## FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

## **EL PASO COUNTY, COLORADO**

July 2019

Prepared for: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903 **Engineering Review** 

**Development Department** 

Prepared by:



Project #09-007 SF -19-004

Note: Full project review requires the Sand Creek Channel Design Report to be completed and accepted prior to an adjacent development's drainage report full review.

## FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

#### DRAINAGE PLAN STATEMENTS

#### **ENGINEERS STATEMENT**

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

on my part in prepar	ring this report.
Virgil A. Sanchez, P For and on Behalf o	.E. #37160 f M&S Civil Consultants, Inc
DEVELOPER'S ST	ATEMENT
I, the developer have and plan.	e read and will comply with all the requirements specified in this drainage report
BY:James	s F Morley
DATE:	
ADDRESS:	SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903
EL PASO COUNTY	<u>/'S STATEMENT</u>
	with the requirements of El Paso County Land Development Code, Drainage lumes 1 and 2, and the Engineering Criteria Manual, as amended.
BY:	DATE:
Jenni	DATE:  Per Irvine, P.E.
	ty Engineer / ECM Administrator

## FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

#### TABLE OF CONTENTS

PURPOSE	4
GENERAL LOCATION AND DESCRIPTION	4
SOILS	4
HYDROLOGIC CALCULATIONS	4
HYDRAULIC CALCULATIONS	5
FLOODPLAIN STATEMENT	5
DRAINAGE CRITERIA	5
FOUR STEP PROCESS	5
EXISTING DRAINAGE CONDITIONS	6
PROPOSED DRAINAGE CHARACTERISTICS	6
CHANNEL IMPROVEMENTS	8
WATER QUALITY PROVISIONS	9
EROSION CONTROL	9
CONSTRUCTION COST OPINION	10
DRAINAGE & BRIDGE FEES	11
STERLING RANCH FIL. NO.1 - SIA	11
SUMMARY	12
REFERENCES	13

#### **APPENDIX**

Vicinity Map Soils Map FIRM Panel W/ Revised LOMR Hydrologic Calculations Hydraulic Calculations Drainage Maps 3

## FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

#### **PURPOSE**

This document is the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. This report was previously discussed, as a preliminary drainage report, in the "Master Development Drainage Report for Sterling Ranch Filing No. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The following report is an analysis of the drainage for Homestead at Sterling Ranch Filing No. 2, single family lots, onsite and offsite drainage.

#### GENERAL LOCATION AND DESCRIPTION

Homestead at Sterling Ranch Filing No. 2 is located in the SE ¼ of the NW ¼, the SW ¼ of the NE ¼, and the NW ¼ of the NE ¼ of Section 33, Township 12 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, and the NE ¼ of the SW ¼ of Section 33, Township 12 South, Range 65 West of the 6<sup>th</sup> Principal Meridian within unincorporated El Paso County, Colorado. The site is bound on the south by an existing detention pond, to the north by Briargate Parkway and to the east by Sand Creek. Existing Dines Boulevard runs along the western site boundary. An existing residential development, Homestead at Sterling Ranch Filing No. 1, bounds the site to the west and a future commercial parcel bounds the site to the northwest. Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Homestead at Sterling Ranch Filing No. 2 consists of 29.658 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to southwest at grade rates that vary between 2% and 6%.

Land use for Homestead at Sterling Ranch Filing No. 2 is currently listed as AG (Grazing Land). Improvements proposed for the site include paved streets, trails, a full spectrum detention pond, and utilities as normally constructed for a residential development.

#### **SOILS**

Soils for this project are delineated by the map in the appendix as Pring Coarse Sandy Loam (71) and is characterized as Hydrologic Soil Types "B". Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". Vegetation is sparse, consisting of native grasses and weeds.

#### HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

#### HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets can be found in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 and in the appendix of this report.

#### FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0533 G, effective date December 7, 2018. An annotated FIRM Panel is included in the Appendix.

#### **DRAINAGE CRITERIA**

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the ECM, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method.

#### **FOUR STEP PROCESS**

Add July 2019 ECM Update for MS4 permit.

**Step 1 Employ Runoff Reduction Practices**. Roof drains will be directed to side yard swales and as possible to grass lined swales to aid in minimizing direct connection of impervious surfaces.

- Step 2 Implement BMPs that provide a water quality capture volume with slow release. An existing Full Spectrum Detention Facility (see Sterling Ranch Filing Nos. 1&2 MDDP, Pond 4) was planned and constructed to handle tributary flows for the southwest portion of the site. All remaining tributary areas from the site will be treated in a proposed temporary Full Spectrum Detention Facility, Interim Pond 1. Both ponds will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours.
- **Step 3 Stabilize streams.** With the full spectrum detention facilities in place, the runoff from the proposed residential development will be reduced to predevelopment conditions. The developed discharge from the site is less that existing and therefore is not anticipated to have negative effects on downstream drainageways. Additionally, the Sand Creek Channel will be reinforced with selected areas of rip rap bank protection, vegetative slope stabilization, check structures and drop structures.
- **Step 4** Consider need for Industrial and Commercial BMPs. No industrial or commercial land uses are proposed with this development. The proposed residential development area will implement a Stormwater Management Plan (SWMP) incorporation proper housekeeping procedures. Onsite drainage will be routed through proposed private temporary Full Spectrum Detention Facility (FSD), Interim Pond 1, to minimize introduction of contaminates to the county's public drainage systems.

#### **EXISTING DRAINAGE CONDITIONS**

The Homestead at Sterling Ranch Filing No. 2 site consists of 29.658 acres and is situated west of the Sand Creek Watershed. This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 (henceforth referred to as "Sterling Ranch Filing Nos. 1&2 MDDP"). Homestead at Sterling Ranch Filing No. 2 and the surrounding areas, with the exception of the existing Barbarick Subdivision; have already been graded during the overlot of the subdivision. Please refer to the Sterling Ranch Filing Nos. 1&2 MDDP by MS Civil Consultants for information on historic conditions and overlot drainage patterns. A copy of the existing conditions map has been provided in the appendix.

#### PROPOSED DRAINAGE CHARACTERISTICS

#### **General Concept Drainage Discussion**

The following is a description of the onsite basins, offsite bypass flows and the overall drainage characteristics for the development of Sterling Ranch Filing No. 2. The development of Sterling Ranch Filing No. 2 consists of residential streets and cul-de-sacs, proposed storm drainage improvements, and lots located within the filing boundary. The proposed development results in drainage patterns and flow values that are the same or less than those in the Sterling Ranch Filing Nos. 1&2 MDDP. Surface flow is designated as Design Points (DP). The following DPs and Basins were determined using the Rational Method since this method offers a more conservative approach to drainage. It should be noted that all calculations and drainage basins have been revised to reflect the new criteria updates by the El Paso County/City of Colorado Springs Drainage Criteria Manual. For comparison, the asterisk (\*) symbol in the detailed drainage discussions below represents each Basin or Design Point as labeled in the Sterling Ranch Filing Nos. 1&2 MDDP. Asterisk symbols on the Proposed Drainage Map in the appendix also represent Basins, Design Points and Pipe Runs as presented in the Sterling Ranch Filing Nos. 1&2 MDDP.

#### **Detailed Drainage Discussion (Design Points)**

**DP2\***, 5.39 acres, consists of Basin B\* planned residential lots and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=8.0 cfs and Q100=19.3 cfs has been calculated for DP2\*. The surface runoff is routed via overlot grading and planned swales to two existing 15' CDOT Type R at-grade inlets. The flows are routed east via a 36" RCP to DP5.

**DP3\***, 2.92 acres, consists of Basin C\* residential lots within Homestead at Sterling Ranch Filing No. 1, and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.2 cfs and Q100=10.1 cfs has been calculated for DP3\*. The surface runoff is routed via overlot grading and proposed swales to an existing 5' CDOT type R sump inlet. The flows captured by the inlet are routed to existing Detention Pond 4.

**DP4\***, 9.36 acres, consists of Basin D\* and Basin E\* residential lots within Homestead at Sterling Ranch Filing No. 1 and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and Basin F\* (Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=16.1 cfs and Q100=36.7 cfs has been calculated for DP4. The surface runoff is routed via overlot grading and curb and gutter to DP4\* which will be collected by a 15' CDOT type R at-grade inlet. The intercepted flow (Q5=13.3 cfs and Q100=20.0 cfs) will combine with flows from DP3\* and be routed east via a 30" RCP (PR6\*, Q5=16.8 cfs and Q100=29.4 cfs) to existing Detention Pond 4.

**DP5\***, 0.80 acres, consists of Basin G\* residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Basin H\* existing Dines Boulevard, with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year and flowby from Sterling Ranch Filing Nos. 1&2 MDDP DP4\*. Developed runoff of Q5=4.2 and Q100=19.7 cfs has been calculated for DP5\*. The surface runoff is routed via overlot grading and curb and gutter to DP5\* which is collected by an existing 15' CDOT type R at-grade inlet. DP5\* has an intercepted flow of (Q5=4.2 cfs and Q100=14.7 cfs) and of flowby of (Q5=0.0 cfs and Q100=5.0 cfs). Flowby from DP5\* continues on to Pond FSD13, east of Dines Boulevard. See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

**DP6\***, 4.68 acres, consists of Sterling Ranch Filing Nos. 1&2 MDDP Basins J\* and K\* planned residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Sterling Ranch Filing Nos. 1&2 MDDP Basin I\* (Wheatland Drive) and Basin L\* (Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=14.1 cfs and Q100=26.7cfs has been calculated for DP6\*. The surface runoff is routed via overlot grading and curb and gutter to DP6\* which is collected by an existing 15' CDOT type R at-grade inlet. DP6\* has an intercepted flow of (Q5=12.1 cfs and Q100=17.2 cfs) and of flowby of (Q5=2.0 cfs and Q100=9.5 cfs). Flowby from DP6\* continues on to Pond FSD13, east of Dines Boulevard. See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

**DP7**, 4.42 acres, consists of Basin P proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=5.7 and Q100=13.8 cfs has been calculated for DP7. Surface runoff is routed via overlot grading and curb and gutter to DP7 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer. The flows from DP7 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

**DP8**, 3.78, acres, consists of Basin Q proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.9 and Q100=11.8 cfs has been calculated for DP8. Surface runoff is routed via overlot grading and curb and gutter to DP8 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer. The flows from DP8 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

**DP9**, acres, consists of Basin R proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=2.2 and Q100=5.4 cfs has been calculated for DP9. Surface runoff is routed via overlot grading and curb and gutter to DP9 which is collected by a proposed 5' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet combine with captured flows contributed from Design Points 7 & 8 and are routed to existing Detention Pond 4 by Pipe Run 4 (Q5=12.4 and Q100=30.1 cfs). Pipe Run 4 connects to existing Sterling Ranch Filing Nos. 1&2 MDDP Pipe Run 10\* (Q5=12.5 and Q100=30.4 cfs) and is discharged into the forebay of existing Detention Pond 4. Flows contributed to the forebay of existing Pond 4 are approximately equal to those anticipated by the MDDP, therefore Pond 4 has the capacity for SWQ and Full Spectrum Detention for these flows.

**DP10,** 9.14, acres, consists of Basin T proposed residential lots with runoff coefficients of 0.30 for the 5-year and 0.50 for the 100-year. Developed runoff of Q5=9.4 and Q100=15.6 cfs has been calculated for DP10. Surface runoff is routed via overlot grading and curb and gutter to DP10 which is collected by a proposed 15' CDOT type R at-grade inlet. DP10 has an intercepted flow of (Q5=9.1 cfs and Q100=12.7 cfs) and of flowby of (Q5=0.3 cfs and Q100=2.9 cfs). Flows captured by the proposed 15' CDOT type R at-grade inlet are routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

**DP11,** 1.48, acres, consists of Basin V1 proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=1.9 and Q100=15.6 cfs has been calculated for

DP11. Surface runoff is routed via overlot grading and curb and gutter to DP11 which is collected by a proposed 15' CDOT type R at-grade inlet. DP11 has an intercepted flow of (Q5=1.9 cfs and Q100=12.7 cfs) and of flowby of (Q5=0.0 cfs and Q100=2.9 cfs). Flows captured by the proposed 15' CDOT type R at-grade inlet are routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

**DP12**, 4.50, acres, consists of Basin U proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and flowby from DP10. Developed runoff of Q5=6.2 cfs and Q100=17.2 cfs has been calculated for DP12. Surface runoff is routed via overlot grading and curb and gutter to DP12 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

**DP13**, 0.83, acres, consists of Basin V2 proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and flowby from DP11. Developed runoff of Q5=1.2 and Q100=5.9 cfs has been calculated for DP13. Surface runoff is routed via overlot grading and curb and gutter to DP13 which is collected by a proposed modified 5' length by 4.5' wide CDOT type R sump inlet.

**DP14**, 0.56, acres, consists of Basin W1 proposed full spectrum detention Pond 1 with runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and contributed flow from pipe run 9. Developed runoff of Q5=19.6 cfs and Q100=52.4 cfs has been calculated for DP14. All flows captured by inlets at Design Points DP10, DP11, DP12 and DP13 are routed by Pipe Run 9 (PR9, Q5=17.9 and Q100=47.1 cfs) to the forebay in Pond 1 and combine with surface runoff within Basin W1. An outlet structure with an orifice plate and restrictor plate regulates release rates and provides treatment to all flows tributary to DP14. See the Water Quality Provisions discussion in this report for more information on Pond 1.

Basins labeled on the Proposed Drainage Map marked with a "\*", were previously analyzed and shown in the Final Drainage report for Sterling Ranch Filing No. 1. These basins are; B\*, C\*, D\*, E\*, F\*, G\*, H\*, I\*, L\*, &S\*. They are shown on the Proposed Drainage Map for continuity. Basins K & J additionally contribute to Design Points 3, 4, 5 &6. Therefore, the inlets sizing at these design points has been verified.

#### **Detailed Drainage Discussion (Drainage Basins)**

**Basins X1, X2, W1, and Y1** (0.78, 1.04, 0.86 and 0.084 acres respectively), consists of proposed residential backyard lots located along the eastern boundary of the site with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year. Developed runoff of (Q5=0.8, 1.1, 0.2, and 0.8 cfs and Q100=2.8, 3.7, 1.7, and 3.0 cfs respectively has been calculated for the basins. Runoff produced within the residential backyard lots, of Basins X1, X2, W1 and Y1 will be conveyed in backyard swales and as sheet flow to a Sand Filter Basin within each lot. The <u>treated</u> flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. A 20' wide typical drainage easement is provided within the lots to accommodate the BMP's. The facilities constructed are to be privately maintained.

**Basins X, W2, and Y** (0.22, 0.26, and 0.09 acres respectively), consists primarily of vegetated tracts and portion of residential backyards that will discharge as sheet flow to the Sand Creek Channel. The developed flow rates from Basins X, W2, and Y are Q5=0.2, 0.1, 0.1 cfs and Q100=0.8, 0.8, and 0.3 respectively. The total combined developed area being discharge to the channel is less than one acre.

#### **CHANNEL IMPROVEMENTS**

Slope grading and intermittent channel bank lining has been proposed for portions of the developable areas adjacent to Sand Creek to protect the developed lots and prevent excessive erosion until the DBPS recommended Sand Creek Channel improvements are installed. The proposed slope grading is intended to reduce outer bank grades and bring uniformity to areas where significant riling and destabilization has

8

SR metro district

State that it's not practicable to provide WQCV for these areas if that is the case.

occurred. Proposed channel stabilization improvements includes placement of soil riprap and turf reinforcement matting along embankment toes and along embankment slopes, both of which will function to retain soils and vegetation during heavy rains or larger flood flow events. All disturbed areas, not hardscaped will be re-vegetated with native species grasses, per El Paso County erosion control standards. Storm sewer outfalls into Sand Creek shall be protected by low-tailwater riprap basins. The outfall protection is shown on the accompanying drainage map in the appendix. Refer to the Homestead Filing No.2 Grading and Erosion Control Plans for riprap and turf reinforcement map placement and construction details.

Permanently installed check structures and rip-rap channel lining will be installed within Sand Creek Channel to handle the runoff from fully developed Sterling Ranch and up-gradient watershed in accordance with the Sand Creek DBPS. A discussion regarding the timing of these channel improvements is provided in a subsequent paragraph titled Sterling Ranch Filing No. 1 Subdivision Improvement agreement which follows the Construction Costs segment of this report. Financial Assurance shall be posted for the proposed Sand Creek Channel Improvements and Bank Stabilization (Slope Protection)

#### WATER QUALITY PROVISIONS

The proposed Full Spectrum Detention Facility, Pond 1 functions to provide detention storage and water quality facility for runoff produced onsite from tributary Basins T, U, V1, V2 and W1. This water quality facility is designed to treat 0.245 ac-ft of water quality storage (WQCV), 0.741 ac-feet of excess urban runoff volume (EURV) and 1.331 ac-ft of 100-year storage. A rolled erosion control blanketed emergency spillway, concrete forebay, trickle channel and outlet structure, and gravel maintenance access road has been designed for Pond 1.

A 24" RCP pipe extending from the proposed modified 6'x2.9' CDOT Type D sump inlet (see Design Point 13) will convey discharge from the pond to Sand Creek. . Runoff discharged to Sand Creek is anticipated to reach peak flow rates of Q5=0.7 cfs and Q100=23.4 cfs. A soil riprap stilling basin has been provided at the termination of the pipe to arrest erosion.

The WQCV and EURV required for the site has been determined using the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II. Refer to the water quality facility sizing calculations located within the appendix of this report (see UD-Detention Worksheet in appendix).

As previously discussed, refer to Sterling Ranch Filing Nos. 1&2 MDDP for additional information regarding existing FSD Pond 4.

#### **EROSION CONTROL**

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved "Early Grading Plan for Sterling Ranch Phase I <u>Onsite</u> Grading & Erosion Control", November 18, 2015. And "Early Grading Plan for Sterling Ranch Phase I <u>Offsite</u> Grading & Erosion Control", December 3, 2015. Grading and Erosion control operations are currently underway (July 2019). Grading and Erosion Control will cease with the final development of the site in the next 6-12 months.

#### CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FIL. NO. 2

#### **Drainage Facilities:**

Drainage improvements are planned with the development of Homestead at Sterling Ranch Filing No. 2. A majority of the construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing No. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Any additional improvements and costs are listed below.

The following list of drainage improvements are **Non-Reimbursable**. The Reimbursable facilities are outlined in the Sterling Ranch Filing No. 1 Final Drainage Report and Sterling Ranch MDDP. Refer to the MDDP for Sterling Ranch Cost and Fee Analysis Report (February 2019).

Item	Description	Quar	tity	Unit C	ost	Cost
1.	18" RCP	31	LF	\$40	/LF	\$1,240.00
2.	24" RCP	127	LF	\$50	/LF	\$6,350.00
3.	30" RCP	998	LF	\$85	/LF	\$84,830.00
4.	36" RCP	8	LF	\$105	/LF	\$840.00
5.	42" RCP	699	LF	\$185	/LF	\$129,315.00
6.	24" FES	1	EA	\$750	/EA	\$750.00
8.	42" FES	1	EA	\$1,250	/EA	\$1,250.00
9.	5.0'x4.5' CDOT Type R Sump Inlet	1	EA	\$4,000	/EA	\$4,000.00
10.	10' CDOT Type R Sump Inlet	4	EA	\$4,700	/EA	\$18,800.00
11.	15' CDOT Type R At-Grade Inlet	2	EA	\$6,000	/EA	\$12,000.00
12.	4.0' Type II MH	1	EA	\$3,500	/EA	\$3,500.00
13.	5.0' Type II MH	2	EA	\$4,000	/EA	\$8,000.00
14.	6.0' Type II MH	1	EA	\$4,500	/EA	\$4,500.00
17.	5.0'x6.0' MH	2	EA	\$6,500	/EA	\$13,000.00
18.	5.5'x5.5' MH	1	EA	\$6,500	/EA	\$6,500.00
19.	Headwall/Wingwall	1	EA	\$6,000	/EA	\$6,000.00
20.	Full Spectrum Det. Pond 1	1	EA	\$15,000	/EA	\$15,000.00
21.	FSD Pond 1 Outlet Structure	1	EA	\$12,600	/EA	\$12,600.00
22.	Ind. Lot Sand Filter Basins w/6" Pipe	26	EA	\$2,000	/EA	\$52,000.00
23	18" Drain Basin Manholes w/Lids	27	EA	\$1,000	/EA	27,000.00
24	12" ADS Pipe	1,658		\$26	/LF	43,108.00

Total \$ \$450,583.00

The following list of drainage improvements are **Reimbursable** for the improvements to the Sand Creek Channel adjacent to Homestead at Sterling Ranch Filing No.2.

#### **Sand Creek Channel Improvements**

Item	Description	Quar	ıtity	Unit C	ost		Cost
1.	Rip Rap Protection	1,100	Ton	\$80	/Ton		\$88,000.00
2.	Drop/Check Structures	5	EA	\$50,000	/EA		\$250,000.00
3.	Slope Stabilization Blankets	5,698	SY	\$6	/SY	_	\$34,188.00
						Total	\$372,188.00

#### DRAINAGE & BRIDGE FEES - HOMESTEAD AT STERLING RANCH FIL. NO. 2

This site is within the Sand Creek Drainage Basin. The 2019 Drainage and Bridge Fees per El Paso County for the HOMESTEAD AT STERLING RANCH FILING NO. 2 site are as follows:

Per Homestead at Sterling Ranch Filing No. 2 Plat – **Total Area** 29.658 Acres

**HOMESTEAD AT STERLING RANCH FILING NO. 2 FEES:** 

 Drainage Fees:
 29.658 x
 46% \$
 18,940.00 =
 \$ 258,392.36

 Bridge Fees:
 29.658 x
 46% \$
 5,559.00 =
 \$ 75,839.66

Total \$ 334,232.02

#### STERLING RANCH FILING NO. 1 - SUBDIVISION IMPROVEMENTS AGREEEMENT

Sterling Ranch Filing No. 1 final plat and SIA has been recorded, and addressed the following drainage improvements Not located/and located in the Sand Creek Channel. The following SIA paragraphs outlined drainage for Sterling Ranch in the following manner;

2. Drainage and Landscaping Tracts: Improvements on Tracts A, B, F, H, I, J, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z, AA and CC as identified on the final plat of Filing No. 1 will be completed to the satisfaction of the County and District and, upon said completion, the improvements will be dedicated to and accepted by the District. Improvements on Tract D (Sand Creek) will be completed to the satisfaction of the County and upon said completion; the improvements will be dedicated to and accepted by the County. The ownership and maintenance of storm drain facilities and structures not located on the foregoing tracts shall be determined as follows. All storm pipes shall be owned and maintained by the District except where located in County road rights of way (see Paragraph 5 below), in which case the County shall own and maintain the storm drain facilities and structures, including but not limited to, inlets and manholes. A typical cross section describing the ownership and maintenance responsibilities of drainage improvements within County rights of way is attached as Exhibit C hereto.

#### 7. Timing of Construction and Acceptance:

- a. **Drainage Improvements Not Located in Sand Creek Channel**: Except as set forth below in subsection 6.b. (drainage improvements located in Sand Creek Channel), all drainage improvements described in Exhibit A and constructed within the Drainage and Landscaping Tracts identified in paragraph 2 above shall be completed by the Subdivider and District, meeting all applicable standards for preliminary acceptance, prior to the recording of the first replat of Tracts C, E, G, K or BB. In the event that a portion of the drainage improvements are not completed prior to the recording of the first replat, then prior to such recording collaterial sufficient in the opinion of the County to assure completion of the improvements must be posted by the Subdivider and a deadline by which such drainage improvements shall be completed shall be established by written agreement.
- b. **Drainage Improvements Located in Sand Creek Channel (Tract D):** The District agrees that it will construct or cause the construction of all drainage improvements to be located in Tract D as well as future tracts within Sterling Ranch containing the Sand Creek Channel in accordance with the following:
- i. Bank stabilization of the Sand Creek channel shall be required prior to any replats or other final plats adjacent to the channel. The design and installation of said improvements shall be accomplished and guaranteed through the normal subdivision review and collateralization process.
- ii. Other drainage improvements in Tract D and future tracts containing the Sand Creek Channel, such as drop structures, check structures and similar stabilization or protection improvements, will be designed and constructed by the District with the final construction drawings to be approved by the County no later than the final platting of the 700<sup>th</sup> single family lot within the boundaries of the approved Sterling Ranch Sketch Plan and the completion of all said improvements no later than the 800<sup>th</sup> single family lot with the boundaries of the approved Sterling Ranch Sketch Plan.
- iii. In order to assure completion of the drainage improvements required in Subsection 6.b.ii above as well as a fair apportionment of the costs of said drainage improvements amongst adjacent Sterling Ranch subdividers, the District agrees to establish a Sand Creek Channel Drainage Fee to be paid into a District Escrow Fund by adjacent subdividers at the time of final platting. The amount of the fee shall be a minimum of One Thousand Dollars

(\$1,000.00) per single family lot. The details of the proposed Sand Creek Channel Drainage Fee and the District Escrow Fund shall be agreed to by the parties in advance of the submittal of the first replat of or subdivision of the Master Pad Sites or other property located within Sterling Ranch.

A full copy of the recorded SIA is located in the files of El Paso County and EPC Clerk and Recorders office under Reception No. 218714151

#### **SUMMARY**

Development of this site will not adversely affect the surrounding development per this final drainage report with no negative impacts to the neighboring developments. The existing and proposed drainage facilities will adequately convey, detain and route runoff from tributary and onsite flows to the Sand Creek Drainage channel. Full Spectrum Detention and Water Quality Ponds will be used to discharge developed flows into Sand Creek per the Urban Drainage criteria flow rates, which are at or less than the historic flow. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. The development of the HOMESTEAD AT STERLING RANCH FILING NO. 2 project(s) shall not adversely affect adjacent or downstream property.

This filing comprising of 104 Single Family Lots is adjacent to 47.8% of Tract D as platted in Sterling Ranch Filing No. 1. Financial Assurance in the amount of \$450,583.00 for Public Storm Sewer, and \$334,232.02 for the Sand Creek Channel Improvements adjacent to this filing shall be provided by the developer prior to recordation of the final plat. See completed and approved Financial Assurance Estimate provided to El Paso County.

