# FINAL DRAINAGE REPORT FOR ZINDORF — MCDANIEL'S SUBDIVISION

PCD FILE NO. MS-22-006

#### PREPARED BY

Richard Gallegos, P.E. RESPEC 121 S. Tejon St., Suite 1110 Colorado Springs, CO 80903

#### PREPARED FOR

Greg Zindorf Z Investments LLC PO Box 50005 Colorado Springs, CO

July 2023





#### **ENGINEER'S STATEMENT**

This report and plan for the drainage design of Zindorf - McDaniels Subdivision, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I understand that El Paso County does not, and will not, assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richard Gallegos, P.E.

Date

Registered Professional Engineer State of Colorado No. 36247



## **DEVELOPER'S STATEMENT**

Greg Zindorf hereby certifies that the drainage facilities for the Zindorf - McDaniels Subdivision shall be constructed according to the design presented in this report. I understand that EI Paso County does not, and will not, assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to El Paso County; and cannot, on behalf of the Zindorf - McDaniels Road guarantee that final drainage design review will absolve Greg Zindorf and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

GREG ZINDORF	12-20-2022							
Authorized Signature  Greg Zindorf  Printed Name	Date							
Owner Title  FI DACO COUNTY CTATEMENT	_ Address:	PO Box 50005 Colorado Springs, CO						

## EL PASU GUUNI I STATEMENT

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

	_	
Joshua Palmer, P.E.	Date	

County Engineer/ECM Administrator

PCD FILE NO. MS-22-006



# **TABLE OF CONTENTS**

1.0	PURPOSE	1
2.0	SOIL CONDITIONS	1
3.0	DRAINAGE CRITERIA	1
4.0	EXISTING DRAINAGE CONDITIONS	2
5.0	DEVELOPED DRAINAGE CONDITIONS	3
6.0	WATER QUALITY	6
	FLOODPLAIN STATEMENT	
9.01	LOODPLAIN STATEMENT	6
	DRAINAGE BASIN FEES	
11.0	CONSTRUCTION COST OPINION	7
12.0	CONCLUSIONS	7
13.0	REFERENCES	3

# **BACK POCKET**

APPENDIX A - MAPS

**APPENDIX B - CALCULATIONS** 

APPENDIX C - ELLICOTT CONSOLIDATED FLOODPLAIN ANALYSIS

**APPENDIX D - DESIGN CHARTS** 

**BACK POCKET - DRAINAGE MAPS** 



#### 1.0 PURPOSE

This drainage report is for the design of Zindorf – McDaniels Subdivision (McDaniels Tract). The site is located at 22755 McDaniels Road, Calhan CO in eastern El Paso County. See Vicinity Map in the Appendix below for reference. It is further described as the Northeast One-Quarter of the Northeast One-Quarter of Section 11, Township 14 South, Range 63 West of the 6<sup>th</sup> P.M.

This site is located in the Ellicott Consolidation – CHBS1200 Drainage Basin. Work will include subdividing the 39.7-acre site into four residential lots. An existing home will remain, and the driveway will be reconstructed. On the other three lots, home pads and gravel driveways will be constructed.

#### 2.0 SOIL CONDITIONS

According to the El Paso County Area Soil Survey, the soil on the site is classified as follows:

SOIL#	SOIL TYPE	HYDROLOGIC CLASSIFICATION
19	Columbine Gravelly Sandy Loam	Α
28	Ellicot Loamy Coarse Sand	Α
95	Truckton Loamy Sand	Α

The Columbine soil can be described as having a very high permeability, very low surface runoff, and slight hazard of erosion. The Ellicot soil also can be described as very low surface runoff and slight erosion hazard. The Truckton soil includes a moderate hazard of erosion and low water surface runoff. The soil classification used for this study is 'A'. See Soils Map below in the Appendix for reference.

#### 3.0 DRAINAGE CRITERIA

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual*. The Rational Method for computation of runoff was used.

Q = cia Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration required for the runoff

to become established

a = drainage basin size in acres

The storm recurrence intervals used for this study were the 5-year storm and the 100-year storm. ManningSolver Version 1.019 was used in this analysis to calculate the Manning's normal depth within the proposed swale.



#### 4.0 EXISTING DRAINAGE CONDITIONS

The overall site consists of 39.7 acres, of this area approximately 1.03 acres is developed as a single family home, yard, and gravel driveway accessing McDaniel's Road. The areas of the site not covered by gravel road or the residential home are covered with short grass pastures. These undeveloped areas include slopes that range from 0.5% to 2.4%. The overall existing site is approximately 2.1% impervious. See Existing Drainage Map in Appendix for reference.

Flows from Sub-basins EX1 through EX3 and OS1 through OS3 are tributary to the Ellicott Consolidated Drainage Basin (CHBS1200).

Sub-basin OS1 contains 8.67 acres and drains southeast into Subbasin EX2. It produces flows of 1.1 cfs for the 5-year storm and 8.2 cfs for the 100-year storm. These flows sheetflow and continue towards the FEMA 100-year floodway in the middle of the site.

Sub-basin OS2 contains 0.49 acres and drain southwest into the Haegler Ranch floodway that runs through the middle of the site. It produces flows of 0.1 cfs for the 5-year storm and 1.0 cfs for the 100-year storm. These flows sheetflow to the southwest.

Sub-basin OS3 contains 1.02 acres and drains the east along McDaniels Road. It contains half of McDaniels Road that drains south into the ditch. It produces flows of 0.5 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. All flows north of the site are directed into a drainage ditch that flows into a culvert under McDaniels Road. These flows bypass the development occurring on the site in a ditch along North Log Road. Flows overtopping the intersection of McDaniels Road and North Log Road sheetflow to the east.

Sub-basin EX1 contains 1.06 acres and drains due southwest. It produces flows of 0.2 cubic feet per second (cfs) for the 5-year storm and 1.4 cfs for the 100-year storm. These flows are directed to the southerly direction.

Sub-basin EX2 contains 14.59 acres and drains southeast into the Haeglar Ranch floodway in the middle of the site. It produces flows of 1.8 cfs for the 5-year storm and 14.0 cfs for the 100-year storm. These flows sheetflow to the southeast.

Sub-basin EX3 contains 22.89 acres and sheetflows to the southwest into the Haegler Ranch floodway in the middle of the site. It produces flows of 3.5 cfs for the 5-year storm and 22.8 cfs for the 100-year storm. These flows will combine with flows from Sub-basin EX2, Sub-basin EX3, Sub-basin OS1, Sub-basin OS2, and Sub-basin OS3 to produce total flows of 7.1 cfs for the 5-year storm and 48.0 cfs for the 100-year storm at Design Point 1. FEMA Zone 'A' 100-year floodplain flows entering the site are approximately 1,900 cfs.

The total flow leaving the site at Design Point 1 (DP1) is 7.1 cfs for the 5-year storm and 48.0 cfs for the 100-year storm. The estimated runoff amounts produced for the project under Existing Conditions are shown in Table 1 below.

Page 2



TABI	LE 1 – EXISTING CONDITIONS	
Sub-basin	Q <sub>5</sub> (CFS)	Q <sub>100</sub> (CFS)
EX1	0.2	1.4
EX2	1.8	14.0
EX3	3.5	22.8
0\$1	1.1	8.2
0\$2	0.1	1.0
0\$3	0.5	1.5
DP1 (EX2 + EX3 + OS1 + OS2 + OS3)	7.1	48.0

#### 5.0 ELLICOTT CONSOLIDATED FLOODPLAIN ANALYSIS

FEMA has previously studied the Ellicott Consolidated floodway with limited results presented on the Flood Insurance Rate Map and Flood Insurance Study. The available information from FEMA is presented in the appendix of this report. The peak 100-year flow rate of 7,019 at the confluence of the East Tributary is the only flow value provided in the study, and is located approximately 1.6 miles downstream of our site.

The information provided in the FEMA study does not provide sufficient detail to determine the channel's stability. A more detailed analysis hydraulic analysis was completed utilizing several sources of information, including

- Colorado LiDAR data from the Colorado Hazard Mapping and Risk MAP Portal
- FEMA GIS data
- Hydrologic and hydraulic data from the "Haegler Ranch Basin Drainage Basin Planning Study,"
   by URS, May 2009

A HEC-RAS version 6.2 hydraulic model was prepared utilizing the same cross section locations as the previous FEMA study, except for modifications made at Log Road at the downstream end of the project. Cross sections in this vicinity were modified to cross the channel and better consider the roadway alignment and profile. A total of eight cross sections were used to model 2609 linear feet of channel, including an existing 48" CMP under Log Road. Peak flow rates of 570 cfs for the 5-year and 3200 cfs for the 100-year storms were used and are based upon the downstream most portion of the Haegler Ranch Basing Drainage Planning Study (DBPS) located at McDaniels Road. A total tributary area of 16.6 square miles drains to McDaniels Road. Mannings coefficients of 0.074 for light brush and 0.065 for native grasses were used and are the same values recommended in the DBPS. Photographs from 2023 are also included in the appendix of this report to help support the assumptions used.

The project site is located between HEC-RAS river cross section station s 3609 to 1814, see Floodplain Evaluation Map in the appendix. The additional cross sections located downstream of the site were used to model the backwater effects resulting from the Log Road crossing. Within the site, three key items were reviewed to help determine that the natural channel is scour stable:





- 1. Vegetative cover at the site, including shrubs, native grasses and trees appear well established indicating that the channel is stable.
- 2. The computed flow velocities through the project site range between 2.04 fps and 5.91 fps for the 100-year flow rate. The publication by Craig Fischenich with the USAE Research and Development Center, "Stability Thresholds for Stream Restoration Materials," dated May 2001, indicates that for long native grasses the maximum permissible velocity of a channel is 7.0 fps.
- 3. The Froude number for the 100-year storm ranges from 0.17 to .74 indicating a subcritical flow regime. Any number less than 1.0 (critical depth), and, ideally less than 0.80, is expected to be stable.

Based upon the floodplain analysis completed as part of this study, no additional channel stabilization measure are needed as a result of this project. The channel in it's natural condition is considered scour stable.

## **6.0 DEVELOPED DRAINAGE CONDITIONS**

Although the overall site consists of 39.7 acre only approximately 1.37 acres will be disturbed. The site will be subdivided into four separate lots with three house and gravel driveway being constructed on the four lots. The existing house will remain and the gravel driveway will be reconstructed. See Proposed Conditions Map below in Appendix for reference.

The overall drainage pattern will remain the same as existing conditions with developed flows directed to the same locations as described in the Existing Conditions Section. Proposed site imperviousness is 2.8%, versus 2.1% in the existing conditions.

Sub-basin OS1 contains 8.67 acres and drains southeast into Subbasin PP2. It produces flows of 1.1 cfs for the 5-year storm and 8.2 cfs for the 100-year storm. These flows continue towards the FEMA 100-year floodway in the middle of the site.

Sub-basin OS2 contains 0.49 acres and drain southwest into the Haegler Ranch floodway that runs through the middle of the site. It produces flows of 0.1 cfs for the 5-year storm and 1.0 cfs for the 100-year storm. These flows sheetflow to the southwest and will combine with flows from Design Point 1, described above.

