

# **FINAL DRAINAGE REPORT**

for

# BLACK FOREST OFFICE The North Half of the NE Quarter of the SE Quarter of Section 7 Township 12 South, Range 65 West of the 6<sup>th</sup> P.M. County of El Paso, State of Colorado 12740 Black Forest Road Colorado Springs, Colorado 80908

2N Civil Job No. 19015 September 11, 2020 Revised November 20, 2020 Revised January 19, 2021

PREPARED FOR: Black Forest, LLC 8655 Table Butte Road Colorado Springs, Colorado 80908-1224 Contact: Rad Jackson, Project Manager

Engineer: 2N Civil, LLC 6 Inverness Court East, Suite 125 Englewood, Colorado 80112 Contact: Ryan Eichele, PE, Project Manager Todd West, PE Project Engineer



#### **Engineer's Statement**

The attached drainage plan and report were prepared under my direct supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions in preparing this report.

SIGNATURE: \_\_\_\_\_\_ Todd Eric West, PE Colorado Registration No. 37643 For and on behalf of 2N Civil, LLC

#### **Developer's Statement**

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name

By:			
Title:		 	
Address:			

#### El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E. County Engineer / ECM Administrator Date

Conditions:



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#### 1) GENERAL LOCATION AND DESCRIPTION

#### (a) Location

The Black Hills Office property, addressed as 12740 Black Hills Road, is the north half of the Northeast Quarter of the Southeast Quarter of Section 7, Township 12 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, County of El Paso, State of Colorado. Black Forest Road bounds the site on the east. Rural Residential development (Zoning RR-5) surrounds the site on the north, south, and west. An existing asphalt and gravel road provides access to the vacant parcel. There are no major drainageways on the site.

#### (b) Description of property and Proposed Improvements

The subject property contains approximately 4.83 acres. Sparse ground cover consists of native weeds with a few trees at the northeast corner of the site. A shallow ridgeline divides the site, directing the east portion of the site to the north, and the west portion of the site to the west. The National Resources Conservation Service Web Soil Survey classifies the in situ soils as Hydrologic Group B, which exhibit a moderate infiltration rate when thoroughly wet.

There are no major drainage ways or irrigation facilities on the site. Existing gas and electric facilities run along the property frontage adjacent to Black Forest Road, but do not affect the development of the site.

The development will consist of a single story 4,400 sf office building with a full, walk-out basement of equal size with a 3,250-sf studio/shop building on the 4.83 acres. The office building will house the Owner's corporate functions for Metal Roof Innovations, Ltd. company (strategic planning, accounting, sales/marketing management).

An existing barn (currently under construction) was permitted under the A-5 zoning. Construction began in the spring of 2020. The barn will be re-purposed in use as a studio/shop to supplement the corporate functions. No manufacturing, warehousing, shipping, wholesale or retail sales will take place at this facility.

#### 2) DRAINAGE BASINS AND SUB-BASINS

(a) Major Basin Description

The site is tributary to the upper reach of Kettle Creek drainage basin (FOMO3000),



that flows from north to south approximately 1,500 feet west of the site. The report Drainage Basin Planning Study for Kettle Creek Basin was reviewed in the preparation of this report. The Study is a planning document and is not intended as a basis for final design, and thus has no direct influence on the design of this site. Developed flows will be attenuated as described in this report in order to follow the historic discharge rates as described in the Study.

Based on the FEMA Map No. 08041C0315G, Panel 315 of 1300, with an effective date of 12/07/18 the site is located within Zone X, areas of minimal flood hazard. No portion of the site is located within the 100 year floodplain. The FIRM Map is included in the Appendix on page 17. The upper reach of the Kettle Creek basin is sparsely developed and includes single family homes on large acreages.

#### (b) Sub-Basin Description

The site historically drains north and west. The site has been divided into three subbasins, H-1, H-2, and H-3 and design points have been provided at each to identify the historic rate of discharge form the site (refer to Historic Basin Map included at the end of this report). A portion of Black Forest Road flows east onto the site, and is included in Basin H-2. These offsite flows will continue to follow their historic drainage path onto the site and will flow north and east to design point H2 (historic) and P2 (proposed) following development of the site.

The development of the site will occur on the upper portion of the lot, with the majority of the new impervious areas directed to a proposed detention facility that will intercept flow prior to discharge to the west.

#### 3) DRAINAGE DESIGN CRITERIA

(a) Development Criteria Reference

The City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2 (DCMV1 & DCMV2) was utilized per El Paso County's stormwater quality design criteria as well as the applicable standards from the County's Engineering Criteria Manual (ECM).

(b) Hydrologic Criteria

The Rational Method was selected to calculate existing and proposed runoff rates from the site for the 5 year (minor storm) and 100 year (major storm) recurrence intervals. The design rainfall will be from DCMV1 Table 6-2 Rainfall Depths for Colorado Springs.



Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth
2	1.19	1.70	2.10
5	1.50	2.10	2.70
10	1.75	2.40	3.20
25	2.00	2.90	3.60
50	2.25	3.20	4.20
100	2.52	3.50	4.60

#### Table 6-2. Rainfall Depths for Colorado Springs

Where Z= 6,840 ft/100

The most current version of UDFCD's Peak Runoff Prediction by the Rational Method, Version 2.00 released May 2017 was used to determine flows. The Runoff Coefficients from DCMV1, Table 6-6 were input to determine peak runoff values.

The development will implement Full Spectrum Detention (FSD) utilizing an Extended Detention Basin (EDB) to capture and treat runoff prior to discharge downstream. Full Spectrum Detention (FSD) is a design concept that provides control of the full range of runoff rates that pass through detention facilities.

#### 4) DRAINAGE FACILITY DESIGN

#### (a) General Concept

The area being developed has been divided into three subbasins. Basin PR-1 includes the paved parking area and portions of the buildings (office and warehouse) and perimeter landscaping. Basin PR-1 will flow within the asphalt parking lot to a new 5' Type R inlet, where it will be conveyed to the pond via an 18" RCP pipe. Due to the small size of the development, per the UD-BMP\_v3.07 spreadsheet by MHFD, a forebay is not necessary for this size site.

Basin PR-2 will collect flow from a portion of the office roof, which will be conveyed to the detention basin via an earthen swale. Basin PR-3, located along the northern limit of the development, will flow north following the historic drainage path and is not tributary to the proposed pond.

Basins PR-4 and PR-5 include areas in which the historic and proposed impervious values will not be affected by the development of the site. These basins have been



delineated to compare historic discharge rates to those following development. As shown within the Summary Runoff Table included on the Historic Basin Map and Proposed Basin Map and included below, development of the site will result in a decrease in discharge rates at the design points that are located where flows exit the site.

The imperviousness value of 45.61%, which represents the composite value for the area tributary to the pond, was used to determine the required EDB. The UD-Detention spreadsheet can be found in the Appendix.

The drainage concept for the development does not alter historic drainage patterns. The detention pond will act to limit the stormwater release rate to predevelopment conditions.

(b) Specific Details

The development will implement Full Spectrum Detention (FSD) utilizing an Extended Detention Basin (EDB) to capture and treat runoff prior to discharge downstream. The proposed detention pond is designed using the UDFCD spreadsheet, UD-Detention v.4.03. This design considers the water quality capture volume (WQCV), excess urban runoff volume (EURV), and 100-year detention volume. The EDB serves to limit the release rate to pre-development conditions. This is illustrated by the decrease in flow from historic to proposed conditions when comparing design point H1 to P1, H2 to P2, and H3 to P3 (historic and proposed, respectively) as shown in the tables below. Refer the accompanying drainage maps for locations of design points.

HISTORIC COI	HISTORIC CONDITIONS						
DESIGN POINT	CONTRIBUTING BASIN(S)	CONTRIBUTING AREA (AC)	Q₅ (cfs)	Q <sub>100</sub> (cfs)	NOTES:		
H1	H-1	1.72	0.63	5.86	Releases undetained (following historic flow path)		
H2	H-2	2.96	1.97	9.75	Releases undetained (following historic flow path)		
Н3	H-3	0.23	0.11	0.83	Releases undetained (following historic flow path)		



PROPOSED CONDITIONS						
DESIGN POINT	CONTRIBUTING BASIN(S)	CONTRIBUTING AREA (AC)	Q₅ (cfs)	Q <sub>100</sub> (cfs)	NOTES:	
P1	PR-1, PR-2, PR-4	2.16	0.47	4.62	Releases offsite (developed basins PR-1 and PR-2 are detained prior to release)	
P2	PR-3	2.60	1.53	8.33	Releases undetained (following historic flow path)	
Р3	PR-5	0.15	0.05	0.52	Releases undetained (following historic flow path)	

The outlet of the EDB pond has been directed to the flowline of an existing drainageway, serving to minimize the potential for erosion. In addition, a low tailwater basin will be installed at the end of the EDB pond outfall pipe. This feature consists of a riprap-lined depression that will dissipate the energy of the pond discharge. This design, together with the net decrease in flow from historic conditions, will serve to protect downstream drainageways.

A ten-foot-wide gravel maintenance path provides access to the EDB. The path will provide vehicular access to the bottom of the pond for removing sediment and debris that will collect in the trickle channel and outlet works. The report titled *Stormwater Best Management Practices Inspection and Maintenance Plan (IM Plan) for Black Forest Office*, prepared by 2N Civil for the Owner and/or his assigns, shall be followed to ensure the ongoing performance of the drainage facilities associated with this project.

The cost estimate for the proposed drainage improvements is provided on page 34 in the Appendix of this report.

The Developer shall be responsible for all associated drainage impact fees including, but not limited to, the Drainage Basin Fees associated with the development of this project as outlined in the El Paso County Municipal Code.

#### 5) OTHER GOVERNMENT AGENCY REQUIREMENTS

A permit issued by the *State of Colorado for Stormwater Discharges Associated with Construction Activity* detailing construction management BMPs will be obtained prior to construction activities.

No other government agency requirements are anticipated for this project.



#### 6) DRAWING CONTENTS

(a) General Location Map

A Vicinity Map is included in the Appendix.

(b) Drainage Plan

Refer to the Proposed Drainage Plan in the Appendix for basin delineation, drainage routes and flows, and proposed stormwater facilities.

7) CONCLUSION

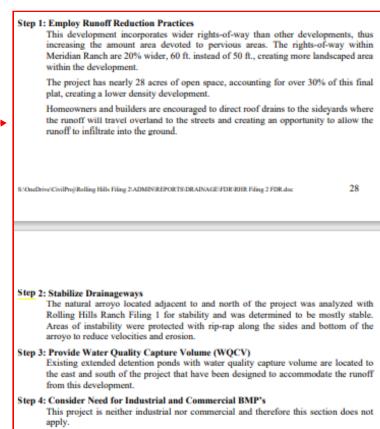
In our professional opinion, the proposed development will pose an insignificant change in the historic drainage patterns of the existing site. The development of the office and warehouse will include construction of an Extended Detention Basin, which will provide detention of the WQCV, EURV, and 100 year flow. This facility will slow the rate of discharge from the site to pre-development conditions and promote infiltration. These runoff reduction measures ensure that the capacity of the downstream drainageways will not be negatively affected by the construction of these improvements.

