

**AN AMENDMENT TO THE
MASTER DRAINAGE DEVELOPMENT PLAN
FOR
WATERVIEW**

WATERVIEW NORTH

EL PASO COUNTY, COLORADO

October 2020

PREPARED FOR:

CPR Entitlements, LLC

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PROJECT NO. 02-19-05

PCD File No. SKP202

CERTIFICATIONS

Design Engineer’s Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. This drainage report has been prepared to satisfy criteria established and set forth by El Paso County for drainage reports. This drainage report is in conformance with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Charles K. Cothorn, P.E. #24997

Seal

Owner/Developer’s Statement:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

By (signature): _____

Date: _____

Title: CPR Entitlements, LLC

P.A. Koscielski, Manager

Address: 31 N. Tejon, Suite 500

Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.,
County Engineer / ECM Administrator

Date

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INTRODUCTION

Waterview North is a proposed multi-use development located within the greater Waterview Subdivision, in El Paso County, Colorado. The Waterview North site encompasses approximately 116.5 acres of development that include Industrial, Commercial and Residential uses with varying density.

Purpose & Scope of Study

This report is presented in conjunction with the Sketch Plan Amendment for Waterview as an Amendment to the Master Drainage and Development Plan for Waterview. Improvements proposed as part of Waterview North, Phase III of development on the Waterview Sketch Plan Amendment, are included as reference material in Appendix B. The purpose of this Amendment is to append findings presented with previously approved MDDP Amendments as well as the original Master Development and Drainage Plan (MDDP) for Waterview. Proposed changes to Land Use associated with the Amended Sketch Plan for Waterview are accompanied by updated hydrology calculations, updated Water Quality and Detention Pond Designs, and updated hydraulic calculations. Developments shown on the referenced, Amended Sketch Plan for Waterview are proposed in a manner that satisfies the requirements and criteria set forth by El Paso County's Engineering Criteria Manual as well as Volumes 1 and 2 of the Drainage Criteria Manual. Runoff quantities and proposed facilities have been calculated and sized using current El Paso County Development Standards and Drainage Criteria.

GENERAL DESCRIPTION AND LOCATION

Waterview North is located within the Waterview Subdivision, which encompasses approximately 721.8 acres. Waterview North occupies approximately 116.5 acres of the Northeast corner of the Waterview Sketch Plan. The Southwest Corner of the property coincides with the Northeast Corner of the intersection at Powers Boulevard and Bradley Road, in El Paso County, Colorado. The site is bound on the west and south by Powers Boulevard and Bradley Road, respectively. The Colorado Springs Airport lies to north, beyond a 3400' swath of undeveloped property. The Colorado Springs City Limits coincide with the northern boundary of Waterview North. The eastern boundary of the site and the Widefield Transportation Center D3 to the east are separated by a 1200-foot wide swath of undeveloped land and Foreign Trade Zone Blvd.

Of the 116.5 acres that is Waterview North, Residential accounts for 69 acres, Industrial covers 28.5 acres and Commercial occupies 18.6 acres.

Climate

The climate of the site is typical of a sub-humid to semiarid climate with mild summers and winters. The average temperature is 31F degrees in the winter and 68.4F degrees in the summer. Total annual precipitation is 15.21 inches.

Floodplain Statement

The Flood Insurance Rate Map (FIRM No. 08041C 0768G dated 12/07/2018) indicates that there is no floodplain in the vicinity of the proposed site. Please refer to the Annotated FIRM Panel, located in Appendix A at the back of this report.

Utilities & Other Encumbrances

There is an existing petroleum line that runs north / south on the westerly portion of Waterview North, along the inside of the eastern boundary of the Powers Boulevard easement. Said gas line is reflected on the plans and drainage exhibits.

There is a pair of existing 42” CMP culverts that cross Bradley Road approximately 950 feet to the east of the intersection at Powers Boulevard.

There are above-ground power lines that cross Bradley Road and follow the eastern boundary of the site. Distribution lines exist among said group of above-ground power lines.

Referenced Drainage Studies

Waterview North occupies the northeast quadrant of the greater Waterview Subdivision and straddles two major drainage basins as identified by El Paso County. A DBPS for each of the 2 major basins were referenced in addition to two Final Drainage Reports for nearly adjacent portions of the Waterview Subdivision and one Amendment to the MDDP for Waterview. A listing of the referenced Studies and Reports is as follows:

- *Jimmy Camp Creek Drainage Basin Planning Study: Development of Alternatives and Design of Selected Plan Report*”, by Kiowa Engineering, dated March 2015.
- *West Fork Jimmy Camp Creek Drainage Basin Planning Study*”, by Kiowa Engineering, dated October 2003.
- *“Amendment to the MDDP for Waterview “*, completed by Springs Engineering and approved in July of 2014.
- *“Final Drainage Report for Trails at Aspen Ridge, Filing No. 1”*, completed by Matrix Design Group and approved in January of 2020.
- *“Final Drainage Report for Trails at Aspen Ridge, Filing No. 2”*, completed by Matrix Design Group and approved in February of 2020.

SOIL CONDITIONS

Soils that underly the project site and the site’s offsite tributary areas are analyzed and classified by their Hydrologic Soil Type. Soils can be classified into four different hydrologic groups; A, B, C, & D. This manner of classification is applied to account for a soils’ potential to produce runoff.

Hydrologic group “A” is characterized by well-drained coarse-grained soils that have high infiltration rates and high rates of saturated hydraulic conductivity. Type “A” soils have low runoff potential. Group “D” typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock. As such, Type D soils have very slow infiltration rates and a high runoff potential. Please refer to the Soils Map, included in Appendix A. The table on the following page summarizes site soils by Hydrologic Type.

Pre-Development site conditions may be described as undeveloped high desert terrain having sparse natural vegetative cover ($\leq 50\%$ cover) consisting of brush, weeds and grass with brush being the most abundant. About a third of onsite soils are classified as type A. It should be noted that post development consideration of onsite areas does not recognize type A soil. All type A soils, onsite, are to be

considered as Type B Soils for post development conditions. The following is a summary table which lists the various soils of which the site is comprised:

Site Soil Summary Table

Map Unit Symbol	Map Unit Name	Hydrologic Soil Type	Acreage of AOI	Percentage of AOI
8	Blakeland loamy sand, 1 to 9 % slopes	A	43.7	32.50%
31	Fort Collins loam, 3 to 8 % slopes	B	33.2	24.70%
56	Nelson-Tassel fine sandy loams 3 to 18% slopes	B	33.4	24.80%
86	Stoneham sandy loam, 3 to 8 % slopes	B	19.8	14.70%
95	Truckton loamy sand, 1 to 9% slopes	A	0.2	0.10%
108	Wiley silt loam, 3 to 9 % slopes	B	4.4	3.30%
Totals for Area of Interest			134.7	100%

DRAINAGE BASINS & SUB-BASINS

The Waterview North development site is located within 2 major drainage basins; Big Johnson/Crews Gulch and Jimmy Camp Creek. The sites location lies in the upper reaches of each of the mentioned major watersheds. Portions of the site that belong to the Big Johnson/Crews Gulch Basin Tributary occupy western and northwestern reaches of the property. The western portion of the offsite tributary to Waterview North also belongs to the Big Johnson/Crews Gulch Basin Tributary. A portion of the site that covers the western boundary of Waterview North, characterized as Basin BJD-EX14 on the Pre-Dev Basin Map, located in Appendix B, presently drains to the west, over and across Powers Boulevard and ultimately into Big Johnson/Crews Gulch Basin. CDOT construction of Powers Boulevard Improvements will result in a hydraulic barrier to surface runoff generated over Basin BJD-EX14, as it presently conveys. Post Development conditions refer to the subject area as Basin BJDEV-14. While runoff generated over Basin BJDEV14 will not continue to convey in historic fashion as surface flow that crosses Powers Blvd., it is assumed that construction of the Powers Blvd. Improvements will maintain the historic drainage pattern in some form or fashion, and Basin BJDEV14 runoff will continue to convey to Big Johnson/Crews Gulch Basin. Post development conditions for this site consider this basin as undeveloped since construction of CDOT improvements to Powers will likely predate its development into a commercial property.

The remainder of Waterview North lies within one of two sub-basins belonging to the Jimmy Camp Creek Tributary. A 10-acre piece that occupies the southwest corner of the property is part of the West Fork Tributary to Jimmy Camp Creek. The remainder of the site, as well as the eastern portion of the offsite tributary are part of the MarkSheffel Tributary to Jimmy Camp Creek.

Basin IDs used in this study agree with those established for each of the Tributaries in the reference material. Areas ultimately tributary to Big Johnson/Crews Gulch Basin are labelled with a “BJD”

prefix, those tributary to Jimmy Camp Creek have a “JCD” prefix. Concentration points and Ponds are all labelled to be consistent with the reference material with the exception of Design Pt. A, which corresponds to Design Point “1-OS” as referenced from the Final Drainage Reports for Trails at Aspen Ridge, Filing No. 1 & Trails at Aspen Ridge, Filing No. 2.

Approximately 82 acres of Waterview North lie in the upper reaches of the Marksheffel Tributary to Jimmy Camp Creek. This drainage basin was studied in the “*Jimmy Camp Creek Drainage Basin Planning Study: Development of Alternatives and Design of Selected Plan Report*”, by Kiowa Engineering, dated March 2015.

Approximately 16.2 acres of Waterview North lie in the upper reaches of the West Fork Tributary to Jimmy Camp Creek. This drainage basin was studied in the “*West Fork Jimmy Camp Creek Drainage Basin Planning Study*”, by Kiowa Engineering, dated October 2003, and in The FDRs for Trails at Aspen Ridge, Filing No.1 and Filing No.2.

Development of Waterview North will comply with the findings presented in each of the above-mentioned Studies by providing onsite detention and water quality treatment for developed runoff. Offsite areas that lie upstream of Waterview North will be required to provide onsite detention and water quality treatment as they develop.

Design, phasing, responsibility and maintenance of proposed improvements will be discussed in future final drainage reports, at a later time. Fees will be assessed and paid according to current rates at the time of platting for each filing.

Sub-Basin Description

Historic Drainage Patterns

The historic drainage patterns of the site were analyzed in the Master Development Drainage Plan for Waterview by Merrick and Company. Offsite tributary areas are re-examined in this study. The offsite tributary to Waterview North lies to the north. A portion of the offsite tributary, approximately 63 acres, lies within the Big Johnson/Crews Gulch Basin Tributary. The remaining portion of the offsite watershed amounts to 56.7 acres, all of which lies within the Marksheffel Tributary to Jimmy Camp Creek. The reason that the offsite tributary was re-examined is because review of the existing topography along the north boundary of the site revealed a depression whose volume exceeds 35 acre-feet. Most of the Big Johnson/Crews Gulch offsite tributary area (54 out of 63 acres, area BJD-12a) appears to drain into this depression. Soils in this region are classified as Hydrologic Type A. The hydraulic conductivity for soils that coincide with the offsite pond’s location translates to a percolation rate that exceeds 8-inches per hour. The remainder of the offsite tributary to Big Johnson/Crews Gulch Basin drains to an existing Box Culvert Crossing along Powers Blvd.

Onsite Basin JCDEX-3.3 consists of ten acres that coincide with the southwest corner of the property. JCDEX-3.3 runoff conveys to an existing dual 42-inch CMP crossing under Bradley Road where it discharges from the site and continues to convey south.

Runoff produced over the Marksheffel tributary to Jimmy Camp Creek accounts for the majority of onsite runoff generated. The portion of the Marksheffel Tributary considered with this analysis is represented by offsite Basins JCD OS-1A & JCD OS-1B, and by onsite Basins JCDEX-3.1 & JCDEX-3.2. Runoff generated over these basins conveys to the south and east and discharges from the site over the eastern boundary. Runoff produced on JCDEX-3.2 flows south and then east being conveyed

eastward in the north side Bradley Road ditch combined with Bradley Road runoff within the Bradley Road RIGHT-OF-WAY. JCDEX-3.2 runoff and Bradley Road runoff leaves the Bradley Road RIGHT-OF-WAY and flows north across the subject property as Bradley Road approaches the eastern property boundary; this is due to no continuation of the north Bradley Road ditch east of the property related to a utility corridor access running north south along the east side of the subject property. Bradley Road ditch flow including Basin JCDEX3.2 runoff then flows north and combines with Basin JCDEX3.1 runoff and discharges across the southern portion of the eastern boundary of the site at a low point in the utility access corridor. Flows generated over the other 3 basins discharge across the eastern site boundary as well. Topography along the eastern boundary does not seem to indicate the presence of concentrated flow patterns, although the southern portion of the eastern boundary bears a depression. Design Point JCD-D has been loosely placed to coincide with said depression. Please refer to the Pre-Development Drainage Map, included in Appendix B. The length of the low region along the eastern boundary is between 300 and 400 feet. About 30' beyond the depression due east, there lies an elevated mound of dirt (utility access). Above-ground power poles follow the eastern boundary. With the exception of the mentioned mound of dirt, the manner of fall in and around this area is generally to the east and south of east. Runoff will convey eastward, north of Bradley Road in somewhat of an unconcentrated manner, for 950 to 1000 feet. As runoff approaches the western side of Foreign Trade Boulevard, the depression in which the runoff conveys narrows to form a headwater pool for the culvert crossing at Foreign Trade Boulevard. Said culvert crossing consists four-48" Diameter RCPs.

Off-Site Drainage

There are two off-site basins for Waterview North. One of them is located in the Big Johnson/Crews Gulch Tributary and the other lies within the Marksheffel Tributary to Jimmy Camp Creek. These basins were analyzed in the MDDP for Waterview by Merrick. Flows generated over these areas have been re-calculated in this study with the discovery of the depression located within Basin BJD-12a.

DRAINAGE DESIGN CRITERIA

Development Criteria Reference

The El Paso County Drainage Criteria Manual (DCM), Volumes 1 & 2 were used in preparation of this report in conjunction with El Paso County's Engineering Criteria Manual (ECM) and Resolutions 15-042 and 19-245.

In addition to the DCM, Denver's Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District, latest update, have been used to supplement the DCM for water quality capture criteria.

Hydrologic Criteria

Rational Method

The rational method was used to calculate onsite peak flows, as required by the current City of Colorado Springs/El Paso County Drainage Criteria Manual (DCM) for drainage basins having an area of less than 130 acres. The 5-year and 100-year storms constitute the major and minor events with these analyses, respectively.

Rational Method calculations are included in Appendix B, at the back of the report. Rational Method results are summarized and in tabular format on each of the respective drainage exhibits.

The results of the rational analysis are used to evaluate hydraulic street and channel capacities and to size storm drain appurtenances and components such as drop inlets/catch basins and pipe sizes. The Rational Method uses the following equation:

$$Q=C*i*A$$

Where:

Q = Maximum runoff rate in cubic feet per second (cfs)

C = Runoff coefficient

i = Average rainfall intensity (inches per hour)

A = Area of drainage sub-basin (acres)

Runoff Coefficients

Rational Method runoff coefficients are referenced from Table 6-6 of the Drainage Criteria Manual. Pre-Development runoff coefficients are based on hydrologic soil type and vegetative cover type. Weighted runoff coefficients for existing or pre-development conditions are calculated for basins comprised by more than one hydrologic soil type. Weighted runoff coefficients for post development conditions are based on hydrologic soil type and anticipated land use. Weighted coefficient calculations are not performed for basins that consist of one hydrologic soil type, for which one type of land use is anticipated. Please refer to the Runoff Coefficient Exhibit, included in Appendix B. Summary tables for runoff coefficients during both pre and post development conditions are included as well as a map which shows the site with land-use and soil-type overlays. Percent Impervious for each basin during pre-development conditions is assumed to be zero.

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis-- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Percent Impervious values, runoff coefficients, and curve numbers for each basin during post development conditions are weighted according to the combination of hydrologic soil type and land use-type. There are proposed residential areas where the density exceeds 8 dwelling units per acre. Runoff coefficients for these areas are extrapolated from the values shown with Table 6-6.

Time of Concentration

Time of concentration values are calculated as required by the DCM. The time of concentration consists of the initial time of overland flow (Ti), characterized by Equation 6-8 from the DCM, and the travel time (Tt) for channel or street flow to the inlet or point of interest, characterized by Equation 6-9 from the DCM. Equation 6-9 includes a conveyance coefficient, Cv, whose value is chosen from Table 6-7 of the DCM. Table 6.7 is shown below:

Table 6-7. Conveyance Coefficient, C_v

Type of Land Surface	C_v
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

*For buried riprap, select C_v value based on type of vegetative cover.

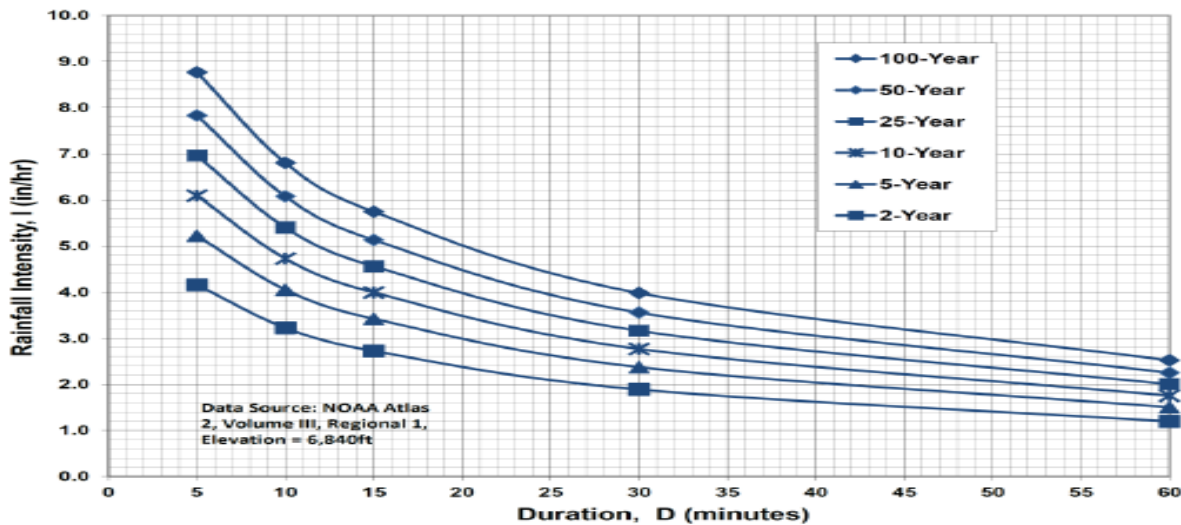
Pre-Development Conveyance Coefficients are representative of short pasture and lawns. Post Development Conveyance Coefficients reflect grassed waterways, which coincide with the 90-foot zoning buffers proposed along the northern and eastern property boundaries, and paved areas or shallow paved swales which coincide with proposed onsite streets and parking.

The time of concentration (T_c) is equal to the sum of the initial and travel times (Equation 6-7 from the DCM). A minimum time of concentration of 10-minutes is used for modeling undeveloped conditions and for developed conditions in non-urban areas. A minimum T_c of 5 minutes is utilized during post development conditions for urban areas.

Rainfall Intensity

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Drainage Criteria Manual. Table 6-2 lists the rainfall depth for the Major and Minor 1-hour storm events. The rainfall depths are translated into intensity values to be used with the rational formula by application of the IDF curves described on Figure 6-5 and shown, below. The referenced table and figures may be found in the front portion of Appendix B.

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



Curves presented on Figure 6-5 are developed from the IDF Equations shown below:

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Culvert Design

There are two culverts that exist along this site's boundary from which onsite flows discharge. An existing 10' by 6' RCBC along Powers Blvd. , and a dual 42-inch diameter CMP crossing under Bradley Road. Both culverts are analyzed during pre and post development conditions in this study. Placement of a proposed culvert along the north side of Bradley Road, adjacent to the eastern boundary of the site, is discussed and design calculations are included. Said calculations are located in Appendix D and were executed using HY-8. While the use of culverts is anticipated with future development of this property, there are no culverts proposed as part of this study.

Detention Storage Criteria

This report addresses the preliminary design of the detention / water quality ponds within the proposed development. Proposed ponds are designed as Full Spectrum. Pond hydraulics, treatment efficacy, and outlet structure performance are modelled with MHFD's software, MHFD-Detention_v4 02.

Storage volumes and outflows have been calculated for all detention facilities proposed herein. The proposed ponds serve to offsite peak developed flows adequately. The final design for each pond will be completed and submitted for approval with a subsequent Final Drainage Report, at a later time. The dimensions and performance of subsequent final pond designs are subject to change as long as code requirements are satisfied. Please note, while Pond A serves to treat developed runoff from proposed onsite commercial areas, the actual development for each of the commercially zoned lots will require that the developer be responsible for balancing and treating their own post development runoff. That is, each commercial lot will require its own pond.

HYDROLOGIC ANALYSES

Pre-Development Drainage Analysis

Big Johnson/Crews Gulch Basin & Jimmy Camp Creek Basins

Adjacent portions of the Big Johnson/Crews Gulch and Jimmy Camp Creek watersheds are presented on the Pre-Development Drainage Map, included in Appendix B.

Big Johnson/Crews Gulch Basin Tributary

The portion of the site that belongs to Big Johnson/Crews Gulch Tributary produces runoff that concentrates at Design Point BJD-K. There is also an offsite basin, BJD-12b that covers 9.54 acres and produces runoff that conveys to Design Point BJD-K. The peak flow rate that occurs at Design Point BJD-K during pre-development conditions is equal to 4 cfs and 31 cfs for the 5 and 100-year storms, respectively.

Offsite Basin BJD-12a runoff conveys into an existing 34+ acre-foot depression. The volume of the depression exceeds the volume of runoff for both 5 and 100-yr events. A basin calculation using the MHFD-Detention_v4 02 spreadsheet is included in Appendix C and shows the volume of runoff for the various events versus the volume of the existing offsite pond/depression. Runoff produced over Basin BJD-12a is not accepted onsite and does not impact Design Point BJD-K.

Runoff produced over Basin BJDEX14 conveys to the south and west, as sheet flow, over and across Powers Boulevard.

Jimmy Camp Basin

The historic basins for both tributaries of Jimmy Camp Creek are analyzed with the rational formula. Flows shown with the basin identifiers on the Drainage Exhibits reflect the results of said rational analysis. The Pre-Dev Drainage Basin Map and calculations are included in Appendix B for reference and are summarized below:

- Design Point A ($Q_5=4\text{cfs}$, $Q_{100}=31\text{cfs}$) is located on the north side of the adjacent western portion of Bradley Road. Design Pt. A receives runoff generated over Basin JCDEX-3.3. These flows convey south, across Bradley Road via an existing dual 42" CMP Culvert Crossing. Flows conveyed by the dual culvert crossing discharge into an existing swale on the south side of Bradley and continue to convey south. Design Point A is represented by Design Point 1-OS in the referenced FDR for Filing No. 1 of Trails at Aspen Ridge. Referenced peak flow rate values at Design Point 1-OS during pre-development conditions equal 5.0 cfs and 25.3cfs for the 5 & 100-year events, respectively. Flows discharged from Design Pt. A feed the West Fork Tributary to Jimmy Camp Creek.
- Design Point JCD-D has been placed to loosely coincide with a depression that occurs along the eastern boundary of the site. Said depression stretches 300 feet across, due north from the northern edge of Bradley Road, and is approximately 1-foot deep at its deepest point as measured along the eastern property boundary. A mound of dirt has been placed within said depression, by others, just beyond the eastern property boundary, as part of utility access from Bradley Road north for the existing power poles along the east boundary. Said mound of dirt serves to obscure historic flow patterns. Design Point JCD-D is the location where runoff from the north side of Bradley Road ROW, onsite Basins JCDEX-3.1 & JCDEX-3.2 and offsite Basins JCD-OS1A & JCD-OS1B combine and convey east to feed the Marksheffel Tributary to Jimmy Camp Creek. Major and minor flows at Design Point JCD-D are equal to 84cfs & 12cfs, respectively.

Post Development Drainage Analysis

Big Johnson/Crews Gulch Basin

Onsite runoff generated over areas that belong to the Big Johnson/Crews Gulch Basin Tributary are captured and conveyed into Pond BJD-K, with the exception of onsite Basin BJDEV-14.

The portion of the site that covers the western boundary of Waterview North, characterized as Basin BJDEV14 on the Post Development Drainage Plan, presently drains to the west over and across Powers Boulevard and ultimately into Big Johnson/Crews Gulch Basin. CDOT construction of Powers Boulevard Improvements will result in a hydraulic barrier to surface runoff generated over Basin BJD-EX14, as it presently conveys. Post Development conditions refer to the subject area as Basin BJDEV-14. While runoff generated over Basin BJDEV14 will not continue to convey in historic fashion, as surface flow that crosses Powers Blvd., it is assumed that construction of the Powers Improvements will see the historic drainage pattern maintained in some form or fashion, and Basin BJDEV14 runoff will continue to convey to Big Johnson/Crews Gulch Basin. Developed Flows from BJDEV-14 will be treated prior to being discharged at or below the historic peak rate. For the post development analysis included herein, Basin BJD-EX14 (undeveloped) runoff is routed across Basin JCD-DEV3.3 and into proposed Pond A. Post development discharge from Pond A was calculated to be 1cfs & 17 cfs for the minor and major events, respectively. Post Development rates of discharge from Pond A do not exceed Historic rates, so the proposed pond is in conformance.

Pond BJD-K

Flows generated over onsite Basin BJD-12c convey into Pond BJD-K. Pond BJD-K is located about 70 feet to the west of the site and serves the site entirely about 100% of the time. Pond BJD-K serves the site with a full spectrum of flows. BJD-K and Pond A are under 100% of the time. Powers Boulevard is a series of ponds so that peak flows are not exceeded.

Clarify. The developed drainage map is showing this basin is routed into Pond A. Update Pond A calculation to include basin BJDEV-14 for the pond sizing.

However, if basin BJDEV-14 is supposed to have it's own wq/detention then show the pond on the proposed drainage map and provide the pond calculation. Assuming discharge is as shown on the proposed map then Pond A must be redesigned as a pond in a series.

The pre-developed rate of discharge from the site at Design Point BJD-K was determined to be 4 and 31cfs for the 5 and 100-year events. The post development peak rate of discharge at the same location is 1 and 9 cfs for the 5 and 100-year events, respectively. In the Amendment to the MDDP for Waterview, completed by Springs Engineering and approved in July of 2014, post development flows at the same location were shown to be 239cfs and 215cfs for the major and minor storms, respectively. The depression shown to the north of the Waterview North site on the pre & post development Drainage Exhibits is not accounted for in the referenced analysis.

Suitable Outfall

The existing 10' by 6' RCBC Crossing under Powers Blvd. feeds a man-made channel that conveys south to the location of an anticipated culvert crossing under future Bradley Road improvements, then further south into Big Johnson Reservoir. The channel is shown on Sheet 4, Proposed Drainage Map for Waterview II, from the Amendment to Waterview MDDP, produced by Springs Engineering on 7/21/2014 and approved on 8/28/2014. Flows at the existing RCBC Crossing under Powers Blvd are shown to be 109.8 cfs and 170.9 cfs for the 10 & 100-year events, respectively. Post Development discharge at Design Point BJD-K, as presented with the findings contained

herein, amount to 1 & 9 cfs for the 5 & 100-year events, respectively. The channel improvements, as they exist, are more than adequate to accommodate outfall from the Waterview North site.

Jimmy Camp Creek Basin

There are 2 onsite and 2 offsite drainage basins located within the Marksheffel Tributary to Jimmy Camp Creek.

Offsite Basins JCDOS-1A & JCDOS-1B account for 56.7 acres of undeveloped offsite tributary. Runoff generated from these basins is accepted onsite. Runoff from these two basins is accommodated for during post development conditions by an onsite, grass lined diversion channel. Said channel is proposed within a 90-foot wide landscape buffer that follows the northern and eastern boundaries of the site. The subject diversion channel's width will exceed 30-feet, so it will be constructed with access ways on both sides so as to satisfy requirements set forth by ECM Section 3.3.3.K.1. The diversion channel shall be free of fencing and proposed structures and will not be used to store construction materials. Flows conveyed within the proposed channel will convey east, along the northern boundary, then south, adjacent to the eastern boundary of the site. Flows conveyed within this channel will combine with discharge from Pond JCD-D before discharging across the eastern boundary. Possible conveyance to the east is discussed as part of suitable outfall for Pond JCD-D below.

Onsite developed flows will convey to Pond JCD-D where runoff will be treated, and peak flows attenuated to at or below historic levels prior to discharging from the pond. Pond JCD-D is situated along the eastern boundary of the site. Onsite runoff is generated over 2 basins; JCDEV-3.1 & JCDEV-3.2. Runoff from JCDEV-3.2 will convey south and east to Pond JCD-D; site grading will modify existing conditions and will not allow flow from this basin to enter Bradley Road ROW. Discharge into Pond JCD-D will either be by way of a culvert crossing under the entrance to the site, or through future storm drain improvements for the area. Runoff produced over area JCDEV-3.1 will convey to Pond JCD-D as a combination of surface flows and storm drain discharge. Basins JCDEV-3.1 & JCDEV-3.2 account for approximately 82 acres of onsite development.

Pond JCD-D

Pond JCD-D has a volume of 11.25 Acre-Feet and is designed to provide Full Spectrum Treatment to onsite developed runoff. The Water Quality Capture Volume (WQCV) for the pond is 2.317 Acre-Ft and the Excess Urban Runoff Volume (EURV) is 7.441 Acre-Ft. Pond JCD-D is approximately 8.0 feet deep on the high side of the containment berm. The peak outflow from Pond JCD-D, given a 100-yr event, is equal to 101 cfs. Discharge from Pond JCD-D combine with offsite flows from basins JCDOS-1A & JCDOS-1B prior to discharging east.

Suitable Outfall

Flows that discharge from Pond JCD-D combine with the offsite flows in the eastside diversion channel along with the northerly roadside ditch of Bradley Road; the Bradley Road ditch flow is blocked from following Bradley Road east and leaves the right-of-way and flows north onto the subject property as described in the historic conditions section of this report. Runoff that is tributary to this confluence, offsite flows from the diversion channel, discharge from Pond JCD-D and Bradley Road ditch flow must discharge from the site to the east.