Sub-basin OS3 contains 1.02 acres and drains the east along McDaniels Road. It contains half of McDaniels Road that drains south into the ditch. It produces flows of 0.5 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. All flows north of the site are directed into a drainage ditch that flows into a culvert under McDaniels Road. These flows bypass the development occurring on the site in a ditch along North Log Road. Flows overtopping the intersection of McDaniels Road and North Log Road sheetflow to the east.

Page 4

Sub-basin PP1 contains 1.06 acres and drains due southwest. It produces flows of 0.2 cfs for the 5-year storm and 1.4 cfs for the 100-year storm. These flows sheetflow in a southerly direction.



Sub-basin PP2 contains 14.59 acres and drains southeast into the Haeglar Ranch floodway in the middle of the site. It produces flows of 1.8 cfs for the 5-year storm and 14.0 cfs for the 100-year storm. These flows sheetflow to the southeast.

Sub-basin PP3 contains 22.89 acres and sheetflows to the southwest into the Haegler Ranch floodway in the middle of the site. It produces flows of 3.9 cfs for the 5-year storm and 22.9 cfs for the 100-year storm. These flows will combine with flows from Sub-basin PP2, Sub-basin PP3, Sub-basin OS1, Sub-basin OS2, and Sub-basin OS3 to produce total flows of 7.5 cfs for the 5-year storm and 48.0 cfs for the 100-year storm at Design Point 1. The majority of runoff will sheet flow and have similar time of concentrations as seen in the existing conditions. The 100-year peak rate in the proposed conditions is the same as that of the existing, and the 5-year increases 0.4 cfs in the proposed conditions, existing 5-year flow rate of 7.1 cfs versus the proposed flow rate of 7.5 cfs. Because the peak flow rate for the 100-year storm event remains unchanged, and only a slight increase in the 5-year flow rate is seen, mitigation is not required. All flows north of the site are directed into a drainage ditch that flows into a culvert under McDaniels Road. These flows bypass the development occurring on the site in a ditch along North Log Road. Flows overtopping the intersection of McDaniels Road and North Log Road sheetflow to the east.

Flows from Design Point 1 will sheetflow into Ellicott Consolidated channel and continue downstream toward an existing public 48" CMP under Log Road. The flows from the floodplain do overtop Log Road and continue downstream to the southeast. The computed flows are either generated from this site, or sheet flow through the site from adjacent parcels, but do not include the flows within the floodplain from the upstream watershed.

The estimated runoff amounts produced for the project for Developed Conditions are shown in Table 2 below.

	TABLE 2 - DEVELOPED CONDITIONS	
Sub-basin	Q <sub>5</sub> (CFS)	Q <sub>100</sub> (CFS)
PP1	0.2	1.4
PP2	1.8	14.0
PP3	3.9	22.9
0\$1	1.1	8.2
0\$2	0.1	1.0
0\$3	0.5	1.5
DP1 (PP2 + PP3 +OS1 + OS2 + OS3)	7.5	48.0



#### **6.0 WATER QUALITY**

The total disturbance for this development will be 1.37 acres. According to the El Paso County Engineering Criteria Manual (ECM), "The following types of sites and associated land disturbances are excluded from the requirements of this Section 1.7". Furthermore, in El Paso County ECM Appendix I.7, 1.B, a "Large Lot Singe Family Site" is excluded from the requirements defined in Section 1.7. Since this site will be divided in single-family residential lots greater than 2.5 acres in size per dwelling and having a total lot imperviousness of less than 10 percent, the site can be excluded from water quality control measure requirements.

## 7.0 EROSION CONTROL PLAN

The site construction consists of four single family residential lots, which includes four houses and gravel driveways that all occupy greater than 2.5 acres in size per dwelling and a total lot imperviousness of less than 10 percent. With single family residential lots greater than 2.5 acres in size and less than 10 percent imperviousness, the site is excluded from stormwater quality control measures and ESQCP requirements. Although exclusions apply, each lot is still responsible for providing appropriate temporary control measures when each site is developed, which may include items such as silt fence, vehicle tracking control surfaces, etc.

#### 8.0 FLOODPLAIN STATEMENT

Portions of the site are within the designated FEMA 100-year floodplain and designated FEMA 100-year floodway as designated on Map No. 08041C0810G and Map No. 08041C0807G, both dated December 7<sup>th</sup>, 2018. A large portion of the site consists of a FEMA Flood Zone 'AE'. A small portion on the north end of the site is considered a FEMA Flood Zone 'A'.

All structures will be a minimum of 150' away from the FEMA delineated Zone AE floodplains and homes shall be constructed in accordance with El Paso County's Chapter 12 for to either elevate any residence 1' above the 100-year base flood elevation of 6090 (NAVD 88 Datum), or floodproof the structure for any areas below the floodplain elevation. There is currently not an approved drainage basin planning study for the Ellicott Consolidated (CHBS1200) Drainage Basin, and no County identified improvements were identified for this segment of stream. Based upon field observations, significant vegetation consisting of rangeland grasses, shrubs and trees exist in the area meaning the floodplain area is scour stable. No baseflow exists within the channel. For these reasons, drainageway improvements and channel stabilization requirements have not been identified for the drainageway shown in the Drainage Maps below. No improvements are proposed for this drainageway as a result, an no additional hydraulic analysis beyond what FEMA has provided is needed for this Final Drainage Report.



Indicate what flows were used in the analysis (FEMA lists 7019 cfs but HEC-RAS shows 3200 cfs). Indicate what velocity, FR # and how these all meet channel requirements from DCM.



#### 9.0 DRAINAGE BASIN FEES

The proposed development is located within the Ellicott Consolidated Drainage Basin.

#### 2023 Ellicott Consolidated Drainage Fees

There are no drainage fees associated with the Ellicott Consolidated Drainage Basin.

#### 2023 Ellicott Consolidated Bridge Fees

There are no bridge fees associated with the Ellicott Consolidated Drainage Basin.

#### 10.0 CONSTRUCTION COST OPINION

There are no proposed drainage structures for this project, therefore, no engineer's estimate of probable costs are required for this drainage report.

#### 11.0 CONCLUSIONS

For this 39.7-acre site, the site will be divided into four separate lots. The existing gravel driveway will be removed and reconstructed, while the 1850 sf house will remain. Three additional home pads and gravel driveways will be constructed on the other lots. The total estimated new disturbance area of the site will be 1.37 acres, which will allow for new driveways for all four lots, and home construction on three of the lots. The fourth lot currently has a single family residence, which will remain and only the gravel driveway will be reconfigured. Construction will occur within drainage sub-basin PP3. The development increases total routed flows exiting the site at Design Point 1 (DP1) from 7.1 cfs to 7.5 cfs for the 5-year storm, while the 100-year storm flow remains unchanged at 48.0 cfs. This is a 5.6% increase for the 5-year storm. These increases do not warrant the need for detention, nor water quality as each lot is also greater than five acres in size. All developed flows will continue to flow along existing drainage patterns. All areas disturbed by construction will be repaired, and erosion control measures will be installed during construction of the proposed site. The proposed project will not, with respect to stormwater runoff, negatively impact the adjacent properties and downstream properties. Because there is no increase to the 100-year peak flow rates from the site and only a minimal increase in the 5-year event, the proposed development will not adversely impact adjacent and downstream properties.



# **12.0 REFERENCES**

Haegler Ranch Drainage Basin Planning Study, URS Corporation, Dated May 2009.

LiDAR Data, Colorado Hazard Mapping and Risk MAP Portal, obtained 2023

Municipal Code Corporation (2018). Engineering Criteria Manual of El Paso County, Colorado (ECM)

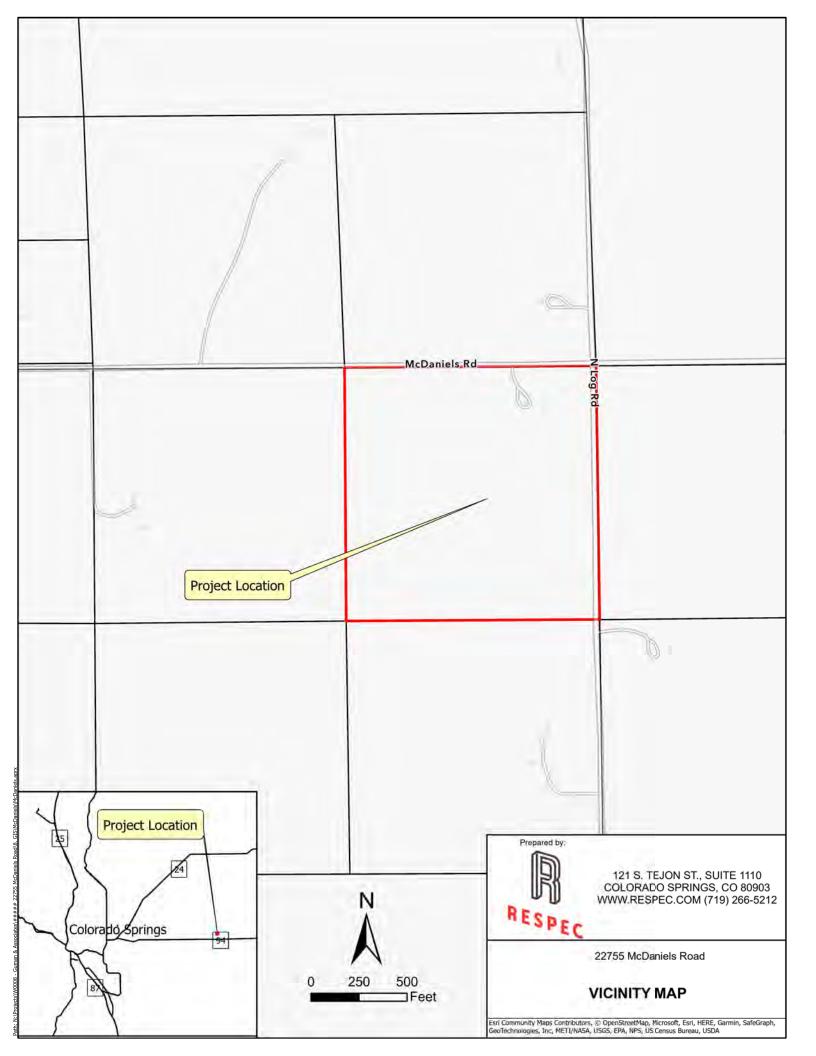
Municipal Code Corporation (2018). Drainage Criteria Manual of El Paso County, Colorado (DPM)

**USDA, NRCS.** Soil Survey of El Paso County Area, Colorado.



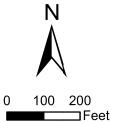
# **APPENDIX A**

**MAPS** 





Map Unit Symbol	Map Unit Name	Rating
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	А
28	Ellicot loamy coarse sand, 0 to 5 percent slopes	А
95	Truckton loamy sand, 1 to 9 percent slopes	А

