April 17, 2019 Revised April 30, 2019

SR Land, LLC 20 Boulder Crescent Street, 2nd Floor Colorado Springs, Colorado 80903

Attn: Chaz Collins

Re: Pavement Recommendations Vollmer Road Improvements Vollmer Road and Dines Boulevard El Paso County, Colorado

Dear Mr. Collins:

As requested, Entech Engineering, Inc. has obtained samples of the subgrade soils from a section of the roadway for proposed acceleration and deceleration lanes and widening at the intersection of Vollmer Road and Dines Boulevard, in El Paso County, Colorado. The roadway improvements extend both sides of the intersection of Dines Boulevard and Vollmer Road. Laboratory testing to determine the pavement support characteristics of the soils was performed. This letter presents the results of the laboratory testing and pavement recommendations for the roadways.

Project Description

The project consists of the paving of the widening of Vollmer Road and acceleration/deceleration lanes for Vollmer Road at the intersection of Dines Boulevard. Subsurface Soil Investigation and laboratory testing was performed to determine the pavement support characteristics of the soils. The extent of the roadway construction is shown in the Test Boring Location Plan, Figure 1.

Subgrade Conditions

Five exploratory test borings were drilled in the roadway to depths of approximately 5 to 10 feet. The Boring Logs are presented in Appendix A. Sieve Analysis and Atterberg Limit testing were performed on soil samples obtained from the test borings for the purpose of classification. Sieve analyses performed indicated the percent passing the No. 200 sieve for the roadway subgrade soils ranged from approximately 18 to 30 percent. Atterberg Limit Tests performed on the samples resulted in Liquid Limits ranging from 31 to 39 and no value and Plastic Indexes of 16 to 20 and non-plastic. Three general soil types were encountered at the subgrade depth (Soil Types 1, 2, and 3). Soil Type 1 consisted of silty sand fill and clayey sand fill which classified as A-1-b and A-2-6 soils based on the AASHTO classification system. Soil Type 2 consisted of native silty sand fill with thin clay lenses which classified as A-1-b and A-2-6 soils. Soil Type 3 consisted of silty sandstone which classified as A-1-b and A-2-4 soils. The Type 1, 2, and 3 soils encountered in the area of the proposed roadway improvements typically have good pavement support characteristics. Mitigation of sandstone may be required and discussed in the mitigation section of this report. Sulfate testing of the subgrade indicated that the soils exhibit a negligible potential for sulfate attack. Groundwater was not encountered in the test borings.





505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238



SR Land, LLC Pavement Recommendations Vollmer Road Improvements El Paso County, Colorado Page 2

Swell testing conducted on Soil Types 1 and 2 showed swells ranging between 0.2 and 0.7 percent, indicating low expansion potentials. These limits are below the level in which mitigation is required (2.0 percent). Laboratory test results are presented in Appendix B and are summarized on Table 1.

California Bearing Ratio (CBR) testing was performed on a sample of Soil Type 1 to determine the support characteristic of the subgrade soils for the roadway sections. The results of the CBR testing, are presented in Appendix B and summarized as follows:

<u>CBR Test Results</u> <u>Soil Type 1 – Clayey Sand Fill</u> R @ 90% = 12.0 R @ 95% = 22.0 Use R = 22.0 for design

Classification Testing	
Liquid Limit	39
Plasticity Index	20
Percent Passing 200	24.5
AASHTO Classification	A-2-6
Group Index	1
Unified Soils Classification	SC

Pavement Design

The CBR testing was used to determine pavement sections for this site. The pavement sections were determined utilizing the El Paso County "Pavement Design Criteria and Report". The following classification and ESAL value were used for this roadway improvement project. Vollmer Road classifies as an urban minor arterial which uses an 18K ESAL value of 1,971,000 for design. Composite and full depth pavement sections are provided. Design parameters used in the pavement analysis are as follows:

Reliability (Urban Minor Arterial)	85%
Serviceability Index	0070
Rural Minor Arterial	2.5
"R" Value Subgrade - ST 1	22.0
Resilient Modulus	5,273 psi
Structural Coefficients:	
Hot Bituminous Pavement	0.44
Aggregate Base Course	0.11
Recycled Concrete Base Course	0.11

SR Land, LLC Pavement Recommendations Vollmer Road Improvements El Paso County, Colorado Page 3

Pavement calculations are attached in Appendix C. Pavement sections recommended for this project are summarized as follows:

Pavement Sections – Soil Type 1 – R=22

Urban Minor Arterial – ESAL = 1,971,000 – Vollmer Road

Alternatives	Asphalt (in)	Base Course (in)
1 – Asphalt Over Aggregate Base Course	5.5	13.5 (aggregate)
2 – Asphalt Over Recycled Concrete Base Course**	5.5	13.5 (recycled conc.)
3 – Full Depth Asphalt	9.0	-

¹ Full depth sections are only allowed over chemically treated or suitable subgrade.

* Minimum sections required by the El Paso County Pavement Design Criteria and Report.

** Class 5 or 6 from an approved source as required by the El Paso County Pavement Design Criteria and Report

It should be noted that construction activity for the acceleration and decelerations has not begun at the time of this investigation. Fill is proposed south of the existing roadway to develop the intersection with Dines Boulevard. Entech has been involved with the overlot grading for the subdivision south of this intersection. It is our understanding that the fill will be generated from this subdivision which contains similar soil properties and should perform similarly to the soils in the drill area along Vollmer Road. The fill proposed for construction should be submitted to Entech prior to construction to determine the suitability of the material and compatibility with the soil obtained from this investigation. The soil conditions within the new roadway subgrade areas should be reviewed after site grading is completed to determine if the existing road section thickness is appropriate versus the designed composite sections presented in this report.

Mitigation

El Paso County criteria requires mitigation of expansive soils for roadway subgrade that have a swell of 2 percent or greater with a 150 pound per square foot surcharge. Four samples at subgrade depth were tested that resulted in volume changes ranging between 0.2 to 0.7 percent. Based on the testing mitigation for expansive soils will not be required.

Mitigation for high bearing sandstone may be required and should be determined after the roadway grading is completed. Typical mitigation for sandstone can include removals of 12 to 18-inches of the material below the base course. The overexcavation should be observed by Entech prior to backfilling with fill. The fill should be approved as stated above before placement. The removed sandstone may be used as fill, however should not contain nodules larger than 2.5 inches nominal diameter.

SR Land, LLC Pavement Recommendations Volimer Road Improvements El Paso County, Colorado Page 4

Roadway Construction - Full Depth Asphalt and Asphalt on Aggregate Base Course Alternatives

Prior to placement of the asphalt, the subgrade should be proofrolled and compacted to a minimum of 95 percent of its maximum Standard Proctor Dry Density, ASTM D-698 at -1 to +2 percent of optimum moisture content or 95 percent of its maximum Modified Proctor Dry Density, ASTM D-1557 at ± 2 percent of optimum moisture content. Any loose or soft areas should be removed and replaced with suitable materials. Base course materials should be compacted to a minimum of 95 percent of its maximum Modified Proctor Dry Density, ASTM D-1557 at ± 2 percent of its maximum Modified Proctor Dry Density, ASTM D-1557 at ± 2 percent of its maximum Modified Proctor Dry Density, ASTM D-1557 at ± 2 percent of optimum moisture content. Special attention should be given to areas adjacent to manholes, inlet structures and valves.