There are two primary feasible options. Both options assume the confluence of Pond JCD-D discharge, the east side diversion channel and the northerly roadside ditch for Bradley Road:

Add bullet point

- Unconcentrated Discharge: The diversion channel, the pond discharge and flow from Bradley Road right-of-way would naturally follow the existing flow to the east through an existing depression where ponding would occur until flow is deep enough to continue east. Control of this discharge could be enhanced with a flow spreader consisting of a weir approximately 300-feet long matching the existing depression width. Flow over this weir is estimated to be about 4-inches deep under 100-year conditions. Erosion protection could be added upstream and downstream of the weir. This option allows flows to follow existing flow patterns to the east; however, it does not address the issue that Bradley Road runoff does not stay within Bradley Road.
- Concentrated Discharge: Concentrated discharge to a public right-of-way could be accomplished by correcting the Bradley Road ditch issue east of the property by installing a culvert through the existing berm. Preliminary sizing indicates the culvert would be 48-inches and approximately 100-feet long. This correction would Bradley Road right-of-way runoff to stay in the right-of-way and would allow discharge of Pond JCD right-of-way. Any long-term detrimental effects and to areas further to the east from the site significantly reduced. Errant and erratic flow unconcentrated fashion, or as sheet flow, could

Based on conversation with the design engineer there are two options being considered for basin JCDEV3.3.

Rewrite narrative to clearly state that two options are currently being considered within JCDEV3.3. Recommend separating the two options into two bullet points similar to the above outfall alternative for pond D.

For each option clearly identify the wq/detention for basin BJDEV14 since this basin is being routed through Pond A.

Pond A

Detention Pond A, shown on the post development of the western portion of Bradley Road, serves to commercially zoned portion of the site. Please note that commercially zoned areas will be lot specific. The responsible for treating and balancing their own runoff proposed Pond A or from each of the proposed catchment Design Point A. Design Point A marks the location of an existing dual 42-inch diameter CMP crossing under Bradley Road. This culvert crossing was analyzed in the FDR for Filing 1 of The Trails at Aspen Ridge. Design Point A in the Pre-Development Analysis included with this study coincides with Design Point 1-OS from the referenced Study. Table 7.7a from page 12 of the above-mentioned FDR indicates major and minor peak flow rates of 4 and 27 cfs, respectively, at Design Point OS-1, or Design Point A. Given this existing crossings' proximity to a proposed entrance to the site, the high side of the culvert crossing will likely be appended with a junction structure. The outlet pipe from Pond A will terminate into said junction structure where flows will convey south to the low side of the culvert crossing. Per the Filing 1 Final Drainage Report for Trails at Aspen Ridge, a 24-inch RCP storm pipe will be sleeved into one of the existing 42-inch CMP cross road pipes to minimize disturbance to Bradley Road and avoid conflicts with existing utilities. The second 42-inch diameter CMP at this location will be plugged. Onsite peak discharge rates from the site at Design Point A amount to 1 & 17 cfs for the minor and major events, respectively.

Suitable Outfall

Pond A will discharge from the site through a 24" RCP pipe that is sleeved through one of the dual 42-inch diameter CMPs that crosses under Bradley Road as referenced from the FDR for Trails at Aspen Ridge, Filing No. 1. The calculated discharge at Design Point A is less than the reference values from which the downstream improvements were designed. Design Point A continues to provide a suitable outfall for developed runoff from this project site.

The following is a table that summarizes some of the properties of each of the proposed ponds:

WATERVIEW NORTH POND SUMMARY TABLE

POND ID	WQVC	EURV	TOTAL VOL.	MAX DEPTH	LENGTH TO WIDTH	POND DIMENSIONS OF MAIN CHANNEL	100-YR DEPTH	SURFACE AREA AT 100-YR	PEAK FLOWS			
									Q(5) _i n	Q(100) _i n	Q(5) _{ou} t	Q(100) _{ou} t
	(Ac-Ft)	(Ac-Ft)	(Ac-Ft)	(Ft)		(Ft. x Ft.)	(Ac-Ft)	(Ac.)	(c.f.s.)	(c.f.s.)	(c.f.s.)	(c.f.s.)
POND A	0.347	1.029	1.517	7.0	2.5	165 x 94	5.920	0.320	38	84	1	17
POND BJD-K	0.50	1.67	2.51	6.5	2.0	210 x 125	5.17	0.54	37	74	1	9
POND JCD-D	2.32	7.44	11.25	8.0	2.0	403 x 229	7.53	2.08	164	320	14	101

As commercial, industrial and residential development begins in this area, storm drain improvements will be implemented and drainage systems designed. Each Phase of residential and/or commercial development will require site-specific Preliminary and/or Final Drainage Studies to ensure that new developments do not increase peak rates of discharge or result in adverse effect to surrounding, upstream or downstream properties or facilities. Development of each commercial lot will also require a preliminary and or final drainage study as each lot will be required to balance its developed runoff.

REFERENCE MATERIALS

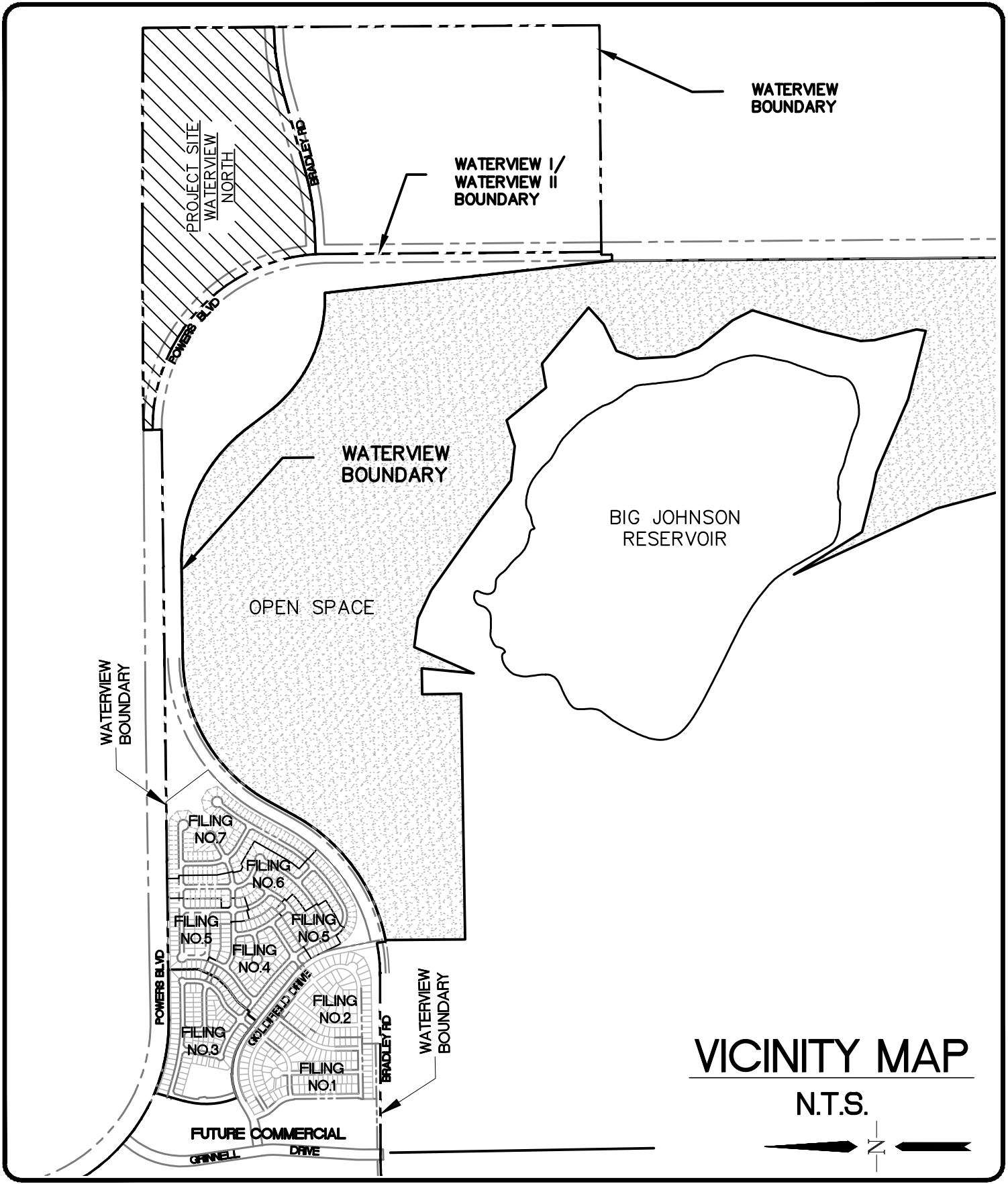
1. “City of Colorado Springs/El Paso County Drainage Criteria Manual” September 1987, Revised November 1991, Revised October 1994.
2. “City of Colorado Springs/El Paso County Drainage Criteria Manual, Volume 2: Stormwater Quality Policies, Procedures and Best Management Practices” November 1, 2002.
3. Soils Survey of El Paso County Area, Natural Resources Conservation Services of Colorado.
4. **“Master Development Drainage Plan for Waterview”**, by Merrick & Co., May 2006
5. **“Big Johnson/Crews Gulch Basin/Crews Gulch Drainage Basin Planning Study”**, Kiowa Engineering Corporation, September 1991.
6. **“Final Drainage Report for Trails at Aspen Ridge, Filing No. 1”** by The Matrix Design Group, January, 2020.
7. **“Final Drainage Report for Trails at Aspen Ridge, Filing No. 2”** by The Matrix Design Group, February, 2020.
8. **“Amendment to the MDDP for Waterview”** by Springs Engineering, July, 2014.

APPENDIX A

VICINITY MAP

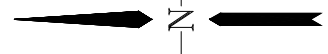
SOILS MAP

ANNOTATED FIRMette



VICINITY MAP

N.T.S.



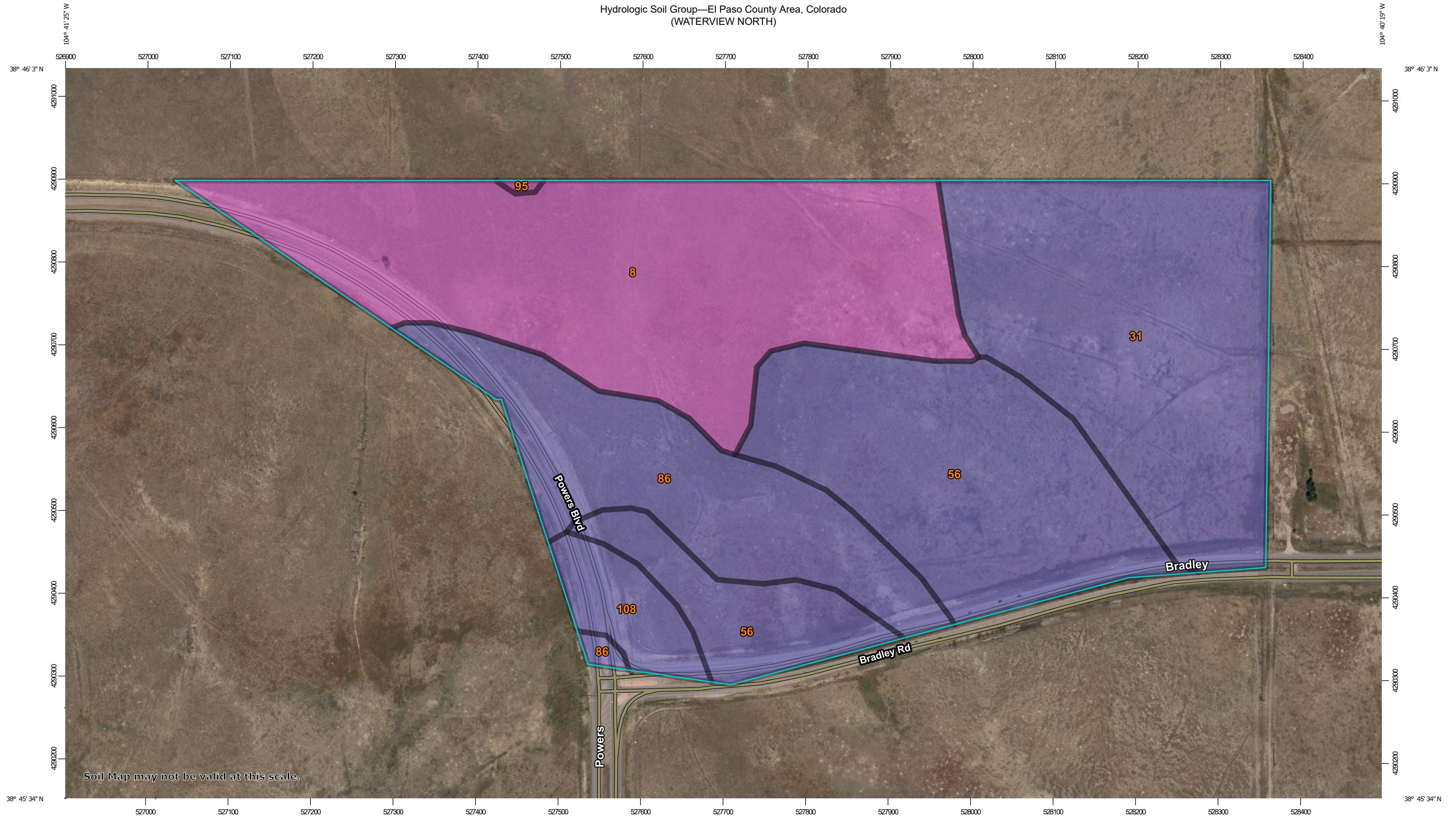
WATERVIEW MDDP AMEND VICINITY MAP

DSE *Dakota Springs
Engineering*

31 N. TEJON, SUITE 518
 COLORADO SPRINGS, CO 80918
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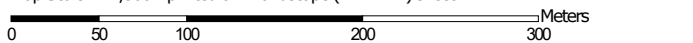
FIGURE 1

Hydrologic Soil Group—El Paso County Area, Colorado
(WATERVIEW NORTH)



Soil Map may not be valid at this scale.

Map Scale: 1:4,300 if printed on B landscape (17" x 11") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84



Hydrologic Soil Group—El Paso County Area, Colorado
(WATERVIEW NORTH)

MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines


-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	43.7	32.5%
31	Fort Collins loam, 3 to 8 percent slopes	B	33.2	24.7%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	B	33.4	24.8%
86	Stoneham sandy loam, 3 to 8 percent slopes	B	19.8	14.7%
95	Truckton loamy sand, 1 to 9 percent slopes	A	0.2	0.1%
108	Wiley silt loam, 3 to 9 percent slopes	B	4.4	3.3%
Totals for Area of Interest			134.7	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

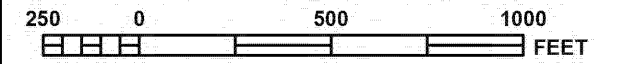
Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



MAP SCALE 1" = 500'



PANEL 0768G

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS

PANEL 768 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0768	G
EL PASO COUNTY	080059	0768	G

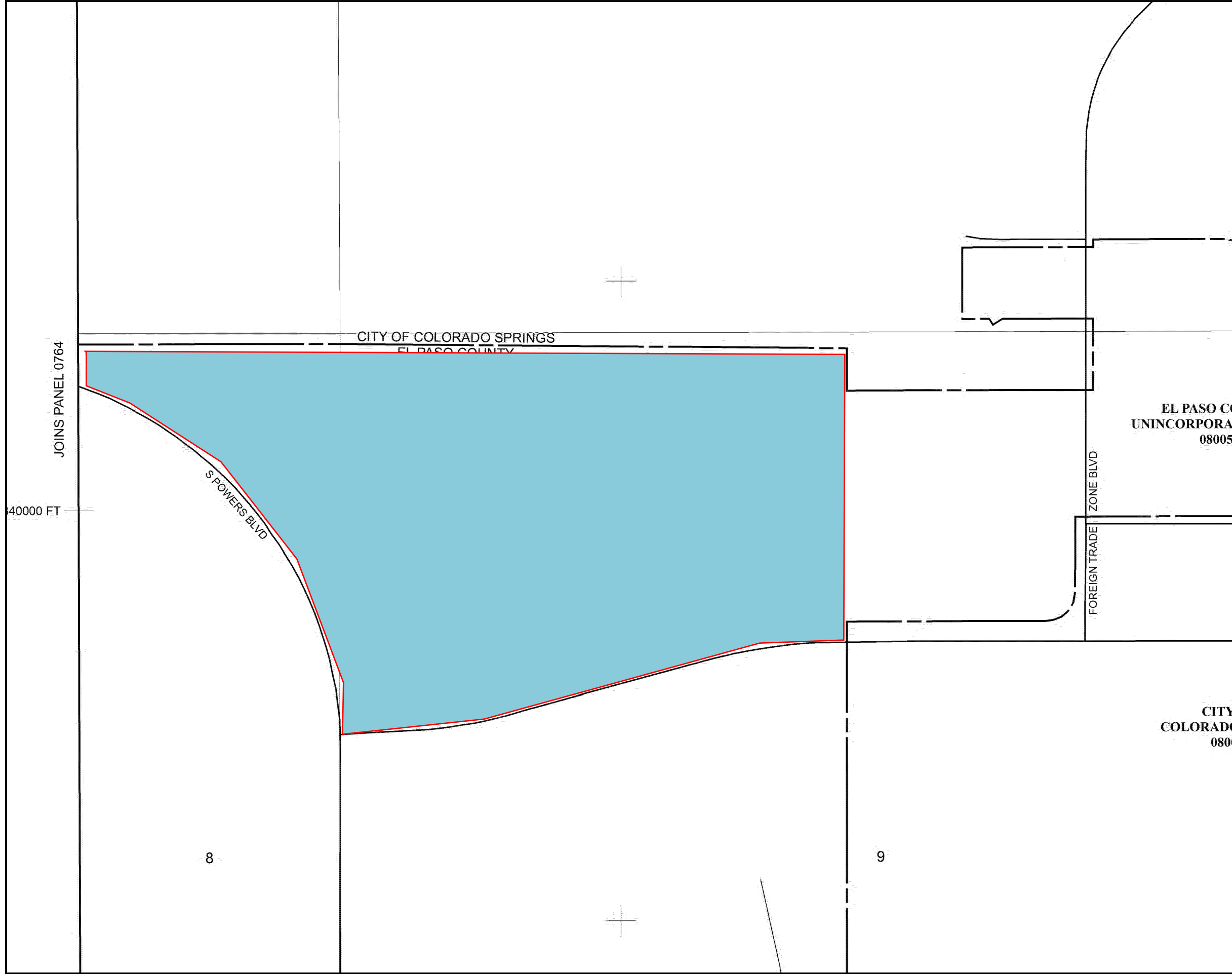
Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER
08041C0768G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency



This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at www.msc.fema.gov

APPENDIX B

PRE & POST DEVELOPMENT RATIONAL ANALYSES

PRE-DEVELOPMENT BASIN MAP

POST DEVELOPMENT DRAINAGE PLAN

EL PASO COUNTY REFERENCE INFO
RATIONAL ANALYSIS

For Colorado Springs and much of the Fountain Creek watershed, the 1-hour depths are fairly uniform and are summarized in Table 6-2. Depending on the location of the project, rainfall depths may be calculated using the described method and the NOAA Atlas maps shown in Figures 6-6 through 6-17.

Table 6-2. Rainfall Depths for Colorado Springs

Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth
2	<u>1.19</u>	1.70	2.10
5	<u>1.50</u>	2.10	2.70
10	<u>1.75</u>	2.40	3.20
25	<u>2.00</u>	2.90	3.60
50	<u>2.25</u>	3.20	4.20
100	<u>2.52</u>	3.50	4.60

Where $Z = 6,840 \text{ ft}/100$

These depths can be applied to the design storms or converted to intensities (inches/hour) for the Rational Method as described below. However, as the basin area increases, it is unlikely that the reported point rainfalls will occur uniformly over the entire basin. To account for this characteristic of rain storms an adjustment factor, the Depth Area Reduction Factor (DARF) is applied. This adjustment to rainfall depth and its effect on design storms is also described below. The UDFCD UD-Rain spreadsheet, available on UDFCD's website, also provides tools to calculate point rainfall depths and Intensity-Duration-Frequency curves² and should produce similar depth calculation results.

2.2 Design Storms

Design storms are used as input into rainfall/runoff models and provide a representation of the typical temporal distribution of rainfall events when the creation or routing of runoff hydrographs is required. It has long been observed that rainstorms in the Front Range of Colorado tend to occur as either short-duration, high-intensity, localized, convective thunderstorms (cloud bursts) or longer-duration, lower-intensity, broader, frontal (general) storms. The significance of these two types of events is primarily determined by the size of the drainage basin being studied. Thunderstorms can create high rates of runoff within a relatively small area, quickly, but their influence may not be significant very far downstream. Frontal storms may not create high rates of runoff within smaller drainage basins due to their lower intensity, but tend to produce larger flood flows that can be hazardous over a broader area and extend further downstream.

- **Thunderstorms:** Based on the extensive evaluation of rain storms completed in the Carlton study (Carlton 2011), it was determined that typical thunderstorms have a duration of about 2 hours. The study evaluated over 300,000 storm cells using gage-adjusted NEXRAD data, collected over a 14-year period (1994 to 2008). Storms lasting longer than 3 hours were rarely found. Therefore, the results of the Carlton study have been used to define the shorter duration design storms.

To determine the temporal distribution of thunderstorms, 22 gage-adjusted NEXRAD storm cells were studied in detail. Through a process described in a technical memorandum prepared by the City of Colorado Springs (City of Colorado Springs 2012), the results of this analysis were interpreted and normalized to the 1-hour rainfall depth to create the distribution shown in Table 6-3 with a 5 minute time interval for drainage basins up to 1 square mile in size. This distribution represents the rainfall

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis-- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_t) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Table 6-7. Conveyance Coefficient, C_v

Type of Land Surface	C_v
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

*For buried riprap, select C_v value based on type of vegetative cover.

- Ex. Good in
- En.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_t) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \quad (\text{Eq. 6-10})$$

Where:

t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional “calibration” of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

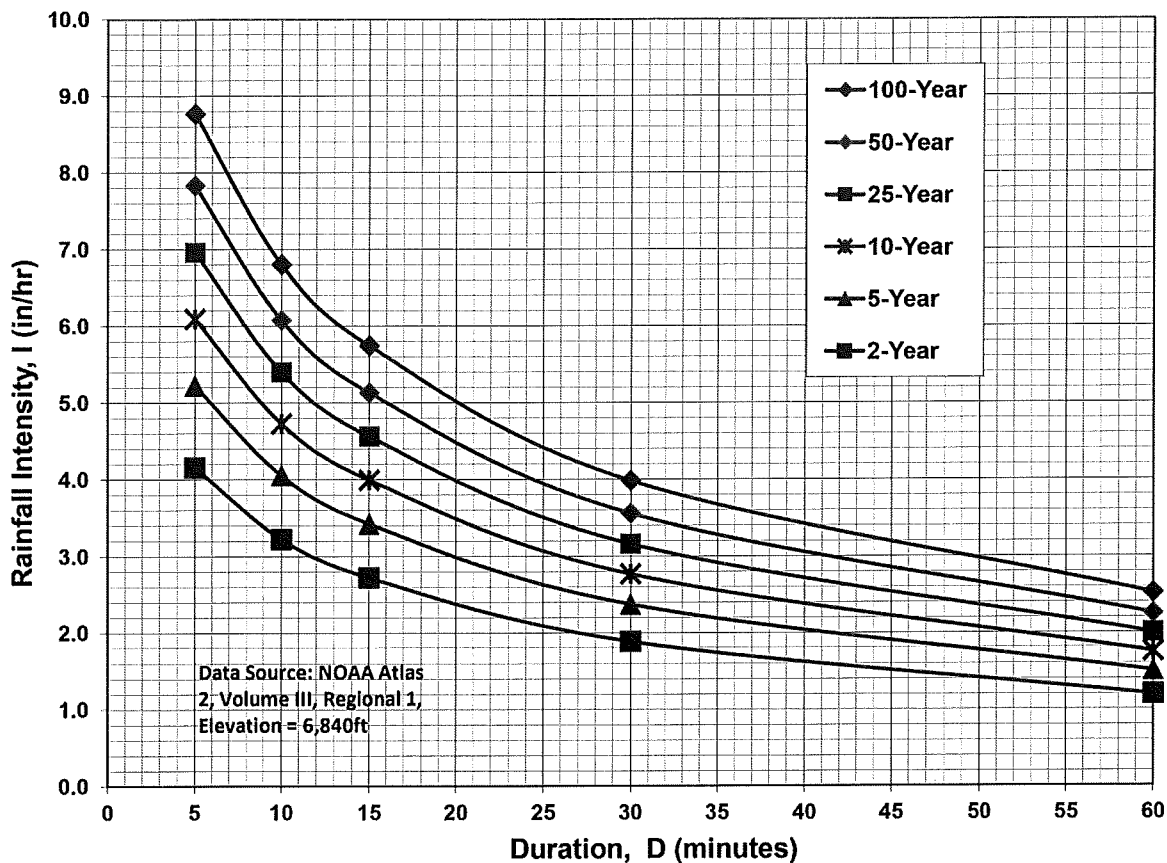
3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

**PRE-DEVELOPMENT RATIONAL ANALYSIS
SUMMARY**

WATERVIEW NORTH - EXISTING (RATIONAL METHOD Q=CIA)

BASIN	TOTAL FLOWS				AREA TOTAL (Ac)	WEIGHTED		OVERLAND				CHANNEL				Tc TOTAL (min)	INTENSITY		COMMENTS		
	Q(5) (c.f.s.)	Q(100) (c.f.s.)	CA(equiv.)			C(5)	C(100)	C(5)	Length (ft)	Slope (ft)	Ti (min)	Length (ft)	Slope (%)	Description Code	Convey Factor (K)		Velocity (fps)	Tt (min)		I(5) (in/hr)	I(100) (in/hr)
BJD-12a	8.3	60.6	4.34	19.00	54.28	0.08	0.35	0.08	300	3.7%	21.5	1,784	3.5%	3	7	1.3	22.7	44.2	1.9	3.2	
BJD-12b	2.0	14.8	0.76	3.34	9.54	0.08	0.35	0.08	295	2.8%	23.3	377	6.2%	3	7	1.7	3.6	26.9	2.6	4.4	
BJD-12c	2.8	20.5	1.46	6.38	18.23	0.08	0.35	0.08	300	3.3%	22.3	1,104	1.5%	3	7	0.9	21.5	43.7	1.9	3.2	
BJDEX-14	1.9	13.7	0.49	2.16	6.16	0.08	0.35	0.08	112	9.8%	9.5	377	9.1%	3	7	2.1	3.0	12.5	3.8	6.4	
JCD-OS1A	5.2	38.1	2.88	12.60	36.00	0.08	0.35	0.08	247	4.0%	19.0	2,545	4.6%	3	7	1.5	28.3	47.2	1.8	3.0	
JCD-OS1B	4.6	33.6	1.66	7.25	20.70	0.08	0.35	0.08	200	8.5%	13.3	1,167	5.8%	3	7	1.7	11.5	24.8	2.8	4.6	
JCD-EX3.1	9.4	69.1	5.49	24.01	68.60	0.08	0.35	0.08	300	8.3%	16.4	2,633	3.5%	3	7	1.3	33.5	49.9	1.7	2.9	
JCD-EX3.2	3.0	22.2	1.06	4.62	13.21	0.08	0.35	0.08	244	9.0%	14.4	958	6.6%	3	7	1.8	8.9	23.3	2.9	4.8	
JCD-EX3.3	2.6	19.1	0.80	3.50	10.00	0.08	0.35	0.08	297	11.8%	14.6	398	7.5%	3	7	1.9	3.5	18.0	3.2	5.4	
Design Points																					
A	4.2	30.8	1.29	5.66	16.16	0.08	0.35	0.08	297	11.8%	14.6	398	7.5%	3	7	1.9	3.5	18.0	3.2	5.4	Basin JCD-EX.3.3
BJD-12b	2.0	14.8	0.76	3.34	9.54	0.08	0.35	0.08	295	2.8%	23.3	377	6.2%	3	7	1.7	3.6	26.9	2.6	4.4	
BJD-12c	2.8	20.5	1.46	6.38	18.23	0.08	0.35	0.08	300	3.3%	22.3	1,104	1.5%	3	7	0.9	21.5	43.7	1.9	3.2	
BJD-K	4.3	31.2	2.22	9.72	27.77	0.08	0.35	0.08	300	3.3%	22.3	1,104	1.5%	3	7	0.9	21.5	43.7	1.9	3.2	Basins BJD-12b & BJD-12c
JCD-D	10.4	76.2	10.02	43.86	125.30	0.08	0.35	0.08	247	4.0%	19.0	4,881	3.8%	3	7	1.4	59.6	78.6	1.0	1.7	JCD-D WITHOUT JCD-EX3.2
JCD-EX3.1	9.4	69.1	5.49	24.01	68.60	0.08	0.35	0.08	300	8.3%	16.4	2,633	3.5%	3	7	1.3	33.5	49.9	1.7	2.9	
JCD-EX3.2	3.0	22.2	1.06	4.62	13.21	0.08	0.35	0.08	244	9.0%	14.4	958	6.6%	3	7	1.8	8.9	23.3	2.9	4.8	
JCD-OS1A	5.2	38.1	2.88	12.60	36.00	0.08	0.35	0.08	247	4.0%	19.0	2,545	4.6%	3	7	1.5	28.3	47.2	1.8	3.0	
JCD-OS1B	4.6	33.6	1.66	7.25	20.70	0.08	0.35	0.08	200	8.5%	13.3	1,167	5.8%	3	7	1.7	11.5	24.8	2.8	4.6	BASINS JCD-EX3.1, JCD-EX3.2, JCD-OS1.A, & JCD-OS1.B
JCD-D	11.5	84.2	11.08	48.48	138.51	0.08	0.35	0.08	247	4.0%	19.0	4,881	3.8%	3	7	1.4	59.6	78.6	1.0	1.7	

Code	Description	K
1	Heavy meadow	2.5
2	Tillage/field	5
3	Short pasture and lawns	7
4	Nearly bare ground	10
5	Grassed waterway	15
6	Paved areas and shallow paved swales	20

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_i^{0.33}}$$

$$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$$

Computed $t_c = t_i + t_t$

$I_{100} = -2.52 \ln(D) + 12.735$
$I_{50} = -2.25 \ln(D) + 11.375$
$I_{25} = -2.00 \ln(D) + 10.111$
$I_{10} = -1.75 \ln(D) + 8.847$
$I_5 = -1.50 \ln(D) + 7.583$
$I_2 = -1.19 \ln(D) + 6.035$
<small>Note: Values calculated by equations may not precisely duplicate values read from figure.</small>

Only basin JCD-EX3.3 is tributary to Design Point A based on the narrative that BJDEX-14 presently flows over Powers Blvd; therefore total flows at design point A should match JCD-EX3.

