elevations determined. ZONE A. Base Flood Elevations determined.	ZONE AN Prood deptise of 1 to 3 feet (usually areas of ponding); Base flood Bendors determined. ZONE AD Food deptise floot 3 feet (usually areas of sping terrains) areage dentise determined. To 2 feet (usual floot floot and usual from the set of a set of the set o	determined. Special Parad Atea Formerly protected from the 1% annual chance not by a flood corand system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to	ZONE A99 Area to be protected from 1% annual cuarter froot by a Federal flood protection be protected from 1% annual charter flood by a Federal flood protection system under construction; no Base Flood Elevations determined.	ZONE V Cossial flood zone with velocity hazard (wave action); no Base Flood Bevations determined. ZONE VE Cossial flood zone with velocity hazard (wave action); Base Flood	Elevators determined.	The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.	OTHER FLOOD AREAS Areas of U.S.A mausi ontension food; areas of 1% annual chance flood with areage deptis of less than 1 foot or with dialingge areas less than 1	square mile; and areas protected by levees from 1% annual chance flood.  OTHER AREAS	ZONE X Areas determined to be outside the 0.2% annual chance floodplain. ZONE D Areas in which flood hazards are undetermined, but possible.	COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS	OTHERWISE PROTECTED AREAS (OPAs)     OTHERWISE PROTECTED AREAS (OPAs)     Another in Second Harver datase	How and the second s	Come D Boundary     Care S Boundary     Care S and OPA boundary	Boundary dividing Special Flood Hazard Areas of different Base     Boundary dividing Special Flood Hazard Areas of different Base     Boundary Dividing Special Floor Areas of the	<ul> <li>31.3 Base Flood Elevation mile and value; elevation in teet- (EL 987) Base Flood Elevation value where uniform within zone; elevation in feet.</li> </ul>	* ketterended to the North American Vertical Jakum of 1988 (NAVID 58)	(23)(23) Transect line print (77 30 000)	32° 22° 30.00° Datim of 1982 (MJD 53) 475 <sup>3000</sup> -N 1000-meter Universal Transverse Mercator grid ticks, 2008 13	600000 FT 500-foot prid ticks: Colorado State Plane coordinate states carato and ticks: Colorado State Plane coordinate Janhar Conformat Coor Plancerbox 2023.	DX5510 Bentance community care inspection bins FRM parents	• M1.5 River Mile	MAP REPOSITORIES Refer to May preparatives area for Mup Index EFFECTIVE DATE of COUNTINUMP FLOOR TRUSTANCE RETTE MAP	EFFECTIVE DATE(s) OF REVISION(s) TO THIS PANEL DECEMBER 7, 2019 - to update motione immals, us oblate applications and Special Flood Hazard Areas, to update motion map format, to add creads and to Special Flood Hazard Areas, to update motions its started Letters of Map Revision.	For community map revision history prior to countywide mapping, refer to the Community Map History Table Kocated in the Flood Tissuance Study report for this jurisdiction. Coll externment if Roman Even Coll Resume Revision and 1.400-658 6630.		MAP SCALE 1*= 500           250         0           261         100           274         100	150 0 150 300 ETERS	PANEL 0556G	And Link     FIRM       FILD ASO COUNTY,     FLOOD INSURANCE RATE MAP       FLOOD INSURANCE RATE MAP     FLOOD INSURANCE RATE MAP       FLOOD INSURANCE RATE RATE MAP     FLOOD INSURANCE RATE MAP       FLOOD INSURANCE RATE MAP     FLOOD INSURANCE RATE MAP       FLOOD INSTITUTION RATE RATE RATE RATE RATE RATE RATE RATE	
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To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **Chodways** have been determined. users are necrourged to consult the Flood Profiles and Floodway. Data and/or Summary of Sillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be avaite that EFEs shown on the FIRM represent rounded whole-floot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation in thereford should not be used as the sole source of flood elevation information. Accordingly, the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0 North Ametican Victual Datum of 1980 (NAVDBD). Users of this FRM should be aware that coastal flood elevations are also provided in the Summary of Sillivater Elevations table in the Flood insurance Study report for this jurisdution. Elevations and/or floodpala managore flewations table in the Summary of Sillivater Elevations table should be used for construction and/or floodpala managore Sillivater Elevations table should be used for construction and/or floodpalin management purposes when they are higher than the elevations shown on this FIRM.

1425000 FT

Boundaries of the **floodways** were computed at cross sections and interpolated between the section of the secti

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refet to section 2.4 Flood Protection the servers of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

the The projection used in the preparation of this map was Universal Transve transversion (UIX) more 13. The proceeding adam was Nonversal Transve Differences in datum, spheroid, projection or UTX zones zones used in differences in map datemt jurisicitoris may result in slight positio differences in map features across jurisicitoris may result in slight positio differences of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum** of 1388 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same worklaad fatum. For finamation regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.garioaa.gov/ or contact the National Geodetic Survey at the following address.

NGS Information Services NOAA, NNGS:12 National Geodetic Survey SSMC-3, #2002 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **banch marks** shown on this map, please contact the information Sprevices Statent of the National Geodetic Survey at (201) 71:5-522 or visit its websile at http://www.ngs.nota.gov/

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodpain defineations have house shown on the pervious FIRM for his jurisdiction. The floodpains and floodways that were transferred from the previous. FIRM may have been adjusted to controm to these new stream channel confluations. FIRM may have been adjusted to conform to these new stream channel confluations. As a result, the Flood Perfiels and Floodway Data tables in the Prodo flustance Study Report (which contains authoritative hydraulic data) may reflect stream channel datances that effer from what is shown on this map. The profile baselines depicted on this map. Propriesent the hydraulic conding baselines that match the flood profiles pared Floodway Data Tables in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to amaxashors or de-amexations may have concurred after this map was published. map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county strowing the layout of map panets; community map repository addresses; and a Listing of Community and Program dates for each community as well as a listing of the panets on which each community is located. Contact FEMA Map Service Center (INSC) via the FEMA Map Information eXchange (FMIX). Available spoulds? for information on available products are with this FIRM. Available spoulds? for information on available products for the Available spoulds. The available products may include previously issued Letters of Map Change. a flood intransme SLUX Report, and/or digital versions of this map. The MSC may also be transfed by Fax at 1-800-359-9520 and its website at Mtp://www.msc.fema.gov/

i you have **questions about this map** or questions concerning the National Flood nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or isit the FEMA website at http://www.fema.gov/business/infp.

site at http://www.reune.g-... El Paso County Vertical Datum Offset Table Vertsal Datum Offset (ft)

Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map

 $\vdash$  This Digital Flood Insurance Rate Map (DFIRM) was produced through a propriating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

104° 39° 0' 0.00"

JOINS PANEL 0552

1420000 FT

1415000 FT 38° 58' 7.50"



39° 0' 0.00"

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **Codevays** the ween determined, users are necouraged to consult the Flood Profiles and Floodvay. Data and/or Summary of Sillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be avaite that EFEs shown on the FIRM represent runded whole-doot elevations. These BFEs are interheded for flood insurance rating purposes only and should not be used as the sole score of flood dimstranet resting purposes only and should not be used as the sole score of flood dimstranet relation and the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only andward of 0.0 North shown Vertical Data of 1988 (NNVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Silivatar Elevations table in the Flood instance Study report of this landiculon. Elevations shown in the summary of Silivatar Elevations table should be used for construction and/or floodpain management purposes when they are higher than the elevations shown on floodpain.

1425000 FT

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway region for and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transver-tionation (UTIN) across 13. The proceeding adam was Universal Transver Differences in datum, spheroid, projection of UTIN zones zones used in 1. Differences in map data-met jurisicitions may result in slight positio differences in map features across jurisicitions may result in slight positio differences in map features across jurisicition boundaries. These differences do affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum** of **1388 (NAVD88)**. These flood elevations must be compared to structure and ground elevations telenced to the same workland faturn. For findmation regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address.

NGS Information Services NOAA, NNIGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks strown on this map, please contact the information Services Batchen of the National Geodetic Survey at (301) 713-3224 or visit its website at http://www.ngs.noaa.gov/

Base Map information shown on this FIRM was provided in digital format by EI Paso County. Clostods Ostings Utilities (by of Foruntia Bureau of Land Management, National Oceanic and Armospheric Administration. United States Geological Survey, and Anderson Consulting Engineers, inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodpain defineations that those shown on the provuse FIRM form ins jurisdiction. The floodpains and floodways that were transfered from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Sludy Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from with its shown on this map. The profile baselines supplication on this map. The professor the hydraulic modeling baselines that match the flood profiles baselines may devide significantly from the new base map channel representation and may appear outside of the floodplain.

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Please refer to the separately printed **Map Index** for an overview map of the count princip the kyport or map patients, community map repository addresses; and . Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is cated. Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMX), 1-277-355-255-71 minimum structure on available products may include previously issued Letters of Map 20 range, a Flood Insurance SUby Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9520 and its website at http://www.mscfema.govi.

you have questions about this map or questions concerning the National Flood surance Program in generic, please call **1877-Fload MAP** (1-877-335-2627) or an thor cart workshot an home investigation and intervention of the structure of the struc am in ebsite

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION ical Datum Offset (ft) El Paso County Vertical Datum Offset Table Vertic Flooding Source

Panel Location Map

This Digital Flood Insurance Rate Map (DFIRM) was produced through a propriating Technical Partner (CTP) agreement between the State of Colorado Water Constration Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

1415000 FT 38° 58' 7.50"

1420000 FT

101NS PANEL 0551



USDA Natural Resources

**Conservation Service** 



USDA

### Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.4	2.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	450.7	52.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	385.4	44.9%
Totals for Area of Interest			858.5	100.0%

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



# **EAST FORK**

 Region ID:
 CO

 Workspace ID:
 C020200817220340831000

 Clicked Point (Latitude, Longitude):
 38.99090, -104.54663

 Time:
 2020-08-17 16:03:57 -0600



Grandview Reserve

#### **Basin Characteristics**

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	4	percent
DRNAREA	Area that drains to a point on a stream	0.84	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4.9	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.86	inches

Parameter Code	Parameter Description	Value	Unit
RCN	Runoff-curve number as defined by NRCS (http://policy.nrcs.usda.gov/OpenNonWebContent.aspx? content=17758.wba)	58.28	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.22	dimensionless

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Application Version: 4.4.0

### EAST FORK TRIBUTARY BASIN DELINATION

 Region ID:
 CO

 Workspace ID:
 CO20200817220732890000

 Clicked Point (Latitude, Longitude):
 38.99085, -104.55989

 Time:
 2020-08-17 16:07:50 -0600



Grandview Reserve

#### **Basin Characteristics**

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	3	percent
DRNAREA	Area that drains to a point on a stream	0.22	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4.92	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.86	inches

Parameter Code	Parameter Description	Value	Unit
RCN	Runoff-curve number as defined by NRCS (http://policy.nrcs.usda.gov/OpenNonWebContent.aspx? content=17758.wba)	54.53	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.23	dimensionless

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Application Version: 4.4.0

# **MAIN STEM**

 Region ID:
 CO

 Workspace ID:
 C020200817221517278000

 Clicked Point (Latitude, Longitude):
 38.98969, -104.56703

 Time:
 2020-08-17 16:15:34 -0600



Grandview Reserve

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	3	percent
DRNAREA	Area that drains to a point on a stream	0.17	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.87	inches

Parameter Code	Parameter Description	Value	Unit
RCN	Runoff-curve number as defined by NRCS (http://policy.nrcs.usda.gov/OpenNonWebContent.aspx? content=17758.wba)	55.04	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.22	dimensionless

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Application Version: 4.4.0

# **MAIN STEM TRIBUTARY NUMBER 2**

 Region ID:
 CO

 Workspace ID:
 CO20200817221139984000

 Clicked Point (Latitude, Longitude):
 38.99101, -104.56354

 Time:
 2020-08-17 16:11:57 -0600



Basin Characteristics		Grandview Reserve		
Parameter Code	Parameter Descriptio	n	Value	Unit
BSLDEM10M	Mean basin slope cor	mputed from 10 m DEM	3	percent
DRNAREA	Area that drains to a	point on a stream	0.44	square miles
I24H100Y	Maximum 24-hour pre once in 100 years	ecipitation that occurs on average	4.94	inches
I24H2Y	Maximum 24-hour pre once in 2 years - Equi index	ecipitation that occurs on average valent to precipitation intensity	1.87	inches

Parameter Code	Parameter Description	Value	Unit
RCN	Runoff-curve number as defined by NRCS (http://policy.nrcs.usda.gov/OpenNonWebContent.aspx? content=17758.wba)	56.49	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.23	dimensionless

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Application Version: 4.4.0



Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix B
Basin	Park/Open	High					Total	Total	Composite Percent	Predominant Soil	5 Year C	100 Year
Description	Space	Density/Schools	Med/High Density	Med Density	Low Density	Commercial	Impervious	Acreage	Impervious	Group	Factor	C Factor
Impervious Percentage	10%	65%	55%	45%	25%	75%						
A1	12.68	0.00	0.00	32.70	0.00	0.00	15.98	45.38	35.22%	В	0.38	0.71
					Poi	nd A		45.38	35.22%			
B1	0.00	0.00	0.00	37.00	0.00	0.00	16.65	37.00	45.00%	A	0.4	0.61
B2	1.24	0.00	0.00	23.65	0.00	0.00	10.77	24.89	43.26%	A	0.38	0.59
B3	7.42	12.64	53.20	45.64	0.00	0.00	58.76	118.90	49.42%	А	0.36	0.5
					Po	nd B		180.79	47.66%			
C1	4.19	30.61	1.70	41.33	0.00	0.00	39.85	77.83	51.20%	A	0.38	0.59
					Po	nd C		77.83	51.20%			
D1	0.60	0.00	0.00	23.73	0.00	0.00	10.74	24.33	44.14%	A	0.39	0.6
D2	5.60	64.10	0.00	0.00	0.00	8.20	48.38	77.90	62.10%	А	0.39	0.6
					Poi	nd D		102.23	57.82%			
E1	32.26	0.00	0.00	0.00	56.34	0.00	17.31	88.60	19.54%	В	0.12	0.59
					Po	nd E		88.60	19.54%			
F1	0.00	0.00	0.00	0.00	33.73	0.00	8.43	33.73	25.00%	В	0.15	0.61
F2	18.34	40.50	0.00	0.00	0.00	8.80	34.76	67.64	51.39%	В	0.36	0.7
F3	0.00	0.00	0.00	12.84	0.00	0.00	5.78	12.84	45.00%	В	0.45	0.74
F4	6.24	0.00	29.80	15.77	0.00	0.00	24.11	51.81	46.54%	В	0.37	0.64
					Ро	nd F		166.02	44.02%			
G1	4.88	0.00	0.00	15.25	0.00	0.00	7.35	20.13	36.52%	В	0.25	0.66
G2	0.00	0.00	0.00	0.00	15.14	0.00	3.79	15.14	25.00%	В	0.45	0.74
					Poi	nd G		35.27	31.57%			
H1	0.70	0.00	0.00	0.00	20.01	0.00	5.07	20.71	24.49%	A	0.38	0.75
H2	0.70	0.00	0.00	17.85	0.00	0.00	8.10	18.55	43.68%	В	0.43	0.75
H3	0.76	0.00	0.00	5.25	0.00	0.00	2.44	6.01	40.57%	В	0.4	0.72
H4	5.34	0.00	0.00	22.31	0.00	0.00	10.57	27.65	38.24%	В	0.37	0.7
					Poi	nd H		72.92	35.91%			

## Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

_				Unit	t Hydrograp	oh Paramet	ers and Res	sults			Excess	Precip.		Storm Hy	/drograph	
					W50		W75	Time to					Time to		Total	Runoff per
				W50	Before	W75	Before	Peak		Volume	Excess	Excess	Peak	Peak Flow	Volume	Unit Area
Catchment Name/ID	User Comment for Catchment	СТ	Ср	(min.)	Peak	(min.)	Peak	(min.)	Peak (cfs)	(c.f)	(inches)	(c.f.)	(min.)	(cfs)	(c.f.)	(cfs/acre)
A1		0.157	0.143	37.3	5.59	19.4	3.95	9.3	57	164,729	0.25	40,666	35.0	13	40,592	0.29
B1		0.158	0.131	33.0	4.82	17.2	3.41	8.0	53	134,310	0.08	11,390	35.0	4	11,363	0.12
B2		0.158	0.109	58.5	6.42	30.4	4.54	10.7	20	90,351	0.08	7,662	40.0	2	7,665	0.07
B3		0.158	0.221	39.1	8.15	20.3	5.76	13.6	142	431,607	0.08	36,602	40.0	12	36,572	0.10
C1		0.158	0.183	30.3	5.75	15.7	4.06	9.6	120	281,797	0.08	23,898	35.0	10	23,870	0.13
D1		0.157	0.108	31.5	4.11	16.4	2.91	6.9	36	88,318	0.25	21,803	35.0	8	21,721	0.33
D2		0.157	0.182	37.7	6.77	19.6	4.78	11.3	97	282,777	0.25	69,809	40.0	22	69,820	0.29
E1		0.157	0.193	28.9	5.77	15.0	4.08	9.6	144	321,618	0.25	79,397	35.0	32	79,287	0.37
F1		0.157	0.125	37.2	5.07	19.4	3.58	8.5	42	122,440	0.25	30,227	35.0	10	30,151	0.29
F2		0.157	0.171	45.1	7.42	23.5	5.24	12.4	70	245,533	0.25	60,614	40.0	16	60,563	0.24
F3		0.157	0.081	37.8	3.84	19.6	2.72	6.4	16	46,609	0.25	11,506	35.0	4	11,472	0.28
F4		0.157	0.151	43.2	6.52	22.5	4.61	10.9	56	186,981	0.25	46,160	40.0	13	46,174	0.25
G1		0.157	0.099	38.8	4.45	20.2	3.14	7.4	24	73,072	0.25	18,039	35.0	6	17,996	0.28
G2		0.157	0.087	42.3	4.33	22.0	3.06	7.2	17	54,958	0.25	13,567	35.0	4	13,536	0.26
H1		0.158	0.101	43.7	4.89	22.7	3.45	8.1	22	75,177	0.08	6,375	35.0	2	6,365	0.09
H2		0.157	0.095	37.0	4.21	19.2	2.97	7.0	24	67,337	0.25	16,623	35.0	5	16,581	0.29
H3		0.157	0.057	32.6	2.94	16.9	2.08	4.9	9	21,816	0.25	5,384	35.0	2	5,324	0.32
H4		0.157	0.114	36.7	4.72	19.1	3.33	7.9	35	100,370	0.25	24,778	35.0	8	24,718	0.29

#### Printouts for Storm Hydrographs

	flow in cfs																	
in minutes																		
ime	7	11	g	8	7	5	5	1	ಗ	2	'n	5	15	5	루	7	φ	4
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	0.00	0.00	0.00	0.01	0.01	0.00	0.01	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25	4.37	0.49	0.15	0.79	0.97	3.50	6.05	10.68	3.53	3.91	1.60	3.64	2.24	1.57	0.20	2.24	0.93	3.12
30	10.53	3.60	1.09	6.02	7.25	7.38	16.27	26.19	8.12	11.07	3.32	9.60	4.86	3.39	1.51	4.78	1.85	6.93
35	13.03	4.33	1.65	10.87	9.95	8.12	21.83	32.34	9.70	15.57	3.65	12.69	5.57	3.87	1.85	5.37	1.92	8.07
45	11.55	3.53	1.62	11.26	7.98	6.50	20.38	26.01	8.49	15.82	3.11	12.23	4.86	3.47	1.67	4.59	1.53	6.96
50	10.17	3.04	1.54	10.00	6.77	5.67	17.95	22.15	7.48	14.39	2.76	11.00	4.32	3.11	1.50	4.06	1.35	6.14
55	9.05	2.66	1.43	8.60	5.79	4.90	15.88	18.86	6.66 5.88	12.88	2.47	9.83	3.87	2.81	1.33	3.61	1.17	5.45
65	7.10	2.03	1.20	6.77	4.36	3.80	12.42	14.16	5.23	10.56	1.95	8.00	3.08	2.27	1.09	2.84	0.92	4.27
70	6.40	1.81	1.12	5.94	3.79	3.34	11.15	12.11	4.73	9.49	1.77	7.19	2.79	2.06	0.98	2.57	0.82	3.86
75	5.77	1.58	1.04	5.41	3.22	2.88	10.06	10.06	4.26	8.60	1.60	6.55	2.52	1.88	0.89	2.31	0.71	3.47
85	4.50	1.30	0.90	4.88	2.00	2.41	7.91	6.93	3.32	7.26	1.42	5.45	2.27	1.56	0.82	1.79	0.50	2.68
90	3.87	0.93	0.82	3.84	1.88	1.73	6.84	6.11	2.85	6.61	1.08	4.92	1.75	1.39	0.68	1.53	0.43	2.28
95	3.26	0.83	0.77	3.32	1.69	1.55	5.78	5.38	2.41	5.96	0.91	4.39	1.50	1.23	0.61	1.30	0.38	1.94
100	2.83	0.75	0.72	2.81	1.50	1.38	4.97	3.95	2.10	4.67	0.79	3.85	1.29	0.92	0.54	1.14	0.35	1.70
110	2.35	0.60	0.63	2.21	1.12	1.06	4.09	3.25	1.74	4.03	0.66	2.90	1.06	0.82	0.40	0.95	0.27	1.41
115	2.13	0.53	0.58	2.03	0.93	0.90	3.72	2.54	1.58	3.55	0.60	2.63	0.97	0.76	0.36	0.86	0.24	1.27
120	1.92	0.45	0.53	1.86	0.74	0.74	2.99	1.84	1.42	3.04	0.54	2.44	0.88	0.70	0.34	0.77	0.20	1.14
130	1.49	0.30	0.44	1.50	0.36	0.43	2.63	0.49	1.10	2.81	0.43	2.07	0.71	0.59	0.29	0.59	0.13	0.87
135	1.28	0.22	0.39	1.33	0.17	0.27	2.27	0.14	0.94	2.59	0.37	1.89	0.62	0.53	0.26	0.51	0.09	0.74
140	1.06	0.15	0.35	1.15	0.01	0.12	1.91	0.06	0.79	2.37	0.31	1.71	0.53	0.48	0.24	0.42	0.05	0.61
150	0.64	0.01	0.31	0.80	0.01	0.01	1.19	0.03	0.47	1.94	0.20	1.35	0.36	0.37	0.19	0.25	0.01	0.34
155	0.43	0.00	0.29	0.62	0.01	0.01	0.84	0.02	0.32	1.72	0.14	1.17	0.28	0.32	0.17	0.16	0.00	0.21
160	0.22	0.00	0.28	0.45	0.00	0.01	0.48	0.02	0.16	1.51	0.08	0.99	0.19	0.26	0.15	0.07	0.00	0.09
170	0.03	0.00	0.24	0.11	0.00	0.00	0.06	0.01	0.02	1.07	0.01	0.64	0.04	0.15	0.10	0.01	0.00	0.01
175	0.01	0.00	0.23	0.01	0.00	0.00	0.03	0.00	0.01	0.86	0.00	0.46	0.01	0.10	0.07	0.01	0.00	0.01
180	0.01	0.00	0.21	0.01	0.00	0.00	0.02	0.00	0.01	0.64	0.00	0.28	0.01	0.05	0.05	0.00	0.00	0.01
190	0.01	0.00	0.18	0.00	0.00	0.00	0.01	0.00	0.00	0.22	0.00	0.03	0.00	0.01	0.01	0.00	0.00	0.00
195	0.00	0.00	0.16	0.00	0.00	0.00	0.01	0.00	0.00	0.07	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00
200	0.00	0.00	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
205	0.00	0.00	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
215	0.00	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
220	0.00	0.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
230	0.00	0.00	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
235	0.00	0.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
240	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
250	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
255	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
260	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
205	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
275	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
280	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
285 290	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
295	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
300	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
305	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
315	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
320	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
325	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
335	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
340	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### Printouts for Unit Hydrographs

	flow in cfs																	
ne in minutes																		
tin	A1	B1	B2	B3	1	D1	D2	E1	F1	F2	F3	F4	61	62	H1	Н2	H3	44 14
5	40.28	42.09	12.13	63.61	82.42	32.48	55.24	98.24	32.62	35.61	14.87	33.35	20.73	14.60	17.60	20.82	8.64	28.84
10	57.05	52.23	19.82	128.67	120.14	35.66	95.11	143.90	42.37	66.66	15.76	55.34	24.18	16.70	22.15	23.32	8.39	35.18
15	55.14	49.14	19.80	142.11	113.71	32.86	95.34	135.22	40.64	69.88	14.91	55.08	23.11	16.08	21.50	22.10	7.65	33.53
20	50.23	42.59	19.29	135.55	96.28	27.58	88.48	111.47	36.78	67.16	13.37	52.19	21.00	14.87	20.10	19.77	6.45	30.09
25	42.58	36.47	18.42	120.63	81.39	24.10	76.12	94.77	31.35	61.81	11.56	47.11	18.05	13.08	17.96	17.02	5.72	25.74
30	38.19	31.93	17.17	102.86	69.70	20.86	66.79	79.97	28.11	53.81	10.39	40.94	16.29	11.74	15.92	15.24	4.99	23.02
35	33.80	27.39	15.55	91.99	58.90	17.81	59.27	68.09	24.87	48.71	9.22	37.24	14.54	10.64	14.50	13.46	4.28	20.30
40	29.41	24.26	14.30	81.13	52.19	15.90	51.76	59.63	21.63	44.21	8.05	33.54	12.78	9.53	13.08	11./1	3.85	17.61
45	26.49	21.61	13.35	/0.68	45.48	14.00	46.02	51.18	19.57	39.70	7.32	29.84	11.49	8.43	11.66	10.66	3.41	16.01
50	23.93	18.96	12.40	64.49	38.78	12.09	41.69	42.72	17.67	35.20	5.62	26.88	10.45	7.76	10.59	9.61	2.98	14.41
55	21.37	16.30	11.45	58.31	32.07	10.19	37.36	34.27	15.77	32.56	5.93	24.72	9.41	7.10	9.75	8.50	2.54	12.81
60	16.81	13.05	10.50	52.12 45.04	25.30	8.28 6.0E	33.03	27.80	13.87	29.94	5.23	22.50	8.38 7.24	0.45 E 70	8.92	7.50	2.10	0.61
70	12.60	0.79	9.72	20.75	22.24	6.21	20.70	24.90	10.07	27.33	2.94	19.25	6.20	5.79	0.00 7.24	5.40	1.71	9.01
70	11 22	9.78	9.10	22 57	17.77	5.69	24.37	10.24	8 20	24.72	2 17	16.00	5.27	J.14 A AQ	6.40	1.40	1.30	6.95
80	10.47	8.90	8.03	28.12	15.53	5.08	18 15	16.52	7 75	19.50	2 94	13.93	4.65	3.83	5.56	4.38	1.42	6.31
85	9.62	7 13	7.47	26.06	13.30	4 41	16.13	13 70	7.12	16.89	2.54	11 77	4.03	3 30	4 72	3.88	1 13	5.78
90	8 76	6.25	6.91	24.00	11.06	3 77	15.71	10.89	6.49	14.28	2.71	10.65	3.96	3.08	4.72	3 53	0.98	5.70
95	7.91	5.36	6.34	21.94	8.83	3.14	13.82	8.07	5.86	13.26	2.24	9.93	3.62	2.86	3.97	3.18	0.84	4.71
100	7.06	4.48	5.78	19.87	6.59	2.50	12.38	5.25	5.22	12.39	2.01	9.21	3.27	2.64	3.69	2.83	0.69	4.18
105	6.20	3.59	5.22	17.81	4.36	1.87	10.94	2.43	4.59	11.51	1.78	8.49	2.92	2.42	3.41	2.48	0.55	3.65
110	5.35	2.71	4.65	15.75	2.12	1.23	9.49	0.00	3.96	10.64	1.55	7.77	2.58	2.20	3.13	2.13	0.40	3.11
115	4.50	1.82	4.09	13.69	0.00	0.60	8.05		3.32	9.77	1.32	7.05	2.23	1.99	2.85	1.78	0.26	2.58
120	3.64	0.94	3.83	11.63		0.00	6.61		2.69	8.90	1.08	6.33	1.89	1.77	2.57	1.43	0.11	2.04
125	2.79	0.06	3.65	9.57			5.17		2.06	8.03	0.85	5.62	1.54	1.55	2.29	1.08	0.00	1.51
130	1.94	0.00	3.46	7.50			3.72		1.43	7.16	0.62	4.90	1.20	1.33	2.02	0.72		0.98
135	1.08		3.27	5.44			2.28		0.79	6.29	0.39	4.18	0.85	1.11	1.74	0.37		0.44
140	0.23		3.08	3.38			0.84		0.16	5.42	0.16	3.46	0.50	0.89	1.46	0.02		0.00
145	0.00		2.90	1.32			0.00		0.00	4.55	0.00	2.74	0.16	0.68	1.18	0.00		
150			2.71	0.00						3.68		2.02	0.00	0.46	0.90			
155			2.52							2.81		1.30		0.24	0.62			
160			2.33							1.94		0.58		0.02	0.34			
165			2.15							1.07		0.00		0.00	0.06			
170			1.96							0.20					0.00			
1/5			1.//							0.00								
100			1.58															
100			1.40															
195			1.21															
200			0.83															
205			0.64															
210			0.46															
215			0.27															
220			0.08															
225			0.00					1										

CUHP Pre Development 100 Year

## Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

_				Unit	t Hydrograp	oh Paramet	ers and Res	ults			Excess	Precip.		Storm Hy	ydrograph	
					W50		W75	Time to					Time to		Total	Runoff per
				W50	Before	W75	Before	Peak		Volume	Excess	Excess	Peak	Peak Flow	Volume	Unit Area
Catchment Name/ID	User Comment for Catchment	СТ	Ср	(min.)	Peak	(min.)	Peak	(min.)	Peak (cfs)	(c.f)	(inches)	(c.f.)	(min.)	(cfs)	(c.f.)	(cfs/acre)
A1		0.156	0.142	37.3	5.57	19.4	3.93	9.3	57	164,729	1.56	257,605	45.0	67	257,125	1.47
B1		0.157	0.130	33.0	4.80	17.2	3.39	8.0	53	134,310	1.17	157,714	40.0	49	157,336	1.32
B2		0.157	0.109	58.5	6.39	30.4	4.52	10.6	20	90,351	1.17	106,094	50.0	21	106,130	0.83
B3		0.157	0.220	39.1	8.11	20.3	5.73	13.5	142	431,607	1.17	506,815	45.0	140	506,418	1.18
C1		0.157	0.182	30.3	5.72	15.7	4.04	9.5	120	281,797	1.17	330,900	40.0	111	330,490	1.43
D1		0.156	0.107	31.5	4.10	16.4	2.90	6.8	36	88,318	1.56	138,112	40.0	40	137,590	1.64
D2		0.156	0.181	37.7	6.75	19.6	4.77	11.2	97	282,777	1.56	442,208	45.0	115	442,279	1.47
E1		0.156	0.192	28.8	5.76	15.0	4.07	9.6	144	321,618	1.56	502,948	40.0	158	502,220	1.78
F1		0.156	0.124	37.2	5.06	19.4	3.57	8.4	42	122,440	1.56	191,472	45.0	49	190,993	1.47
F2		0.156	0.170	45.1	7.40	23.5	5.23	12.3	70	245,533	1.56	383,966	50.0	87	383,641	1.28
F3		0.156	0.081	37.7	3.83	19.6	2.71	6.4	16	46,609	1.56	72,888	45.0	18	72,670	1.43
F4		0.156	0.150	43.2	6.50	22.5	4.59	10.8	56	186,981	1.56	292,403	45.0	68	292,494	1.32
G1		0.156	0.099	38.8	4.44	20.2	3.14	7.4	24	73,072	1.56	114,270	45.0	28	113,996	1.41
G2		0.156	0.087	42.3	4.31	22.0	3.05	7.2	17	54,958	1.56	85,944	45.0	20	85,743	1.32
H1		0.157	0.100	43.7	4.86	22.7	3.44	8.1	22	75,177	1.17	88,277	45.0	22	88,139	1.06
H2		0.156	0.095	37.0	4.20	19.2	2.97	7.0	24	67,337	1.56	105,301	45.0	27	105,031	1.46
H3		0.156	0.057	32.6	2.93	16.9	2.07	4.9	9	21,816	1.56	34,116	40.0	10	33,729	1.58
H4		0.156	0.114	36.7	4.70	19.1	3.32	7.8	35	100,370	1.56	156,958	45.0	41	156,578	1.48