The road subgrade soils should be evaluated after grading is complete. Pavement sections provided should be reviewed after site grading is completed.

In addition to the above guidance, the asphalt, cement, subgrade conditions, compaction of materials and roadway construction methods shall meet the El Paso County specifications.

We trust that this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Stan C. Culp, P.E. Senior Engineer

SCC/sc

Encl.

Entech Job No. 190249 AAprojects/2019/190249/190249 pr_r **Reviewed by:**

h C. Goode, Jr., P.E. sident

TABLE

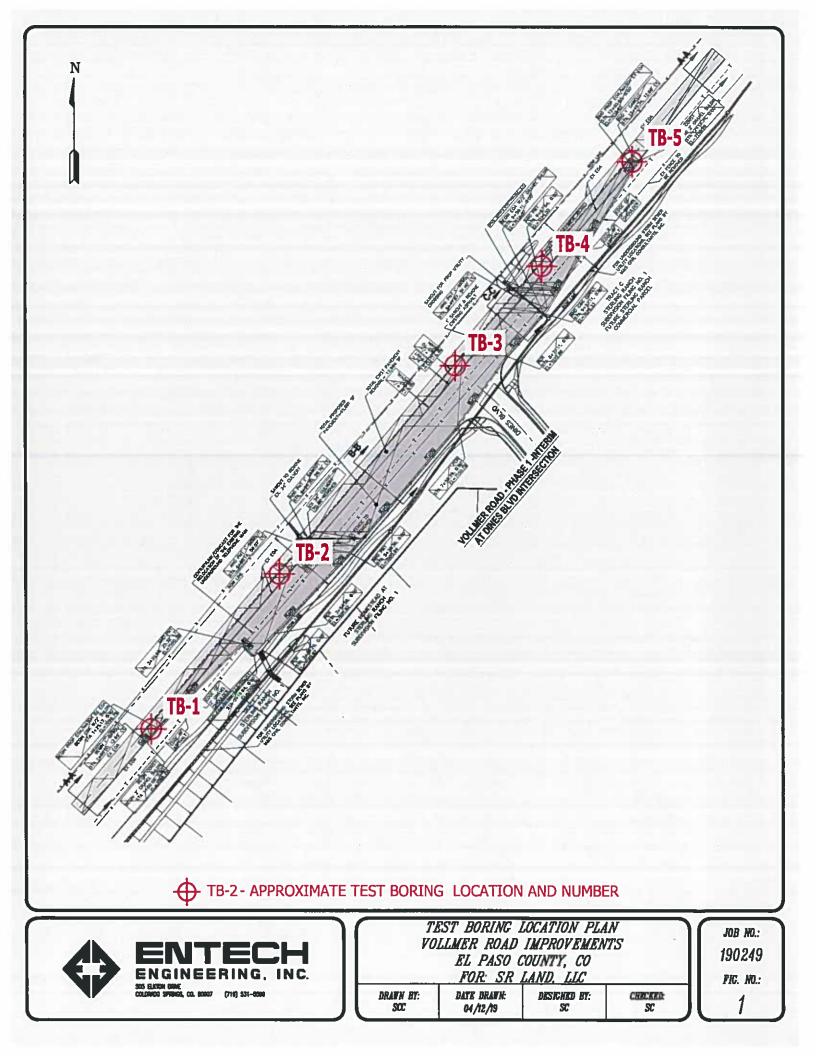
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SUMMARY OF LABORATORY TEST RESULTS

CLIENT SR LAND, LLC PROJECT VOLLMER RD. IMPROVEMENTS JOB NO. 190249

TEST TOL TEST NO. TEST NO. DRY (%) PASSING (%) LIOUID INDEX PLASTIC INDEX NUMERL (WT%) SWELL (WIFED SOIL PORING FT) (%) (%) (WT%) CASS. (%) CASS. FILL, SAND, CLAYEY 1 1 1.2 13.3 13.5 23.1 36 20 A-2.6 0.2 SC FILL, SAND, CLAYEY 1 2 1.2 11.8 113.0 29.6 33 17 <0.01 A-2.6 0.6 SC FILL, SAND, CLAYEY 2 4 0.3 11.2 11.8 NV NP A-2.6 0.6 SC FILL, SAND, CLAYEY 2 4 0.3 11.2 20.3 31 7 <0.01 A-2.6 <th></th> <th>_</th> <th></th> <th></th> <th></th> <th>_</th> <th>_</th> <th>_</th> <th>_</th> <th>_</th>		_				_	_	_	_	_
TEST DRV PASSING LIQUID PLASTIC SWELL BORING FT) (%) (PCF) (%)	SOIL DESCRIPTION	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, SILTY	SAND, SILTY	SAND, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY
TEST DRV DRV PASSING LIQUID PLASTIC ASHTO BORING FTJ (%) (PCF) (%)	UNIFIED CLASSIFICATION	SC	SC	SC	WS	SM	SC	SM	WS	WS
TEST DRY PASSING LIQUID PLASTIC BORING FT) (%) (PCF) (%) (%) (%) NO. (FT) (%) (PCF) (%) (%) (%) 1 0-3 11.8 112.5 24.5 39 20 1 1-2 12.3 113.5 23.1 36 20 2 1-2 11.8 113.0 29.6 33 17 3 1-2 11.8 113.0 29.6 33 17 4 0-3 11.3.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 5 1-2 11.8 113.0 29.6 33 17 6 0-3 111.3 23.5	SWELL/ CONSOL (%)	0.2	0.6	0.4			0.7			
TEST DRY PASSING LIQUID PLASTIC BORING FT) (%) (PCF) (%) (%) (%) NO. (FT) (%) (PCF) (%) (%) (%) 1 0-3 11.8 112.5 24.5 39 20 1 1-2 12.3 113.5 23.1 36 20 2 1-2 11.8 113.0 29.6 33 17 3 1-2 11.8 113.0 29.6 33 17 4 0-3 11.3.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 4 1-2 11.8 113.0 29.6 33 17 5 1-2 11.8 113.0 29.6 33 17 6 0-3 111.3 23.5	AASHTO CLASS.	A-2-6	A-2-6	A-2-6	A-1-b	A-1-b	A-2-6	A-1-b	A-2-4	A-2-4
TEST DRY PASSING LIQUID BORING DETH WATER DRY PASSING LIQUID NO. (FT) (%) (PCF) (%) (%) (%) 1 0-3 11.8 112.5 24.5 39 (%) 1 1-2 12.3 113.5 23.1 36 33 2 1-2 11.8 113.0 29.6 33 36 3 1-2 11.8 113.0 29.6 33 36 37 4 0-3 11.3 113.0 29.6 33 36 37 4 1-2 11.8 113.0 29.6 33 37 36 3 1-2 11.8 113.0 29.6 33 37 36 4 1-2 13.9 111.3 23.5 31 31 37 5 1-2 13.9 111.3 23.5 31 31 31	SULFATE (WT %)			<0.01			<0.01		<0.01	
TEST DRY PASSING BORING DEPTH WATER DRY PASSING NO. (FT) (%) (PCF) (%) 1 0-3 11.8 112.5 24.5 1 1-2 12.3 113.5 23.1 2 1-2 11.8 113.5 23.1 3 1-2 11.8 113.0 29.6 4 1-2 13.9 111.3 23.5 5 1-2 13.9 111.3 23.5 3 10 31.9 13.9 11.3	PLASTIC INDEX (%)	20	20	17	dN	ЧP	16	NP	NP	٩N
TEST DRY BORING DEPTH WATER DRY NO. (FT) (%) (PCF) 1 0-3 11.8 112.5 1 1-2 12.3 113.5 2 1-2 12.3 113.5 3 1-2 11.8 113.0 3 1-2 11.8 113.0 3 1-2 11.8 113.0 3 1-2 11.8 113.0 3 1-2 11.8 113.0 3 1-2 11.8 113.0 3 1-2 13.9 111.3 5 1-2 13.9 111.3 3 10 13.9 111.3	LIQUID LIMIT (%)	39	36	33	N	NV	31	٨٧	NV	NV
TEST DEPTH WATER BORING DEPTH WATER NO. (FT) (%) 1 0-3 11.8 1 1-2 12.3 2 1-2 12.3 3 1-2 11.8 4 0-3 11.8 5 1-2 13.9 3 1-2 13.9 4 5 1-2		24.5	23.1	29.6	18.8	17.8	23.5	19.3	31.9	19.1
TEST BORING NO. NO. 2 2 3 3 3 5 5 4 4 4 4 4 4 4 4 4 2 2 2 2 2 2 2 3 3 3 3		112.5	113.5	113.0			111.3	-	-	
TEST BORING NO. NO. 2 2 3 3 3 5 5 4 4 4 4 4 4 4 4 4 2 2 2 2 2 2 2 3 3 3 3	WATER (%)	11.8	12.3	11.8			13.9			
	DEPTH (FT)	6-3	1-2	1-2	1-2	ი. ი	1-2	1-2	10	5
Solt TYPE 1 1 1 1 1 1 3 3 3 3 3 3 3 3	TEST BORING NO.	-	-	2	e	4	4	5	9	4
	SOIL	1, CBR	1	-	1	2	2	e	8	6