Update the values on the narrative (pg 14). What should be stated in the narrative is that your calculated (2.6/19.1cfs) are less than what's calculated in Trails FDR (5.0/25.3 cfs); therefore, this verifies the Trails drainage system provides adequate capacity to route flows from basin JCD-EX3.3.

Similar type of statement should be noted in the developed condition to clearly verify the receiving off-site system has adequate capacity.

However, if DPA values (4.2/30.8) is based on diversion of BJDEX-14 to DP A due to future CDOT construction of Powers Blvd then update the comments section for DPA in this worksheet. Also provide a statement regarding this development's conformance with the receiving offsite system designed/constructed by Trails FDR.

PRE-DEVELOPMENT WEIGHTED CURVE NUMBER & RUNOFF COEFFICIENT CALCULATIONS

Waterview North

BASIN ID	Total Area (Ac.)	HSG A/B	% IMPERV	WEIGHTED RESULTANT VALUES			ca-equivalent		Initial Abstraction(Ia)
				CN	C ₅	C ₁₀₀	CA ₅	CA ₁₀₀	
<i>BJD-12a</i>	<i>54.28</i>	<i>A</i>	<i>0.0</i>	28.0	0.08	0.35	4.3424	19.00	2.571428571
<i>BJD-12b</i>	<i>9.54</i>	<i>A</i>	<i>0.0</i>	28.0	0.08	0.35	0.7632	3.34	2.571428571
<i>BJD-12c</i>	<i>18.23</i>	<i>A/B</i>	<i>0.0</i>	46	0.08	0.35	1.4584	6.38	1.173913043
<i>BJDEX-14</i>	<i>6.16</i>	<i>B</i>	<i>0.0</i>	46.0	0.08	0.35	0.4928	2.16	1.173913043
<i>JCD-OS1A</i>	<i>36.00</i>	<i>A</i>	<i>0.0</i>	28.0	0.08	0.35	2.88	12.60	2.571428571
<i>JCD-OS1B</i>	<i>20.70</i>	<i>A/B</i>	<i>0.0</i>	34.3	0.08	0.35	1.656	7.25	1.915451895
<i>JCDEX-3.1</i>	<i>68.60</i>	<i>A/B</i>	<i>0.0</i>	40.6	0.08	0.35	5.488	24.01	1.463054187
<i>JCDEX-3.2</i>	<i>13.21</i>	<i>B</i>	<i>0.0</i>	46.0	0.08	0.35	1.0568	4.62	1.173913043
<i>JCDEX-3.3</i>	<i>10.00</i>	<i>B</i>	<i>0.0</i>	46.0	0.08	0.35	0.8	3.50	1.173913043

Note: Antecedent Runoff Condition = 1, Runoff Coefficients referenced from Table 6-6, CNs referenced from Table 6-9 of the DCM.

Land Use ID	% Imp.	5-yr (C) HSG A & B	100-yr (C) HSG A & B	CN HSG A	CN HSG B
*Brush/Weed/Grass	0	0.08	0.35	28	46
INDUSTRIAL	80	0.59	0.7	81	88
COMMERCIAL	95	0.81	0.88	89	92
**RESIDENTIAL	80	0.6	0.68	82	90

* Offsite Basin land use is Pasture/Meadow For the Rational Analysis and Brush- brush weed grass for the UH Analysis - unless noted otherwise.

Length-Weighted Slope Calculations

Version 2.00 released May 2017

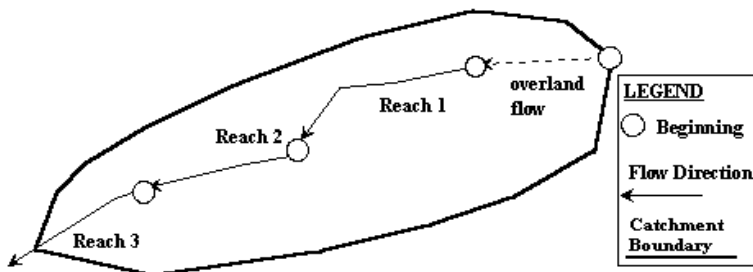
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12a	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	300.00	6054.00	6043.00	0.037
Total Overland Length (ft)		300.00	Length-Weighted Slope (ft/ft)	0.037

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	789.00	6043.00	6003.00	0.051
SC2	995.00	6003.00	5981.00	0.022
Total Channelized Length (ft)		1784.00	Length-Weighted Slope (ft/ft)	0.035

Length-Weighted Slope Calculations

Version 2.00 released May 2017

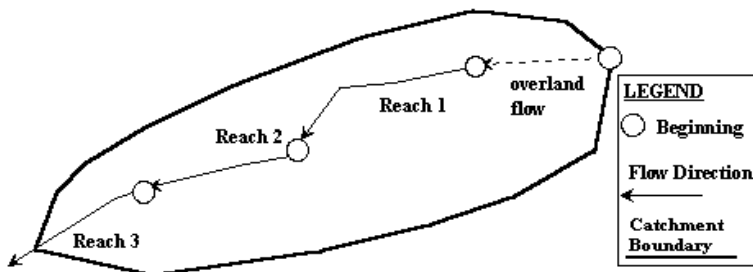
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12b	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	295.00	6018.30	6010.00	0.028
Total Overland Length (ft)	295.00	Length-Weighted Slope (ft/ft)		0.028

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	355.00	6010.00	5988.00	0.062
Total Channelized Length (ft)	355.00	Length-Weighted Slope (ft/ft)		0.062

Length-Weighted Slope Calculations

Version 2.00 released May 2017

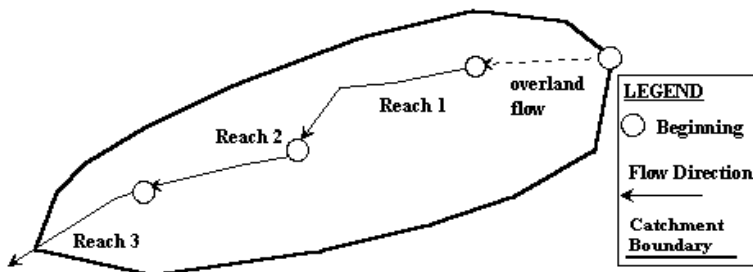
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12c	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	300.00	6000.00	5990.25	0.033
Total Overland Length (ft)		300.00	Length-Weighted Slope (ft/ft)	0.033

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	656.00	5990.25	5975.90	0.022
SC2	448.00	5975.90	5973.75	0.005
Total Channelized Length (ft)		1104.00	Length-Weighted Slope (ft/ft)	0.015

Length-Weighted Slope Calculations

Version 2.00 released May 2017

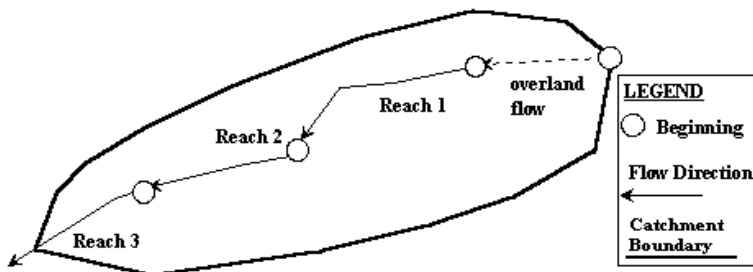
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJDEX-14	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	112.00			0.098
Total Overland Length (ft)		Length-Weighted Slope (ft/ft)		0.098

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	377.00			0.091
Total Channelized Length (ft)		Length-Weighted Slope (ft/ft)		0.091

Length-Weighted Slope Calculations

Version 2.00 released May 2017

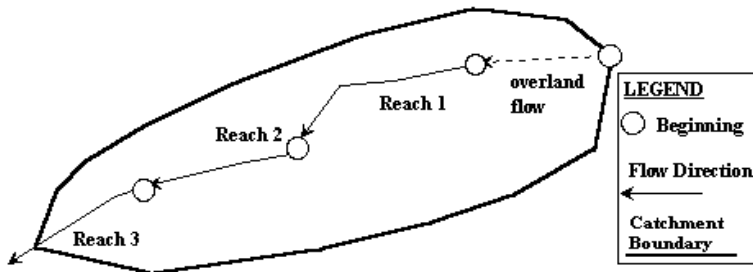
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD-EX3.1	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	300.00	5996.00	5971.00	0.083
Total Overland Length (ft)	300.00	Length-Weighted Slope (ft/ft)		0.083

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	899.00	5971.50	5930.50	0.046
SC2	1734.00	5930.50	5880.00	0.029
Total Channelized Length (ft)	2633.00	Length-Weighted Slope (ft/ft)		0.035

Length-Weighted Slope Calculations

Version 2.00 released May 2017

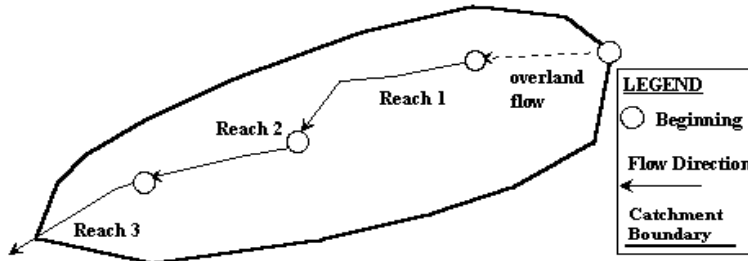
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEX3.2	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	244.00	5994.00	5972.00	0.090
Total Overland Length (ft)	244.00	Length-Weighted Slope (ft/ft)		0.090

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	985.00	5972.00	5908.00	0.065
Total Channelized Length (ft)	985.00	Length-Weighted Slope (ft/ft)		0.065

Length-Weighted Slope Calculations

Version 2.00 released May 2017

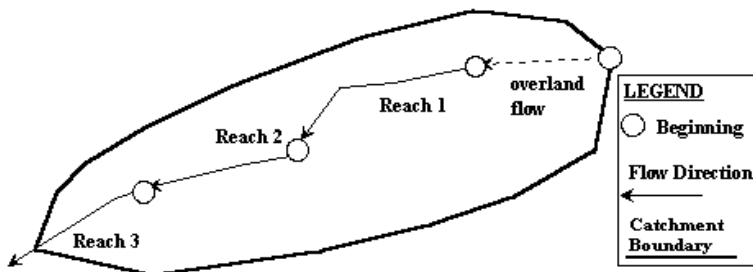
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/21/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD OS-1B	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	200.00	6013.50	6000.00	0.068
Total Overland Length (ft)		200.00	Length-Weighted Slope (ft/ft)	
			0.068	

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	1167.00	6000.00	5932.00	0.058
Total Channelized Length (ft)		1167.00	Length-Weighted Slope (ft/ft)	
			0.058	

Length-Weighted Slope Calculations

Version 2.00 released May 2017

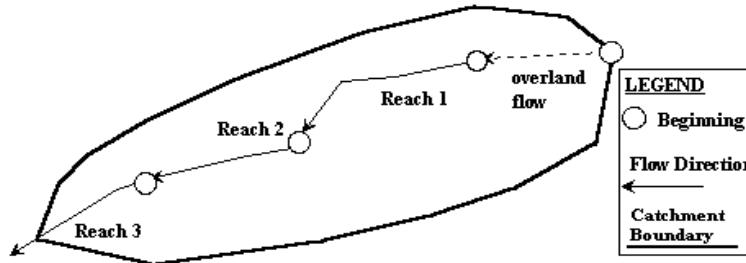
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD EX-3.3	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	297.00	5995.00	5960.00	0.118
Total Overland Length (ft)		297.00	Length-Weighted Slope (ft/ft)	0.118

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	398.00	5960.00	5930.00	0.075
Total Channelized Length (ft)		398.00	Length-Weighted Slope (ft/ft)	0.075

Length-Weighted Slope Calculations

Version 2.00 released May 2017

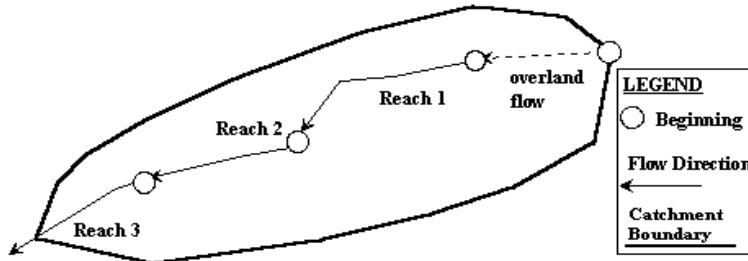
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD OS-1A	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	247.00	6076.00	6066.00	0.040
Total Overland Length (ft)	247.00	Length-Weighted Slope (ft/ft)		0.040

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	2545.00	6066.00	5950.00	0.046
Total Channelized Length (ft)	2545.00	Length-Weighted Slope (ft/ft)		0.046

PRE DEVELOPMENT RATIONAL ANALYSIS

WEIGHTED T_c CALCS

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

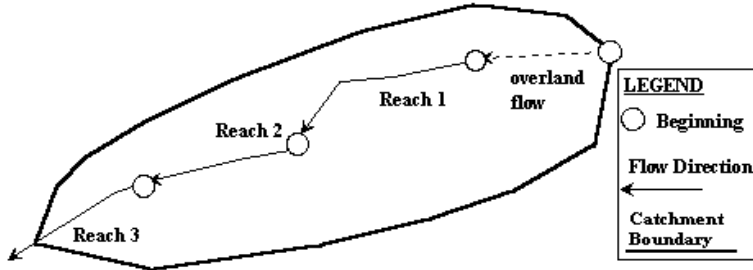
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12a	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	300.00	0.037	0.08	20.71
Weighted Totals	300.00	0.037	Total t_i (min)	20.71

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	789.00	0.051	7	8.32
SC-2	995.00	0.022	7	15.97
Weighted Totals	1784.00	0.035	Total t_i (min)	24.29

Computed t_c (min)	45.00
Regional t_c (min)	43.70
Selected t_c (min)	43.70

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

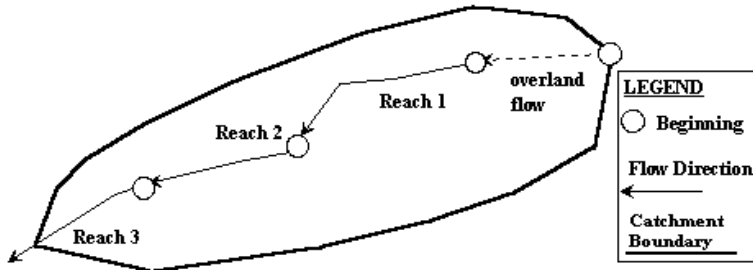
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12b	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	295.00	0.028	0.02	23.84
Weighted Totals	295.00	0.028	Total t_i (min)	23.84

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	355.00	0.062	7	3.39
Weighted Totals	355.00	0.062	Total t_i (min)	3.39

Computed t_c (min)	27.24
Regional t_c (min)	28.64
Selected t_c (min)	27.24

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

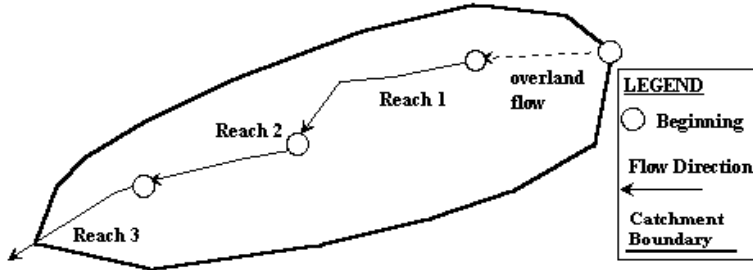
Designer: Chad Binder

Company: Dakota Springs Engineering

Date: 8/14/2020

Project: Waterview North

Location: NE Corner at Powers Blvd & Bradley Rd.



Subcatchment Name	Percent Imperviousness (%)
BJD-12c	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	300.00	0.330	0.08	10.08
Weighted Totals	300.00	0.330	Total t_i (min)	10.08

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	1104.00	0.015	7	21.46
Weighted Totals	1104.00	0.015	Total t_i (min)	21.46

Computed t_c (min)	31.54
Regional t_c (min)	42.69
Selected t_c (min)	31.54

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

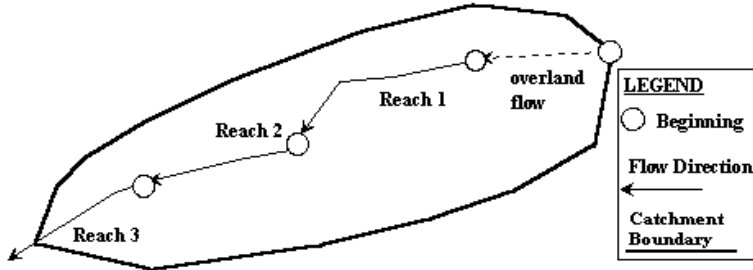
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJDEX14	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	112.00	0.098	0.08	9.18
Weighted Totals	112.00	0.098	Total t_i (min)	9.18

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	353.00	0.091	7	2.79
Weighted Totals	353.00	0.091	Total t_i (min)	2.79

Computed t_c (min)	11.96
Regional t_c (min)	28.17
Selected t_c (min)	11.96

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

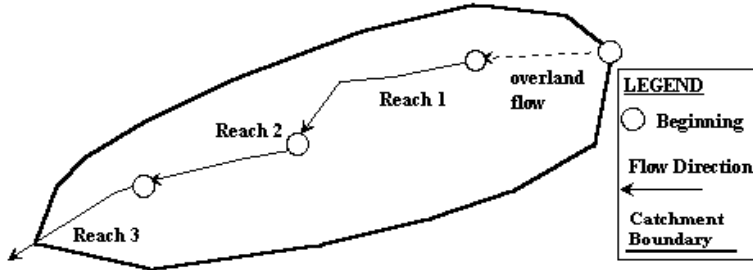
Designer: Chad Binder

Company: Dakota Springs Engineering

Date: 8/14/2020

Project: Waterview North

Location: NE Corner at Powers Blvd & Bradley Rd.



Subcatchment Name	Percent Imperviousness (%)
JCD OS-1A	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	247.00	0.040	0.02	19.39
Weighted Totals	247.00	0.040	Total t_i (min)	19.39

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	2545.00	0.045	7	28.56
Weighted Totals	2545.00	0.045	Total t_i (min)	28.56

Computed t_c (min)	47.96
Regional t_c (min)	48.22
Selected t_c (min)	47.96

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

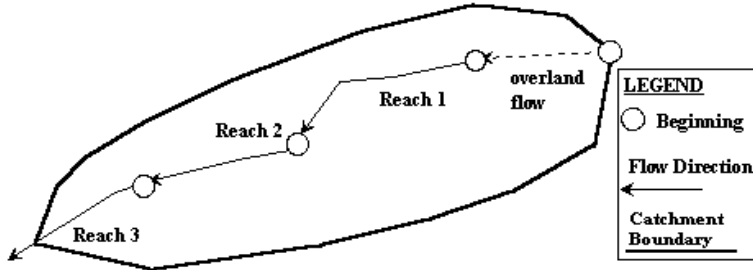
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/21/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD OS-1B	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	200.00	0.068	0.08	13.84
Weighted Totals	200.00	0.068	Total t_i (min)	13.84

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	1167.00	0.058	7	11.54
Weighted Totals	1167.00	0.058	Total t_i (min)	11.54

Computed t_c (min)	25.37
Regional t_c (min)	34.97
Selected t_c (min)	25.37

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

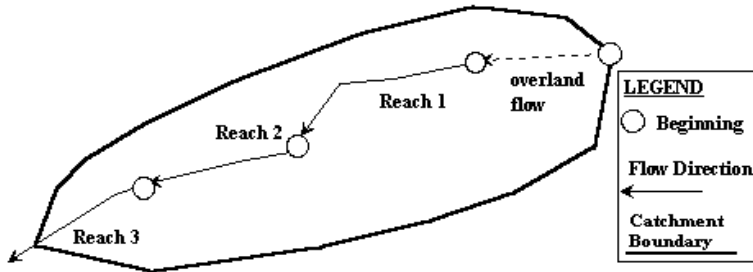
Designer: Chad Binder

Company: Dakota Springs Engineering

Date: 8/14/2020

Project: Waterview North

Location: NE Corner at Powers Blvd & Bradley Rd.



Subcatchment Name	Percent Imperviousness (%)
JCDEX3.1	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	300.00	0.083	0.08	15.87
Weighted Totals	300.00	0.083	Total t_i (min)	15.87

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	899.00	0.045	7	10.09
SC-2	1734.00	0.030	7	23.84
Weighted Totals	2633.00	0.035	Total t_i (min)	33.93

Computed t_c (min)	49.79
Regional t_c (min)	52.02
Selected t_c (min)	49.79

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

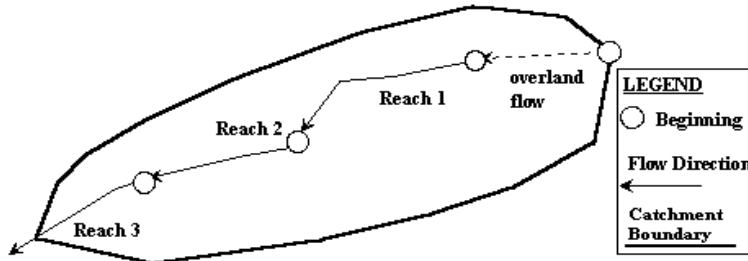
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEX-3.2	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	244.00	0.090	0.08	13.93
Weighted Totals	244.00	0.090	Total t_i (min)	13.93

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	958.00	0.066	7	8.88
Weighted Totals	958.00	0.066	Total t_i (min)	8.88

Computed t_c (min)	22.81
Regional t_c (min)	32.91
Selected t_c (min)	22.81

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

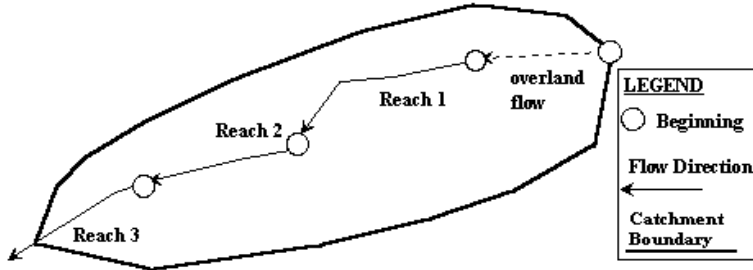
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/14/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEX3.3	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	297.00	0.118	0.08	14.06
Weighted Totals	297.00	0.118	Total t_i (min)	14.06

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	398.00	0.075	7	3.46
Weighted Totals	398.00	0.075	Total t_i (min)	3.46

Computed t_c (min)	17.52
Regional t_c (min)	28.69
Selected t_c (min)	17.52

POST DEVELOPMENT RATIONAL ANALYSIS
SUMMARY

WATERVIEW NORTH - POST DEVELOPMENT (RATIONAL METHOD Q=CIA)

BASIN	TOTAL FLOWS				AREA TOTAL (Ac)	WEIGHTED		OVERLAND				CHANNEL				Tc TOTAL (min)	INTENSITY		COMMENTS		
	Q(5) (c.f.s.)	Q(100) (c.f.s.)	CA(equiv.)			C(5)	C(100)	C(5)	Length (ft)	Slope (ft)	Ti (min)	Length (ft)	Slope (%)	Description Code	Convey Factor (K)		Velocity (fps)	Tt (min)		I(5) (in/hr)	I(100) (in/hr)
BJD-12a	8.3	60.6	4.34	19.00	54.28	0.08	0.35	0.08	300	3.7%	21.5	1,784	3.5%	3	7	1.3	22.7	44.2	1.9	3.2	
BJD-12b	2.0	14.8	0.76	3.34	9.54	0.08	0.35	0.08	295	2.8%	23.3	377	5.8%	3	7	1.7	3.7	27.1	2.6	4.4	Bypasses Pond BJD-K to DP-BJD-K
BJD-12c	37.2	74.1	10.76	12.76	18.23	0.59	0.70	0.59	100	2.5%	7.0	1,304	1.6%	6	20	2.5	8.6	15.6	3.5	5.8	
BJDEX-14	1.9	13.7	0.49	2.16	6.16	0.08	0.35	0.08	112	9.8%	9.5	377	9.1%	3	7	2.1	3.0	12.5	3.8	6.4	Route through JCD-DEV3.3 into Pond A
BJDEV-14	23.9	44.4	4.64	5.13	6.16	0.75	0.83	0.75	100	9.5%	3.1	366	8.5%	6	20	5.8	1.0	5.0	5.2	8.7	Future Condition - Qout to Big Johnson Res.
JCD-OS1A	5.2	38.1	2.88	12.60	36.00	0.08	0.35	0.08	247	4.0%	19.0	2,545	4.6%	3	7	1.5	28.3	47.2	1.8	3.0	
JCD-OS1B	4.5	32.9	1.66	7.25	20.70	0.08	0.35	0.08	200	6.8%	14.3	1,167	5.8%	3	7	1.7	11.5	25.9	2.7	4.5	
JCD-DEV3.1	137.2	272.6	41.16	48.71	68.60	0.60	0.71	0.60	100	7.5%	4.8	2,850	3.8%	6	20	3.9	12.2	17.0	3.3	5.6	
JCD-DEV3.2	35.6	67.8	7.93	8.98	13.21	0.60	0.68	0.60	100	10.9%	4.3	1,128	6.9%	6	20	5.3	3.6	7.8	4.5	7.5	
JCD-DEV3.3	38.2	70.9	7.60	8.40	10.00	0.76	0.84	0.76	100	6.7%	3.4	733	8.5%	6	20	5.8	2.1	5.5	5.0	8.4	To Pond A
Design Points																					
Pond A	38.2	83.7																			Pond A Tributary
DP A	1	17																			Pond A Qout (refer to pond calcs)
BJD-12b	2.0	14.8	0.76	3.34	9.54	0.08	0.35	0.08	295	2.8%	23.3	377	6.2%	3	7	1.7	3.6	26.9	2.6	4.4	Bypasses Pond BJD-K to DP-BJD-K
BJD-12c	37.2	74.1	10.76	12.76	18.23	0.59	0.70	0.59	100	2.5%	7.0	1,304	1.6%	6	20	2.5	8.6	15.6	3.5	5.8	Pond BJD-K Qin
BJD-K	1.0	9.0																			Pond BJD-K Qout (refer to pond calcs)
JCD-DEV3.1	137.2	272.6	41.16	48.71	68.60	0.60	0.71	0.60	100	7.5%	4.8	2,850	3.8%	6	20	3.9	12.2	17.0	3.3	5.6	
JCD-DEV3.2	35.6	67.8	7.93	8.98	13.21	0.60	0.68	0.60	100	10.9%	4.3	1,128	6.9%	6	20	5.3	3.6	7.8	4.5	7.5	
POND JCD-D	164	320	49.09	57.69	81.81	0.60	0.70	0.60	100	7.5%	4.8	2,850	3.8%	6	20	3.9	12.2	17.0	3.3	5.6	POND JCD-D Qin
JCD-OS1.A	5.2	38.1	2.88	12.60	36.00	0.08	0.35	0.08	247	4.0%	19.0	2,545	4.6%	3	7	1.5	28.3	47.2	1.8	3.0	Bypass Pond JCD-D to DP-JCD-D
JCD-OS1.B	4.6	33.6	1.66	7.25	20.70	0.08	0.35	0.08	200	8.5%	13.3	1,167	5.8%	3	7	1.7	11.5	24.8	2.8	4.6	Bypass Pond JCD-D to DP-JCD-D

Code	Description	K
1	Heavy meadow	2.5
2	Tillage/field	5
3	Short pasture and lawns	7
4	Nearly bare ground	10
5	Grassed waterway	15
6	Paved areas and shallow paved swales	20

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_i^{0.33}}$$

$$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$$

Computed $t_c = t_i + t_t$

$I_{100} = -2.52 \ln(D) + 12.735$
$I_{50} = -2.25 \ln(D) + 11.375$
$I_{25} = -2.00 \ln(D) + 10.111$
$I_{10} = -1.75 \ln(D) + 8.847$
$I_5 = -1.50 \ln(D) + 7.583$
$I_2 = -1.19 \ln(D) + 6.035$
<small>Note: Values calculated by equations may not precisely duplicate values read from figure.</small>

DP BJD-K represents flows going into the existing culvert. Narrative notes the pond outflow and bypass flow does not coincide with each other; therefore DP BJD-K peak flow should be the larger of the two flows which is BJD-12b. Update the narrative and drainage map values.

Provide calculations for Design Point JCD-D which is the cumulative flow from Pond Qout and the bypass flow.

POST DEVELOPMENT WEIGHTED CURVE NUMBER & RUNOFF COEFFICIENT CALCULATIONS

Waterview North

BASIN ID	Total Area (Ac.)	HSG A/B	% IMPERV	DESIGNATED LAND USE (% OF BASIN)			WEIGHTED RESULTANT VALUES			ca-equivalent		Initial Abstraction(Ia)
				I-2	COMMERCIAL	RESIDENTIAL	CN	C ₅	C ₁₀₀	CA ₅	CA ₁₀₀	
BJD-12a	54.28	A	0.0				68.0	0.08	0.35	4.3424	19.00	0.470588235
BJD-12b	9.54	A	0.0				68.0	0.08	0.35	0.7632	3.34	0.470588235
BJD-12c	18.23	A/B	80.0	18.23								
				1			88	0.59	0.7	10.7557	12.76	0.136363636
BJDEV-14	6.16	B	91.1	1.61	4.55							
				0.26	0.74		91.0	0.75	0.83	4.6354	5.13	0.098901099
JCD-OS1A	36.00	A	0.0				68.0	0.08	0.35	2.88	12.60	0.470588235
JCD-OS1B	20.70	A/B	0.0				71.9	0.08	0.35	1.656	7.25	0.391788448
JCDEV-3.1	68.60	A/B	82.2	8.36	6.86	53.98						
				0.12	0.10	0.79	90.7	0.6	0.71	42.877	48.60	0.102008032
JCDEV-3.2	13.21	B	80.0			13.21						
JCDEV-3.3	10.00	B	91.7			1.00						
					7.77	2.23	90.0	0.60	0.68	7.926	8.98	0.111111111
					0.78	0.22	91.6	0.76	0.84	7.6317	8.35	0.092251567

Note: Antecedent Runoff Condition = 2, Runoff Coefficients referenced from Table 6-6, CNs referenced from Table 6-10 of the DCM.

