May 28, 2021

Tech Contractors 3575 Kenyon Street, Ste 200 San Diego, California 92110



ENTECH

505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

Attn: Raul Guzman

Re: Additional Investigation, Road Subgrade Conditions

Meridian Ranch - Rolling Hills Ranch, Filings 1 through 4

SE of Sunrise Ridge Drive and Rex Road

El Paso County, Colorado

Ref: Entech Engineering, Inc., Soil, Geology and Geologic Hazard Evaluation - Meridian

Ranch - Rolling Hills Ranch, Filings 1 through 4, El Paso County, Colorado, Dated

September 20, 2019, Entech Job No. 190300

Dear Mr. Guzman:

As requested, personnel of Entech Engineering, Inc. have investigated the soils/groundwater conditions at Test Borings 24 and 33. The purpose of drilling was to evaluate the conditions with respect to shallow groundwater encountered in the original investigation.

The recent test borings encountered water at 12 and 15 feet, in Test Borings 24 and 33, respectively. Test Boring 24, when originally drilled, had water at 10 feet. Subsequent observation several days after drilling showed water at 2 feet. The shallow water noted on June 6, 2019 is believed to be the result of recent precipitation events running into the boring prior to the reading and not the active groundwater level. The original water depths during drilling and the recent water depths are believed to be the actual conditions.

We trust that this report has provided you with all the information that you required. Should you have any questions or require additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING

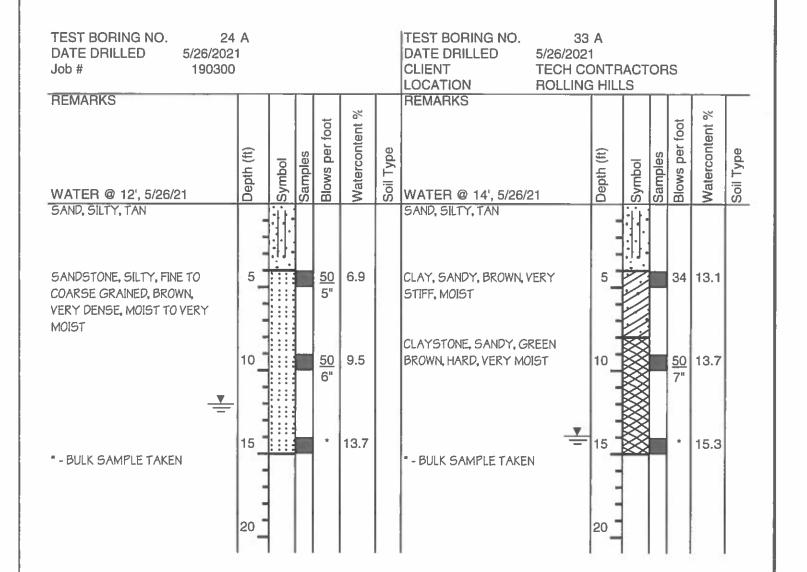
Me

President

JCG/am

Encl.

Entech Job No. 190300 AAprojects/2019/190300 road subgrade





	TEST	F BORING LO	OG
DRAWN:	DATE	CHECKED:	DATE:

JOB NO: 190300 FIG NO: A- 1



ENTECH ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

SUBSURFACE SOIL INVESTIGATION MERIDIAN RANCH - ROLLING HILLS RANCH, FILINGS 1 - 4 EL PASO COUNTY, COLORADO

Prepared for:

Tech Contractors 3575 Kenyon Street, Suite 200 San Diego, California 92110

Attn: Mr. Raul Guzman

July 15, 2019 Revised April 29, 2020

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Daniel P. Stegman

DPS/ts

Encl.

Entech Job No. 190300 AAprojects/2019/190300/190300 SSI Reviewed by:

President

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SUBSURFACE SOIL INVESTIGATION MERIDIAN RANCH - ROLLING HILLS RANCH, FILINGS 1 - 4 EL PASO COUNTY, COLORADO

1.0 INTRODUCTION

The project consists of the development of the site for the construction of single-family residences in Rolling Hills Ranch Filings 1 - 4. Development is expected to include site grading, installation of subsurface utilities, roadways, and drainage structures. The subdivision is in Meridian Ranch in the northern portion of El Paso County, Colorado. The approximate location of the project site is shown on the Vicinity Map, Figure 1. The test boring locations are shown on Figure 2, the Test Boring Location Plan, with the approximate delineation of soil types and potential groundwater areas depicted on the figures.

This report describes the subsurface investigation conducted for the site and provides recommendations for development design and construction. The Subsurface Soil Investigation included the drilling of forty-nine test borings across the site, collecting samples of soil, and conducting a geotechnical evaluation of the investigation findings. All drilling and subsurface investigation activities were performed by Entech Engineering, Inc. (Entech). The contents of this report, including the geotechnical evaluation and recommendations, are subject to the limitations and assumptions presented in Section 17.0.

2.0 PROJECT AND SITE DESCRIPTION

The project will consist of developing the site for single family residential structures. The planned lots are located in the Rolling Hills Ranch subdivision in Meridian Ranch. The investigation was performed at predetermined locations designated based on the roadway alignment and proposed grading on the site plan provided to us. At the time of drilling, the site was vacant and not developed. The site is not graded for the planned development. Site grading plans were provided to us with proposed cuts up to 13 feet and fills up to 15 feet. The majority of the cuts and fills are in the 2 to 10-foot range. The site has a gradual slope towards the southeast. Vegetation consisted of grasses and weeds. Existing residences and Falcon High School were located to the west and south of the site, undeveloped land immediately north, and Eastonville Road to the east. Natural earthen drainage trends to the southeast traversing the property from near the intersection of Rex Road and Sunrise Ridge Drive towards Eastonville Road at a point approximately 2000 feet northeast of Falcon High School. Fill piles of soil encompass approximately 3 acres in the northwest quadrant of the proposed subdivision. and approximately 20-acres of land south of this area was previously excavated, likely for nearby developments. The large area of soil removals and fill piles are not depicted on the topographic mapping for this site. Other smaller piles of manmade materials and straw bales were noted south and west of the natural drainage.

3.0 SUBSURFACE EXPLORATIONS AND LABORATORY TESTING

Subsurface conditions on the site were explored by drilling forty-nine test borings at the approximate locations shown on Figure 2. The boring locations were determined and staked by others. The borings were drilled within the proposed roadway alignments. The borings were drilled to depths of 20 to 25 feet below the existing ground surface (bgs). The drilling was performed using a truck-mounted, continuous flight auger-drilling rig supplied and operated by Entech. Boring logs descriptive of the subsurface conditions encountered during drilling are presented in Appendix A. At the conclusion and subsequent to drilling, observations for groundwater levels were made in each of the open boreholes.

Soil and bedrock samples were obtained from the borings utilizing the Standard Penetration Test (ASTM D-1586) using 2-inch O.D. split-barrel and California samplers. Results of the Standard Penetration Test (SPT) are included on the boring logs in terms of N-values expressed in blows per foot (bpf). Soil and bedrock samples recovered from the borings were visually classified and recorded on the boring logs. The soil and bedrock classifications were later verified utilizing laboratory testing and grouped by soil type. The soil and bedrock type numbers are included on the boring logs. It should be understood that the soil and bedrock descriptions shown on the boring logs may vary between boring location and sample depth. It should also be noted that the lines of stratigraphic separation shown on the boring logs represent approximate boundaries between soil and bedrock types and the actual stratigraphic transitions may be more gradual or variable with location.

Water content testing (ASTM D-2216) was performed on the samples recovered from the borings, and the results are shown on the boring logs. Grain-Size Analysis (ASTM D-422) and Atterberg Limits testing (ASTM D-4318) were performed on selected samples to assist in classifying the materials encountered in the borings. Volume change testing was performed on selected samples using the Swell/Consolidation Test (ASTM D-4546) and the FHA Swell Test in order to evaluate potential expansion/compression characteristics of the soil and bedrock. Soluble sulfate testing was performed on select soil samples to evaluate the potential for below grade degradation of concrete due to sulfate attack. The Laboratory Testing Results are summarized on Table 1 and are presented in Appendix B.

4.0 SUBSURFACE CONDITIONS

One soil type and two bedrock types were encountered in the test borings drilled for the subsurface investigation: Type 1: native slightly silty to silty sand, clayey to very clayey sand, and sand (SM-SW, SM, SC, SW), Type 2: slightly silty to silty sandstone and clayey to very clayey sandstone (SM-SW, SM, SC), and Type 3: sandy to very sandy claystone (CL). The soil and bedrock were classified in accordance with the Unified Soil Classification System (USCS) and American Association of State Highway and Transportation Officials (AASHTO) System using the laboratory testing results and the observations made during drilling.

4.1 Soil and Bedrock

Soil Type 1 classified as native slightly silty to silty sand, clayey to very clayey sand, and sand (SM-SW, SM, SC, SW). The sand was encountered in all of the test borings at the existing ground surface and extending to depth ranging from 1 to 14 feet below ground surface (bgs). Standard Penetration Testing conducted on the sand resulted in SPT N-values ranging from 4 to 48 blows per foot (bpf), indicating loose to dense states. Water content and grain size testing of selected soil samples resulted in a water content range of 1 to 21 percent, and 5 to 48 percent of the soil particles passing the No. 200 sieve. Atterberg limits testing resulted in Liquid Limits of 26, 29, and no value and Plastic Indexes of 16, 10, and non-plastic, respectively. FHA Swell testing resulted in swell pressure between 70 and 2970 psf, indicating low to high expansion potentials. Swell/Consolidation testing on a sample of silty sand resulted in a volume change of -1.2 percent, indicating a low to moderate consolidation potential. Sulfate testing resulted in 0.00, less than 0.01, and 0.01 percent soluble sulfate by weight, which indicates a negligible potential for below grade concrete degradation due to sulfate attack.

Soil Type 2 classified as slightly silty to silty sandstone and clayey to very clayey sandstone (SM-SW, SM, SC). The sandstone was encountered in all test borings, but Test Boring No. 31, underlying Soil Types 1 and 3 at depths ranging from 1 to 20 feet bgs and extending to depths ranging from 12 to 24 feet bgs and to the termination of the borings (20 to 25 feet). Standard Penetration Testing conducted on the sandstone resulted in SPT N-values from 27 to greater than 50 bpf, which indicates medium dense to very dense states. Water content and grain size testing resulted in a water content range of 2 to 30, and 7 to 50 percent of the soil particles passing the No. 200 sieve. Atterberg Limits testing resulted in Liquid Limit between 26 and 41 and no value with Plastic Indexes between 12 and 20 and non-plastic. Swell/Consolidation testing on the sandstone resulted in volume changes of -1.9 to 3.2 percent, indicating low to moderate consolidation potentials and moderate to high expansion potentials. Sulfate testing on the sandstone resulted in 0.00 and less than 0.01 percent sulfate by weight indicating the sandstone exhibits a negligible potential for below grade concrete degradation due to sulfate attack.

Soil Type 3 classified as sandy to very sandy claystone (CL). The claystone was encountered in Test Boring Nos. 2, 4, 5, 15, 16, 19 thru 24, 27, 31 thru 39, 41, 43, 46, and 48 underlying Soil Types 1 and 2 at depths ranging from 1 to 24 feet bgs and extending to depths ranging from 4

to 24 feet bgs or to the termination of the borings (20 to 25 feet). Standard Penetration Testing conducted on the claystone resulted in SPT N-values of 45 to greater than 50 bpf, which indicates very stiff to hard consistencies. Water content and grain size testing resulted in a water content range of 9 to 19, and 51 to 81 percent the soil size particles passing the No. 200 sieve. Atterberg limits testing resulted in Liquid Limits between 34 and 42 and Plastic Indexes between 15 and 20. FHA Swell testing resulted in a swell pressure of 90 psf, indicating a low expansion potential. Swell/Consolidation testing on the claystone resulted in volume changes of -2.0 to 2.5 percent, indicating moderate to high consolidation and expansion potentials. Sulfate testing on the claystone resulted in 0.00 percent sulfate by weight indicating the claystone exhibits negligible degradation to concrete due to sulfate attack.

4.2 Groundwater

Depth to groundwater was measured in each of the borings at the conclusion of drilling and subsequent to drilling. Groundwater was encountered in thirty-eight of the forty-nine test borings, ranging from depths of 2 to 23 feet bgs. Groundwater may affect building foundation excavations, roadway and utilities construction on this site. It should be noted that groundwater levels could change due to seasonal variations, changes in land runoff characteristics and future development including nearby areas. Table 2 presents the estimated depths to bedrock and groundwater.

5.0 PRELIMINIARY DEVELOPMENT CONSIDERATIONS

The following discussion is based on the subsurface conditions encountered in the test borings drilled at the site. This investigation is for the site discussed in 2.0 Project and Site Description. If subsurface conditions different from those described herein are encountered during construction or if the project elements change from those described, Entech Engineering, Inc. should be notified so that the evaluation and recommendations presented can be reviewed and revised if necessary.

Subsurface soil conditions encountered in the test borings drilled on the site generally consisted of native slightly silty to silty sand, clayey to very clayey sand, and sand overlying slightly silty to silty sandstone, clayey to very clayey sandstone, and sandy to very sandy claystone. Bedrock was encountered at depths ranging from 1 to 14 feet bgs. Depths to bedrock are indicated on

the test boring plan and in Table 2. Consideration should be given to several conditions on this site in planning and excavating the development including groundwater, expansive soils and sandstone/claystone materials.

5.1 Groundwater

Groundwater may impact the development. Table 2 presents the depth to groundwater measured in each boring. Subsequent to completion of overlot grading cuts per the grading plan presented to us, the measured water levels will be less than 10 feet in some areas of the site. Groundwater was measured as shallow as two feet in Test Boring No. 24. Fill is proposed in this area. The area may require stabilization prior to placing fill. Claystone was encountered at 4 feet. Unstable conditions should be expected where groundwater is shallow or close to excavated depths. Procedures and equipment to mitigate groundwater impact during and after construction should be anticipated. Pumps, cofferdams, wide area and localized drain systems and other procedures and equipment may be necessary. Shotrock and geotextiles may be appropriate for stabilizing excavations. An underdrain system can be considered for long term groundwater mitigation. Frequently, groundwater levels rise following development as result of increased irrigation and decreased potential area of evaporation.

5.2 Expansive Soils

Expansive soils [clayey sand, claystone, and potentially clay (not encountered in the test borings)] are present on the site exhibiting expansion potential from low to high. Expansive soils where encountered will require mitigation for residential construction. Damage to structures can occur due to expansive soils; occurrence and severity of distress can be reduced by moisture treatments and overexcavation mitigation approaches.

5.3 Sandstone and Claystone

Sandstone and claystone were encountered at shallow depths across the site. Excavation of sandstone and claystone should be expected to be moderate to difficult. Track type equipment likely will be needed to accomplish excavations particularly where harder materials or lenses are present. Upon completion of site grading per the plan provided to us, sandstone is expected to be exposed across the majority of the areas tested.

6.0 SITE GRADING

Shallow bedrock was encountered in approximately half of the test borings. Depth to bedrock in each boring is indicated on the Test Boring Plan, Figure 2. Excavation of dense and hard materials on site is expected to be moderate to difficult with heavy duty earthmoving equipment. Claystone and sandstone materials may require track equipment and ripping teeth. For conditions with no groundwater seepage, cut and fill slopes no steeper than 3 to 1 (horizontal to vertical) should be considered. If seepage occurs, then flatter slopes or a drain system should be considered. Recommendations may be subject to change depending upon particular field conditions.

6.1 Stripping

Debris, topsoil and organic materials should be stripped from the ground surface of areas to be filled. Any uncontrolled fill materials should be completely removed. The materials may be used as fill pending approval if they are free of organic material and debris. Although soft areas are not expected any soft or loose soils should be stabilized or removed to expose suitable material prior to placement of fill. Topsoil may be stored in stock piles and placed at the surface in landscape areas.

6.2 Fill Preparation

Surfaces which will receive fill should be scarified to depths of 6 inches, moisture conditioned to within 0 to 3 percent of optimum moisture, and compacted to minimum of 95 percent of Standard Proctor Dry Density (ASTM D-698) for cohesive materials and within 2 percent of optimum moisture, and compacted to minimum of 95 percent of Modified Proctor Dry Density (ASTM D-1557) for cohesionless soils. On-site natural soils and bedrock are anticipated to be used as site grading fill. Bedrock must be processed and broken down to small gravel-sized materials where placed in the fill. Expansive materials used for fill should be placed at sufficient moisture content to mitigate potential swell. The fill quality will influence the performance of foundations, slabs-on-grade, and pavements. Fill settlement can be minimized by placing thin lifts at suitable moisture content and by verification of compaction with frequent density tests.

6.3 Compaction

Overlot grading fill consisting of granular soils should be placed in lifts to exceed 6 inches following compaction and compacted to at least 95 percent of the maximum dry density determined by Modified Proctor (ASTM D-1557). Clay materials should be placed in compacted lifts less than 6 inches thick compacted to at least 95 percent of maximum Standard Proctor (ASTM D 698) dry density. Fills below 10 feet in depth should be moisture conditioned as above and compacted to 98 percent of Standard Proctor dry density (ASTM D 698) for cohesive materials or 98 percent of maximum modified Proctor Dry Density (ASTM D 1557) for granular materials. The soil materials should be placed at a moisture content conducive to adequate compaction, usually within ±2 percent of optimum moisture content. Fill placement and compaction should be observed and tested by Entech during construction to verify that adequate moisture and density has been achieved.

7.0 POND EMBANKMENT CONSTRUCTION

Test Borings 38 and 39 were drilled in the detention pond located in Tract G. The soils generally consisted of 9 to 10 feet of silty gravelly sand over claystone. The upper sandy soils were encountered at loose to medium dense states. Groundwater was measured at 11 to 18 feet after drilling. In general, the site soils encountered in the pond area are suitable for construction of the proposed pond structures and embankment. Based on the grading plan cuts and fills will be required to construct the pond. Cuts and fills range from 4 to 10 feet. It appears that the pond detention area will be above the groundwater levels. If excavations encroach on the groundwater level unstable soil conditions may be encountered.

Any areas to receive fill should have all topsoil, organic material or debris removed. Fill must be properly benched and compacted to minimize potentially unstable conditions in slope areas. Fill slopes should be 3:1 or flatter. The proposed plans show 4:1 embankment slopes. The subgrade should be scarified and moisture conditioned to within 2% of optimum moisture content and compacted to a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557, prior to placing new fill. Loose areas encountered at the embankment subgrade will require removal and recompaction prior to placing new fill. Areas receiving fill may require stabilization with rock or fabric if shallow groundwater conditions are encountered.

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Entech Engineering, Inc.

New fill should be placed in thin lifts not to exceed 6 inches after compaction while maintaining at least 95% of its maximum Modified Proctor Dry Density, ASTM D-1557. These materials should be placed at a moisture content conducive to compaction, usually 0 to ±2% of Proctor optimum moisture content. The placement and compaction of fill should be observed and tested by Entech during construction. Entech should approve any import materials prior to

placing or hauling them to the site.

8.0 UNDERGROUND UTILITY CONSTRUCTION

Generally, excavation is expected to be moderate to difficult utilizing heavy-duty track hoes. Rock buckets and rock teeth will likely be required where excavations extend into very hard sandstone or cemented materials. Special procedures or equipment may be required to remove water and/or achieve stability in utility trenches where excavations approach or intercept

groundwater.

Utilities including water and sewer lines are usually constructed beneath paved roads. Placement of fill and degree of compaction applied to trench backfill will influence performance of overlying structures including pavements. Fill placed into utility trenches should be compacted according to requirements of the local jurisdiction. Fill should be placed in horizontal lifts having compacted thickness of six inches or less and at a water content conducive adequate compaction, usually within ±2 percent of optimum water content. Typical compaction specifications would be similar to specifications in the Site Grading section. Mechanical

methods should be used for fill placement;

however, heavy equipment should be kept at a distance away from structures to avoid damage. No water flooding techniques of any type should be used for compaction or placement of utility

trench backfill.

Trench backfill should be performed in accordance with El Paso County specifications and requirements. Excavations and excavation shoring/bracing should be performed in accordance with OSHA guidelines.

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9.0 UNDERDRAIN SYSTEM

Depending on final site grading anticipated depths of excavations and structure foundations relative to groundwater occurrence, an underdrain system may be considered to be included as part of sewer system design and installation. The underdrain system drain pipe shall consist of smooth wall non perforated rigid PVC pipe placed at a minimum slope of 2 percent. Shallower pipe grades can be considered for larger diameter underdrain pipes and areas to daylight the drainage systems. Concrete or clay material fill may be strategically placed at the manhole locations to slow the water flow down the trench. The underdrain below sewer should be constructed with adequate depth to allow connection of residence foundation drain systems. Drain elements should be of appropriate slopes and sizes for anticipated flows. Maintenance of the underdrain system should be anticipated. Gravity outlet should be planned such that other developments and properties are not adversely affected.

10.0 PAVEMENT CONSIDERATIONS

Materials exposed at pavement subgrade elevations will be dependent upon native materials exposed at final overlot grading and the specific materials placed as fill at and near finish grade elevations. The predominate materials are generally expected to be silty sand, sandstone, clayey sand, and clay. Materials anticipated at subgrade elevation generally would be rated as good, but some areas likely would be rated as poor AASHTO classifications of A-1-b, A-2-6, and A-4 were determined for the sandstone and upper granular soils. Based on depth to claystone and estimated cut, claystone with AASHTO classification of A-6 and associated poor rating is likely not to be encountered. The claystone classifies as A-6 which has poor asphalt support characteristics. Thickness of asphalt pavements to be anticipated generally range between 4 to 5 inches of asphalt overlying 6 to 10 inches of basecourse depending on specific subgrade materials and Roadway Classification of each particular street. Cement treated subgrade thickness of 10 to 12 inches are common. Actual thickness may exceed anticipated thickness at some areas. For specific thickness determinations, a subsurface investigation and pavement design should be completed after completion of overlot grading.

11.0 ANTICIPATED RESIDENTIAL FOUNDATION SYSTEMS

Subsurface soil conditions consisted of granular materials with some areas of expansive clayey soils and claystone materials. We anticipate conventional spread footing foundation systems will be appropriate for residences constructed on the majority of the site. Where expansive materials are encountered at or near foundation grades, use of spread footings with overexcavation and replacement with non-expansive fill should be expected. Drilled pier foundations may be a suitable alternative where expansive soils are encountered. A Subsurface Soils Investigation report should be prepared after completion of overlot grading to address appropriate foundation systems. Perimeter below grade drain systems should be anticipated for all structures with basements. Overexcavation drains may also be recommended. Figures 3 and 4 present typical details. Shallow groundwater was encountered in numerous test borings. Temporary and permanent dewatering systems may be necessary at various foundation excavations. Shotrock and geotextiles may be appropriate for stabilizing excavations. An area wide subdrain may be considered for discharge of collected water.

12.0 RESIDENCE ON-GRADE FLOOR SLABS

On-grade floor slabs for the planned structures could be supported by on-site non-expansive soils or compacted, non-expansive, structural fill. Loose or expansive soils encountered at or near floor slab grade should be penetrated or overexcavated a distance below slab subgrade and replaced with a non-expansive structural fill to improve floor slab performance. If slab movement and cracks cannot be tolerated a structural floor system should be used. Evaluation of subgrade materials should be included within a Subsurface Soils Investigation for each specific lot.

13.0 CONCRETE DEGRADATION DUE TO SULFATE ATTACK

Sulfate solubility testing was conducted on eight samples recovered from the test borings to evaluate the potential for sulfate attack on concrete placed below surface grade. The test results indicated 0.00 to 0.01 percent soluble sulfate (by weight). The test results indicate the sulfate component of the in-place soils presents a negligible exposure threat to concrete placed below the site grade. Type II cement is recommended for the on-site soils. Additional testing should be conducted following completion of overlot grading.

14.0 EXCAVATION STABILITY

Excavation walls must be properly sloped/benched or otherwise supported in order to maintain stable conditions. All excavation openings and work execution shall conform to OSHA standards as in CFR 29, Part 1926.650-652 (Subport D).

15.0 SURFACE AND SUBSURFACE DRAINAGE

Surface drainage will influence performance of structures at the site including streets and residences. Drainage is recommended around each building perimeter at a minimum slope of 5 percent in the first 10 feet adjacent to exterior foundation walls and for unpaved areas, where possible. For paved areas and other impervious surfaces, a minimum slope of 2 percent is recommended. Drainage should be planned to avoid ponding of water. Collected water and irrigation should discharge well beyond foundation backfill zones. Surface runoff should be designed to avoid sheet flow and erosion. Slopes should be protected from erosion by materials such as mulch or appropriate plants or other methods. All fills and backfills should be properly compacted. Unprotected surfaces may be subject to undesirable, heavy erosion.

16.0 WINTER CONSTRUCTION

In the event construction occurs during winter, concrete and soil materials should be protected from freezing conditions. Concrete should not be placed on frozen soil and once concrete has been placed, it should not be allowed to freeze. Similarly, once exposed, the soil subgrades should not be allowed to freeze. During grading operations and subgrade preparation, care should be taken to avoid burial of snow, ice or frozen material within the planned construction area.

17.0 CONSTRUCTION OBSERVATIONS

It is recommended that Entech observe and document the following activities during construction of the building foundations.

- Excavated subgrades and subgrade preparation.
- Placement of foundation perimeter drains (if installed).
- Placement/compaction of fill materials.
- Placement/compaction of utility bedding and trench backfill.

18.0 CLOSURE

The subsurface investigation, geotechnical evaluation and preliminary recommendations presented in this report are intended for use by Tech Contractors with application to the planned development of the single-family residential project site located in the Rolling Hills Ranch Filings 1 - 4 subdivision in Meridian Ranch in northern El Paso County, Colorado. In conducting the subsurface soil investigation, laboratory testing, engineering evaluation and reporting, Entech Engineering, Inc. endeavored to work in accordance with generally accepted professional geotechnical and geologic practices and principles consistent with the level of care and skill ordinarily exercised by members of the geotechnical profession currently practicing in same locality and under similar conditions. No other warranty, expressed or implied is made. Additional subsurface investigations and testing are recommended to further evaluate the individual sites and roadways after final development plans are prepared and after the site has been graded. During final design and/or construction, if conditions are encountered which appear different from those described in this report, Entech Engineering, Inc. requests that it be notified so that the evaluation and recommendations presented herein can be reviewed and modified as appropriate.

If there are any questions regarding the information provided herein or if Entech Engineering, Inc. can be of further assistance, please do not hesitate to contact us.



TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

TECH CONTRACTORS ROLLING HILLS 190300

CLIENT PROJECT JOB NO.

SOIL DESCRIPTION	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, CLAYEY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND SILTY	SAND, VERY CLAYEY	SAND	SAND, CLAYEY	SAND	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND	SAND, CLAYEY	CLAY, SANDY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SANDSTONE, CLAYEY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY
UNIFIED CLASS.	SM-SW	SM-SW	SC	SM	WS-MS	SM	SM	SM	SC	SW	SC	SW	SM	SM-SW	SM	SM-SW	SW	SC	ರ	SM-SW	SM-SW	SM-SW	SM	SM	SM-SW	SM	SM-SW	SC	SM-SW	SM	သွ	SM	SM	SM	သွ	SM
SWELL/ CONSOL (%)															-1.2																					
FHA SWELL (PSF)				370					460					20					2970							220										
AASHTO CLASS.	A-1-b		A-2-6			A-1-b				A-1-b	A-2-4		A-1-b			A-1-b	A-1-b					A-1-b			A-1-b			A-2-6	A-1-b		A-2-6				A-6	A-1-b
SULFATE (WT %)	<0.01		0.01			0.00																													<0.01	<0.01
PLASTIC INDEX (%)	NP		16			ΝP				٩N	10		NP			ΔN	ΝP					٩N			d _N			14	NP		20				13	Ð
LIQUID LIMIT (%)	N		53			N				N N	26		N			N	N/					N/			≥			32	NV		37				56	N
PASSING NO. 200 SIEVE (%)	8.1	6.1	14.0	15.2	8.4	17.0	18.0	15.6	48.3	4.7	13.3	4.8	13.2	5.9	34.7	11.5	4.9	12.1		6.9	5.4	9.6	17.8	19.6	6.0	20.7	7.3	18.6	7.3	14.2	17.1	12.5	16.0	14.3	38.9	17.5
DRY DENSITY (PCF)															112.9																					
WATER (%)															10.0																					
DEPTH (FT)	2.3	သ	2	2-3	2-3	2-3	2-3	9	2	2-3	2-3	2-3	2	2	2-3	5	2-3	2	က	5	5	2-3	2	2	2.3	2-3	2	9	0	2	ည	2	2	9	8	15
TEST BORING NO.	9	8	2	=	2	23	24	32	27	-	ည	13	14	16	19	92	28	90	99	99	31	88	ස	42	43	47	49	_	17	18	22	2	41	44	9	6
SOIL	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2	2	7	2	2	2	2	2	2

TABLE 1 (cont.)