Please address the 4 step process indicated in ECM Appendix I.7.2. Please list each step and below each step please indicate how it is has been addressed. I have provided an example (see excerpt) as how other consultants address the four step process. —

Also please address drainage basin fees. A statement indicating that drainage basin fees are not due with this site development plan application as you are not platting the lot would be sufficient.

Please feel free to give me a call if you have any questions.

Daniel Torres, 719-208-6783 danieltorres@elpasoco.com





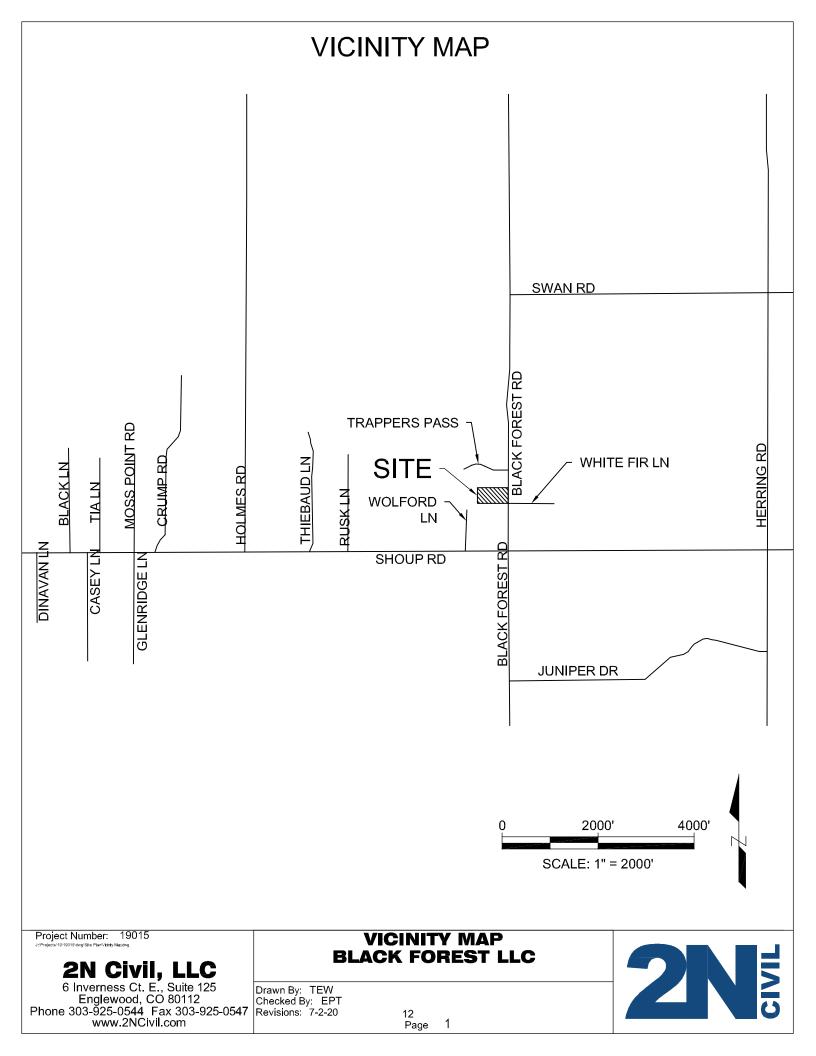
### REFERENCES

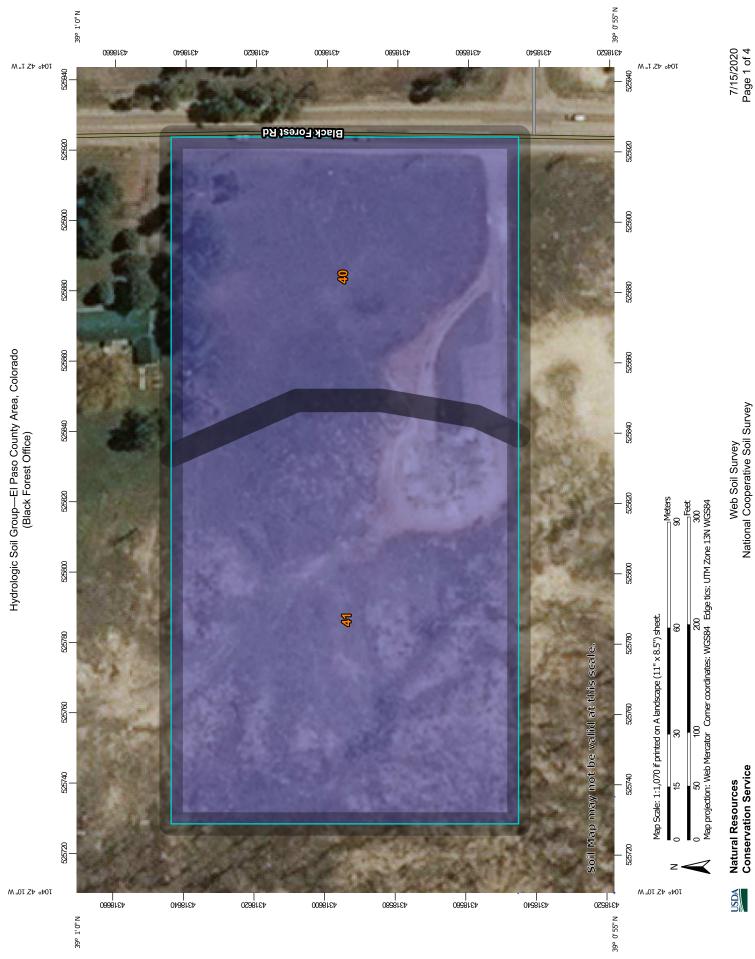
- 1. El Paso County Engineering Criteria Manual (ECM), Revised 12/13/2016.
- 2. Colorado Springs Drainage Criteria Manual Volumes 1 and 2 (DCMV1 & DCMV2), May 2014.
- 3. *Drainage Basin Planning Study for Kettle Creek Basin,* Prepared by JR Engineering, LLC, May 5, 2015.
- Urban Storm Drainage Criteria Manual, Volumes 1, 2, & 3, Urban Drainage and Flood Control District, Volumes 1 & 2 - Originally Published September 1969, Updated March 2017; Volume 3 - Originally Published September 1992, Updated November 2010.
- 5. Stormwater Best Management Practices Inspection and Maintenance Plan (IM Plan) for Black Forest Office, prepared by 2N Civil, LLC, Updated 2020.



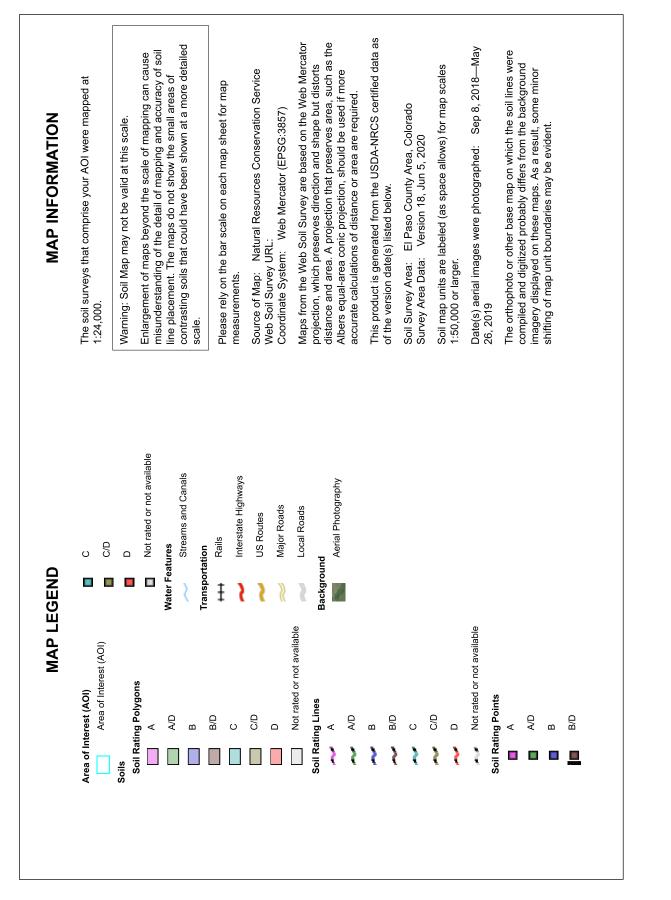
# **APPENDIX A**

Vicinity Map Soils Map FEMA Map





Hydrologic Soil Group—El Paso County Area, Colorado (Black Forest Office)



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
40	Kettle gravelly loamy sand, 3 to 8 percent slopes	В	1.9	40.6%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	В	2.8	59.4%
Totals for Area of Inter	est		4.8	100.0%

# Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

JSDA

# **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

#### NOTES TO USERS

s map is for use in administering the National Flood Insurance Program. It doen necessarily identify all areas subject to flooding, particularly from local drainay reas of small size. The community map repository should be consulted f solibe updated or additional flood hazard information.

obtain more detailed information in areas where Base Flood Elevations (BFE coltain more detailed information in artises where tasks = hood taivations (pi-ts) divide hoodways time to be indetermined, using a tem concepts to consult the Proce-tion Hoodways into the bench determined, using a second second tail and the thirth the Prood Insurance Study (PIS) report that accompanies this FIRM. Users round be aware that BEFs shown on the FIRM represent rounded whele-bench variations. These BFEs are infered for flood levation inferration. Accordingly, old elevation data presented in the FIS report should be utilized in conjunction with eFIRM propriese o construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map appy only landward of 0.0° North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aver that coastal flood elevations are also provided in the Summary of Sallware Elevations table in the Flood Insurance Study report for this jurisdiction. The Summary of Sallware Elevations table simular of Sallware Elevations table should be used for construction and/or index of the study of

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with ergard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdictor.