FIGURE



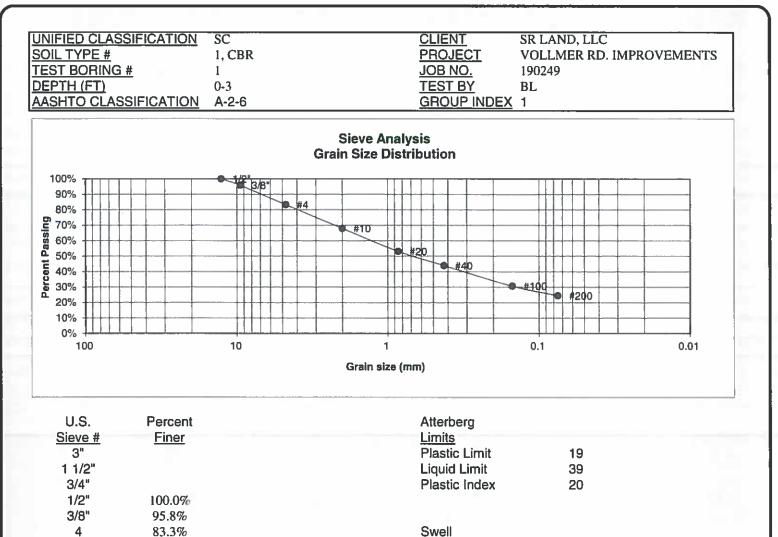
APPENDIX A: Test Boring Logs

TEST BORING NO. 1 DATE DRILLED 3/28/2019 Job # 190249	TEST BORING NO. 2 DATE DRILLED 3/28/2019 CLIENT SR LAND, LLC LOCATION VOLLMER RD. IMPROVEMENTS												
REMARKS DRY TO 5', 3/28/19	Depth (ft) Symbol	Samples	Blows per foot	Watercontent %	Type	REMARKS DRY TO 5', 3/28/1	9	Depth (ft)	Symbol		Blows per foot	Watercontent %	Soil Type
FILL O-5', SAND, CLAYEY, FINE TO COARSE GRAINED, BROWN, LOOSE TO MEDIUM DENSE, MOIST	5 4.		9 17	14.9 10.9	1	FILL 0-5', SAND, CLA TO COARSE GRAINE LOOSE TO MEDIUM D MOIST	D, BROWN,	5				12.7 14.0	1
	15							15					
				• •	• .30	•		• •					
ENTECH ENGINEERING 505 ELKTON DRIVE COLORADO SPRINGS, C	, INC.	907		DRAV	VN;	TEST DATE:	BORING L		ATE /	19		19	DB NO.: 90249 G NO.: A- 1

TEST BORING NO. 3 DATE DRILLED 3/28/2019 Job # 190249	TEST BORING NO.4DATE DRILLED3/28/2019CLIENTSR LAND, LLCLOCATIONVOLLMER RD. IMPROVEMENTS											
REMARKS DRY TO 10', 3/28/19	Depth (ft) Symbol	Samples	Blows per foot	Watercontent %	Soil Type	REMARKS DRY TO 5', 3/28/19	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
FILL O-9', SAND, SILTY, FINE TO COARSE GRAINED, BROWN, MEDIUM DENSE, MOIST	5		21 21	7.2 6.2	=1	SAND, SILTY WITH A CLAY LENSE, FINE TO COARSE GRAINED, BROWN, LOOSE, MOIST SANDSTONE, SILTY, FINE TO COARSE GRAINED, BROWN, DENSE, MOIST	5			8	12.0 11.4	2
SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, DENSE, MOIST	10 - - 15 - -		36	8.0	3		10 15					
	20_						20					
							÷					
ENTECH ENGINEERING 505 ELKTON DRIVE COLORADO SPRINGS, C	, INC.	500		DRAV	WN:	DATE: CHECKED:		DATE /17/	/		19	DB NO.: 90249 IG NO.: A- 2

TEST BORING NO. 5 DATE DRILLED 3/28/201 Job # 190245	9						TEST BORING NO DATE DRILLED CLIENT LOCATION	SR LAND VOLLMEF		IMP	RO	VEM	ENT	6
REMARKS DRY TO 10', 3/28/19 SAND, SILTY, BROWN SANDSTONE, SILTY, FINE TO COARSE GRAINED, BROWN, DENSE TO VERY DENSE, MOIST	(i) 10 15 20	Symbol	Samples	9 8 8 8 8 9 8 8 9 8 8 9 8 8 9 8 9 8 9 8	% Matercontent % 8.2	ω ω Ν Soil Type	REMARKS		10 15 20			Blows per foot	Watercontent %	Soil Type
	1						TEST	BORING L	0G					JOB NO. 90249