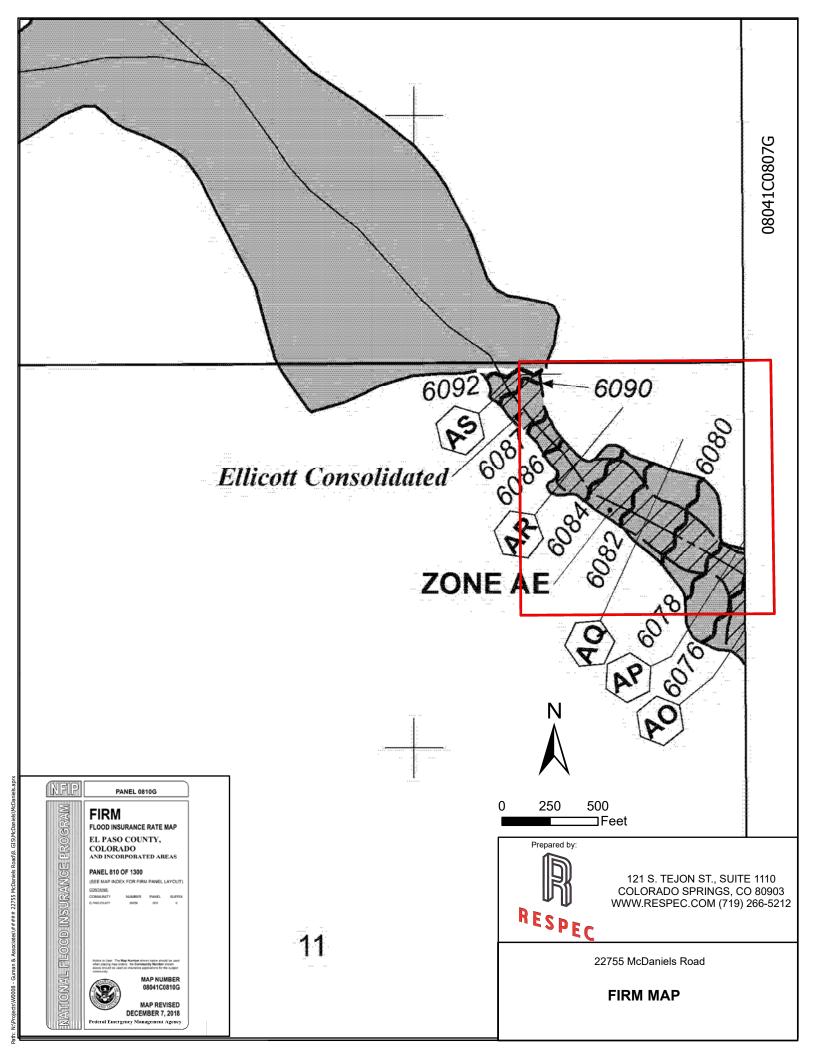


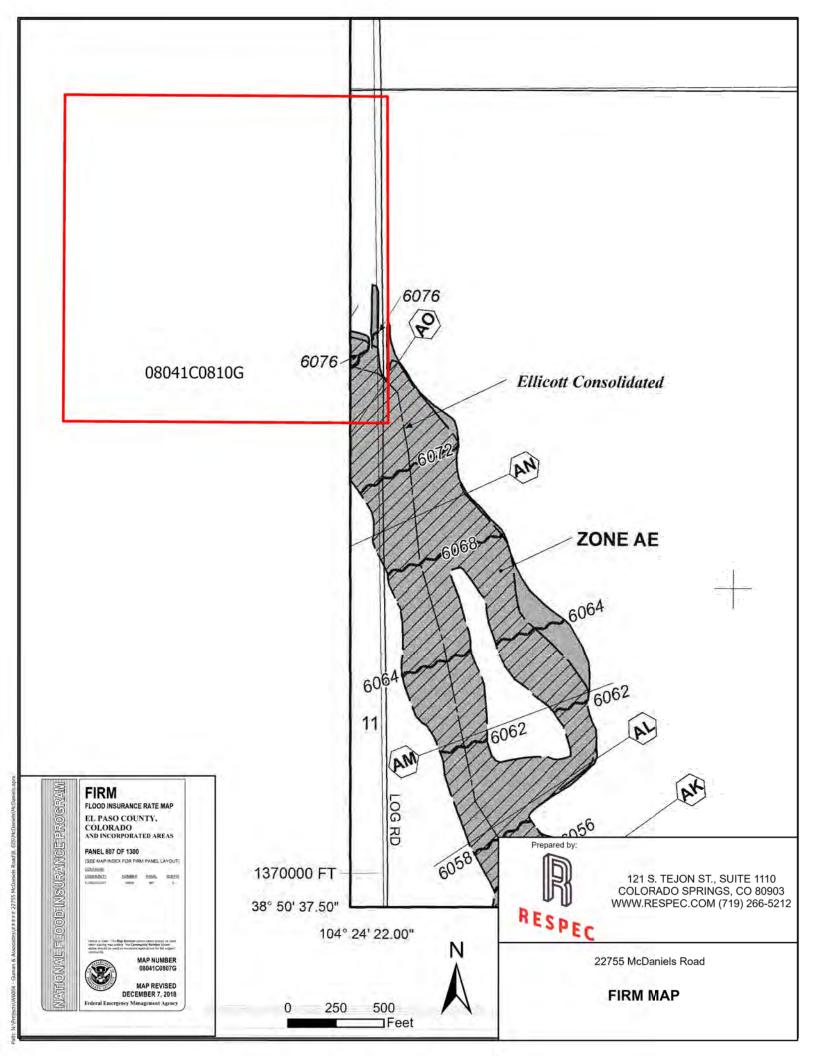


22755 McDaniels Road

SOILS MAP

Esri Community Maps Contributus, D. OpenStreetMap, Microedft, Eiri, HERE, Garmin, SafeGraph, GeoTechnologi METI/NASA, USGS, EPA, NPS, US Census Burenu, USDA, Maxar







# **APPENDIX B**

**CALCULATIONS** 

McDaniels S	Subdivision								
C FACTOR (	CALCULATION	ON SHEET							
<b>EXISTING C</b>									
RUNOFF CC									
TYPE A/B S	OILS								
LAND USE		Imperv %	5 YR	100 YR					
LINDEV		0	0.00	0.25					
UNDEV GRAVEL RC	NA D	0 80	0.08	0.35 0.7					
ASPHALT R		100		0.7					
ROOFS	OAD	90		0.90					
10013		90	0.73	0.01					
				EXISTING C	ONDITIONS				
	TOTAL	SURFACI	E CONDITIO	N AREAS		CALCUL	ATED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100	% IMPE	RVIOUS
DESIG.	(acre)		ROAD	ROAD		YR	YR		
EX1	1.06	1.06	0.00	0.00	0.00	0.08	0.35		0.00
EX2	14.59	14.59		0.00	0.00	0.08	0.35		0.00
EX3	22.86	21.83	0.98	0.00	0.05	0.10	0.37		3.63
OS1	8.67	8.67	0.00	0.00	0.00	0.08	0.35		0.00
OS2	0.49	0.49		0.00	0.00	0.08	0.35		0.00
OS3	1.02	0.60	0.42	0.00	0.00	0.29	0.49		32.94
Site Percent	Impervious	2.11							

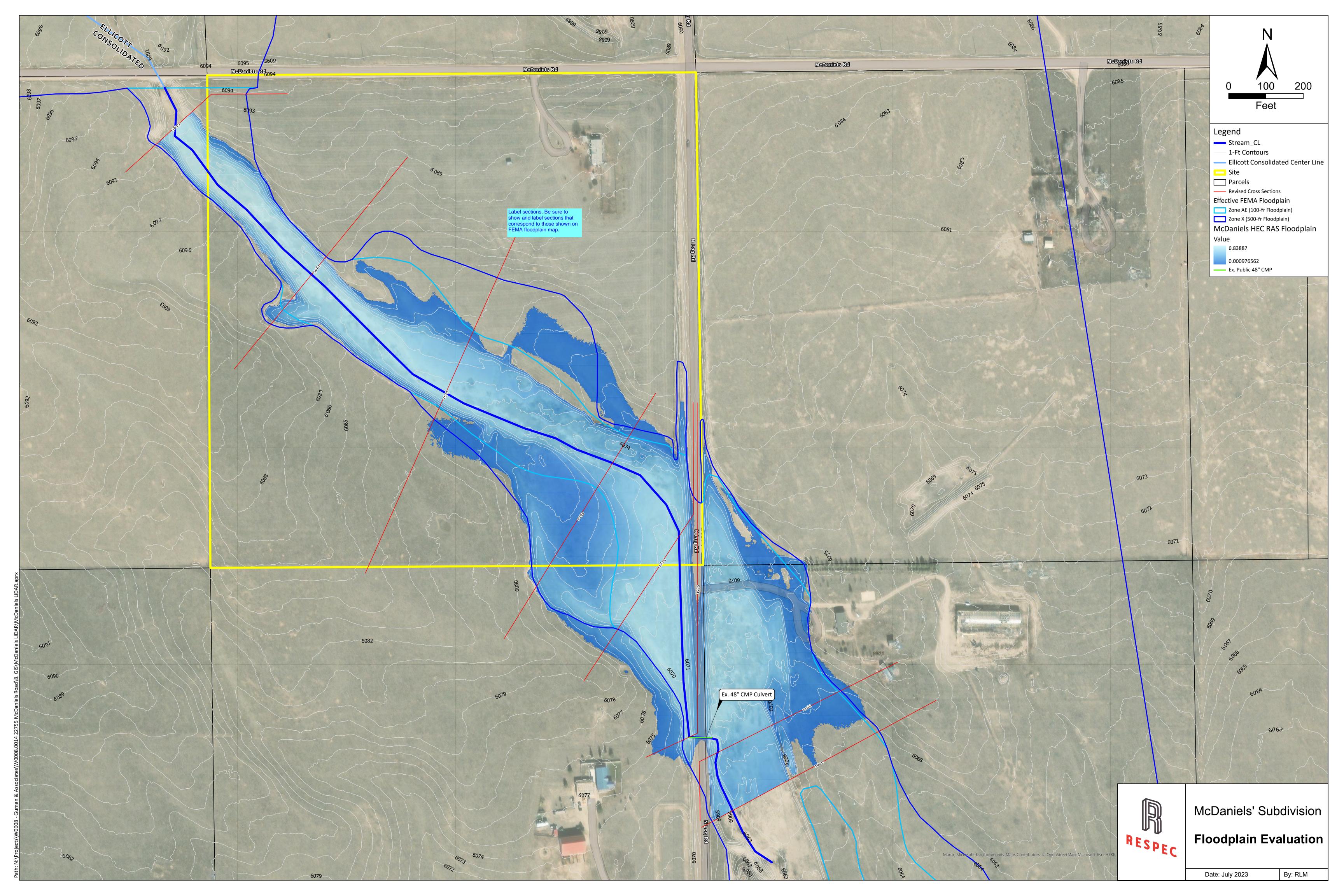
DEVELOPE	D CONDITIO	NS							
RUNOFF CO	DEFICIENT								
TYPE A/B SOILS									
LAND USE		Imperv %	5 YR	100 YR					
UNDEV		0		0.35					
GRAVEL RC		80		0.7					
ASPHALT R	OAD	100		0.96					
ROOFS		90	0.73	0.81					
				Developed	Conditions				
	TOTAL		E CONDITIO			CALCUL	ATED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100	% IMPE	RVIOUS
DESIG.	(acre)		ROAD	ROAD		YR	YR		
PP1	1.06	1.06			0.00		0.35		0.00
PP2	14.59	14.59			0.00	0.08	0.35		0.00
PP3	22.86		4 4	0 0	2				4.89
1 1 3	22.80	21.49	1.16	0.00	0.21	0.11	0.37		
Total	38.51	21.49 37.14					0.37 MPERVIOUS	NESS	2.90
								IESS	
			1.16	0.00		TOTAL SITE		NESS	
Total	38.51	37.14	0.00	0.00	0.21	TOTAL SITE	MPERVIOUS	NESS	2.90
Total OS1	38.51 8.67	37.14 8.67	0.00 0.00	0.00	0.21	0.08 0.08	MPERVIOUS 0.35	NESS	2.90 0.00
Total OS1 OS2	38.51 8.67 0.49	37.14 8.67 0.49	0.00 0.00	0.00 0.00 0.00	0.21 0.00 0.00	0.08 0.08	0.35 0.35	NESS	0.00 0.00