Certain areas not in Special Flood Hazard Areas may be protected by flood cont structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuran Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse deciator (UTR) zone 13. The horizontal datum was NADSS. GTSS0 spheric production of FIRMS for adjacent prioritoric pression and production of FIRMS for adjacent prioritoricon narry result in sight post differences in map features across jurisdiction boundaries. These differences do no affect the accuracy of this FIRM.

lood elevations on this map are referenced to the North American Vertical Datus 1980 (NAVDB3), "These flood elevations must be compared to structure an oversion between the National Geodetic Vertical Datum of 1923 and the Nor merican Vertical Datum of 1988, visit the National Geodetic Survey vestels -the following and the National Geodetic Survey and the following the National Section 2014 (Section 2014) (Sectio Iress:

GS Information Service: IOAA. N/NGS12 NOAA, N/NGS12 Vational Geodetic Survey SSMC-3, #9202 I315 East-West Highway Silver Spring, MD 20910-3282

obtain current elevation, description, and/or location information for bench mari own on this map, please contact the Information Services Branch of the Nation sodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncsa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Pas-County, Colorado Springe Utilities, City of Fountain, Bureau of Land Management Vational Oceanic and Atmospheric Administration, United States Geological Survey and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurication have been adjusted to confirm to these we stream channel configurations. As stream, the Node Northern to these we stream channel configurations. As stream, the Node Northern to these we stream channels and datances that differ from what is shown on this map. The profile baselines depicted and Floody Polaries and Polaries (in the FIS report. As a result, the profile baselines depicted baselines may device significantly from the new base map channel representation and may appear could of the floodplan.

orporate limits shown on this map are based on the best data available at the tin publication. Because changes due to annexations or de-annexations may ha curred after this map was published, map users should contact appropria ammunity officials to verify current corporate limit locations.

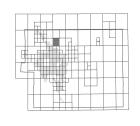
Please refer to the separately printed Map Index for an overview map of the count showing the layout of map panels; community map repository addresses; and using of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community in content.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchang (FMX) 1477-336-2627 for information on available products associated with the FRM. Available products may include pervisually saved Letters of Map Change, FRM. Available products may include pervisually saved Letters of Map Change, the reached perpendicular to 400-356-4000 and is website of the reached perpendicular to 400-356-4000 and is website of 

you have **questions about this map** or questions concerning the National Floo nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) ( sit the FEMA website at http://www.fema.cov/business/nfin

El Paso County Vertical Datum Offset Table					
Flooding Source	Vertical Datum Offset (ft)				
REFER TO SECTION 3.3 OF THE EL PASO COUN FOR STREAM BY STREAM VERTICAL DATUM					





This Digital Flo Cooperating Tec Water Conserva Agency (FEMA). Digital Flood Insurance Rate Map (DFIRM) was produced through a perating Technical Partner (CTP) agreement between the State of Colorado rvation Board (CWCB) and the Federal Emergency Management

Additional Flood Hazard information and resources a

able from local communities and the Colorar



3230000 FT 104" 41' 15.00" 104° 45' 0.00\* 3215000 FT 3220000 FT JOINS PANEL 0305 3225000 FT 201 21 45 000 391 31 45.) SIESTA GRV MONTY PL 66 W. 65 W. EL PASO COUNTY UNINCORPORATED AREAS 00 SECLUDED CREEK 30 29 26 ERRA RIDGE CIR OPEN 987 M/P 1445000 FT 35 COLWTRY ESTATES LN 422200mN ONNAUGHT DR T. 11 S. T. 12 S. T. 11 S. T. 12 S. WILLHAVEN PL FOXCHAS ANA MENOCON IN 1440000 FT 4321000m HOLMES LN COOLWELL DR 5 6 PIEDRA VISTA ST JICARILLA DR EL PASO COUNTY NINCORPORATED AREAS 080059 SCHWENCKS ELEMENTARY DR ZONE D BOUNDARY COINCIDENT WITH FOREST BOUNDARY UANITA ST 1435000 E ZONE AE 7299 7293 AS 7288 738 ADYS LIMITO ZONE D NATIONAL PASO CO 2 mar HIGHLINE PI (a) PIKE NATIONAL FOREST 12 11 UMMINGBIRD L ZONE AE 7310 7316 7321 DARR CI 47-19<sup>200</sup>"N ZONEAE To) Kettle Cree HITE FIR LN Λ BLACK FOREST ZONE AE 24 24 1430000 FT 4318000mN TERRELLIN SITE 13 ZONE AE NIPER DF LEPRECHAUN 8 EL PASO COUNTY UNINCORPORATED AREAS (Z) ZONE AF MILLS BURROWS RD B CSAN' 4317000mN Kettle Creek ۲ 65 3 391 010.001 39° 0 0 00 JOINS PANEL 0527 526007E 1047 417 15 007 \$25000mE 1041 451 0.001 \$2000mg JOINS PANEL 0528 52300mp 524000mp

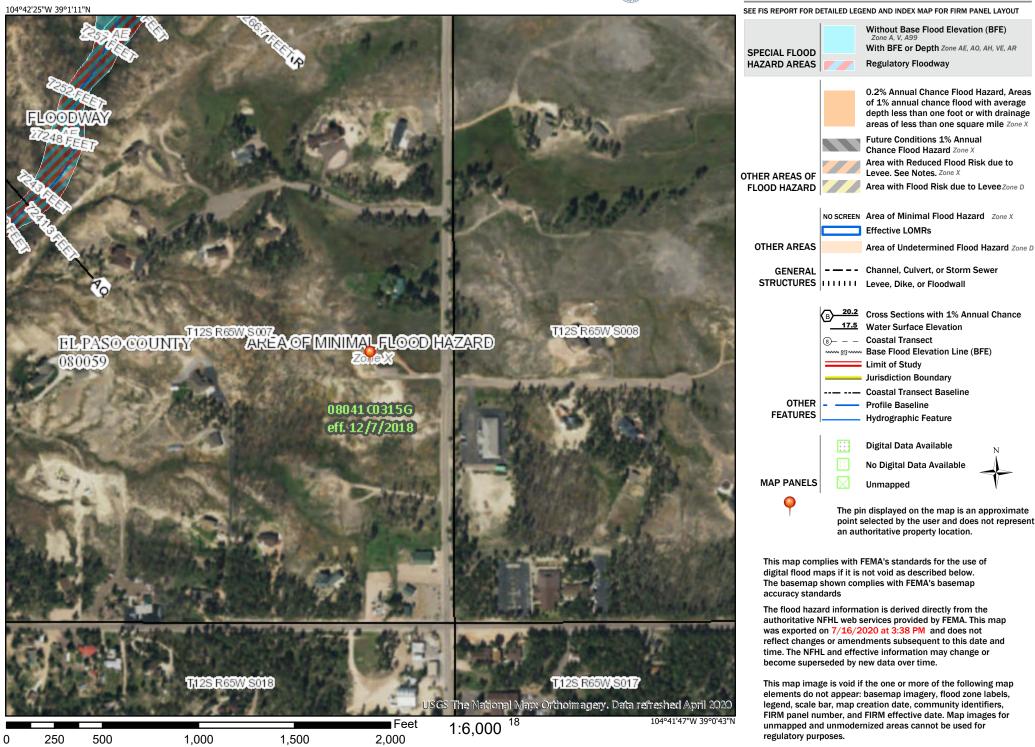
LEGEND SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exteeded in any pixen year. The Special Flood Heard Area is the new subject to flooding by the 1% enrual chance flood. Areas of Special Flood heard include Zenes A, AL, AH, AA, AR, AS, Y, AN VE. The Base Flood Beards in the water-subnet deviation of the values chance flood. No Base Flood Bevations determined. Base Rood Bevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Eevallons determined. ZONE A ZONE AE ZONE AH Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocibles also determined. ZONE AO Spicial Hood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently detertified. Zone All indicates that the former flood control system is being instored to provide protection from the 1% annual chance or greater flood. ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined. FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encreachment so that the 1% annual chance flood can be carried without unistantial increases in flood behalts. OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foct or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X OTHER AREAS ZONE X Areas determined to be outside the 0.2% annual chance floodplain ZONE D Areas in which flood hazards are undetermined, but possible. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) OPAs are normally located within or adjacent to Spe Roodolain boundary Roodway boundar Zone D Boundary ..... CBPS and ORA boundary • Boundary dividing Special Flood Hazard Areas of different Base Flood Bevations, flood depths or flood velocities. ~~ 512 ~~ Base Flood Elevation line and value: elevation in feet\* Base Flood Elevation value where uniform within zone; elevation in feet\* (EL 987) in Vertical Datum of 1988 (NAVD 88) Cross section line 23-----23 Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 97° 07' 30.00° 32° 22' 30.00° 1000-meter Universal Transverse Mercator grid ticks zone 13 47500+N 6000000 FT 000-foot grid ticks: Colorado State Plane coorc ystem, central zone (FIPSZONE 0502), ambert Conformal Conic Projection Bench mark (see explanation in Notes to Users section of this FIRM panel) DX5510 M1.5 River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(8) OF REVISION(8) TO THIS PANE 7, 2018 - to update corporate limits, to change Base Floo Hazard Avaia, to update map format, to add roads and ro incorporate previously issued Latters of Map Revision. For community map revision history prior to countywide mapping, refer to the Con Map History Table located in the Flood Insurance Study report for this turisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620. MAP SCALE 1" = 1000' 500 0 HHH 1000 2000 -METERS NFP PANEL 0315G WW FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS PANEL 315 OF 1300 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) COMMUNITY NUMBER PANEL SUFFIX INTRONAL FL te Map Number shown below should be prep orders: the Community Number MAP NUMBER 08041C0315G MAP REVISED

DECEMBER 7, 2018 Federal Emergency Management Agency

# National Flood Hazard Layer FIRMette



### Legend





## **APPENDIX B**

Hydrologic Calculations

19

#### **Black Forest Office**

Composite Impervious Calculations - Historic Conditions Date: January 19, 2021



#### **Historic Conditions**

Information from UCFCD Volume 1 Table 6-6 Type B NRCS Hydrologic Soils Group

Land Use	% Impervious	C5	C100
Streets (Paved)	100%	0.90	0.96
Streets (Gravel)	80%	0.59	0.74
Drive and Walks	100%	0.90	0.96
Roofs	90%	0.73	0.83
Lawns	0%	0.08	0.50

I. Land Use Breakdown

		Area (square feet)				
Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
H-1	0	1,249	0	0	73,645	74,894
H-2	13,100	4,204	0	2,769	108,867	128,940
H-3	0	862	0	0	9,331	10,193
						214,027

		Area (acres)				
Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
H-1	0.00	0.03	0.00	0.00	1.69	1.719
H-2	0.30	0.10	0.00	0.06	2.50	2.960
H-3	0.00	0.02	0.00	0.00	0.21	0.234
Total						4.913

II. Composite Basin Imperviousness and Runoff Coefficients

			I <sub>Weighted C5</sub> =	IWeighted C100 =	I <sub>Weighted</sub> Basin =
			Σ (C5*Area) /	Σ (C100*Area) /	Σ (%I*Area) /
Basin	Σ (% I * Area)	Σ Area (ac)	Σ Area	Σ Area	Σ Area
H-1	0.02	1.719	0.09	0.50	1.3%
H-2	0.44	2.960	0.19	0.56	14.7%
H-3	0.02	0.234	0.12	0.52	6.8%

#### **Black Forest Office**

**Composite Impervious Calculations - Proposed Conditions** Date: January 19, 2021



#### **Proposed Conditions**

Information from UCFCD Volume 1 Table 6-6 Type B NRCS Hydrologic Soils Group

Land Use	% Impervious	C5	C100
Streets (Paved)	100%	0.90	0.96
Streets (Gravel)	80%	0.59	0.74
Drive and Walks	100%	0.90	0.96
Roofs	90%	0.73	0.83
Lawns	0%	0.08	0.50

