EPCD File No. SF-19-004

Prepared For:

SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

> August 18, 2020 Project No. 25188.00

Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593



ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. # 32314 For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: SR Land, LLC

By:

Title: Address:

20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. County Engineer/ ECM Administrator Date

Conditions:



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REVISED APPENDIX MATERIALS SF-3 Minor Basins X1, X2, W1, & Y1 SF-3 Major Basins X1, X2, W1, & Y1 MHFD Detention workbook Sand Filter 1 MHFD Detention workbook Sand Filter 2 Proposed basin map (limited to Basins X1, X2, W1, & Y1)



PURPOSE

This document is an Addendum to the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. The purpose of this report is to update the approved "Final Drainage Report for Homestead at Sterling Ranch Filing No. 2". The scope of the updates included in this addendum are limited to proposed Basins W1, X1, X2, & Y1. More specifically, this Addendum proposes to replace the proposed individual lot Sand Filters for lots 13-24, 28-35, and 36-41 with two common Sand Filters, one to serve basin X1, lots 36-41, and one to serve basins W1, X2, & Y1.

The text below replaces the original corresponding text from the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. The revised sections of the original report are marked in the table of contents below, and also crossed out/highlighted in the attached original report. Crossed out text is replaced and highlighted text is modified or discussed further herein.

PROPSED DRAINAGE CHARACTERISTICS

DETAILED DRAINAGE DISCUSSION (DESIGN POINTS)

BASIN X1 (0.78 acres), consists of proposed residential backyards of lots 36-41 along the eastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear southwest corner of each lot. The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.8 cfs, Q100 = 2.8 cfs) in both the 5 and 100 year storms. Collected flows will then be piped to a proposed full-spectrum sand filter, with a 12-hour drain time and a 4" perforated underdrain. The treated flows from the sand filter will be discharged via an outlet structure to the adjacent Sand Creek.

BASIN X2 (1.04 acres), consists of proposed residential backyards of lots 28-35 along the southern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear southwest corner of each lot (DP2). The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 1.1 cfs, Q100 = 3.7 cfs) in both the 5 and 100 year storms. Collected flows will then be piped west via 12" HDPE pipe following the rear lot lines towards DP3.1, where flows in the pipe combine with collected flows from Basin W1.

BASIN W1 (0.86 acres), consists of proposed residential backyards of lots 19-24 along the southeastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it



will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear corner of each lot (DP3). The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.9 cfs, Q100 = 3.1 cfs) in both the 5 and 100 year storms. Collected flows will then be piped southwest via 12" HDPE pipe following the rear lot lines towards DP3.1, where flows in the pipe combine with collected flows from Basin X2 (Q5 = 1.5 cfs, Q100 = 5.5 cfs).

Flows in the pipe at DP3.1 are then piped to DP4.1 where they combine with collected flows from Basin Y1 (Q5 = 2.1 cfs, Q100 = 7.5 cfs).

BASIN Y1 (0.84 acres), consists of proposed residential backyards of lots 13-18 along the southeastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear corner of each lot (DP4). The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.8 cfs, Q100 = 3.0 cfs) in both the 5 and 100 year storms. Collected flows will then be piped southwest via 12" HDPE pipe following the rear lot lines to a proposed full spectrum sand filter at DP4.1, where flows combine with collected flows from Basin X2 and W1 (Q5 = 2.1 cfs, Q100 = 7.5 cfs).

The basin characteristics, hydrologic parameters, runoff and rational calcs for Basins X1, X2, W1, and Y1 have remained consistent with the approved Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. However, the routing of the basins has changed and therefore revised SF-3 forms are included in the appendix section of this report. A revised basin map, showing the changes within the above described basins is also attached to this report.

WATER QUALITY PROVISIONS

Runoff produced within the residential backyard lots, of Basin X1 will be conveyed in backyard swales, collected in drain basins and directed to a full-spectrum sand filter (sand filter 1). The treated flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. Sand filter basin 1 is designed to provide 0.01 ac-ft of water quality storage (WQCV), 0.025 ac-feet of excess urban runoff volume (EURV) and 0.03 ac-ft of 100-year storage for a total design volume of 0.065 ac-ft. Sand filter basin 1 was designed to have a 12 hour WQCV drain time and a peak outflow for the 100 year design storm of 0.3 cfs. The sand filter will outfall via an orifice controlled 12" HDPE pipe and FES directly to the adjacent Sand Creek channel. Sand filter basin 1 will also include a 4" perforated underdrain system and emergency overflow spillway designed to pass the peak 100-yr flow rate with one foot of freeboard above the design water surface elevation. The peak discharge rate of the proposed sand filter is at or below the historic flows for the basin which it serves.

Runoff produced within the residential backyard lots, of Basins X2, W1, and Y1 will be conveyed in backyard swales, collected in drain basins and directed to a full-spectrum sand filter (sand filter 2). The treated flows will be collected by private storm sewer systems and discharged, ultimately, into



the Sand Creek Channel. The sand filter will outfall via an orifice controlled 12" HDPE pipe that is directly connected to the existing 60" RCP storm sewer outfall pipe of existing "Pond 4".

Sand filter basin 2 is designed to provide 0.035 ac-ft of water quality storage (WQCV), 0.095 ac-feet of excess urban runoff volume (EURV) and 0.107 ac-ft of 100-year storage for a total design volume of 0.238 ac-ft. Sand filter basin 2 was designed to have a 12 hour WQCV drain time and a peak outflow for the 100 year design storm of 1.8 cfs. The sand filter will outfall via an orifice controlled 12" HDPE pipe directly connected to the existing 60" RCP pipe to the south that serves as the outfall to "Pond 4" constructed with Sterling Ranch Filing No. 1. Sand filter basin 2 will also include a 4" perforated underdrain system and emergency overflow spillway designed to pass the peak 100-yr flow rate with one foot of freeboard above the design water surface elevation. The peak discharge rate of the proposed sand filter is at or below the historic flows for the basins which it serves.

Both proposed sand filters are contained within existing Tract D, of the Homestead at Sterling Ranch Filing No. 2 development. The proposed sand filter facilities are to be privately maintained by the Sterling Ranch Metropolitan District. Access to maintain these sand filter basins is from the regional trail along sand creek.

The proposed sand filters were sized using the MHFD Detention workbook and printouts are included in the Hydraulic Calculations section of this report.

CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FIL. NO. 2

Drainage improvements are planned with the development of Homestead at Sterling Ranch Filing No. 2. A majority of the construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Any additional improvements and costs are listed below.

The following list of drainage improvements is Non-Reimbursable. The Reimbursable facilities are outlined in the Sterling Ranch Filing No. 1 Final Drainage Report and Sterling Ranch MDDP. Refer to the MDDP for Sterling Ranch Cost and Fee Analysis Report (February 2019).



J[·]R ENGINEERING

ltem	Description	Quantity Prev	Quantity Now	Unit	Ur	nit Cost		Cost
1	18" RCP	31	31	LF	\$	40	\$	1,240
2	24" RCP	127	127	LF	\$	50	\$	6,350
3	30" RCP	998	998	LF	\$	85	\$	84,830
4	36" RCP	8	8	LF	\$	105	\$	840
5	42" RCP	699	699	LF	\$	185	\$:	129,315
6	24" FES	1	1	EA	\$	750	\$	750
8	42" FES	1	1	EA	\$	1,250	\$	1,250
9	5.0'x4.5' CDOT Type R Sump Inlet	1	1	EA	\$	4,000	\$	4,000
10	10' CDOT Type R Sump Inlet	4	4	EA	\$	4,700	\$	18,800
11	15' CDOT Type R At-Grade Inlet	2	2	EA	\$	6,000	\$	12,000
12	4.0' Type II MH	1	1	EA	\$	3,500	\$	3,500
13	5.0' Type II MH	2	2	EA	\$	4,000	\$	8,000
14	6.0' Type II MH	1	1	EA	\$	4,500	\$	4,500
17	5.0'x6.0' MH	2	2	EA	\$	6,500	\$	13,000
18	5.5'x5.5' MH	1	1	EA	\$	6,500	\$	6,500
19	Headwall/Wingwall	1	1	EA	\$	6,000	\$	6,000
20	Full Spectrum Det. Pond 1	1	1	EA	\$	15,000	\$	15,000
21	FSD Pond 1 Outlet Structure	1	1	EA	\$	12,600	\$	12,600
22	Ind. Lot Sand filter	26	0	EA	\$	2,000	\$	-
23	18" Drain basin MH	27	0	EA	\$	1,000	\$	-
24	12" Storm pipe	1,658	2,433	LF	\$	26	\$	63,258
25	12" Nyloplast Drain basin w/ 12" dome grate	0	28	EA	\$	1,000	\$	28,000
26	Sand Filter Basin 1	0	1	LS	\$	4,000	\$	4,000
27	Sand Filter Basin 2	0	1	LS	\$	6,000	\$	6,000
28	12" FES	0	4	EA	\$	350	\$	1,400
						TOTAL	\$1	431,133



REVISED APPENDIX MATERIALS



STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Location ign Storm			rings											ulated ecked	By:	REB 3/18/2	0			
				DIREC	TRUN	NOFF			т	OTAL I	RUNOF	F		PIPE	-		RAVE	LTIM	IE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	X1	0.78	0.22	7.3	0.17	4.60	0.8					0.8	0.17	2.0	18	250	2.6	1.6	Runoff from Basin X1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to pvt. Full-specrum sand filter @ DP1.1
	2	X2	1.04	0.22	7.3	0.23	4.60	1.1					1.1	0.23	2.0	12	950	3.1	5.1	Runoff from Basin X2, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3	W1	0.86	0.22	7.3	0.19	4.60	0.9					0.9	0.19	2.0	12	250	2.8	1.5	Runoff from Basin W1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3.1								13.9	0.42	3.64	1.5								Combined flow in private 12" HDPE pipe @ DP3.1, piped to private full-spectrum sand filter @ DP-4.1
	4	Y1	0.84	0.22	7.3	0.18	4.60	0.8					0.8	0.18	2.0	12	350	3.0		Runoff from Basin Y1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP4.1
	4.1								15.8	0.60	3.44	2.1								Combined flow in private 12" HDPE pipe @ DP4.1, inflow to proposed private full-spectrum sand filter

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Location: sign Storm:			ings										lculate Checke I			20			
				DIR	ECT RU	JNOFF			Т	OTAL R	UNOFF		PI	PE	-	TRAVE	LTIM	IE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr) Q (cfs)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	X1	0.78	0.46	7.3	0.36	7.72	2.8	5			2.8	0.36	1.5	12	250	3.2		Runoff from Basin X1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to pvt. Full-specrum sand filter @ DP1.1
	2	X2	1.04	0.46	7.3	0.48	7.72	3.7				3.1	0.48	1.5	12	950	3.5		Runoff from Basin X2, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3	W1	0.86	0.46	7.3	0.40	7.72	3.1				3.3	0.40	1.5	12	250	3.3		Runoff from Basin W1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3.1								13.1	0.88	6.26 5	5							Combined flow in private 12" HDPE pipe @ DP3.1, piped to private full-spectrum sand filter @ DP-4.1
	4	Y1	0.84	0.46	7.3	0.39	7.72	3.0)			3.0	0.39	1.5	12	350	3.3		Runoff from Basin Y1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP4.1
	4.1								14.8	1.27	5.94 7	5							Combined flow in private 12" HDPE pipe @ DP4.1, inflow to proposed private full-spectrum sand filter

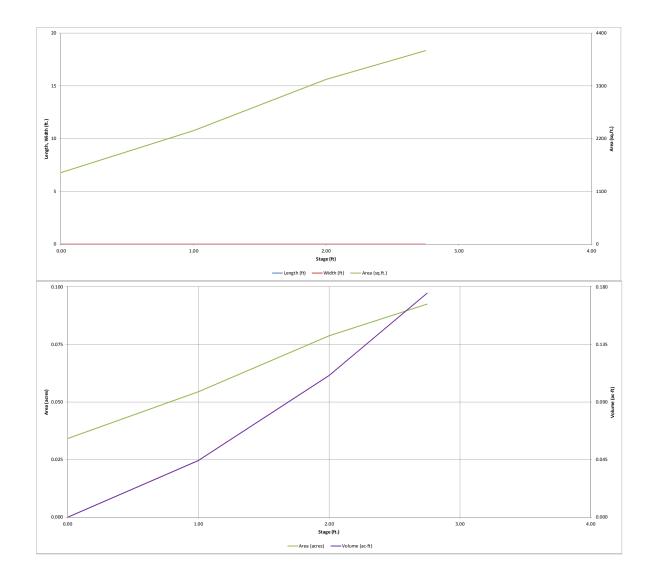
Notes: Street and Pipe C*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.00 (December 2019)

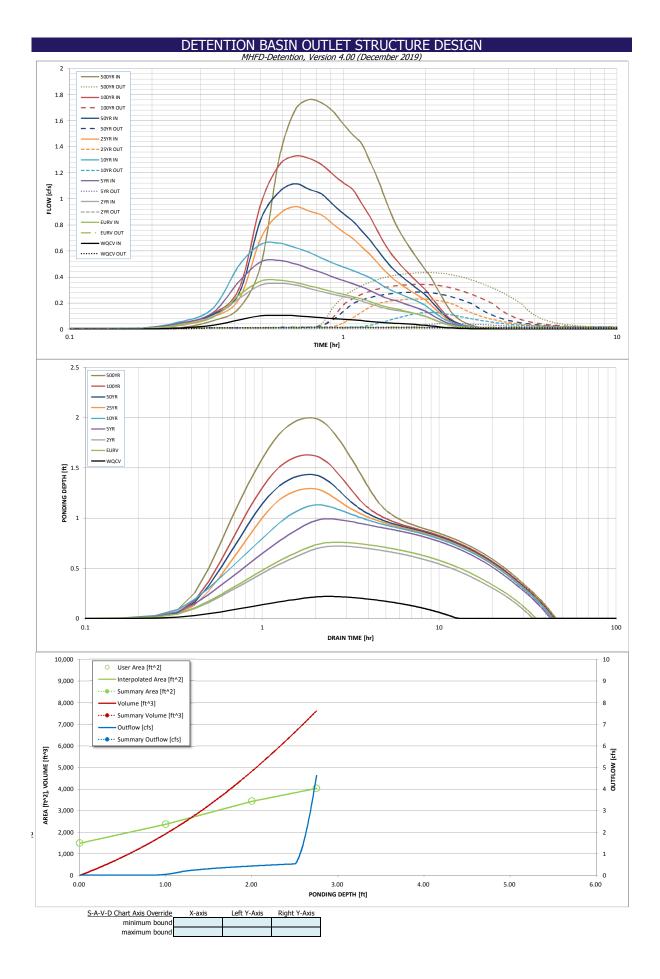
			Ranch Filing I	No. 2				
Basin ID:	Sand Filter -	Basin X1						
ZONE 3 ZONE ZONE	2 DNE 1	_						
100-YR EURY WOOV		T						
VOLOMET EDRY WOCY		R.					1	
ZONE	1 AND 2	100-YEA	AR E		Depth Increment =		ft	-
POOL Example Zone	CES	on (Retenti	on Pond)		Stage - Storage	Stage	Optional Override	L
	J	•			Description	(ft)	Stage (ft)	
Watershed Information		1			Media Surface		0.00	
Selected BMP Type =	SF	-			7090		1.00	
Watershed Area =	0.78 450	acres			7091		2.00	_
Watershed Length = Watershed Length to Centroid =	450 225	ft ft			7091.75		2.75	-
Watershed Slope =	0.020	ft/ft						-
Watershed Imperviousness =	42.00%	percent						-
Percentage Hydrologic Soil Group A =	0.0%	percent						
Percentage Hydrologic Soil Group B =	100.0%	percent						
Percentage Hydrologic Soil Groups C/D =	0.0%	percent						
Target WQCV Drain Time =	12.0	hours						
Location for 1-hr Rainfall Depths =								-
After providing required inputs above incl depths, dick 'Run CUHP' to generate runo	iuding 1-hour i ff hydrographs	ainfall using						-
the embedded Colorado Urban Hydro	graph Procedu	re.	Optional Use	r Overrides				-
Water Quality Capture Volume (WQCV) =	0.010	acre-feet		acre-feet				L
Excess Urban Runoff Volume (EURV) =	0.035	acre-feet		acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	0.033	acre-feet	1.19	inches				L
5-yr Runoff Volume (P1 = 1.5 in.) =	0.049	acre-feet	1.50	inches				_
10-yr Runoff Volume (P1 = 1.75 in.) = 25-yr Runoff Volume (P1 = 2 in.) =	0.063	acre-feet acre-feet	1.75	inches inches				
50-yr Runoff Volume (P1 = 2.25 in.) =	0.083	acre-feet	2.00	inches				+
100-yr Runoff Volume (P1 = 2.52 in.) =	0.119	acre-feet	2.52	inches				+
500-yr Runoff Volume (P1 = 3.14 in.) =	0.160	acre-feet		inches				
Approximate 2-yr Detention Volume =	0.026	acre-feet		•				
Approximate 5-yr Detention Volume =	0.036	acre-feet						
Approximate 10-yr Detention Volume =	0.049	acre-feet						
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	0.054	acre-feet acre-feet						-
Approximate 100-yr Detention Volume =	0.065	acre-feet						-
· · · · · · · · · · · · · · · · · · ·								-
Define Zones and Basin Geometry								
Zone 1 Volume (WQCV) =	0.010	acre-feet						
Zone 2 Volume (EURV - Zone 1) =	0.025	acre-feet						
Zone 3 Volume (100-year - Zones 1 & 2) =	0.030	acre-feet acre-feet						
Total Detention Basin Volume = Initial Surcharge Volume (ISV) =	0.065 N/A	acre-feet ft ³						
Initial Surcharge Depth (ISD) =	N/A	ft						+
Total Available Detention Depth (H _{total}) =	user	ft						
Depth of Trickle Channel $(H_{TC}) =$	N/A	ft						
Slope of Trickle Channel (S _{TC}) =	N/A	ft/ft						
Slopes of Main Basin Sides (S _{main}) =	user	H:V						1
Basin Length-to-Width Ratio (R _{L/W}) =	user	J						⊢
Initial Surcharge Area (A _{ISV}) =	user	ft²						⊢
Surcharge Volume Length (L _{ISV}) =	user	ft						\vdash
Surcharge Volume Width (W_{ISV}) =	user	ft						L
Depth of Basin Floor (H _{FLOOR}) =	user	ft						
Length of Basin Floor (L_{FLOOR}) =	user	ft						
Width of Basin Floor (W _{FLOOR}) = Area of Basin Floor (A _{FLOOR}) =	user	ft ft ²						+
Volume of Basin Floor (V _{FLOOR}) =	user	π ft ³						+
Depth of Main Basin (H _{MAIN}) =	user	ft						⊢
Length of Main Basin (L _{MAIN}) =	user	ft						1
Width of Main Basin (W_{MAIN}) =	user	ft						
Area of Main Basin (A _{MAIN}) =	user	ft ²						L
Volume of Main Basin (V _{MAIN}) =	user	ft ³						⊢
Calculated Total Basin Volume (V _{total}) =	user	acre-feet						⊢
								F
								⊢
								F
								F
								F
								L

Depth Increment = Stage - Storage Description	Stage (ft)	ft Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volum (ac-ft)
Media Surface		0.00	-			1,488	0.034		
7090		1.00				2,367	0.054	1,927	0.044
7091		2.00				3,428	0.079	4,825	0.111
7091.75		2.75	-			4,028	0.092	7,621	0.175
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.00 (December 2019)



	DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.00 (December 2019)													
Project:	Homestead at Ster	MHF ling Ranch Filing No		ion 4.00 (Decemb	ier 2019)									
Basin ID:	Sand Filter - Basin													
ZONE 3				Estimated	Estimated									
				Stage (ft)	Volume (ac-ft)	Outlet Type								
VOLUME EURY WOCV			Zone 1 (WQCV)	0.27	0.010	Filtration Media								
	100-YEAR ORIFICE		Zone 2 (EURV)	0.82	0.025	Circular Orifice								
PERMANENT ORIFICES	ONINCE		Zone 3 (100-year)	1.35	0.030	Circular Orifice								
POOL Example Zone	Configuration (Re	tention Pond)	I	Total (all zones)	0.065									
User Input: Orifice at Underdrain Outlet (typically u	used to drain WQCV	in a Filtration BMP)				-	Calculated Paramet	ers for Underdrain						
Underdrain Orifice Invert Depth =	2.10	ft (distance below t	he filtration media su	urface)	Unde	rdrain Orifice Area =	0.0	ft²						
Underdrain Orifice Diameter =	0.50	inches			Underdra	in Orifice Centroid =	0.02	feet						
User Input: Orifice Plate with one or more orifices Invert of Lowest Orifice =							Calculated Paramet	<u>ers for Plate</u> ft ²						
Depth at top of Zone using Orifice Plate =	N/A N/A	-	bottom at Stage = 0 bottom at Stage = 0	-		ifice Area per Row = Iliptical Half-Width =	N/A N/A	feet						
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	bottom at Stage = 0	(10)		otical Slot Centroid =	N/A	feet						
Orifice Plate: Orifice Area per Row =	N/A	inches			-	Elliptical Slot Area =	N/A	ft ²						
								1.4						
User Input: Stage and Total Area of Each Orifice R	ow (numbered from	lowest to highest)												
	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)						
Stage of Orifice Centroid (ft)		N/A	N/A	N/A	N/A	N/A	N/A	N/A						
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	l					
	Row Q (ontional)	Row 10 (optional)	Pow 11 (ontional)	Pow 12 (ontional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Pow 16 (antional)	1					
Stage of Orifice Centroid (ft)	Row 9 (optional) N/A	N/A	Row 11 (optional) N/A	Row 12 (optional) N/A	N/A	N/A	Row 15 (optional) N/A	Row 16 (optional) N/A						
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A						
							1973		1					
User Input: Vertical Orifice (Circular or Rectangula	r <u>)</u>						Calculated Paramet	ers for Vertical Orific	e					
	Zone 2 Circular	Zone 3 Circular					Zone 2 Circular	Zone 3 Circular						
Invert of Vertical Orifice =	0.29	0.87	-	bottom at Stage = 0	-	ertical Orifice Area =	0.00		ft²					
Depth at top of Zone using Vertical Orifice =	0.87	1.42	-	bottom at Stage = 0) ft) Vertic	al Orifice Centroid =	0.02	0.17	feet					
Vertical Orifice Diameter =	0.50	4.00	inches											
User Input: Overflow Weir (Dropbox with Flat or S	Not Selected	Not Selected				te lless Educ II	Not Selected	Not Selected						
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	N/A N/A	N/A N/A	feet	ottom at Stage = 0 ft)		te Upper Edge, $H_t =$ Weir Slope Length =	N/A N/A	N/A N/A	feet feet					
Overflow Weir Hone Luge Length =	N/A	N/A	H:V		Grate Open Area / 1		N/A N/A	N/A	ICCL					
Horiz. Length of Weir Sides =	N/A	N/A	feet		Overflow Grate Ope	-	N/A	N/A	ft ²					
Overflow Grate Open Area % =	N/A	N/A	%, grate open area			en Area w/ Debris =	N/A	N/A	ft ²					
Debris Clogging % =	N/A	N/A	%			·								
			•											
User Input: Outlet Pipe w/ Flow Restriction Plate (0			ngular Orifice)											
	Not Selected	Not Selected			<u>(</u>	Calculated Parameter			<u>e</u>					
Depth to Invert of Outlet Pipe =	N/A						Not Selected	Not Selected						
Circular Orifice Diameter =		N/A	-	asin bottom at Stage =	= 0 ft) (Outlet Orifice Area =	Not Selected N/A	Not Selected N/A	ft²					
	N/A	N/A N/A	ft (distance below ba inches	-	= 0 ft) 0	Outlet Orifice Area = et Orifice Centroid =	Not Selected N/A N/A	Not Selected N/A N/A	ft² feet					
		-	-	-	= 0 ft) (Outlet Orifice Area = et Orifice Centroid =	Not Selected N/A	Not Selected N/A	ft²					
User Input: Emergency Spillway (Rectangular or Tr	N/A	-	-	-	= 0 ft) 0	Outlet Orifice Area = et Orifice Centroid =	Not Selected N/A N/A	Not Selected N/A N/A N/A	ft² feet					
	N/A	N/A	-	Half-Ce	= 0 ft) (Outle entral Angle of Restri	Outlet Orifice Area = et Orifice Centroid =	Not Selected N/A N/A N/A	Not Selected N/A N/A N/A	ft² feet					
User Input: Emergency Spillway (Rectangular or Tr	N/A	N/A	inches	Half-Ce	= 0 ft) (Outle entral Angle of Restri Spillway I	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe =	Not Selected N/A N/A N/A <u>Calculated Paramet</u>	Not Selected N/A N/A N/A ers for Spillway	ft² feet					
<u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	N/A apezoidal) 2.50 10.00 4.00	N/A ft (relative to basin feet H:V	inches	Half-Ce	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard =	Not Selected N/A N/A N/A Calculated Paramet 0.12 4.12 0.09	Not Selected N/A N/A N/A ers for Spillway feet feet acres	ft² feet					
<u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length =	N/A rapezoidal) 2.50 10.00	N/A ft (relative to basin feet	inches	Half-Ce	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at	Outlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard =	Not Selected N/A N/A N/A Calculated Paramet 0.12 4.12	Not Selected N/A N/A N/A ers for Spillway feet feet	ft² feet					
<u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	N/A apezoidal) 2.50 10.00 4.00	N/A ft (relative to basin feet H:V	inches	Half-Ce	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard =	Not Selected N/A N/A N/A Calculated Paramet 0.12 4.12 0.09	Not Selected N/A N/A N/A ers for Spillway feet feet acres	ft² feet					
User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overr	N/A ft (relative to basin feet H:V feet <i>de the default CUH</i>	inches bottom at Stage = 0 2 hydrographs and ru	- Half-Ce D ft) <i>Inoff volumes by en</i> tr	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at Basin Volume at	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard = the Inflow Hydrograp	Not Selected N/A N/A N/A O.12 4.12 0.09 0.17	Not Selected N/A N/A N/A ers for Spillway feet feet acres acre-ft W through AF).	ft ² feet radians					
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User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overnow WQCV 0.53 0.010	N/A ft (relative to basin feet H:V feet <u>de the default CUHP</u> EURV 1.07 0.035 0.035	inches bottom at Stage = 0 ² hydrographs and ru 2 Year 1.19 0.033 0.033	Half-Ce 0 ft) 1.50 0.049 0.049	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at Basin Area at Basin Volume at tering new values in 1.75 0.063 0.063	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = <u>the Inflow Hydrogray</u> 25 Year 2.00 0.083 0.083	Not Selected N/A N/A N/A N/A Output 0.12 4.12 0.09 0.17 So Year 2.25 0.099 0.099	Not Selected N/A N/A N/A Krs for Spillway feet feet acres acre-ft W through AF). 100 Year 2.52 0.119 0.119	ft ² feet radians 500 Year 3.14 0.160 0.160					
User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overr WQCV 0.53 0.010 0.010 0.0	N/A ft (relative to basin feet H:V feet de the default CUHP EURV 1.07 0.035 0.035 0.0	inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.033	Half-Ce D ft) 5 Year 1.50 0.049	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at Basin Area at Basin Volume at tering new values in 1.75 0.063	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = the Inflow Hydrograf 2.00 0.083	Not Selected N/A N/A N/A O.12 4.12 0.09 0.17 So Year 2.25 0.099	Not Selected N/A N/A N/A ers for Spillway feet feet acres acre-ft <i>W through AF).</i> 100 Year 2.52 0.119	ft ² feet radians 500 Year 3.14 0.160					
User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overn WQCV 0.53 0.010 0.00 0.0	N/A ft (relative to basin feet H:V feet <i>de the default CUHP</i> EURV 1.07 0.035 0.035 0.0 0.0	inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.033 0.033 0.1	Half-Ce D ft) 5 Year 1.50 0.049 0.2	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at Basin Volume at tering new values in 10 Year 1.75 0.063 0.063 0.2	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = the Inflow Hydrogray 25 Year 2.00 0.083 0.083 0.4	Not Selected N/A N/A N/A Onlog N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A ers for Spillway feet feet acres acre-ft <i>W through AF).</i> 100 Year 2.52 0.119 0.119 0.7	ft ² feet radians 500 Year 3.14 0.160 0.160 1.0					
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User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overn WQCV 0.53 0.010 0.010 0.00 0.00 0.11 0.0 0.12 N/A	N/A ft (relative to basin feet H:V feet <i>de the default CUH/</i> EURV 1.07 0.035 0.035 0.035 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	inches bottom at Stage = 0 ² hydrographs and ru 2 Year 1.19 0.033 0.13 0.03 0.07 0.4 0.0 N/A Vertical Orifice 1	Half-Ce 0 ft)	= 0 ft) (Outl entral Angle of Restri Spillway I Stage at Basin Area at Basin Area at Basin Volume at tering new values in 1.75 0.063 0.063 0.063 0.063 0.2 0.31 0.7 0.1 0.7 0.1 0.5	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>the Inflow Hydrogray</u> 25 Year 2.00 0.083 0.083 0.4 0.58 0.9 0.2	Not Selected N/A N/A N/A O.12 A.12 0.09 0.17 Not stable (Columns U O.17 Not	Not Selected N/A N/A N/A N/A ers for Spillway feet acres acres acre-ft W through AF). 100 Year 2.52 0.119 0.719 0.313 0.3 0.5	ft ² feet radians 500 Year 3.14 0.160 0.160 1.0 1.30 1.8 0.4 Vertical Orific					
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User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overn WQCV 0.53 0.010 0.010 0.00 0.0 0.0 0.0 0.10 0.0 0.10 0.0 0.0 0.0 0.10 0.0 0.10 0.0 0.1 0.0 0.1 0.0 0.1 0.1 0.1 0.2 0.3 0.4 N/A N/A 12	N/A ft (relative to basin feet H:V feet URV 1.07 0.035 0.035 0.035 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 N/A Vertical Orifice 1 N/A 34	Inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.033 0.033 0.1 0.07 0.4 0.0 0.07 0.4 0.0 N/A Vertical Orifice 1 N/A N/A 33	Half-Ce D ft) Half-Ce D ft) Half-Ce 5 Year 1.50 0.049 0.049 0.20 0.20 0.5 0.0 0.20 0.5 0.0 0.3 Vertical Orifice 2 N/A N/A 41	= 0 ft) (Outlentral Angle of Restri Spillway I Stage at Basin Area at Basin Area at Basin Volume at tering new values in 1.75 0.063 0.063 0.063 0.2 0.31 0.7 0.1 0.5 Vertical Orifice 2 N/A N/A 41	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = <u>25 Year</u> 2.00 0.083 0.083 0.083 0.083 0.4 0.58 0.9 0.2 0.5 Vertical Orifice 2 N/A N/A 41	Not Selected N/A N/A N/A N/A N/A Old 0.12 4.12 0.09 0.17 Dhs table (Columns 50 Year 2.25 0.099 0.6 0.72 1.1 0.3 0.5 Vertical Orifice 2 N/A 41	Not Selected N/A N/A N/A N/A ers for Spillway feet feet acres acre-ft W through AF). 100 Year 2.52 0.119 0.119 0.119 0.7 0.93 1.3 0.3 0.5 Vertical Orifice 2 N/A N/A 41	ft ² feet radians 500 Year 3.14 0.160 0.160 1.0 1.30 1.30 1.30 1.30 1.30 1.4 0.4 /ertical Orifice N/A V/A 40					
User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Mount Start	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overn WQCV 0.53 0.010 0.00 0.010 0.00 0.1 0.0 N/A Filtration Media N/A 12 13	N/A ft (relative to basin feet H:V feet 0.035 0.035 0.0 0.035 0.0 0.00 0.4 0.00 N/A Vertical Orifice 1 N/A N/A 34 35	inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.033 0.1 0.03 0.1 0.07 0.4 0.0 0.4 0.0 0.4 0.0 0.4 0.0 N/A Vertical Orifice 1 N/A N/A N/A N/A 33 34	Half-Ce D ft) Half-Ce 5 Year 1.50 0.049 0.20 0.5 0.03 Vertical Orifice 2 N/A N/A 41 42	= 0 ft) 0 Outlentral Angle of Restri Spillway I Stage at Basin Area at Basin Volume at Tering new values in 10 Year 1.75 0.063 0.063 0.2 0.7 0.1 0.7 0.1 0.5 Vertical Orifice 2 N/A N/A 41 43	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>the Inflow Hydrogray</u> 25 Year 2.00 0.083 0.083 0.083 0.4 0.58 0.9 0.2 0.5 Vertical Orifice 2 N/A N/A N/A 41 43	Not Selected N/A O.12 4.12 0.09 0.17 Dhs table (Columns I Dohs table (Columns I 0.099 0.6 0.72 1.1 0.3 0.5 Vertical Orifice 2 N/A N/A 41 43	Not Selected N/A N/A N/A N/A ers for Spillway feet feet acres acre-ft W through AF). 100 Year 2.52 0.119 0.7 0.93 1.3 0.3 0.5 Vertical Orifice 2 N/A N/A 41 44	ft ² feet radians 500 Year 3.14 0.160 0.160 1.0 1.30 1.8 0.4 (ertical Orifica N/A N/A N/A 40 44					
User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	N/A apezoidal) 2.50 10.00 4.00 1.50 The user can overn WQCV 0.53 0.010 0.010 0.00 0.0 0.0 0.0 0.0 N/A Filtration Media N/A 12	N/A ft (relative to basin feet H:V feet URV 1.07 0.035 0.035 0.035 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 N/A Vertical Orifice 1 N/A 34	Inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.033 0.033 0.1 0.07 0.4 0.0 0.07 0.4 0.0 N/A Vertical Orifice 1 N/A N/A 33	Half-Ce D ft) Half-Ce D ft) Half-Ce 5 Year 1.50 0.049 0.049 0.20 0.20 0.5 0.0 0.20 0.5 0.0 0.3 Vertical Orifice 2 N/A N/A 41	= 0 ft) (Outlentral Angle of Restri Spillway I Stage at Basin Area at Basin Area at Basin Volume at tering new values in 1.75 0.063 0.063 0.063 0.2 0.31 0.7 0.1 0.5 Vertical Orifice 2 N/A N/A 41	Dutlet Orifice Area = et Orifice Centroid = ictor Plate on Pipe = Design Flow Depth= : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = : Top of Freeboard = <u>25 Year</u> 2.00 0.083 0.083 0.083 0.083 0.4 0.58 0.9 0.2 0.5 Vertical Orifice 2 N/A N/A 41	Not Selected N/A N/A N/A N/A N/A Old 0.12 4.12 0.09 0.17 Dhs table (Columns 2.25 0.099 0.699 0.099 0.6 0.72 1.1 0.3 0.5 Vertical Orifice 2 N/A 41	Not Selected N/A N/A N/A N/A ers for Spillway feet feet acres acre-ft W through AF). 100 Year 2.52 0.119 0.119 0.119 0.7 0.93 1.3 0.3 0.5 Vertical Orifice 2 N/A N/A 41	ft ² feet radians 500 Year 3.14 0.160 0.160 1.0 1.30 1.8 0.4 0.4 /ertical Orifice N/A N/A 40					



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

	The user can ow	verride the calcul	ated inflow hydr	ographs from th	is workbook with	inflow hydrogra	aphs developed in	n a separate prog	ram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5100 1111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	0:15:00	0.01	0.03	0.03	0.04	0.05	0.04	0.05	0.04	0.06
	0:20:00	0.03	0.09	0.10	0.13	0.16	0.09	0.11	0.12	0.16
	0:25:00	0.07	0.26	0.24	0.37	0.49	0.23	0.28	0.31	0.50
	0:30:00	0.10	0.37	0.34	0.52	0.65	0.70	0.84	0.96	1.31
	0:35:00	0.11	0.38	0.35	0.53	0.66	0.88	1.05	1.26	1.68
	0:40:00	0.10	0.36	0.34	0.50	0.63	0.94	1.12	1.33	1.76
	0:45:00	0.09	0.33	0.31	0.46	0.59	0.91	1.07	1.31	1.74
	0:50:00	0.09	0.31	0.29	0.43	0.55	0.88	1.04	1.26	1.67
	0:55:00 1:00:00	0.08	0.29	0.27	0.40	0.51	0.81	0.96	1.19	1.57
	1:05:00	0.08	0.27	0.25	0.37	0.48	0.75	0.89	1.12	1.49 1.42
	1:10:00	0.07	0.23	0.24	0.33	0.43	0.63	0.85	0.97	1.42
	1:15:00	0.06	0.21	0.19	0.30	0.40	0.57	0.69	0.86	1.16
	1:20:00	0.05	0.19	0.18	0.27	0.36	0.51	0.61	0.75	1.01
	1:25:00	0.05	0.17	0.16	0.24	0.32	0.45	0.54	0.65	0.88
	1:30:00	0.05	0.16	0.15	0.23	0.30	0.40	0.48	0.58	0.77
	1:35:00	0.04	0.15	0.14	0.21	0.28	0.36	0.43	0.52	0.69
	1:40:00	0.04	0.14	0.13	0.20	0.26	0.33	0.39	0.46	0.62
	1:45:00	0.04	0.13	0.13	0.18	0.24	0.30	0.35	0.42	0.56
	1:50:00	0.04	0.12	0.12	0.17	0.22	0.27	0.32	0.38	0.51
	1:55:00	0.03	0.11	0.11	0.15	0.20	0.25	0.29	0.34	0.45
	2:00:00 2:05:00	0.03	0.10	0.10	0.14	0.18	0.22	0.26	0.30	0.40
	2:10:00	0.03	0.08	0.08	0.12	0.15	0.19 0.15	0.22	0.25	0.34
	2:15:00	0.02	0.07	0.07	0.09	0.12	0.15	0.18	0.21	0.28
	2:20:00	0.02	0.03	0.00	0.06	0.10	0.12	0.14	0.10	0.17
	2:25:00	0.01	0.03	0.03	0.05	0.06	0.07	0.08	0.09	0.12
	2:30:00	0.01	0.03	0.03	0.04	0.05	0.05	0.06	0.07	0.09
	2:35:00	0.01	0.02	0.02	0.03	0.04	0.04	0.05	0.05	0.07
	2:40:00	0.01	0.02	0.02	0.03	0.03	0.03	0.04	0.04	0.06
	2:45:00	0.00	0.02	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:50:00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	2:55:00	0.00	0.01	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	3:00:00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	3:05:00 3:10:00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:15:00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:20:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	3:25:00	0.00	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.01
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

ummary Stage-Area-Volume ne user can create a summary		<u>tionships</u>				e will populate au	tomatically
ne user should graphically com	stage	ary S-A-V-D table	e to the full S-A-	V-D table in the Volume	chart to confirm Volume	n it captures all ke Total	y transition points.
Stage - Storage Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	Outflow [cfs]	
							For best results, include th
							stages of all grade slope changes (e.g. ISV and Flo
							from the S-A-V table on
							Sheet 'Basin'.
						-	Also include the inverts of outlets (e.g. vertical orifice
							overflow grate, and spillwa
							where applicable).
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							4
							-
							1
						1	4

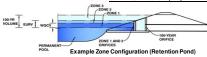
DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention_v4 00 (Sand Filter X1 Basin).xlsm, Outlet Structure

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.00 (December 2019)

Project: Homestead at Sterling Ranch Filing No. 2 Basin ID: Sand Filter - Basins Y1, W1, X2



PERMANENT Example Zone		on (Retentio	on Pond)	
Watershed Information				
Selected BMP Type =	SF	1		
Watershed Area =	2.74	acres		
Watershed Length =	750	Ĥ		
Watershed Length to Centroid =	375	ft		
Watershed Slope =	0.020	ft/ft		
Watershed Imperviousness =	45.00%	percent		
Percentage Hydrologic Soil Group A =	0.0%	percent		
Percentage Hydrologic Soil Group B =	100.0%	percent		
Percentage Hydrologic Soil Groups C/D =	0.0%	percent		
Target WQCV Drain Time =	12.0	hours		
Location for 1-hr Rainfall Depths =	User Input	1		
After providing required inputs above inc depths, dick 'Run CUHP' to generate runc the embedded Colorado Urban Hydro	ff hydrographs	using	Optional User	Override
Water Quality Capture Volume (WQCV) =	0.035	acre-feet		acre-feet
Excess Urban Runoff Volume (EURV) =	0.131	acre-feet		acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.124	acre-feet	1.19	inches
5-yr Runoff Volume (P1 = 1.5 in.) =	0.181	acre-feet	1.50	inches
10-yr Runoff Volume (P1 = 1.75 in.) =	0.232	acre-feet	1.75	inches
25-yr Runoff Volume (P1 = 2 in.) =	0.302	acre-feet	2.00	inches
50-yr Runoff Volume (P1 = 2.25 in.) =	0.358	acre-feet	2.25	inches
100-yr Runoff Volume (P1 = 2.52 in.) =	0.429	acre-feet	2.52	inches
500-yr Runoff Volume (P1 = 3.14 in.) =	0.574	acre-feet		inches
Approximate 2-yr Detention Volume =	0.098	acre-feet		
Approximate 5-yr Detention Volume =	0.135	acre-feet		
Approximate 10-yr Detention Volume =	0.182	acre-feet		
Approximate 25-yr Detention Volume =	0.201	acre-feet		
Approximate 50-yr Detention Volume =	0.210	acre-feet		
Approximate 100-yr Detention Volume =	0.238	acre-feet		
Define Zones and Basin Geometry				
Zone 1 Volume (WQCV) =	0.035	acre-feet		
Zone 2 Volume (EURV - Zone 1) =	0.095	acre-feet		
Zone 3 Volume (100-year - Zones 1 & 2) =	0.107	acre-feet		
Total Detention Basin Volume =	0.238	acre-feet		

Zone z volume (conv - zone i) =	0.055	acrenteer
Zone 3 Volume (100-year - Zones 1 & 2) =	0.107	acre-feet
Total Detention Basin Volume =	0.238	acre-feet
Initial Surcharge Volume (ISV) =	N/A	ft ³
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	N/A	ft
Slope of Trickle Channel (S _{TC}) =	N/A	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{SV}) =$ Surcharge Volume Length $(L_{SV}) =$ Surcharge Volume Width $(W_{SV}) =$ Depth of Basin Floor $(H_{LOOR}) =$ Length of Basin Floor $(M_{LOOR}) =$ Width of Basin Floor $(W_{LOOR}) =$ Area of Basin Floor $(N_{LOOR}) =$ Volume of Basin Floor $(N_{LOOR}) =$ Depth of Main Basin $(H_{MAIR}) =$ Length of Main Basin $(H_{MAIR}) =$ user ft² user user user user user user user user Length of Main Basin (H_{MAIN}) = <u>user</u> Length of Main Basin (L_{MAIN}) = <u>user</u> Width of Main Basin (L_{MAIN}) = <u>user</u> Area of Main Basin (M_{MAIN}) = <u>user</u> Volume of Main Basin (V_{MAIN}) = <u>user</u> Calculated Total Basin Volume (V_{total}) = <u>user</u> acre-feet

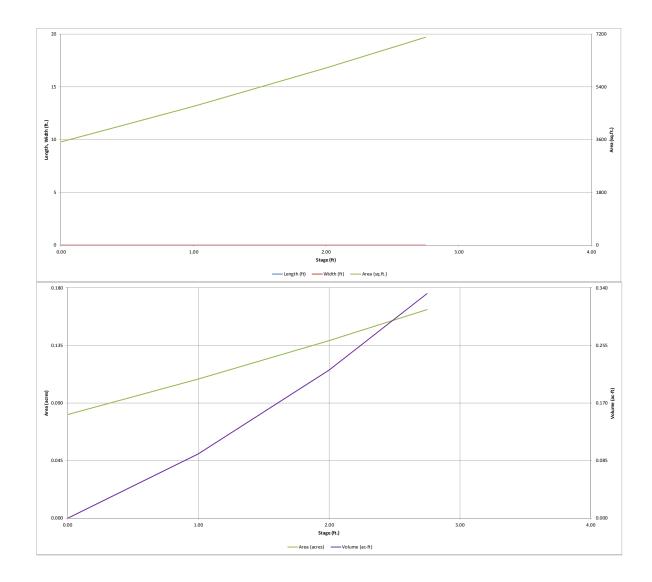
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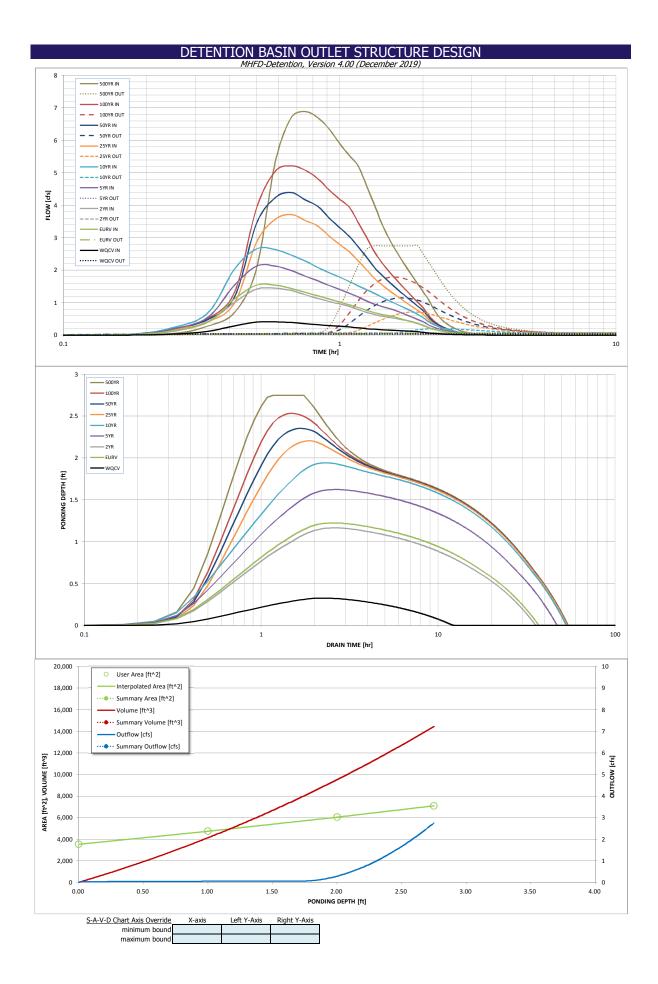
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ond)		Depth Increment = Stage - Storage Description	Stage (ft)	ft Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
		Media Surface 7057		0.00	-			3,524 4,732	0.081	4,128	0.095
		7058		2.00	-		-	6,037	0.139	9,512	0.218
		7058.75		2.75				7,090	0.163	14,435	0.331
				2				.,			
					1						
					-						
					-		-				
					-						
onal User	Overrides										
	acre-feet										
	acre-feet										
1.19	inches				-						
1.50	inches				-						
1.75	inches										
2.00	inches				-						
2.25	inches										
2.52	inches										
	inches										
					-		-				
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			1	1							

DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.00 (December 2019)



DETENTION BASIN OUTLET STRUCTURE DESIGN											
MHFD-Detention, Version 4.00 (December 2019) Project: Homestead at Sterling Ranch Filing No. 2											
-	Sand Filter - Basins										
ZONE 3				Estimated	Estimated						
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type					
VOLUME EURY woor Zone 1 (WQCV) 0.41 0.035 Filtration Media											
i land	100-YEAR ORIFICE		Zone 2 (EURV)	1.32	0.095	Circular Orifice					
PERMANENT ORIFICES			Zone 3 (100-year)	2.14	0.107	Circular Orifice					
Example Zone	Configuration (Ret	ention Pond)		Total (all zones)	0.238						
User Input: Orifice at Underdrain Outlet (typically	used to drain WQCV	in a Filtration BMP)				-	Calculated Paramet				
Underdrain Orifice Invert Depth =	2.10		he filtration media su	urface)		rdrain Orifice Area =	0.0	ft ²			
Underdrain Orifice Diameter =	0.95	inches			Underdrai	in Orifice Centroid =	0.04	feet			
User Input: Orifice Plate with one or more orifices	or Elliptical Clot Wai	(typically used to d		UDV in a codimentat	ion PMD)		Colorida De const				
Invert of Lowest Orifice =	N/A		bottom at Stage = 0			fice Area per Row =	Calculated Paramet N/A	ft ²			
Depth at top of Zone using Orifice Plate =	N/A		bottom at Stage = 0		-	liptical Half-Width =	N/A	feet			
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	j-			tical Slot Centroid =	N/A	feet			
Orifice Plate: Orifice Area per Row =	N/A	inches			-	Elliptical Slot Area =	N/A	ft²			
User Input: Stage and Total Area of Each Orifice F			[1	1	1	[
	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)			
Stage of Orifice Centroid (ft)		N/A	N/A	N/A	N/A	N/A	N/A	N/A			
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A			
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)			
Stage of Orifice Centroid (ft)		N/A	N/A	N/A	N/A	N/A	N/A	N/A			
Orifice Area (sq. inches)		N/A	N/A	N/A	N/A	N/A	N/A	N/A			
				•	•	•		<u>, , , , , , , , , , , , , , , , , , , </u>			
User Input: Vertical Orifice (Circular or Rectangula	· · · · · · · · · · · · · · · · · · ·		I				Calculated Paramet	ters for Vertical Orific	<u>e</u>		
	Zone 2 Circular	Zone 3 Circular					Zone 2 Circular	Zone 3 Circular	2		
Invert of Vertical Orifice =	0.60	1.75	-	bottom at Stage = 0	-	ertical Orifice Area =	0.00	0.79	ft ²		
Depth at top of Zone using Vertical Orifice =	1.73	2.62	-	bottom at Stage = 0) ft) Vertic	al Orifice Centroid =	0.03	0.50	feet		
Vertical Orifice Diameter =	0.80	12.00	inches								
User Input: Overflow Weir (Dropbox with Flat or S	loped Grate and Out	let Pipe OR Rectang	ular/Trapezoidal Wei	ir (and No Outlet Pip	e)		Calculated Paramet	ters for Overflow Weir	r		
oser input. Overnow weir (Dropbox weir hat or o	Not Selected	Not Selected					Not Selected	Not Selected	-		
Overflow Weir Front Edge Height, Ho =	N/A	N/A	ft (relative to basin b	ottom at Stage = 0 ft)) Height of Grat	te Upper Edge, H _t =	N/A	N/A	feet		
Overflow Weir Front Edge Length =	N/A	N/A	feet			Neir Slope Length =	N/A	N/A	feet		
Overflow Weir Grate Slope =	N/A	N/A	H:V		Grate Open Area / 1	00-yr Orifice Area =	N/A	N/A			
Horiz. Length of Weir Sides =	N/A	N/A	feet								
Overflow Grate Open Area % =	N/A	N/A									
Debris Clogging % =	N/A	N/A									
	Debris Clogging % = N/A N/A %										
User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)											
User Input: Outlet Pipe w/ Flow Restriction Plate (ictor Plate, or Recta			Overflow Grate Ope			N/A Flow Restriction Plat	ft²		
	Not Selected	ictor Plate, or Recta Not Selected	ngular Orifice)		Overflow Grate Ope	Calculated Parameter	s for Outlet Pipe w/ Not Selected	N/A Flow Restriction Plat Not Selected	ft ²		
Depth to Invert of Outlet Pipe =	Not Selected N/A	ictor Plate, or Recta Not Selected N/A	ngular Orifice) ft (distance below ba	isin bottom at Stage =	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area =	s for Outlet Pipe w/ Not Selected N/A	N/A Flow Restriction Plat Not Selected N/A	ft² <u>e</u> ft²		
	Not Selected	ictor Plate, or Recta Not Selected	ngular Orifice)	isin bottom at Stage =	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid =	s for Outlet Pipe w/ Not Selected N/A N/A	N/A Flow Restriction Plat Not Selected N/A N/A	ft ²		
Depth to Invert of Outlet Pipe =	Not Selected N/A	ictor Plate, or Recta Not Selected N/A	ngular Orifice) ft (distance below ba	isin bottom at Stage =	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid =	s for Outlet Pipe w/ Not Selected N/A	N/A Flow Restriction Plat Not Selected N/A	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe =	Not Selected N/A N/A	ictor Plate, or Recta Not Selected N/A	ngular Orifice) ft (distance below ba	isin bottom at Stage =	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid =	s for Outlet Pipe w/ Not Selected N/A N/A	N/A Flow Restriction Plat Not Selected N/A N/A N/A	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter =	Not Selected N/A N/A	ictor Plate, or Recta Not Selected N/A N/A	ngular Orifice) ft (distance below ba	isin bottom at Stage = Half-Ce	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid =	s for Outlet Pipe w/ Not Selected N/A N/A N/A	N/A Flow Restriction Plat Not Selected N/A N/A N/A	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = <u>User Input: Emergency Spillway (Rectangular or Ti</u>	Not Selected N/A N/A	ictor Plate, or Recta Not Selected N/A N/A	ngular Orifice) ft (distance below ba inches	isin bottom at Stage = Half-Ce	Overflow Grate Ope	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe =	s for Outlet Pipe w/ Not Selected N/A N/A N/A <u>Calculated Paramet</u>	N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A ters for Spillway	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = <u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	Not Selected N/A N/A apezoidal) 2.75 16.67 4.00	tictor Plate, or Recta Not Selected N/A N/A t (relative to basin feet H:V	ngular Orifice) ft (distance below ba inches	isin bottom at Stage = Half-Ce	Overflow Grate Ope 0 ft) C 0 ft) Outle entral Angle of Restri Spillway I Stage at Basin Area at	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	s for Outlet Pipe w/ Not Selected N/A N/A N/A N/A Calculated Paramet 0.21 4.00 0.16	N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = <u>User Input: Emergency Spillway (Rectangular or Ti</u> Spillway Invert Stage= Spillway Crest Length =	Not Selected N/A N/A rapezoidal) 2.75 16.67	ictor Plate, or Recta Not Selected N/A N/A ft (relative to basin feet	ngular Orifice) ft (distance below ba inches	isin bottom at Stage = Half-Ce	Overflow Grate Ope 0 ft) C 0 ft) Outle entral Angle of Restri Spillway I Stage at Basin Area at	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard =	s for Outlet Pipe w/ Not Selected N/A N/A N/A Calculated Paramet 0.21 4.00	N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A ters for Spillway feet feet	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = <u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	Not Selected N/A N/A apezoidal) 2.75 16.67 4.00	tictor Plate, or Recta Not Selected N/A N/A t (relative to basin feet H:V	ngular Orifice) ft (distance below ba inches	isin bottom at Stage = Half-Ce	Overflow Grate Ope 0 ft) C 0 ft) Outle entral Angle of Restri Spillway I Stage at Basin Area at	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	s for Outlet Pipe w/ Not Selected N/A N/A N/A N/A Calculated Paramet 0.21 4.00 0.16	N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = <u>User Input: Emergency Spillway (Rectangular or Tr</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	Not Selected N/A N/A apezoidal) 2.75 16.67 4.00 1.04	ictor Plate, or Recta Not Selected N/A N/A ft (relative to basin feet H:V feet	ngular Orifice) ft (distance below ba inches bottom at Stage = 0	nsin bottom at Stage = Half-Ce 9 ft)	Overflow Grate Ope 0 ft) C 0 utle entral Angle of Restri Spillway I Stage at Basin Area at Basin Volume at	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	s for Outlet Pipe w/ Not Selected N/A N/A N/A Calculated Paramet 0.21 4.00 0.16 0.33	N/A Flow Restriction Plat Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft	ft² <u>e</u> ft²		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = User Input: Emergency Spillway (Rectangular or Tr Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	Not Selected N/A N/A apezoidal) 2.75 16.67 4.00 1.04	ictor Plate, or Recta Not Selected N/A N/A ft (relative to basin feet H:V feet de the default CUHP EURV	ngular Orifice) ft (distance below ba inches bottom at Stage = 0 <u>hydrographs and ru</u> 2 Year	isin bottom at Stage = Half-Ce 0 ft) <u>inoff volumes by entt</u> 5 Year	Overflow Grate Ope 0 ft) C 0 ft) C 0 ft) Spillway I Stage at Basin Area at Basin Volume at ering new values in 10 Year	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = the Inflow Hydrogray 25 Year	s for Outlet Pipe w/ Not Selected N/A N/A N/A O.21 4.00 0.16 0.33 2015 table (Columns 1 50 Year	N/A Flow Restriction Plat Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft W through AF). 100 Year	ft ² e ft ² feet radians		
Depth to Invert of Outlet Pipe = Circular Orifice Diameter = User Input: Emergency Spillway (Rectangular or Ti Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) =	Not Selected N/A N/A 2.75 16.67 4.00 1.04	ictor Plate, or Recta Not Selected N/A N/A ft (relative to basin feet H:V feet de the default CUHP EURV 1.07	ngular Orifice) ft (distance below ba inches bottom at Stage = 0 <u>hydrographs and no 2 Year</u> 1.19	isin bottom at Stage = Half-Ce 0 ft) <u>Inoff volumes by ento</u> <u>5 Year</u> 1.50	Overflow Grate Ope 0 ft) C 0 ft) C 0 trial Angle of Restri Spillway [Stage at Basin Area at Basin Volume at ering new values in n 10 Year 1.75	Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = the Inflow Hydrogray 25 Year 2.00	s for Outlet Pipe w/ Not Selected N/A N/A N/A Calculated Paramet 0.21 4.00 0.16 0.33 0.33 0hs table (Columns I 50 Year 2.25	N/A Flow Restriction Plat Not Selected N/A N/A N/A ters for Spillway feet feet acre-ft W through AF). 100 Year 2.52	ft ² feet radians 500 Year 3.14		
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DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

lculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate p

	The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.									
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00 11111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.19	0.00	0.16	0.01	0.00	0.04
	0:20:00	0.12	0.40	0.42	0.55	0.69	0.41	0.48	0.51	0.71
	0:25:00	0.29	1.12	1.01	1.55	2.05	1.00	1.19	1.33	2.06
	0:30:00	0.40	1.54	1.42	2.13	2.66	2.87	3.44	3.91	5.31
	0:35:00	0.41	1.54	1.44	2.13	2.64	3.56	4.23	5.04	6.70
	0:40:00	0.39	1.44	1.37	1.99	2.47	3.72	4.39	5.22	6.89
	0:45:00	0.35	1.32	1.24	1.82	2.28	3.53	4.17	5.08	6.70
	0:50:00	0.32	1.21	1.13	1.67	2.08	3.36	3.97	4.82	6.35
	0:55:00	0.29	1.11	1.04	1.53	1.92	3.05	3.60	4.47	5.90
	1:00:00 1:05:00	0.27	1.02	0.96	1.41	1.79	2.79	3.31	4.19	5.54
	1:10:00	0.25	0.93	0.88	1.29	1.65	2.56 2.28	3.04 2.72	3.94 3.47	5.21 4.61
	1:15:00	0.22	0.05	0.79	1.05	1.32	2.20	2.72	3.02	4.03
	1:20:00	0.18	0.69	0.63	0.96	1.29	1.75	2.09	2.58	3.45
	1:25:00	0.10	0.64	0.59	0.89	1.18	1.56	1.86	2.25	3.02
	1:30:00	0.16	0.60	0.55	0.82	1.07	1.39	1.66	1.98	2.66
	1:35:00	0.15	0.55	0.51	0.77	0.98	1.25	1.48	1.76	2.35
	1:40:00	0.14	0.50	0.48	0.69	0.89	1.11	1.32	1.55	2.07
	1:45:00	0.13	0.45	0.45	0.62	0.81	0.99	1.17	1.36	1.82
	1:50:00	0.12	0.40	0.41	0.55	0.72	0.87	1.03	1.18	1.57
	1:55:00	0.10	0.35	0.36	0.48	0.64	0.76	0.89	1.01	1.34
	2:00:00	0.09	0.30	0.31	0.42	0.54	0.65	0.76	0.85	1.13
	2:05:00 2:10:00	0.07	0.24	0.24	0.33	0.43	0.50	0.59	0.65	0.87
	2:15:00	0.05	0.19 0.15	0.19 0.15	0.26	0.34	0.37	0.43	0.48	0.64
	2:20:00	0.04	0.13	0.13	0.21	0.23	0.29	0.33	0.30	0.49
	2:25:00	0.03	0.12	0.10	0.14	0.19	0.18	0.20	0.20	0.29
	2:30:00	0.02	0.08	0.09	0.11	0.15	0.14	0.16	0.16	0.22
	2:35:00	0.02	0.07	0.07	0.09	0.12	0.11	0.13	0.12	0.17
	2:40:00	0.02	0.05	0.06	0.07	0.10	0.09	0.10	0.09	0.13
	2:45:00	0.01	0.04	0.05	0.06	0.08	0.07	0.08	0.07	0.09
	2:50:00	0.01	0.03	0.04	0.05	0.06	0.05	0.06	0.05	0.07
	2:55:00	0.01	0.03	0.03	0.04	0.05	0.04	0.05	0.04	0.06
	3:00:00	0.01	0.02	0.02	0.03	0.04	0.03	0.04	0.03	0.05
	3:05:00	0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	3:10:00 3:15:00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	3:20:00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	3:25:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	3:30:00	0.00	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

ummary Stage-Area-Volume ne user can create a summar		<u>tionships</u>					tomatically				
ne user should graphically co	stage	ary S-A-V-D table	e to the full S-A-	V-D table in the Volume	chart to confirm Volume	n it captures all ke Total	y transition points.				
Stage - Storage Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	Outflow [cfs]					
							For best results, include th				
							stages of all grade slope changes (e.g. ISV and Flo				
							from the S-A-V table on Sheet 'Basin'.				
							Also include the inverts of outlets (e.g. vertical orifice				
							overflow grate, and spillwa				
							where applicable).				
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DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention_v4 00 (Sand Filter Y1 W1 X2 Basins).xlsm, Outlet Structure

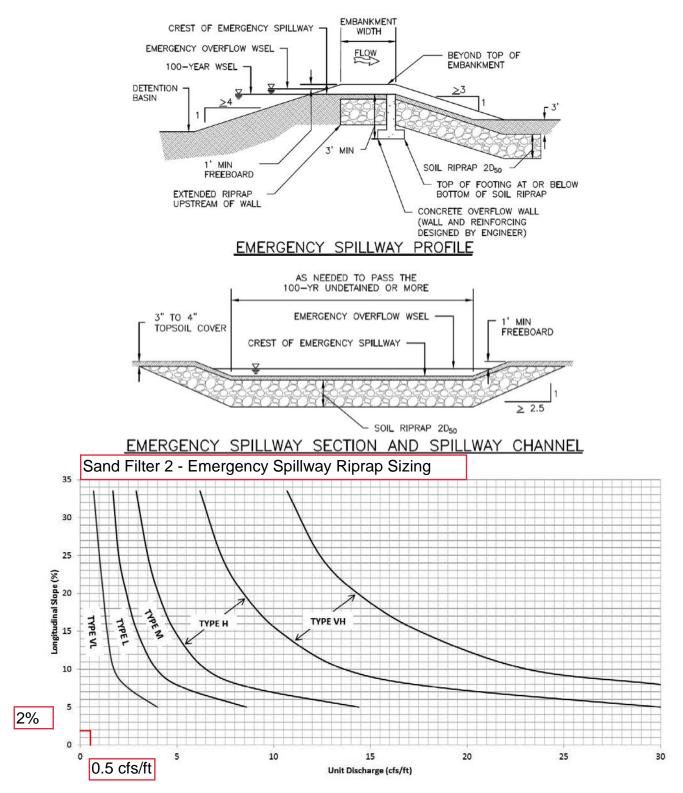


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C₅	C 100	t _c (min)	Q₅ (cfs)	Q ₁₀₀ (cfs)
X1	0.78	25%	0.22	0.46	7.3	0.8	2.8
X2	1.04	25%	0.22	0.46	7.3	1.1	3.7
W1	0.86	25%	0.22	0.46	7.3	0.9	3.1
Y1	0.84	25%	0.22	0.46	7.3	0.8	3.0

DESIGN POINT								
-	Q5	Q100						
DP	Total	Total						
1	0.8	2.8						
2	1.1	3.1						
3	0.9	3.0						
3.1	1.5	5.5						
4	0.8	3.0						
4.1	2.1	7.5						

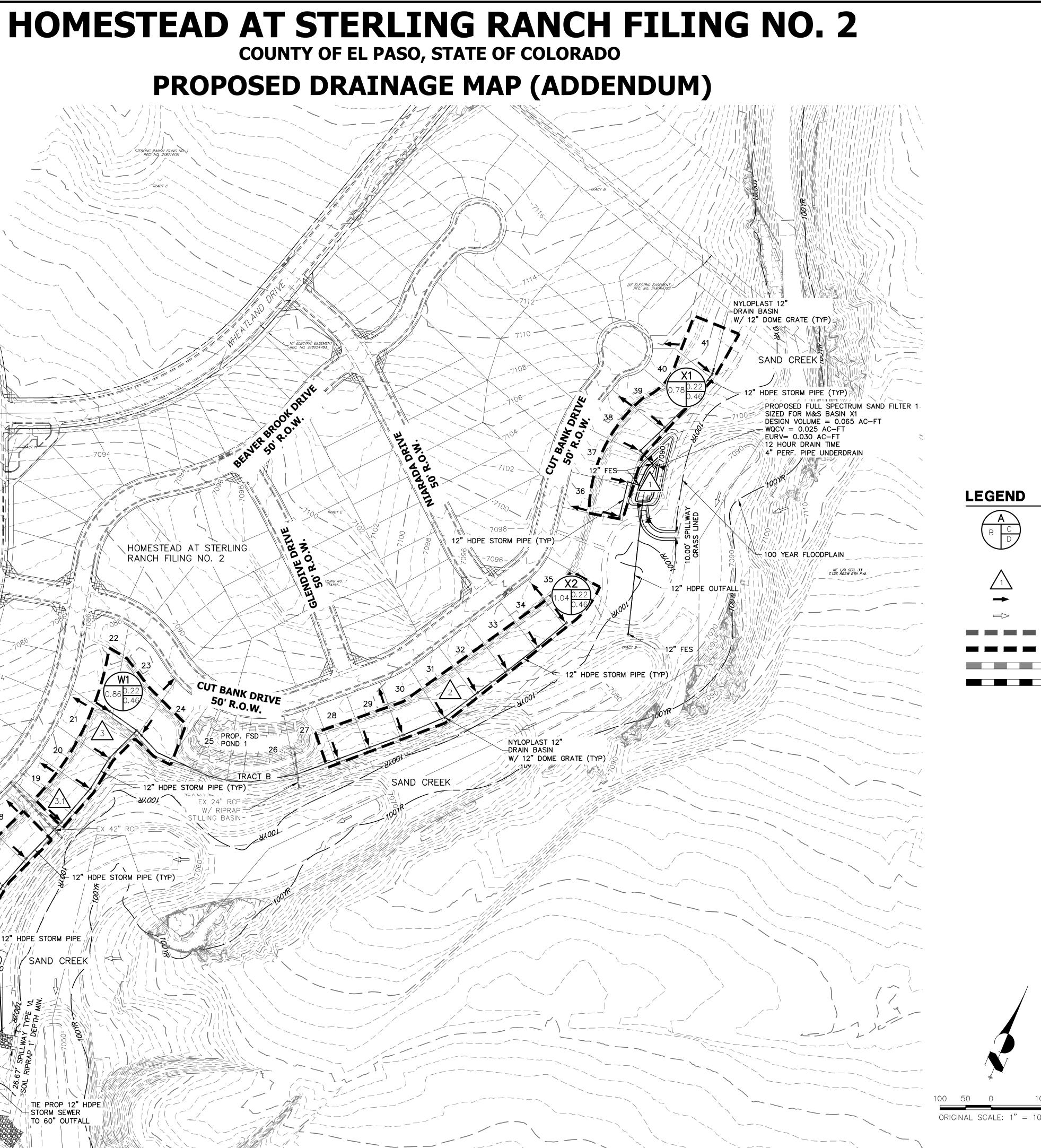
12" HDPE STORM PIPE SAND CREEK

TIE PROP 12" HDPE STORM SEWER

NYLOPLAST 12" DRAIN BASIN W/ 12" DOME GRATE(TYP) 🚿 PROPOSED FULL SPECTRUM SAND FILTER 2 SIZED FOR M&S BASINS W1, X2, & Y1 DESIGN VOLUME = 0.238 AC-FT WQCV = 0.035 AC-FT EURV= 0.095 AC-FT 12 HOUR DRAIN TIME

ÉLECTRIC EASEME REC. NO. 2180547

" PERF. PIPE UNDERDRAIN



ORIGINAL SCALE: 1" = 100'

PROPOSED DRAINAGE MAP (ADDENDUM) HOMESTEAD AT STERLING RANCH FILING NO. 2 JOB NO. 25188.00 08/18/2020 SHEET 1 OF 1

BASIN ID A: SUB-BASIN DESIGNATION B: AREA (AC) C: 5 YEAR STORM COEFFICIENT

DRAINAGE DISCHARGE DESIGN POINT

PROPOSED FLOW DIRECTION

HISTORIC FLOW DIRECTION

EXISTING DRAINAGE BASIN

EXISTING STORM SEWER

PROPOSED STORM SEWER

PROPOSED DRAINAGE BASIN

D: 100 YEAR STORM COEFFICIENT



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FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO.2

EL PASO COUNTY, COLORADO

March 2020

Prepared for: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

Prepared by:



CIVIL CONSULTANTS, INC. 102 E. Pikes Peak, Suite 500 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-007 SF-19-004

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drain age report and plan.

James F Morley BY TITLE: DATE:

ADDRESS: SR Land, LLC 20 Boulder Crescent, Suite 210 ColoradoSprings, CO80903

EL PASO COUNTY'S STATEMENT

Filedinaccordancewith the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

BY:	DATE:	

Jennifer Irvine, P.E. County Engineer / ECM Administrator

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

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APPENDIX

VicinityMap SoilsMap FIRMPanelW/Revised LOMR HydrologicCalculations HydraulicCalculations DrainageMaps 3

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

PURPOSE Additional language added in Addendum above

This document is the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. This report was previously discussed, as a preliminary drainage report, in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The following report is an analysis of the drainage for Homestead at Sterling Ranch Filing No. 2, single family lots, onsite and offsite drainage.

GENERAL LOCATION AND DESCRIPTION

Homestead at Sterling Ranch Filing No. 2 is located in the SE ¹/₄ of the NW ¹/₄, the SW ¹/₄ of the NE ¹/₄, and the NW ¹/₄ of the NE ¹/₄ of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian, and the NE ¹/₄ of the SW ¹/₄ of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridianwithin unincorporated El Paso County, Colorado. The site is bound on the south by an existing detention pond, to the north by Briargate Parkway and to the east by Sand Creek. ExistingDines Boulevard runs along the western site boundary. An existing residential development, Homestead at Sterling Ranch Filing No. 1, bounds the site to the west and a future commercial parcel bounds the site to the northwest. Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Homestead at Sterling Ranch Filing No. 2consists of 29.658 acresand ispresently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to southwest at grade rates that vary between 2% and 6%.

Land use for Homestead at Sterling Ranch Filing No. 2is currently listed as AG(Grazing Land). Improvements proposed for the site include pavedstreets, trails, a full spectrum detention pond, and utilities normally constructed for a residential development.

SOILS

Soils for this project are delineated by the map in the appendix as Pring Coarse Sandy Loam (71) and is characterized as Hydrologic Soil Types "B".Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". Vegetation is sparse, consisting of native grasses and weeds.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets can be found in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 and in the appendix of this report.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0533G, effective date December 7, 2018.An annotated FIRM Panel is included in the Appendix.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the ECM, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method.July 2019 ECM updated for MS4 permit.

FOUR STEP PROCESS

Step 1 Employ Runoff Reduction Practices. Roof drains will be directed to side yard swales and as possible to grass lined swales to aid in minimizing direct connection of impervious surfaces.

Step 2 Implement BMPs that provide a water quality capture volume with slow release. – An existing Full Spectrum Detention Facility (see Sterling Ranch Filing Nos. 1&2 MDDP, Pond 4)was planned and constructed to handle tributary flows for the southwest portion of the site. All remaining tributary areas from the site will be treated in a proposed temporary Full Spectrum Detention Facility, Interim Pond 1. Both ponds will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours.

Step 3 Stabilize streams. – With the full spectrum detention facilities in place, the runoff from the proposed residential development will be reduced to predevelopment conditions. The developed discharge from the site is less that existing and therefore is not anticipated to have negative effects on downstream drainageways. Additionally, the Sand Creek Channel will be reinforced with selected areas of rip rap bank protection, vegetative slope stabilization, check structures and drop structures.

Step 4 Consider need for Industrial and Commercial BMPs. – No industrial or commercial land uses are proposed with this development. The proposed residential development area will implement a Stormwater Management Plan (SWMP) incorporation proper housekeeping procedures. Onsite drainage will be routed through proposed private temporary Full Spectrum Detention Facility (FSD), Interim Pond 1, to minimize introduction of contaminates to the county's public drainage systems.

EXISTING DRAINAGE CONDITIONS

The Homestead at Sterling Ranch Filing No. 2 site consists of 29.658 acres and is situated west of the Sand Creek Watershed. This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing Nos. 1&2 MDDP").

See the Historic conditions map, the Homestead at Sterling Ranch Filing No. 2 site lies within the Basin EX-4 (Q5 = 71 cfs, Q100 = 352 cfs) and is a 330 acre area of land located on the western portion of the site, including the Sand Creek channel. A portion of this basin extends off-site to the northwest of Vollmer Road, and at the time this map was created was undeveloped property. Runoff from the basin generally travels from north to south until it reaches the northern boundary of the site, being conveyed in the Sand Creek channel. Homestead at Sterling Ranch Filing No. 2 and the surrounding areas, with the exception of the existing Barbarick Subdivision; have already been graded during the overlot of the subdivision. Please refer to the Sterling Ranch Filing Nos. 1&2 MDDP by MS Civil Consultants for information on existing conditions and overlot drainage patterns. A copy of the historic and existing conditions map has been provided in the appendix.

PROPOSED DRAINAGE CHARACTERISTICS

General Concept Drainage Discussion

The following is a description of the onsite basins, offsite bypass flows and the overall drainage characteristics for the development of Sterling Ranch Filing No. 2. The development of Sterling Ranch Filing No. 2 consists of residential streets and cul-de-sacs, proposedstorm drainage improvements, and lots located within the filing boundary. The proposed development results in drainage patterns and flow values thatare the same or less thanthose in the Sterling Ranch Filing Nos. 1&2 MDDP. Surface flow is designated as Design Points (DP). The following DPs and Basins were determined using the Rational Method since this method offers a more conservative approach to drainage. It should be noted that all calculations and drainage basins have been revised to reflect the new criteria updates by the El Paso County/City of Colorado Springs Drainage Criteria Manual. For comparison, the **asterisk (*)** symbol in the detailed drainage discussions below represents each Basin or Design Point as labeled in the Sterling Ranch Filing Nos. 1&2 MDDP.Asterisk symbols on the Proposed Drainage Map in the appendix also represent Basins, Design Points and Pipe Runs as presented in the Sterling Ranch Filing Nos. 1&2 MDDP.

Detailed Drainage Discussion (Design Points)

DP2*, 5.39 acres, consists ofBasin B*planned residential lots and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=8.0 cfs and Q100=19.3 cfs has been calculated for DP2*. The surface runoff is routed via overlot grading and planned swales to two existing 15' CDOT Type R at-grade inlets. The flows are routed east via a 36" RCP to DP5.

DP3*, 2.92 acres, consists ofBasin C* residential lots within Homestead at Sterling Ranch Filing No. 1, and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.2 cfs and Q100=10.1 cfs has been calculated for DP3*. The surface runoff is routed via overlot grading and proposed swales to an existing 5' CDOT type R sump inlet. The flows captured by the inlet are routed to existing Detention Pond 4.

DP4*, 9.36 acres, consists ofBasin D* and Basin E*residential lots within Homestead at Sterling Ranch Filing No. 1 and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and BasinF* (Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=16.1 cfs and Q100=36.7 cfs has been calculated for DP4. The surface runoff is routed via overlot grading and curb and gutter to DP4* which will be collected by a 15' CDOT type R atgrade inlet. The intercepted flow (Q5=13.3 cfs and Q100=20.0 cfs) will combine with flows from DP3* and be routed east via a 30" RCP (PR6*, Q5=16.8 cfs and Q100=29.4 cfs) to existing Detention Pond 4.

DP5*,0.80 acres, consists ofBasin G* residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Basin H* existing Dines Boulevard, with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year and flowby from Sterling Ranch Filing Nos. 1&2 MDDP DP4*. Developed runoff of Q5=4.2 and Q100=19.7cfs has been calculated for DP5*. The surface runoff is routed via overlot grading and curb and gutter to DP5* which is collected by an existing 15' CDOT type R at-grade inlet. DP5* has an intercepted flow of (Q5=4.2cfs and Q100=14.7cfs) and of flowby of (Q5=0.0cfs and Q100=5.0cfs). Flowby from DP5* continues on toPond FSD13, east of Dines Boulevard.See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

DP6*, 4.68 acres, consists of Sterling Ranch Filing Nos. 1&2 MDDP Basins J* and K*planned residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Sterling Ranch Filing Nos. 1&2 MDDP Basin I* (Wheatland Drive) and Basin L*(Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=14.1 cfs and Q100=26.7cfs has been calculated for DP6*. The surface runoff is routed via overlot grading and curb and gutter to DP6* which is collected by an existing 15' CDOT type R at-grade inlet. DP6* has an intercepted flow of (Q5=12.1cfs and Q100=17.2cfs) and of flowby of (Q5=2.0 cfs and Q100=9.5cfs).Flowby from DP6* continues on to Pond FSD13, east of Dines Boulevard. See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

DP7,4.42 acres, consists ofBasin Pproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=5.7 and Q100=13.8cfs has been calculated for DP7. Surface runoff is routed via overlot grading and curb and gutter to DP7 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer. The flows from DP7 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

DP8,3.78, acres, consists ofBasin Qproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.9 and Q100=11.8cfs has been calculated for DP8. Surface runoff is routed via overlot grading and curb and gutter to DP8 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer.The flows from DP8 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

DP9, acres, consists ofBasin Rproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=2.2 and Q100=5.4cfs has been calculated for DP9. Surface runoff is routed via overlot grading and curb and gutter to DP9 which is collected by a proposed 5' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inletcombine with capturedflows contributed from Design Points 7 & 8 and are routed to existing Detention Pond 4 by Pipe Run 4 (Q5=12.4 and Q100=30.1cfs). Pipe Run 4 connects to existing Sterling Ranch Filing Nos. 1&2 MDDP Pipe Run 10* (Q5=12.5 and Q100=30.4 cfs) and is discharged into the forebay of existing Detention Pond 4. Flows contributed to the forebay of existing Pond 4 are approximately equal to those anticipated by the MDDP, therefore Pond 4 has the capacity for SWQ and Full Spectrum Detention for these flows.

DP10, 9.14, acres, consists of Basin T proposed residential lots with runoff coefficients of 0.30 for the 5-year and 0.50 for the 100-year. Developed runoff of Q5=9.4 and Q100=15.6cfs has been calculated for

DP10. Surface runoff is routed via overlot grading and curb and gutter to DP10 which is collected by a proposed 15' CDOT type R at-grade inlet. DP10 has an intercepted flow of (Q5=9.1 cfs and Q100=12.7cfs) and of flowby of (Q5=0.3cfs and Q100=2.9cfs). Flows captured by the proposed 15' CDOT type R at-grade inletare routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP11,1.48, acres, consists ofBasin V1proposed residential lots with runoff coefficients of 0.38 for the 5year and 0.55 for the 100-year. Developed runoff of Q5=1.9 and Q100=15.6 cfs has been calculated for DP11. Surface runoff is routed via overlot grading and curb and gutter to DP11 which is collected by a proposed 15' CDOT type R at-grade inlet. DP11 has an intercepted flow of (Q5=1.9cfs and Q100=12.7cfs) and of flowby of (Q5=0.0cfs and Q100=2.9cfs). Flows captured by the proposed 15' CDOT type R at-grade inlet are routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP12,4.50, acres, consists ofBasin Uproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and flowby from DP10. Developed runoff of Q5=6.2cfs and Q100=17.2 cfs has been calculated for DP12. Surface runoff is routed via overlot grading and curb and gutter to DP12 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP13,0.83, acres, consists ofBasin V2proposed residential lots with runoff coefficients of 0.38 for the 5year and 0.55 for the 100-year and flowby from DP11. Developed runoff of Q5=1.2 and Q100=5.9cfs has been calculated for DP13. Surface runoff is routed via overlot grading and curb and gutter to DP13 which is collected by a proposed modified 5' length by 4.5' wide CDOT type R sump inlet.

