Engineering Review

EPC Planning & Community Development Department



FINAL DRAINAGE REPORT

for

BLACK FOREST OFFICE

The North Half of the NE Quarter of the SE Quarter of Section 7

Township 12 South, Range 65 West of the 6th P.M.

County of El Paso, State of Colorado

12740 Black Forest Road

Colorado Springs, Colorado 80908

"Cursory comments only! Please see attached checklist for a FDR in the Comment letter". The above note was on the version one (1) review. Please include all the necessary items on the next submittal.

2N Civil Job No. 19015 September 11, 2020 Revised November 20, 2020

PREPARED FOR:

Black Forest, LLC 8655 Table Butte Road Colorado Springs, Colorado 80908-1224 Contact: Rad Jackson, Project Manager

Engineer: 2N Civil, LLC 6 Inverness Court East, Suite 125 Englewood, Colorado 80112 Contact: Ryan Eichele, PE, Project Manager Todd West, PE Project Engineer

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Engineer's Statement

The attached drainage plan and report were prepared under my direct supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions in preparing this report.

SIGNATURE:	
Todd Eric West, PE	
Colorado Registration No. 37643	
For and on behalf of 2N Civil, LLC	
Developer's Statement	
	ply with all of the requirements specified in this drainage
report and plan.	, , , , , , , , , , , , , , , , , , , ,
Business Name	
Ву:	
Title:	
Address:	
El Paso County Statement:	
Filed in accordance with Section 51.1 of	the El Paso Land Development Code, as amended.
	
Director of Public Works	Date
Conditions:	↓
Conditions.	
El Paso County:	
	nts of the Drainage Criteria Manual, Volumes 1
and 2, El Paso County Engineering Crit amended.	eria Manual and Land Development Code as
arriended.	
Jennifer Irvine, P.E.Date	
County Engineer / ECM Administrator	

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1) GENERAL LOCATION AND DESCRIPTION

(a) Location

The Black Hills Office property, addressed as 12740 Black Hills Road, is the north half of the Northeast Quarter of the Southeast Quarter of Section 7, Township 12 South, Range 65 West of the 6th Principle Meridian, County of El Paso, State of Colorado. Black Forest Road bounds the site on the east. Rural Residential development (Zoning RR-5) surrounds the site on the north, south, and west. An existing asphalt and gravel road provides access to the vacant parcel. Therefered interest says 4.77 drainageways on the site.

(b) Description of property and Proposed Improvements

The subject property contains approximately 4.83 acres. Sparse ground cover consists of native weeds with a few trees at the northeast corner of the site. A shallow ridgeline divides the site, directing the east portion of the site to the north, and the west portion of the site to the west. The National Resources Conservation Service Web Soil Survey classifies the in situ soils as Hydrologic Group B, which exhibit a moderate infiltration rate when thoroughly wet.

There are no major drainage ways or irrigation facilities on the site.

The development will consist of a single story 4,400 sf office building with a full, walk-out basement of equal size with a 3,250-sf studio/shop building on the 4.77 acres. The office building will house the Owner's corporate functions for Metal Roof Innovations, Ltd. company (strategic planning, accounting, sales/marketing management).

An existing barn (currently under construction) was permitted under the A-5 zoning. Construction began in the spring of 2020. The barn will be re-purposed in use as a studio/shop to supplement the corporate functions. No manufacturing, warehousing, shipping, wholesale or retail sales will take place at this facility.

2) DRAINAGE BASINS AND SUB-BASINS

(a) Major Basin Description

The site is tributary to the upper reach of Kettle Creek drainage basin (FOMO3000), that flows from north to south approximately 1,500 feet west of the site. This basin is an unstudied basin included in the El Paso County drainage basin fee program.

Address drainage fees. Fees were paid when the site was originally platted?



Based on the FEMA Map No. 08041C0315G with an effective date of 12/07/18 (included in the Appendix) the site is located within Zone X, areas of minimal flood hazard. No portion of the site is located within the 100 year floodplain. The upper reach of the Kettle Creek basin is sparsely developed and includes single family homes on large acreages.

(b) Sub-Basin Description

Include panel and call out the page the Firm panel is on. In this report.

The site historically drains north and west. The development of the site will occur on the upper portion of the lot, with the majority of the new impervious areas directed to a proposed detention facility that will intercept flow prior to discharge to the west.

3) DRAINAGE DESIGN CRITERIA

(a) Development Criteria Reference

The City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2 (DCMV1 & DCMV2) was utilized per El Paso County's stormwater quality design criteria as well as the applicable standards from the County's Engineering Criteria Manual (ECM).

(b) Hydrologic Criteria

The Rational Method was selected to calculate existing and proposed runoff rates from the site for the 5 year (minor storm) and 100 year (major storm) recurrence intervals. The design rainfall will be from DCMV1 Table 6-2 Rainfall Depths for Colorado Springs.

Table 6-2. Rainfall Depths for Colorado Springs

Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth				
2	(1.19)	1.70	2.10				
5	1.50	2.10	2.70				
10	(1.75)	2.40	3.20				
25	2.00	2.90	3.60				
50	(2.25)	3.20	4.20				
100	2.52	3.50	4.60				

Where Z = 6,840 ft/100

The most current version of UDFCD's Peak Runoff Prediction by the Rational



Method, Version 2.00 released May 2017 was used to determine flows. The Runoff Coefficients from DCMV1, Table 6-6 were input to determine peak runoff values.

The development will implement Full Spectrum Detention (FSD) utilizing an Extended Detention Basin (EDB) to capture and treat runoff prior to discharge downstream. Full Spectrum Detention (FSD) is a design concept that provides control of the full range of runoff rates that pass through detention facilities.

4) DRAINAGE FACILITY DESIGN

(a) General Concept

The area being developed has been divided into three subbasins. Basin PR-1 includes the paved parking area and portions of the buildings (office and warehouse) and perimeter landscaping. Basin PR-1 will flow within the asphalt parking lot to a new 5' Type R inlet, where it will be conveyed to the pond via an 18" RCP pipe. Due to the small size of the development, per the UD-BMP_v3.07 spreadsheet by MHFD, a forebay is not necessary for this size site.

Basin PR-2, located along the south property line, will collect flow from a portion of the office roof, which will be conveyed to the detention basin via an earthen swale. Basin PR-3, located along the northern limit of the development, will flow north following the historic drainage path and is not tributary to the proposed pond.

The imperviousness value of 45.61%, which represents the composite value for the area tributary to the pond, was used to determine the required EDB. The UD-Detention spreadsheet can be found in the Appendix.

The drainage concept for the development does not alter historic drainage patterns. The detention pond will act to limit the stormwater release rate to predevelopment conditions.

(b) Specific Details

The development will implement Full Spectrum Detention (FSD) utilizing an Extended Detention Basin (EDB) to capture and treat runoff prior to discharge downstream. The proposed detention pond is designed using the UDFCD spreadsheet, UD-Detention v.4.03. This design considers the water quality capture volume (WQCV), excess urban runoff volume (EURV), and 100-year detention volume.