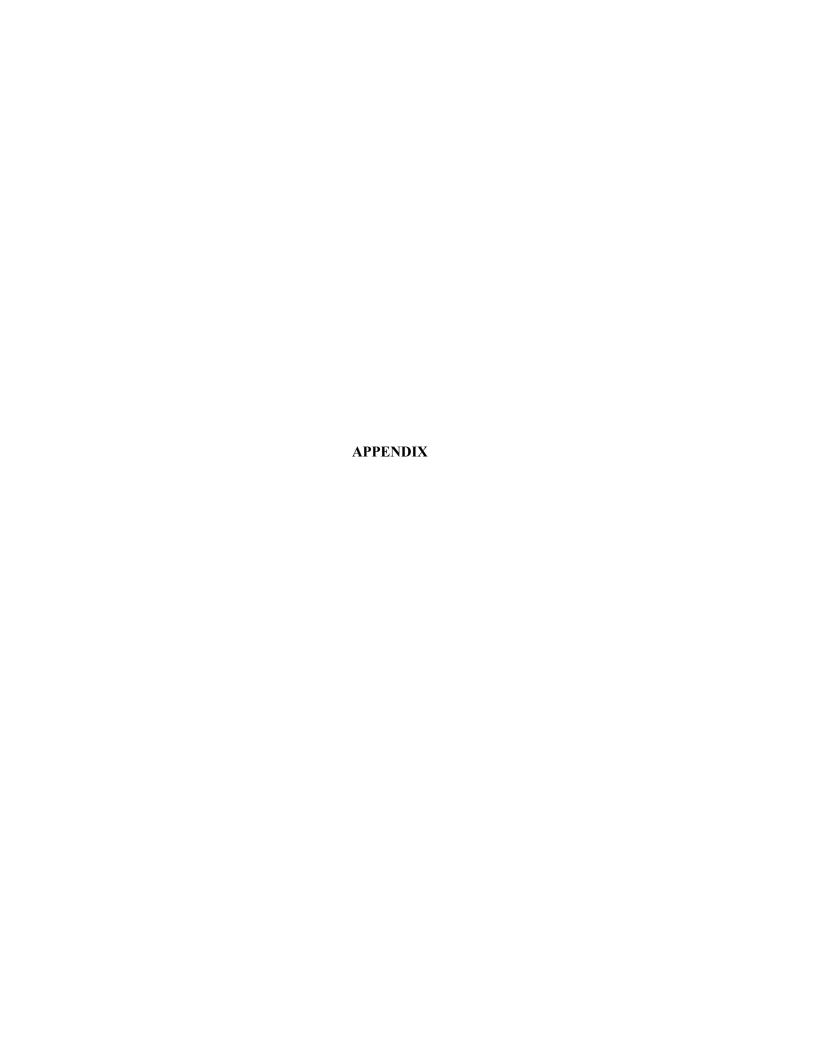
(not verified with this review)

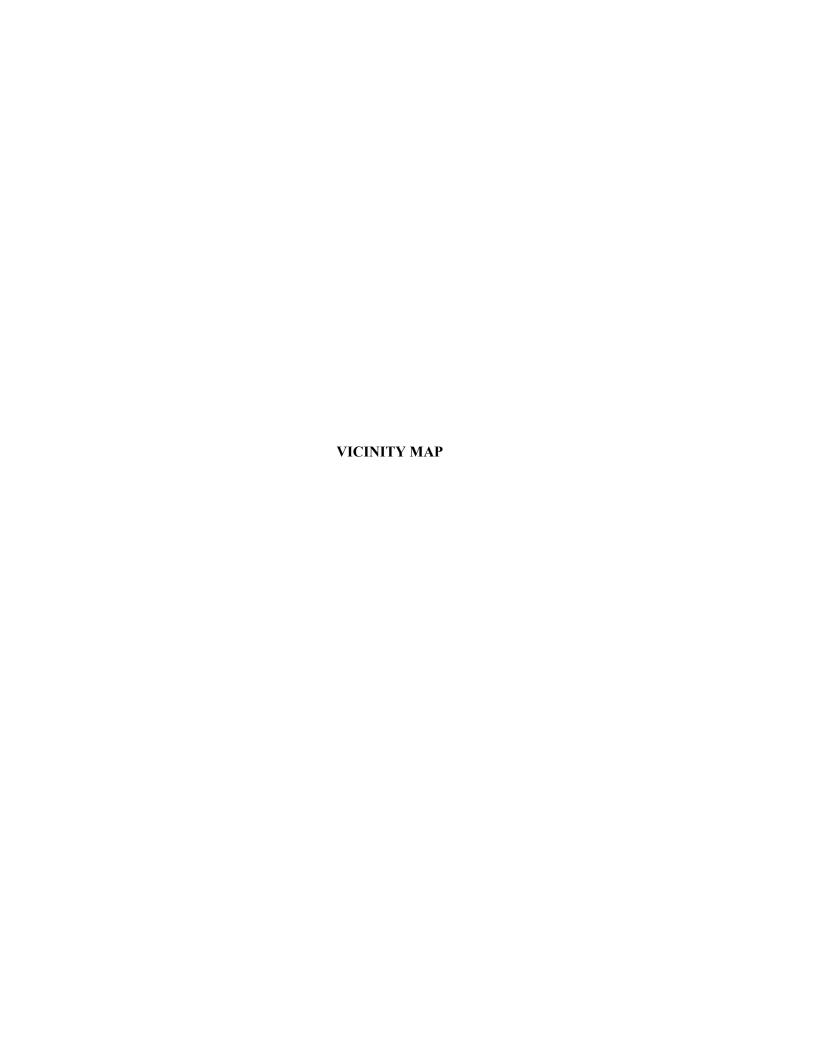
#### REFERENCES

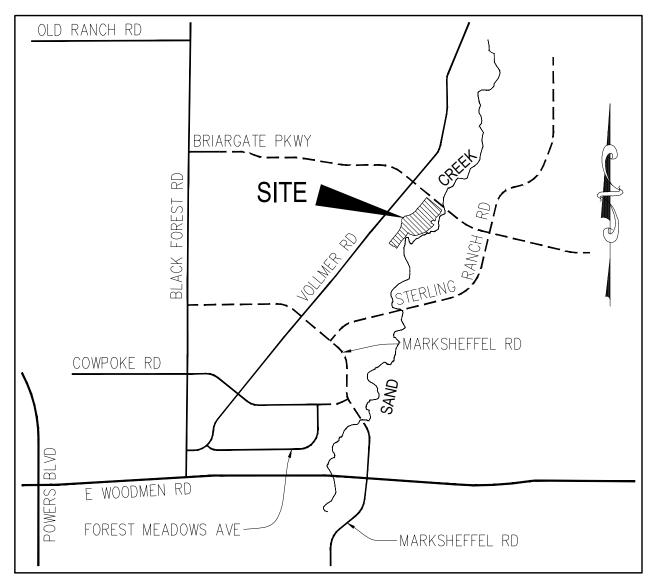
- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2.) "Urban Storm Drainage Criteria Manuals, Volumes 1-3"
- 3.) NRSC Web Soil Survey Map for El Paso County. http://websoilsurvey.nrcs.usda.gov
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date March 17, 1997.
- 5.) "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996
- 6.) "Sterling Ranch-Phase 1 Offsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 7.) "Sterling Ranch-Phase 1 Onsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 8.) "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2 and Final Drainage Report for Sterling Ranch Filing No. 1", prepared by M&S Civil Consultants, Inc., dated April 2017

#### MDDP - October 2018?

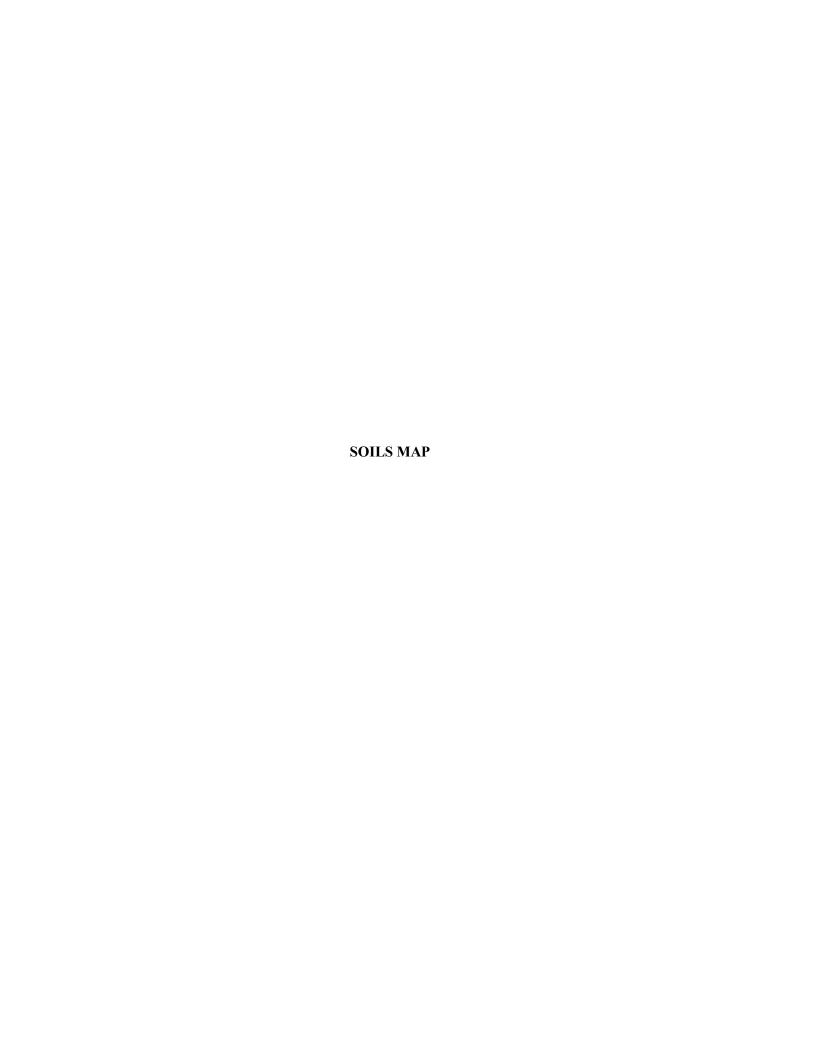
https://epcdevplanstorage.blob.core.windows.net/project/86c36538 -3e85-4819-b33c-7c6669f72731/6a2033b4-24b4-41e5-8386-26c82 3111a87.pdf

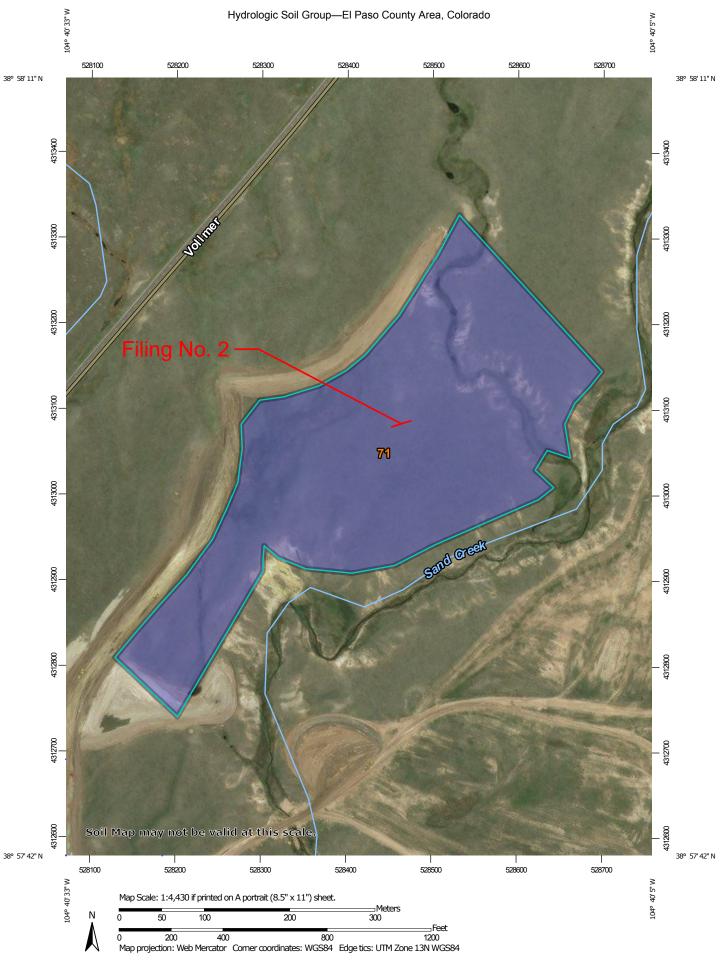






VICINITY MAP N.T.S.





#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Not rated or not available Date(s) aerial images were photographed: May 22, 2016—Mar 9. 2017 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

### **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	29.0	100.0%
Totals for Area of Intere	est		29.0	100.0%

### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

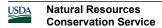
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

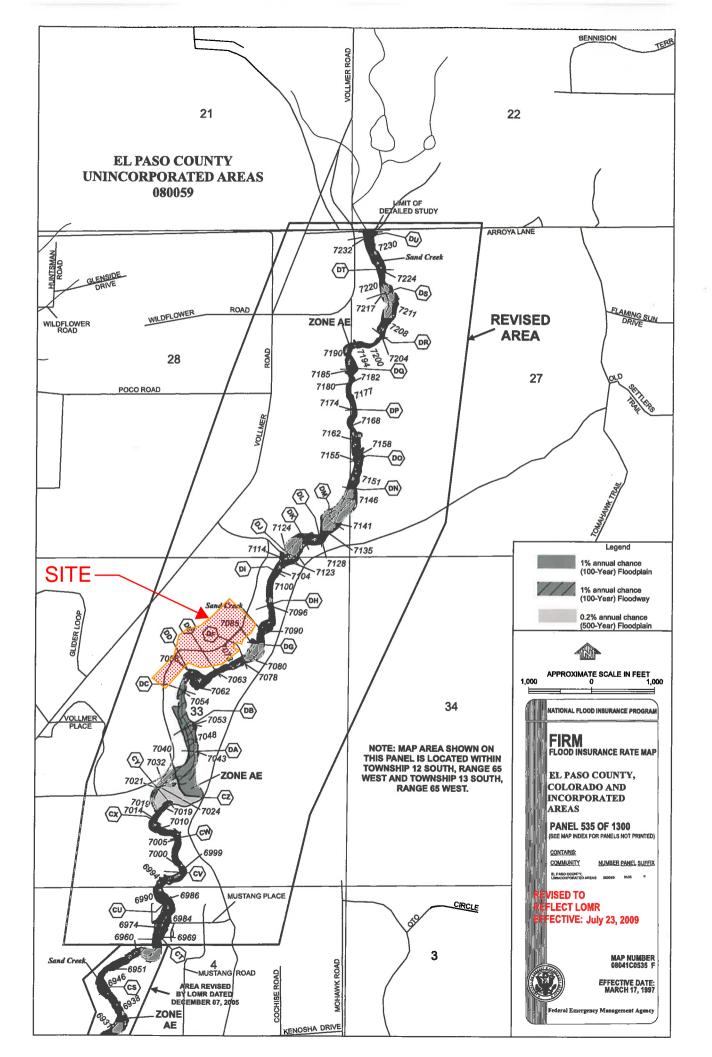
Aggregation Method: Dominant Condition



Component Percent Cutoff: None Specified

Tie-break Rule: Higher



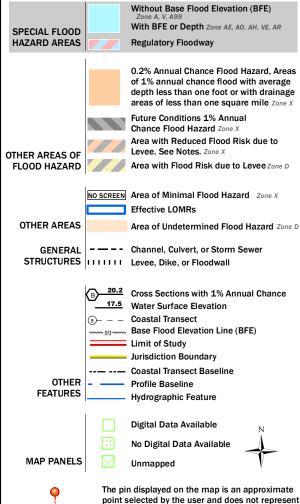


## National Flood Hazard Layer FIRMette



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



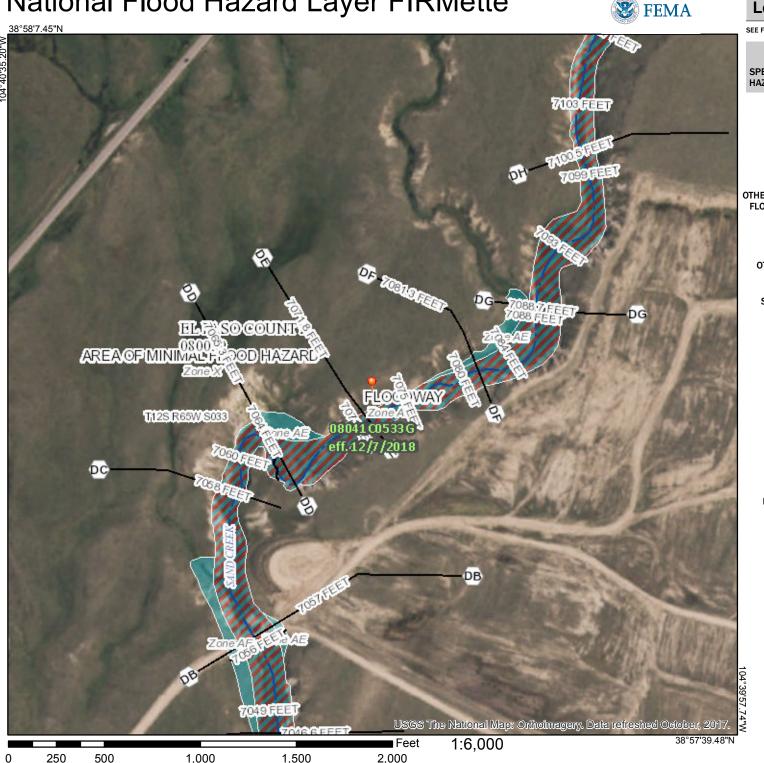
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

accuracy standards

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 1/23/2019 at 7:09:44 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Latitude: 38.964784

Longitude: 104.67180

NGVD 29 height:

Datum shift(NAVD 88 minus NGVD 29): 1.196 meter

1.196 meters = 3.92 feet

NAVD88 - 3.92 feet = NGVD29

## **STORM 4 Outfall to Sand Creek Channel**

Cross Section DE = 7071.8 NAVD88

7071.8 NAVD88 - 3.92 feet = 7067.88 NGVD29



## (not reviewed in detail)

# HOMESTEAD AT STERLING RANCH FILING NO. 2 FINAL DRAINAGE REPORT

## (Area Drainage Summary)

From Area Runoff Coe	fficient Summa	ıry		OVERLAND			STREET / CHANNEL FLOW				Time of Travel $(T_t)$		INTENSITY **		TOTAL FLOWS		
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{C}$	Length	Slope	Velocity	$T_t$	TOTAL	СНЕСК	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	Q <sub>100</sub>
	(Acres)	From DCM	I Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
					Propo	osed Ar	ea Dra	inage S	umma	ry							ļ
ONSITE BASINS																	
J	0.43	0.22	0.46	0.22	90	1.8	12.0	0	2.0%	3.0	0.0	12.0	10.5	4.1	6.8	0.4	1.3
K	0.61	0.22	0.46	0.22	75	1.5	10.9	0	2.0%	3.0	0.0	10.9	10.4	4.1	6.8	0.5	1.9
P	4.42	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	5.7	13.8
$\varrho$	3.78	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	4.9	11.8
R	1.57	0.38	0.55	0.38	100	2	10.3	450	1.6%	3.0	2.5	12.8	13.1	3.8	6.3	2.2	5.4
T	9.14	0.30	0.50	0.30	100	2	11.5	942	2.1%	3.0	5.2	16.7	15.8	3.4	5.8	9.4	26.4
$oldsymbol{U}$	4.50	0.38	0.55	0.38	100	2	10.3	457	1.5%	3.0	2.5	12.9	13.1	3.8	6.3	6.4	15.6
V1	1.48	0.38	0.55	0.38	100	2	10.3	600	2.0%	3.0	3.3	13.6	13.9	3.7	6.2	2.1	5.0
V2	0.83	0.38	0.55	0.38	100	2	10.3	360	1.6%	3.0	2.0	12.3	12.6	3.8	6.4	1.2	2.9
W1	0.56	0.08	0.35	0.08	35	8	3.9	160	0.5%	2.3	1.2	5.1	11.1	5.2	8.7	0.2	1.7
W2	0.26	0.08	0.35	0.08	35	8	3.9	0	0.3%	2.3	0.0	5.0	10.2	5.2	8.7	0.1	0.8
X	0.22	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.8
X1	0.78	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	2.8
X2	1.04	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	1.1	3.7
Y	0.09	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.1	0.3
Y1	0.84	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	3.0
Y2	0.21	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.7
OFFSITE BASINS*																	•
<b>B</b> *	5.39	0.38	0.55	0.38	60	1.2	8.0	1381	2.8%	3.0	7.6	16.3	18.0	3.4	5.7	8.0	19.3
C*	2.92	0.38	0.55	0.38	100	1.2	12.2	411	3.0%	3.0	2.3	14.5	12.8	3.8	6.3	4.2	10.1
D*	2.90	0.38	0.55	0.38	100	2	10.3	245	2.1%	3.0	1.3	11.7	11.9	3.9	6.5	4.3	10.4
E*	5.34	0.38	0.55	0.38	100	2	10.3	61	3.3%	3.0	0.3	10.7	10.9	4.0	6.8	8.2	19.9
F*	1.12	0.90	0.96	0.90	10	0.2	0.9	1525	2.8%	3.0	8.4	9.3	18.5	4.2	7.1	4.3	7.7
<i>G</i> *	0.61	0.22	0.46	0.22	100	2	12.6	0	2.2%	3.0	0.0	12.6	10.6	4.0	6.8	0.5	1.9
H*	0.19	0.90	0.96	0.90	10	0.2	0.9	280	2.1%	3.0	1.5	5.0	11.6	5.2	8.7	0.9	1.6
<i>I</i> *	2.10	0.90	0.96	0.90	10	0.2	0.9	1082	2.5%	3.0	5.9	6.9	16.1	4.7	7.9	8.9	15.9
	1.54	0.90	0.96	0.90	10	0.2	0.9	1805	2.1%	3.0	9.9	10.8	20.1	4.0	6.7	5.6	10.0
S*	1.97	0.08	0.35	0.08	60	10	5.6	270	0.5%	2.3	2.0	7.6	11.8	4.5	7.6	0.7	5.3

<sup>\*</sup> For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

Calculated by: ET/CMN

Date: 7/30/2019

Checked by: VAS

<sup>\*\*</sup> Intensity equations assume a minimum travel time of 5 minutes.

# HOMESTEAD AT STERLING RANCH FILING NO. 2 FINAL DRAINAGE REPORT (Basin Routing Summary)

	From Area Runoff Coefficient Summary		•		OVE	RLAND	0	PIPE		NNEL FLO	W	Time of Travel $(T_t)$	INTEN	SITY **	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	$Q_{100}$	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
				ED L	PRAINA	IGE BA	SIN R	OUTIN	G SUM	MARY							
2*	B*	2.34	3.39									16.3	3.4	5.7	8.0	19.3	(2) EX. 15' AT-GRADE INLETS
3*	C*	1.11	1.61									12.8	3.8	6.3	4.2	10.1	EX. 6' SUMP INLET
4*	D*, E*, F*	4.14	5.61									11.7	3.9	6.5	16.1	36.7	EX. 15' AT-GRADE INLET
5*	G*, H*, FLOWBY DP4*	1.07	3.02									11.7	3.9	6.5	4.2	19.7	EX. 15' AT-GRADE INLET
6*	I*, J, K, L*	3.50	3.97									10.8	4.0	6.7	14.1	26.7	EX. 15' AT-GRADE INLET
7	P	1.68	2.43									16.4	3.4	5.7	5.7	13.8	PROP. 10' SUMP INLET
0	0	1.44	2.00									16.4	2.4	6.7	4.0	11.0	
8	Q	1.44	2.08									16.4	3.4	5.7	4.9	11.8	PROP. 10' SUMP INLET
9	R	0.60	0.86									12.8	3.8	6.3	2.2	5.4	PROP. 10' SUMP INLET
10	T	2.74	2.69									15.8	3.4	5.8	9.4	15.6	PROP. 15' AT-GRADE INLET
10	•	2.74	2.09									15.6	3.4	5.6	2.4	13.0	Total CA100=3.86 Split Between
																	DP10 & DP11 For Crown Overflow
11	V1	0.56	2.69									15.8	3.4	5.8	1.9	15.6	PROP. 15' AT-GRADE INLET
																	Total CA100=3.86 Split Between
12	U, FLOWBY DP10	1.80	2.98									15.8	3.4	5.8	6.2	17.2	DP10 & DP11 For Crown Overflow PROP. 10' SUMP INLET
12	C, FLOW BY DITIO	1.00	2.70									13.0	5	5.0	0.2	17.2	I ROL TO SOMI INLET
13	V2, FLOWBY DP11	0.32	0.96						,			13.6	3.7	6.2	1.2	5.9	PROP. MODIFIED
																	5'x4.5' SUMP INLET
14	W1, PR9	5.35	8.52									13.6	3.7	6.2	19.6	52.4	CUMULATIVE
	, -, -, -												,	,			DETENTION POND

<sup>\*</sup> For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

\*\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET/CMN
Date: 9/4/2018
Checked by: VAS

## HOMESTEAD AT STERLING RANCH FILING NO. 2 **DRAINAGE CALCULATIONS**

## (Storm Sewer Routing Summary)

				Intensity**		tensity**	Flo	)w	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	$I_5$	I 100	<b>Q</b> 5	Q 100	
1	DP7	1.68	2.43	16.4	3.4	5.7	5.7	13.8	24" RCP
2	DP8	1.44	2.08	16.4	3.4	5.7	4.9	11.8	18" RCP
3	PR1, PR2	3.12	4.51	16.4	3.4	5.7	10.6	25.7	24" RCP
4	DP9, PR3	3.71	5.37	17.0	3.3	5.6	12.4	30.1	30" RCP
5	DP10	2.64	2.20	15.8	3.4	5.8	9.1	12.7	18" RCP
6	DP11	0.55	2.20	15.8	3.4	5.8	1.9	12.7	18" RCP
7	PR5, PR6	3.19	4.39	16.0	3.4	5.7	10.9	25.3	30" RCP
8	DP12	1.80	2.98	15.8	3.4	5.8	6.2	17.2	24" RCP
9	DP13, PR7, PR8	5.31	8.33	16.6	3.4	5.7	17.9	47.1	42" RCP
10	UD-Detention_v3.07						<b>0.</b> 7	23.4	Outlet Structure & 18" CMP
11	Pipe Run continued from MDDP DP1	5* to Sand Creek	. Flow values ar	e that of MDDI	Pipe Run	15* (PR15*).	42.1	76.8	42" RCP
12	Lots 36-41						0.0	1.3	12" ADS
13	Lots 28-35			0.0	1.6	12" ADS			
14	Lots 19-24				0.0	1.5	12" ADS		
15	Lots 13-18						0.0	1.4	12" ADS

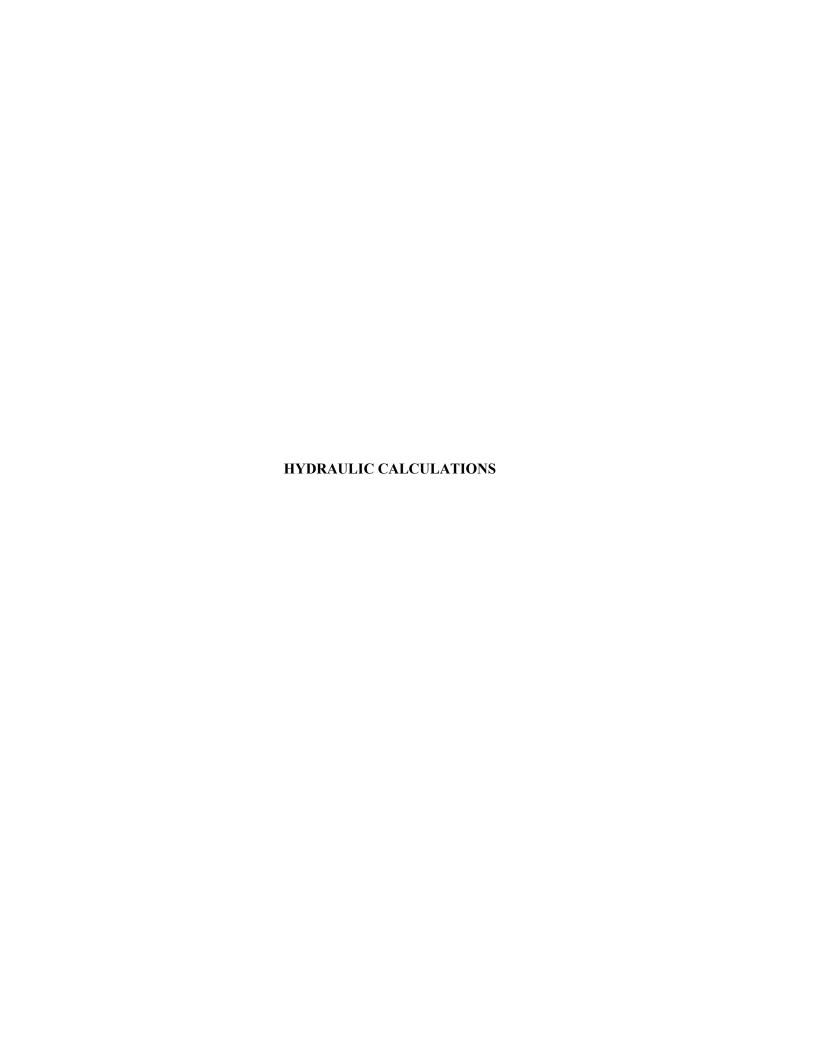
<sup>\*</sup> For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

DP - Design Point

EX - Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: CMN Date: 9/4/2018 Checked by: VAS

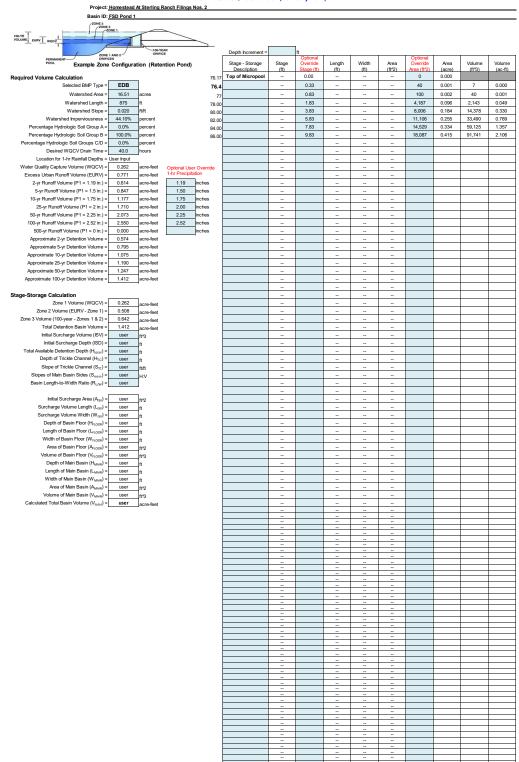
<sup>\*\*</sup> Intensity equations assume a minimum travel time of 5 minutes.