I. Land Use Breakdown

		A	Area (square feet)			_
Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
PR-1	14,245	0	2,969	1,640	4,374	23,228
PR-2	0	1,007	2,735	4,401	26,055	34,197
PR-3	10,364	0	375	1,609	100,980	113,328
PR-4	0	0	0	0	36,455	36,455
PR-5	0	0	0	0	6,640	6,640
						213,848

			Area (acres)			
Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
PR-1	0.33	0.00	0.07	0.04	0.10	0.533
PR-2	0.00	0.02	0.06	0.10	0.60	0.785
PR-3	0.24	0.00	0.01	0.04	2.32	2.602
PR-4	0.00	0.00	0.00	0.00	0.84	0.837
PR-5	0.00	0.00	0.00	0.00	0.15	0.152
Total						4.909

II. Composite Basin Imperviousness and Runoff Coefficients

			IWeighted C5 =	IWeighted C100 =	I <sub>Weighted Basin</sub> =
			Σ (C5*Area) /	Σ (C100*Area) /	Σ (%I*Area) /
Basin	Σ (% I * Area)	Σ Area (ac)	Σ Area	Σ Area	Σ Area
PR-1	0.43	0.533	0.73	0.86	80.5%
PR-2	0.17	0.785	0.24	0.59	21.9%
PR-3	0.28	2.602	0.17	0.55	10.8%
PR-4	0.00	0.837	0.08	0.50	0.0%
PR-5	0.00	0.152	0.08	0.50	0.0%

Composite Imperviousness Value for Watershed Tribuary to Pond (used in MHFD-Detention Spreadsheet for EDB Pond)

Basins PR-1 & PR-2	Σ Area (ac)	1.32	% I <sub>Watershed =</sub>	45.61%

	Calculation of Peak Runoff using Rational Method																																					
Co	signer: TE mpany: 2N Date: 1/ Project: Bla	N Civil 12/2021 lack Fore			-	Cells of th Cells of th	his color an	e for requi	red user-in nal override	e values			S <sub>1</sub> <sup>0.33</sup> L <sub>t</sub>	L <sub>t</sub>	Computed	$t_c = t_i + t_t$	Lt Lt			10 (non-urban)		toda Docion	-14 \)		1-hour rainfall	t UDFCD location depth, P1 (in) =	2-yr 1.19 a	5-yr 1.50 b	10-yr 25 1.75 2. c	5-yr 50-y .00 2.2	-yr 100-yr 25 2.52	r 500-yr		btained fro			 ()	
Lo	cation: <u>12</u>	2740 Blad	ck Forest Rd,	Colo Springs, CO		Cells of th		e for calcu off Coeffi		ts based o	n overrides		$60K\sqrt{S_t}$ 6	OV <sub>t</sub>	0	.c = (20 1/1	60(14i + 9)	$\sqrt{S_t}$		elized (Travel) F	m , min (Compu	iteu t <sub>c</sub> , Regiona	al t <sub>c</sub> )}		ensity Equatio	n Coefficients	28.50		0.786	, (b	$b + t_c)^c$		<del></del>			Q(cfs) = CI		
Subcato Nan		Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	2-yr	5-yr	10-yr			100-уі	r 500-yr	Overland Flow Length L <sub>i</sub> (ft)		D/S Elevation (ft) (Optional)	Overland Flow Slope S <sub>i</sub> (ft/ft)	Overland Flow Time t <sub>i</sub> (min)		U/S Elevation (ft) (Optional)		T , , ,	NRCS	Channelized Flow Velocity V <sub>t</sub> (ft/sec)		Computed t <sub>c</sub> (min)	Regional t <sub>c</sub> (min)	Selected t <sub>c</sub> (min)	2-yr			i-yr 50-y	,	r 500-yr	2-yr	5-yr	10-yr		100-yr	500-yr
PR	1	0.53	В	80.5	0.65	0.68	0.71	0.75	0.78	0.80		89.68	72.40	68.00	0.049	4.28	309.47	68.00	58.35	0.031	20	3.53	1.46	5.74 5.20	13.76	5.74	3.89	4.90	5.71 6.	.53 7.3	35 8.23	—	1.34	1.77	2.15	2.63	3.51	
PR	2	0.79	В	21.9	0.14	0.16	0.23	0.39	0.45	0.53		11.35	74.90	72.00	0.256	1.95 1.79	172.30	72.00	55.00	0.099	20	6.28	0.46	2.41 2.25	23.03	5.00	4.04	5.09	5.94 6.	.78 7.6	63 8.55	=	0.45	0.66	1.09	2.06	 3.54 3.96	
PR	3	2.60	В	10.8	0.06	0.08	0.14	0.32	0.39	0.48		96.55	69.74	65.00	0.049	10.74 9.76	345.08	65.00	48.00	0.049	7	1.55	3.70	14.45 13.46	26.63	14.45	2.75	3.47	4.04 4.	.62 5.20	20 5.82	=	0.44	0.69	1.52	3.81	 7.21 8.33	
PR	4	0.84	В	0.0	0.00	0.00	0.06	0.25	0.33	0.43		107.30	64.36	51.88	0.116	9.15 8.49	138.47	51.88	41.00	0.079	7	1.96	1.18	10.33 9.66	26.91	10.33	3.18	4.01	4.67 5.	.34 6.0	01 6.73		0.00	0.00	0.22	1.11	 2.40	
PR	5	0.15	В	0.0	0.00	0.00	0.06	0.25	0.33	0.43		14.55	64.00	63.00	0.069	4.01	22.69	63.00	58.69	0.190	7	3.05	0.12	4.13 3.84	26.10	10.00	3.22	4.06	4.73 5.	.41 6.09	6.82		0.00	0.00	0.04	0.20	0.44	
																														=	—	=	=	$\square$	$\square$	$\square$		
H-	1	1.72	В	1.3	0.01	0.01	0.07	0.26	0.34	0.43		42.88	74.05	66.00	0.188	4.91 4.54	304.44	66.00	41.00	0.082	7	2.01	2.53	7.44	27.70	10.00	3.22	4.06	4.73 5.	41 6.0	09 6.82		0.03	0.05	0.55	2.39	5.07 5.86	
He	2	2.96	В	14.7	0.09	0.11	0.18	0.34	0.41	0.49		96.55	69.74	65.00	0.049	10.43 9.55	345.08	65.00	48.00	0.049	7	1.55	3.70	14.13 13.25	25.84	14.13	2.78	3.50	4.09 4.	<u>67 5.2</u>	25 5.88	-	0.73	1.10 1.97	2.12	4.72	8.61 9.75	
H-	3	0.02	В	6.8	0.04	0.05	0.11	0.29	0.37	0.46		14.55	64.00	63.00	0.069	3.84 3.57	22.69	63.00	58.69	0.190	7	3.05	0.12	3.97 3.70	24.94	10.00	3.22	4.06	4.73 5.	.41 6.09	09 6.82		0.00	0.00	0.01	0.03	0.06	

### Black Forest Office SUMMARY RUNOFF TABLE

Date: January 19, 2021

### **HISTORIC CONDITIONS**



DESIGN POINT	CONTRIBUTING BASIN(S)	CONTRIBUTING AREA (AC)	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)	NOTES:
H1	H-1	1.72	0.63	5.86	Releases undetained (following historic flow path)
H2	H-2	2.96	1.97	9.75	Releases undetained (following historic flow path)
Н3	H-3	0.23	0.11	0.83	Releases undetained (following historic flow path)

### **PROPOSED CONDITIONS**

DESIGN POINT	CONTRIBUTING BASIN(S)	CONTRIBUTING AREA (AC)	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)	NOTES:
P1	PR-1, PR-2, PR-4	2.16	0.47	4.62	Releases offsite (developed basins PR-1 and PR-2 are detained prior to release)
P2	PR-3	2.60	1.53	8.33	Releases undetained (following historic flow path)
Р3	PR-5	0.15	0.05	0.52	Releases undetained (following historic flow path)
1	PR-1	0.53	1.91	3.77	Releases to EDB Pond
2	PR-2	0.79	0.96	3.96	Releases to EDB Pond

Land Use or Surface	Percent						Runoff Co	efficients					
Characteristics	Impervious	2-у	ear	<mark>(5-</mark> y	ear	10-y	/ear	ر-25	/ear	י-50	/ear	<mark>100-</mark>	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	<mark>0.90</mark>	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	<mark>0.74</mark>
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	<mark>0.96</mark>
Roofs	90	0.71	0.73	<mark>0.73</mark>	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	<mark>0.83</mark>
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

#### Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

### **3.2** Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration  $(t_c)$  consists of an initial time or overland flow time  $(t_i)$  plus the travel time  $(t_i)$  in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time  $(t_i)$  plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion  $(t_i)$  of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.



**APPENDIX C** EDB Calculations

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Depth Increment = 0.20

Stage - Storage Description

Top of Micropool

ft

ide Stage (ft)

0.00

Area (ft<sup>2</sup>)

Width (ft)

Length (ft)

Area (acre)

0.000

rea (ft

13

Volume (ft<sup>3</sup>)

Volume (ac-ft)

Stage (ft)

100-YEAR

ZONE 1 AND 2-ORIFICES PERM Example Zone Configuration (Retention Pond)

#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	1.32	acres
Watershed Length =	390	ft
Watershed Length to Centroid =	160	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	45.61%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban hydro	igraph Procedu	ile.
Water Quality Capture Volume (WQCV) =	0.021	acre-feet
Excess Urban Runoff Volume (EURV) =	0.064	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.058	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.085	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.108	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.140	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.166	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.199	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	0.266	acre-feet
Approximate 2-yr Detention Volume =	0.048	acre-feet
Approximate 5-yr Detention Volume =	0.066	acre-feet
Approximate 10-yr Detention Volume =	0.089	acre-feet
Approximate 25-yr Detention Volume =	0.098	acre-feet
Approximate 50-yr Detention Volume =	0.102	acre-feet
Approximate 100-yr Detention Volume =	0.116	acre-feet

#### Define Zones and

Zone 1 Volume (WQCV) =	0
Zone 2 Volume (EURV - Zone 1) =	0
Zone 3 Volume (100-year - Zones 1 & 2) =	0
Total Detention Basin Volume =	0
Initial Surcharge Volume (ISV) =	, t
Initial Surcharge Depth (ISD) =	, t
Total Available Detention Depth (H <sub>total</sub> ) =	, t
Depth of Trickle Channel $(H_{TC}) =$	, t
Slope of Trickle Channel (S <sub>TC</sub> ) =	ι
Slopes of Main Basin Sides (S <sub>main</sub> ) =	L
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	ι