SOIL DESCRIPTION	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY					
UNIFIED CLASS.	SM	SM	သင	SM	SM	SM-SW 8	SM-SW S	SM	SM	သွ	သွင	SM	သွင	၁၄	SM	SC	သွ	SC	SM	SC	ಠ	ರ	ದ	ರ	ರ	ಠ	占	ರ	ರ	J _O
SWELL/ CONSOL (%)			-0.4							-1.9				3.2			-0.4					1.0	0.0			-0.7			0.7	2.5
FHA SWELL (PSF)																												96		
AASHTO CLASS.		-		A-1-b	A-2-4					A-2-6	A-6			A-6		A-2-6								A-6	A-6					A-7-6
SULFATE (WT %)			0.00	<0.01																										_
PLASTIC INDEX (%)				NP	NP					12	14			14		17								15	17					20
LIQUID LIMIT (%)				N	N N					29	31			28		41								34	34					45
PASSING NO. 200 SIEVE (%)	15.5	26.1	35.4	12.3	28.7	11.6	10.1	16.2	15.5	20.3	48.5	17.8	19.9	49.7	21.2	28.3	49.6	41.1	13.4	45.5	65.1	56.1	58.8	54.2	59.6	51.1	59.7	63.6	56.0	80.8
DRY DENSITY (PCF)			116.5							110.3				84.0			119.9				:	126.8	120.5	99.3		103.3			114.3	115.0
WATER (%)			11.4							9.3				7.4			4.5					7.2	9.5	12.7		12.5			11.5	16.5
DEPTH (FT)	10	2	2	10	15	10	2	10	15	50	22	50	15	50	22	15	2	15	20	15	2	9	20	9	15	20	15	υ.	위	=
TEST BORING NO.	12	3	37	40	25	23	35	27	-	4	2	4	15	20	21	28	59	39	45	46	6	5	16	22	88	48	36	54	8	83
SOIL	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	8	ဗ	ဇာ	9	ဇ	က	9	က	က	3

Table 2: Summary of Test Borings and Water Measurements*

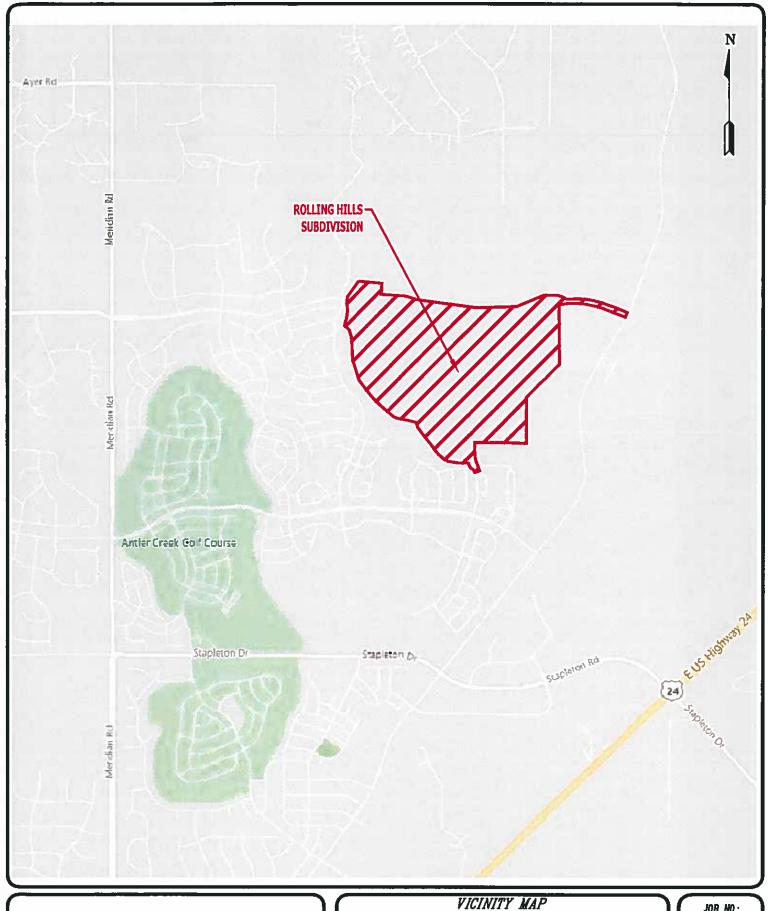
Test	Depth of	Depth to	Depth to	Cut & Fill**	Estimated	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
1	20.0	9.0	9.0	0 to -2	7021.3	7012.3
2	25.0	9.0	13.0	-2 to -4	7031.5	7018.5
3	25.0	1.0	15.0	-2 to -4	7032.3	7017.3
4	20.0	1.0	dry	-2 to -4	7044.0	dry
5	25.0	4.0	14.0	-2 to -4	7044.8	7030.8
6	25.0	14.0	10.0	0 to +2	7054.7	7044.7
7	20.0	1.0	16.5	+2 to +4	7058.6	7042.6
8	20.0	9.0	13.0	0 to -2	7060.1	7047.1
9	20.0	14.0	10.0	+4 to +6	7069.7	7059.7
10	20.0	14.0	14.0	0 to -2	7077.5	7063.5
11	20.0	9.0	9.0	0 to +2	7071.6	7062.6
12	20.0	9.0	14.0	0 to -2	7087.3	7073.3
13	20.0	9.0	14.0	0 to -2	7092.0	7078.0
14	25.0	14.0	18.5	-6 to -8	7105.3	7086.8
15	20.0	9.0	18.0	0 to -2	7108.4	7090.4
16	25.0	9.0	16.0	0 to -2	7110.9	7094.9
17	20.0	1.0	17.5	0 to -2	7121.7	7104.2
18	20.0	4.0	dry	0 to +2	7120.7	dry
19	20.0	4.0	dry	+2 to +4	7126.5	dry
20	20.0	1.0	dry	outside cut/fill	7125.4	dry
21	25.0	1.0	10.0	-6 to -8	7105.7	7095.7
22	20.0	4.0	18.5	-6 to -8	7106.0	7087.5
23	20.0	9.0	dry	+2 to +4	7092.3	dry
24	25.0	4.0	2.0	0 to +2	7072.9	7070.9

Table 2: (Continued)

Test	Depth of	Depth to	Depth to	Cut & Fill**	Est.	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
25	20.0	1.0	12.0	0 to +2	7068.8	7056.8
26	20.0	1.0	17.0	-6 to -8	7049.2	7032.2
27	20.0	9.0	8.0	0 to +2	7071.2	7063.2
28	20.0	9.0	13.5	0 to -2	7082.9	7069.4
29	25.0	4.0	12.0	outside cut/fill	7084.4	7072.4
30	20.0	10.0	8.0	0 to +2	7066.7	7058.7
31	20.0	14.0	dry	0 to -2	7057.5	dry
32	25.0	14.0	13.0	0 to -2	7045.4	7032.4
33	25.0	9.0	7.0	0 to -2	7052.7	7045.7
34	20.0	1.0	9.0	+2 to +4	7042.0	7033.0
35	20.0	3.0	dry	0 to -2	7065.4	dry
36	25.0	1.0	23.0	-6 to -8	7049.4	7026.4
37	20.0	1.0	dry	-2 to -4	7038.8	dry
38	25.0	12.0	10.0	-6 to -8	7032.4	7022.4
39	20.0	9.0	4.0	-6 to -8	7032.5	7028.5
40	20.0	9.0	10.0	+12 to +14	7032.1	7022.1
41	20.0	1.0	17.0	outside cut/fill	7039.1	7022.1
42	25.0	9.0	14.0	outside cut/fill	7046.0	7032.0
43	25.0	4.0	19.0	outside cut/fill	7049.0	7030.0
44	20.0	1.0	dry	outside cut/fill	7064.0	dry
45	25.0	4.0	11.0	outside cut/fill	7072.1	7061.1
46	25.0	4.0	22.0	outside cut/fill	7065.0	7043.0
47	20.0	1.0	dry	outside cut/fill	7058.7	dry
48	20.0	1.0	dry	outside cut/fill	7047.6	dry
49	25.0	14.0	12.0	outside cut/fill	7029.5	7017.5

⁻ Measurement taken subsequent to drilling- Cut and Fill estimates based on map provided by the client





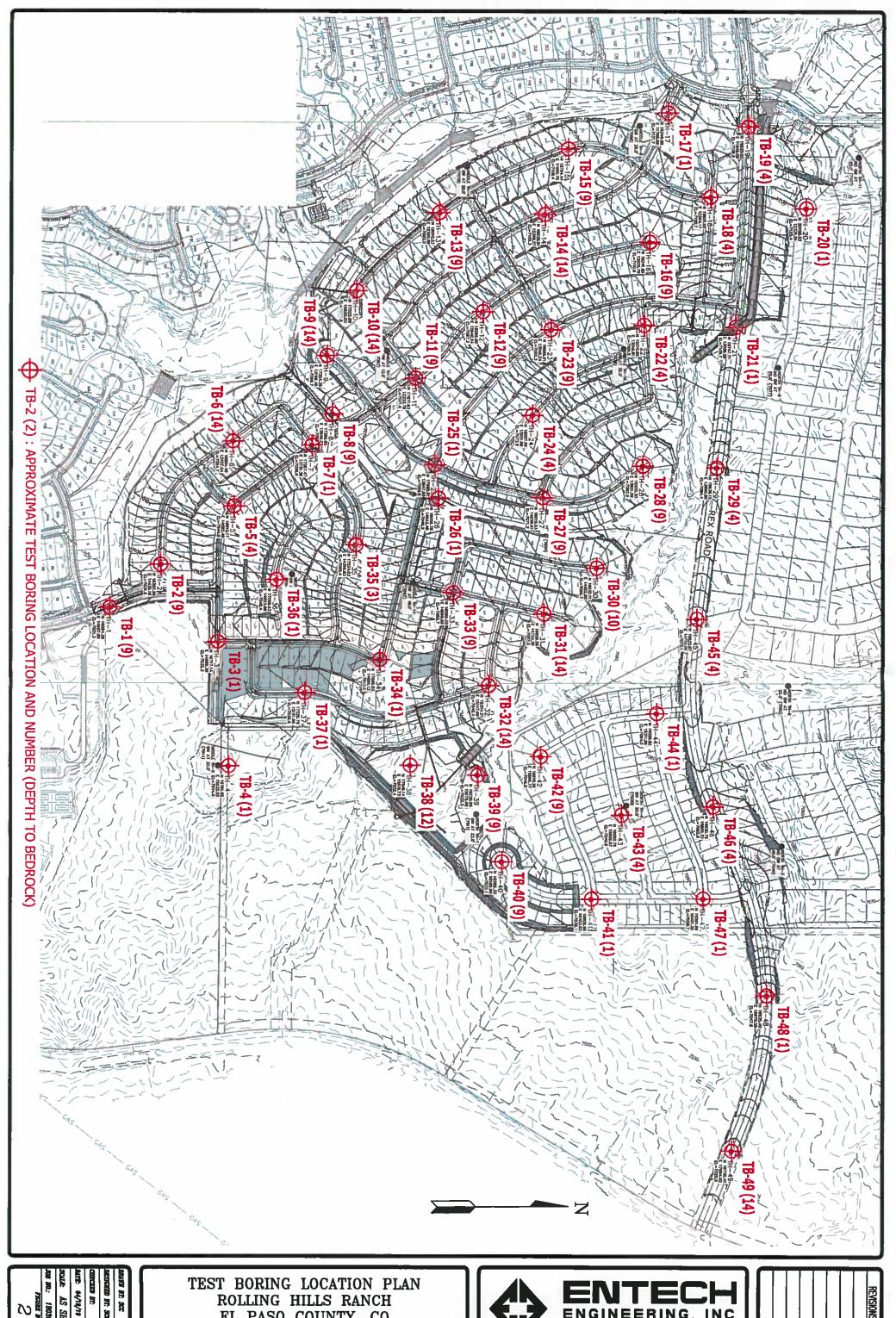


VICINITY MAP									
ROLLING HILLS RANCH									
EL PASO COUNTY, CO									
FOR: TECH CONTRACTORS									

DRAWN BY: DATE DRAWN: SC 04/18/19 DESIGNED BY: CHECKED: SC SC

JOB NO.: 190300

FIG. NO.:



MITE 4/14/19

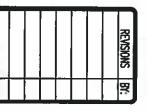
SCALE A/14/19

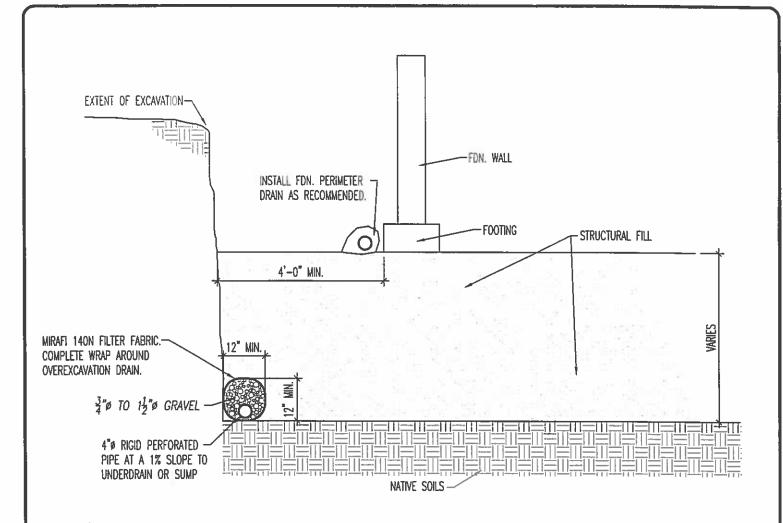
DES MIL 190300

FROME RE: STATE OF SCE

EL PASO COUNTY, CO FOR: TECH CONTRACTORS







OVEREXCAVATION DRAIN DETAIL

N.T.S.

NOTE:

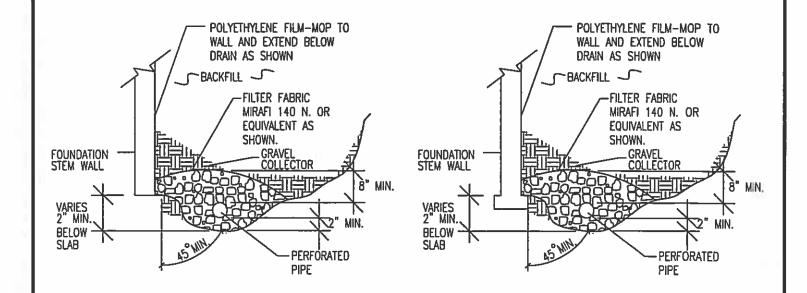
EXTEND DRAIN TO SUMP AS REQ'D.



OVEREXCAVATION	DRAIN	DETAIL

DRAWN BY: DATE DRAWN: DESIGNED BY: CHECKED:

JOB NO.: 190300 FIC. NO.: 3



NOTES:

- -GRAVEL SIZE IS RELATED TO DIAMETER OF PIPE PERFORATIONS-85% GRAVEL GREATER THAN 2x PERFORATION DIAMETER.
- -PIPE DIAMETER DEPENDS UPON EXPECTED SEEPAGE. 4-INCH DIAMETER IS MOST OFTEN USED.
- -ALL PIPE SHALL BE PERFORATED PLASTIC. THE DISCHARGE PORTION OF THE PIPE SHOULD BE NON-PERFORATED PIPE.
- -FLEXIBLE PIPE MAY BE USED UP TO 8 FEET IN DEPTH, IF SUCH PIPE IS DESIGNED TO WITHSTAND THE PRESSURES. RIGID PLASTIC PIPE WOULD OTHERWISE BE REQUIRED.
- -MINIMUM GRADE FOR DRAIN PIPE TO BE 1% OR 3 INCHES OF FALL IN 25 FEET.
- -DRAIN TO BE PROVIDED WITH A FREE GRAVITY OUTFALL, IF POSSIBLE. A SUMP AND PUMP MAY BE USED IF GRAVITY OUT FALL IS NOT AVAILABLE.

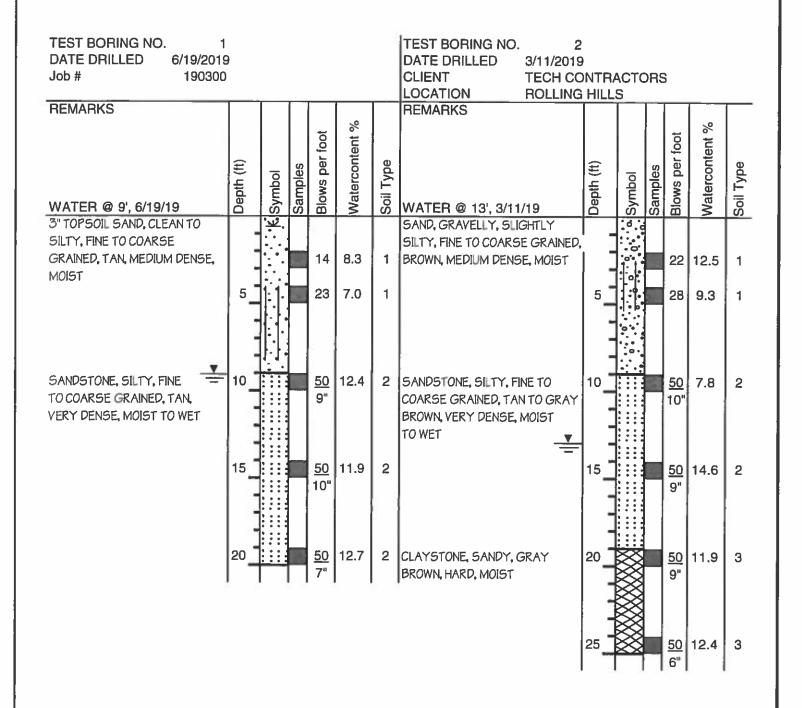


DRAWN: DATE: DESIGNED: CHECKED:

*JOB N*O.: 190300

FIG NO.:

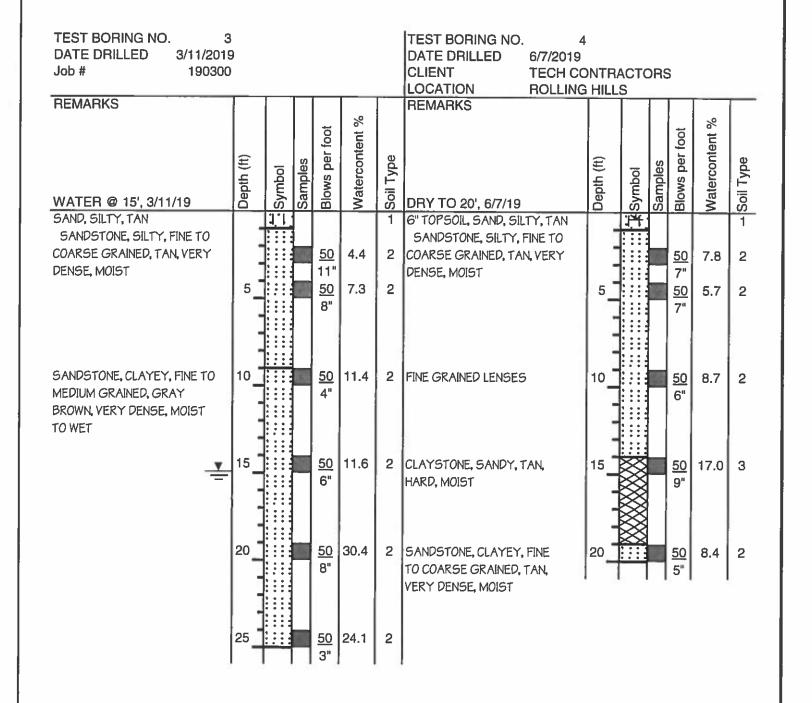
APPENDIX A: Test Boring Logs





TEST BORING LOG									
DRAWN:	DATE	CHECKED	7/1/19						

JOB NO.: 190300 FIG NO.:

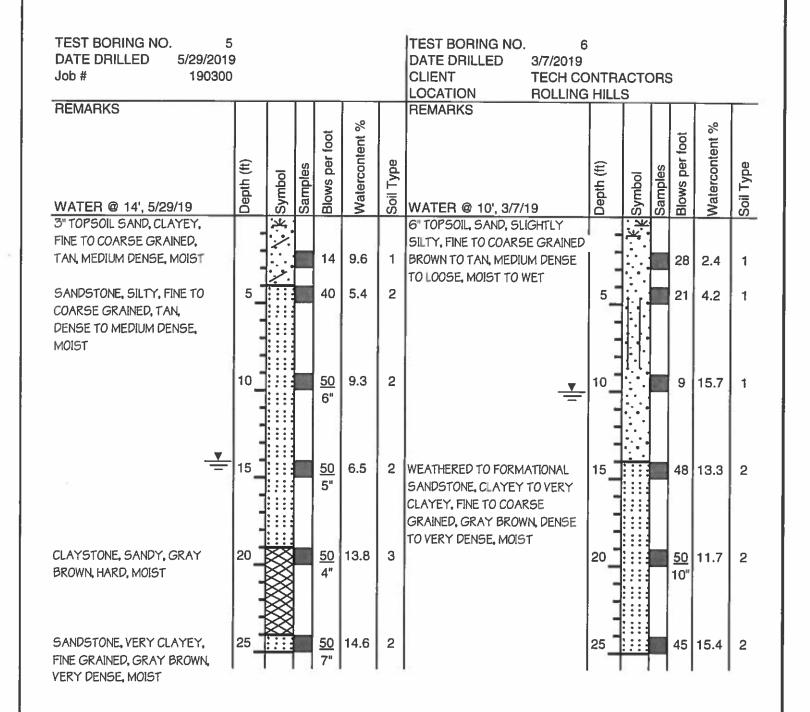




	TEST	BORING LOC	3	
DRAWN:	DATE:	CHECKED	DATE:	

ЈОВ NO.: 190300

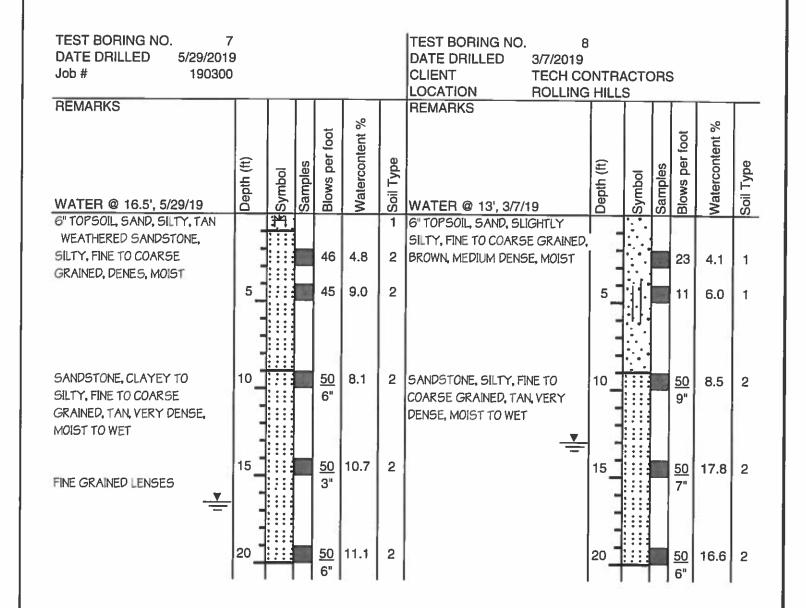
FIG NO:





	TEST	BORING LOG	· · · · · · · · · · · · · · · · · · ·
DRAWN:	DATE:	CHECKED:	7/1/19

JOB NO.: 190300 FIG NO.: A- 3





	TEST BORING LOG		
DRAWN:	DATE:	CHECKED	7/1/19
			

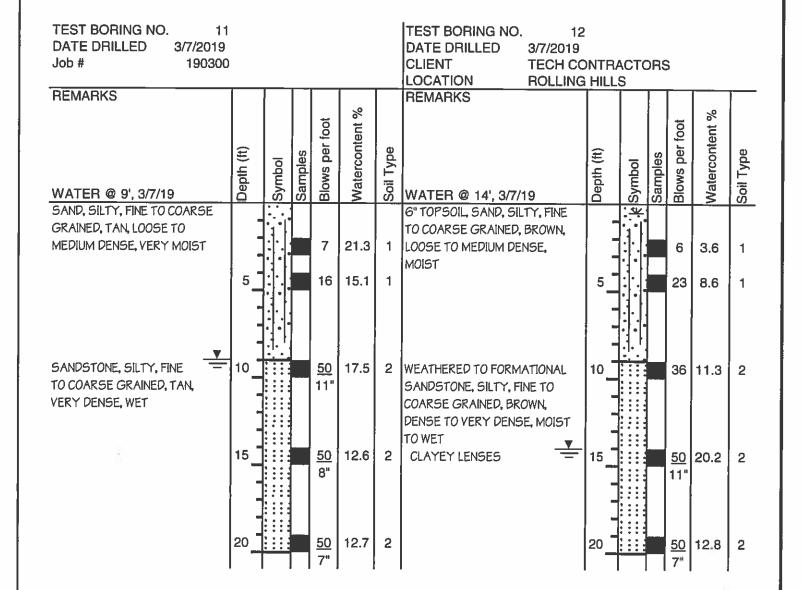
JOB NO.: 190300

TEST BORING NO. TEST BORING NO. 10 DATE DRILLED 3/7/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Watercontent Watercontent Blows per Soil Type Depth (ft) Soil Type Samples Samples Symbol Symbol WATER @ 10', 3/7/19 WATER @ 14', 3/7/19 : <u>*</u> 6" TOPSOIL, SAND, SILTY, FINE 뽀 6" TOPSOIL, SAND, SILTY TO TO COARSE GRAINED, BROWN, CLAYEY, FINE TO COARSE 2.7 MEDIUM DENSE, DRY TO MOIST 16 1 GRAINED, TAN, MEDIUM DENSE, 26 6.2 1 MOIST 5 11 6.6 1 5 19 7.8 1 10 5 SAND, CLAYEY, FINE TO 18.0 1 10 27 12.4 COARSE GRAINED, GRAY BROWN, LOOSE, WET 15 SANDSTONE, SILTY, FINE TO <u>50</u> 8.7 15 12.5 SANDSTONE, CLAYEY, <u>50</u> COARSE GRAINED, TAN, VERY FINE TO COARSE GRAINED. 10" DENSE, MOIST BRPOWN, VERY DENSE TO DENSE, WET <u>50</u> 6" 10.9 2 WEATHERED ZONE 45 13.8



TEST BORING LOG			
DRAWN:	DATE	CHECKED: L DATE:	

JOB NO.: 190300 FIG NO.:





TEST BURING LOG				
DRAWN:	DATE:	CHECKED:	DATE:	

JOB NO.: 190300 FIG NO.:

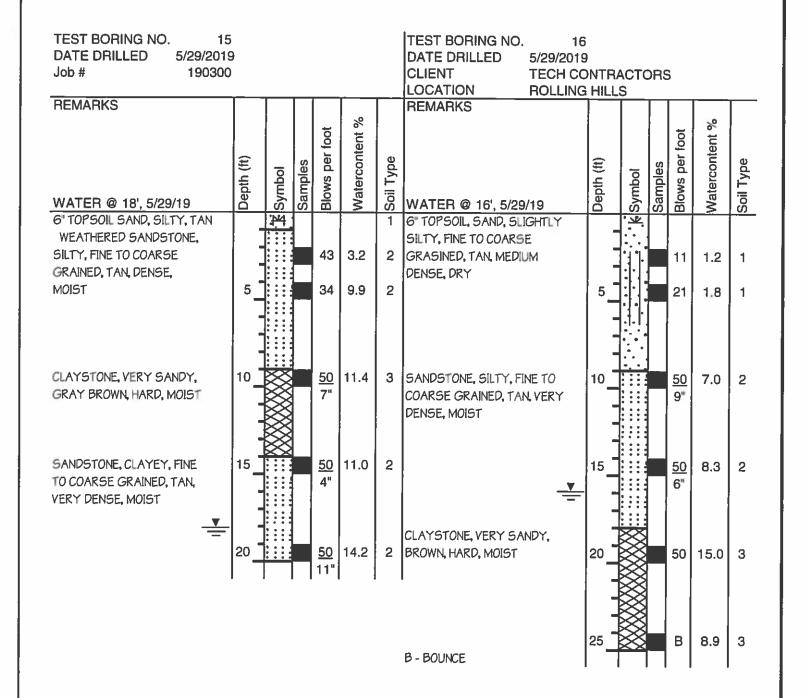
TEST BORING NO. 13 TEST BORING NO. 14 DATE DRILLED DATE DRILLED 5/29/2019 5/29/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Soil Type Depth (ft) Samples Samples Symbol Symbol WATER @ 14', 5/29/19 WATER @ 18.5', 5/29/19 6" TOPSOIL, SAND, CLEAN TO علا 6" TOPSOIL, SAND, SILTY, FINE SILTY, FINE TO COARSE TO COARSE GRAINED, TAN. GRAINED, TAN, LOOSE TO 11 1.4 LOOSE TO MEDIUM DENSE. 13. 1.8 1 MEDIUM DENSE, MOIST DRY TO MOIST 5 6.3 1 14 7 2.3 1 WEATHERED TO FORMATIONAL 10 45 8.4 2 | FINE GRAINED LENSES 10 24 9.1 SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, DENSE TO VERY DENSE. MOIST TO WET 15 48 8.9 2 SANDSTONE, SILTY, FINE TO 15 2 50 6.7 11" COARSE GRAINED, TAN, VERY DENSE, MOIST TO WET <u>50</u> 11.5 20 50 10.6 2 11" 50 12.6 2 9"



TEST BORING LOG				
DRAWN;	DATE	CHECKED:	7/1//19	

JOB NO.: 190300

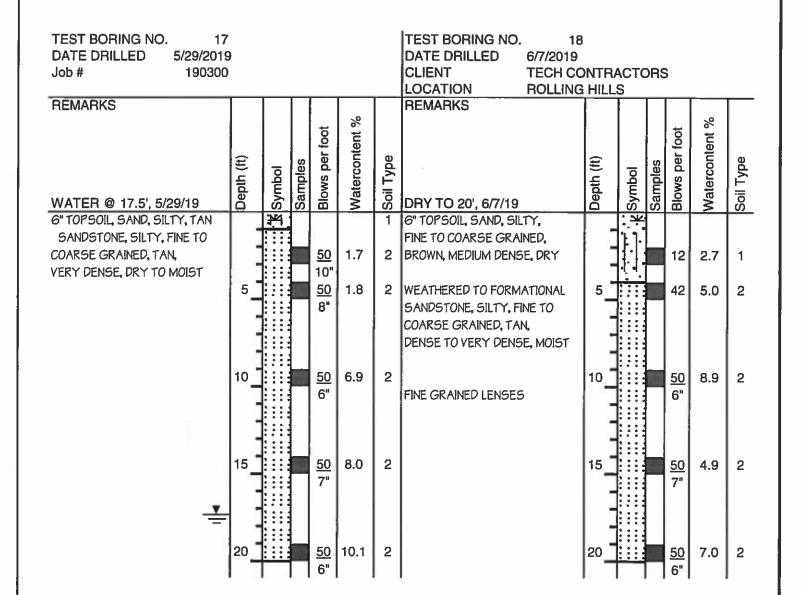
> FIG NO.: A- 7





TEST BORING LOG			
DRAWN:	DATE	CHECKED: A PATE!	