McDaniels Subdivision																		
PROJ.W008																		
DRAINAGE CALCULAT	TION SHEE	Τ																
file:McDaniels Rd.xlsx																		
06/14/22																		
			0.100	05.1/ 4	0100111		Initial Tci			Travel Ti					1400		0.400	
AREA	AREA	C5		C5 X A	C100 X A	1 (61)	Slope	ti	1 (6)	Slope	V	Tt	TC	15	I100	Q5		AREA
DESIG.	(acre)	(5 yr)	(100 yr)			L (ft)	(%)	(min)	L (ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)	DESIG.
EXISTING CONDITIONS																		
EX1	1.06	0.08	0.35			300	1.70	27.73	350	1.70	0.90	6.48	34.21	2.14	3.74	0.2	1.4	EX1
EX2	14.59	0.08	0.35	1.17	5.11	300	2.00	26.28	1400	1.40	0.80	29.17	55.45	1.57	2.75	1.8	14.0	EX2
EX3	22.86	0.10	0.37	2.29	8.46	300	2.00	25.77	1500	1.40	0.80	31.25	57.02	1.54	2.69	3.5	22.8	EX3
001	0.67	0.00	0.05	0.60	2.02	200	4.00	22.04	4000	1 10	0.70	22.04	EC OF	4 5 5	0.70	4 4	0.0	004
OS1 OS2	8.67 0.49	0.08	0.35 0.35	0.69 0.04	3.03 0.17	300 115	1.00 2.40	33.04 15.32	1000 115	1.10 2.40	0.70 1.20	23.81 1.60	56.85 16.92	1.55 3.18	2.70 5.55	1.1 0.1	8.2 1.0	OS1 OS2
OS2 OS3	1.02	0.08	0.35		0.17	30	0.50	5.00	0	0.00	0.00	0.00	5.00	5.19		1.5	4.5	OS2 OS3
DP1 (EX2 + EX3 +	1.02	0.23	0.43	0.30	0.50	30	0.50	3.00	0	0.00	0.00	0.00	3.00	5.19	9.00	1.5	4.5	DP1 (EX2 + EX3 +
OS1 + OS2 + OS3)	47.63	0.09	0.36	4.48	17.27	300	1.00	33.04	2600	1.10	5.00	8.67	54.47	1.59	2.78	7.1	48.0	OS1 + OS2 + OS3)
DEVELOPED CONDITIONS																		
PP1	1.06	0.08	0.35			300	1.70	27.73	350	1.70	0.90	6.48	34.21	2.14		0.2	1.4	PP1
PP2	14.59	0.08	0.35	1.17	5.11	300	2.00	26.28	1400	1.40	0.80	29.17	55.45	1.57	2.75	1.8	14.0	PP2
PP3	22.86	0.11	0.37	2.51	8.46	300	2.00	25.51	1500	1.40	0.80	31.25	56.76	1.55	2.70	3.9	22.9	PP3
OS1	8.67	0.08	0.35	0.69	3.03	300	1.00	33.04	1000	1.10	0.70	23.81	56.85	1.55	2.70	1.1	8.2	OS1
OS2	0.49	0.08	0.35	0.09	0.17	115	2.40	15.32	115	2.40	1.20	1.60	16.92	3.18	5.55	0.1	1.0	OS2
OS3	1.02	0.29	0.49		0.50	30	0.50	5.00	0	0.00	0.00	0.00	5.00	5.19	9.06	1.5	4.5	OS3
DP1 (PP2 + PP3 +	1.02	0.20	0.10	0.00	0.00	- 00	0.00	0.00		0.00	0.00	0.00	0.00	0.10	0.00	1.0	1.0	DP1 (PP2 + PP3 +
OS1 + OS2 + OS3)	47.63	0.10	0.36	4.71	17.27	300	1.00	33.04	2600	1.10	5.00	8.67	54.47	1.59	2.78	7.5	48.0	OS1 + OS2 + OS3)



# **APPENDIX C**

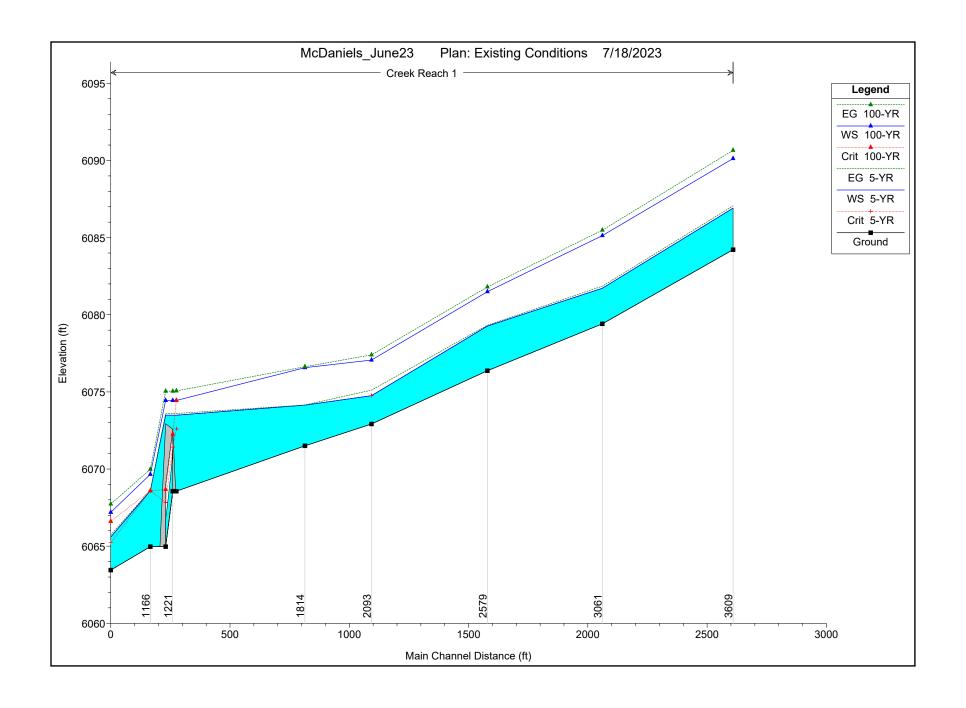
**ELLICOTT CONSOLIDATED FLOODPLAIN ANALYSIS** 

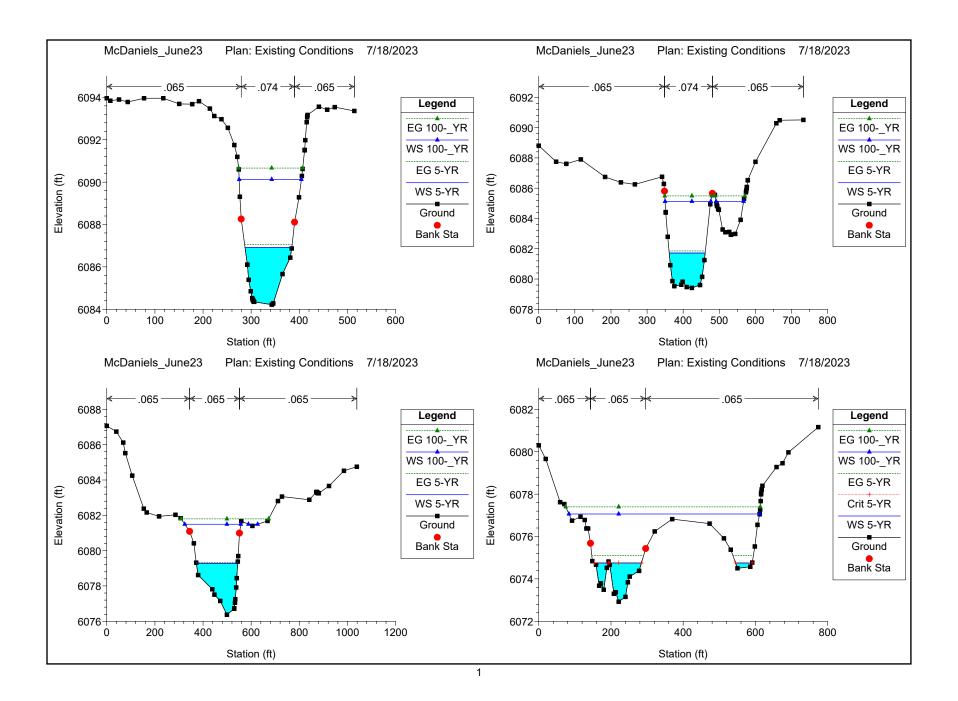


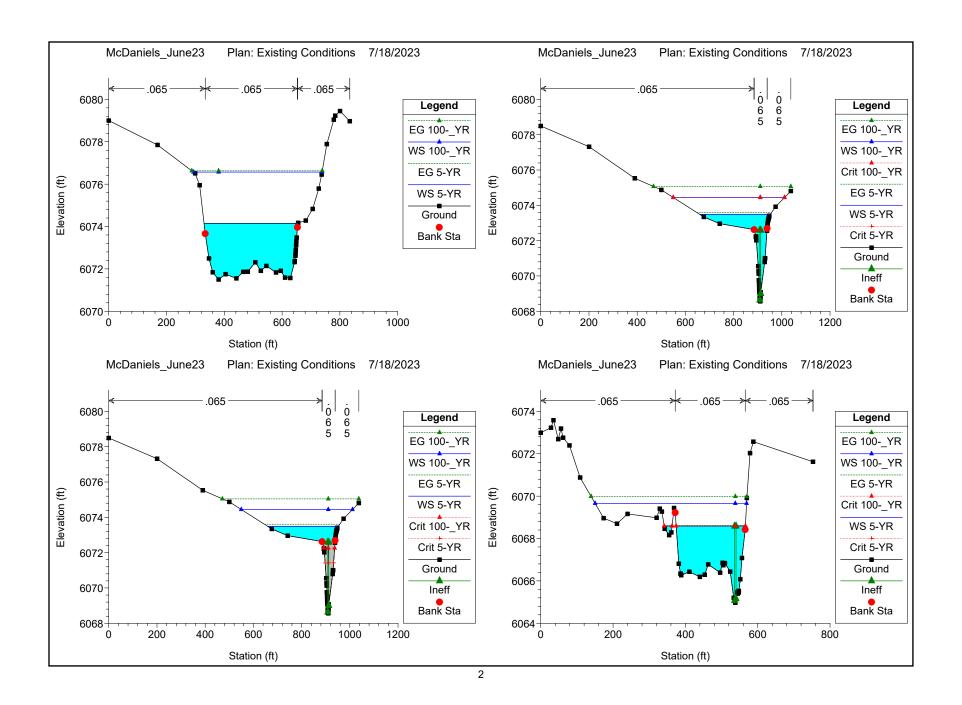
HEC-RAS Plan: Existing River: Creek Reach: Reach 1