5) DRAWING CONTENTS

(a) General Location Map

A Vicinity Map is included in the Appendix.

(b) Drainage Plan

Refer to the Proposed Drainage Plan in the Appendix for basin delineation, drainage routes and flows, and proposed stormwater facilities.

6) CONCLUSION

In our professional opinion, the proposed development will pose an insignificant change in the historic drainage patterns of the existing site. The development of the office and warehouse will include construction of an Extended Detention Basin, which will provide detention of the WQCV, EURV, and 100 year flow. This facility will slow the rate of discharge from the site and promote infiltration. These runoff reduction measures ensure that the capacity of the downstream drainageways will not be negatively affected by the construction of these improvements.

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REFERENCES

- 1. El Paso County Engineering Criteria Manual (ECM), Revised 12/13/2016.
- 2. Colorado Springs Drainage Criteria Manual Volumes 1 and 2 (DCMV1 & DCMV2), May 2014.
- 3. Urban Storm Drainage Criteria Manual, Volumes 1, 2, & 3, Urban Drainage and Flood Control District, Volumes 1 & 2 Originally Published September 1969, Updated March 2017; Volume 3 Originally Published September 1992, Updated November 2010.

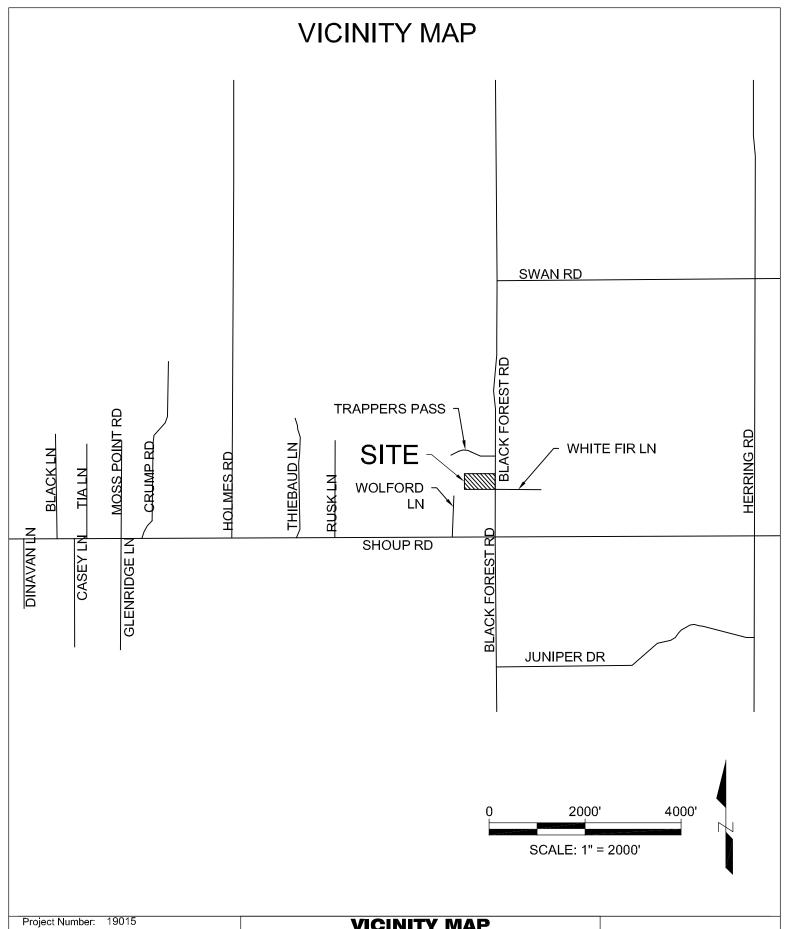
Call out Kettle Creek
Drainage Basin Planning
study. and any other
studies that wee done for
the original development of
this site.

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APPENDIX A

Vicinity Map Soils Map FEMA Map

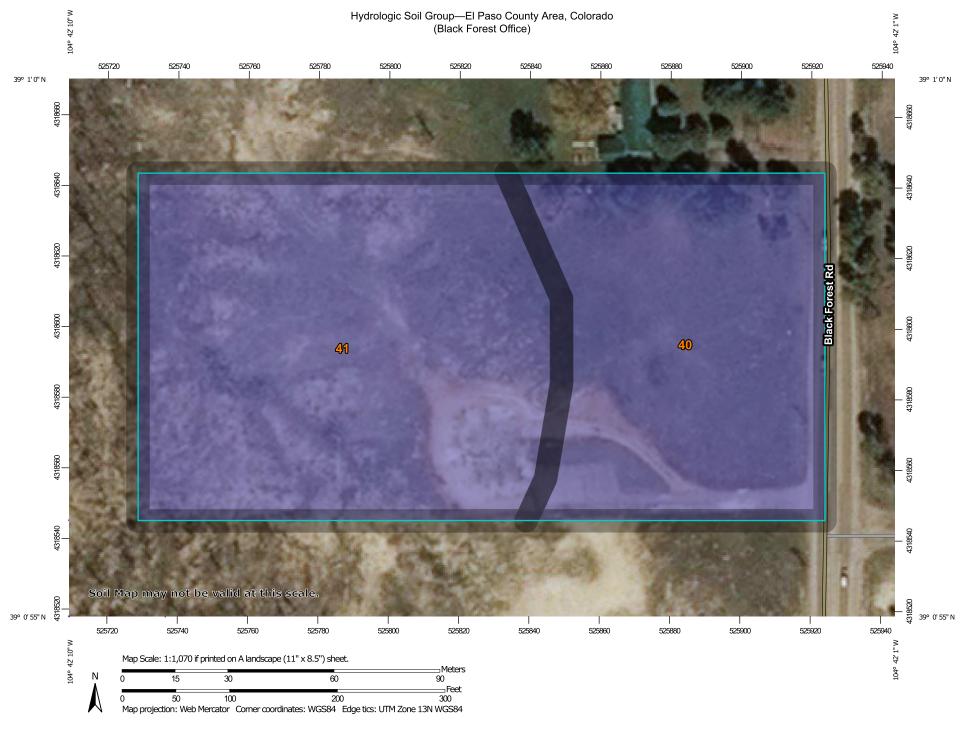


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Englewood, CO 80112
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www.2NCivil.com

VICINITY MAP **BLACK FOREST LLC**

Drawn By: TEW Checked By: EPT Revisions: 7-2-20





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24,000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil Water Features line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals В Transportation B/D Rails Please rely on the bar scale on each map sheet for map С measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available 0 Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Not rated or not available Date(s) aerial images were photographed: Sep 8, 2018—May 26, 2019 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. В B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
40	Kettle gravelly loamy sand, 3 to 8 percent slopes	В	1.9	40.6%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	В	2.8	59.4%
Totals for Area of Intere	est		4.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