JOB NO.: 190300 FIG NO.:





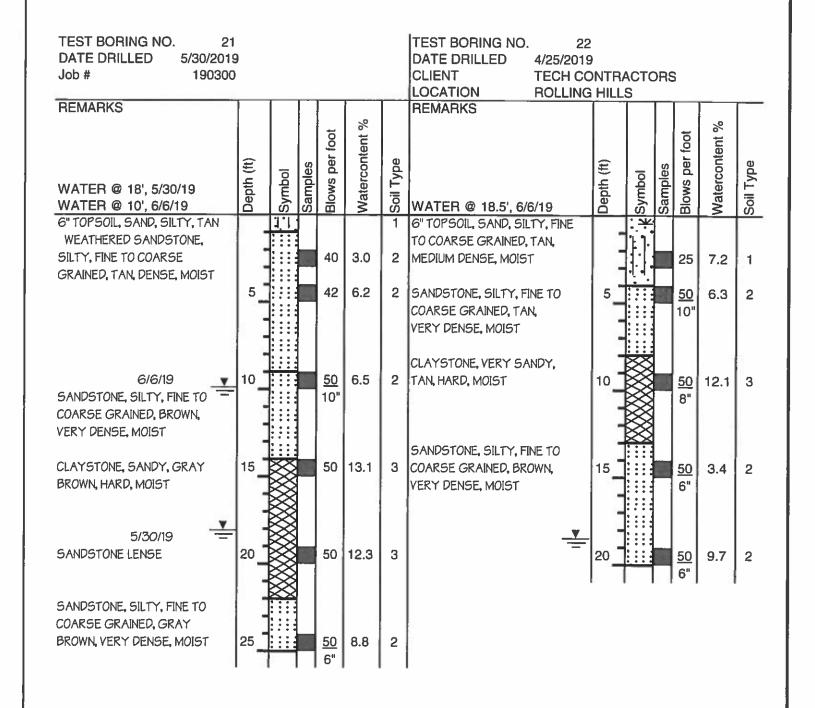
TEST BORING LOG					
DRAWN:	DATE:	CHECKED	h	7/1/19	

TEST BORING NO. 19 TEST BORING NO. 20 DATE DRILLED 6/7/2019 DATE DRILLED 5/30/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Samples Soil Type Samples Symbol Symbol DRY TO 20', 5/30/19 DRY TO 20', 6/7/19 CAVED TO 19', 6/6/19, DRY 24 6" TOPSOIL, SAND, SILTY, FINE 14 6" TOPSOIL, SAND, SILTY, TAN TO COARSE GRAINED, GRAY SANDSTONE, SILTY TO BROWN, MEDIUM DENSE, MOIST 21 7.8 CLAYEY, FINE TO COARSE <u>50</u> 4.8 2 GRAINED, TAN, VERY DENSE, 10" CLAYSTONE, SANDY, GRAY 5 <u>50</u> 10.9 3 DRY TO MOIST <u>50</u> 8.6 2 9" BROWN, HARD, MOIST 9" SANDSTONE, SILTY, FINE TO 10 <u>50</u> 7.8 2 10 50 6.5 2 COARSE GRAINED, TAN, 8" 9" VERY DENSE, MOIST 15 <u>50</u> 5.7 2 CLAYSTONE, SANDY, GRAY 15 3 10.4 <u>50</u> 8" BROWN, HARD, MOIST <u>50</u> 8.9 SANDSTONE, VERY CLAYEY. 2 <u>50</u> 8.0 2" FINE TO COARSE GRAINED. BROWN, VERY DENSE, MOIST



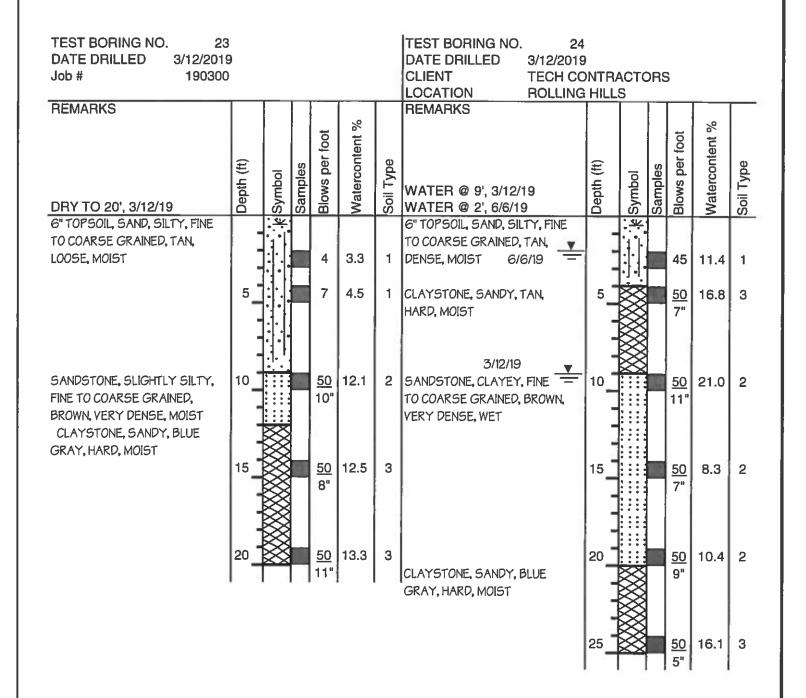
TEST BORING LOG					
DRAWN:	DATE	CHECKED L DATE			

JOB NO.: 190300 FIG NO.:



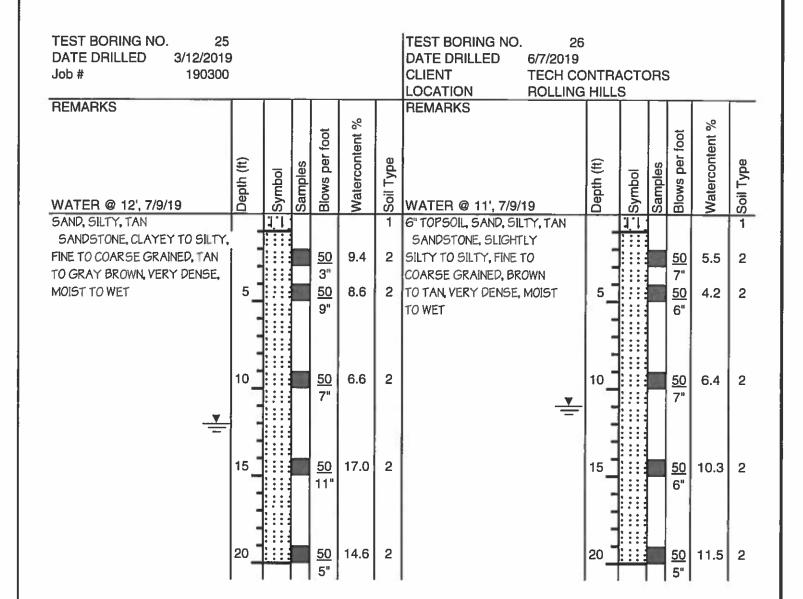


TEST BORING LOG				
DRAWN	DATE:	CHECKED: L DATE		
			_	



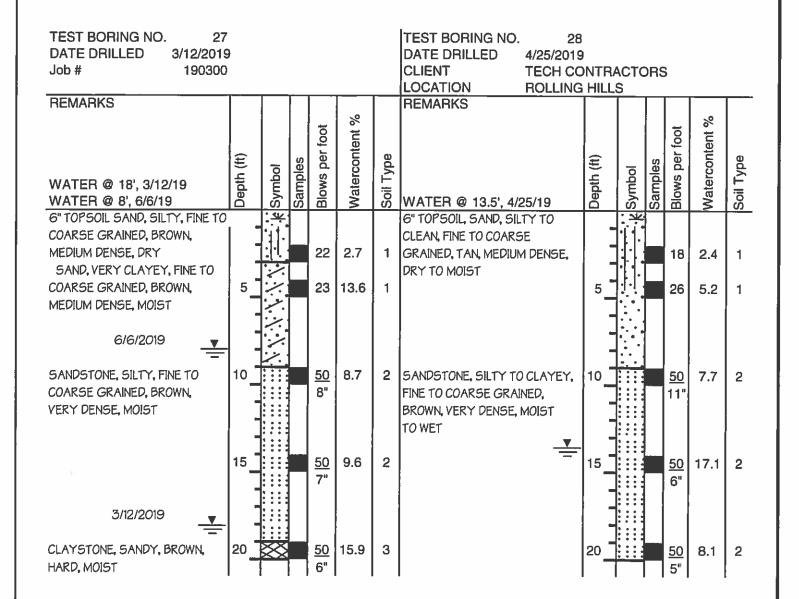


	TE	ST BORING LO	3
DRAWN:	DATE:	CHECKED:	7.12 19



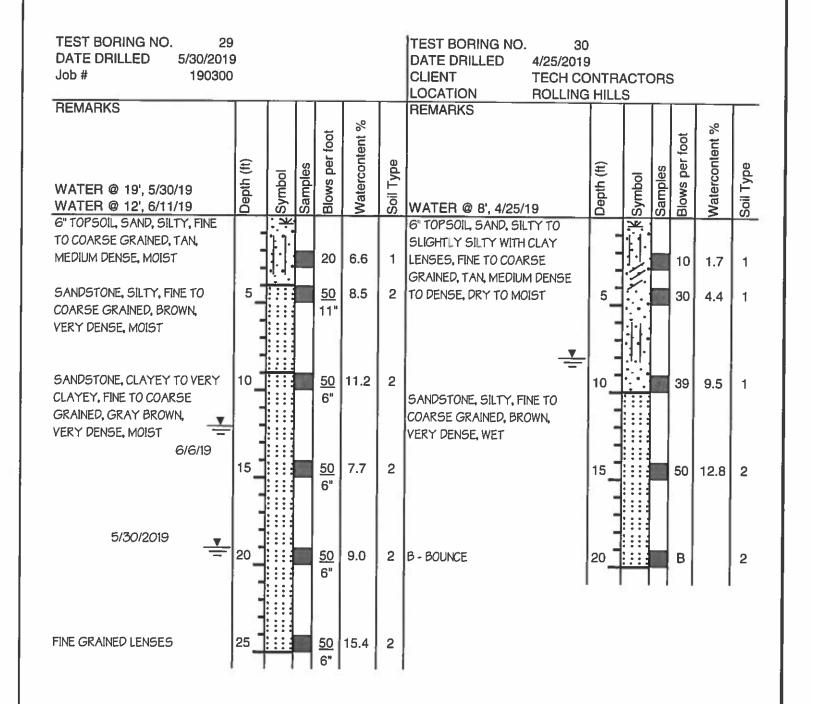


TEST BORING LOG			
DRAWN:	DATE	CHECKED	DATE: 7.12.19



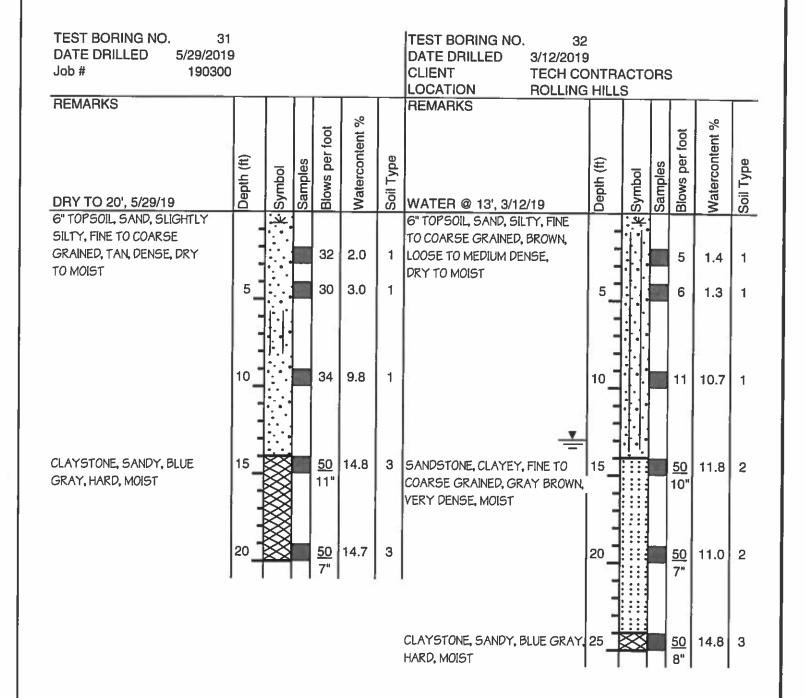


	3		
DRAWN	DATE:	CHECKED:	DATE 19



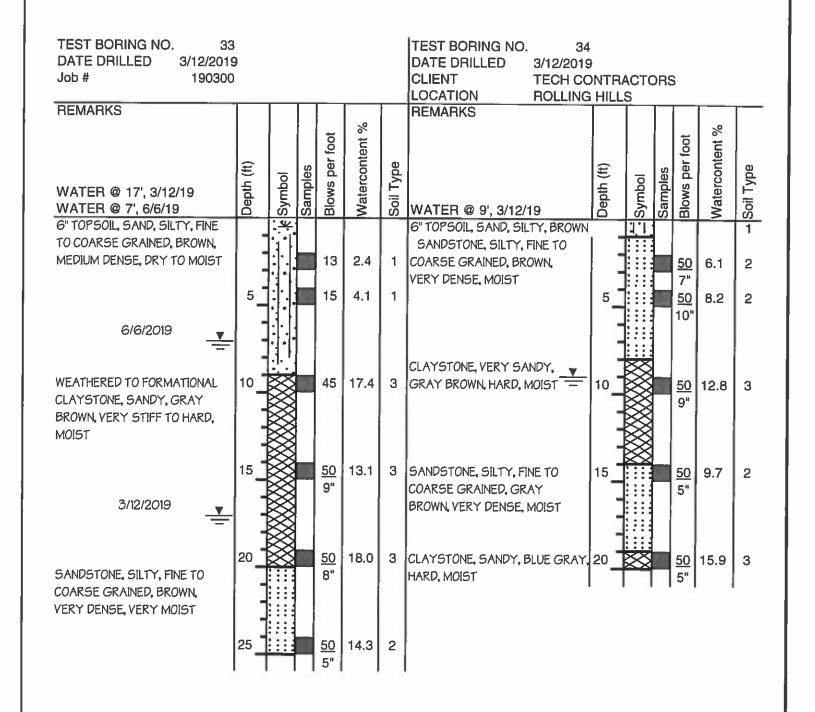


	i		
DRAWN;	DATE	CHECKED	DATE: 7-12-19
			





	TE	ST BORING LOG	
DRAWN:	DATE	CHECKED	PATE/12/19





	TE	ST BORING LO	G
DRAWN:	DATE:	CHECKED:	DATE: 7/12/19

TEST BORING NO. 35 TEST BORING NO. 36 DATE DRILLED 3/12/2019 DATE DRILLED 3/11/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Watercontent % Blows per foot Blows per foot Watercontent Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol DRY TO 20', 3/12/19 WATER @ 13.5', 7/9/19 <u> 44</u> 6" TOPSOIL SAND, SILTY, FINE SAND, SILTY, TAN 1.1 TO COARSE GRAINED, TAN. SANDSTONE, SILTY, FINE TO DENSE, MOIST 48 3.6 COARSE GRAINED, TAN, VERY <u>50</u> 3.1 2 SANDSTONE, SLIGHTLY SILTY 7" DENSE, MOIST 2 TO SILTY, FINE TO COARSE 50 6.0 5 50 3.7 2 GRAINED, BROWN, VERY DENSE. 6" MOIST 10 <u>50</u> 8.9 2 10 <u>50</u> 10.9 2 9" 6" 9.7 2 CLAYSTONE, VERY SANDY, BLUE 15. 50 15 12.2 <u>50</u> GRAY, HARD, MOIST CLAYSTONE, SANDY, BLUE GRAY, HARD, MOIST <u>50</u> 11.7 3 SANDSTONE, CLAYEY, FINE TO 20 2 <u>50</u> 13.4 COARSE GRAINED, GRAY BROWN 10" TO BROWN, VERY DENSE. MOIST TO WET <u>50</u> 2 16.8



	TES	ST BORING LOC	ì	
DRAWN	DATE:	CHECKED:	1/12/19	

JOB NO: 190300 FIG NO:

TEST BORING NO.

37

DATE DRILLED Job#

3/12/2019 190300

TEST BORING NO. DATE DRILLED

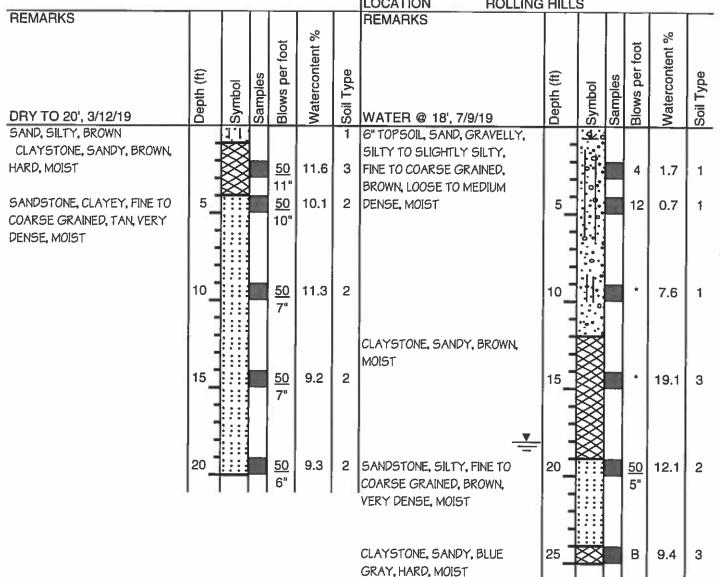
38 6/7/2019

CLIENT

TECH CONTRACTORS

LOCATION

ROLLING HILLS



" - BULK SAMPLE TAKEN

B-BOUNCE



	TES	ST BORING LOG	
DRAWN:	DATE	CHECKED	7/12/19

JOB NO. 190300 FIG NO.:

TEST BORING NO. 39 TEST BORING NO. 40 DATE DRILLED 5/29/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS ROLLING HILLS** LOCATION **REMARKS** REMARKS Blows per foot Blows per foot Natercontent Watercontent Depth (ft) Samples Soil Type Samples Symbol Symbol WATER @ 11', 7/9/19 WATER @ 10', 3/12/19 <u> 44</u> 6" TOPSOIL, SAND, SILTY, FINE <u>علا:</u> 6" TOPSOIL, SAND, SILTY, FINE TO COARSE GRAINED, TAN. TO COARSE GRAINED, TAN, MEDIUM DENSE, MOIST TO 13 | 10.7 1 DENSE TO MEDIUM DENSE. 32 4.8 1 WET MOIST 5 21 111.7 1 27 6.2 1

50 10.2

14.8

18.4

2

* - BULK SAMPLE TAKEN

CLAYSTONE, SANDY, GRAY

SANDSTONE, VERY CLAYEY,

CLAYSTONE, SANDY, BROWN,

FINE TO COARSE GRAINED.

BROWN, WET

WET

BROWN, HARD, MOIST

10

15



	TES	ST BORING LOG	i
DRAWN:	DATE:	CHECKED:	7/12/19

SANDSTONE, SILTY, FINE TO

COARSE GRAINED, GRAY

TO WET

CLAYEY LENSES

BROWN, VERY DENSE, MOIST

10

15

50 12.9

<u>50</u> | 12.9

15.2

9"

8"

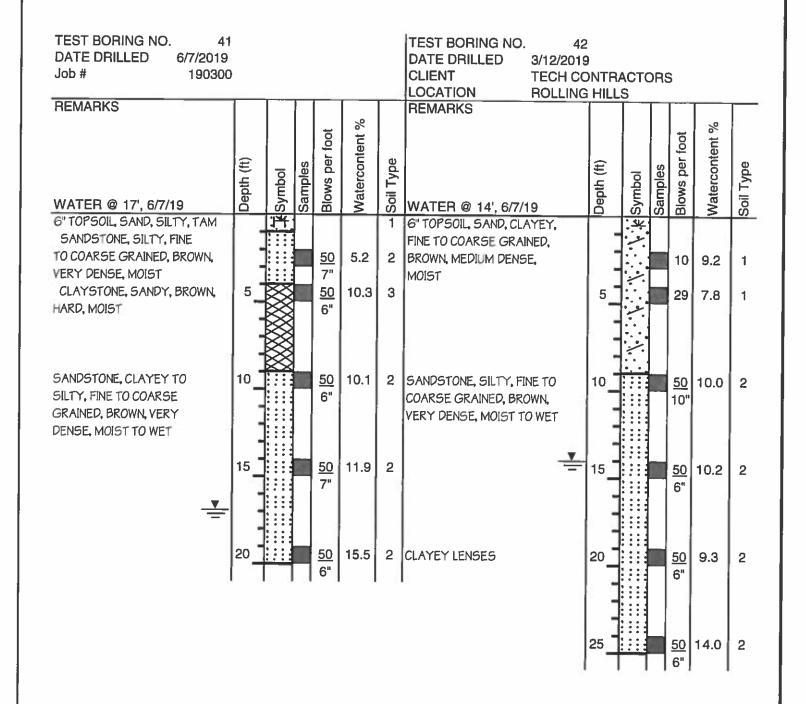
<u>50</u>

2

2

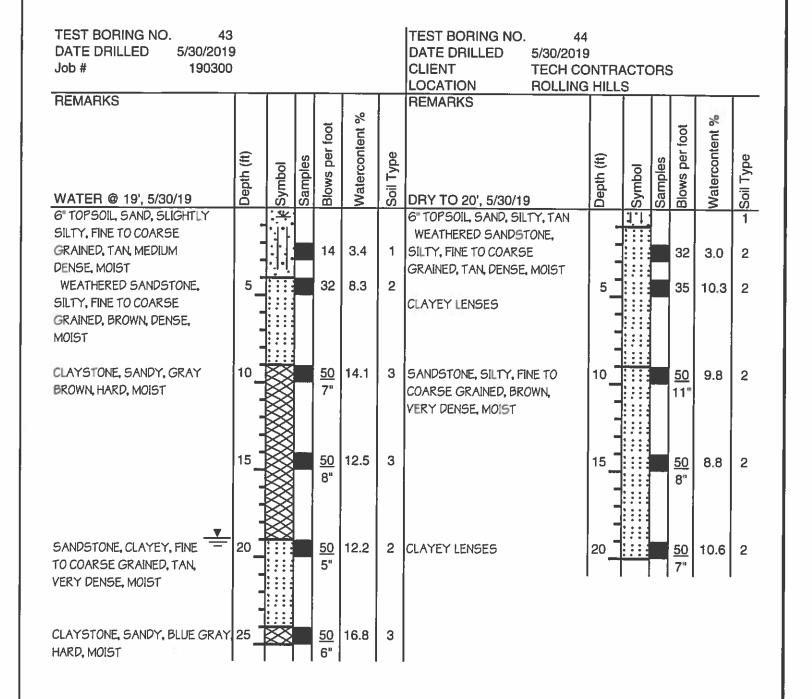
2

JOB NO.: 190300 FIG NO.:





	TEST	BORING LOC	3
DRAWN:	DATE	CHECKED: Km	7/12/19



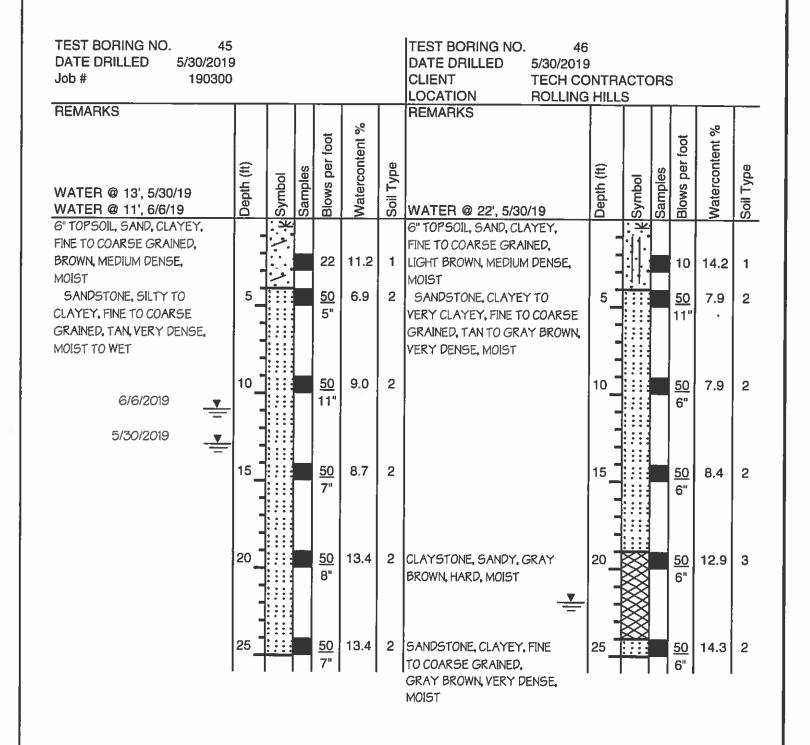


	1231	BONING LOG
DRAWN:	DATE:	CHECKED: A 7/1/19

TEST PODING LOC

JOB NO.: 190300

FIG NO.: A- 22





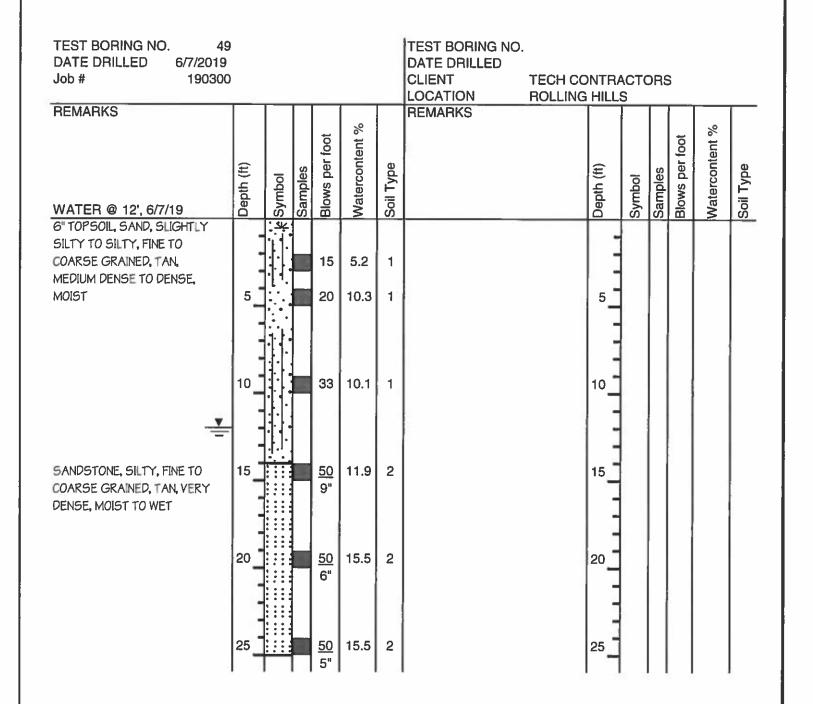
	TEST		
DRAWN:	DATE:	CHECKED: 6 1 PATE/19	CKED: 6 7 PATE/19
		-	-

TEST BORING NO. 47 TEST BORING NO. 48 DATE DRILLED 5/30/2019 6/7/2019 DATE DRILLED Job# 190300 CLIENT TECH CONTRACTORS LOCATION **ROLLING HILLS** REMARKS REMARKS Watercontent % % Blows per foot Blows per foot Watercontent Soil Type Soil Type Samples Samples Symbol Symbol DRY TO 20', 6/7/19 DRY TO 20', 5/30/19 CAVED TO 14', 7/9/19, DRY 6" TOPSOIL, SAND, SILTY, TAN 14 6" TOPSOIL, SAND, SILTY, TAN 1.1 SANDSTONE, SILTY, FINE TO SANDSTONE, CLAYEY TO COARSE GRAINED, BROWN, 9.0 <u>50</u> SILTY, FINE TO COARSE 32 8.9 2 9" VERY DENSE, MOIST GRAINED, BROWN, VERY DENSE. 5 :: <u>50</u> 8.7 2 MOIST 27 7.8 2 10" 10 9.4 <u>50</u> 2 CLAYSTONE, SANDY, BROWN, 10 50 9.6 3 10" HARD, MOIST 9" 15 50 8.8 2 SANDSTONE, SILTY, FINE TO 15 50 5.4 2 10" COARSE GRAINED, TAN, 8" VERY DENSE, MOIST CLAYSTONE, VERY SANDY. 20 <u>50</u> 8.5 2 GRAY BROWN, HARD, MOIST <u>50</u> 9.4 3



TEST BORING LOG		i	
DRAWN:	DATE	CHECKED:	7/12/19

JOB NO.: 190300 FIG NO.:



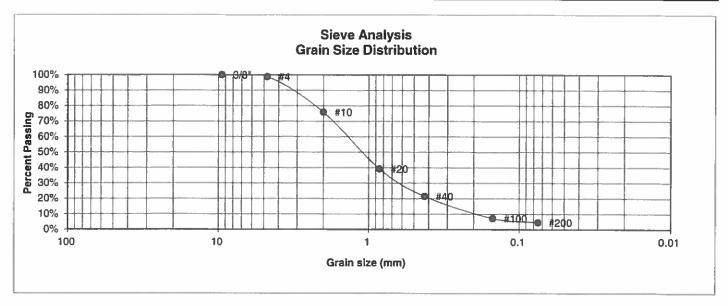


	TEST	BORING LOC	à
DRAWN	DATE	CHECKED	7:/12/19

JOB NO.: 190300

FIG NO.: A- 25 **APPENDIX B: Laboratory Test Results**

UNIFIED CLASSIFICATION	SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	1	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



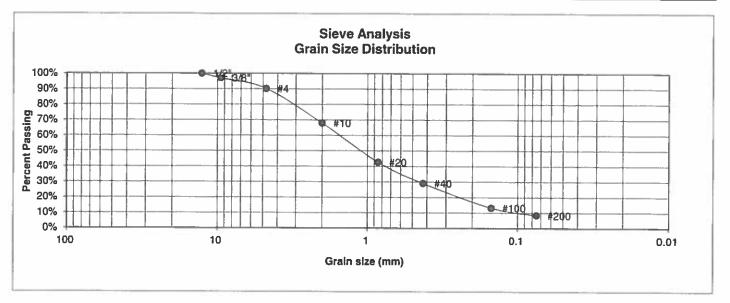
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	0
4	98.7%	Swell
10	75.9%	Moisture at start
20	39.2%	Moisture at finish
40	21.4%	Moisture increase
100	7.2%	Initial dry density (pcf)
200	4.7%	Swell (psf)



	LABORATORY TEST RESULTS		
ľ	DATE	CHECKED A	DATE // 9

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	2	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



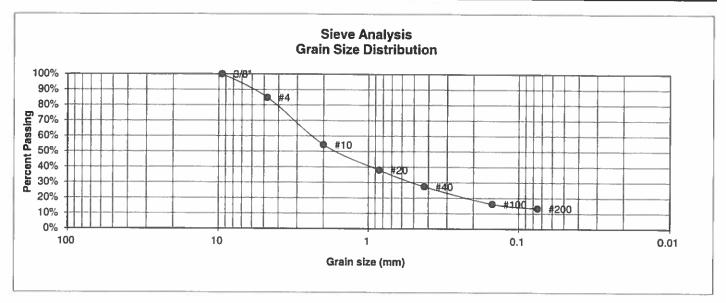
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 97.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	90.2%	<u>Swell</u>
10	67.9%	Moisture at start
20	42.7%	Moisture at finish
40	29.0%	Moisture increase
100	13.2%	Initial dry density (pcf)
200	8.4%	Swell (psf)



LABORATORY TEST RESULTS		
DATE	CHECKED:	DATE: 7/1/19

JOB NO: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	5	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



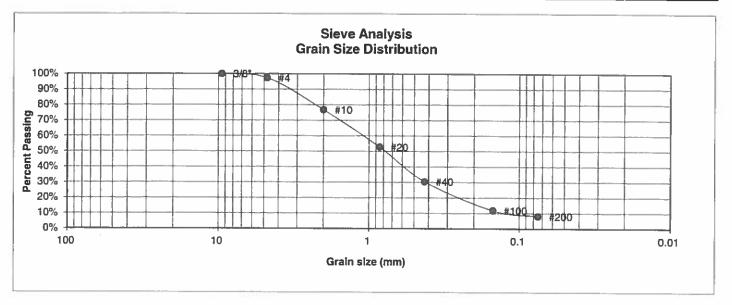
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 16 Liquid Limit 26 Plastic Index 10	
3/8"	100.0%		
4	84.9%	Swell	
10	54.4%	Moisture at start	
20	38.1%	Moisture at finish	
40	27.3%	Moisture increase	
100 200	16.2% 13.3%	Initial dry density (pcf) Swell (psf)	



LABORATORY TEST RESULTS		
 DATE	CHECKED:	DATE: 7/1/19

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	6	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



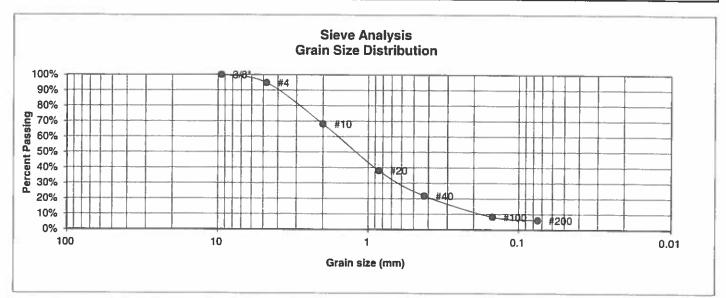
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.3% 76.8%	<u>Swell</u> Moisture at start
20	52.8%	Moisture at finish
40	30.4%	Moisture increase
100	11.8%	Initial dry density (pcf)
200	8.1%	Swell (psf)



LABORATORY TEST RESULTS			
DATE:	CHECKED:	h	DATE /19

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	8	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100 200	94.8% 68.1% 38.0% 21.8% 8.2% 6.1%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

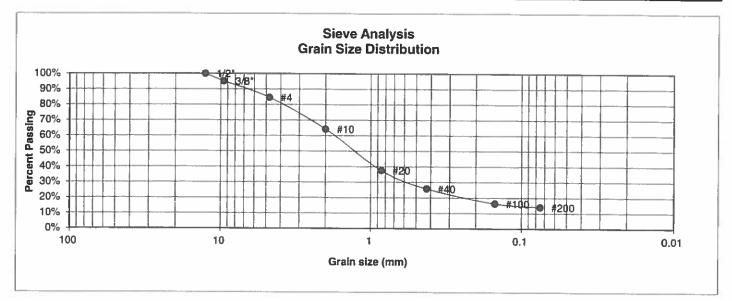


LABORAT	ORY TE	ST	
RESULTS			
DATE	CHECKED	$\overline{}$	

DRAWN: DATE: CHECKED: L DATE:

JOB NO 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	10	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



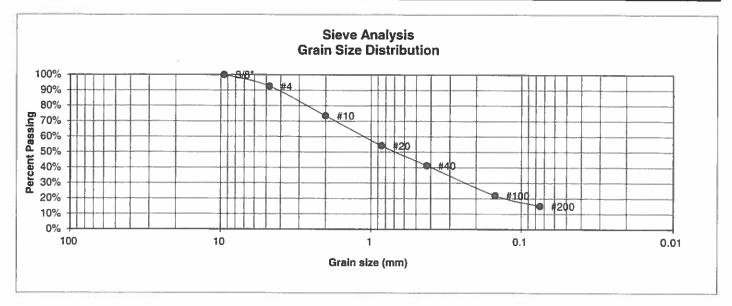
U.S. Sieve # 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 13 Liquid Limit 29 Plastic Index 16
1/2" 3/8"	100.0%	
3/0 4	95.1% 84.6%	Swell
10	64.3%	Moisture at start
20	37.5%	Moisture at finish
40	25.8%	Moisture increase
100 200	16.3% 14.0%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS		
DATE	CHECKED:	DATE: /14

JOB NO: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	11	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



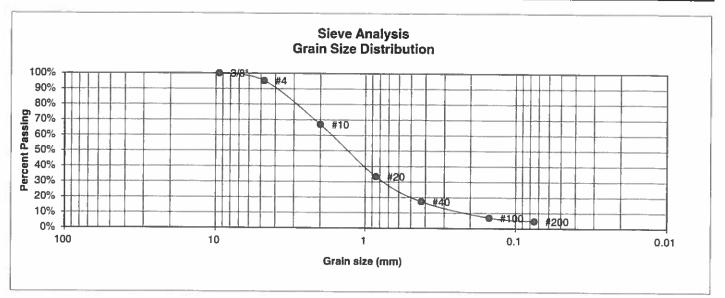
U.S. <u>Sieve #</u> 3" 1 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit	
3/4"		Plastic Index	
1/2"			
3/8"	100.0%		
4	92.6%	<u>Swell</u>	
10	73.5%	Moisture at start	12.1%
20	54.1%	Moisture at finish	19.1%
40	41.3%	Moisture increase	6.9%
100	22.0%	Initial dry density (pcf)	110
200	15.2%	Swell (psf)	370



LABORATO RESULTS	ORY TEST	
DATE:	CHECKED:	DATE /

JOB NO.: 190300

UNIFIED CLASSIFICATION	SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	13	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



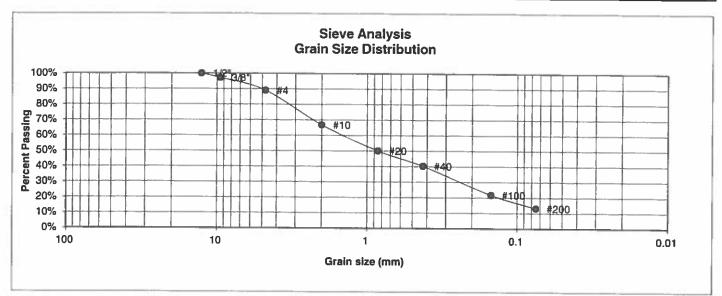
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	95.2%	<u>Swell</u>
10	67.0%	Moisture at start
20	33.4%	Moisture at finish
40	17.3%	Moisture increase
100	7.0%	Initial dry density (pcf)
200	4.8%	Swell (psf)



LABORATO	ORY TEST	
RESULTS		
DATE	CHICALOR .	DATE

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	14	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



4 89.0% Swell 10 66.8% Moisture at start 20 50.1% Moisture at finish 40 40.2% Moisture increase 100 21.8% Initial dry density (pcf)	U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 97.2%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
20 50.1% Moisture at finish 40 40.2% Moisture increase 100 21.8% Initial dry density (pcf)			
40 40.2% Moisture increase 100 21.8% Initial dry density (pcf)			
100 21.8% Initial dry density (pcf)			
initial dry density (pc)	40	40.2%	Moisture increase
	100 200	21.8% 13.2%	Initial dry density (pcf) Swell (psf)

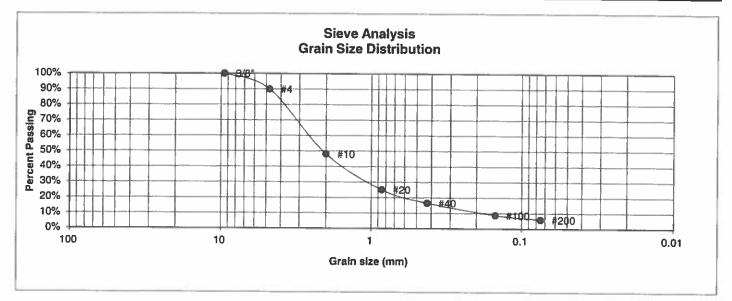


LABORATORY TEST	
RESULTS	

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JOB NO 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	16	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



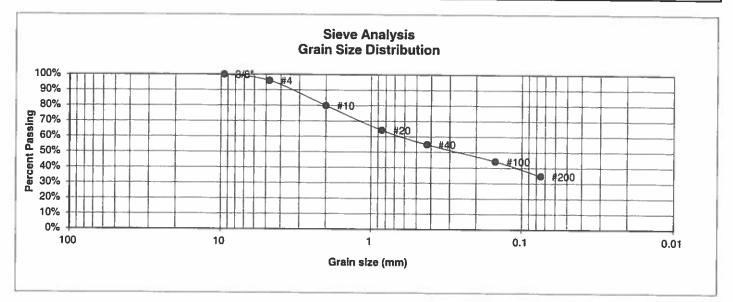
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index	
3/8"	100.0%		
4	89.9%	Swell	
10	48.1%	Moisture at start	13.5%
20	25.1%	Moisture at finish	21.9%
40	16.5%	Moisture increase	8.4%
100	8.7%	Initial dry density (pcf)	100
200	5.9%	Swell (psf)	70



	LABORATORY TEST RESULTS	
DATE:	CHECKED:	DATE/ 7/1/19

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	19	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



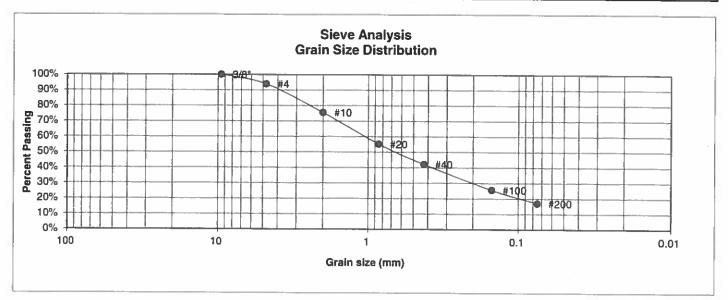
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	96.1%	Swell
10	80.0%	Moisture at start
20	64.1%	Moisture at finish
40	55.0%	Moisture increase
100	44.2%	Initial dry density (pcf)
200	34.7%	Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE:	CHECKED	DATE

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	23	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL

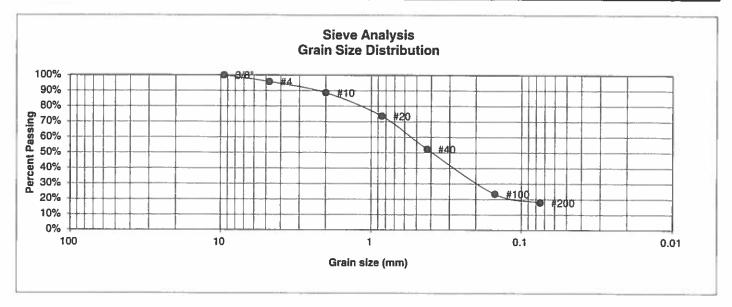


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index	NP NV NP
4	94.0%	Swell	
10	75.5%	Moisture at star	t
20 40	55.2% 42.1%	Moisture at finis Moisture increa	
100 200	25.6% 17.0%	Initial dry densit Swell (psf)	y (pcf)



LABORATORY TEST RESULTS			
DATE	CHECKED	h	DATE/ //9

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	24	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



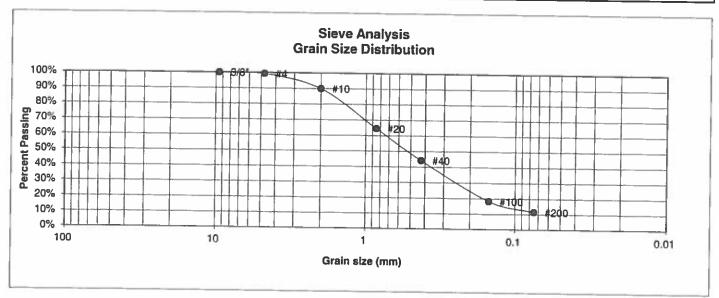
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	95.8%	<u>S</u> well
10	88.7%	Moisture at start
20	73.6%	Moisture at finish
40	52.3%	Moisture increase
100 200	23.5% 18.0%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS			
DATE	CHECKED:	h	DATE 7/1/19

JOB NO. 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1		TECH CONTRACTORS
TEST BORING #	26	PROJECT	ROLLING HILLS
DEPTH (FT)	20 5	JOB NO.	190300
DEL III (F1)		<u>TEST BY</u>	BL



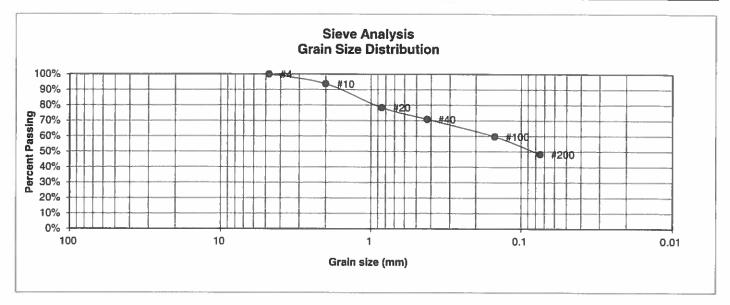
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	99.3% 90.0%	<u>Swell</u> Moisture at start
20 40	64.6% 44.2%	Moisture at start Moisture at finish Moisture increase
100 200	18.3% 11.5%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY TE	EST	
DATE	CHECKED:	ん	DATE: 1/19

JOB NO. 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	27	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



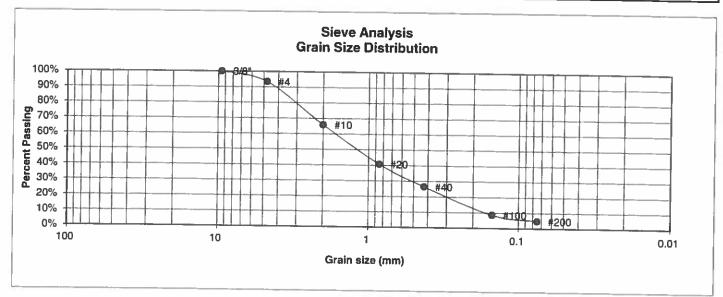
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	93.7%	Moisture at start 14.0%
20	78.5%	Moisture at finish 20.9%
40	70.9%	Moisture increase 6.9%
100	59.7%	Initial dry density (pcf) 103
200	48.3%	Swell (psf) 460



LABORATORY TEST RESULTS			
DATE	CHECKED:	7/1/19	

JOB NO.: 190300

UNIFIED CLASSIFICATION	SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	28	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



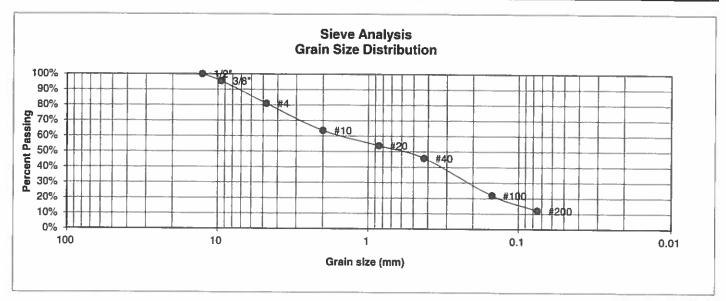
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	93.4%	<u>Swell</u>
10	65.9%	Moisture at start
20	40.8%	Moisture at finish
40	26.4%	Moisture increase
100	8.7%	Initial dry density (pcf)
200	4.9%	Swell (psf)



	LABORATORY TEST RESULTS				
DRAWN:	DATE	CHECKED: DATE:			

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS	
SOIL TYPE #	1	PROJECT	ROLLING HILLS	
TEST BORING #	30	JOB NO.	190300	97
DEPTH (FT)	2-3	TEST BY	BL	



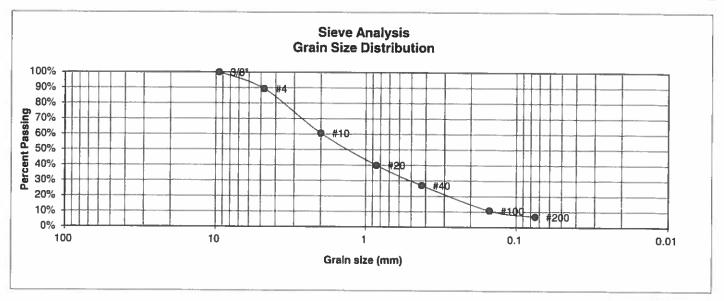
U.S.	Percent	Atterberg	
Sieve #	<u>Finer</u>	<u>Limits</u>	
3"		Plastic Limit	
1 1/2"		Liquid Limit	
3/4"		Plastic Index	
1/2"	100.0%		
3/8"	95.5%		
4	81.0%	<u>Swell</u>	
10	63.6%	Moisture at start 13.1%	6
20	53.9%	Moisture at finish 19.6%	%
40	45.8%	Moisture increase 6.5%	%
100	21.9%	Initial dry density (pcf) 9°	7
200	12.1%	Swell (psf) 2970	0



LABORATO RESULTS	ORY TI	EST		
DATE:	CHECKED:	h	DATE	119

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	30	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



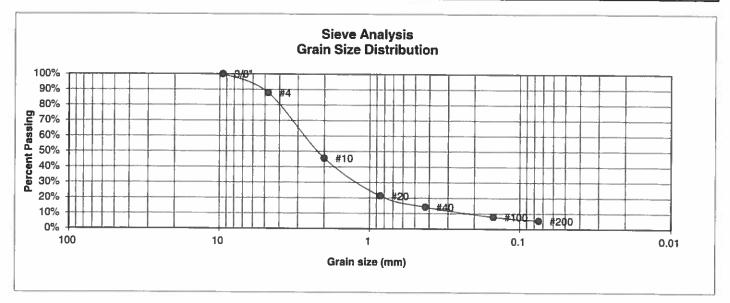
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8" 4	100.0% 89.3%	Swell
10	60.6%	Moisture at start
20 40	40.0% 26.9%	Moisture at finish Moisture increase
100 200	10.8% 6.9%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS				
DATE	CHECKED:	DATE //9		

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	31	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



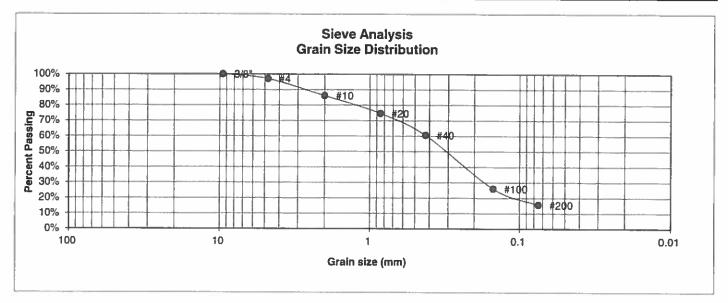
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	87.9%	Swell
10	45.6%	Moisture at start
20	21.3%	Moisture at finish
40	14.2%	Moisture increase
100 200	7.8% 5.4%	Initial dry density (pcf) Swell (psf)



	LABORATE RESULTS	ORY TE	EST	
Ī	DATE	CHECKED:	h	DATE //9

ЈОВ NO 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	32	JOB NO.	190300
DEPTH (FT)	0	TEST BY	BL



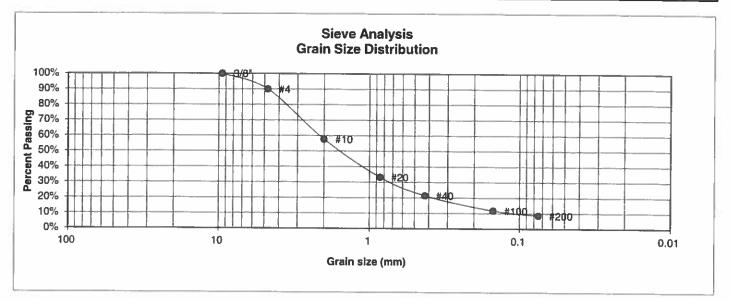
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2"	100.00	
3/8"	100.0%	
4	97.1%	<u>Swell</u>
10	86.1%	Moisture at start
20	74.7%	Moisture at finish
40	60.6%	Moisture increase
100	26.1%	Initial dry density (pcf)
200	15.6%	Swell (psf)



RESULTS	ORY TEST	
DATE	CHECKED	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	38	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



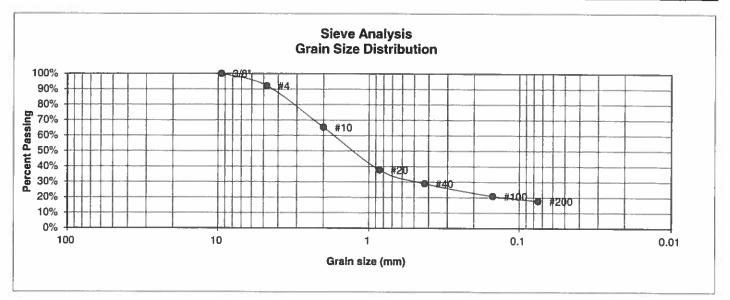
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP	
3/8"	100.0%		
4	90.0%	Swell	
10	57.7%	Moisture at start	
20	33.2%	Moisture at finish	
40	21.4%	Moisture increase	
100 200	11.7% 8.6%	Initial dry density (pcf) Swell (psf)	



LABORATORY TEST RESULTS				
DRAWN:	DATE:	CHECKED:	h	DATE: 7/1/19

JOB NO: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	Ī	PROJECT	ROLLING HILLS
TEST BORING #	39	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



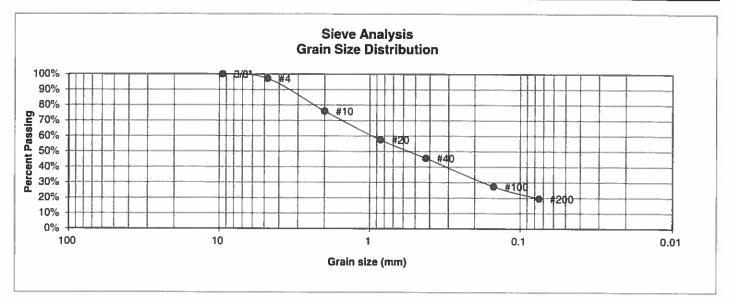
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	92.2%	<u>Swell</u>
10	65.3%	Moisture at start
20	37.7%	Moisture at finish
40	29.0%	Moisture increase
100 200	20.8% 17.8%	Initial dry density (pcf) Swell (psf)



LABOF	RATORY TEST
RESUI	_TS
DATE	CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	42	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



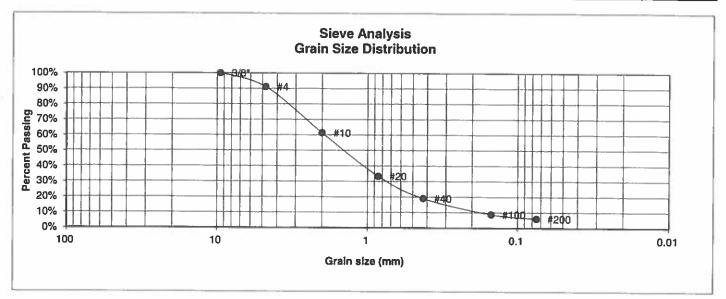
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	97.2%	<u>Swell</u>
10	76.1%	Moisture at start
20	57.5%	Moisture at finish
40	45.6%	Moisture increase
100	27.4%	Initial dry density (pcf)
200	19.6%	Swell (psf)



LABORATORY TEST RESULTS			
DATE:	CHECKED:	h	DATE 7/1/19

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	43	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



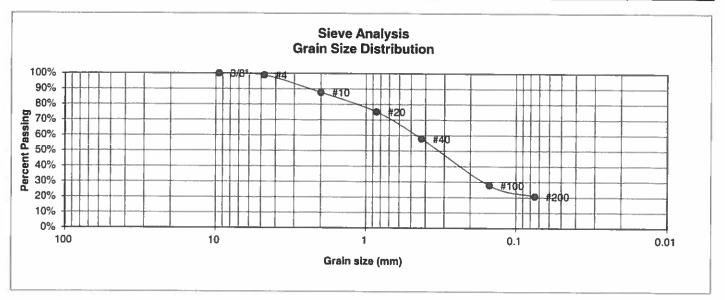
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	91.1%	<u>Swell</u>
10	61.3%	Moisture at start
20	33.3%	Moisture at finish
40	19.0%	Moisture increase
100	8.7%	Initial dry density (pcf)
200	6.0%	Swell (psf)



LABOR RESUL	ATORY TEST TS	•
DATE:	CHE CKED:	DATE: 7/1/19

JOB NO. 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	47	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



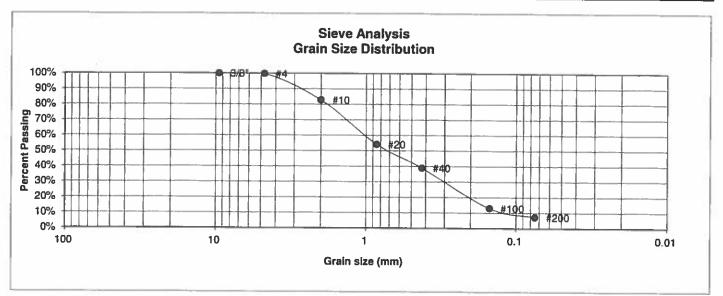
U.S.	Percent	Atterberg
Sieve #	<u>Finer</u>	<u>Limits</u>
3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"		
3/8"	100.0%	
4	98.8%	<u>Swell</u>
10	87.7%	Moisture at start 13.9%
20	75.2%	Moisture at finish 18.6%
40	57.8%	Moisture increase 4.8%
100	27.8%	Initial dry density (pcf) 103
200	20.7%	Swell (psf) 220



LABORATO RESULTS	ORY TEST	
DATE	CHECKED:	7 DATE://4

JOB NO. 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	49	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



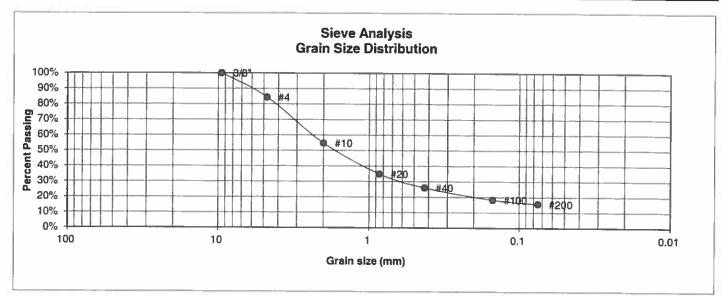
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.8%	<u>Swell</u>
10	82.8%	Moisture at start
20	54.2%	Moisture at finish
40	38.9%	Moisture increase
100	13.0%	Initial dry density (pcf)
200	7.3%	Swell (psf)



LABORATORY TEST RESULTS		
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JOB NO. 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	1	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



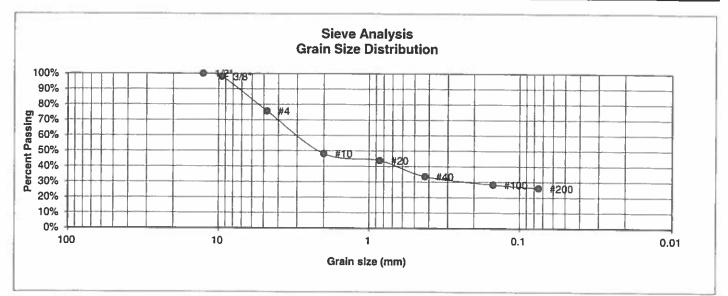
U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	84.4%	<u>Swell</u>
10	54.8%	Moisture at start
20 40	34.9% 26.0%	Moisture at statt Moisture at finish Moisture increase
100	18.2%	Initial dry density (pcf)
200	15.5%	Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE	CHECKED:	DATE:

JOB NO. 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	3	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 98.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	75.7%	<u>Swell</u>
10	48.2%	Moisture at start
20	43.8%	Moisture at finish
40	33.5%	Moisture increase
100	28.3%	Initial dry density (pcf)
200	26.1%	Swell (psf)

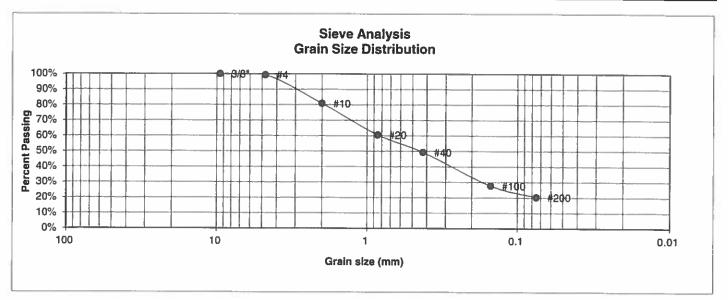


LABORATORY TEST	
RESULTS	

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JOB NO: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	4	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



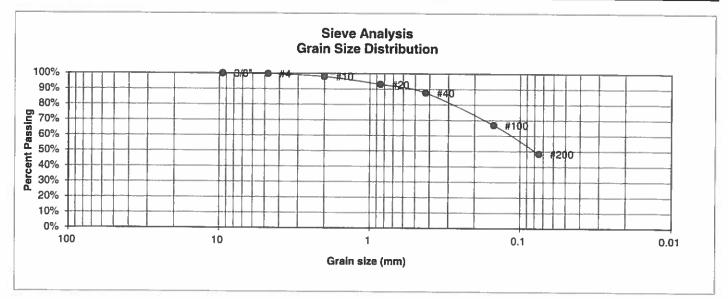
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 29 Plastic Index 12
4	99.4%	<u>Swell</u>
10	80.9%	Moisture at start
20	60.6%	Moisture at finish
40	49.3%	Moisture increase
100 200	27.7% 20.3%	Initial dry density (pcf) Swell (psf)



RESULTS	ORY TEST	
DATE	CHECKED:	DATE

JOB NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	5	JOB NO.	190300
DEPTH (FT)	25	TEST BY	BL



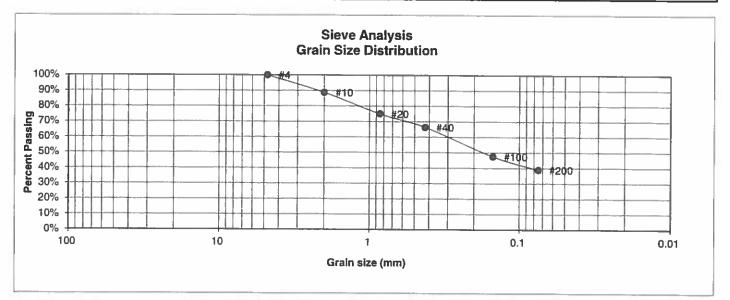
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 31 Plastic Index 14
3/8"	100.0%	
4	99.7%	Swell
10	98.0%	Moisture at start
20	93.0%	Moisture at finish
40	87.6%	Moisture increase
100	67.0%	Initial dry density (pcf)
200	48.5%	Swell (psf)



LABORATORY TEST RESULTS			
DRAWN:	DATE	CHECKED	DATE //9

JOB NO. 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	6	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



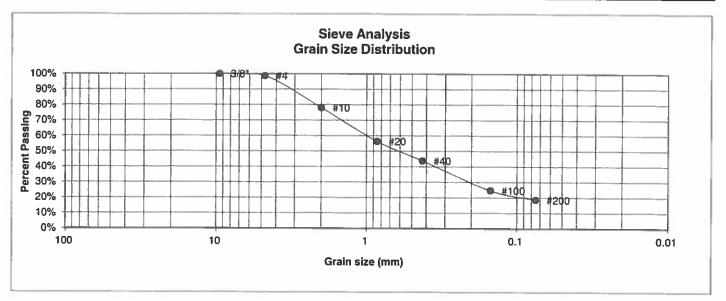
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 13 Liquid Limit 26 Plastic Index 13
4	100.0%	Swell
10	88.7%	Moisture at start
20	75.0%	Moisture at finish
40	66.3%	Moisture increase
100 200	47.5% 38.9%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY T	EST	
DATE	CHECKED:	1/1_	DATE //a

JOB NO: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	7	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



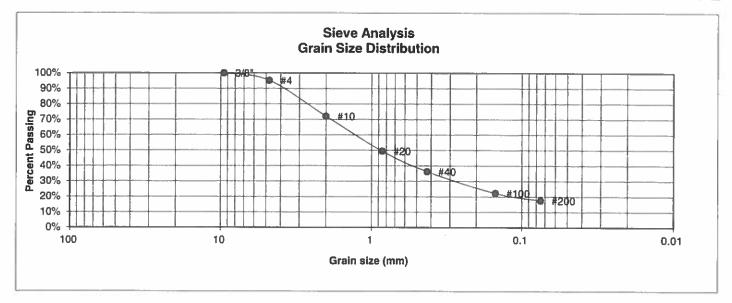
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 18 Liquid Limit 32 Plastic Index 14
3/8"	100.0%	
4	98.7%	<u>Sweli</u>
10	78.1%	Moisture at start
20	56.3%	Moisture at finish
40	43.8%	Moisture increase
100	24.6%	Initial dry density (pcf)
200	18.6%	Swell (psf)



LABORATO RESULTS		EST	
DATE	CHECKED:	ん	DATE: //9

JOB NO. 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	9	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



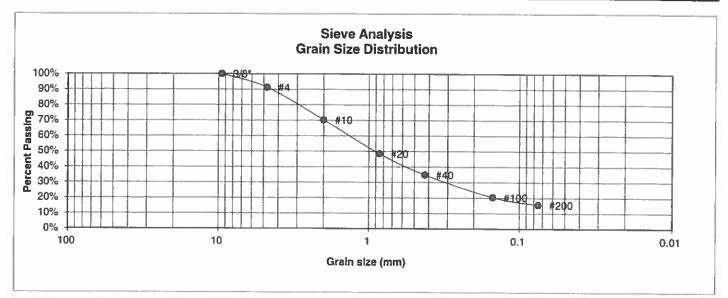
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	95.3%	<u>Swell</u>
10	72.0%	Moisture at start
20	49.5%	Moisture at finish
40	36.2%	Moisture increase
100	22.3%	Initial dry density (pcf)
200	17.5%	Swell (psf)



LABORATO RESULTS	ORY TEST	
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JOB NO: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	12	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