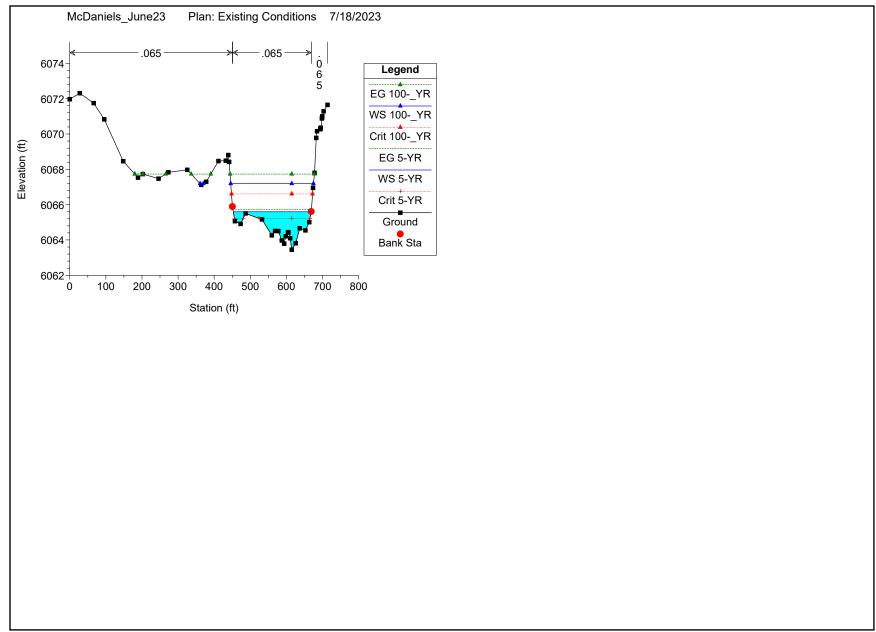
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Val Chal	Flow Area	Top Width	Froude # Chl
Reacii	River Sta	Profile							Vel Chnl			Froude # Crii
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach 1	3609	5-YR	570.00	6084.22	6086.91		6087.06	0.009843	3.07	185.91	97.05	0.39
Reach 1	3609	100-YR	3200.00	6084.22	6090.13		6090.66	0.010752	5.91	552.72	129.32	0.48
Reach 1	3061	5-YR	570.00	6079.41	6081.72		6081.85	0.009166	2.97	191.95	99.59	0.38
Reach 1	3061	100-YR	3200.00	6079.41	6085.13		6085.49	0.008188	4.97	696.78	203.06	0.41
Reach 1	2579	5-YR	570.00	6076.37	6079.27		6079.32	0.003368	1.91	298.05	171.93	0.26
Reach 1	2579	100-YR	3200.00	6076.37	6081.50		6081.80	0.007120	4.43	729.05	271.04	0.42
Reach 1	2093	5-YR	570.00	6072.92	6074.75	6074.75	6075.11	0.053393	4.88	122.53	173.74	0.91
Reach 1	2093	100-YR	3200.00	6072.92	6077.06		6077.40	0.011847	5.18	798.25	528.22	0.53
Reach 1	1814	5-YR	570.00	6071.50	6074.14		6074.15	0.000435	0.81	706.10	325.46	0.10
Reach 1	1814	100-YR	3200.00	6071.50	6076.57		6076.63	0.001031	2.04	1665.55	444.88	0.17
Reach 1	1275	5-YR	570.00	6068.56	6073.49	6072.60	6073.60	0.004497	2.98	274.92	293.02	0.32
Reach 1	1275	100-YR	3200.00	6068.56	6074.44	6074.44	6075.07	0.022462	8.11	631.73	461.52	0.74
Reach 1	1221		Culvert									
Reach 1	1166	5-YR	570.00	6064.97	6068.59	6068.59	6068.62	0.001328	1.38	416.37	213.24	0.17
Reach 1	1166	100-YR	3200.00	6064.97	6069.66	6068.59	6069.99	0.009293	4.76	771.19	418.96	0.47
Reach 1	1000	5-YR	570.00	6063.45	6065.60	6065.22	6065.74	0.020012	2.98	191.22	215.85	0.56
Reach 1	1000	100-YR	3200.00	6063.45	6067.19	6066.61	6067.73	0.020008	5.90	546.94	238.09	0.66

FEMA flow in channel is 7019 cfs. Where was 3200 cfs obtained?











Woody shrubs along channel thalweg on north end of site (looking southeast)



Native grasses within channel within midpoint of property (looking northwest)



Native grasses within channel within midpoint of property (looking southeast)



48" CMP at North Log Road crossing (downstream of project, looking west)



48" CMP at North Log Road Crossing (downstream of project, looking east)

#### HEC-RAS HEC-RAS 6.2 March 2022 U.S. Army Corps of Engineers Hydrologic Engineering Center 609 Second Street

Davis, California

Х	Х	XXXXXX	XXXX			XX	XX	Х	X	XXXX	
X	X	X	X	X		X	X	X	X	X	
X	X	X	X			X	X	X	X	X	
XXXXXXX		XXXX	X		XXX	XXXX		XXXXXX		XXXX	
X	X	X	X	X		X	X	X	X	Х	2
X	X	X	X X			X	X	X	X	X	S
X	X	XXXXXX	XXXX			Х	X	X	X	XXXXX	

PROJECT DATA

Project Title: McDaniels\_June23 Project File : McDaniels\_Jun23.prj Run Date and Time: 7/18/2023 7:05:20 AM

Project in English units

#### PLAN DATA

Plan Title: Existing Conditions

Plan File : n:\Projects\W0008 - Guman & Associates\W0008.0014 22755 McDaniels Road\5. ENG\HEC-

RAS\McDaniels\_Jun23.p01

Geometry Title: McDaniels

Geometry File: n:\Projects\W0008 - Guman & Associates\W0008.0014 22755 McDaniels Road\5. ENG\HEC-

RAS\McDaniels\_Jun23.g01

: DBPS Flows Flow Title

Flow File : n:\Projects\W0008 - Guman & Associates\W0008.0014 22755 McDaniels Road\5. ENG\HEC-

RAS\McDaniels\_Jun23.f01

Plan Summary Information:

8 Number of: Cross Sections = Multiple Openings = 0 Culverts = 1 Inline Structures = 0 0 Lateral Structures = Bridges

Computational Information

Water surface calculation tolerance = 0.01Critical depth calculation tolerance = 0.01 Maximum number of iterations = 20Maximum difference tolerance = 0.3 Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary

Conveyance Calculation Method: At breaks in n values only

Friction Slope Method: Average Conveyance Computational Flow Regime: Subcritical Flow

#### FLOW DATA

Flow Title: DBPS Flows

Flow File: n:\Projects\W0008 - Guman & Associates\W0008.0014 22755 McDaniels Road\5. ENG\HEC-

RAS\McDaniels\_Jun23.f01

Flow Data (cfs)

River	Reach	RS	5-YR	100-YR
Creek	Reach 1	3609	570	3200

Boundary Conditions

 River
 Reach
 Profile
 Upstream
 Downstream

 Creek
 Reach 1
 5-YR
 Normal S = 0.02

 Creek
 Reach 1
 100-YR
 Normal S = 0.02

GEOMETRY DATA

Geometry Title: McDaniels

Geometry File: n:\Projects\W0008 - Guman & Associates\W0008.0014 22755 McDaniels Road\5. ENG\HEC-

RAS\McDaniels\_Jun23.g01

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 3609

INPUT

Description:

Station :	Elevation	Data	num=	50					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	6093.96	7.5	6093.84	25.5	6093.9	43.5	6093.78	77.5	6093.96
117.5	6093.96	150.6	6093.69	177.5	6093.68	191.5	6093.82	214.2	6093.47
223.4	6093.12	238.2	6092.97	251.6	6092.56	265.1	6091.75	271.1	6091.19
274.1	6090.6	276.5	6089.31	279.3	6088.26	292	6086.11	292.1	6086.1
294.8	6085.39	299.1	6084.85	302	6084.53	302.9	6084.47	303.4	6084.44
303.9	6084.42	304.8	6084.38	305.6	6084.36	306.2	6084.35	342.6	6084.22
345.6	6084.27	345.8	6084.28	365	6085.66	381.2	6086.44	384.1	6086.87
390.2	6088.11	399.2	6089.28	405.3	6090.29	406.7	6090.62	410.9	6091.5
411	6091.52	412.4	6091.98	415.2	6092.83	416.3	6093.06	416.6	6093.12
417	6093.17	440.6	6093.56	457.7	6093.42	473.6	6093.54	514.27	6093.36

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .065 279.3 .074 390.2 .065

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 279.3 390.2 548 548 548 .1 .3

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 3061

INPUT

Description:

DODOL IPO.									
Station 1	Elevation	Data	num=	50					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	6088.81	48	6087.75	76.4	6087.61	116.5	6087.9	183.6	6086.74
227.5	6086.38	266.2	6086.25	341.5	6086.75	346.4	6086.28	348.2	6085.8
351.4	6084.42	351.5	6084.39	357.1	6082.79	364.4	6080.91	370.3	6079.86
375.6	6079.53	394.8	6079.62	398.4	6079.82	409.7	6079.47	424	6079.41
446.7	6079.6	452.5	6080.14	458.8	6081.25	475.1	6084.94	480.9	6085.66
487.9	6085.56	492.2	6084.98	493.5	6084.85	493.9	6084.82	496.7	6084.63
498.8	6084.57	509.2	6083.27	516.9	6083.09	527.7	6083.11	532	6082.94
532.4	6082.92	544.1	6082.98	559	6083.91	568.5	6085.31	573.7	6085.72
574.6	6085.84	575.7	6085.99	576	6086.04	576.3	6086.08	578.8	6086.52
578.9	6086.53	600.2	6087.74	657.9	6090.29	667	6090.49	732.82	6090.51

Manning's n Values num= 3

Sta n Val Sta n Val Sta n Val

0 .065 348.2 .074 480.9 .065

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 348.2 480.9 482 482 482 .1 .3

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 2579

INPUT

Description:

Station Elevation Data 47 num= Sta Elev Sta Elev Sta Elev Sta Elev 0 6087.06 39.9 6086.74 68.4 6086.12 77.2 6085.52 Sta 105.6 6084.25 306.8 6081.84 153.8 6082.38 165.9 6082.16 285.6 6082.03 217.3 6081.94 344.4 6081.09 361.9 6080.41 371.4 6079.32 379.5 6078.62 438.5 6077.81 447.3 6077.51 471.4 6077.15 499.1 6076.37 529.4 6076.71 529.6 6076.74 537.6 6077.91 532.7 6077.05 533.9 6077.25 545.9 6079.69 551.3 6080.99 540 6078.44 605 6081.4 544.5 6079.38 559 6081.67 668.1 6081.68 711.1 6082.81 727.7 6083.06 841.5 6082.88 869.9 6083.31 871.6 6083.32 872.2 6083.32 873.1 6083.31 873.8 6083.3 874.6 6083.28 876.6 6083.26 877.7 6083.26 878.8 6083.25 881 6083.25 875.1 6083.27 923.1 6083.66 985.2 6084.52 1038.69 6084.75

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .065 344.4 .065 551.3 .065

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 344.4 551.3 486 486 486 .1 .3