DP14,0.56, acres, consists ofBasin W3proposed full spectrum detention Pond 1with runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and contributed flow from pipe run 9. Developed runoff of Q5=19.6cfs and Q100=52.4cfs has been calculated for DP14. All flows captured by inlets at Design Points DP10, DP11, DP12 and DP13 are routed by Pipe Run 9 (PR9, Q5=17.9 and Q100=47.1 cfs) to the forebay inPond 1 and combine withsurface runoff within Basin W1. An outlet structure with an orifice plate and restrictor plate regulates release rates and provides treatment to all flows tributary to DP14. See the Water Quality Provisions discussion in this report for more information on Pond 1.

Basins labeled on the Proposed Drainage Map marked with a "*", were previously analyzed and shown in the Final Drainage report for Sterling Ranch Filing No. 1. These basins are; B*, C*, D*, E*, F*, G*, H*, I*, L*, &S*. They are shown on the Proposed Drainage Map for continuity. Basins K & J additionally contribute to Design Points 3, 4, 5 &6. Therefore, the inlets sizing at these design points has been verified.

Detailed Drainage Discussion (Drainage Basins)

Basins X1, X2,W1, and Y1(0.78, 1.04, 0.86 and 0.084 acres respectively), consists of proposedresidential backyard lotslocated along the eastern boundary of the sitewith runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year.Developed runoff of (Q5=0.8, 1.1, 0.2, and 0.8c fs and Q100=2.8, 3.7, 1.7, and 3.0 cfsrespectively has been calculated for the basins. Runoff produced within the residential backyard lots, of Basins X1, X2, W1 and Y1 will be conveyed in backyard swalesand as sheet flow to a Sand Filter Basin within each lot. The <u>treated</u> flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. A 20' wide typical drainage easement is provided within the lots to accommodate the BMP's. The facilities constructed are to be privately maintained by the Sterling Ranch metro district.

Basins X, W2, and Y (0.22, 0.26, and 0.09 acres respectively), consists primarily of vegetated tracts and portion of residential backyards that will discharge as sheet flow to the Sand Creek Channel. The developed flow rates from Basins X, W2, and Y are Q5=0.2, 0.1, 0.1 cfs and Q100=0.8, 0.8, and 0.3 respectively. The total combined developed area being discharge to the channel is less than one acre. It

is not practicable to provide WQCV for these areas, as stated earlier in this paragraph, areas consists primarily of vegetated tracts with no development.

CHANNEL IMPROVEMENTS

Slope grading and intermittent channel bank lining has been proposed for portions of the developable areas adjacent to Sand Creek to protect the developed lots and prevent excessive erosion until the DBPS recommended Sand Creek Channel improvements are installed. The proposed slope grading is intended to reduce outer bankgrades and bring uniformity to areas where significant riling and destabilization has occurred. Proposed channel stabilization improvements includes placement of soil riprap and turf reinforcement matting along embankment toes and along embankment slopes, both of which will function to retain soils and vegetation during heavy rains or larger flood flow events. All disturbed areas, not hardscaped will be re-vegetated with native species grasses, per El Paso County erosion control standards. Storm sewer outfalls into Sand Creek shall be protected by low-tailwater riprap basins. The outfall protection is shown on the accompanying drainage map in the appendix. Refer to the Homestead Filing No.2 Grading and Erosion Control Plans for riprap and turf reinforcement map placement and construction details.

Permanently installed check structures and rip-rap channel lining will be installed within Sand Creek Channel to handle the runoff from fully developed Sterling Ranch and up-gradient watershed in accordance with the Sand Creek DBPS. A discussion regarding the timing of these channel improvements is provided in a subsequent paragraph titled Sterling Ranch Filing No. 1 Subdivision Improvement agreement which follows the Construction Costs segment of this report. Financial Assurance shall be posted for the proposed Sand Creek Channel Improvements and Bank Stabilization (Slope Protection and grade control structures).

WATER QUALITY PROVISIONS

The proposed Full Spectrum Detention Facility, Pond 1 functions to provide detention storage and water quality facility for runoff produced onsite from tributary Basins T, U, V1, V2 and W3. This water quality facility is designed to treat 0.245 ac-ft of water quality storage (WQCV), 0.741 ac-feet of excess urban runoff volume (EURV) and 1.331 ac-ft of 100-year storage. A rolled erosion control blanketed emergency spillway, concrete forebay, trickle channel and outlet structure, and gravel maintenance access road has been designed for Pond 1.

A 24" RCP pipeextending from the proposed modified 6'x2.9' CDOT Type D sump inlet (see Design Point 13) will convey discharge from the pond to Sand Creek. Runoff discharged to Sand Creek is anticipated to reach peak flow rates of Q5=0.7 cfs and Q100=23.4 cfs. A soil riprap stilling basin has been provided at the termination of the pipe to arrest erosion.

Runoff produced within the residential backyard lots, of Basins X1, X2, W1 and Y1 will be conveyed in backyard swales and as sheet flow to a Sand Filter Basin within each lot. The <u>treated</u> flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. This water quality facility, for each Sand Filter Basin, is designed to treat 0.001 ac-ft of water quality storage (WQCV), 0.005 ac-feet of excess urban runoff volume (EURV) and 0.014 ac-ft of 100-year storage.A 20' wide typical drainage easement is provided within the lots to accommodate the BMP's. The facilities constructed are to be privately maintained by the Sterling Ranch Metropolitan District. Access to maintain these sand filter basins is from the regional trail along sand creek.

The WQCV and EURV required for the site has been determined using the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II. Refer to the water quality

facility sizing calculations located within the appendix of this report(see UD-Detention Worksheet in appendix).

As previously discussed, refer to Sterling Ranch Filing Nos. 1&2 MDDP for additional information regarding existing FSD Pond 4. The previously approved FSD Pond was constructed with the Sterling Ranch Filing No. 1 construction drawings in 2018-2019.

EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved "Early Grading Plan for Sterling Ranch Phase I <u>Onsite</u> Grading & Erosion Control", November 18, 2015. And "Early Grading Plan for Sterling Ranch Phase I <u>Offsite</u> Grading & Erosion Control", December 3, 2015. Grading and Erosion control operations are currently underway (July 2019). Grading and Erosion Control will cease with the final development of the site in the next 6-12 months.

CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FIL. NO. 2

Drainage Facilities:

Updated Cost Opinion included in Addendum above

Drainage improvements are planned with the development of Homestead at Sterling Ranch Filing No. 2. A majority of the construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Any additional improvements and costs are listed below.

The following list of drainage improvements are **Non-Reimbursable**. The Reimbursable facilities are outlined in the Sterling Ranch Filing No. 1 Final Drainage Report and Sterling Ranch MDDP. Refer to the MDDP for Sterling Ranch Cost and Fee Analysis Report (February 2019).

Item	Description	Quantity	Unit Cost	
1.	18" RCP	31 LF	\$40 /LF	\$1,240.00
2.	24" RCP	127 LF	\$50 /LF	\$6,350.00
3.	-30" RCP	998 LF	\$85 /LF	\$84,830.00
4.	36" RCP	<u>8 LF</u>	\$105 /LF	\$840.00
5	42" RCP	<u>699 LF</u>	\$185 /LF	\$129,315.00
<u>6.</u>	24" FES	1 EA	\$750 /EA	\$750.00
8.	42" FES	1 EA	\$1,250 /EA	\$1,250.00
9.	5.0'x4.5' CDOT Type R Sump Inlet	1 EA	\$4,000 /EA	\$4,000.00
10.	10' CDOT Type R Sump Inlet	4 EA	\$4,700 /EA	\$18,800.00
11.	15' CDOT Type R At-Grade Inlet	2 EA	\$6,000 /EA	\$12,000.00
12.	4.0' Type II MH	1 EA	\$3,500 /EA	\$3,500.00
13.	5.0' Type II MH	2 EA	\$4,000 /EA	\$8,000.00
14.	6.0' Type II MH	1 EA	\$4,500 /EA	\$4,500.00
17.	5.0'x6.0' MH	2 EA	\$6,500 /EA	\$13,000.00
18.	5.5'x5.5' MH	1 EA	\$6,500 /EA	\$6,500.00
<u>19.</u>	Headwall/Wingwall	1 EA	\$6,000 /EA	\$6,000.00
20.	Full Spectrum Det. Pond 1	<u>1 EA</u>	\$15,000 /EA	\$15,000.00

21.	FSD Pond 1 Outlet Structure	1	EA	\$12,600	/EA		\$12,600.00
22.	Ind. Lot Sand Filter Basins w/6" Pipe	26	EA	\$2,000	/EA		\$52,000.00
23	18" Drain Basin Manholes w/Lids	27	EA	\$1,000	/EA		27,000.00
24	12" ADS Pipe	1,658		\$26	/LF		43,108.00
	1	,				Total \$	\$450 583 00

The following list of drainage improvements are **Reimbursable** for the improvements to the Sand Creek Channel adjacent to Homestead at Sterling Ranch Filing No.2. The reimbursement is up to the amount as shown in the DBPS or as adjusted through the City/EPC Drainage Board.

Sand Creek Channel Improvements

Item	Description	Quantity		Unit Cost			Cost
1.	Rip Rap Protection	390	Ton	\$80	/Ton		\$31,200.00
2.	Drop/Check Structures	5	EA	\$75,000	/EA		\$375,000.00
3.	Slope Stabilization Blankets	7,435	SY	\$6	/SY	_	\$44,610.00
						Total	\$450,810.00

DRAINAGE & BRIDGE FEES – HOMESTEAD AT STERLING RANCH FIL. NO. 2

This site is within the Sand Creek Drainage Basin. The 2019 Drainageand BridgeFees per El Paso County for the HOMESTEAD AT STERLING RANCH FILING NO. 2site are as follows:

Per Homesteadat Sterling Ranch Filing No. 2 Plat –			Total Area	29.658 Acres					
HOMESTEAD AT	STERLIN	IG R	ANCH F	ILING	G NO. 2 FEES:				
Drainage Fees:	29.658	Х	46%	\$	18,940.00	=		\$	258,392.36
Bridge Fees:	29.658	х	46%	\$	5,559.00	=		\$	75,839.66
-							Total	\$	334,232.02

STERLING RANCH FILING NO. 1 - SUBDIVISION IMPROVEMENTS AGREEEMENT

Sterling Ranch Filing No. 1 final plat and SIA has been recorded, and addressed the following drainage improvements Not located/and located in the Sand Creek Channel. The following SIA paragraphs outlined drainage for Sterling Ranch in the following manner;

2. Drainage and Landscaping Tracts: Improvements on Tracts A, B, F, H, I, J, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z, AA and CC as identified on the final plat of Filing No. 1 will be completed to the satisfaction of the County and District and, upon said completion, the improvements will be dedicated to and accepted by the District. Improvements on Tract D (Sand Creek) will be completed to the satisfaction of the County and upon said completion; the improvements will be dedicated to and accepted by the District. The ownership and maintenance of storm drain facilities and structures not located on the foregoing tracts shall be determined as follows. All storm pipes shall be owned and maintained by the District except where located in County road rights of way (see Paragraph 5 below), in which case the County shall own and maintain the storm drain facilities and structures, including but not limited to, inlets and manholes. A typical cross section describing the ownership and maintenance responsibilities of drainage improvements within County rights of way is attached as <u>Exhibit C</u> hereto.

7. Timing of Construction and Acceptance:

a. **Drainage Improvements Not Located in Sand Creek Channel**: Except as set forth below in subsection 6.b. (drainage improvements located in Sand Creek Channel), all drainage improvements described in <u>Exhibit A</u> and constructed within the Drainage and Landscaping Tracts identified in paragraph 2 above shall be completed by the

Subdivider and District, meeting all applicable standards for preliminary acceptance, prior to the recording of the first replat of Tracts C, E, G, K or BB. In the event that a portion of the drainage improvements are not completed prior to the recording of the first replat, then prior to such recording collaterial sufficient in the opinion of the County to assure completion of the improvements must be posted by the Subdivider and a deadline by which such drainage improvements shall be completed shall be established by written agreement.

b. **Drainage Improvements Located in Sand Creek Channel (Tract D):** The District agrees that it will construct or cause the construction of all drainage improvements to be located in Tract D as well as future tracts within Sterling Ranch containing the Sand Creek Channel in accordance with the following:

i. Bank stabilization of the Sand Creek channel shall be required prior to any replats or other final plats adjacent to the channel. The design and installation of said improvements shall be accomplished and guaranteed through the normal subdivision review and collateralization process.

ii. Other drainage improvements in Tract D and future tracts containing the Sand Creek Channel, such as drop structures, check structures and similar stabilization or protection improvements, will be designed and constructed by the District with the final construction drawings to be approved by the County no later than the final platting of the 700th single family lot within the boundaries of the approved Sterling Ranch Sketch Plan and the completion of all said improvements no later than the 800th single family lot with the boundaries of the approved Sterling Ranch Sketch Plan.

iii. In order to assure completion of the drainage improvements required in Subsection 6.b.ii above as well as a fair apportionment of the costs of said drainage improvements amongst adjacent Sterling Ranch subdividers, the District agrees to establish a Sand Creek Channel Drainage Fee to be paid into a District Escrow Fund by adjacent subdividers at the time of final platting. The amount of the fee shall be a minimum of One Thousand Dollars (\$1,000.00) per single family lot. The details of the proposed Sand Creek Channel Drainage Fee and the District Escrow Fund shall be agreed to by the parties in advance of the submittal of the first replat of or subdivision of the Master Pad Sites or other property located within Sterling Ranch.

A full copy of the recorded SIA is located in the files of El Paso County and EPC Clerk and Recorders office under Reception No. 218714151

SUMMARY

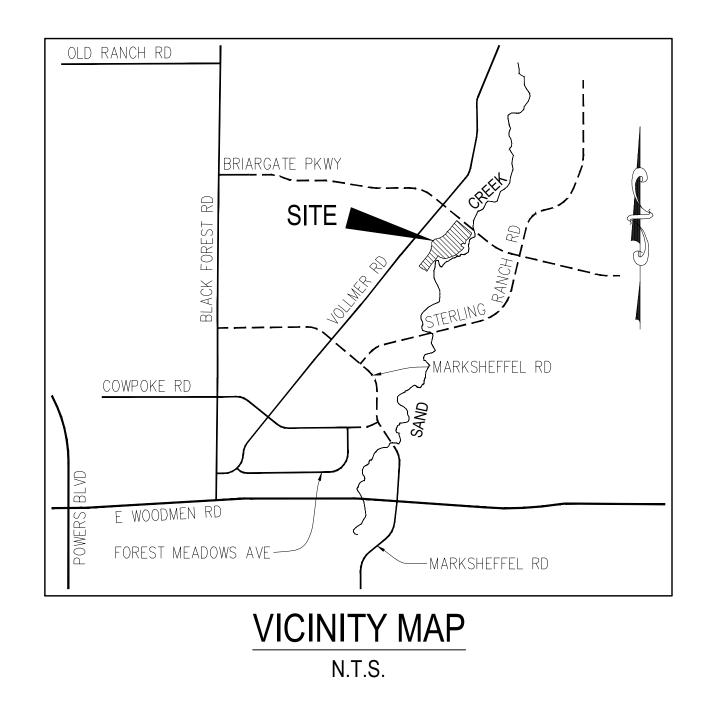
Development of this site will not adversely affect the surrounding development per this final drainage report with no negative impacts to the neighboring developments. The existing and proposed drainage facilities will adequately convey, detain and route runoff fromtributary and onsite flows to the Sand Creek Drainage channel. Full Spectrum Detention and Water Quality Ponds will be used to discharge developed flows into Sand Creek per the Urban Drainage criteria flow rates, which are at or less than the historic flow. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. The development of the HOMESTEAD AT STERLING RANCH FILING NO. 2project(s)shall not adversely affect adjacent or downstream property.

REFERENCES

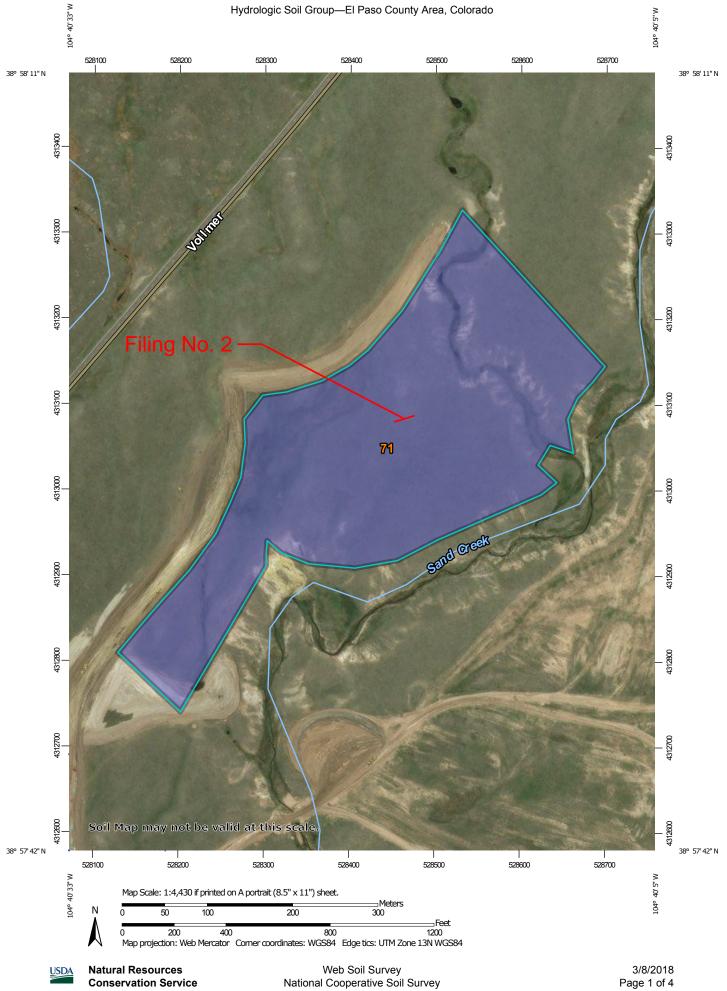
- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2.) "Urban Storm Drainage Criteria Manuals, Volumes 1-3"
- 3.) NRSC Web Soil Survey Map for El Paso County. http://websoilsurvey.nrcs.usda.gov
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date December 7, 2018.
- 5.) "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996
- 6.) "Sterling Ranch-Phase 1 Offsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 7.) "Sterling Ranch-Phase 1 Onsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 8.) "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2 and Final Drainage Report for Sterling Ranch Filing No. 1", prepared by M&S Civil Consultants, Inc., dated April 2017
- 9.) "Sterling Ranch Filing Nos. 1&2 MDDP" prepared by MS Civil Consultants, Inc., dated October 2018.

APPENDIX

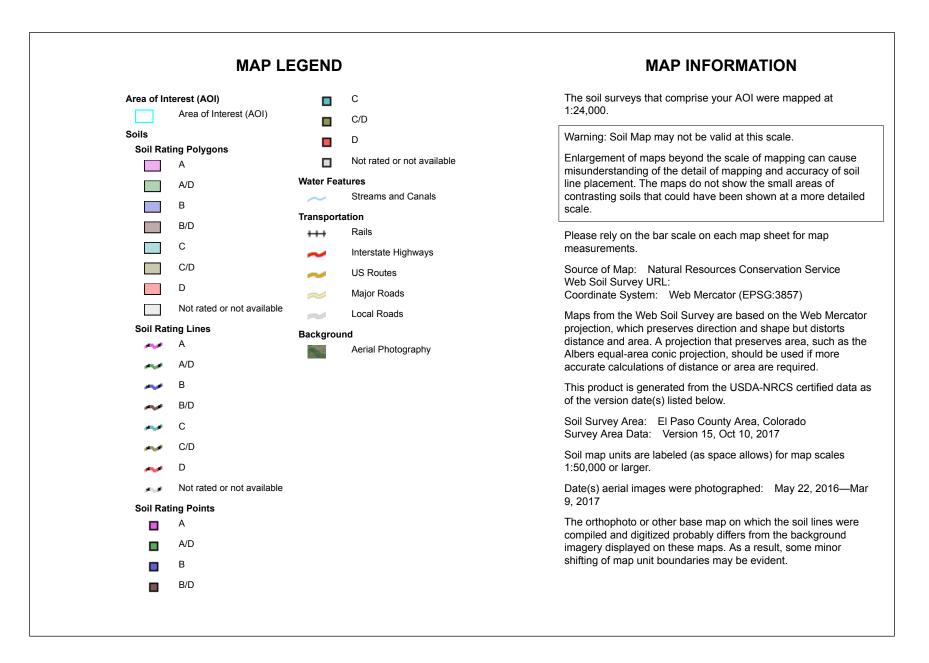
VICINITY MAP



SOILS MAP



Conservation Service



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	29.0	100.0%
Totals for Area of Intere	st		29.0	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

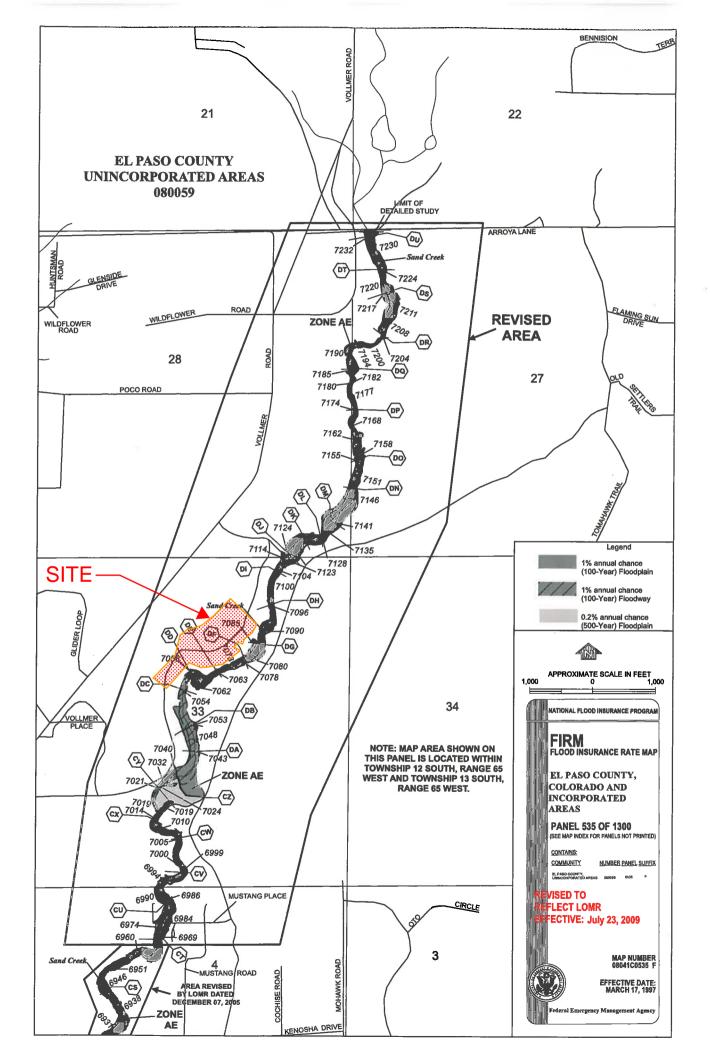
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified Tie-break Rule: Higher

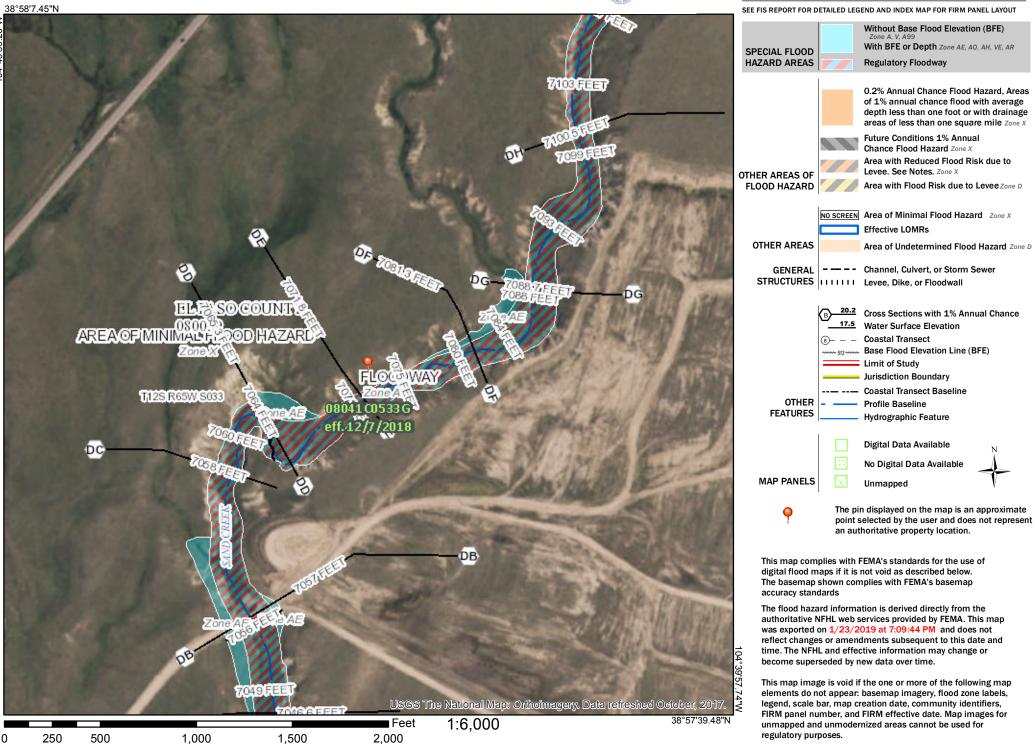
FIRM PANEL W/ REVISED LOMR



National Flood Hazard Layer FIRMette



Legend



Questions concerning the VERTCON process may be mailed to <u>NGS</u>

Latitude: 38.964784

Longitude: 104.67180

NGVD 29 height:

Datum shift(NAVD 88 minus NGVD 29): 1.196 meter

1.196 meters = 3.92 feet

NAVD88 - 3.92 feet = NGVD29

STORM 4 Outfall to Sand Creek Channel

Cross Section DE = 7071.8 NAVD88

7071.8 NAVD88 - 3.92 feet = 7067.88 NGVD29

HYDROLOGIC CALCULATIONS

HOMESTEAD AT STERLING RANCH FILING NO. 2 FINAL DRAINAGE REPORT

(Area Drainage Summary)