#### Printouts for Storm Hydrographs

	flow in cfs																	
time in minutes	A1	81	82	83	5	D1	D2	1	H	ы	æ	5	61	62	H1	H2	H3	H4
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.01	0.00	0.01	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
20	8.12	3.13	0.03	4.86	6.18	6.49	11.23	19.84	6.56	7.27	2.97	6.77	4 15	2.92	1 31	4.16	1.72	5.78
30	34.59	26.76	8.08	44.30	53.77	25.80	50.87	85.32	27.24	33.89	11.70	30.29	16.76	11.74	11.22	16.64	6.64	23.63
35	55.93	43.27	15.49	97.67	95.72	36.82	90.40	139.23	42.28	63.07	16.51	52.88	24.75	17.20	18.33	24.08	8.94	35.59
40	64.93	48.76	18.92	129.21	110.70	40.00	109.38	157.99	48.34	79.01	18.22	63.75	27.87	19.43	21.16	26.79	9.51	40.19
45	64.59	48.19	20.36	140.35	108.85	39.34	114.87	155.63	49.45	85.76	18.42	67.62	28.46	20.06	21.89	27.12	9.32	40.86
55	61.26	40.75	20.19	127.94	90.29	34.77	106.51	135.02	45.25	83.59	16.83	64.71	26.19	18.75	19.74	24.71	8.30	37.23
60	57.64	36.45	19.11	117.17	79.70	32.18	100.16	123.69	42.57	79.90	15.87	61.71	24.78	17.90	18.34	23.24	7.72	34.96
65	54.17	32.98	18.06	106.73	71.53	30.21	94.06	114.66	40.04	76.47	14.98	58.85	23.43	17.05	17.02	21.88	7.28	32.86
70	49.50	29.39	16.95	95.81	63.09	26.87	86.32	101.69	36.49	71.24	13.57	54.41	21.31	15.53	15.43	19.83	6.47	29.87
80	39.66	23.88	14.61	77.59	45.94	20.04	69.44	72.09	29.24	59.04	10.92	49.38	17.27	12.84	12.74	15.86	4.91	23.82
85	35.05	19.22	13.48	69.37	38.02	16.98	61.48	60.25	25.85	53.80	9.69	40.70	15.40	11.62	11.61	14.01	4.19	20.99
90	30.75	16.13	12.47	61.54	32.26	14.46	54.04	51.51	22.66	48.89	8.53	36.78	13.66	10.48	10.54	12.25	3.57	18.32
95	26.60	13.89	11.62	54.03	28.03	12.58	46.90	44.50	19.60	44.35	7.40	33.11	11.95	9.39	9.51	10.59	3.11	15.80
100	22.94	12.24	10.80	40.05	24.54	9.70	35.55	32.88	15.01	39.99	5.68	29.55	9.12	7.30	7.50	9.19	2.75	12.18
110	18.18	9.62	9.45	35.53	18.50	8.47	31.77	27.72	13.44	31.55	5.10	22.87	8.17	6.44	6.54	7.31	2.14	10.90
115	16.30	8.47	8.77	32.01	15.69	7.31	28.48	22.84	12.06	27.80	4.58	20.38	7.35	5.79	5.80	6.55	1.87	9.75
120	14.59	7.37	8.10	28.94	12.97	6.22	25.53	18.25	10.79	24.99	4.12	18.44	6.63	5.26	5.26	5.86	1.61	8.71
125	11.49	5.29	6.78	23.51	7.70	4.19	20.20	9.50	9.62	22.75	3.08	15.27	5.33	4.78	4.81	4.61	1.37	6.80
135	10.07	4.20	6.11	20.95	5.08	3.19	17.76	5.87	7.45	18.98	2.89	13.89	4.74	3.94	4.05	4.03	0.92	5.93
140	8.73	3.16	5.48	18.46	2.69	2.20	15.47	3.75	6.46	17.33	2.52	12.59	4.18	3.56	3.69	3.48	0.69	5.09
145	7.39	2.12	5.01	16.03	1.47	1.36	13.20	2.42	5.47	15.78	2.16	11.37	3.64	3.20	3.35	2.93	0.47	4.26
150	4.72	0.63	4.66	13.61	0.84	0.87	8.68	0.88	3.48	14.31	1.79	9.09	2.55	2.80	2.69	2.30	0.29	2.58
160	3.38	0.36	4.11	8.77	0.25	0.35	6.42	0.45	2.49	11.57	1.06	7.96	2.01	2.17	2.36	1.28	0.12	1.77
165	2.17	0.20	3.86	6.35	0.13	0.20	4.29	0.17	1.60	10.20	0.72	6.83	1.47	1.83	2.03	0.80	0.07	1.09
170	1.37	0.11	3.63	3.98	0.05	0.11	2.67	0.04	1.00	8.84	0.44	5.70	0.97	1.49	1.70	0.51	0.04	0.70
180	0.56	0.02	3.18	1.17	0.01	0.04	1.09	0.03	0.41	6.11	0.18	3.45	0.39	0.80	1.05	0.20	0.02	0.28
185	0.33	0.00	2.96	0.66	0.00	0.01	0.67	0.02	0.25	4.75	0.11	2.36	0.25	0.50	0.72	0.12	0.00	0.16
190	0.18	0.00	2.74	0.36	0.00	0.01	0.38	0.01	0.13	3.39	0.06	1.46	0.15	0.32	0.41	0.06	0.00	0.08
195	0.08	0.00	2.52	0.19	0.00	0.00	0.19	0.01	0.06	2.17	0.03	0.93	0.08	0.21	0.22	0.03	0.00	0.03
205	0.01	0.00	2.07	0.03	0.00	0.00	0.02	0.00	0.01	0.88	0.00	0.37	0.01	0.08	0.07	0.00	0.00	0.01
210	0.01	0.00	1.85	0.00	0.00	0.00	0.01	0.00	0.01	0.56	0.00	0.22	0.00	0.04	0.04	0.00	0.00	0.00
215	0.01	0.00	1.63	0.00	0.00	0.00	0.01	0.00	0.00	0.33	0.00	0.11	0.00	0.02	0.02	0.00	0.00	0.00
220	0.00	0.00	1.41	0.00	0.00	0.00	0.01	0.00	0.00	0.18	0.00	0.04	0.00	0.00	0.01	0.00	0.00	0.00
230	0.00	0.00	0.97	0.00	0.00	0.00	0.00	0.00	0.00	0.08	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
235	0.00	0.00	0.75	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
240	0.00	0.00	0.53	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
245	0.00	0.00	0.32	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
255	0.00	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
260	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
265	0.00	0.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
270	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2/3	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
285	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
290	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
295	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
305	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
310	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
315	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
320	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
330	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
335	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
340	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### Printouts for Unit Hydrographs

	flow in cfs																	
e in minutes																		
time	A1	B1	B2	83	5	12	D2	<b>E</b>	1	E	£	4	61	ß	보	£	떂	7
5	40.40	42.25	12.21	64.08	82.83	32.53	55.47	98.57	32.71	35.78	14.89	33.49	20.77	14.63	17.67	20.86	8.64	28.91
10	57.06	52.24	19.84	129.10	120.16	35.66	95.22	143.91	42.37	66.77	15.76	55.38	24.18	16.70	22.15	23.33	8.39	35.19
15	55.13	49.12	19.80	142.11	113.65	32.85	95.32	135.16	40.63	69.88	14.91	55.08	23.11	16.08	21.49	22.10	7.65	33.52
20	50.21	42.56	19.29	135.46	96.16	27.57	88.44	111.36	36.77	67.15	13.37	52.17	21.00	14.87	20.09	19.76	6.45	30.08
25	42.57	36.46	18.41	120.46	81.35	24.10	76.05	94.73	31.34	61.78	11.56	47.08	18.04	13.08	17.95	17.02	5.72	25.74
30	38.18	31.92	17.16	102.78	69.66	20.85	66.76	79.93	28.10	53.77	10.39	40.93	16.29	11.74	15.92	15.24	4.99	23.02
35	33.79	27.37	15.54	91.92	58.88	17.80	59.25	68.07	24.86	48.70	9.22	37.23	14.53	10.63	14.50	13.46	4.28	20.29
40	29.40	24.25	14.30	81.06	52.17	15.90	51.73	59.61	21.62	44.19	8.04	33.53	12.78	9.53	13.08	11./1	3.85	17.61
45	20.48	19.05	13.35	70.65	45.40 20.7E	13.99	40.01	42.70	19.50	39.09	7.32	29.82	10.45	8.43 7.76	10.50	10.66	3.41	10.01
55	23.92	16.95	12.40	59.29	22.04	10.19	27.25	24.24	17.07	22.55	5.02	20.07	0.45	7.70	0.75	9.01	2.97	14.41
60	18.80	13.64	10.50	52.09	25 33	8 28	37.35	27 79	13.77	29.94	5.23	24.71	8 38	6.45	8.91	7 50	2.34	11 20
65	16.24	10.99	9,72	45.91	22.24	6.95	28.69	24.97	11.97	27.33	4,53	20.40	7.34	5.79	8.07	6.45	1.71	9,60
70	13.68	9.78	9.16	39.72	20.00	6.31	24.36	22.15	10.07	24.71	3.84	18.24	6.30	5.14	7.23	5.39	1.56	8.00
75	11.32	8.90	8.59	33.53	17.76	5.68	20.03	19.33	8.39	22.10	3.17	16.08	5.26	4.48	6.39	4.58	1.42	6.85
80	10.47	8.01	8.03	28.11	15.53	5.04	18.15	16.52	7.75	19.49	2.94	13.92	4.65	3.83	5.56	4.23	1.27	6.31
85	9.61	7.13	7.47	26.05	13.29	4.41	16.71	13.70	7.12	16.88	2.71	11.77	4.31	3.30	4.72	3.88	1.13	5.78
90	8.76	6.24	6.90	23.99	11.06	3.77	15.26	10.88	6.49	14.27	2.48	10.65	3.96	3.08	4.25	3.53	0.98	5.25
95	7.91	5.36	6.34	21.93	8.82	3.14	13.82	8.06	5.85	13.25	2.24	9.93	3.61	2.86	3.97	3.18	0.84	4.71
100	7.05	4.47	5.78	19.87	6.58	2.50	12.38	5.24	5.22	12.38	2.01	9.21	3.27	2.64	3.69	2.83	0.69	4.18
105	6.20	3.59	5.21	17.80	4.35	1.87	10.93	2.42	4.59	11.51	1.78	8.49	2.92	2.42	3.41	2.48	0.55	3.64
110	5.35	2.70	4.65	15.74	2.11	1.23	9.49	0.00	3.95	10.64	1.55	7.77	2.58	2.20	3.13	2.13	0.40	3.11
115	4.49	1.82	4.09	13.68	0.00	0.60	8.05		3.32	9.77	1.32	7.05	2.23	1.99	2.85	1.78	0.25	2.58
120	3.64	0.94	3.83	11.62		0.00	6.60		2.69	8.90	1.08	6.33	1.89	1.77	2.57	1.43	0.11	2.04
125	2.79	0.05	3.65	9.56			5.16		2.06	8.03	0.85	5.61	1.54	1.55	2.29	1.07	0.00	1.51
130	1.93	0.00	3.46	7.49 E 42			3.72		1.42	7.16	0.62	4.89	1.19	1.33	2.01	0.72		0.97
140	0.23		3.27	3.45			0.83		0.79	5.42	0.39	4.17	0.85	0.89	1.75	0.37		0.44
145	0.23		2 90	1 31			0.00		0.10	4 55	0.15	2 74	0.50	0.67	1.45	0.02		0.00
150	0.00		2.71	0.00			0.00		0.00	3.68	0.00	2.02	0.00	0.46	0.89	0.00		
155			2.52							2.81		1.30		0.24	0.61			
160			2.33							1.94		0.58		0.02	0.34			
165			2.14							1.07		0.00		0.00	0.06			
170			1.96							0.20					0.00			
175			1.77							0.00								
180			1.58															
185			1.39															
190			1.21															
195			1.02															<b>  </b>
200			0.83															<b>↓</b>
205			0.64															┟────┤
210			0.46															┝───┤
215			0.27															┝───┤
220			0.00															
225			0.00															

5-Year Post Development CUHP

## Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

_				Unit	t Hydrograp	oh Paramet	ers and Res	sults			Excess	Precip.		Storm Hy	ydrograph	
					W50		W75	Time to					Time to		Total	Runoff per
				W50	Before	W75	Before	Peak		Volume	Excess	Excess	Peak	Peak Flow	Volume	Unit Area
Catchment Name/ID	User Comment for Catchment	СТ	Ср	(min.)	Peak	(min.)	Peak	(min.)	Peak (cfs)	(c.f)	(inches)	(c.f.)	(min.)	(cfs)	(c.f.)	(cfs/acre)
A1		0.097	0.131	25.0	4.03	13.0	2.84	6.7	85	164,729	0.57	94,676	35.0	31	94,308	0.68
B1		0.092	0.139	18.2	3.44	9.5	2.43	5.7	95	134,310	0.58	77,837	30.0	29	77,220	0.80
B2		0.093	0.113	33.3	4.40	17.3	3.11	7.3	35	90,351	0.56	50,405	35.0	12	50,284	0.48
B3		0.109	0.171	35.1	6.09	18.2	4.30	10.2	159	431,607	0.31	135,184	35.0	37	135,109	0.31
C1		0.089	0.205	15.3	3.91	7.9	2.76	6.5	238	281,797	0.64	181,072	30.0	76	180,336	0.97
D1		0.092	0.115	17.3	3.03	9.0	2.14	5.1	66	88,318	0.67	59,557	30.0	24	58,560	0.99
D2		0.084	0.229	15.9	4.30	8.3	3.04	7.2	229	282,777	0.87	246,138	30.0	98	245,292	1.26
E1		0.114	0.151	26.8	4.61	13.9	3.25	7.7	155	321,618	0.41	131,675	35.0	47	131,227	0.53
F1		0.107	0.097	32.8	3.94	17.1	2.78	6.6	48	122,440	0.47	56,968	35.0	16	56,751	0.48
F2		0.088	0.198	21.9	4.83	11.4	3.41	8.1	145	245,533	0.75	184,862	35.0	60	183,986	0.89
F3		0.092	0.087	20.4	2.87	10.6	2.03	4.8	30	46,609	0.68	31,862	30.0	11	31,302	0.88
F4		0.121	0.121	41.5	5.37	21.6	3.79	8.9	58	186,981	0.36	67,763	35.0	17	67,675	0.34
G1		0.096	0.093	25.2	3.31	13.1	2.34	5.5	37	73,072	0.59	43,083	30.0	14	42,758	0.68
G2		0.107	0.067	37.3	3.43	19.4	2.42	5.7	19	54,958	0.47	25,571	35.0	7	25,468	0.43
H1		0.109	0.078	39.3	3.85	20.4	2.72	6.4	25	75,177	0.31	23,258	35.0	6	23,195	0.27
H2		0.092	0.101	20.5	3.09	10.6	2.18	5.2	42	67,337	0.67	45,076	30.0	16	44,528	0.88
H3		0.094	0.058	19.2	2.36	10.0	1.67	3.9	15	21,816	0.64	13,878	30.0	5	13,432	0.87
H4		0.095	0.111	22.8	3.45	11.9	2.44	5.7	57	100,370	0.61	61,173	30.0	21	60,592	0.76

#### Printouts for Unit Hydrographs

flow in cfs

ime in minutes	1	1	5	ņ	1	1	2	1	1	2	œ	4	I	12	1	2	3	4
- - -	<b>∢</b> 22 22	02.25	20.00	102 50	220 52		100.00	ш 120.02	44.26	115.64	20.50	42.62	27.02	19.62	12 02	12 42	14.61	
10	77.55 97.79	95.25	24 71	102.39	220.55	57.20	212 52	120.95	44.50	142.27	29.50	42.02 59.19	25.94	10.02	25.05	28.00	12 72	52.06
15	70.87	64.60	32 47	154.15	146.87	42 55	148 71	136.86	47.44	117 23	20.77	56 54	30.18	17.61	24.44	30.20	9.82	43.13
20	57.63	49.16	28.07	139.10	107.74	32.08	108.63	110.77	37.50	92.72	16.66	52.59	24.96	15.66	21.07	24.25	7.67	35.72
25	47.82	39.67	24.21	116.79	80.83	25.68	83.75	93.90	32.69	72.89	13.46	46.34	20.75	13.62	18.22	19.53	6.26	28.56
30	39.89	30.81	21.23	103.58	53.91	19.28	58.88	77.26	28.57	61.39	11.05	41.06	17.44	12.21	16.48	16.06	5.00	24.34
35	34.20	21.94	18.25	90.37	40.79	13.08	41.89	67.52	24.45	50.16	8.64	37.09	14.97	10.80	14.74	12.59	3.73	20.17
40	28.51	17.08	16.20	78.14	31.82	10.94	33.60	57.77	21.87	38.93	6.23	33.12	12.50	9.45	13.00	9.12	2.78	16.00
45	22.81	14.12	14.45	70.52	22.85	8.81	25.30	48.03	19.44	28.50	5.21	29.15	10.02	8.61	11.70	7.55	2.35	11.83
50	17.12	11.17	12.70	62.89	13.88	6.68	17.01	38.28	17.01	24.76	4.40	26.80	7.55	7.77	10.67	6.39	1.93	10.13
55	15.14	8.21	10.96	55.26	4.91	4.55	8.72	30.20	14.58	21.02	3.60	24.47	6.69	6.93	9.63	5.24	1.51	8.74
60	13.25	5.26	9.21	47.63	0.00	2.41	0.43	26.95	12.15	17.28	2.80	22.14	5.86	6.09	8.60	4.08	1.09	7.35
65	11.35	2.30	7.46	40.01		0.28	0.00	23.70	9.73	13.53	1.99	19.80	5.04	5.25	7.56	2.92	0.66	5.96
70	9.45	0.00	6.57	32.38		0.00		20.45	8.85	9.79	1.19	17.47	4.21	4.41	6.53	1.77	0.24	4.57
75	7.55		5.99	29.45				17.20	8.04	6.05	0.39	15.14	3.39	3.73	5.49	0.61	0.00	3.18
80	5.65		5.41	26.90				13.96	7.23	2.30	0.00	12.80	2.56	3.45	4.78	0.00		1.79
85	3.76		4.83	24.36				10.71	6.42	0.00		11.25	1.74	3.17	4.43			0.40
90	1.86		4.24	21.82				7.46	5.61			10.48	0.92	2.89	4.09			0.00
95	0.00		3.66	19.28				4.21	4.80			9.70	0.09	2.61	3.74			
100			3.08	16.73				0.96	3.99			8.92	0.00	2.33	3.40			
105			2.50	14.19				0.00	3.18			8.14		2.05	3.05			
110			1.91	11.65					2.37			7.37		1.77	2.71			
115			1.33	9.11					1.57			6.59		1.49	2.36			
120			0.75	6.57					0.76			5.81		1.21	2.02			
125			0.16	4.02					0.00			5.03		0.93	1.67			
130			0.00	1.48								4.25		0.65	1.33			
135				0.00								3.48		0.37	0.98			
140												2.70		0.09	0.64			
145												1.92		0.00	0.29			
150												1.14			0.00			
155												0.37						
160												0.00						

#### Printouts for Storm Hydrographs

	flow in cfs																	
ies																		
nut																		
E C																		
e ir																		
tim	A1	B1	B2	B3	C	D1	D2	E1	F1	F2	F3	F4	G1	62	H1	Н2	НЗ	Ŧ
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.36	0.64	0.20	0.23	1.74	0.44	2.08	0.18	0.10	0.95	0.20	0.04	0.18	0.04	0.05	0.28	0.09	0.30
15	2.32	4.09	1.30	1.64	11.12	2.79	13.53	1.21	0.67	6.30	1.29	0.24	1.17	0.28	0.33	1.79	0.56	1.93
20	6.67	9.83	3.33	5.52	26.84	6.88	33.61	5.50	2.52	16.68	3.21	1.29	3.22	1.04	1.05	4.47	1.38	5.10
25	20.87	22.60	7.93	17.10	59.49	18.93	77.51	25.66	9.83	42.33	8.75	7.68	9.89	4.07	3.28	12.38	4.00	15.21
30	30.38	29.46	11.46	31.45	/5.68	24.15	98.47	43.67	15.39	59.83	11.36	14.72	13.78	6.23	5.43	16.24	5.21	20.93
35	30.72	26.67	12.02	36.88	66.79	21.82	89.51	46.88	16.28	60.11	10.60	17.33	13.54	6.55	5.68	15.19	4.80	20.15
40	27.81	10.22	11.45	33.92	54.47	16.39	74.71	42.71	12.34	33.80	9.29	16.19	12.20	6.29 E 70	5.48	11.51	4.14	17.97
45 50	24.51	19.22	0.82	32.80	26.85	13.44	52.27	37.28	12.93	40.80	8.00	14.80	10.85	5.79	5.07	11.52	3.55	13.00
55	10.27	12.00	9.02	25.05	20.70	10.72	13.60	28.65	11.00	26.51	6.07	12.55	9.65	/ 01	4.00	8.67	2.50	12.22
60	17.19	12.08	8.45	20.33	26.55	9.18	37.60	25.03	10.42	31.82	5.18	12 40	7 70	4.51	3.96	7 40	2.33	10.64
65	15.12	10.81	7.94	22.29	22.96	8.12	32.85	22.34	9.59	27.79	4.57	11.31	6.80	4.17	3.65	6.51	1.94	9.21
70	13.24	9.76	7.45	20.59	19.65	7.15	28.46	19.37	8.80	25.18	4.16	10.45	5.97	3.90	3.41	5.91	1.74	8.23
75	11.79	8.53	6.89	18.85	16.26	6.00	23.71	16.54	7.92	22.91	3.71	9.69	5.33	3.60	3.17	5.26	1.52	7.41
80	10.62	7.22	6.30	17.03	13.53	4.85	19.26	14.42	6.99	20.51	3.23	8.91	4.82	3.27	2.93	4.59	1.29	6.62
85	9.57	6.07	5.76	15.23	12.11	3.89	16.78	12.86	6.11	18.18	2.78	8.12	4.36	2.94	2.68	3.95	1.07	5.87
90	8.59	5.20	5.35	13.56	11.42	3.34	15.58	11.48	5.49	15.96	2.36	7.34	3.93	2.63	2.44	3.35	0.88	5.16
95	7.65	4.76	5.07	12.35	10.98	3.08	14.84	10.17	5.07	13.90	2.00	6.56	3.52	2.36	2.21	2.83	0.74	4.47
100	6.58	4.29	4.75	11.49	9.92	2.75	13.45	8.75	4.63	11.66	1.65	5.77	3.04	2.14	2.00	2.33	0.63	3.69
105	5.52	3.91	4.43	10.66	9.00	2.49	12.15	7.33	4.21	9.81	1.45	5.11	2.58	1.98	1.85	2.03	0.57	2.99
110	4.54	3.64	4.12	9.86	8.35	2.30	11.26	5.94	3.80	8.73	1.33	4.64	2.14	1.83	1.74	1.86	0.53	2.52
115	3.70	3.43	3.83	9.09	7.88	2.17	10.60	4.61	3.41	8.10	1.24	4.29	1.76	1.69	1.63	1.74	0.49	2.27
120	3.19	3.19	3.52	8.32	7.31	2.00	9.84	3.37	3.02	7.53	1.15	3.97	1.51	1.55	1.52	1.61	0.46	2.09
125	2.62	2.47	3.05	7.36	5.48	1.52	7.54	2.39	2.55	6.26	0.91	3.63	1.23	1.38	1.38	1.28	0.35	1.70
130	2.11	1.84	2.57	6.30	3.83	1.12	5.34	1.80	2.09	4.91	0.70	3.29	0.99	1.21	1.23	0.99	0.27	1.34
135	1.69	1.37	2.11	5.27	2.67	0.82	3.79	1.42	1.65	3.82	0.54	2.96	0.80	1.05	1.09	0.76	0.20	1.06
140	1.35	0.74	1.70	4.28	1.82	0.60	2.04	1.15	1.23	2.98	0.42	2.03	0.64	0.89	0.95	0.58	0.15	0.65
140	0.86	0.74	1.07	2.50	0.80	0.42	1.70	0.30	0.64	1 75	0.31	2.32	0.31	0.74	0.69	0.44	0.01	0.05
155	0.67	0.32	0.89	1.83	0.50	0.20	0.79	0.56	0.52	1 31	0.23	1 71	0.32	0.55	0.05	0.33	0.06	0.38
160	0.51	0.25	0.74	1.42	0.29	0.14	0.47	0.43	0.42	0.98	0.13	1.41	0.25	0.33	0.45	0.18	0.04	0.29
165	0.40	0.16	0.62	1.18	0.13	0.08	0.23	0.33	0.34	0.73	0.09	1.12	0.19	0.24	0.34	0.13	0.03	0.22
170	0.31	0.09	0.51	0.98	0.03	0.04	0.08	0.25	0.28	0.52	0.06	0.83	0.15	0.18	0.25	0.09	0.02	0.16
175	0.23	0.04	0.42	0.82	0.00	0.01	0.00	0.19	0.22	0.36	0.04	0.55	0.11	0.15	0.19	0.05	0.01	0.11
180	0.17	0.01	0.35	0.67	0.00	0.00	0.00	0.14	0.18	0.23	0.02	0.35	0.08	0.12	0.15	0.03	0.00	0.08
185	0.12	0.00	0.29	0.56	0.00	0.00	0.00	0.10	0.14	0.13	0.01	0.24	0.06	0.10	0.13	0.01	0.00	0.05
190	0.08	0.00	0.23	0.46	0.00	0.00	0.00	0.07	0.11	0.06	0.00	0.19	0.04	0.08	0.11	0.00	0.00	0.03
195	0.05	0.00	0.19	0.38	0.00	0.00	0.00	0.05	0.09	0.02	0.00	0.15	0.02	0.07	0.09	0.00	0.00	0.01
200	0.02	0.00	0.15	0.30	0.00	0.00	0.00	0.03	0.07	0.00	0.00	0.12	0.01	0.05	0.08	0.00	0.00	0.00
205	0.01	0.00	0.11	0.24	0.00	0.00	0.00	0.02	0.05	0.00	0.00	0.10	0.00	0.04	0.06	0.00	0.00	0.00
210	0.00	0.00	0.08	0.18	0.00	0.00	0.00	0.01	0.04	0.00	0.00	0.08	0.00	0.03	0.05	0.00	0.00	0.00
215	0.00	0.00	0.06	0.14	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.06	0.00	0.03	0.04	0.00	0.00	0.00
220	0.00	0.00	0.04	0.10	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.05	0.00	0.02	0.03	0.00	0.00	0.00
220	0.00	0.00	0.02	0.07	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.04	0.00	0.01	0.03	0.00	0.00	0.00
230	0.00	0.00	0.01	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.01	0.02	0.00	0.00	0.00
240	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00
245	0,00	0,00	0,00	0.00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0.01	0,00	0,00	0,01	0,00	0,00	0.00
250	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
255	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
260	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
265	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
270	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
275	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

## Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

				Unit	t Hydrograp	oh Paramet	ers and Res	ults			Excess	Precip.		Storm H	ydrograph	
					W50		W75	Time to					Time to		Total	Runoff per
				W50	Before	W75	Before	Peak		Volume	Excess	Excess	Peak	Peak Flow	Volume	Unit Area
Catchment Name/ID	User Comment for Catchment	СТ	Ср	(min.)	Peak	(min.)	Peak	(min.)	Peak (cfs)	(c.f)	(inches)	(c.f.)	(min.)	(cfs)	(c.f.)	(cfs/acre)
A1		0.096	0.134	24.4	4.01	12.7	2.83	6.7	87	164,729	1.93	317,756	40.0	101	316,720	2.22
B1		0.091	0.141	17.8	3.42	9.2	2.42	5.7	98	134,310	1.82	243,813	35.0	97	241,630	2.62
B2		0.092	0.115	32.5	4.38	16.9	3.09	7.3	36	90,351	1.79	161,555	40.0	42	161,041	1.70
B3		0.089	0.250	19.5	5.26	10.2	3.72	8.8	285	431,607	1.88	813,554	40.0	295	807,930	2.48
C1		0.088	0.210	14.7	3.88	7.6	2.74	6.5	247	281,797	1.91	539,141	35.0	238	535,192	3.07
D1		0.092	0.116	17.1	3.02	8.9	2.14	5.0	67	88,318	2.03	179,570	35.0	70	176,587	2.88
D2		0.083	0.230	15.8	4.30	8.2	3.04	7.2	231	282,777	2.25	634,968	35.0	252	632,818	3.24
E1		0.113	0.150	26.5	4.56	13.8	3.23	7.6	157	321,618	1.75	563,176	40.0	178	561,356	2.01
F1		0.106	0.096	32.4	3.90	16.9	2.76	6.5	49	122,440	1.81	221,916	40.0	59	221,037	1.75
F2		0.088	0.199	21.7	4.82	11.3	3.40	8.0	146	245,533	2.12	520,116	40.0	171	517,601	2.53
F3		0.091	0.088	20.1	2.86	10.5	2.02	4.8	30	46,609	2.04	95,234	35.0	33	93,473	2.56
F4		0.090	0.168	22.4	4.39	11.7	3.10	7.3	108	186,981	2.06	385,413	40.0	125	383,174	2.42
G1		0.095	0.095	24.6	3.29	12.8	2.33	5.5	38	73,072	1.94	142,048	40.0	44	140,977	2.18
G2		0.106	0.067	36.8	3.40	19.2	2.41	5.7	19	54,958	1.81	99,609	45.0	24	99,196	1.58
H1		0.107	0.078	38.6	3.80	20.1	2.69	6.3	25	75,177	1.49	111,730	45.0	28	111,424	1.33
H2		0.092	0.102	20.2	3.08	10.5	2.18	5.1	43	67,337	2.03	136,549	35.0	48	134,796	2.57
H3		0.093	0.059	18.9	2.36	9.8	1.66	3.9	15	21,816	1.99	43,454	35.0	16	42,019	2.60
H4		0.094	0.113	22.3	3.44	11.6	2.43	5.7	58	100,370	1.96	197,106	35.0	65	195,054	2.34

#### Printouts for Storm Hydrographs

	flow in cfs																	
e in minutes																		
tim	A1	B1	B2	B3	C	D1	D2	E1	F1	F2	F3	F4	61	62	Н1	Н2	Н3	H4
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.94	1.68	0.52	4.22	4.78	1.15	5.37	0.48	0.27	2.45	0.53	1.71	0.48	0.11	0.13	0.73	0.23	0.79
15	3.15	5.42	1.79	15.33	15.49	3.64	18.05	1.65	0.90	8.65	1.69	5.85	1.57	0.37	0.45	2.35	0.73	2.57
20	8.70	11.45	4.00	34.16	32.52	8.58	40.38	7.60	3.38	20.68	4.00	14.14	4.16	1.40	1.40	5.60	1.74	6.52
25	28.66	29.50	10.41	82.19	78.37	24.79	95.14	38.37	14.16	53.76	11.42	39.02	13.48	5.86	4.98	16.26	5.32	20.51
30	/4.80	/9.4/	28.38	209.96	197.61	59.58	206.21	118.53	40.66	125.47	27.36	93.76	34.55	16.72	18.14	39.34	13.13	51.86
35	97.97	97.08	39.09	293.34	238.03	70.07	252.18	157.02	58.90	167.34	32.93	122.79	43.48	22.15	25.18	47.62	14.96	64.71
40	95.76	91.72 81.74	42.20	255.27	188 54	59.25	200.64	178.04	58 16	160.16	29.55	117 59	43.93	23.00	27.31	40.23	13 70	60.43
50	88.61	71.93	39.52	241 02	158 77	52 39	182.92	159.94	55.68	145.90	26.81	107.63	38.81	23.33	26.37	38.80	12 35	55 33
55	80.64	61.06	36.70	210.38	128.15	44.77	154.98	145.85	52.10	131.63	23.79	97.40	35.39	21.94	24.69	34.43	10.81	49.97
60	73.72	51.53	33.93	181.32	108.02	38.53	133.43	134.19	48.66	118.30	21.04	88.02	32.46	20.78	23.06	30.45	9.45	45.14
65	67.40	45.18	31.76	156.70	93.56	34.56	118.85	123.94	46.04	106.27	18.72	79.39	29.76	19.73	21.51	27.09	8.44	40.65
70	57.62	37.36	28.86	133.61	72.90	28.24	97.25	107.68	41.56	90.84	15.78	67.48	25.37	18.01	19.61	22.80	7.03	34.05
75	48.65	30.42	25.90	111.95	54.03	22.66	76.20	90.77	36.98	77.55	13.35	57.62	21.48	16.38	17.89	19.26	5.84	28.96
80	41.32	23.90	22.84	92.09	37.59	17.26	56.56	75.87	32.23	65.51	11.01	48.88	18.30	14.67	16.16	15.88	4.69	24.47
85	35.33	18.17	19.94	74.04	27.23	12.61	40.76	64.74	27.82	54.76	8.95	41.21	15.71	13.05	14.51	12.91	3.68	20.55
90	30.19	13.24	17.37	58.22	21.17	8.92	31.25	55.66	23.97	45.42	7.12	34.55	13.49	11.51	12.93	10.27	2.78	17.14
95	25.62	9.81	15.52	44.14	17.61	6.75	25.52	47.90	21.14	36.94	5.47	28.49	11.50	10.09	11.40	7.89	2.02	14.01
100	21.38	7.91	14.06	33.30	15.21	5.47	21.73	40.83	18.87	29.27	4.09	22.92	9.66	8.92	9.98	5.89	1.52	11.11
105	17.42	6.73	12.77	27.35	13.68	4.57	19.13	34.26	16.87	22.78	3.22	17.88	7.94	8.04	8.89	4.60	1.23	8.49
110	13.78	5.95	11.60	23.68	12.61	3.96	17.35	28.05	15.05	18.35	2.68	13.86	6.34	7.30	8.07	3.81	1.03	6.41
115	10.62	5.43	10.50	21.24	11.96	3.53	16.10	22.23	13.36	15.62	2.31	11.46	4.94	6.63	/.3/	3.28	0.89	5.17
120	8.3Z	5.07	9.45	19.57	11.75	3.23	15.37	10.77	11.75	13.81	2.05	9.95	3.80	6.02 F. 2C	6.74	2.90	0.79	4.39
125	0.51	2.65	6.80	15.66	6.09	2.37	8 30	8 10	8 35	8 30	1.55	7.04	2.90	5.50	5.08	2.19	0.58	2.49
130	4.73	2.00	5.52	8 70	0.09	1.72	6.01	5.78	6.33	6.30	0.83	3.91	1.63	4.72	1.82	1.00	0.42	1.84
140	2.61	1 55	4 31	6.55	2.89	0.93	4 27	4 12	5.15	4 58	0.63	3.26	1.03	3 56	4.82	0.88	0.31	1.34
145	1.91	1.13	3.21	4.92	1.91	0.66	2.93	2.90	3.70	3.47	0.47	2.44	0.90	3.00	3.67	0.66	0.17	0.99
150	1.39	0.81	2.32	3.64	1.29	0.47	2.00	2.02	2.57	2.64	0.35	1.86	0.66	2.45	3.11	0.50	0.13	0.75
155	1.04	0.58	1.76	2.65	0.79	0.33	1.33	1.36	1.85	1.99	0.26	1.41	0.49	1.91	2.56	0.37	0.09	0.57
160	0.80	0.40	1.36	1.97	0.41	0.22	0.80	0.91	1.35	1.51	0.20	1.08	0.37	1.40	2.02	0.28	0.07	0.44
165	0.62	0.26	1.05	1.39	0.15	0.13	0.40	0.69	0.98	1.15	0.14	0.84	0.29	0.96	1.49	0.20	0.05	0.34
170	0.49	0.14	0.81	0.91	0.02	0.07	0.13	0.54	0.70	0.85	0.10	0.63	0.23	0.68	1.00	0.14	0.03	0.25
175	0.37	0.06	0.63	0.53	0.00	0.02	0.00	0.43	0.50	0.58	0.06	0.45	0.18	0.50	0.66	0.09	0.02	0.18
180	0.28	0.02	0.49	0.26	0.00	0.00	0.00	0.33	0.35	0.37	0.03	0.30	0.13	0.36	0.46	0.05	0.01	0.12
185	0.19	0.00	0.39	0.08	0.00	0.00	0.00	0.25	0.26	0.21	0.01	0.18	0.09	0.26	0.33	0.02	0.00	0.07
190	0.12	0.00	0.32	0.00	0.00	0.00	0.00	0.18	0.21	0.09	0.00	0.09	0.06	0.19	0.24	0.00	0.00	0.04
195	0.07	0.00	0.26	0.00	0.00	0.00	0.00	0.12	0.17	0.02	0.00	0.03	0.03	0.13	0.18	0.00	0.00	0.01
200	0.03	0.00	0.10	0.00	0.00	0.00	0.00	0.07	0.13	0.00	0.00	0.00	0.02	0.10	0.13	0.00	0.00	0.00
205	0.01	0.00	0.16	0.00	0.00	0.00	0.00	0.04	0.10	0.00	0.00	0.00	0.00	0.08	0.10	0.00	0.00	0.00
210	0.00	0.00	0.12	0.00	0.00	0.00	0.00	0.01	0.08	0.00	0.00	0.00	0.00	0.00	0.07	0.00	0.00	0.00
215	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.00	0.00	0.00	0.03	0.00	0.00	0.00	0.00
225	0.00	0.00	0.03	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.03	0.04	0.00	0.00	0.00
230	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.02	0.03	0.00	0.00	0.00
235	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.02	0.00	0.00	0.00
240	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.00
245	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00
250	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
255	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
260	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
265	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

## Printouts for Unit Hydrographs

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5	79.48	95.51	30.93	212.33	229.82	66.81	201.50	131.02	45.09	117.17	29.92	92.63	37.90	18.89	23.57	43.06	14.85	56.70
10	84.67	87.92	35.54	282.68	215.27	57.76	213.46	154.59	47.98	143.83	27.05	104.96	36.56	18.95	24.84	39.42	12.85	54.86
15	71.63	65.18	33.09	218.45	147.65	42.75	148.95	137.43	44.32	117.53	20.92	85.95	30.43	17.77	23.57	30.43	9.89	43.38
20	58.21	48.97	28.30	170.33	107.98	32.20	108.75	111.17	37.59	92.99	16.68	69.02	25.18	15.74	21.25	24.29	7.66	35.92
25	47.87	39.61	24.48	132.75	78.94	25.61	83.53	93.98	32.85	72.85	13.48	54.84	20.77	13.71	18.39	19.57	6.27	28.68
30	40.08	30.32	21.34	107.50	49.89	19.02	58.31	77.43	28.63	61.37	11.00	46.28	17.51	12.26	16.59	16.00	4.96	24.34
35	34.09	21.04	18.21	82.24	39.94	13.05	41.79	67.50	24.41	49.89	8.52	38.16	14.92	10.82	14.79	12.42	3.65	20.00
40	28.10	16.93	16.26	57.04	30.26	10.85	33.38	57.58	21.90	38.40	6.04	30.04	12.33	9.48	12.98	8.85	2.77	15.66
45	22.11	13.83	14.43	48.62	20.58	8.66	24.98	47.65	19.41	28.45	5.18	21.93	9.74	8.62	11.74	7.51	2.33	11.51
50	16.99	10.74	12.59	40.20	10.90	6.46	16.57	37.72	16.92	24.63	4.35	18.95	7.50	7.76	10.67	6.32	1.89	10.06
55	15.00	7.64	10.76	31.78	1.22	4.26	8.16	30.14	14.43	20.80	3.52	16.25	6.63	6.90	9.60	5.12	1.46	8.61
60	13.00	4.55	8.92	23.36	0.00	2.07	0.00	26.83	11.95	16.97	2.70	13.54	5.77	6.04	8.53	3.93	1.02	7.17
65	11.00	1.45	7.15	14.94		0.00		23.53	9.65	13.14	1.87	10.83	4.91	5.18	7.46	2.74	0.58	5.72
70	9.01	0.00	6.53	6.53				20.22	8.82	9.32	1.04	8.13	4.04	4.32	6.39	1.55	0.15	4.27
75	7.01		5.92	0.00				16.91	7.99	5.49	0.22	5.42	3.18	3.72	5.32	0.36	0.00	2.82
80	5.01		5.31					13.60	7.16	1.66	0.00	2.72	2.31	3.43	4.76	0.00		1.38
85	3.02		4.70					10.29	6.33	0.00		0.01	1.45	3.15	4.41			0.00
90	1.02		4.09					6.98	5.50			0.00	0.59	2.86	4.05			
95	0.00		3.47					3.67	4.67				0.00	2.57	3.69			
100			2.86					0.36	3.84					2.29	3.34			
105			2.25					0.00	3.01					2.00	2.98			
110			1.64						2.18					1.71	2.62			
115			1.03						1.35					1.43	2.27			
120			0.41						0.52					1.14	1.91			
125			0.00						0.00					0.85	1.55			
130														0.57	1.19			
135														0.28	0.84			
140														0.00	0.48			
145															0.12			
150															0.00			



Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix C

## SWMM Model Pre Development 5 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ SWMM Pre Development 5 Year \*\*\*\*\*\*\*\*\*\* NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/01/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal ---------Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 3.918 12.024 External Outflow ..... 12.024 3.918 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... -0.002

SWMM Model Pre Development 5 Year \*\*\*\*\* All links are stable.