Land Use	% Imp.	5-yr (C)	100-yr (C)	CN	CN
ID		HSG A & B	HSG A & B	HSG A	HSG B
*Brush/Weed/Grass	0	0.08	0.35	68	79
INDUSTRIAL	80	0.59	0.7	81	88
COMMERCIAL	95	0.81	0.88	89	92
**RESIDENTIAL	80	0.6	0.68	82	90

* Offsite Basin land use is Pasture/Meadow For the Rational Analysis and Brush- brush weed grass for the UH Analysis - unless noted otherwise.

** Runoff Coefficients for residential were extrapolated from values shown on Table 6.6(8 units per acre) of the DCM to match proposed density (12 units per acre).

POST DEVELOPMENT RATIONAL ANALYSIS
WEIGHTED SLOPE CALCS

Length-Weighted Slope Calculations

Version 2.00 released May 2017

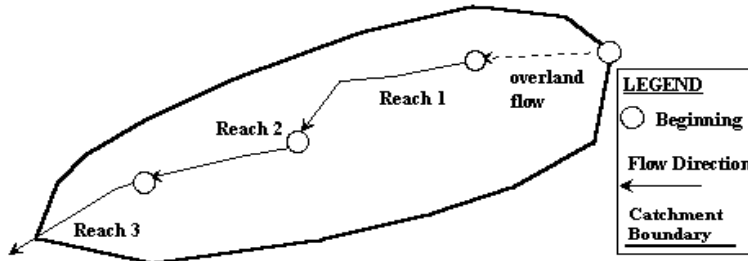
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12a	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	300.00	6054.00	6043.00	0.037
Total Overland Length (ft)		300.00	Length-Weighted Slope (ft/ft)	0.037

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	789.00	6043.00	6003.00	0.051
SC2	995.00	6003.00	5981.00	0.022
Total Channelized Length (ft)		1784.00	Length-Weighted Slope (ft/ft)	0.035

Length-Weighted Slope Calculations

Version 2.00 released May 2017

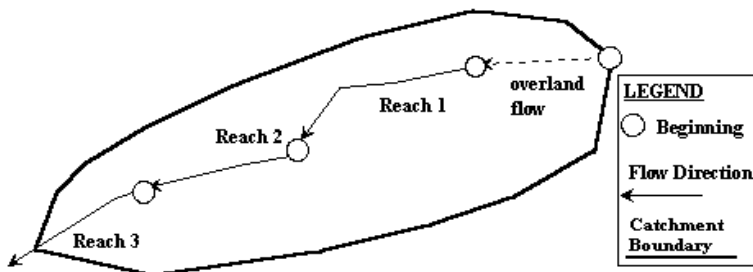
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12b	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	295.00	6018.30	6010.00	0.028
Total Overland Length (ft)	295.00	Length-Weighted Slope (ft/ft)		0.028

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	355.00	6010.00	5988.00	0.062
Total Channelized Length (ft)	355.00	Length-Weighted Slope (ft/ft)		0.062

Length-Weighted Slope Calculations

Version 2.00 released May 2017

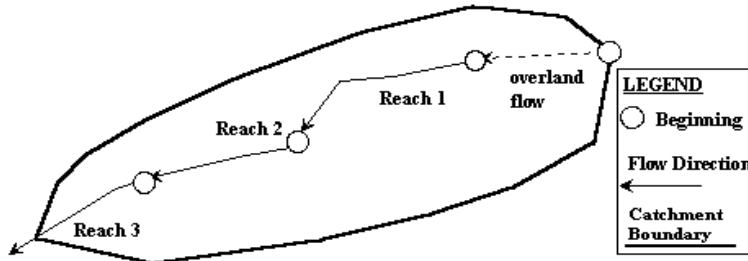
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12c	80

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	100.00	5999.50	5997.00	0.025
Total Overland Length (ft)		100.00	Length-Weighted Slope (ft/ft)	0.025

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	856.20	5997.00	5975.90	0.025
sc2	448.00	5975.90	5973.90	0.004
Total Channelized Length (ft)		1304.20	Length-Weighted Slope (ft/ft)	0.018

Length-Weighted Slope Calculations

Version 2.00 released May 2017

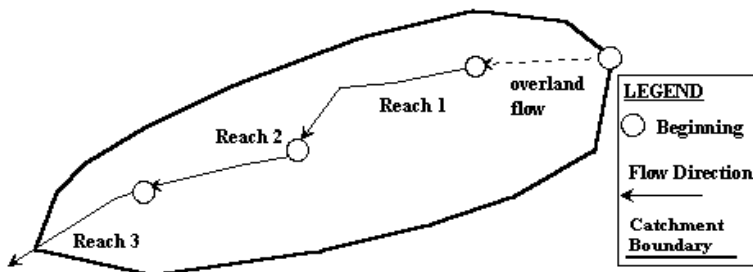
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJDEV-14	91.1

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	100.00	6002.50	5993.00	0.095
Total Overland Length (ft)	100.00	Length-Weighted Slope (ft/ft)		0.095

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	365.50	5993.00	5962.00	0.085
Total Channelized Length (ft)	365.50	Length-Weighted Slope (ft/ft)		0.085

Length-Weighted Slope Calculations

Version 2.00 released May 2017

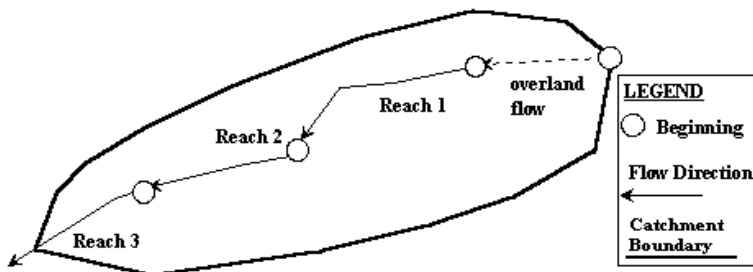
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV-3.1	82.2

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	100.00	5996.00	5988.50	0.075
Total Overland Length (ft)		Length-Weighted Slope (ft/ft)		
100.00		0.075		0.075

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	2850.00	5988.50	5879.30	0.038
Total Channelized Length (ft)		Length-Weighted Slope (ft/ft)		
2850.00		0.038		0.038

Length-Weighted Slope Calculations

Version 2.00 released May 2017

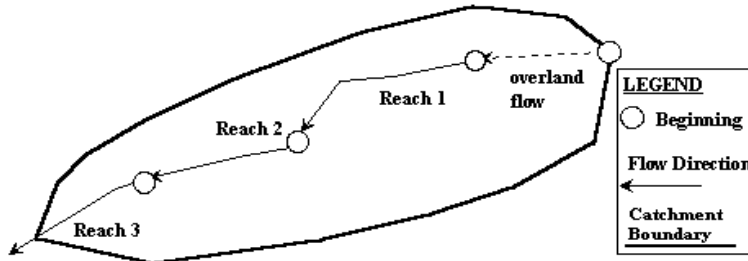
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV-3.2	80

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	100.00	5996.20	5985.30	0.109
Total Overland Length (ft)	100.00	Length-Weighted Slope (ft/ft)		0.109

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	1128.00	5985.30	5907.00	0.069
Total Channelized Length (ft)	1128.00	Length-Weighted Slope (ft/ft)		0.069

Length-Weighted Slope Calculations

Version 2.00 released May 2017

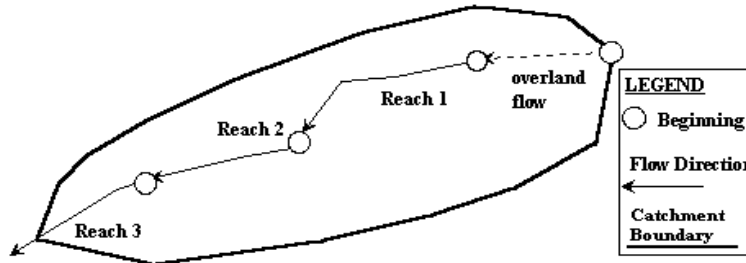
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/24/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV-3.3	91.7

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	100.00	5997.00	5990.30	0.067
Total Overland Length (ft)	100.00	Length-Weighted Slope (ft/ft)		0.067

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	409.20	5990.30	5952.75	0.092
SC1	323.40	5952.75	5928.00	0.077
Total Channelized Length (ft)	732.60	Length-Weighted Slope (ft/ft)		0.085

Length-Weighted Slope Calculations

Version 2.00 released May 2017

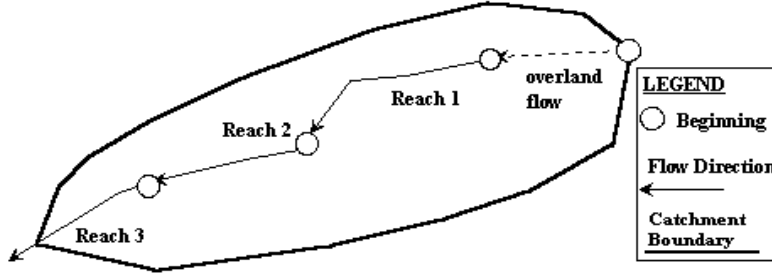
Designer: Chad Binder

Company: Dakota Springs Engineering

Date: 3/28/2020

Project: Waterview North

Location: NE Corner at Powers Blvd & Bradley Rd.



Subcatchment Name	Percent Imperviousness (%)
JCD-OS1A	5

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	247.00	6076.00	6066.00	0.040
Total Overland Length (ft)	247.00	Length-Weighted Slope (ft/ft)		0.040

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) <i>(Optional)</i>	D/S Elevation (ft) <i>(Optional)</i>	Channelized Flow Slope S_i (ft/ft)
SC1	2545.00	6066.00	5950.00	0.046
Total Channelized Length (ft)	2545.00	Length-Weighted Slope (ft/ft)		0.046

Length-Weighted Slope Calculations

Version 2.00 released May 2017

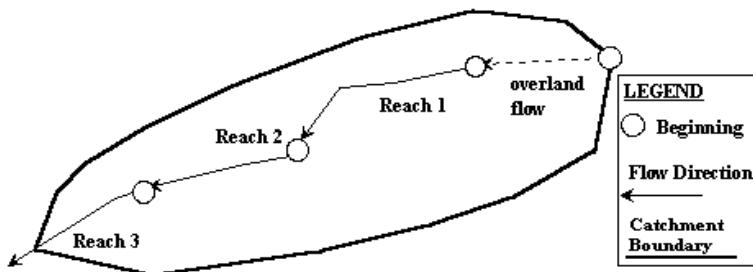
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD-OS1B	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)
OVERLAND FLOW	200.00	6013.50	6000.00	0.068
Total Overland Length (ft)		200.00	Length-Weighted Slope (ft/ft)	
			0.068	

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S_i (ft/ft)
SC1	1167.00	6000.00	5932.00	0.058
Total Channelized Length (ft)		1167.00	Length-Weighted Slope (ft/ft)	
			0.058	

POST DEVELOPMENT RATIONAL ANALYSIS

WEIGHTED T_c CALCS

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

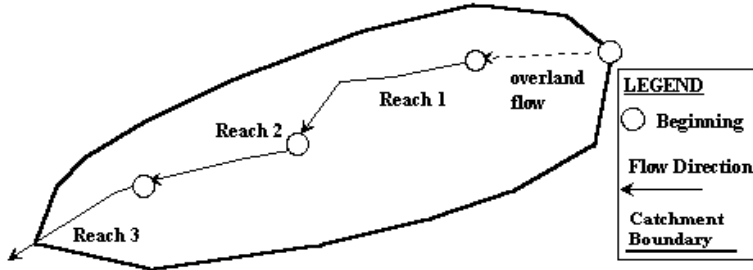
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12a	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	300.00	0.037	0.08	20.71
Weighted Totals	300.00	0.037	Total t_i (min)	20.71

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	789.00	0.049	7	8.49
SC-2	995.00	0.022	7	15.97
Weighted Totals	1784.00	0.034	Total t_i (min)	24.46

Computed t_c (min)	45.17
Regional t_c (min)	43.93
Selected t_c (min)	43.93

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

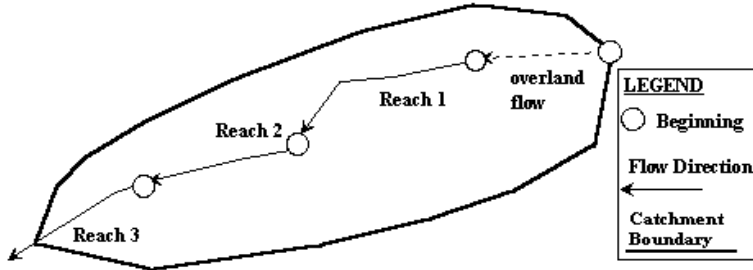
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12b	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	295.00	0.028	0.08	22.52
Weighted Totals	295.00	0.028	Total t_i (min)	22.52

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	355.00	0.062	7	3.39
Weighted Totals	355.00	0.062	Total t_i (min)	3.39

Computed t_c (min)	25.91
Regional t_c (min)	28.64
Selected t_c (min)	25.91

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

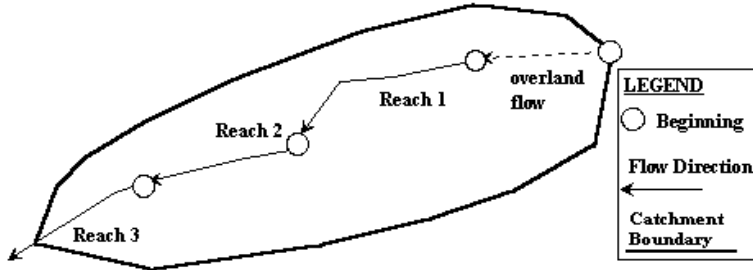
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJD-12c	80

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	100.00	0.025	0.59	6.81
Weighted Totals	100.00	0.025	Total t_i (min)	6.81

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	856.20	0.022	20	4.81
SC-2	448.00	0.004	10	11.81
Weighted Totals	1304.20	0.016	Total t_i (min)	16.62

Computed t_c (min)	23.42
Regional t_c (min)	20.96
Selected t_c (min)	20.96

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

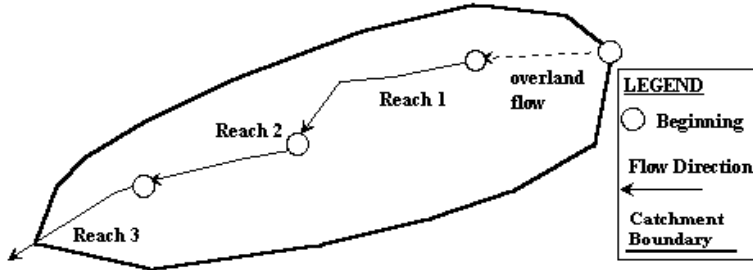
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
BJDEV-14	91.1

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	100.00	0.095	0.75	3.01
Weighted Totals	100.00	0.095	Total t_i (min)	3.01

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	365.50	0.085	20	1.04
Weighted Totals	365.50	0.085	Total t_i (min)	1.04

Computed t_c (min)	4.05
Regional t_c (min)	11.47
Selected t_c (min)	5.00

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

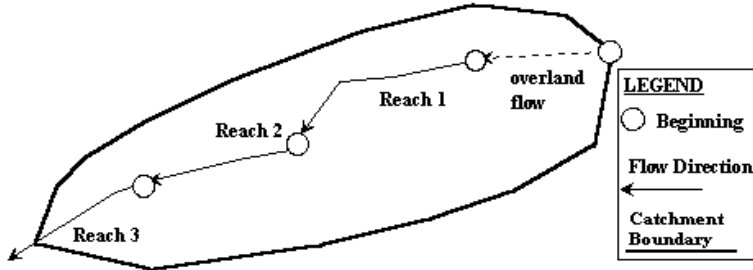
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/19/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV3.1	82.2

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	100.00	0.075	0.60	4.64
Weighted Totals	100.00	0.075	Total t_i (min)	4.64

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	2850.00	0.038	20	12.18
Weighted Totals	2850.00	0.038	Total t_i (min)	12.18

Computed t_c (min)	16.83
Regional t_c (min)	23.91
Selected t_c (min)	16.83

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

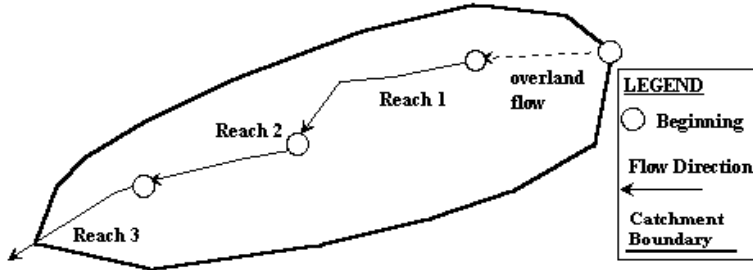
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV3.2	80

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_s	Overland Flow Time t_i (min)
OVERLAND FLOW	100.00	0.109	0.60	4.10
Weighted Totals	100.00	0.109	Total t_i (min)	4.10

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	1128.00	0.069	20	3.58
Weighted Totals	1128.00	0.069	Total t_i (min)	3.58

Computed t_c (min)	7.68
Regional t_c (min)	15.94
Selected t_c (min)	7.68

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

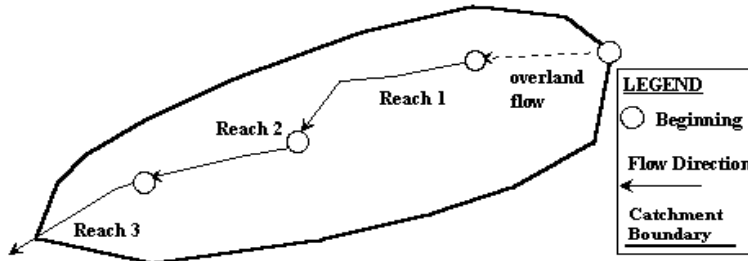
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/24/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCDEV3.3	91.7

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	100.00	0.067	0.76	3.28
Weighted Totals	100.00	0.067	Total t_i (min)	3.28

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	732.60	0.085	20	2.09
Weighted Totals	732.60	0.085	Total t_i (min)	2.09

Computed t_c (min)	5.37
Regional t_c (min)	12.33
Selected t_c (min)	5.37

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

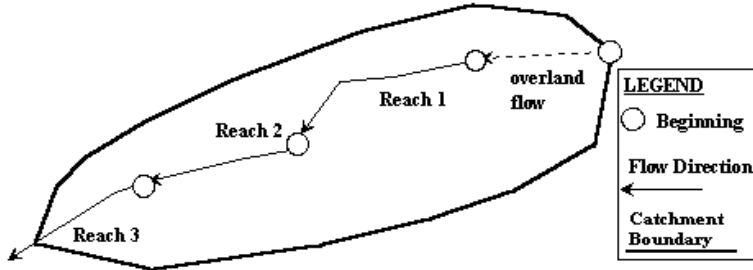
Designer: Chad Binder

Company: Dakota Springs Engineering

Date: 8/18/2020

Project: Waterview North

Location: NE Corner at Powers Blvd & Bradley Rd.



Subcatchment Name	Percent Imperviousness (%)
JCD-OS1A	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	247.00	0.040	0.08	18.32
Weighted Totals	247.00	0.040	Total t_i (min)	18.32

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	2545.00	0.046	7	28.25
Weighted Totals	2545.00	0.046	Total t_i (min)	28.25

Computed t_c (min)	46.57
Regional t_c (min)	47.97
Selected t_c (min)	46.57

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

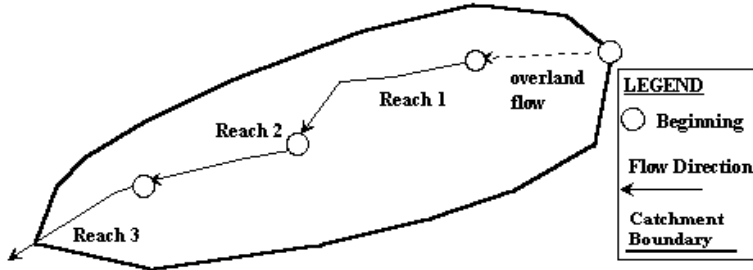
Designer: *Chad Binder*

Company: *Dakota Springs Engineering*

Date: *8/18/2020*

Project: *Waterview North*

Location: *NE Corner at Powers Blvd & Bradley Rd.*



Subcatchment Name	Percent Imperviousness (%)
JCD-OS1B	0

OVERLAND FLOW

Reach ID	Overland Flow Length L_i (ft)	Overland Flow Slope S_i (ft/ft)	5-yr Runoff Coefficient, C_5	Overland Flow Time t_i (min)
OVERLAND FLOW	200.00	0.068	0.08	13.84
Weighted Totals	200.00	0.068	Total t_i (min)	13.84

CHANNELIZED FLOW

Reach ID	Channelized Flow Length L_i (ft)	Channelized Flow Slope S_i (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Time t_i (min)
SC-1	1167.00	0.058	7	11.54
Weighted Totals	1167.00	0.058	Total t_i (min)	11.54

Computed t_c (min)	25.37
Regional t_c (min)	34.97
Selected t_c (min)	25.37

APPENDIX C

DETENTION CALCULATIONS

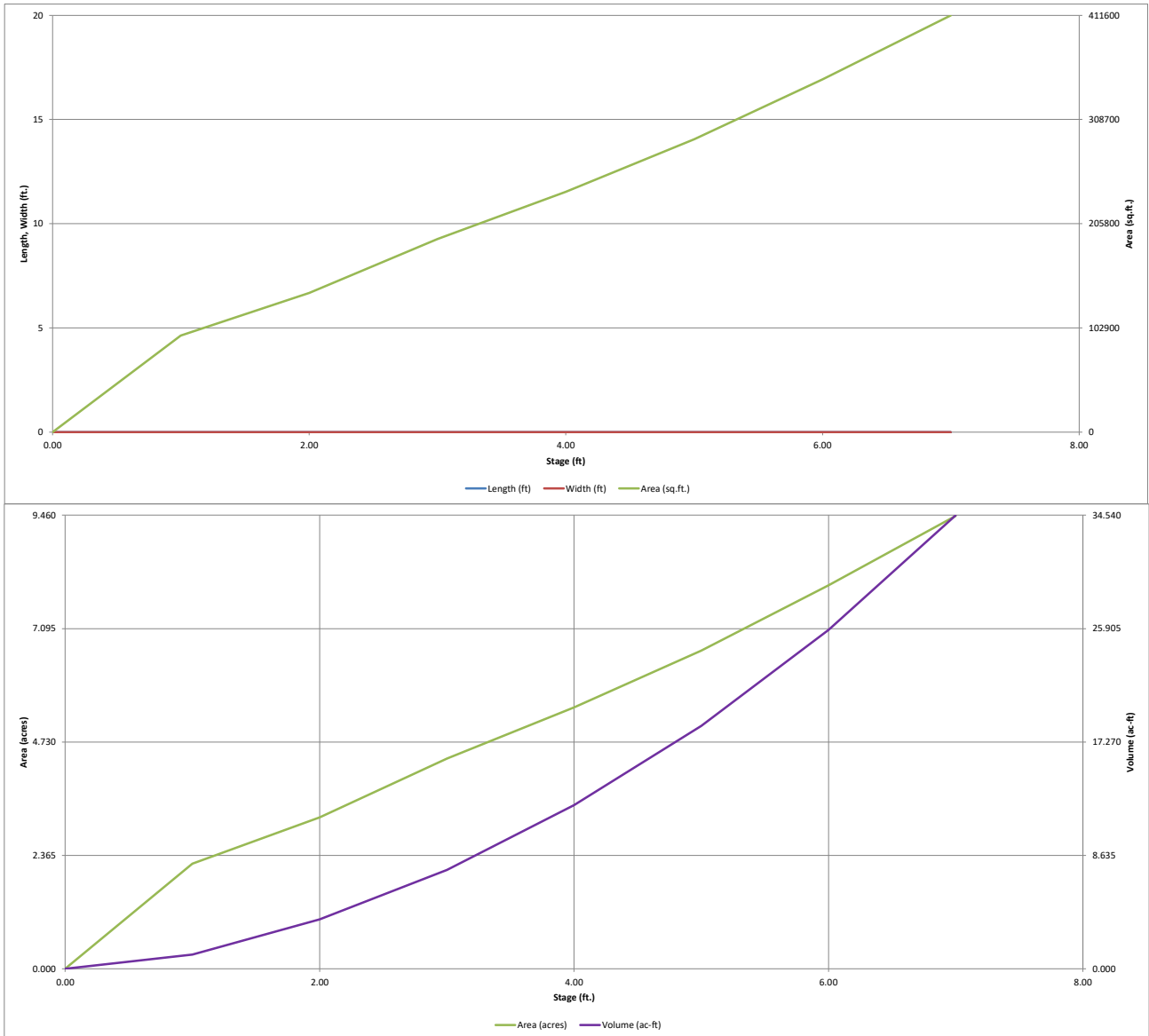
WATER QUALITY CALCULATIONS

EX. OFFSITE POND

FED BY OFFSITE BASIN BJD-12A

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.02 (February 2020)



POND DESIGN & ANALYSIS

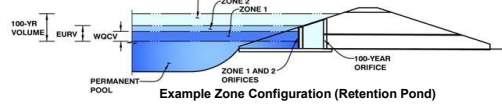
Proposed Pond BJD-K

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.02 (February 2020)

Project: **Waterview North**

Basin ID: **Pond BJD-K**



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB
Watershed Area =	18.23 acres
Watershed Length =	1,403 ft
Watershed Length to Centroid =	778 ft
Watershed Slope =	0.018 ft/ft
Watershed Imperviousness =	80.00% percent
Percentage Hydrologic Soil Group A =	17.3% percent
Percentage Hydrologic Soil Group B =	82.7% percent
Percentage Hydrologic Soil Groups C/D =	0.0% percent
Target WQCV Drain Time =	40.0 hours
Location for 1-hr Rainfall Depths =	User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.499 acre-feet
Excess Urban Runoff Volume (EURV) =	1.671 acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.422 acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.882 acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.257 acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.690 acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.084 acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.543 acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	4.535 acre-feet
Approximate 2-yr Detention Volume =	1.279 acre-feet
Approximate 5-yr Detention Volume =	1.681 acre-feet
Approximate 10-yr Detention Volume =	2.073 acre-feet
Approximate 25-yr Detention Volume =	2.261 acre-feet
Approximate 50-yr Detention Volume =	2.371 acre-feet
Approximate 100-yr Detention Volume =	2.509 acre-feet

Optional User Overrides

	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
	inches

Define Zones and Basin Geometry

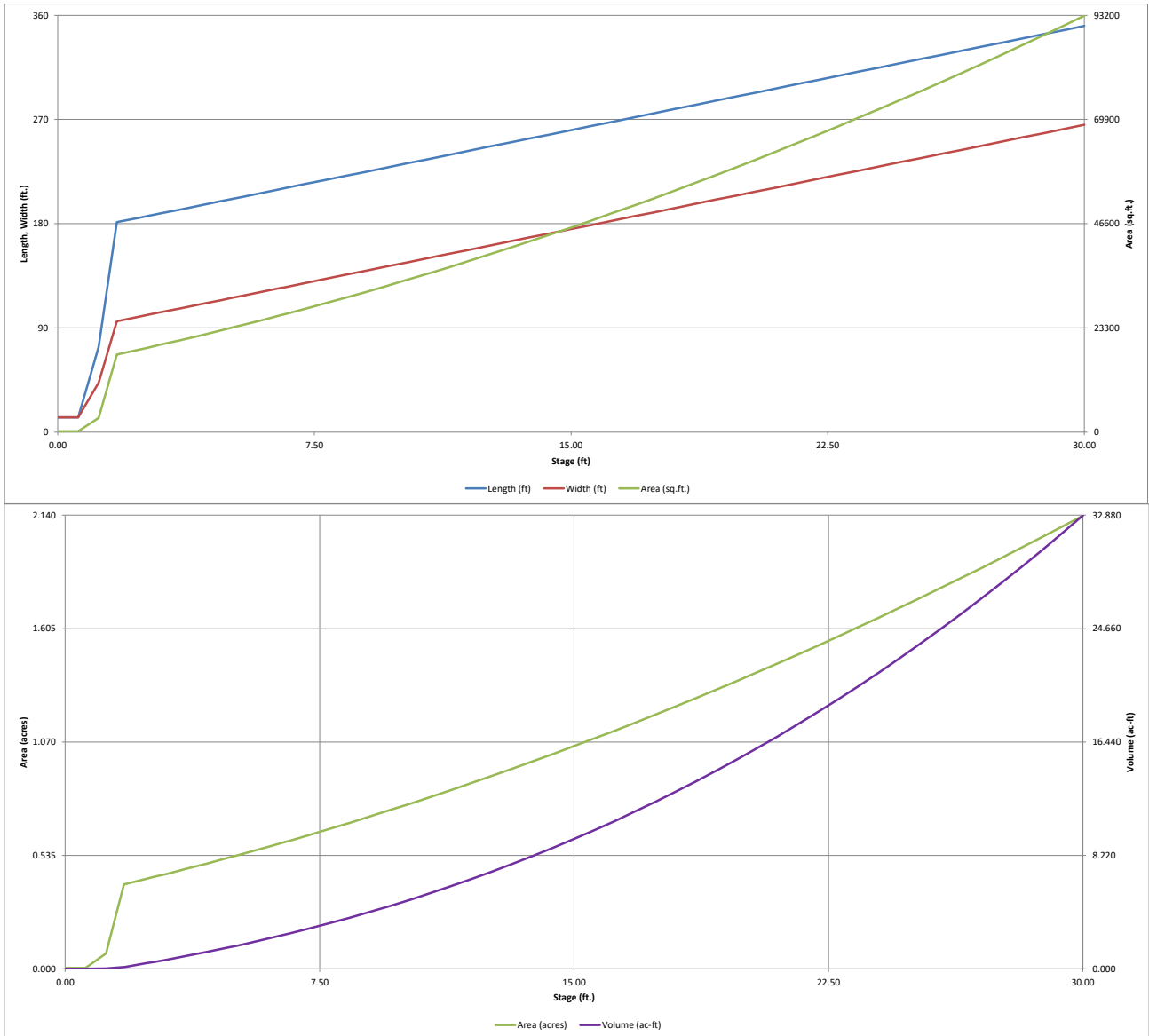
Zone 1 Volume (WQCV) =	0.499 acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.172 acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.838 acre-feet
Total Detention Basin Volume =	2.509 acre-feet
Initial Surcharge Volume (ISV) =	65 ft ³
Initial Surcharge Depth (ISD) =	0.40 ft
Total Available Detention Depth (H _{total}) =	6.50 ft
Depth of Trickle Channel (H _{TC}) =	0.50 ft
Slope of Trickle Channel (S _{TC}) =	0.005 ft/ft
Slopes of Main Basin Sides (S _{main}) =	3 H:V
Basin Length-to-Width Ratio (R _{LW}) =	2
Initial Surcharge Area (A _{ISV}) =	163 ft ²
Surcharge Volume Length (L _{ISV}) =	12.8 ft
Surcharge Volume Width (W _{ISV}) =	12.8 ft
Depth of Basin Floor (H _{FLOOR}) =	0.83 ft
Length of Basin Floor (L _{FLOOR}) =	181.3 ft
Width of Basin Floor (W _{FLOOR}) =	95.8 ft
Area of Basin Floor (A _{FLOOR}) =	17,358 ft ²
Volume of Basin Floor (V _{FLOOR}) =	5,313 ft ³
Depth of Main Basin (H _{MAIN}) =	4.77 ft
Length of Main Basin (L _{MAIN}) =	209.9 ft
Width of Main Basin (W _{MAIN}) =	124.4 ft
Area of Main Basin (A _{MAIN}) =	26,105 ft ²
Volume of Main Basin (V _{MAIN}) =	102,953 ft ³
Calculated Total Basin Volume (V _{total}) =	2,489 acre-feet