Weig	Weighted Percent Imperviousness of FSD Pond 1									
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)						
T	9.14	0.30	40	365.60						
$oldsymbol{U}$	4.50	0.38	53	238.50						
V1	1.48	0.38	53	78.44						
V2	0.83	0.38	53	43.99						
W1	0.56	0.08	2	1.12						
Totals	16.51			727.65						
Imperviousness of FSD Pond 1	44.1	%								

#### **DETENTION BASIN STAGE-STORAGE TABLE BUILDER**

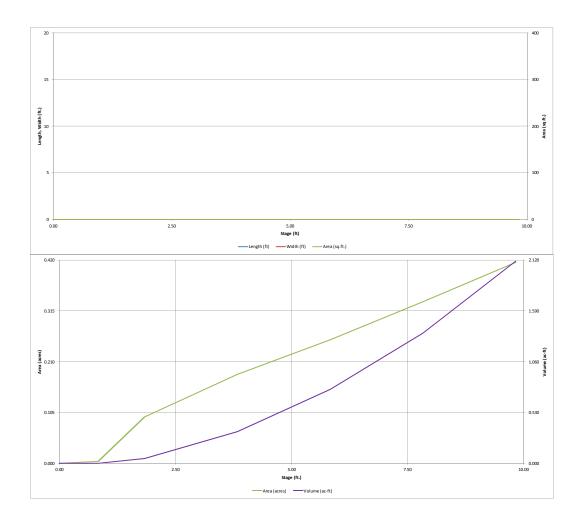
UD-Detention, Version 3.07 (February 2017)



UD-Peterition\_v3.07.x/sm, Basin 7/31/2019, 9:30 AM

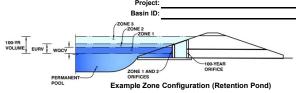
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



#### **Detention Basin Outlet Structure Design**

#### UD-Detention, Version 3.07 (February 2017)



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.45	0.262	Orifice Plate
Zone 2 (EURV)	5.84	0.508	Orifice Plate
!one 3 (100-year)	8.00	0.642	Weir&Pipe (Restrict)
•		1.412	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter = N/A inches

Calculate	ed Parameters for Un	derdrai
Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	5.84	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	23.40	inches
Orifice Plate: Orifice Area per Row =	1.19	sq. inches (diameter = 1-3/16 inches)

Calculated Parameters for Plate					
WQ Orifice Area per Row =	8.264E-03	ft <sup>2</sup>			
Elliptical Half-Width =	N/A	feet			
Elliptical Slot Centroid =	N/A	feet			
Elliptical Slot Area =	N/A	ft <sup>2</sup>			

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.95	3.89					
Orifice Area (sq. inches)	1.19	1.19	1.19					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated	Calculated Parameters for Vertical Orifice				
	Not Selected	Not Selected			
Vertical Orifice Area =	N/A	N/A	ft <sup>2</sup>		
Vertical Orifice Centroid =	N/A	N/A	feet		

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.84	N/A	ft (relative to basin bottom at Stage = 0 ft
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Slope =	3.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	2.91	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated			
	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, $H_t$ =	6.81	N/A	feet
Over Flow Weir Slope Length =	3.07	N/A	feet
Grate Open Area / 100-yr Orifice Area =	7.21	N/A	should be $\geq 4$
Overflow Grate Open Area w/o Debris =	12.88	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	6.44	N/A	ft <sup>2</sup>
<del>-</del>			_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

put: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectan			gular Orifice)	Calculated Parameter	rs for Outlet Pipe w/ Flow Restriction Plate			
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected		
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.79	N/A	ft <sup>2</sup>	
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.63	N/A	feet	
Restrictor Plate Height Above Pipe Invert =	13.30	•	inches Half-Central Angle o	f Restrictor Plate on Pipe =	1.68	N/A	radians	

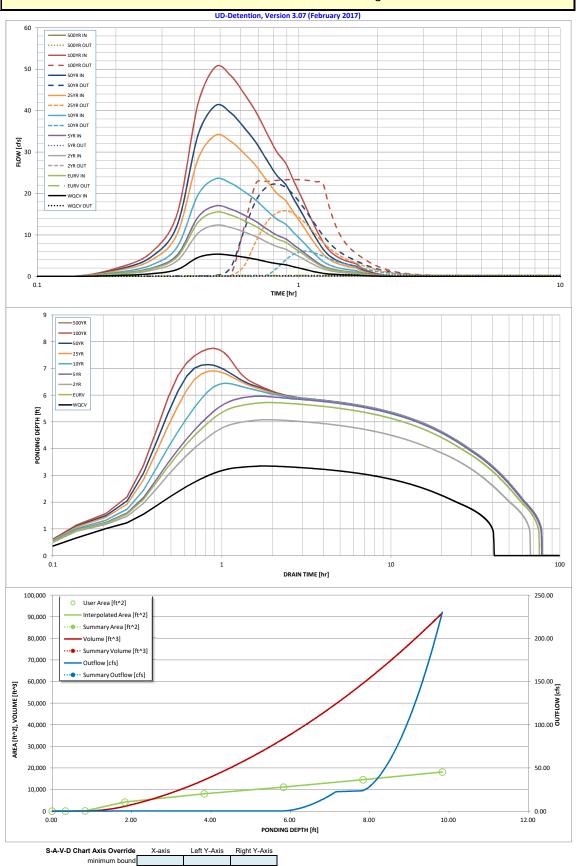
User Input: Emerg	gency Spillway	(Rectangular or	Trapezoidal)

oser input zine.Benej spiniaj (nestanj	Saidi oi itapezoidai,	
Spillway Invert Stage=	7.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	17.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway				
Spillway Design Flow Depth=	0.89	feet		
Stage at Top of Freeboard =	9.69	feet		
sin Area at Top of Freeboard =	0.41	acres		

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.262	0.771	0.614	0.847	1.177	1.710	2.073	2.550	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.262	0.771	0.614	0.847	1.176	1.710	2.074	2.551	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.27	0.84	1.16	1.55	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.3	0.4	4.4	13.9	19.2	25.5	0.0
Peak Inflow Q (cfs) =	5.3	15.5	12.4	17.0	23.5	34.1	41.2	50.5	#N/A
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.7	6.0	15.8	22.3	23.4	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.5	1.4	1.1	1.2	0.9	#N/A
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.4	1.2	1.7	1.8	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	39	69	62	71	69	66	63	61	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	73	65	76	75	74	73	72	#N/A
Maximum Ponding Depth (ft) =	3.35	5.72	5.08	5.96	6.44	6.91	7.15	7.75	#N/A
Area at Maximum Ponding Depth (acres) =	0.16	0.25	0.23	0.26	0.28	0.30	0.31	0.33	#N/A
Maximum Volume Stored (acre-ft) =	0.245	0.741	0.588	0.802	0.932	1.067	1.137	1.331	#N/A

#### **Detention Basin Outlet Structure Design**



maximum bound

#### **Detention Basin Outlet Structure Design**

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK #N/A

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.40	0:00:00		0.00	0.00			0.00		0.00	401/0
4.12 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	0:04:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:08:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:12:22	0.24	0.68	0.55	0.75	1.03	1.47	1.77	2.15	#N/A
1.214	0:16:29	0.64	1.85	1.48	2.02	2.79	4.01	4.84	5.91	#N/A
	0:20:36	1.65	4.74	3.79	5.20	7.16	10.30	12.42	15.18	#N/A
	0:24:43	4.55	13.03	10.43	14.28	19.66	28.29	34.10	41.64	#N/A
	0:28:50	5.34	15.51	12.37	17.02	23.54	34.08	41.22	50.54	#N/A
	0:32:58	5.08	14.81	11.80	16.25	22.50	32.61	39.48	48.45	#N/A
	0:37:05	4.62	13.48	10.75	14.80	20.49	29.69	35.94	44.09	#N/A
	0:41:12	4.11	12.05	9.59	13.23	18.35	26.64	32.27	39.64	#N/A
	0:45:19	3.53	10.41	8.28	11.44	15.90	23.13	28.07	34.53	#N/A
	0:49:26	3.08	9.07	7.22	9.96	13.83	20.09	24.40	30.06	#N/A
	0:53:34	2.79	8.22	6.54	9.03	12.54	18.22	22.11	27.22	#N/A
	0:57:41	2.79	6.79	5.39	7.47	10.41	15.18	18.44	22.73	#N/A
	1:01:48									
		1.84	5.56	4.40	6.12	8.55	12.50	15.21	18.77	#N/A
	1:05:55	1.40	4.29	3.39	4.73	6.64	9.78	11.93	14.77	#N/A
	1:10:02	1.02	3.21	2.52	3.54	5.01	7.43	9.10	11.31	#N/A
	1:14:10	0.75	2.32	1.83	2.56	3.64	5.45	6.70	8.37	#N/A
	1:18:17	0.59	1.79	1.42	1.97	2.79	4.15	5.08	6.32	#N/A
	1:22:24	0.48	1.47	1.16	1.62	2.29	3.38	4.13	5.12	#N/A
	1:26:31	0.41	1.25	0.99	1.38	1.94	2.86	3.49	4.32	#N/A
	1:30:38	0.36	1.10	0.87	1.21	1.70	2.50	3.05	3.77	#N/A
	1:34:46	0.33	0.99	0.78	1.09	1.52	2.24	2.73	3.38	#N/A
	1:38:53	0.30	0.91	0.72	1.00	1.40	2.06	2.51	3.10	#N/A
	1:43:00	0.22	0.67	0.53	0.73	1.03	1.52	1.85	2.29	#N/A
	1:47:07	0.16	0.49	0.39	0.54	0.75	1.11	1.35	1.67	#N/A
	1:51:14	0.12	0.36	0.28	0.40	0.55	0.81	0.99	1.23	#N/A
	1:55:22	0.09	0.26	0.21	0.29	0.41	0.60	0.74	0.91	#N/A
	1:59:29	0.06	0.19	0.15	0.21	0.30	0.44	0.53	0.66	#N/A
	2:03:36	0.04	0.13	0.11	0.15	0.21	0.31	0.38	0.47	#N/A
	2:07:43			0.08			0.23		0.47	#N/A
	2:11:50	0.03	0.10		0.11	0.15		0.28		
		0.02	0.06	0.05	0.07	0.10	0.15	0.19	0.24	#N/A
	2:15:58	0.01	0.04	0.03	0.04	0.06	0.10	0.12	0.15	#N/A
	2:20:05	0.00	0.02	0.01	0.02	0.03	0.05	0.06	0.08	#N/A
	2:24:12	0.00	0.01	0.00	0.01	0.01	0.02	0.03	0.04	#N/A
	2:28:19	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	#N/A
	2:32:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:36:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:40:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:44:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:48:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:53:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:57:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:01:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:05:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:09:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:13:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:17:46	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:21:53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:26:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:30:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:34:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:38:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:42:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:46:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:50:43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:54:50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:58:58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:03:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:07:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:11:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:15:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:19:34 4:23:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:23:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:27:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:36:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:40:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:44:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:48:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:52:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:56:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
l										



PROJECT:	Homestead Filing No. 2
DATE:	

Micropool Surface Area	Tribm	tag Area	= 16.51 AC	
TIA IXA			= 44.1%	
(0.441 x 1451)				
TIA = 7.3 ~ 8.0	, in			
From Micropool Sizing Chan	of (SA)	Micropoof	SA = 40 st	2
				2
Foreboy Volume for PSD Pa	_			
Topontary Area - 16.51.				
Min. Forebuy Voiume - 3	1 1		WOFED 7-5,	, EDB
Wacv for FoD Pond = a.	262 Ac-	A		Management and the second seco
Total Volume Regid. = 0.0	3 (0.242	13540	- 342cf	
Arca = 283 - 7 (wall) =				
		Footb	a 15 1 H	
( forebay) (dust) (10/10		70.00	y 15 depth	TO THE PARTY OF TH
(torchan) (dysta) (volun proud				
		to 207 +1		1000
Since notch in Forebry to Q100 = 47.1 cfs => 0.02 x 5	a comman	CUOPEL	T-5 EDS	
(4100 = 41.1 cts = 0.02 x 5	7.7 = 0.99	LUR		9 ,
Using Ret. Weir Egn.	Q = 3.24	1121.118	7	<i>H.</i> /
Solve for L = 2.6" 0	= 0,94	// % ~		continues animateur
		use a 2.	6"notch	- Annual Control
			The state of the s	



PROJECT:	Homestead Filing No. 2	
TROJECT.	No. of the second secon	
DATE:		

Q: os.	Apron For	Panel 1	
Riprop Sizina	) which I w	Panel 1	
Q100 = 47.1 cfs	(Ping Bung)		
D <sub>2</sub> = 42° = 3.5′			
01.5 < 6 The	n use Figure	9-38 (UDFC	D Nol 5)
47.1 = 2.05	< 6 Therefore county	re use Figure	9-38 01.5 - 17.1 = 7.19 01.5 (3.5)" = 7.19
Use Type L	D <sub>50</sub> =9"		(3, 5)
Rioras Deptin			
T=2-0s			
Law Teinheater Ripre			
FES	9' 1-w=7'-1	6 1 X00	
Toewall	11.5'		

## **DETENTION BASIN STAGE-STORAGE TABLE BUILDER**

UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2 Basin ID: Lots 14, 15, 21-24, 41 Lot size 10,319 sq ft-15,049 sq ft -100-YEAR ORIFICE Depth Increment = Example Zone Configuration (Retention Pond) Stage - Storage Stage Override Length Width Area Override Area Volume Volume Description (ft) (ft^2) (acre) (ac-ft) Media Surface 0.00 77 0.002 7065.27 **Required Volume Calculation** Selected BMP Type = 0.50 152 0.003 0.001 7065.5 Watershed Area : 0.18 1.00 328 0.004 acres ------0.008 174 Note: L / W R 7066 82 1.50 543 0.012 390 0.009 Watershed Length = L/W Ratio = 7066.50 Watershed Slope = 0.080 ft/ft 2.00 796 0.018 722 0.017 7067.00 Watershed Imperviousness = 42.00% percent ------Percentage Hydrologic Soil Group A = ----Percentage Hydrologic Soil Group B = 100.0% -percent Percentage Hydrologic Soil Groups C/D = ercent Desired WQCV Drain Time = 12.0 hours Location for 1-hr Rainfall Depths = User Input ----Water Quality Capture Volume (WQCV) = 0.002 -acre-feet Optional User Override 1-hr Precipitation Excess Urban Runoff Volume (EURV) = 0.008 acre-feet 2-yr Runoff Volume (P1 = 1.19 in.) = 0.006 acre-feet 1.19 inches 5-yr Runoff Volume (P1 = 1.5 in.) = 0.009 acre-feet 1.50 inches --------10-yr Runoff Volume (P1 = 1.75 in.) = 0.012 acre-feet 1.75 inches --25-yr Runoff Volume (P1 = 2 in.) = 0.018 2 00 acre-feet inches 50-yr Runoff Volume (P1 = 2.25 in.) = 0.022 acre-feet 2.25 inches 100-yr Runoff Volume (P1 = 2.52 in.) = 0.027 acre-feet 2.52 inches ------500-yr Runoff Volume (P1 = 0 in.) = 0.000 acre-feet Approximate 2-yr Detention Volume = 0.006 acre-feet Approximate 5-yr Detention Volume = acre-feet Approximate 10-yr Detention Volume = 0.011 acre-feet ----Approximate 25-yr Detention Volume = 0.012 acre-feet ----Approximate 50-yr Detention Volume = 0.013 acre-feet --\_\_ \_\_ Approximate 100-yr Detention Volume 0.015 Stage-Storage Calculation ------Zone 1 Volume (WQCV) = 0.002 acre-feet Zone 2 Volume (EURV - Zone 1) = 0.006 acre-feet

UD-Detention_v3.07 LOT 15.xlsm, Basin	7/25/2019, 1:40 PM

--

--

--

--

--

Zone 3 Volume (100-year - Zones 1 & 2) =

Total Available Detention Depth (H<sub>total</sub>) =

Total Detention Basin Volume =

Initial Surcharge Volume (ISV) =

Initial Surcharge Depth (ISD) =

Depth of Trickle Channel (H<sub>TC</sub>) =

Slope of Trickle Channel (S<sub>TC</sub>) =

Slopes of Main Basin Sides (S<sub>main</sub>) =

0.007

0.015

N/A

N/A

user

N/A

N/A

user

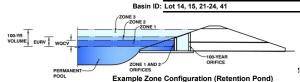
acre-feet

ft^3

ft/ft

## UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.71	0.002	Filtration Media
Zone 2 (EURV)	1.41	0.006	Rectangular Orifice
one 3 (100-year)	1.90	0.007	Rectangular Orifice
•		0.015	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.10 ft (distance below the filtration media surface)
Underdrain Orifice Diameter = 0.13 inches

Calculate	a i ai ai ii c cci s i oi	Onaciait
Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Underdrain Orifice Centroid =	0.01	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

Calcu	lated Parameters to	r Plate
WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A							
Orifice Area (sq. inches)	N/A							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Zone 3 Rectangular	
Invert of Vertical Orifice =	0.71	1.41	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	1.41	1.90	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	2.00	inches
Vertical Orifice Width =	1.00	6.00	inches

Calculated Parameters for Vertical Orifice						
	Zone 2 Rectangular	Zone 3 Rectangular				
Vertical Orifice Area =	0.01	0.08	ft <sup>2</sup>			
Vertical Orifice Centroid =	0.08	0.08	feet			

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.88	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	1.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	1.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir				
	Not Selected	Not Selected		
Height of Grate Upper Edge, H <sub>t</sub> =	1.88	N/A	feet	
Over Flow Weir Slope Length =	1.00	N/A	feet	
Grate Open Area / 100-yr Orifice Area =	N/A	N/A	should be >	
Overflow Grate Open Area w/o Debris =	0.70	N/A	ft <sup>2</sup>	
Overflow Grate Open Area w/ Debris =	0.35	N/A	ft <sup>2</sup>	
•			_	

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =	N/A	N/A	ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	N/A	N/A	inches
			Half-Central Ang

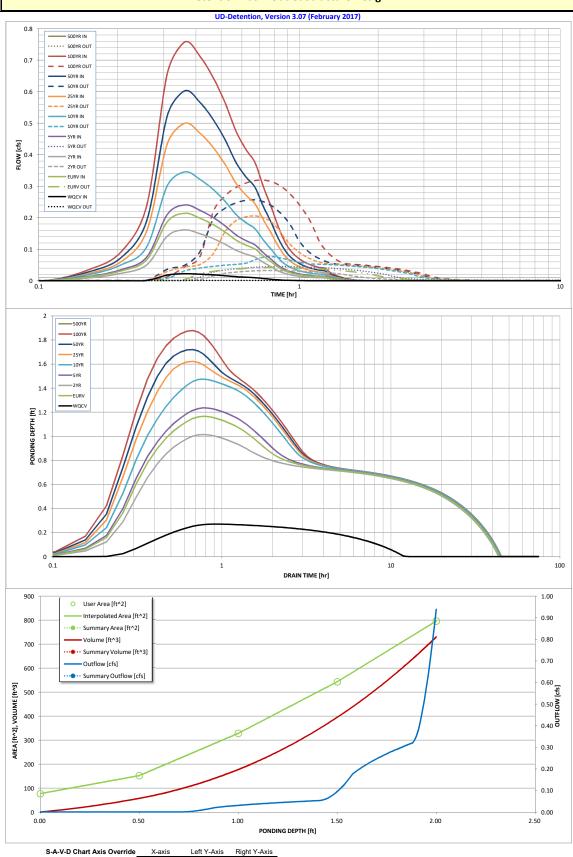
Calculated Parameter	s for Outlet Pipe w/	FIOW RESUICTION PIA	ıe
	Not Selected	Not Selected	
Outlet Orifice Area =	N/A	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	N/A	N/A	feet
Postrictor Plate on Pine -	N/A	N/A	radian

User Input: Emergency Spillway (Rectangular or Trapezoidal)

oser input zine.Benej spinivaj (nestanj	baiai oi iiapezoiaai,	
Spillway Invert Stage=	1.90	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	2.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.25	feet

Calcula	ted Parameters for S	pillway
Spillway Design Flow Depth=	0.14	feet
Stage at Top of Freeboard =	2.29	feet
Basin Area at Top of Freeboard =	0.02	acres

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.002	0.008	0.006	0.009	0.012	0.018	0.022	0.027	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.001	0.007	0.006	0.008	0.012	0.018	0.021	0.027	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.32	0.97	1.34	1.78	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.0
Peak Inflow Q (cfs) =	0.0	0.2	0.2	0.2	0.3	0.5	0.6	0.8	#N/A
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	8.1	1.4	1.2	1.1	1.0	#N/A
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	40	40	39	38	35	33	30	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	43	43	43	43	42	41	40	#N/A
Maximum Ponding Depth (ft) =	0.27	1.17	1.01	1.24	1.47	1.62	1.72	1.88	#N/A
Area at Maximum Ponding Depth (acres) =	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	#N/A
Maximum Volume Stored (acre-ft) =	0.001	0.005	0.004	0.006	0.009	0.011	0.012	0.014	#N/A

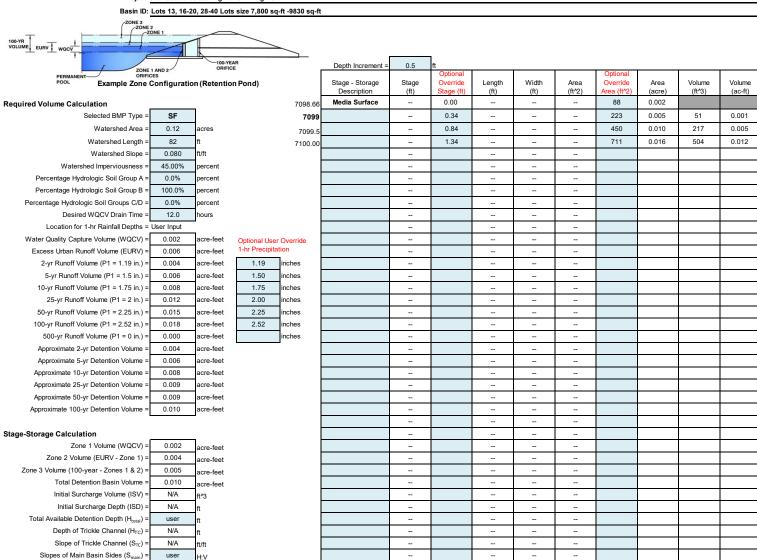


minimum bound maximum bound

## **DETENTION BASIN STAGE-STORAGE TABLE BUILDER**

UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2

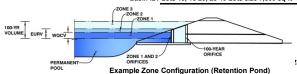


UD-Detention v3.07 LOT 40.xlsm, Basin

## UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2

Basin ID: Lots 13, 16-20, 28-40 Lots size 7,800 sq-ft -9830 sq-ft



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.40	0.002	Filtration Media
Zone 2 (EURV)	0.89	0.004	Rectangular Orifice
one 3 (100-year)	1.24	0.005	Rectangular Orifice
		0.010	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.10 ft (distance below the filtration media surface)
Underdrain Orifice Diameter = 0.13 inches

Culculate	a raidilicters for	Onaciaia
Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Underdrain Orifice Centroid =	0.01	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

Calcu	lated Parameters for	Plate
WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A							
Orifice Area (sq. inches)	N/A							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Zone 3 Rectangular	
Invert of Vertical Orifice =	0.40	0.89	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	0.89	1.24	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	2.00	inches
Vertical Orifice Width =	1.00	3.50	inches

Calculated	Parameters for Vert	ical Orifice	
	Zone 2 Rectangular	Zone 3 Rectangular	
Vertical Orifice Area =	0.01	0.05	ft <sup>2</sup>
Vertical Orifice Centroid =	0.08	0.08	fee

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.24	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	1.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	1.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated	Parameters for Ove	rflow Weir	
	Not Selected	Not Selected	
Height of Grate Upper Edge, $H_t$ =	1.24	N/A	feet
Over Flow Weir Slope Length =	1.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	N/A	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	0.70	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	0.35	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =	N/A	N/A	ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	N/A	N/A	inches
•			Half-Cen

		Not Selected	Not Selected	
age = 0 ft)	Outlet Orifice Area =	N/A	N/A	ft <sup>2</sup>
	Outlet Orifice Centroid =	N/A	N/A	feet
Half-Central Angle	of Restrictor Plate on Pipe =	N/A	N/A	radiar

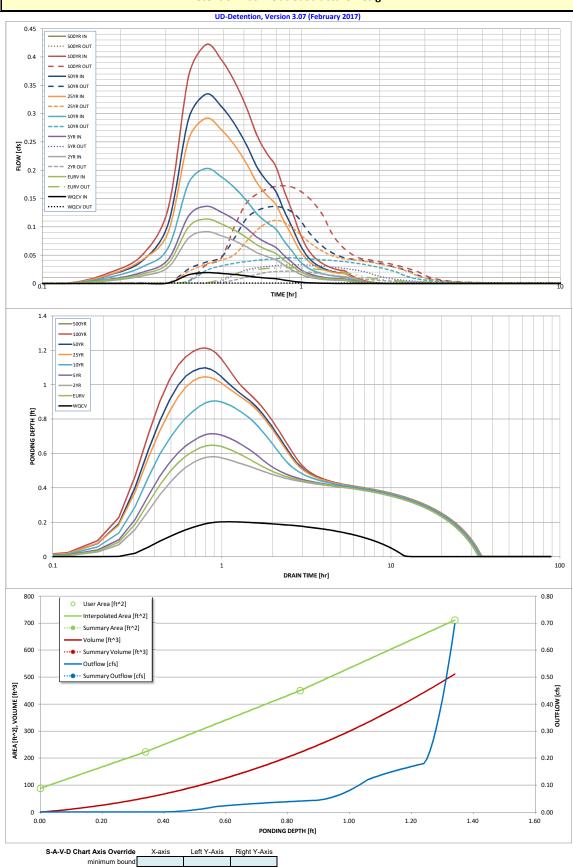
Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

	,	
Spillway Invert Stage=	1.24	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	2.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.25	feet

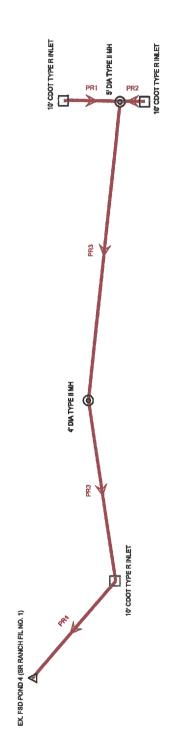
ted Parameters for S	pillway
0.14	feet
1.63	feet
0.02	acres
	0.14 1.63

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.002	0.006	0.004	0.006	0.008	0.012	0.015	0.018	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.001	0.005	0.004	0.006	0.008	0.012	0.014	0.018	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.28	0.88	1.21	1.61	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0
Peak Inflow Q (cfs) =	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.4	#N/A
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	10.1	1.4	1.1	1.0	0.9	#N/A
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	31	31	30	29	28	27	25	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	32	32	32	33	32	32	31	#N/A
Maximum Ponding Depth (ft) =	0.20	0.65	0.58	0.71	0.91	1.05	1.10	1.21	#N/A
Area at Maximum Ponding Depth (acres) =	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	#N/A
Maximum Volume Stored (acre-ft) =	0.001	0.003	0.003	0.004	0.006	0.007	0.008	0.010	#N/A



maximum bound

4

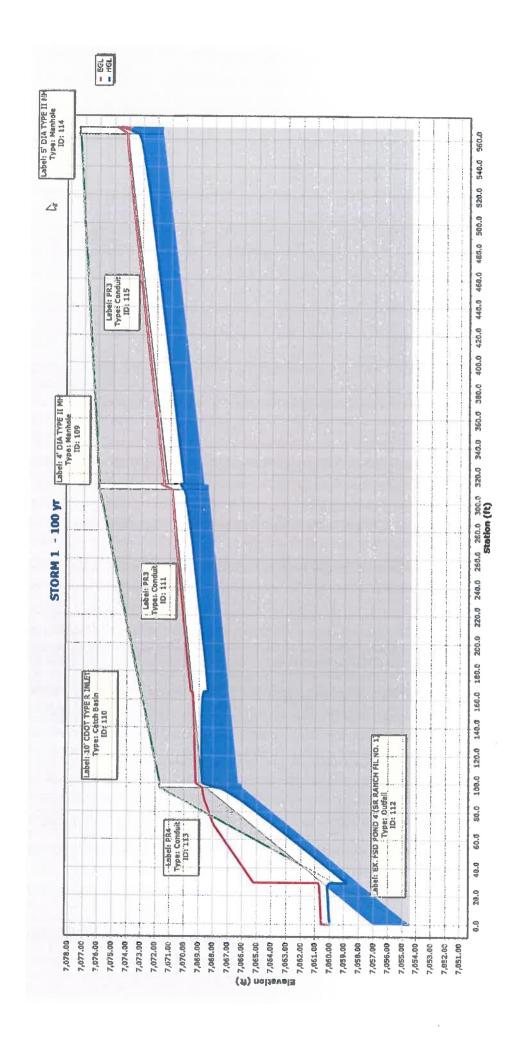


Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

> Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

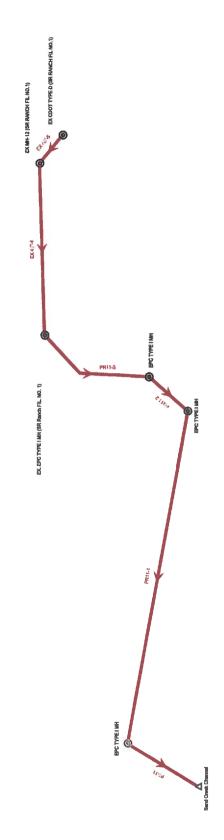
## Conduit FlexTable: Table - 1 STRM 18.2

Rise         Flow (cfs)         Flow / Capacity (Design)         Length (Unified)         Velocity (ft/s)           (ft)         (cfs)         (Design)         (ft)         (ft/s)           (%)         (%)         (5.70         62.7         213.1         8.83
30.10
11.80
Upstream Upstream Structure Structure Hydraulic Grade Velocity (In-Line (In) Governing) (ft)
7,070.34
,068.77
,074.54
,075.57
7,075.49



Scenario: 100 yr

## STEM 3 THEL EXHZ" SRI

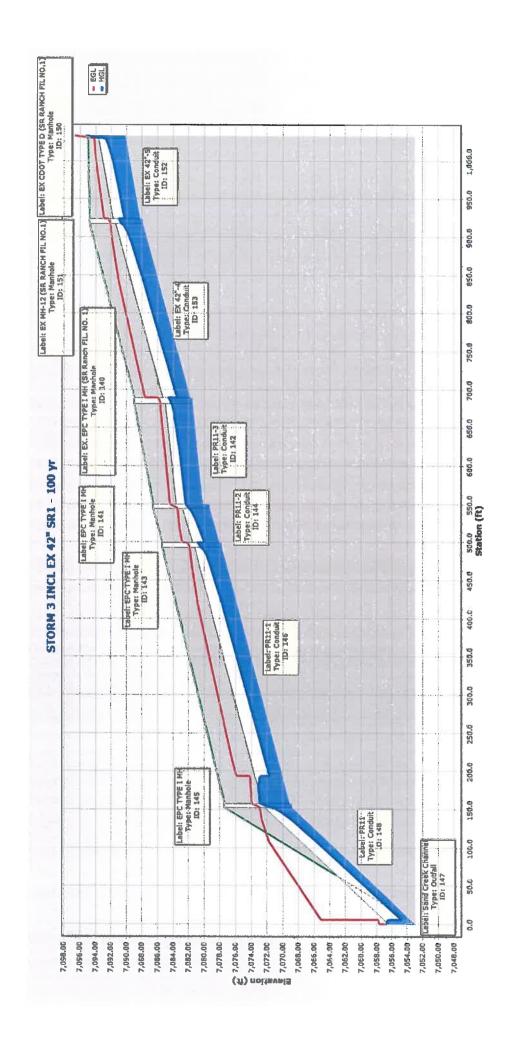


Bertley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

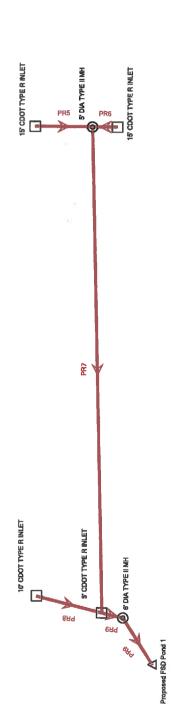
Bentley Systems, Inc. Haestad Methods Solution Center 27 Slemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

# Conduit FlexTable: Table - 1 STRM 3 INCL 42" SR1

									_								
Depth (Critical)	(£)	2.74	2.74	2.74	2.74	2.74		2.74	Invert (Stop)	<b>£</b>		7,080.11	7,078.00	7,069.11	7,053.00	7,088.21	7,081.79
Depth (Normal)	(£)	2.29	1.70	1.71	1.16	1.93		1.69	Invert (Start)	£		7,081.49	7,079.31	7,077.70	7,068.81	7,090,07	7,087.91
Froude Number	(Normal)	1.432	2.541	2.507	5.244	1.992		2.553	Elevation Ground	(Start)		7,088.97	7,086.56	7,085.36	7,077.40	7,095.00	7,094.77
Velocity	(trys)	11.50	16.58	16.43	27.41	14.12		16.64	Upstream	Structure	(F)	0.38	0.38	0.38	1.43	2.48	0.38
Length (Unified)	(ft)	138.4	20.8	341.2	155.1	110.4		235.2	Upstream	Structure	Coefficient	0.270	0.270	0.270	1.020	1.770	0.270
Flow / Capacity	(Design) (%)	76.4	47.5	48.1	23.9	58.8		47.3	Upstream	Structure Velocity (In-	Governing) (ft/s)	9.24	11.32	9.24	7.98	9.50	9.24
Flow	(ds)	76.80	76.80	76.80	76.80	76.80		76.80	Upstream	Structure	Line (In)	7,084.61	7,082.43	7,080.82	7,072.98	7,095.29	7,091.03
Rise	(ft)								Headloss	€		1.80	1.23	7.46	14.85	1.78	6.04
Upstream	Structure	EX. EPC TYPE I MH (SR Ranch EII NO 1)	EPC TYPE I MH	EPC TYPE I MH	EPC TYPE I MH	EX CDOT TYPE D (SR RANCH	EX MH-12 (SR	RANCH FIL NO.1)	Hydraulic Grade	Line (Out)	3	7,082.43	7,080.82	7,072.98	7,056.70	7,091.03	7,084.61
Label		PR11-3	PR11-2	PR11-1	PR11	EX 42"-5		EX 42"-4	Hydraulic Grade	Line (In)	3	7,084.23	7,082.05	7,080.44	7,071.55	7,092.81	7,090.65