\*\*\*\*\*\*

Routing Time Step Summary \*\*\*\*\*\*

Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.00	
Percent	Not Converging	:	0.00	

## \*\*\*\*\*

Node Depth Summary \*\*\*\*\*\*

Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time Occu days	of Max rrence hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0	00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.08	0.31	6945.31	0	00:35	0.30
24	JUNCTION	0.10	0.44	6934.44	0	00:40	0.44
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.10	0.48	6911.48	0	00:35	0.48
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.11	0.48	6900.48	0	00:35	0.48
65	JUNCTION	0.17	0.69	6880.69	0	00:36	0.69
66	JUNCTION	0.24	0.89	6868.89	0	00:40	0.89
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.11	0.43	6902.43	0	00:35	0.42

	SWMM Mode	el Pre De	velopmer	nt 5 Year			
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.11	0.48	6872.48	0	00:35	0.47
85	JUNCTION	0.06	0.30	6874.30	0	00:35	0.30
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.11	0.44	6911.44	0	00:41	0.43
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.11	0.42	6900.42	0	00:36	0.42
PondH	JUNCTION	0.11	0.47	6866.47	0	00:36	0.47
PondF	JUNCTION	0.24	0.89	6866.89	0	00:41	0.88
PondD	JUNCTION	0.10	0.48	6881.48	0	00:37	0.47
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
31	OUTFALL	0.00	0.00	6953.00	0	00:00	0.00
51	OUTFALL	0.00	0.00	6920.00	0	00:00	0.00
74	OUTFALL	0.00	0.00	6897.00	0	00:00	0.00
67	OUTFALL	0.00	0.00	6865.50	0	00:00	0.00

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Node Inflow Summary \*\*\*\*\*\*\*\*\*

Total	Flow		Maximum	Maximum		Lateral	
TUCAL	FIOW		Lateral	Total	Time of Max	Inflow	
Inflow	Balance						
	Funda		Inflow	Inflow	Occurrence	Volume	
Volume Node	Error	Туре	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent				-	C	
10		JUNCTION	13.03	13.03	0 00:35	0.304	
0.304	0.000						
20		JUNCTION	4.33	4.33	0 00:35	0.085	
0.085	0.000						
21		JUNCTION	1.66	1.66	0 00:40	0.0573	
0.0573	0.000						

		SWMM Mod	del Pre De	velopment	5 Yea	ar	
22		JUNCTION	11.85	11.85	0	00:40	0.274
0.274	0.000						
23		JUNCTION	0.00	5.99	0	00:35	0
0.142	0.000						
24		JUNCTION	0.00	11.85	0	00:40	0
0.274	0.000						
30		JUNCTION	9.95	9.95	0	00:35	0.179
0.179	0.000						
40		JUNCTION	8.12	8.12	0	00:35	0.162
0.162	0.000						
41		JUNCTION	22.23	22.23	0	00:40	0.522
0.522	0.000						
42		JUNCTION	0.00	8.12	0	00:35	0
0.162	0.000						
50		JUNCTION	32.34	32.34	0	00:35	0.593
0.593	0.000						
60		JUNCTION	9.70	9.70	0	00:35	0.226
0.226	0.000						
61		JUNCTION	16.46	16.46	0	00:40	0.453
0.453	0.000						
62		JUNCTION	3.65	3.65	0	00:35	0.0858
0.0858	0.000						
63		JUNCTION	12.98	12.98	0	00:40	0.345
0.345	0.000						
64		JUNCTION	0.00	13.35	0	00:35	0
0.311	0.000						
65		JUNCTION	0.00	26.04	0	00:36	0
0.657	0.000						
66		JUNCTION	0.00	16.46	0	00:40	0
0.453	0.000						
70		JUNCTION	5.57	5.57	0	00:35	0.135
0.135	0.000						
71		JUNCTION	3.87	3.87	0	00:35	0.101
0.101	0.000						
72		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
73		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
80		JUNCTION	1.85	1.85	0	00:35	0.0476
0.0476	0.000						
81		JUNCTION	5.37	5.37	0	00:35	0.124
0.124	0.000						
82		JUNCTION	1.92	1.92	0	00:35	0.0398
0.0398	0.000						
83		JUNCTION	8.07	8.07	0	00:35	0.185
0.185	0.000						
84		JUNCTION	0.00	7.22	0	00:35	0
0.172	0.000						

		SWMM Mode	l Pre Dev	/elopment	5 Yea	ır	
85		JUNCTION	0.00	1.92	0	00:35	0
0.0398	0.000						
PondC		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000						
PondA		JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000						
PondB		JUNCTION	0.00	17.56	0	00:41	0
0.416	0.000						
PondE		JUNCTION	0.00	32.34	0	00:35	0
0.593	0.000						
PondG		JUNCTION	0.00	9.42	0	00:36	0
0.236	0.000						
PondH		JUNCTION	0.00	17.11	0	00:36	0
0.397	0.000						
PondF		JUNCTION	0.00	42.32	0	00:41	0
1.11	0.000						
PondD		JUNCTION	0.00	30.00	0	00:38	0
0.685	0.000						
Outfall2		OUTFALL	0.00	17.56	0	00:41	0
0.416	0.000						
Outfall1		OUTFALL	0.00	13.03	0	00:35	0
0.304	0.000						
Outfall4		OUTFALL	0.00	17.11	0	00:36	0
0.397	0.000						
Outfall3		OUTFALL	0.00	30.00	0	00:38	0
0.685	0.000						
31		OUTFALL	0.00	9.95	0	00:35	0
0.179	0.000						
51		OUTFALL	0.00	32.34	0	00:35	0
0.593	0.000						
74		OUTFALL	0.00	9.42	0	00:36	0
0.236	0.000						
67		OUTFALL	0.00	42.32	0	00:41	0
1.11	0.000						

No nodes were flooded.

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	SWMM	Model Pre	Development	5 Year
	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CFS	CFS	10^6 gal
Outfall2	67.36	3.82	17.56	0.416
Outfall1	55.28	3.40	13.03	0.304
Outfall4	59.31	4.14	17.11	0.397
Outfall3	60.56	7.00	30.00	0.685
31	50.97	2.17	9.95	0.179
51	51.53	7.12	32.34	0.593
74	58.61	2.49	9.42	0.236
67	65.97	10.41	42.32	1.110
System	58.70	40.55	169.75	3.918

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Link Flow Summary \*\*\*\*\*\*\*\*\*

Link Type	Maximum  Flow  CFS	Time Occu days	of Max urrence hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100 DUMMY	13.03		 00:35			
200 DUMMY	4.33	0	00:35			
201 DUMMY	1.66	0	00:40			
202 CONDUI	T 5.95	0	00:36	10.09	0.00	0.04
204 DUMMY	11.85	0	00:40			
205 CONDUI	T 11.83	0	00:41	11.82	0.01	0.06
300 DUMMY	9.95	0	00:35			
400 DUMMY	8.12	0	00:35			
401 CONDUI	T 8.03	0	00:37	8.38	0.02	0.10
402 DUMMY	22.23	0	00:40			
500 DUMMY	32.34	0	00:35			
601 DUMMY	16.46	0	00:40			
602 CONDUI	T 16.42	0	00:41	6.99	0.07	0.18
603 DUMMY	9.70	0	00:35			
604 DUMMY	3.65	0	00:35			
605 CONDUI	T 13.32	0	00:36	11.62	0.01	0.07
606 DUMMY	12.98	0	00:40			
607 CONDUI	T 26.04	0	00:36	12.42	0.02	0.09
700 DUMMY	5.57	0	00:35			
701 DUMMY	3.87	0	00:35			
702 DUMMY	3.87	0	00:35			
703 CONDUI	T 3.86	0	00:36	4.80	0.01	0.08
801 DUMMY	1.85	0	00:35			

	SWMM Mo	del Pre De	velop	oment 5	Year		
802	DUMMY	5.37	0	00:35			
803	CONDUIT	7.18	0	00:36	6.34	0.01	0.07
804	DUMMY	1.92	0	00:35			
806	DUMMY	8.07	0	00:35			
805	CONDUIT	1.91	0	00:37	4.00	0.01	0.06
301	DUMMY	9.95	0	00:35			
101	DUMMY	13.03	0	00:35			
206	DUMMY	17.56	0	00:41			
501	DUMMY	32.34	0	00:35			
704	DUMMY	9.42	0	00:36			
807	DUMMY	17.11	0	00:36			
608	DUMMY	42.32	0	00:41			
403	DUMMY	30.00	0	00:38			

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Conduit Surcharge Summary \*\*\*\*\*\*\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Apr 10 17:42:01 2020 Analysis ended on: Fri Apr 10 17:42:01 2020 Total elapsed time: < 1 sec EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/01/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal \_ Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 193.874 63.177 External Outflow ..... 193.874 63.177 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... -0.000

#### \*\*\*\*\*\*

Routing ******	Time Step Summary ******			
Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.00	
Percent	Not Converging	:	0.00	

\*\*\*\*\*\*

Node Depth Summary \*\*\*\*\*\*\*\*

72

Time of Max Reported Average Maximum Maximum Depth Depth HGL **Occurrence** Max Depth Node Feet Feet Feet days hr:min Feet Туре - - - -10 JUNCTION 0.00 0.00 6975.00 0 00:00 0.00 20 0.00 JUNCTION 0.00 6982.00 0 00:00 0.00 0.00 21 JUNCTION 0.00 6953.00 0 00:00 0.00 22 JUNCTION 0.00 0.00 6936.00 0 00:00 0.00 23 0.08 0.31 6945.31 JUNCTION 0 00:35 0.30 24 JUNCTION 0.13 0.58 6934.58 0 00:40 0.58 30 0.00 JUNCTION 0.00 6985.00 0 00:00 0.00 40 JUNCTION 0.00 0.00 6918.00 0 00:00 0.00 41 JUNCTION 0.00 0.00 6888.00 0 00:00 0.00 42 JUNCTION 0.10 0.48 6911.48 0 00:35 0.48 50 0.00 0.00 0 JUNCTION 6945.00 00:00 0.00 60 0.00 0.00 6942.00 0.00 JUNCTION 0 00:00 61 JUNCTION 0.00 0.00 6893.00 0 00:00 0.00 62 JUNCTION 0.00 0.00 6908.00 0 00:00 0.00 63 JUNCTION 0.00 0.00 6882.00 0 00:00 0.00 64 JUNCTION 0.11 0.48 6900.48 0 00:35 0.48 65 0.17 0.69 JUNCTION 6880.69 0 00:36 0.69 66 0.24 0.89 6868.89 0 00:40 0.89 JUNCTION 70 0.00 0.00 JUNCTION 6923.00 0 00:00 0.00 71 JUNCTION 0.00 0.00 6908.00 0 00:00 0.00

0.00

6904.00

0

00:00

0.00

0.00

JUNCTION

	SWMM 5	Year Out	put Ex 9	9-21-20			
73	JUNCTION	0.11	0.43	6902.43	0	00:35	0.42
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.11	0.48	6872.48	0	00:35	0.47
85	JUNCTION	0.06	0.30	6874.30	0	00:35	0.30
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.13	0.58	6911.58	0	00:40	0.58
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.11	0.42	6900.42	0	00:36	0.42
PondH	JUNCTION	0.11	0.47	6866.47	0	00:36	0.47
PondF	JUNCTION	0.24	0.89	6866.89	0	00:41	0.88
PondD	JUNCTION	0.10	0.48	6881.48	0	00:37	0.47
31	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
51	JUNCTION	0.00	0.00	6920.00	0	00:00	0.00
67	JUNCTION	0.00	0.00	6865.50	0	00:00	0.00
74	JUNCTION	0.00	0.00	6897.00	0	00:00	0.00
0S1	JUNCTION	0.00	0.00	6950.00	0	00:00	0.00
0S2	JUNCTION	0.00	0.00	6924.00	0	00:00	0.00
053	JUNCTION	0.00	0.00	6930.00	0	00:00	0.00
0S4	JUNCTION	0.00	0.00	6905.00	0	00:00	0.00
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00

## \*\*\*\*\*

Node Inflow Summary \*\*\*\*\*\*\*\*\*

			Maximum	Maximum		Lateral	
Total	Flow		_	_			
T., (]., .	Deleves		Lateral	Total	Time of Max	Inflow	
TUTION	Balance		Inflow	Inflow	Occupponco	Volumo	
Volume	Error		THLTOM	THITOM	occurrence	VOLUME	
Node		Туре	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent	21			2	C	
10			12 02	12 03	0 00.35	0 304	
τO		JUNCTION	12.02	12.02	0 00.55	0.504	

# SWMM 5 Year Output Ex 9-21-20

0 304	a aaa						
20	0.000	JUNCTION	4.33	4.33	0	00:35	0.085
0.085	0.000						
21		JUNCTION	1.66	1.66	0	00:40	0.0573
0.0573	0.000		11 OE	11 OE	0	00.10	0 274
0.274	0.000	JUNCTION	11.05	11.05	U	00.40	0.274
23	0.000	JUNCTION	0.00	5.99	0	00:35	0
0.142	0.000						
24		JUNCTION	0.00	21.23	0	00:40	0
0.452	0.000		0.05	0.05	0	00.25	0 170
30	0 000	JUNCIION	9.95	9.95	0	00:35	0.1/9
10.179	0.000		8 1 2	8 1 2	a	QQ • 35	0 162
40 0.162	0.000	JUNCTION	0.12	0.12	0	00.55	0.102
41	0.000	JUNCTION	22.23	22.23	0	00:40	0.522
0.522	0.000				-		
42		JUNCTION	0.00	8.12	0	00:35	0
0.162	0.000						
50		JUNCTION	32.34	32.34	0	00:35	0.593
0.593	0.000		0.70	0 70	•	00.05	0.000
60	0 000	JUNCIION	9.70	9.70	0	00:35	0.226
61	0.000		16 46	16 46	Q	00.10	0 153
0.453	0.000	JUNCTION	10.40	10.40	0	00.40	0.455
62	0.000	JUNCTION	3.65	3.65	0	00:35	0.0858
0.0858	0.000						
63		JUNCTION	12.98	12.98	0	00:40	0.345
0.345	0.000						
64		JUNCTION	0.00	13.35	0	00:35	0
0.311	0.000		0.00	26.04	0	00.00	0
65 0 657	0 000	JUNCIION	0.00	26.04	0	00:36	0
66	0.000		0 00	16 46	a	00·10	Q
0.453	0.000	JUNCTION	0.00	10.40	0	00.40	0
70		JUNCTION	5.57	5.57	0	00:35	0.135
0.135	0.000						
71		JUNCTION	3.87	3.87	0	00:35	0.101
0.101	0.000						
72		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000		0.00	2 07	0	00.25	0
/3	0 000	JUNCIION	0.00	3.8/	0	00:35	0
80	0.000		1 85	1 25	a	00.35	0 0176
0.0476	0.000	JOINCITON	1.05	1.05	0	00.55	0.0470
81		JUNCTION	5.37	5.37	0	00:35	0.124
0.124	0.000						
82		JUNCTION	1.92	1.92	0	00:35	0.0398

# SWMM 5 Year Output Ex 9-21-20

0 0398	a aaa						
83	0.000	JUNCTION	8.07	8.07	0	00:35	0.185
0.185	0.000	5011012011	0107	0107	Ũ	00133	01205
84		JUNCTION	0.00	7.22	0	00:35	0
0.172	0.000						
85		JUNCTION	0.00	1.92	0	00:35	0
0.0398	0.000						
PondC		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000		0.00	42.02	•	00.05	
PondA	0 000	JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000		0.00	26.06	٥	00.40	٥
	0 000	JUNCTION	0.00	26.96	0	00:40	0
DondE	0.000		0 00	22 24	Q	00.35	0
0 593	0 000	JUNCTION	0.00	52.54	0	00.55	0
PondG	0.000		9 99	189 42	Q	00·36	0
29.3	0.000	JUNCTION	0.00	107.42	0	00.50	Ū
PondH	0.000	JUNCTION	0.00	17.11	0	00:36	0
0.397	0.000	5011012011	0.00	_/ •	Ũ	00.50	Ū
PondF		JUNCTION	0.00	42.32	0	00:41	0
1.11	0.000				Ū.		·
PondD		JUNCTION	0.00	30.00	0	00:38	0
0.685	0.000						
31		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000						
51		JUNCTION	0.00	93.34	0	00:35	0
10.4	0.000						
67		JUNCTION	0.00	231.47	0	00:40	0
30.4	0.000						
74		JUNCTION	0.00	189.42	0	00:36	0
29.3	0.000						
0S1		JUNCTION	67.00	67.00	0	00:00	10.8
10.8	0.000				_		
052		JUNCTION	59.00	59.00	0	00:00	9.53
9.53	0.000		64 00	<i>c1</i> 00	•	~~ ~~	0.00
053	0 000	JUNCTION	61.00	61.00	0	00:00	9.86
9.85	0.000		190 00	100 00	٥	00.00	20 1
20 1	0 000	JUNCTION	100.00	100.00	0	00.00	29.1
0utfall2	0.000	ΟΠΤΕΛΙΙ	0 00	85 96	a	00.10	0
10 1	0 000	UUTTALL	0.00	05.50	0	00.40	0
Outfall1	0.000	ΟΠΤΕΔΙΙ	9 99	80 03	Q	00·35	Ø
11.1	0.000	CONTREE	0.00	00.05	Ŭ	00.35	Ŭ
Outfall4		OUTFALL	0.00	341.05	0	00:36	0
41.2	0.000				-		·
Outfall3	-	OUTFALL	0.00	30.00	0	00:38	0
0.685	0.000						

\*\*\*\*\*\*

Node Flooding Summary \*\*\*\*\*\*\*\*\*

No nodes were flooded.

## \*\*\*\*\*

Outfall Loading Summary \*\*\*\*\*\*\*\*\*\*

Outfall Node	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
	Pcnt	CFS	CFS	10^6 gal
Outfall2	100.00	62.68	85.96	10.120
Outfall1	100.00	68.88	80.03	11.121
Outfall4	100.00	255.45	341.05	41.246
Outfall3	60.56	7.00	30.00	0.685
System	90.14	394.01	536.81	63.172

DUMMY

DUMMY

CONDUIT

\*\*\*\*\*

Link Flow Summary

601 602

603

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

Link	Туре	Maximum  Flow  CFS	Time Occu days	of Max Irrence hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	 13.03	0	00:35			
200	DUMMY	4.33	0	00:35			
201	DUMMY	1.66	0	00:40			
202	CONDUIT	5.95	0	00:36	10.09	0.00	0.04
204	DUMMY	11.85	0	00:40			
205	CONDUIT	21.20	0	00:40	14.13	0.01	0.08
300	DUMMY	9.95	0	00:35			
400	DUMMY	8.12	0	00:35			
401	CONDUIT	8.03	0	00:37	8.38	0.02	0.10
402	DUMMY	22.23	0	00:40			
500	DUMMY	32.34	0	00:35			

0 00:40

0 00:41

0 00:35

6.99

0.07

0.18

16.46

16.42

9.70

	SWMM	5 Year Out	put E	Ex 9-21-2	0		
604	DUMMY	3.65	0	00:35			
605	CONDUIT	13.32	0	00:36	11.62	0.01	0.07
606	DUMMY	12.98	0	00:40			
607	CONDUIT	26.04	0	00:36	12.42	0.02	0.09
700	DUMMY	5.57	0	00:35			
701	DUMMY	3.87	0	00:35			
702	DUMMY	3.87	0	00:35			
703	CONDUIT	3.86	0	00:36	4.80	0.01	0.08
801	DUMMY	1.85	0	00:35			
802	DUMMY	5.37	0	00:35			
803	CONDUIT	7.18	0	00:36	6.34	0.01	0.07
804	DUMMY	1.92	0	00:35			
806	DUMMY	8.07	0	00:35			
805	CONDUIT	1.91	0	00:37	4.00	0.01	0.06
301	DUMMY	9.95	0	00:35			
101	DUMMY	13.03	0	00:35			
206	DUMMY	26.96	0	00:40			
501	DUMMY	32.34	0	00:35			
704	DUMMY	189.42	0	00:36			
807	DUMMY	17.11	0	00:36			
608	DUMMY	42.32	0	00:41			
403	DUMMY	30.00	0	00:38			
41	DUMMY	9.95	0	00:35			
42	DUMMY	93.34	0	00:35			
43	DUMMY	231.47	0	00:40			
44	DUMMY	189.42	0	00:36			
45	DUMMY	180.00	0	00:00			
46	DUMMY	67.00	0	00:00			
47	DUMMY	59.00	0	00:00			
48	DUMMY	61.00	0	00:00			

\*\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:32:27 2020 Analysis ended on: Mon Sep 21 16:32:27 2020 Total elapsed time: < 1 sec

## SWMM Model Pre Development 100 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ SWMM 100 Year Pre Development NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/01/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal ---------Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 26.931 82.644 External Outflow ..... 82.609 26.919 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... 0.043

SWMM Model Pre Development 100 Year \*\*\*\*\*\*\* Link 608 (1)

\*\*\*\*\*\*

Routing Time Step Summary \*\*\*\*\*\*

:	30.00 sec
:	30.00 sec
:	30.00 sec
:	0.00
:	1.04
:	0.00
	::

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Node Depth Summary

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Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time Occu days	of Max rrence hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0	00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.21	0.59	6945.59	0	00:45	0.58
24	JUNCTION	0.36	1.43	6935.43	0	00:45	1.42
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.24	1.05	6912.05	0	00:40	1.05
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.27	1.04	6901.04	0	00:45	1.03
65	JUNCTION	0.43	1.52	6881.52	0	00:45	1.52
66	JUNCTION	0.61	2.08	6870.08	0	00:50	2.08
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.27	0.94	6902.94	0	00:45	0.94

	SWMM Model	l Pre Dev	elopment	: 100 Year			
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.32	1.19	6873.19	0	00:45	1.18
85	JUNCTION	0.15	0.64	6874.64	0	00:40	0.64
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.39	1.43	6912.43	0	00:46	1.42
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.27	0.94	6900.94	0	00:46	0.94
PondH	JUNCTION	0.32	1.18	6867.18	0	00:46	1.18
PondF	JUNCTION	0.61	2.08	6868.08	0	00:51	2.08
PondD	JUNCTION	0.25	1.05	6882.05	0	00:42	1.05
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
31	OUTFALL	0.00	0.00	6953.00	0	00:00	0.00
51	OUTFALL	0.00	0.00	6920.00	0	00:00	0.00
74	OUTFALL	0.00	0.00	6897.00	0	00:00	0.00
67	OUTFALL	0.00	0.00	6865.50	0	00:00	0.00

\*\*\*\*\*

Node Inflow Summary \*\*\*\*\*\*\*\*\*

	 F1		Maximum	Maximum		Lateral	
Ισται	FIOM		Lateral	Total	Time of Max	Inflow	
Inflow	Balance						
			Inflow	Inflow	Occurrence	Volume	
Volume Node	Error	Туре	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent				-	C	
10		JUNCTION	13.03	13.03	0 00:35	0.304	
0.304	0.000						
20		JUNCTION	4.33	4.33	0 00:35	0.085	
0.085	0.000						
21		JUNCTION	20.74	20.74	0 00:50	0.794	
0.794	0.000						

		SWMM Mode	el Pre Dev	velopment	100 Ye	ear	
22		JUNCTION	140.35	140.35	0	00:45	3.79
3.79	0.000						
23		JUNCTION	0.00	23.90	0	00:45	0
0.879	0.000						
24		JUNCTION	0.00	140.35	0	00:45	0
3.79	0.000						
30		JUNCTION	110.70	110.70	0	00:40	2.47
2.47	0.000						
40		JUNCTION	40.00	40.00	0	00:40	1.03
1.03	0.000						
41		JUNCTION	114.87	114.87	0	00:45	3.31
3.31	0.000				_		_
42		JUNCTION	0.00	40.00	0	00:40	0
1.03	0.000						
50		JUNCIION	157.99	157.99	0	00:40	3.76
3.76	0.000						4 45
60	0.000	JUNCIION	49.45	49.45	0	00:45	1.43
1.43	0.000		06 70	06 70	0	00.50	2.07
61	0.000	JUNCITON	86.73	86.73	0	00:50	2.8/
2.8/	0.000		10 42	10 40	0	00.45	0 544
	0 000	JUNCTION	18.42	18.42	0	00:45	0.544
62	0.000		67 92	67 00	0	00.45	2 10
2 10	0 000	JUNCTION	07.02	07.02	0	00.45	2.19
2.19	0.000		0 00	67 97	0	00.15	0
1 07	0 000	JUNCTION	0.00	07.07	0	00.45	U
65	0.000		0 00	135 62	a	00.15	0
4 16	0 000	JONCTION	0.00	155.02	U	00.45	Ū
10	0.000		a aa	86 73	Q	00·50	Q
2.87	0,000	Somerion	0.00	00.75	Ŭ	00.50	Ŭ
70	0.000	JUNCTION	28.46	28.46	0	00:45	0.853
0.853	0,000				· ·		
71		JUNCTION	20.06	20.06	0	00:45	0.641
0.641	0.000				-		
72		JUNCTION	0.00	20.06	0	00:45	0
0.641	0.000						
73		JUNCTION	0.00	20.06	0	00:45	0
0.641	0.000						
80		JUNCTION	21.89	21.89	0	00:45	0.659
0.659	0.000						
81		JUNCTION	27.12	27.12	0	00:45	0.786
0.786	0.000						
82		JUNCTION	9.51	9.51	0	00:40	0.252
0.252	0.000						
83		JUNCTION	40.86	40.86	0	00:45	1.17
1.17	0.000						
84		JUNCTION	0.00	49.01	0	00:45	0
1.44	0.000						

		SWMM Model	Pre Dev	elopment	100 Ye	ar	
85		JUNCTION	0.00	9.51	0	00:40	0
0.252	0.000						
PondC		JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000						
PondA		JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000						
PondB		JUNCTION	0.00	164.21	0	00:46	0
4.66	0.000						
PondE		JUNCTION	0.00	157.99	0	00:40	0
3.76	0.000						
PondG		JUNCTION	0.00	48.48	0	00:45	0
1.49	0.000						
PondH		JUNCTION	0.00	99.16	0	00:45	0
2.87	0.000						
PondF		JUNCTION	0.00	221.11	0	00:46	0
7.02	0.000						
PondD		JUNCTION	0.00	154.35	0	00:45	0
4.34	0.000						
Outfall2		OUTFALL	0.00	164.21	0	00:46	0
4.66	0.000						
Outfall1		OUTFALL	0.00	13.03	0	00:35	0
0.304	0.000						
Outfall4		OUTFALL	0.00	99.16	0	00:45	0
2.87	0.000						
Outfall3		OUTFALL	0.00	154.35	0	00:45	0
4.34	0.000						
31		OUTFALL	0.00	110.70	0	00:40	0
2.47	0.000						
51		OUTFALL	0.00	157.99	0	00:40	0
3.76	0.000						
74		OUTFALL	0.00	48.48	0	00:45	0
1.49	0.000						
67		OUTFALL	0.00	221.11	0	00:46	0
7.02	0.000						

No nodes were flooded.

	SWMM Model Pre Development 100 Year						
	Flow	Avg	Max	Total			
	Freq	Flow	Flow	Volume			
Outfall Node	Pcnt	CFS	CFS	10^6 gal			
Outfall2	76.53	37.73	164.21	4.665			
Outfall1	55.28	3.40	13.03	0.304			
Outfall4	67.08	26.46	99.16	2.867			
Outfall3	67.92	39.52	154.35	4.336			
31	53.89	28.39	110.70	2.472			
51	58.47	39.76	157.99	3.757			
74	67.08	13.78	48.48	1.494			
67	74.31	58.49	221.11	7.022			
System	65.07	247.53	962.28	26.917			

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Link Flow Summary \*\*\*\*\*\*\*\*\*

Link	Туре	Maximum  Flow  CFS	Time Occu days	of Max Irrence hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	13.03	0	00:35			
200	DUMMY	4.33	0	00:35			
201	DUMMY	20.74	0	00:50			
202	CONDUIT	23.89	0	00:46	15.49	0.01	0.08
204	DUMMY	140.35	0	00:45			
205	CONDUIT	140.32	0	00:46	24.86	0.09	0.20
300	DUMMY	110.70	0	00:40			
400	DUMMY	40.00	0	00:40			
401	CONDUIT	39.84	0	00:42	13.30	0.10	0.21
402	DUMMY	114.87	0	00:45			
500	DUMMY	157.99	0	00:40			
601	DUMMY	86.73	0	00:50			
602	CONDUIT	86.65	0	00:51	11.22	0.36	0.42
603	DUMMY	49.45	0	00:45			
604	DUMMY	18.42	0	00:45			
605	CONDUIT	67.80	0	00:45	19.12	0.05	0.15
606	DUMMY	67.82	0	00:45			
607	CONDUIT	135.63	0	00:46	20.33	0.08	0.19
700	DUMMY	28.46	0	00:45			
701	DUMMY	20.06	0	00:45			
702	DUMMY	20.06	0	00:45			
703	CONDUIT	20.04	0	00:46	7.87	0.08	0.19
801	DUMMY	21.89	0	00:45			

	SWMM Mod	lel Pre Dev	relopr	nent 100	Year		
802	DUMMY	27.12	0	00:45			
803	CONDUIT	48.96	0	00:46	11.36	0.06	0.17
804	DUMMY	9.51	0	00:40			
806	DUMMY	40.86	0	00:45			
805	CONDUIT	9.46	0	00:42	6.45	0.04	0.13
301	DUMMY	110.70	0	00:40			
101	DUMMY	13.03	0	00:35			
206	DUMMY	164.21	0	00:46			
501	DUMMY	157.99	0	00:40			
704	DUMMY	48.48	0	00:45			
807	DUMMY	99.16	0	00:45			
608	DUMMY	221.11	0	00:46			
403	DUMMY	154.35	0	00:45			

\*\*\*\*\*\*\*

Conduit Surcharge Summary \*\*\*\*\*\*\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Apr 10 13:11:18 2020 Analysis ended on: Fri Apr 10 13:11:18 2020 Total elapsed time: < 1 sec

#### SWMM 100 Year Output EX 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/01/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal \_ Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 272.651 836.701 External Outflow ..... 836.646 272.634 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... 0.007
SWMM 100 Year Output EX 9-21-20 Highest Flow Instability Indexes \* Link 205 (1) Link 608 (1) Link 206 (1) \*\*\*\*\*\* Routing Time Step Summary \*\*\*\*\*\* Minimum Time Step 30.00 sec : Average Time Step : 30.00 sec Maximum Time Step : 30.00 sec Percent in Steady State : 0.00 Average Iterations per Step : 1.03 Percent Not Converging 0.00 :

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Node Depth Summary \*\*\*\*\*\*\*\*

		Average	Maximum Denth	Maximum HGL	Time	of Max	Reported Max Denth
Node	Туре	Feet	Feet	Feet	days	hr:min	Feet
10	JUNCTION	0.00	0.00	6975.00		00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.28	0.97	6945.97	0	00:45	0.97
24	JUNCTION	0.45	1.91	6935.91	0	00:45	1.91
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.24	1.05	6912.05	0	00:40	1.05
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.27	1.04	6901.04	0	00:45	1.03
65	JUNCTION	0.43	1.52	6881.52	0	00:45	1.52
66	JUNCTION	0.61	2.08	6870.08	0	00:50	2.08
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00

	SWMM 100	) Year Ou	tput EX	9-21-20			
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.27	0.94	6902.94	0	00:45	0.94
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.32	1.19	6873.19	0	00:45	1.18
85	JUNCTION	0.15	0.64	6874.64	0	00:40	0.64
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.48	1.91	6912.91	0	00:45	1.90
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.27	0.94	6900.94	0	00:46	0.94
PondH	JUNCTION	0.32	1.18	6867.18	0	00:46	1.18
PondF	JUNCTION	0.61	2.08	6868.08	0	00:51	2.08
PondD	JUNCTION	0.25	1.05	6882.05	0	00:42	1.05
31	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
51	JUNCTION	0.00	0.00	6920.00	0	00:00	0.00
67	JUNCTION	0.00	0.00	6865.50	0	00:00	0.00
74	JUNCTION	0.00	0.00	6897.00	0	00:00	0.00
0S1	JUNCTION	0.00	0.00	6950.00	0	00:00	0.00
0S2	JUNCTION	0.00	0.00	6924.00	0	00:00	0.00
0S3	JUNCTION	0.00	0.00	6930.00	0	00:00	0.00
0S4	JUNCTION	0.00	0.00	6905.00	0	00:00	0.00
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00

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Node Inflow Summary

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-----------\_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ -----Maximum Maximum Lateral Total Flow Lateral Total Time of Max Inflow Inflow Balance Inflow Inflow **Occurrence** Volume Volume Error Node CFS CFS days hr:min 10^6 gal 10^6 Туре Percent gal \_\_\_\_\_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ -----

1.92 1.18 0.794 3.79 0 0
1.18 0.794 3.79 0 0
1.18 0.794 3.79 0 0
0.794 3.79 0 0
0.794 3.79 0 0
3.79 0 0
3.79 0 0
0 0
0
0
0
2.47
1.03
3.31
0
3.76
1.43
2 07
2.8/
0 511
0.544
2 19
2.13
0
0
0
0.853
0.641
0
0
Q
U
0.659
0.659
0.659 0.786

		SWMM	100 Year 0	utput EX	9-21-2	9	
82		JUNCTION	9.51	9.51	0	00:40	0.252
0.252	0.000						
83		JUNCTION	40.86	40.86	0	00:45	1.17
1.17	0.000			40.04	•	00.45	
84	0 000	JUNCIION	0.00	49.01	0	00:45	0
1.44 or	0.000		0 00	0 51	0	00.10	0
0 0 252	a aaa	JUNCTION	0.00	9.51	Ø	00.40	0
PondC	0.000	JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000				Ū		-
PondA		JUNCTION	0.00	66.80	0	00:45	0
1.92	0.000						
PondB		JUNCTION	0.00	317.41	0	00:45	0
8.22	0.000						
PondE		JUNCTION	0.00	157.99	0	00:40	0
3.76	0.000			642.40	•	00.45	
Pondg	0 000	JUNCITON	0.00	643.48	0	00:45	0
97.0 PondH	0.000		0 00	00 16	Q	00.15	0
2 87	a aaa	JUNCTION	0.00	55.10	0	00.45	0
PondF	0.000	JUNCTION	0.00	221.11	0	00:46	0
7.02	0.000				-		-
PondD		JUNCTION	0.00	154.35	0	00:45	0
4.34	0.000						
31		JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000				-		_
51	0 000	JUNCIION	0.00	374.99	0	00:40	0
38.8	0.000		0 00	964 53	0	00.16	0
105	a aaa	JUNCTION	0.00	004.52	Ø	00.40	0
74	0.000	JUNCTION	0.00	643.48	0	00:45	0
97.6	0.000			0.000.00	Ū		-
0S1		JUNCTION	413.00	413.00	0	00:00	66.7
66.7	0.000						
0S2		JUNCTION	280.00	280.00	0	00:00	45.2
45.2	0.000						
053		JUNCTION	217.00	217.00	0	00:00	35.1
35 0	.000				0	00.00	06.1
054 96 1	0 000	JUNCTION	595.00	595.00	0	00:00	96.1
0utfall2	0.000	ΟΠΤΕΔΙΙ	9 99	597 <i>4</i> 1	a	00·15	0
53.4	0.000	OUTIALL	0.00	JJ/ • + I	0	00.45	0
Outfall1	0.000	OUTFALL	0.00	479.80	0	00:45	0
68.6	0.000						
Outfall4		OUTFALL	0.00	1335.77	0	00:45	0
146	0.000						
Outfall3		OUTFALL	0.00	154.35	0	00:45	0
4.34	0.000						

Node Flooding Summary \*\*\*\*\*\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*\*

Outfall Loading Summary \*\*\*\*\*\*\*\*\*\*\*\*

Outfall Node	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
	Pcnt	CFS	CFS	10^6 gal
Outfall2	100.00	330.89	597.41	53.430
Outfall1	100.00	424.90	479.80	68.605
Outfall4	100.00	905.71	1335.77	146.242
Outfall3	67.92	39.52	154.35	4.336
System	91.98	1701.02	2567.34	272.613

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*\*

Link	Туре	Maximum  Flow  CFS	Time Occu days	of Max Irrence hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	 66.80		00:45			
200	DUMMY	48.76	0	00:40			
201	DUMMY	20.74	0	00:50			
202	CONDUIT	68.51	0	00:45	21.36	0.04	0.14
204	DUMMY	140.35	0	00:45			
205	CONDUIT	248.90	0	00:45	29.30	0.16	0.27
300	DUMMY	110.70	0	00:40			
400	DUMMY	40.00	0	00:40			
401	CONDUIT	39.84	0	00:42	13.30	0.10	0.21
402	DUMMY	114.87	0	00:45			
500	DUMMY	157.99	0	00:40			
601	DUMMY	86.73	0	00:50			
602	CONDUIT	86.65	0	00:51	11.22	0.36	0.42

	SWMM	100 Year 0	utput	EX 9-21-	20		
603	DUMMY	49.45	0	00:45			
604	DUMMY	18.42	0	00:45			
605	CONDUIT	67.80	0	00:45	19.12	0.05	0.15
606	DUMMY	67.82	0	00:45			
607	CONDUIT	135.63	0	00:46	20.33	0.08	0.19
700	DUMMY	28.46	0	00:45			
701	DUMMY	20.06	0	00:45			
702	DUMMY	20.06	0	00:45			
703	CONDUIT	20.04	0	00:46	7.87	0.08	0.19
801	DUMMY	21.89	0	00:45			
802	DUMMY	27.12	0	00:45			
803	CONDUIT	48.96	0	00:46	11.36	0.06	0.17
804	DUMMY	9.51	0	00:40			
806	DUMMY	40.86	0	00:45			
805	CONDUIT	9.46	0	00:42	6.45	0.04	0.13
301	DUMMY	110.70	0	00:40			
101	DUMMY	66.80	0	00:45			
206	DUMMY	317.41	0	00:45			
501	DUMMY	157.99	0	00:40			
704	DUMMY	643.48	0	00:45			
807	DUMMY	99.16	0	00:45			
608	DUMMY	221.11	0	00:46			
403	DUMMY	154.35	0	00:45			
41	DUMMY	110.70	0	00:40			
42	DUMMY	374.99	0	00:40			
43	DUMMY	864.52	0	00:46			
44	DUMMY	643.48	0	00:45			
45	DUMMY	595.00	0	00:00			
46	DUMMY	413.00	0	00:00			
47	DUMMY	280.00	0	00:00			
48	DUMMY	217.00	0	00:00			

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:37:19 2020 Analysis ended on: Mon Sep 21 16:37:19 2020 Total elapsed time: < 1 sec SWMM 5 Year Post Development

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*

Analysis Options \*\*\*\*\*\*\*\*\*

Flow Units	CFS	
Process Models:		
Rainfall/Runoff	NO	
RDII	NO	
Snowmelt	NO	
Groundwater	NO	
Flow Routing	YES	
Ponding Allowed	NO	
Water Quality	NO	
Flow Routing Method	KINWAVE	
Starting Date	01/01/2005	00:00:00
Ending Date	01/02/2005	06:00:00
Antecedent Dry Days	0.0	
Report Time Step	00:05:00	
Routing Time Step	30.00 sec	

********	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*******		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	39.629	12.914
External Outflow	23.957	7.807
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	15.654	5.101
Continuity Error (%)	0.045	

### \*\*\*\*\*\*\*\*\*\*\*

#### \*\*\*\*\*\*

Routing *****	Time Step Summary *******			
Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.01	
Percent	Not Converging	:	0.00	