4.12

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool	0.00		12.8	12.8	163		0.004		
ISV	0.40		12.8	12.8	163		0.004	65	0.00150
	0.60		12.8	12.8	163		0.004	98	0.00224
	1.20		73.7	42.8	3,150		0.072	552	0.01268
Floor	1.73		181.3	95.8	17,358		0.398	5,483	0.12588
	1.80		181.7	96.2	17,474		0.401	6,702	0.15387
	2.40		185.3	99.8	18,488		0.424	17,490	0.40151
Zone 1 (WQCV)	2.63		186.7	101.2	18,883		0.433	21,787	0.50017
	3.00		188.9	103.4	19,527		0.448	28,893	0.66329
	3.60		192.5	107.0	20,592		0.473	40,927	0.93956
	4.20		196.1	110.6	21,683		0.498	53,608	1.23068
Zone 2 (EURV)	4.80		199.7	114.2	22,800		0.523	66,952	1.53701
	5.06		201.2	115.7	23,292		0.535	72,944	1.67456
	5.40		203.3	117.8	23,943		0.550	80,974	1.85890
	6.00		206.9	121.4	25,112		0.576	95,689	2.19671
Zone 3 (100-year)	6.53		210.1	124.6	26,166		0.601	109,276	2.50863
	6.60		210.5	125.0	26,306		0.604	111,113	2.55079
	7.20		214.1	128.6	27,527		0.632	127,261	2.92152
	7.80		217.7	132.2	28,773		0.661	144,150	3.30923
	8.40		221.3	135.8	30,046		0.690	161,795	3.71429
	9.00		224.9	139.4	31,344		0.720	180,210	4.13706
	9.60		228.5	143.0	32,669		0.750	199,413	4.57789
	10.20		232.1	146.6	34,019		0.781	219,418	5.03714
	10.80		235.7	150.2	35,395		0.813	240,241	5.51516
	11.40		239.3	153.8	36,797		0.845	261,897	6.01232
	12.00		242.9	157.4	38,225		0.878	284,402	6.52897
	12.60		246.5	161.0	39,679		0.911	307,772	7.06547
	13.20		250.1	164.6	41,159		0.945	332,022	7.62217
	13.80		253.7	168.2	42,664		0.979	357,167	8.19944
	14.40		257.3	171.8	44,196		1.015	383,224	8.79762
	15.00		260.9	175.4	45,754		1.050	410,208	9.41708
15.60		264.5	179.0	47,337		1.087	438,134	10.05817	
16.20		268.1	182.6	48,947		1.124	467,018	10.72125	
16.80		271.7	186.2	50,582		1.161	496,875	11.40668	
17.40		275.3	189.8	52,243		1.199	527,721	12.11481	
18.00		278.9	193.4	53,930		1.238	559,572	12.84600	
18.60		282.5	197.0	55,643		1.277	592,443	13.60061	
19.20		286.1	200.6	57,382		1.317	626,349	14.37900	
19.80		289.7	204.2	59,147		1.358	661,307	15.18151	
20.40		293.3	207.8	60,938		1.399	697,331	16.00852	
21.00		296.9	211.4	62,755		1.441	734,438	16.86037	
21.60		300.5	215.0	64,598		1.483	772,642	17.73743	
22.20		304.1	218.6	66,466		1.526	811,960	18.64004	
22.80		307.7	222.2	68,361		1.569	852,407	19.56857	
23.40		311.3	225.8	70,281		1.613	893,998	20.52338	
24.00		314.9	229.4	72,228		1.658	936,750	21.50482	
24.60		318.5	233.0	74,200		1.703	980,677	22.51324	
25.20		322.1	236.6	76,198		1.749	1,025,795	23.54901	
25.80		325.7	240.2	78,222		1.796	1,072,120	24.61248	
26.40		329.3	243.8	80,272		1.843	1,119,667	25.70402	
27.00		332.9	247.4	82,348		1.890	1,168,452	26.82396	
27.60		336.5	251.0	84,450		1.939	1,218,490	27.97269	
28.20		340.1	254.6	86,578		1.988	1,269,797	29.15054	
28.80		343.7	258.2	88,732		2.037	1,322,389	30.35788	
29.40		347.3	261.8	90,911		2.087	1,376,281	31.59506	
30.00		350.9	265.4	93,117		2.138	1,431,488	32.86244	

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

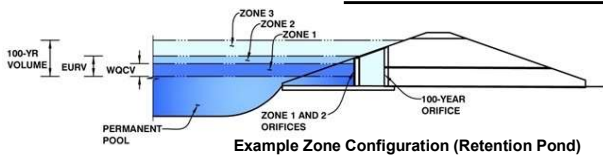
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention, Version 4.02 (February 2020)*

Project: Waterview North
Basin ID: Pond BJD-K



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.63	0.499	Orifice Plate
Zone 2 (EURV)	5.06	1.172	Orifice Plate
Zone 3 (100-year)	6.53	0.838	Weir&Pipe (Restrict)
Total (all zones)		2.509	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	5.00	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

Calculated Parameters for Plate

WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.00	3.00	3.75				
Orifice Area (sq. inches)	2.20	6.00	6.00	6.00				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice

	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft ²
Vertical Orifice Centroid =	N/A	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.53	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	8.00	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	5.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	% , grate open area/total area
Debris Clogging % =	0%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H _u =	7.78	N/A	feet
Overflow Weir Slope Length =	5.15	N/A	feet
Grate Open Area / 100-yr Orifice Area =	46.99	N/A	
Overflow Grate Open Area w/o Debris =	28.86	N/A	ft ²
Overflow Grate Open Area w/ Debris =	28.86	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	6.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.61	N/A	ft ²
Outlet Orifice Centroid =	0.29	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.05	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	8.52	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	18.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.91	feet
Stage at Top of Freeboard =	10.43	feet
Basin Area at Top of Freeboard =	0.79	acres
Basin Volume at Top of Freeboard =	5.22	acre-ft

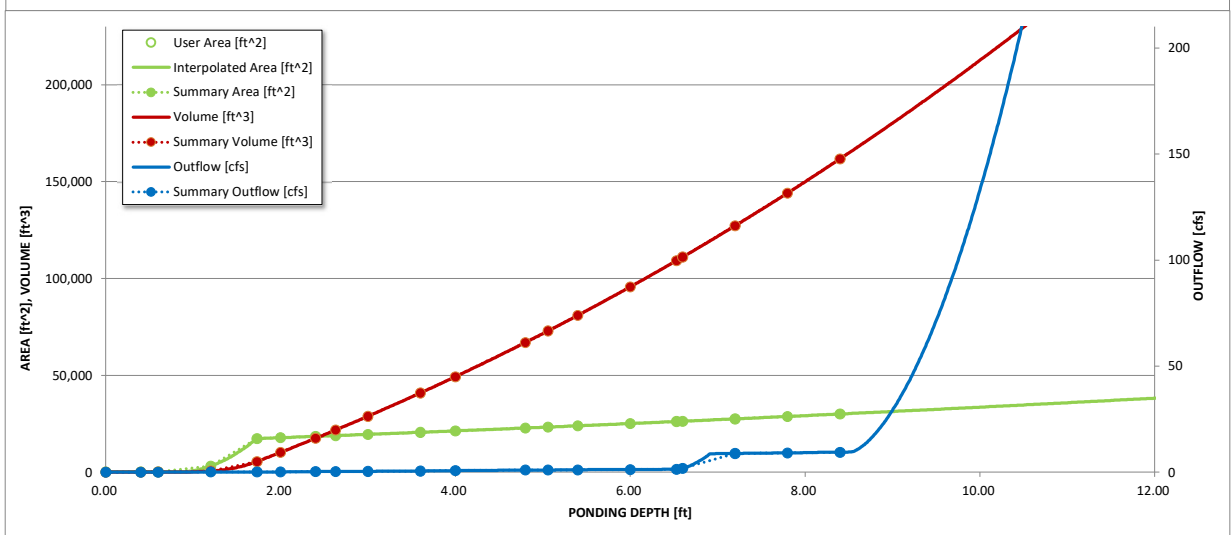
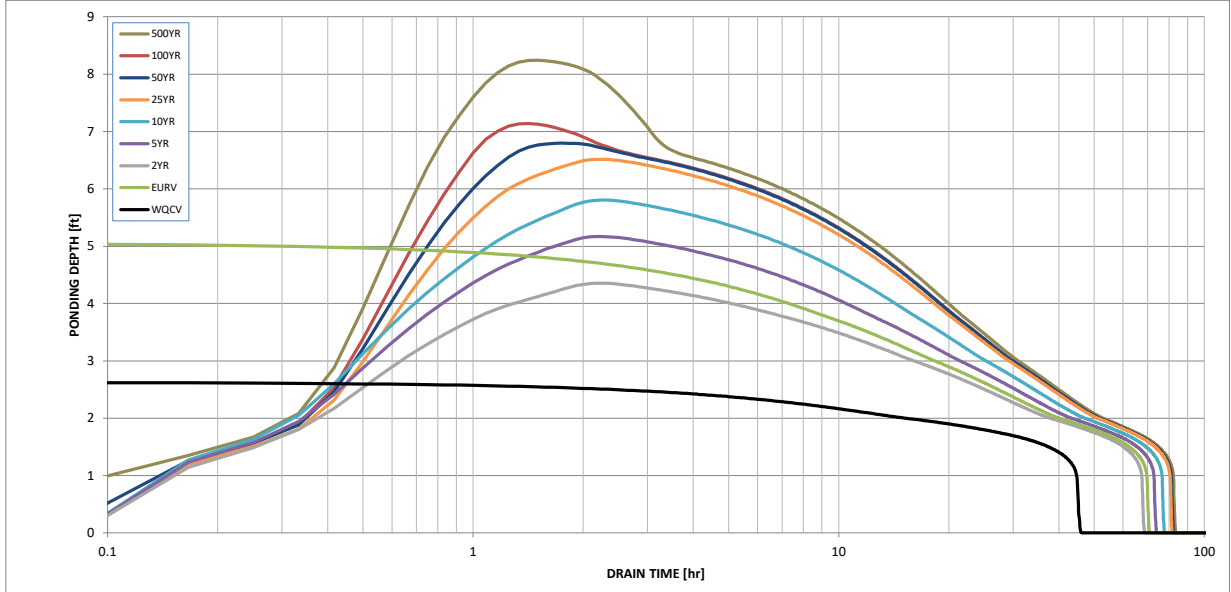
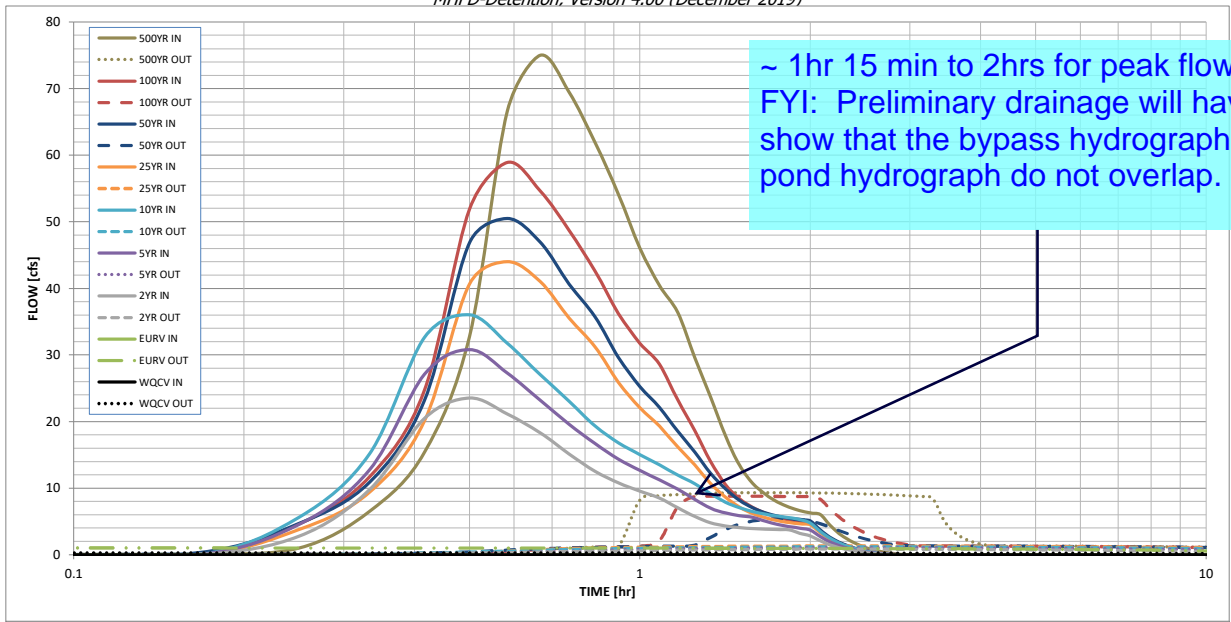
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
One-Hour Rainfall Depth (in) =	N/A	N/A	1.422	1.882	2.257	2.690	3.084	3.543	4.535
CUHP Runoff Volume (acre-ft) =	0.499	1.671	1.422	1.882	2.257	2.690	3.084	3.543	4.535
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.6	3.7	6.0	11.7	15.1	19.7	27.9
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.03	0.20	0.33	0.64	0.83	1.08	1.53
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.9	1.1	1.2	1.3	5.4	8.8	9.3
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.3	0.2	0.1	0.1	0.4	0.4	0.3
Peak Inflow Q (cfs) =	N/A	N/A	23.5	30.8	36.0	44.0	50.5	58.9	75.0
Peak Outflow Q (cfs) =	0.3	1.0	0.9	1.1	1.2	1.3	5.4	8.8	9.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.2	0.1	0.4	0.4	0.3
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	0.1	0.3	0.3
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	43	63	62	65	68	70	69	68	65
Time to Drain 99% of Inflow Volume (hours) =	45	68	66	71	74	77	77	77	76
Maximum Ponding Depth (ft) =	2.63	5.06	4.35	5.17	5.81	6.52	6.80	7.14	8.24
Area at Maximum Ponding Depth (acres) =	0.43	0.53	0.50	0.54	0.57	0.60	0.61	0.63	0.68
Maximum Volume Stored (acre-ft) =	0.500	1.675	1.306	1.734	2.082	2.497	2.666	2.877	3.605

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



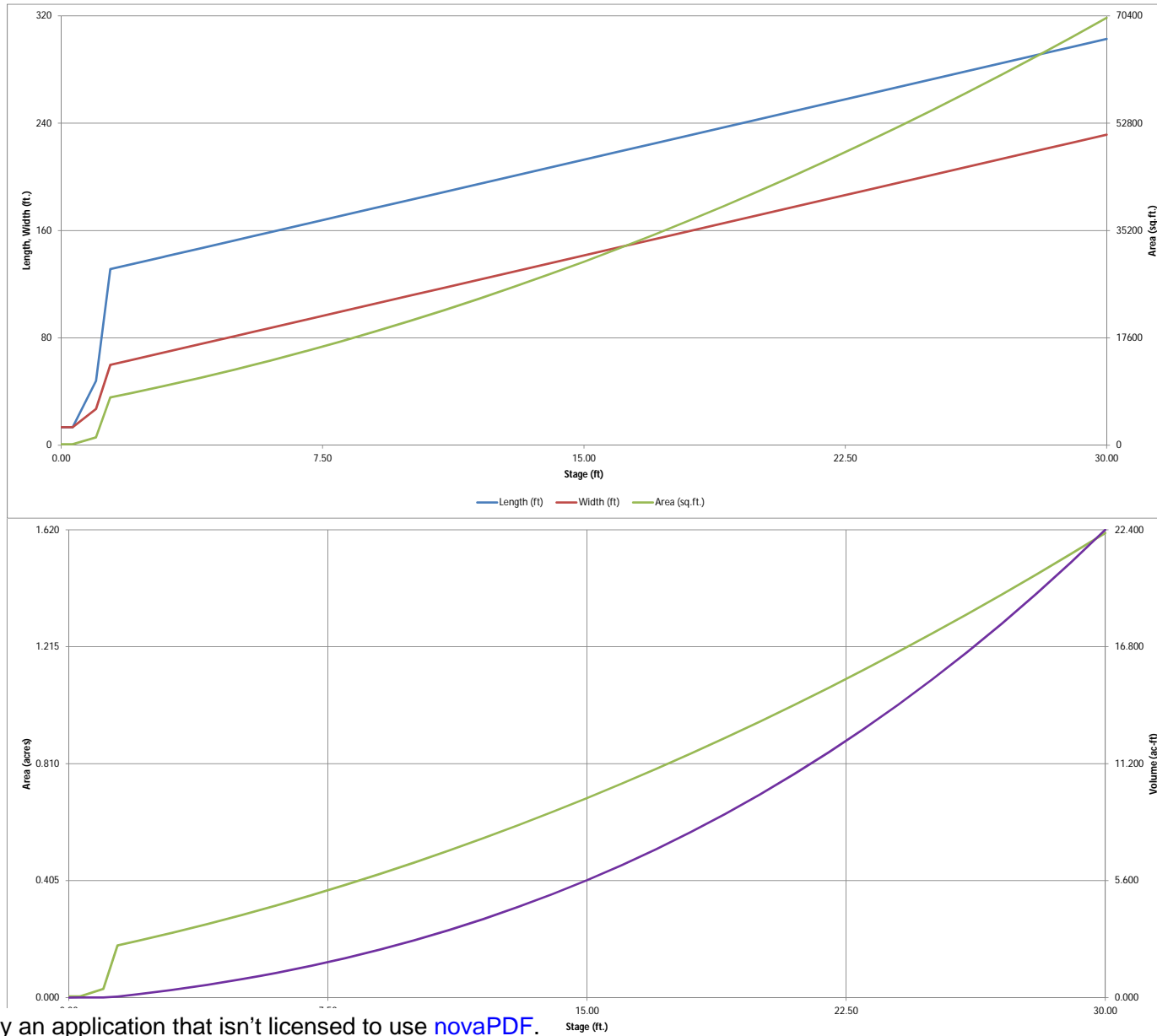
S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

POND DESIGN & ANALYSIS

Proposed Pond A

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

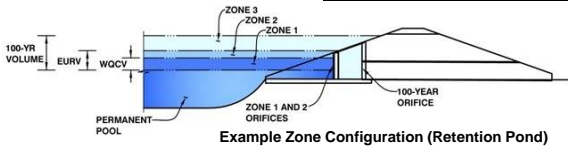
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: **Waterview North**
Basin ID: **Proposed Pond A**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.92	0.347	Orifice Plate
Zone 2 (EURV)	5.53	0.682	Orifice Plate
Zone 3 (100-year)	7.02	0.488	Weir&Pipe (Restrict)
Total (all zones)		1.517	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = 5.30 ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = N/A inches
Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parameters for Plate
WQ Orifice Area per Row = N/A ft²
Elliptical Half-Width = N/A feet
Elliptical Slot Centroid = N/A feet
Elliptical Slot Area = N/A ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50	2.25	3.00	4.00			
Orifice Area (sq. inches)	1.00	1.82	2.00	3.00	4.00			

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = N/A ft²
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.30	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	8.00	N/A	feet
Overflow Weir Gate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	3.50	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	0%	N/A	%

Calculated Parameters for Overflow Weir
Height of Gate Upper Edge, H₁ = 6.18 feet
Overflow Weir Slope Length = 3.61 feet
Gate Open Area / 100-yr Orifice Area = 15.16 ft²
Overflow Gate Open Area w/o Debris = 20.20 ft²
Overflow Gate Open Area w/ Debris = 20.20 ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	12.70		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = 1.33 ft²
Outlet Orifice Centroid = 0.59 feet
Half-Central Angle of Restrictor Plate on Pipe = 1.99 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 6.20 ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = 16.00 feet
Spillway End Slopes = 3.00 H:V
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = 0.89 feet
Stage at Top of Freeboard = 8.09 feet
Basin Area at Top of Freeboard = 0.39 acres
Basin Volume at Top of Freeboard = 1.92 acre-ft

Routed Hydrograph Results

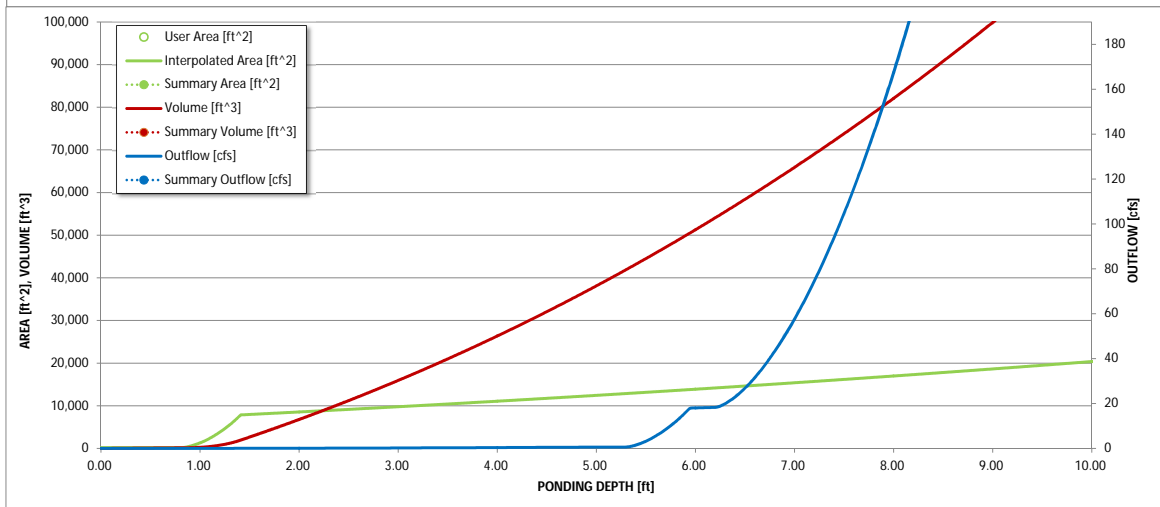
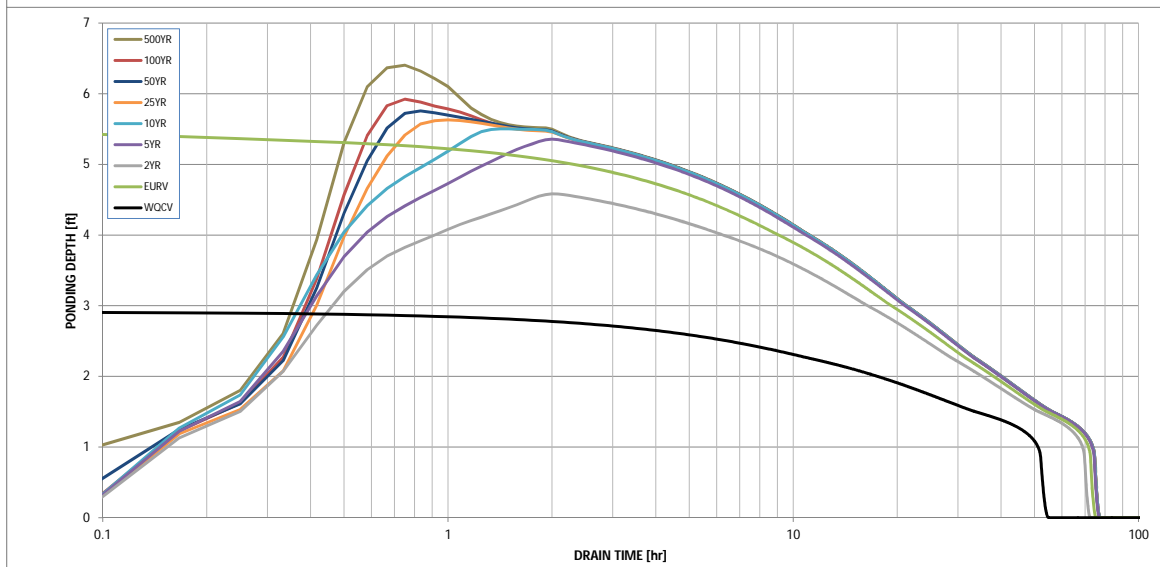
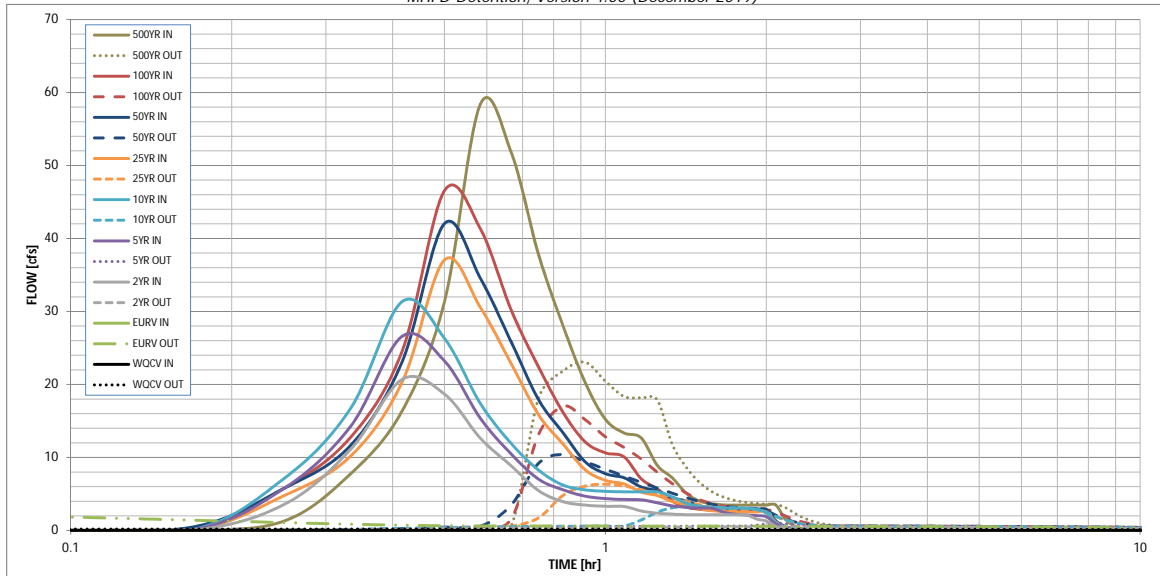
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period	N/A	N/A							
One-Hour Rainfall Depth (in)	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft)	0.347	1.029	0.818	1.062	1.260	1.465	1.666	1.887	2.386
Inflow Hydrograph Volume (acre-ft)	N/A	N/A	0.818	1.062	1.260	1.465	1.666	1.887	2.386
CUHP Predevelopment Peak Q (cfs)	N/A	N/A	1.7	4.7	7.2	12.2	15.2	19.0	26.5
OPTIONAL Override Predevelopment Peak Q (cfs)	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre)	N/A	N/A	0.17	0.47	0.72	1.22	1.52	1.90	2.65
Peak Inflow Q (cfs)	N/A	N/A	20.7	26.6	31.4	37.0	42.0	46.5	58.4
Peak Outflow Q (cfs)	0.2	3.0	0.5	1.0	3.3	6.3	10.4	17.0	23.0
Ratio Peak Outflow to Predevelopment Q	N/A	N/A	N/A	0.2	0.5	0.5	0.7	0.9	0.9
Structure Controlling Flow	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps)	N/A	0.16	N/A	0.0	0.1	0.3	0.5	0.8	0.9
Max Velocity through Grate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours)	50	64	63	65	63	62	60	58	54
Time to Drain 99% of Inflow Volume (hours)	52	70	68	72	72	71	70	69	68
Maximum Ponding Depth (ft)	2.92	5.53	4.58	5.36	5.50	5.63	5.76	5.92	6.40
Area at Maximum Ponding Depth (acres)	0.22	0.30	0.27	0.30	0.30	0.31	0.31	0.32	0.33
Maximum Volume Stored (acre-ft)	0.348	1.031	0.758	0.977	1.022	1.058	1.098	1.151	1.307