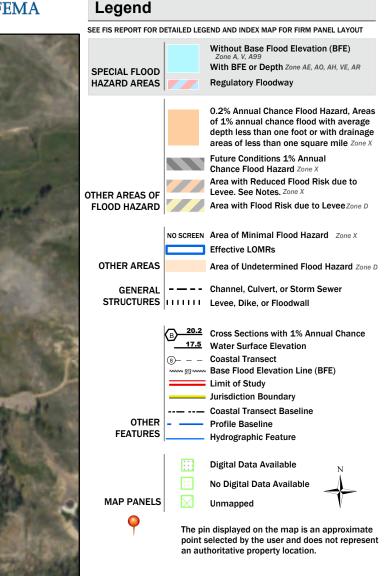
Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

National Flood Hazard Layer FIRMette

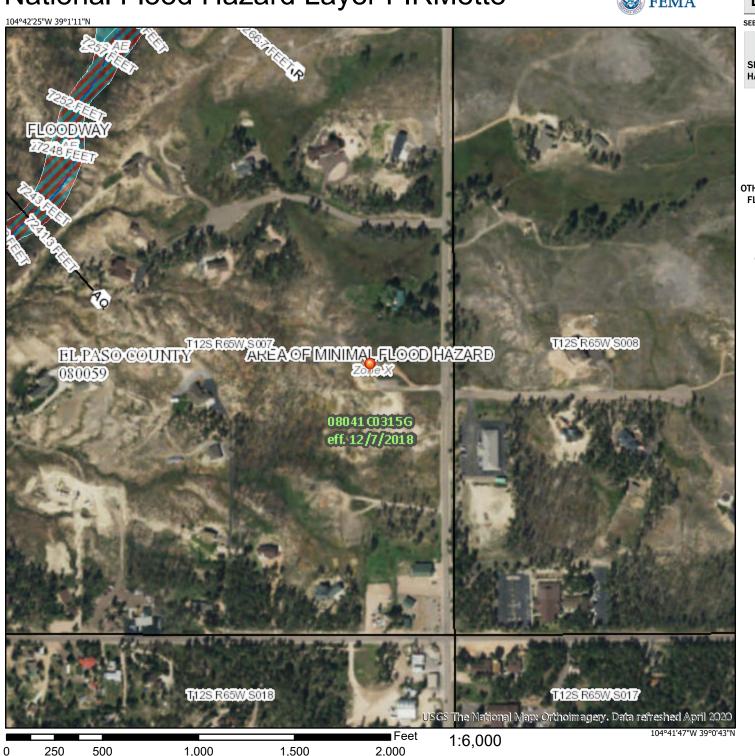




This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/16/2020 at 3:38 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



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APPENDIX B

Hydrologic Calculations

Black Forest Office

Composite Impervious Calculations - Proposed Conditions

Date: November 13, 2020



Proposed Conditions

Information from UCFCD Volume 1 Table 6-6 Type B NRCS Hydrologic Soils Group

Land Use	% Impervious	C5	C100
Streets (Paved)	100%	0.90	0.96
Streets (Gravel)	80%	0.59	0.74
Drive and Walks	100%	0.90	0.96
Roofs	90%	0.73	0.83
Lawns	0%	0.08	0.50

I. Land Use Breakdown

Area (square feet)

Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
PR-1	14,245	0	2,969	1,640	4,374	23,228
PR-2	0	1,007	2,735	4,401	26,055	34,197
PR-3	0	0	375	1,609	0	1,984

59,409

Area (acres)

Basin	Paved	Gravel	Drive/Walk	Roofs	Lawns	Σ Area
PR-1	0.33	0.00	0.07	0.04	0.10	0.533
PR-2	0.00	0.02	0.06	0.10	0.60	0.785
PR-3	0.00	0.00	0.01	0.04	0.00	0.046

Total 1.364

II. Composite Basin Imperviousness and Runoff Coefficients

			$I_{\text{Weighted C5}} = \Sigma \text{ (C5*Area) /}$	$I_{\text{Weighted C100}} = \Sigma \text{ (C100*Area) /}$	$I_{\text{Weighted Basin}} = \Sigma (\%I*Area) /$
Basin	Σ (% I * Area)	Σ Area (ac)	Σ Area	Σ Area	Σ Area
PR-1	0.43	0.533	0.73	0.86	80.5%
PR-2	0.17	0.785	0.24	0.59	21.9%
PR-3	0.04	0.046	0.76	0.85	91.9%

Composite Imperviousness Value for Watershed Tribuary to Pond (used in MHFD-Detention Spreadsheet for EDB Pond)

Rasins PR-1 & PR-2	7 1 2 2 2 2 2	1 22	% Watershed =	4F C10/
Basins PR-1 & PR-2	Σ Area (ac)	1.32	⁷⁰ Watershed =	45.61%

Calculation of Peak Runoff using Rational Method

 Company: 2N Civil

 Date: 11/9/2020
 Cells of

 Project: Black Forest Office
 Cells of

Cells of this color are for required user-input
Cells of this color are for optional override values
Cells of this color are for calculated results based on overrides

 $t_{i} = \frac{0.395(1.1 - C_{5})\sqrt{L_{i}}}{S_{i}^{0.33}}$ $t_{t} = \frac{L_{t}}{cov/G} = \frac{L_{t}}{60V}$

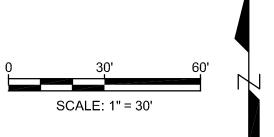
 $t_{minimum} = 10 \text{ (non-urban)}$ $Selected t_c = max(t_{minimum}, min(Computed t_c, Regional t_c))$

 $\frac{\text{Select UDFCD location for NOAA Atlas 14 Rainfall Depths from the pulldown list OR enter your own of the pull of the pull$

Q(cfs) = CIA

																	00(1111)	, V - C																					
							Runc	off Coeffic	ent, C				Overla	and (Initial) Flo	w Time				Channe	elized (Travel) F	low Time			Tim	ne of Concentr	ation		Ra	infall Intens	ity, I (in/hr)					Pea	ık Flow, Q (c	fs)		
Subcatch Nam		Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	s 2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	Overland Flow Length L _i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S _i (ft/ft)		Channelized Flow Length L _t (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)			Regional t _c (min)	Selected t _c (min)	2-yr	5-yr 10	yr 25-y	r 50-yr	100-yr	500-yr	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr
PR-	0	0.53	В	80.5	0.65	0.68	0.71	0.75	0.78	0.80	0.83	89.68	72.40	68.00	0.049	4.28	309.47	68.00	58.35	0.031	20	3.53	1.46	5.74	13.76	5.74	3.89	4.90 5.	1 6.5	7.35	8.23		1.34	1.77	2.15	2.63	3.04	3.51	
PR-	U	J.33	ь	60.5		0.73				0.86		69.06	72.40	66.00	0.049	3.74	309.47	00.00	36.33	0.031	20	3.33	1.40	5.20	13.70									1.91				3.77	
PR-2	0	70	В	21.9	0.14	0.16	0.23	0.39	0.45	0.53	0.62	11.35	74.90	72.00	0.256	1.95	172.30	72.00	55.00	0.099	20	6.28	0.46	2.41	23.03	5.00	4.04	5.09 5.	6.7	7.63	8.55		0.45	0.66	1.09	2.06	2.70	3.54	
1111-2	Ů	5.75	5	21.5		0.24				0.59		11.00	14.50	72.00	0.200	1.79	172.00	72.00	55.00	0.000	20	0.20	0.40	2.25	20.00									0.96				3.96	
PR-S	0	0.05	В	91.9	0.76	0.78	0.80	0.83	0.84	0.85	0.87	5.00			0.050	0.76	60.00			0.005	20	1.41	0.71	1.46	11.02	5.00	4.04	5.09 5.	94 6.7	7.63	8.55		0.14	0.18	0.22	0.26	0.30	0.34	
-						0.76										0.81								1.51										0.18		\longrightarrow		_	
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N1/2 NE1/4 SE1/4 SE1/4 OF SECTION 07, TOWNSHIP 12 SOUTH, RANGE 65 WEST OF THE 6TH P.M., EL PASO COUNTY, COLORADO