\*\*\*\*\*\*

Node Depth Summary \*\*\*\*\*\*\*\*

66

Average Maximum Maximum Time of Max Reported Depth Depth HGL **Occurrence** Max Depth Node Type Feet Feet Feet days hr:min Feet ----10 JUNCTION 0.00 0.00 6975.00 0 00:00 0.00 20 0.00 0.00 6982.00 00:00 0.00 JUNCTION 0 21 0.00 JUNCTION 0.00 6953.00 0 00:00 0.00 0.00 22 JUNCTION 0.00 6936.00 0 00:00 0.00 23 0.04 0.75 6945.75 0.74 JUNCTION 0 00:30 24 JUNCTION 0.21 1.17 6935.17 0 00:30 1.16 30 0.00 0.00 0.00 JUNCTION 6985.00 0 00:00 31 JUNCTION 0.17 0.20 6953.20 0 02:23 0.20 0.59 67 JUNCTION 0.16 6866.09 0 01:57 0.59 40 JUNCTION 0.00 0.00 6918.00 0 00:00 0.00 41 0.00 0.00 JUNCTION 6888.00 0 00:00 0.00 42 0.03 0.82 6911.82 0.81 JUNCTION 0 00:30 50 JUNCTION 0.00 0.00 6945.00 0 00:00 0.00 51 JUNCTION 0.03 0.21 6920.21 0 01:12 0.21 60 JUNCTION 0.00 0.00 6942.00 0 00:00 0.00 61 JUNCTION 0.00 0.00 6893.00 0 00:00 0.00 62 0.00 JUNCTION 0.00 6908.00 0 00:00 0.00 63 0.00 0.00 6882.00 0 00:00 0.00 JUNCTION 0.03 64 JUNCTION 0.66 6900.66 0 00:35 0.66 65 JUNCTION 0.05 1.10 6881.10 0 00:35 1.10

0.08

JUNCTION

1.71

6869.71

0

00:35

1.71

		SWMM 5 Yea	ır Outpu	t			
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.03	0.55	6902.55	0	00:35	0.54
74	JUNCTION	0.02	0.24	6897.24	0	01:15	0.24
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.04	0.80	6872.80	0	00:30	0.79
85	JUNCTION	0.02	0.48	6874.48	0	00:30	0.47
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.16	0.59	6865.59	0	01:57	0.59
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	5.89	6.37	6917.37	0	01:30	6.37
PondC	STORAGE	4.70	5.56	6961.56	0	02:23	5.56
PondA	STORAGE	4.01	4.67	6953.67	0	01:46	4.67
PondD	STORAGE	5.54	6.51	6887.51	0	02:25	6.51
PondE	STORAGE	4.04	4.77	6927.77	0	01:12	4.77
PondF	STORAGE	5.76	6.73	6872.73	0	02:02	6.73
PondG	STORAGE	0.11	1.20	6901.20	0	01:15	1.20
PondH	STORAGE	4.49	5.12	6871.12	0	02:09	5.12

Node Inflow Summary \*\*\*\*\*\*\*\*\*\*

\_\_\_\_\_ -----

_			Maximum	Maximum		Lateral	
Total	Flow		Lateral	Total	Time of Max	Inflow	
Inflow	Balance		Inflow	Inflow	Occurrence	Volume	
Volume	Error	Tuno	CES	CES	dave hnimin	10^6 gp]	10^6
gal	Percent	туре	CF3	CFS	uays mainin	IO O BAT	10 0
10		JUNCTION	30.72	30.72	0 00:35	0.705	
0.705	0.000						
20	0.000	JUNCTION	29.46	29.46	0 00:30	0.578	
21	0.000	JUNCTION	12.02	12.02	0 00:35	0.376	

			SWMM 5 Yea	r Output			
0.376	0.000		00 76	00 76	0	00.20	2.04
22	0 000	JUNCITON	92.76	92.76	0	00:30	2.04
2.04	0.000		0 00	40 92	a	00·30	0
0.954	0.000	JONCTION	0.00	40.52	U	00.50	0
24	01000	JUNCTION	0.00	93.26	0	00:30	0
2.96	0.000				÷		-
30		JUNCTION	77.99	77.99	0	00:30	1.38
1.38	0.000						
31		JUNCTION	0.00	1.52	0	02:23	0
0.925	0.000						
67		JUNCTION	0.00	23.06	0	01:57	0
2.4	-0.000						
40		JUNCTION	24.15	24.15	0	00:30	0.438
0.438	0.000						
41		JUNCTION	98.47	98.47	0	00:30	1.83
1.83	0.000						
42		JUNCTION	0.00	24.15	0	00:30	0
0.438	-0.000						
50		JUNCTION	46.88	46.88	0	00:35	0.982
0.982	0.000						
51		JUNCTION	0.00	18.70	0	01:12	0
0.69	0.000						
60		JUNCTION	16.28	16.28	0	00:35	0.424
0.424	0.000						
61		JUNCTION	60.11	60.11	0	00:35	1.38
1.38	0.000						
62		JUNCTION	11.36	11.36	0	00:30	0.234
0.234	0.000						
63		JUNCTION	42.32	42.32	0	00:30	0.975
0.975	0.000						
64		JUNCTION	0.00	26.88	0	00:35	0
0.659	0.000						
65		JUNCTION	0.00	69.12	0	00:35	0
1.63	0.000				_		_
66		JUNCTION	0.00	60.11	0	00:35	0
1.38	0.000				-		
70		JUNCTION	13.78	13.78	0	00:30	0.32
0.32	0.000		6 55		•	00.05	0 101
/1	0.000	JUNCTION	6.55	6.55	0	00:35	0.191
0.191	0.000		0 00		•	00.25	0
/2	0.000	JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000		0.00		0	00.25	0
/3	0.000	JUNCITON	0.00	0.55	0	25:00	0
0.191	0.000		0 00	0.05	0	01.15	0
74 0 E1	0 000	JUNCITON	0.00	9.05	0	01:12	0
00 TC'0	-0.000		E 60	5 60	Q	00.25	0 17 <b>0</b>
00		JOINCITON	00.0	2.00	0	00.33	0.1/3

Page 4

			SWMM 5 Yea	ar Output			
0.173	0.000						
81		JUNCTION	16.24	16.24	0	00:30	0.333
0.333	0.000						
82		JUNCTION	5.21	5.21	0	00:30	0.1
0.1	0.000				•		
83		JUNCITON	20.93	20.93	0	00:30	0.453
0.453	0.000		0.00	21 67	0	00.20	0
84	0 000	JUNCITON	0.00	21.67	0	00:30	0
85	0.000		0 00	5 21	Q	00.30	0
0J 0 1	0 000	JUNCTION	0.00	5.21	U	00.50	0
0.1	0.000	ΟΠΤΕΔΙΙ	9 99	34 45	a	01·30	Q
2.22	- 0.000	OUTIALL	0.00	54.45	U	01.90	Ŭ
Outfall	1	OUTFALL	0.00	5.43	0	01:46	0
0.441	0.000				÷		-
Outfall4	4	OUTFALL	0.00	35.27	0	01:51	0
3.71	0.000						
Outfall:	3	OUTFALL	0.00	2.52	0	02:25	0
1.43	0.000						
PondB		STORAGE	0.00	134.27	0	00:31	0
3.91	0.047						
PondC		STORAGE	0.00	77.99	0	00:30	0
1.38	0.005						
PondA		STORAGE	0.00	30.72	0	00:35	0
0.705	0.012				-		_
PondD	0 000	STORAGE	0.00	120.96	0	00:30	0
2.2/	0.003	CTODACE	0.00	46.00	•	00.05	
Ponde	0 110	STORAGE	0.00	46.88	0	00:35	0
0.982	0.118	CTODACE	0.00	120.20	0	00.25	0
	0 014	STURAGE	0.00	129.20	0	00:35	0
BondG	0.014	STOPAGE	0 00	70 07	Q	00.25	0
P01100	0 116	STURAGE	0.00	20.07	U	00.55	0
PondH	0.110	STORAGE	a aa	47 25	a	00·32	Q
1.06	0.001	JIONAGE	0.00	7/ • 43	U	00.52	0
	3.001						

No nodes were flooded.

<b>C</b> 14		Average	Avg	Evap	Exfil	Maximum	Max	Time
ot Max	Maximum	Volume	Pcnt	Pont	Pcnt	Volume	Pont	
Occurrenc	e Outflow	VOLUME	i circ	i circ	i ene	VOIUME	i ene	
Storage	e Unit	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
hr:min	CFS							
PondB		241.825	30	0	0	296.729	37	0
01:30	34.45	111 256	4.0	•	•	474 430	20	•
PondC	1 50	111.256	19	0	0	174.130	30	0
PondA	1.52	53,736	15	0	0	79.797	22	0
01:46	5.43			•	· ·			·
PondD		192.634	28	0	0	287.984	41	0
02:24	2.52			-	-			-
PondE	10 70	56.473	16	0	0	85.437	24	0
PondF	18.70	235 289	29	a	a	351 325	44	a
02:02	16.38	255.205	25	U	Ũ	551.525		0
PondG		2.647	0	0	0	31.290	6	0
01:15	9.05							
PondH		88.617	17	0	0	127.653	25	0
02:09	4.21							

### SWMM 5 Year Output

### \*\*\*\*\*

	Flow Freq	Avg Flow	Max Flow	Total Volume
Outfall Node	Pcnt	CFS	CFS	10^6 gal
Outfall2	99.64	2.76	34.45	2.223
Outfall1	99.67	0.55	5.43	0.441
Outfall4	99.67	4.61	35.27	3.709
Outfall3	99.69	1.78	2.52	1.434
System	99.67	9.70	73.13	7.806

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SWMM 5 Year Output

# Link Flow Summary \*\*\*\*\*\*\*\*\*

Link	Туре	Maximum  Flow  CFS	Time Occu days	of Max urrence hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	 30.72	 а	 00·35			
200		29.46	0	00.33 00·30			
201	DUMMY	12.02	0	00:35			
202	CONDUIT	40.84	0	00:31	18.27	0.02	0.11
203	CONDUIT	1.52	0	02:24	6.34	0.00	0.05
204	DUMMY	92.76	0	00:30			
205	CONDUIT	93.43	0	00:31	22.09	0.06	0.17
300	DUMMY	77.99	0	00:30			
400	DUMMY	24.15	0	00:30			
401	CONDUIT	23.53	0	00:32	11.46	0.06	0.16
402	DUMMY	98.47	0	00:30			
500	DUMMY	46.88	0	00:35			
601	DUMMY	60.11	0	00:35			
602	CONDUIT	60.09	0	00:35	10.17	0.25	0.34
603	DUMMY	16.28	0	00:35			
604	DUMMY	11.36	0	00:30			
605	CONDUIT	26.88	0	00:35	14.61	0.02	0.09
606	DUMMY	42.32	0	00:30			
607	CONDUIT	69.12	0	00:31	16.65	0.04	0.14
700	DUMMY	13.78	0	00:30			
701	DUMMY	6.55	0	00:35			
702	DUMMY	6.55	0	00:35			
703	CONDUIT	6.54	0	00:36	5.62	0.03	0.11
801	DUMMY	5.68	0	00:35			
802	DUMMY	16.24	0	00:30			
803	CONDUIT	21.49	0	00:32	8.87	0.03	0.11
804	DUMMY	5.21	0	00:30			
806	DUMMY	20.93	0	00:30			
805	CONDUIT	5.08	0	00:32	5.42	0.02	0.09
808	CONDUIT	23.06	0	01:57	2.25	0.00	0.06
800	CONDUIT	8.95	0	01:25	2.34	0.00	0.02
600	CONDUIT	18.26	0	01:17	5.75	0.00	0.03
101	DUMMY	5.43	0	01:46			
206	DUMMY	34.45	0	01:30			
301	DUMMY	1.52	0	02:23			
501	DUMMY	18.70	0	01:12			
704	DUMMY	9.05	0	01:15			
807	DUMMY	4.21	0	02:09			
608	DUMMY	16.38	0	02:02			
403	DUMMY	2.52	0	02:25			

### SWMM 5 Year Output

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No conduits were surcharged.

Analysis begun on: Mon Apr 13 19:10:46 2020 Analysis ended on: Mon Apr 13 19:10:46 2020 Total elapsed time: < 1 sec

### SWMM 5 Year Output 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/02/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal \_ Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 949.387 309.372 External Outflow ..... 930.375 303.177 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 6.548 20.095 Continuity Error (%) ..... -0.114

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Routing Time Step Summary \*\*\*\*\*\*\*\*\*\*\*

Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.00	
Percent	Not Converging	:	0.00	

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Node Depth Summary \*\*\*\*\*\*\*\*\*

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Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time Occu days	of Max rrence hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0	00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.04	0.75	6945.75	0	00:30	0.74
24	JUNCTION	0.21	1.17	6935.17	0	00:30	1.16
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
31	JUNCTION	0.17	0.20	6953.20	0	02:23	0.20
67	JUNCTION	1.87	1.97	6867.47	0	01:59	1.97
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.03	0.82	6911.82	0	00:30	0.81
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
51	JUNCTION	0.71	0.71	6920.71	0	00:32	0.71
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.03	0.66	6900.66	0	00:35	0.66
65	JUNCTION	0.05	1.10	6881.10	0	00:35	1.10
66	JUNCTION	0.08	1.71	6869.71	0	00:35	1.71
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00

	SWMM 5	5 Year	Output 9-	21-20			
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.03	0.55	6902.55	0	00:35	0.54
74	JUNCTION	1.36	1.40	6898.40	0	01:15	1.40
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.04	0.80	6872.80	0	00:30	0.79
85	JUNCTION	0.02	0.48	6874.48	0	00:30	0.47
0S1	JUNCTION	0.45	0.45	6953.05	0	00:00	0.45
0S3	JUNCTION	0.71	0.71	6923.51	0	00:00	0.71
0S4	JUNCTION	1.21	1.21	6901.01	0	00:00	1.21
0S2	JUNCTION	0.42	0.42	6924.42	0	00:00	0.42
Outfall2	OUTFALL	0.42	0.42	6910.42	0	03:03	0.42
Outfall1	OUTFALL	0.45	0.45	6947.45	0	01:12	0.45
Outfall4	OUTFALL	1.87	1.97	6866.97	0	01:59	1.97
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.42	6.96	6917.96	0	02:52	6.96
PondC	STORAGE	4.70	5.56	6961.56	0	02:23	5.56
PondA	STORAGE	5.16	6.43	6955.43	0	02:35	6.43
PondD	STORAGE	5.57	6.66	6887.66	0	02:07	6.65
PondE	STORAGE	3.99	4.85	6927.85	0	01:03	4.85
PondF	STORAGE	5.76	6.72	6872.72	0	02:04	6.72
PondG	STORAGE	0.11	1.20	6901.20	0	01:15	1.20
PondH	STORAGE	4.38	5.01	6871.01	0	02:39	5.01

Node Inflow Summary \*\*\*\*\*\*\*\*\*\*

			Maximum	Maximum		Lateral	
lotal	FIOW		Lateral	Total	Time of Max	Inflow	
INTIOW	Balance		Inflow	Inflow	Occurrence	Volume	
Volume Node	Error	Туре	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent						
10 0.705	0.000	JUNCTION	30.72	30.72	0 00:35	0.705	

		SWMM	5 Year Ou	utput 9-21	-20		
20		JUNCTION	29.46	29.46	0	00:30	0.578
0.578	0.000						
21		JUNCTION	12.02	12.02	0	00:35	0.376
0.376	0.000						
22		JUNCTION	92.76	92.76	0	00:30	2.04
2.04	0.000						
23		JUNCTION	0.00	40.92	0	00:30	0
0.954	0.000				_		_
24		JUNCTION	0.00	93.26	0	00:30	0
2.96	0.000						4
30		JUNCTION	77.99	77.99	0	00:30	1.38
1.38	0.000			4 50			
31	0.000	JUNCIION	0.00	1.52	0	02:23	0
0.925	0.000			201 12	•	04 50	
6/	0.000	JUNCIION	0.00	201.42	0	01:59	0
14/	0.000		24.45	24.45	•		0 420
40	0.000	JUNCITON	24.15	24.15	0	00:30	0.438
0.438	0.000		00.47	00 47	0	00.20	1 02
41	0.000	JUNCIION	98.47	98.47	0	00:30	1.83
1.83	0.000		0.00	24.45	0	00.20	0
42	0 000	JUNCTION	0.00	24.15	0	00:30	0
0.438	-0.000		16 00	46 00	0	00.25	0,000
50	0 000	JUNCTION	46.88	46.88	0	00:35	0.982
0.98Z	0.000		0 00	9E 04	0	01.02	0
50	0 000	JUNCITON	0.00	05.04	0	01.05	0
60	0.000		16 28	16 28	Q	00.35	0 121
00 0 1 2 1	0 000	JUNCTION	10.20	10.20	0	00.55	0.424
61	0.000		60 11	60 11	a	00·35	1 38
1 38	0 000	JUNCTION	00.11	00.11	0	00.55	1.50
62	0.000		11.36	11,36	a	00·30	0.234
0.234	0,000	5011011011	11.50	11.30	Ū	00.50	0.251
63	0.000	JUNCTION	42.32	42.32	0	00:30	0.975
0.975	0.000	5011012011		.2.32	Ũ	00.00	01070
64		JUNCTION	0.00	26.88	0	00:35	0
0.659	0.000				-		-
65		JUNCTION	0.00	69.12	0	00:35	0
1.63	0.000				•		·
66		JUNCTION	0.00	60.11	0	00:35	0
1.38	0.000						
70		JUNCTION	13.78	13.78	0	00:30	0.32
0.32	0.000						
71		JUNCTION	6.55	6.55	0	00:35	0.191
0.191	0.000						
72		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						
73		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						

		SWMM 5 Year Output 9-21-20							
74		JUNCTION	0.00	189.05	0	01:15	0		
146	0.000								
80		JUNCTION	5.68	5.68	0	00:35	0.173		
0.173	0.000								
81		JUNCTION	16.24	16.24	0	00:30	0.333		
0.333	0.000								
82		JUNCTION	5.21	5.21	0	00:30	0.1		
0.1	0.000								
83		JUNCTION	20.93	20.93	0	00:30	0.453		
0.453	0.000								
84		JUNCTION	0.00	21.67	0	00:30	0		
0.507	0.000				-		_		
85		JUNCTION	0.00	5.21	0	00:30	0		
0.1	0.000		<b>67 0 0</b>	<b>67</b> 00					
051		JUNCTION	67.00	67.00	0	00:00	54.1		
54.1	0.000				-				
053		JUNCIION	61.00	61.00	0	00:00	49.3		
49.3	0.000		100.00	400.00					
054		JUNCTION	180.00	180.00	0	00:00	145		
145	0.000				-				
052		JUNCTION	59.00	59.00	0	00:00	47.7		
47.7	0.000				_		_		
Out+all	.2	OUTFALL	0.00	61.68	0	02:52	0		
49.4	0.000								
Outfall	.1	OUTFALL	0.00	67.69	0	02:35	0		
54.5	0.000								
Outfall	.4	OUTFALL	0.00	276.10	0	01:07	0		
198	0.000								
Outfall	.3	OUTFALL	0.00	8.58	0	02:07	0		
1.45	0.000								
PondB		STORAGE	0.00	134.27	0	00:31	0		
3.91	-0.000								
PondC		STORAGE	0.00	77.99	0	00:30	0		
1.38	0.005								
PondA		STORAGE	0.00	30.72	0	00:35	0		
0.705	0.003								
PondD		STORAGE	0.00	120.96	0	00:30	0		
2.27	0.003								
PondE		STORAGE	0.00	46.88	0	00:35	0		
0.982	0.190								
PondF		STORAGE	0.00	129.20	0	00:35	0		
3.01	0.010								
PondG		STORAGE	0.00	20.07	0	00:35	0		
0.51	0.116								
PondH		STORAGE	0.00	47.25	0	00:32	0		
1.06	0.003								

		SWMM	5 Year	Output	9-21-20									
******	**********	*												
Node F] ******	.ooding Summar **************	y *												
No node	es were floode	d.												
****** Storage *****	**************************************													
		Average	Avg	Evap	Exfil	Maximum	Max	Time						
от мах	Maximum	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt							
Occurrenc Storage hr:min	e Outflow Unit CFS	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days						
PondB	2.62	321.956	38	0	0	389.908	46	0						
02:51 PondC	2.68	111.256	19	0	0	174.130	30	0						
02:23 PondA	1.52	59.417	29	0	0	88.970	44	0						
02:35 PondD	0.69	184.527	30	0	0	278,950	45	0						
02:07 PondE	8.58	16 171	16	0	Ø	72 /197	25	0						
01:03	24.04	220.240	20	0	0		40	0						
02:03	15.59	238.240	29	0	0	555,902	45	Ø						
PondG 01:15	9.05	2.647	0	0	0	31.289	6	0						
PondH 02:39	1.11	86.593	14	0	0	132.766	21	0						

# \* Outfall Loading Summary \*

Flow	Avg	Max	Total
Freq	Flow	Flow	Volume

SWMM 5 Year Output 9-21-20							
Outfall Node	Pcnt	CFS	C	FS :	10^6 gal		
Outfall2	99.97	61.16	61.	68	49.385		
Outfall1	99.97	67.44	67.	69	54.456		
Outfall4	99.89	245.24	276.	10	197.866		
Outfall3	99.69	1.80	8.	58	1.447		
System	99.88	375.63	407.	24	303.154		
*****							
Link Flow Summary ******************							
		 Maximum	Time	of Max	Maximum	Max/	Max/
link	Туро	Flow	Occu dave	rrence	Veloc	Full	Full Donth
K			uays				
100	DUMMY	30.72	0	00:35			
200	DUMMY	29.46	0	00:30			
201	DUMMY	12.02	0	00:35			
202	CONDUIT	40.84	0	00:31	18.27	0.02	0.11
203	CONDUIT	1.52	0	02:24	6.34	0.00	0.05
204	DUMMY	92.76	0	00:30			
205	CONDUIT	93.43	0	00:31	22.09	0.06	0.17
300	DUMMY	77.99	0	00:30			
400	DUMMY	24.15	0	00:30			
401	CONDUIT	23.53	0	00:32	11.46	0.06	0.16
402	DUMMY	98.47	0	00:30			
500	DUMMY	46.88	0	00:35			
601	DUMMY	60.11	0	00:35			
602	CONDUIT	60.09	0	00:35	10.17	0.25	0.34
603	DUMMY	16.28	0	00:35			
604	DUMMY	11.36	0	00:30			
605	CONDUIT	26.88	0	00:35	14.61	0.02	0.09
606	DUMMY	42.32	0	00:30			
607	CONDUIT	69.12	0	00:31	16.65	0.04	0.14
700	DUMMY	13.78	0	00:30			
701	DUMMY	6.55	0	00:35			
702	DUMMY	6.55	0	00:35			
703	CONDUIT	6.54	0	00:36	5.62	0.03	0.11
801	DUMMY	5.68	0	00:35			
802	DUMMY	16.24	0	00:30			
803	CONDUIT	21.49	0	00:32	8.87	0.03	0.11
804	DUMMY	5.21	0	00:30			
806	DUMMY	20.93	0	00:30			
805	CONDUIT	5.08	0	00:32	5.42	0.02	0.09

	SWMM	5 Year	Output	9-21-20			
808	CONDUIT	201.42	0	01:59	4.47	0.03	0.20
800	CONDUIT	189.04	0	01:19	6.57	0.02	0.14
600	CONDUIT	84.88	0	01:06	9.93	0.00	0.06
EastForkTrib	CONDUIT	61.00	0	00:32	3.08	0.01	0.07
EastFork	CONDUIT	180.00	0	00:24	4.29	0.03	0.15
MainStem	CONDUIT	67.00	0	01:15	2.39	0.00	0.05
MainStemTrib	CONDUIT	59.00	0	03:06	2.28	0.00	0.04
101	DUMMY	0.69	0	02:35			
206	DUMMY	2.68	0	02:52			
301	DUMMY	1.52	0	02:23			
501	DUMMY	24.04	0	01:03			
704	DUMMY	9.05	0	01:15			
807	DUMMY	1.11	0	02:39			
608	DUMMY	15.59	0	02:04			
403	DUMMY	8.58	0	02:07			

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:22:13 2020 Analysis ended on: Mon Sep 21 16:22:14 2020 Total elapsed time: 00:00:01

#### SWMM 100 Year Output

SWMM 100 Year Post Development

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/02/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal \*\*\*\*\*\*\*\* ----------Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 123.320 40.186 External Outflow ..... 105.086 34.244 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 18.084 5.893 Continuity Error (%) ..... 0.122

All links are stable.

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Routing	Time Step Summary ******			
Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.02	
Percent	Not Converging	:	0.00	

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Node Depth Summary \*\*\*\*\*\*\*\*\*

		Average Depth	Maximum Depth	Maximum HGL	Time Occu	of Max rrence	Reported Max Depth
Node	Туре	Feet	Feet	Feet	days	hr:min	Feet
10	JUNCTION	0.00	0.00	6975.00	0	00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.06	1.35	6946.35	0	00:35	1.34
24	JUNCTION	0.27	2.22	6936.22	0	00:51	2.22
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
31	JUNCTION	0.24	1.68	6954.68	0	00:59	1.68
67	JUNCTION	0.24	2.30	6867.80	0	01:13	2.30
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.05	1.40	6912.40	0	00:35	1.38
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
51	JUNCTION	0.04	0.74	6920.74	0	00:49	0.74
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.06	1.19	6901.19	0	00:40	1.19
65	JUNCTION	0.09	1.92	6881.92	0	00:40	1.92

		SWMM 100	Year Outp	but			
66	JUNCTION	0.13	3.12	6871.12	0	00:40	3.12
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.06	1.02	6903.02	0	00:45	1.02
74	JUNCTION	0.05	0.60	6897.60	0	01:12	0.60
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.07	1.45	6873.45	0	00:40	1.45
85	JUNCTION	0.03	0.82	6874.82	0	00:35	0.81
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.24	2.30	6867.30	0	01:13	2.30
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.72	9.85	6920.85	0	01:16	9.85
PondC	STORAGE	5.17	7.08	6963.08	0	00:59	7.08
PondA	STORAGE	5.81	8.60	6957.60	0	01:13	8.59
PondD	STORAGE	5.66	8.08	6889.08	0	01:04	8.08
PondE	STORAGE	4.04	5.84	6928.84	0	00:49	5.84
PondF	STORAGE	5.86	8.17	6874.17	0	01:09	8.17
PondG	STORAGE	0.20	2.69	6902.69	0	01:12	2.68
PondH	STORAGE	4.95	6.51	6872.51	0	01:12	6.51

Node Inflow Summary \*\*\*\*\*\*\*\*\*

	-1		Maximum	Maximum		Lateral	
lotal	FIOW		Lateral	Total	Time of Max	Inflow	
Inflow	Balance		Lucci ui	TOCUL		1111104	
			Inflow	Inflow	Occurrence	Volume	
Volume	Error						
Node		Type	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent				2	0	
10		JUNCTION	100.64	100.64	0 00:40	2.37	
2.37	0.000						
20		JUNCTION	97.08	97.08	0 00:35	1.81	
1.81	0.000						

		ear Output					
21		JUNCTION	42.26	42.26	0	00:40	1.2
1.2	0.000						
22		JUNCTION	295.27	295.27	0	00:40	6.04
6.04	0.000						
23		JUNCTION	0.00	136.17	0	00:35	0
3.01	0.000				_		_
24	0.000	JUNCTION	0.00	334.84	0	00:51	0
9.43	-0.000		220.02	220.02	0	00.25	,
30	0 000	JUNCITON	238.03	238.03	0	00:35	4
4 21	0.000		0 00	115 75	Q	00.50	0
2 20	a aaa	JUNCTION	0.00	113.75	0	00.55	0
67	0.000		0.00	270.41	9	01·13	Ø
9.72	-0.000	50110111011	0.00	2,0.11	Ũ	01.15	Ũ
40		JUNCTION	70.07	70.07	0	00:35	1.32
1.32	0.000						
41		JUNCTION	252.18	252.18	0	00:35	4.73
4.73	0.000						
42		JUNCTION	0.00	70.07	0	00:35	0
1.32	0.000						
50		JUNCTION	178.04	178.04	0	00:40	4.2
4.2	0.000						
51		JUNCTION	0.00	164.75	0	00:49	0
3.95	0.000		50.05	50.05	~		4 65
60 1 CF	0.000	JUNCITON	58.95	58.95	0	00:40	1.65
1.65	0.000		170 00	170 00	0	00.10	2 07
2 97	0 000	JUNCITON	170.90	170.90	Ø	00.40	5.07
62	0.000		32 93	32 93	a	00·35	0 699
0.699	0.000	Soliciton	52.55	52.75	Ũ	00.55	0.000
63		JUNCTION	124.89	124.89	0	00:40	2.87
2.87	0.000				-		
64		JUNCTION	0.00	90.88	0	00:40	0
2.35	0.000						
65		JUNCTION	0.00	215.63	0	00:40	0
5.22	0.000						
66		JUNCTION	0.00	170.90	0	00:40	0
3.87	0.000						
70		JUNCTION	43.95	43.95	0	00:40	1.05
1.05	0.000		22.05	22.05	0	00.45	0 740
/1	0.000	JUNCITON	23.95	23.95	0	00:45	0.742
0./42 70	0.000		0 00	22 05	0	00.45	0
12 0 710	0 000	JUNCITON	0.00	23.93	Ø	45	0
72	0.000		0 00	23 95	a	00.15	Q
0.742	0 000	JUNCITON	0.00	رد ، رے	U	00.45	U
74	0.000	JUNCTION	0.00	42.13	0	01:12	Ø
1.79	-0.000				-		Ū

			SWMM 100 Y	ear Output	:		
80		JUNCTION	27.62	27.62	0	00:45	0.833
0.833	0.000						
81		JUNCTION	47.62	47.62	0	00:35	1.01
1.01	0.000						
82		JUNCTION	15.60	15.60	0	00:35	0.314
0.314	0.000						
83		JUNCTION	64.71	64.71	0	00:35	1.46
1.46	0.000				~		2
84		JUNCIION	0.00	/3./3	0	00:40	0
1.84	0.000		0.00	15 60	0	00.25	0
85	0 000	JUNCITON	0.00	15.60	0	00:35	0
0.314	0.000		0.00	256 11	0	01.10	0
		UUIFALL	0.00	250.11	0	01:10	0
10.5 Outfall1	0.000	ΟΠΤΕΛΙΙ	0 00	53 05	Q	01.13	Q
2 03	A AAA	OUTTALL	0.00		0	01.15	0
$0_{1}+f_{2}$	0.000	ΟΠΤΕΛΙΙ	0 00	178 86	Q	01.05	0
16 7	a aaa	OUTTALL	0.00	470.00	0	01.05	0
Outfall3	0.000	Ουτεαιι	0.00	160.70	0	01:04	0
5.21	0.000	00117122	0.00	2001/0	Ũ	02101	0
PondB		STORAGE	0.00	447.00	0	00:49	0
12.4	0.062				-		-
PondC		STORAGE	0.00	238.03	0	00:35	0
4 e	.130						
PondA		STORAGE	0.00	100.64	0	00:40	0
2.37	0.096						
PondD		STORAGE	0.00	320.21	0	00:35	0
6.05	0.105						
PondE		STORAGE	0.00	178.04	0	00:40	0
4.2	0.178						
PondF		STORAGE	0.00	385.87	0	00:41	0
9.08	0.109						
PondG		STORAGE	0.00	67.73	0	00:40	0
1.8	0.079				_		
PondH		STORAGE	0.00	153.03	0	00:38	0
3.61	0.143						

No nodes were flooded.

\*\*\*\*\*\*

## SWMM 100 Year Output

		Average	Avg	Evap	Exfil	Maximum	Max	Time
of Max	Maximum	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
Occurrence Storage hr:min	ce Outflow e Unit CFS	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
PondB	256 11	363.135	43	0	0	827.701	97	0
PondC	200.11	146.763	26	0	0	299.338	52	0
PondA	52 05	75.030	37	0	0	152.554	76	0
PondD	160 70	192.591	31	0	0	418.291	67	0
PondE	164 75	48.028	17	0	0	106.230	37	0
PondF	220.20	250.108	31	0	0	549.589	67	0
PondG	12 12	5.811	1	0	0	88.594	16	0
PondH 01:12	80.17	131.315	21	0	0	268.983	42	0

### \*\*\*\*\*

Outfall Node	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
	Pcnt	CFS	CFS	10^6 gal
Outfall2	99.64	12.77	256.11	10.280
Outfall1	99.69	2.53	53.95	2.035
Outfall4	99.67	20.76	478.86	16.717
Outfall3	99.69	6.47	160.70	5.209
System	99.67	42.53	924.48	34.241

SWMM 100 Year Output

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Link Flow Summary \*\*\*\*\*\*\*\*\*

		Maximum	Time	of Max	Maximum	Max/	Max/
	_	Flow	0ccu	rrence	Veloc	Full	Full
Link	Туре	CFS	days	hr:min	t/sec	Flow	Depth
100	DUMMY	100.64	0	00:40			
200	DUMMY	97.08	0	00:35			
201	DUMMY	42.26	0	00:40			
202	CONDUIT	136.36	0	00:36	26.17	0.08	0.19
203	CONDUIT	115.74	0	00:59	23.03	0.37	0.42
204	DUMMY	295.27	0	00:40			
205	CONDUIT	334.86	0	00:51	31.89	0.22	0.32
300	DUMMY	238.03	0	00:35			
400	DUMMY	70.07	0	00:35			
401	CONDUIT	69.37	0	00:36	15.63	0.17	0.28
402	DUMMY	252.18	0	00:35			
500	DUMMY	178.04	0	00:40			
601	DUMMY	170.90	0	00:40			
602	CONDUIT	170.58	0	00:41	13.26	0.71	0.62
603	DUMMY	58.95	0	00:40			
604	DUMMY	32.93	0	00:35			
605	CONDUIT	90.74	0	00:41	20.83	0.06	0.17
606	DUMMY	124.89	0	00:40			
607	CONDUIT	215.42	0	00:40	23.26	0.13	0.24
700	DUMMY	43.95	0	00:40			
701	DUMMY	23.95	0	00:45			
702	DUMMY	23.95	0	00:45			
703	CONDUIT	23.94	0	00:45	8.29	0.09	0.20
801	DUMMY	27.62	0	00:45			
802	DUMMY	47.62	0	00:35			
803	CONDUIT	73.66	0	00:40	12.80	0.09	0.21
804	DUMMY	15.60	0	00:35			
806	DUMMY	64.71	0	00:35			
805	CONDUIT	15.43	0	00:37	7.47	0.06	0.16
808	CONDUIT	270.40	0	01:13	4.87	0.04	0.23
800	CONDUIT	41.98	0	01:17	4.06	0.00	0.06
600	CONDUIT	164.38	0	00:51	12.48	0.01	0.09
101	DUMMY	53.95	0	01:13			
206	DUMMY	256.11	0	01:16			
301	DUMMY	115.75	0	00:59			
501	DUMMY	164.75	0	00:49			
704	DUMMY	42.13	0	01:12			
807	DUMMY	80.17	0	01:12			
608	DUMMY	229.20	0	01:09			
		Da	~~ 7				

		SWMM 100	Year O	)utput
403	DUMMY	160.70	0	01:04

No conduits were surcharged.

Analysis begun on: Mon Apr 13 19:00:38 2020 Analysis ended on: Mon Apr 13 19:00:38 2020 Total elapsed time: < 1 sec

### SWMM 100 Year Output 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/02/2005 06:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\*\* Volume Volume Flow Routing Continuity acre-feet 10^6 gal \_ Dry Weather Inflow ..... 0.000 0.000 Wet Weather Inflow ..... 0.000 0.000 Groundwater Inflow ..... 0.000 0.000 RDII Inflow ..... 0.000 0.000 External Inflow ..... 3854.070 1255.906 External Outflow ..... 3828.229 1247.485 Flooding Loss ..... 0.000 0.000 Evaporation Loss ..... 0.000 0.000 Exfiltration Loss ..... 0.000 0.000 Initial Stored Volume .... 0.000 0.000 Final Stored Volume ..... 9.185 28.186 Continuity Error (%) ..... -0.061

SWMM 100 Year Output 9-21-20 \*\*\*\*\*\* All links are stable.