From Area Runoff Coeff	îcient Summa	ury			OVER	LAND		STRE	ET / CH	IANNEL F	FLOW	Time of T	Travel (T _t)	INTENS	SITY **	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C100	C ₅	Length	Height	T _C	Length	Slope	Velocity	Tt	TOTAL	СНЕСК	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
					Prop	osed Ar	ea Dra	inage S	umma	ry		<u> </u>					
ONSITE BASINS					•					•							
J	0.43	0.22	0.46	0.22	90	1.8	12.0	0	2.0%	3.0	0.0	12.0	10.5	4.1	6.8	0.4	1.3
K	0.61	0.22	0.46	0.22	75	1.5	10.9	0	2.0%	3.0	0.0	10.9	10.4	4.1	6.8	0.5	1.9
Р	4.42	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	5.7	13.8
Q	3.78	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	4.9	11.8
R	1.57	0.38	0.55	0.38	100	2	10.3	450	1.6%	3.0	2.5	12.8	13.1	3.8	6.3	2.2	5.4
Т	9.14	0.30	0.50	0.30	100	2	11.5	942	2.1%	3.0	5.2	16.7	15.8	3.4	5.8	9.4	26.4
U	4.50	0.38	0.55	0.38	100	2	10.3	457	1.5%	3.0	2.5	12.9	13.1	3.8	6.3	6.4	15.6
V1	1.48	0.38	0.55	0.38	100	2	10.3	600	2.0%	3.0	3.3	13.6	13.9	3.7	6.2	2.1	5.0
V2	0.83	0.38	0.55	0.38	100	2	10.3	360	1.6%	3.0	2.0	12.3	12.6	3.8	6.4	1.2	2.9
W1	0.86	0.22	0.46	0.22	80	6	7.3	0	0.0%	2.3	0.0	7.3	10.4	4.6	7.7	0.9	3.1
W2	0.26	0.08	0.35	0.08	35	8	3.9	0	0.3%	2.3	0.0	5.0	10.2	5.2	8.7	0.1	0.8
W3	0.56	0.08	0.35	0.08	35	8	3.9	160	0.5%	2.3	1.2	5.1	11.1	5.2	8.7	0.2	1.7
X	0.22	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.8
X1	0.78	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	2.8
X2	1.04	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	1.1	3.7
Y	0.09	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.1	0.3
Y1	0.84	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	3.0
Y2	0.21	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.7
OFFSITE BASINS*																	
<i>B</i> *	5.39	0.38	0.55	0.38	60	1.2	8.0	1381	2.8%	3.0	7.6	16.3	18.0	3.4	5.7	8.0	19.3
<i>C</i> *	2.92	0.38	0.55	0.38	100	1.2	12.2	411	3.0%	3.0	2.3	14.5	12.8	3.8	6.3	4.2	10.1
D*	2.90	0.38	0.55	0.38	100	2	10.3	245	2.1%	3.0	1.3	11.7	11.9	3.9	6.5	4.3	10.4
<i>E</i> *	5.34	0.38	0.55	0.38	100	2	10.3	61	3.3%	3.0	0.3	10.7	10.9	4.0	6.8	8.2	19.9
	1.12	0.90	0.96	0.90	10	0.2	0.9	1525	2.8%	3.0	8.4	9.3	18.5	4.2	7.1	4.3	7.7
<u>G*</u>	0.61	0.22	0.46	0.22	100	2	12.6	0	2.2%	3.0	0.0	12.6	10.6	4.0	6.8	0.5	1.9
H*	0.19	0.90	0.96	0.90	10	0.2	0.9	280	2.1%	3.0	1.5	5.0	11.6	5.2	8.7	0.9	1.6
	2.10	0.90	0.96	0.90	10	0.2	0.9	1082	2.5%	3.0	5.9	6.9	16.1	4.7	7.9	8.9	15.9
<i>L</i> *	1.54	0.90	0.96	0.90	10	0.2	0.9	1805	2.1%	3.0	9.9	10.8	20.1	4.0	6.7	5.6	10.0
S*	1.97	0.08	0.35	0.08	60	10	5.6	270	0.5%	2.3	2.0	7.6	11.8	4.5	7.6	0.7	5.3

* For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

** Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET/CMN Date: 1/14/2020 Checked by: VAS

	From Area Runoff Coefficient Summary		(1	Bas		<i>outin</i> _{rland}	ig St	umm		NNEL FLO	u/	Time of Travel (T_t)	INTEN	SITY **	TOTAL	FLOWS	1
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	INTEN I5	I ₁₀₀	Q5	Q100	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
	1			ED D	DRAINA	IGE BA	SIN R	OUTIN	G SUM	MARY							
2*	B*	2.34	3.39									16.3	3.4	5.7	8.0	19.3	(2) EX. 15' AT-GRADE INLETS
3*	C*	1.11	1.61									12.8	3.8	6.3	4.2	10.1	EX. 6' SUMP INLET
4*	D*, E*, F*	4.14	5.61									11.7	3.9	6.5	16.1	36.7	EX. 15' AT-GRADE INLET
5*	G*, H*, FLOWBY DP4*	1.07	3.02									11.7	3.9	6.5	4.2	19.7	EX. 15' AT-GRADE INLET
6*	I*, J, K, L*	3.50	3.97									10.8	4.0	6.7	14.1	26.7	EX. 15' AT-GRADE INLET
7	Р	1.68	2.43									16.4	3.4	5.7	5.7	13.8	PROP. 10' SUMP INLET
8	Q	1.44	2.08									16.4	3.4	5.7	4.9	11.8	PROP. 10' SUMP INLET
9	R	0.60	0.86									12.8	3.8	6.3	2.2	5.4	PROP. 10' SUMP INLET
10	Т	2.74	2.69									15.8	3.4	5.8	9.4	15.6	PROP. 15' AT-GRADE INLET Total CA100=3.86 Split Between
11	V1	0.56	2.69									15.8	3.4	5.8	1.9	15.6	DP10 & DP11 For Crown Overflow PROP. 15' AT-GRADE INLET Total CA100=3.86 Split Between
12	U, FLOWBY DP10	1.80	2.98									15.8	3.4	5.8	6.2	17.2	DP10 & DP11 For Crown Overflow PROP. 10' SUMP INLET
13	V2, FLOWBY DP11	0.32	0.96									13.6	3.7	6.2	1.2	5.9	PROP. MODIFIED 5'x4.5' SUMP INLET
14	W3, PR9	5.35	8.52									13.6	3.7	6.2	19.6	52.4	CUMULATIVE DETENTION POND

MS CIVIL, INC. Drain Calcs Homestead 2 (formerly SR FILING 1 Complete).xls

HOMESTEAD AT STERLING RANCH FILING NO. 2 DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					In	tensity**	Fla)w	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T _C	I_5	I 100	Q 5	Q 100	
1	DP7	1.68	2.43	16.4	3.4	5.7	5.7	13.8	24" RCP
2	DP8	1.44	2.08	16.4	3.4	5.7	4.9	11.8	18" RCP
3	PR1, PR2	3.12	4.51	16.4	3.4	5.7	10.6	25.7	24" RCP
4	DP9, PR3	3.71	5.37	17.0	3.3	5.6	12.4	30.1	30" RCP
5	DP10	2.64	2.20	15.8	3.4	5.8	9.1	12.7	18" RCP
6	DP11	0.55	2.20	15.8	3.4	5.8	1.9	12.7	18" RCP
7	PR5, PR6	3.19	4.39	16.0	3.4	5.7	10.9	25.3	30" RCP
8	DP12	1.80	2.98	15.8	3.4	5.8	6.2	17.2	24" RCP
9	DP13, PR7, PR8	5.31	8.33	16.6	3.4	5.7	17.9	47.1	42" RCP
10	UD-Detention_v3.07						0.7	23.4	Outlet Structure & 18" CMP
11	Pipe Run continued from MDDP DP1:	5* to Sand Creek	. Flow values ar	e that of MDDI	Pipe Run	15* (PR15*).	42.1	76.8	42" RCP
12	Lots 36-41						0.0	1.3	12" ADS
13	Lots 28-35						0.0	1.6	12" ADS
14	Lots 19-24						0.0	1.5	12" ADS
15	Lots 13-18						0.0	1.4	12" ADS

* For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP

prepared by MS Civil Consultants, dated April 2017

** Intensity equations assume a minimum travel time of 5 minutes.

- DP Design Point
- EX Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: CMN Date: 1/14/2020 Checked by: VAS

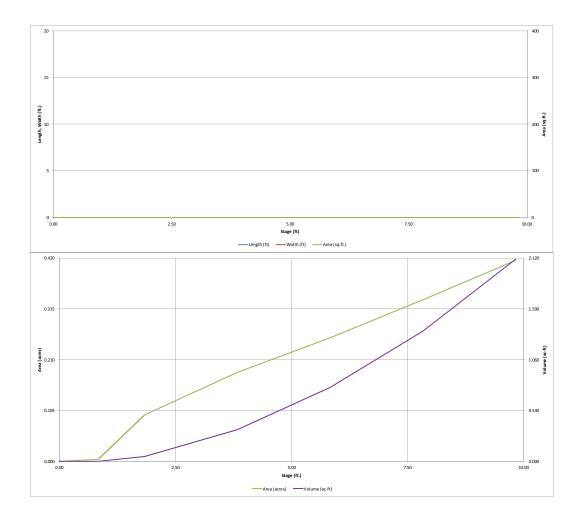
Updated SF-3 routing for Basins X1, X2, W1, & Y1 included in Addendum above.

HYDRAULIC CALCULATIONS

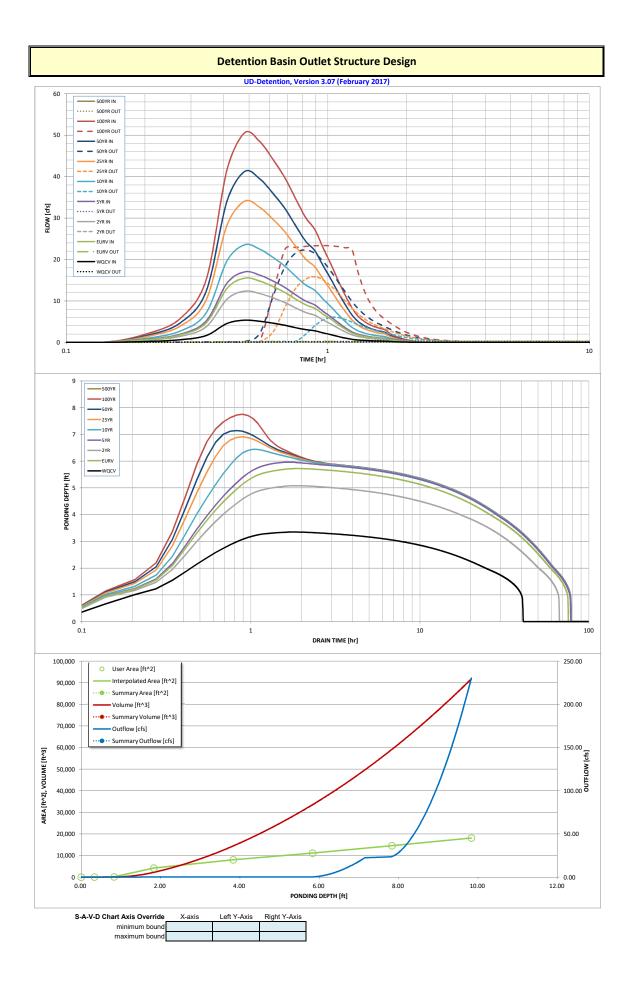
Weig	hted Percent	t Imperviou	sness of FSD Pond	1
Contributing Basins	Area (Acres)	<i>C</i> ₅	Impervious % (I)	(Acres)*(I)
Т	9.14	0.30	40	365.60
U	4.50	0.38	53	238.50
V1	1.48	0.38	53	78.44
V2	0.83	0.38	53	43.99
W1	0.56	0.08	2	1.12
Totals	16.51			727.65
Imperviousness of FSD Pond 1	44.1	%		

			DETENT		SIN STAGE-S	TORAG		BUILD	ER					
				UD-Dete	ntion, Version				-11					
	Homestead /		Ranch Filings	Nos. 2										
ZONE 3	2													
		T	~	~										
		100-YE ORIFIC	AR CE		Depth Increment =		ft							
PERMANENT ORIFI	E 1 AND 2 ICES B Configurat	tion (Rete	ntion Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Required Volume Calculation				76.17	Description Top of Micropool	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 	(ft*2) 	Area (ft*2) 0	(acre) 0.000	(ft*3)	(ac-ft)
Selected BMP Type =	EDB			76.4			0.33			-	40	0.001	7	0.000
Watershed Area = Watershed Length =	16.51 875	acres ft		77 78.00			0.83				100 4,187	0.002	40 2,143	0.001 0.049
Watershed Slope =	0.020	ft/ft		80.00			3.83			-	8,006	0.184	14,378	0.330
Watershed Imperviousness = Percentage Hydrologic Soil Group A =	44.10% 0.0%	percent percent		82.00 84.00			5.83 7.83				11,106 14,529	0.255	33,490 59,125	0.769
Percentage Hydrologic Soil Group B = Percentage Hydrologic Soil Groups C/D =	100.0% 0.0%	percent percent		86.00			9.83		-	-	18,087	0.415	91,741	2.106
Desired WQCV Drain Time =	40.0	hours								-				
Location for 1-hr Rainfall Depths = Water Quality Capture Volume (WQCV) =		acre-feet	o											
Excess Urban Runoff Volume (EURV) =	0.202	acre-feet	Optional Use 1-hr Precipita	ation				-		-				
2-yr Runoff Volume (P1 = 1.19 in.) = 5-yr Runoff Volume (P1 = 1.5 in.) =	0.614	acre-feet acre-feet	1.19	inches inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	1.177	acre-feet	1.75	inches						-				
25-yr Runoff Volume (P1 = 2 in.) = 50-yr Runoff Volume (P1 = 2.25 in.) =	1.710	acre-feet acre-feet	2.00	inches inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	2.550	acre-feet	2.52	inches						-				
500-yr Runoff Volume (P1 = 0 in.) = Approximate 2-yr Detention Volume =	0.000	acre-feet acre-feet		inches										
Approximate 5-yr Detention Volume =	0.795	acre-feet								-				
Approximate 10-yr Detention Volume = Approximate 25-yr Detention Volume =	1.075	acre-feet acre-feet											+	
Approximate 50-yr Detention Volume =	1.247	acre-feet								-				
Approximate 100-yr Detention Volume =	1.412	acre-feet												
Stage-Storage Calculation		1								-				
Zone 1 Volume (WQCV) = Zone 2 Volume (EURV - Zone 1) =	0.262	acre-feet acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	0.642	acre-feet								-				
Total Detention Basin Volume = Initial Surcharge Volume (ISV) =	1.412 user	acre-feet ft/3												
Initial Surcharge Depth (ISD) =	user	ft								-				
Total Available Detention Depth (H _{total}) = Depth of Trickle Channel (H _{TC}) =	user user	ft ft												
Slope of Trickle Channel (S_{TC}) = Slopes of Main Basin Sides (S_{main}) =	user	ft/ft							-	-				
Basin Length-to-Width Ratio (R _{L/W}) =	user user	H:V												
Initial Surcharge Area (A _{SV}) =	user	-												
Surcharge Volume Length (L _{ISV}) =	user	ft*2 ft						-		-				
Surcharge Volume Width (W _{ISV}) = Depth of Basin Floor (H _{FLOOR}) =	user	ft ft												
Length of Basin Floor (L _{FLOOR}) =	user	π ft								-				
Width of Basin Floor (W _{FLOOR}) = Area of Basin Floor (A _{FLOOR}) =	user	ft ft*2												
Volume of Basin Floor (V _{FLOOR}) =	user	ft/3								-				
Depth of Main Basin (H _{MAIN}) = Length of Main Basin (L _{MAIN}) =	user	ft ft												
Width of Main Basin (W _{MAIN}) =	user	ft								-				
Area of Main Basin (A _{MAIN}) = Volume of Main Basin (V _{MAIN}) =	user	ft/2 ft/3												
Calculated Total Basin Volume (V _{total}) =		acre-feet												
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UD-Detention, Version 3.07 (February 2017)



		Dete	ention Basin (Outlet Struct	ure Design				
			UD-Detention, Ve	rsion 3.07 (Februar	ry 2017)				
Project:									
Basin ID:									
ZONE 2 ZONE 1				Stage (ft)	Zone Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	3.45	0.262	Orifice Plate	1		
± ± • • •	100-YEA		Zone 2 (EURV)	5.84	0.508	Orifice Plate			
ZONE 1 AND 2- ORIFICES	ORIFICE	n			0.508	Weir&Pipe (Restrict)			
	Configuration (Re	tention Pond)	'one 3 (100-year)	8.00	1.412	Total	l		
Jser Input: Orifice at Underdrain Outlet (typically us					1.412	1	ed Parameters for Ur	aderdrain	
Underdrain Orifice Invert Depth =	N/A		ne filtration media sur	face)	Unde	erdrain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches				ain Orifice Centroid =	N/A	feet	
Iser Input: Orifice Plate with one or more orifices o		1					lated Parameters for	_	
Invert of Lowest Orifice =	0.00		pottom at Stage = 0 ft			rifice Area per Row =	8.264E-03	ft ²	
Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing =	5.84 23.40	ft (relative to basin b inches	oottom at Stage = 0 ft)		Iliptical Half-Width = ptical Slot Centroid =	N/A N/A	feet feet	
Orifice Plate: Orifice Area per Row =	1.19	sq. inches (diameter	= 1-3/16 inches)		EIII	Elliptical Slot Area =	N/A	ft ²	
	1115	sq. menes (diameter	1 0/ 10 meneo/			Emplical block and	,,,	<u>l</u> u	
Iser Input: Stage and Total Area of Each Orifice				Den 4 (Daw 5 (Den 6 (attendi	Den Z (anti-anti-	Daw 9 (antianati	1
Store of Orifice Controld (#)	Row 1 (required) 0.00	Row 2 (optional) 1.95	Row 3 (optional) 3.89	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Orifice Centroid (ft) Orifice Area (sq. inches)	1.19	1.95	3.89						
									-
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)]
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
User Input: Vertical Orifice (Circ	cular or Postangular)					Calculator	Parameters for Vert	tical Orifica	
Oser input. Vertical Office (Circ	Not Selected	Not Selected	1			Calculater	Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin b	ottom at Stage = 0 ft) v	ertical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin b	-		cal Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches					•	-
						<u></u>		n	
User Input: Overflow Weir (Dropbox) and G		Not Selected	1			Calculated	Parameters for Ove	T	1
	Zone 3 Weir	Not Selected	ft (relative to basin bo	ttom at Stage = 0 ft)	Height of G		Zone 3 Weir	Not Selected	feet
User Input: Overflow Weir (Dropbox) and G Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =		Not Selected N/A N/A	ft (relative to basin bo feet	ttom at Stage = 0 ft)		Calculated rate Upper Edge, H _t = Weir Slope Length =		T	feet feet
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 5.84	N/A			Over Flow	ate Upper Edge, H _t =	Zone 3 Weir 6.81	Not Selected N/A	-
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 5.84 6.00 3.00 2.91	N/A N/A N/A N/A	feet		Over Flow Grate Open Area /	rate Upper Edge, H _t = Weir Slope Length =	Zone 3 Weir 6.81 3.07 7.21 12.88	Not Selected N/A N/A N/A N/A	feet should be <u>></u> 4 ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 5.84 6.00 3.00 2.91 70%	N/A N/A N/A N/A N/A	feet H:V (enter zero for fl	at grate)	Over Flow Grate Open Area / Overflow Grate Op	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area =	Zone 3 Weir 6.81 3.07 7.21	Not Selected N/A N/A N/A	feet should be ≥ 4
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 5.84 6.00 3.00 2.91	N/A N/A N/A N/A	feet H:V (enter zero for fl feet	at grate)	Over Flow Grate Open Area / Overflow Grate Op	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris =	Zone 3 Weir 6.81 3.07 7.21 12.88	Not Selected N/A N/A N/A N/A	feet should be <u>></u> 4 ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50%	N/A N/A N/A N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t %	at grate)	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44	Not Selected N/A N/A N/A N/A N/A	feet should be ≥ 4 ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict	N/A N/A N/A N/A N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t %	at grate)	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction Plat	feet should be ≥ 4 ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50%	N/A N/A N/A N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t % gular Orifice)	at grate)	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O Overflow Grate O	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44	Not Selected N/A N/A N/A N/A N/A	feet should be ≥ 4 ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Cir	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict Zone 3 Restrictor	N/A N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected	feet H:V (enter zero for fl feet %, grate open area/t % gular Orifice)	at grate) otal area	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate Op (rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Parameter	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected	feet should be \geq 4 ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Slobe = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Cir Depth to Invert of Outlet Pipe =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restric Zone 3 Restrictor 0.25	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A	feet H:V (enter zero for fl feet %, grate open area/t % gular Orifice) ft (distance below bas	at grate) otal area in bottom at Stage = 0	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate Op (rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A	feet should be \geq 4 ft ² ft ² te ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Sides = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrictor 0.25 24.00 13.30	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A	feet H:V (enter zero for fl feet %, grate open area/t % (ular Orifice) ft (distance below basi inches	at grate) otal area in bottom at Stage = 0	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate Op (ft)	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A	feet should be \geq 4 ft ² ft ² te ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sldes = Overflow Grate Open Area % = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate (Cin Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrictor 0.25 24.00 13.30 gular or Trapezoidal)	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t % ular Orifice) ft (distance below bas inches inches	at grate) iotal area in bottom at Stage = 0 Half-	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O (t) (t) (t) Out Central Angle of Rest	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A Spillway	feet should be ≥ 4 ft ² ft ² te ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Open Area % = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate (Cir Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Invert Stage=	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict Zone 3 Restrictor 0.25 24.00 13.30 gular or Trapezoidal) 7.80	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t % (ular Orifice) ft (distance below basi inches	at grate) iotal area in bottom at Stage = 0 Half-	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O Overflow Grate O (tt) Out Central Angle of Rest Spillway	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula v Design Flow Depth=	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A N/A Spillway feet	feet should be ≥ 4 ft ² ft ² te ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrictor 0.25 24.00 13.30 gular or Trapezoidal) 7.80 17.00	N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A ft (relative to basin t feet	feet H:V (enter zero for fl feet %, grate open area/t % ular Orifice) ft (distance below bas inches inches	at grate) iotal area in bottom at Stage = 0 Half-	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O ((ft) Central Angle of Rest Spillway Stage a	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula Posign Flow Depth= tt Top of Freeboard =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 Sofor Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89 9.69	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A Spillway feet feet	feet should be ≥ 4 ft ² ft ² te ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Open Area % = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate (Cir Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Invert Stage=	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict Zone 3 Restrictor 0.25 24.00 13.30 gular or Trapezoidal) 7.80	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A	feet H:V (enter zero for fl feet %, grate open area/t % ular Orifice) ft (distance below bas inches inches	at grate) iotal area in bottom at Stage = 0 Half-	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O ((ft) Central Angle of Rest Spillway Stage a	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula v Design Flow Depth=	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A N/A Spillway feet	feet should be ≥ 4 ft ² ft ² te ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ch Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict Zone 3 Restrictor 0.25 24.00 13.30 gular or Trapezoidal) 7.80 17.00 4.00	N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A t (relative to basin t feet H:V	feet H:V (enter zero for fl feet %, grate open area/t % ular Orifice) ft (distance below bas inches inches	at grate) iotal area in bottom at Stage = 0 Half-	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O ((ft) Central Angle of Rest Spillway Stage a	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula Posign Flow Depth= tt Top of Freeboard =	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 Sofor Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89 9.69	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A Spillway feet feet	feet should be ≥ 4 ft ² ft ² te ft ² ft ²
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restricter Plate Height Above Pipe Invert Stage Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Deak Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (ps) = Max Velocity through Grate 2 (ps) = Time to Drain 9% of Inflow Volume (hours) =	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict 0.25 24.00 13.30 gular or Trapezoidal) 7.80 17.00 4.00 1.00 WQCV 0.53 0.262 0.262 0.262 0.262 0.00 0.0 5.3 0.1 N/A Plate N/A N/A 39 40	N/A N/A N/A N/A N/A N/A itor Plate, or Rectang Not Selected N/A N/A itor Plate, or Rectang Not Selected N/A N/A ft (relative to basin to feet H:V feet H:V feet 0.771 0.00 15.5 0.2 N/A Plate N/A 69 73	feet H:V (enter zero for fl feet %, grate open area/t % ular Orifice) ft (distance below basi inches inches bottom at Stage = 0 ft; 0.614 0.614 0.02 0.3 1.2.4 0.2 N/A Plate N/A N/A N/A Science Science N/A N/A Science Science N/A N/A Science Science Science Science Science Science Science Science Science N/A Science Sci Science Sci Sci Science Science Science Science Science Sci	at grate) otal area in bottom at Stage = 0 Half- 1.50 0.847 0.847 0.03 0.4 1.7.0 0.7 1.5 Overflow Grate 1 0.0 N/A 71 76	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate O Overflow Grate O Overflow Grate O Overflow Grate O Overflow Grate 1 0.4 N/A N/A 69 75	ate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = pen Area w/o Debris = Calculated Parameter Outlet Orifice Centroid = rictor Plate on Pipe = Calcula Design Flow Depth= at Top of Freeboard = to Top of Freeboard = to Top of Freeboard = 1.710 0.84 1.3.9 34.1 15.8 1.1 Overflow Grate 1 1.2 N/A 66 74	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 rs for Outlet Pipe w/ Zone 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89 9.69 0.41 50 Year 2.25 2.073 2.074 1.16 19.2 41.2 22.3 1.2 Outlet Plate 1 1.7 N/A 63 73	Not Selected N/A Spillway feet feet acres 2.550 2.551 1.55 25.5 50.5 23.4 0.9 Outlet Plate 1 1.8 N/A 61 72	feet should be ≥ 4 ft ² ft ² ft ² feet radians #N/A #N/A #N/A #N/A #N/A #N/A #N/A
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Huight Above Pipe Invert = One-Hour Rainfall Depth (In) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours)	Zone 3 Weir 5.84 6.00 3.00 2.91 70% 50% rcular Orifice, Restrict 0.25 24.00 13.30 gular or Trapezoidal) 7.80 17.00 4.00 1.00 WQCV 0.53 0.262 0.262 0.262 0.262 0.262 0.00 0.0 5.3 0.1 N/A Plate N/A 39	N/A N/A N/A N/A N/A N/A tor Plate, or Rectang Not Selected N/A N/A thread to the selected N/A N/A N/A tf (relative to basin to feet H:V feet 0.0771 0.771 0.00 15.5 0.2 N/A Plate N/A Plate N/A	feet H:V (enter zero for fl feet %, grate open area/t % (ular Orifice) ft (distance below basi inches inches bottom at Stage = 0 ft; 0.614 0.614 0.614 0.02 0.3 112.4 0.2 N/A Plate N/A Plate N/A 62	at grate) otal area in bottom at Stage = 0 Half- 1.50 0.847 0.847 0.03 0.4 1.7.0 0.7 1.5 Overflow Grate 1 0.0 N/A 71	Over Flow Grate Open Area / Overflow Grate Op Overflow Grate Op Overflow Grate Op (ft) Out Central Angle of Rest Spillway Stage a Basin Area a Basin Area a 10 Year 1.75 1.177 0.27 4.4 23.5 6.0 1.4 Overflow Grate 1 0.4 N/A 69	rate Upper Edge, H _t = Weir Slope Length = 100-yr Orifice Area = en Area w/ Debris = Calculated Parameter Outlet Orifice Centroid = rictor Plate on Pipe = Calcula Posign Flow Depth= tr Top of Freeboard = tr Top of Freeboard = 25 Year 2.00 1.710 1.710 0.84 13.9 34.1 15.8 1.1 Overflow Grate 1 1.2 N/A 66	Zone 3 Weir 6.81 3.07 7.21 12.88 6.44 2one 3 Restrictor 1.79 0.63 1.68 ted Parameters for S 0.89 9.69 0.41 2.25 2.073 2.074 1.16 19.2 41.2 22.3 1.2 Outlet Plate 1 1.7 N/A 63	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A NA NA NA NA N/A N/A N/A N/A Spillway feet feet feet 2.52 2.550 2.55 25.5 50.5 23.4 0.9 Outlet Plate 1 1.8 N/A	feet should be ≥ 4 ft ² ft ² ft ² feet radians



Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename:

	Storm Inflow H			ention, Versio			iranhs develope	d in a separate p	rogram	
	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval										
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.12 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	0:04:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:08:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:12:22	0.24	0.68	0.55	0.75	1.03	1.47	1.77	2.15	#N/A
1.214	0:16:29 0:20:36	0.64	1.85	1.48	2.02	2.79	4.01	4.84	5.91	#N/A
	0:24:43	1.65 4.55	4.74	3.79 10.43	5.20 14.28	7.16 19.66	10.30 28.29	12.42 34.10	15.18 41.64	#N/A #N/A
	0:28:50	5.34	15.51	12.37	17.02	23.54	34.08	41.22	50.54	#N/A
	0:32:58	5.08	14.81	11.80	16.25	22.50	32.61	39.48	48.45	#N/A
	0:37:05	4.62	13.48	10.75	14.80	20.49	29.69	35.94	44.09	#N/A
	0:41:12	4.11	12.05	9.59	13.23	18.35	26.64	32.27	39.64	#N/A
	0:45:19	3.53	10.41	8.28	11.44	15.90	23.13	28.07	34.53	#N/A
	0:49:26	3.08	9.07	7.22	9.96	13.83	20.09	24.40	30.06	#N/A
	0:53:34	2.79	8.22	6.54	9.03	12.54	18.22	22.11	27.22	#N/A
	0:57:41	2.28	6.79	5.39	7.47	10.41	15.18	18.44	22.73	#N/A
	1:01:48	1.84	5.56	4.40	6.12	8.55	12.50	15.21	18.77	#N/A
	1:05:55	1.40	4.29	3.39	4.73	6.64	9.78	11.93	14.77	#N/A
	1:10:02 1:14:10	1.02	3.21	2.52	3.54	5.01	7.43	9.10	11.31	#N/A
	1:14:10	0.75	2.32	1.83	2.56	3.64	5.45 4.15	6.70 5.08	8.37	#N/A
	1:22:24	0.59	1.79	1.42	1.97	2.79	4.15	4.13	6.32 5.12	#N/A #N/A
	1:26:31	0.48	1.47	0.99	1.82	1.94	2.86	3.49	4.32	#N/A #N/A
	1:30:38	0.41	1.25	0.33	1.38	1.54	2.50	3.45	3.77	#N/A
	1:34:46	0.33	0.99	0.78	1.09	1.52	2.24	2.73	3.38	#N/A
	1:38:53	0.30	0.91	0.72	1.00	1.40	2.06	2.51	3.10	#N/A
	1:43:00	0.22	0.67	0.53	0.73	1.03	1.52	1.85	2.29	#N/A
	1:47:07	0.16	0.49	0.39	0.54	0.75	1.11	1.35	1.67	#N/A
	1:51:14	0.12	0.36	0.28	0.40	0.55	0.81	0.99	1.23	#N/A
	1:55:22	0.09	0.26	0.21	0.29	0.41	0.60	0.74	0.91	#N/A
	1:59:29	0.06	0.19	0.15	0.21	0.30	0.44	0.53	0.66	#N/A
	2:03:36	0.04	0.13	0.11	0.15	0.21	0.31	0.38	0.47	#N/A
	2:07:43	0.03	0.10	0.08	0.11	0.15	0.23	0.28	0.34	#N/A
	2:11:50 2:15:58	0.02	0.06	0.05	0.07	0.10	0.15	0.19	0.24	#N/A
	2:15:58	0.01	0.04	0.03	0.04	0.06	0.10	0.12	0.15	#N/A #N/A
	2:24:12	0.00	0.02	0.01	0.02	0.03	0.03	0.08	0.08	#N/A #N/A
	2:28:19	0.00	0.01	0.00	0.01	0.01	0.02	0.01	0.04	#N/A
	2:32:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:36:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:40:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:44:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:48:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:53:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:57:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:01:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:05:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:09:31 3:13:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:13:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:21:53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:26:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:30:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:34:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:38:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:42:29 3:46:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:46:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:54:50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:58:58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:03:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:07:12 4:11:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:11:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:19:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:23:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:27:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:31:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:36:02 4:40:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:44:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:48:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:52:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:56:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A



20 BOULDER CRESCENT, STE 110 COLORADO SPRINGS, CO 80903 (719) 955-5485

PROJECT: Homistead Filing No. 2 DATE:

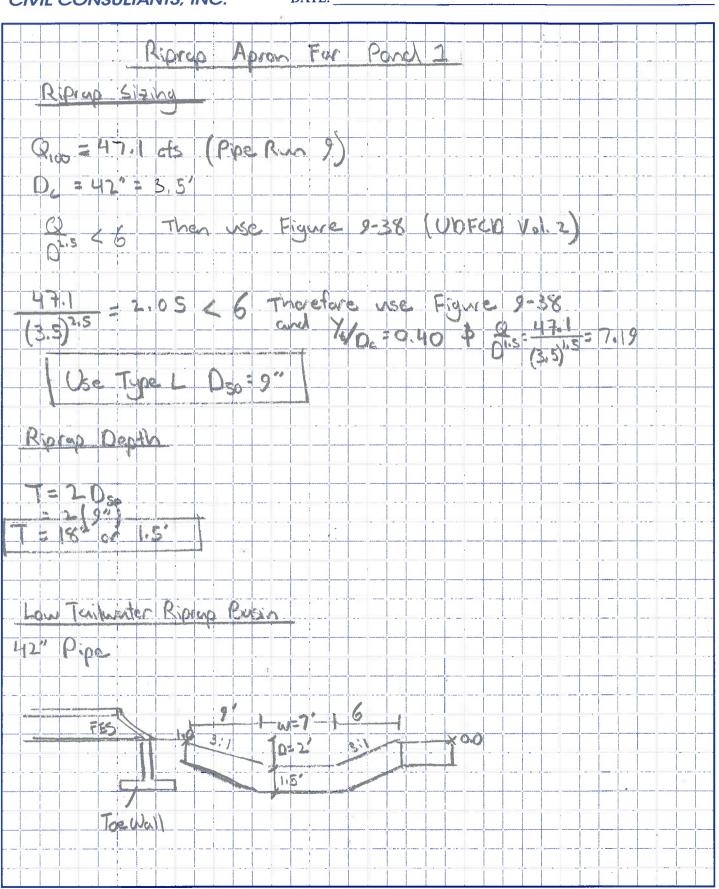
Micropool Surface Area Tributage Anew = 165TAG TIA IXA Imperviousness = 44.1% (0.441 × 1651) TIA = 7.3 ~ 8.0 From Micropool Sizing Chart (SA) Micropool SA = 40 st Forebay Volume for FSD Pond Tribiting Area = 14.51 AC min. Forebay Usume - 3.0% of WOCV (40FED F5, EDB-4) WACK For For Pond = 0.262 Az-FT Total Volume Regd. = 0.03 (0.202) 43540 = 342ct Area = 283 -7 (wall) = 276 st 276 × 1.25 ht = 345 > 342 Fortbay 15 depth (torebay) (dysth) (volnore) area provide Since notch in Forebay to accomutate 220 51 100 yr. Q100 = 47.1 cfs => 0.02 x 47.1 = 0.94. (UDFCD T-S EDB) Using Ret. Weir Egn. Q = 3.247 L.H 1.48-0.566.L 1.9 H. 19 1+2L 1.87 Solve for L = 2.6" 0=0,94 use a 2.6" notch

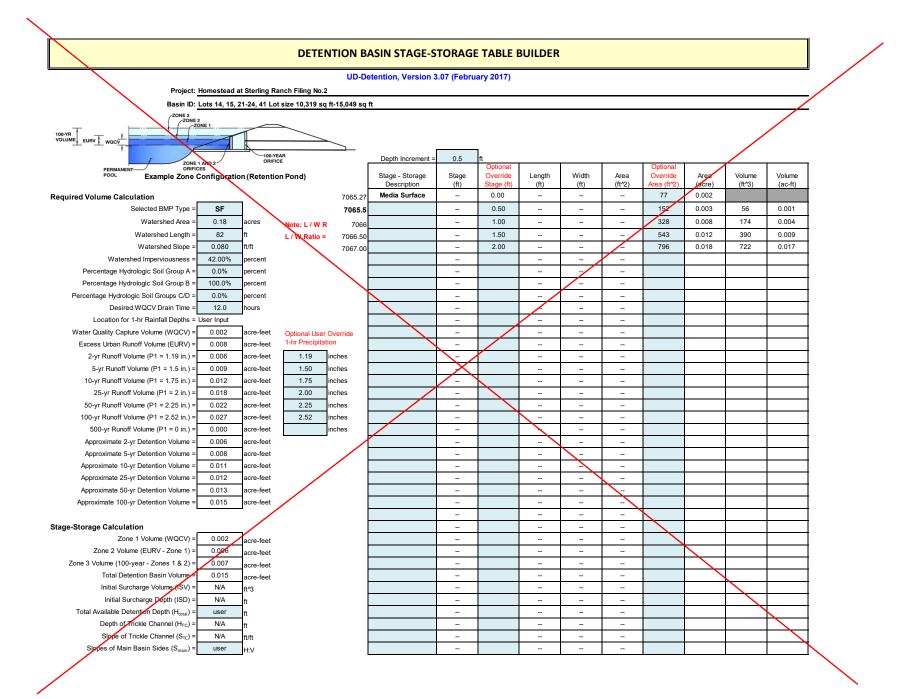


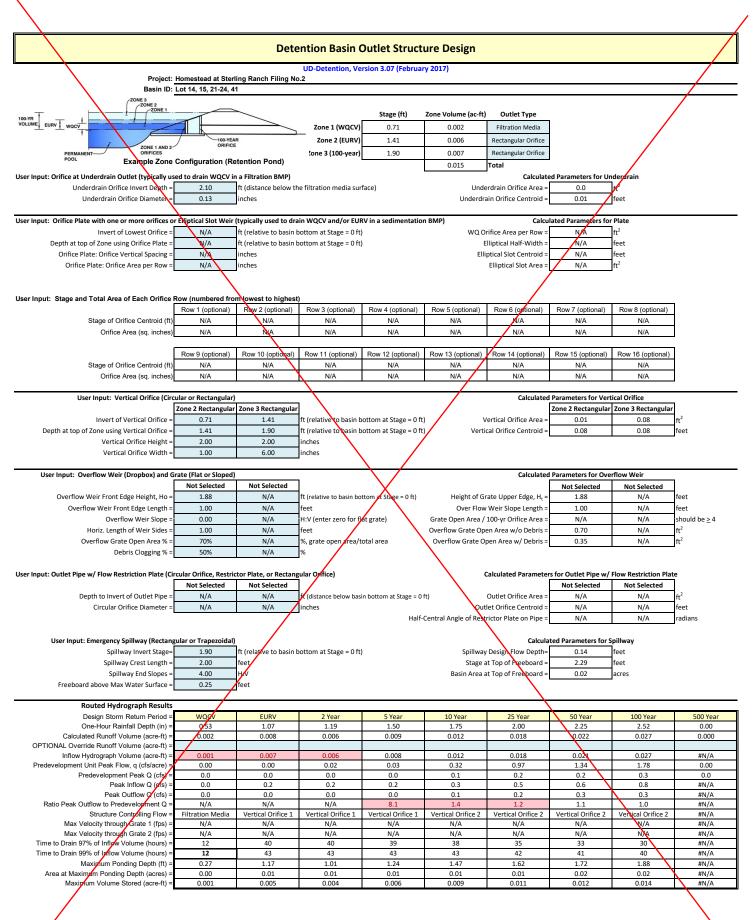


PROJECT: Homestead Filing No. 2

DATE:

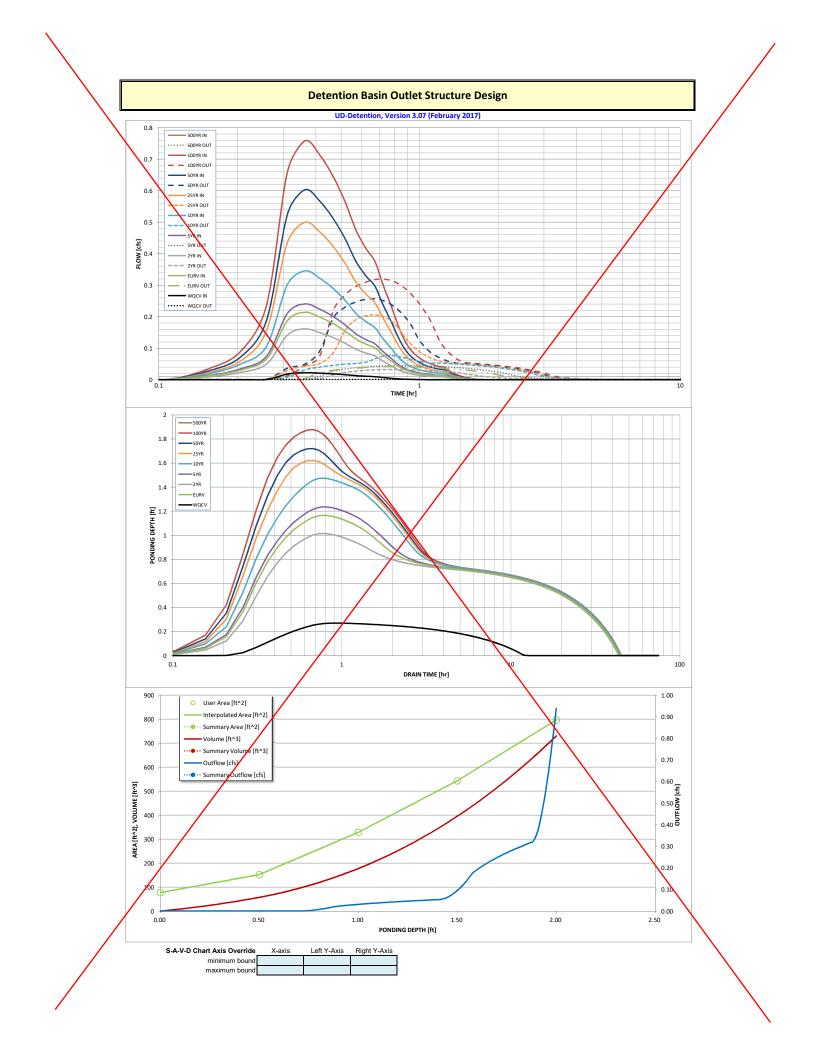


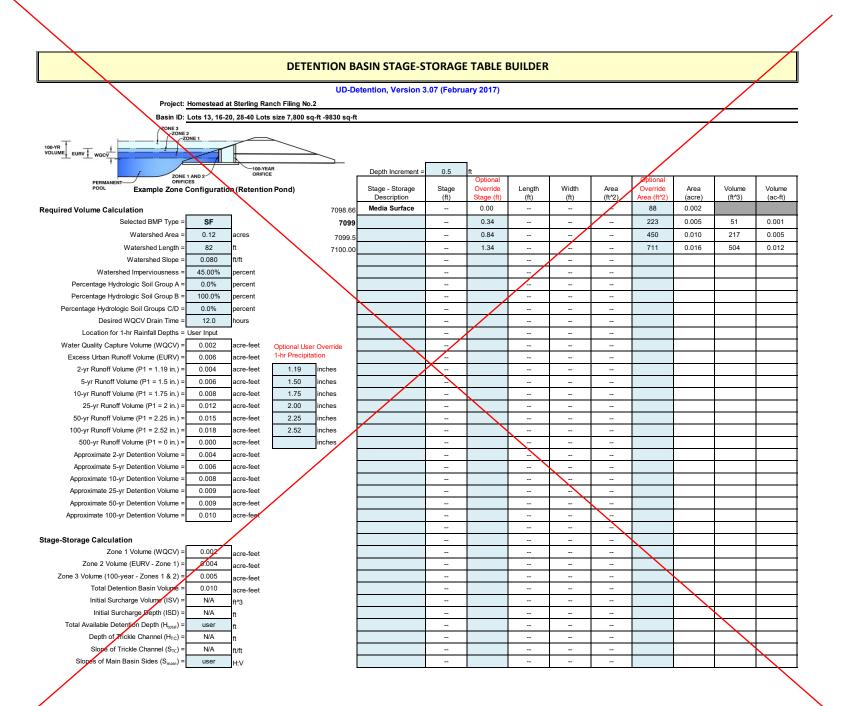




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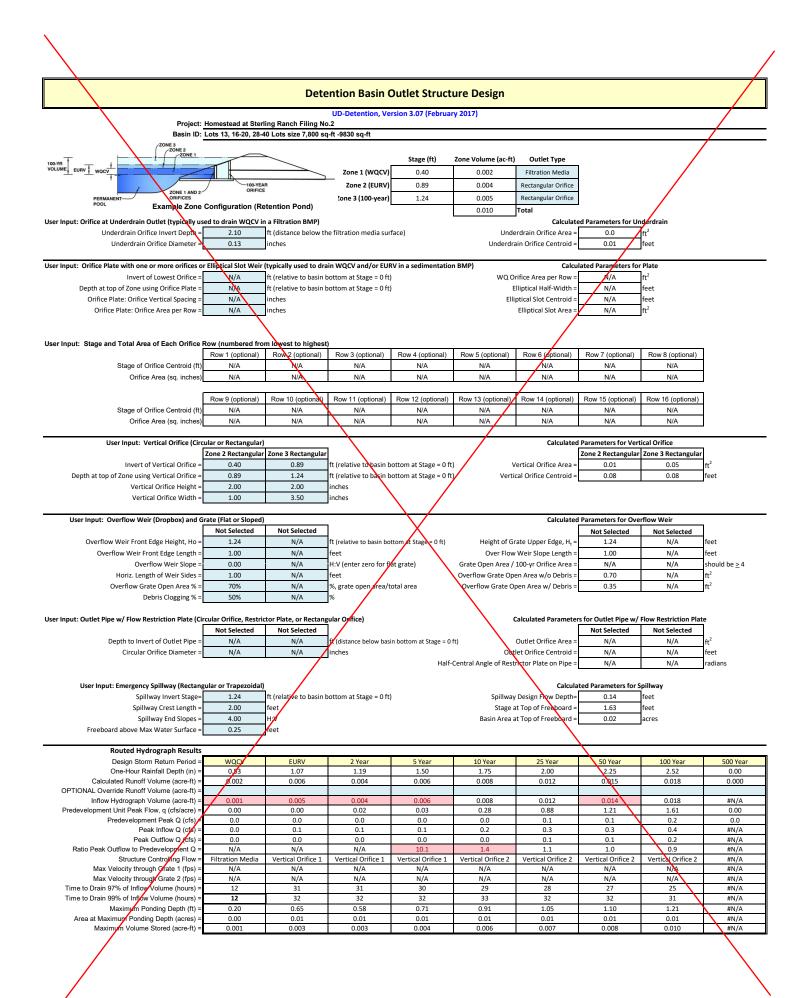
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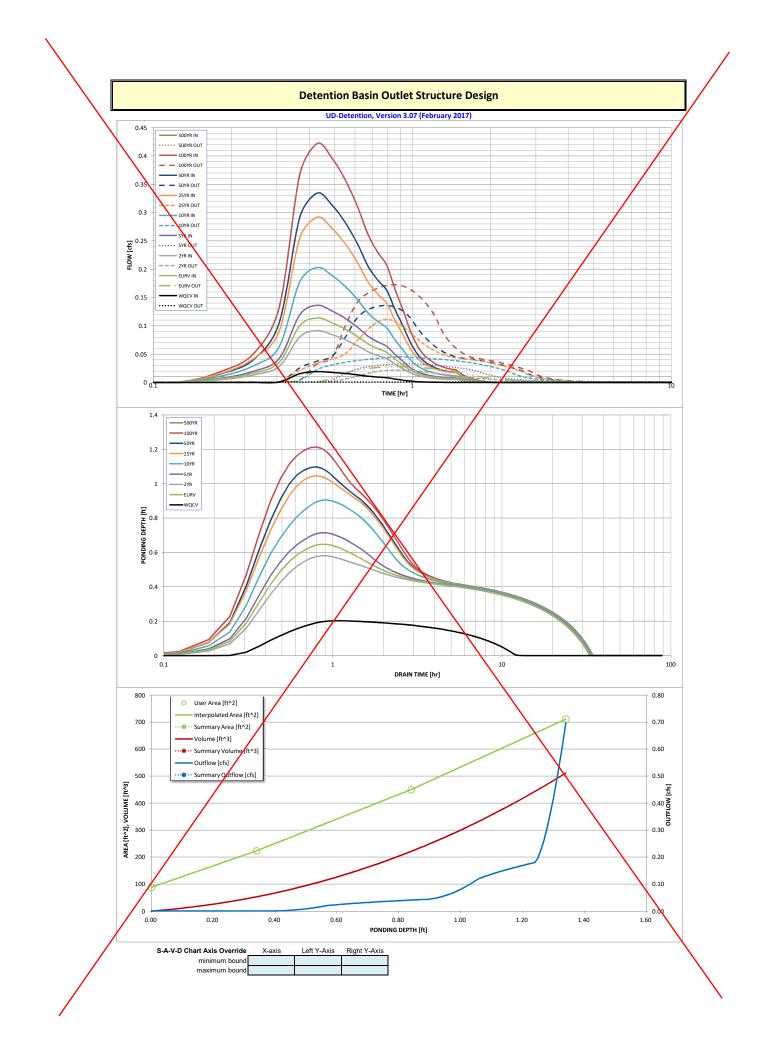




UD-Detention_v3.07_LOT 40.xlsm, Basin

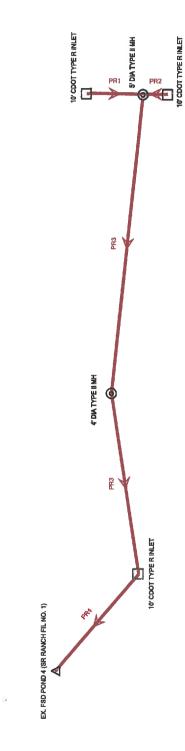
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Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Sulte 200 W Watertown, CT 06795 USA +1-203-755-1666

Storm 1, Storm 2.stsw 2/19/2019

Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

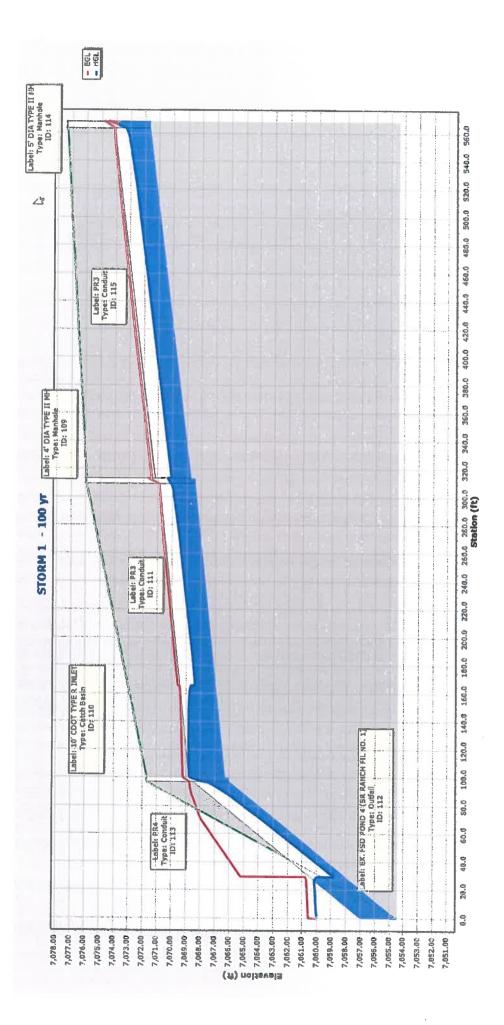
Depth (Critical)	(t)	1.73	1.87	1.73	1.23	1.34	Invert (Stop) (ft)	7,066.27	7,054.50	7,068.70	7,072.12	7,072.12
Depth (Normal)	(ft)	1.43	0.79	1.37	0.85	0.70	Invert (Start) (ft)	7,068.40	7,065.97	7,071.62	7,072.18	7,073.55
Froude Number	(Normal)	1.432	5.300	1.557	2.023	3.425	Elevation Ground (Start) (ft)	7,075.93	7,071.69	7,077.37	7,077.10	7,077.10
Flow / Capacity Length (Unified) Velocity	(ft/s)	8.82	22.71	9.31	3.76	13.97	Upstream Structure Headloss (ft)	0.21	0.93	1.19	1.02	0.61
Length (Unified)	(Ļ)	213.1	98.7	254.1	3.2	27.2	Upstream Structure Headloss Coefficient	0.270	1.020	1.520	1.000	1.020
Flow / Capacity	(Design) (%)	62.7	21.5	58.4	37.9	26.6	Upstream Structure Velocity (In- Governing) (ft/s)	9.31	5.24	4.39	3.76	6.18
Flow	(cfs)	25.70	30.10	25.70	11.80	13.80	Upstream Structure Hydraulic Grade Line (In) (ft)	7,070.34	7,068.77	7,074.54	7,075.57	7,075.49
Rise	(¥)						Headloss (ft)	1.36	7.84	3.27	0.01	0.35
Upstream	Structure	4' DIA TYPE II MH	10' CDOT TYPE R INLET	5' DIA TYPE II MH	10' CDOT TYPE R INLET	10' CDOT TYPE R INLET	Hydraulic Grade Line (Out) (ft)	7,068.77	7,060.00	7,070.07	7,074.54	7,074.54
Label		PR3	PR4	PR3	PR2	PR1	Hydraulic Grade Line (In) (ft)	7,070.13	7,067.84	7,073.35	7,074.55	7,074.89