PROPOSED BASIN MAP

PROPOSED **BASIN MAP**

PR-BASIN

LEGEND ————— BUILDING LINE

EXISTING —— — — RIGHT OF WAY

CP 99 SPIKE IN STUMP

____ELEV.=7367.04'

Provide design points with historic and developed flows to

demonstrate the proposal. See checklist for further

comments to for a complete submittal.

SANITARY SEWER MAIN SANITARY SEWER MANHOLE SANITARY SERVICE LINE STORM SEWER MAIN STORM SEWER INLET STORM SEWER MANHOLE ----- 12" WATER LINE 8" WATER LINE - 4" WATER LINE FIRE HYDRANT VALVE WATER SERVICE & METER OVERHEAD UTILITY LINE

RANGE LINE

ELECTRIC MANHOLE LIGHT POLE POWER POLE ELECTRIC BOX RAIL POLE BURIED COMM. LINE GAS LINE

BURIED ELECTRIC LINE

MAJOR CONTOUR MINOR CONTOUR

LANDSCAPING STORM SEWER CLEANOUT STORM SEWER MANHOLE 0.0 .00 _ RUNOFF COEFFICIENT BASIN DESIGN POINT RUNOFF FLOW ARROW PROPOSED BASIN LIMITS

Summary Runoff Table

— *—5225* — —

CONTRIBUTING	CONTRIBUTING			
BASIN(S)	AREA (AC)	Q ₅ (cfs)	Q ₁₀₀ (cfs)	NOTES:
PR-1	0.53	1.91	3.77	Releases to EDB Pond
PR-2	0.79	0.96	3.96	Releases to EDB Pond
PR-3	0.05	0.18	0.34	Releases undetained (following historic flow path
	PR-1	BASIN(S) AREA (AC) PR-1 0.53 PR-2 0.79	BASIN(S) AREA (AC) Q ₅ (cfs) PR-1 0.53 1.91 PR-2 0.79 0.96	BASIN(S) AREA (AC) Q5 (cfs) Q100 (cfs) PR-1 0.53 1.91 3.77 PR-2 0.79 0.96 3.96

	N 89°53'11" W, 635.20'	EX. OVERHEAD- ELECTRIC LINE
Will need a design point here and	EX. CHICKEN COOP ELEV.=7348.02' 386	
discussion. What will happen here? concentrated flow?	PR-3 0.046 0.76 ac 0.85	
PR-2		BLACK BLACK
0.79 0.24 ac 0.59		2355 SK FORES 1380.2" W. 329.70. B.0.2" W. 329.70. 129.80. 12
	1364 EX.— SEPTIC SYSTEM	T ROAD ST. CHECTRIC METER EXI. TELEPHONE-
	PR-1 0.53 0.73	EX. 460 FILE ROLL AND
1360	OFFICE ac 0.86 - 7370- 7373	T371 EX. 12" DIA POLE POLE T305 B
1362	7369	EX. ASPHALT REMAIN

12790 BLACK FOREST ROAD

COLORADO SPRINGS, CO 80908-3402

PARCEL # 5207000003

CAUTION: NOTICE TO CONTRACTOR

THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE LOCAL UTILITY LOCATION CENTER AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATIONS OF THE UTILITIES. IT SHALL BE THE Know what's below.

RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT

Call before you dig. WITH THE PROPOSED IMPROVEMENTS SHOWN ON THE PLANS.



BENCHMARK

Provide two plan/maps; have them as the

last pages of the report. One to show historic conditions, one to show developed

See checklist for all the criteria of these

maps Drainage basins off and on site etc.

SURVEY CONTROL POINTS AS SHOWN HEREON. ALL ELEVATIONS ARE BASED UPON NAVD88 VERTICAL DATUM.

12660 BLACK FOREST ROAD COLORADO SPRINGS, CO 80908

PARCEL # 5207000005

Chapter 6 Hydrology

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent						Runoff Co	efficients					
Characteristics	Impervious	2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Hydrology Chapter 6

For Colorado Springs and much of the Fountain Creek watershed, the 1-hour depths are fairly uniform and are summarized in Table 6-2. Depending on the location of the project, rainfall depths may be calculated using the described method and the NOAA Atlas maps shown in Figures 6-6 through 6-17.

Table 6-2. Rainfall Depths for Colorado Springs

Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth
2	1.19	1.70	2.10
5	(1.50)	2.10	2.70
10	1.75	2.40	3.20
25	2.00	2.90	3.60
50	2.25	3.20	4.20
100	2.52	3.50	4.60

Where Z = 6,840 ft/100

These depths can be applied to the design storms or converted to intensities (inches/hour) for the Rational Method as described below. However, as the basin area increases, it is unlikely that the reported point rainfalls will occur uniformly over the entire basin. To account for this characteristic of rain storms an adjustment factor, the Depth Area Reduction Factor (DARF) is applied. This adjustment to rainfall depth and its effect on design storms is also described below. The UDFCD UD-Rain spreadsheet, available on UDFCD's website, also provides tools to calculate point rainfall depths and Intensity-Duration-Frequency curves² and should produce similar depth calculation results.

2.2 Design Storms

Design storms are used as input into rainfall/runoff models and provide a representation of the typical temporal distribution of rainfall events when the creation or routing of runoff hydrographs is required. It has long been observed that rainstorms in the Front Range of Colorado tend to occur as either short-duration, high-intensity, localized, convective thunderstorms (cloud bursts) or longer-duration, lower-intensity, broader, frontal (general) storms. The significance of these two types of events is primarily determined by the size of the drainage basin being studied. Thunderstorms can create high rates of runoff within a relatively small area, quickly, but their influence may not be significant very far downstream. Frontal storms may not create high rates of runoff within smaller drainage basins due to their lower intensity, but tend to produce larger flood flows that can be hazardous over a broader area and extend further downstream.

■ Thunderstorms: Based on the extensive evaluation of rain storms completed in the Carlton study (Carlton 2011), it was determined that typical thunderstorms have a duration of about 2 hours. The study evaluated over 300,000 storm cells using gage-adjusted NEXRAD data, collected over a 14-year period (1994 to 2008). Storms lasting longer than 3 hours were rarely found. Therefore, the results of the Carlton study have been used to define the shorter duration design storms.