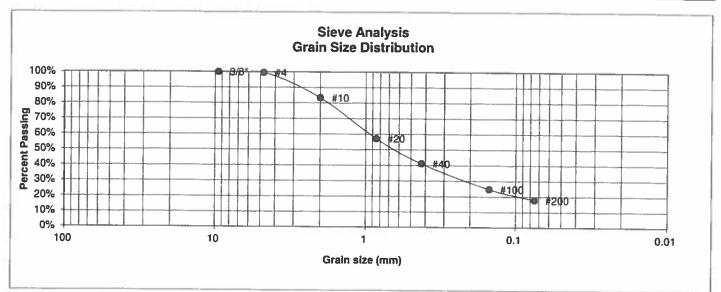
4 91.3% <u>Swell</u> 10 70.3% Moisture at start 20 48.5% Moisture at finish 40 34.9% Moisture increase	U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
40 34.9% Moisture increase	4	91.3%	
200 15.5% Swell (psf)	40 100	34.9% 20.4%	Moisture increase Initial dry density (pcf)



LABORATORY TEST RESULTS				
DRAWN	DATE	CHECKED:	DATE	

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	14	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



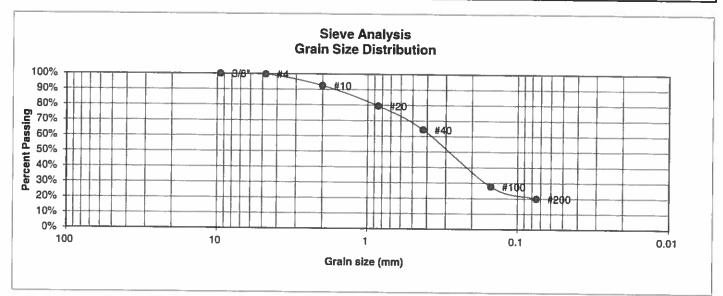
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.5% 83.3%	<u>Swell</u> Moisture at start
20 40	57.2% 41.1%	Moisture at finish Moisture increase
100 200	24.8% 17.8%	Initial dry density (pcf) Swell (psf)



RESULTS				
DATE	CHECKED:	2	DATE:/10	

JOB NO. 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	15	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



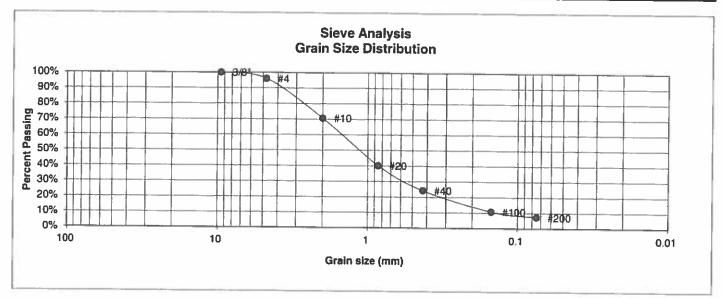
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100	99.7% 92.5% 79.5% 64.2% 27.7%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf)
200	19.9%	Swell (psf)



LABORATORY TEST RESULTS			
DATE:	CHECKED:	DATE: 1/9	

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	17	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



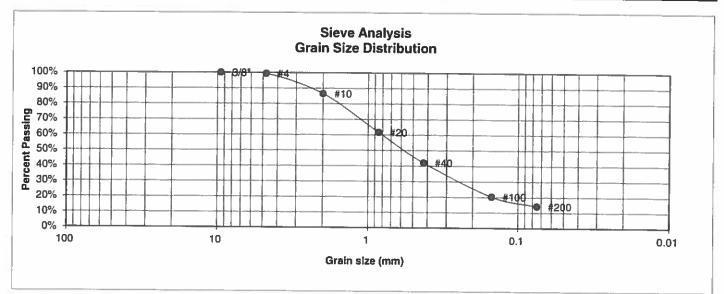
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	96.1% 70.6%	<u>Swell</u> Moisture at start
20	40.1%	Moisture at finish
40	24.3%	Moisture increase
100	10.8%	Initial dry density (pcf)
200	7.3%	Swell (psf)



LABORATORY TEST RESULTS			
DATE	CHECKED:	DATE:	

JOB NO: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	18	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



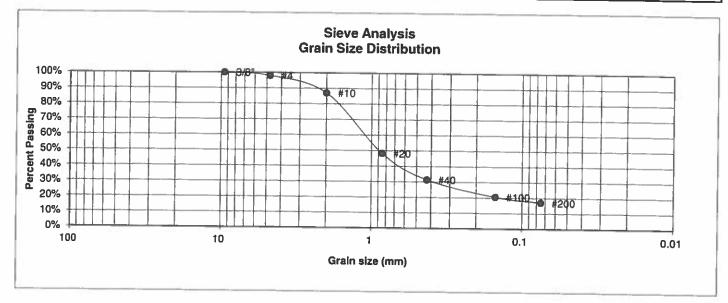
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.4% 86.5%	<u>Swell</u> Moisture at start
20 40 100	61.7% 42.1% 20.3%	Moisture at finish Moisture increase Initial dry density (pcf)
200	14.2%	Swell (psf)



LABOR, RESUL	ATORY TEST	
DATE	CHECKED:	DATE /19

JOB NO: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	20	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100 200	98.1% 87.0% 48.2% 31.3% 20.5% 17.1%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

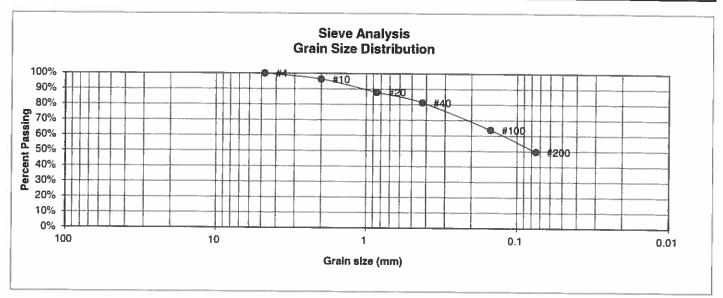


LABORATORY TEST RESULTS				
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> JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	20	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



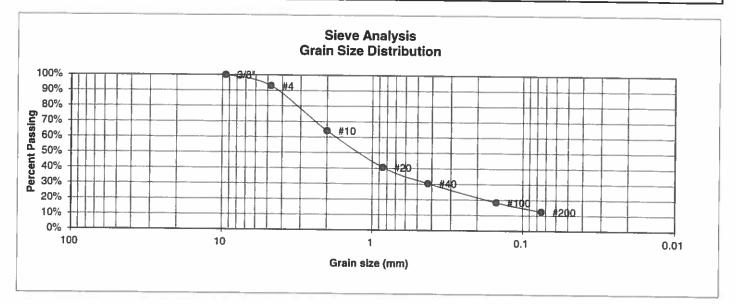
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 14 Liquid Limit 28 Plastic Index 14
4	100.0%	Swell
10	96.3%	Moisture at start
20	88.0%	Moisture at finish
40	81.3%	Moisture increase
100	63.8%	Initial dry density (pcf)
200	49.7%	Swell (psf)



LABORATORY TEST RESULTS			
DATE	CHECKED:	DATE: 7/1/9	

JOB NO 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	21	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	93.0%	Swell
10	64.1%	Moisture at start
20 40	40.6% 30.4%	Moisture at finish Moisture increase
100 200	18.4% 12.5%	Initial dry density (pcf) Swell (psf)

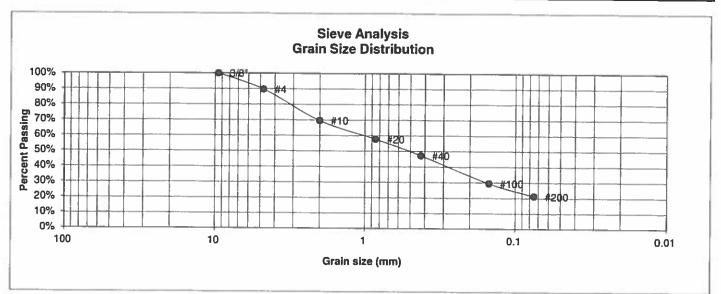


LABORATORY TEST	
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	21	JOB NO.	190300
DEPTH (FT)	25	TEST BY	BL



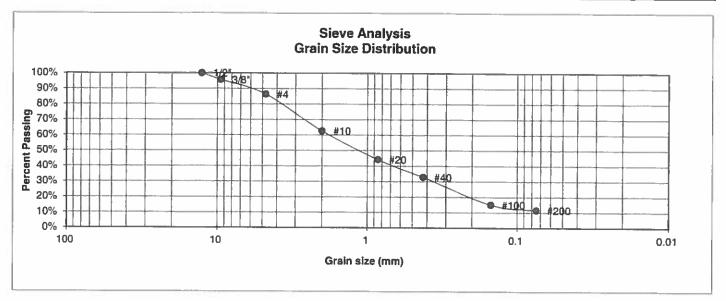
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20	89.6% 69.6%	Swell Moisture at start
40 100 200	57.7% 47.2% 29.5% 21.2%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORATOR RESULTS	ORY TE	ST	
DATE	CHECKED:	ん	DATE 7/14

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	23	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



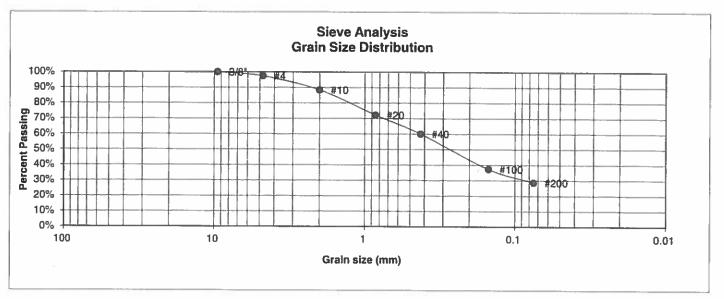
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 95.7%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	86.4%	<u>Swell</u>
10	62.6%	Moisture at start
20	44.2%	Moisture at finish
40	32.8%	Moisture increase
100	15.0%	Initial dry density (pcf)
200	11.6%	Swell (psf)



RESULTS			
DATE	CHECKED:	DATE /19	

JOB NO: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	25	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



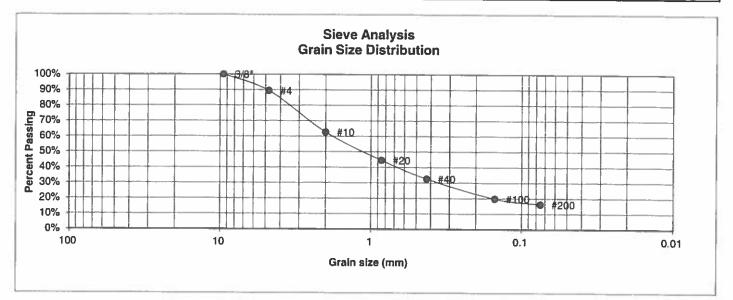
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.4%	Swell
10	88.4%	Moisture at start
20 40	72.2% 60.1%	Moisture at finish Moisture increase
100 200	37.4% 28.7%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE	CHECKED	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	27	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



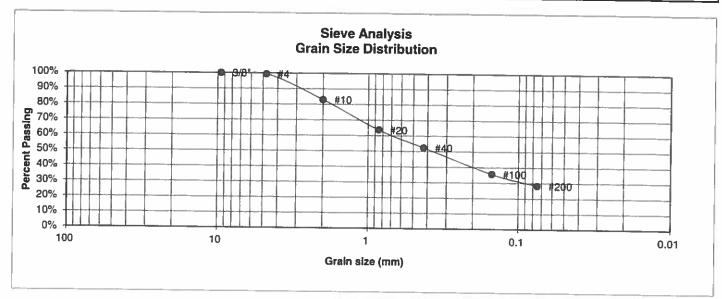
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	89.4%	Swell
10	62.7%	Moisture at start
20	44.5%	Moisture at finish
40	32.5%	Moisture increase
100 200	19.8% 16.2%	Initial dry density (pcf) Swell (psf)



RESULTS	ORY T	EST	
DATE	CHECKED:	h.	791759

JOB NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	28	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	99.4%	Swell
10	83.0%	Moisture at start
20	63.6%	Moisture at finish
40	52.4%	Moisture increase
100 200	35.7% 28.3%	Initial dry density (pcf) Swell (psf)

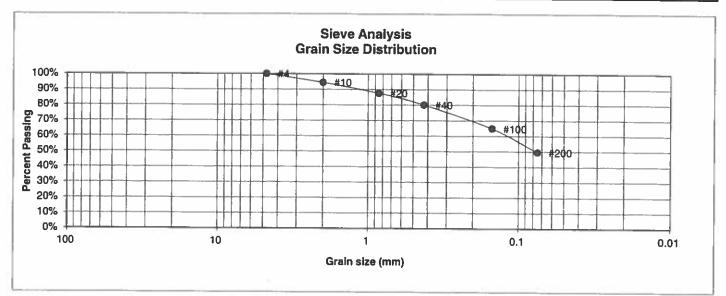


LABORATOR RESULTS	ORY TEST	
DATE	CHECKED A	DATE

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> JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	29	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



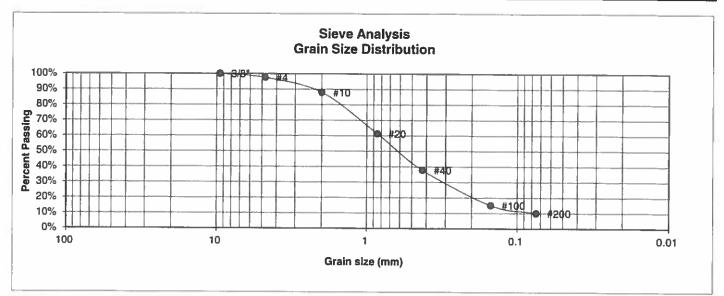
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	Swell
10	94.5%	Moisture at start
20	87.6%	Moisture at finish
40	80.1%	Moisture increase
100	64.9%	Initial dry density (pcf)
200	49.6%	Swell (psf)



LABORATORY TEST RESULTS				
DATE	CHECKED:	DATE:		

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	35	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



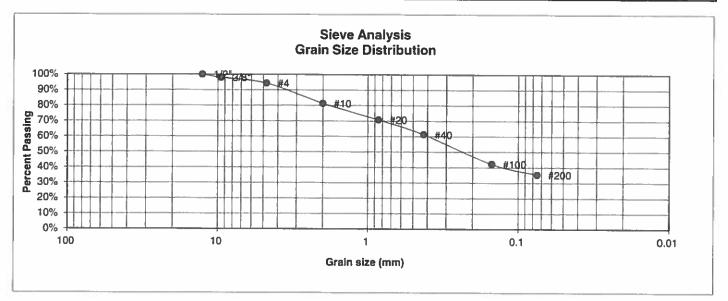
U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	97.5% 87.9%	<u>Swell</u> Moisture at start
20 40 100	61.3% 37.8% 15.2%	Moisture at finish Moisture increase Initial dry density (pcf)
200	10.1%	Swell (psf)



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JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	37	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



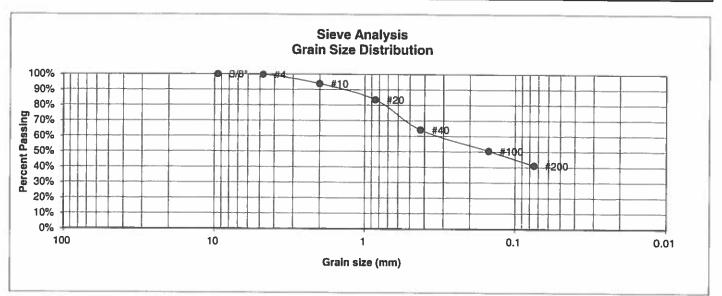
U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 98.1%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	94.3%	<u>Swell</u>
10	81.4%	Moisture at start
20	70.8%	Moisture at finish
40	61.3%	Moisture increase
100	42.3%	Initial dry density (pcf)
200	35.4%	Swell (psf)



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UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	39	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



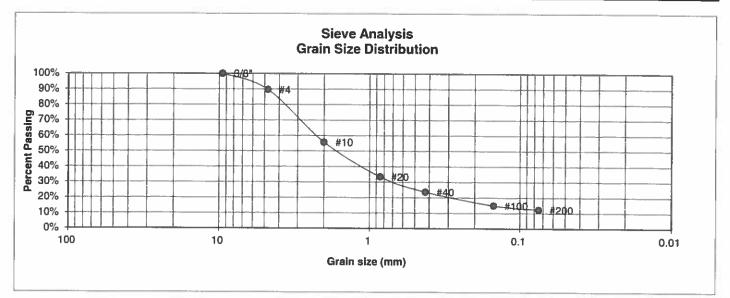
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.7%	<u>Swell</u>
10	93.8%	Moisture at start
20	83.5%	Moisture at finish
40	64.1%	Moisture increase
100	50.5%	Initial dry density (pcf)
200	41.1%	Swell (psf)



LABORATORY TEST RESULTS			
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JOB NO. 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	40	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	89.7%	<u>Swell</u>
10	55.7%	Moisture at start
20	33.4%	Moisture at finish
40	23.7%	Moisture increase
100	14.9%	Initial dry density (pcf)
200	12.3%	Swell (psf)

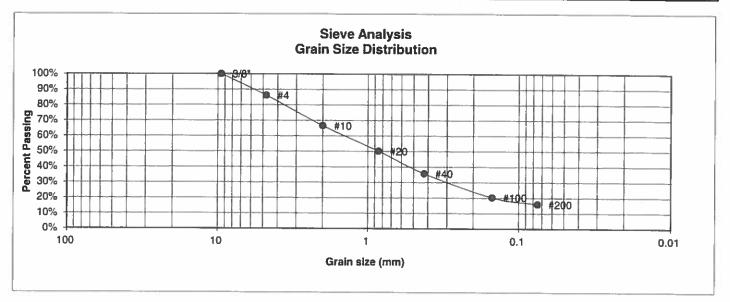


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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	41	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



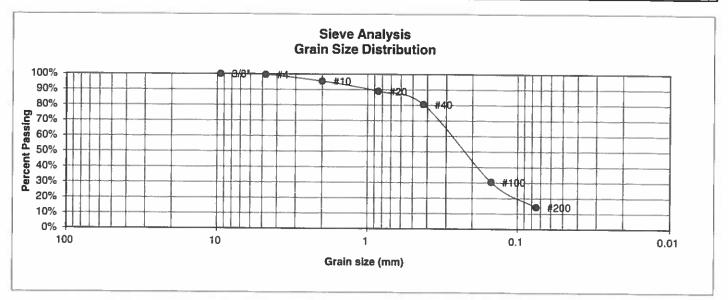
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	86.2%	<u>Swell</u>
10	66.5%	Moisture at start
20	50.2%	Moisture at finish
40	35.7%	Moisture increase
100	20.3%	Initial dry density (pcf)
200	16.0%	Swell (psf)



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UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	44	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



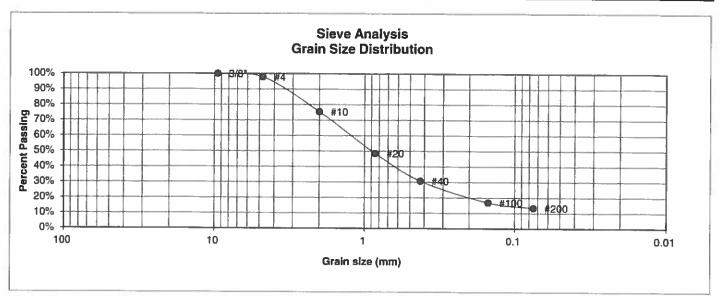
U.S. Sieve # 3" 1 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit
3/4" 1/2" 3/8" 4	100.0%	Plastic Index
10	99.6% 95.4%	<u>Swell</u> Moisture at start
20 40	89.0% 80.6%	Moisture at finish Moisture increase
100 200	30.5% 14.3%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS				
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	45	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



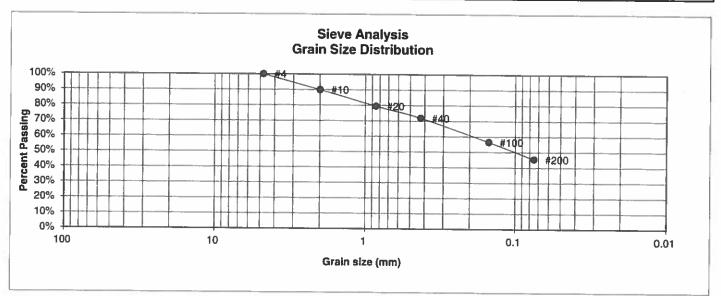
U.S.	Percent	Atterberg
Sieve #	<u>Finer</u>	<u>Limits</u>
3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"		
3/8"	100.0%	
4	97.9%	<u>Swell</u>
10	75.4%	Moisture at start
20	48.6%	Moisture at finish
40	30.7%	Moisture increase
100	16.9%	Initial dry density (pcf)
200	13.4%	Swell (psf)



	LABORATORY TEST RESULTS			
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	46	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



4 100.0% Swell 10 89.9% Moisture at start 20 79.5% Moisture at finish 40 71.8% Moisture increase 100 56.5% Initial dry density (pcf)	U.S. <u>Sieve #</u> 3" 1 1/2" 3/4* 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
20 79.5% Moisture at finish 40 71.8% Moisture increase 100 56.5% Initial dry density (pcf)	=	100.0%	<u>Swell</u>
40 71.8% Moisture increase 100 56.5% Initial dry density (pcf)	10	89.9%	Moisture at start
100 56.5% Initial dry density (pcf)	20	79.5%	Moisture at finish
initial dry density (pci)	40	71.8%	Moisture increase
200 45.5% Swell (nsf)	100 200		Initial dry density (pcf)

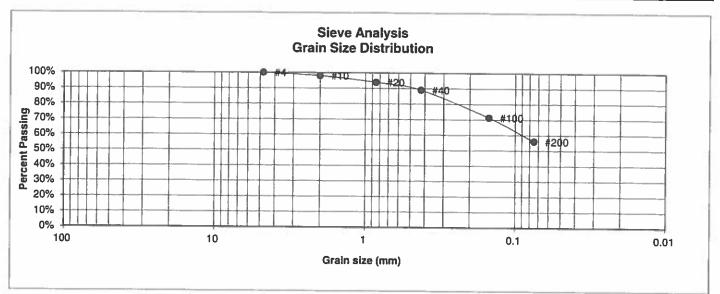


LABORATORY TEST RESULTS			
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JOB NO.: 190300

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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	15	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



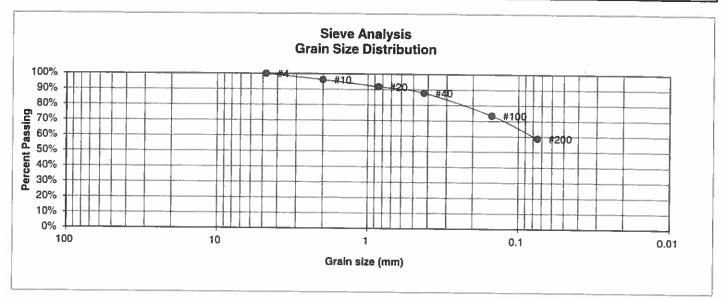
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10	100.0% 98.1%	Swell
		Moisture at start
20	93.9%	Moisture at finish
40	89.0%	Moisture increase
100	71.3%	Initial dry density (pcf)
200	56.1%	Swell (psf)



LABORATORY TEST RESULTS		
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JOB NO.: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	16	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



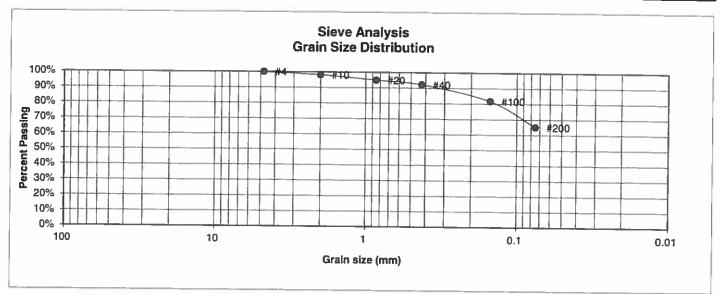
U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	96.2%	Moisture at start
20	91.8%	Moisture at finish
40	87.9%	Moisture increase
100 200	73.5% 58.8%	Initial dry density (pcf) Swell (psf)



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JOB NO.: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	19	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>S</u> well
10	98.2%	Moisture at start
20	95.0%	Moisture at finish
40	92.2%	Moisture increase
100	81.7%	Initial dry density (pcf)
200	65.1%	Swell (psf)

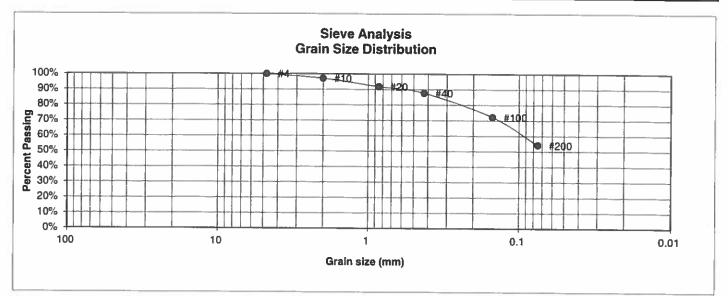


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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	22	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



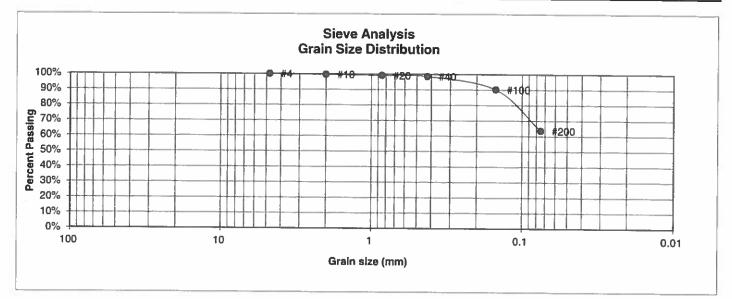
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 19 Liquid Limit 34 Plastic Index 15
4 10 20 40 100 200	100.0% 97.1% 91.9% 87.7% 72.3% 54.2%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	24	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



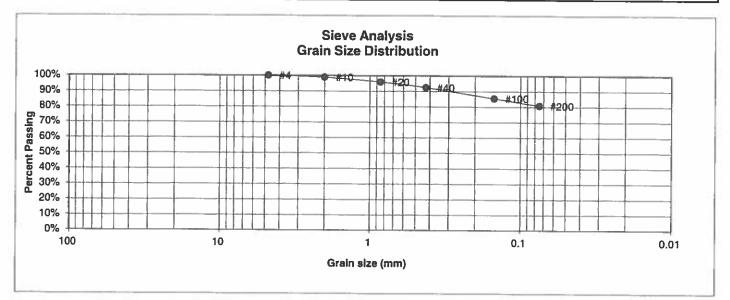
U.S.	Percent	Atterberg
Sieve #	<u>Finer</u>	<u>Limits</u>
3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"		
3/8"		
4	100.0%	<u>Swell</u>
10	99.7%	Moisture at start 14.5%
20	99.1%	Moisture at finish 24.3%
40	98.5%	Moisture increase 9.8%
100	90.2%	Initial dry density (pcf) 90
200	63.6%	Swell (psf) 90



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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	33	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



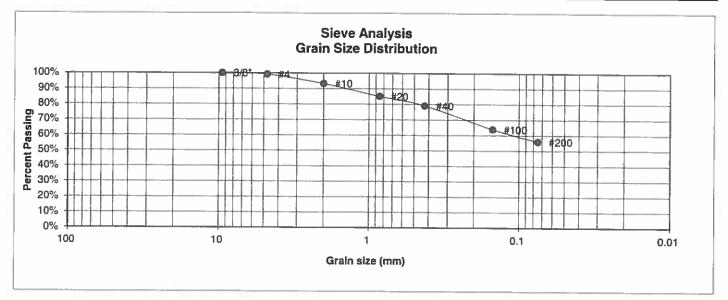
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 22 Liquid Limit 42 Plastic Index 20
4	100.0%	Swell
10	99.0%	Moisture at start
20	96.0%	Moisture at finish
40	92.5%	Moisture increase
100	85.5%	Initial dry density (pcf)
200	80.8%	Swell (psf)



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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	34	JOB NO.	190300
DEPTH (FT)	_10	TEST BY	BL



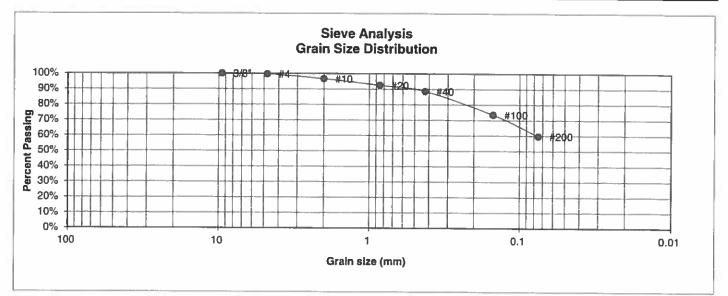
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.2%	<u>Swell</u>
10	93.2%	Moisture at start
20	85.1%	Moisture at finish
40	79.1%	Moisture increase
100	63.9%	Initial dry density (pcf)
200	56.0%	Swell (psf)



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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	36	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



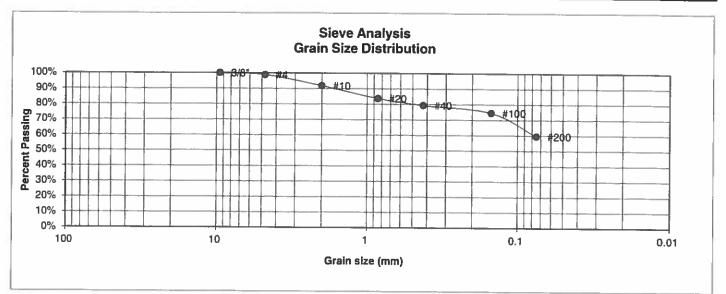
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.6%	<u>Swell</u>
10	96.7%	Moisture at start
20	92.5%	Moisture at finish
40	88.6%	Moisture increase
100	73.6%	Initial dry density (pcf)
200	59.7%	Swell (psf)



RESULTS	ORY TEST	
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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	38	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 17 Liquid Limit 34 Plastic Index 17
3/8"	100.0%	
4	98.9%	Swell
10	91.9%	Moisture at start
20	83.7%	Moisture at finish
40	79.3%	Moisture increase
100	74.6%	Initial dry density (pcf)
200	59.6%	Swell (psf)

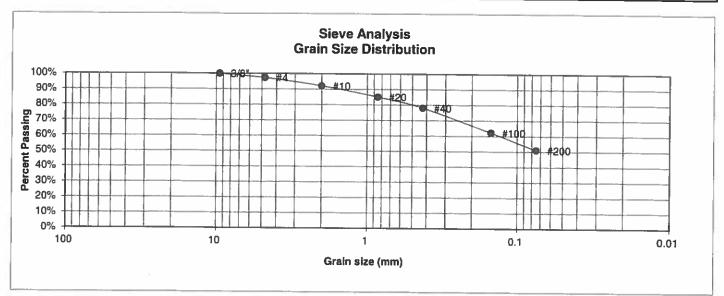


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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	48	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20	97.3% 92.1% 85.1%	Swell Moisture at start
40 100 200	78.1% 62.2% 51.1%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