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 2093

INPUT

Description:

Station Elevation Data 49 num= Sta Elev Sta Elev 59.2 6077.62 71 6077.53 Sta Elev Sta Elev Sta 0 6080.3 19.3 6079.66 59.2 6077.62 71 6077.53 115.6 6076.93 127.4 6076.78 132 6076.38 136.8 6076.38 92.1 6076.75 143.3 6075.68 148.5 6074.84 158.6 6074.67 167.3 6073.68 172 6073.79 180 6073.49 188.5 6074.52 193.2 6074.82 196.7 6074.66 208.1 6073.3 213.4 6073.37 221.4 6072.92 240.2 6073.15 246.8 6073.84 251.9 6074.11 277.8 6074.38 296.2 6075.43 321 6076.24 369.5 6076.82 472.9 6076.61 512.8 6075.91 296.2 6075.43 531.6 6075.38 550.4 6074.5 585.7 6074.57 591.3 6074.77 598.5 6075.53 605.8 6076.55 611.6 6077.05 611.8 6077.06 613.1 6077.27 615.6 6077.99 616 6078.07 617.3 6078.21 617.4 6078.22 658.5 6079.28 675 6079.46 691.5 6079.97 774.14 6081.16 614.5 6077.67 619.4 6078.39

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .065 143.3 .065 296.2 .065

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 143.3 296.2 279 279 279 .1 .3

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 1814

INPUT

Description:

Station Elevation Data num= 44

Sta Elev Sta Elev Sta Elev Sta Elev

```
334.1 6073.66
      0 6079
                    169 6077.85 299.1 6076.51 314.7 6075.95

    347.1
    6072.49
    360.1
    6071.84
    380.2
    6071.5
    404.4
    6071.75

    465.6
    6071.86
    481.4
    6071.87
    507.4
    6072.31
    526.5
    6071.91

                                                                       442 6071.55
                                                                      545.7 6072.14
                                   610.3 6071.59 628.7 6071.57 643.2 6072.32
   579.2 6071.83 595.5 6071.91
                                                    646.2 6072.67
   643.8 6072.37 645.8 6072.62 646.1 6072.65
                                                                      646.9 6072.79
                                   648.9 6073.19 649.5 6073.31 653.9 6074.01 654.7 6074.08
   647.5 6072.9
                   648.6 6073.12
                                                                      650.4 6073.48
   653.3 6073.96 653.4 6073.97
                                                                      655.8 6074.17
   682.1 6074.28 706 6074.83 726.9 6075.79 736.8 6076.45
                                                                      755 6077.89
   778.9 6079.04 784.1 6079.23 800.6 6079.45 834.33 6078.97
Manning's n Values
                          num=
     Sta n Val Sta n Val Sta n Val 0 .065 334.1 .065 653.3 .065
Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 334.1 653.3 539 539 .1 .3
                                   539 539
                                                   539
                                                                    .1 .3
CROSS SECTION
RIVER: Creek
                         RS: 1275
REACH: Reach 1
TNDIIT
Description:
742.3 6072.96 884.3 6072.63 885.1 6072.62 892.6 6072.24 892.8 6072.22
                                                    902.1 6070.55
   892.9 6072.22 893.1 6072.19 894.3 6072.02
903.9 6070.13 904.8 6069.76 905.5 6069.52
                                                                      903.3 6070.27
                                                     906.1 6069.29
                                                                       906.3 6069.21
   906.8 6069.08 907.8 6068.77 908.3 6068.65
                                                    909.3 6068.6
                                                                      909.6 6068.59
   910.5 6068.56 910.8 6068.63 911.5 6068.8 912.4 6068.97
                                                                      912.7 6069.07
   928.9 6070.79 930.3 6070.99 930.4 6071.01
939.4 6072.72 939.9 6072.79 940.9 6072.94
                                                    938.6 6072.56
941.4 6073.01
                                                                      939.2 6072.69
                                                                      942.7 6073.12
   943.6 6073.19 944.7 6073.23 945.5 6073.27 945.8 6073.28
                                                                      946.9 6073.34
                   948 6073.41 974.1 6073.92 1037.31 6074.81
    947 6073 35

      Manning's n Values
      num=
      3

      Sta
      n Val
      Sta
      n Val
      Sta

      0
      .065
      885.1
      .065
      939.2

                                     Sta n Val
                                            .065
Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
109 109 109
                                                                      .3 .5
   912.5 1037.31 6072.59
CULVERT
RIVER: Creek
                     RS: 1221
REACH: Reach 1
INPUT
Description:
Distance from Upstream XS =
                                 15
Deck/Roadway Width = 30
Weir Coefficient = 2.6
Upstream Deck/Roadway Coordinates
   num= 10
                                                     Sta Hi Cord Lo Cord
    Sta Hi Cord Lo Cord
                             Sta Hi Cord Lo Cord
     0 6078.49 6060 200.3 6077.32 6060 390.3 6075.53 6060
   500.3 6074.87 6060 676.3 6073.34
                                              6060
                                                     742.3 6072.96
                                                                       6060
   884.3 6072.63
                    6060
                           885.1 6072.62
                                              6060
                                                     961.4 6072.57
                                                                       6060
 1126.32 6071.62
                    6060
Upstream Bridge Cross Section Data
Station Elevation Data num= 49
Sta Elev Sta Elev Sta
                                            Elev
                                                    Sta
                                                               Elev
                                                                                Elev
                                                                       Sta
```

```
    0 6078.49
    200.3 6077.32
    390.3 6075.53
    500.3 6074.87

    742.3 6072.96
    884.3 6072.63
    885.1 6072.62
    892.6 6072.24

    892.9 6072.22
    893.1 6072.19
    894.3 6072.02
    902.1 6070.55

                                                                                                676.3 6073.34
                                                                                                 892.8 6072.22
                                                                                                 903.3 6070.27
     903.9 6070.13 904.8 6069.76 905.5 6069.52 906.1 6069.29
                                                                                                906.3 6069.21
                                                 908.3 6068.65
                                                                         909.3 6068.6
     906.8 6069.08 907.8 6068.77
                                                                                                 909.6 6068.59
    910.5 6068.56 910.8 6068.63 911.5 6068.8 912.4 6068.97
928.9 6070.79 930.3 6070.99 930.4 6071.01 938.6 6072.56
                                                                                                  912.7 6069.07
                                                                                                 939.2 6072.69
    939.4 6072.72 939.9 6072.79 940.9 6072.94
                                                                          941.4 6073.01
                                                                                                 942.7 6073.12
    943.6 6073.19
                           944.7 6073.23 945.5 6073.27 945.8 6073.28
948 6073.41 974.1 6073.92 1037.31 6074.81
                                                                          945.8 6073.28
                                                                                                 946.9 6073.34
       947 6073.35
Manning's n Values num= 5
Sta n Val Sta n Val Sta
^ 065 885.1 .065 939.2
                                                   3
Sta n Val
                                                              .065
Bank Sta: Left Right Coeff Contr. Expan.

885.1 939.2 .3 .5

Ineffective Flow num= 2

Sta L Sta R Elev Permanent

0 908.5 6072.59 F

912.5 1037.31 6072.59 F
    912.5 1037.31 6072.59
Downstream Deck/Roadway Coordinates
     num= 10
      Sta Hi Cord Lo Cord
                                         Sta Hi Cord Lo Cord Sta Hi Cord Lo Cord
    0 6078.49 6060 200.3 6077.32 6060 390.3 6075.53 6060
500.3 6074.87 6060 676.3 6073.34 6060 742.3 6072.96 6060
884.3 6072.63 6060 885.1 6072.62 6060 961.4 6072.57 6060
  1126.32 6071.62 6060
Downstream Bridge Cross Section Data
Station Elevation Data num= 50

        Sta
        Elev
        Sta
        Elev
        Sta
        Elev

        35.1
        6073.58
        48.5
        6072.69
        55.9
        6073.19

     Sta Elev Sta Elev
     0 6072.99 28.4 6073.23 35.1 6073.58 48.5 6072.69 55.9 6073.19 61.8 6072.76 79.4 6072.39 108.9 6070.88 173.8 6068.96 210.8 6068.7
       240 6069.16 320.3 6068.98 329.2 6069.41 334.9 6069.27 342.6 6068.46
    355 6068.16 361.3 6068.29 368.5 6069.44 371.8 6069.22 381.9 6066.81 386.4 6066.34 386.7 6066.34 388.6 6066.27 411 6066.43 440.1 6066.19 453.5 6066.29 463.1 6066.78 496 6066.39 502.9 6066.85 504.4 6066.77
    505 6066.74 509.4 6066.84 523.8 6066.44 533.6 6065.2 538.1 6064.97 543.4 6065.46 544.6 6065.4 546.1 6065.44 547.1 6065.47 547.5 6065.48 547.6 6065.5 547.8 6065.53 552.1 6066.08 556.5 6067.08 565.4 6068.42
    565.5 6068.45 569.9 6069.91 578.8 6072.03 588 6072.57 752.92 6071.62
Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
              .065 371.8 .065 565.4 .065
Bank Sta: Left Right Coeff Contr. Expan.

371.8 565.4 .3 .5

Ineffective Flow num= 2

Sta L Sta R Elev Permanent

0 536.1 6068.58 F
    540.1 752.92 6068.58
Upstream Embankment side slope = 3 horiz. to 1.0 vertical
Downstream Embankment side slope = 3 horiz. to 1.0 vertical
Maximum allowable submergence for weir flow = .98
Elevation at which weir flow begins = 6072.59
Energy head used in spillway design
Spillway height used in design
Weir crest shape
                                                               = Broad Crested
Number of Culverts = 1
FHWA Chart # 2 - Corrugated Metal Pipe Culvert
FHWA Scale # 2 - Mitered to conform to slope
Solution Criteria = Highest U.S. EG
Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance Loss Coef Exit Loss Coef
```

15 30 .024 .024 0 .5 1 Upstream Elevation = 6068.56 Centerline Station = 910.5

Downstream Elevation = 6064.97

Centerline Station = 538.1

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 1166

TNPIIT

Description:

Station Elevation Data num= Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev 55.9 6073.19 0 6072.99 28.4 6073.23 35.1 6073.58 48.5 6072.69 61.8 6072.76 79.4 6072.39 108.9 6070.88 173.8 6068.96 210.8 6068.7 240 6069.16 320.3 6068.98 329.2 6069.41 334.9 6069.27 342.6 6068.46 355 6068.16 361.3 6068.29 386.4 6066.34 386.7 6066.34 368.5 6069.44 371.8 6069.22 388.6 6066.27 411 6066.43 381.9 6066.81 440.1 6066.19 453.5 6066.29 463.1 6066.78 496 6066.39 502.9 6066.85 504.4 6066.77 533.6 6065.2 538.1 6064.97 505 6066.74 543.4 6065.46 509.4 6066.84 523.8 6066.44 544.6 6065.4 546.1 6065.44 547.1 6065.47 547.5 6065.48 547.6 6065.5 547.8 6065.53 552.1 6066.08 556.5 6067.08 565.4 6068.42 565.5 6068.45 569.9 6069.91 578.8 6072.03 588 6072.57 752.92 6071.62

ing's n Values num=
Sta n Val Sta n Val Manning's n Values Sta n Val 0 .065 371.8 .065 565.4 .065