To determine the temporal distribution of thunderstorms, 22 gage-adjusted NEXRAD storm cells were studied in detail. Through a process described in a technical memorandum prepared by the City of Colorado Springs (City of Colorado Springs 2012), the results of this analysis were interpreted and normalized to the 1-hour rainfall depth to create the distribution shown in Table 6-3 with a 5 minute time interval for drainage basins up to 1 square mile in size. This distribution represents the rainfall

Final Drainage Report Page 11



APPENDIX C

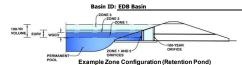
EDB Calculations

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches
2.25 inches
3.14 inches

Project: Black Forest Office



Watershed Information

Selected BMP Type =	EDB							
Watershed Area =	1.32	acres						
Watershed Length =	390	ft						
Watershed Length to Centroid =	160	ft						
Watershed Slope =	0.040	ft/ft						
Watershed Imperviousness =	45.61%	percent						
Percentage Hydrologic Soil Group A =	0.0%	percent						
Percentage Hydrologic Soil Group B =	100.0%	percent						
Percentage Hydrologic Soil Groups C/D =	0.0%	percent						
Target WQCV Drain Time =	40.0	hours						
Location for 1-hr Rainfall Depths = User Input								

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.											
Water Quality Capture Volume (WQCV) =	0.021	acre-feet									
Excess Urban Runoff Volume (EURV) =	0.064	acre-feet									
2-yr Runoff Volume (P1 = 1.19 in.) =	0.058	acre-feet									
5-yr Runoff Volume (P1 = 1.5 in.) =	0.085	acre-feet									
10-yr Runoff Volume (P1 = 1.75 in.) =	0.108	acre-feet									
25-yr Runoff Volume (P1 = 2 in.) =	0.140	acre-feet									
50-yr Runoff Volume (P1 = 2.25 in.) =	0.166	acre-feet									
100-yr Runoff Volume (P1 = 2.52 in.) =	0.199	acre-feet									
500-yr Runoff Volume (P1 = 3.14 in.) =	0.266	acre-feet									
Approximate 2-yr Detention Volume =	0.048	acre-feet									
Approximate 5-yr Detention Volume =	0.066	acre-feet									
Approximate 10-yr Detention Volume =	0.089	acre-feet									
Approximate 25-yr Detention Volume =	0.098	acre-feet									
Approximate 50-yr Detention Volume =	0.102	acre-feet									
Approximate 100-yr Detention Volume =	0.116	acre-feet									

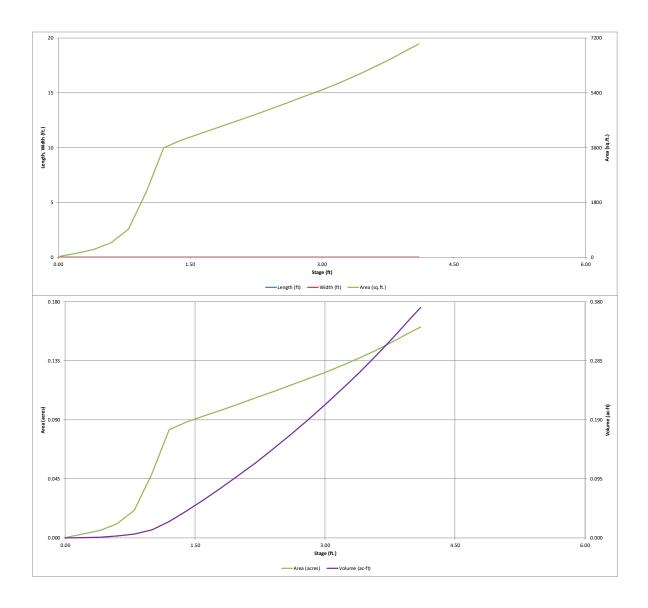
Define Zones and Basin Geometry

erine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.021	acre-fee
Zone 2 Volume (EURV - Zone 1) =	0.042	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	0.052	acre-fee
Total Detention Basin Volume =	0.116	acre-fee
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft 3
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$		ft²
Volume of Main Basin (V _{MAIN}) =	user	ft 3
Calculated Total Basin Volume $(V_{total}) =$	user	acre-feet

Depth Increment =	0.20	ft				Optional			
Stage - Storage	Stage	Optional Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft²)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool		0.00	-		-	13	0.000	4-	0
		0.20	-		-	121	0.003	13	0.000
		0.40				247	0.006	50	0.001
		0.60	-		-	465	0.011	121	0.003
		0.80 1.00	-		-	917 2,126	0.021	260 564	0.006
		1.00	_		_	3,590	0.049	1,135	0.013
		1.40	-		-	3,848	0.088	1,879	0.043
		1.60	_			4,044	0.093	2,668	0.061
	-	1.80	-			4,242	0.097	3,497	0.080
	-	2.00	-		-	4,442	0.102	4,365	0.100
		2.20	-		-	4,646	0.107	5,274	0.121
	-	2.40	1		-	4,855	0.111	6,224	0.143
		2.60	-		-	5,066	0.116	7,216	0.166
		2.80	-			5,279	0.121	8,251	0.189
		3.00	-		-	5,495	0.126	9,328	0.214
	-	3.20 3.40	-		-	5,726 5,978	0.131 0.137	10,450	0.240
		3.60	-		-	6,248	0.137	11,621 12,843	0.207
	-	3.80	_		-	6,538	0.150	14,122	0.324
		4.00	_		-	6,847	0.157	15,461	0.355
		4.10	-		-	7,008	0.161	16,153	0.371
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MHFD-Detention_v4 03 11-13-20.x/sm, Basin 11/10/2020, 11:49 AM

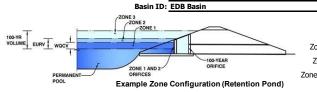


M#FD-Detention_w4 03 11-13-20.x/sm, Basin 11/10/2020, 11:49 AM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Black Forest Office



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.14	0.021	Orifice Plate
Zone 2 (EURV)	1.63	0.042	Orifice Plate
one 3 (100-year)	2.15	0.052	Weir&Pipe (Restrict)
•	Total (all zones)	0.116	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ Or

Depth at top of Zone using Orifice Plate = 1.63 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 6.50 inches

Orifice Plate: Orifice Area per Row = N/A inches

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.54	1.09					
Orifice Area (sq. inches)	0.14	0.14	0.50					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A

ft (relative to basin bottom at Stage = 0 ft)
ft (relative to basin bottom at Stage = 0 ft)
inches