APPENDIX B: Laboratory Test Results



Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

ENTECH ENGINEERING, INC.
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

10

20

40

100

200

68.0%

53.1%

43.9%

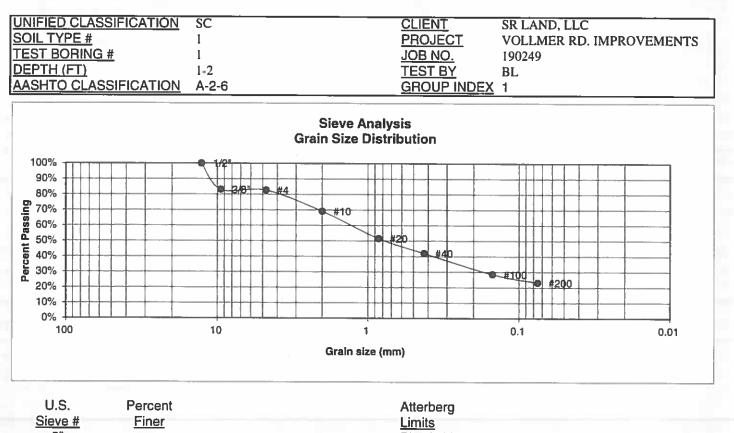
30.7%

24.5%

LABOF RESUL		Y TEST	
DATE:	CHECH	KED:	Y LIT LIG

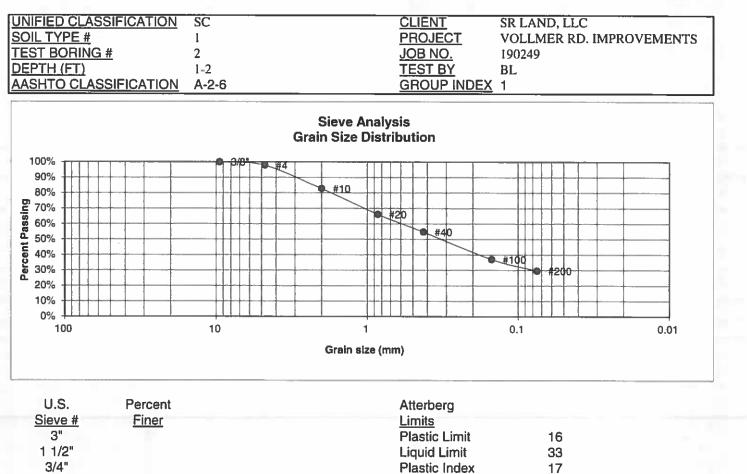
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B-(



<u>Sieve #</u> 3"	Finer	Limits Plastic Limit	17
1 1/2"		Liquid Limit	36
3/4"		Plastic Index	20
1/2"	100.0%		
3/8"	83.1%		
4	82.6%	<u>Swell</u>	
10	69.1%	Moisture at start	
20	51.6%	Moisture at finish	
40	42.0%	Moisture increase	
100	28.5%	Initial dry density (pcf)	
200	23.1%	Swell (psf)	

\diamond	ENTECH ENGINEERING, INC.	LABORATORY TEST RESULTS			JOB NO.: 190249 FIG NO.:	
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN	DATE:		DATE 4/17/19	B-2



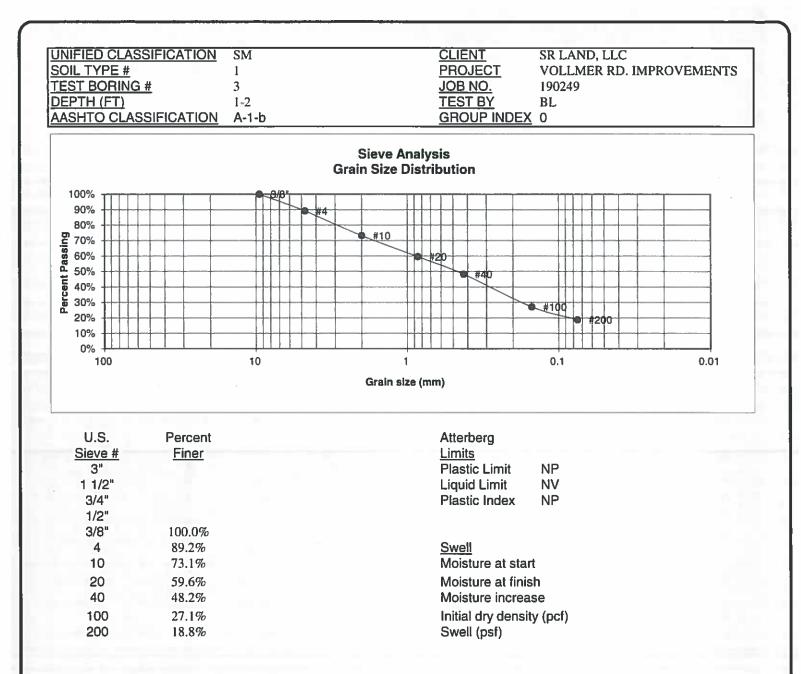
1/2"		
3/8"	100.0%	
4	97.8%	Swell
= 10 =	82.7%	Moisture at start
20	66.1%	Moisture at finish
40	54.7%	Moisture increase
100	37.0%	Initial dry density (pcf)
200	29.6%	Swell (psf)

DRAWN:

	ENTECH
	ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

LABORATORY TEST RESULTS			
	DATE;		DATE

JOB NO.:
190249
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2-2



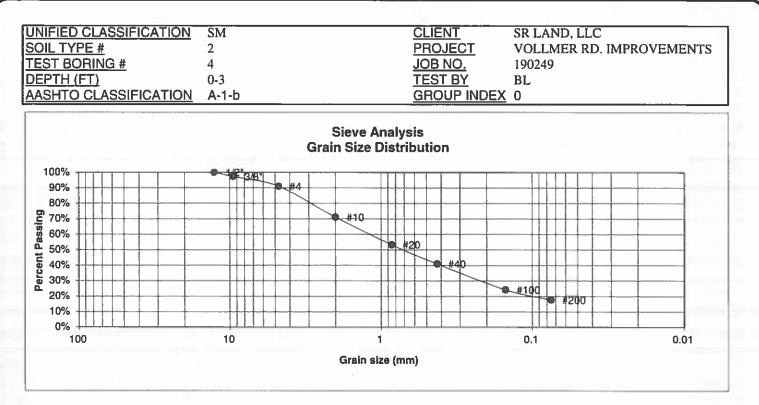
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ENGINEERING, INC.
505 ELKTON DRIVE
COLORADO SPRINGS, COLORADO 80907

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DATE:		DATE:

DRAWN:

JOB NO :
190249 FIG NO.:
B-4

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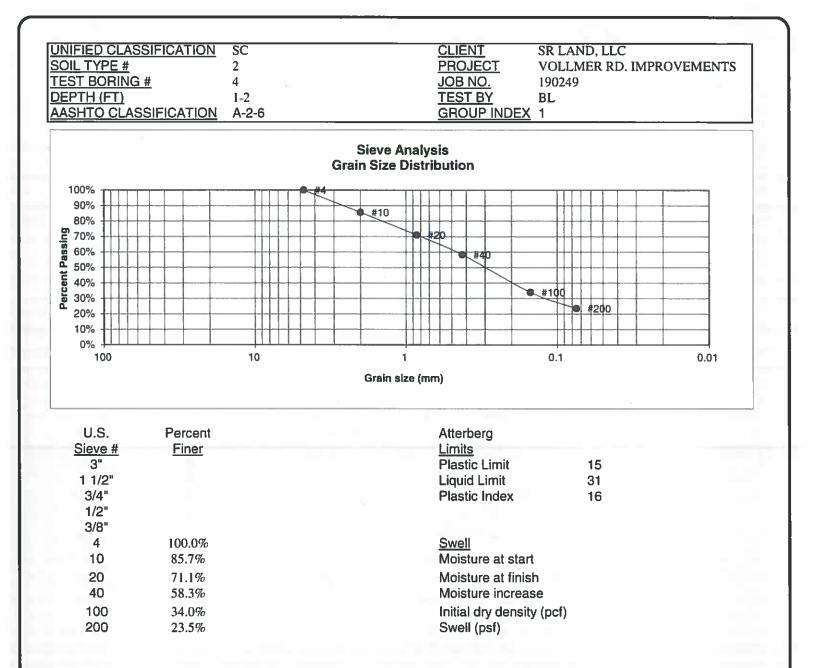