\*\*\*\*\*\*

Routing Time Step Summary \*\*\*\*\*\*

Minimum	Time Step	:	30.00	sec
Average	Time Step	:	30.00	sec
Maximum	Time Step	:	30.00	sec
Percent	in Steady State	:	0.00	
Average	Iterations per Step	:	1.02	
Percent	Not Converging	:	0.00	

### \*\*\*\*\*

Node Depth Summary \*\*\*\*\*\*

Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time Occu days	of Max rrence hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00		00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0	00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0	00:00	0.00
23	JUNCTION	0.06	1.35	6946.35	0	00:35	1.34
24	JUNCTION	0.27	2.22	6936.22	0	00:51	2.22
30	JUNCTION	0.00	0.00	6985.00	0	00:00	0.00
31	JUNCTION	0.24	1.68	6954.68	0	00:59	1.68
67	JUNCTION	3.45	4.11	6869.61	0	01:12	4.11
40	JUNCTION	0.00	0.00	6918.00	0	00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0	00:00	0.00
42	JUNCTION	0.05	1.40	6912.40	0	00:35	1.38
50	JUNCTION	0.00	0.00	6945.00	0	00:00	0.00
51	JUNCTION	1.48	1.48	6921.48	0	00:21	1.48
60	JUNCTION	0.00	0.00	6942.00	0	00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0	00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0	00:00	0.00
64	JUNCTION	0.06	1.19	6901.19	0	00:40	1.19
65	JUNCTION	0.09	1.92	6881.92	0	00:40	1.92
66	JUNCTION	0.13	3.12	6871.12	0	00:40	3.12
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00

	SWMM	100 Year (	Dutput 9	-21-20			
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.06	1.02	6903.02	0	00:45	1.02
74	JUNCTION	2.57	2.66	6899.66	0	01:12	2.66
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.07	1.45	6873.45	0	00:40	1.45
85	JUNCTION	0.03	0.82	6874.82	0	00:35	0.81
0S1	JUNCTION	1.33	1.33	6953.93	0	00:00	1.33
0S3	JUNCTION	1.48	1.48	6924.28	0	00:00	1.48
0S4	JUNCTION	2.38	2.38	6902.18	0	00:00	2.38
0S2	JUNCTION	1.06	1.06	6925.06	0	00:00	1.06
Outfall2	OUTFALL	1.06	1.06	6911.06	0	01:47	1.06
Outfall1	OUTFALL	1.33	1.33	6948.33	0	00:39	1.33
Outfall4	OUTFALL	3.45	4.11	6869.11	0	01:12	4.11
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.72	9.85	6920.85	0	01:16	9.85
PondC	STORAGE	5.17	7.08	6963.08	0	00:59	7.08
PondA	STORAGE	5.81	8.60	6957.60	0	01:13	8.59
PondD	STORAGE	5.66	8.08	6889.08	0	01:04	8.08
PondE	STORAGE	4.04	5.84	6928.84	0	00:49	5.84
PondF	STORAGE	5.86	8.17	6874.17	0	01:09	8.17
PondG	STORAGE	0.20	2.69	6902.69	0	01:12	2.68
PondH	STORAGE	4.95	6.51	6872.51	0	01:12	6.51

Node Inflow Summary \*\*\*\*\*\*\*\*\*\*

 Totol	 51		Maximum	Maximum		Lateral	
IOTAL	FIOW		Lateral	Total	Time of Max	Inflow	
TULTOM	Barance		Inflow	Inflow	Occurrence	Volume	
Volume Node	Error	Туре	CFS	CFS	days hr:min	10^6 gal	10^6
gal	Percent						
10 2.37	0.000	JUNCTION	100.64	100.64	0 00:40	2.37	

		SWMM	100 Year	Output 9-	21-20		
20		JUNCTION	97.08	97.08	0	00:35	1.81
1.81	0.000						
21		JUNCTION	42.26	42.26	0	00:40	1.2
1.2	0.000						
22		JUNCTION	295.27	295.27	0	00:40	6.04
6.04	0.000				-		_
23	0.000	JUNCIION	0.00	136.17	0	00:35	0
3.01	0.000		0.00	224 84	0	00.51	0
24	0 000	JUNCTION	0.00	334.84	0	00:51	0
30	-0.000		228 02	228 03	Q	00.35	Л
1	a aaa	JUNCTION	230.05	230.05	0	00.55	4
31	0.000		0.00	115.75	Q	00·59	0
3.39	0.000	50110112011	0.00	113.75	Ũ	00.55	Ŭ
67		JUNCTION	0.00	865.98	0	01:12	0
489	0.000				-		-
40		JUNCTION	70.07	70.07	0	00:35	1.32
1.32	0.000						
41		JUNCTION	252.18	252.18	0	00:35	4.73
4.73	0.000						
42		JUNCTION	0.00	70.07	0	00:35	0
1.32	0.000						
50		JUNCTION	178.04	178.04	0	00:40	4.2
4.2	0.000						
51	0.000	JUNCIION	0.00	381.75	0	00:49	0
1/9	0.000				٥	00.10	1 65
00 1 65	0 000	JUNCTION	20.92	56.95	0	00:40	1.05
1.05 61	0.000		170 90	170 90	a	00.10	3 87
3.87	0,000	JUNCTION	1/0.00	1/0.90	0	00.40	5.07
62	0.000	JUNCTION	32,93	32,93	0	00:35	0.699
0.699	0.000		0_000	0_000	Ū.		
63		JUNCTION	124.89	124.89	0	00:40	2.87
2.87	0.000						
64		JUNCTION	0.00	90.88	0	00:40	0
2.35	0.000						
65		JUNCTION	0.00	215.63	0	00:40	0
5.22	0.000						
66		JUNCTION	0.00	170.90	0	00:40	0
3.87	0.000				-		
70	0.000	JUNCTION	43.95	43.95	0	00:40	1.05
1.05	0.000		22.05	22.05	0	00.45	0 742
/1	0 000	JUNCTION	23.95	23.95	0	00:45	0.742
U./4Z	0.000		0 00	22 OF	0	00.15	Q
12 0 710	0 000	JUNCITON	0.00	23.93	Ø	00.45	0
73	0.000		0.00	23.95	a	00·15	a
0.742	0.000	0011011011	0.00	,	Ŭ	00.15	Ŭ
_							

		SWMM	100 Year	Output 9-	21-20		
74		JUNCTION	0.00	637.13	0	01:12	0
482	0.000						
80		JUNCTION	27.62	27.62	0	00:45	0.833
0.833	0.000						
81		JUNCTION	47.62	47.62	0	00:35	1.01
1.01	0.000						
82		JUNCTION	15.60	15.60	0	00:35	0.314
0.314	0.000						
83		JUNCTION	64.71	64.71	0	00:35	1.46
1.46	0.000						
84		JUNCTION	0.00	73.73	0	00:40	0
1.84	0.000						
85		JUNCTION	0.00	15.60	0	00:35	0
0.314	0.000						
0S1		JUNCTION	413.00	413.00	0	00:00	334
334	0.000						
0S3		JUNCTION	217.00	217.00	0	00:00	175
175	-0.000						
0S4		JUNCTION	595.00	595.00	0	00:00	481
481	0.000						
0S2		JUNCTION	280.00	280.00	0	00:00	226
226	0.000						
Outfal	12	OUTFALL	0.00	536.11	0	01:16	0
236	0.000						
Outfal	11	OUTFALL	0.00	466.95	0	01:13	0
335	0.000						
Outfal	14	OUTFALL	0.00	1291.25	0	01:05	0
671	0.000						
Outfal	13	OUTFALL	0.00	160.70	0	01:04	0
5.21	0.000						
PondB		STORAGE	0.00	447.00	0	00:49	0
12.4	0.062						
PondC		STORAGE	0.00	238.03	0	00:35	0
4	0.130						
PondA		STORAGE	0.00	100.64	0	00:40	0
2.37	0.096						
PondD		STORAGE	0.00	320.21	0	00:35	0
6.05	0.105						
PondE		STORAGE	0.00	178.04	0	00:40	0
4.2	0.178						
PondF		STORAGE	0.00	385.87	0	00:41	0
9.08	0.109						
PondG		STORAGE	0.00	67.73	0	00:40	0
1.8	0.079						
PondH		STORAGE	0.00	153.03	0	00:38	0
3.61	0.143						

****** Node F ******	************* looding Summa ************* es were flood	SWMM 1 ** ry ** ed.	00 Year	Outpu	ıt 9-21-20	9		
****** Storag *****	************* e Volume Summ ***********	*** ary ***						
of Max	 Maximum	Average	Avg	Evap	Exfil	Maximum	Max	Time
		Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
Occurren Storag hr:min	ce Outflow e Unit CFS	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
PondB 01:15	256.11	363.135	43	0	0	827.701	97	0
PondC 00:58	115.75	146.763	26	0	0	299.338	52	0
PondA 01:12	53.95	75.030	37	0	0	152.554	76	0
PondD	160 70	192.591	31	0	0	418.291	67	0
PondE	100.70	48.028	17	0	0	106.230	37	0
00:48 PondF	164.75	250.108	31	0	0	549.589	67	0
01:09 PondG	229.20	5 811	1	Q	ß	88 594	16	0
01:11	42.13	121 215		0	0		10	0
01:12	80.17	101.010	21	0	U	200.903	42	U

Flow	Avg	Max	Total				
Freq	Flow	Flow	Volume				
	SWM	M 100 Year	Outpu	t 9-21-	20		
------------------------------	---------	------------	--------	---------	---------	------	-------
Outfall Node	Pcnt	CFS	C	FS 1	0^6 gal		
Outfall2	99.97	292.00	536.	 11	235.796		
Outfall1	99.97	415.18	466.9	95	335.258		
Outfall4	99.92	831.58	1291.	25	671.130		
Outfall3	99.69	6.47	160.	70	5.209		
System	99.89	1545.23	2428.	13 1	247.393		
*****							
Link Flow Summary **********							
		Maximum	lime (	ot Max	Maximum	Max/	Max/
Link	Tuno		dovic	hnumin	veroc	FUII	FUII
L111K	туре	CF3	uays		TL/Sec	F10W	Depth
100	DUMMY	100.64	0	00:40			
200	DUMMY	97.08	0	00:35			
201	DUMMY	42.26	0	00:40			
202	CONDUIT	136.36	0	00:36	26.17	0.08	0.19
203	CONDUIT	115.74	0	00:59	23.03	0.37	0.42
204	DUMMY	295.27	0	00:40			
205	CONDUIT	334.86	0	00:51	31.89	0.22	0.32
300	DUMMY	238.03	0	00:35			
400	DUMMY	70.07	0	00:35			
401	CONDUIT	69.37	0	00:36	15.63	0.17	0.28
402	DUMMY	252.18	0	00:35			
500	DUMMY	178.04	0	00:40			
601	DUMMY	170.90	0	00:40			
602	CONDUIT	170.58	0	00:41	13.26	0.71	0.62
603	DUMMY	58.95	0	00:40			
604	DUMMY	32,93	0	00:35			
605	CONDUIT	90.74	0	00:41	20.83	0.06	0.17
606	DUMMY	124.89	0	00:40			
607	CONDUIT	215.42	0	00:40	23.26	0.13	0.24
700	DUMMY	43.95	0	00:40			
701	DUMMY	23.95	0	00:45			
702	DUMMY	23.95	0	00:45			
703	CONDUIT	23.94	0	00:45	8.29	0.09	0.20
801	DUMMY	27.62	0	00:45			
802	DUMMY	47.62	0	00:35			
803	CONDUIT	73.66	0	00:40	12.80	0.09	0.21
804	DUMMY	15.60	0	00:35	_		
806	DUMMY	64.71	0	00:35			
805	CONDUIT	15.43	0	00:37	7.47	0.06	0.16

	SWMM	100 Year	Outpu	t 9-21-20			
808	CONDUIT	865.97	0	01:12	6.70	0.14	0.41
800	CONDUIT	637.10	0	01:15	9.35	0.06	0.27
600	CONDUIT	381.54	0	00:50	16.34	0.02	0.15
EastForkTrib	CONDUIT	217.00	0	00:21	4.75	0.02	0.15
EastFork	CONDUIT	595.00	0	00:16	6.34	0.10	0.30
MainStem	CONDUIT	413.00	0	00:40	4.75	0.03	0.13
MainStemTrib	CONDUIT	280.00	0	01:49	4.12	0.02	0.11
101	DUMMY	53.95	0	01:13			
206	DUMMY	256.11	0	01:16			
301	DUMMY	115.75	0	00:59			
501	DUMMY	164.75	0	00:49			
704	DUMMY	42.13	0	01:12			
807	DUMMY	80.17	0	01:12			
608	DUMMY	229.20	0	01:09			
403	DUMMY	160.70	0	01:04			

\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:06:21 2020 Analysis ended on: Mon Sep 21 16:06:21 2020 Total elapsed time: < 1 sec



Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix D

		Prelimina	ry Desigr	n Procedur	e Form: Fu	II Spectrum	Detention (F	SD) Routin	ıg
			COS PO	CM-FSD Preli	minary Desig	n (Beta Versio	n 1.00, Septemi	oer 2019)	Sheet 1 of 3
	STOR		FR		Designer: Project:	Chris McFarlan	erve Pond A		
COLOPADO	SIUN				Date:	April 6, 2020	erve Fond A		Last Edited: April 13, 2020
		ENTERP	RISE			1 .7			1
I. Select WQCV/EURV PCM Type:					Ð	tended Detention E	Basin (EDB)	•	
corresponding PCM worksheet. The sele	e information fi cted PCM work	rom the (sheet							
must be completed before the import will	work.								
2. WQCV/EURV Outlet Details						Input Pa	cos DCM	-	
A) Average Infiltration Rate of WQCV					i =	N/A	N/A	in / hr	
<ul> <li>B) Depth to Centroid of Underdrain Outlet C</li> <li>C) Underdrain Outlet Orifice Area</li> </ul>	rifice from filte	r media surface		Un	y = derdrain Ao =	N/A N/A	N/A N/A	inches sa in	
D) Number of WQCV Orifice Rows	_			# V	VQCV rows =	10	10		
F) WQCV Orifice Area (A <sub>o</sub> ) per Row	Rows			011	WQCV Ao =	0.61	0.61	sq in	
<ul> <li>G) Maximum Stage of WQCV (includes ISD</li> <li>H) EURV Orifice Area (A.) in Single Row</li> </ul>	and Trickle Cl	hannel Depth)		Max	FURV Ao =	3.40 2.96	2.96	ft sa in	
I) Maximum Stage of EURV (includes ISD a	nd Trickle Cha	innel Depth)		Max	Stage <sub>EURV</sub> =	4.50	4.50	ft	
<ol> <li>J) Discharge Coefficient for all WQCV/EUR</li> </ol>	V Outlet Orifice	e(s)			Cd =	0.60	0.60	1	
. Flood Control Surcharge Basin Geometry (a	bove EURV) -	See Figure				Innut Pa	rameters		User can override default flood surcharge
the PCM Geometry in an upward direction v	without a transi	ition bench.				User	COS	-	between the top of the PCM and the Flood
A) Length of Basin at Top of FURV					L <sub>PCM</sub> =	370.3	370.3	ft	Surcharge Volume by entering larger dimensions in C), D). and E).
B) Width of Basin at Top of EURV	o of Flord O	trol Curchann \		Store -+ -	W PCM =	113.6	113.6	ft #	See the Figure to the right.
D) Length of Basin at Top of Transition Bench (Botton	ch (Bottom of F	าแ or Surcharge) Flood Control St	urcharge)	Stage at To	L Bench =	4.60 <u>371.</u> 1	4.60 371.1	ft	Bench Slope is 4H:1V in length direction
E) Width of Basin at Top of Transition Bench E) Average Side Slopes of Flood Control St	h (Bottom of Fl	ood Control Sur	rcharge)		W Bench = Z Surcharge =	114.4	114.4 4.00	ft ft / ft	Bench Slope is 4H:1V in width direction
(Recommend no steeper than 3H:1V slo	pe. Use zero f	for vertical walls.	5.)		Surcharge -	4.00	₩.UU	<b>」</b>	
Tributary Watershed Hydrology				1					
<ul> <li>A) Input hydrology data (copy/paste) from m</li> </ul>	odel runs	2 Year	5 Year	Pre-Dev 10 Year	25 Year	ak Flow (cfs) 50 Year	100 Year	500 Year	
B) Adjust "Time Interval" to match	Time Interva	┍━━━┖	13.03				57.08		J
hydrograph data	5.0	minutes	Dec	6 Development	mt Otama laft		- ()		
5-yr and 100-yr Hydrology Required	(min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year	
(Other Storms are Optional)	0:00		0.00				0.00		
	0:05		2.12				2.93		
	0:15		6.24 19.45				8.14		4
	0:25		29.43				70.19		1
	0:30		30.68 28.10				95.65 100.37		1
	0:40		24.84				96.25		
	0:45		19.61				81.43		1
	0:55		17.40				74.41		4
	1:05		13.43				58.60		1
	1:10 1:15		10.74				49.54 42.06		1
	1:20		9.68				35.93		4
	1:30		7.74				26.07		1
	1:35		6.69 5.63				21.81 17.82		1
	1:45		4.64				14.14		1
	1:50		3.79				10.94 8.55		1
	2:00		2.68				6.51		
	2:10		1.73				3.64		1
	2:15		1.39				2.70		1
	2:25		0.88				1.45		1
	2:30 2:35		0.68				1.07 0.82		1
	2:40		0.41				0.64		
	2:45		0.32				0.30		1
	2:55		0.17				0.29		4
	3:05		0.08				0.13		1
	3:10		0.05				0.07		1
	3:20		0.01				0.01		
	3:20		0.00				0.00		1
	3:35								4
	3:45								1
	3:50								1
	4:00								4
	4:10								1
	4:15								1
	4:25								1
	4:30 4:35								1
	4:40								
	4:45								1
	4:55								
	5:05								1
	5:10								4
	5:20								1
	5:25								4
								1	4

5:45	5:40				
5:50 5:55 6:00	5:45				
5:55 6:00 6:00 6:00 6:00 6:00 6:00 6:00	5:50				
6:00	5:55				
0.00	6:00				

		Prelimin	ary Desigr	Procedure	e Form: Fu	II Spectrum	Detention (F	SD) Routin	g				
			COS PC	M-FSD Prelin	minary Desig	n (Beta Versior	1.00, Septemb	oer 2019)	Sheet 2 of 3				
					Designer:	Chris McFarlan	d						
	WA	TER RES	OURCES		Project:	Grandview Res	erve Pond A						
COLORADO		ENC	AINEERING		Date:	April 6, 2020			Last Edited: April 13, 2020				
SPRINGS			_										
OLYMPIC CITY USA													
5. Flood Control Outlet Structure Type				Overflow	v Weir/Grate Out	et Pine Restriction i	Emergency Spillway	av 🔻					
A) Select Flood Control Outlet Structure	е Туре							-,					
<ol> <li>Overflow Weir (Dropbox) and Grate (Fla (Assumes that top of grate is flush wit</li> </ol>	t or Sloped) h the top of the cor	crete dropbo	()			Input Pa User	cos						
A) Overflow Weir Front Edge Height (re	lative to Stage = 0	ft)			H <sub>weir front</sub> =	4.50	4.50	ft					
<ul> <li>B) Overflow Weir Front Edge Length (in</li> </ul>	side edge of droph	ox)			L <sub>weir front</sub> =	8.00	9.00	ft					
<ul> <li>C) Overflow Weir Grate Slope (H:V, ent</li> <li>D) Horizontal Length of Weir Sides (insi</li> </ul>	er zero for flat grat	e) v)		Horizor	ntal L <sub>weir sides</sub> =	0.00	5.00	π/π ft					
<ul> <li>E) Overflow Grate Open Area % (grate)</li> </ul>	open area / total g	rate area)		Grate	Open Area =	70%	70%	%					
F) Debris Clogging %				Debr	ris Clogging =	50%	50%	%					
<ul> <li>G) Height of Grate Upper Edge (at back H) Overflow Grate Slope Length (inside</li> </ul>	edge of dropbox)			Slo	ppe Lweir sides =	4.50	4.50	ft					
I) Overflow Grate Open Area (without d	lebris)			Open Are	a (No Clogging) =	44.80	31.50	sq ft		Ð			
J) Overflow Grate Open Area (with deb	ris)			Open A	Area ( <sub>Clogged</sub> ) =	22.40	15.75	sq ft		outin			
7. Outlet Pipe with Flow Restriction Plate										iD) Rc			
A) Select Type of Outlet Restriction					Circula	r Outlet Pipe w/ Res	trictor Plate	1	•	(FS			
(Circular Pipe w/ Restrictor Plate, Circ	ular Orifice or Rec	tangular Orific	e)			Input Do	romotoro			Ð			
						User	COS	•		ġ			
						Input	DCM	_		ete			
<ul> <li>B) Depth to Invert of Outlet Pipe (relative and the second second</li></ul>	ve to Stage = 0 ft)			Pipe I	nvert Depth =	1.50	1.50	ft		Ő			
C) Outlet Pipe Diameter	wort			Pip	e Diameter =	36.00	30.00	inches		5			
E) Half-Central Angle of Restrictor Plate	e on Pipe				Theta =	1.82	2.63	radians		ctī			
F) Outlet Orifice Area					Outlet Ao =	4.63	4.78	sq ft		ě			
G) Height of Outlet Orifice Centroid abo	ve Outlet Pipe Inve	ert (		0	Outlet <sub>centroid</sub> = <u>1.06</u> <u>1.22</u> ft Open Area Ratio = <u>9.68</u> <u>6.59</u>								
<ul> <li>H) Ratio of Grate Open Area / 100-yr O</li> </ul>	rifice Area (should	be≥4)		Open Area Natio - 9.06 0.09									
8. Emergency Spillway (Rectangular or Tra	apezoidal)					Input Pa User	rameters COS			Form:			
A) Spillway Invert Stage (relative to Sta	ae = 0 ft)				Hanilluser invest =	Input 5 90	DCM 6.00	ft		2			
B) Spillway Crest Length	3)				L <sub>spillway crest</sub> =	42.00	33.00	ft		npe			
C) Spillway End Slopes (H:V)					S <sub>spillway ends</sub> =	4.00	4.00	ft / ft		ö			
D) Freeboard above Maximum Water S E) Spillway Design Flow Depth	urface			Freel	Depthenilluou =	1.00	1.00	ft ft		Ě			
F) Stage at Top of Freeboard				Freeboard	Top Stage =	7.70	8.00	ft		ы			
G) Basin Area at Top of Freeboard				Max	Basin Area =	1.27	1.29	acres		Jesi			
9. Routed Hydrograph Results										ary [			
Design Storm Return Period = WQ	CV EURV	2 Year	5 Year	10 Year	User Input 25 Year	50 Year	100 Year	500 Year		ii.			
Inflow Hydrograph Volume (ac-ft) = 0.6	4 1.66		2.16				7.27			re			
Predevelopment Peak Q (Cts) = N// Peak Inflow (cfs) = N//	A N/A	<u> </u>	30.7				57.1			Δ.			
Peak Outflow (cfs) = 0.3	3 0.5	1	4.6				56.3						
Ratio (Outflow/Predevelopment) = N//	A N/A		0.4				1.0						
Structure Controlling Flow = Orifice Max Velocity through Grate =	Plate Orifice Plate Δ NI/Δ		Overflow Grate		<u> </u>		Outlet Pipe 1 2	<u> </u>					
Time to Drain 97% of Volume (hr) = 39	69	t	73	-			61						
Time to Drain 99% of Volume (hr) = 41	72		77				72						
Maximum Ponding Depth (ft) = 3.4	0 4.50		4.70				5.90						
Maximum Volume Stored (ac-ft) = 0.6	4 1.66		1.87				3.11						
			Results	based on CO	S DCM Inputs	6							
Design Storm Return Period = WQ0	2 EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year					
Predevelopment Peak Q (cfs) = N//	A N/A		13.0				57.1						
Peak Inflow (cfs) = N//	A N/A		30.7				100.4						
Peak Outflow (cfs) = 0.0	5 0.5	ļ	4.3				57.5						
Structure Controlling Flow = Orifice	Plate Orifice Plate		U.3 Overflow Grate				Outlet Pipe						
Max Velocity through Grate = N//	A N/A		0.2				1.8						
Time to Drain 97% of Volume (hr) = 39	69		73				61						
I ime to Drain 99% of Volume (hr) = 41	72	l	/7 4 70		-		<u>/2</u>	-					
Area at Max Ponding Depth (it) = 0.8	0 0.97		0.98				1.09						
Maximum Volume Štored (aċ-ft) = 0.6	4 1.66		1.87				3.11						



		Preliminary Desig	n Procedure Form: Fi	ull Spectrum Detention (F	SD) Routin	g	
		COS PO	CM-FSD Preliminary Desig	n (Beta Version 1.00, Septem)	oer 2019)	Sheet 1 of 3	
	STOR		Designer: Proiect:	Grandview Reserve Pond B			
COLORADO	01011	ENTERPRISE	Date:	April 6, 2020		Last Edited: April 13, 2020	
SPRINGS							
OLYMPIC CITY USA							
						1	
. Select WQCV/EURV PCM Type: Imports the Stage-Area-Volume-Discharg	ge information fr	om the	E	xtended Detention Basin (EDB)	•		
corresponding PCM worksheet. The sele	ected PCM work	sheet					
must be completed before the import will	WORK.						
. WQCV/EURV Outlet Details				Input Parameters	_		
A) Average Infiltration Rate of WOCV			i =	User Input COS DCM	in / hr		
B) Depth to Centroid of Underdrain Outlet (	Orifice from filter	r media surface	y =	N/A N/A	inches		
D) Number of WQCV Orifice Rows			# WQCV rows =	14 N/A N/A	sqin		
<ul> <li>E) Vertical Spacing between WQCV Orifice</li> <li>F) WQCV Orifice Area (A<sub>2</sub>) per Row</li> </ul>	e Rows		Orifice Spacing = WQCV Ao =	4.0 4.0 1.49 1.49	inches sa in		
G) Maximum Stage of WQCV (includes ISE	D and Trickle Ch	nannel Depth)	Max Stage WQCV =	4.70 4.70	ft .		
<ul> <li>I) Burky Onlice Area (A<sub>o</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	and Trickle Cha	nnel Depth)	Max Stage <sub>EURV</sub> =	6.00 6.00	sq in ft		
J) Discharge Coefficient for all WQCV/EUF	RV Outlet Orifice	(s)	Cd =	0.60 0.60	]		
Fland Control Surphone Basic Controls		Con Finance					
Flood Control Surcharge Basin Geometry ( Default Flood Surcharge Geometry inputs	above EURV) - 3 represent a con	See Figure itinuation of		Input Parameters		geometry inputs to create a transition bench	
the PCM Geometry in an upward direction	without a transit	tion bench.		User COS Input DCM		between the top of the PCM and the Flood Surcharge Volume by entering larger	
A) Length of Basin at Top of EURV			L PCM =	644.7 644.7	ft	dimensions in C), D), and E).	
<ul> <li>с) vviatn of Basin at Top of EURV</li> <li>C) Stage at Top of Transition Bench (Botto)</li> </ul>	m of Flood Cont	trol Surcharge)	Stage at Top of Bench =	191.2         191.2           6.10         6.10	ft	See the Figure to the right.	
D) Length of Basin at Top of Transition Ber E) Width of Basin at Top of Transition Berg	nch (Bottom of F	Flood Control Surcharge)	L Bench = W Bench =	645.5 645.5 192.0 192.0	ft ft	Bench Slope is 4H:1V in length direction Bench Slope is 4H:1V in width direction	
F) Average Side Slopes of Flood Control S	Surcharge above	Transition Bench	Z Surcharge =	4.00 4.00	ft / ft		
recommend no steeper than 3H:1V slo	ope. Use zero f	or vertical Walls.)					
Tributary Watershed Hydrology							
<ul> <li>A) Input hydrology data (copy/paste) from r</li> </ul>	model runs	2 Year 5 Year	Pre-Development Pe 10 Year 25 Year	eak Flow (cfs) 50 Year 100 Year	500 Year		1
	Time Internel	17.56		164.21			
<li>B) Adjust "Time Interval" to match hydrograph data</li>	5.0	minutes					
5-vr and 100-vr Hydrology Required	Time (min)	2 Year 5 Year	st-Development Storm Infl 10 Year 25 Year	ow Hydrographs (cfs) 50 Year 100 Year	500 Year		2
(Other Storms are Optional)	0:00	0.00		0.00			
	0:05	0.69		2.08			
	0:15	16.64		20.58			
	0:25	68.16		179.82			
	0:30	75.65		276.49 307.62			
	0:40	64.91 58.24		331.81			
	0:50	52.24		365.58			
	0:55	47.02		346.26			
	1:05	39.68 36.25		290.00 252.97			
	1:15	32.60		216.52			
	1:20	29.09		182.15			
	1:30	23.97		127.70			
	1:40	20.74		96.42			6
	1:45 1:50	19.35		85.46			
	1:55	16.77 14.81		68.63 60.20			9
	2:05	12.66		51.42			
	2:10	10.67		42.95 35.32			
	2:20	7.28		28.18			
	2:30	4.82		15.96			
	2:35	4.08		9.39			
	2:45	3.19		7.53			
	2:55	2.60		4.98			
	3:00	2.39		4.12			
	3:10	2.09		2.97			
	3:20	1.86		2.21			
	3:25	1.77		2.08			
	3:35 3:40	1.63		1.88			
	3:45	1.54		1.75	1		
	3:50	1.51		1.70			
	4:00	1.47		1.65			
	4:10	1.46		1.64			
	4:15 4:20	1.46		1.64 1.64			
	4:25	1.45		1.64			
	4:30	1.45		1.63			
	4:40 4:45	1.45		1.63			
	4:50	1.44		1.63			
	4:55 5:00	1.44		1.63			
	5:05	1.44		1.62			
	5:15	1.43		1.62			
	5:20	1.43		1.62			
	5:30	1.43		1.61			
	5:35	1.43		1.61		1	1

5:40	1.42		1.61	
5:45	1.42		1.61	
5:50	1.42		1.60	
5:55	1.42		1.60	
6:00				

			Prelimin	ary Design	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g	
				COS PC	M-FSD Prelin	minary Desig	n (Beta Versior	n 1.00, Septemb	oer 2019)	Sheet 2 of 3	
						Designer:	Chris McFarlan	d			
		WA	TER RES	OURCES		Project:	Grandview Res	erve Pond B			
COLORADO				BINEERING		Date:	April 6, 2020			Last Edited: April 13, 2020	
SPRINGS	<b>,</b>										
OLYMPIC CITY USA											
5. Flood Control Outlet Structure T	уре				Overflov	v Weir/Grate, Out	let Pipe Restriction i	& Emergency Spillwa	ay 🔻		
A) Select Flood Control Outlet S	Structure Type	e						5 5 1			_
<ol> <li>Overflow Weir (Dropbox) and Gr (Assumes that top of grate is f</li> </ol>	ate (Flat or S lush with the	iloped) top of the con	crete dropbo	<)			Input Pa User	rameters COS	-		
A) Overflow Weir Front Edge He	eight (relative	to Stage = 0	ft)			H <sub>weir front</sub> =	6.00	6.00	ft		
<ul> <li>B) Overflow Weir Front Edge Le</li> </ul>	ength (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	17.00	17.00	ft		
C) Overflow Weir Grate Slope (I D) Horizontal Length of Weir Sid	H:V, enter zei des (inside ed	ro for flat grat	e) v)		Horizor	s <sub>weir sides</sub> = tal L <sub>weir sides</sub> =	0.00	0.00	ft / ft		
E) Overflow Grate Open Area %	6 (grate open	area / total gr	ate area)		Grate	Open Area =	70%	70%	%		
F) Debris Clogging %	(at back side	of drophox)			Debr	ris Clogging = Harrata tan =	50%	50%	% ft		
H) Overflow Grate Slope Length	inside edge	of dropbox)			Slo	ppe L <sub>weir sides</sub> =	17.00	7.00	ft		
I) Overflow Grate Open Area (w	vithout debris	)			Open Are	a (No Clogging) =	202.30	83.30	sq ft		bu
<li>J) Overnow Grate Open Area (w</li>	viu'i debris)				Open P	Clogged) -	101.15	41.65	sqii		outi
7. Outlet Pipe with Flow Restriction	Plate									-	SD) R
A) Select Type of Outlet Restric	tion	Orifice of Reel	tongulor Orifig	)		Circula	r Outlet Pipe w/ Res	trictor Plate		•	Ш,
(Circular Pipe w/ Restrictor Pia	ate, Circular (	Jrince or Rec	langular Onlic	e)			Input Pa	rameters			tion
							User	COS	•		ent
B) Depth to Invert of Outlet Pipe	(relative to S	Stage = 0 ft)			Pipe I	nvert Depth =	1.50	1.50	ft		Det
C) Outlet Pipe Diameter	(101001010101	stage enty			Pip	e Diameter =	54.00	48.00	inches		Ξ
D) Restrictor Plate Height above E) Helf Control Angle of Bostria	e Pipe Invert	line			F	Plate Height =	37.00	42.00	inches		tr
<ul> <li>F) Outlet Orifice Area</li> </ul>	<ul> <li>Half-Central Angle of Restrictor Plate on Pipe</li> <li>Outlet Orifice Area</li> </ul>					Outlet Ao =	1.95	2.42	sq ft		bec
G) Height of Outlet Orifice Centr	roid above Ou	utlet Pipe Inve	rt			Outlet <sub>centroid</sub> =	1.73	1.87	ft		IS I
<ul> <li>H) Ratio of Grate Open Area / 1</li> </ul>	00-yr Orifice	Area (should	be≥4)		Open	i Area Ratio =	17.42	7.14	l		E.
8. Emergency Spillway (Rectangula	ar or Trapezo	oidal)					Input Pa	rameters			orm:
							Input	DCM	_		ч о
<ul> <li>A) Spillway Invert Stage (relativ</li> <li>B) Spillway Creat Lag ath</li> </ul>	e to Stage = (	0 ft)				H <sub>spillway invert</sub> =	9.50	9.30	ft		- ng
C) Spillway End Slopes (H:V)						S <sub>spillway ends</sub> =	4.00	4.00	ft / ft		ce
D) Freeboard above Maximum	Water Surfac	e			Freet	board Depth=	1.00	1.00	ft		Pro
<ul> <li>E) Spillway Design Flow Depth</li> <li>E) Stage at Top of Freeboard</li> </ul>					Freeboard	Top Stage =	0.90	1.00		- uß	
G) Basin Area at Top of Freeboard	ard				Max	Basin Area =	3.70	3.68	acres		Desig
9. Routed Hydrograph Results											lary C
Design Storm Return Period =	WQCV	EURV	2 Year	Resu 5 Year	ts based on 10 Year	User Input 25 Year	50 Year	100 Year	500 Year		imin
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73		6.67				31.72			le
Predevelopment Peak Q (cfs) = Peak Inflow (cfs) =	N/A N/A	N/A N/A		17.6				366.2			<u>а</u>
Peak Outflow (cfs) =	1.1	1.4		1.4				166.4			
Ratio (Outflow/Predevelopment) =	N/A Orifice Plate	N/A Orifice Plat-		0.1				1.0 Outlet Disc			
Max Velocity through Grate =	N/A	N/A		0.0				0.8			
Time to Drain 97% of Volume (hr) =	40	68		76				61			
I ime to Drain 99% of Volume (hr) = Maximum Ponding Depth (ft) =	42	6.00		80 6.10				/3 9.10			
Area at Max Ponding Depth (ac) =	1.92	2.83		2.85				3.32			
Maximum Volume Stored (ac-ft) =	2.41	5.73		6.04				15.28			
Design Storm Return Period =	WQCV	EURV	2 Year	Results 5 Year	based on CO 10 Year	S DCM Input 25 Year	s 50 Year	100 Year	500 Year		
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73		6.67				31.72			
Predevelopment Peak Q (cfs) = Peak Inflow (cfs) =	N/A N/A	N/A N/A		75.7				366.2			
Peak Outflow (cfs) =	1.1	1.4		1.4				166.5			
Ratio (Outflow/Predevelopment) =	N/A	N/A Orifio- Di-t		0.1				1.0			
Max Velocity through Grate =	N/A	N/A		0.0				2.0			
Time to Drain 97% of Volume (hr) =	40	68		76				61			
I ime to Drain 99% of Volume (hr) = Maximum Ponding Depth (#) =	42	72		80 6.10			L	73			
Area at Max Ponding Depth (ac) =	1.92	2.83		2.85				3.34			
Maximum Volume Stored (ac-ft) =	2.41	5.73		6.04				15.62			



		Prelimina	ry Desigr	n Procedur	e Form: Fu	II Spectrum	Detention (F	SD) Routir	ng
			COS PO	CM-FSD Preli	minary Desig	n (Beta Versio	1 1.00, Septemb	oer 2019)	Sheet 1 of 3
	STOR		FR		Project:	Grandview Res	erve Pond C		
COLORADO	01011	ENTERP	RISE		Date:	April 6, 2020			Last Edited: April 08, 2020
SPRINGS									
OLYMPIC CITY USA									
									1
<ol> <li>Select WQCV/EURV PCM Type: Imports the Stage-Area-Volume-Discharg</li> </ol>	ge information fr	rom the			E	tended Detention E	lasin (EDB)	•	
corresponding PCM worksheet. The sele	ected PCM work	sheet							
must be completed before the import will	WOIK.								
2. WQCV/EURV Outlet Details						Input Pa	rameters		
A) Average Infiltration Rate of WOCV					i =	User Input	COS DCM	in / hr	
B) Depth to Centrol of Underdrain Outlet	Orifice from filte	r media surface			y =	N/A	N/A	inches	
D) Number of WQCV Orifice Rows				# <b>V</b>	VQCV rows =	12	N/A 12	sqin	
E) Vertical Spacing between WQCV Orifice F) WQCV Orifice Area (A <sub>2</sub> ) per Row	e Rows			Orif	ice Spacing = WOCV Ao =	4.0	4.0	inches sa in	
<ul> <li>G) Maximum Stage of WQCV (includes ISI</li> <li>H) FURX (A) in Single Association (A) in Single Association</li> </ul>	D and Trickle Ch	hannel Depth)		Max	Stage WQCV =	4.00	4.00	ft	
<ul> <li>I) EURV Office Area (A<sub>0</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	and Trickle Cha	nnel Depth)		Max	Stage <sub>EURV</sub> =	6.00	6.00	sq in ft	
J) Discharge Coefficient for all WQCV/EUF	RV Outlet Orifice	e(s)			Cd =	0.60	0.60	]	
2. Fland Control Suphrane Basia Constants		Cas Fierras							Here any survival default fleed surphysics
<ol> <li>Flood Control Surcharge Basin Geometry ( Default Flood Surcharge Geometry inputs</li> </ol>	apove EURV) -	oee ⊢igure ntinuation of				Input Pa	rameters		user can override default flood surcharge geometry inputs to create a transition bench
the PCM Geometry in an upward direction	without a transit	tion bench.				User	COS DCM		between the top of the PCM and the Flood Surcharge Volume by entering larger
A) Length of Basin at Top of EURV					L <sub>PCM</sub> =	453.3	453.3	ft	dimensions in C), D), and E).
о) vviatn or вазіл at Top of EURV C) Stage at Top of Transition Bench (Botto	m of Flood Con	trol Surcharge)		Stage at To	p of Bench =	6.10	177.8 6.10	ft	See the Figure to the right.
<ul> <li>D) Length of Basin at Top of Transition Ber</li> <li>E) Width of Basin at Top of Transition Ber</li> </ul>	nch (Bottom of F	Flood Control Su	urcharge)		L <sub>Bench</sub> = W <sub>Bench</sub> =	454.1 178.6	454.1 178.6	rt ft	Bench Slope is 4H:1V in length direction Bench Slope is 4H:1V in width direction
F) Average Side Slopes of Flood Control S	Surcharge above	Transition Ben	ch		Z <sub>Surcharge</sub> =	4.00	4.00	ft / ft	
(Recommend no steeper than 3H:1V sl	ope. Use zero f	or vertical walls	.)						
4. Tributary Watershed Hydrology									
A) Input hydrology data (copy/paste) from r	model runs	2 Year	5 Year	Pre-Dev 10 Year	velopment Pe 25 Year	ak Flow (cfs) 50 Year	100 Year	500 Year	4
	Time later al		9.95				120.21		1
<li>B) Adjust "Time Interval" to match hydrograph data</li>	5.0	minutes							
5-yr and 100-yr Hydrology Required	Time (min)	2 Year	Pos 5 Year	t-Developme	25 Year	ow Hydrograph 50 Year	ns (cfs) 100 Year	500 Year	
(Other Storms are Optional)	0:00	2 100	0.00	i o i oui	20 100	oo rour	0.00	000 100	
	0:05		1.75				4.56		
	0:15		27.93				32.42		
	0:25		78.99				190.43		
	0:30		71.29 58.22				238.04 222.59		
	0:40		47.28				193.29		4
	0:50		32.22				131.89		1
	1:00		27.64 23.60				95.05		-
	1:05		20.00				74.37		
	1:15		14.05				38.35		1
	1:20 1:25		12.80				27.93		1
	1:30		11.62				18.07		4
	1:40		9.56				14.06		1
	1:45 1:50		8.84				12.98		1
	1:55		7.74				12.15		
	2:05		4.08				6.49		1
	2:10 2:15		2.79				4.48 3.04		1
	2:20		1.21				1.99		1
	2:30		0.49				0.80		1
	2:35 2:40		0.25				0.40		1
	2:45		0.01				0.01		4
	2:55		0.00				0.00		1
	3:00								1
	3:10								
	3:20								1
	3:25								1
	3:35								1
	3:45								1
	3:50 3:55							1	1
	4:00								
	4:10								1
	4:15 4:20								4
	4:25								1
	4:30								1
	4:40 4:45								4
	4:50								1
	4:55 5:00								1
	5:05								4
	5:15								1
	5:20 5:25								1
	5:30								4
	5:35								1