 Calculated Parameters for Vertical Orifice

 Not Selected
 Not Selected

 Vertical Orifice Area =
 N/A
 N/A
 ft²

 Vertical Orifice Centroid =
 N/A
 N/A
 feet

Calculated Parameters for Overflow Weir

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.63	N/A	ft (relative to basin bottom at Stage =	0 ft) Height of Grate Upper Edge, $H_t =$	2.63	N/A	feet
Overflow Weir Front Edge Length =	4.00	N/A	feet	Overflow Weir Slope Length =	4.12	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V (Grate Open Area / 100-yr Orifice Area =	47.77	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet (Overflow Grate Open Area w/o Debris =	11.54	N/A	ft ²
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area	Overflow Grate Open Area w/ Debris =	5.77	N/A	ft ²
Debris Clogging % =	50%	N/A	%				

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

0.39

acre-ft

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	3.40	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.24	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.17	N/A	feet
strictor Plate Height Above Pipe Invert =	3.50		inches Half-Central Angle of	of Restrictor Plate on Pipe =	0.91	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

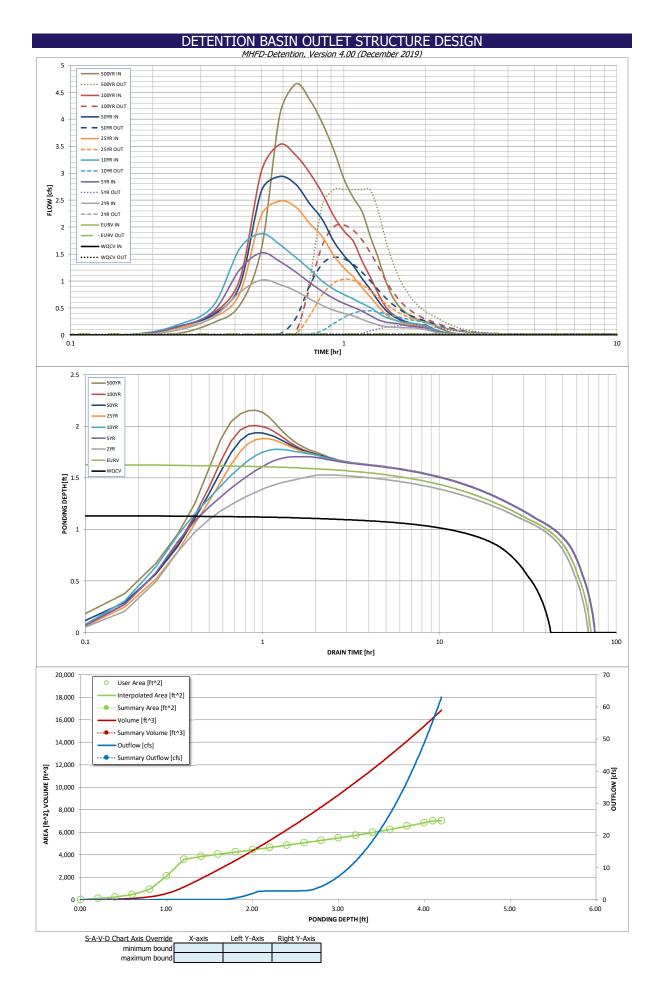
Rest

Fr

Spillway Invert Stage=	2.62	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	5.00	feet
Spillway End Slopes =	4.00	H:V
reeboard above Max Water Surface =	1.62	feet

Basin Volume at Top of Freeboard =

Routed Hydrograph Results	The user can over	rride the default CUF	HP hydrographs and	d runoff volumes by	entering new valu	es in the Inflow Hyd	drographs table (Co	olumns W through A	1 <i>F).</i>
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.021	0.064	0.058	0.085	0.108	0.140	0.166	0.199	0.266
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.058	0.085	0.108	0.140	0.166	0.199	0.266
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	0.5	0.7	1.2	1.5	1.9	2.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.13	0.35	0.53	0.93	1.17	1.46	2.04
Peak Inflow Q (cfs) =	N/A	N/A	1.0	1.5	1.9	2.5	2.9	3.5	4.7
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.2	0.4	1.0	1.4	2.0	2.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.8	0.9	1.1	1.0
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.0	0.1	0.1	0.2	0.2
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	62	60	64	62	60	58	56	53
Time to Drain 99% of Inflow Volume (hours) =	41	68	65	70	69	68	67	66	64
Maximum Ponding Depth (ft) =	1.14	1.63	1.53	1.71	1.78	1.88	1.94	2.01	2.15
Area at Maximum Ponding Depth (acres) =	0.07	0.09	0.09	0.10	0.10	0.10	0.10	0.10	0.11
Maximum Volume Stored (acre-ft) =	0.021	0.064	0.055	0.071	0.077	0.088	0.093	0.100	0.116



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00 0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.04
	0:20:00	0.00	0.00	0.10	0.16 0.44	0.20 0.55	0.13	0.17	0.16 0.41	0.23 0.55
	0:25:00	0.00	0.00	0.79	1.22	1.61	0.78	0.92	1.04	1.61
	0:30:00	0.00	0.00	1.02	1.52	1.88	2.23	2.68	3.05	4.09
	0:35:00	0.00	0.00	0.94	1.36	1.68	2.48	2.94	3.54	4.66
	0:40:00 0:45:00	0.00	0.00	0.82 0.67	1.17 0.97	1.44 1.22	2.37	2.80	3.33	4.37 3.94
	0:50:00	0.00	0.00	0.55	0.81	1.00	1.83	2.15	2.63	3.44
	0:55:00	0.00	0.00	0.46	0.68	0.85	1.48	1.74	2.21	2.90
	1:00:00	0.00	0.00	0.40	0.59	0.75	1.25	1.48	1.93	2.54
	1:05:00 1:10:00	0.00	0.00	0.36 0.29	0.51 0.44	0.67 0.59	1.08 0.88	1.28	1.74 1.37	2.29 1.83
	1:15:00	0.00	0.00	0.23	0.36	0.51	0.71	0.85	1.07	1.44
	1:20:00	0.00	0.00	0.19	0.28	0.41	0.53	0.64	0.77	1.04
	1:25:00	0.00	0.00	0.16	0.24	0.34	0.40	0.48	0.54	0.73
	1:30:00 1:35:00	0.00	0.00	0.15 0.14	0.22 0.21	0.29	0.31 0.25	0.37	0.40	0.55 0.44
	1:40:00	0.00	0.00	0.14	0.18	0.24	0.23	0.25	0.32	0.44
	1:45:00	0.00	0.00	0.13	0.17	0.22	0.19	0.22	0.22	0.31
	1:50:00	0.00	0.00	0.13	0.15	0.21	0.18	0.20	0.20	0.27
	1:55:00 2:00:00	0.00	0.00	0.11	0.14	0.19	0.17	0.19	0.18	0.24
	2:05:00	0.00	0.00	0.10	0.13	0.17 0.12	0.16 0.12	0.18	0.17 0.12	0.23 0.17
	2:10:00	0.00	0.00	0.05	0.07	0.09	0.08	0.09	0.09	0.12
	2:15:00	0.00	0.00	0.04	0.05	0.06	0.06	0.07	0.06	0.09
	2:20:00 2:25:00	0.00	0.00	0.03	0.03	0.05	0.04	0.05	0.04	0.06
	2:30:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:35:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	2:40:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:45:00 2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00 3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00 3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Į.	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft²]	Area [acres]	Volume [ft³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floo
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of
							outlets (e.g. vertical orifice
							overflow grate, and spillwa
							where applicable).
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POND OUTLET PIPE