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit NP Liquid Limit NV Plastic Index NP	
1/2" 3/8" 4 10	100.0% 97.3% 91.0% 71.1%	<u>Swell</u> Moisture at start	
20 40 100 200	53.3% 41.0% 24.2% 17.8%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)	

	ENTECH
	ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

	LABORATORY TEST RESULTS			ſ
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190249
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2-5

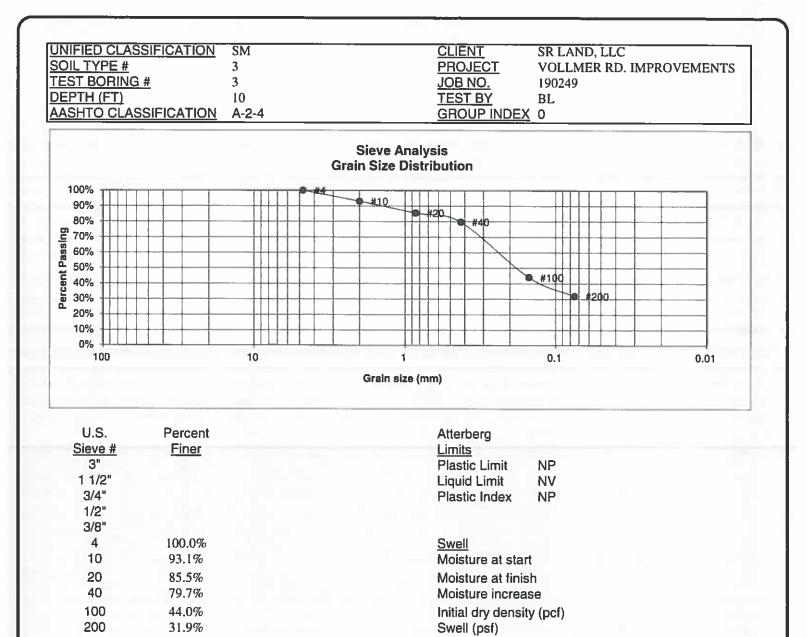


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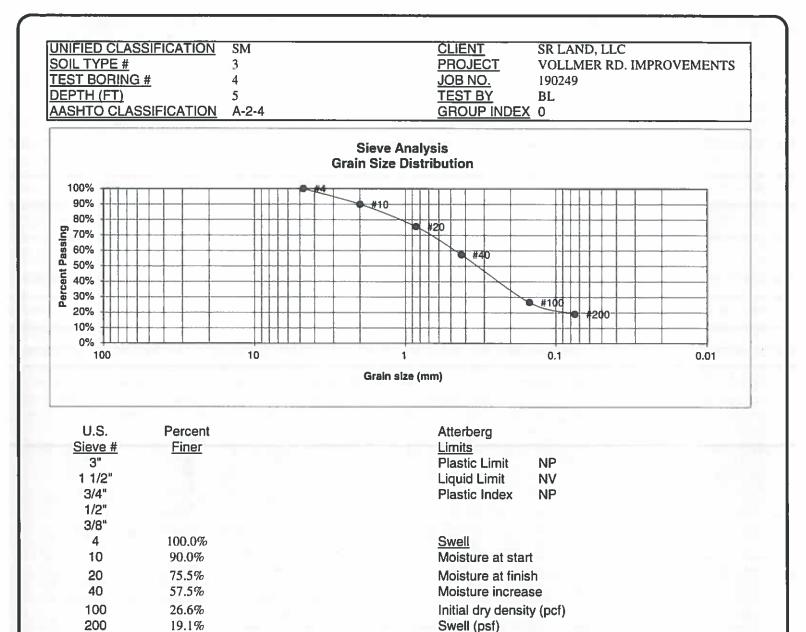


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	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	1	DRAWN:	DATE:	CHECKED:

JOB NO:
190249 FIG NO.:
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DATE: 4/17/19

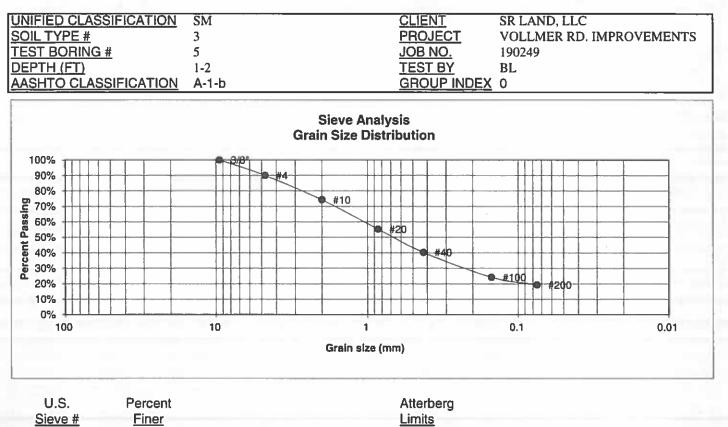
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505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