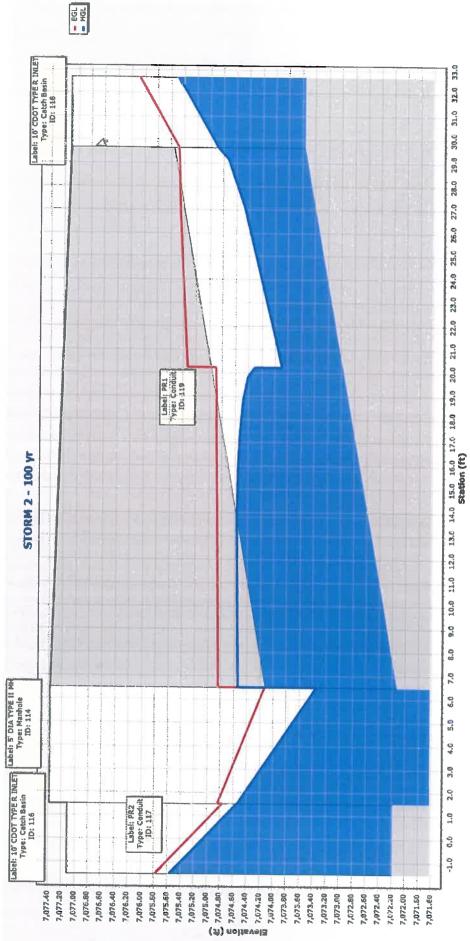
Conduit FlexTable: Table - 1 STRM 1&2

Storm 1, Storm 2.stsw 2/21/2019

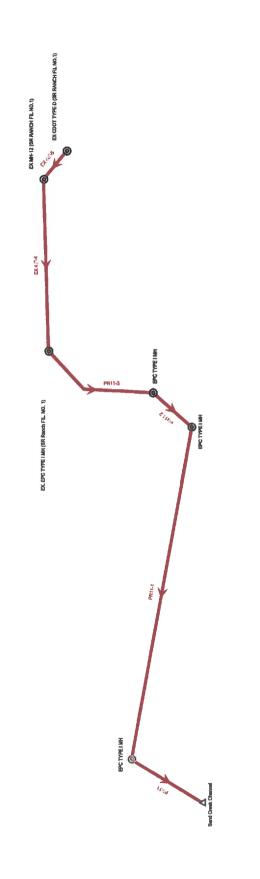
Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

> Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666





Scenario: 100 yr Stew 3 then Ex42" SR1



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Storm 3 incl fil 1 section.stsw 2/21/2019

Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

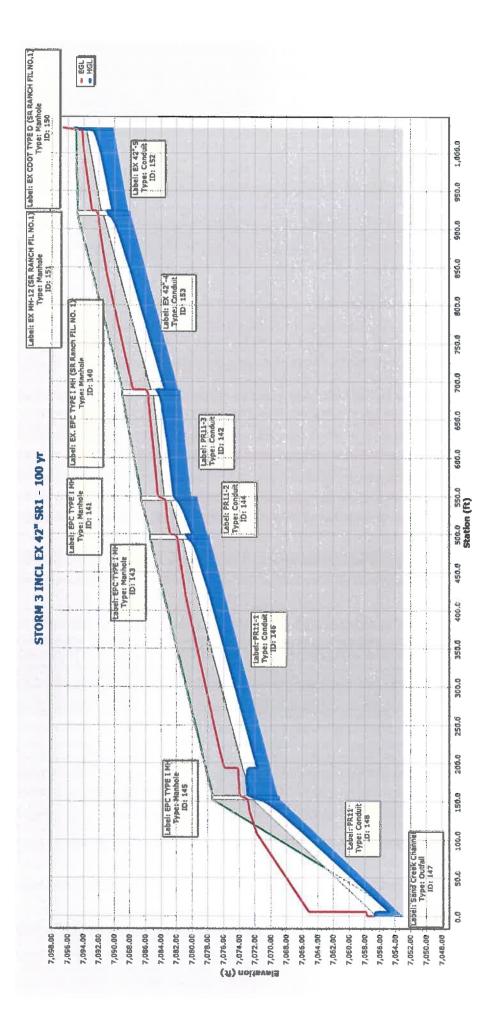
		2			VUINNIL LIGATADIG: TADIG - TOTAN JINVE 42				
Label	Upstream	Rise	Flow	Flow / Capacity	Length (Unified)	Velocity	Froude Number	Depth (Normal)	Depth (Critical)
	Structure	(ft)	(cfs)	(Design) (%)	(¥)	(ft/s)	(Normal)	(¥)	(¥)
	EX. EPC TYPE I				1	•			
PR11-3	MH (SR Ranch FIL. NO. 1)		76.80	76.4	138.4	11.50	1.432	2.29	2.74
PR11-2	EPC TYPE I MH		76.80	47.5	50.8	16.58	2.541	1.70	2.74
PR11-1	EPC TYPE I MH		76.80	48.1	341.2	16.43	2.507	1.71	2.74
PR11	EPC TYPE I MH		76.80	23.9	155.1	27.41	5.244	1.16	2.74
	EX CDOT TYPE								
EX 42"-5	D (SR RANCH		76.80	58.8	110.4	14.12	1.992	1.93	2.74
	LIL NU.L								
	EX MH-12 (SR			с Т Т	225.2		C L C	c.	
EX 12 14	NO.1)		10.01	5.14	7.002	10.01	500.2	F0.1	2. ,/4
Hydraulic Grade	Hydraulic Grade	Headloss	Upstream	Upstream	Upstream	Upstream	Elevation Ground	Invert (Start)	Invert (Stop)
Line (In)	Line (Out)	(¥)	Structure	Structure	Structure	Structure	(Start)	(¥)	(tt)
(¥)	(¥)		Hydraulic Grade	Velocity (In-	Headloss	Headloss	(¥)		
			Line (In) (ft)	Governing) (ft/s)	Coefficient	(¥)			
7,084.23	7,082.43	1.80	7,084.61	9.24	0.270	0.38	7,088.97	7,081.49	7,080.11
7,082.05	7,080.82	1.23	7,082.43	11.32	0.270	0.38	7,086.56	7,079.31	7,078.00
7,080.44	7,072.98	7.46	7,080.82	9.24	0.270	0.38	7,085.36	7,077.70	7,069.11
7,071.55	7,056.70	14.85	7,072.98	7.98	1.020	1.43	7,077.40	7,068.81	7,053.00
7,092.81	7,091.03	1.78	7,095.29	9.50	1.770	2.48	7,095.00	7,090.07	7,088.21
7,090.65	7,084.61	6.04	7,091.03	9.24	0.270	0.38	7,094.77	7,087.91	7,081.79

Conduit FlexTable: Table - 1 STRM 3 INCL 42" SR1

Storm 3 incl fil 1 section.stsw 2/21/2019

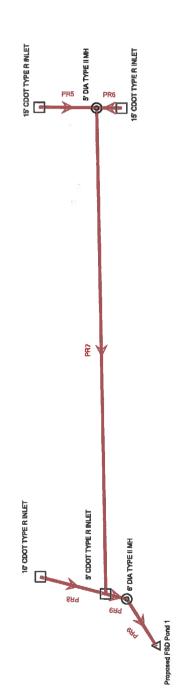
Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

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Scenario: 100 yr 578.M 5, 6, 7

s^a



Bentley StormCAD CONNECT Edition [10.01.04] Page 1 of 1

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Storm 5, Storm 6, Storm 7.stsw 2/19/2019

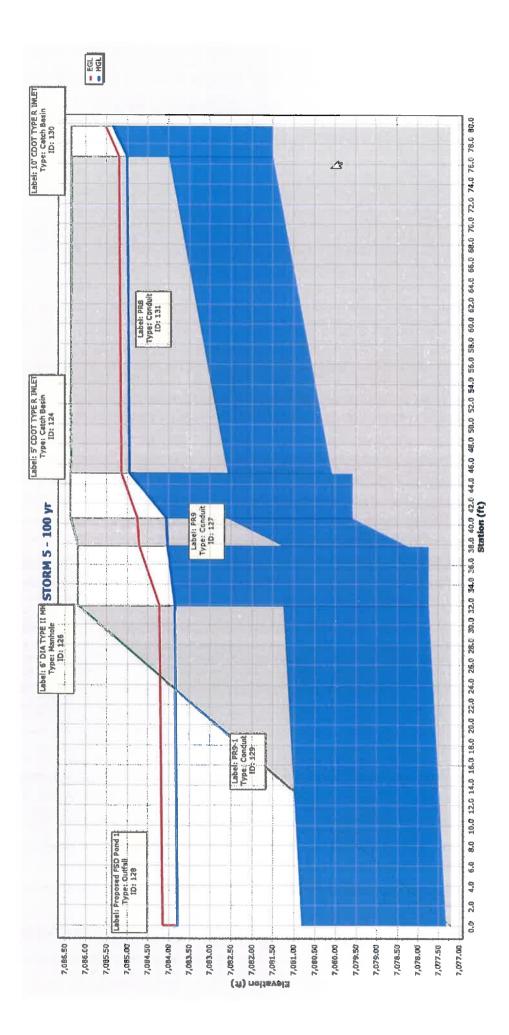
Label	Upstream Structure	Rise (ft)	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)
PR6	15' CDOT TYPE R INLET		12.70	85.5	2.5	7.19	1.674	1.07	1.34
PR5	15' CDOT TYPE R INLET		12.70	55.2	26.5	13.34	2.948	0.80	1.34
PR7	5' DIA TYPE II MH		25.30	49.2	475.5	10.43	1.867	1.24	1.71
PR9	5' CDOT TYPE R INLET		47.10	17.3	8.0	6.66	6.560	0.84	2.24
PR9-1	6' DIA TYPE II MH		47.10	42.6	34.9	4.90	1.755	1.60	2.14
PR8	10' CDOT TYPE R INLET		17.20	20.9	35.4	3.50	3.114	0.78	1.40
Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)
7,090.47	7,090.43	0.04	7,091.28	7.19	1.020	0.82	7,093.41	7,088.59	7,088.54
7,091.15	7,090.43	0.72	7,092.07	7.62	1.020	0.92	7,093.57	7,089.81	7,088.54
7,089.25	7,084.94	4.31	7,090.43	7.19	1.520	1.17	7,093.68	7,087.54	7,080.07
7,084.06	7,084.02	0.04	7,084.94	3.50	1.280	0.88	7,086.36	7,079.57	7,078.23
7,083.85	7,083.77	0.08	7,084.02	6.66	0.470	0.18	7,086.18	7,077.73	7,077.31
7,085.01	7,084.94	0.06	7,085.34	3.50	1.770	0.34	7,086.34	7,081.49	7,080.07

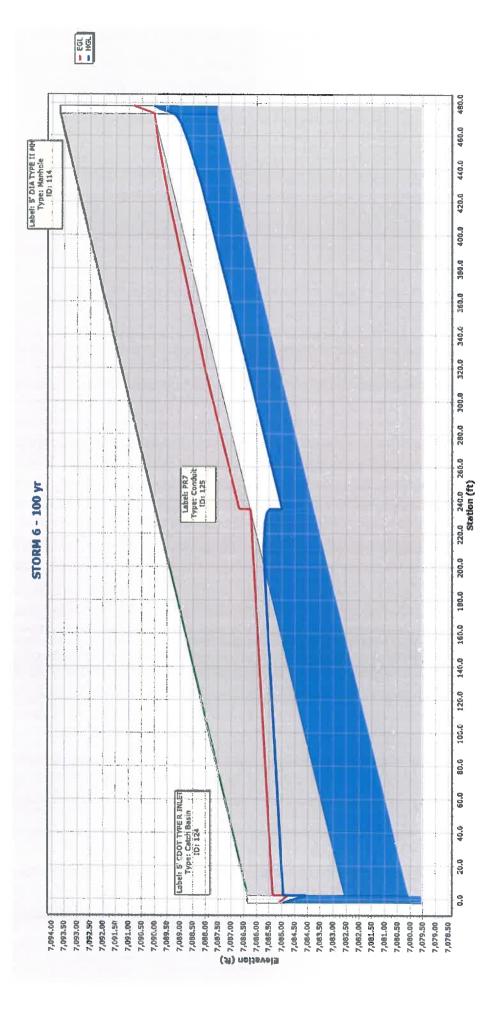
Conduit FlexTable: Table - 1 STRM 5,6,7

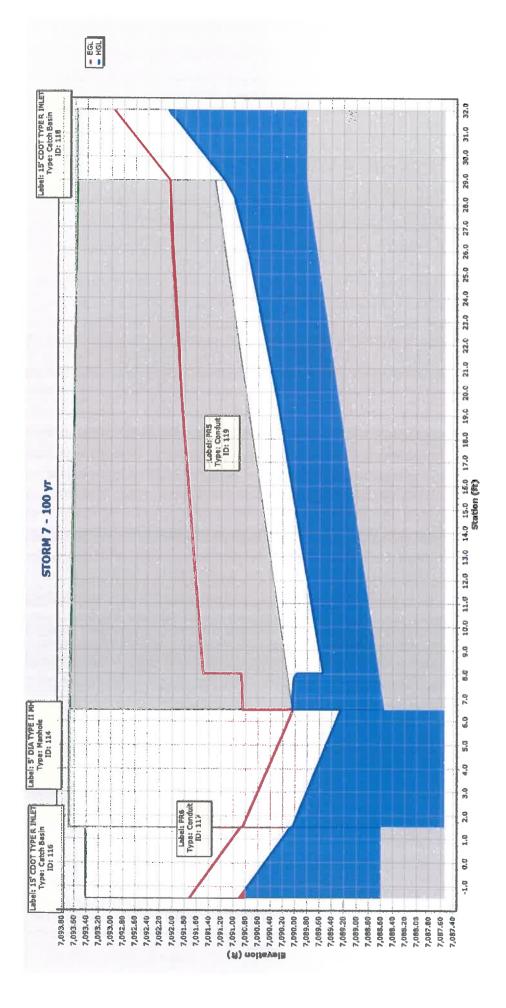
Storm 5, Storm 6, Storm 7.stsw 2/21/2019

Bentley StormCAD CONNECT Edition [10.01.04] Page 1 of 1

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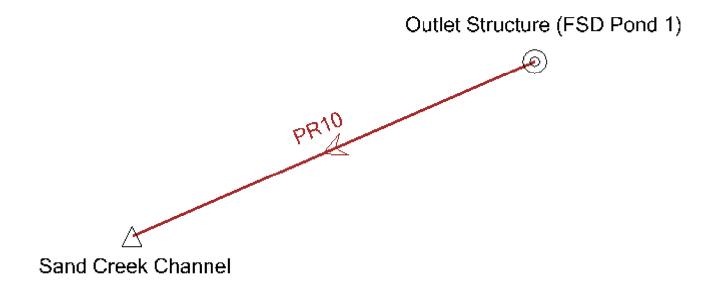






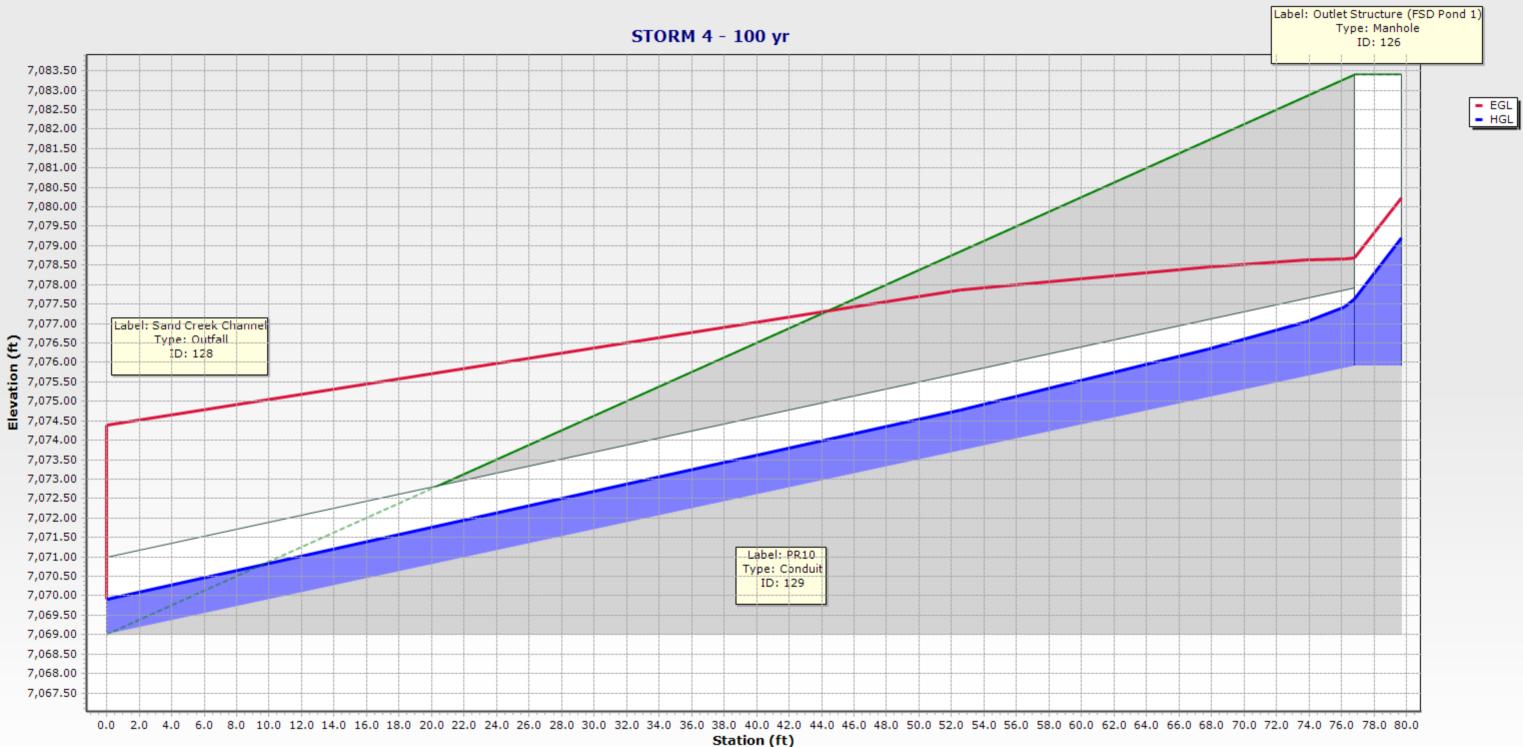
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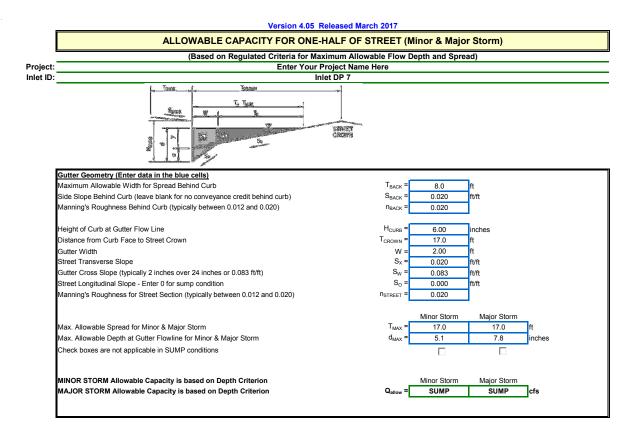
STRM 4 POND 1 OUTFALL INDEX MAP

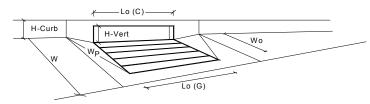


Conduit FlexTable: STRM 4 POND 1 7-30-19

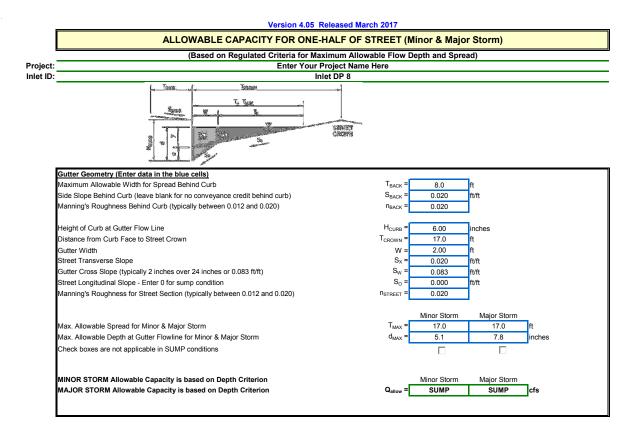
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
PR10	129	Outlet Structure (FSD Pond 1)	23.50	40.3	78.2	17.56	3.772	0.88	1.72	7,078.68	7,074.39	7,077.64	7,069.91	7.73	7,079.20
Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)										
8.17	1.500	1.56	7,083.40	7,075.92	7,069.00										

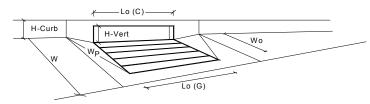




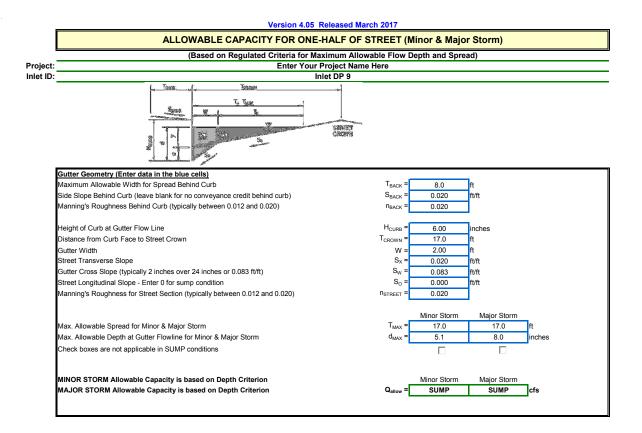


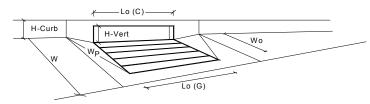
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	5.7	13.8	cfs



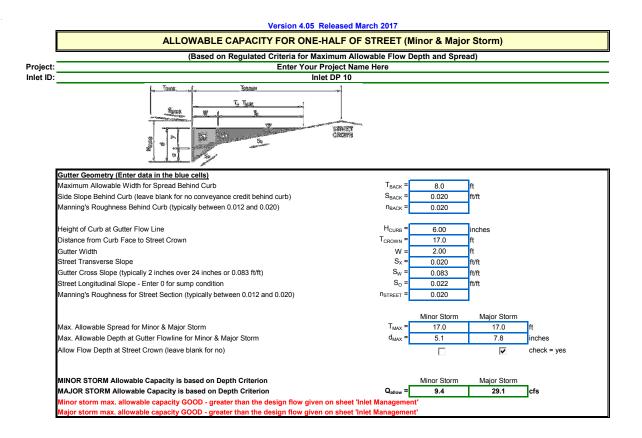


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.9	11.8	cfs

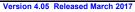


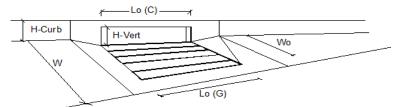


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.65	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.7	9.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.2	5.4	cfs

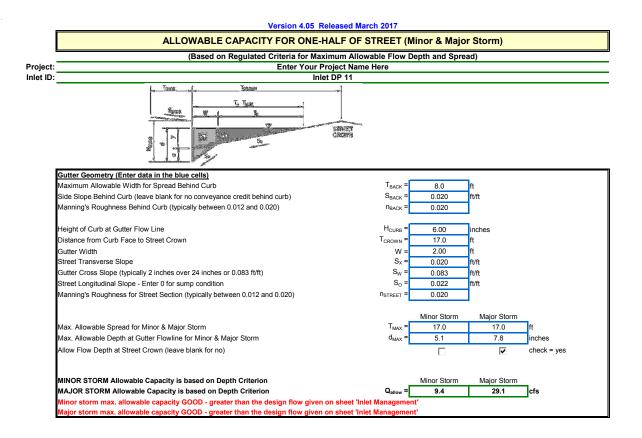


INLET ON A CONTINUOUS GRADE



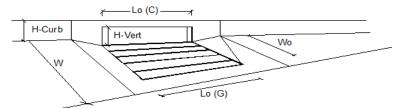


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	w _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	9.1	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.3	2.9	cfs
Capture Percentage = Q _a /Q _o =	С% =	97	82	%

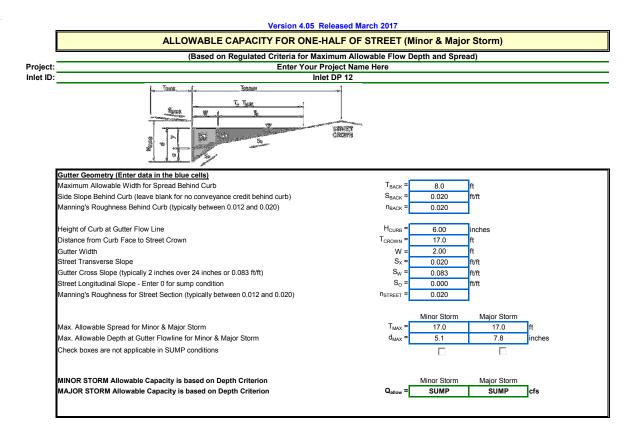


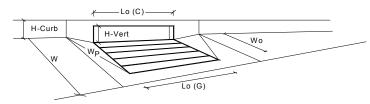
INLET ON A CONTINUOUS GRADE



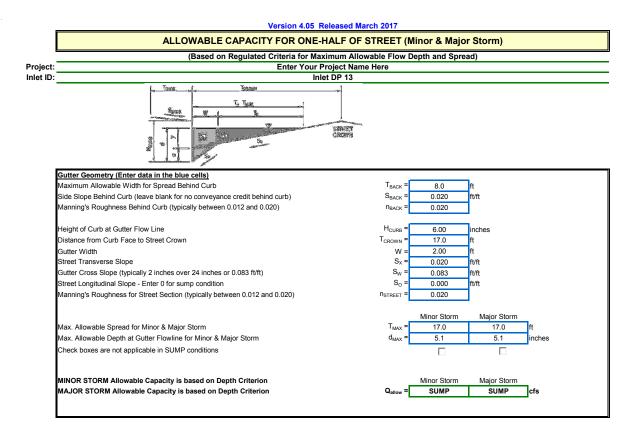


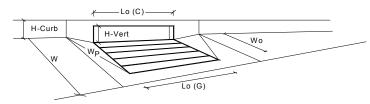
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.9	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	82	%