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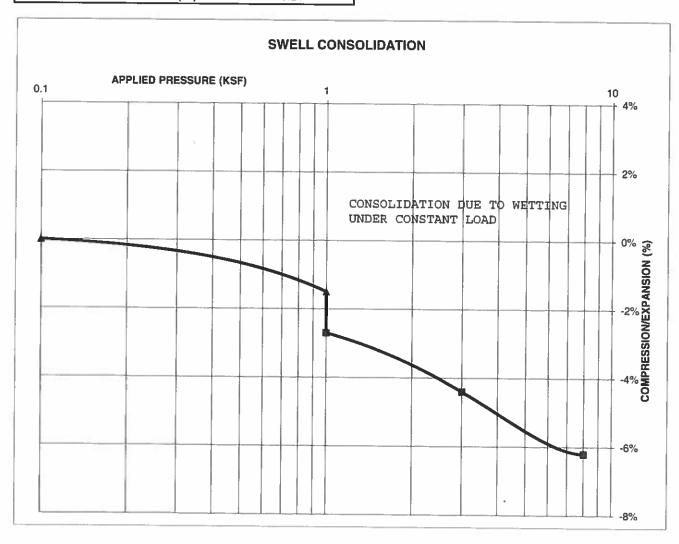
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TEST BORING #	19	DEPTH(ft)	2-3	
DESCRIPTION	SM	SOIL TYPE	1	
NATURAL UNIT DRY	WEIG	HT (PCF)	113	
NATURAL MOISTURE	CON	TENT	10.0%	
SWELL/CONSOLIDAT			-1.2%	

JOB NO. 190300 CLIENT TECH CONTRACTORS PROJECT ROLLING HILLS





SWELL CONSOLIDATION
TEST RESULTS

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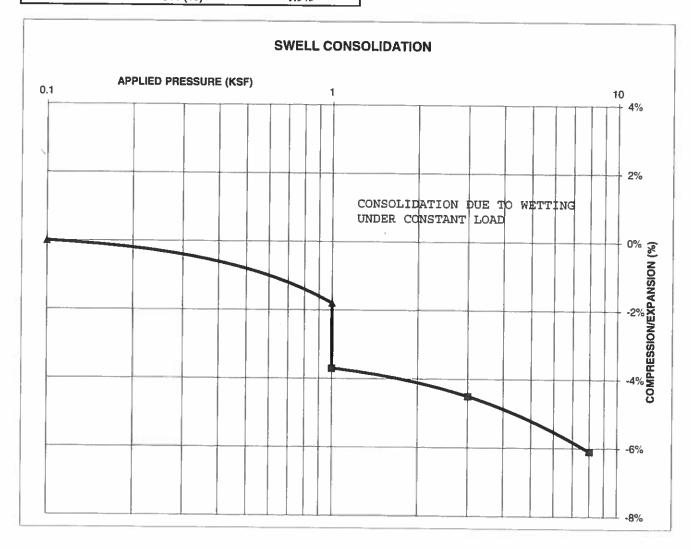
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TEST BORING #	4	DEPTH(ft)	20
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	WEIGI	HT (PCF)	110
NATURAL MOISTURE			9.3%
SWELL/CONSOLIDAT			-1.9%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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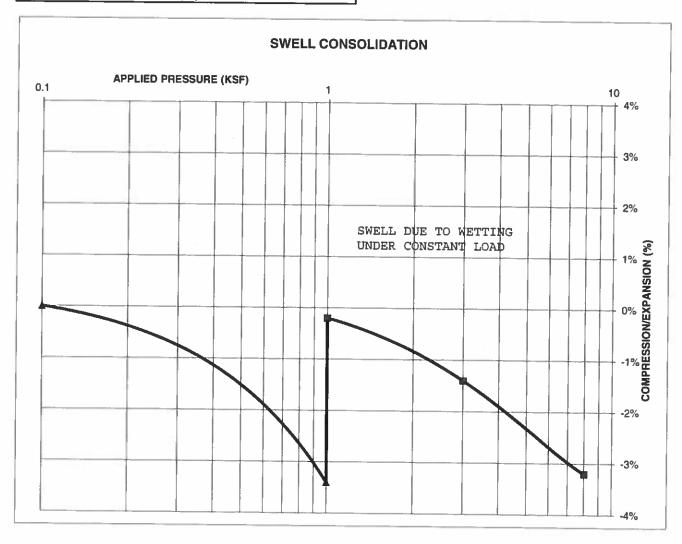
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TEST BORING #	20	DEPTH(ft)	20
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	/ WEIGI	HT (PCF)	84
NATURAL MOISTUR	RE CON	TENT	7.4%
SWELL/CONSOLIDA	ATION (S	%)	3.2%

JOB NO. 190300 CLIENT TECH CONTRACTORS PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

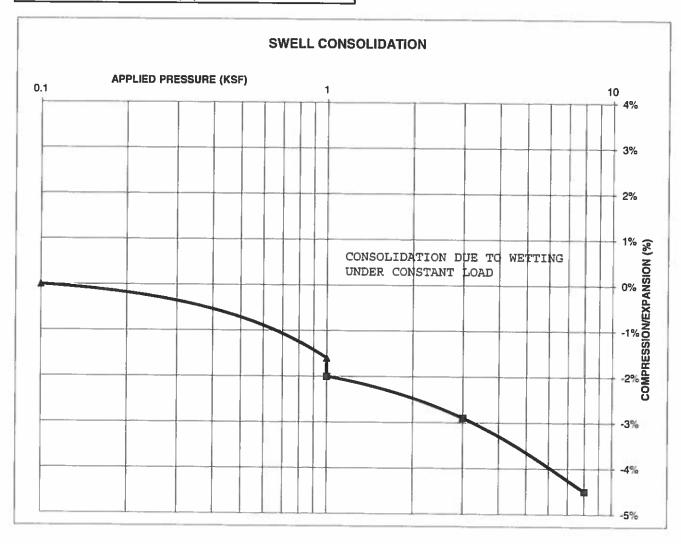
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JOB NO.:: 190300

TEST BORING #	29	DEPTH(ft)	10
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	WEIGI	HT (PCF)	120
NATURAL MOISTUR	E CON	TENT	4.5%
SWELL/CONSOLIDA	TION (%)	-0.4%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION	
TEST RESULTS	

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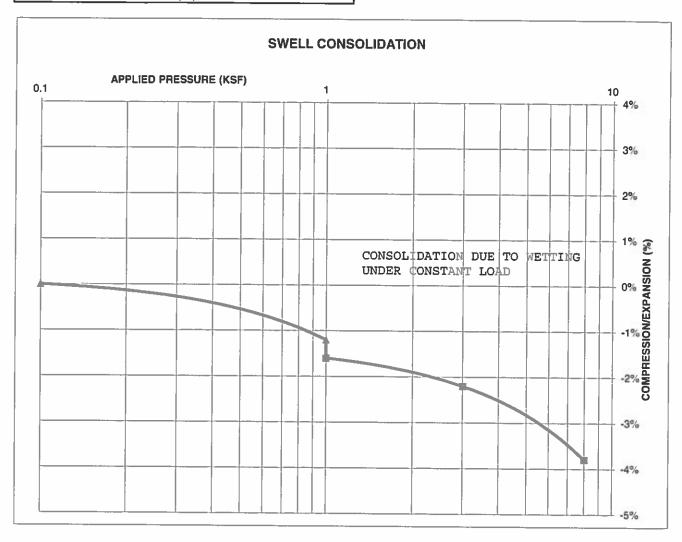
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DATE: 7/14/19

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TEST BORING # 37 DEPTH(ft) 5
DESCRIPTION SC SOIL TYPE 2
NATURAL UNIT DRY WEIGHT (PCF) 117
NATURAL MOISTURE CONTENT 11.4%
SWELL/CONSOLIDATION (%) -0.4%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION	
TEST RESULTS	

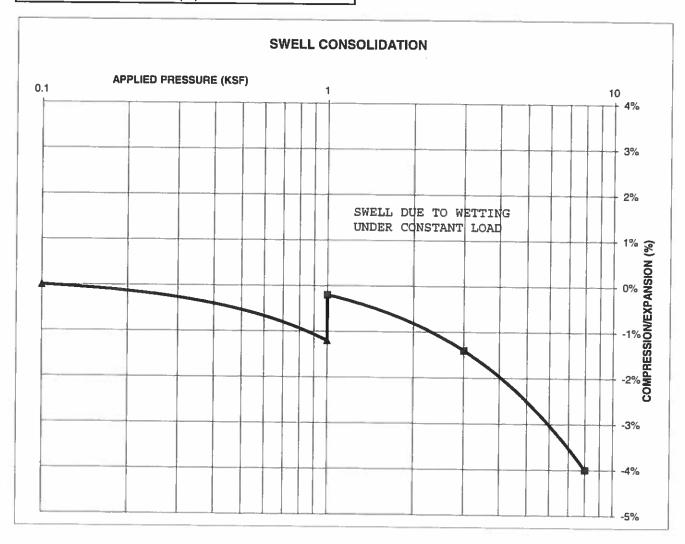
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TEST BORING #	15	DEPTH(ft)	10
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY	/ WEIGI	HT (PCF)	127
NATURAL MOISTUR	RE CON	TENT	7.2%
SWELL/CONSOLIDATION (%)			1.0%

JOB NO. 190300 CLIENT TECH CONTRACTORS PROJECT ROLLING HILLS





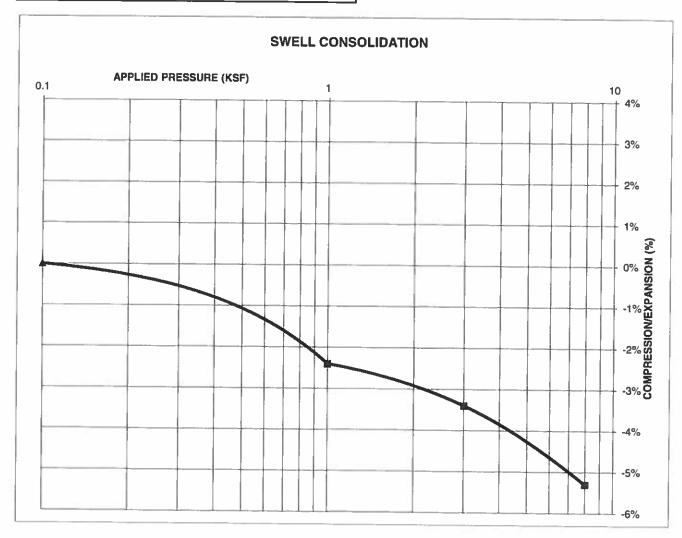
SWELL CONSOLIDATION		
TEST RESULTS		

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JOB NO.: 190300

TEST BORING #	16	DEPTH(ft)	20
DESCRIPTION	CL	SOIL TYPE	2
•			3
NATURAL UNIT DRY	WEIG	HT (PCF)	121
NATURAL MOISTURI			9.5%
			- 10 / 10
SWELL/CONSOLIDA	HON (%)	0.0%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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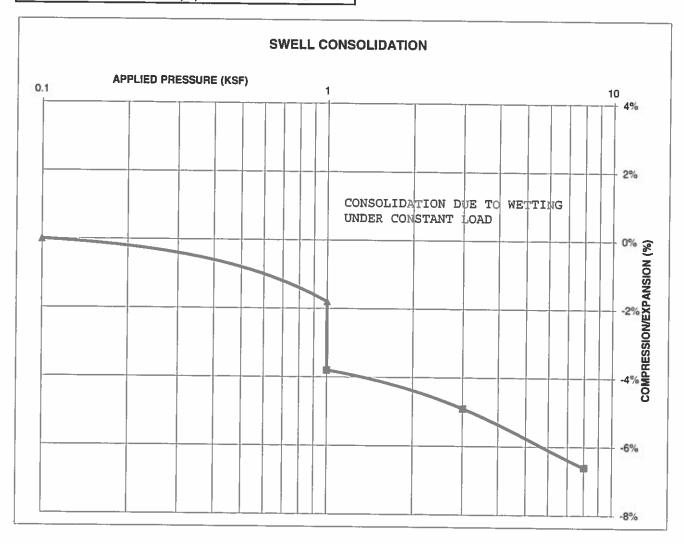
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JOB NO.: 190300

	<u> </u>			
	TEST BORING #	22	DEPTH(ft)	10
	DESCRIPTION	CL.	SOIL TYPE	3
				3
	NATURAL UNIT DRY	WEIGH	11 (PCF)	99
	NATURAL MOISTUR	E CON.	TENT	12.7%
ı	SWELL/CONSOLIDATION (%)			-2.0%

JOB NO. 190300 CLIENT TECH CONTRACTORS PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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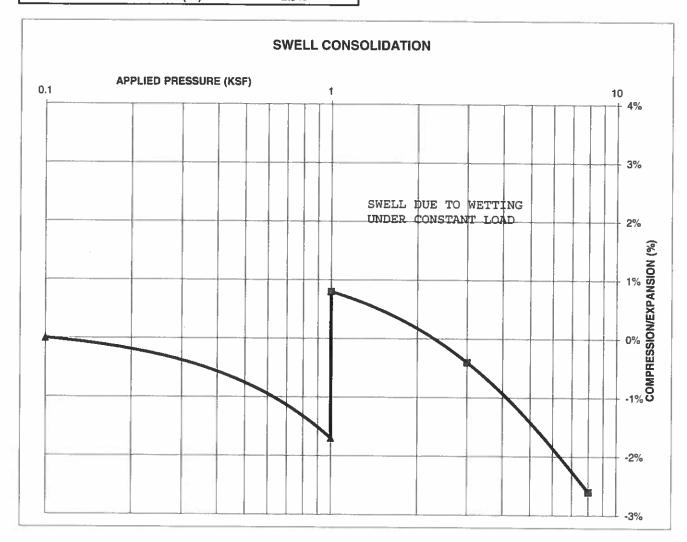
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JOB NO.: 190300

TEST BORING # 33 DEPTH(ft) 10
DESCRIPTION 0 SOIL TYPE 3
NATURAL UNIT DRY WEIGHT (PCF) 115
NATURAL MOISTURE CONTENT 16.5%
SWELL/CONSOLIDATION (%) 2.5%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION	NC
TEST RESULTS	

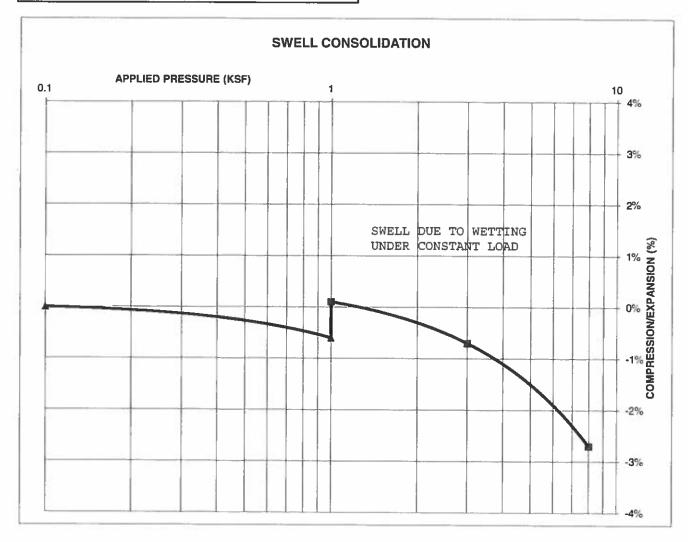
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JOB NO.... 190300

TEST BORING # 34 DEPTH(ft) 10
DESCRIPTION CL SOIL TYPE 3
NATURAL UNIT DRY WEIGHT (PCF) 114
NATURAL MOISTURE CONTENT 11.5%
SWELL/CONSOLIDATION (%) 0.7%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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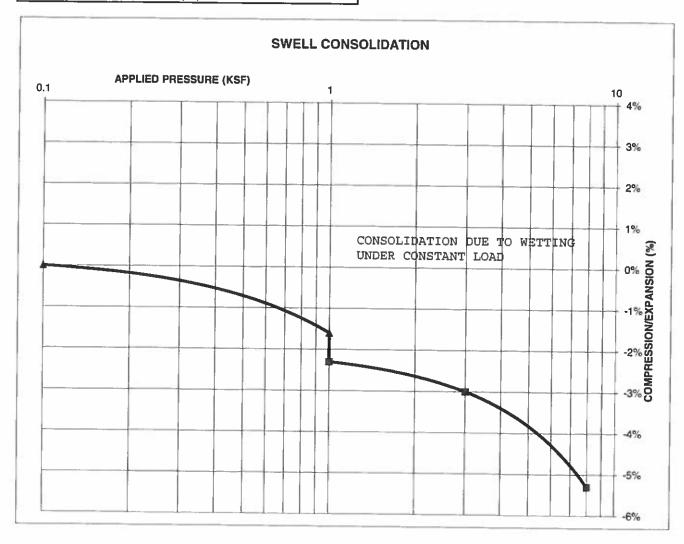
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TEST BORING #	48	DEPTH(ft)	20
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY	WEIG	HT (PCF)	103
NATURAL MOISTUR	E CON	TENT	12.5%
SWELL/CONSOLIDATION (%)		-0.7%	

JOB NO. 190300 CLIENT TECH CONTRACTORS PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

DRAWN: DATE:

CHECKED: 7/1/9

JOB NO.: 190300

 CLIENT
 TECH CONTRACTORS
 JOB NO.
 190300

 PROJECT
 ROLLING HILLS
 DATE
 3/28/2019

 LOCATION
 ROLLING HILLS
 TEST BY
 BL

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-6	2-3	1	SM-SW	<0.01
TB-10	5	1	sc	0.01
TB-6	20	2	sc	<0.01
TB-9	15	2	SM	<0.01
TB-23	2-3	1	SM	0.00
TB-37	5	2	SC	0.00
TB-40	10	2	SM	<0.01
TB-13	2-3	1	SW	0.00
TB-14	20	2	SM	<0.01
TB-15	10	3	CL	<0.01
TB-31	5	1	SM-SW	<0.01
TB-39	5	11	SM	<0.01
TB-39	15	2	SC	<0.01
TB-22	10	3	CL	<0.01
TB-28	2-3	1	sw	<0.01
TB-28	15	2	SC	0.00
TB-26	5	1	SM-SW	<0.01
TB-38	2-3	1	SM-SW	<0.01
TB-38	15	3	CL	0.03
TB-48	20	3	CL	0.00

QC BLANK PASS



		RATORY TEST ATE RESULTS
DRAWN:	DATE:	CHECKED: 7/DATE:

JOB NO.: 190300 FIG NO.:

SUBSURFACE SOIL INVESTIGATION MERIDIAN RANCH - ROLLING HILLS RANCH EL PASO COUNTY, COLORADO

Prepared for:

Tech Contractors 3575 Kenyon Street, Suite 200 San Diego, California 92110

Attn: Mr. Raul Guzman

July 15, 2019

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Reviewed by:

President

Daniel P. Stegman

DPS/ts

Encl.

Entech Job No. 190300 AAprojects/2019/190300/190300 SSI September 20, 2019



ENTECH ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

Tech Contractors 3575 Kenyon Street, Ste 200 San Diego, California 92110

Attn: Raul Guzman

Re: Soil, Geology and Geologic Hazard Evaluation

Meridian Ranch - Rolling Hills Ranch, Filings 1 through 4

SE of Sunrise Ridge Drive and Rex Road

El Paso County, Colorado

Dear Mr. Guzman:

As requested, personnel of Entech Engineering, Inc. have investigated the above referenced site to evaluate the conditions with respect to geology and geologic hazards affecting development of the site. The subsurface soil conditions were investigated by Entech Engineering, Inc., Test Boring Logs (Appendix A) and Summary of Laboratory Testing Results are included with this report.

The project consists of single-family residential development on an approximate 250–acre site. The site lies in El Paso County, Colorado, approximately 4 miles north of Falcon, Colorado. The approximate location of the site is shown on the Vicinity Location Map, Figure 1.

The topography of the site is gently to moderately sloping rolling hills that generally slope in a southeasterly direction. Minor drainages exist on the site that trend in south-southeasterly directions. The drainages were dry at the time of this investigation. The site lies in portions of S½ of Section 20, and Northern portion of Section 29 Township 12 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado. The site is currently vacant. The Site Plan/Proposed Grading is presented in Figure 3.

Forty-nine test borings were drilled on the site as a part of a Subsurface Soil Investigation dated July 15, 2019, (Reference 1). The Test Boring Logs are included in Appendix A. Laboratory Test Results are summarized in Table 1. Information from this report was used evaluating the site.

The scope of this report includes a geologic analysis/evaluation of the site utilizing published geologic data, available subsurface soils information and site-specific mapping of major geologic features, and identification of geologic hazards with respect to the development with recommended mitigation techniques. The Natural Resource Conservation Service (NRCS), previously the Soil Conservation Service (SCS) Survey was also reviewed to evaluate the site.

SOIL AND GEOLOGIC CONDITIONS

Soil Survey

The Natural Resource Conservation Service (NRCS) (Reference 2, Figure 3), previously the Soil Conservation Service (Reference 3) has mapped two soil types on the site. Complete descriptions of the soils are presented in Appendix B. In general, the soils consist of gravelly, sandy loam and sandy loam. The soils are described as follows:

Type	Description
19	Columbine gravelly sand loam, 0-3% slopes
83	Stapleton sandy loam, 3-8% slopes

Soils

The soils encountered in the test borings from Subsurface Soil Investigation consisted of slightly silty to silty sand, clayey sand, and clean sand overlying slightly silty to silty sandstone, clayey to very clayey sandstone with interbedded layers of sandy to very sandy claystone. The upper soils were encountered at medium dense to dense states and moist conditions. The upper sands have low expansion potential, however, the claystone and very clayey sandstone have moderate to high expansion potential.

Groundwater

Groundwater was encountered at depths ranging from 2 to 23 feet in thirty-eight of the test borings drilled on this site (Reference 1). Areas of potentially seasonal shallow and seasonal shallow groundwater have been mapped on the site and are discussed later in this report. Fluctuations in groundwater conditions may occur due to variations in rainfall or other factors not readily apparent at this time. Isolated sand layers within the soil profile can carry water in the subsurface. Contractors should be cognizant of the potential for the occurrence of subsurface water features during construction.

Geology

Approximately 16 miles west of the site is a major structural feature known as the Rampart Range Fault. This fault marks the boundary between the Great Plains Physiographic Province and the Southern Rocky Mountain Province. The site exists within a large structural feature known as the Denver Basin. Bedrock in the area is typically gently dipping in a northwesterly direction (Reference 4). The bedrock underlying the site consists of the Dawson Arkose Formation of Tertiary Age. The Dawson Formation typically consists of coarse-grained arkosic sandstone with interbedded layers of fine-grained sandstone, siltstone or claystone. Overlying the Dawson are deposits of alluvial, residual, and man-made soils.

The geology of the site was evaluated using the *Geologic Map of the Falcon Quadrangle*, by Morgan and White in 2012, (Reference 5, Figure 4). The geology of the site is indicated in Figure 5. Five mappable units were identified on this site which are described as follows:

Qaf Artificial Fill of Quaternary Age: These are man-made fill deposits associated with recent on-site grading and stockpiles.

Qal Recent Alluvium of Quaternary Age: These are recent stream deposits associated with the defined drainages on site. They generally consist of silty to clayey sands and may contain highly organic soil.

Qa₂ Alluvium Two of Quaternary Age: These are water deposited as stream terrace deposits that typically consist of silty to clayey sands and may contain clay layers. The Alluvium two correlates with the Piney Creek Alluvium.

Qa₃ Alluvium Three of Quaternary Age: These are water deposited as stream terrace deposits that typically consist of silty to clayey sands and may contain clay layers. The Alluvium Three correlates with the Broadway Alluvium.

Dawson Arkose Formation of Tertiary Age: The Dawson Formation typically consists of arkosic sandstone with interbedded fine-grained sandstone, siltstone and claystone. Overlying this formation is a variable layer of residual soil. The residual soils were derived from the in-situ weathering of the bedrock materials on-site. These soils consisted of silty sands and may contain layers of sandy clays.

ENGINEERING GEOLOGIC HAZARDS

Mapping has been performed on this site to identify areas where various geologic conditions exist of which developers should be cognizant during the planning, design and construction stages should new construction be proposed. The engineering geologic hazards identified on this site include artificial fill, potentially seasonal shallow groundwater areas, and shallow groundwater areas (Figure 6). Areas of shallow bedrock will also be encountered on this site. These hazards and recommended mitigation techniques are discussed as follows:

Artificial Fill

An area of fill was mapped on the site in the northeastern portion associated with a dam, and in the north central portion that is associated with a large fill pile that is considered uncontrolled, and areas of fill may exist that are not mapped due to on-going site grading.

<u>Mitigation</u>: It is anticipated the uncontrolled fill piles will be removed during site grading. Any uncontrolled fill encountered beneath foundations should be removed and recompacted at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557.

Loose Soils

Loose soils were encountered in some of the borings drilled on site. Loose soils if encountered beneath the foundation or floor slabs will require mitigation.

<u>Mitigation</u>: Should loose soils be encountered beneath foundations or floor slabs, mitigation will be necessary. Overexcavation and recompaction at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 is a suitable mitigation, which is common in the area. An overexcavation depth of 2 to 3 feet is anticipated for loose soils.

Expansive Soils

Expansive soils were encountered in some of the test borings drilled on-site. These occurrences are typically sporadic; therefore, none have been indicated on the maps. These clays and claystones, if encountered beneath foundations, can cause differential movement in the structure foundation. These occurrences should be identified and dealt with on an individual basis.

Mitigation: Should expansive soils be encountered beneath the foundation, mitigation will be necessary. Mitigation of expansive soils will require special foundation design. Overexcavation and replacement with non-expansive soils at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 is a suitable mitigation, which is common in the area. Another alternative in areas of highly expansive soils is the use of drilled pier foundation systems. Typical minimum pier depths are on the order of 25 feet and requiring penetration into the bedrock material a minimum of 4 to 6 feet, depending upon building loads. Floor slabs on expansive soils should be expected to experience movement. Overexcavation and replacement has been successful in minimizing slab movements. The use of structural floors should be considered for basement construction on highly expansive clays. Final recommendations should be determined after additional investigation of each building site.

Potentially Seasonal Shallow and Seasonal Shallow Groundwater Area

Drainages are located along the western, northern and southeastern portions of the site. In these areas, the potential for periodically high subsurface moisture conditions and frost heave potential exists. In these areas, the potential exists for shallow groundwater during high moisture periods. The drainages will be avoided or regraded during site development, and the seasonal shallow groundwater area will be avoided by the proposed development.

Mitigation: Foundations must have a minimum 30-inch depth for frost protection. In areas where high subsurface moisture conditions are anticipated periodically, subsurface perimeter drains are recommended to help prevent the intrusion of water into areas below grade. It is anticipated much of these areas would be filled during site grading further raising foundations above the groundwater level. Any grading in these areas should be done to direct surface flow around construction to avoid areas of ponded water. All organic material would be completely removed prior to fill placement. Specific recommendations concerning the affects of groundwater on site

grading and construction are included in the Subsurface Soil Investigation (Reference 1). Further investigation will be necessary to determine the groundwater depth after final grading. The site does not lie within any floodplain zones according to the FEMA Map No. 08041CO552G, dated December 7, 2018 (Figure 7, Reference 6). Exact locations of floodplain and specific drainage studies are beyond the scope of this report. Finished floor levels must be located a minimum of one foot above floodplain levels.

RELEVANCE OF GEOLOGIC CONDITIONS TO LAND USE PLANNING

As mentioned, the proposed development will be single-family residential. The existing geologic and engineering geologic conditions will impose some constraints on development and construction. The geologic conditions on the site include artificial fill, expansive or loose soils, and potentially seasonal shallow groundwater areas which can be satisfactorily mitigated through proper engineering design and construction practices or regrading and avoidance.

The upper granular soils encountered in the borings drilled on the site were generally encountered at medium dense to very dense states. Loose or uncontrolled fill soils, if encountered in roads or beneath foundations, will require recompaction. Expansive layers may also be encountered in the soil on this site. Expansive soils, if encountered, will require special foundation design. These soils will not prohibit development.

An area of fill was mapped on the site in the northeastern portion that is associated with the road and pond embankment, and a large fill pile is located in the northern portion of the site. Other minor areas associated with small fill piles that are considered uncontrolled, and areas of fill may exist. It is anticipated the fill piles would be removed during site grading. Any uncontrolled fill encountered beneath foundations and floor slabs will require removal and recompaction at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557.

Areas of shallow bedrock will be encountered on this site. Shallow bedrock will likely be encountered in those areas mapped as Tda-Dawson Formation, or Soil Types 2 or 3 on Figure 2. Bedrock depths are indicated on Table 2 and in Figures 3 and 6. Difficult excavation should be anticipated in areas of shallow bedrock. Higher allowable bearing capacities will also be expected in areas of shallow bedrock.

Groundwater was encountered at 2 to 23 feet in the thirty-eight of the forty-nine test borings. Groundwater depths are indicated on Table 2. Areas of potentially seasonal shallow and seasonally shallow groundwater have been mapped on this site. (Figure 6). These areas can be avoided by construction or are being regraded. Specific recommendations concerning the effects of groundwater on site grading and construction are discussed in the Subsurface Soil Investigation (Reference 1). The site should not be affected by any delineated 100-year FEMA floodplains (Figure 7, Reference 6).

In summary, the site granular soils will likely provide suitable support for roads and shallow foundations. The geologic conditions encountered on site can be mitigated with proper engineering and construction practices. Specific recommendations have been made in the Subsurface Soil Investigation (Reference 1).

CLOSURE

It should be pointed out that because of the nature of data obtained by random sampling of such variable nonhomogeneous materials as soil and rock, it is important that we be informed of any differences observed between surface and subsurface conditions encountered in construction and those assumed in the body of this report. Construction and design personnel should be made familiar with the contents of this report. Specific site recommendations have been made in the Preliminary Subsurface Soil Investigation (Reference 1). Specific construction and foundation recommendations will be provided when investigations are completed for new construction after overlot grading.

This report has been prepared for Tech Contractors for application to the proposed development in accordance with generally accepted geologic, soil and engineering practices. No other warranty expresses or implied is made.

We trust that this report has provided you with all the information that you required. Should you have any questions or require additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Logan L. Langford, P. G. Engineering Geologist

LLL/hg

Encl.Entech Job No. 190300 AAprojects/2019/190300 sg&ghs Reviewed by:

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- 2. Natural Resources Conservation Service. September 23, 2016. *Web Soil Survey.* United States Department of Agriculture. http://websoilsurvey.sc.egov..usda.gov.
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- Morgan, Matthew L. and White, Jonathan L. 2012. Falcon Quadrangle Geologic Map, El Paso County, Colorado. Colorado Geological Survey. Open-File Report 12-05.
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FIGURES

TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

TECH CONTRACTORS
ROLLING HILLS CLIENT PROJECT JOB NO.

HILLS	
ROLLING	100300
OJECT	CIV

SOIL DESCRIPTION	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, CLAYEY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND SILTY	SAND, VERY CLAYEY	SAND	SAND, CLAYEY	SAND	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND	SAND, CLAYEY	CLAY, SANDY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SANDSTONE, CLAYEY	SANDSTONE. SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE SILTY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY
UNIFIED CLASS.	SM-SW	SM-SW	SC	SM	SM-SW	SM	SM	SM	SC	SW	SC	SW	SM	SM-SW	SM	SM-SW	SW	SC	ರ	SM-SW	SM-SW	SM-SW	SM	SM	SM-SW	SM	SM-SW	SC	SM-SW SAN	-	SC	SM	SM	SM		\vdash
SWELL/ CONSOL (%)															-1.2																					
FHA SWELL (PSF)				370					460					70					2970							220										
AASHTO CLASS.	A-1-b		A-2-6			A-1-b				A-1-b	A-2-4		A-1-b			A-1-b	A-1-b					A-1-b			A-1-b			A-2-6	A-1-b		A-2-6				A-6	A-1-b
SULFATE (WT %)	<0.01		0.01			0.00																													<0.01	<0.01
PLASTIC INDEX (%)	ΝP		16			NP				NP	10		AN D			NP	ΔN					٩			Z L			14	NP		20				13	₽ Q
LIQUID LIMIT (%)	N		53			N				>N	56		>2			N						N			2			32	N<		37				56	N
PASSING NO. 200 SIEVE (%)	8.1	6.1	14.0	15.2	8.4	17.0	18.0	15.6	48.3	4.7	13.3	4.8	13.2	5.9	34.7	11.5	4.9	12.1		6.9	5.4	8.6	17.8	19.6	6.0	20.7	7.3	18.6	7.3	14.2	17.1	12.5	16.0	14.3	38.9	17.5
DRY DENSITY (PCF)															112.9									=												
WATER (%)															10.0										1											
рертн (FT)	2-3	2	5	2-3	2-3	2-3	2-3	2	2	2-3	2-3	2-3	2	2	2-3	2	2-3	2	က	2	2	2-3	ς,	2	2-3	2-3	2	9	9	2	2	9	9	9	20	15
TEST BORING NO.	9	88	9	Ξ	2	23	24	32	27	-	2	13	14	91	19	56	28	30	8	90	31	88	38	42	43 i	47	46	,	17	18	20	21	41	4	9	თ
SOIL	-	-	-	-	-	-	-	-	-	-	-pro-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2	2	2	2	2	2	2	2	2

TABLE 1 (cont.)