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FIG NO
B-8



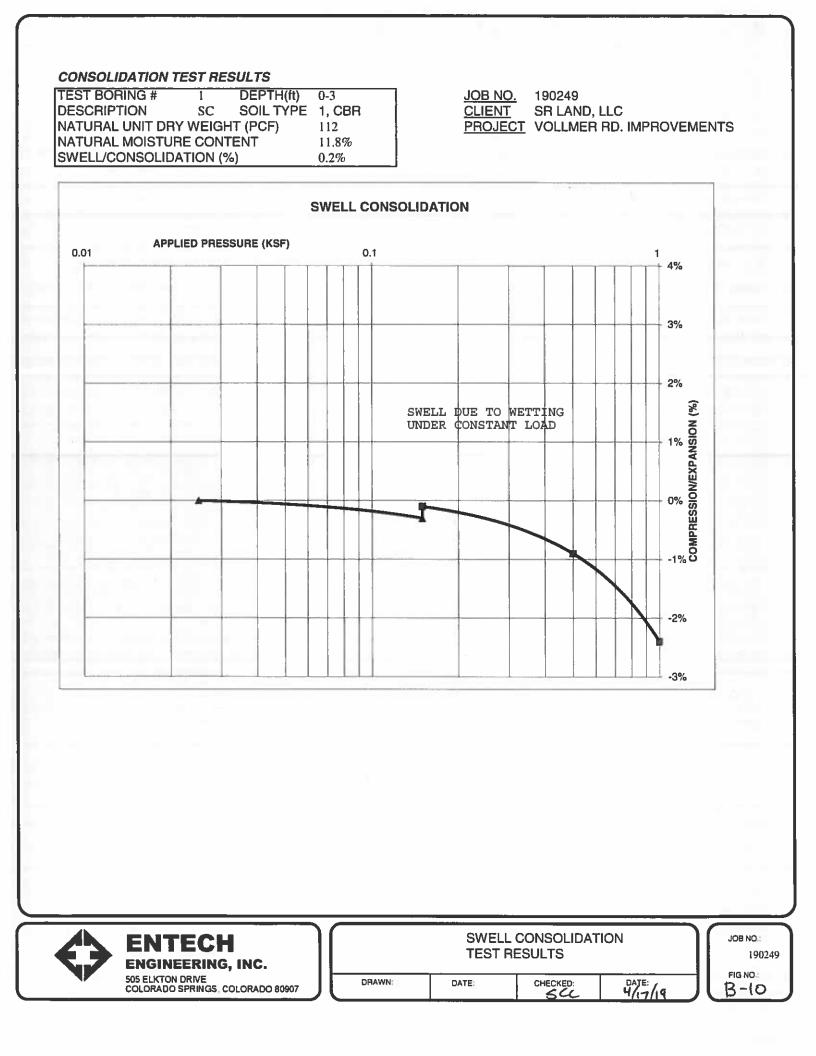
Sieve #	<u>Finer</u>		Limits
3"	2		Plastic Limit NP
1 1/2"			Liquid Limit NV
3/4"			Plastic Index NP
1/2"			
3/8"	100.0%		
4	89.9%		Swell
10	74.2%		Moisture at start
20	55.3%		Moisture at finish
40	40.2%	47	Moisture increase
100	24.2%		Initial dry density (pcf)
200	19.3%		Swell (psf)



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LABORATORY TEST RESULTS				
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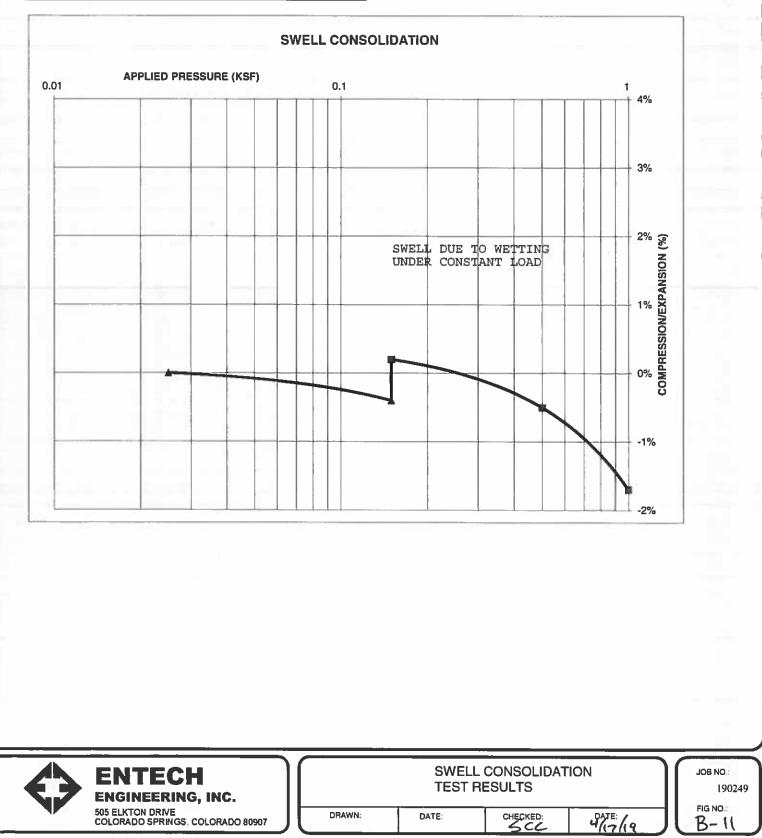
JOB NO.: 190249 FIG NO.: B-9



CONSOLIDATION TEST RESULTS

TEST BORING #	1	DEPTH(ft)	1-2	Ī
DESCRIPTION	SC	SOIL TYPE	1	
NATURAL UNIT DRY	WEIG	HT (PCF)	113	
NATURAL MOISTUR	E CON	TENT	12.3%	
SWELL/CONSOLIDA	TION (S	%)	0.6%	

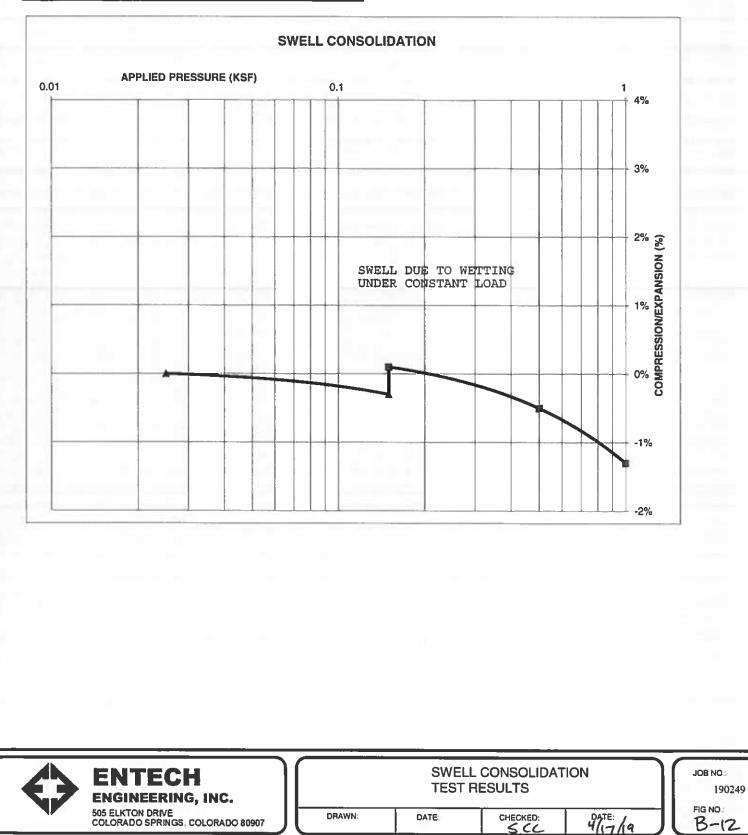
JOB NO. 190249 CLIENT SR LAND, LLC PROJECT VOLLMER RD. IMPROVEMENTS



CONSOLIDATION TEST RESULTS

ĺ	TEST BORING #	2	DEPTH(ft)	1-2
ĺ	DESCRIPTION	SC	SOIL TYPE	1
	NATURAL UNIT DR'	Y WEIGH	IT (PCF)	113
	NATURAL MOISTUR	RE CONT	FENT	11.8%
	SWELL/CONSOLID/	ATION (?	6)	0.4%