FYI: Final pond design will need this

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

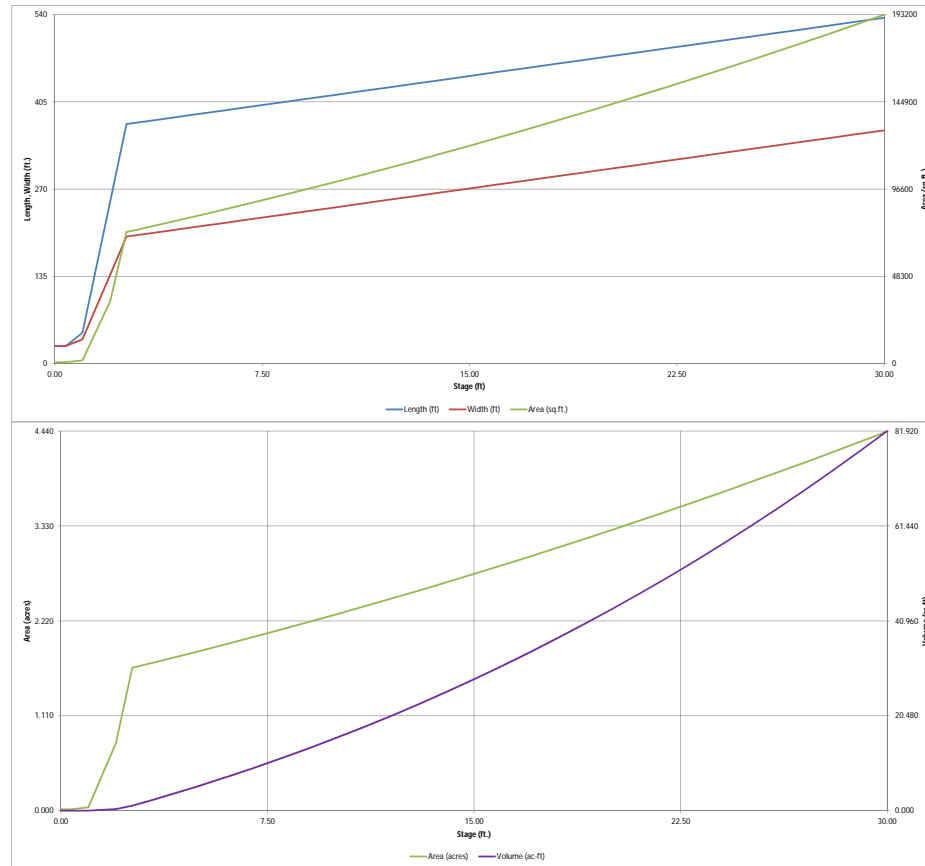
Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WOCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00_min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.04	1.26
	0:15:00	0.00	0.00	3.51	5.71	7.05	4.73	5.73	5.73	7.72
	0:20:00	0.00	0.00	11.06	14.20	16.66	10.14	11.60	12.72	16.37
	0:25:00	0.00	0.00	20.69	26.59	31.35	20.31	23.11	24.56	31.32
	0:30:00	0.00	0.00	18.68	23.22	26.33	37.05	42.03	46.54	58.37
	0:35:00	0.00	0.00	12.65	15.39	17.42	30.57	34.59	41.36	51.78
	0:40:00	0.00	0.00	8.85	10.46	11.91	22.84	25.81	30.18	37.78
	0:45:00	0.00	0.00	5.45	7.02	8.27	15.84	17.90	22.39	28.02
	0:50:00	0.00	0.00	3.95	5.57	6.21	11.84	13.38	16.18	20.26
	0:55:00	0.00	0.00	3.47	4.69	5.57	8.31	9.40	12.13	15.22
	1:00:00	0.00	0.00	3.31	4.37	5.36	6.87	7.78	10.63	13.36
	1:05:00	0.00	0.00	3.28	4.25	5.29	6.37	7.22	10.08	12.67
	1:10:00	0.00	0.00	2.67	4.19	5.28	5.25	5.96	7.07	8.92
	1:15:00	0.00	0.00	2.37	3.79	5.28	4.79	5.43	5.70	7.21
	1:20:00	0.00	0.00	2.24	3.36	4.62	3.96	4.49	4.03	5.09
	1:25:00	0.00	0.00	2.16	3.16	3.75	3.56	4.03	3.19	4.03
	1:30:00	0.00	0.00	2.15	3.07	3.34	2.98	3.37	2.90	3.66
	1:35:00	0.00	0.00	2.15	3.03	3.14	2.70	3.06	2.78	3.50
	1:40:00	0.00	0.00	2.15	2.48	3.06	2.60	2.94	2.76	3.48
	1:45:00	0.00	0.00	2.15	2.22	3.05	2.55	2.89	2.76	3.48
	1:50:00	0.00	0.00	2.15	2.11	3.05	2.54	2.88	2.76	3.48
	1:55:00	0.00	0.00	1.56	2.04	2.86	2.54	2.88	2.76	3.48
	2:00:00	0.00	0.00	1.28	1.88	2.42	2.54	2.88	2.76	3.48
	2:05:00	0.00	0.00	0.57	0.85	1.09	1.15	1.31	1.25	1.58
	2:10:00	0.00	0.00	0.22	0.36	0.45	0.49	0.56	0.53	0.67
	2:15:00	0.00	0.00	0.08	0.14	0.16	0.19	0.22	0.21	0.26
	2:20:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.03	0.04
	2:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

POND DESIGN & ANALYSIS

Proposed Pond JCD-D

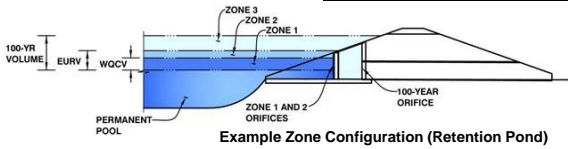
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN
MHFD-Detention, Version 4.02 (February 2020)

Project: **Waterview North**
Basin ID: **Pond JCD-D**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.33	2.317	Orifice Plate
Zone 2 (EURV)	6.11	5.124	Orifice Plate
Zone 3 (100-year)	7.98	3.812	Weir&Pipe (Restrict)
Total (all zones)		11.254	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = inches

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50	2.25	3.00	3.75	4.50	5.25	
Orifice Area (sq. inches)	7.20	7.20	7.20	7.20	7.20	7.20	10.00	

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>
Depth at top of Zone using Vertical Orifice =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>
Vertical Orifice Diameter =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>

ft (relative to basin bottom at Stage = 0 ft)
ft (relative to basin bottom at Stage = 0 ft)
inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>
Overflow Weir Front Edge Length =	<input type="text" value="16.00"/>	<input type="text" value="N/A"/>
Overflow Weir Gate Slope =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>
Horiz. Length of Weir Sides =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>
Overflow Gate Open Area % =	<input type="text" value="80%"/>	<input type="text" value="N/A"/>
Debris Clogging % =	<input type="text" value="0%"/>	<input type="text" value="N/A"/>

ft (relative to basin bottom at Stage = 0 ft)
feet
H:V
feet
%, gate open area/total area
%

Calculated Parameters for Overflow Weir
Height of Gate Upper Edge, H₁ = feet
Overflow Weir Slope Length = feet
Gate Open Area / 100-yr Orifice Area = ft²
Overflow Gate Open Area w/o Debris = ft²
Overflow Gate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	<input type="text" value="2.50"/>	<input type="text" value="N/A"/>
Outlet Pipe Diameter =	<input type="text" value="42.00"/>	<input type="text" value="N/A"/>
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="29.10"/>	<input type="text" value="N/A"/>

ft (distance below basin bottom at Stage = 0 ft)
inches
inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

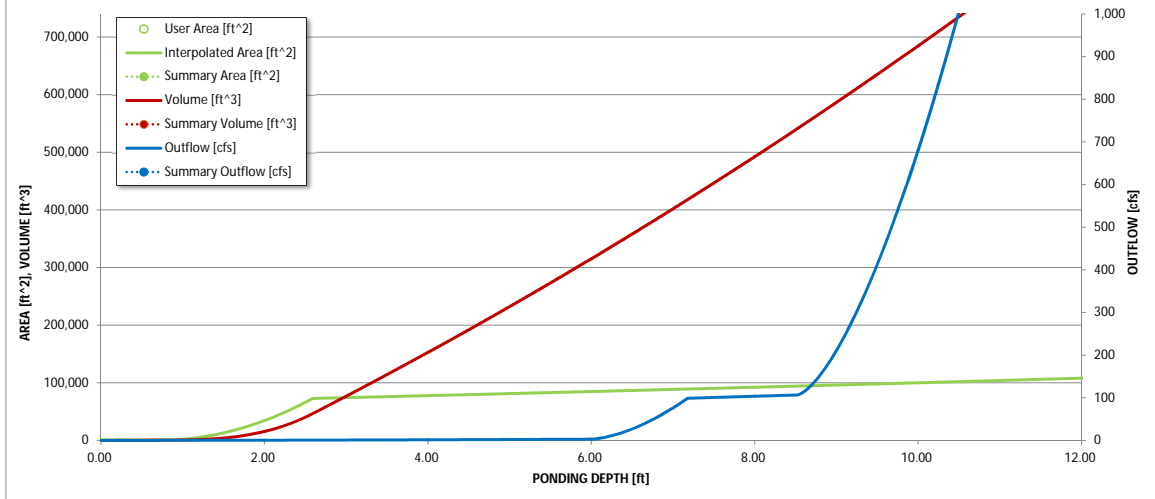
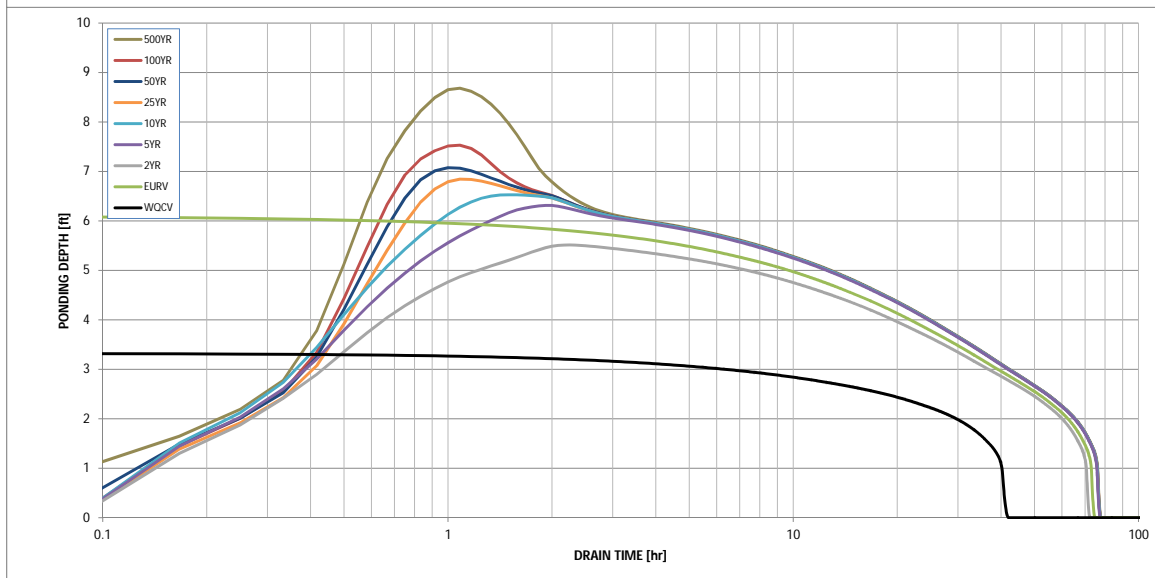
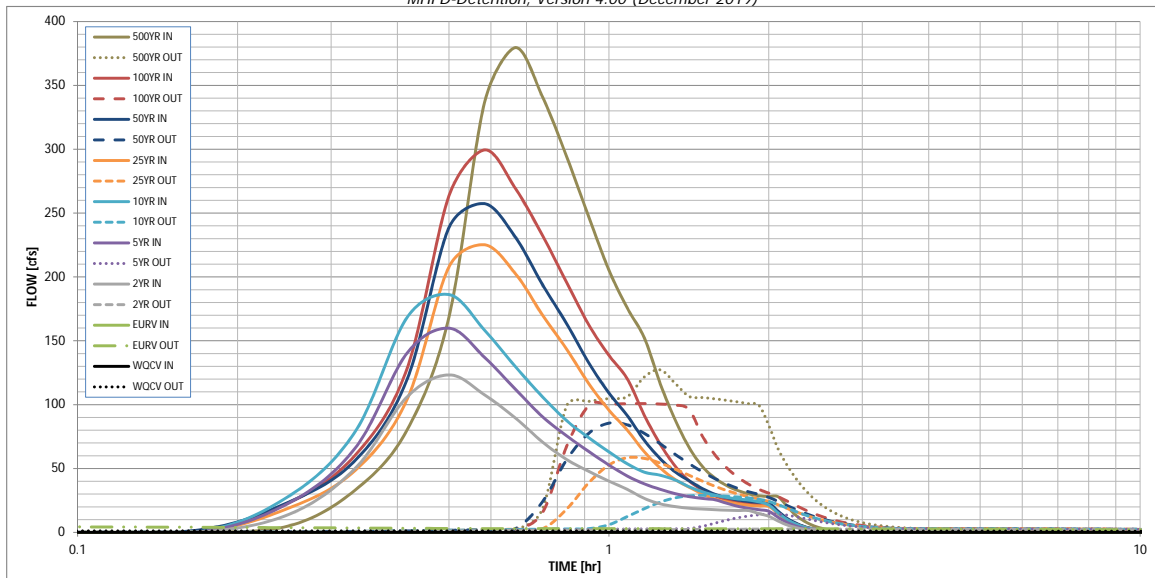
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A							
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	2.317	7.441	6.656	8.777	10.527	12.444	14.246	16.293	20.810
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	6.656	8.777	10.527	12.444	14.246	16.293	20.810
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	9.0	25.2	38.2	68.3	85.7	108.8	151.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.31	0.47	0.83	1.05	1.33	1.85
Peak Inflow Q (cfs) =	N/A	N/A	123.3	159.8	186.2	225.2	257.4	299.5	379.6
Peak Outflow Q (cfs) =	1.1	4.9	2.6	14.4	29.0	58.5	85.5	100.9	127.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	0.8	0.9	1.0	0.9	0.8
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	0.04	N/A	0.2	0.5	1.0	1.6	1.8	2.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	66	64	68	66	65	64	63	60
Time to Drain 99% of Inflow Volume (hours) =	40	71	69	73	72	72	71	71	69
Maximum Ponding Depth (ft) =	3.33	6.11	5.51	6.31	6.53	6.84	7.08	7.53	8.68
Area at Maximum Ponding Depth (acres) =	1.73	1.96	1.91	1.97	1.99	2.02	2.04	2.08	2.18
Maximum Volume Stored (acre-ft) =	2.327	7.449	6.290	7.842	8.258	8.900	9.367	10.313	12.760

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WOCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00_min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	1.59	0.16	5.10
	0:15:00	0.00	0.00	14.15	23.04	28.48	19.10	23.80	23.23	33.29
	0:20:00	0.00	0.00	50.26	66.23	79.11	48.68	56.50	60.59	79.89
	0:25:00	0.00	0.00	105.91	140.18	168.04	103.66	119.29	127.90	168.58
	0:30:00	0.00	0.00	123.28	159.84	186.20	207.81	238.54	263.41	336.48
	0:35:00	0.00	0.00	107.68	137.06	158.38	225.16	257.38	299.46	379.56
	0:40:00	0.00	0.00	89.60	112.13	129.83	202.69	231.19	269.44	341.03
	0:45:00	0.00	0.00	70.76	90.54	106.18	170.19	194.04	232.50	293.96
	0:50:00	0.00	0.00	56.99	75.53	87.41	143.28	163.24	195.41	247.01
	0:55:00	0.00	0.00	47.78	63.30	74.13	116.43	132.70	162.49	205.52
	1:00:00	0.00	0.00	40.13	52.78	63.03	95.75	109.25	138.74	175.60
	1:05:00	0.00	0.00	33.67	44.13	53.67	80.04	91.39	120.16	152.11
	1:10:00	0.00	0.00	26.55	37.95	47.15	62.99	71.96	91.54	116.20
	1:15:00	0.00	0.00	22.31	33.70	44.73	50.35	57.60	68.88	87.99
	1:20:00	0.00	0.00	20.20	30.32	41.00	41.34	47.29	51.83	66.34
	1:25:00	0.00	0.00	18.91	28.03	35.68	35.34	40.40	40.27	51.59
	1:30:00	0.00	0.00	18.23	26.54	31.75	30.05	34.31	33.19	42.54
	1:35:00	0.00	0.00	17.75	25.57	29.13	26.21	29.89	28.58	36.62
	1:40:00	0.00	0.00	17.40	22.78	27.34	23.87	27.20	25.54	32.72
	1:45:00	0.00	0.00	17.17	20.42	26.13	22.25	25.33	23.52	30.14
	1:50:00	0.00	0.00	17.07	18.85	25.28	21.23	24.16	22.37	28.66
	1:55:00	0.00	0.00	14.71	17.77	23.89	20.66	23.49	21.97	28.12
	2:00:00	0.00	0.00	12.62	16.54	21.45	20.30	23.08	21.79	27.88
	2:05:00	0.00	0.00	8.89	11.73	15.12	14.57	16.56	15.73	20.13
	2:10:00	0.00	0.00	5.81	7.66	9.98	9.59	10.90	10.40	13.30
	2:15:00	0.00	0.00	3.79	4.96	6.55	6.36	7.22	6.89	8.81
	2:20:00	0.00	0.00	2.36	3.09	4.13	4.03	4.58	4.37	5.58
	2:25:00	0.00	0.00	1.39	1.92	2.53	2.52	2.87	2.73	3.49
	2:30:00	0.00	0.00	0.73	1.12	1.42	1.48	1.68	1.61	2.05
	2:35:00	0.00	0.00	0.31	0.53	0.64	0.72	0.81	0.77	0.99
	2:40:00	0.00	0.00	0.10	0.16	0.18	0.22	0.25	0.24	0.30
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

APPENDIX D

CULVERT ANALYSES

**HY-8 Culvert Analysis Report
Ex. 10x6 RCBC Xing under
Powers Blvd.**

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 50 cfs

Design Flow: 98 cfs

Maximum Flow: 250 cfs

Flows at Crossing: Powers Blvd - Ex.10'x6' RCBC

<i>Headwater Elevation (ft)</i>	<i>Total Discharge (cfs)</i>	<i>Culvert 1 Discharge (cfs)</i>	<i>Roadway Discharge (cfs)</i>	<i>Iterations</i>
5974.65	50.00	50.00	0.00	1
5975.00	70.00	70.00	0.00	1
5975.44	98.00	98.00	0.00	1
5975.62	110.00	110.00	0.00	1
5975.90	130.00	130.00	0.00	1
5976.16	150.00	150.00	0.00	1
5976.43	170.00	170.00	0.00	1
5976.68	190.00	190.00	0.00	1
5976.92	210.00	210.00	0.00	1
5977.15	230.00	230.00	0.00	1
5977.38	250.00	250.00	0.00	1
5984.00	798.03	798.03	0.00	<i>Overtopping</i>

Rating Curve Plot for Crossing: Powers Blvd - Ex.10'x6' RCBC

Total Rating Curve
Crossing: Powers Blvd - Ex.10'x6' RCBC

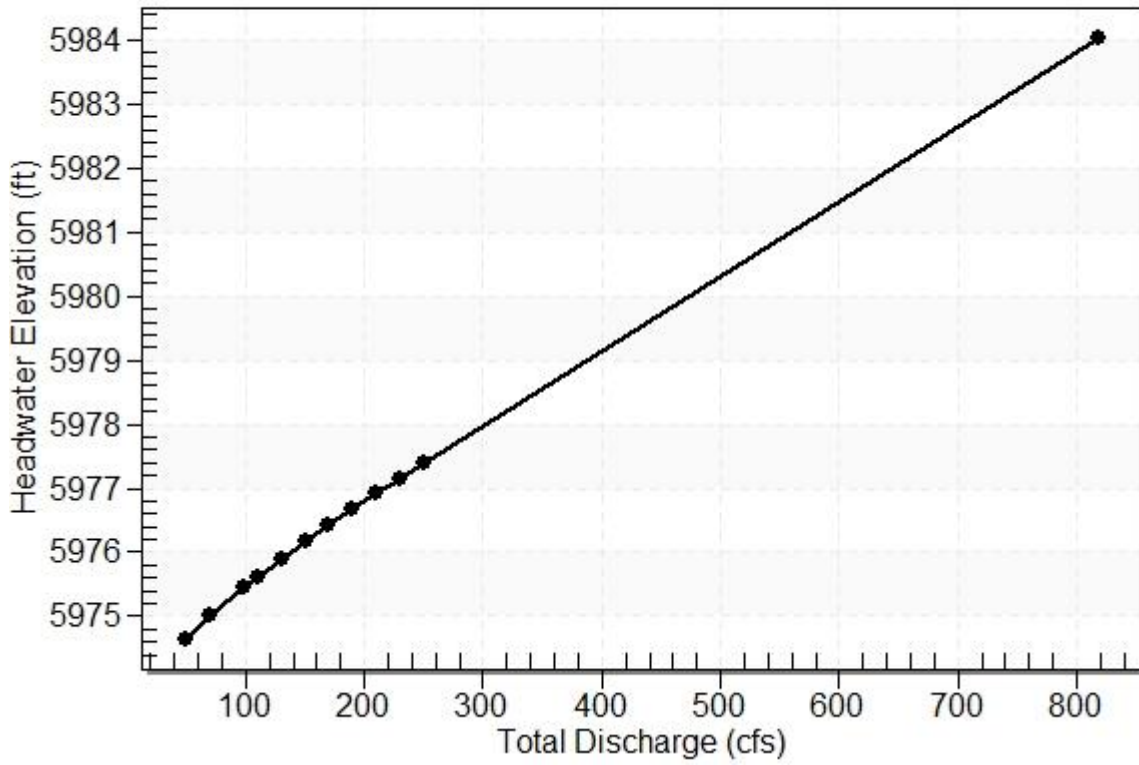
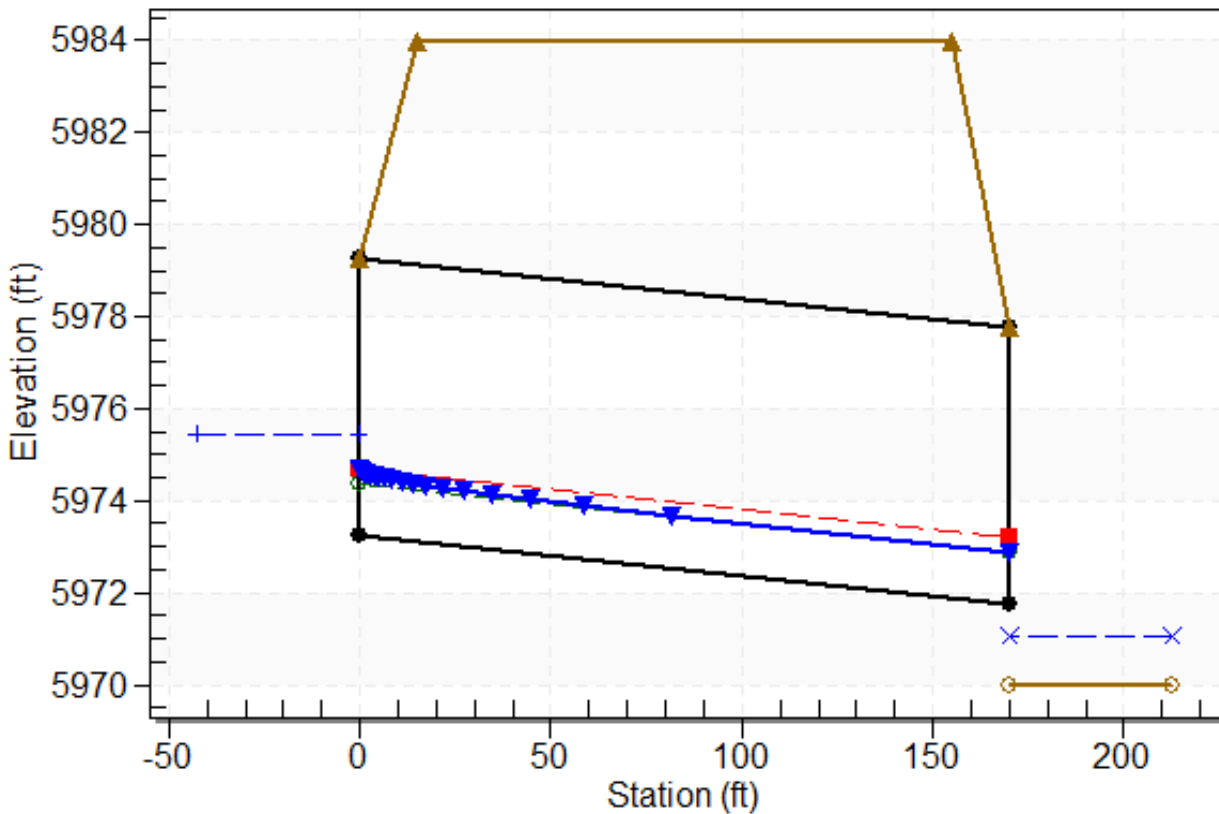
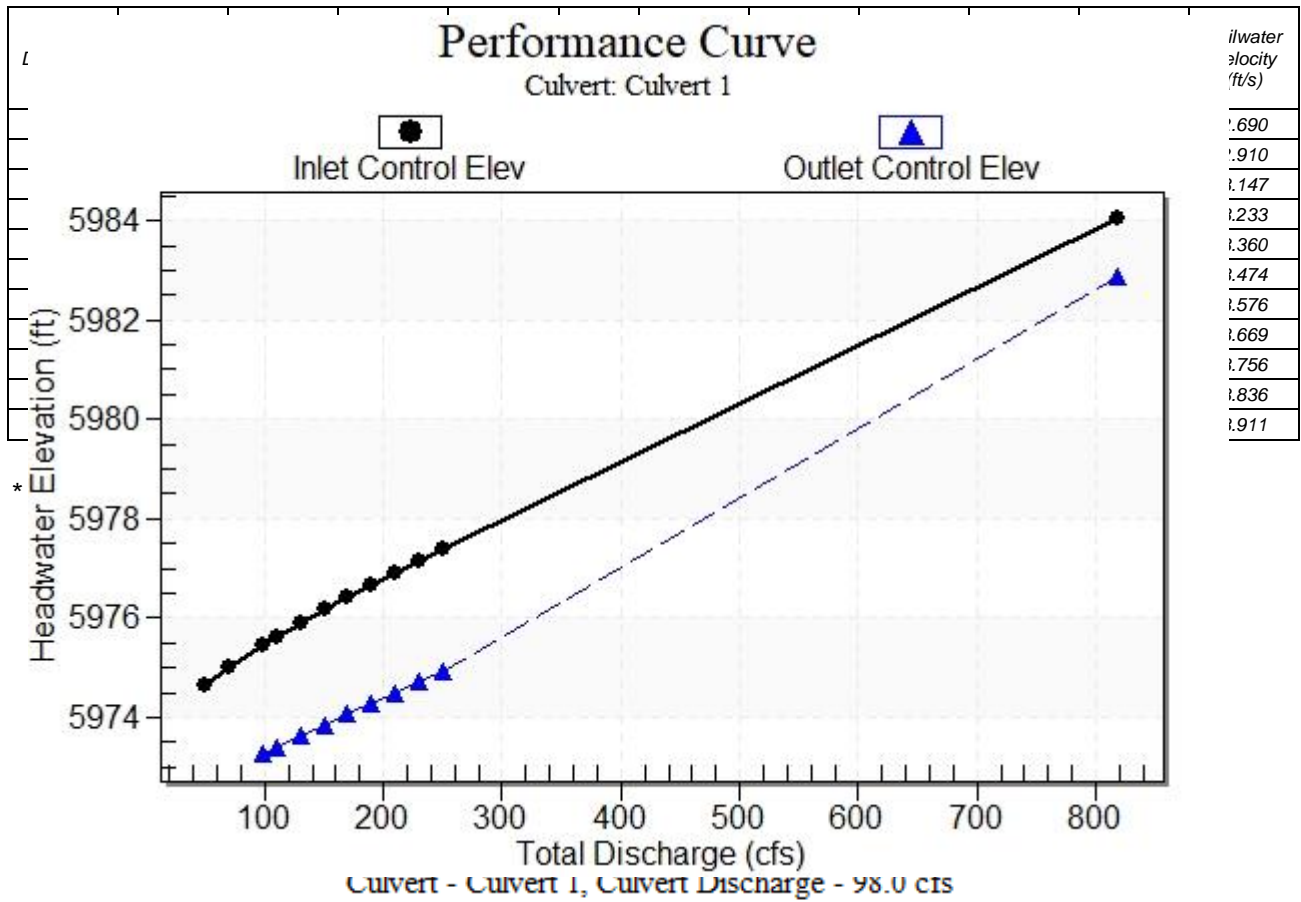


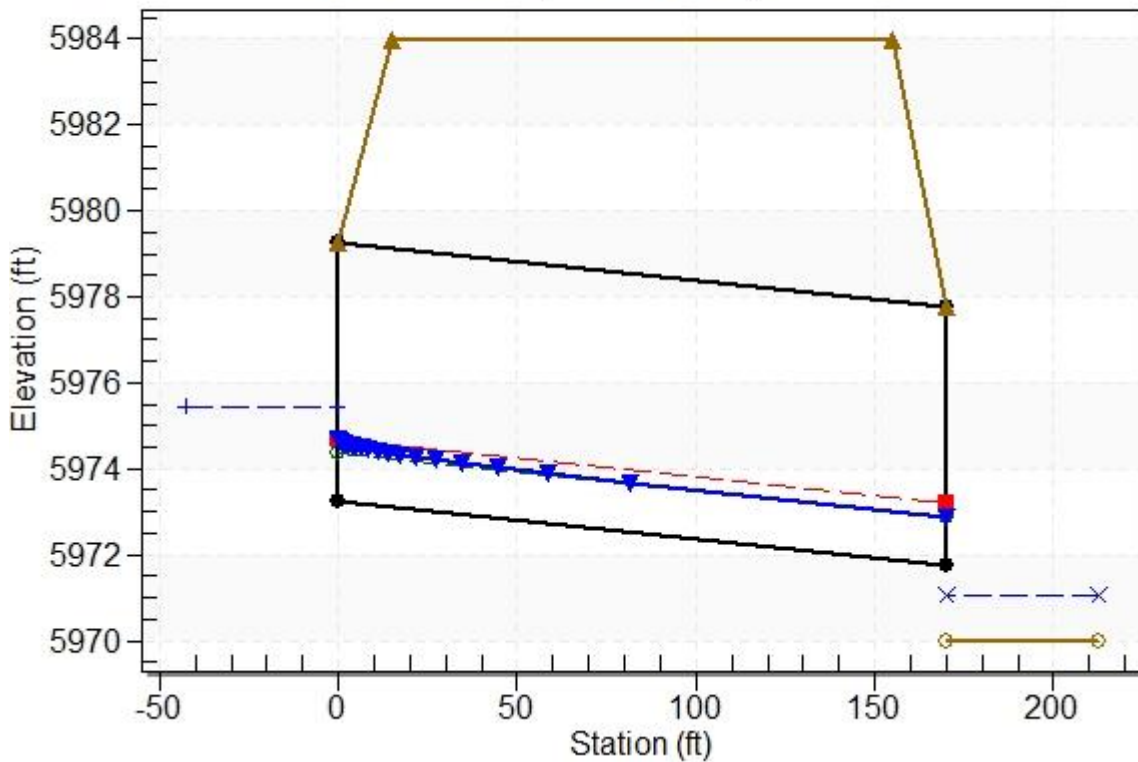
Table 2 - Culvert Summary Table: Culvert 1



Culvert Performance Curve Plot: Culvert 1

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - Powers Blvd - Ex. 10'x6' RCBC, Design Discharge - 98.0 cfs
Culvert - Culvert 1, Culvert Discharge - 98.0 cfs



Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 5973.25 ft

Outlet Station: 170.00 ft

Outlet Elevation: 5971.75 ft

Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Concrete Box

Barrel Span: 10.00 ft

Barrel Rise: 6.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0150

Culvert Type: Straight

Inlet Configuration: Square Edge (30-75° flare) Wingwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: Powers Blvd - Ex.10'x6' RCBC)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
50.00	5970.77	0.77	2.69	0.30	0.70
70.00	5970.89	0.89	2.91	0.35	0.71
98.00	5971.04	1.04	3.15	0.41	0.72
110.00	5971.09	1.09	3.23	0.43	0.72
130.00	5971.17	1.17	3.36	0.46	0.72
150.00	5971.25	1.25	3.47	0.49	0.73
170.00	5971.32	1.32	3.58	0.52	0.73
190.00	5971.38	1.38	3.67	0.54	0.73
210.00	5971.44	1.44	3.76	0.57	0.74
230.00	5971.50	1.50	3.84	0.59	0.74
250.00	5971.56	1.56	3.91	0.61	0.74

Tailwater Channel Data - Powers Blvd - Ex.10'x6' RCBC

Tailwater Channel Option: Irregular Channel

Channel Slope: 0.0063

User Defined Channel Cross-Section:

(ft)	Coord No.	Station (ft)	Elevation	Manning's n
	1	0.00	5974.00	0.0300
	2	112.00	5972.00	0.0300
	3	147.00	5970.00	0.0250
	4	155.00	5970.00	0.0300

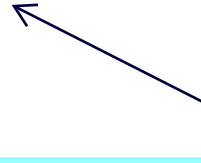
5	205.00	5972.00	0.0300
6	330.00	5974.00	0.0000

Roadway Data for Crossing: Powers Blvd - Ex.10'x6' RCBC

- Roadway Profile Shape: Constant Roadway Elevation
- Crest Length: 510.00 ft
- Crest Elevation: 5984.00 ft
- Roadway Surface: Paved
- Roadway Top Width: 140.00 ft

HY-8 Culvert Analysis Report

*Ex. DUAL 42" CMP CULVERT CROSSING
BRADLEY ROAD*



Revise calculation. Per the narrative one is being plugged and the other is reduced.