#### Initial Surcharge Surcharge Depth Length Width o Area Volume Depth of Main Basin $(H_{MAIN}) =$ user n Length of Main Basin $(H_{MAIN}) =$ Width of Main Basin $(W_{MAIN}) =$ user user Area of Main Basin ( $A_{MAIN}$ ) = Volume of Main Basin ( $V_{MAIN}$ ) = user ff ۰ ft³ user acre-fee

Calculated Total Basin Volume (V<sub>total</sub>) =

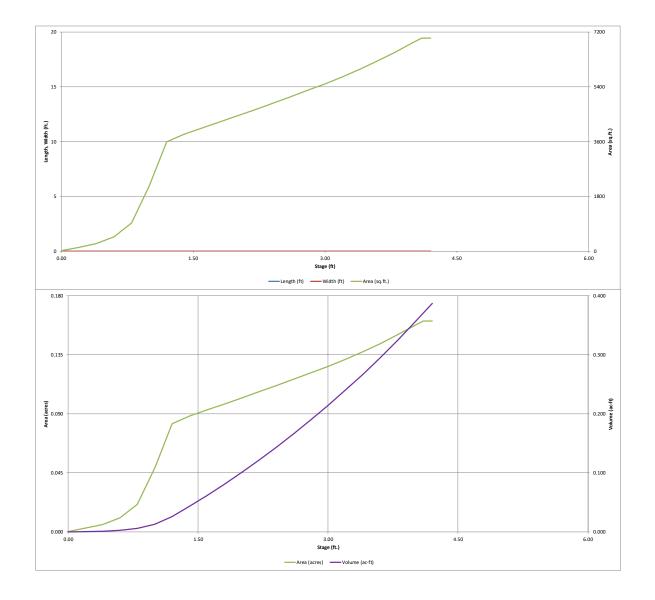
23-yr Detention volume -	0.050	acie-ieec
50-yr Detention Volume =	0.102	acre-feet
00-yr Detention Volume =	0.116	acre-feet
Basin Geometry		
Zone 1 Volume (WQCV) =	0.021	acre-feet
olume (EURV - Zone 1) =	0.042	acre-feet
100-year - Zones 1 & 2) =	0.052	acre-feet
Detention Basin Volume =	0.116	acre-feet
Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Surcharge Depth (ISD) =	user	ft
Detention Depth (H <sub>total</sub> ) =	user	ft
of Trickle Channel (H <sub>TC</sub> ) =	user	ft
of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
1ain Basin Sides (S <sub>main</sub> ) =	user	H:V
n-to-Width Ratio (R <sub>L/W</sub> ) =	user	
		•
Surcharge Area $(A_{ISV}) =$	user	ft <sup>2</sup>
e Volume Length $(L_{ISV}) =$	user	ft
e Volume Width $(W_{ISV}) =$	user	ft
of Basin Floor $(H_{FLOOR}) =$	user	ft
of Basin Floor $(L_{FLOOR}) =$	user	ft
of Basin Floor $(W_{FLOOR}) =$	user	ft
of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>
of Basin Floor $(V_{FLOOR}) =$	user	ft <sup>3</sup>
(11) D (11)		0

user

		Top of Micropool		0.00	-	 -	13	0.000		
				0.20	-	 -	121	0.003	13	0.000
				0.40	-	 -	247	0.006	50	0.001
				0.60		 	465	0.011	121	0.003
				0.80		 	917	0.021	260	0.005
				1.00	-	 	2,126	0.049	564	0.013
				1.20	-	 -	3,590	0.082	1,135	0.026
				1.40		 	3,848	0.088	1,879	0.043
				1.60	-	 -	4,044	0.088	2,668	0.043
				1.80				0.095		0.080
				2.00	-	 -	4,242 4,442	0.102	3,497	0.080
									4,365	
				2.20		 	4,646	0.107	5,274	0.121
				2.40		 	4,855	0.111	6,224	0.143
				2.60	-	 -	5,066	0.116	7,216	0.166
ptional User O				2.80	-	 -	5,279	0.121	8,251	0.189
	re-feet			3.00		 -	5,495	0.126	9,328	0.214
	re-feet			3.20	-	 -	5,726	0.131	10,450	0.240
	ches			3.40	-	 -	5,978	0.137	11,621	0.267
	ches			3.60	-	 -	6,248	0.143	12,843	0.295
	ches			3.80	-	 -	6,538	0.150	14,122	0.324
	ches			4.00		 	6,847	0.157	15,461	0.355
2.25 inc	ches			4.10	-	 -	7,008	0.161	16,153	0.371
2.52 inc	ches			4.20		 	7,008	0.161	16,854	0.387
3.14 inc	ches					 				
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#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

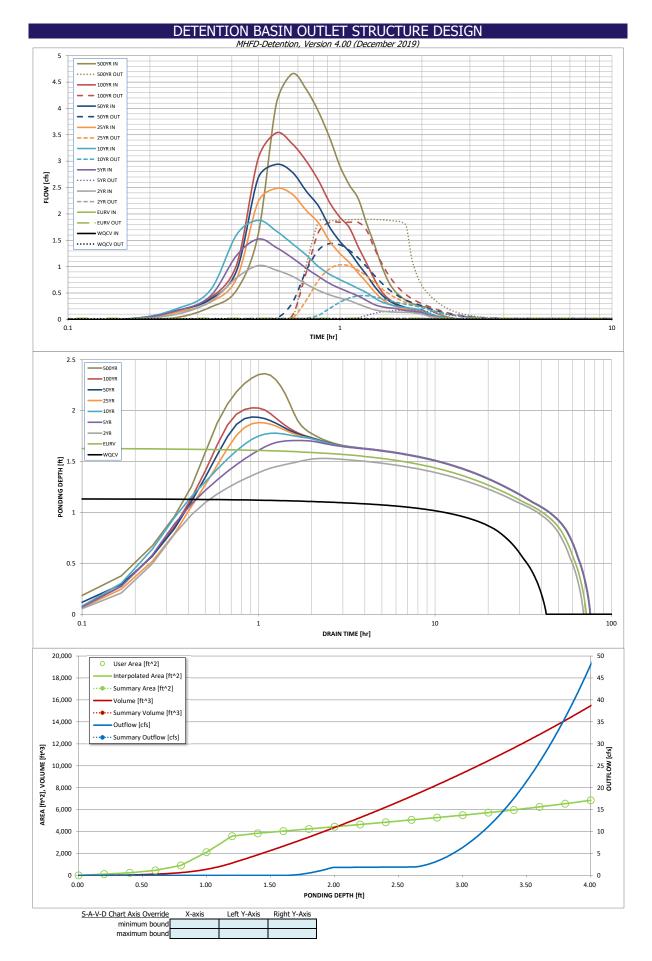
MHFD-Detention, Version 4.03 (May 2020)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