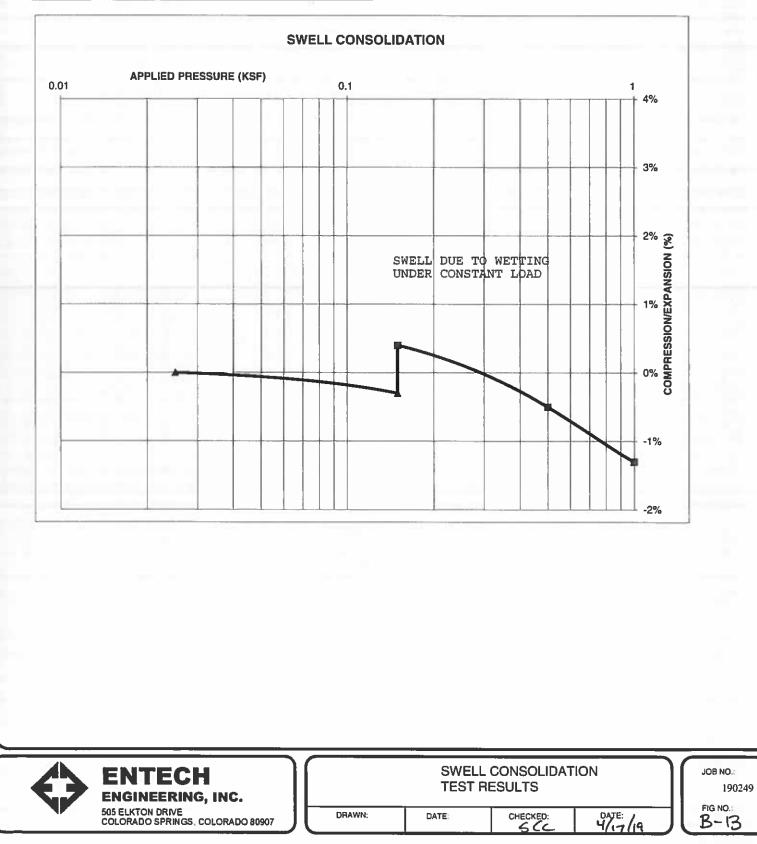
JOB NO. 190249 CLIENT SR LAND, LLC PROJECT VOLLMER RD. IMPROVEMENTS

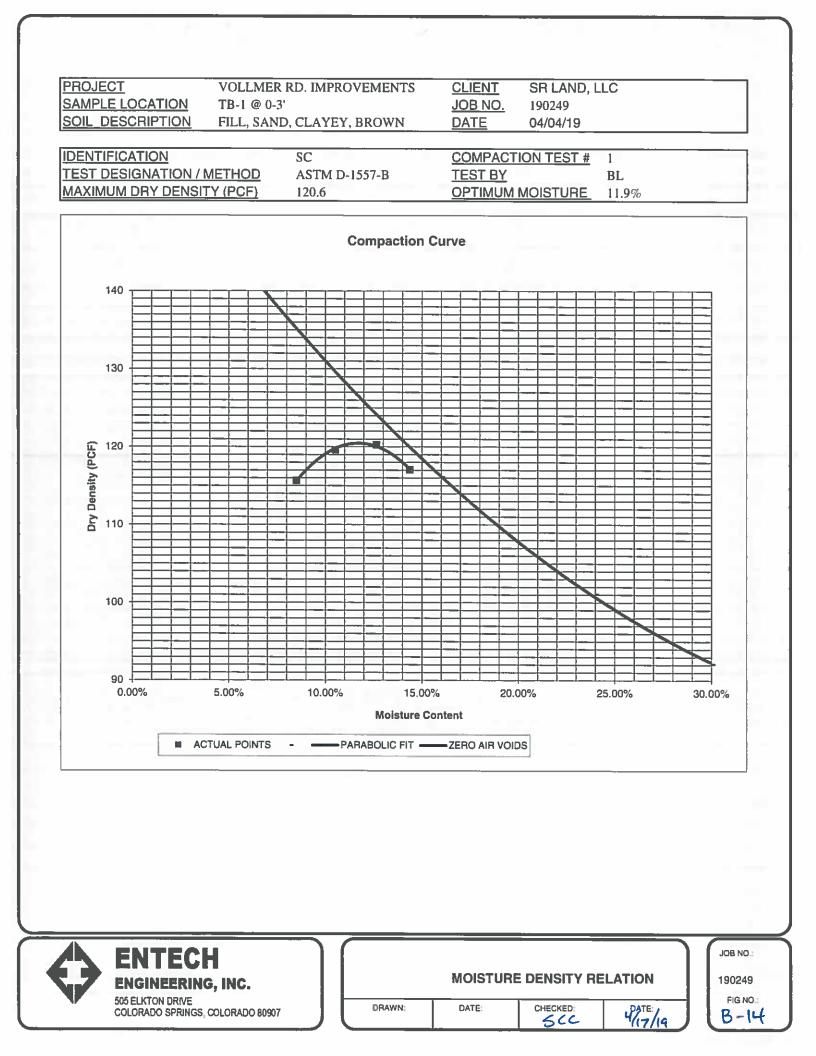


CONSOLIDATION TEST RESULTS

TEST BORING #	4	DEPTH(ft)	1-2
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	WEIGH	HT (PCF)	111
NATURAL MOISTUR	E CON	FENT	13.9%
SWELL/CONSOLIDA	TION (9	%)	0.7%

JOB NO.	190249
CLIENT	SR LAND, LLC
PROJECT	VOLLMER RD. IMPROVEMENTS





CBR TEST LOAD DATA

PISTON

PISTON

JOB NO: 190249 CLIENT: SR LAND, LLC PROJECT: VOLLMER RD. IMPROVEMENTS SOIL TYPE: 1

					D. IIVII KO V LI	
DIAMETER (cm)	AREA (in ²)		SOIL TYPE:	1		
4.958	2.99250919	-	_			
	10 BLOWS		25 BLOWS		56 BLOWS	
PENETRATION	MOLD #	7	MOLD #	6	MOLD #	12
DEPTH	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS
(INCHES)	(LBS)	(PSI)	(LBS)	(PSI)	(LBS)	(PSI)
0.000	0	0.00	0	0.00	0	0.00
0.025	59	19.72	88	29.41	96	32.08
0.050	86	28.74	138	46.12	187	62.49
0.075	121	40.43	174	58.15	254	84.88
0.100	143	47.79	216	72.18	299	99.92
0.125	184	61.49	267	89.22	330	110.28
0.150	191	63.83	309	103.26	392	130.99
0.175	211	70.51	354	118.30	415	138.68
0.200	237	79.20	395	132.00	476	159.06
0.300	325	108.60	535	178.78	601	200.83
0.400	390	130.33	640	213.87	723	241.60
0.500	461	154.05	741	247.62	851	284.38