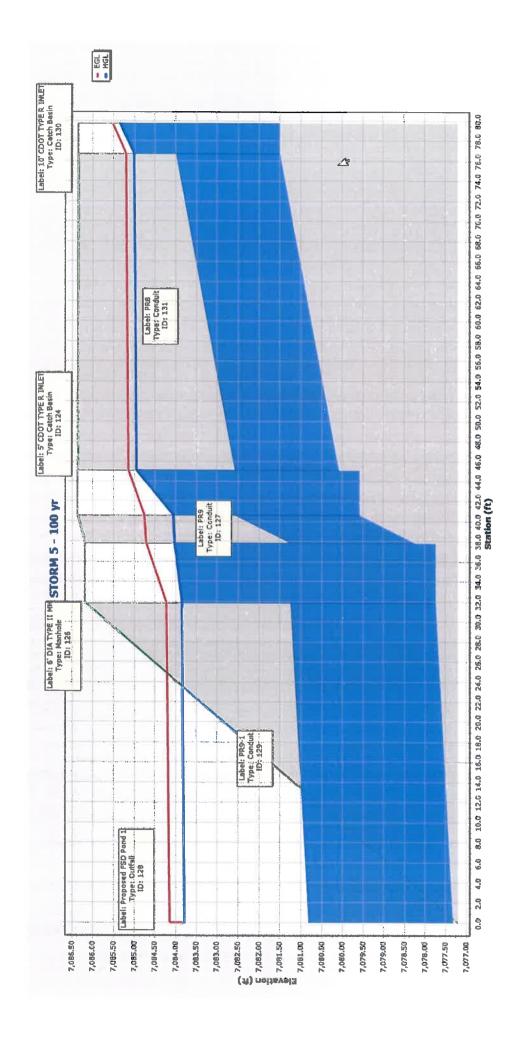


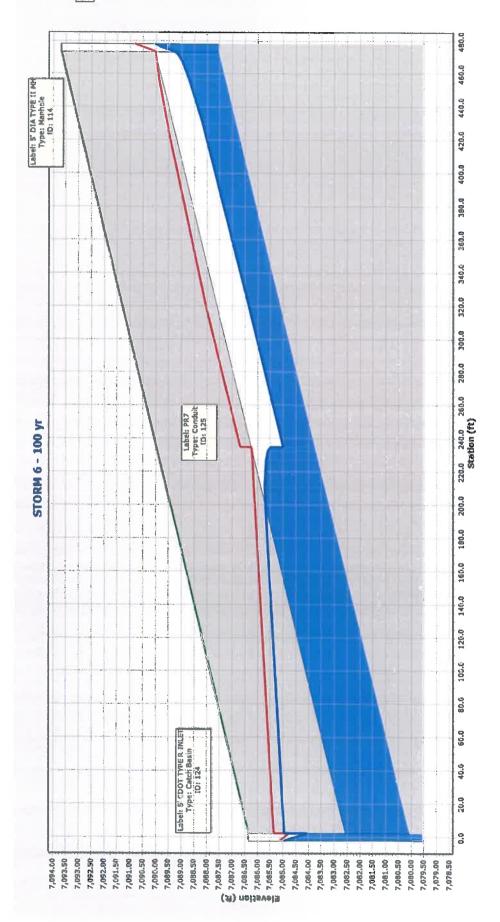
## STRM 5,6,7

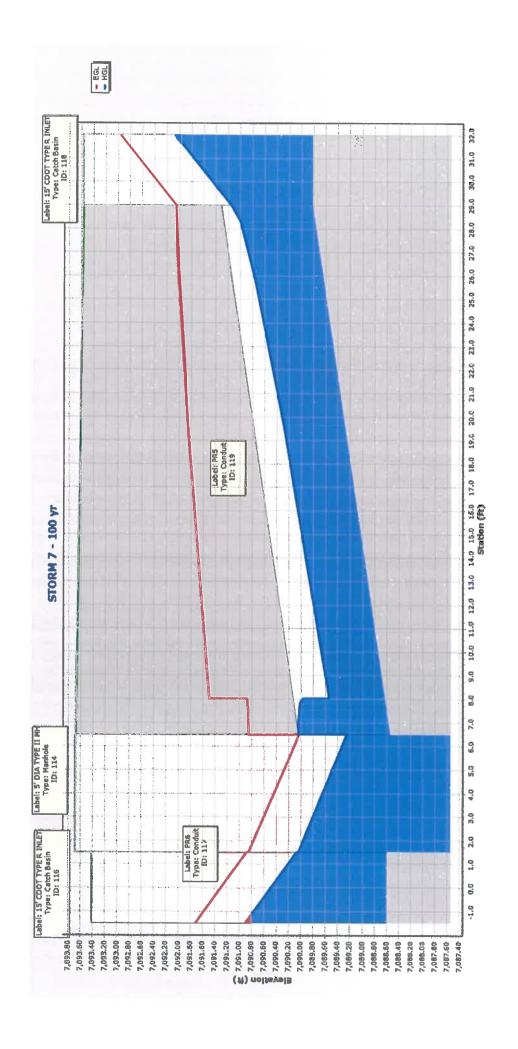


# Conduit FlexTable: Table - 1 STRM 5,6,7

Depth (Critical) (ft)	1.34	1.34	1.71	2.24	2.14	1.40	Invert (Stop) (ft)	7,088.54	7,088.54	7,080.07	7,078.23	7,077.31	7,080.07
Depth (Normal) (ft)	1.07	0.80	1.24	0.84	1.60	0.78	Invert (Start) (ft)	7,088.59	7,089.81	7,087.54	7,079.57	7,077.73	7,081.49
Froude Number (Normal)	1.674	2.948	1.867	6.560	1.755	3.114	Elevation Ground (Start) (ft)	7,093.41	7,093.57	7,093.68	7,086.36	7,086.18	7,086.34
Velocity (ft/s)	7.19	13.34	10.43	99'9	4.90	3.50	Upstream Structure Headloss (ft)	0.82	0.92	1.17	0.88	0.18	0.34
How / Capacity Length (Unified) Velocity (ft) (ft)	2.5	26.5	475.5	8.0	34.9	35.4	Upstream Structure Headloss Coefficient	1.020	1.020	1.520	1.280	0.470	1.770
Flow / Capacity (Design)	(%)	55.2	49.2	17.3	42.6	20.9	Upstream Structure Velocity (In- Governing) (ft/s)	7.19	7.62	7.19	3.50	99'9	3.50
Flow (cfs)	12.70	12.70	25.30	47.10	47.10	17.20	Upstream Structure Hydraulic Grade Line (In)	7,091.28	7,092.07	7,090.43	7,084.94	7,084.02	7,085.34
Rise (ft)							Headloss (ft)	0.04	0.72	4.31	0.04	0.08	90.0
Upstream Structure	15' CDOT TYPE R INI FT	15' CDOT TYPE R INLET	5' DIA TYPE II MH	5' CDOT TYPE R INLET	6' DIA TYPE II MH	10' CDOT TYPE R INLET	Hydraulic Grade Line (Out) (ft)	7,090.43	7,090.43	7,084,94	7,084.02	7,083.77	7,084.94
Label	PR6	PR5	PR7	PR9	PR9-1	PR8	Hydraulic Grade Line (In) (ft)	7,090.47	7,091.15	7,089.25	7,084.06	7,083.85	7,085.01







## STRM 4 POND 1 OUTFALL INDEX MAP

Outlet Structure (FSD Pond 1)

PR10

Sand Creek Channel

## Conduit FlexTable: STRM 4 POND 1 7-30-19

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
PR10	129	Outlet Structure (FSD Pond 1)	23.50	40.3	78.2	17.56	3.772	0.88	1.72	7,078.68	7,074.39	7,077.64	7,069.91	7.73	7,079.20
Upstream Structure Velocity (In- Governing)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)										

(ft/s)

8.17

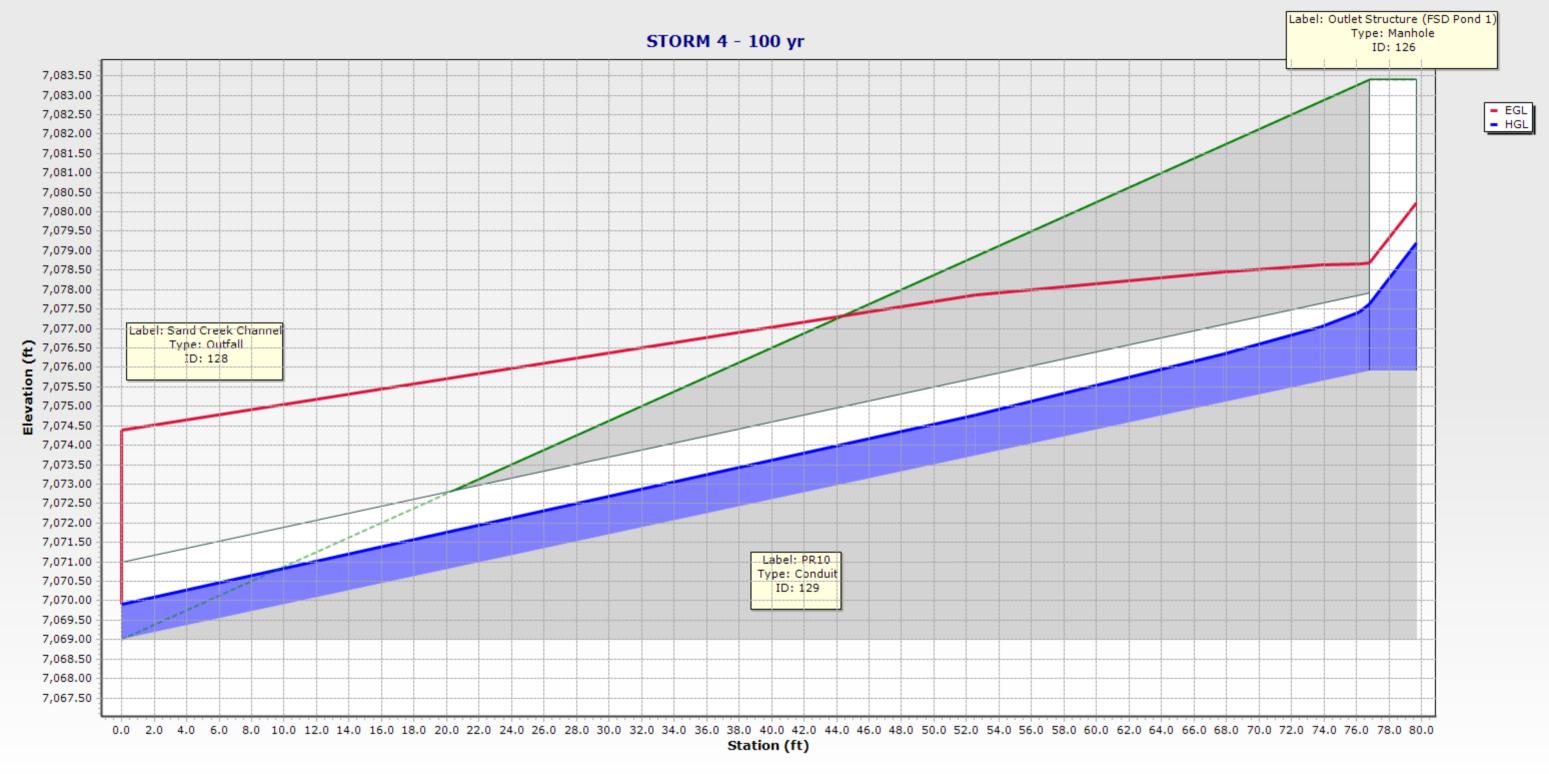
1.500

1.56

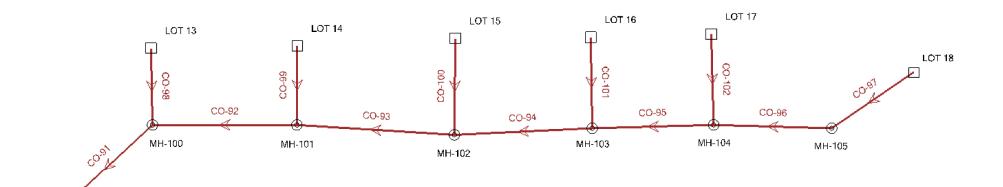
7,083.40

7,075.92

7,069.00



## **LOTS 13-18 INDEX MAP**



EX 54IN O-**1**3

## **Conduit FlexTable: LOTS 13-18**

	Conduct Fextualist 2010 10 10														
Label	ID	Upstream	Flow	Flow / Capacity	Length (Unified)	Velocity	Froude Number	Depth (Normal)	Depth (Critical)	Energy Grade	Energy Grade	Hydraulic Grade	Hydraulic Grade	Headloss	Upstream
		Structure	(cfs)	(Design)	(ft)	(ft/s)	(Normal)	(ft)	(ft)	Line (In)	Line (Out)	Line (In)	Line (Out)	(ft)	Structure
			` '	(%)	, ,	,	, ,	` '	` ,	(ft)	(ft)	(ft)	(ft)	. ,	Hydraulic Grade
															Line (In)
															(ft)
CO-91	346	MH-100	1.40	11.5	48.7	10.34	4.544	0.23	0.50	7,057.60	7,054.83	7,057.40	7,054.78	2.62	7,057.60
CO-92	348	MH-101	1.20	14.0	92.5	7.71	3.213	0.25	0.46	7,062.23	7,057.69	7,062.05	7,057.60	4.45	7,062.23
CO-93	350	MH-102	0.90	23.2	68.5	4.02	1.450	0.33	0.40	7,062.93	7,062.30	7,062.78	7,062.23	0.54	7,062.93
CO-94	352	MH-103	0.60	15.5	63.7	3.58	1.447	0.27	0.32	7,063.56	7,062.98	7,063.44	7,062.93	0.51	7,063.56
CO-95	354	MH-104	0.40	10.4	70.3	3.17	1.431	0.22	0.26	7,064.27	7,063.61	7,064.18	7,063.56	0.62	7,064.28
CO-96	356	MH-105	0.20	5.2	59.0	2.59	1.396	0.15	0.18	7,064.86	7,064.30	7,064.79	7,064.28	0.52	7,064.86
CO-97		LOT 18	0.20	12.4	17.3	5.60	3.407	0.12	0.22	7,066.74	7,065.82	7,066.65	7,065.33	1.33	7,066.78
CO-98		LOT 13	0.20	19.4	13.4	9.18	6.057	0.10	0.25	7,061.24	7,058.91	7,061.11	7,057.60	3.51	7,061.30
CO-99		LOT 14	0.30	22.9	11.4	5.41	2.775	0.16	0.28	7,063.11	7,062.78	7,063.00	7,062.36	0.64	7,063.17
CO-100		LOT 15	0.30	35.6	11.4	3.94	1.763	0.21	0.28	7,063.59	7,063.42	7,063.48	7,063.19	0.29	7,063.65
CO-101		LOT 16	0.20	9.3	11.4	6.86	4.501	0.10	0.22	7,065.46	7,064.55	7,065.37	7,063.82	1.55	7,065.50
CO-102	368	LOT 17	0.20	9.1	11.4	6.94	4.577	0.10	0.22	7,066.31	7,065.37	7,066.22	7,064.62	1.60	7,066.35
Upstream	Upstream	Upstream	Elevation Ground	Invert (Start)	Invert (Stop)										
Structure	Structure	Structure	(Start)	(ft)	(ft)										
Velocity (In-	Headloss	Headloss	(ft)												
Governing)	Coefficient	(ft)													
(ft/s)															
9.18	1.020	0.20	7,060.00	7,052.03	7,056.90										
2.06	1.020	0.18	7,064.83	7,057.00	7,061.59										
1.75	1.020	0.15	7,066.63	7,061.69	7,062.38										