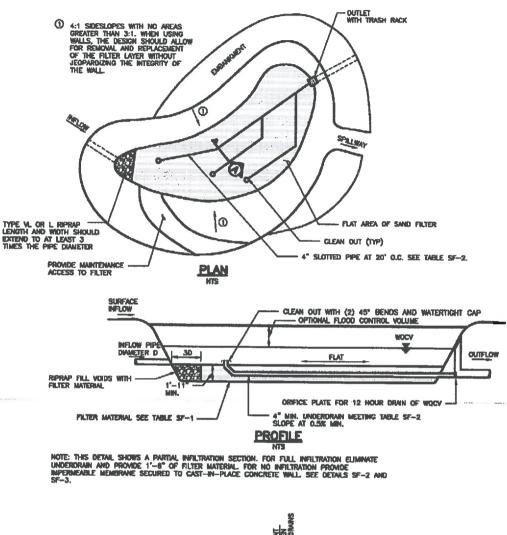
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.2	17.2	cfs

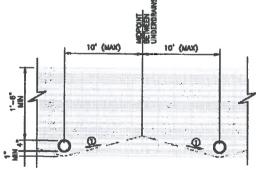




Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.65	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.7	9.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.2	5.9	cfs

EDB AND SFB DETAILS





(1) SLOPE (STRNGHT GRADE) SUBGRADE (2-10%) TO UNDERDRAIN TO REDUCE SATURATED SOIL CONDITIONS BETWEEN STORM EVENTS (OPTIONAL)





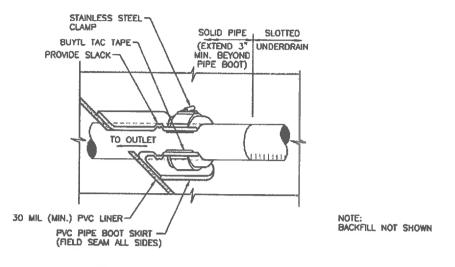
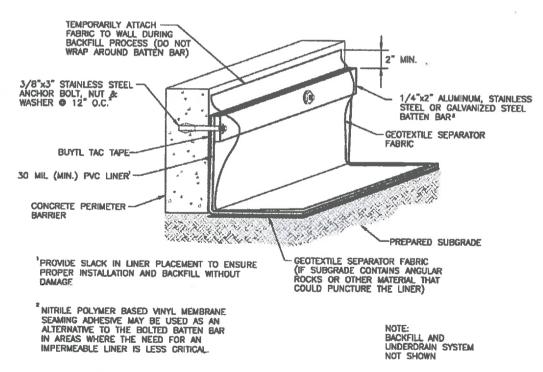
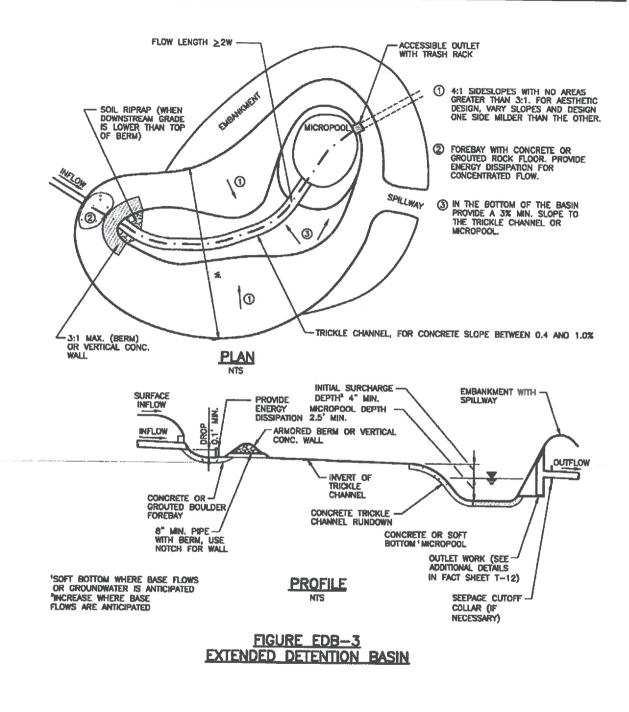


Figure SF-2. Geomembrane Liner/Underdrain Penetration Detail



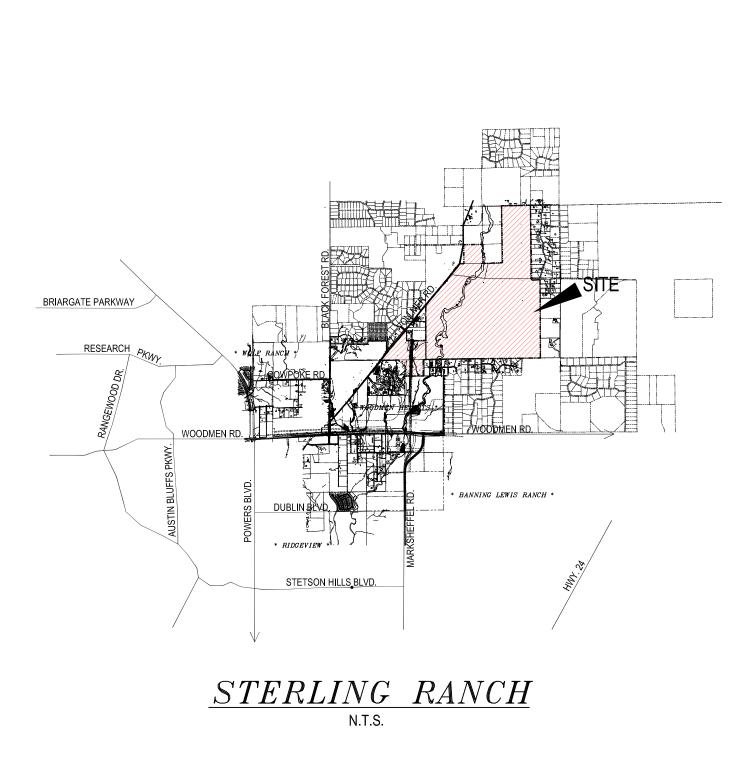


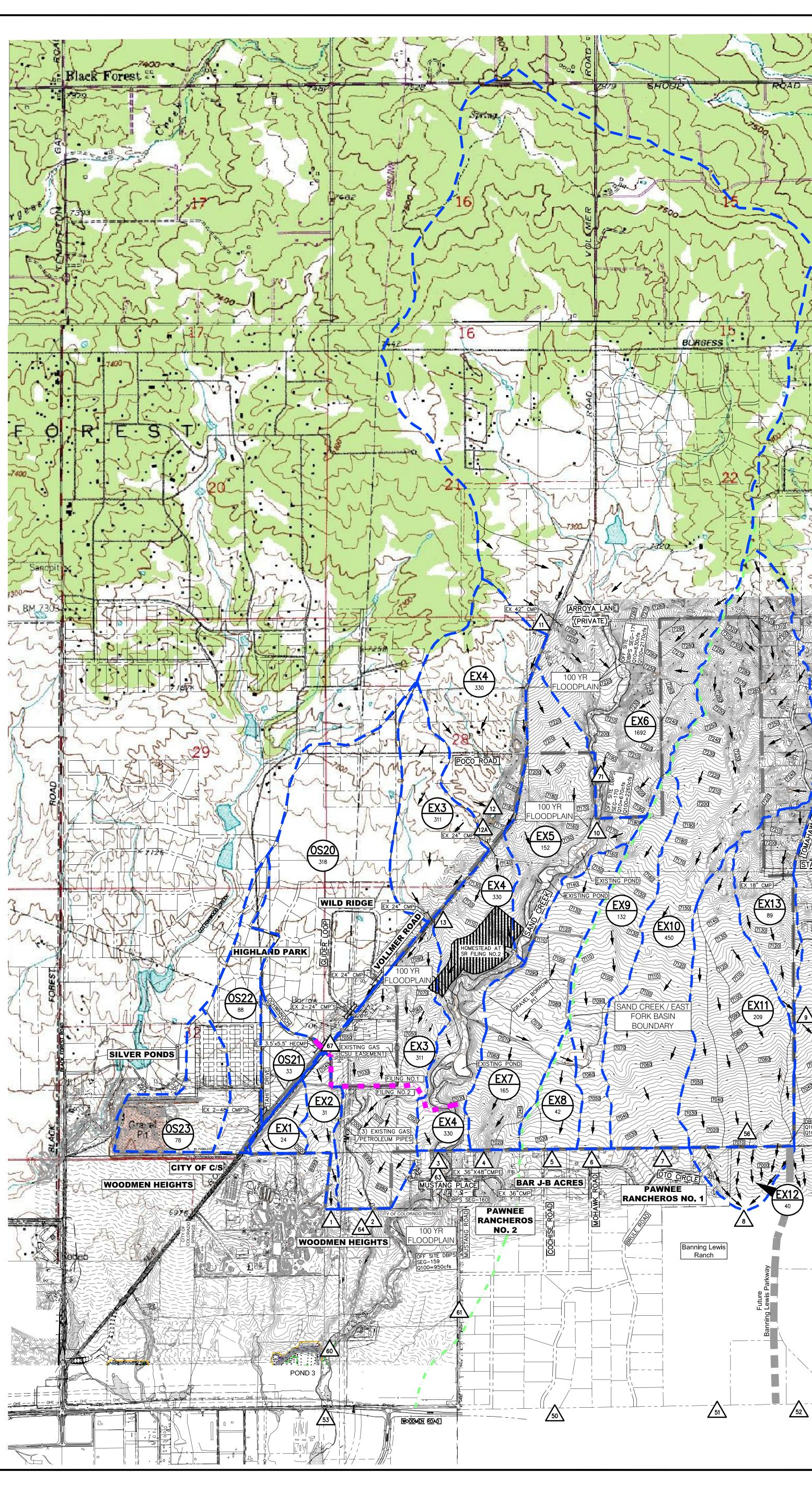




Additional Details are provided in BMP Fact Sheet T-12. This includes outlet structure details including orifice plates and trash racks.

HISTORIC, EXISTING AND PROPOSED DRAINAGE MAPS





HISTORIC CONDITION

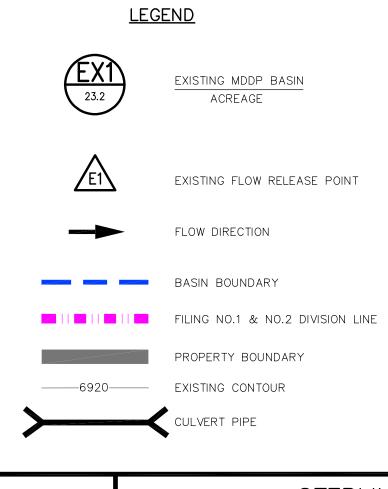
BASIN	AREA (acres)	Q 5 (CFS)	Q 100 (CFS)
EX-1	24	3	40
EX-2	31	3	45
EX-3	311	49	341
EX-4	330	71	352
EX-5	152	14	209
EX-6	1692	118	2168
EX-7	165	12	197
EX-8	42	4	64
EX-9	132	11	149
EX-10	450	48	474
EX-11	209	17	261
EX-12	40	5	65
EX-13	89	6	114
0S-20	318	61	310
0S-21	33	8	38
0S-22	88	18	91
0S-23	78	34	84

* N PAF HISTORIC PATTERNS ON THE WEST SIDE OF VOLLMER ROAD.

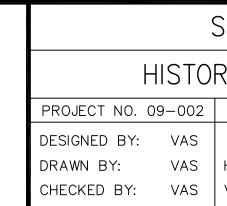
HISTORIC CONDITION

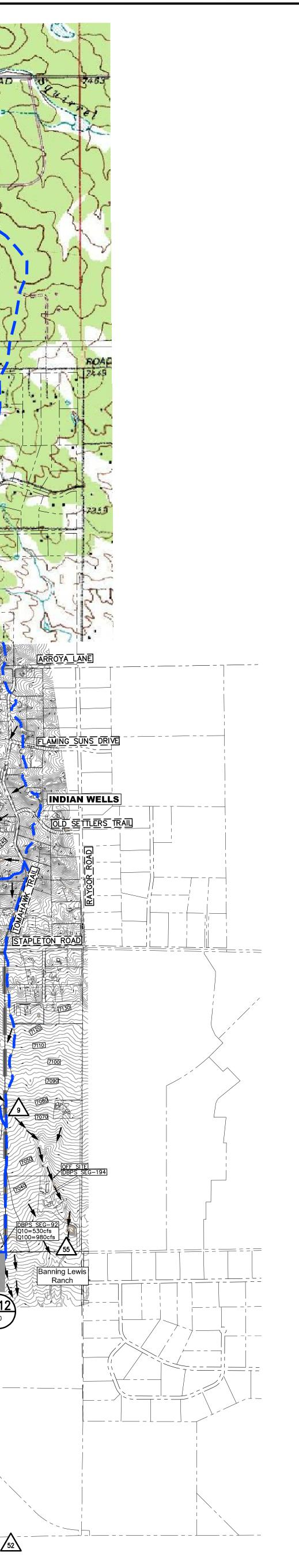
		DESIC	<u> SN P</u>	STNIC	$\hat{\mathbf{b}}$	
DESIGN POINT	SQ. MI.	Q 5 (CFS)	Q 100 (CFS)	SQ. MI.	DBPS Q100	DBPS DP/ID
1	0.09	5	84			
2	0.49	49	341	0.74	465	64
3	0.52	139	2610	4.33	2552	63
4	0.26	12	197			
5	0.07	4	64			
6	0.21	11	149			
7	0.70	48	474			
8	0.39	18	305			
9	0.14	6	114			
10	2.64	122	2245	3.27	2245	71
11	0.09	5	83			
12A	0.01	3	16			
12	0.27	10	200			
13	0.17	6	126			
* NOTE:	50 M			0.48	#	55
NOIL.	SQ. M STANT		ACH	0.53	1210	56
DESIG			DBPS	5.38	2629	60

1" = 1000' 0 250 500 1000 2000 Scale in Feet





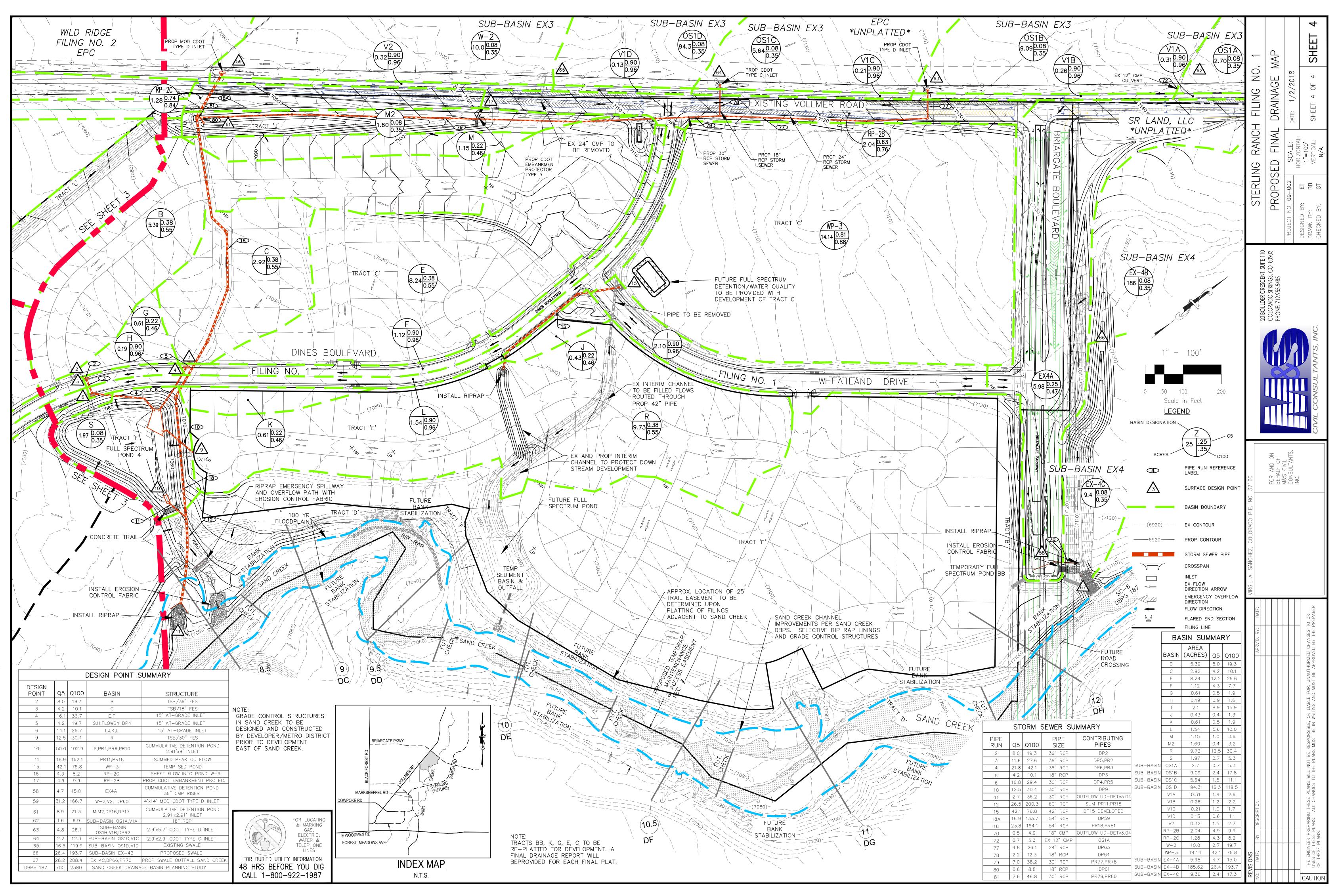


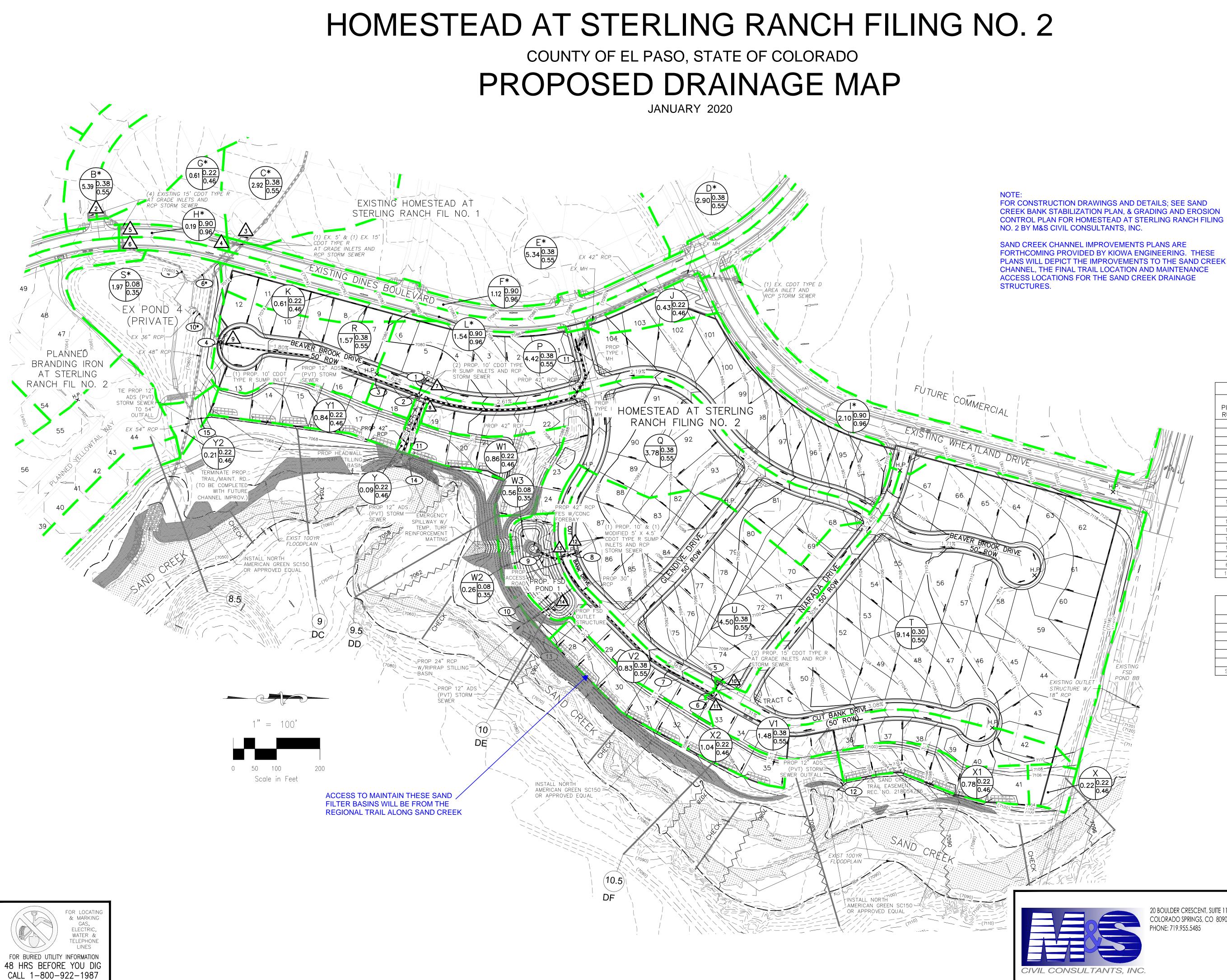


STERLING RANCH

HISTORIC – DRAINAGE MAP PROJECT NO. 09-002FILE: 0: \\dwg\Eng Exhibits\MDDP HISTORICDESIGNED BY:VASSCALEDATE:2/6/17

JUALL			
HORIZ: 1"=1000' VERT: N/A	SHEET 1 OF 1		





LEGEND





SURFACE DESIGN POINT



BASIN	BOUNDARY

-- (6920)-- EXISTING CONTOUR

PROP CONTOUR

HOMESTEAD FILING NOS. 2&3 BOUNDARY PROPOSED STORM SEWER PIPE

EXISTING STORM SEWER PIPE

CROSSPAN

- INLET
- EXISTING FLOW DIRECTION ARROW PROPOSED FLOW DIRECTION ARROW
- FLARED END SECTION
- HIGH POINT
- LOW POINT

STORM SEWER SUMMARY				
PIPE RUN	Q_5	Q ₁₀₀	PIPE SIZE	CONTRIBUTING PIPES/DESIGN POINTS
1	5.7	13.8	18"RCP	DP7
2	4.9	11.8	18" RCP	DP8
3	10.6	25.7	24" RCP	PR1, PR2
4	12.4	30.1	30" RCP	DP9, PR3
5	9.1	12.7	18" RCP	DP10
6	1.9	12.7	18" RCP	DP11
7	10.9	25.3	30" RCP	PR5, PR6
8	6.2	17.2	24" RCP	DP12
9	17.9	47.1	42" RCP	DP13, PR7, PR8
10	0.7	23.5	24" RCP	OUTLET STRUC.
11	42.1	76.8	42" RCP	CONTINUED FROM MDDP DP15*
12	0.0	1.3	12" ADS	LOTS 36-41
13	0.0	1.6	12" ADS	LOTS 28-35
14	0.0	1.5	12" ADS	LOTS 19-24
15	0.0	1.4	12" ADS	LOTS 13-18
4*	21.8	42.1	36" RCP	SEE MDDP*
6*	16.8	29.4	30" RCP	SEE MDDP*
10*	12.5	30.4	30" RCP	SEE MDDP*

BASI	ARY		
BASIN	AREA (ACRES)	Q ₅	Q ₁₀₀
01	NSITE BASINS	•	
J	0.43	0.4	1.3
K	0.61	0.5	1.9
P	4.42	5.7	13.8
Q	3.78	4.9	11.8
R	1.57	2.2	5.4
Т	9.14	9.4	26.4
U	4.50	6.4	15.6
V1	1.48	2.1	5.0
V2	0.83	1.2	2.9
W1	0.56	0.2	1.7
W2	0.26	0.1	0.8
W3	0.56	0.2	1.7
Х	0.22	0.2	0.8
X1	0.78	0.8	2.8
X2	1.04	1.1	3.7
Y	0.09	0.1	0.3
Y1	0.84	0.8	3.0
Y2	0.21	0.2	0.7
B*	5.39	8.0	19.3
C*	2.92	4.2	10.1
 D*	2.90	4.3	10.4
 E*	5.34	8.2	19.9
 F*	1.12	4.3	7.7
G*	0.61	0.5	1.9
H*	0.19	0.9	1.6
*	2.10	8.9	15.9
L*	1.54	5.6	10.0

1.97 0.7 5.7

S*

FULL	SPECTRUM	DETENTION
	INTERIM PO	DND 1

	•
WQ VOLUME	0.245 AC-FT
EURV VOLUME	0.741 AC-FT
100 YR STORAGE VOLUME	1.331 AC-FT
100 YR WATER SURFACE EL	7083.91
SPILLWAY CREST EL	7084.16
TOP OF EMBANKMENT EL	7086.00
SPILLWAY DESIGN FLOW DEPTH	0.84 FT

	DESIGN POINT SUMMARY			
DESIGN POINT	Q 5	Q ₁₀₀	BASIN	STRUCTURE
2*	8.0	19.3	В*	(2) EX. 15' AT-GRADE INLETS
3*	4.2	10.1	C*	EX. 6' SUMP INLET
4*	16.1	36.7	D*, E*, F*	EX. 15' AT-GRADE INLET
5*	4.2	19.7	G*, H*, FLOWBY DP4*	EX. 15' AT-GRADE INLET
6*	14.1	26.7	I*, J*, K*, L*	EX. 15' AT-GRADE INLET
7	5.7	13.8	Р	PROP. 10' SUMP INLET
8	4.9	11.8	Q	PROP. 10' SUMP INLET
9	2.2	5.4	R	PROP. 5' SUMP INLET
10	9.4	15.6	Т	PROP. 15' AT-GRADE INLET
11	1.9	15.6	V1	PROP. 15' AT-GRADE INLET
12	6.2	17.2	U, FLOWBY DP10	PROP. 10' SUMP INLET
13	1.2	5.9	V2, FLOWBY DP11	PROP. 5' SUMP INLET
14	19.6	52.4	W3, PR9	CUMULATIVE DETENTION POND
* For detailed information on Desina Points. Basins. Flowby, or Pipe Runs see Sterlin				

* For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

Refer to Homestead at Sterling Ranch Filling No. 2 Grading and Erosion Control Plan for additional interim channel stabilization improvements.

All elevations provided on map are referenced in NGVD29

HOMESTEAD AT STERLING RANCH FIL. NO. 2 PROPOSED DRAINAGE MAP PROJECT NO. 09-007 SCALE: DATE: 01/15/2020 HORIZONTAL DESIGNED BY: CMN 1"=100' DRAWN BY: CMN PDM SHEET 1 OF 1 VERTICAL: CHECKED BY: VAS N/A

20 BOULDER CRESCENT, SUITE 110 COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485