	MHFD-Detention,	Version 4.03	(Mav 2020)
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	Black Forest Office								
	EDB Basin (PR-1 a	ind PR-2)							
ZONE 2 ZONE 2 ZONE 1				Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	1.14	0.021	Orifice Plate	1		
	100-YEAR								
ZONE 1 AND 2	ORIFICE		Zone 2 (EURV)	1.63	0.042	Orifice Plate			
PERMANENT ORIFICES			Zone 3 (100-year)	2.15	0.052	Weir&Pipe (Restrict)			
Example Zone	Configuration (Re	etention Pond)		Total (all zones)	0.116				
User Input: Orifice at Underdrain Outlet (typical	ly used to drain W(	OCV in a Filtration P	MP)			1	Calculated Parame	eters for Underdrain	<b>.</b>
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Underd	rain Orifice Area =	N/A	ft <sup>2</sup>	<u>+</u>
•		•		surface)			-		
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifice	ces or Elliptical Slot	Weir (typically use	d to drain WQCV a	nd/or EURV in a se	dimentation BMP)		Calculated Parame		
Invert of Lowest Orifice =	0.00	ft (relative to basir	n bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	N/A	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	1.63	ft (relative to basir	h bottom at Stage =	= 0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	6.50	inches			Ellipti	cal Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	inches			•	lliptical Slot Area =	N/A	ft <sup>2</sup>	
	N/X	inches			-		14/13	Tuc	
User Input: Stage and Total Area of Each Orific	e Row (numbered	from lowest to high	<u>iest)</u>				r		-
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	]
Stage of Orifice Centroid (ft)	0.00	0.54	1.09						
Orifice Area (sq. inches)	0.14	0.14	0.50						1
			1.50						1
	Dow 0 (	Dow 10 (antiana 1)	Dow 11 (antiana 1)	Dow 12 (	Dow 12 (	Daw 14 (antian P	Dow 15 /	Dow 16 (antion 1)	1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	4
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									J
User Input: Vertical Orifice (Circular or Rectang	jular)						Calculated Parame	eters for Vertical Or	ifice
· · · · · ·	Not Selected	Not Selected					Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A		ft (relative to basir	bottom at Stage -	-0ft) Vor	tical Orifice Area =	N/A	N/A	ft²
				-	•				
Depth at top of Zone using Vertical Orifice =	N/A		ft (relative to basir	i bottom at Stage =	= 0 π) vertical	Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat	or Sloped Grate and	l Outlet Pine OR Re	ctangular/Trapezoi	dal Weir (and No C	)utlet Pine)		Calculated Parame	eters for Overflow \	Veir
User Input: Overflow Weir (Dropbox with Flat o			ctangular/Trapezoi	dal Weir (and No C	Dutlet Pipe)			eters for Overflow \	<u>Veir</u>
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 1.63	Not Selected N/A	ft (relative to basin I		ft) Height of Grate		Zone 3 Weir 2.63	Not Selected N/A	feet
	Zone 3 Weir 1.63 4.00	Not Selected N/A N/A	ft (relative to basin I feet	pottom at Stage = 0	ft) Height of Grate Overflow W	eir Slope Length =	Zone 3 Weir 2.63 4.12	Not Selected N/A N/A	
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 1.63	Not Selected N/A N/A	ft (relative to basin I	pottom at Stage = 0	ft) Height of Grate	eir Slope Length =	Zone 3 Weir 2.63	Not Selected N/A	feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	Zone 3 Weir 1.63 4.00	Not Selected N/A N/A	ft (relative to basin I feet	oottom at Stage = 0 Gra	ft) Height of Grate Overflow W	'eir Slope Length = 0-yr Orifice Area =	Zone 3 Weir 2.63 4.12	Not Selected N/A N/A	feet
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 1.63 4.00 4.00 4.00 70% 50% e (Circular Orifice, 1	Not Selected N/A N/A N/A N/A N/A Restrictor Plate, or	ft (relative to basin I feet H:V feet %, grate open are %	pottom at Stage = 0 Gra Ov a/total area O	ft) Height of Grate Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open	'eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 2.63 4.12 69.46 11.54 5.77 s for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction P	feet feet ft <sup>2</sup> ft <sup>2</sup>
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 1.63 4.00 4.00 4.00 70% 50% e (Circular Orifice, 1	Not Selected N/A N/A N/A N/A N/A Restrictor Plate, or Not Selected	ft (relative to basin I feet H:V feet %, grate open are %	oottom at Stage = 0 Gra Ov a/total area O	ft) Height of Grate Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open <u>Cal</u>	leir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 2.63 4.12 69.46 11.54 5.77 s for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction P	feet feet ft <sup>2</sup> ft <sup>2</sup>
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Ed Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Zone 3 Weir 1.63 4.00 4.00 70% 50% 20m 3 Restrictor 3.40 18.00 2.70 7.Trapezoidal) 2.62 5.00 4.00 1.00 7 <i>the user can over</i> WQCV N/A 0.021 N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A Restrictor Plate, or Not Selected N/A N/A N/A N/A t (relative to basin feet H:V feet H:V feet H:V feet N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	ft (relative to basin I feet H:V feet %, grate open are % Rectangular Orifice ft (distance below be inches inches n bottom at Stage = HP hydrographs an 2 Year 1.19 0.058 0.2 2 Year 1.19 0.058 0.2 0.2 0.13 1.0 0.0 N/A Plate N/A N/A 60 65 1.53	bottom at Stage = 0 Gra Ov a/total area O ) asin bottom at Stage Half-Cent = 0 ft) d runoff volumes b 5 Year 1.50 0.085 0.085 0.085 0.085 0.5 0.35 1.5 0.2 0.4 Overflow Weir 1 0.0 N/A 64 70 1.71	ft) Height of Grate Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/o Debris = lculated Parameters utlet Orifice Area = c Orifice Centroid = tor Plate on Pipe = esign Flow Depth= op of Freeboard = op of Freeboard = op of Freeboard = iop of Freeboard = 25 Year 2.00 0.140 0.140 0.140 0.93 2.5 1.0 0.8 Overflow Weir 1 0.1 N/A 60 68 1.88	Zone 3 Weir 2.63 4.12 69.46 11.54 5.77 5.77 6 for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.13 0.80 Calculated Parame 0.33 3.95 0.16 0.35 0.35 0.166 0.166 1.5 1.7 2.9 1.4 0.9 0.1 N/A 58 67 1.94	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A / Flow Restriction P Not Selected N/A N/A N/A N/A Restriction P Not Selected N/A N/A N/A Courter for Spillway feet feet feet acres acre-ft Columns W through 100 Year 2.52 0.199 1.9 1.9 1.46 3.5 1.8 1.0 Outlet Plate 1 0.2 N/A 56 66 2.03	feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year 3.14 0.266 0.266 0.266 0.266 0.266 0.264 0.264 0.204 4.2.36
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfail Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Zone 3 Weir 1.63 4.00 4.00 70% 50% 2 (Circular Orifice, 1 Zone 3 Restrictor 3.40 18.00 2.70 Trapezoidal) 2.62 5.00 4.00 1.00 7 <i>the user can over</i> WQCV N/A 0.021 N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A Restrictor Plate, or Not Selected N/A N/A N/A N/A ft (relative to basir feet H:V feet ride the default CU EURV N/A 0.064 N/A	ft (relative to basin I feet H:V feet %, grate open are % Rectangular Orifice ft (distance below be inches inches h bottom at Stage = hbottom at Stage = <u>HP hydrographs an</u> <u>2 Year</u> <u>1.19</u> 0.058 0.258 0.2 <u>0.13</u> 1.0 0.0 N/A Plate N/A N/A N/A O O 60 65	bottom at Stage = 0 Gra Ov a/total area O ) asin bottom at Stage Half-Cent = 0 ft) d runoff volumes b 5 Year 1.50 0.085 0.5 0.35 1.5 0.2 0.4 Overflow Weir 1 0.0 N/A Overflow Weir 1 0.0 N/A 64 70	ft) Height of Grate Overflow Wate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open ( 2 a) e 0 ft) Ou Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Area at T Basin Area at T Basin Volume at T 1.75 0.108 0.108 0.7 0.53 1.9 0.4 0.6 Overflow Weir 1 0.0 N/A 62 69	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = iculated Parameters utlet Orifice Area = : Orifice Centroid = tor Plate on Pipe = esign Flow Depth= iop of Freeboard = iop of Freeboard = 0.140 0.140 1.2 0.93 2.5 1.0 0.8 Overflow Weir 1 0.1 N/A 60 68	Zone 3 Weir 2.63 4.12 69.46 11.54 5.77 5.77 2.08 3.95 0.13 0.80 Calculated Parame 0.33 3.95 0.16 0.35 0.16 0.35 0.166 1.5 1.17 2.9 1.4 0.9 Overflow Weir 1 0.1 N/A 58 67	Not Selected         N/A         Ioo Year         2.52         0.199         1.9         1.46         3.5         1.8         1.0         Outlet Plate 1         0.2         N/A         56         66	feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year 3.14 0.266 0.266 2.7 2.04 4.7 1.9 0.7 00/tel Plat 0.7 0.0/tel Plat 0.0/tel



### DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

	The user can o	verride the calcu	ulated inflow hy	drographs from	this workbook v	with inflow hydro	ographs develop	oed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.04
	0:15:00	0.00	0.00	0.10	0.16	0.20	0.13	0.17	0.16	0.23
	0:20:00	0.00	0.00	0.34	0.44	0.55	0.33	0.38	0.41	0.55
	0:25:00	0.00	0.00	0.79	1.22	1.61	0.78	0.92	1.04	1.61
	0:30:00	0.00	0.00	1.02	1.52	1.88	2.23	2.68	3.05	4.09
	0:35:00	0.00	0.00	0.94	1.36	1.68	2.48	2.94	3.54	4.66
	0:40:00	0.00	0.00	0.82	1.17	1.44	2.37	2.80	3.33	4.37
	0:45:00	0.00	0.00	0.67	0.97	1.22	2.07	2.44	3.01	3.94
	0:50:00 0:55:00	0.00	0.00	0.55	0.81	1.00 0.85	1.83 1.48	2.15	2.63 2.21	3.44 2.90
	1:00:00	0.00	0.00	0.48	0.68	0.85	1.46	1.74	1.93	2.90
	1:05:00	0.00	0.00	0.36	0.59	0.67	1.08	1.48	1.93	2.29
	1:10:00	0.00	0.00	0.29	0.44	0.59	0.88	1.05	1.37	1.83
	1:15:00	0.00	0.00	0.23	0.36	0.51	0.71	0.85	1.07	1.44
	1:20:00	0.00	0.00	0.19	0.28	0.41	0.53	0.64	0.77	1.04
	1:25:00	0.00	0.00	0.16	0.24	0.34	0.40	0.48	0.54	0.73
	1:30:00	0.00	0.00	0.15	0.22	0.29	0.31	0.37	0.40	0.55
	1:35:00	0.00	0.00	0.14	0.21	0.26	0.25	0.30	0.32	0.44
	1:40:00	0.00	0.00	0.14	0.18	0.24	0.22	0.25	0.26	0.36
	1:45:00	0.00	0.00	0.13	0.17	0.22	0.19	0.22	0.22	0.31
	1:50:00	0.00	0.00	0.13	0.15	0.21	0.18	0.20	0.20	0.27
	1:55:00 2:00:00	0.00	0.00	0.11 0.10	0.14	0.19 0.17	0.17 0.16	0.19 0.18	0.18	0.24
	2:05:00	0.00	0.00	0.10	0.13	0.17	0.10	0.18	0.17	0.23
	2:10:00	0.00	0.00	0.05	0.07	0.09	0.08	0.15	0.09	0.12
	2:15:00	0.00	0.00	0.04	0.05	0.06	0.06	0.07	0.06	0.09
	2:20:00	0.00	0.00	0.03	0.03	0.05	0.04	0.05	0.04	0.06
	2:25:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:30:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	2:35:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	2:40:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00 3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00 4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

user should graphically co	ompare the sumr	nary S-A-V-D ta	able to the full S	-A-V-D table in	the chart to cor		all key transition points.
Stage - Storage Description	Stage [ft]	Area [ft <sup>2</sup> ]	Area [acres]	Volume [ft <sup>-3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, inclue
							stages of all grade slo changes (e.g. ISV and
							from the S-A-V table of Sheet 'Basin'.
							Also include the invert outlets (e.g. vertical o
							overflow grate, and s
							where applicable).
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#### MHFD-Detention\_v4 03 01-19-21.xlsm, Outlet Structure

#### **BLACK FOREST OFFICE**

#### POND OUTLET PIPE

D =	18 inches
D =	1.5 ft
A =	1.77 sq ft
<b>V</b> <sub>Allowed</sub>	6.05 ft/s

**Q** = 2.00 cfs

#### Use Type M Riprap Minimum

Required Riprap Rock Size		Req'd Riprap Type Based off $P_{d}$	Riprap Type	D <sub>50</sub> -Median Rock Size (in.)	
P <sub>d</sub>	6.31	>	L	L	9
V =	6.05 ft/s			М	12
g =	32.20 ft/sq sec			Н	18
d =	0.1 (assumed value)			B18	18 (Grouted)

By Figure HS-20 in Drainage Criteria Manual Vol. 2, Type L Riprap is Mandated Using Type L