5:45         5:50         5:55         6:00	5:40				
5:50 <td>5:45</td> <td></td> <td></td> <td></td> <td></td>	5:45				
5:55 6:00	5:50				
6:00	5:55				
	6:00				

			Prelimin	ary Desigr	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g				
				COS PC	M-FSD Prelin	minary Desig	n (Beta Version	n 1.00, Septemb	er 2019)	Sheet 2 of 3				
						Designer:	Chris McFarlan	d						
		WA	TER, RES	OURCES		Project:	Grandview Res	erve Pond C						
COLORADO				BINEERING		Date:	April 6, 2020			Last Edited: April 08, 2020				
SPRINGS	<b>,</b>													
OLYMPIC CITY USA														
5. Flood Control Outlet Structure Ty	/pe				Overflov	v Weir/Grate, Out	let Pipe Restriction	& Emergency Spillwa	ev 🔻					
A) Select Flood Control Outlet S	tructure Type	9						5 5 1						
6. Overflow Weir (Dropbox) and Gra (Assumes that top of grate is fl	ate (Flat or S lush with the	loped) top of the con	crete dropbo	<)			Input Pa User	rameters COS						
A) Overflow Weir Front Edge He	ight (relative	to Stage = 0 f	t)			H <sub>weir front</sub> =	6.00	6.00	ft					
<ul> <li>B) Overflow Weir Front Edge Lei</li> </ul>	ngth (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	12.00	11.00	ft					
<ul> <li>C) Overflow Weir Grate Slope (H</li> <li>D) Horizontal Length of Weir Sid</li> </ul>	H:V, enter zer les (inside ed	ro for flat grate	e) ()		Horizor	S <sub>weir sides</sub> = ntal L <sub>weir sides</sub> =	0.00	0.00	ft/ft ft					
E) Overflow Grate Open Area %	(grate open	area / total gr	s, ate area)		Grate	Open Area =	70%	70%	%					
F) Debris Clogging %	(at back side	of dropbox)			Debr	ris Clogging = Hamto top =	50%	50%	% ft					
H) Overflow Grate Slope Length	(inside edge	of dropbox)			Slo	ppe L <sub>weir sides</sub> =	12.00	11.00	ft					
I) Overflow Grate Open Area (w	ithout debris)	)			Open Are	a (No Clogging) =	100.80	84.70	sq ft		бu			
<ul> <li>J) Overnow Grate Open Area (w</li> </ul>	nu i depris)				Open P	Clogged/ =	JU.4U	42.35	sq II		outi			
7. Outlet Pipe with Flow Restriction	Plate										SD) R			
A) Select Type of Outlet Restrict	ion	Vifico or Br -	angular Or#-	·•)		Circula	r Outlet Pipe w/ Res	trictor Plate		•	۲ (E			
(Circular Pipe W/ Restrictor Pla	ite, Circular C	Junce or Reci	angular Onlic	e)			Input Pa	rameters			tion			
							User	COS			ent			
B) Depth to Invert of Outlet Pipe	(relative to S	Stage = 0 ft)			Pipe I	nvert Depth =	1 50	1.50	ft		Det			
C) Outlet Pipe Diameter	(10)0010 10 10	Jugo o II)			Pip	e Diameter =	48.00	42.00	inches		Ε			
D) Restrictor Plate Height above E) Helf Control Angle of Pastrict	Pipe Invert	line			F	Plate Height =	33.13	39.36	inches		tru			
F) Outlet Orifice Area	E) Half-Central Angle of Restrictor Plate on Pipe F) Outlet Orifice Area					Outlet Ao =	9.25	9.37	sq ft		bec			
G) Height of Outlet Orifice Centry	oid above Ou	utlet Pipe Inve	rt			Outlet <sub>centroid</sub> =	1.54	1.71	ft		I S			
H) Ratio of Grate Open Area / 10	00-yr Orifice	Area (should l	be≥4)		Open	i Area Ratio =	10.90	9.04			Ful			
8. Emergency Spillway (Rectangula	ar or Trapezo	idal)					Input Pa	rameters			orm:			
							Input	DCM	-		е			
<ul> <li>A) Spillway Invert Stage (relative</li> <li>B) Spillway Coast Log ath</li> </ul>	e to Stage = (	D ft)				H <sub>spillway invert</sub> =	8.00	999.00	ft		- ng			
C) Spillway End Slopes (H:V)						S <sub>spillway ends</sub> =	4.00	42.00	ft / ft		če			
D) Freeboard above Maximum V	Vater Surface	e			Freel	board Depth=	1.00	1.00	ft		Pro			
<ul> <li>E) Spillway Design Flow Depth</li> <li>E) Stage at Top of Freeboard</li> </ul>					Freeboard	Deptn <sub>spillway</sub> = 1 Top Stage =	1.00		ft ft					
G) Basin Area at Top of Freeboard	ard				Max	Basin Area =	2.34		acres		esiç			
9. Routed Hydrograph Results											ary D			
Design Storm Return Period =	WOCV	EURV	2 Year	Resu 5 Year	ts based on 10 Year	User Input 25 Year	50 Year	100 Year	500 Year		min			
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79		4.34				12.42			reli			
Predevelopment Peak Q (cfs) =	N/A	N/A		10.0				120.2			₽.			
Peak Outflow (cfs) =	0.6	1.7		1.5				119.2						
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0						
Structure Controlling Flow = Max Velocity through Grate =	Orifice Plate N/A	Orifice Plate N/A		Orifice Plate N/A				Outlet Pipe 1 2						
Time to Drain 97% of Volume (hr) =	39	67		65				63						
Time to Drain 99% of Volume (hr) =	41	72		69				72						
Area at Max Ponding Depth (ft) =	4.00	1.85		1.80				1.98						
Maximum Volume Stored (ac-ft) =	1.36	4.79		4.07				6.91		l				
Design Storm Return Period =	WQCV	EURV	2 Year	Results 5 Year	based on CO 10 Year	S DCM Inputs 25 Year	s 50 Year	100 Year	500 Year					
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79		4.34			/ 001	12.42						
Predevelopment Peak Q (cfs) =	N/A	N/A		10.0				120.2						
Peak innow (Cfs) = Peak Outflow (cfs) =	0.6	1.7		1.5				116.8						
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0						
Structure Controlling Flow = Max Velocity through Grate =	Orifice Plate	Orifice Plate		Orifice Plate			L	Overflow Grate						
Time to Drain 97% of Volume (hr) =	39	67		65				63						
Time to Drain 99% of Volume (hr) =	41	72		69				72						
Maximum Ponding Depth (ft) = Area at Max Ponding Depth (ac) =	4.00	b.00 1.85		5.60				7.10						
Maximum Volume Stored (ac-ft) =	1.36	4.79		4.07				6.91						



		Preliminary Desig	gn Procedure Form: I	Full Spectrum Detention	(FSD) Routir	ng	
		COSF	PCM-FSD Preliminary Des	ign (Beta Version 1.00, Septe	mber 2019)	Sheet 1 of 3	
	STOR	MWATER	Projec	t: Grandview Reserve Pond D			
COLORADO		ENTERPRISE	Date	e: April 6, 2020		Last Edited: April 13, 2020	
SPRINGS							
OLYMPIC CITY <b>USA</b>							
1. Select WQCV/EURV PCM Type:				Extended Detention Basin (EDB)	•		
Imports the Stage-Area-Volume-Discharg corresponding PCM worksheet. The sele	e information fr ted PCM work	om the sheet					
must be completed before the import will	work.						
				Input Parametera			
2. WQCV/EURV Oullet Details				User Input COS DCN	1		
<ul> <li>A) Average Infiltration Rate of WQCV</li> <li>B) Depth to Centroid of Underdrain Outlet (</li> </ul>	Orifice from filter	r media surface	ı y	= N/A N/A = N/A N/A	in / hr inches		
C) Underdrain Outlet Orifice Area D) Number of WQCV Orifice Rows			Underdrain Ao # WQCV rows	= N/A N/A = 13 13	sq in		
<ul> <li>E) Vertical Spacing between WQCV Orifice</li> <li>E) WQCV Orifice Area (A) per Row</li> </ul>	Rows		Orifice Spacing WOCV An	= 4.0 4.0 = 1.34 1.34	inches		
G) Maximum Stage of WQCV (includes ISE	and Trickle Ch	nannel Depth)	Max Stage WQCV	= 4.50 4.50	ft		
<ul> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	and Trickle Cha	nnel Depth)	Max Stage <sub>EURV</sub>	= <u>20.83</u> <u>20.83</u> = <u>6.50</u> <u>6.50</u>	ft		
<ul> <li>J) Discharge Coefficient for all WQCV/EUF</li> </ul>	V Outlet Orifice	(s)	Cd	= 0.60 0.60			
8. Flood Control Surcharge Basin Geometry (a	above EURV) - :	See Figure				User can override default flood surcharge	
Default Flood Surcharge Geometry inputs	represent a con without a transit	itinuation of		Input Parameters	_	geometry inputs to create a transition bench	
A) Longth of Daria at Tag. ( CUD) (				Input DCM	ft	Surcharge Volume to entering larger	
<ul> <li>A) Length of Basin at Top of EURV</li> <li>B) Width of Basin at Top of EURV</li> </ul>			W PCM	= <u>588.5</u> <u>588.5</u> = <u>180.1</u> <u>180.1</u>	ft	See the Figure to the right.	
<ul> <li>C) Stage at Top of Transition Bench (Botton D) Length of Basin at Top of Transition Ber</li> </ul>	m of Flood Con tch (Bottom of F	trol Surcharge)	Stage at Top of Bench L Bench	= 6.60 6.60 = 589.3 589.3	ft	Bench Slope is 4H:1V in length direction	
E) Width of Basin at Top of Transition Bend E) Average Side Slopes of Flood Control S	h (Bottom of Flo	ood Control Surcharge)	W Bench	= <u>180.9</u> <u>180.9</u> = <u>4.00</u> <u>4.00</u>	ft ft/ft	Bench Slope is 4H:1V in width direction	
(Recommend no steeper than 3H:1V sk	ope. Use zero f	or vertical walls.)	- surcharge	4.00			
Tributany Waterched Hydrology			1				
		0.1/22	Pre-Development F	Peak Flow (cfs)	500.11	1	
<ul> <li>A) Input hydrology data (copy/paste) from r</li> </ul>	nodel runs	2 Year 5 Year 30.00	10 Year 25 Year	50 Year 100 Year 154.35	500 Year		:
<ul> <li>B) Adjust "Time Interval" to match hydrograph data</li> </ul>	Time Interval 5.0	minutes					
5-vr and 100-vr Hydrology Required	Time (min)	2 Year 5 Year	ost-Development Storm In 10 Year 25 Year	flow Hydrographs (cfs) 50 Year 100 Year	500 Year	]	
(Other Storms are Optional)	0:00	0.00		0.00			
	0:05	1.91		5.05		1	
	0:15 0:20	36.44 87.25		44.44 108.47		4	
	0:25	118.48		244.10			
	0:35	95.70		305.49		1	
	0:40	67.12		239.63		1	
	0:50 0:55	56.09 48.05		204.40		1	
	1:00	41.91 36.47		156.02		4	
	1:10	30.68		102.47		1	
	1:20	21.41		56.75		1	
	1:25	19.34		42.46		1	
	1:35 1:40	16.52		28.16 24.40		1	
	1:45	13.77		21.80		}	
	1:55	12.02		18.83		1	
	2:00	6.95		10.86		1	
	2:10 2:15	4.98		7.82		1	
	2:20	2.44		3.93		4	
	2:30	1.13	1 1	1.86		1	
	2:35	0.72	1 1	0.67		1	
	2:45	0.20		0.31		1	
	2:55 3:00	0.04		0.05		1	
	3:05	0.01	1	0.01		1	
	3:15	0.00	1	0.00		1	
	3:20 3:25			0.00		1	
	3:30 3:35					1	
	3:40					]	
	3:50					1	
	4:00					1	
	4:05 4:10					1	
	4:15					}	
	4:25					1	
	4:30 4:35					1	
	4:40 4:45					}	
	4:50					}	
	5:00					1	
	5:05					1	
	5:15 5:20					1	
	5:25 5:30					4	
	5:35					1	1

5:45 5:50 5:50
5:50
5:55
6:00

			Prelimin	ary Desigr	Procedure	e Form: Fu	II Spectrum	Detention (F	SD) Routin	g	
				COS PC	M-FSD Prelin	minary Desig	n (Beta Versior	n 1.00, Septemb	er 2019)	Sheet 2 of 3	
						Designer:	Chris McFarlan	d			
		WA	TER RES	OURCES		Project:	Grandview Res	erve Pond D			
			ENC	INEERING		Date:	April 6, 2020			Last Edited: April 13, 2020	
SPRINGS	,			_							
OLYMPIC CITY USA											
5. Flood Control Outlet Structure Ty	/pe				Overflow	w Weir/Grate Out	let Pine Restriction	& Emergency Spillw	av 🔻		1
A) Select Flood Control Outlet S	tructure Type	e						a anto gana, ap	·, ·		
6. Overflow Weir (Dropbox) and Gr. (Assumes that top of grate is fl	ate (Flat or S lush with the	loped) top of the con	crete dropbo	<)			Input Pa User	rameters COS			
A) Overflow Weir Front Edge He	ight (relative	to Stage = 0 f	t)			H <sub>weir front</sub> =	6.50	6.50	Ift		
B) Overflow Weir Front Edge Le	ngth (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	11.00	9.00	ft		
C) Overflow Weir Grate Slope (H	H:V, enter zei	ro for flat grat	e)		Horizor	S <sub>weir sides</sub> = ntal Luorador =	0.00	0.00	ft / ft		
E) Overflow Grate Open Area %	(grate open	area / total or	ate area)		Grate	Open Area =	70%	70%	%		
F) Debris Clogging %		, i	,		Debr	ris Clogging =	50%	50%	%		
<ul> <li>G) Height of Grate Upper Edge</li> <li>H) Overflow Grate Slope Longth</li> </ul>	(at back side	of dropbox)			Sic	m <sub>grate top</sub> =	6.50	6.50	ft ft		
<ul> <li>I) Overflow Grate Slope Length</li> <li>I) Overflow Grate Open Area (w</li> </ul>	ithout debris	)			Open Are	ea (No Clogging) =	84.70	56.70	sq ft		D
J) Overflow Grate Open Area (w	ith debris)				Open A	Area ( <sub>Clogged</sub> ) =	42.35	28.35	sq ft		utin
7. Outlet Pipe with Flow Restriction	Plate										D) Ro
A) Select Type of Outlet Restrict	ion					Circula	r Outlet Pipe w/ Res	strictor Plate		•	(FS
(Circular Pipe w/ Restrictor Pla	te, Circular (	Drifice or Rect	angular Orific	e)			Input Pa	rameters			io
							User	COS			enti
R) Dopth to Invert of Outlot Ding	(relative to 6	Store = 0.00			Pine I	nvert Depth -	Input 1.50	DCM 1.50	<b>H</b>		ē
C) Outlet Pipe Diameter	(relative to a	stage – 0 it)			Pip	be Diameter =	48.00	48.00	inches		Ē
D) Restrictor Plate Height above	Pipe Invert				Ē	Plate Height =	44.00	44.00	inches		Ľ.
E) Half-Central Angle of Restrict E) Outlet Orifice Asso	tor Plate on F	Pipe				Theta =	2.56	2.56	radians		ect
<ul> <li>G) Height of Outlet Orifice Centr</li> </ul>	oid above Ou	utlet Pipe Inve	rt			Outlet Ao = Outlet <sub>centroid</sub> =	12.07	12.07	ft		s S
H) Ratio of Grate Open Area / 1	00-yr Orifice	Area (should l	be≥4)		Open	Area Ratio =	7.02	4.70	j		Ē
8. Emergency Spillway (Rectangula	ar or Trapezo	idal)					Input Pa	rameters			orm:
		2.60				u -1	Input	DCM	14		е Е
<ul> <li>A) Spillway Invert Stage (relative B) Spillway Crest Length</li> </ul>	e to Stage = t	J IL)				L <sub>spillway crest</sub> =	8.00	999.00 42.00	ft		qr
C) Spillway End Slopes (H:V)						S <sub>spillway ends</sub> =	4.00	4.00	ft / ft		ő
D) Freeboard above Maximum V	Vater Surfac	е			Freet	board Depth=	1.00	1.00	ft		Å
<ul> <li>E) Splitway Design Flow Depth</li> <li>F) Stage at Top of Freeboard</li> </ul>					Freeboard	d Top Stage =	10.00		ft		Б
G) Basin Area at Top of Freeboa	ard				Max	Basin Area =	2.95		acres		Jesi
9. Routed Hydrograph Results											lary D
Design Storm Return Period =	WQCV	EURV	2 Year	Resu 5 Year	Its based on 10 Year	25 Year	50 Year	100 Year	500 Year		ці.
Inflow Hydrograph Volume (ac-ft) =	1.96	6.56		6.97				18.57			e
Predevelopment Peak Q (cfs) =	N/A	N/A		30.0				154.4			
Peak Inflow (cfs) = Peak Outflow (cfs) =	0,9	IN/A 2.2		2.2				314.4			
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.1				1.0			
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Orifice Plate				Outlet Pipe			
Time to Drain 97% of Volume (br) =	1N/A 40	IN/A 67		1N/A 70				62			
Time to Drain 99% of Volume (hr) =	42	72		75				72			
Maximum Ponding Depth (ft) =	4.50	6.50		6.50				7.90			
Maximum Volume Stored (ac-ft) =	1.71	∠.43 6.56		∠.43 6.59				2.63			
				Results	based on CO	S DCM Inputs					
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year		
Predevelopment Peak O (cfs) =	1.96 N/A	6.56 N/A		6.97 30.0				18.57			
Peak Inflow (cfs) =	N/A	N/A		118.5				314.4			
Peak Outflow (cfs) =	0.9	2.2		2.2				153.1			
Katio (Uuttlow/Predevelopment) = Structure Controlling Flow =	N/A Orifice Plate	N/A Orifice Plate		0.1 Orifice Plate		-		1.0 Overflow Grate			
Max Velocity through Grate =	N/A	N/A		N/A				2.8			
Time to Drain 97% of Volume (hr) =	40	67		70				63			
I ime to Drain 99% of Volume (hr) = Maximum Ponding Depth (ft) =	42	72		75				72			
Area at Max Ponding Depth (ac) =	1.71	2.43		2.43				2.66			
Maximum Volume Štored (ac-ft) =	1.96	6.56		6.59				10.66		]	
L											



		Preliminary Desig	n Procedure Form: F	ull Spectrum Detention (FSD	) Routing
		COS F	CM-FSD Preliminary Designed	gn (Beta Version 1.00, September 2	2019) Sheet 1 of 3
	STOR	MWATER	Designer Project	Grandview Reserve Pond E	
COLORADO	UTUTI	ENTERPRISE	Date	April 6, 2020	Last Edited: April 13, 2020
SPRINGS					
OLYMPIC CITY USA					
<ol> <li>Select WQCV/EURV PCM Type: Imports the Stage-Area-Volume-Discharg</li> </ol>	ge information fi	rom the		Extended Detention Basin (EDB)	•
corresponding PCM worksheet. The sele	ected PCM work	sheet			
must be completed before the import will	I WOIK.				
2. WQCV/EURV Outlet Details				Input Parameters	
A) Average Infiltration Rate of WQCV			i	User Input COS DCM	/ br
B) Depth to Centroid of Underdrain Outlet	Orifice from filte	r media surface	y:	N/A N/A inc	thes
D) Number of WQCV Orifice Rows			# WQCV rows =	= 10 10	11
E) Vertical Spacing between WQCV Orifice F) WQCV Orifice Area (A <sub>2</sub> ) per Row	e Rows		Orifice Spacing = WOCV Ao =	4.0 4.0 inc 0.67 0.67 sq	in .
G) Maximum Stage of WQCV (includes ISI	D and Trickle Cl	hannel Depth)	Max Stage WQCV	3.60 3.60 ft	
<ul> <li>I) EURV Office Area (A<sub>0</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	and Trickle Cha	nnel Depth)	Max Stage <sub>EURV</sub> =	4.50 4.50 ft	In
<ul> <li>J) Discharge Coefficient for all WQCV/EUF</li> </ul>	RV Outlet Orifice	e(s)	Cd =	0.60 0.60	
	EUDIA	0.5			
<ol> <li>FIGOD CONTROL SURCHARGE Basin Geometry ( Default Flood Surcharge Geometry inputs</li> </ol>	above EURV) - represent a cor	oee ⊢igure ntinuation of		Input Parameters	User can override detault flood surcharge geometry inputs to create a transition bench
the PCM Geometry in an upward direction	without a transi	tion bench.		User COS Input DCM	between the top of the PCM and the Flood Surcharge Volume by entering larger
A) Length of Basin at Top of EURV			L PCM	327.0 327.0 ft	dimensions in C), D), and E).
о) vviotn of Basin at Top of EURV C) Stage at Top of Transition Bench (Botto	om of Flood Con	trol Surcharge)	Stage at Top of Bench	<b>127.7</b> Tt <b>4.60</b> 4.60 ft	See the Figure to the right.
D) Length of Basin at Top of Transition Ber E) Width of Basin at Top of Transition Ber	nch (Bottom of F	Flood Control Surcharge)	L Bench = W Bench =	327.8 327.8 ft 128.5 128.5 ft	Bench Slope is 4H:1V in length direction Bench Slope is 4H:1V in width direction
F) Average Side Slopes of Flood Control S	Surcharge above	Transition Bench	Z Surcharge =	4.00 4.00 ft /	ft
(Recommend no steeper than 3H:1V sl	ope. Use zero f	or vertical Walls.)			
1. Tributary Watershed Hydrology					
A) Input hydrology data (copy/paste) from r	model runs	2 Year 5 Year	Pre-Development P 10 Year 25 Year	eak Flow (cfs) 50 Year 100 Year 5	500 Year
P) Adjust "Time Interval" to match	Time Interva	32.34		157.99	
hydrograph data	5.0	minutes			
5-vr and 100-vr Hydrology Required	Time (min)	2 Year 5 Year	10 Year 25 Year	low Hydrographs (cfs) 50 Year 100 Year 5	500 Year
(Other Storms are Optional)	0:00	0.00		0.00	
	0:00	1.11		1.54	
	0:15	5.07		7.00 35.29	
	0:25	41.87		110.52	
	0:30	40.50		162.17 176.94	
	0:40	37.83		172.03	
	0:50	29.04		147.26	
	1:00	22.65		124.96	
	1:05	19.67 16.82		109.31 92.46	
	1:15	14.63		77.36	
	1:25	11.61		56.57	
	1:30	10.30		48.68 41.54	
	1:40	7.47		34.92	
	1:50	4.75		22.81	
	1:55	3.50		17.32	
	2:05	1.86		8.45	
	2:10	1.43		4.29	
	2:20	0.92		3.03	
	2:30	0.57		1.42	
	2:40	0.44		0.50	
	2:45 2:50	0.26		0.55	
	2:55	0.15		0.34	
	3:05	0.07		0.19	
	3:10	0.05		0.13	
	3:20	0.02		0.04	
	3:30	0.00		0.00	
	3:35	0.00		0.00	
	3:45	0.00			
	3:55	0.00			
	4:00	0.00			
	4:10 4:15	0.00			
	4:20				
	4:25				
	4:35				
	4:45				
	4:50				
	5:00 5:05				
	5:10				
	5:15				
	5:25				
	5:35				

5:45        5:50        5:55        6:00	5:40				
5:50	5:45				
5:55 6:00 C C C C C C C C C C C C C C C C C C	5:50				
6:00	5:55				
	6:00				

			Prelimin	ary Desigr	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g	
				COS PC	M-FSD Prelin	minary Desig	n (Beta Versio	n 1.00, Septemb	oer 2019)	Sheet 2 of 3	
						Designer:	Chris McFarlar	ıd			
		WA	TER, RES	OURCES		Project:	Grandview Res	erve Pond E			
COLORADO			ENC	INEERING		Date:	April 6, 2020			Last Edited: April 13, 2020	
SPRINGS	<b>,</b>										
OLYMPIC CITY USA											
5. Flood Control Outlet Structure T	уре				Overflov	v Weir/Grate, Out	let Pipe Restriction	& Emergency Spillwa	ay 🔻		
A) Select Flood Control Outlet S	Structure Type	e						5 5 1			
6. Overflow Weir (Dropbox) and Gr (Assumes that top of grate is f	ate (Flat or S lush with the	loped) top of the con	crete dropbo	()			Input Pa User	rameters COS			
A) Overflow Weir Front Edge He	eight (relative	to Stage = 0	t)			H <sub>weir front</sub> =	4,50	4.50	ft		
<ul> <li>B) Overflow Weir Front Edge Le</li> </ul>	ength (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	15.00	9.00	ft		
C) Overflow Weir Grate Slope (I D) Horizontal Length of Weir Sid	H:V, enter zei des (inside ed	ro for flat grat	∋) /)		Horizor	s <sub>weir sides</sub> = tal L <sub>weir sides</sub> =	0.00	0.00	ft / ft		
E) Overflow Grate Open Area %	6 (grate open	area / total gr	ate area)		Grate	Open Area =	70%	70%	%		
F) Debris Clogging %	(-+   :- -	-f			Debr	ris Clogging =	50%	50%	%		
H) Overflow Grate Slope Length	(inside edge	of dropbox)			Slo	ppe L <sub>weir sides</sub> =	15.00	9.00	ft		
I) Overflow Grate Open Area (w	vithout debris	) ,			Open Are	a (No Clogging) =	157.50	56.70	sq ft		Ð
<li>J) Overflow Grate Open Area (v</li>	vith debris)				Open A	(Clogged) =	/8./5	28.35	sq tt		outi
7. Outlet Pipe with Flow Restriction	Plate										SD) R
A) Select Type of Outlet Restric	tion	Orifing of D	ongular Orif	o)		Circula	r Outlet Pipe w/ Re	strictor Plate		▼	Ë,
(Circular Pipe w/ Restrictor Pia	ate, Circular (	Jrince or Rec	angular Onlic	e)			Input Pa	rameters			tion
							User	COS	•		ent
B) Depth to Invert of Outlet Pipe	(relative to S	Stage = 0 ft)			Pipe I	nvert Depth =	1 50	1.50	ft		Det
C) Outlet Pipe Diameter	(101001010101	stage enty			Pip	e Diameter =	60.00	54.00	inches		Ξ
D) Restrictor Plate Height above E) Helf Control Angle of Bostria	) Restrictor Plate Height above Pipe Invert Half-Central Angle of Restrictor Plate on Pipe				F	Plate Height =	43.00	50.00	inches		tru
F) Outlet Orifice Area	) Half-Central Angle of Restrictor Plate on Pipe ) Outlet Orifice Area					Outlet Ao =	15.06	2.59	sq ft		bec
G) Height of Outlet Orifice Centr	Outlet Orifice Area Height of Outlet Orifice Centroid above Outlet Pipe Invert					Outlet <sub>centroid</sub> =	1.99	2.18	ft		I S
<ul> <li>H) Ratio of Grate Open Area / 1</li> </ul>	00-yr Orifice	Area (should	oe≥4)		Open	i Area Ratio =	10.46	3.69			Ful
8. Emergency Spillway (Rectangula	ar or Trapezo	oidal)					Input Pa User	rameters COS			orm:
A) Californi Invest Change (calatio		0.40					Input	DCM	14		ē
<ul> <li>A) Spillway Invert Stage (relativ</li> <li>B) Spillway Crest Length</li> </ul>	e to Stage = I	υπ)				Lenilway creat =	5.80	999.00	ft		qr
C) Spillway End Slopes (H:V)						S <sub>spillway ends</sub> =	4.00	4.00	ft / ft		Sce
<ul> <li>D) Freeboard above Maximum</li> <li>E) Spillway Design Flow Depth</li> </ul>	Water Surfac	e			Freel	Depthoniture =	1.00	1.00	ft ft		L L
F) Stage at Top of Freeboard					Freeboard	i Top Stage =	7.50		ft		uß
G) Basin Area at Top of Freebo	ard				Max	Basin Area =	1.22		acres		Desi
9. Routed Hydrograph Results				Dec	te bacad ar	lleor pout					nary
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year		in.
Inflow Hydrograph Volume (ac-ft) =	0.81	1.70		3.01				12.89			Pe
Peak Inflow (cfs) =	N/A	N/A N/A		46.6				176.9			4
Peak Outflow (cfs) =	0.3	0.4		18.0				164.2			
Ratio (Outflow/Predevelopment) = Structure Controlling Flow =	N/A Orifice Plate	N/A Orifice Plate		0.6 Overflow Groto				1.0 Outlet Pipe			
Max Velocity through Grate =	N/A	N/A		0.1				1.0			
Time to Drain 97% of Volume (hr) =	44	69		71				54			
Maximum Ponding Depth (ft) =	46 3,60	4,50		4,80				5.70			
Area at Max Ponding Depth (ac) =	0.88	0.96		0.98				1.06			
Maximum Volume Stored (ac-ft) =	0.81	1.70		1.99		I		2.91	1		
Design Storm Return Period =	WQCV	EURV	2 Year	Results 5 Year	based on CO 10 Year	25 Year	s 50 Year	100 Year	500 Year		
Inflow Hydrograph Volume (ac-ft) =	0.81	1.70		3.01				12.89			
Predevelopment Peak Q (cfs) = Peak Inflow (cfs) =	N/A N/A	N/A N/A		32.3 46.6				158.0			
Peak Outflow (cfs) =	0.3	0.4		16.3				153.2			
Ratio (Outflow/Predevelopment) =	N/A	N/A Orifio- Di-t		0.5				1.0 Operations 2			
Max Velocity through Grate =	N/A	N/A		0.3				2.8			
Time to Drain 97% of Volume (hr) =	44	69		71				54			
I ime to Drain 99% of Volume (hr) = Maximum Ponding Depth (ft) =	46	72		76 4 90				69 6 10			
Area at Max Ponding Depth (ac) =	0.88	0.96		0.99				1.10			
Maximum Volume Stored (ac-ft) =	0.81	1.70		2.09				3.34			



		Preliminary Desig	n Procedure Form: Fu	ull Spectrum Detention (FS	SD) Routin	g	
		COS PO	CM-FSD Preliminary Desig	n (Beta Version 1.00, Septemb	er 2019)	Sheet 1 of 3	
	STOR	MWATER	Designer: Project:	Grandview Reserve Pond F			
COLORADO		ENTERPRISE	Date:	April 6, 2020		Last Edited: April 13, 2020	
SPRINGS							
OLYMPIC CITY USA							
1. Select WQCV/EURV PCM Type:			F	xtended Detention Basin (EDB)	•		
Imports the Stage-Area-Volume-Discharg	e information fr	rom the				I	
must be completed before the import will	work.	sneet					
							-
. WQCV/EURV Outlet Details				User Input COS DCM			
<ul> <li>A) Average Infiltration Rate of WQCV</li> <li>B) Depth to Centroid of Underdrain Outlet (</li> </ul>	Drifice from filter	r media surface	i = v =	N/A N/A N/A N/A	in / hr inches		
C) Underdrain Outlet Orifice Area			Underdrain Ao = #WOCV rows =	N/A N/A	sq in		
E) Vertical Spacing between WQCV Orifice	Rows		Orifice Spacing =	4.0 4.0	inches		
<ul> <li>G) Maximum Stage of WQCV (includes ISE</li> </ul>	and Trickle Ch	hannel Depth)	Max Stage <sub>WQCV</sub> =	4.80 4.50	sq in ft		
<ul> <li>H) EURV Orifice Area (A<sub>o</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	Ind Trickle Char	nnel Depth)	EURV Ao = Max Stage <sub>EURV</sub> =	1.55 7.84 6.00 6.00	sq in ft		
J) Discharge Coefficient for all WQCV/EUR	V Outlet Orifice	e(s)	Cd =	0.60 0.60			
Flood Control Surcharge Basin Geometry (a	above FURV) - S	See Figure				User can override default flood surcharge	
Default Flood Surcharge Geometry inputs	represent a con	ntinuation of		Input Parameters		geometry inputs to create a transition bench	
the PCM Geometry in an upward direction	williout a transit	uon bench.		Input DCM		Surcharge Volume by entering larger	
<ul> <li>A) Length of Basin at Top of EURV</li> <li>B) Width of Basin at Top of EURV</li> </ul>			L PCM = W PCM =	570.9 570.9 217.0 217.0	ft	dimensions in C), D), and E). See the Figure to the right.	
C) Stage at Top of Transition Bench (Botton D) Length of Basin at Top of Transition Ben	m of Flood Cont ich (Bottom of F	trol Surcharge)	Stage at Top of Bench = L Bench =	6.10 6.10 571.7 571.7	ft ft	Bench Slope is 4H:1V in length direction	
E) Width of Basin at Top of Transition Benc	h (Bottom of Flo	ood Control Surcharge)	W Bench =	217.8 217.8	ft ft/ft	Bench Slope is 4H:1V in width direction	
(Recommend no steeper than 3H:1V slo	ope. Use zero f	for vertical walls.)	∠ Surcharge =	4.00 4.00	n./ n.		
Tributon (Watarch - J. Ludon)			1				
A) Input hydrology	adal		Pre-Development Pe	ak Flow (cfs)	E00 V		
A) input nyurology data (copy/paste) from n	TUDAEI FUNS	2 rear 5 Year 42.34	10 rear 25 Year	221.11	DUU Year		
<li>B) Adjust "Time Interval" to match hydrograph data</li>	Time Interval 5.0	minutes					
5-vr and 100-vr Hydrology Required	Time (min)	2 Year 5 Year	st-Development Storm Infl 10 Year 25 Year	ow Hydrographs (cfs) 50 Year 100 Year	500 Year		
(Other Storms are Optional)	0:00	0.00		0.00			
	0:10	5.98		8.99			
	0:15	58.79		25.32 77.64			
	0:25	94.74 103.82		207.48 301.83			
	0:35	97.47 87.23		329.97 323.46			
	0:45	77.84		304.34			
	0:50	61.26		281.05			
	1:00	54.52		237.51 211.11			
	1:10	45.22		185.26 161.15			
	1:20	36.24		139.03			
	1:30	28.34		101.90			
	1:35 1:40	24.61		86.26 72.79			
	1:45 1:50	19.05		62.33 54.79			
	1:55	16.04		48.91			
	2:05	11.69		35.81			
	2:10 2:15	9.57 7.79		29.96 24.91			
	2:20 2:25	6.28 5.03		20.57 16.95			
	2:30	4.03		13.95			
	2:35	2.52		9.20			
	2:45 2:50	1.92 1.38		7.18			
	2:55 3:00	0.95 0.65		3.69 2.49			
	3:05	0.46		1.70			
	3:15	0.33		0.81			
	3:20 3:25	0.18		0.56			
	3:30	0.11		0.26			
	3:40	0.06		0.13			
	3:45	0.03		0.10			
	3:55 4:00	0.02		0.05			
	4:05 4:10	0.01		0.03			
	4:15	0.00		0.02			
	4:20			0.00			
	4:30 4:35						
	4:40						
	4:50						
	5:00						
	5:05 5:10						
	5:15 5:20						
	5:25						
	5:35						