1.69

1.26

5.60

2.35

2.82

2.69

2.69

2.35

2.35

1.020

1.020

1.020

1.500

1.500

1.500

1.500

1.500

1.500

0.12

0.09

0.06

0.13

0.19

0.17

0.17

0.13

0.13

7,066.67

7,068.56

7,068.56

7,069.29

7,064.83

7,066.63

7,066.67

7,068.56

7,068.56

7,062.48

7,063.22

7,064.02

7,065.21

7,057.50

7,062.19

7,062.98

7,063.72

7,064.52

7,063.12

7,063.92

7,064.61

7,066.43

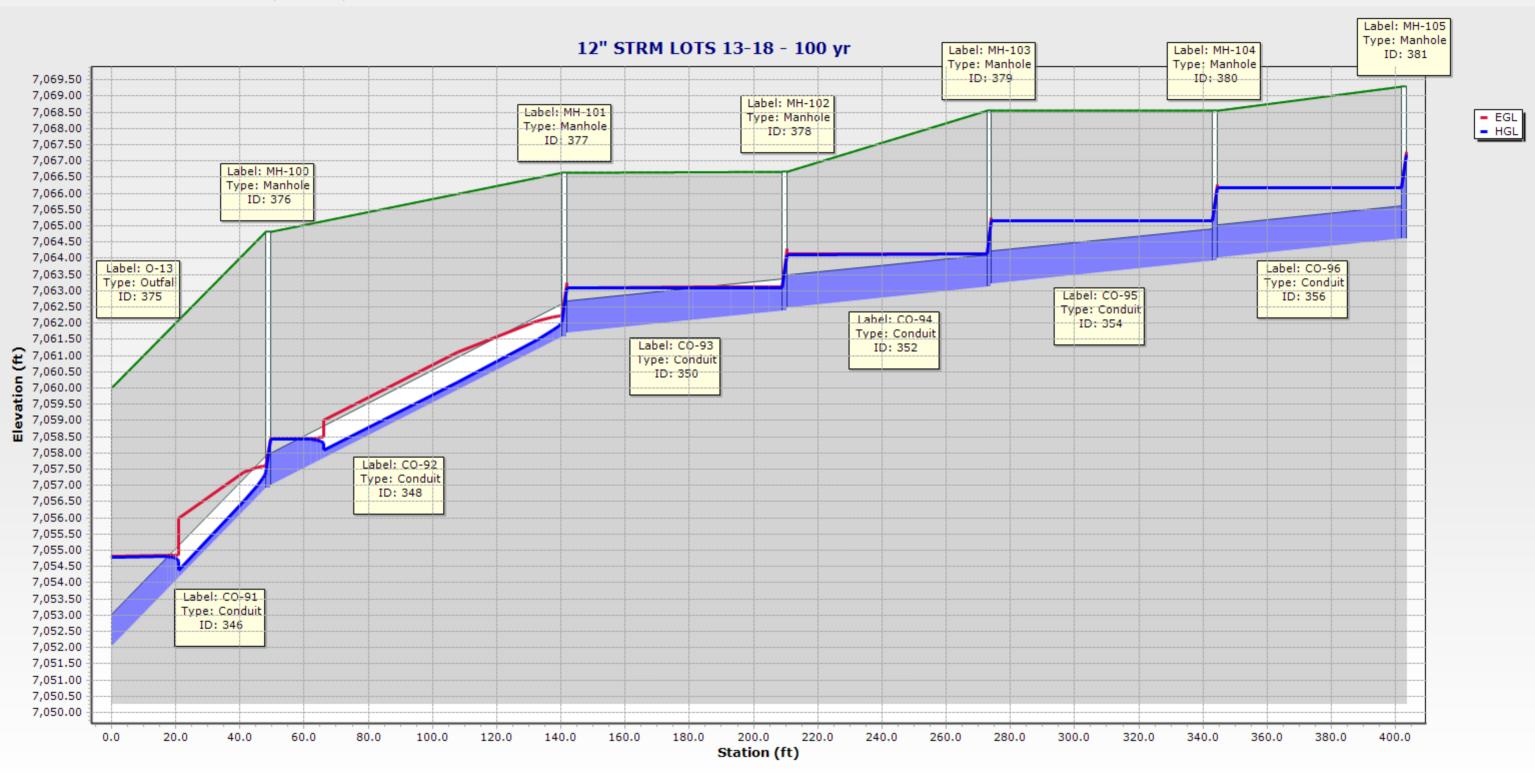
7,060.86

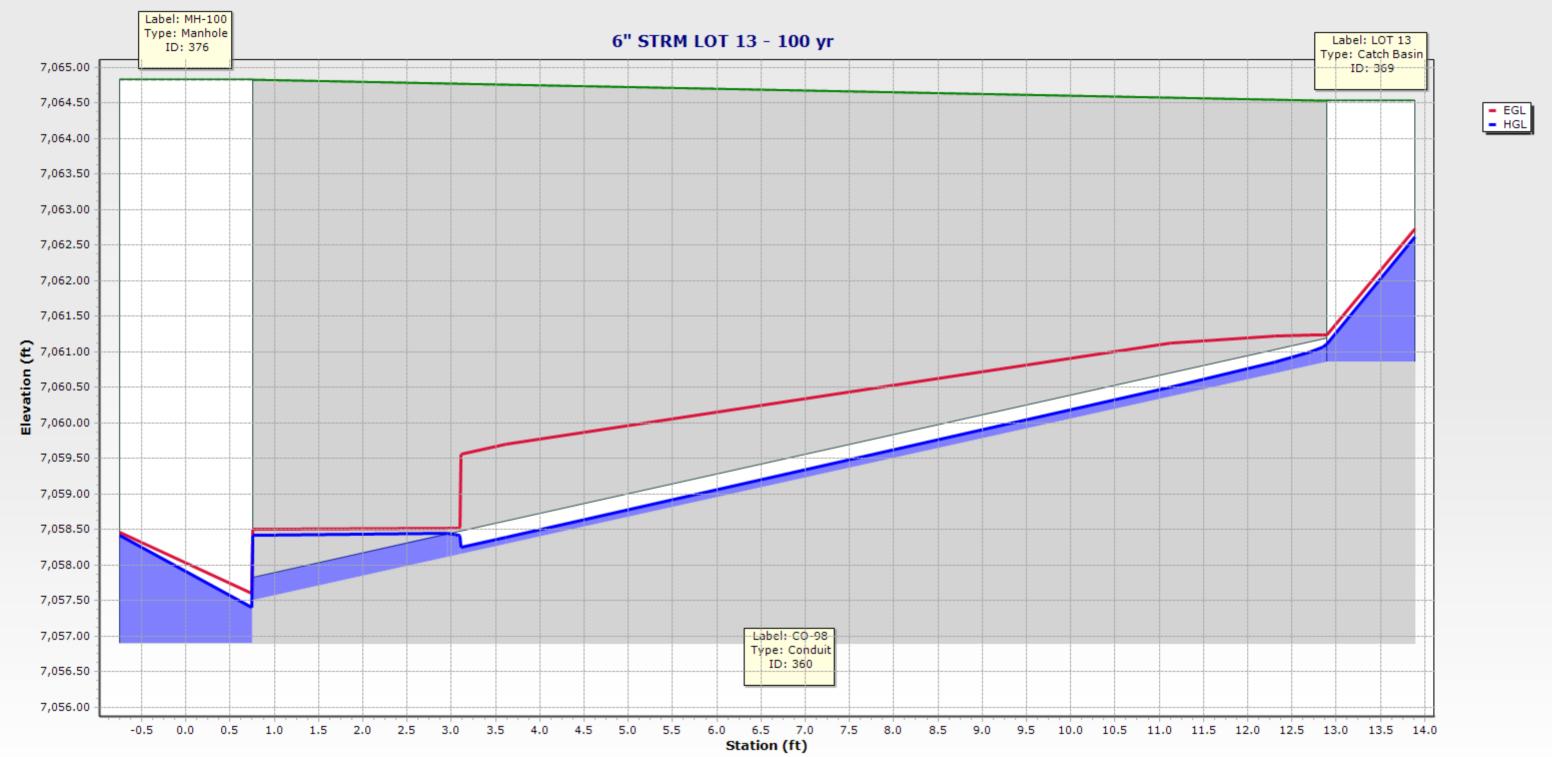
7,062.72

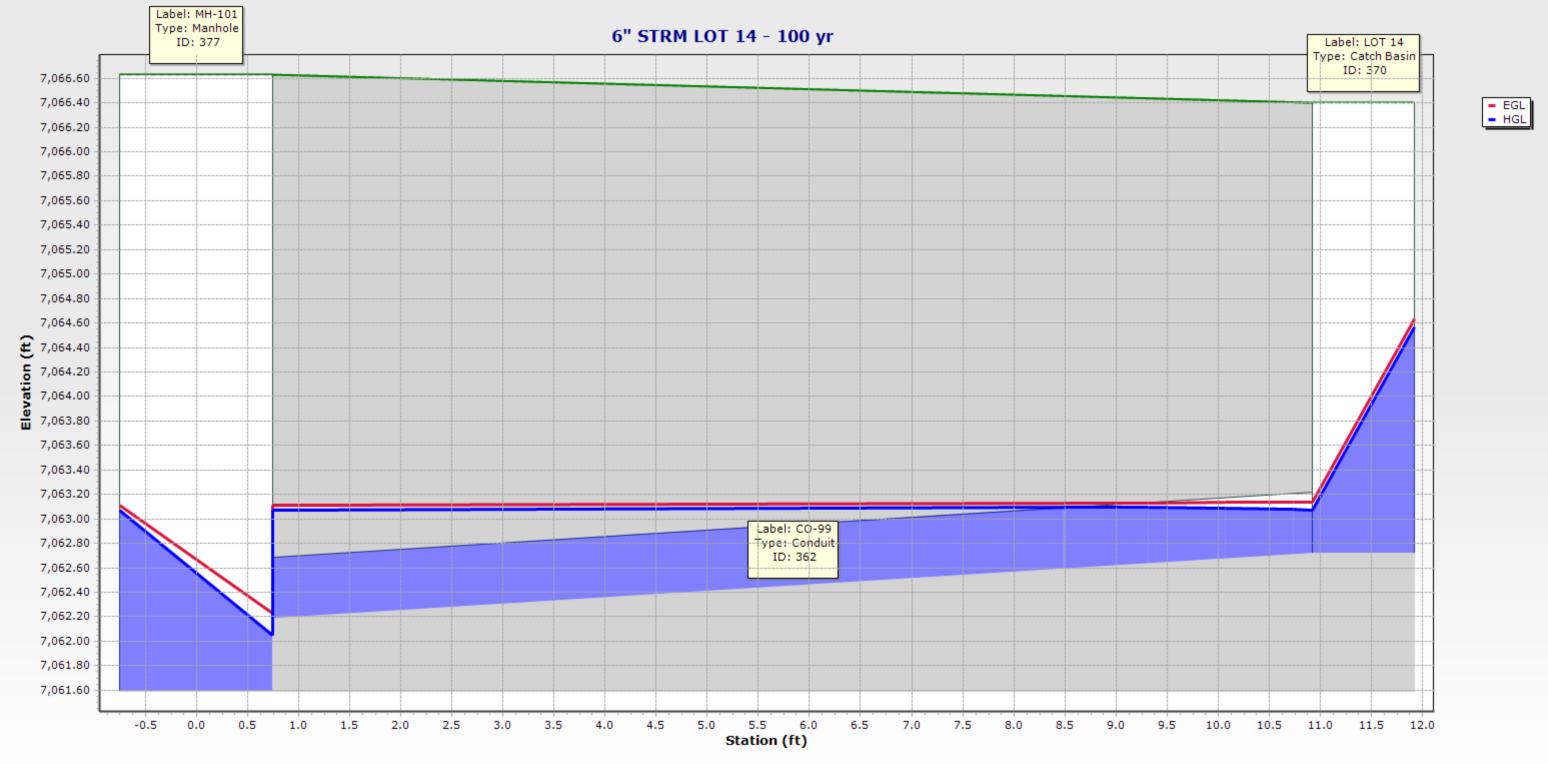
7,063.20

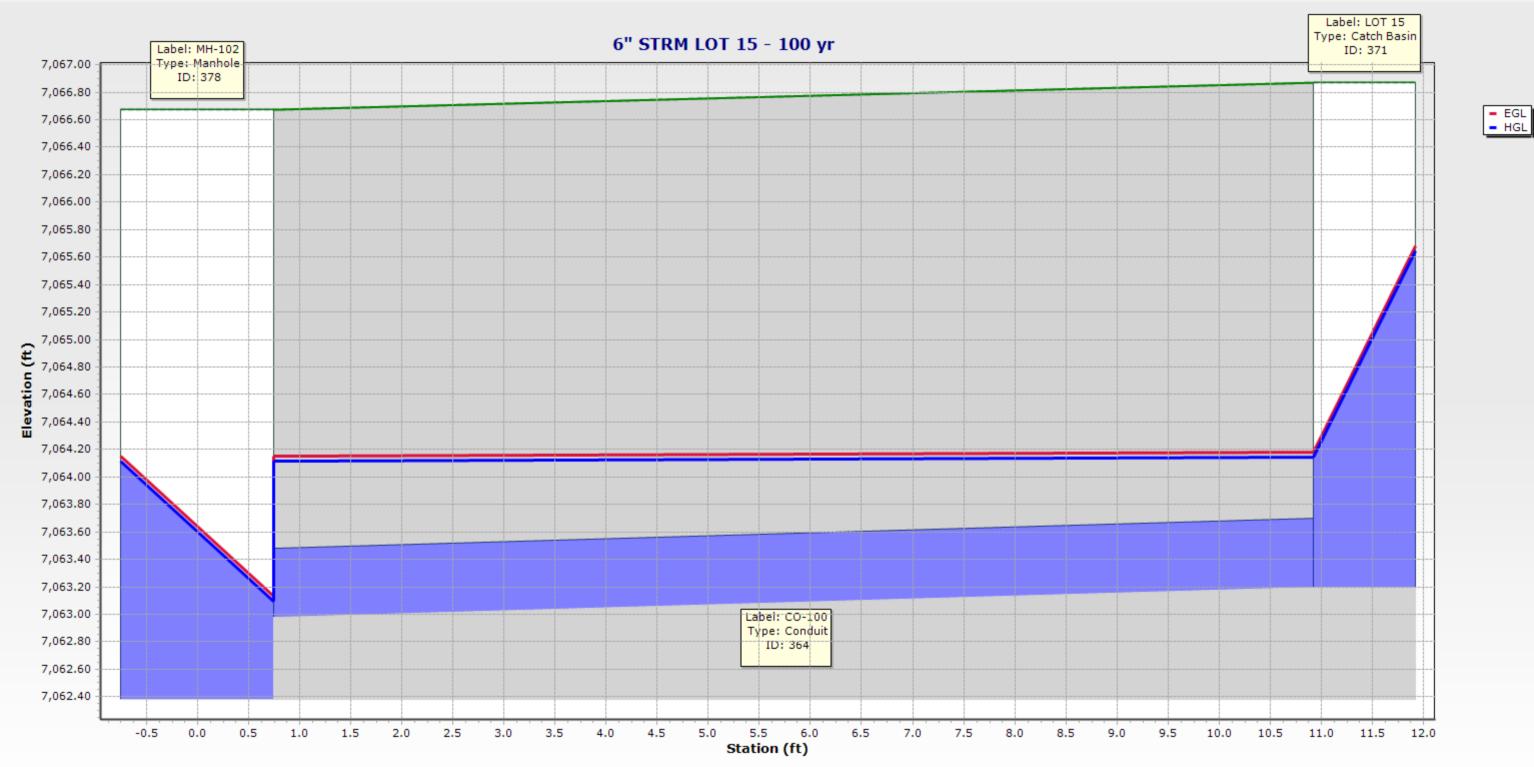
7,065.15

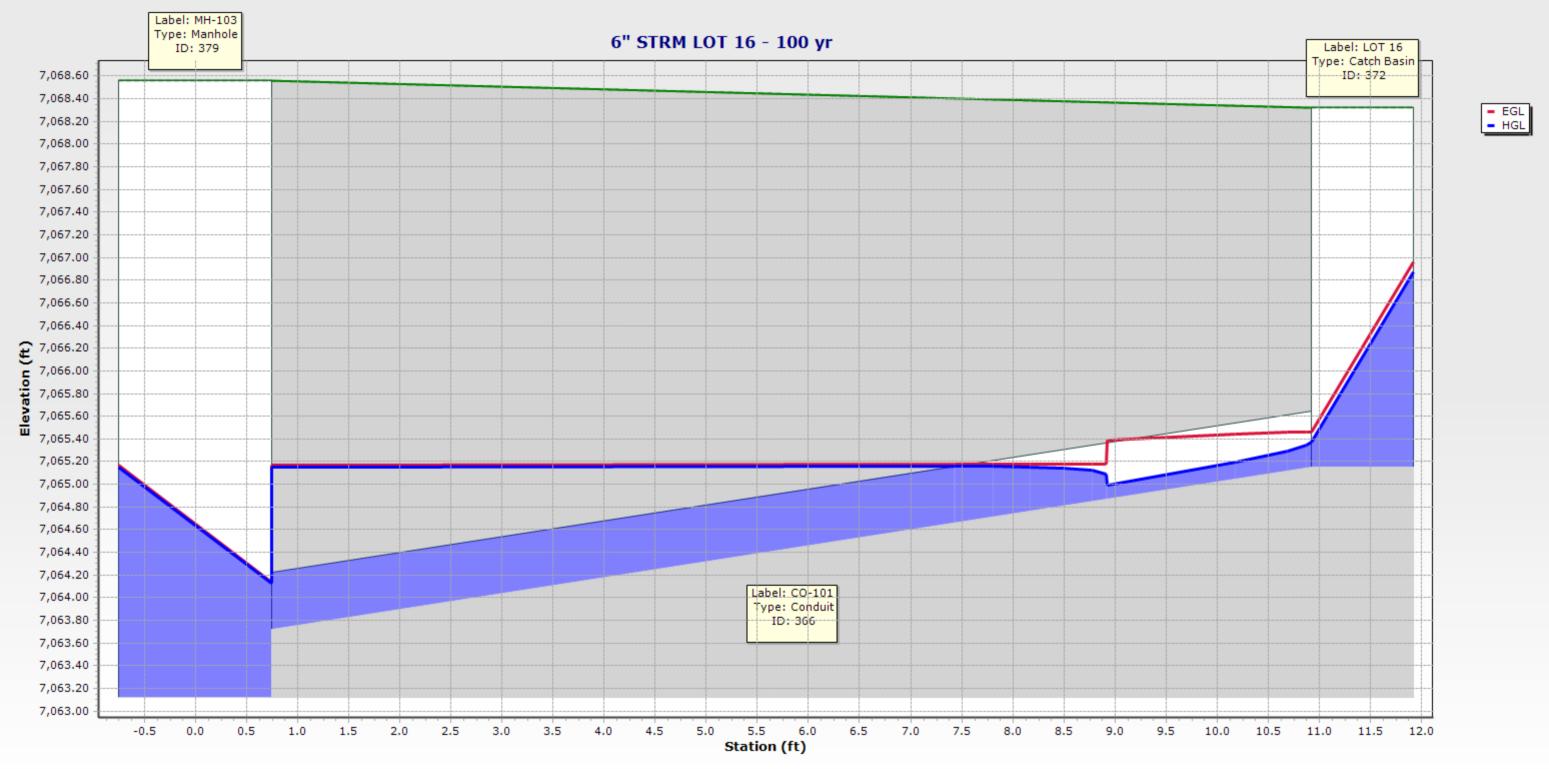
7,066.00

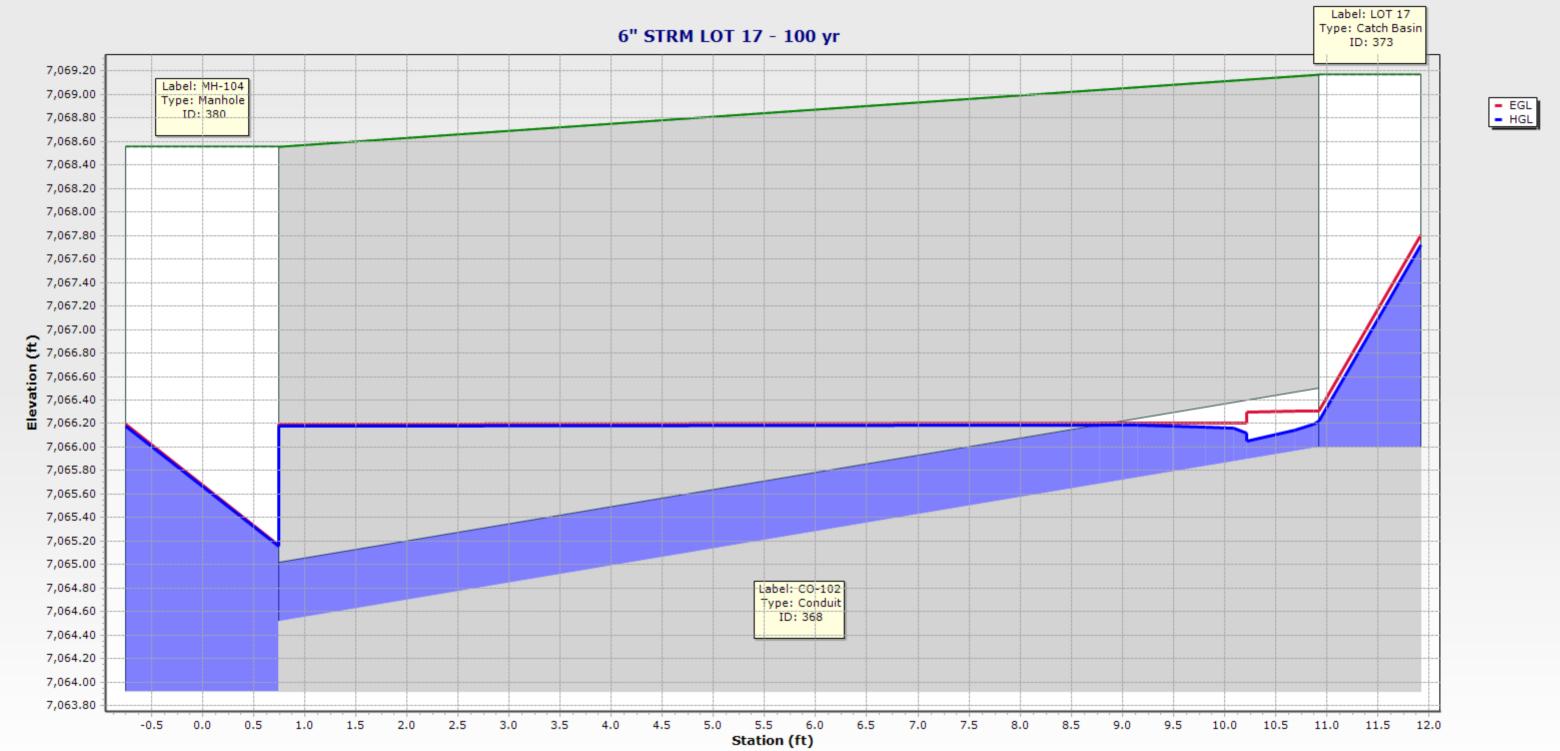


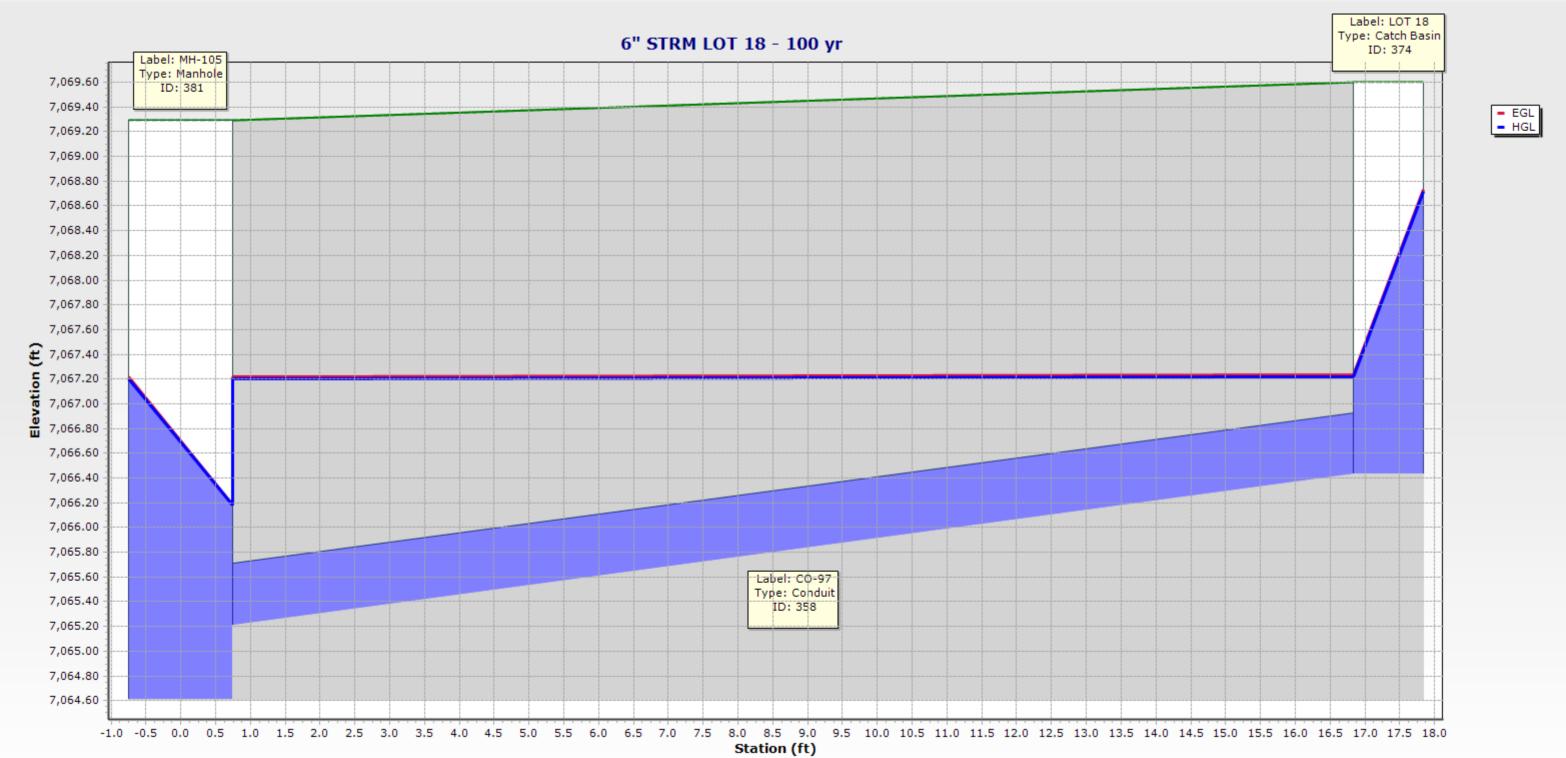


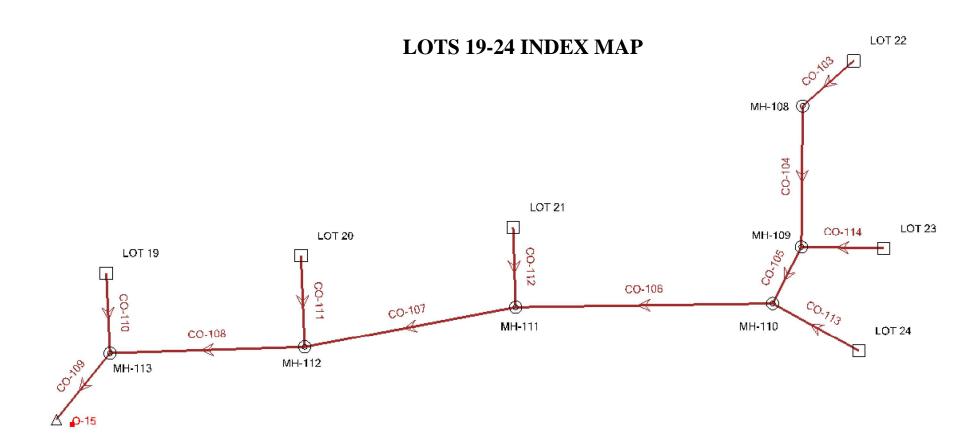












## **Conduit FlexTable: LOTS 19-24**

Label	ID	Upstream	Flow	Flow / Capacity	Length (Unified)	Velocity	Froude Number	Depth (Normal)	Depth (Critical)	Energy Grade	Energy Grade	Hydraulic Grade	Hydraulic Grade	Headloss	Upstream
		Structure	(cfs)	(Design)	(ft)	(ft/s)	(Normal)	(ft)	(ft)	Line (In)	Line (Out)	Line (In)	Line (Out)	(ft)	Structure
				(%)						(ft)	(ft)	(ft)	(ft)		Hydraulic Grade
															Line (In)
															(ft)
CO-103	400	LOT 22	0.30	26.4	8.3	4.87	2.391	0.18	0.28	7,076.34	7,076.16	7,076.23	7,075.85	0.38	7,077.73
CO-104	402	MH-108	0.30	7.1	56.4	3.10	1.543	0.18	0.23	7,075.46	7,074.94	7,075.39	7,074.93	0.45	7,075.47
CO-105	404	MH-109	0.60	4.4	12.0	8.64	4.839	0.14	0.32	7,074.93	7,073.52	7,074.81	7,073.47	1.34	7,074.93
CO-106	406	MH-110	0.90	7.6	61.7	8.88	4.338	0.19	0.40	7,073.47	7,067.75	7,073.32	7,067.67	5.64	7,073.47
CO-107	408	MH-111	1.10	20.3	68.8	5.40	2.026	0.31	0.44	7,067.67	7,066.37	7,067.50	7,066.28	1.22	7,067.67
CO-108	410	MH-112	1.30	25.0	82.9	5.51	1.946	0.34	0.48	7,066.28	7,064.83	7,066.09	7,064.73	1.36	7,066.28
CO-109	412	MH-113	1.50	6.1	26.1	17.27	8.934	0.17	0.52	7,064.73	7,056.75	7,064.52	7,056.69	7.83	7,064.73
CO-110		LOT 19	0.20	1.4	11.3	6.41	4.758	0.08	0.18	7,066.60	7,065.32	7,066.53	7,064.68	1.85	7,066.63
CO-111		LOT 20	0.20	24.0	12.8	3.49	1.763	0.17	0.22	7,066.76	7,066.56	7,066.67	7,066.38	0.30	7,066.80
CO-112		LOT 21	0.20	24.0	12.7	3.49	1.768	0.17	0.22	7,068.21	7,068.02	7,068.12	7,067.83	0.30	7,068.25
CO-113		LOT 24	0.30	39.5	19.2	3.64	1.576	0.22	0.28	7,074.21	7,073.94	7,074.10	7,073.74	0.36	7,074.27
CO-114	422	LOT 23	0.30	11.2	4.6	8.98	5.603	0.11	0.28	7,076.36	7,076.07	7,076.25	7,075.22	1.03	7,076.42
Upstream	Upstream	Upstream	Elevation Ground	Invert (Start)	Invert (Stop)										
Structure	Structure	Structure	(Start)	(ft)	(ft)										
Velocity (In-	Headloss	Headloss	(ft)												
Governing)	Coefficient	(ft)													
(ft/s)															
2.69	1.000	1.50	7,079.62	7,075.95	7,075.66										
4.53	1.020	0.08	7,080.13	7,075.16	7,074.49										
0.90	1.020	0.12	7,080.15	7,074.49	7,073.02										