#### Length of Riprap Required - Basin Length Minimum

L = 4D		
D =	1.5 ft	
L =	6.00 ft	

$L = D^{1/2}$	x (V/2)
D =	1.5 ft
V =	6.05 ft/s
L =	3.70 ft

Using the Greater of the Two Lengths, L = 6

#### **Basin Minimum Width**

W = 4D	
D =	1.5 ft - Diameter of Circular Conduit
VV =	6.00 ft

#### Minimum Thickness of Riprap, T

T =  $1.75 \times D_{50}$   $D_{50}$  = 9 inches T = 1.31 ft



# **APPENDIX D**

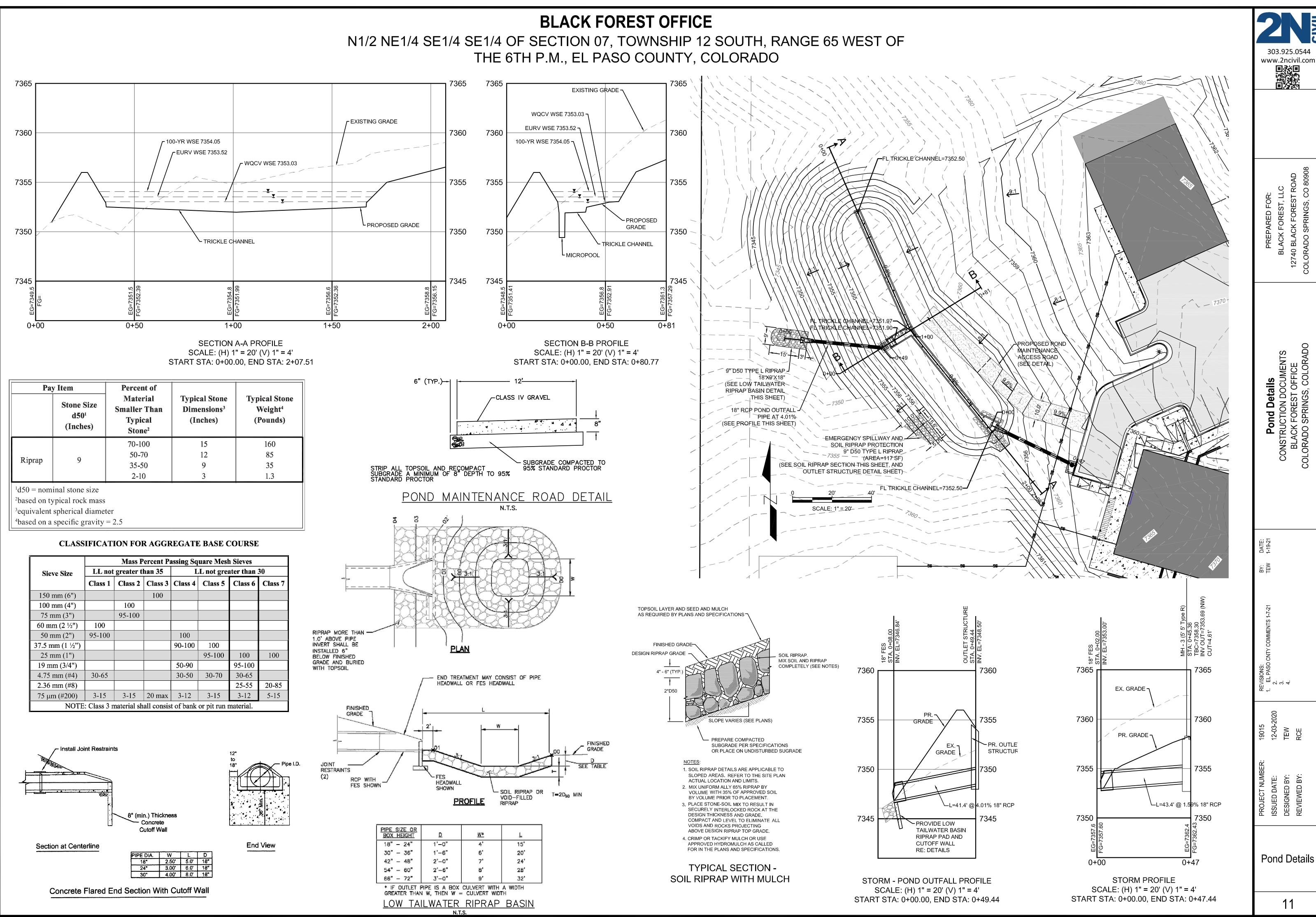
EDB Construction Plans Historic Drainage Map Proposed Drainage Map

#### ITEMIZED COST ESTIMATE Proposed Drainage Facilities Black Forest Office

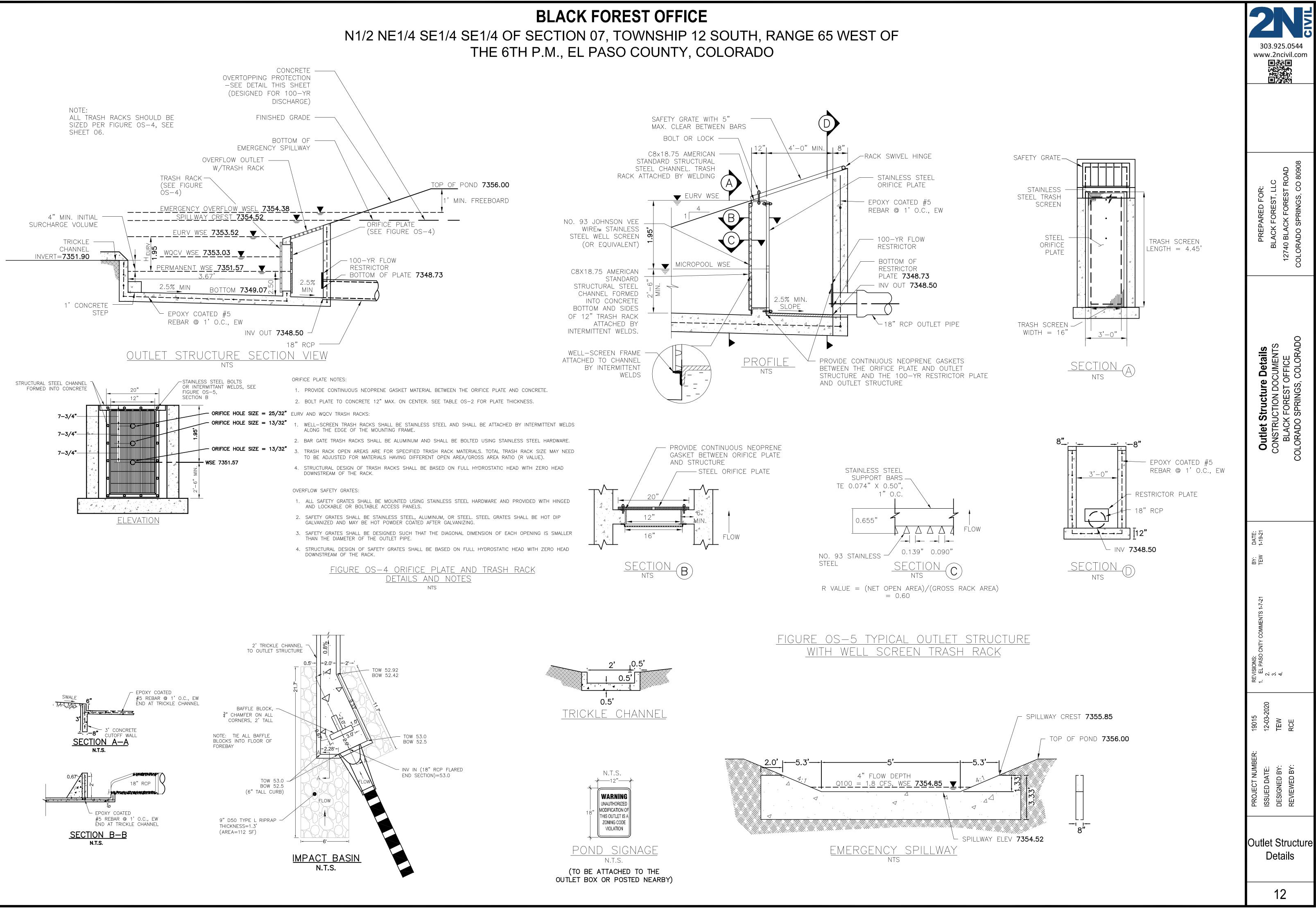
Date: January 19, 2021

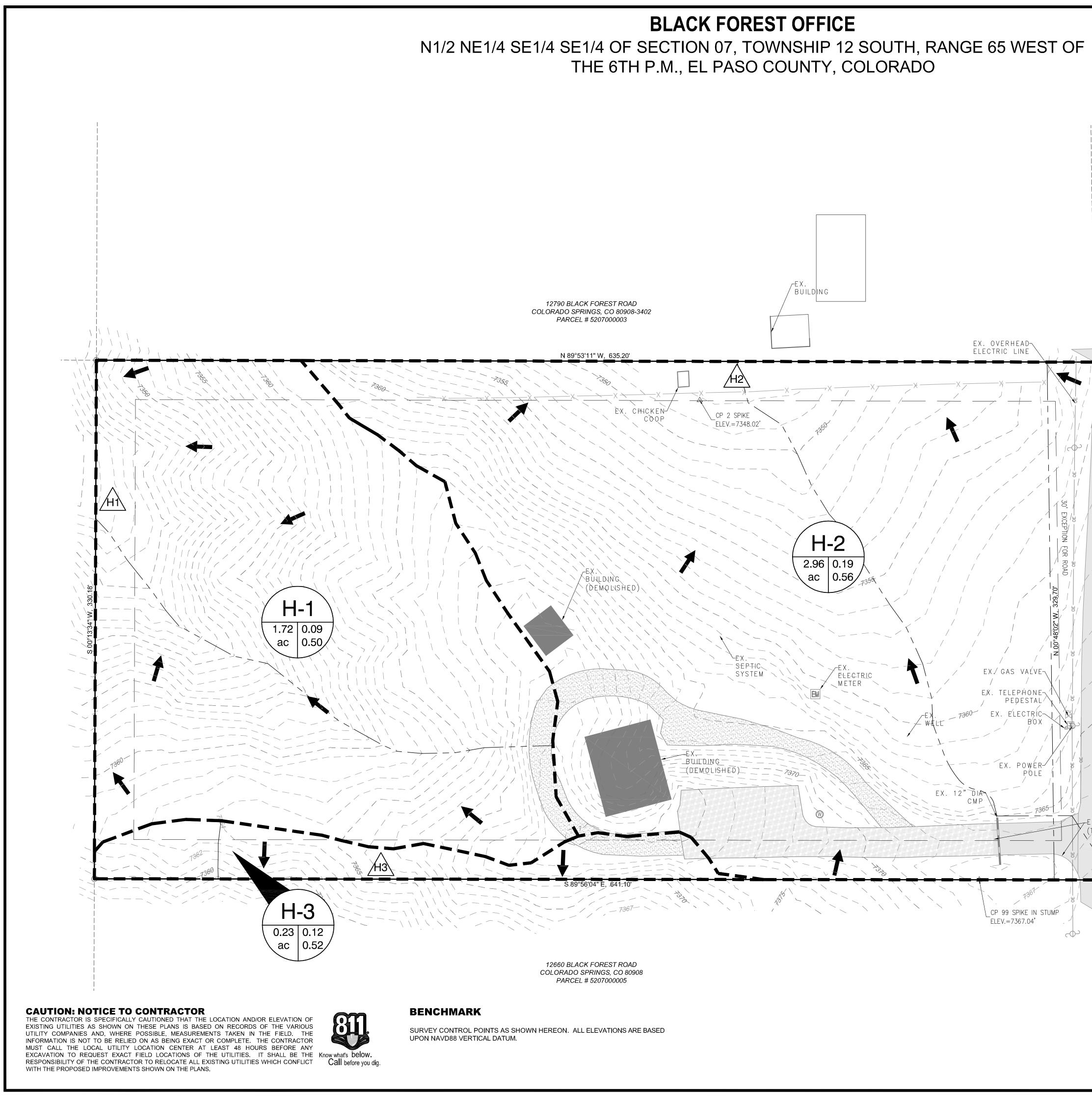
Storm Sewer Utility	Unit	Quantity	Unit Cost	Amount
Permanent Pond/BMP Construction	CY	187	\$20.00	\$3,740
Permanent Pond/BMP Construction (Spillway)	EA	1	\$850.00	\$850
Permanent Pond/BMP Construction (Outlet Structure)	EA	1	\$20,000.00	\$20,000
5' Type R Curb Inlet	EA	1	\$5,542.00	\$5 <i>,</i> 542
18" RCP	LF	71	\$65.00	\$4,615
18" RCP Flared End Section	EA	2	\$390.00	\$780
			Subtotal	\$35,527