5:45 5:50 5:50
5:50
5:55
6:00

				Prelimin	ary Desigr	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g	
<form><form></form></form>					COS PC	M-FSD Prelin	minary Desig	n (Beta Versior	n 1.00, Septemi	oer 2019)	Sheet 2 of 3	
<form></form>							Designer:	Chris McFarlan	d			
				TER RES			Project:	Grandview Res	erve Pond F			
<form></form>				ENC	AINEERING		Date:	April 6, 2020			Last Edited: April 13, 2020	
	COLOIOLD	)										
9. Post Carted Outer Browner Type	OLYMPIC CITY USA											
Al: Steel: Pleor Coulds Outed Burkum Type       Define Wind (Dopping) and Case (Har ar Reco) (Harman State (Har bet for a for an article of the counced explosit)       Image: Plant State (Har Bet Har Bet State (Har Bet State (H	5. Flood Control Outlet Structure T	уре								_		
• Output       • Output <td< td=""><td>A) Select Flood Control Outlet S</td><td>structure Type</td><td>e</td><td></td><td></td><td>Overflov</td><td>v Weir/Grate, Out</td><td>let Pipe Restriction</td><td>&amp; Emergency Spillw</td><td>ay 🔻</td><td></td><td></td></td<>	A) Select Flood Control Outlet S	structure Type	e			Overflov	v Weir/Grate, Out	let Pipe Restriction	& Emergency Spillw	ay 🔻		
• Order Word (Depoin) and Care (Hao Signed) (Annem Nather Boyd In Status Mark Nather Boyd In Careboan Careboan (Depoint) (Mark Shafe) (Habe Use Signed Para) (Depoint) (Mark Shafe) (Habe Use Shafe) (Habe Use Shafe) (Mark Shafe) (Habe Use Shafe) (Mark Shafe) (M	,	,										
A) Order Wwer Froet Edge Lendt (ratione Singe of Dig)       Image: Singe Lendth (Singe Singer S	<ol> <li>Overflow Weir (Dropbox) and Gr (Assumes that top of grate is f</li> </ol>	ate (Flat or S lush with the	loped) top of the con	crete dropbo	<)			Input Pa User	rameters COS	-		
B) Outdow War Prot figs integer (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the problem (and the days)       Image: And the days of the	A) Overflow Weir Front Edge He	eight (relative	to Stage = 0	ft)			H <sub>weir front</sub> =	6.00	6.00	ft		
C)       Outbook Weigheld Stopp 4 by, date zero for date good (main real)       International transmission	<ul> <li>B) Overflow Weir Front Edge Le</li> </ul>	ngth (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	13.00	10.00	ft		
<ul> <li></li></ul>	C) Overflow Weir Grate Slope (	H:V, enter zei	ro for flat grat	e)		Horizor	S <sub>weir sides</sub> =	0.00	0.00	ft/ft		
Pi beier Cogging 'S       Deski Cogging 'S	<ul> <li>F) Overflow Grate Open Area %</li> </ul>	arate open	area / total gr	x) rate area)		Grate	Open Area =	70%	70%	%		
0. Height of Gate Upper Edge (it back site of display)       Stepper (it back site of dit back site of display)       Stepper (it back	F) Debris Clogging %	10		,		Debr	ris Clogging =	50%	50%	%		
In the dependence of the begin (in the be	G) Height of Grate Upper Edge	(at back side	of dropbox)			SIC	H <sub>grate top</sub> =	6.00	6.00	ft		
J       Open Area (unit code)	<ul> <li>I) Overflow Grate Slope Length</li> <li>I) Overflow Grate Open Area (w</li> </ul>	i (inside eage /ithout debris	) (xoaqoro io			Open Are	a (No Clonging) =	118.30	70.00	sa ft		5
2. Outlet Pipe vin Pipe Restriction Plate       Creater Diper of Calital Additional Pipe (relative los Stage = 0 fit)       Image: Pipe Vince Plate (Creative Plate Creative Calital Pipe Vince)       Image: Pipe Vince Plate (Creative Pipe Vince)       Image: Pipe Vince Plate (Creative Plate Creative Calital Pipe Vince)       Image: Pipe Vince Plate (Creative Pipe Vince)       Image: Pipe Vince Plate (Creative Plate Vince)       Image: Pipe Vince Plate (Creative Plate Vince)       Image: Pipe Vince Plate Vince Plate (Creative Plate Vince)       Image: Pipe Vince Plate Vince	J) Overflow Grate Open Area (w	/ith debris)	,			Open A	Area ( <sub>Clogged</sub> ) =	59.15	35.00	sq ft		ţ,
1. Outer Plow with Flow Restriction Flate.       Circular Office or Restangular Office.       Circular Office of Rest. Circular Office or Restangular Office.       Incluse Ventor Office Network       Incluse Ventor Office Ne												Rot
A) Beach Type of Outlier Research     Calcular Page of Outlier Research Tortices     Image	7. Outlet Pipe with Flow Restriction	Plate									-	(DS
Instruction     Inst	<ul> <li>A) Select Type of Outlet Restrict (Circular Pipe w/ Restrictor Pipe)</li> </ul>	tion ate Circular (	Orifice or Rect	angular Orific	e)		Circula	r Outlet Pipe w/ Res	trictor Plate		•	Ľ,
a) Depth to baret of Ouder Rps (relative to Stage = 0 ft)  <	(onotial ripe wittestrotor ric				0)			Input Pa	rameters	_		tio
B) Dight is breed of Outlet Pipe (value to Stage = 0.1)       Pipe breed Depth = <u>minute</u> =								User	COS			ie i
•••••••••••••••••••••••••••••	B) Depth to Invert of Outlet Pipe	(relative to S	Stage = 0 ft)			Pipe I	nvert Depth =	1.50	1.50	ft		ē
D) Restrictor Plate Height above Ppol Inert B) Hald-Control Age of Restrictor Plate on Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate on Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate on Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate on Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate on Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate Of Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate Of Upits Pipe Inert B) Restrictor Plate Age of Restrictor Plate Of Upits Plate Age of Upits Plate Age of Upits Plate Age of Plate Age of Upits Plate Age of Upit	C) Outlet Pipe Diameter	(10101110 10 1	stage – e trj			Pip	e Diameter =	66.00	60.00	inches		Ε
E) Hall-Contral Angle of Restrictor Plate on Ppee       Thetas = 1.98 (2.60 modes)       Thetas = 1.98 (2.6	D) Restrictor Plate Height above	Pipe Invert				Ē	Plate Height =	46.05	54.00	inches		Ē
1) United Units Area     During Units Area     During Units Area     To Area     T	E) Half-Central Angle of Restric	Half-Central Angle of Restrictor Plate on Pipe Outlet Orifice Area					Theta =	1.98	2.50	radians		ect
H) Rate of Grate Open Area (100-yr Ortice Area (should be 2-4)       Open Area Ratio =       0.58       3.76         8. Emergency Spillway (Rectangular or Trapezoidal)       User Area Ratio =       0.68       3.76       0.500       11       0.500       11       0.500       11       0.500       11       0.500       11       0.500       11       0.500       11       0.500       11       0.500       11       11       0.500       11       11       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       0.500       11       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15       11       15	G) Height of Outlet Orifice Centr	oid above Ou	utlet Pipe Inve	rt			Outlet A0 =	2.14	2.38	ft		sp g
B. Emergency Spillway (Rectangular or Trapezoidal)         Imput Parameters         Other Construction         Imput Parameters         Other Construction         Imput Parameters         Imput Paramet	H) Ratio of Grate Open Area / 1	00-yr Orifice	Area (should	be ≥ 4)		Open	Area Ratio =	6.68	3.76	1		5
A) Spillway Invert Stage (relative to Stage = 0 ft)     User     COS       B) Spillway Crest Length     User     COS       C) Spillway End Stopes (HV)     Dipert Stage and Top of Freeboard     1000     1000     ft       B) Stage at Top of Freeboard     Submay Stafe Stopes (HV)     Submay Stafe St	8. Emergency Spillway (Rectangula	ar or Trapezo	oidal)					Input Pa	rameters			rm: E
A) Spilway Invert Stage (reliative to Stage = 0 ft)       B) Spilway Crest Length       H_gluay unit = 1280 999.00 ft								User Input	COS DCM			ЪЧ
B) Splitway Credit Length (1) Splitway Credit Calops, Hol Splitway (1) Splitway Credit Calops, Hol Splitway Credit Calops, Hol Sp	A) Spillway Invert Stage (relative	e to Stage = (	0 ft)				H <sub>spillway invert</sub> =	7.60	999.00	ft #		n
D) Freeboard above Maximum Water Surface       Freeboard Depth       100	<ul> <li>B) Spillway Crest Length</li> <li>C) Spillway End Slopes (HV)</li> </ul>						Lspillway crest = Sepillway ende =	126.00	42.00	ft / ft		ĕ
E) Spillway Design Flow Depth       Flow Depth using =       0.90       ft	D) Freeboard above Maximum V	Nater Surfac	e			Freel	board Depth=	1.00	1.00	ft		ē
P) Stage at Top of Freeboard       Preeboard       Preeboard Top Stage #       3.50       tt       dt       dt <td< td=""><td>E) Spillway Design Flow Depth</td><td></td><td></td><td></td><td></td><td>Flow</td><td>Depth<sub>spillway</sub> =</td><td>0.90</td><td></td><td>ft</td><td></td><td><u>с</u></td></td<>	E) Spillway Design Flow Depth					Flow	Depth <sub>spillway</sub> =	0.90		ft		<u>с</u>
9. Routed Hydrograph Results     Naccine     Results based on User Input       Design Storm Return Period = Inflow Hydrograph Volume (act) = Peak Inflow (cl) = Return Volume (sc) = Return Volume (sc) = Return Volume (sc) = Return Volume (sc) = Time to Drain 97% of Volume (nr) = Time to Drain 97% of Volume (nr) = Return Volume (sc) = Return Volume (s	<ul> <li>F) Stage at Top of Freeboard</li> <li>G) Basin Area at Top of Freeboard</li> </ul>	ard				Freeboard	Basin Area =	9.50		nt acres		sig
9. Routed Hydrograph Kesults       Results based on User Input         Design Storm Return Period Inflow Hydrograph Volume (ch) =       VacCv       EURV       2 Year       50 Year       50 Year       500 Year         Predevelopment Peak Q(cfs) =       N/A       N/A       42.3       22.11       26.3       50.4       22.5       5.94       22.5       24.5       22.11       26.3       20.11       27.3       20.11       27.3       20.11       27.3       20.11       10.1       22.1       20.3       20.11       10.1       22.7       3       0.0100 Wear       500 Year       10.1       10.1       0.0100 Wear       500 Year       10.9       10.1										-		ъ De
Design Storm Return Period =       WQCV       EURV       2 Year       5 Year       10 Year       26 Year       100 Year       500 Year         Inflow Hydrograph Volume (cits) =       N/A       N/A       42.3       -       223.1       -         Predevelopment Peak Q (cits) =       N/A       N/A       42.3       -       221.1       -         Ratio (Quiftov(cits) =       N/A       N/A       42.3       -       227.3       -         Ratio (Quiftov(cits) =       1.1       1.5       15.1       -       227.3       -         Structure Controlling Flow =       Onflee Plane       Owerlew Grate       -       0.04ter Ppe       -         Max/mol/Prodevelopment) =       N/A       N/A       0.2       -       1.9       -         Time to Drain 97% of Volume (hr) =       42       68       72       -       61       -         Time to Drain 97% of Volume (hr) =       42       77       -       72       -       61       -         Maximum Ponding Depth (fit) =       4.80       6.00       6.30       -       7.60       -       -         Maximum Polume Stored (ac-ft) =       2.62       5.94       6.82       -       10.070       - <td< td=""><td>9. Routed Hydrograph Results</td><td></td><td></td><td></td><td>Resu</td><td>Its based on</td><td>User Input</td><td></td><td></td><td></td><td>1</td><td>Jina</td></td<>	9. Routed Hydrograph Results				Resu	Its based on	User Input				1	Jina
Bit Mont (galage) routine (galage)     2.02     3.94     7.00     20.1       Predevelopmet Peak (Gis)     N/A     N/A     103.8     221.1       Peak Outflow (Gis)     N/A     N/A     103.8     330.0       Ratio (Outflow/Predevelopment)     N/A     N/A     0.4     0.10       Structure Controlling Flow     Outflow (Gis)     N/A     N/A     0.4       Max Velocity through Grate     N/A     0.4     1.0       Time to Drain 97% of Volume (hr)     45     72     61       Area at Max Ponding Depth (Gis)     2.12     2.84     2.89     3.08       Maximum Volume Stored (ac-ft)     2.12     2.84     2.89     10.70       Design Storm Return Period     2.52     5.94     6.82     10.70       Predevelopment Peak (Gis)     N/A     10.3     25.11     10.94       Predevelopment Peak (Gis)     1.1     1.4     13.2     22.11       Maximum Volume Stored (ac-ft)     2.12     2.84     2.89     3.08       Predevelopment Peak (Gis)     1.0     10.94     20.37     10.94       Predevelopment Peak (Gis)     1.0     10.94     20.37     20.37       Predevelopment Peak (Gis)     1.1     1.4     13.2     22.1.1       Peak Untflow (Gis)<	Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year		li
Peak Inflow (cfs) = Peak Outflow (cfs) = NA         N/A         N/A         103.8         330.0           Ratio (Outflow/Predevelopment) = Structure Controlling Flow = Max Velocity through Grate = Time to Drain 99% of Volume (hr) = 42         0.15         15.1         227.3           Time to Drain 99% of Volume (hr) = Maximum Ponding Depth (a) = 2.52         0.77         0.72         1.9           Maximum Ponding Depth (a) = Inflow Hydrograph Volume (hr) = 4.5         4.5         72         77         72           Area at Max Ponding Depth (b) = Maximum Volume (ac-ft) = Design Storm Return Period Inflow Hydrograph Volume (ac-ft) = Structure Controlling Flow = Maximum Volume (cfs) = N/A         N/A         4.2         2.89         3.08           Ratio (Outflow/Fredevelopment Peak (cfs) = Structure Controlling Flow = Maximum Volume (cfs) = N/A         N/A         4.2         2.99         3.08           Ratio (Outflow/Fredevelopment Peak (cfs) = Structure Controlling Flow = Max Velocity through Grate = N/A         N/A         4.2.3         2.21         5.94           Ratio (Outflow/Fredevelopment Peak (cfs) = Structure Controlling Flow = Max Velocity through Grate Time to Drain 97% of Volume (hr) = 3.8         N/A         0.0.2         3.0           N/A         N/A         0.02         3.0         7.80         4.50         6.82           Max Velocity through Grate Max Velocity through Grate Time to Drain 97% of Volume (hr) = 3.8         7.8 <td>Predevelopment Peak O (cfs) =</td> <td>2.02 N/A</td> <td>5.94 N/A</td> <td></td> <td>42.3</td> <td></td> <td></td> <td></td> <td>20.37</td> <td>t</td> <td></td> <td>P 2</td>	Predevelopment Peak O (cfs) =	2.02 N/A	5.94 N/A		42.3				20.37	t		P 2
Peak Outflow (cfs) =       1.1       1.5       15.1       227.3         Ratio (Outflow/Prodevelopment) =       N/A       N/A       0.4       1.0         Structure Controlling Flow =       N/A       N/A       0.4       0.016         Time to Drain 97% of Volume (hr) =       42       68       72       1.3         Time to Drain 97% of Volume (hr) =       45       72       77       72         Maximum Ponding Depth (ft) =       4.8.0       6.00       6.30       7.60         Area at Max Ponding Depth (ac) =       2.12       2.84       2.89       3.08         Maximum Volume Stored (ac-ft) =       2.21       2.84       2.89       3.08         Design Storm Return Period =       2.21       2.94       7.80       26.37         Predevelopment Peak Q (cfs) =       N/A       N/A       42.3       26.37         Predevelopment Peak Q (cfs) =       N/A       N/A       42.3       22.11         Peak Outflow (cfs) =       N/A       N/A       42.3       22.11         Predevelopment Peak Q (cfs) =       N/A       N/A       42.3       22.11         Peak Outflow (cfs) =       N/A       N/A       3.80.0       1.0.4         Structure Contoling Flow =	Peak Inflow (cfs) =	N/A	N/A		103.8				330.0			
NA       NA       U.4       1.0         Structure Controlling Flow = Once Plate       Overflow Grate       Outlet Plap         Max Velocity through Grate = NA       NA       0.2       1.9         Time to Drain 99% of Volume (hr) = 42       68       72       61         Max Max Ponding Depth (ac) = 2.12       2.84       2.89       3.08         Area at Max Ponding Depth (ac) = 2.62       5.94       6.822       10.70         Design Storm Return Period = 2.62       Results based on COS DCM Inputs         Predevelopment Peak Q (cfs) = NA       N/A       42.3       22 Year       50 Year         Predevelopment Peak Q (cfs) = NA       N/A       42.3       22 Year       25 Year       50 Year         Predevelopment Peak Q (cfs) = NA       N/A       10.8       30.0       10.0       10.1         Structure Controlling Flow Max Velocity through Grate NA       N/A       0.03       1.0       10.1         Structure Controlling Flow Max Velocity through Grate NA       N/A       0.03       10.0       10.1         Structure Controlling Flow Max Velocity through Grate NA       N/A       0.2       3.0       10.0         Structure Controlling Flow Max Velocity through Grate NA       N/A       0.03       10.0       10.1	Peak Outflow (cfs) =	1.1	1.5		15.1				227.3			
Outcome main         Oracle Table         Oracle Table         Oracle Table         Oracle Table           Max Velocity through Grate =         IVA         N/A         0.2         1.9           Time to Drain 97% of Volume (hr) =         42         68         72         61           Time to Drain 99% of Volume (hr) =         45         72         77         72           Maximum Ponding Depth (hc) =         2.12         2.84         2.89         3.06           Area at Max Ponding Depth (ac) =         2.62         5.94         6.82         10.70           Design Storm Return Period =         2.212         2.84         2.89         2.02         50 Year           Inflow Hydrograph Volume (ac-ft) =         2.212         5.94         7.80         26.37           Predevelopment Peak Q (cfs) =         N/A         N/A         42.3         22.11           Pack Inflow (cfs) =         N/A         103.8         300.0         10.0           Peak Outflow (cfs) =         N/A         0.03         10.0         10.0           Structure Controlling Flow         Oracle Table         Overflow Grade         0.0         0.0           Max Velocity through Grate =         N/A         0.2         3.0         10.0	Ratio (Outflow/Predevelopment) =	N/A Orifice Plate	N/A Orifice Ploto		U.4 Overflow Croto				1.0 Outlet Pinc			
Time to Drain 97% of Volume (hr) =       42       68       72       61         Time to Drain 99% of Volume (hr) =       45       72       77       72         Maximum Ponding Depth (ft) =       4.80       6.00       6.30       7.60         Area at Max Ponding Depth (ft) =       2.12       2.84       2.89       3.08         Maximum Volume Stored (ac-ft) =       2.62       5.94       6.82       10.70         Design Storm Return Period =       WQCV       EURV       2 Year       5 Year       10 Year         Predevelopment Peak (cfs) =       N/A       7.80       221.1       5.94       6.82         Predevelopment Peak (cfs) =       N/A       10.3.8       390.0       221.1         Peak Inflow (cfs) =       N/A       10.3.8       390.0       10         Ratio (Outfow/Predevelopment) =       N/A       10.3.8       390.0       10         Structure Controlling Flow =       Onder Pate       Overflow Grate       0verflow Grate       0verflow Grate         Max Wooding Unough (frate =       N/A       0.2       3.0       10       10         Time to Drain 97% of Volume (hr) =       38       73       78       73         Maximum Ponding Depth (ft) =       4.50	Max Velocity through Grate =	N/A	N/A		0.2				1.9			
Time to Drain 99% of Volume (hr) =       45       72       77       72         Maximum Ponding Depth (ft) =       4.80       6.00       6.30       7.60         Area at Max Ponding Depth (ac) =       2.12       2.84       2.89       3.08         Maximum Volume Stored (ac-ft) =       2.62       5.94       6.82       10.70         Results based on COS DCM Inputs         WQCV EURV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year         Inflow Hydrograph Volume (ac-ft) =       2.21       5.94       7.80         Predevelopment Peak Q (cfs) =       N/A       10.23       330.0         Pack Inflow (cfs) =       1.1       1.4       13.2       214.5         Ratio (Outflow/Pedevelopment) =       N/A       0.03       1.0       0verlaw Grate         Max Velocity through Grate =       N/A       0.24       3.0       1.1         Max Velocity through Grate =       N/A       0.24       3.0       1.1         Time to Drain 99% of Volume (hr) =       38       73       78       73         Maximum Ponding Depth (ft) =       1.81       2.84       2.89       3.11         Maximum Ponding Depth (ft) =       2.84       2.89       3.11       1.32 <td>Time to Drain 97% of Volume (hr) =</td> <td>42</td> <td>68</td> <td></td> <td>72</td> <td></td> <td></td> <td></td> <td>61</td> <td></td> <td>1</td> <td></td>	Time to Drain 97% of Volume (hr) =	42	68		72				61		1	
Maxmum Ponding Deptn (a) =       4.80       6.00       6.30       7.60         Area at Max Ponding Deptn (a) =       2.12       2.84       2.89       3.08         Maximum Volume Stored (ac-ft) =       2.62       5.94       6.82       10.70         Design Storm Return Period =       Image: Constraint of the stored (ac-ft) =       2.12       2.84       2.89       10.70         Inflow Hydrograph Volume (ac-ft) =       2.21       5.94       7.80       10.70       25 Year       50 Year       100 Year       500 Year         Predevelopment Peak Q (cfs) =       NA       NA       42.3       22.11       10.70         Peak Inflow (cfs) =       NA       NA       40.3.8       30.0       10         Peak Mid(st) =       NA       NA       0.0.3       10       0xethors Grade         Maximum Conting Flow       Oxethors Grade       Oxethors Grade       0xethors Grade       0xethors Grade         Max Velocity through Grate =       NA       NA       0.2       3.0       11         Time to Drain 97% of Volume (hr) =       38       73       78       73       73         Maximum Ponding Depth (ft) =       1.81       2.84       2.89       3.11       11.32         Maximum Ponding D	Time to Drain 99% of Volume (hr) =	45	72		77				72			
Maximum Volume Stored (ac-ft) =         2.02         2.03         0.00           Design Storm Return Period =         WQCV         EURV         2 Year         5 Year         10 70           Inflow Hydrograph Volume (ac-ft) =         22.1         5.94         7.80         10.70           Predevelopment Peak Q (ds) =         NA         NA         42.3         22.1.1           Peak Inflow (ds) =         NA         NA         42.3         22.1.1           Peak Notic (ds) =         NA         NA         40.3.8         30.00           Peak Notic (ds) =         NA         NA         40.3.8         30.00           Pask Inflow (ds) =         NA         NA         0.3         0.1.0           Structure Controlling Flow =         Once Pate Critec Pate         Overflow Grate           Max Velocity through Grate =         NIA         N/A         0.2           Time to Drain 97% of Volume (hr) =         38         73         78           Maximum Ponding Depth (ft) =         18.1         2.84         2.89           Area at Max Ponding Depth (ft) =         18.1         2.84         2.89           Maximum Volume Stored (ac-ft) =         2.21         5.94         3.11	Maximum Ponding Depth (ft) = Area at Max Ponding Depth (ac) =	4.80	0.00	<u> </u>	0.30		<u> </u>		7.60			
Results based on COS DCM Inputs           Design Storm Return Period =           Unflow Hydrograph Volume (ac-th) =         2.21         5.94         7.80         26 Year         50 Year         100 Year         260 Year           Predevelopment Peak (cfs) =         NA         NA         42.3         22.11            Peak Inflow (cfs) =         NA         NA         42.3         22.11            Peak Num (cfs) =         NA         NA         42.3         21.1            Peak Outflow (cfs) =         NA         NA         42.3         21.1            Structure Controlling Flow =         NIA         NIA         0.3         1.0            Structure Controlling Flow =         Onfice Ptate         Overflow Crate         Overflow Grate            Max Velocity through Grate =         NIA         NIA         0.2         3.0            Time to Drain 97% of Volume (hr) =         36         69         74         63            Time to Drain 97% of Volume (hr) =         3.8         73         78         73            Area at Max Ponding Depth (ac) =         1.81         2.84         2.89         3.11 <td< td=""><td>Maximum Volume Stored (ac-ft) =</td><td>2.62</td><td>5.94</td><td></td><td>6.82</td><td></td><td></td><td></td><td>10.70</td><td><u> </u></td><td></td><td></td></td<>	Maximum Volume Stored (ac-ft) =	2.62	5.94		6.82				10.70	<u> </u>		
Design Storm Return Period =         WOCV         EURV         2 Year         5 Year         10 Year         25 Year         100 Year         500 Year           Inflow Hydrograph Volume (ac-th) =         2.21         5.94         7.80         26.37         221.1         221.1           Predevelopment Peak Q(cfs) =         NA         N/A         42.3         221.1         221.1           Peak Inflow (cfs) =         NA         N/A         103.8         330.0         241.5           Peak Outflow (cfs) =         N/A         N/A         0.3         0.10         244.5           Structure Controlling Flow =         Order Pate         Overflow Crate         0.400         0.2         3.0           Time to Drain 97% of Volume (hr) =         36         69         74         63         73           Time to Drain 99% of Volume (hr) =         38         73         78         73         78           Maximum Ponding Depth (hz) =         1.81         2.84         2.89         3.11         4.82           Maximum Volume Stored (ac-ft) =         2.21         5.94         6.82         11.32         5.04					Results	based on CO	S DCM Inputs	s			l i i i i i i i i i i i i i i i i i i i	
Initial organ         Call         Column         Call         Column         Call         Column         Call         Call <thcall< th="">         Call         <thcall< th="">         Call         Call<td>Design Storm Return Period =</td><td>WQCV</td><td>EURV</td><td>2 Year</td><td>5 Year</td><td>10 Year</td><td>25 Year</td><td>50 Year</td><td>100 Year</td><td>500 Year</td><td></td><td></td></thcall<></thcall<>	Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year		
Peak Inflow (cfs) =         N/A         I/03.8         330.0           Peak Outflow (cfs) =         1.1         1.4         13.2         214.5           Ratio (Outflow/Pedevelopment) =         N/A         N/A         0.3         1.0           Structure Controlling Flow =         Ortice Plate         Overflow Crate         Overflow Grate           Max Velocity through Grate =         N/A         0.3         0.2         3.0           Time to Drain 97% of Volume (hr) =         36         69         74         63           Time to Drain 97% of Volume (hr) =         38         73         78         73           Maximur Ponding Depth (ht) =         4.50         6.00         6.30         7.80           Area at Max Ponding Depth (ac) =         1.81         2.84         2.89         3.11           Maximum Volume Stored (ac-ft) =         2.21         5.94         6.82         11.32	Predevelopment Peak O (cfs) =	2.21 N/A	5.94 N/A		42.3				20.37	<u> </u>		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Peak Inflow (cfs) =	N/A	N/A	1	103.8				330.0		1	
Ratio (Outflow/Predevelopment)         N/A         0.3         1.0           Structure Controlling Flow         Onfoe Plate         Onfoe Plate         Overflow Grate           Max Velocity through Grate         N/A         0.2         3.0           Time to Drain 97% of Volume (hr)         36         69         74         63           Time to Drain 97% of Volume (hr)         38         73         78         73           Maximum Ponding Depth (t)         4.50         6.00         6.30         7.80           Area at Max Ponding Depth (ac) =         1.81         2.84         2.89         3.11           Maximum Volume Stored (ac-ft) =         2.21         5.94         6.82         11.32	Peak Outflow (cfs) =	1.1	1.4		13.2				214.5			
Structure Controlling From =         Ontice Plate         Overflow Grate         Overflow Grate           Max Velocity through Grate =         NA         N/A         0.2         3.0           Time to Drain 97% of Volume (hr) =         36         69         74         63           Time to Drain 99% of Volume (hr) =         38         73         78         63           Maximum Ponding Depth (h) =         4.50         6.00         6.30         7.80           Area at Max Ponding Depth (ac) =         1.81         2.84         2.89         3.11           Maximum Volume Stored (ac-ft) =         221         5.94         6.82         11.32	Ratio (Outflow/Predevelopment) =	N/A	N/A		0.3				1.0			
Time to Drain 97% of Volume (hr) =         36         69         74         63           Time to Drain 99% of Volume (hr) =         38         73         78         73           Maximum Ponding Depth (ft) =         4.50         6.00         6.30         7.80           Area at Max Ponding Depth (gt) =         1.81         2.84         2.89         3.11           Maximum Volume Stored (ac-ft) =         2.21         5.94         6.82         11.32	Structure Controlling Flow = Max Velocity through Grate =	Orifice Plate	Orifice Plate	<u> </u>	Overflow Grate		<u> </u>		Overflow Grate			
Time to Drain 99% of Volume (hr) =       38       73       78       73         Maximum Ponding Depth (h) =       4.50       6.00       6.30       7.80         Area at Max Ponding Depth (ac) =       1.81       2.84       2.89       3.11         Maximum Volume Stored (ac-ft) =       2.21       5.94       6.82       11.32	Time to Drain 97% of Volume (hr) =	36	69		74				63			
Maximum Ponding Depth (ft) =         4.50         6.00         6.30         7.80           Area at Max Ponding Depth (ac) =         1.81         2.84         2.89         3.11           Maximum Volume Stored (ac-ft) =         2.21         5.94         6.82         11.32	Time to Drain 99% of Volume (hr) =	38	73		78				73			
Area at wax Funding Deput (ac) -     1.01     2.04     2.09     3.11       Maximum Volume Stored (ac-ft) =     2.21     5.94     6.82     11.32	Maximum Ponding Depth (ft) =	4.50	6.00	<u> </u>	6.30				7.80			
	Maximum Volume Stored (ac-ft) =	2.21	∠.04 5.94		6.82				11.32			