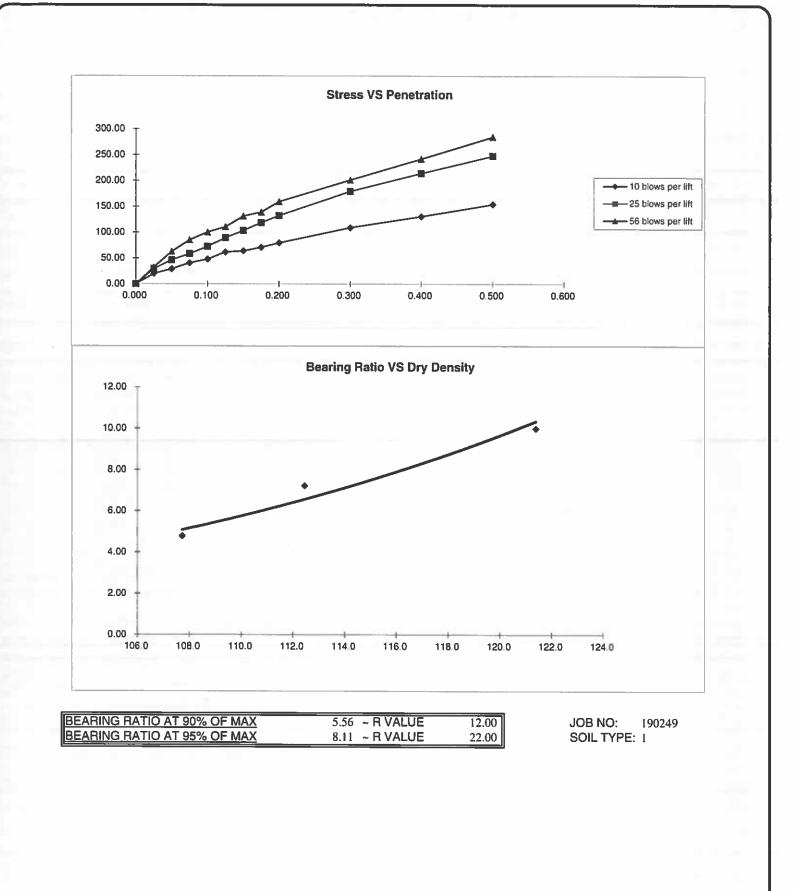
FINAL MOISTURE CONTENT

	MOLD #	7	MOLD #	6	MOLD #	12
CAN #		359	-	356		353
WT. CAN		6.75	1	6.86		6.82
WT. CAN+WET		177.81		196.61		182.09
WT. CAN+DRY		157.54		175.48		163.5
<u>WT. H20</u>		20.27		21.13		18.59
WT. DRY SOIL		150.79		168.62		156.68
MOISTURE CONTENT		13.44%		12.53%	=	11.86%
WET DENSITY (PCF)		120.5		125.8		135.8
DRY DENSITY (PCF)		107.7		112.5		121.4
BEARING RATIO		4 79		7.00		0.00
BEARING RATIO		4.78		7.22		9.99
90% OF DRY DENSITY	109.2					
95% OF DRY DENSITY	115.3					
BEARING RATIO AT 90% OF MAX		5.56	~ R VALUE	12		
BEARING RATIO AT 95% OF MAX		8.11	~ R VALUE	22		
					1	



	CBR TEST DATA					
					F	
J	DRAWN:	DATE:	CHECKED:	DATE:	B-	

JOB NO.: 190249 FIG NO.: B-15



\bigcirc	ENTECH ENGINEERING, INC.		CALIFOR	INIA BEARING	RATIO	JOB NO.: 190249 FIG NO.:
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE		DATE /19	B-16

CLIENT	SR LAND, LLC	JOB NO.	190249
PROJECT	VOLLMER RD. IMPROVEMENTS	DATE	4/12/2019
LOCATION	VOLLMER RD. IMPROVEMENTS	TEST BY	BL
			-

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-1	1-2	1	SC	<0.01
TB-4	1-2	2	SC	<0.01
TB-3	10	3	SM	<0.01
	A			
100				· · · · · · · · · · · · · · · · · · ·
			-	
				-
-				

QC BLANK PASS



			RATORY TEST		JOB NO.: 190249 FIG NO.:
J	DRAWN:	DATE:		4/1-7/19	B-17

APPENDIX C: Pavement Design Calculations

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA

VOLLMER ROAD IMPROVEMENTS - URBAN MINOR ARTERIAL

SOIL TYPE 1, CBR #1

Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL $(W_{18}) =$	1,971,000
Hveem Stabilometer (R Value) Results:	R =	22
Standard Deviation	$S_o =$	0.45
Loss in Serviceability	Δpsi =	2.5
Reliability	Reliability =	85
Reliability (z-statistic)	$Z_R =$	-1.04
Soil Resilient Modulus	M _R =	5273
Weighted Structural Number (WSN):		WSN =

Weighted Structural Number (WSN):

DESIGN TABLES AND EQUATIONS

$S_1 = [(R - 5) / 11.29] + 3$
$M_{\rm P} = 10^{[(S_1 + 18.72)/6.24]}$

 $k = M_{\rm R}/19.4$ Where: M_R = resilient modulus (psi) S₁ = the soil support value R = R-value obtained from the Hveem stabilometer CBR = California Bearing Ratio

Reliability (%)	Z _R (z-statistic)
80	-0.84
85	-1.04
90	-1.28
93	-1.48
94	-1.56
95	-1.65
96	-1.75
97	-1.88
98	-2.05
99	-2.33
99.9	-3.09
99.99	-3.75

 $\log_{10}W_{18} = Z_R^* S_0^+ 9.36^* \log_{10}(SN+1) - 0.20 + ----$

Left Right

6.29

6.29

Difference

0.0

$$\log_{10} \left[\frac{\Delta PSI}{4.2 - 1.5} \right]$$

$$0.40 + \frac{1094}{(SN+1)^{5.19}}$$

+ 2.32*log10MR- 8.07

3.88

Fig. No. C-1

DESIGN CALCULATIONS

DESIGN DATA VOLLMER ROAD IMPROVEMENTS - URBAN MINOR ARTERIAL

SOIL TYPE 1, CBR # 1		
Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL = 1	,971,000
Hveem Stabilometer (R Value) Results:	R =	22
Weighted Structural Number (WSN):	WSN =	3.88

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Aggregate Base Course

 D_1 = Depth of Asphalt (inches) D_2 = Depth of Base Course (inches)

FOR FULL DEPTH ASPHALT SECTION (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 8.8$ inches of Full Depth Asphalt Use 9.0 inches Full Depth

FOR ASPHALT + AGGREGATE BASE COURSE SECTION

Asphalt Thickness (t) = 5.5 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 13.3$ inches of Aggregate Base Course, use 13.5 inches

RECOMMENDED ALTERNATIVES

- 1. 5.5 inches of Asphalt + 13.5 inches of Aggregate Base Course, or
- 2. 9.0 inches of Asphalt

Job No. 190249 Fig. No. C-2

DESIGN CALCULATIONS

DESIGN DATA VOLLMER ROAD IMPROVEMENTS - URBAN MINOR ARTERIAL

SOIL TYPE 1, CBR # 1		
Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL = 1,971,000)
Hveem Stabilometer (R Value) Results:	R = 22	
Weighted Structural Number (WSN):	WSN = 3.88	

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Recyled Concrete Base Course

 D_1 = Depth of Asphalt (inches) D_2 = Depth of Base Course (inches)

FOR FULL DEPTH ASPHALT SECTION (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 8.8$ inches of Full Depth Asphalt Use 9.0 inches Full Depth

FOR ASPHALT + RECYCLED CONCRETE BASE COURSE SECTION

Asphalt Thickness (t) = 5.5 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 13.3$ inches of Recycled Concrete Base Course, use 13.5 inches

RECOMMENDED ALTERNATIVES

- 1. 5.5 inches of Asphalt + 13.5 inches of Recycled Concrete Base Course, or
- 2. 9.0 inches of Asphalt

Job No. 190249 Fig. No. C-3