0.15

0.17

0.19

0.21

0.10

0.13

0.13

0.17

0.17

7,078.40

7,071.56

7,069.39

7,068.00

7,069.52

7,069.62

7,071.57

7,077.49

7,079.64

7,072.92

7,067.06

7,065.61

7,064.00

7,066.35

7,066.45

7,067.90

7,073.82

7,075.97

7,067.16

7,065.71

7,064.10

7,053.50

7,064.60

7,066.21

7,067.66

7,073.52

7,075.09

1.75

2.22

2.36

6.41

2.02

2.35

2.35

2.69

2.69

1.020

1.020

1.020

1.020

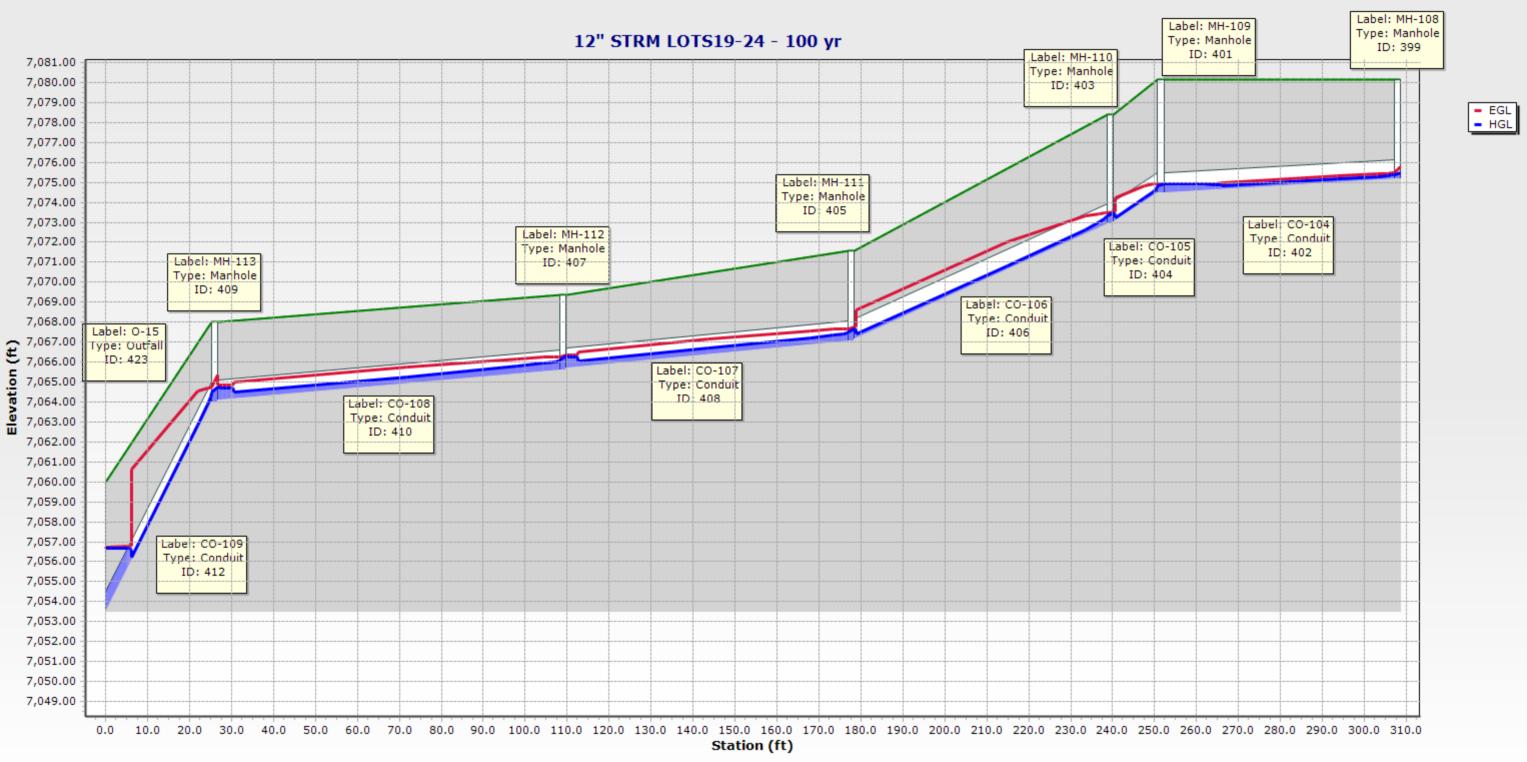
1.500

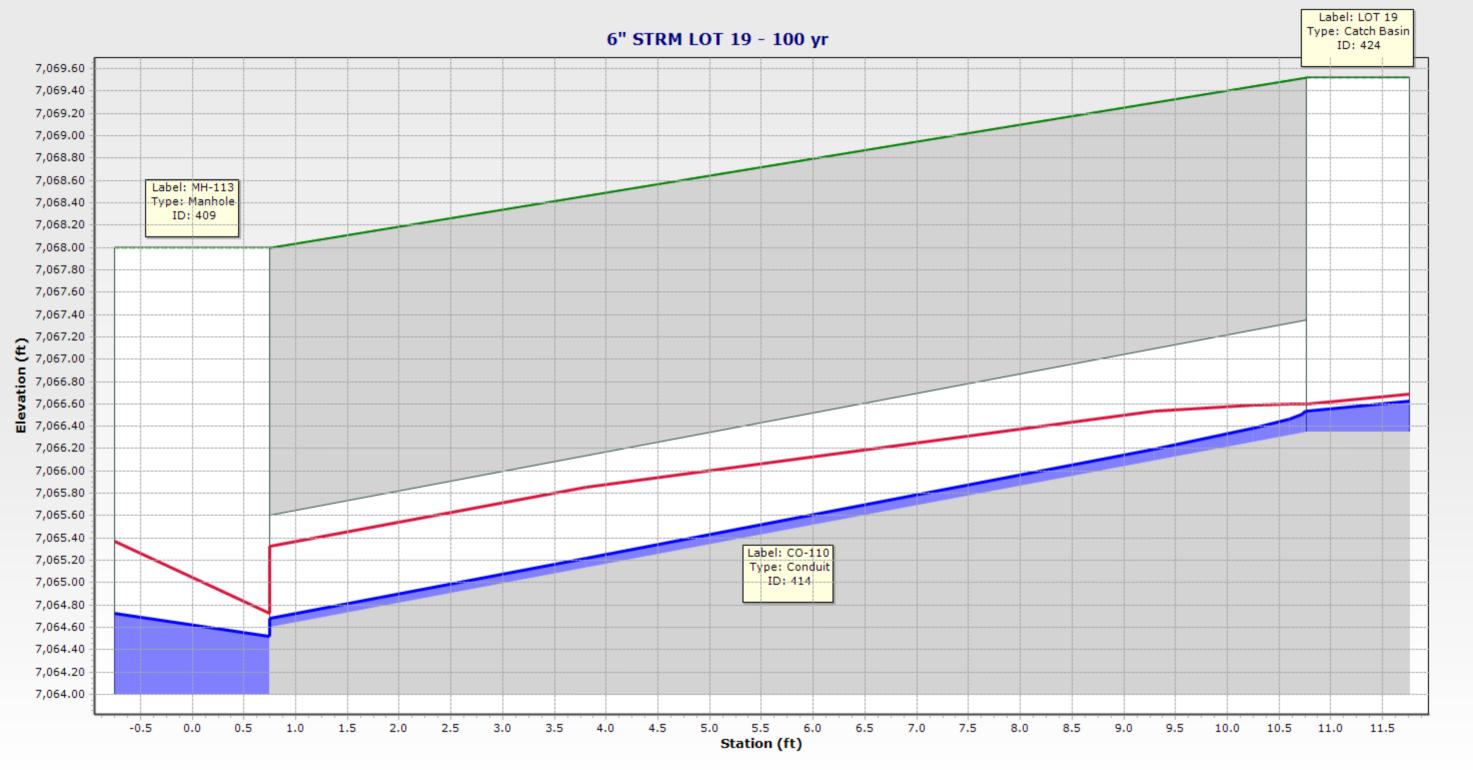
1.500

1.500

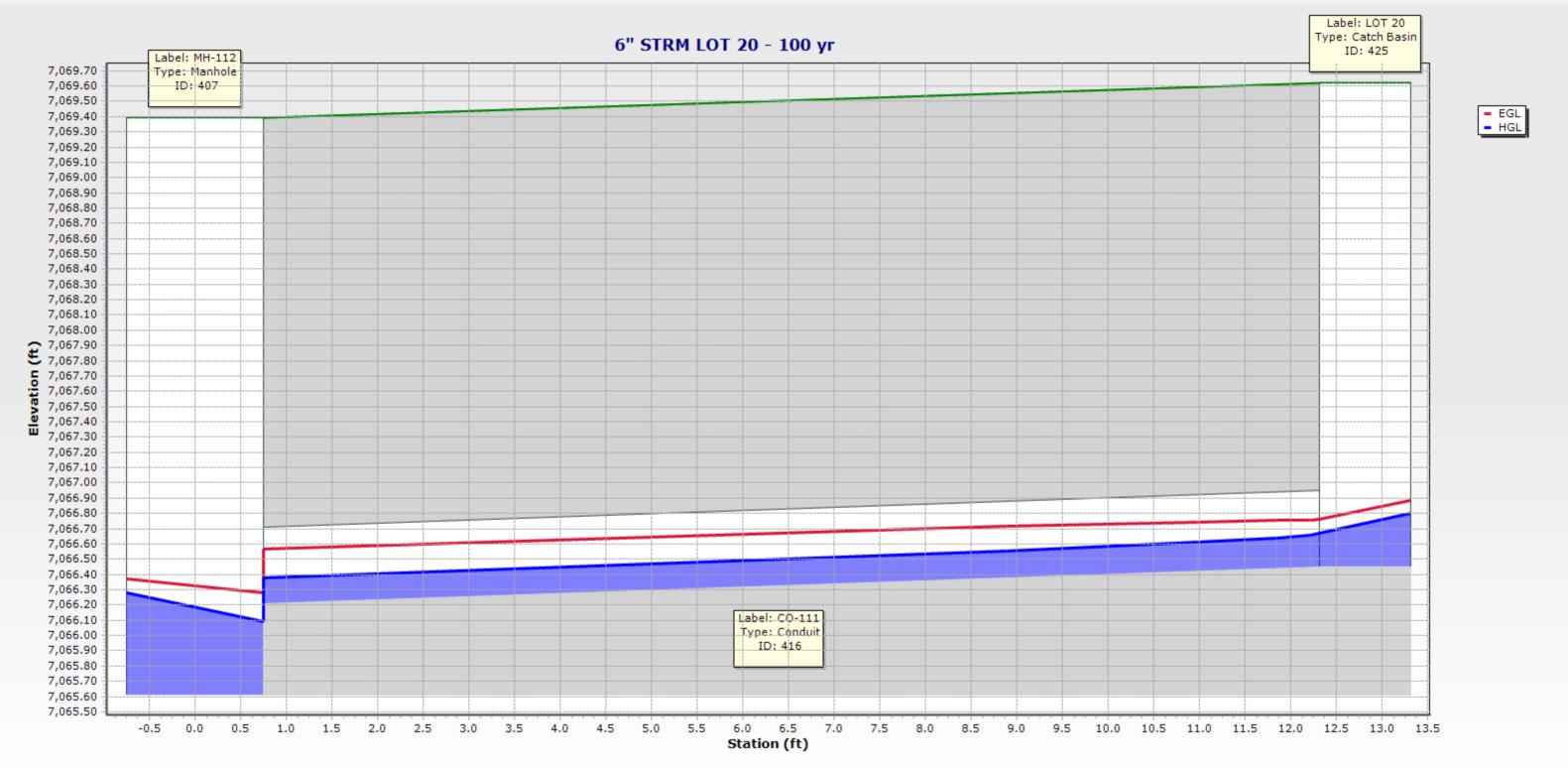
1.500

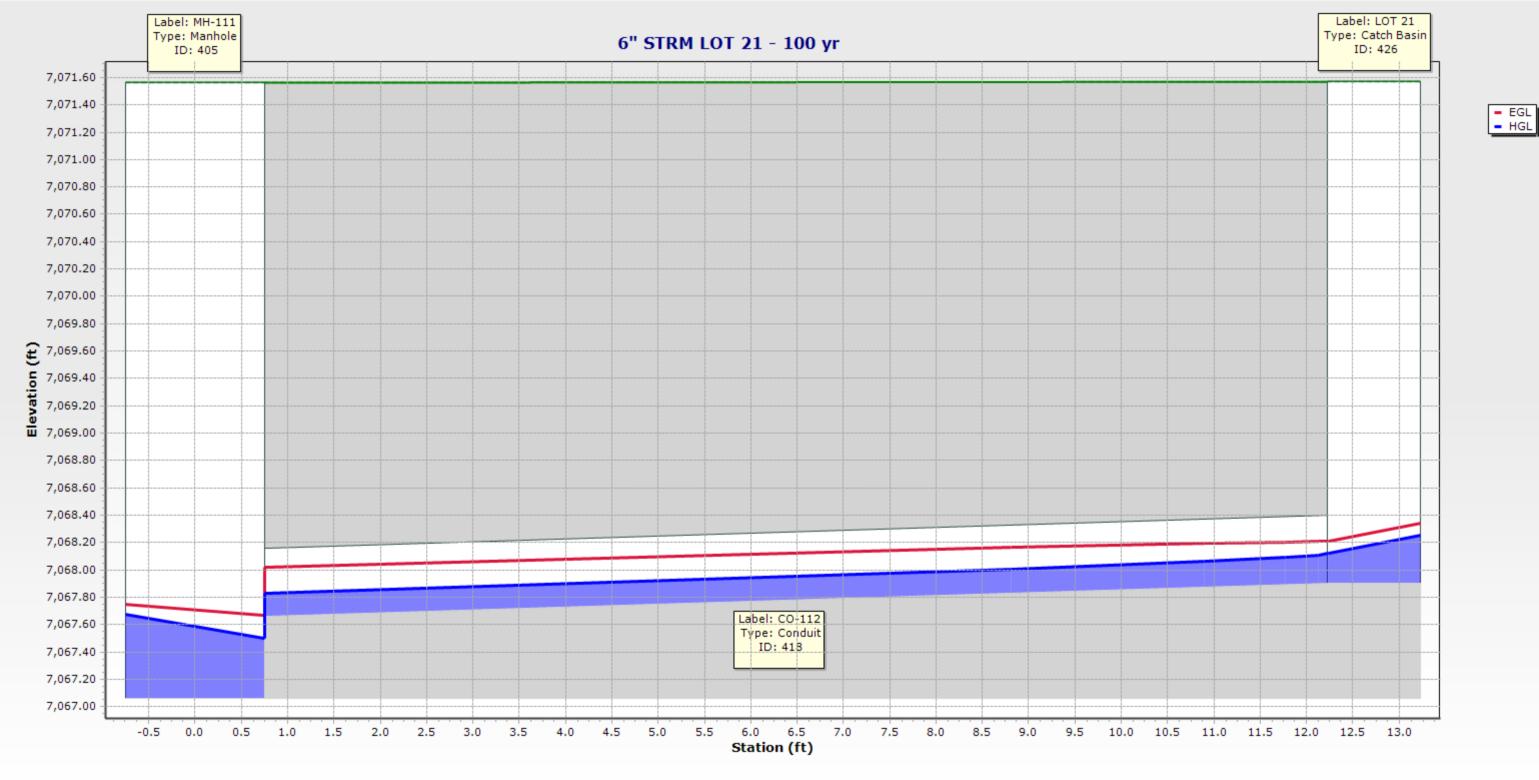
1.500

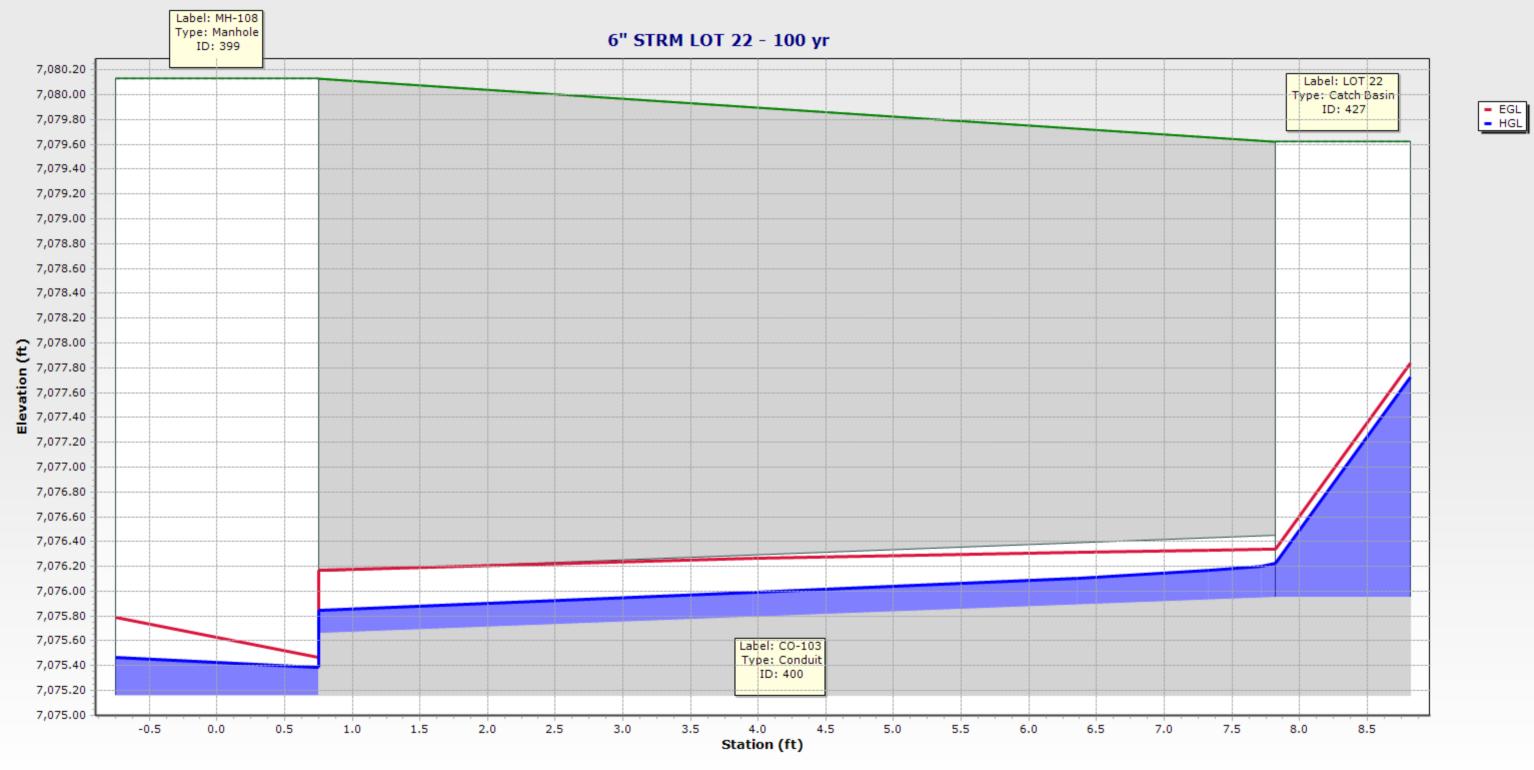


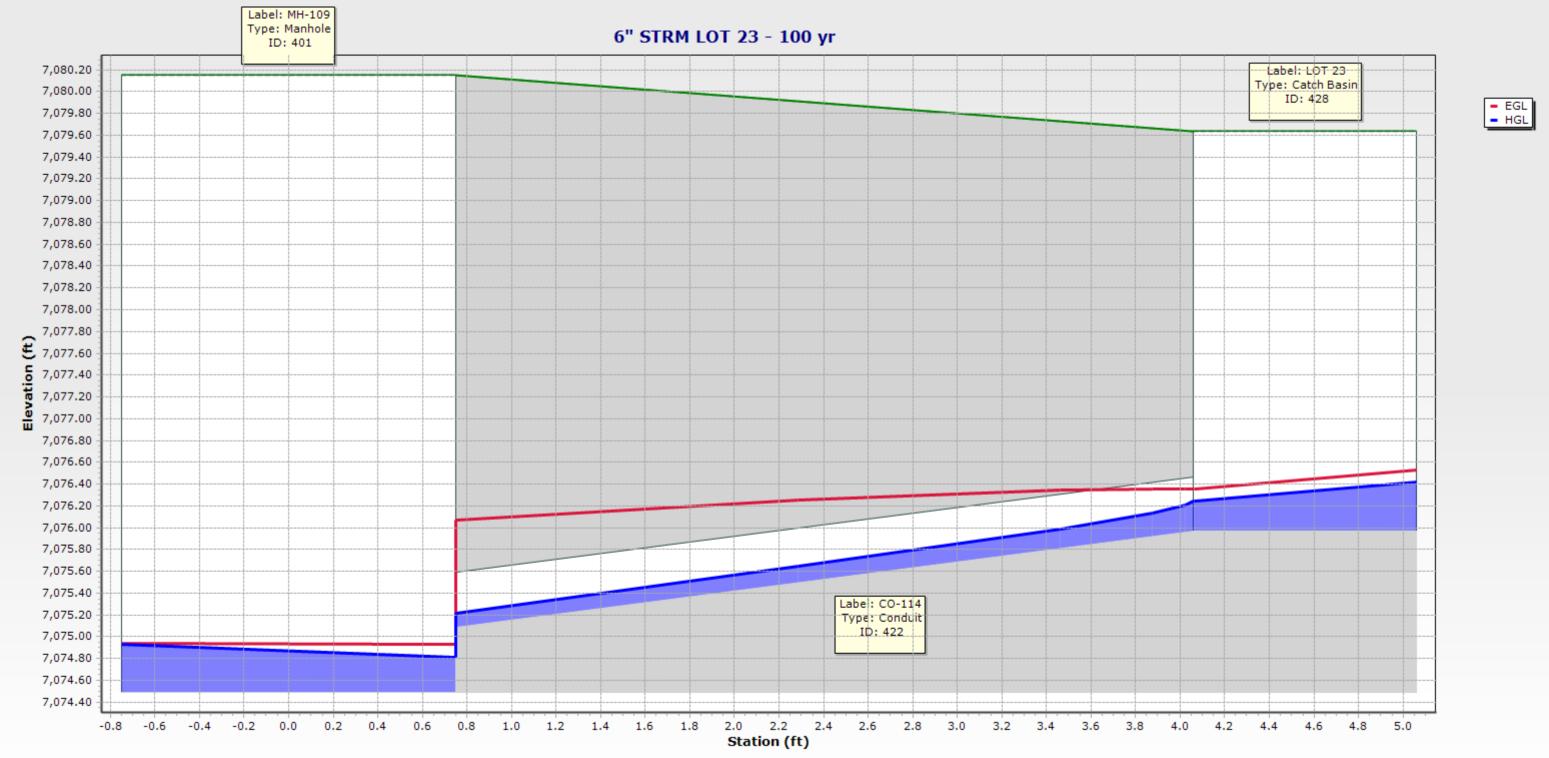


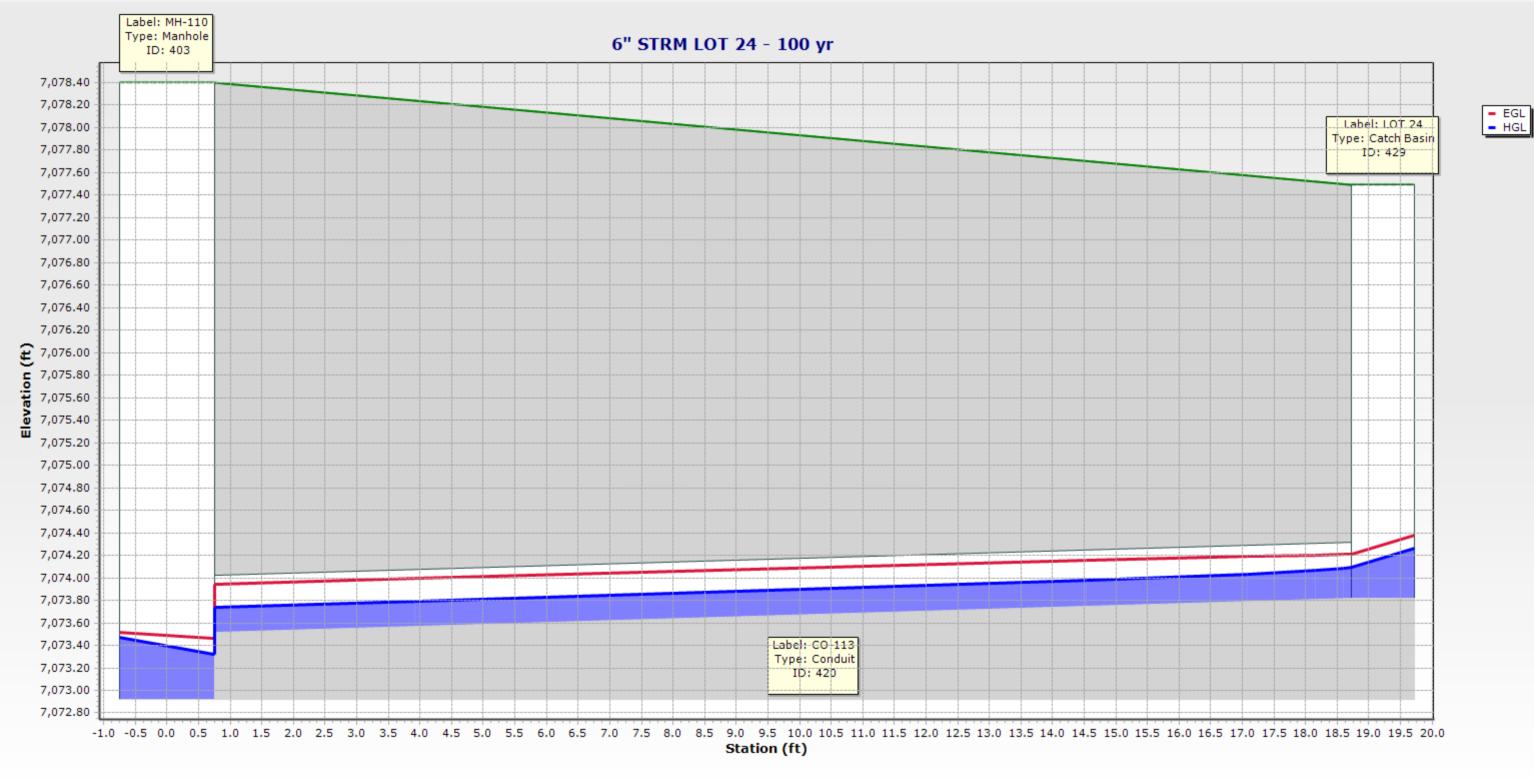


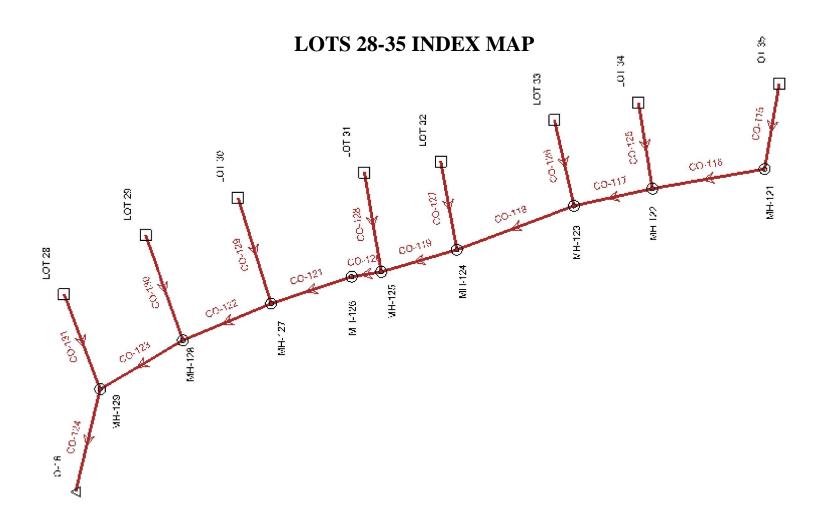








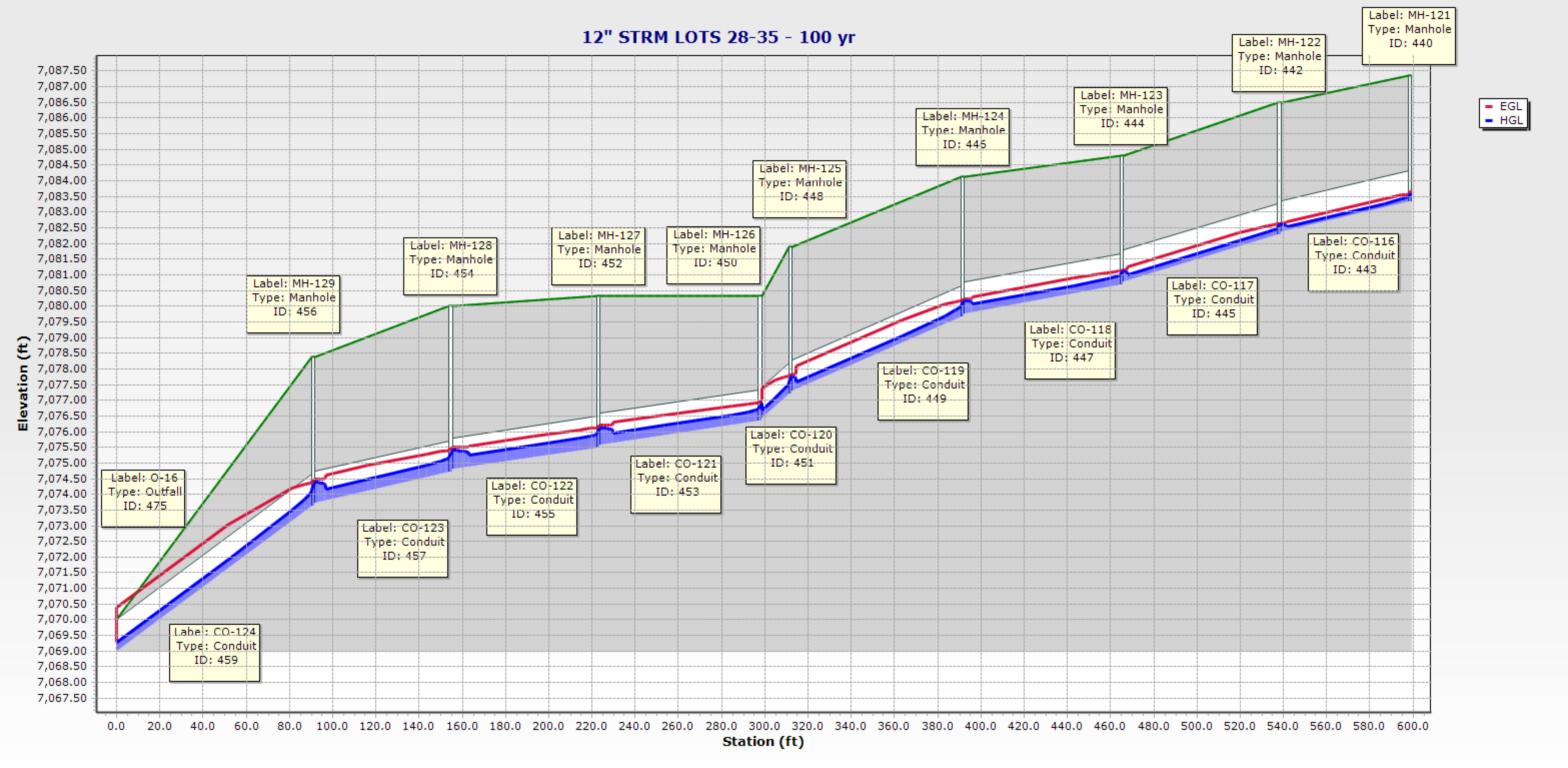


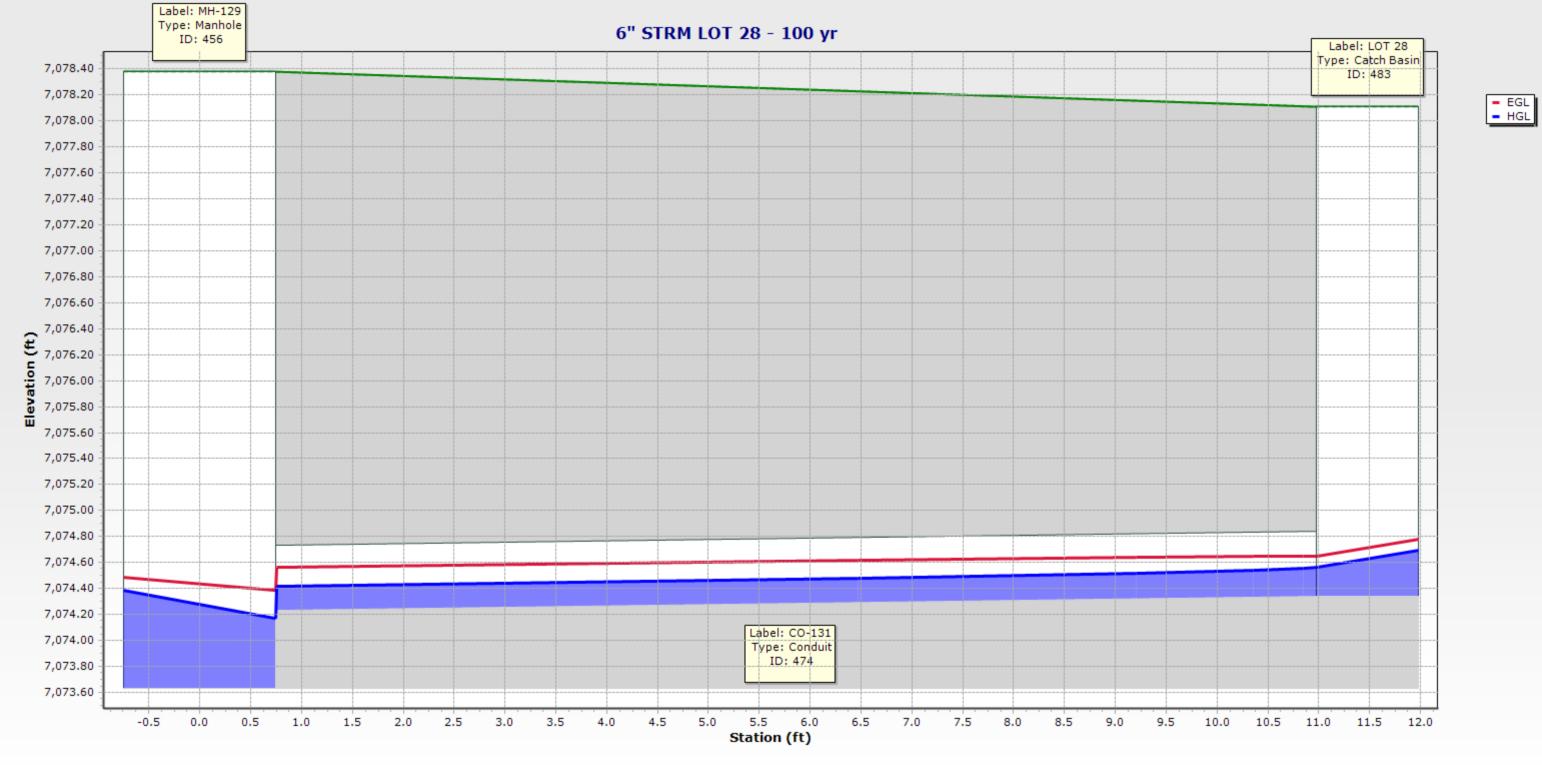


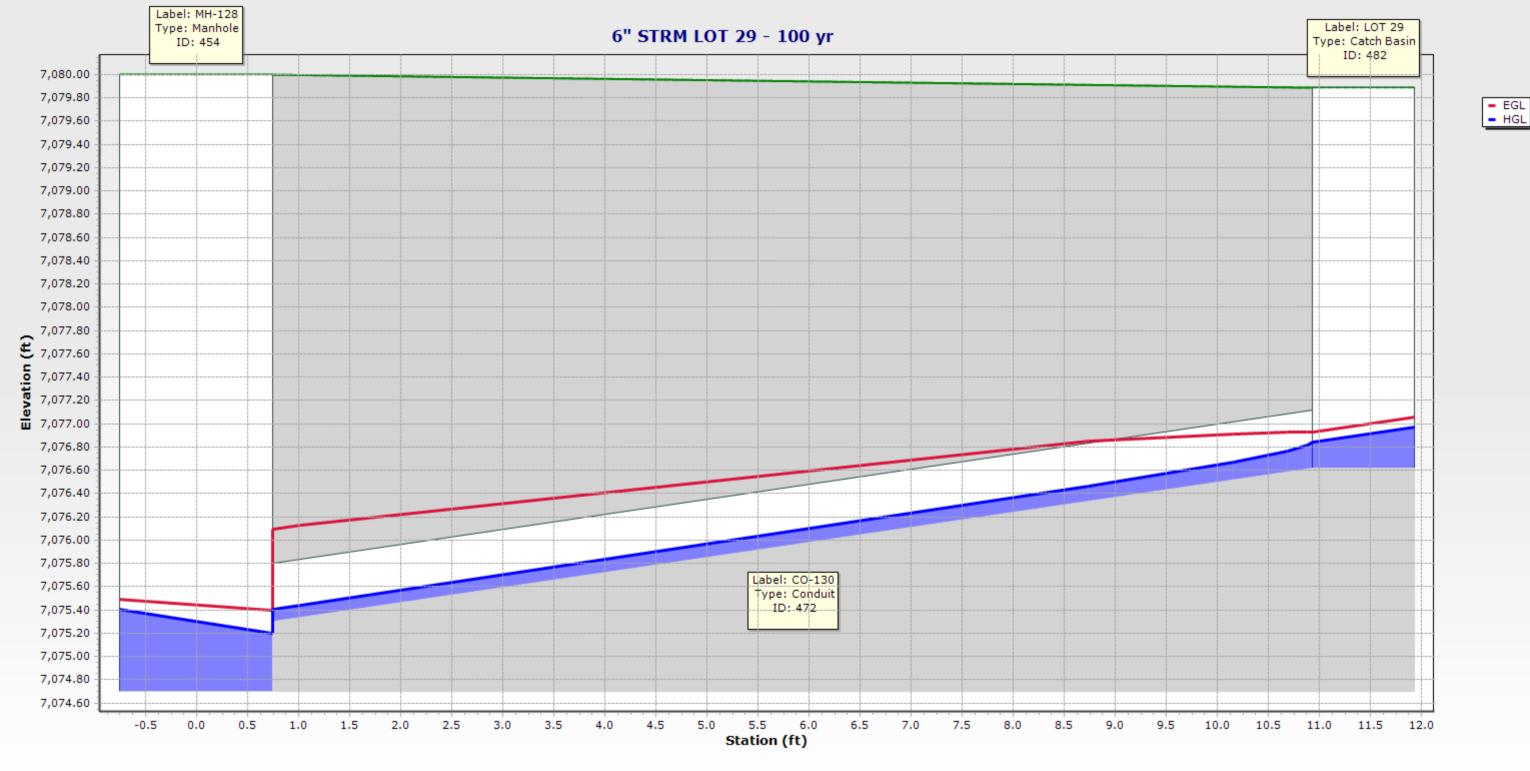
## **Conduit FlexTable: LOTS 28-35**

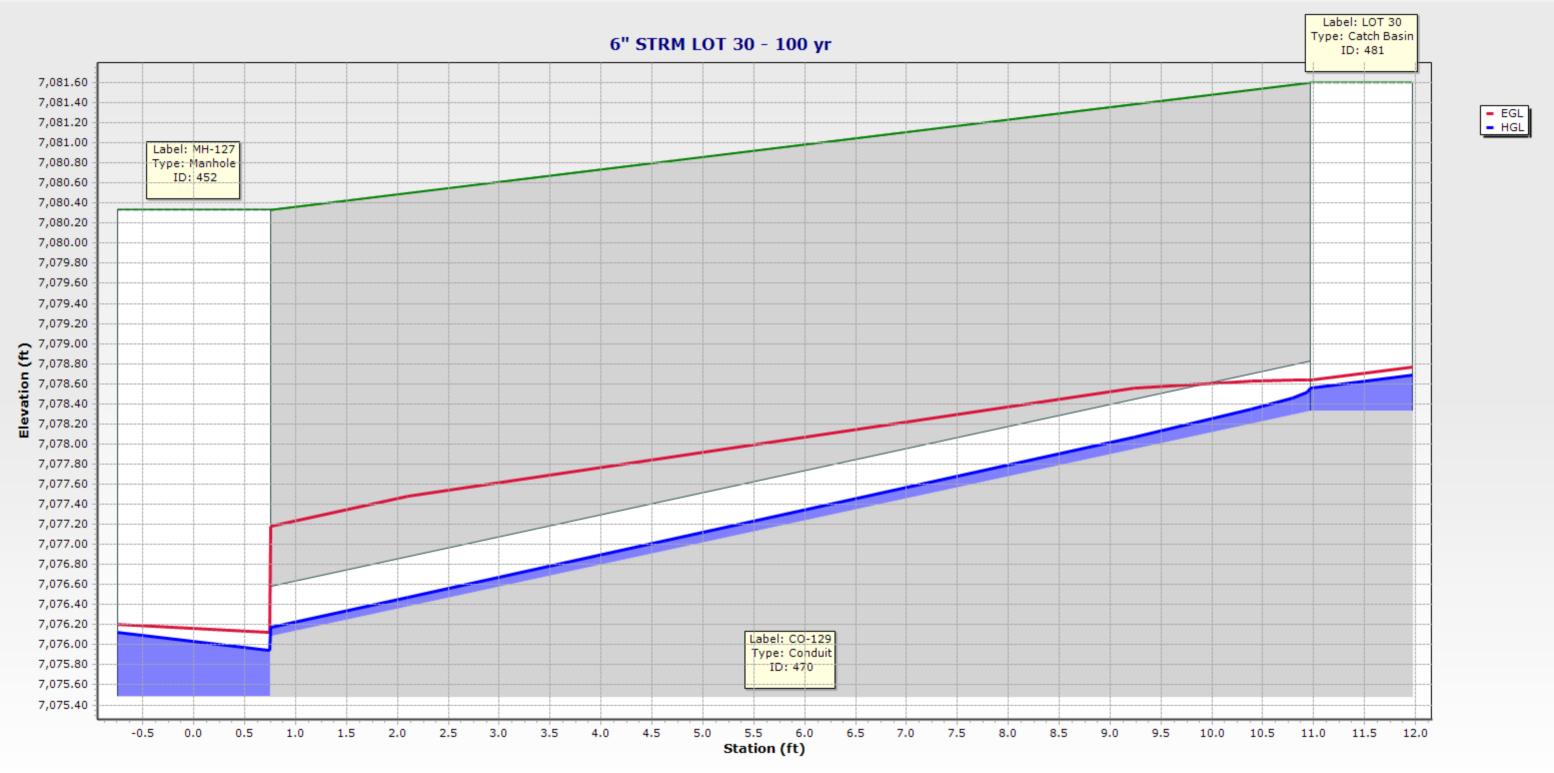
_	Conduit Fick Table! 20 Co														
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In)
															(ft)
CO-115	441	LOT 35	0.20	32.9	24.9	2.78	1.278	0.20	0.22	7,084.48	7,084.24	7,084.39	7,084.12	0.28	7,084.52
CO-116	443	MH-121	0.20	4.1	60.4	3.05	1.741	0.14	0.18	7,083.57	7,082.64	7,083.50	7,082.62	0.89	7,083.57
CO-117	445	MH-122	0.40	7.3	73.1	4.07	2.015	0.18	0.26	7,082.61	7,081.17	7,082.52	7,081.12	1.40	7,082.62
CO-118	447	MH-123	0.60	13.9	73.5	3.87	1.614	0.25	0.32	7,081.12	7,080.23	7,081.00	7,080.18	0.83	7,081.12
CO-119	449	MH-124	0.80	12.0	79.5	5.72	2.483	0.23	0.37	7,080.17	7,077.84	7,080.03	7,077.77	2.26	7,080.18
CO-120	451	MH-125	1.00	11.2	14.2	7.51	3.319	0.23	0.42	7,077.77	7,077.02	7,077.61	7,076.91	0.70	7,077.77
CO-121	453	MH-126	1.00	21.5	74.7	4.71	1.738	0.32	0.42	7,076.91	7,076.21	7,076.75	7,076.12	0.63	7,076.91
CO-122	455	MH-127	1.20	31.2	68.5	4.33	1.430	0.38	0.46	7,076.12	7,075.49	7,075.94	7,075.40	0.54	7,076.12
CO-123	457	MH-128	1.40	29.4	63.6	5.28	1.776	0.37	0.50	7,075.40	7,074.49	7,075.20	7,074.39	0.81	7,075.40
CO-124	459	MH-129	1.60	18.4	91.1	8.44	3.258	0.29	0.54	7,074.38	7,070.40	7,074.17	7,069.29	4.88	7,074.39
CO-125		LOT 34	0.20	32.6	11.8	2.80	1.288	0.20	0.22	7,083.29	7,083.18	7,083.20	7,083.06	0.15	7,083.33
CO-126		LOT 33	0.20	32.4	10.7	2.81	1.297	0.20	0.22	7,081.70	7,081.60	7,081.61	7,081.48	0.14	7,081.74
CO-127		LOT 32	0.20	23.8	11.0	3.51	1.779	0.17	0.22	7,080.78	7,080.61	7,080.69	7,080.43	0.27	7,080.82
CO-128		LOT 31	0.20	14.2	11.4	5.08	2.976	0.13	0.22	7,078.71	7,078.31	7,078.62	7,077.92	0.71	7,078.75
CO-129	470	LOT 30	0.20	7.4	11.5	8.06	5.616	0.09	0.22	7,078.64	7,077.18	7,078.55	7,076.17	2.38	· ·
CO-130		LOT 29	0.20	9.7	11.4	6.66	4.328	0.11	0.22	7,076.93	7,076.09	7,076.84	7,075.41	1.44	7,076.97
CO-131	474	LOT 28	0.20	28.0	11.5	3.12	1.509	0.18	0.22	7,074.65	7,074.56	7,074.56	7,074.41	0.15	7,074.69
Upstream Structure Velocity (In-	Upstream Structure Headloss	Upstream Structure Headloss	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)										