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 166 .3 .5

371.8 565.4 166 166
Ineffective Flow num= 2
Sta L Sta R Elev Permanent 0 536.1 6068.58 F 540.1 752.92 6068.58 F

CROSS SECTION

RIVER: Creek

REACH: Reach 1 RS: 1000

INPUT

Description:

Station Elevation Data num=
Sta Elev Sta Elev
0 6071.97 27.7 6072.31 49 Sta Elev Sta Elev Sta Elev 66.2 6071.75 95.7 6070.83 148.1 6068.46 189 6067.53 202.6 6067.73 245.9 6067.47 273.1 6067.83 325.4 6067.97 364.1 6067.12 377.8 6067.29 411.9 6068.47 441.4 6068.42 450.5 6065.89 457.4 6065.06 432.3 6068.49 473.1 6064.91 439.1 6068.81 486.9 6065.5 532.4 6065.16 559.7 6064.26 568.8 6064.51 577.8 6064.5 587 6063.97 604.4 6064.44 605.2 6064.43 593.8 6063.79 598 6064.21 605.8 6064.42 625.7 6063.81 673.7 6066.95 637 6064.66 678 6067.8 610.3 6064.1 614.7 6063.45 652.6 6064.54 663.4 6065.01 668.9 6065.61 682.6 6069.78 684.8 6070.16 693.9 6070.27 694.4 6070.3 695.3 6070.36 698.4 6070.88 698.8 6070.93 699.5 6071 703 6071.28 713.77 6071.65

Manning's n Values 3 num= Sta n Val Sta n Val Sta n Val .065 668.9 .065 .065 450.5

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 450.5 668.9 50 50 50 .1 .3

SUMMARY OF MANNING'S N VALUES

River:Creek

Reach	River Sta.	n1	n2	n3
Reach 1	3609	.065	.074	.065
Reach 1	3061	.065	.074	.065
Reach 1	2579	.065	.065	.065
Reach 1	2093	.065	.065	.065
Reach 1	1814	.065	.065	.065
Reach 1	1275	.065	.065	.065
Reach 1	1221	Culvert		
Reach 1	1166	.065	.065	.065
Reach 1	1000	.065	.065	.065

#### SUMMARY OF REACH LENGTHS

River: Creek

Reach	River Sta.	Left	Channel	Right
Reach 1	3609	548	548	548
Reach 1 Reach 1	3061 2579	482 486	482 486	482 486
Reach 1 Reach 1	2093 1814	279 539	279 539	279 539
Reach 1	1275	109	109	109
Reach 1	1221	Culvert		
Reach 1 Reach 1	1166 1000	166 50	166 50	166 50
1100011 1	1000	50	50	50

#### SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Creek

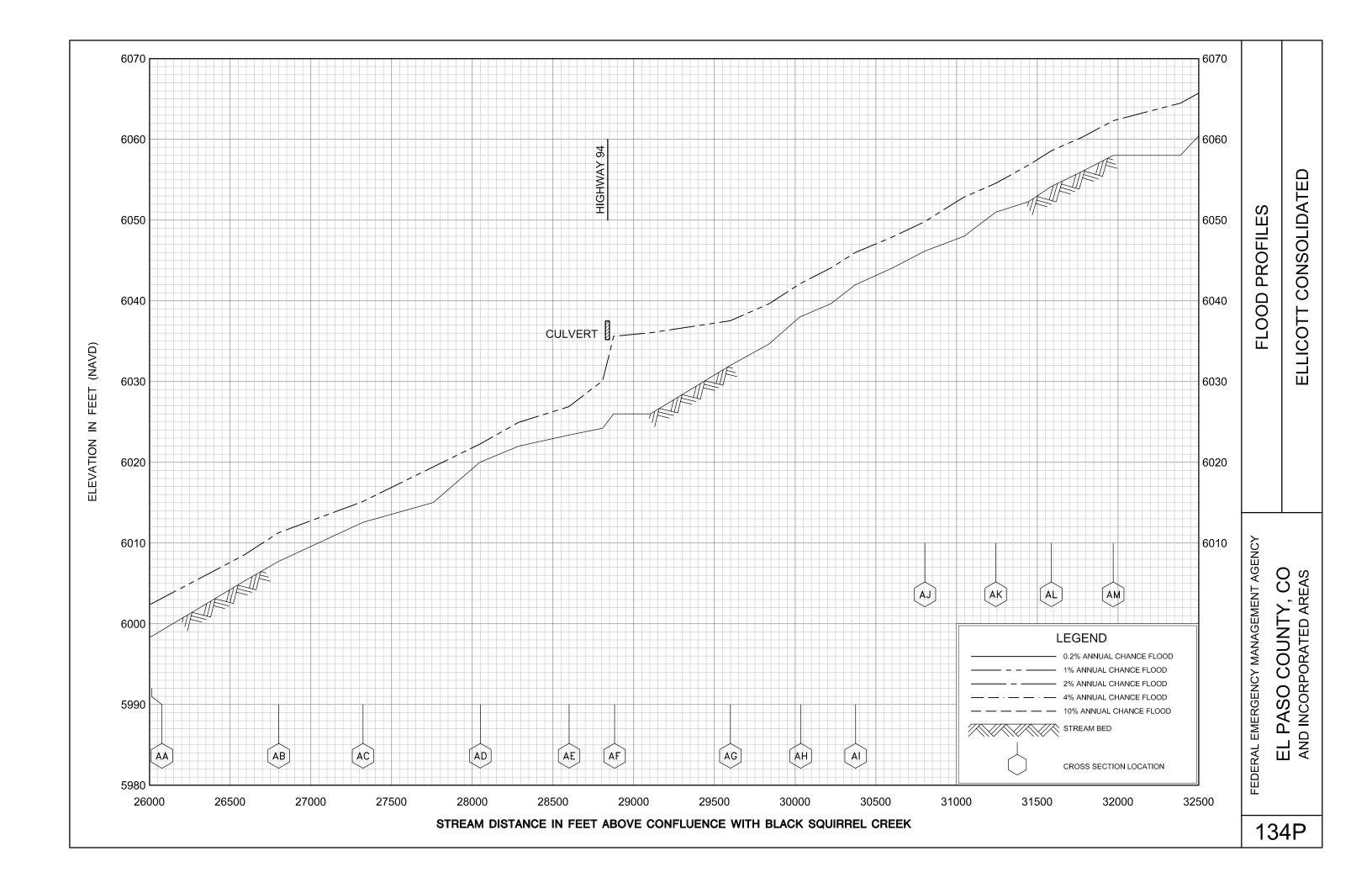
Reach	River Sta	. Contr.	Expan.
Reach 1	3609	.1	.3
Reach 1	3061	.1	.3
Reach 1	2579	.1	.3
Reach 1	2093	.1	.3
Reach 1	1814	.1	.3
Reach 1	1275	.3	.5
Reach 1	1221	Culvert	
Reach 1	1166	.3	.5
Reach 1	1000	.1	.3

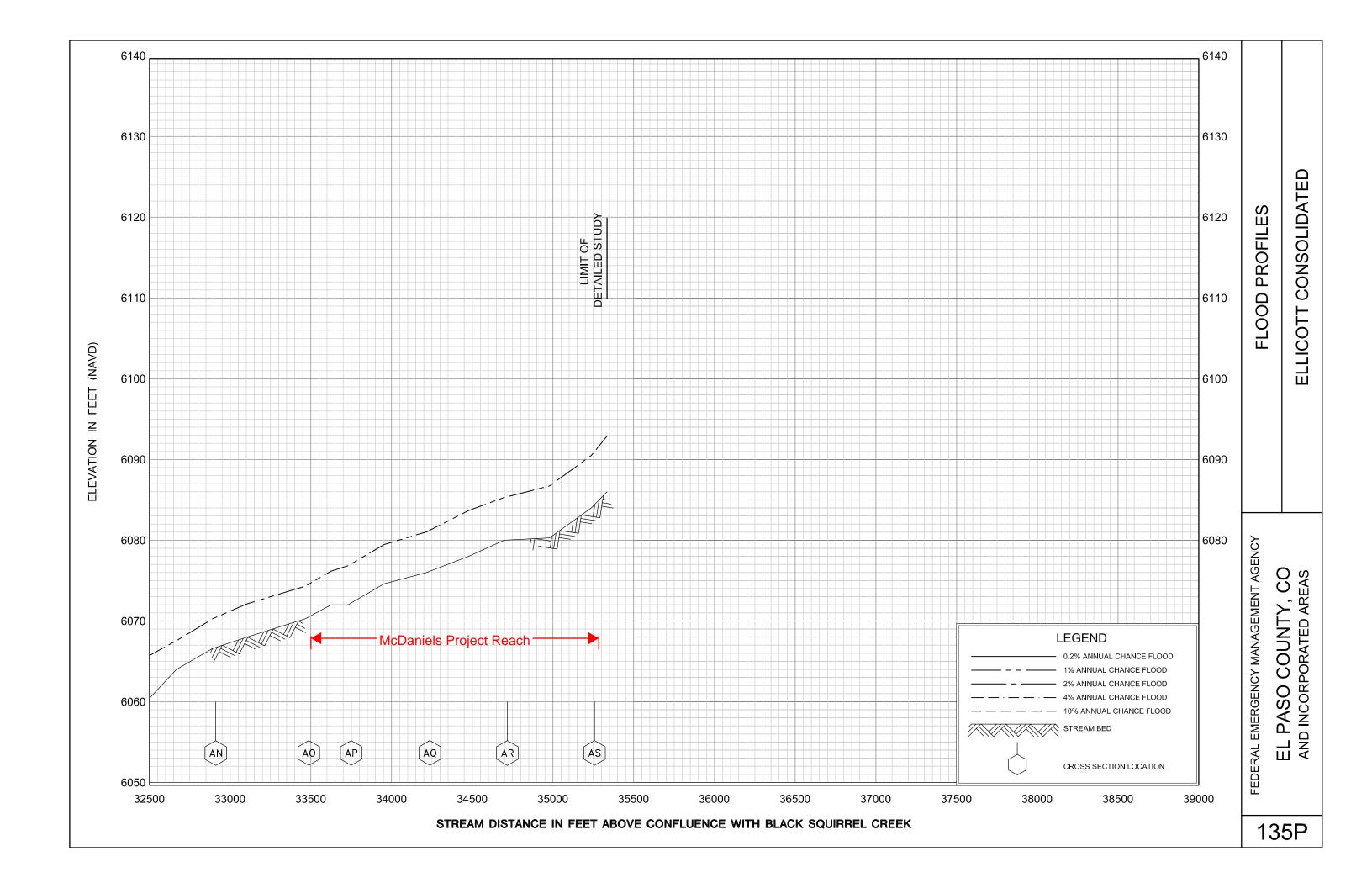
Table 4. Summary of Discharges (cont.)