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 5 cfs

Design Flow: 47 cfs

Maximum Flow: 80 cfs

Table 1 - Summary of Culvert Flows at Crossing: BRADLEY XING DUAL 42 CMP

<i>Headwater Elevation (ft)</i>	<i>Total Discharge (cfs)</i>	<i>Culvert 2 Discharge (cfs)</i>	<i>Roadway Discharge (cfs)</i>	<i>Iterations</i>
5924.35	5.00	5.00	0.00	1
5924.38	12.50	12.50	0.00	1
5924.40	20.00	20.00	0.00	1
5924.43	27.50	27.50	0.00	1
5924.45	35.00	35.00	0.00	1
5924.47	42.50	42.50	0.00	1
5924.48	47.00	47.00	0.00	1
5924.53	57.50	57.50	0.00	1
5924.73	65.00	65.00	0.00	1
5924.93	72.50	72.50	0.00	1
5925.14	80.00	80.00	0.00	1
5930.00	182.33	182.33	0.00	Overtopping

Rating Curve Plot for Crossing: BRADLEY XING DUAL 42 CMP

Total Rating Curve
Crossing: BRADLEY XING DUAL 42 CMP

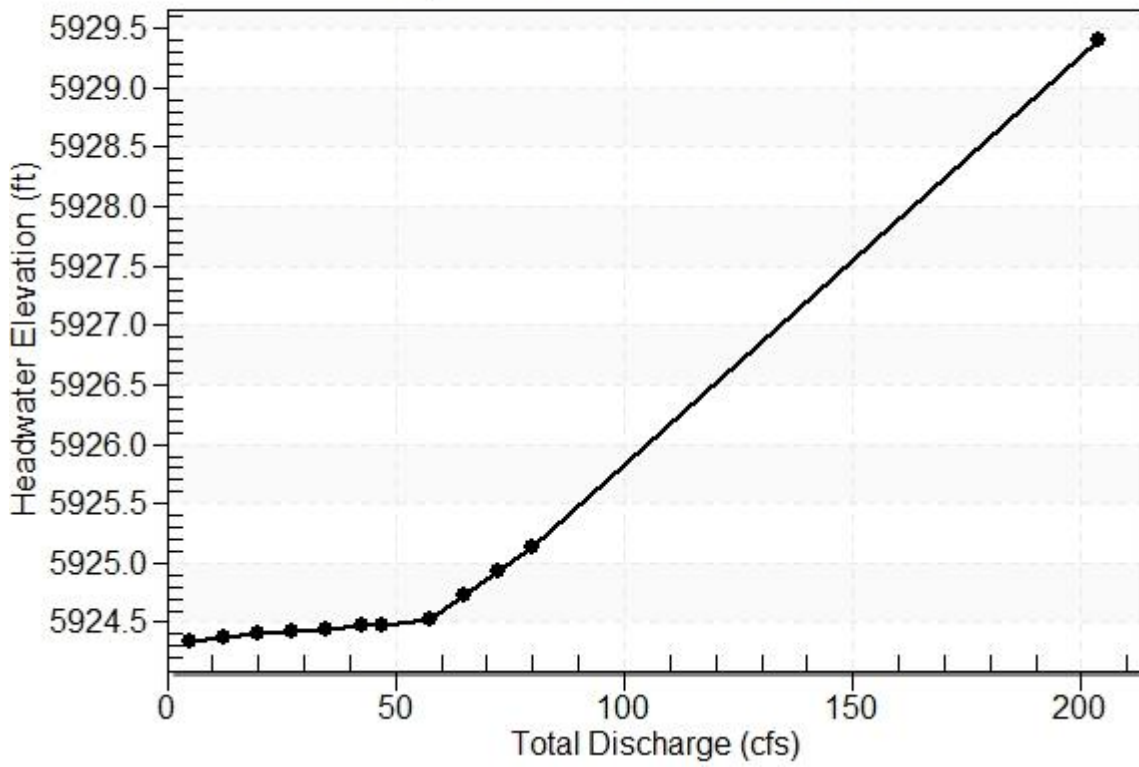


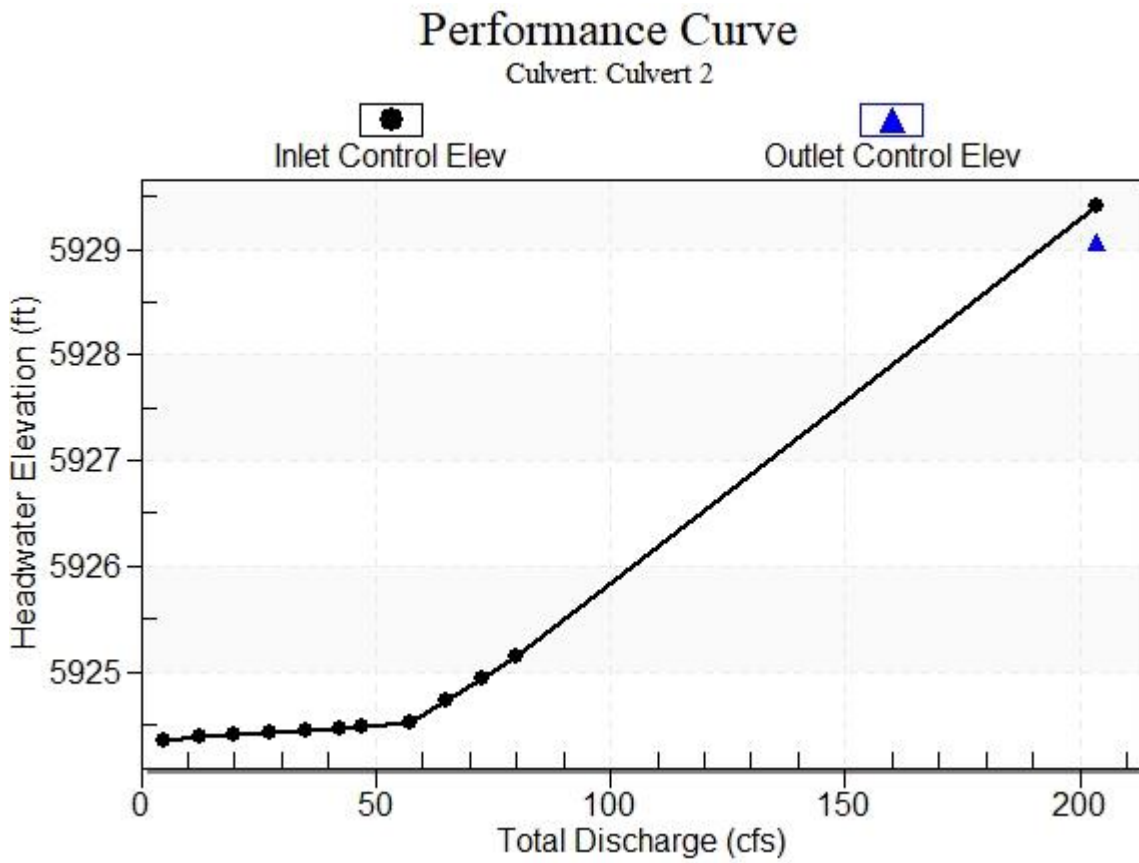
Table 2 - Culvert Summary Table: Culvert 2

<i>Total Discharge (cfs)</i>	<i>Culvert Discharge (cfs)</i>	<i>Headwater Elevation (ft)</i>	<i>Inlet Control Depth (ft)</i>	<i>Outlet Control Depth (ft)</i>	<i>Flow Type</i>	<i>Normal Depth (ft)</i>	<i>Critical Depth (ft)</i>	<i>Outlet Depth (ft)</i>	<i>Tailwater Depth (ft)</i>	<i>Outlet Velocity (ft/s)</i>	<i>Tailwater Velocity (ft/s)</i>
5.00	5.00	5924.35	2.347	0.0*	1-S2n	0.413	0.471	0.413	0.041	3.903	1.210
12.50	12.50	5924.38	2.379	0.0*	1-S2n	0.647	0.752	0.647	0.071	5.108	1.730
20.00	20.00	5924.40	2.405	0.0*	1-S2n	0.817	0.957	0.817	0.093	5.857	2.076
27.50	27.50	5924.43	2.427	0.0*	1-S2n	0.959	1.127	0.959	0.113	6.422	2.345
35.00	35.00	5924.45	2.448	0.0*	1-S2n	1.087	1.277	1.087	0.130	6.874	2.571
42.50	42.50	5924.47	2.467	0.0*	1-S2n	1.203	1.413	1.203	0.146	7.260	2.767
47.00	47.00	5924.48	2.478	0.0*	1-S2n	1.269	1.489	1.269	0.155	7.463	2.874
57.50	57.50	5924.53	2.525	0.0*	1-S2n	1.415	1.655	1.415	0.175	7.884	3.100
65.00	65.00	5924.73	2.730	0.0*	1-S2n	1.515	1.764	1.515	0.188	8.145	3.245
72.50	72.50	5924.93	2.934	0.0*	1-S2n	1.611	1.868	1.611	0.200	8.380	3.381
80.00	80.00	5925.14	3.139	0.0*	1-S2n	1.705	1.967	1.705	0.212	8.594	3.506

* Full Flow Headwater elevation is below inlet invert.

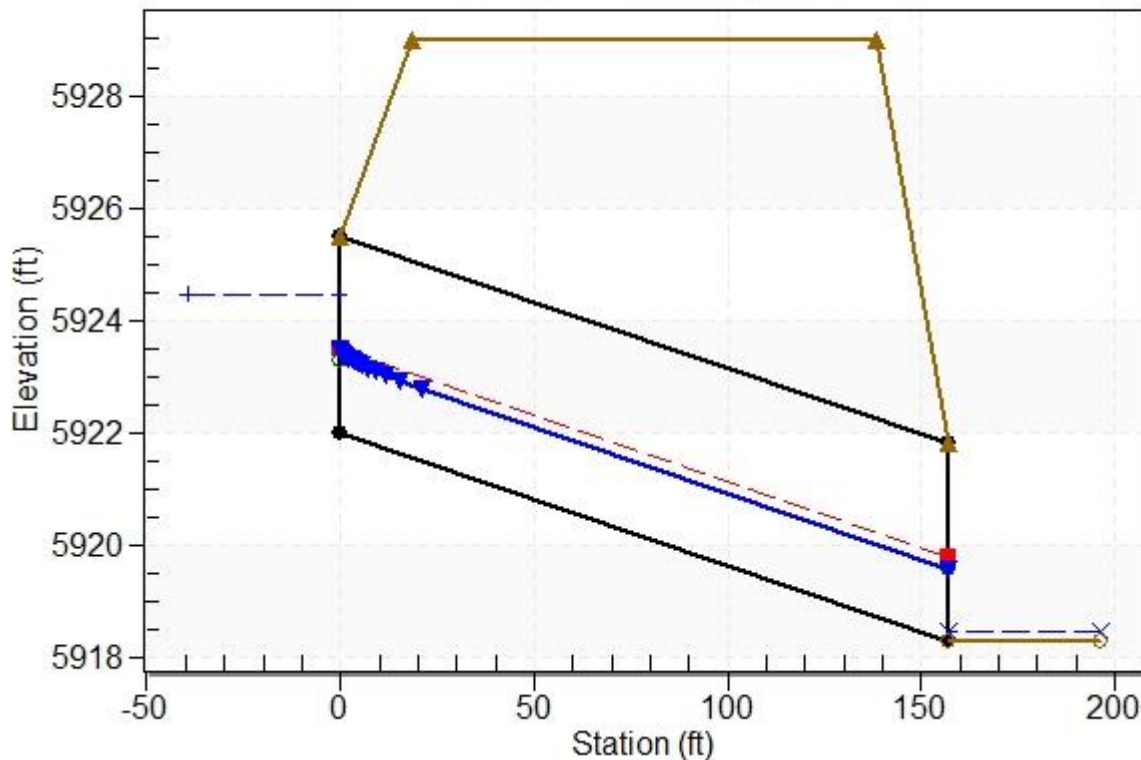
Straight Culvert
Inlet Elevation (invert): 5922.00 ft, Outlet Elevation (invert): 5918.32 ft
Culvert Length: 157.10 ft, Culvert Slope: 0.0234
Inlet Throat Elevation: 5922.00 ft, Inlet Crest Elevation: 5924.31 ft

Culvert Performance Curve Plot: Culvert 2



Water Surface Profile Plot for Culvert: Culvert 2

Crossing - BRADLEY XING DUAL 42 CMP, Design Discharge - 47.0 cfs
Culvert - Culvert 2, Culvert Discharge - 47.0 cfs



Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 5924.00 ft

Outlet Station: 157.00 ft

Outlet Elevation: 5918.32 ft

Number of Barrels: 2

Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 3.50 ft

Barrel Material: Corrugated Steel

Embedment: 0.00 in

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: Yes

Table 3 - Downstream Channel Rating Curve (Crossing: BRADLEY XING DUAL 42

<i>Flow (cfs)</i>	<i>Water Surface Elev (ft)</i>	<i>Depth (ft)</i>	<i>Velocity (ft/s)</i>	<i>Shear (psf)</i>	<i>Froude Number</i>
5.00	5918.36	0.04	1.21	0.08	1.06
12.50	5918.39	0.07	1.73	0.13	1.16
20.00	5918.41	0.09	2.08	0.17	1.22
27.50	5918.43	0.11	2.34	0.21	1.25
35.00	5918.45	0.13	2.57	0.24	1.28
42.50	5918.47	0.15	2.77	0.27	1.31
47.00	5918.48	0.16	2.87	0.29	1.32
57.50	5918.49	0.17	3.10	0.33	1.34
65.00	5918.51	0.19	3.24	0.35	1.36
72.50	5918.52	0.20	3.38	0.38	1.37
80.00	5918.53	0.21	3.51	0.40	1.39

CMP)**Tailwater Channel Data - BRADLEY XING DUAL 42 CMP***Tailwater Channel Option: Trapezoidal Channel**Bottom Width: 100.00 ft**Side Slope (H:V): 35.00 (_:1)**Channel Slope: 0.0300**Channel Manning's n: 0.0250**Channel Invert Elevation: 5918.32 ft***Roadway Data for Crossing: BRADLEY XING DUAL 42 CMP***Roadway Profile Shape: Irregular Roadway Shape (coordinates)**Irregular Roadway Cross-Section:*

<i>Coord No.</i>	<i>Station (ft)</i>	<i>Elevation (ft)</i>
0	0.00	5929.00
1	60.00	5930.00
2	120.00	5929.00

*Roadway Surface: Paved**Roadway Top Width: 120.00 ft*

DIVERSION CHANNEL ANALYSES

Hydraulic Analysis Report

Project Data

Project Title:

Designer:

Project Date: Friday, May 29, 2020

Project Units: U.S. Customary Units

Notes:

Channel Analysis: North Diversion Channel 1

Notes:

Input Parameters

Channel Type: Trapezoidal

Side Slope 1 (Z1): 4.0000 ft/ft

Side Slope 2 (Z2): 4.0000 ft/ft

Channel Width: 8.0000 ft

Longitudinal Slope: 0.0309 ft/ft

Manning's n: 0.0300

Flow: 38.0000 cfs

Result Parameters

Depth: 0.6444 ft

Area of Flow: 6.8159 ft²

Wetted Perimeter: 13.3136 ft

Hydraulic Radius: 0.5119 ft

Average Velocity: 5.5752 ft/s

Top Width: 13.1550 ft

Froude Number: 1.3650

Critical Depth: 0.7749 ft

Critical Velocity: 4.4178 ft/s

Critical Slope: 0.0158 ft/ft

Critical Top Width: 14.20 ft

Calculated Max Shear Stress: 1.2425 lb/ft²

Calculated Avg Shear Stress: 0.9871 lb/ft²

FYI: This will need to be addressed with the preliminary/final drainage report. See the criteria below.

6.5.2 Channel Velocity

Concrete, riprap, or soil cement linings as approved by the City/County shall be used where channel bottom velocities exceed 6.0 ft/sec. Grass lined channels shall not be used where velocity exceeds permissible velocities in Table 10-4 or the Froude number is greater than 0.9 for the 100-year storm.

Channel Analysis: North Diversion Channel 2

Notes:

Input Parameters

Channel Type: Trapezoidal

Side Slope 1 (Z1): 4.0000 ft/ft

Side Slope 2 (Z2): 4.0000 ft/ft

Channel Width: 8.0000 ft

Longitudinal Slope: 0.0344 ft/ft

Manning's n: 0.0300

Flow: 72.0000 cfs

Result Parameters

Depth: 0.8874 ft

Area of Flow: 10.2487 ft²

Wetted Perimeter: 15.3175 ft

Hydraulic Radius: 0.6691 ft

Average Velocity: 7.0253 ft/s

Top Width: 15.0990 ft

Froude Number: 1.5027

Critical Depth: 1.1205 ft

Critical Velocity: 5.1482 ft/s

Critical Slope: 0.0143 ft/ft

Critical Top Width: 16.96 ft

Calculated Max Shear Stress: 1.9048 lb/ft²

Calculated Avg Shear Stress: 1.4362 lb/ft²

Selected Profile: FHWA Profile (read-only)

Culvert Assessment Profiles

Culvert Assessment Profile Name: Standard (read-only)

Maximum Excavation Depth: 20 ft

Maximum Shallow Cover: 4 ft

Maximum Small Pipe Size: 36 in

Minimum Manned Entry Size: 48 in

Riprap Classes

Riprap Name: CLASS I

Riprap Class: I

The following values are an 'average' of the size fraction range for the selected riprap class.

d100: 12 in

d85: 9 in

d50: 6.5 in

d15: 4.5 in

Riprap Name: CLASS II

Riprap Class: II

The following values are an 'average' of the size fraction range for the selected riprap class.

d100: 18 in

d85: 13 in

d50: 9.5 in

d15: 7 in

Riprap Name: CLASS III

Riprap Class: III

The following values are an 'average' of the size fraction range for the selected riprap class.

d100: 24 in

d85: 17 in

d50: 12.5 in

d15: 9 in

Riprap Name: CLASS IV

Riprap Class: IV

The following values are an 'average' of the size fraction range for the selected riprap class.

d100: 30 in

d85: 21 in

d50: 15.5 in

d15: 10.5 in

Riprap Name: CLASS V

Riprap Class: V

The following values are an 'average' of the size fraction range for the selected riprap class.

d100: 36 in

d85: 25.5 in

d50: 18.5 in

d15: 13 in

Riprap Name: CLASS VI

POND JCD-D OUTLET TO
N. BRADLEY ROAD DITCH
SINGLE 48" RCP CUVLERT

HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 80 cfs

Design Flow: 120 cfs

Maximum Flow: 150 cfs

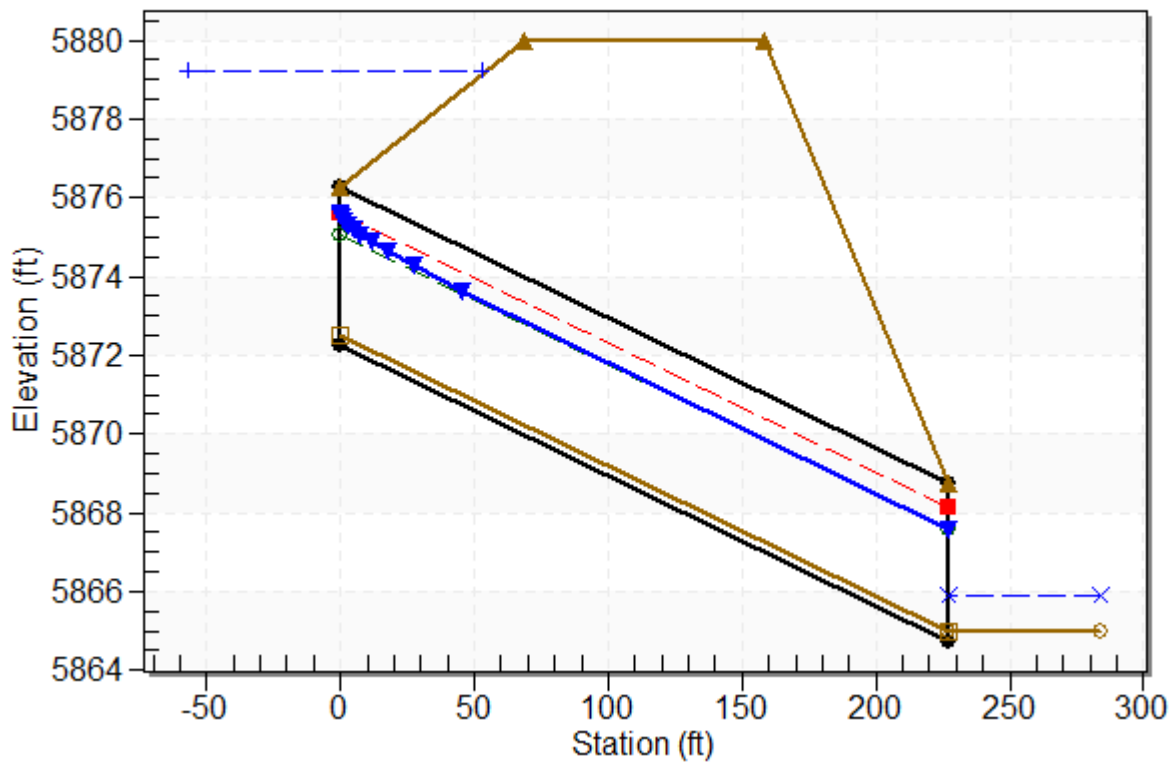
Table 1 - Summary of Culvert Flows at Crossing: N. BRADLEY RD DITCH TO DP

Headwater Elevation (ft)	Total Discharge (cfs)	JCD-D Discharge (cfs)	Roadway Discharge (cfs)	Iterations
5876.84	80.00	80.00	0.00	1
5877.19	87.00	87.00	0.00	1
5877.57	94.00	94.00	0.00	1
5877.98	101.00	101.00	0.00	1
5878.41	108.00	108.00	0.00	1
5878.86	115.00	115.00	0.00	1
5879.21	120.00	120.00	0.00	1
5879.86	129.00	129.00	0.00	1
5880.03	136.00	131.20	4.42	16
5880.06	143.00	131.53	11.08	5
5880.08	150.00	131.79	17.74	4
5880.00	130.80	130.80	0.00	Overtopping

Water Surface Profile Plot for Culvert: JCD-D

Crossing - N. BRADLEY RD DITCH TO DP JCD-D, Design Discharge - 120.0 cfs

Culvert - JCD-D, Culvert Discharge - 120.0 cfs



Culvert Data Summary - JCD-D

- Barrel Shape: Circular
- Barrel Diameter: 4.00 ft
- Barrel Material: Concrete
- Embedment: 3.00 in
- Barrel Manning's n: 0.0120 (top and sides)
- Manning's n: 0.0250 (bottom)
- Culvert Type: Straight
- Inlet Configuration: Square Edge with Headwall
- Inlet Depression: Yes

Table 2 - Culvert Summary Table: JCD-D

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
80.00	80.00	5876.84	4.339	0.0*	5-S2n	2.008	2.539	2.019	0.700	11.433	5.172
87.00	87.00	5877.19	4.694	0.0*	5-S2n	2.107	2.656	2.107	0.735	11.842	5.330
94.00	94.00	5877.57	5.073	0.258	5-S2n	2.205	2.768	2.205	0.769	12.163	5.478
101.00	101.00	5877.98	5.477	1.473	5-S2n	2.302	2.869	2.302	0.802	12.466	5.619
108.00	108.00	5878.41	5.908	2.228	5-S2n	2.398	2.966	2.398	0.834	12.754	5.754
115.00	115.00	5878.86	6.365	3.014	5-S2n	2.495	3.058	2.495	0.865	13.024	5.882
120.00	120.00	5879.21	6.708	3.553	5-S2n	2.564	3.114	2.564	0.887	13.207	5.969
129.00	129.00	5879.86	7.363	4.655	5-S2n	2.692	3.212	2.692	0.925	13.520	6.122
136.00	131.20	5880.03	7.530	4.834	5-S2n	2.723	3.236	2.723	0.954	13.593	6.234
143.00	131.53	5880.06	7.556	4.880	5-S2n	2.728	3.239	2.728	0.982	13.603	6.343
150.00	131.79	5880.08	7.576	4.917	5-S2n	2.732	3.242	2.732	1.010	13.612	6.449

* Full Flow Headwater elevation is below inlet invert.