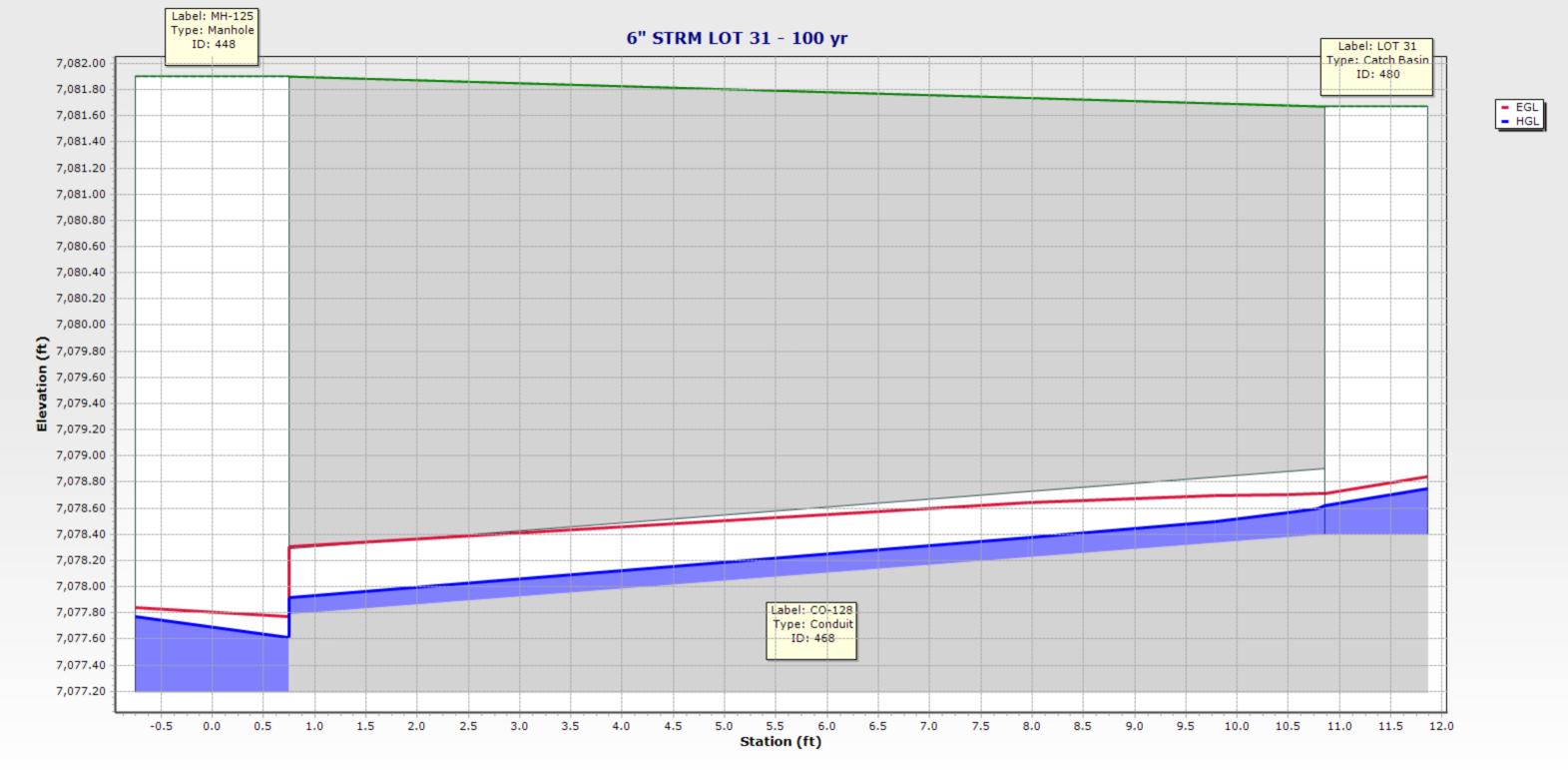
CO 131	17 1	LO1 20	0.20	20.0	11.5
Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)
2.35	1.500	0.13	7,087.44	7,084.17	7,083.92
2.78	1.020	0.06	7,087.35	7,083.32	7,082.36
1.26	1.020	0.09	7,086.48	7,082.26	7,080.78
1.69	1.020	0.12	7,084.80	7,080.68	7,079.76
1.95	1.020	0.14	7,084.14	7,079.66	7,077.29
2.14	1.020	0.16	7,081.90	7,077.19	7,076.43
2.67	1.020	0.16	7,080.33	7,076.33	7,075.58
2.29	1.020	0.18	7,080.33	7,075.48	7,074.80
2.43	1.020	0.20	7,080.00	7,074.70	7,073.73
2.56	1.020	0.22	7,078.38	7,073.63	7,069.00
2.35	1.500	0.13	7,086.25	7,082.98	7,082.86
2.35	1.500	0.13	7,084.66	7,081.39	7,081.28
2.35	1.500	0.13	7,083.74	7,080.47	7,080.26
2.35	1.500	0.13	7,081.67	7,078.40	7,077.79
2.35	1.500	0.13	7,081.60	7,078.33	7,076.08
2.35	1.500	0.13	7,079.89	7,076.62	7,075.30
2.35	1.500	0.13	7,078.11	7,074.34	7,074.23

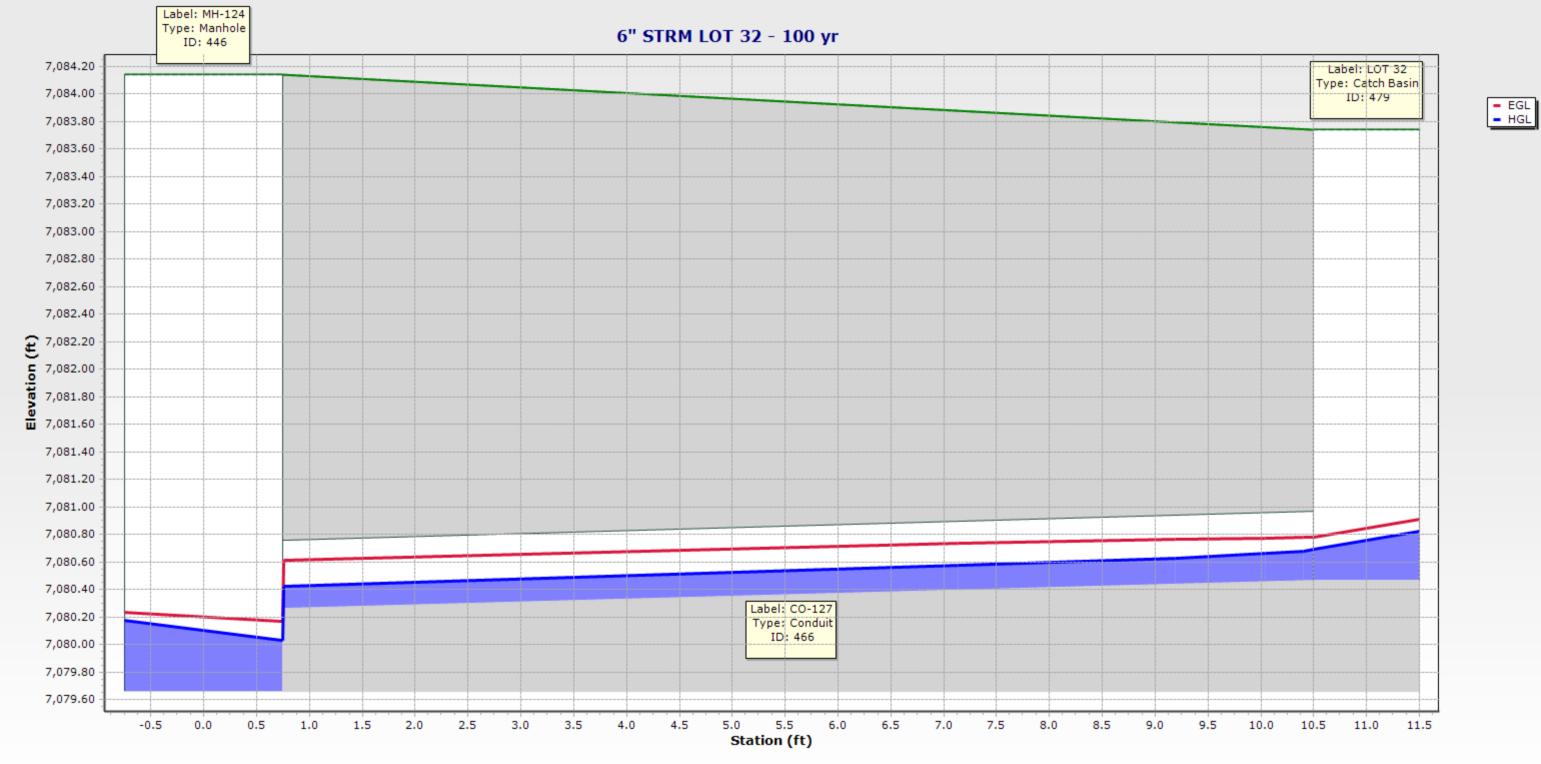


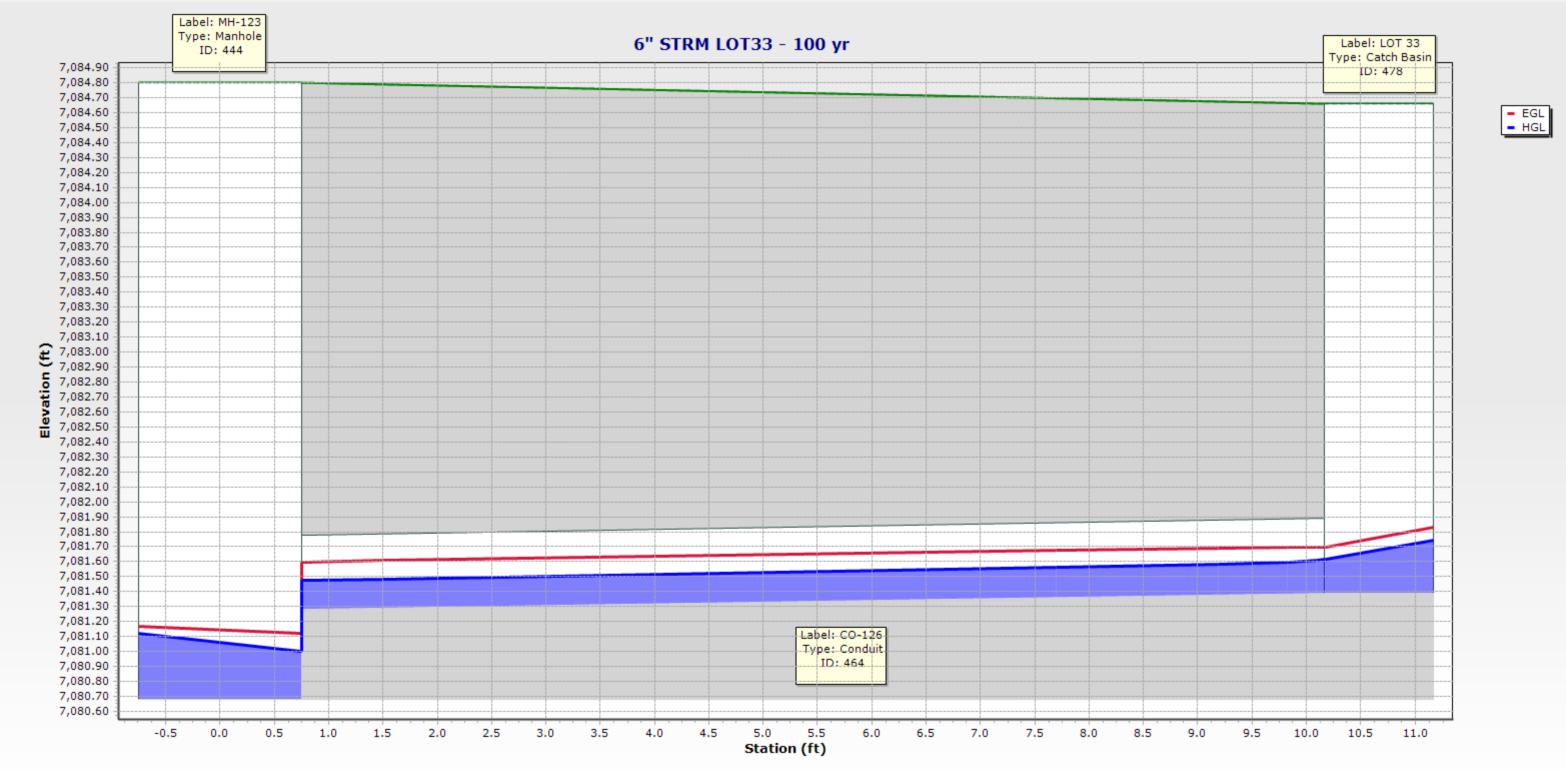


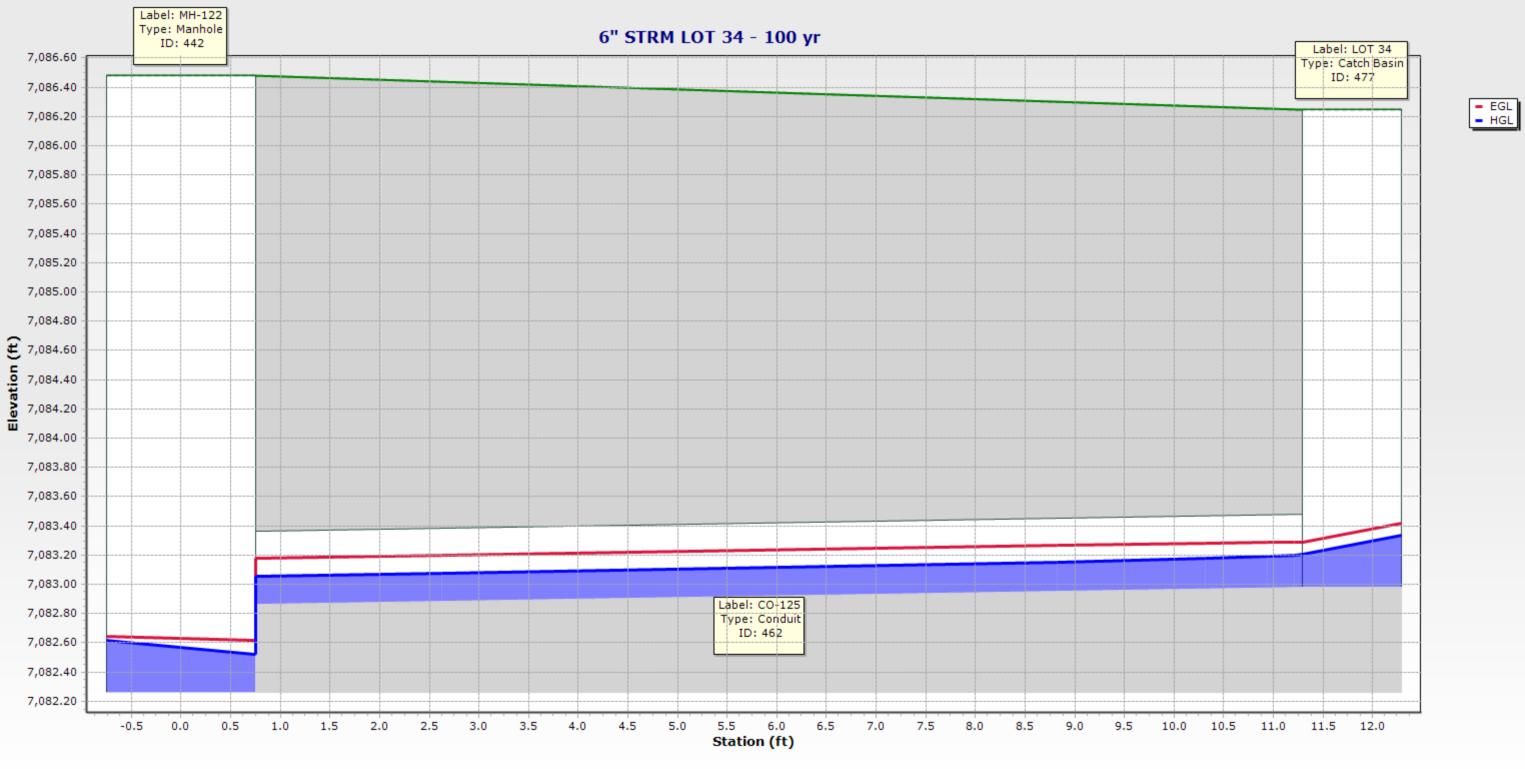


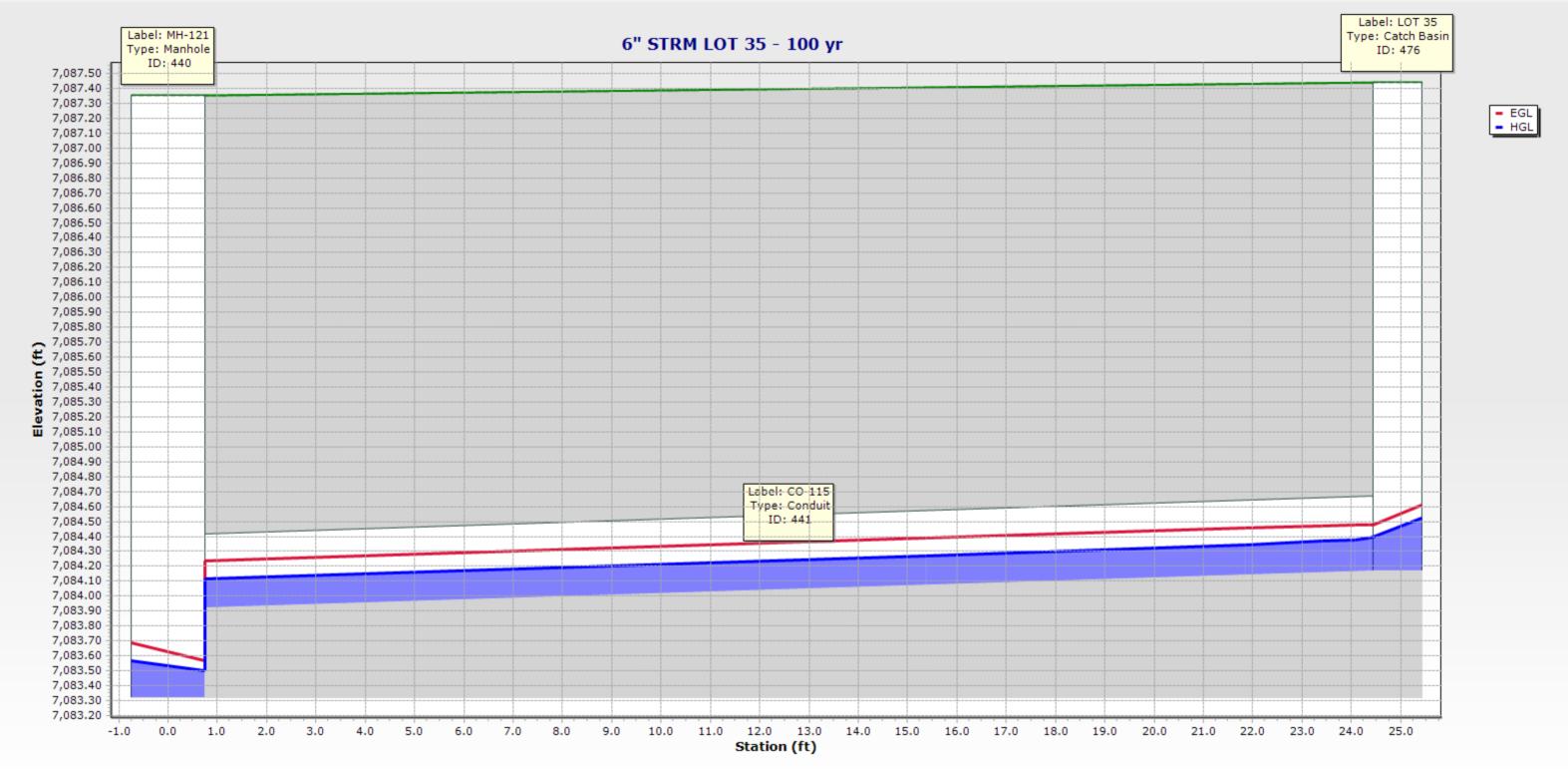




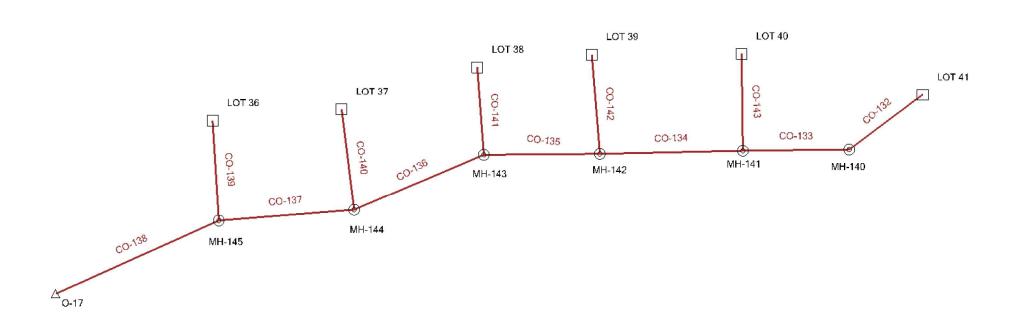








# **LOTS 36-41 INDEX MAP**



## **Conduit FlexTable: LOTS 36-41**

	_							CA I abici E							
Label	ID	Upstream	Flow	Flow / Capacity	Length (Unified)	Velocity	Froude Number	Depth (Normal)	Depth (Critical)	Energy Grade	Energy Grade	Hydraulic Grade	Hydraulic Grade	Headloss	Upstream
		Structure	(cfs)	(Design)	(ft)	(ft/s)	(Normal)	(ft)	(ft)	Line (In)	Line (Out)	Line (In)	Line (Out)	(ft)	Structure
				(%)						(ft)	(ft)	(ft)	(ft)		Hydraulic Grade
															Line (In)
															(ft)
CO-132	496	LOT 41	0.30	27.0	21.2	4.80	2.340	0.18	0.28	7,096.89	7,096.18	7,096.78	7,096.10	0.68	7,096.95
CO-133	498	MH-140	0.30	7.7	58.6	2.93	1.425	0.19	0.23	7,096.09	7,095.54	7,096.02	7,095.50	0.51	7,096.10
CO-134	500	MH-141	0.50	6.2	69.9	5.71	2.947	0.17	0.29	7,095.50	7,092.47	7,095.39	7,092.42	2.97	7,095.50
CO-135	502	MH-142	0.70	11.4	64.0	5.19	2.285	0.23	0.35	7,092.42	7,090.83	7,092.29	7,090.77	1.52	7,092.42
CO-136	504	MH-143	0.90	12.6	60.2	6.22	2.666	0.24	0.40	7,090.77	7,088.74	7,090.62	7,088.66	1.95	7,090.77
CO-137	506	MH-144	1.10	18.5	67.5	5.79	2.233	0.29	0.44	7,088.66	7,087.10	7,088.49	7,087.01	1.48	7,088.66
CO-138	508	MH-145	1.30	31.2	29.2	4.69	1.550	0.38	0.48	7,087.01	7,086.72	7,086.82	7,086.39	0.44	7,087.01
CO-139	510	LOT 36	0.20	32.2	11.5	2.83	1.307	0.19	0.22	7,087.37	7,087.26	7,087.28	7,087.13	0.15	7,087.41
CO-140	512	LOT 37	0.20	14.1	11.2	5.10	2.996	0.13	0.22	7,089.07	7,088.68	7,088.98	7,088.66	0.32	7,089.11
CO-141	514	LOT 38	0.20	32.2	11.5	2.83	1.307	0.19	0.22	7,091.25	7,091.14	7,091.16	7,091.01	0.15	7,091.29
CO-142	516	LOT 39	0.20	33.6	11.5	2.74	1.249	0.20	0.22	7,092.96	7,092.86	7,092.87	7,092.74	0.13	7,092.89
CO-143	518	LOT 40	0.20	13.0	12.4	5.38	3.227	0.12	0.22	7,096.80	7,096.27	7,096.71	7,095.82	0.89	7,096.84
Upstream	Upstream	Upstream	Elevation Ground	Invert (Start)	Invert (Stop)										
Structure	Structure	Structure	(Start)	(ft)	(ft)										
Velocity (In-	Headloss	Headloss	(ft)												
Governing)	Coefficient	(ft)													
(ft/s)															
2.69	1.500	0.17	7,100.17	7,096.50	7,095.79										
2.38	1.020	0.08	7,100.17	7,095.79	7,095.20										
1.51	1.020	0.11	7,099.19	7,095.10	7,092.04										