D =	18 inches	
D =	1.5 ft	Q = 2.00 cfs
A =	1.77 sq ft	
V _{Allowed}	6.05 ft/s	

Use Type M Riprap Minimum

Required	d Riprap Rock Size		Req'd Riprap Type Based off P _d	Riprap Type	D ₅₀ -Median Rock Size (in.)
P_d	6.31	→	L	L	9
V =	6.05 ft/s	,	-	M	12
g =	32.20 ft/sq sec			Н	18
d =	0.1 (assumed value)			B18	18 (Grouted)

By Figure HS-20 in Drainage Criteria Manual Vol. 2, Type L Riprap is Mandated Using Type L $\,$

Length of Riprap Required - Basin Length Minimum

L – 4D		
D =	1.5 ft	
L =	6.00 ft	
$L = D^{1/2}$	x (V/2)	
$L = D^{1/2}$ $D =$	² x (V/2) 1.5 ft	
D =	1.5 ft	

Using the Greater of the Two Lengths, L = 6

Basin Minimum Width

W = 4D

D = 1.5 ft - Diameter of Circular Conduit
W = 6.00 ft

Minimum Thickness of Riprap, T

 $T = 1.75 \times D_{50}$ $D_{50} = 9 \text{ inches}$ T = 1.31 ft

N1/2 NE1/4 SE1/4 SE1/4 OF SECTION 07, TOWNSHIP 12 SOUTH, RANGE 65 WEST OF THE 6TH P.M., EL PASO COUNTY, COLORADO



DET STRUCTURE LET

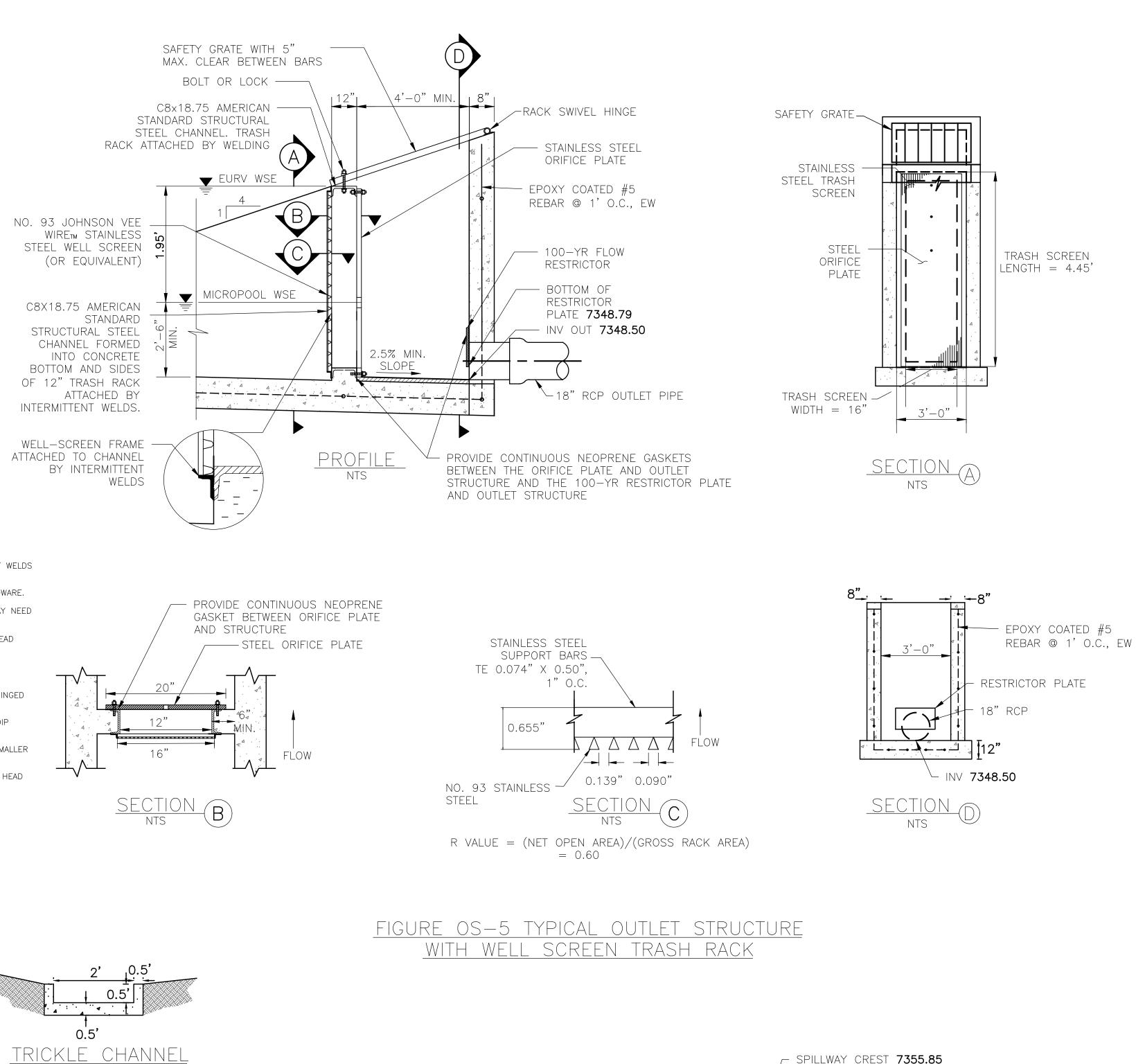
> ← 0 m 4

TOP OF POND 7356.00

- SPILLWAY ELEV **7354.52**

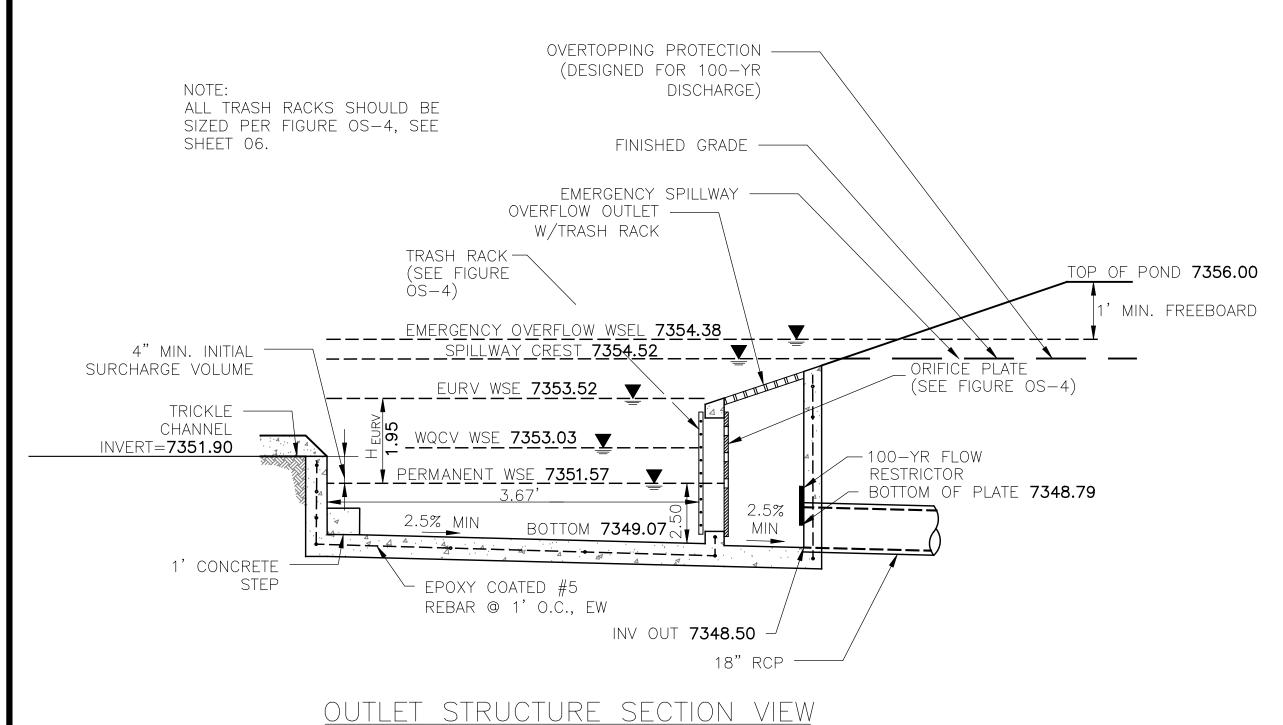
OUTLET STRUCTURE

DETAILS



4" FLOW DEPTH

EMERGENCY SPILLWAY



-STAINLESS STEEN BOLTS OR INTERMITTANT WELDS, SEE

ORIFICE HOLE SIZE = 13/32"

ORIFICE HOLE SIZE = 13/32"

STRUCTURAL STEEL CHANNEL FORMED INTO CONCRETE

7-3/4"-

7-3/4"-

7-3/4"-

ELEVATION

SECTION A-A

SECTION B-B

- 1. PROVIDE CONTINUOUS NEOPRENE GASKET MATERIAL BETWEEN THE ORIFICE PLATE AND CONCRETE.