<form><form></form></form>			Preliminary D	Design	Procedure	e Form: Fu	II Spectrum	Detention (F	SD) Routin	ng	
<form><form><form><form></form></form></form></form>			C	COS PCI	M-FSD Prelin	ninary Desig	n (Beta Version	n 1.00, Septem	ber 2019)	Sheet 1 of 3	
<form><form></form></form>		STOR		R		Proiect:	Grandview Res	erve Pond G			
<form></form>	COLORADO	0101	ENTERPRIS	E		Date:	April 6, 2020			Last Edited: April 13, 2020	
<form></form>	SPRINGS										
<form></form>	OLYMPIC CITY <b>USA</b>										
<form></form>	1. Select WQCV/EURV PCM Type:					E	stended Detention F	lasin (EDB)	•		
<form></form>	Imports the Stage-Area-Volume-Discharg	e information fr	rom the								
	must be completed before the import will	work.	sneet								
											-
	2. WQCV/EURV Outlet Details						Input Pa User Input	cos DCM	-		
	A) Average Infiltration Rate of WQCV B) Depth to Centroid of Underdrain Outlet (	)rifice from filter	r media surface			i = v =	N/A N/A	N/A N/A	in / hr inches		
	C) Underdrain Outlet Orifice Area				Und # M	derdrain Ao =	N/A	N/A	sq in		
	E) Vertical Spacing between WQCV Orifice	Rows			Orifi	ce Spacing =	4.0	4.0	inches		
<form></form>	<ul> <li>F) WQCV Orfice Area (A<sub>o</sub>) per Row</li> <li>G) Maximum Stage of WQCV (includes ISE</li> </ul>	and Trickle Ch	nannel Depth)		Max	Stage work =	0.49 3.20	0.49 3.20	sq in ft		
	<ul> <li>H) EURV Orifice Area (A<sub>o</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	ind Trickle Chai	nnel Depth)		Max	EURV Ao = Stage <sub>EURV</sub> =	1.94 4.00	1.94 4.00	sq in ft		
	J) Discharge Coefficient for all WQCV/EUR	V Outlet Orifice	e(s)			Cd =	0.60	0.60			
<text></text>	Eland Control Surpharga Basin Coometry /		Soo Eiguro							Heer can everyide default flood oursharge	
	Default Flood Surcharge Geometry inputs	represent a con	tinuation of				Input Pa	rameters	-	geometry inputs to create a transition bench	
bigs aff of the aff o	the PCM Geometry in an upward direction	without a transit	tion bench.				User Input	DCM	_	between the top of the PCM and the Flood Surcharge Volume by entering larger	
<ul> <li>Be a final provide the relations the robust control backboard provide the ro</li></ul>	<ul> <li>A) Length of Basin at Top of EURV</li> <li>B) Width of Basin at Top of EURV</li> </ul>					L <sub>PCM</sub> = W <sub>PCM</sub> =	349.7 105.4	349.7 105.4	ft	dimensions in C), D), and E). See the Figure to the right.	
	C) Stage at Top of Transition Bench (Botton	m of Flood Cont	trol Surcharge)	arce)	Stage at To	p of Bench =	4.10	4.10	ft ft	Bench Slone is 4H:4V in length direction	
	E) Width of Basin at Top of Transition Bend	h (Bottom of Flo	ood Control Surchar	rge)		W Bench =	106.2	106.2	ft	Bench Slope is 4H:1V in width direction	
	<ul> <li>Average Side Slopes of Flood Control Si (Recommend no steeper than 3H:1V slope)</li> </ul>	urcharge above ope. Use zero f	or vertical walls.)			∠ Surcharge =	4.00	4.00			
in order to provide the construction of the constr	Tributary Watershed Hydrology				Pre-Dev	elopment Pe	ak Flow (cfs)			]	
	<ul> <li>A) Input hydrology data (copy/paste) from n</li> </ul>	nodel runs	2 Year 5 Y 9.	rear .42	10 Year	25 Year	50 Year	100 Year 48.48	500 Year	1	
Trie         Teal Quarkament Storn blogs Hydrographs (cf)           100 yr Hydroky Repaired         100 yr         100 yr         100 yr           100 yr Hydroky Repaired         100 yr         100 yr         100 yr           100 yr Hydroky Repaired         100 yr         100 yr         100 yr           100 yr         100 yr         100 yr         100 yr           110 yr         100 y	<li>B) Adjust "Time Interval" to match hydrograph data</li>	Time Interval	minutes							-	9
	F ut and 100 ut Hudralamy Required	Time	2 Voor 5	Post	-Developme	nt Storm Infl	ow Hydrograph	ns (cfs)	E00 Voor	]	
015     015     016       025     1269     01755       025     1269     01755       025     026     0756       025     0275     0756       025     0275     0757       026     0275     0757       027     0275     0757       028     0277     0573       029     0277     0573       029     0277     0573       029     0277     0573       029     0277     0573       029     0277     0533       029     0277     0533       029     0277     0533       029     0277     0533       029     0277     0533       029     029     0335       029     029     0335       029     029     0335       029     029     0335       029     029     040       029     029     040       029     029     040       020     029     040       020     029     040       020     029     040       020     029     040       020     029     040       020	(Other Storms are Optional)	0:00	2 fear <b>3</b>	.00	10 fear	25 fear	50 fear	0.00	500 real		
0 15     3.86     0     9.55       0 23     0 206     0     9.346       0 35     0 872     0     9.346       0 40     16.84     0     6.51       0 40     16.84     0     9.746       0 40     16.84     0     9.746       0 40     16.84     0     9.746       0 40     16.84     0     9.746       0 40     11.85     0     9.746       0 40     11.85     0     9.746       1 10     0.90     0     3.832       1 10     0.90     0     3.832       1 10     0.90     0     3.832       1 10     0.90     0     16.97       1 10     0.90     0     16.37       1 20     7.67     0     13.36       1 30     5.98     0     13.31       1 50     3.32     0     10.01       1 50     3.32     0     16.37       1 50     3.32     0     16.34       2 50     2 25     0     7.10       2 50     1 5.9     15.9     15.9       2 50     1 5.9     1 5.9     1 5.9       2 50     0 5.9     0 5.9 <t< td=""><td></td><td>0:05</td><td>0.</td><td>.18 .27</td><td></td><td></td><td></td><td>0.49</td><td></td><td>1</td><td></td></t<>		0:05	0.	.18 .27				0.49		1	
050     1021     4738       050     2006     0206       051     1023     02071       052     1234     02031       053     1234     02031       054     1234     02031       055     1245     02031       050     1374     02031       100     1011     04033       103     1021     03352       103     1021     03352       103     1232     02331       103     1232     02331       103     1232     02331       103     1232     02331       103     1232     02331       103     1232     02331       103     1232     02331       103     1232     03331       104     444     14331       105     1333     0345       106     1333     0345       107     200     287       108     444     1433       109     243     1333       101     138     443       102     139     1444       103     1445     1434       105     139     1434       106     139 <td< td=""><td></td><td>0:15</td><td>3.</td><td>.86 2.69</td><td></td><td></td><td></td><td>5.05 17.55</td><td></td><td>4</td><td></td></td<>		0:15	3.	.86 2.69				5.05 17.55		4	
043         1025           040         1683         6661           045         1623         1023           040         1112         1023           100         1112         14453           103         100         1112           103         100         1112           103         100         1112           103         100         1112           104         1410           105         100           106         1017           107         100           108         100           109         100           100         742           101         100           102         100           103         100           104         4044           105         1033           106         1033           107         1033           108         1033           109         1033           100         1033           101         1033           102         1033           103         1034           104         1035 <t< td=""><td></td><td>0:25</td><td>19</td><td>9.21</td><td></td><td></td><td></td><td>47.38</td><td></td><td>1</td><td></td></t<>		0:25	19	9.21				47.38		1	
0.00     10.05     0.00       0.03     11.12     0.03       0.05     11.12     0.03       100     11.12     0.03       1105     0.00     0.01       1105     0.00     0.01       1105     0.00     0.01       1105     0.00     0.01       1105     0.00     0.01       1105     0.00     0.01       120     7.42     0.03       120     7.42     0.03       131     0.00     0.01       132     0.00     0.01       133     0.02     0.02       140     4.04     0.03       143     4.05     0.03       145     4.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03       145     0.05     0.03		0:35	18	3.72				67.51		1	
050     13.74     0     57.80       105     110.01     44.0       105     110.01     44.0       105     6.00     33.52       115     6.00     33.55       115     6.00     33.55       126     0.07     22.86       137     0.07     22.86       130     5.98     22.03       135     5.26     10.87       140     4.05     10.87       140     4.05     10.83       150     3.52     11.83       155     3.52     0.40       200     2.00     0.40       201     1.00     5.93       215     1.68     4.40       202     2.00     0.40       210     1.00     5.93       211     1.00     5.93       212     1.01     1.00       203     0.02     2.24       213     1.62     1.00       224     0.02     2.24       235     0.62     1.00       240     0.42     0.73       255     0.22     0.044       310     0.01     0.019       311     0.07     0.039       320     0.02 </td <td></td> <td>0:40 0:45</td> <td>16</td> <td>5.24</td> <td></td> <td></td> <td></td> <td>66.01 62.38</td> <td></td> <td>1</td> <td></td>		0:40 0:45	16	5.24				66.01 62.38		1	
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116 $0.06$ $33.56$ $116$ $0.06$ $23.56$ $128$ $6.67$ $23.48$ $133$ $0.98$ $22.05$ $134$ $4.64$ $1153$ $144$ $4.64$ $11533$ $144$ $4.64$ $11533$ $144$ $4.64$ $11533$ $145$ $526$ $11188$ $150$ $526$ $11188$ $150$ $526$ $11188$ $150$ $526$ $11188$ $150$ $126$ $1276$ $210$ $190$ $593$ $210$ $190$ $593$ $230$ $0.62$ $254$ $230$ $0.62$ $190$ $240$ $0.46$ $130$ $240$ $0.66$ $0.99$ $330$ $0.177$ $0.39$ $340$ $0.077$ $534$ $350$ $0.177$ $0.39$ $350$ $0.177$ $0.39$ $350$ $0.107$ $0.09$		1:00	11	0.01				49.93			
113     0.40     338       123     7.07     23.38       123     0.98     22.33       133     5.28     16.97       140     4.54     16.97       140     4.54     16.97       140     4.54     16.97       140     4.54     16.97       140     4.54     16.97       140     4.54     10.11       155     3.12     10.10       200     2.67     8.48       201     1.39     4.44       202     2.66     7.10       210     1.93     4.44        221     1.68     3.35       222     1.68     3.45       230     0.42     2.44       240     0.46     3.45       241     0.46     13.86       243     0.36     0.98       244     0.46     0.13       245     0.27     0.44       300     0.13     0.98       311     0.10     0.18       325     0.22     0.08       330     0.03     0.06       331     0.02     0.04       344     0.03     0.06       345     0.01     0.04		1:10	9.	.05				38.52		1	
120     6.67     223       130     5.98     183       133     5.28     183       145     4.05     183       145     3.52     1133       145     3.52     1133       200     2.67     8.48       211     1.63     1.63       200     2.67     8.48       211     2.63     7.18       213     2.63     4.44       214     1.55     3.52       215     1.58     4.43       216     1.58     3.52       220     1.30     4.44       221     1.30     4.44       223     1.65     3.52       244     0.35     0.54       255     0.22     0.54       250     0.28     0.73       255     0.22     0.54       300     0.17     0.18       311     0.07     0.13       322     0.65     0.03       323     0.04     0.07       334     0.05     0.04       340     0.02     0.04       341     0.02     0.04       342     0.03     0.04       343     0.01     0.03		1:15 1:20	8.	.20				33.58 29.30		1	
133 $5.28$ $1897$ $146$ $405$ $1531$ $150$ $352$ $1183$ $150$ $357$ $940$ $205$ $225$ $740$ $210$ $190$ $593$ $215$ $158$ $433$ $220$ $130$ $444$ $223$ $130$ $444$ $223$ $135$ $357$ $236$ $062$ $250$ $236$ $062$ $250$ $236$ $062$ $250$ $244$ $035$ $099$ $246$ $035$ $039$ $246$ $035$ $039$ $316$ $017$ $038$ $316$ $017$ $013$ $330$ $005$ $009$ $325$ $044$ $007$ $333$ $005$ $0092$ $325$ $014$ $007$ $333$ $005$ $019$ $346$ $007$ $013$ $355$ $001$ <td< td=""><td></td><td>1:25 1:30</td><td>6. 5.</td><td>.67 .98</td><td></td><td></td><td></td><td>25.48 22.03</td><td></td><td>1</td><td></td></td<>		1:25 1:30	6. 5.	.67 .98				25.48 22.03		1	
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1.50     3.42     11.53       155     3.27     10.10       205     2.26     7.10       210     1.90     5.93       211     1.58     4.433       220     1.30     4.404       225     1.05     3.25       230     0.62     2.24       245     0.35     0.99       245     0.35     0.99       245     0.35     0.99       245     0.35     0.99       245     0.35     0.99       245     0.35     0.99       250     0.28     0.93       250     0.28     0.93       300     0.17     0.39       315     0.06     0.13       316     0.13     0.28       330     0.17     0.03       3310     0.10     0.01       335     0.02     0.03       340     0.02     0.03       335     0.02     0.03       345     0.01     0.02       355     0.02     0.03       345     0.01     0.02       356     0.41     0.02       405     0.00     0.01       405     0.00       4		1:45	4.	.05				13.93		1	
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			Prelimin	ary Desigr	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g		
				COS PC	M-FSD Prelin	minary Desig	n (Beta Versior	1.00, Septemb	er 2019)	Sheet 2 of 3		
						Designer:	Chris McFarlan	d				
		WA	TER, RES	OURCES		Project:	Grandview Res	erve Pond G				
COLORADO				INEERING		Date:	April 6, 2020			Last Edited: April 13, 2020		
SPRINGS	<b>,</b>											
OLYMPIC CITY USA												
5. Flood Control Outlet Structure T	уре				Overflov	v Weir/Grate. Out	let Pipe Restriction i	& Emergency Spillw	v V			
A) Select Flood Control Outlet S	Structure Type	e						5 5 1				
<ol><li>Overflow Weir (Dropbox) and Gr (Assumes that top of grate is f</li></ol>	ate (Flat or S lush with the	loped) top of the con	crete dropbo	<)			Input Pa User	rameters COS				
A) Overflow Weir Front Edge He	eight (relative	to Stage = 0	t)			H <sub>weir front</sub> =	4.00	4.00	ft			
B) Overflow Weir Front Edge Le	ength (inside e	edge of dropb	ox)			L <sub>weir front</sub> =	26.00	26.00	ft			
<ul> <li>C) Overflow Weir Grate Slope (</li> <li>D) Horizontal Length of Weir Si</li> </ul>	H:V, enter zei des (inside ed	ro for flat grat lae of dropbo	e) ()		Horizor	S <sub>weir sides</sub> = ntal L <sub>weir sides</sub> =	0.00	26.00	ft / ft ft			
E) Overflow Grate Open Area %	6 (grate open	area / total gr	s, ate area)		Grate	Open Area =	70%	70%	%			
F) Debris Clogging %	(at back side	of drophox)			Debr	ris Clogging = Harrata tan =	50%	50%	% ft			
H) Overflow Grate Slope Length	inside edge	of dropbox)			Slo	ppe L <sub>weir sides</sub> =	26.00	26.00	ft			
I) Overflow Grate Open Area (v	vithout debris	)			Open Are	a (No Clogging) =	473.20	473.20	sq ft		bu	
<ol> <li>J) Overnow Grate Open Area (v</li> </ol>	viu'i debris)				Open P	Clogged) -	∠30.6U	230.6U	sd II		outi	
7. Outlet Pipe with Flow Restriction	Plate										SD) R	
A) Select Type of Outlet Restric	tion	Orifice of Reel	ongular Orifig	)		Circula	r Outlet Pipe w/ Res	trictor Plate		•	Ë,	
(Circular Fipe w/ Restrictor Fi	ate, Circular (	Juice of Rec	angular Oninc	e)			Input Pa	rameters	_		tior	
							User	COS			tent	
<ul> <li>B) Depth to Invert of Outlet Pipe</li> </ul>	(relative to \$	Stage = 0 ft)			Pipe I	nvert Depth =	1.50	1.50	ft		Det	
C) Outlet Pipe Diameter		<b>o</b> ,			Pip	e Diameter =	30.00	27.00	inches		Ę	
<ul> <li>D) Restrictor Plate Height above</li> <li>E) Half-Central Angle of Restrict</li> </ul>	) Restrictor Plate Height above Pipe Invert ) Half-Central Angle of Restrictor Plate on Pipe				ŀ	Plate Height = Theta =	22.22	26.24	inches radians		ctr	
F) Outlet Orifice Area	Half-Central Angle of Restrictor Plate on Pipe Outlet Orifice Area					Outlet Ao =	3.90	3.94	sq ft		bed	
G) Height of Outlet Orifice Cent	Outlet Orifice Area Height of Outlet Orifice Centroid above Outlet Pipe Invert Batio of Grate Onen Area (100 vr Orifice Area (should be > 4)				Onen	Outlet <sub>centroid</sub> =	1.03	1.12	ft		s =	
H) Kallo of Grate Open Area / 1	G) Height of Outlet Orifice Centroid above Outlet Pipe Invert H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)				Open	Alea Natio =	121.39	119.97	1		Ŀ	
8. Emergency Spillway (Rectangul	ar or Trapezo	oidal)					Input Pa User	rameters COS			E C	
A) Californi Invest Change (calati		0.40					Input	DCM	14		ē	
<ul> <li>A) Spillway Invert Stage (relative</li> <li>B) Spillway Crest Length</li> </ul>	e to Stage = t	011)				L <sub>spillway crest</sub> =	5.40	4.90	ft		np	
C) Spillway End Slopes (H:V)						$S_{spilway ends} = \frac{4.00}{4.00} + \frac{4.00}{10} + \frac{4.00}$						
<ul> <li>D) Freeboard above Maximum</li> <li>E) Spillway Design Flow Depth</li> </ul>	Water Surfac	e			Freel	Depthoniture =	1.00	1.00	ft ft		Pr Pr	
F) Stage at Top of Freeboard					Freeboard	i Top Stage =	6.70	6.80	ft		uß	
G) Basin Area at Top of Freebo	ard				Max Basin Area = 1.08 1.09 acres							
9. Routed Hydrograph Results				Beer	to bood	lloor Innut					nary	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year		in.	
Inflow Hydrograph Volume (ac-ft) = Predevelopment Peak O (cfs) =	0.47 N/A	1.15 N/A		1.57 9.4				5.51			e e	
Peak Inflow (cfs) =	N/A	N/A		20.1		1		67.5			-	
Peak Outflow (cfs) =	0.2	0.3		9.4				47.1				
Structure Controlling Flow =	N/A Orifice Plate	N/A Orifice Plate		I.U Overflow Grate				1.U Outlet Pipe				
Max Velocity through Grate =	N/A	N/A		0.0				0.1				
Lime to Drain 97% of Volume (hr) =	41	69 72		73				63 74				
Maximum Ponding Depth (ft) =	3.20	4.00		4.10		1		4.80				
Area at Max Ponding Depth (ac) =	0.67	0.85		0.85				0.91				
waximum volume Stored (aC-ft) =	0.47	1.15	l	1.24	hasod on CO	S DCM Innet		60.1	1			
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year			
Inflow Hydrograph Volume (ac-ft) =	0.47	1.15		1.57				5.51				
Peak Inflow (cfs) =	N/A	N/A N/A		20.1				67.5				
Peak Outflow (cfs) =	0.2	0.3		9.4				47.1				
Ratio (Outflow/Predevelopment) = Structure Controlling Flow =	N/A Orifice Plate	N/A Orifice Plate		1.0 Overflow Grete				1.0 Outlet Dina				
Max Velocity through Grate =	N/A	N/A		0.0				0.1				
Time to Drain 97% of Volume (hr) =	41	69		73				63				
Maximum Ponding Depth (ft) =	43	4,00		/8 4,10				(4 4,80				
Area at Max Ponding Depth (ac) =	0.67	0.85		0.85				0.91				
Maximum Volume Stored (ac-ft) =	0.47	1.15		1.24				1.85				
L											-	



		Preliminary Desig	n Procedure Form: F	ull Spectrum Detention (	FSD) Routin	ng	
		COS P	CM-FSD Preliminary Desig	gn (Beta Version 1.00, Septem	nber 2019)	Sheet 1 of 3	
	STOR	MWATER	Designer Proiect	Grandview Reserve Pond G			
COLORADO	01014	ENTERPRISE	Date	April 6, 2020		Last Edited: April 13, 2020	
SPRINGS							
OLYMPIC CITY USA							
1 Select WOCV/EURV PCM Type				Extended Detention Basin (EDB)		1	
Imports the Stage-Area-Volume-Discharg	ge information fr	rom the					
must be completed before the import will	work.	sneet					
2. WQCV/EURV Outlet Details				User Input COS DCM	_		
<ul> <li>A) Average Infiltration Rate of WQCV</li> <li>B) Depth to Centroid of Underdrain Outlet (</li> </ul>	Orifice from filte	r media surface	i = v =	N/A N/A	in / hr inches		
C) Underdrain Outlet Orifice Area			Underdrain Ao =	N/A N/A	sq in		
E) Vertical Spacing between WQCV Orifice	Rows		Orifice Spacing =	4.0 4.0	inches		
<ul> <li>G) Maximum Stage of WQCV (includes ISE</li> </ul>	and Trickle Ch	hannel Depth)	Max Stage work	3.80 3.80	ft		
<ul> <li>H) EURV Orifice Area (A<sub>o</sub>) in Single Row</li> <li>I) Maximum Stage of EURV (includes ISD a</li> </ul>	and Trickle Cha	nnel Depth)	EURV Ao = Max Stage <sub>EURV</sub> =	4.73 4.73 5.00 5.00	sq in ft		
J) Discharge Coefficient for all WQCV/EUF	RV Outlet Orifice	e(s)	Cd =	<b>0.60</b> 0.60	3		
Elood Control Surcharge Basin Geometry (a	above EURV) -	See Figure				User can override default flood surcharge	
Default Flood Surcharge Geometry inputs	represent a cor	ntinuation of		Input Parameters		geometry inputs to create a transition bench	
A) Least of D				Input DCM	<b>_</b> #	Surcharge Volume by entering larger	
A) Length of Basin at Top of EURV B) Width of Basin at Top of EURV			W PCM =	408.4 468.4 141.1 141.1	ft	connerisions in C), D), and E). See the Figure to the right.	
C) Stage at Top of Transition Bench (Botton D) Length of Basin at Top of Transition Ber	m of Flood Con hch (Bottom of F	trol Surcharge) Flood Control Surcharge)	Stage at Top of Bench = L Bench =	5.10 5.10 469.2 469.2	ft ft	Bench Slope is 4H:1V in length direction	
E) Width of Basin at Top of Transition Bend E) Average Side Slopes of Elocal Control S	ch (Bottom of Fl	ood Control Surcharge)	W Bench =	<b>141.9 141.9 4 00</b>	ft ft/ft	Bench Slope is 4H:1V in width direction	
(Recommend no steeper than 3H:1V slo	ope. Use zero f	for vertical walls.)	— surchafge	4.00			
Tributary Watershed Hydrology			u				
A) Input hydrology data (conv/paste) from r	nodel runs	2 Year 5 Year	Pre-Development P	50 Year 100 Year	500 Year	1	
B) Adjust "Time Interval" to match	Time leter-	17.11	101001 2010dl	99.16	Sou real	1	
hydrograph data	5.0	minutes					
5-yr and 100-yr Hydrology Required	(min)	2 Year 5 Year	10 Year 25 Year	50 Year 100 Year	500 Year		ļ
(Other Storms are Optional)	0:00	0.00		0.00		-	
	0:10	3.42		4.91			
	0:20	29.97	1	40.46			
	0:30	46.22		147.68			
	0:35	41.85 36.79		145.92			
	0:45 0:50	32.51 28.57		134.77 122.07		1	
	0:55	24.90 21.86		110.10 99.42		1	
	1:05	19.69 17.78		85.33 73.97		4	
	1:15	15.86		63.12 53.30		1	
	1:25	12.24		44.73	1	1	
	1:35	9.00	1 1	29.80		1	
	1:40 1:45	7.68 6.80		24.16 19.99		1	
	1:50 1:55	6.25 5.79		17.20		1	
	2:00	4.96		12.77			
	2:10	3.32		8.57		1	
	2:20	2.10	1 1	5.80		1	
	2:25	1.75 1.37		4.76 3.85		1	
	2:35 2:40	1.07 0.81		3.04 2.31		1	
	2:45 2:50	0.60 0.43		1.65		4	
	2:55	0.31		0.76			
	3:05	0.17		0.34		1	
	3:10	0.12		0.23		1	
	3:20 3:25	0.07		0.12		1	
	3:30 3:35	0.05		0.07		1	
	3:40 3:45	0.03		0.05		]	
	3:50	0.02		0.03		1	
	4:00	0.01		0.02		1	
	4:05 4:10	0.01		0.01		1	
	4:15 4:20			0.00		1	
	4:25 4:30						
	4:35		1 1			1	
	4:40		1 1			1	
	4:50 4:55					1	
	5:00 5:05					1	
	5:10					1	
	5:20					1	
	5:25 5:30					1	
	5:35					J	

5:45 5:50 5:50
5:50
5:55
6:00

			Prelimin	ary Design	Procedure	e Form: Fu	III Spectrum	Detention (F	SD) Routin	g			
				COS PC	M-FSD Prelin	minary Desig	n (Beta Versio	n 1.00, Septemb	er 2019)	Sheet 2 of 3			
Designer: Chris McFarland													
	WATER RESOURCES							Project: Grandview Reserve Pond G					
COLORADO			ENC	INEERING	Date: April 6, 2020 Last Edited: April 13, 2020								
SPRINGS													
OLYMPIC CITY USA													
5. Flood Control Outlet Structure T		Overflow Weir/Grate Outlet Pine Restriction % Emergency Snillway											
A) Select Flood Control Outlet Structure Type						Overnow wenyonale, Ouder Fipe resolution of unlegency opinway							
<ol> <li>Overflow Weir (Dropbox) and Grate (Flat or Sloped) (Assumes that top of grate is flush with the top of the concrete dropbox)</li> </ol>						Input Parameters User COS							
A) Overflow Weir Front Edge Height (relative to Stage = 0.ft)						Huse foot 5 00 ft							
B) Overflow Weir Front Edge Length (inside edge of dropbox)						$L_{weir front} = \frac{0.00}{9.00} \frac{0.00}{7.00}$ ft							
C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)						Sweir sides = 0.00 0.00 ft / ft							
<ul> <li>D) Horizontal Length of Weir Sides (inside edge of droppox)</li> <li>E) Overflow Grate Open Area % (grate open area / total grate area)</li> </ul>						Open Area =	70%	7.00	%				
F) Debris Clogging %						ris Clogging =	50%	50%	%				
H) Overflow Grate Slope Length	(al Dack Side ) (inside edge	or aroppox) of dropbox)			Slo	ppe L <sub>weir sides</sub> =	9.00	7.00	ft				
I) Overflow Grate Open Area (v	vithout debris	)			Open Are	a (No Clogging) =	56.70	34.30	sq ft		Ē		
<ul> <li>J) Overflow Grate Open Area (v</li> </ul>			Open A	vrea ( <sub>Clogged</sub> ) =	28.35	17.15	sq ft		outii				
7. Outlet Pipe with Flow Restriction	Plate										SD) R		
A) Select Type of Outlet Restriction Circular Outlet Pipe w/ Restrictor Plate													
(Circular Pipe w/ Restrictor Pla	ate, Circular (	Unifice or Rect	angular Orific	e)			Input Pa	rameters			ion		
							User	COS			eut		
R) Dopth to Invert of Outlot Ding	(relative to (	Stago = 0 ft)			Dine I	nvert Depth -	Input 150	DCM 1 EO			Det		
C) Outlet Pipe Diameter	(relative to a	stage – 0 it)			Pip	e Diameter =	42.00	42.00	inches		Ξ		
D) Restrictor Plate Height above		F	Plate Height =	34.00	34.00	inches		t					
E) Hait-Central Angle of Restrictor Plate on Pipe Theta =								2.24	radians so ft		ec		
G) Height of Outlet Orifice Centr	roid above Ou	utlet Pipe Inve	rt			Outlet <sub>centroid</sub> =	1.54	1.54	ft		Š		
H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4) Open Area Ratio = 6.80 4.11											L L		
8. Emergency Spillway (Rectangula		Input Parameters											
						Input DCM							
A) Spillway Invert Stage (relativ	e to Stage = 0	0 ft)				Hspilway invert = 6.70 999.00 ft							
C) Spillway End Slopes (H:V)						$S_{\text{spillway ends}} = \frac{136.00}{4.00} \frac{27.00}{\text{ft}/\text{ft}}$							
D) Freeboard above Maximum Water Surface					Freeboard Depth= 1.00 1.00 ft						2		
E) Spillway Design Flow Depth E) Stage at Top of Freeboard					Freeboard	Deptn <sub>spillway</sub> =	0.50		ft		L L		
G) Basin Area at Top of Freeboard						Basin Area =	1.89		acres		esiç		
9. Routed Hydrograph Results											ary D		
Design Storm Return Period =	WQCV	EURV	2 Year	Resu 5 Year	ts based on 10 Year	User Input 25 Year	50 Year	100 Year	500 Year		nin		
Inflow Hydrograph Volume (ac-ft) =	1.03	2.73		3.25				11.08			reli		
Predevelopment Peak Q (cfs) =	N/A	N/A		17.1				99.2			₽.		
Peak Outflow (cfs) =	0.4	0.7		4.2				101.9					
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0					
Structure Controlling Flow = Max Velocity through Grate =	Orifice Plate N/A	Orifice Plate N/A		Overflow Grate				Outlet Pipe 1.7					
Time to Drain 97% of Volume (hr) =	39	68		73				62					
Time to Drain 99% of Volume (hr) =	41	72		77				72					
Area at Max Ponding Depth (ac) =	1.09	1.52		1.53				1.65					
Maximum Volume Stored (ac-ft) =	1.03	2.73		2.90				4.65		]			
Design Storm Return Period =	WQCV	EURV	2 Year	Results 5 Year	based on CO 10 Year	S DCM Inputs 25 Year	s 50 Year	100 Year	500 Year				
Inflow Hydrograph Volume (ac-ft) =	1.03	2.73		3.25				11.08					
Predevelopment Peak Q (cfs) =	N/A	N/A		17.1				99.2					
Peak innow (cfs) = Peak Outflow (cfs) =	0.4	0.7		40.∠ <b>3.6</b>				98.1					
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0					
Structure Controlling Flow = Max Velocity through Grate =	Orifice Plate	Orifice Plate		Overflow Grate			L	Overflow Grate					
Time to Drain 97% of Volume (hr) =	39	68		73				62					
Time to Drain 99% of Volume (hr) =	41	72		77				73					
Maximum Ponding Depth (ft) = Area at Max Ponding Depth (ac) =	3.80	5.00		5.20				6.40 1,68					
Maximum Volume Stored (ac-ft) =	1.03	2.73		3.05				4.98		1			



![](_page_143_Picture_0.jpeg)

Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix E




E

			And the second s			= -		6970			1	5		1		8 9198
GIECK RANCH I PLAN VIEW MAIN STEM #	THIS DRAWING NOT TO BE US CONSTRUCTIC STUDIES UNDE PERFORMED F	Note: See Technica		MS-R4b MS-R5	RECOMME	MS-R4b MS-R5	Reach	0 100	A	Be	238	unies shown as one environmental calego	Potentia	Ripariar	Ripariar	Environment
DBPS	S IS CONCEPTUA ED AS THE SOLE DN. OR REMEDIAL ER EPC DOT'S DII PRIOR TO SUCH (	Il Addenda for g		Chai Vegetatio	NDED PLAN	1.76 1.88	Slope (%)				IJ	of the above	al Wetlands	n Poor	1: Good	al Key
AUGUST 2007	L IN NATURE AND BASIS FOR FINA ACTION, FURTH RECTION SHOUL DECISIONS	rade control da		nnelization n Augmentat	IMPROVEME	1094 4 573 5	Q <sub>100</sub> \ (cfs) (1	2-ft cc	5-ft cc	Struct	Road	Cross	Reac	Strea	Propo Cond Flood	egend
C7706-2 PL 6D 038 33	D IS L DESIGN, HER D BE	<u></u>		<u> </u>	INTS	.24	/100 U/S)	ontours	ontours	ures on Lines	0	sections	nes	ms	osed Future itions 100-yr Limits	





<u>s</u>			<u>\</u>	<u> </u>		
GIECK RANCH DBPS PLAN VIEW AIN STEM TRIBUTARY-2 #2	Note: See Technical Addenda for THIS DRAWING IS CONCEPT NOT TO BE USED AS THE SC CONSTRUCTION, OR REMEI STUDIES UNDER EPC DOT'S PERFORMED PRIOR TO SUC	RECOMMENDED PLA Reach MST2-R2 Vegeta	Reach Slope (%) MST2-R2 1.93	0 100 200 Feet	Riparian: Poor Potential Wetlands The channel is considered dry unless shown as one of the above environmental categories.	Environmental Key Ponds Riparian: Good
AUGUST 2007	r grade control da UNAL IN NATURE A DIAL ACTION, FUR DIAL ACTION, FUR DIAL ACTION, FUR H DECISIONS,	IN IMPROVEN	Q <sub>100</sub> (cfs) 271	Stru 5-ft 2-ft	Rep Cro	
лана С7706-2 РІ. 6D 038 48	LD BE SIGN,	ALION	V <sub>100</sub> (fVs) 3.16	ads ictures tion Lines contours contours	earms aches ach Breaklines ss-sections	d posed Future nditions 100-yr od Limits





GIECH EAST FO	TESSET	<u> </u>	<u> </u>	<u>а</u> п	<u>,                                     </u>	The cha unless s environr	R S	Envir
K RANCH E PLAN VIEW RK TRIBU	IIS DRAWING DT TO BE USI NSTRUCTIO UDIES UNDE RFORMED P		ECOMMEI each -T1-R2a -T1-R2b	Reach -T1-R2a -T1-R2b		nnel is consid hown as one mantal calego	Riparian Potentia	Ponds Riparian
)BPS TARY #3	FIS CONCEPT ED AS THE SC N, OR REME R EPC DOTS R EPC DOTS		NDED PL/ As-nee As-nee	Slope (%) 1.83 1.60	H Feet	ered dry of the above ries.	l: Poor I Wetlands	al Key :: Good
AUGUS	TUAL IN NATI TUAL IN NATI DIAE BASIS F DIAL ACTION CH DECISION		AN IMPRC ded Impr ded Impr	Q <sub>100</sub> (cfs) 217 217	$\langle 0 \rangle$			Leg
T 2007 C77	L, FURTHER SHOULD BE IS.		)VEMENT: ovements ovements	V <sub>100</sub> (ft/s) 2.68	Structures Section Li 5-ft contou 2-ft contou	Reach Bre Cross-sec Roads	Streams Reaches	<b>Proposed</b> Condition. Flood Lim
038 89	SIGN		0			tions		Future s 100-yr its





Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Jan 25 2019

### East Fork Tributary 1 Reach 3 - Proposed Channel\_Capacity

Trapezoidal		Highlighted	
Bottom Width (ft)	= 25.00	Depth (ft)	= 1.75
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 217.00
Total Depth (ft)	= 3.00	Area (sqft)	= 56.00
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.88
Slope (%)	= 0.69	Wetted Perim (ft)	= 39.43
N-Value	= 0.040	Crit Depth, Yc (ft)	= 1.24
		Top Width (ft)	= 39.00
Calculations		EGL (ft)	= 1.98
Compute by:	Known Q		
Known Q (cfs)	= 217.00		



Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Jan 25 2019

### East Fork Tributary 1 Reach 3 - Proposed Channel\_Velocity

Trapezoidal		Highlighted	
Bottom Width (ft)	= 25.00	Depth (ft)	= 1.49
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 217.00
Total Depth (ft)	= 3.00	Area (sqft)	= 46.13
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 4.70
Slope (%)	= 0.69	Wetted Perim (ft)	= 37.29
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.24
		Top Width (ft)	= 36.92
Calculations		EGL (ft)	= 1.83
Compute by:	Known Q		
Known Q (cfs)	= 217.00		



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Jan 18 2019

### East Fork Tributary 1 Reach 2 - Proposed Channel\_Capacity

Trapezoidal		Highlighted	
Bottom Width (ft)	= 38.00	Depth (ft)	= 1.12
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 177.00
Total Depth (ft)	= 2.00	Area (sqft)	= 47.58
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.72
Slope (%)	= 1.58	Wetted Perim (ft)	= 47.24
N-Value	= 0.050	Crit Depth, Yc (ft)	= 0.86
		Top Width (ft)	= 46.96
Calculations		EGL (ft)	= 1.34
Compute by:	Known Q		
Known Q (cfs)	= 177.00		



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Jan 18 2019

### East Fork Tributary 1 Reach 2 - Proposed Channel\_Velocity

Trapezoidal		Highlighted	
Bottom Width (ft)	= 38.00	Depth (ft)	= 0.86
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 177.00
Total Depth (ft)	= 2.00	Area (sqft)	= 35.64
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 4.97
Slope (%)	= 1.58	Wetted Perim (ft)	= 45.09
N-Value	= 0.032	Crit Depth, Yc (ft)	= 0.86
		Top Width (ft)	= 44.88
Calculations		EGL (ft)	= 1.24
Compute by:	Known Q		
Known Q (cfs)	= 177.00		



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Main Stem Trib 2

### Gieck Manch Hubble 2 - Proposed Channel Section Capacity Check

Trapezoidal		Highlighted	
Bottom Width (ft)	= 60.00	Depth (ft)	= 0.92
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 220.00
Total Depth (ft)	= 2.00	Area (sqft)	= 58.59
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.76
Slope (%)	= 2.00	Wetted Perim (ft)	= 67.59
N-Value	= 0.050	Crit Depth, Yc (ft)	= 0.74
		Top Width (ft)	= 67.36
Calculations		EGL (ft)	= 1.14
Compute by:	Known Q		
Known Q (cfs)	= 220.00		



Compute by:

Known Q (cfs)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Known Q

= 220.00

Main Stem Trib 2

### Gieck Ranch Hubblery 2 - Proposed Channel Section Velocity Check

Trapezoidal	
Bottom Width (ft)	= 60.00
Side Slopes (z:1)	= 4.00, 4.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.00
N-Value	= 0.032
Calculations	

Highlighted	
Depth (ft)	= 0.70
Q (cfs)	= 220.00
Area (sqft)	= 43.96
Velocity (ft/s)	= 5.00
Wetted Perim (ft)	= 65.77
Crit Depth, Yc (ft)	= 0.74
Top Width (ft)	= 65.60
EGL (ft)	= 1.09



#### Gieck Ranch Tributary 2\_Reach 1 - Proposed Channel Section Capacity Check

	Main Stem		
Trapezoidal		Highlighted	
Bottom Width (ft)	= 60.00	Depth (ft)	= 0.92
Side Slopes (z:1)	= 4.00, 4	.00 Q (cfs)	= 220.00
Total Depth (ft)	= 2.00	Area (sqft)	= 58.59
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.76
Slope (%)	= 2.00	Wetted Perim (ft	) = 67.59
N-Value	= 0.050	Crit Depth, Yc (ft	:) = 0.74
		Top Width (ft)	= 67.36
Calculations		EGL (ft)	= 1.14
Compute by:	Known Q		
Known Q (cfs)	= 220.00		



### Gieck Ranch Tributary 2 Reach 1 - Proposed Channel Section Velocity Check

	Main Stem		
Trapezoidal		Highlighted	
Bottom Width (ft)	= 60.00	Depth (ft)	= 0.70
Side Slopes (z:1)	= 4.00, 4.0	0 Q (cfs)	= 220.00
Total Depth (ft)	= 2.00	Area (sqft)	= 43.96
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 5.00
Slope (%)	= 2.00	Wetted Perim (ft)	= 65.77
N-Value	= 0.032	Crit Depth, Yc (ft)	= 0.74
		Top Width (ft)	= 65.60
Calculations		EGL (ft)	= 1.09
Compute by:	Known Q		
Known Q (cfs)	= 220.00		



#### Gieck Ranch Tributary 2 Reach 2 - Proposed Channel Section Capacity Check

	Main Stem			
Trapezoidal			Highlighted	
Bottom Width (ft)	= 60.00		Depth (ft)	= 0.99
Side Slopes (z:1)	= 4.00, 4	.00	Q (cfs)	= 237.00
Total Depth (ft)	= 2.00		Area (sqft)	= 63.32
Invert Elev (ft)	= 1.00		Velocity (ft/s)	= 3.74
Slope (%)	= 1.80		Wetted Perim (ft)	= 68.16
N-Value	= 0.050		Crit Depth, Yc (ft)	= 0.78
			Top Width (ft)	= 67.92
Calculations			EGL (ft)	= 1.21
Compute by:	Known Q			
Known Q (cfs)	= 237.00			



### Gieck Ranch Tributary 2\_Reach 2 - Proposed Channel Section Velocity Check

Trapezoidal	Main Stem	Highlighte	d
Bottom Width (f	i) = 60.00	Depth (ft)	= 0.76
Side Slopes (z:1	) = 4.00, 4	4.00 Q (cfs)	= 237.00
Total Depth (ft)	= 2.00	Area (sqft)	= 47.91
Invert Elev (ft)	= 1.00	Velocity (ft/	(s) = 4.95
Slope (%)	= 1.80	Wetted Per	rim (ft) = 66.27
N-Value	= 0.032	Crit Depth,	Yc (ft) $= 0.78$
		Top Width	(ft) $= 66.08$
Calculations		EGL (ft)	= 1.14
Compute by:	Known C	2	
Known Q (cfs)	= 237.00	0	



Reach (ft)







Grandview Reserve Master Development Drainage Plan Project No.: 191897.01

Appendix F



Basin	Design Point	5 Year Pre Devlopment	100 Year Pre Development
A1	10	13.03	66.80
B1	20	4.33	48.76
B2	21	1.66	20.74
	22	11.85	140.35
	23	5.99	68.56
B3	24	21.23	249.20
C1	30	9.95	110.70
	31	9.95	110.70
D1	40	8.12	40.00
D2	41	22.23	114.87
	42	8.12	40.00
E1	50	32.34	157.99
	51	93.34	374.99
F1	60	9.70	49.45
F2	61	16.46	86.73
F3	62	3.65	18.42
F4	63	12.98	67.82
	64	13.35	67.87
	65	26.04	135.62

	66	16.46	86.73
	67	231.47	864.52
G1	70	5.57	28.46
G2	71	3.87	20.06
	72	3.87	20.06
	73	3.87	20.06
	74	189.42	643.48
H1	80	1.85	21.89
H2	81	5.37	27.12
H3	82	1.92	9.51
H4	83	8.07	40.86
	84	7.22	49.01
	85	1.92	9.51
OS1	OS1	67.00	413.00
OS2	OS2	59.00	280.00
OS3	OS3	61.00	217.00
OS4	OS4	180.00	595.00
	Outfall1	80.03	479.80
	Outfall2	85.96	597.41
	Outfall3	30.00	154.35
	Outfall4	341.05	1335.77

FIG.EX1

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Basin	Design Point	5 Year Pre Devlopment	5 Year Post Development	100 Year Pre Development	100 Year Post Development
A1	10	13.03	30.72	66.80	100.64
B1	20	4.33	29.46	48.76	97.08
B2	21	1.66	12.02	20.74	42.26
	22	11.85	92.76	140.35	295.27
	23	5.99	40.92	68.56	136.17
B3	24	21.23	93.26	249.20	334.84
C1	30	9.95	77.99	110.70	238.03
	31	9.95	1.52	110.70	115.75
D1	40	8.12	24.15	40.00	70.07
D2	41	22.23	98.47	114.87	252.18
	42	8.12	24.15	40.00	70.07
E1	50	32.34	46.88	157.99	178.04
	51	93.34	85.04	374.99	381.75
F1	60	9.70	16.28	49.45	58.95
F2	61	16.46	60.11	86.73	170.90
F3	62	3.65	11.36	18.42	32.93
F4	63	12.98	42.32	67.82	124.89
	64	13.35	26.88	67.87	90.88
	65	26.04	69.12	135.62	215.63
	66	16.46	60.11	86.73	170.90

	67	231.47
G1	70	5.57
G2	71	3.87
	72	3.87
	73	3.87
	74	189.42
H1	80	1.85
H2	81	5.37
H3	82	1.92
H4	83	8.07
	84	7.22
	85	1.92
OS1	OS1	67.00
OS2	OS2	59.00
OS3	OS3	61.00
OS4	OS4	180.00
	Outfall1	80.03
	Outfall2	85.96
	Outfall3	30.00
	Outfall4	341.05

\*THIS VALUE IS HIGHER THAN PRE-EXISTING AND WILL BE ADJUSTED TO MEET CRITERIA WITH THE PRELIMINARY DRAINAGE REPORT

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Job No.:	191897.01
Prepared By:	TBI
Date:	04/14/2020





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	EXISTING STORM DRAIN PIPE
	PROPOSED DRAINAGE CHANNEL
	PROPERTY LINE
	DIRECTIONAL FLOW ARROW
	EMERGENCY OVERFLOW ARROW
	EXISTING 100-YR FLOODWAY
	EXISTING 100-YR FLOODPLAIN
	WATERSHED BOUNDARY
	MAJOR BASIN LINE
	PROPOSED DETENTION LOCATION
	POTENTIAL WATER QUALITY LOCATION
	SWMM CONVEYANCE ELEMENT SWMM PROPOSED PEAK FLOW RATE (CFS) (850)
	DESIGN POINT
	PROPOSED BASIN LABEL
	AREA (AC.) XX XX % IMPERVIOUSNESS
	LAND_USE LOW DENSITY
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	COMMUNITY PARK
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PROPOSED DR	AINAGE CHANNEL
PROPOSED RC	
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EXISTING 100-	-YR FLOODPLAIN
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SWMM CONVE	YANCE FLEMENT SWMM
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Date: 04/14/2020	