1.83

2.05

2.22

2.36

2.35

2.35

2.35

2.35

2.35

STRM LOTS 36-41.stsw 7/29/2019 1.020

1.020

1.020

1.020

1.500

1.500

1.500

0.200

1.500

0.13

0.15

0.17

0.19

0.13

0.13

0.13

0.02

0.13

7,096.23

7,094.42

7,092.69

7,090.47

7,090.33

7,091.83

7,094.01

7,095.72

7,099.56

7,091.94

7,090.22

7,088.05

7,086.34

7,087.06

7,088.76

7,090.94

7,092.65

7,096.49

7,090.32

7,088.15

7,086.44

7,086.00

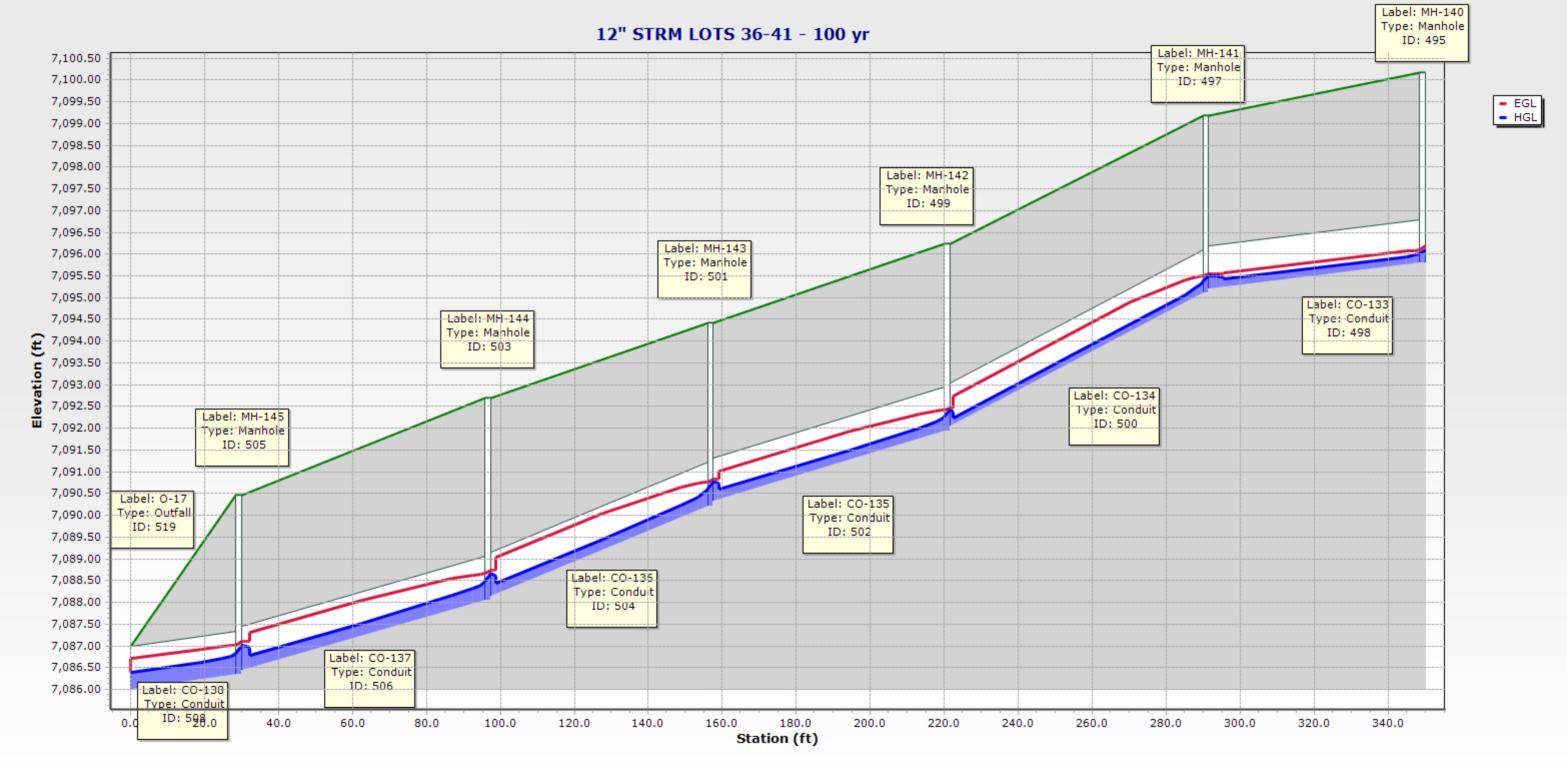
7,086.94

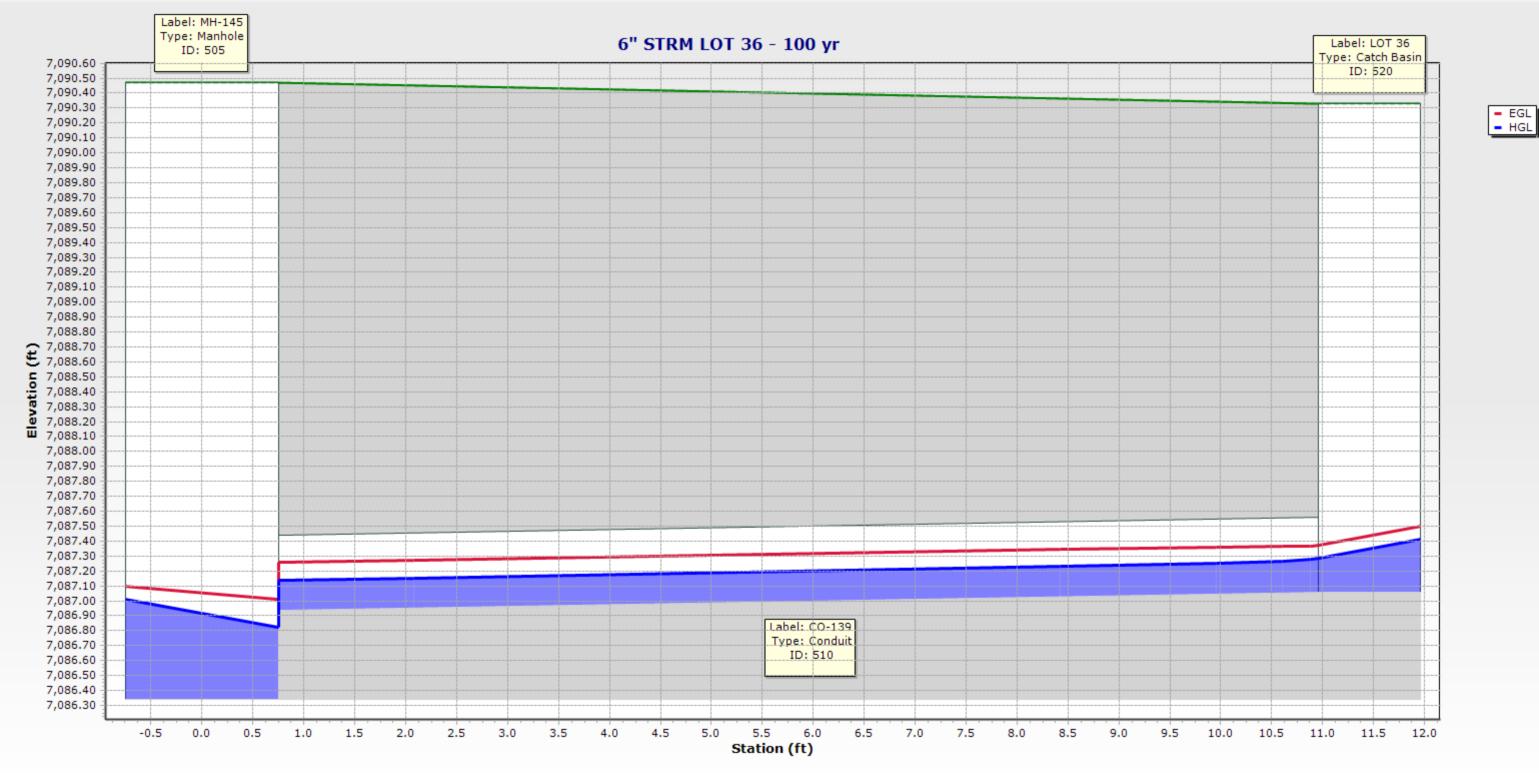
7,088.15

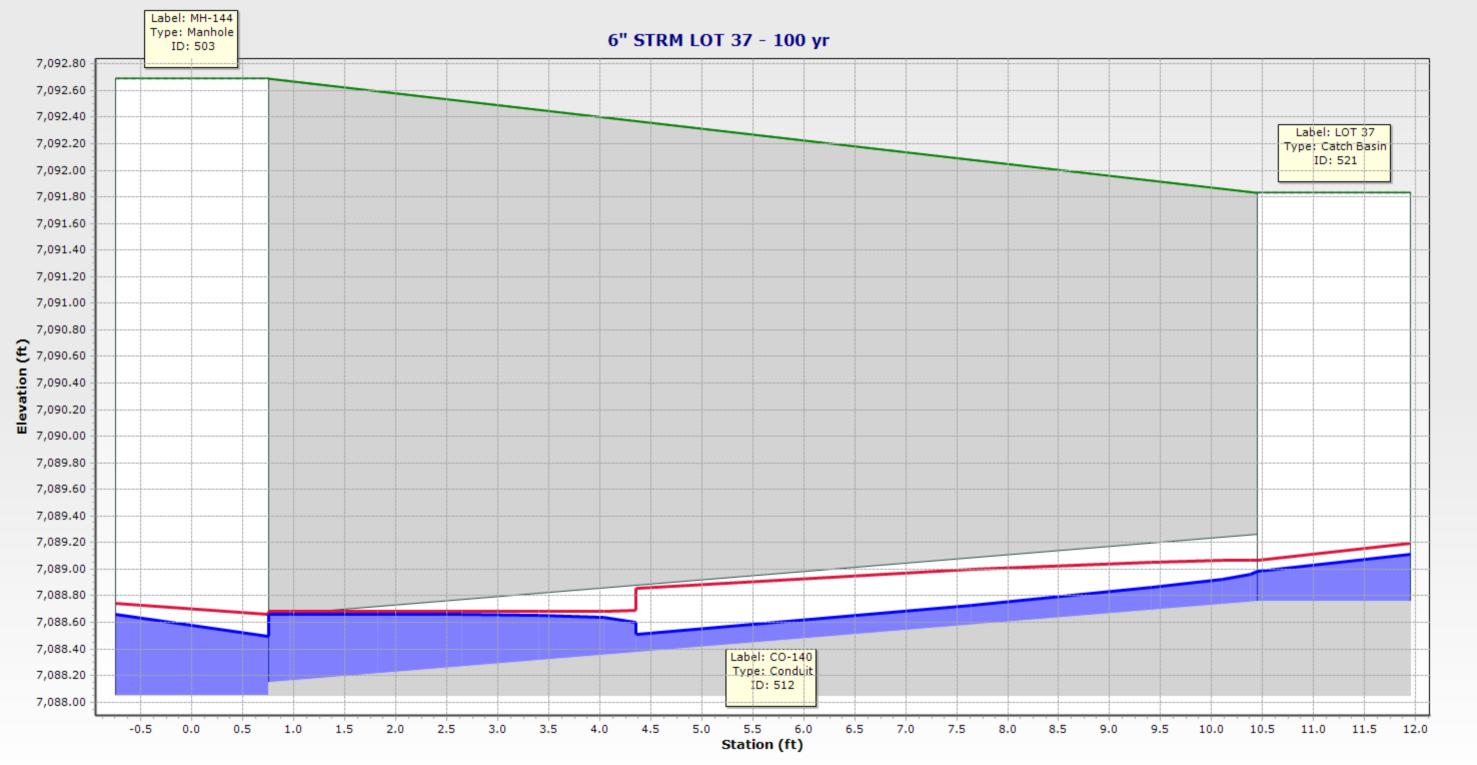
7,090.82

7,092.54

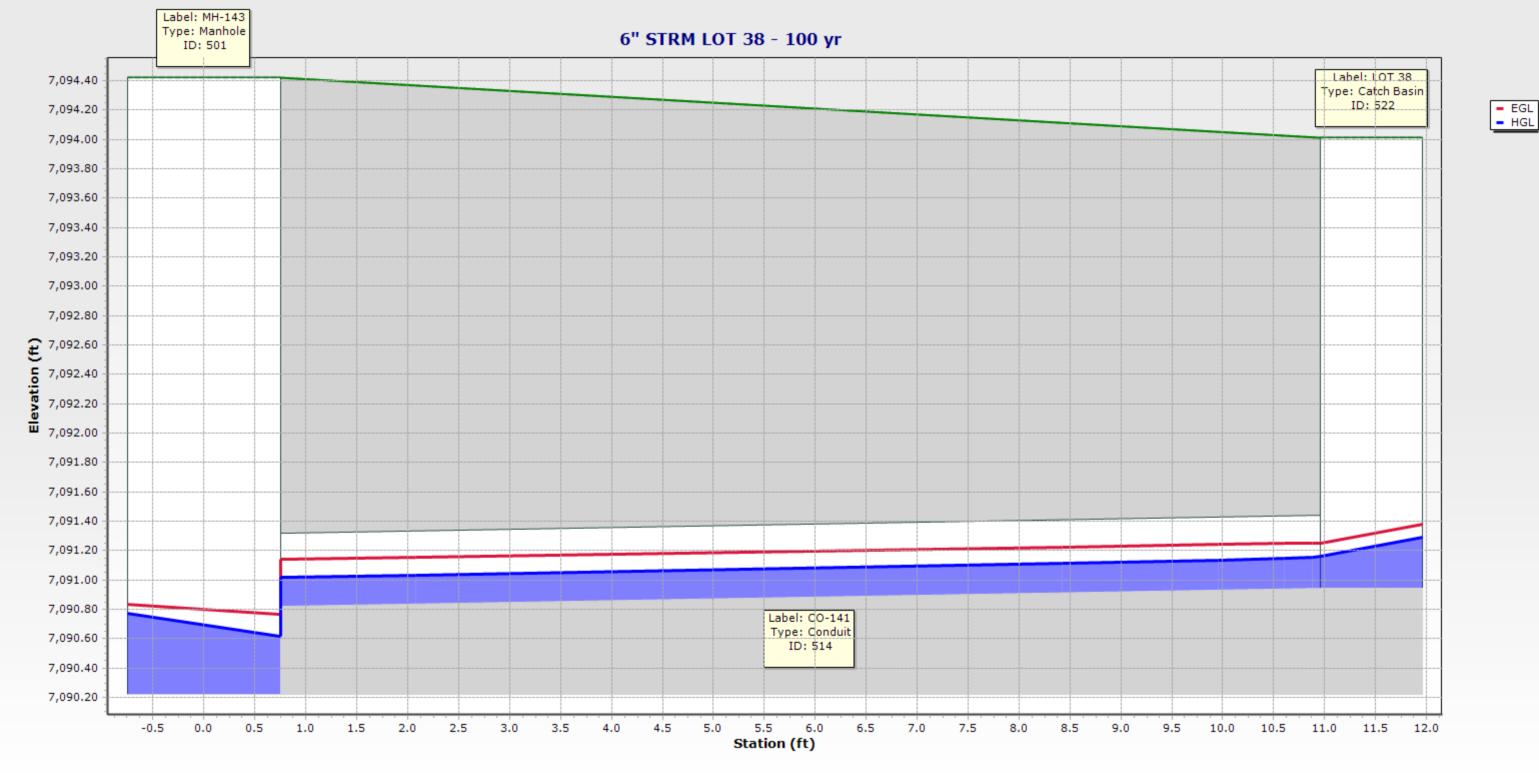
7,095.70

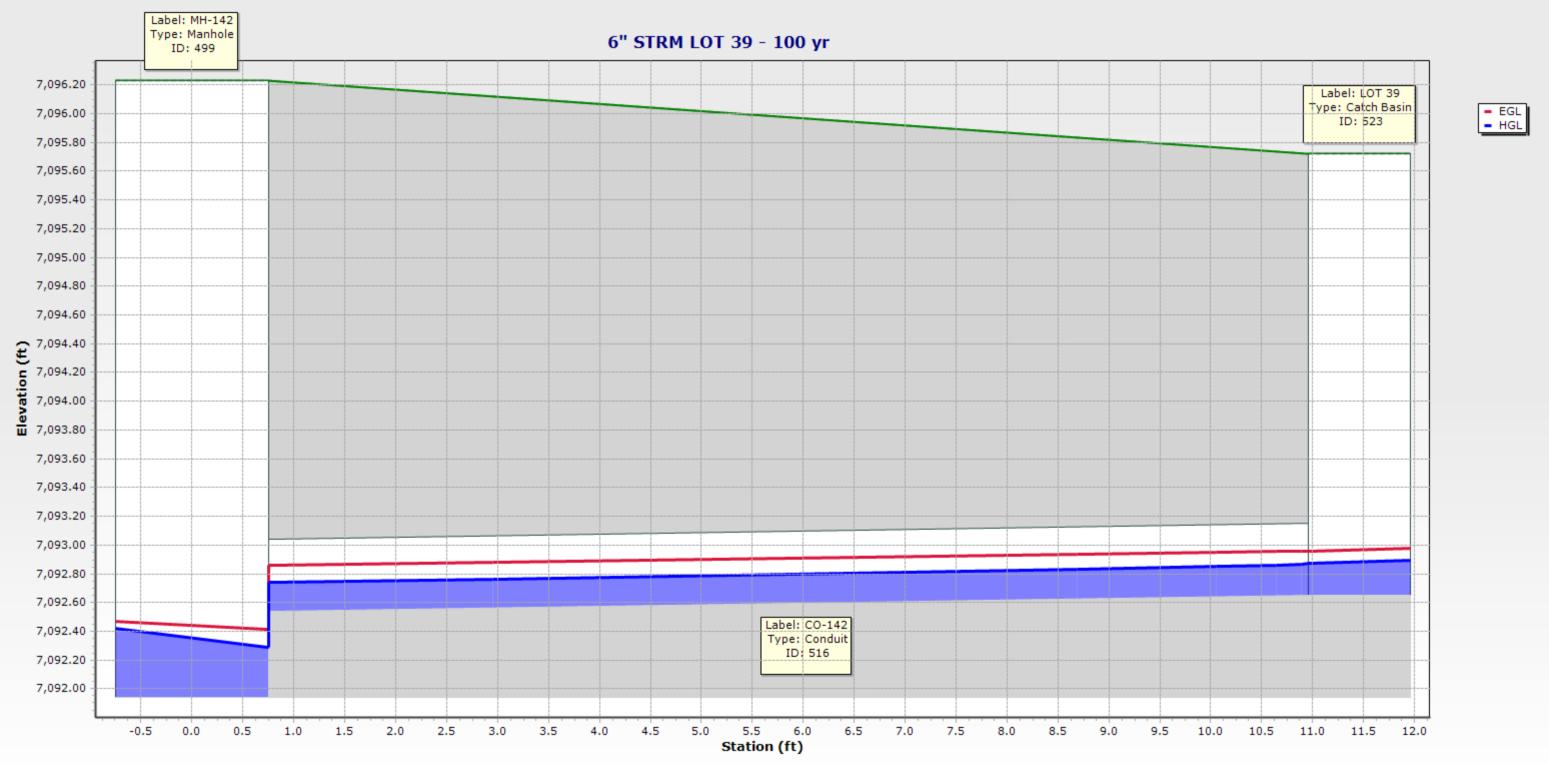


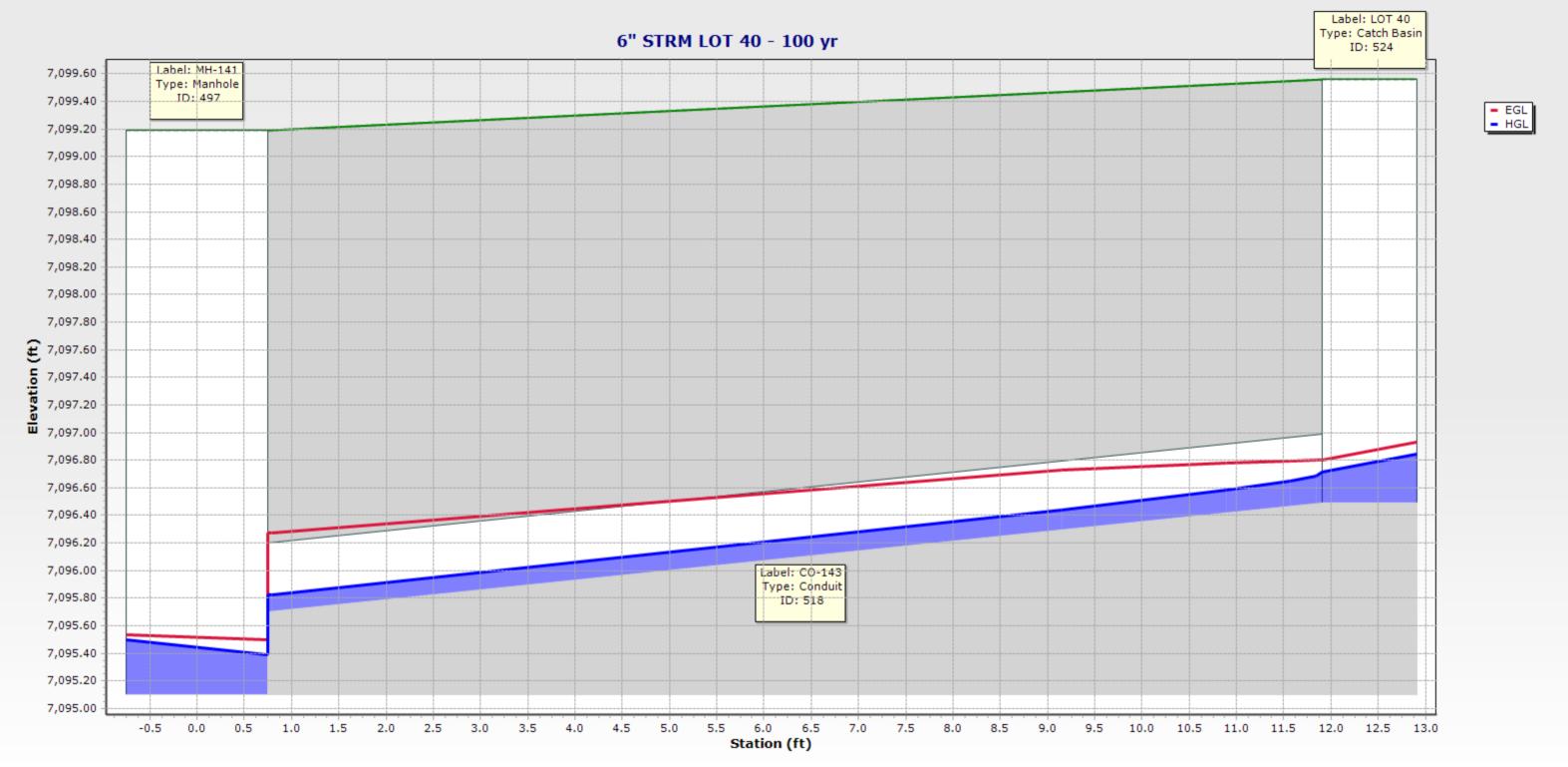


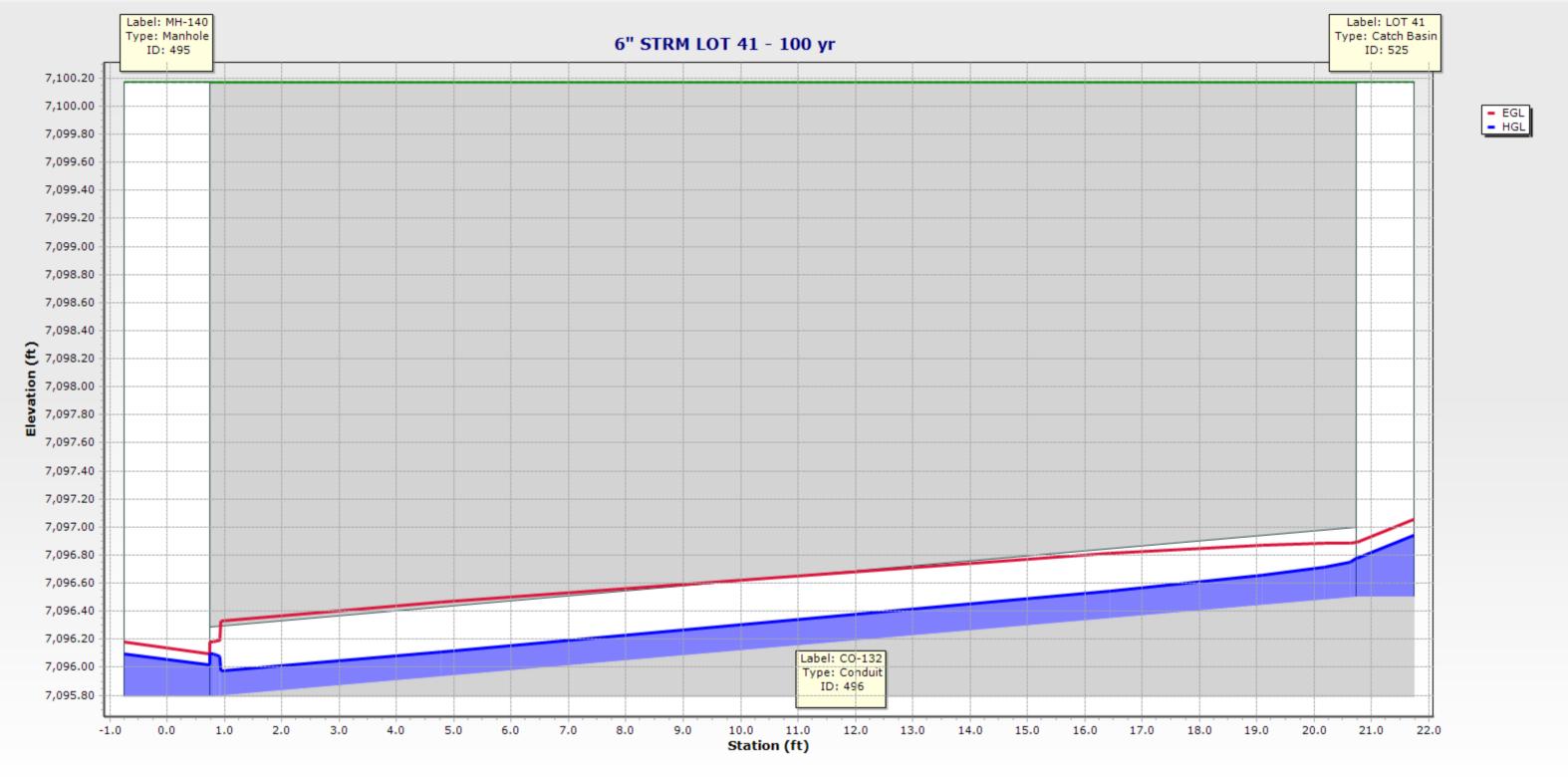




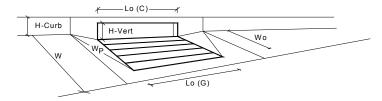






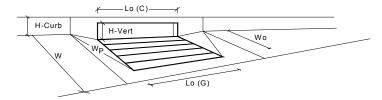


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 7 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



Design Information (Input)  CDOT Type R Curb Opening	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type I	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	•	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition	ion) Q <sub>a</sub> =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q <sub>PEAK REQUIRED</sub> =	5.7	13.8	cfs

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 8 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



Design Information (Input)  CDOT Type R Curb Opening  ▼		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.9	11.8	cfs

#### Version 4.05 Released March 2017 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 9 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions

Minor Storm

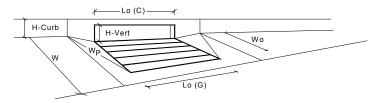
SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

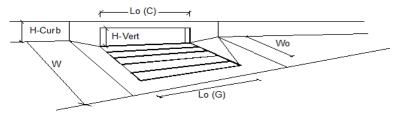


Design Information (Input) CDOT Type R Curb Opening ▼		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.65	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	3.7	9.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.2	5.4	cfs

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 10 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 $T_{CROWN}$ Gutter Width w: 2.00 S<sub>X</sub> : Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.022 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 29.1 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage

fajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

### INLET ON A CONTINUOUS GRADE

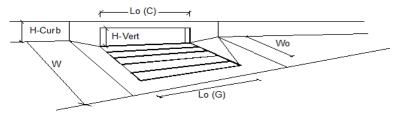


Design Information (Input)  CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>0</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	9.1	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.3	2.9	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	97	82	%

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 11 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 $T_{CROWN}$ Gutter Width w: 2.00 S<sub>X</sub> : Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.022 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 29.1 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage

fajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

### INLET ON A CONTINUOUS GRADE



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	15.00	15.00	ft
Nidth of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.9	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	2.9	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	82	%

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 12 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions

Minor Storm

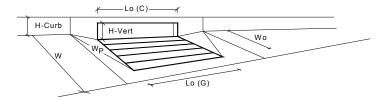
SUMP

Major Storm

SUMP

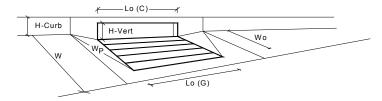
MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion



Design Information (Input) CDOT Type R Curb Opening   ▼		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	7
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Nater Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
ength of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Nidth of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	Ī
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.2	17.2	cfs

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 13 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_W$ 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

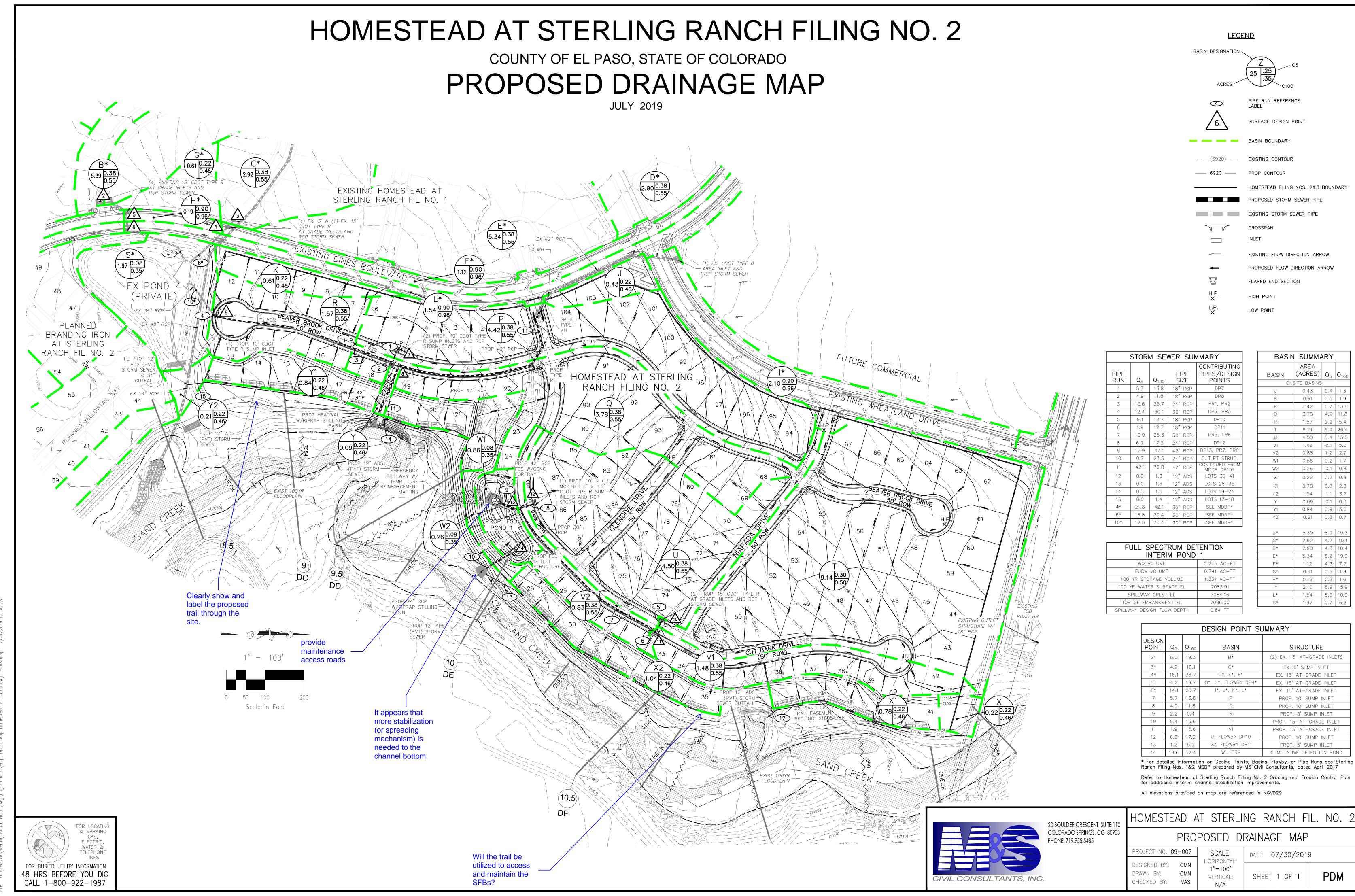


Design Information (Input)	ODOT To a DiOurk Or series		MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical v	/alue 0.60 - 0.80)	C <sub>0</sub> (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening i	n Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Ir	nches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduct	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance R	leduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.65	1.00	
Curb Opening Performance Redu	uction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduct	ion Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
			MINOR	MAJOR	
Total Inlet Interception Ca	apacity (assumes clogged condition)	$Q_a =$	3.7	9.0	cfs
Inlet Capacity IS GOOD for Min	or and Major Storms(>Q PEAK)	Q <sub>PEAK REQUIRED</sub> =	1.2	5.9	cfs

## **DRAINAGE MAP**

Provide existing conditions map

Provide EDB and SFB details



File: 0:\09007A\Sterling Ranch No 6\dwg\Eng Exhibits\Prop. Drain. Map Homestead Fil. No 2.dwg Plotstar