- 2. BOLT PLATE TO CONCRETE 12" MAX. ON CENTER. SEE TABLE OS-2 FOR PLATE THICKNESS

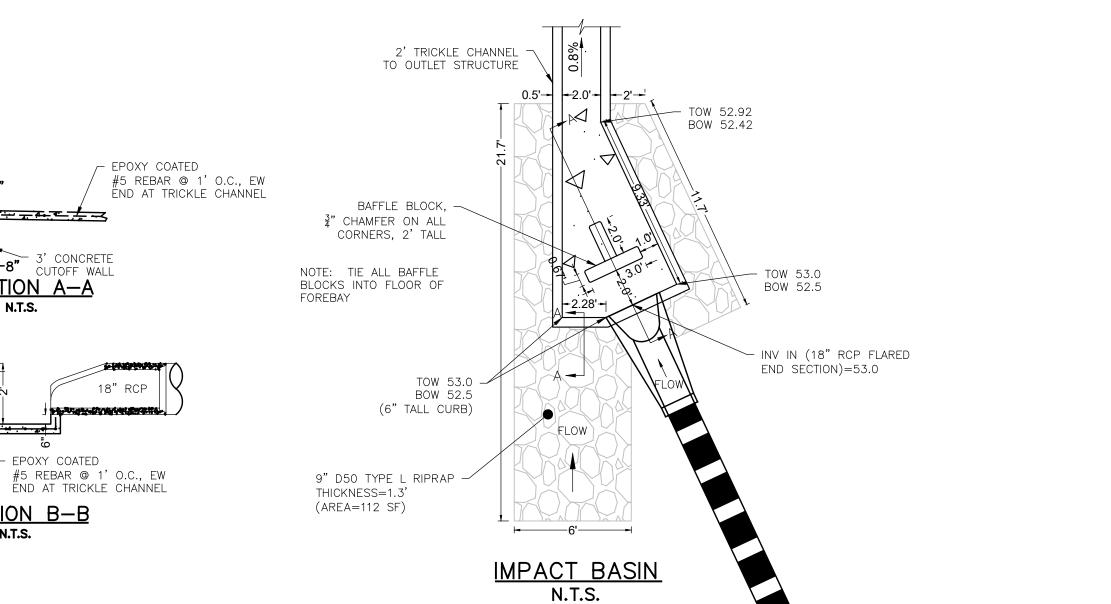
ORIFICE HOLE SIZE = 25/32" EURV AND WQCV TRASH RACKS:

- WELL-SCREEN TRASH RACKS SHALL BE STAINLESS STEEL AND SHALL BE ATTACHED BY INTERMITTENT WELDS ALONG THE EDGE OF THE MOUNTING FRAME.
- 2. BAR GATE TRASH RACKS SHALL BE ALUMINUM AND SHALL BE BOLTED USING STAINLESS STEEL HARDWARE. TRASH RACK OPEN AREAS ARE FOR SPECIFIED TRASH RACK MATERIALS. TOTAL TRASH RACK SIZE MAY NEED TO BE ADJUSTED FOR MATERIALS HAVING DIFFERENT OPEN AREA/GROSS AREA RATIO (R VALUE).
- 4. STRUCTURAL DESIGN OF TRASH RACKS SHALL BE BASED ON FULL HYDROSTATIC HEAD WITH ZERO HEAD

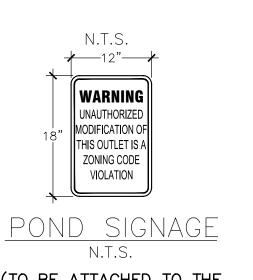
OVERFLOW SAFETY GRATES:

- 1. ALL SAFETY GRATES SHALL BE MOUNTED USING STAINLESS STEEL HARDWARE AND PROVIDED WITH HINGED AND LOCKABLE OR BOLTABLE ACCESS PANELS.
- 2. SAFETY GRATES SHALL BE STAINLESS STEEL, ALUMINUM, OR STEEL. STEEL GRATES SHALL BE HOT DIP GALVANIZED AND MAY BE HOT POWDER COATED AFTER GALVANIZING.
- 3. SAFETY GRATES SHALL BE DESIGNED SUCH THAT THE DIAGONAL DIMENSION OF EACH OPENING IS SMALLER
- 4. STRUCTURAL DESIGN OF SAFETY GRATES SHALL BE BASED ON FULL HYDROSTATIC HEAD WITH ZERO HEAD DOWNSTREAM OF THE RACK.

FIGURE OS-4 ORIFICE PLATE AND TRASH RACK DETAILS AND NOTES



TRICKLE CHANNEL



(TO BE ATTACHED TO THE OUTLET BOX OR POSTED NEARBY)