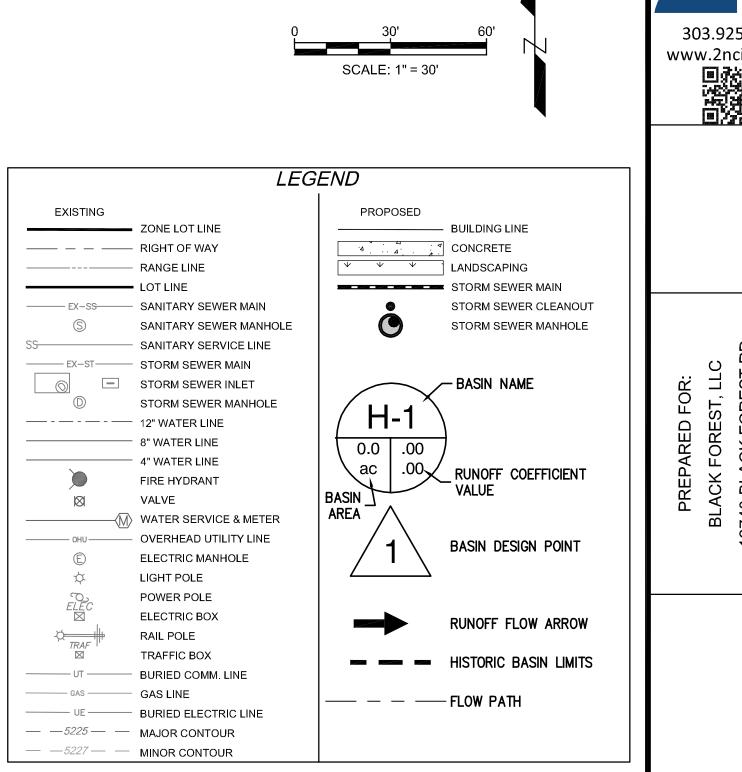
In providing opinions of probable construction cost, the client understands that the Engineer has no control over cost or price of labor, equipment or materials, or over the contractor's method of pricing, and that the opinions of probable construction costs provided herein are made on the basis of the Engineer's qualifications and experience. The Engineer makes no warranty, expressed or implied, to the accuracy of such opinions as compared to bid or actual costs.



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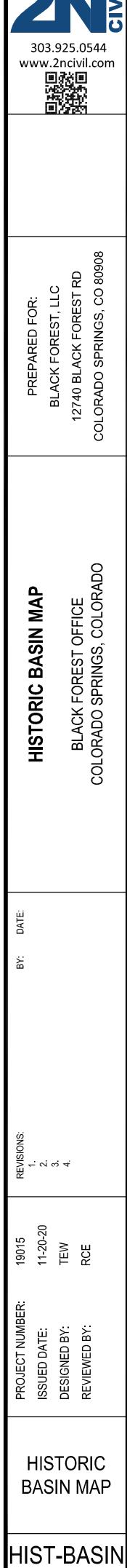


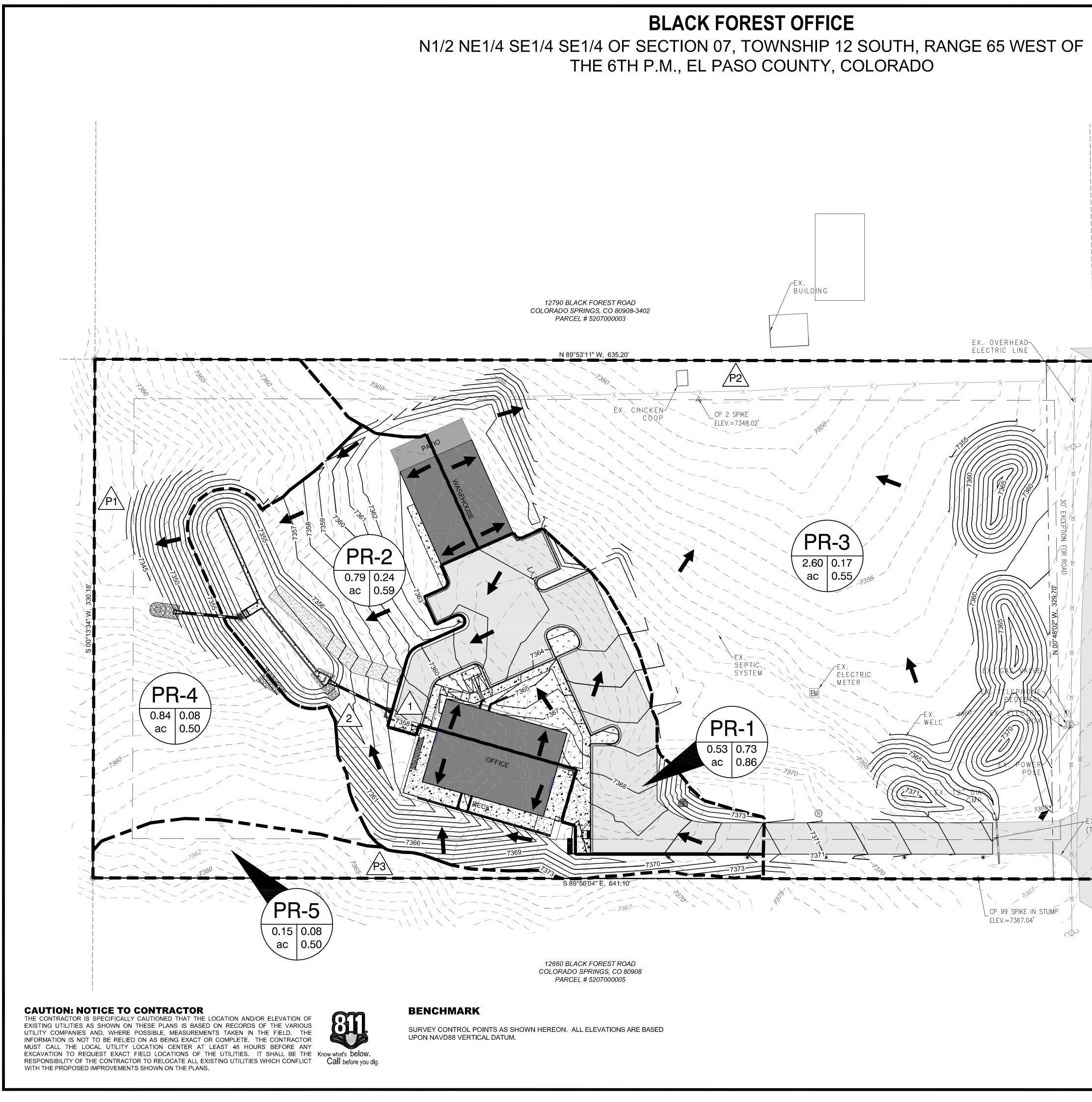


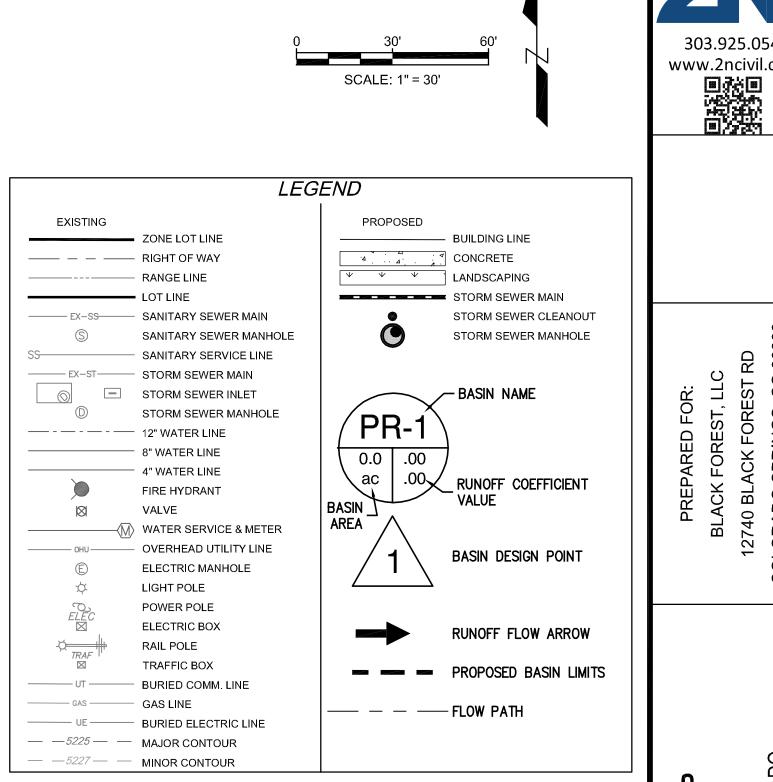


# HISTORIC CONDITIONS

DESIGN	CONTRIBUTING	CONTRIBUTING			
POINT	BASIN(S)	AREA (AC)	Q₅ (cfs)	Q <sub>100</sub> (cfs)	NOTES:
H1	H-1	1.72	0.63	5.86	Releases undetained (following historic flow path)
H2	H-2	2.96	1.97	9.75	Releases undetained (following historic flow path)
H3	H-3	0.23	0.11	0.83	Releases undetained (following historic flow path)

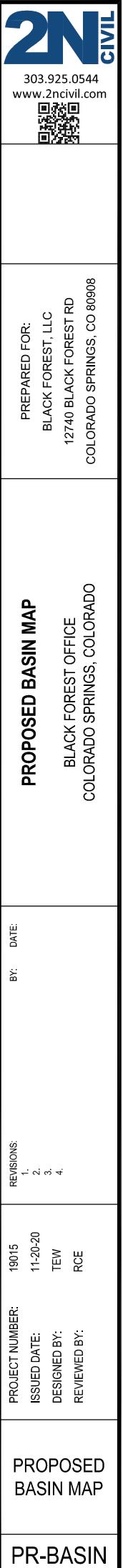






# PROPOSED CONDITIONS

DESIGN	CONTRIBUTING	CONTRIBUTING			
POINT	BASIN(S)	AREA (AC)	Q₅ (cfs)	Q <sub>100</sub> (cfs)	NOTES:
P1	PR-1, PR-2, PR-4	2.16	0.47	4.62	Releases offsite (developed basins PR-1 and PR-2 are detained prior to release)
Ρ2	PR-3	2.60	1.53	8.33	Releases undetained (following historic flow path)
Ρ3	PR-5	0.15	0.05	0.52	Releases undetained (following historic flow path)
1	PR-1	0.53	1.91	3.77	Releases to EDB Pond
2	PR-2	0.79	0.96	3.96	Releases to EDB Pond



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