	Γ	Π	Τ	Π	Τ	≥				Τ	L	Τ	Γ	l	Т		Ī.	l	Γ	L	Ι	Г		Т	Т		Т	Т	Т	Т
SOIL DESCRIPTION	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY					
UNIFIED CLASS.	SM	SM	SC	SM	SM	SM-SW	SM-SW	SM	SM	SC	SC	SM	SC	SC	SM	သွင	SC	SC	SM	SC	苬	ರ	ರ	덩	ರ	ರ	덩	ರ	ರ	CL
SWELL/ CONSOL (%)			-0.4							-1.9				3.2			-0.4					1.0	0.0			-0.7			0.7	2.5
FHA SWELL (PSF)																												8		
AASHTO CLASS.				A-1-b	A-2-4					A-2-6	A-6			A-6		A-2-6								A-6	A-6					A-7-6
SULFATE (WT %)			0.00	<0.01																										
PLASTIC INDEX (%)				AN	NP					12	14			14		17								15	17					20
LIQUID LIMIT (%)				N<	NV					29	31			28		41								34	34					42
PASSING NO. 200 SIEVE (%)	15.5	26.1	35.4	12.3	28.7	11.6	10.1	16.2	15.5	20.3	48.5	17.8	19.9	49.7	21.2	28.3	49.6	41.1	13.4	45.5	65.1	56.1	58.8	54.2	59.6	51.1	59.7	63.6	56.0	80.8
DRY DENSITY (PCF)			116.5							110.3				84.0			119.9					126.8	120.5	99.3		103.3			114.3	115.0
WATER (%)			11.4							9.3				7.4			4.5					7.2	9.5	12.7		12.5			11.5	16.5
DEPTH (FT)	10	5	2	10	15	10	נט	10	15	50	25	20	15	50	25	15	9	15	20	15	S	은	20	9	15	20	15	2	9	10
TEST BORING NO.	12	63	37	40	25	23	35	27	-	4	2	14	15	20	21	28	29	33	45	46	19	2	9	22	88	48	999	24	84	253
SOIL	2	2	7	2	2	2	2	2	2	2	2	2	2	2	2	2	N	2	7	2	3	3	9	3	8	3	8	m	m	20

Table 2: Summary of Test Borings and Water Measurements*

Test	Depth of	Depth to	Depth to	Cut & Fill**	Estimated	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
1	20.0	9.0	9.0	0 to -2	7021.3	7012.3
2	25.0	9.0	13.0	-2 to -4	7031.5	7018.5
3	25.0	1.0	15.0	-2 to -4	7032.3	7017.3
4	20.0	1.0	dry	-2 to -4	7044.0	dry
5	25.0	4.0	14.0	-2 to -4	7044.8	7030.8
6	25.0	14.0	10.0	0 to +2	7054.7	7044.7
7	20.0	1.0	16.5	+2 to +4	7058.6	7042.6
8	20.0	9.0	13.0	0 to -2	7060.1	7047.1
9	20.0	14.0	10.0	+4 to +6	7069.7	7059.7
10	20.0	14.0	14.0	0 to -2	7077.5	7063.5
11	20.0	9.0	9.0	0 to +2	7071.6	7062.6
12	20.0	9.0	14.0	0 to -2	7087.3	7073.3
13	20.0	9.0	14.0	0 to -2	7092.0	7078.0
14	25.0	14.0	18.5	-6 to -8	7105.3	7086.8
15	20.0	9.0	18.0	0 to -2	7108.4	7090.4
16	25.0	9.0	16.0	0 to -2	7110.9	7094.9
17	20.0	1.0	17.5	0 to -2	7121.7	7104.2
18	20.0	4.0	dry	0 to +2	7120.7	dry
19	20.0	4.0	dry	+2 to +4	7126.5	dry
20	20.0	1.0	dry	outside cut/fill	7125.4	dry
21	25.0	1.0	10.0	-6 to -8	7105.7	7095.7
22	20.0	4.0	18.5	-6 to -8	7106.0	7087.5
23	20.0	9.0	dry	+2 to +4	7092.3	dry
24	25.0	4.0	2.0	0 to +2	7072.9	7070.9

Table 2: (Continued)

Test	Depth of	Depth to	Depth to	Cut & Fili**	Est.	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
25	20.0	1.0	12.0	0 to +2	7068.8	7056.8
26	20.0	1.0	17.0	-6 to -8	7049.2	7032.2
27	20.0	9.0	8.0	0 to +2	7071.2	7063.2
28	20.0	9.0	13.5	0 to -2	7082.9	7069.4
29	25.0	4.0	12.0	outside cut/fill	7084.4	7072.4
30	20.0	10.0	8.0	0 to +2	7066.7	7058.7
31	20.0	14.0	dry	0 to -2	7057.5	dry
32	25.0	14.0	13.0	0 to -2	7045.4	7032.4
33	25.0	9.0	7.0	0 to -2	7052.7	7045.7
34	20.0	1.0	9.0	+2 to +4	7042.0	7033.0
35	20.0	3.0	dry	0 to -2	7065.4	dry
36	25.0	1.0	23.0	-6 to -8	7049.4	7026.4
37	20.0	1.0	dry	-2 to -4	7038.8	dry
38	25.0	12.0	10.0	-6 to -8	7032.4	7022.4
39	20.0	9.0	4.0	-6 to -8	7032.5	7028.5
40	20.0	9.0	10.0	+12 to +14	7032.1	7022.1
41	20.0	1.0	17.0	outside cut/fill	7039.1	7022.1
42	25.0	9.0	14.0	outside cut/fill	7046.0	7032.0
43	25.0	4.0	19.0	outside cut/fill	7049.0	7030.0
44	20.0	1.0	dry	outside cut/fill	7064.0	dry
45	25.0	4.0	11.0	outside cut/fill	7072.1	7061.1
46	25.0	4.0	22.0	outside cut/fill	7065.0	7043.0
47	20.0	1.0	dry	outside cut/fill	7058.7	dry
48	20.0	1.0	dry	outside cut/fill	7047.6	dry
49	25.0	14.0	12.0	outside cut/fill	7029.5	7017.5

Measurement taken subsequent to drillingCut and Fill estimates based on map provided by the client



Latigo Blvd

Latigo Ble

Rex Rd

Falcon High School

Londonderry Dr

arry Dr



VICINITY MAP

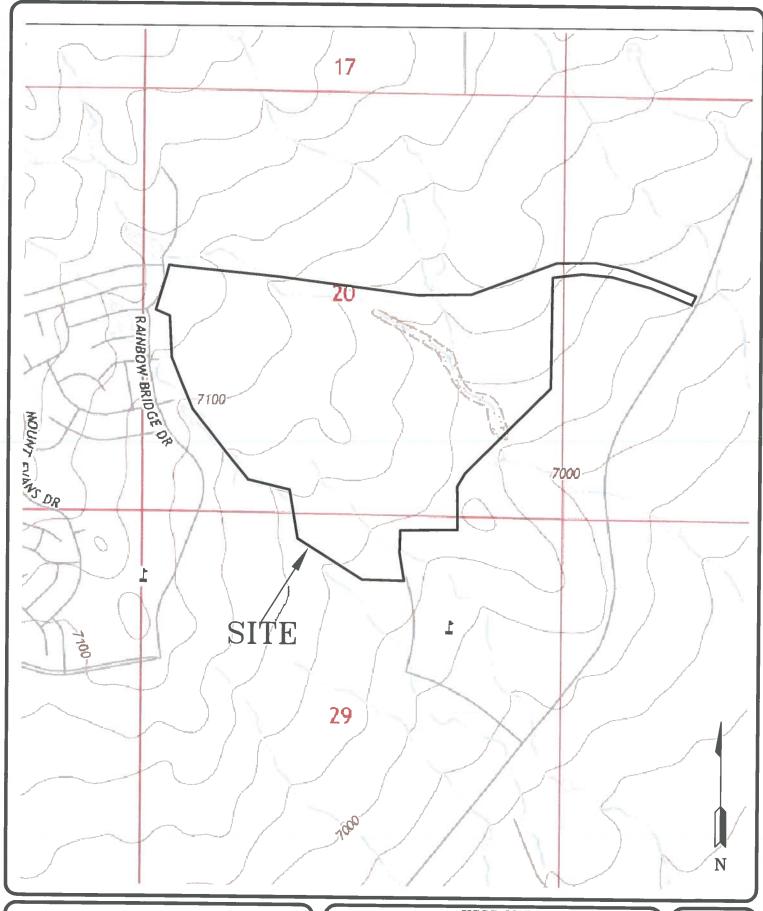
MERIDIAN RANCH - ROLLING HILLS RANCH
FILINGS 1 - 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS

DRAWN: 9/18/19

CHECKED: DATE: FIG NO.: 1

JOB NO.: 190300

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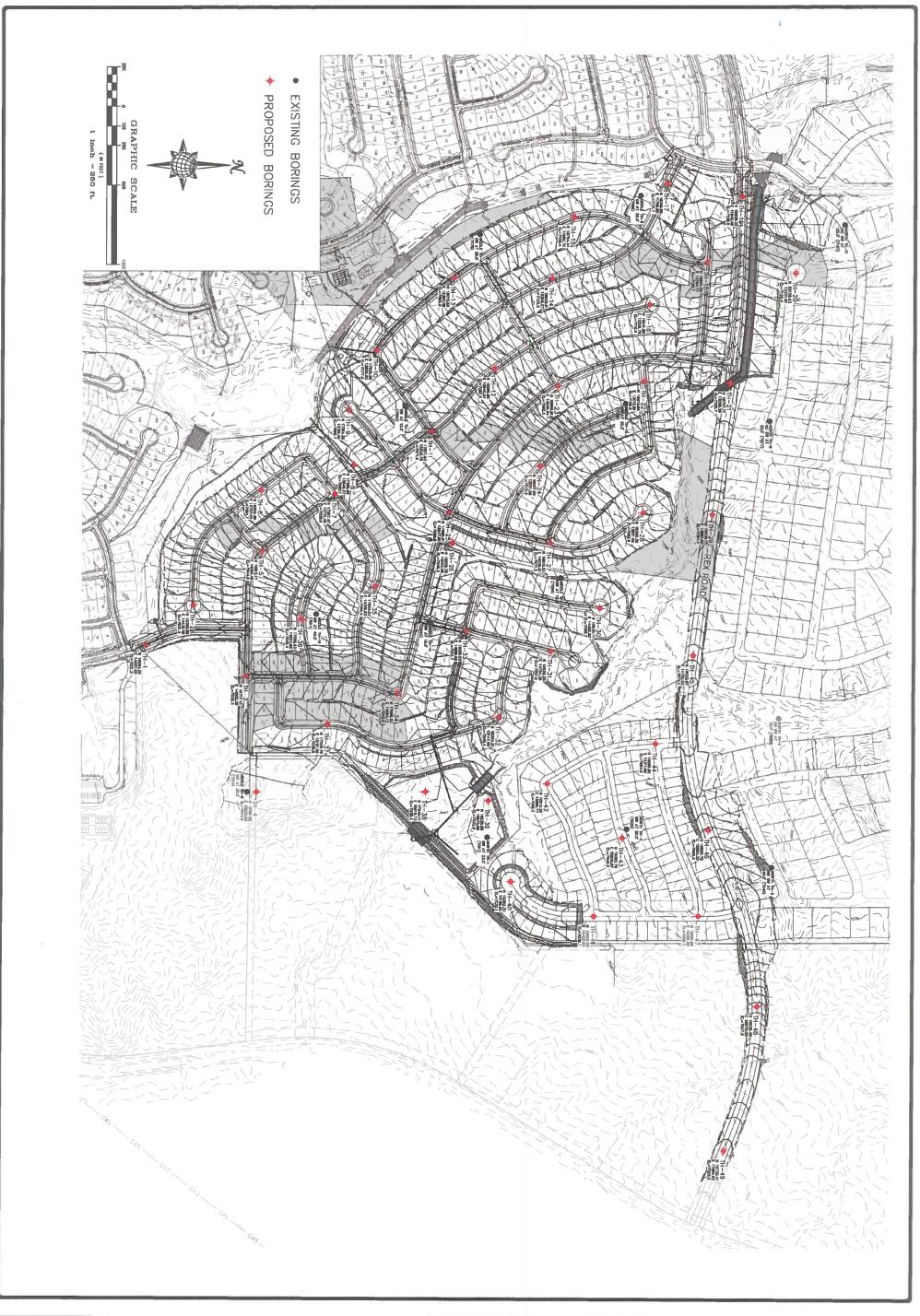
USGS MAP

MERIDIAN RANCH — ROLLING HILLS RANCH
FILINGS 1 — 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS

DRAWN: DATE: CHECKED: DATE:
LLL 9/18/19

JOB NO.: 190300

FIG NO.:

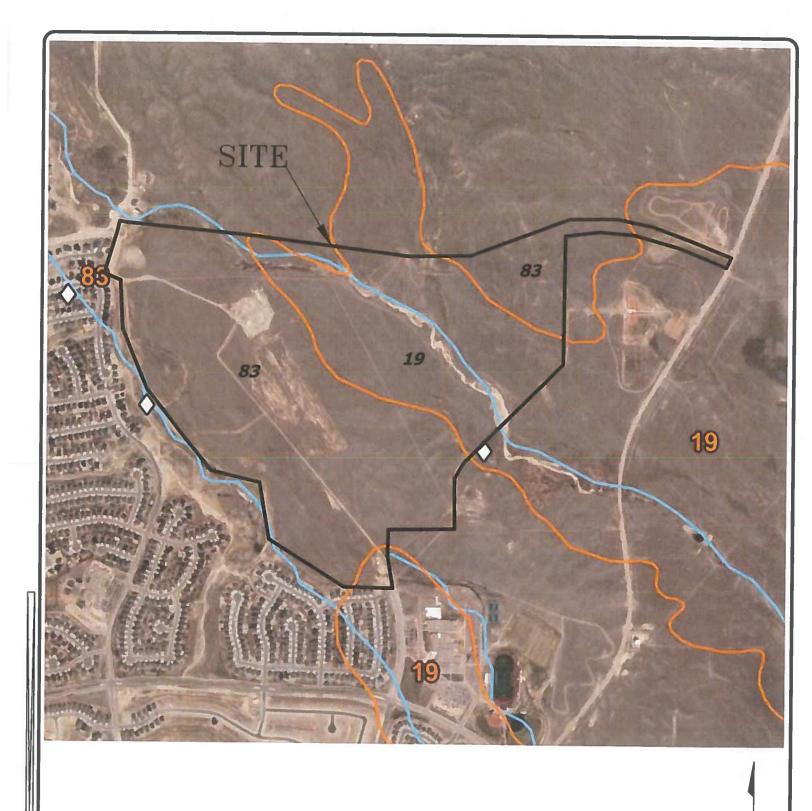




SITE PLAN/PROPOSED GRADING
MERIDIAN RANCH - ROLLING HILLS RANCH
FILINGS 1 - 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS



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				Вү





SOIL SURVEY MAP

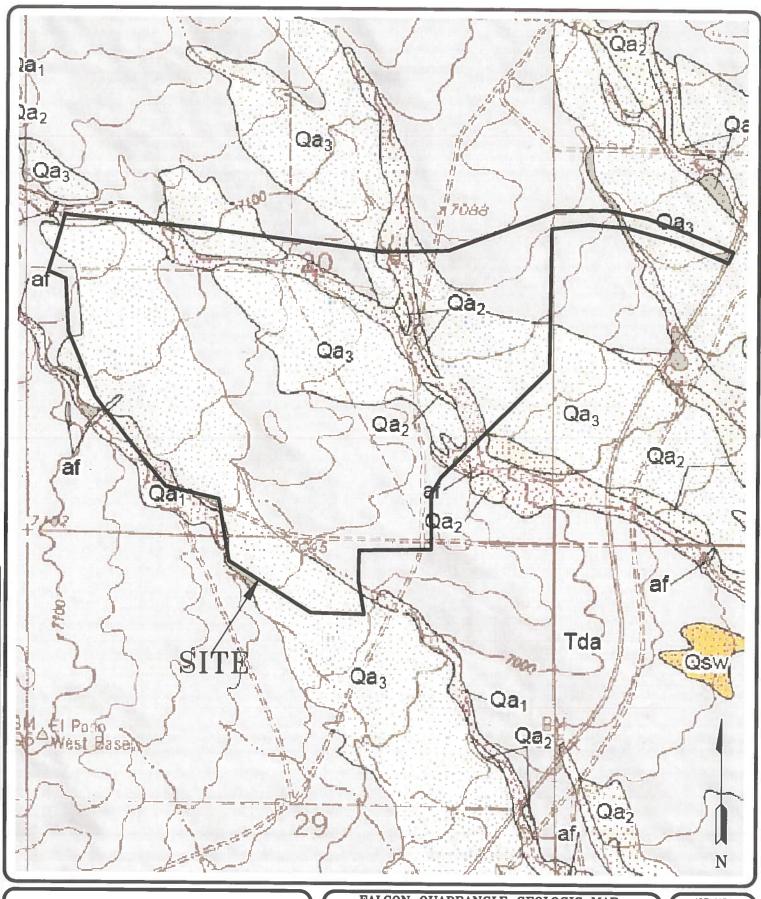
MERIDIAN RANCH - ROLLING HILLS RANCH
FILINGS 1 - 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS

DRAWN: DATE: CHECKED: DATE:
LLL 9/18/19

JOB NO.: 190300

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FIG NO.:

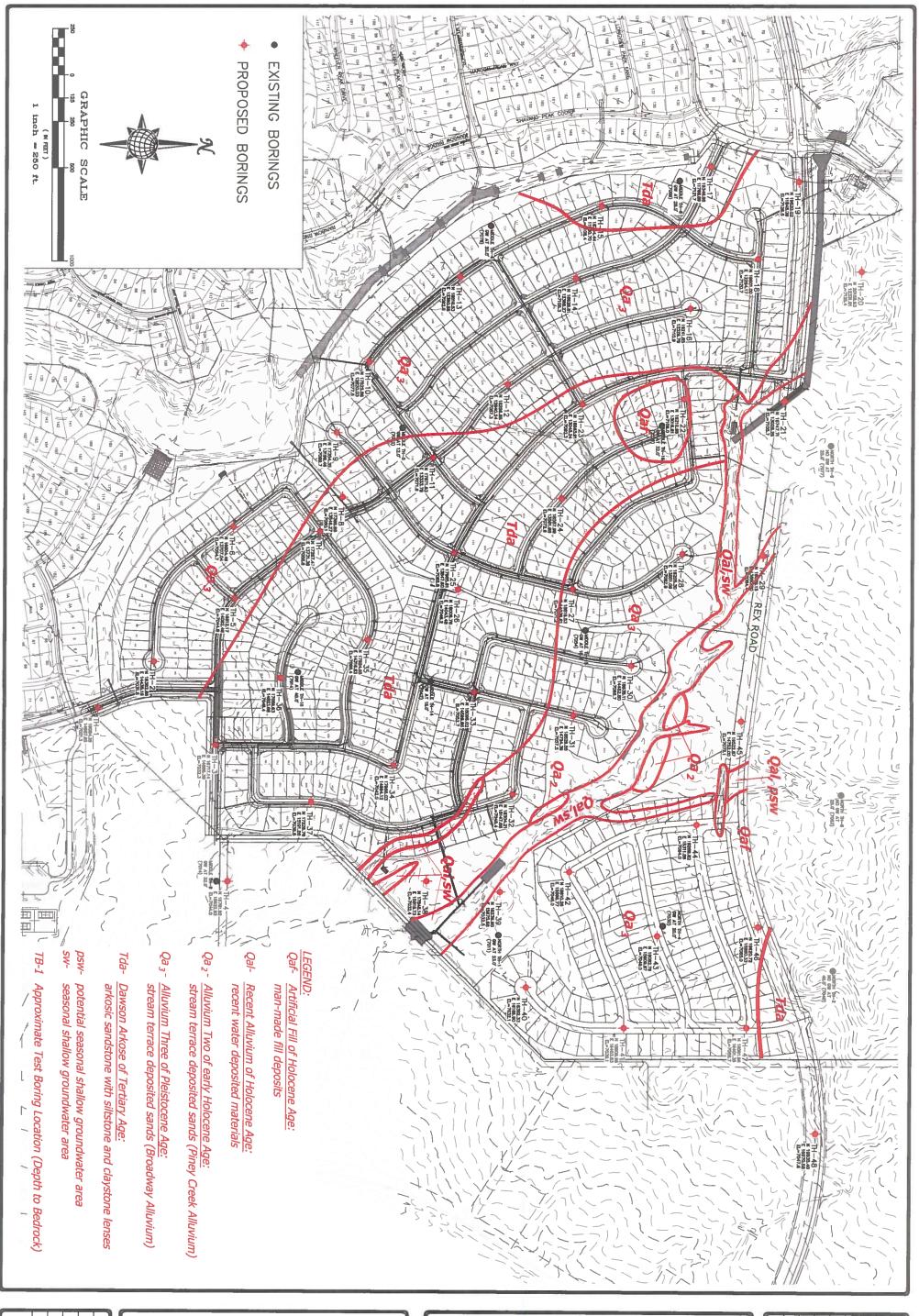




FALCON QUADRANGLE GEOLOGIC MAP MERIDIAN RANCH - ROLLING HILLS RANCH FILINGS 1 - 4 EL PASO COUNTY, CO. FOR: TECH CONTRACTORS						
DRAWN: LLL	DATE: 9/18/19	CHECKED:	DATE:			

JOB NO.: 190300

FIG NO.: 5

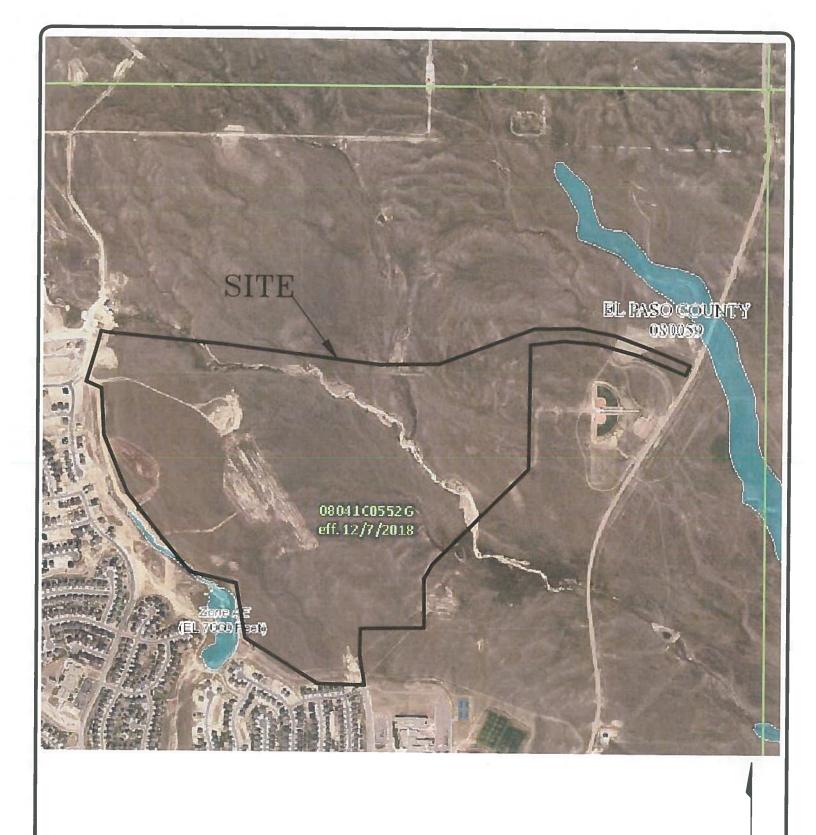




ENGINEERING GEOLOGY MAP
MERIDIAN RANCH - ROLLING HILLS RANCH
FILINGS 1 - 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS



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FEMA FLOODPLAIN MAP
MERIDIAN RANCH - ROLLING HILLS RANCH
FILINGS 1 - 4
EL PASO COUNTY, CO.
FOR: TECH CONTRACTORS

DRAWN: DATE: CHECKED: DATE: LLL 9/18/19

JOB NO.: 190300

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FIG NO.:



TEST BORING NO. TEST BORING NO. 2 DATE DRILLED 6/19/2019 DATE DRILLED 3/11/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % foot Watercontent Watercontent Blows per Blows per Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol Soil WATER @ 9', 6/19/19 WATER @ 13', 3/11/19 3" TOPSOIL SAND, CLEAN TO ¥Ž, SAND, GRAVELLY, SLIGHTLY . o . d SILTY, FINE TO COARSE SILTY, FINE TO COARSE GRAINED, GRAINED, TAN, MEDIUM DENSE, 14 8.3 1 BROWN, MEDIUM DENSE, MOIST 22 12.5 MOIST 5 23 7.0 1 5 28 9.3 1 SANDSTONE, SILTY, FINE 10 50 12.4 2 SANDSTONE, SILTY, FINE TO 10 <u>50</u> 7.8 2 TO COARSE GRAINED, TAN, 9" COARSE GRAINED, TAN TO GRAY 10" VERY DENSE, MOIST TO WET BROWN, VERY DENSE, MOIST TO WET 15 <u>50</u> | 11.9 2 15 50 14.6 2 10" 9" 20 50 12.7 2 CLAYSTONE, SANDY, GRAY 20 50 11.9 9" BROWN, HARD, MOIST 25 50 12.4 3



	TE	EST BORING LO	G	
DRAWN:	DATE	CHECKED	DATE 7/1/19	J

TEST BORING NO. 3 TEST BORING NO. DATE DRILLED 3/11/2019 DATE DRILLED 6/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % Blows per foot Watercontent Watercontent Blows per Depth (ft) Soil Type Samples Depth (ft) Soil Type Symbol Samples Symbol WATER @ 15', 3/11/19 DRY TO 20', 6/7/19 SAND, SILTY, TAN 1.1 T 6" TOPSOIL, SAND, SILTY, TAN 1 SANDSTONE, SILTY, FINE TO SANDSTONE, SILTY, FINE TO :::: COARSE GRAINED, TAN, VERY 50 4.4 2 COARSE GRAINED, TAN, VERY 50 7.8 2 DENSE, MOIST 11" DENSE, MOIST 7" 5 50 7.3 2 5 50 2 5.7 8" 7" SANDSTONE, CLAYEY, FINE TO 10 50 11.4 FINE GRAINED LENSES 10 50 8.7 2 MEDIUM GRAINED, GRAY 4" 6" BROWN, VERY DENSE, MOIST TO WET 15 <u>50</u> 11.6 2 CLAYSTONE, SANDY, TAN, 15 50 17.0 3 6" HARD, MOIST 9" 20 30.4 <u>50</u> 2 SANDSTONE, CLAYEY, FINE 20 <u>50</u> 8.4 2 8" TO COARSE GRAINED, TAN, VERY DENSE, MOIST 25 <u>50</u> 24.1 2

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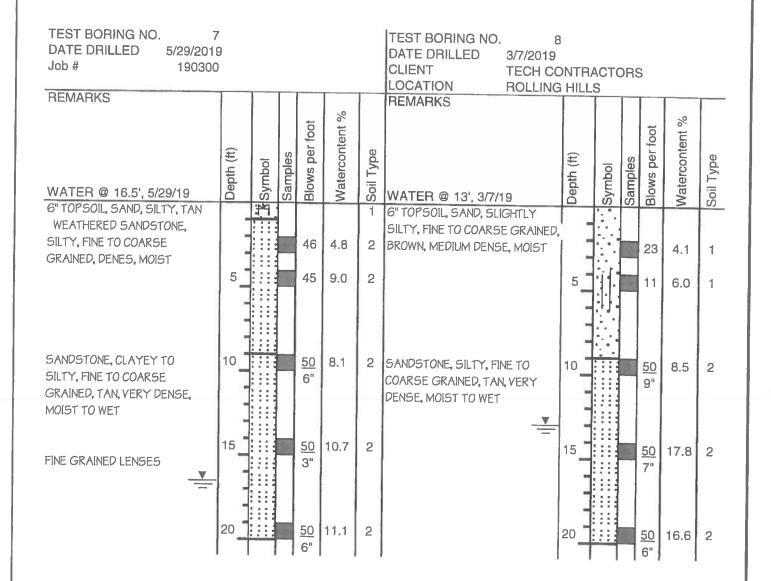


TES	T BORING LO	G
DATE:	CHECKED:	DATE

TEST BORING NO. TEST BORING NO. **DATE DRILLED** 5/29/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT TECH CONTRACTORS LOCATION **ROLLING HILLS** REMARKS **REMARKS** foot Watercontent Watercontent Blows per Ξ Blows per Samples Depth (ft) Samples Symbol Symbol Depth (Soil WATER @ 14', 5/29/19 WATER @ 10', 3/7/19 3" TOPSOIL SAND, CLAYEY, * 6" TOPSOIL, SAND, SLIGHTLY FINE TO COARSE GRAINED. SILTY, FINE TO COARSE GRAINED TAN, MEDIUM DENSE, MOIST 14 9.6 1 BROWN TO TAN, MEDIUM DENSE 28 2.4 TO LOOSE, MOIST TO WET SANDSTONE, SILTY, FINE TO 40 5.4 2 5 21 4.2 COARSE GRAINED, TAN. DENSE TO MEDIUM DENSE. MOIST 10 50 9.3 2 10 9 15.7 1 6" 15 6.5 50 WEATHERED TO FORMATIONAL 15 48 13.3 2 5" SANDSTONE, CLAYEY TO VERY CLAYEY, FINE TO COARSE GRAINED, GRAY BROWN, DENSE TO VERY DENSE, MOIST CLAYSTONE, SANDY, GRAY 20 50 13.8 3 20 50 11.7 2 BROWN, HARD, MOIST 4" 10" SANDSTONE, VERY CLAYEY. 25 <u>50</u> 14.6 2 25 45 15.4 2 FINE GRAINED, GRAY BROWN, VERY DENSE, MOIST



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TEST BORING NO. TEST BORING NO. 10 DATE DRILLED 3/7/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % Blows per foot Watercontent Watercontent Type Type Blows per Depth (ft) Samples Soil Type Symbol Samples Symbol Depth WATER @ 14', 3/7/19 WATER @ 10', 3/7/19 6" TOPSOIL, SAND, SILTY, FINE ** 6" TOPSOIL, SAND, SILTY TO <u>. sv</u> TO COARSE GRAINED, BROWN, CLAYEY, FINE TO COARSE MEDIUM DENSE, DRY TO MOIST 16 2.7 GRAINED, TAN, MEDIUM DENSE, 26 6.2 1 MOIST 5 11 6.6 1 19 7.8 1 SAND, CLAYEY, FINE TO 10 5 18.0 بسير ا 1 \blacksquare 10 27 12.4 1 COARSE GRAINED, GRAY BROWN, LOOSE, WET 15 SANDSTONE, SILTY, FINE TO <u>50</u> 8.7 SANDSTONE, CLAYEY. 15 50 12.5 2 COARSE GRAINED, TAN, VERY FINE TO COARSE GRAINED. 10" DENSE, MOIST BRPOWN, VERY DENSE TO DENSE, WET <u>50</u> 10.9 2 WEATHERED ZONE 20 45 13.8 2