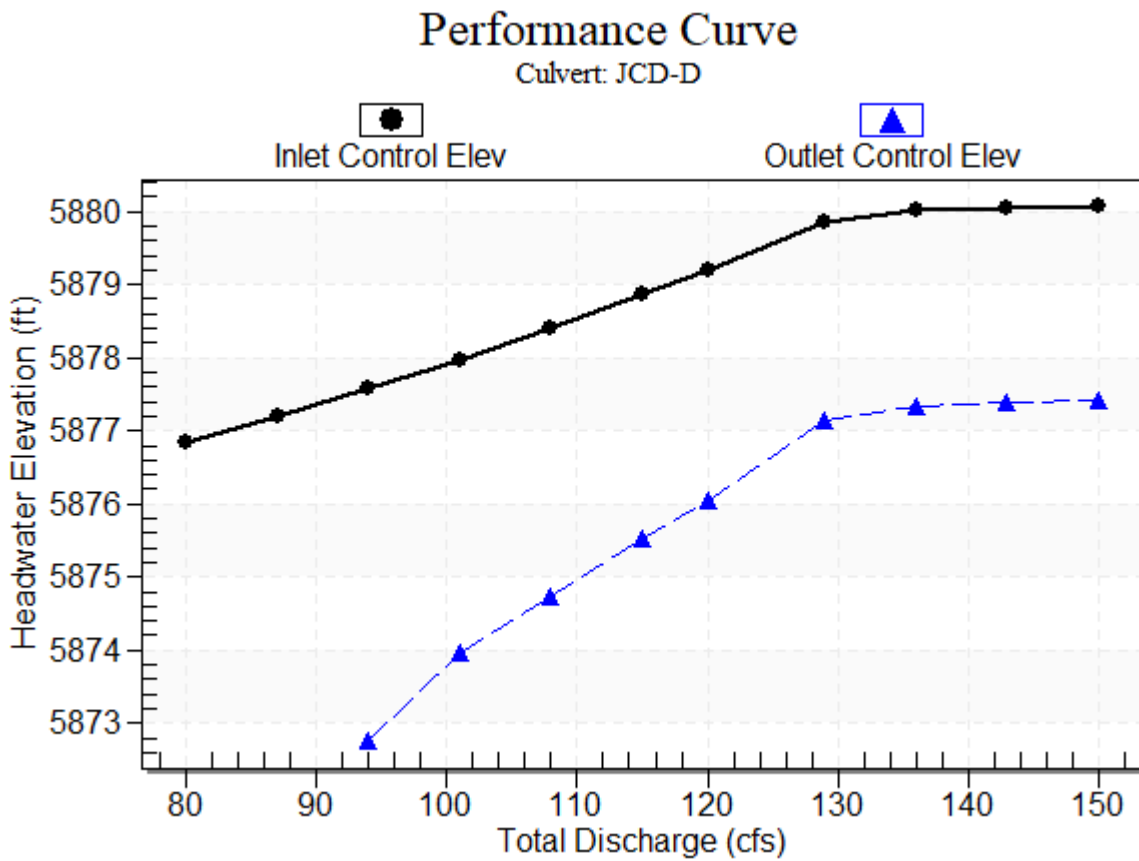
Straight Culvert

Inlet Elevation (invert): 5872.50 ft, Outlet Elevation (invert): 5865.00 ft

Culvert Length: 227.14 ft, Culvert Slope: 0.0330

Inlet Throat Elevation: 5872.50 ft, Inlet Crest Elevation: 5873.13 ft

Culvert Performance Curve Plot: JCD-D



Site Data - JCD-D

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 5872.75 ft

Outlet Station: 227.00 ft

Outlet Elevation: 5864.75 ft

Number of Barrels: 1

Rating Curve Plot for Crossing: N. BRADLEY RD DITCH TO DP JCD-D

Total Rating Curve

Crossing: N. BRADLEY RD DITCH TO DP JCD-D

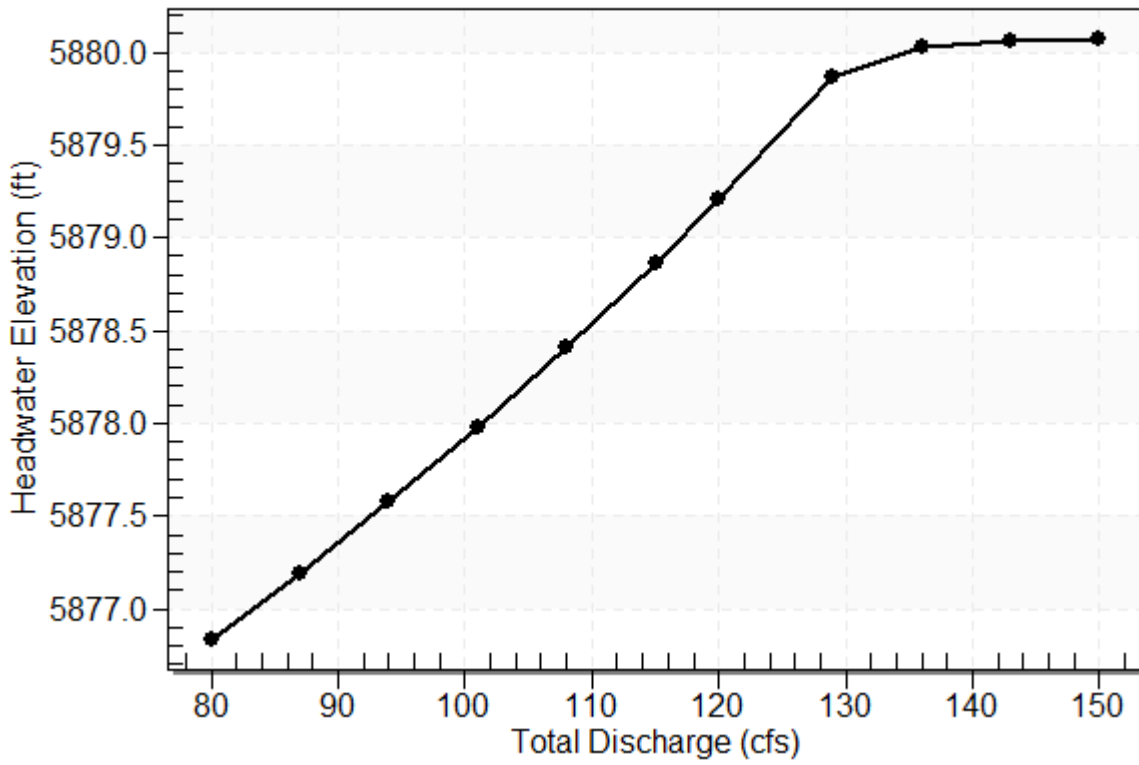


Table 3 - Downstream Channel Rating Curve (Crossing: N. BRADLEY RD DITCH TO

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
80.00	5865.70	0.70	5.17	1.19	1.14
87.00	5865.74	0.74	5.33	1.25	1.15
94.00	5865.77	0.77	5.48	1.31	1.16
101.00	5865.80	0.80	5.62	1.37	1.16
108.00	5865.83	0.83	5.75	1.42	1.17
115.00	5865.87	0.87	5.88	1.47	1.18
120.00	5865.89	0.89	5.97	1.51	1.18
129.00	5865.93	0.93	6.12	1.58	1.19
136.00	5865.95	0.95	6.23	1.63	1.19
143.00	5865.98	0.98	6.34	1.67	1.20
150.00	5866.01	1.01	6.45	1.72	1.20

Tailwater Channel Data - N. BRADLEY RD DITCH TO DP JCD-D

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 20.00 ft

Side Slope (H:V): 3.00 (3:1)

Channel Slope: 0.0273

Channel Manning's n: 0.0350

Channel Invert Elevation: 5865.00 ft

Roadway Data for Crossing: N. BRADLEY RD DITCH TO DP JCD-D

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 333.00 ft

Crest Elevation: 5880.00 ft

Roadway Surface: Gravel

Roadway Top Width: 90.00 ft

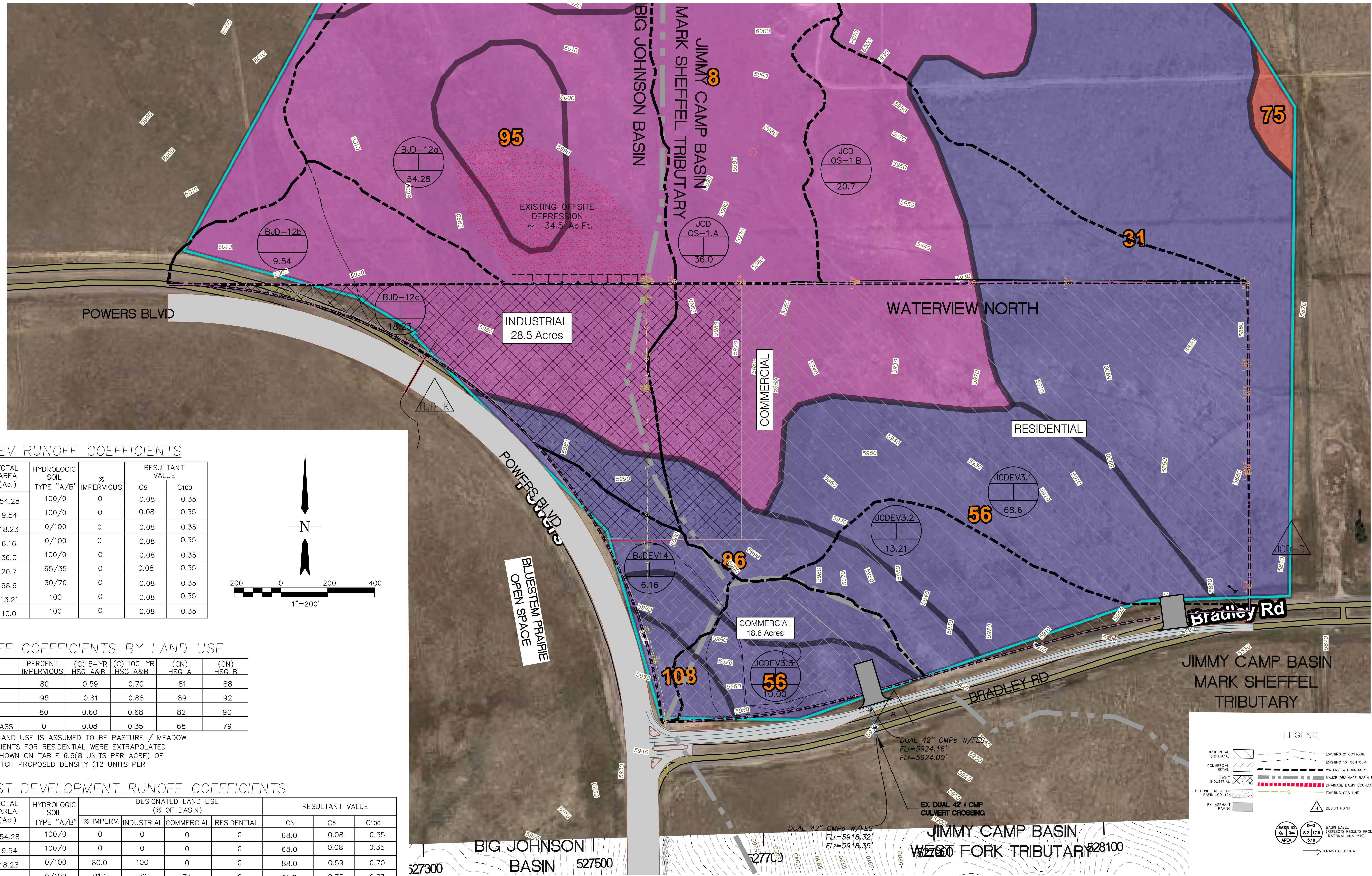
APPENDIX E

RUNOFF COEFFICIENT EXHIBIT

PRE-DEVELOPMENT BASIN MAP

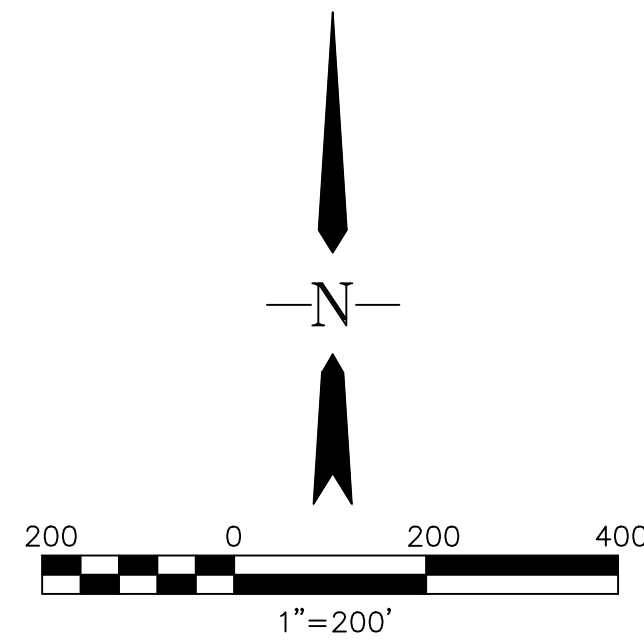
POST DEVELOPMENT DRAINAGE PLAN

RUNOFF COEFFICIENT EXHIBIT



PRE-DEV RUNOFF COEFFICIENTS

BASIN ID	TOTAL AREA (Ac.)	HYDROLOGIC SOIL TYPE "A/B"	% IMPERVIOUS	RESULTANT VALUE	
				C5	C100
BJD-12a	54.28	100/0	0	0.08	0.35
BJD-12b	9.54	100/0	0	0.08	0.35
BJD-12c	18.23	0/100	0	0.08	0.35
BJDEV-14	6.16	0/100	0	0.08	0.35
JCD-OS1A	36.0	100/0	0	0.08	0.35
JCD-OS1B	20.7	65/35	0	0.08	0.35
JCDEV-3.1	68.6	30/70	0	0.08	0.35
JCDEV-3.2	13.21	100	0	0.08	0.35
JCDEV-3.3	10.0	100	0	0.08	0.35



RUNOFF COEFFICIENTS BY LAND USE

LAND USE CLASSIFICATION	PERCENT IMPERVIOUS	(C) 5-YR HSG A&B	(C) 100-YR HSG A&B	(CN) HSG A	(CN) HSG B
INDUSTRIAL	80	0.59	0.70	81	88
COMMERCIAL	95	0.81	0.88	89	92
**RESIDENTIAL	80	0.60	0.68	82	90
*BRUSH\WEEDS\GRASS	0	0.08	0.35	68	79

* OFFSITE BASIN LAND USE IS ASSUMED TO BE PASTURE / MEADOW
 ** RUNOFF COEFFICIENTS FOR RESIDENTIAL WERE EXTRAPOLATED FROM VALUES SHOWN ON TABLE 6.6(8 UNITS PER ACRE) OF THE DCM TO MATCH PROPOSED DENSITY (12 UNITS PER ACRE).

POST DEVELOPMENT RUNOFF COEFFICIENTS

BASIN ID	TOTAL AREA (Ac.)	HYDROLOGIC SOIL TYPE "A/B"	DESIGNATED LAND USE (% OF BASIN)			RESULTANT VALUE			
			% IMPERV.	INDUSTRIAL	COMMERCIAL	RESIDENTIAL	CN	C5	C100
BJD-12a	54.28	100/0	0	0	0	0	68.0	0.08	0.35
BJD-12b	9.54	100/0	0	0	0	0	68.0	0.08	0.35
BJD-12c	18.23	0/100	80.0	100	0	0	88.0	0.59	0.70
BJDEV-14	6.16	0/100	91.1	26	74	0	91.0	0.75	0.83
JCD-OS1A	36.0	100/0	0	0	0	0	68.0	0.08	0.35
JCD-OS1B	20.7	65/35	0	0	0	0	71.9	0.08	0.35
JCDEV-3.1	68.6	0/100	82.2	12	10	79	90.7	0.60	0.71
JCDEV-3.2	13.21	0/100	80.0	0	0	100	90	0.60	0.68
JCDEV-3.3	10.0	0/100	91.7	0	78	22	91.6	0.76	0.84

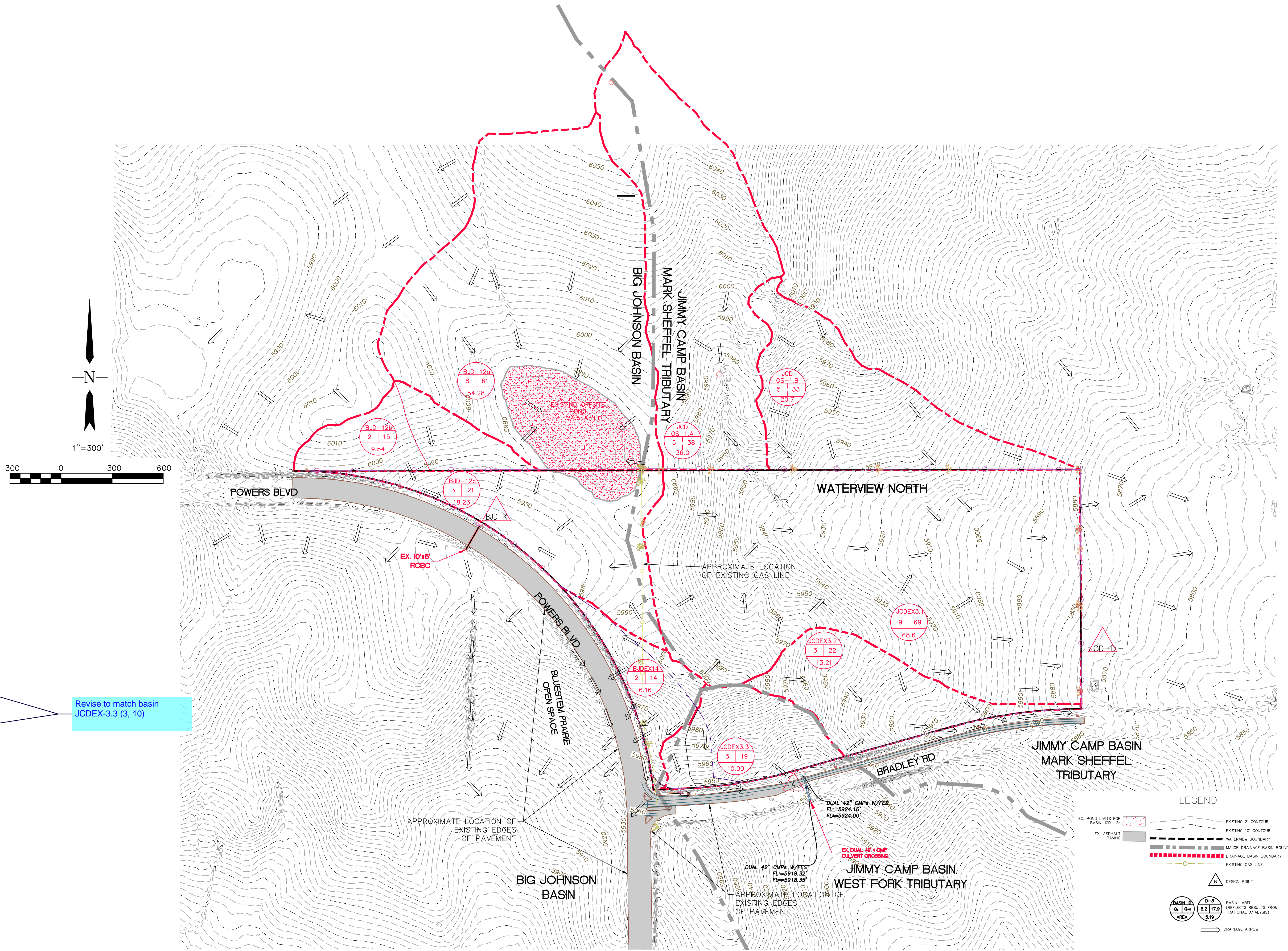
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NO.	DESCRIPTION	DATE	DESIGNED BY:	DATE:	
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			CEB	10-01-20	
			CKC	10-01-20	

48 HOURS BEFORE YOU DIG, CALL UTILITY LOCATORS
 1-800-922-1987
 CITY OF COLORADO SPRINGS DEPT. OF UTILITIES
 GAS, ELECTRIC, WATER AND WASTEWATER

DSE Dakota Springs Engineering
 31 N. TEJON, SUITE 518
 COLORADO SPRINGS, CO 80903
 P: (719) 227-7388
 F: (719) 227-7392

PROJECT: WATerview NORTH
 SHEET TITLE: RUNOFF COEFFICIENT EXHIBIT
 FROM n/a TO n/a
 JOB NO. 02-19-05 SHEET 1 OF 3

PRE-DEVELOPMENT BASIN MAP



BASIN ID	BASIN AREA (Ac.)	DESIGN POINT	RATIONAL ANALYSIS RESULTS	
			Q _s (CFS)	Q ₁₀₀ (CFS)
BJD-12a	54.28		8	61
BJD-12b	9.54		2	15
BJD-12c	18.23		3	21
		BJD-K	4	31
JCD OS-1A	36.0		5	38
JCD OS-1B	20.7		5	33
JCDEX-3.1	68.6		9	69
JCDEX-3.2	13.21		3	22
		JCD-D	12	84
JCDEX-3.3	10.0		3	19
BJDEX14	6.16		2	14
		A	4	31
		A*	5	25

Revise to match basin JCDEX-3.3 (3, 10)

A* - MODELLED AS BASIN OS-1 IN THE FINAL DRAINAGE REPORT FOR FILING 1 OF TRAILS AT ASPEN RIDGE, APP'D ON FEBRUARY 13, 2020.

LEGEND

- EX. POND LIMITS FOR BASIN JCD-12a
- EX. ASPHALT PAVING
- EXISTING 2' CONTOUR
- EXISTING 10' CONTOUR
- WATERVIEW BOUNDARY
- MAJOR DRAINAGE BASIN BOUNDARY
- DRAINAGE BASIN BOUNDARY
- EXISTING GAS LINE
- DESIGN POINT
- BASIN ID, Q_s, Q₁₀₀, AREA
- BASIN LABEL, PRELECTS RESULTS FROM RATIONAL ANALYSIS
- DRAINAGE ARROW

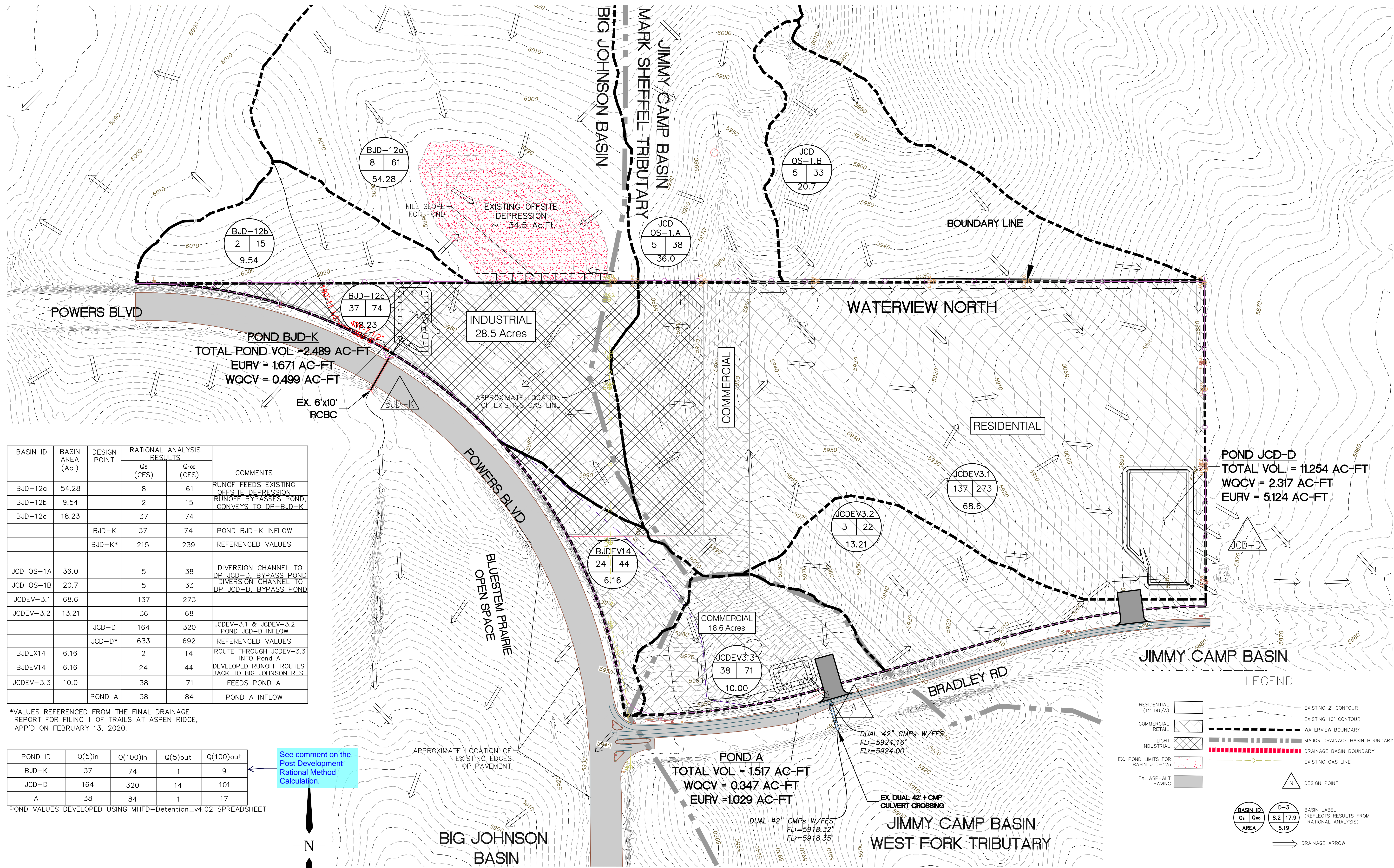
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			CEB	10-1-20	
			CKC	10-1-20	

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DSE Dakota Springs Engineering
 31 N. TEJON, SUITE 518
 COLORADO SPRINGS, CO 80903
 P: (719) 227-7388
 F: (719) 227-7392

PROJECT: WATERVIEW NORTH
 SHEET TITLE: PRE-DEVELOPMENT BASIN MAP
 FROM n/a TO n/a
 JOB NO. 02-19-05 SHEET 2 OF 3

POST DEVELOPMENT DRAINAGE PLAN



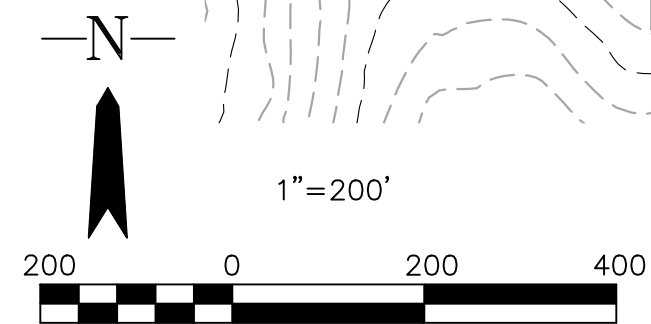
BASIN ID	BASIN AREA (Ac.)	DESIGN POINT	RATIONAL ANALYSIS RESULTS		COMMENTS
			Q _s (CFS)	Q ₁₀₀ (CFS)	
BJD-12a	54.28		8	61	RUNOFF FEEDS EXISTING OFFSITE DEPRESSION
BJD-12b	9.54		2	15	RUNOFF BYPASSES POND, CONVEYS TO DP-BJD-K
BJD-12c	18.23		37	74	
		BJD-K	37	74	POND BJD-K INFLOW
		BJD-K*	215	239	REFERENCED VALUES
JCD OS-1A	36.0		5	38	DIVERSION CHANNEL TO DP JCD-D, BYPASS POND
JCD OS-1B	20.7		5	33	DIVERSION CHANNEL TO DP JCD-D, BYPASS POND
JCDEV-3.1	68.6		137	273	
JCDEV-3.2	13.21		36	68	
		JCD-D	164	320	JCDEV-3.1 & JCDEV-3.2 POND JCD-D INFLOW
		JCD-D*	633	692	REFERENCED VALUES
BJDEV14	6.16		2	14	ROUTE THROUGH JCDEV-3.3 INTO POND A
BJDEV14	6.16		24	44	DEVELOPED RUNOFF ROUTES BACK TO BIG JOHNSON RES.
JCDEV-3.3	10.0		38	71	FEEDS POND A
		POND A	38	84	POND A INFLOW

*VALUES REFERENCED FROM THE FINAL DRAINAGE REPORT FOR FILING 1 OF TRAILS AT ASPEN RIDGE, APP'D ON FEBRUARY 13, 2020.

POND ID	Q(5)in	Q(100)in	Q(5)out	Q(100)out
BJD-K	37	74	1	9
JCD-D	164	320	14	101
A	38	84	1	17

POND VALUES DEVELOPED USING MHPD-Detention_v4.02 SPREADSHEET

See comment on the Post Development Rational Method Calculation.



LEGEND

- RESIDENTIAL (12 DU/A)
- COMMERCIAL RETAIL
- INDUSTRIAL
- EX. POND LIMITS FOR BASIN JCD-12a
- EX. ASPHALT PAVING
- EXISTING 2' CONTOUR
- EXISTING 10' CONTOUR
- WATERVIEW BOUNDARY
- MAJOR DRAINAGE BASIN BOUNDARY
- DRAINAGE BASIN BOUNDARY
- EXISTING GAS LINE
- DESIGN POINT
- BASIN LABEL (REFLECTS RESULTS FROM RATIONAL ANALYSIS)
- DRAINAGE ARROW

REVISIONS:			ENGINEER:		
NO.	DESCRIPTION	DATE	DESIGNED BY:	DATE:	
			CEB	10-1-20	
			CEB	10-1-20	
			CKC	10-1-20	

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31 N. TEJON, SUITE 518
COLORADO SPRINGS, CO 80903
P: (719) 227-7388
F: (719) 227-7392

PROJECT WATERVIEW NORTH
SHEET TITLE POST DEVELOPMENT DRAINAGE PLAN
FROM n/a TO n/a
JOB NO. 02-19-05 SHEET 3 OF 3

MDDP_r2.pdf Markup Summary

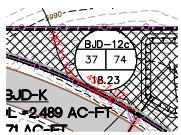
dsdlaforce (15)



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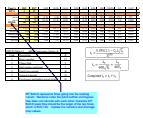
Only basin JCD-EX3.3 is tributary to Design Point A based on the narrative that BJDEX-14 presently flows over Powers Blvd; therefore total flows at design point A should match JCD-EX3. Update the values on the narrative (pg 14). What should be stated in the narrative is that your calculated (2.6/19.1cfs) are less than what's calculated in Trails FDR (5.0/25.3 cfs); therefore, this verifies the Trails drainage system provides adequate capacity to route flows from basin JCD-EX3.3. Similar type of statement should be noted in the developed condition to clearly verify the receiving off-site system has adequate capacity.

However, if DPA values (4.2/30.8) is based on diversion of BJDEX-14 to DP A due to future CDOT construction of Powers Blvd then update the comments section for DPA in this worksheet. Also provide a statement regarding this development's conformance with the receiving offsite system designed/constructed by Trails FDR.



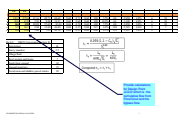
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431'-7 1/2"



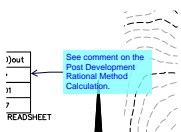
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Date: 10/21/2020 4:00:39 PM
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DP BJD-K represents flows going into the existing culvert. Narrative notes the pond outflow and bypass flow does not coincide with each other; therefore DP BJD-K peak flow should be the larger of the two flows which is BJD-12b. Update the narrative and drainage map values.



Subject: Callout
Page Label: 56
Author: dsdlaforce
Date: 10/21/2020 4:03:03 PM
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Provide calculations for Design Point JCD-D which is the cumulative flow from Pond Qout and the bypass flow.



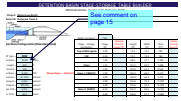
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See comment on the Post Development Rational Method Calculation.

Act/Subject point

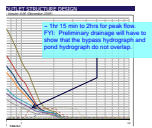
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Add bullet point



Subject: Callout
Page Label: 90
Author: dsdlaforce
Date: 10/21/2020 4:47:06 PM
Status:
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See comment on page 15



Subject: Callout
Page Label: 86
Author: dsdlaforce
Date: 10/21/2020 4:52:36 PM
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~ 1hr 15 min to 2hrs for peak flow.
FYI: Preliminary drainage will have to show that the bypass hydrograph and pond hydrograph do not overlap.



Subject: Cloud+
Page Label: 15
Author: dsdlaforce
Date: 10/21/2020 4:54:42 PM
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Clarify. The developed drainage map is showing this basin is routed into Pond A. Update Pond A calculation to include basin BJDEV-14 for the pond sizing.

However, if basin BJDEV-14 is supposed to have it's own wq/detention then show the pond on the proposed drainage map and provide the pond calculation. Assuming discharge is as shown on the proposed map then Pond A must be redesigned as a pond in a series.

Subject: Callout
Page Label: 17
Author: dsdlaforce
Date: 10/21/2020 4:56:00 PM
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Based on conversation with the design engineer there are two options being considered for basin JCDEV3.3.

Rewrite narrative to clearly state that two options are currently being considered within JCDEV3.3. Recommend separating the two options into two bullet points similar to the above outfall alternative for pond D.

For each option clearly identify the wq/detention for basin BJDEV14 since this basin is being routed through Pond A.

Subject: Callout
Page Label: 92
Author: dsdlaforce
Date: 10/21/2020 4:58:40 PM
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FYI: Final pond design will need this to be at 40hr

CMP CULVERT CROSSING
RADLEY ROAD

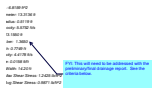
Revise calculation. Per the narrative one is being plugged and the other is reduced.

Subject: Callout
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Revise calculation. Per the narrative one is being plugged and the other is reduced.

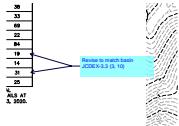


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Subject: Callout
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Author: dsdlaforce
Date: 10/21/2020 5:11:18 PM
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FYI: This will need to be addressed with the preliminary/final drainage report. See the criteria below.



Subject: Callout
Page Label: 138
Author: dsdlaforce
Date: 10/21/2020 5:16:03 PM
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Color: ■
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Revise to match basin JCDEX-3.3 (3, 10)