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	TEST	BORING	LOG	
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TEST BORING NO. 11 TEST BORING NO. 12 DATE DRILLED 3/7/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % Blows per foot Watercontent foot Watercontent Blows per Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol Soil WATER @ 9', 3/7/19 WATER @ 14', 3/7/19 SAND, SILTY, FINE TO COARSE 6" TOPSOIL, SAND, SILTY, FINE * GRAINED, TAN, LOOSE TO TO COARSE GRAINED, BROWN, MEDIUM DENSE, VERY MOIST 7 21.3 LOOSE TO MEDIUM DENSE. 6 3.6 1 MOIST 5 16 | 15.1 1 23 8.6 1 SANDSTONE, SILTY, FINE 10 <u>50</u> 17.5 WEATHERED TO FORMATIONAL 10 36 | 11.3 2 TO COARSE GRAINED, TAN, 11" SANDSTONE, SILTY, FINE TO VERY DENSE, WET COARSE GRAINED, BROWN, DENSE TO VERY DENSE, MOIST TO WET 15]: : : : <u>50</u> 12.6 2 CLAYEY LENSES 15 50 20.2 2 8" 11" 20 <u>50</u> 12.7 2 20 <u>50</u> 12.8 2

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JOB NO.: 190300 FIG NO.:

A- 6

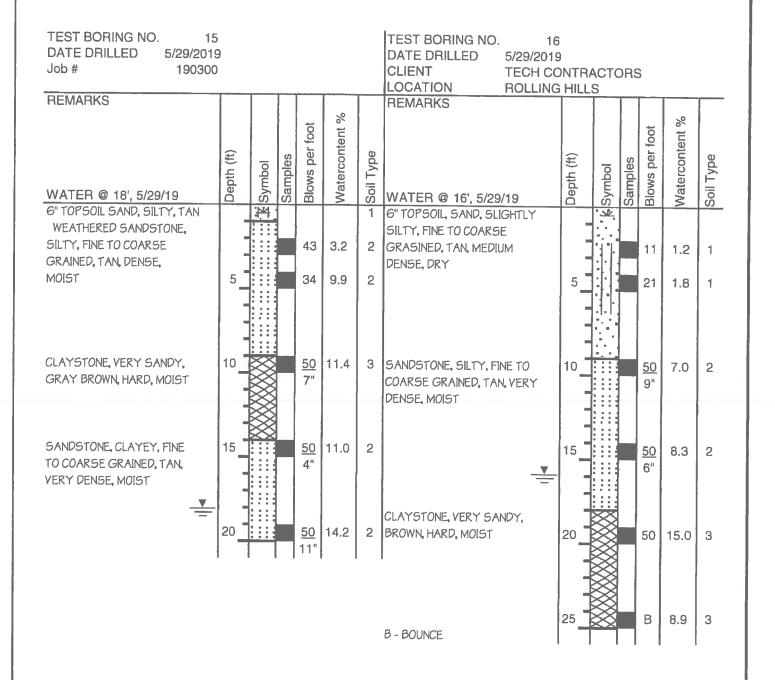
TEST BORING NO. TEST BORING NO. 13 14 DATE DRILLED 5/29/2019 DATE DRILLED 5/29/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Watercontent Watercontent Blows per Depth (ft) Samples Soil Type Symbol Samples Symbol Depth Soil WATER @ 14', 5/29/19 WATER @ 18.5', 5/29/19 6" TOPSOIL, SAND, CLEAN TO علا 6" TOPSOIL, SAND, SILTY, FINE SILTY, FINE TO COARSE TO COARSE GRAINED, TAN, GRAINED, TAN, LOOSE TO 11 1.4 LOOSE TO MEDIUM DENSE, 13 1.8 1 MEDIUM DENSE, MOIST DRY TO MOIST 5 14 6.3 1 5 7 2.3 1 WEATHERED TO FORMATIONAL 10 45 8.4 2 FINE GRAINED LENSES 10 24 9.1 1 SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, DENSE TO VERY DENSE, MOIST TO WET 48 15 8.9 SANDSTONE, SILTY, FINE TO 15 50 6.7 2 COARSE GRAINED, TAN. 11" VERY DENSE, MOIST TO WET 20 <u>50</u> 11.5 2 20 <u>50</u> 10.6 2 11" 25 50 12.6 2

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190300 FIG NO. A- 7



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			/^	7/17/10	

TEST BORING NO. 17 TEST BORING NO. 18 DATE DRILLED 5/29/2019 DATE DRILLED 6/7/2019 Job# 190300 **CLIENT TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Watercontent % Blows per foot foot Watercontent Blows per Type Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol Soil. WATER @ 17.5', 5/29/19 DRY TO 20', 6/7/19 6" TOPSOIL, SAND, SILTY, TAN 14 6" TOPSOIL, SAND, SILTY, SANDSTONE, SILTY, FINE TO FINE TO COARSE GRAINED. COARSE GRAINED, TAN, :: <u>50</u> 1.7 2 BROWN, MEDIUM DENSE, DRY 12 2.7 1 VERY DENSE, DRY TO MOIST 10" 50 1.8 WEATHERED TO FORMATIONAL 5 42 5.0 2 8" SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, DENSE TO VERY DENSE, MOIST 10 2 50 6.9 1::: 10 2 50 8.9 6" FINE GRAINED LENSES 6" 15 50 8.0 2 :::: 15 50 2 4.9 20 <u>50</u> 10.1 2 20 7.0 2 <u>50</u>



TEST BORING LOG

DRAWN: DATE: CHECKED: L. PATE: 7/1/19

JOB NO.: 190300 FIG NO.:

A- 9

TEST BORING NO. 19 TEST BORING NO. 20 DATE DRILLED 6/7/2019 DATE DRILLED 5/30/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Watercontent % Blows per foot foot Watercontent Blows per Ξ Soil Type Samples \equiv Soil Type Samples Symbol Symbol Depth (Depth (DRY TO 20', 5/30/19 DRY TO 20', 6/7/19 CAVED TO 19', 6/6/19, DRY 6" TOPSOIL, SAND, SILTY, FINE : 34 6" TOPSOIL, SAND, SILTY, TAN 14 1 TO COARSE GRAINED, GRAY SANDSTONE, SILTY TO BROWN, MEDIUM DENSE, MOIST 21 7.8 CLAYEY, FINE TO COARSE 1 . . 50 4.8 2 GRAINED, TAN, VERY DENSE. 10" CLAYSTONE, SANDY, GRAY 5 50 10.9 DRY TO MOIST 5 50 2 8.6 9" BROWN, HARD, MOIST 9" SANDSTONE, SILTY, FINE TO 10 50 7.8 2 10 2 50 6.5 COARSE GRAINED, TAN, 8" 9" VERY DENSE, MOIST 15 <u>50</u> 5.7 CLAYSTONE, SANDY, GRAY 15 <u>50</u> 10.4 3 8" BROWN, HARD, MOIST 20 <u>50</u> 8.9 2 SANDSTONE, VERY CLAYEY. 20 2 <u>50</u> 8.0 6" FINE TO COARSE GRAINED. 2" BROWN, VERY DENSE, MOIST

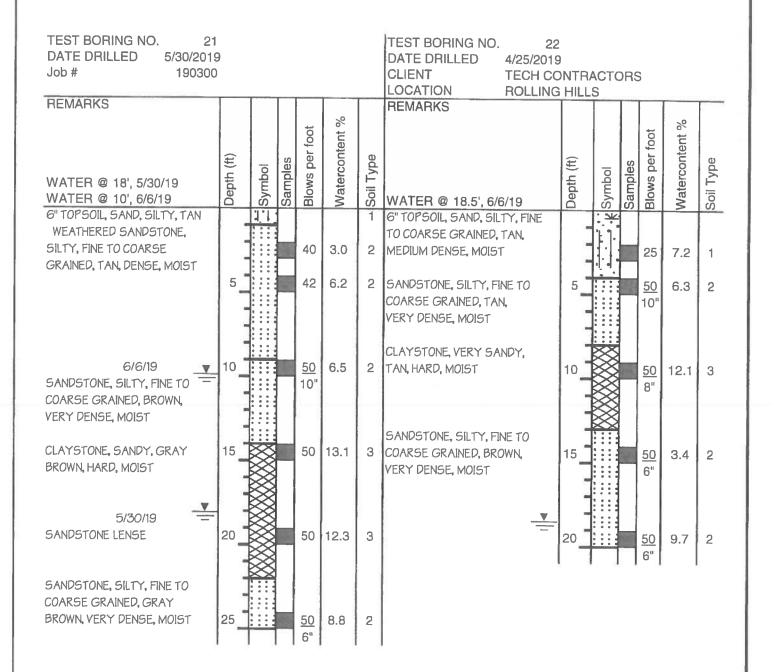


TEST BORING LOG

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JOB NO.: 190300

FIG NO A- 10



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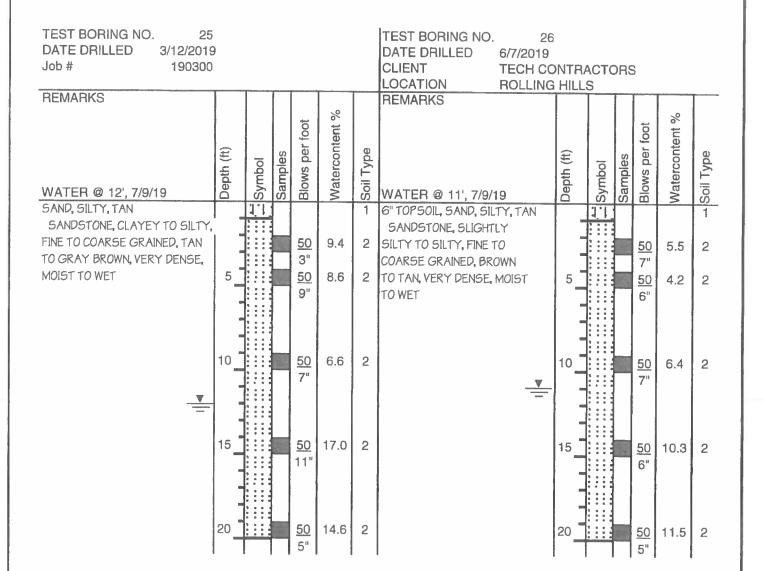


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DATE		CHECKED	4	7/1/19

TEST BORING NO. TEST BORING NO. 23 24 DATE DRILLED 3/12/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS per foot Watercontent Blows per foot Watercontent Soil Type Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol Blows WATER @ 9', 3/12/19 DRY TO 20', 3/12/19 WATER @ 2', 6/6/19 6" TOPSOIL, SAND, SILTY, FINE 6" TOPSOIL, SAND, SILTY, FINE थ TO COARSE GRAINED, TAN. TO COARSE GRAINED, TAN, LOOSE, MOIST 4 3.3 1 DENSE, MOIST 6/6/19 45 11.4 5 7 4.5 1 CLAYSTONE, SANDY, TAN. 5 50 16.8 3 HARD, MOIST 7" 3/12/19 SANDSTONE, SLIGHTLY SILTY. 10 111 <u>50</u> | 12.1 2 SANDSTONE, CLAYEY, FINE = 10 50 21.0 2 FINE TO COARSE GRAINED. 10" TO COARSE GRAINED, BROWN, 11 BROWN, VERY DENSE, MOIST VERY DENSE, WET CLAYSTONE, SANDY, BLUE GRAY, HARD, MOIST 15 50 12.5 3 15 <u>50</u> 8.3 2 8" 20 <u>50</u> 13.3 3 20 2 50 10.4 CLAYSTONE, SANDY, BLUE 9" GRAY, HARD, MOIST <u>50</u> 16.1 3



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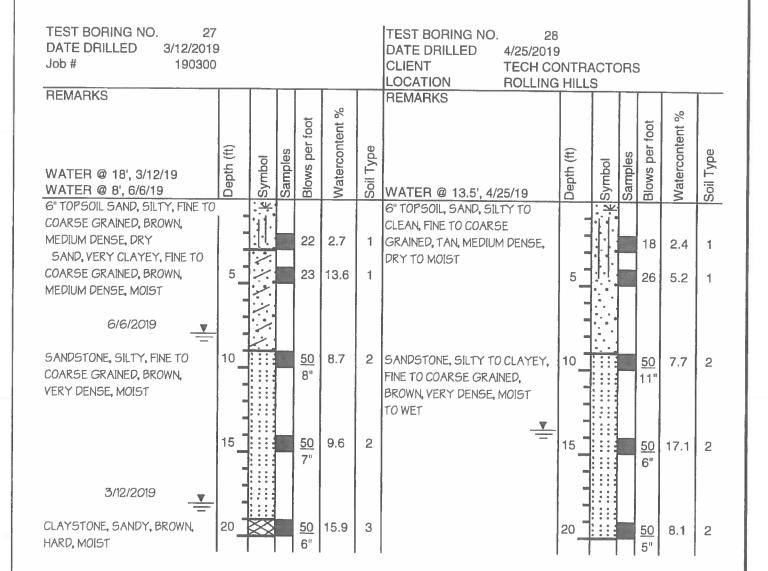




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JOB NO.: 190300

A- 13



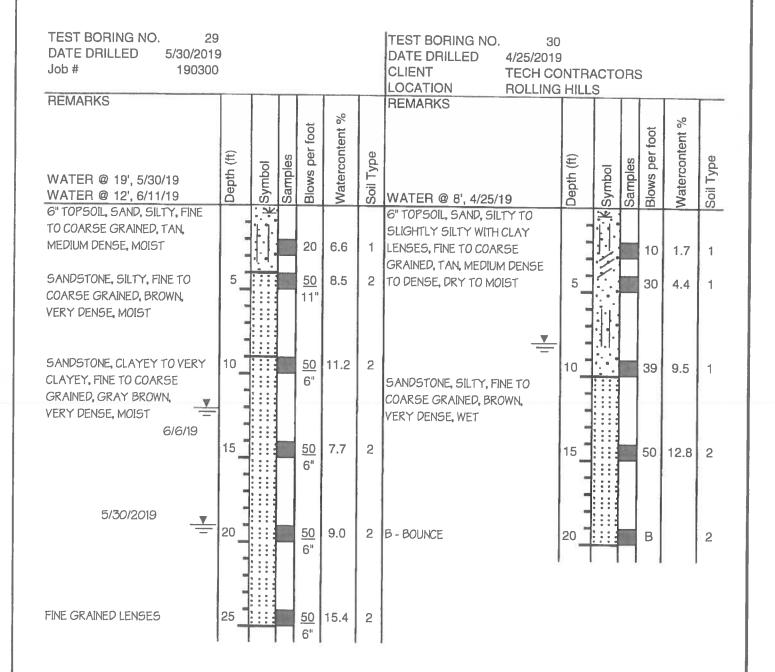


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DATE:	CHECKED:	DATE: 7.12.19

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JOB NO.: 190300

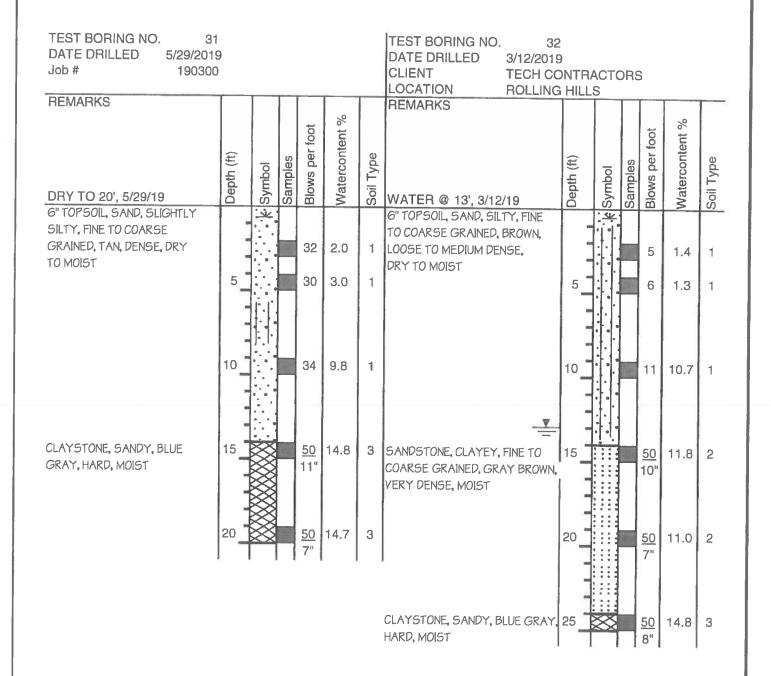
FIG NO.: A- 14



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DATE:	CHECKED	DATE:





	TE	ST BORING LOG	
DRAWN	DATE:	CHECKED:	DATE: 7/12/19

TEST BORING NO. 33 TEST BORING NO. 34 DATE DRILLED 3/12/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % foot Watercontent Watercontent Blows per Type Blows per Œ Ξ Samples Soil Type Symbol Samples Symbol Depth Depth WATER @ 17', 3/12/19 Soil WATER @ 7', 6/6/19 WATER @ 9', 3/12/19 6" TOPSOIL SAND, SILTY, FINE <u>\$</u> 6" TOPSOIL, SAND, SILTY, BROWN 11 1 TO COARSE GRAINED, BROWN, SANDSTONE, SILTY, FINE TO MEDIUM DENSE, DRY TO MOIST 13 2.4 1 COARSE GRAINED, BROWN, 50 6.1 2 VERY DENSE, MOIST 7" 5 15 4.1 1 5 <u>50</u> 8.2 2 10" 6/6/2019 CLAYSTONE, VERY SANDY, WEATHERED TO FORMATIONAL 10 45 17.4 GRAY BROWN, HARD, MOIST 10 50 12.8 3 CLAYSTONE, SANDY, GRAY 9" BROWN, VERY STIFF TO HARD. MOIST 15 50 13.1 SANDSTONE, SILTY, FINE TO 15 50 9.7 2 9" COARSE GRAINED, GRAY 5" 3/12/2019 BROWN, VERY DENSE, MOIST 20 <u>50</u> 18.0 CLAYSTONE, SANDY, BLUE GRAY, 20 <u>50</u> 15.9 3 8" SANDSTONE, SILTY, FINE TO HARD, MOIST COARSE GRAINED, BROWN, VERY DENSE, VERY MOIST <u>50</u> 14.3 2

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TEST	BORING LO	G
DATE:	CHECKED: 2	DATE

JOB NO.: 190300 FIG NO.:

A- 17

TEST BORING NO. 35 TEST BORING NO. 36 DATE DRILLED 3/12/2019 DATE DRILLED 3/11/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS foot Watercontent Watercontent Blows per Type Blows per Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol Soil. DRY TO 20', 3/12/19 WATER @ 13.5', 7/9/19 6" TOPSOIL SAND, SILTY, FINE 44 SAND, SILTY, TAN 1.1 TO COARSE GRAINED, TAN, SANDSTONE, SILTY, FINE TO DENSE, MOIST 48 3.6 1 COARSE GRAINED, TAN, VERY 50 3.1 2 SANDSTONE, SLIGHTLY SILTY DENSE, MOIST 7" TO SILTY, FINE TO COARSE 50 6.0 2 5 50 2 3.7 GRAINED, BROWN, VERY DENSE. 6" MOIST 10 :: 50 2 8.9 10 10.9 <u>50</u> 2 9" 6" 15 50 9.7 2 CLAYSTONE, VERY SANDY, BLUE 15 50 12.2 3 GRAY, HARD, MOIST 6" CLAYSTONE, SANDY, BLUE GRAY, HARD, MOIST 20 <u>50</u> 11.7 3 SANDSTONE, CLAYEY, FINE TO 20 50 13.4 2 6" COARSE GRAINED, GRAY BROWN 10" TO BROWN, VERY DENSE, MOIST TO WET 25 50 16.8 2

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TEST BORING LOG						
DATE	CHECKED:	DATE / a				

JOB NO 190300 FIG NO

A- 18

TEST BORING NO. 37 DATE DRILLED 3/12/2019 Job# 190300

TEST BORING NO. 38 DATE DRILLED 6/7/2019 CLIENT

TECH CONTRACTORS LOCATION BOLLING HILLS

							LOCATION ROLLING	HILL	S				
REMARKS							REMARKS						
DRY TO 20', 3/12/19	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	WATER @ 18', 7/9/19	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
SAND, SILTY, BROWN		1.1				1	6" TOPSOIL, SAND, GRAVELLY,		d ∠ d				
CLAYSTONE, SANDY, BROWN, HARD, MOIST	-			<u>50</u> 11"	11.6	3	SILTY TO SLIGHTLY SILTY, FINE TO COARSE GRAINED, BROWN, LOOSE TO MEDIUM	-	0		4	1.7	1
SANDSTONE, CLAYEY, FINE TO COARSE GRAINED, TAN, VERY DENSE, MOIST	5			<u>50</u> 10"	10.1	2	DENSE, MOIST	5	0	74.0	12	0.7	1
	10_			<u>50</u> 7"	11.3	2		10_			*	7.6	1
	15			<u>50</u> 7"	9.2	2	CLAYSTONE, SANDY, BROWN, MOIST	15			*	19.1	3
	20	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		<u>50</u> 6"	9.3	2	SANDSTONE, SILTY, FINE TO COARSE GRAINED, BROWN, VERY DENSE, MOIST	20_			<u>50</u> 5"	12.1	2
							CLAYSTONE, SANDY, BLUE GRAY, HARD, MOIST	25			В	9.4	3

" - BULK SAMPLE TAKEN

B - BOUNCE



	TEST	BORING LOG	i
DRAWN:	DATE:	CHECKED:	7/12/19

TEST BORING NO. 39 DATE DRILLED 5/29/2019 Job# 190300

TEST BORING NO. 40 DATE DRILLED 3/12/2019 CLIENT TECH CONTRACTORS

				LOCATION ROLLING HILLS						
REMARKS WATER @ 11', 7/9/19	Depth (ft) Symbol	Samples	Watercontent %	Soil Type	REMARKS WATER @ 10', 3/12/19	Depth (ft)	Symbol	Samples Blows per foot	Watercontent %	Soil Type
6" TOPSOIL, SAND, SILTY, FINE TO COARSE GRAINED, TAN, MEDIUM DENSE, MOIST TO WET	*	1	3 10.7	1	6" TOPSOIL, SAND, SILTY, FINE TO COARSE GRAINED, TAN, DENSE TO MEDIUM DENSE, MOIST	-	*	32	4.8	1
	5		1 11.7	1		5_		27	6.2	1
CLAYSTONE, SANDY, GRAY BROWN, HARD, MOIST		5		3	SANDSTONE, SILTY, FINE TO COARSE GRAINED, GRAY BROWN, VERY DENSE, MOIST TO WET	10		<u>50</u> 9"	12.9	2
SANDSTONE, VERY CLAYEY, FINE TO COARSE GRAINED, BROWN, WET	15		14.0	2	CLAYEY LENSES	15		<u>50</u> 8"	12.9	2
CLAYSTONE, SANDY, BROWN, WET	20		18.4	3		20		50 9"	15.2	2

DRAWN:

" - BULK SAMPLE TAKEN



•	EST BORING LOG	
DATE.	CHECKED DATE 2/12/19	

TEST BORING NO. 41 TEST BORING NO. 42 DATE DRILLED 6/7/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS foot Watercontent Watercontent Blows per Blows per € Samples Depth (ft) Soil Type Symbol Samples Symbol Depth Soil WATER @ 17', 6/7/19 WATER @ 14', 6/7/19 6" TOPSOIL, SAND, SILTY, TAM 14 6" TOPSOIL, SAND, CLAYEY, * SANDSTONE, SILTY, FINE FINE TO COARSE GRAINED. TO COARSE GRAINED, BROWN, 50 5.2 2 BROWN, MEDIUM DENSE. 10 9.2 1 VERY DENSE, MOIST 7" MOIST CLAYSTONE, SANDY, BROWN, 5 <u>50</u> 10.3 3 5 29 7.8 1 HARD, MOIST 6" SANDSTONE, CLAYEY TO 10 50 10.1 SANDSTONE, SILTY, FINE TO 10 50 10.0 2 SILTY, FINE TO COARSE 6" COARSE GRAINED, BROWN, 10" GRAINED, BROWN, VERY VERY DENSE, MOIST TO WET DENSE, MOIST TO WET 15 50 11.9 2 15 <u>50</u> 10.2 2 7" 6" <u>_</u> <u>50</u> 15.5 2 CLAYEY LENSES 20 50 9.3 2 6" 25 <u>50</u> 14.0 2

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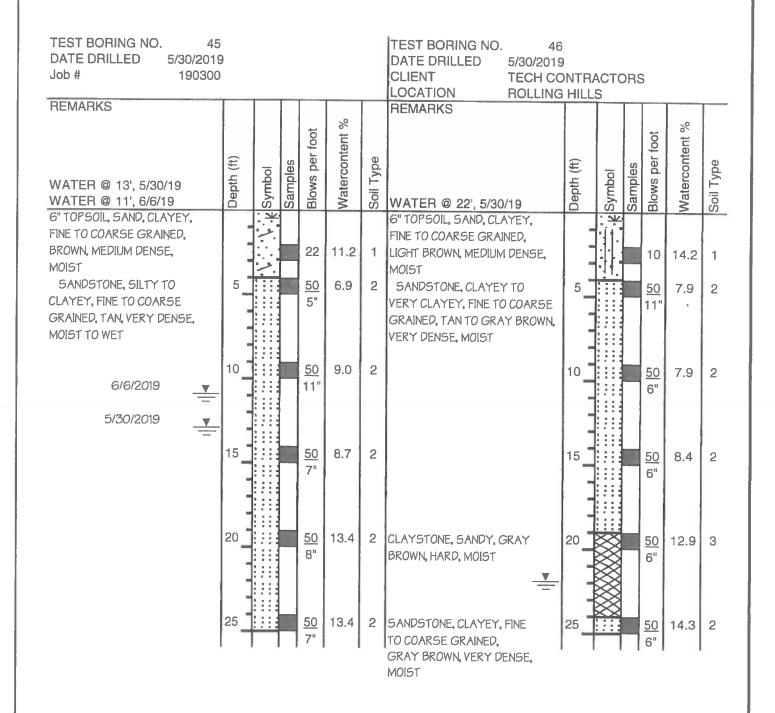
	•	TEST	BORING	LOG	à
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TEST BORING NO. 43 TEST BORING NO. 44 DATE DRILLED 5/30/2019 DATE DRILLED 5/30/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS foot Watercontent Watercontent Blows per Blows per \equiv Samples Soil Type Samples Symbol Symbol Depth (Depth Soil. WATER @ 19', 5/30/19 DRY TO 20', 5/30/19 <u> 4</u> 6" TOPSOIL, SAND, SLIGHTLY 6" TOPSOIL, SAND, SILTY, TAN 11 SILTY, FINE TO COARSE WEATHERED SANDSTONE. GRAINED, TAN, MEDIUM 14 3.4 1 SILTY, FINE TO COARSE 32 3.0 2 DENSE, MOIST GRAINED, TAN, DENSE, MOIST 32 WEATHERED SANDSTONE, 8.3 2 5 : : 2 35 10.3 SILTY, FINE TO COARSE CLAYEY LENSES GRAINED, BROWN, DENSE. MOIST 10 CLAYSTONE, SANDY, GRAY 50 14.1 SANDSTONE, SILTY, FINE TO 10 2 50 9.8 BROWN, HARD, MOIST COARSE GRAINED, BROWN. 11" VERY DENSE, MOIST 15 50 12.5 3 15 50 2 8.8 8" 8" SANDSTONE, CLAYEY, FINE 20 12.2 50 2 CLAYEY LENSES 20 50 2 10.6 TO COARSE GRAINED, TAN, 5" VERY DENSE, MOIST CLAYSTONE, SANDY, BLUE GRAY, 25 <u>50</u> 16.8 3 HARD, MOIST

DRAWN.



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TEST BORING LOG					
	DATE	CHECKED:	7 PATE/19		

TEST BORING NO. 47 TEST BORING NO. 48 DATE DRILLED 5/30/2019 DATE DRILLED 6/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION ROLLING HILLS REMARKS REMARKS % per foot Watercontent Watercontent Blows per Depth (ft) Soil Type Samples Depth (ft) Soil Type Samples Symbol Blows Symbol DRY TO 20', 6/7/19 DRY TO 20', 5/30/19 CAVED TO 14', 7/9/19, DRY 6" TOPSOIL, SAND, SILTY, TAN 14 6" TOPSOIL, SAND, SILTY, TAN 11 SANDSTONE, SILTY, FINE TO SANDSTONE, CLAYEY TO ::: COARSE GRAINED, BROWN, 50 9.0 SILTY, FINE TO COARSE 32 8.9 2 VERY DENSE, MOIST 9" GRAINED, BROWN, VERY DENSE. 5 <u>50</u> 8.7 MOIST 27 7.8 2 10" 10 50 9.4 CLAYSTONE, SANDY, BROWN. 10 50 9.6 3 HARD, MOIST 10" 9" :: 15 <u>50</u> 8.8 2 SANDSTONE, SILTY, FINE TO 15 50 5.4 2 10" COARSE GRAINED, TAN, 8" VERY DENSE, MOIST CLAYSTONE, VERY SANDY, <u>50</u> 8.5 2 GRAY BROWN, HARD, MOIST 20 <u>50</u> 9.4 3



TEST BORING LOG				
DRAWN;	DATE:	CHECKED:	DATE: 7/12/19	

TEST BORING NO. 49 TEST BORING NO. DATE DRILLED 6/7/2019 DATE DRILLED Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Watercontent % Blows per foot Watercontent Blows per Soil Type Depth (ft) Samples Soil Type Depth (ft) Samples Symbol Symbol WATER @ 12', 6/7/19 ** 6" TOPSOIL, SAND, SLIGHTLY SILTY TO SILTY, FINE TO COARSE GRAINED, TAN, 15 5.2 1 MEDIUM DENSE TO DENSE, MOIST 5 20 10.3 1 5 10 33 10.1 1 10 SANDSTONE, SILTY, FINE TO 15 50 11.9 2 15 COARSE GRAINED, TAN, VERY 9" DENSE, MOIST TO WET 20 50 15.5 2 20 6" 25 <u>50</u> 15.5 2 25

DRAWN:



TEST BORING LOG				
DATE:	CHECKED:	7:/12/19		

JOB NO.: 190300 FIG NO.:

A- 25

APPENDIX B: Soil	Survey Descriptions	

El Paso County Area, Colorado

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Columbine

Setting

Landform: Flood plains, fan terraces, fans

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam
C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to

very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Gravelly Foothill (R049BY214CO)

Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: Landform: Swales Hydric soil rating: Yes

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 16, Sep 10, 2018

El Paso County Area, Colorado

83—Stapleton sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 369z Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Stapleton and similar soils: 80 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Stapleton

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose

Typical profile

A - 0 to 11 inches: sandy loam

Bw - 11 to 17 inches: gravelly sandy loam C - 17 to 60 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High

(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: Gravelly Foothill (R049BY214CO)

Hydric soil rating: No

Minor Components

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Fluvaquentic haplaquolls

Percent of map unit: Landform: Swales Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 16, Sep 10, 2018