Peak Discharges (Cubic Feet Per Second)

		Pea	ik Discharges (C	ubic Feet Per Sec	ona)	
Flooding Source and Location	Drainage Area (Square Miles)	10-Year	50-Year	<u>100-Year</u>	<u>500-Year</u>	
East Cherry Creek At Walker Road	10.30	1	1	2,000	1	
East Tributary to Black Squirrel Creek At confluence with Black Squirrel Creek	0.97	1	1	569	1	
East Tributary to Black Squirrel Creek – West Fork Bennett Ranch Basin At Black Squirrel Creek – West Fork Bennett Ranch Basin	0.40	1	1	230	1	
Ellicott Consolidated At confluence with Black Squirrel Creek At confluence with East Tributary	<sup>1</sup>	1 1	<sup>1</sup>	8,000 7,019	¹ ¹ 1	Flow rate through
Ellicott Consolidated – East Tributary At confluence with Ellicott Consolidated	1	1	1	183		project reach
Fairfax Creek At Research Parkway	0.70	1	1	1,000	1	
Fisher's Canyon At confluence with Fountain Creek	5.30	1,420	2,590	3,090	4,800	
Fisher's Canyon-Above Loomis Avenue At West Meadows Drive Upstream of Fisher's Canyon-South Branch	3.59 2.36	1 1	<sup>1</sup> <sup>1</sup>	1,640 440	<sup>1</sup> <sup>1</sup>	
Fisher's Canyon-South Branch At confluence with Fisher's Canyon	1.23	1	1	1,290	1	

<sup>&</sup>lt;sup>1</sup>Data not available







# APPENDIX D

**DESIGN CHARTS** 

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

	Percent		Runoff Coefficients										
	impervious	2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSGA&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business								1					1
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0,53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0,22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0,34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas											-	-	
Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets							+						1
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44		0.50

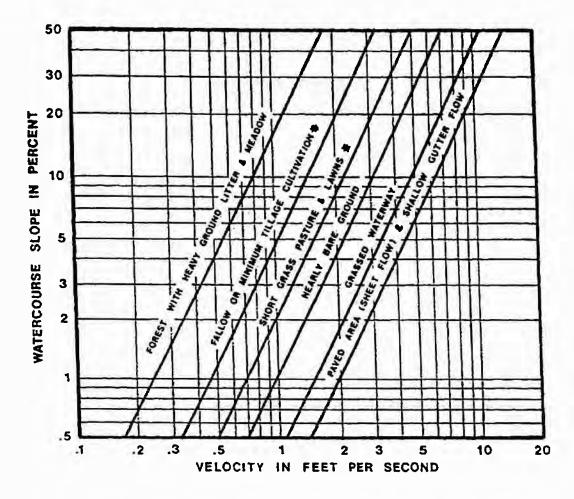


Figure 6-25. Estimate of Average Concentrated Shallow Flow

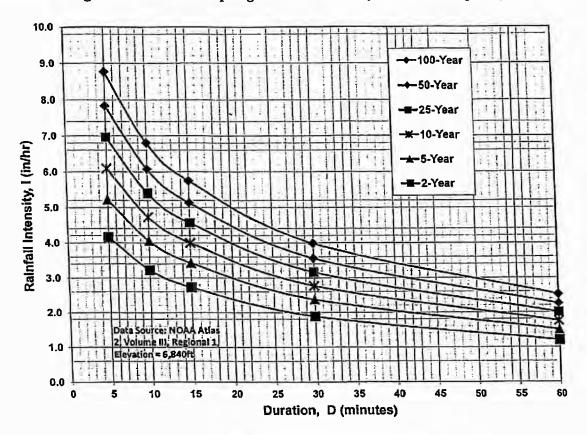


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

#### **IDF** Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \text{ ln}(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Table 2. Permissible Shear and Velocity for Selected Lining Materials<sup>1</sup>

Permissible Shear and Velocity for Selected Lifting Materials  Permissible Permissible C								
Boundary Category	Boundary Type	Shear Stress	Velocity	Citation(s)				
Boundary Category	Boundary Type	(lb/sq ft)	(ft/sec)					
Soils	Fine colloidal sand		(IVSec) 1.5	Λ				
Soils		0.02 - 0.03		A				
	Sandy loam (noncolloidal)	0.03 - 0.04	1.75	A				
	Alluvial silt (noncolloidal)	0.045 - 0.05	2	A				
	Silty loam (noncolloidal)	0.045 - 0.05	1.75 – 2.25	A				
	Firm loam	0.075	2.5	A				
	Fine gravels	0.075	2.5	A				
	Stiff clay	0.26	3 – 4.5	A, F				
	Alluvial silt (colloidal)	0.26	3.75	A				
	Graded loam to cobbles	0.38	3.75	A				
	Graded silts to cobbles	0.43	4	A				
	Shales and hardpan	0.67	6	Α				
Gravel/Cobble	1-in.	0.33	2.5 - 5	Α				
	2-in.	0.67	3 – 6	Α				
	6-in.	2.0	4 - 7.5	Α				
	12-in.	4.0	5.5 – 12	Α				
<u>Vegetation</u>	Class A turf	3.7	6 - 8	E, N				
	Class B turf	2.1	4 - 7	E, N				
	Class C turf	1.0	3.5	E, N				
	Long native grasses	1.2 - 1.7	4 – 6	G, H, L, N				
	Short native and bunch grass	0.7 - 0.95	3 – 4	G, H, L, N				
	Reed plantings	0.1-0.6	N/A	E, N				
	Hardwood tree plantings	0.41-2.5	N/A	E, N				
Temporary Degradable RECPs	Jute net	0.45	1 – 2.5	E, Ĥ, M				
	Straw with net	1.5 – 1.65	1 – 3	Е, Н, М				
	Coconut fiber with net	2.25	3 – 4	E, M				
	Fiberglass roving	2.00	2.5 – 7	E, H, M				
Non-Degradable RECPs	Unvegetated	3.00	5 – 7	E, G, M				
	Partially established	4.0-6.0	7.5 – 15	E, G, M				
	Fully vegetated	8.00	8 – 21	F, L, M				
<u>Riprap</u>	6 – in. d <sub>50</sub>	2.5	5 – 10	H				
<del> </del>	9 – in. d <sub>50</sub>	3.8	7 – 11	H				
	12 – in. d <sub>50</sub>	5.1	10 – 13	H				
	18 – in. d <sub>50</sub>	7.6	12 – 16	H				
	24 – in. d <sub>50</sub>	10.1	14 – 18	 E				
Soil Bioengineering	Wattles	0.2 – 1.0	3	C, I, J, N				
<u>oon Biochgineening</u>	Reed fascine	0.6-1.25	5	E				
	Coir roll	3 - 5	8	E, M, N				
	Vegetated coir mat	4 - 8	9.5	E, M, N				
	Live brush mattress (initial)	0.4 – 4.1	4	Е, IVI, IVI В, Е, I				
	Live brush mattress (grown)	3.90-8.2	12					
	ίθ,			B, C, E, I, N				
	Brush layering (initial/grown)	0.4 – 6.25	12	E, I, N				
	Live fascine	1.25-3.10	6 – 8	C, E, I, J				
Llord Curtosing	Live willow stakes	2.10-3.10	3 – 10	E, N, O				
<u>Hard Surfacing</u>	Gabions	10	14 – 19	D				
1 Ranges of values generally	Concrete	12.5	>18	H				

<sup>&</sup>lt;sup>1</sup> Ranges of values generally reflect multiple sources of data or different testing conditions.

I. Schiechtl, H. M. and R. Stern. (1996).

**A**. Chang, H.H. (1988). **F**. Julien, P.Y. (1995).

**G**. Kouwen, N.; Li, R. M.; and Simons, D.B., (1980). **L**. Temple, D.M. (1980).

**K**. Sprague, C.J. (1999).

**B**. Florineth. (1982)

H. Norman, J. N. (1975).

C. Gerstgraser, C. (1998).

**M**. TXDOT (1999)

**D**. Goff, K. (1999).

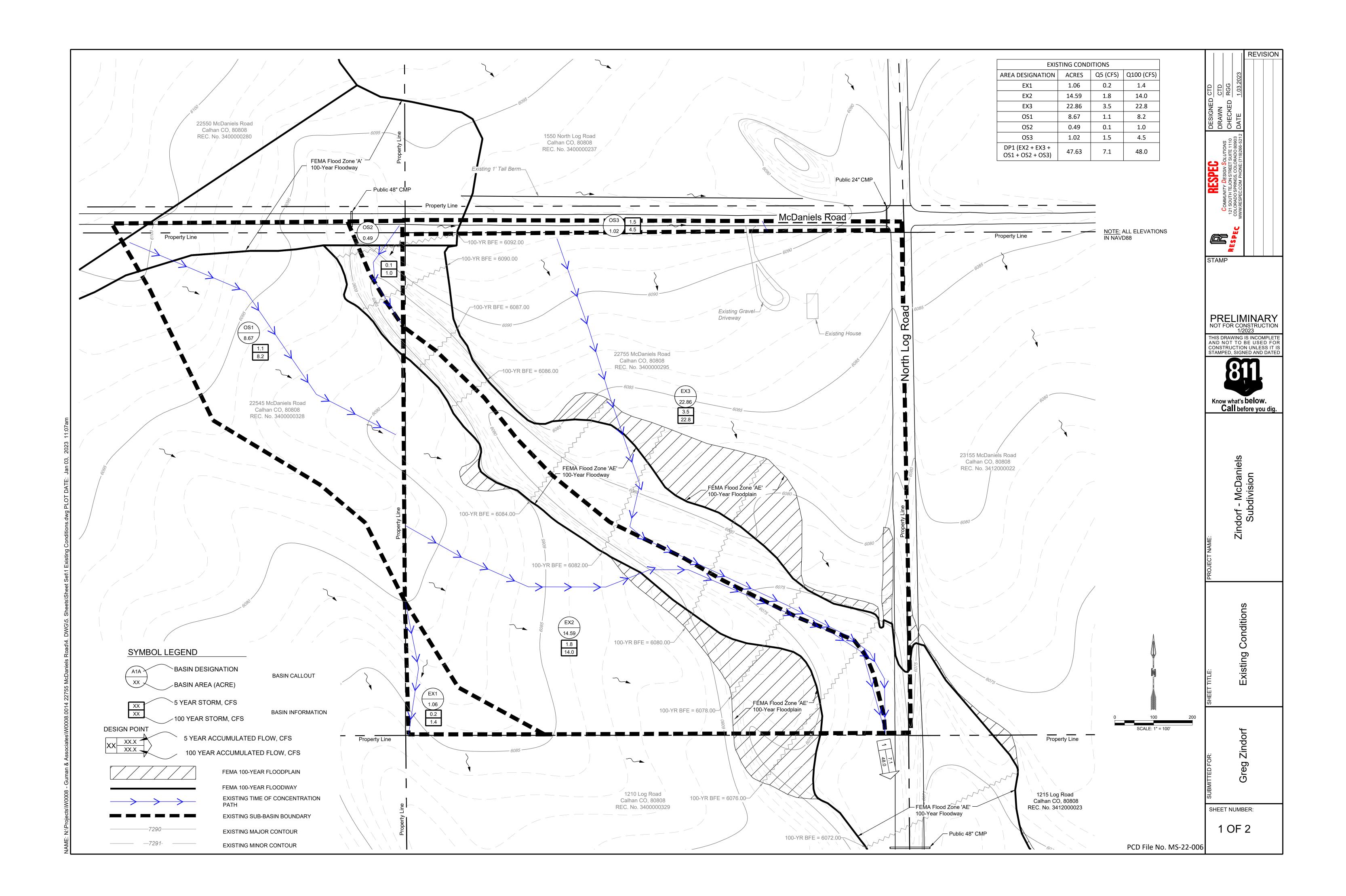
N. Data from Author (2001)

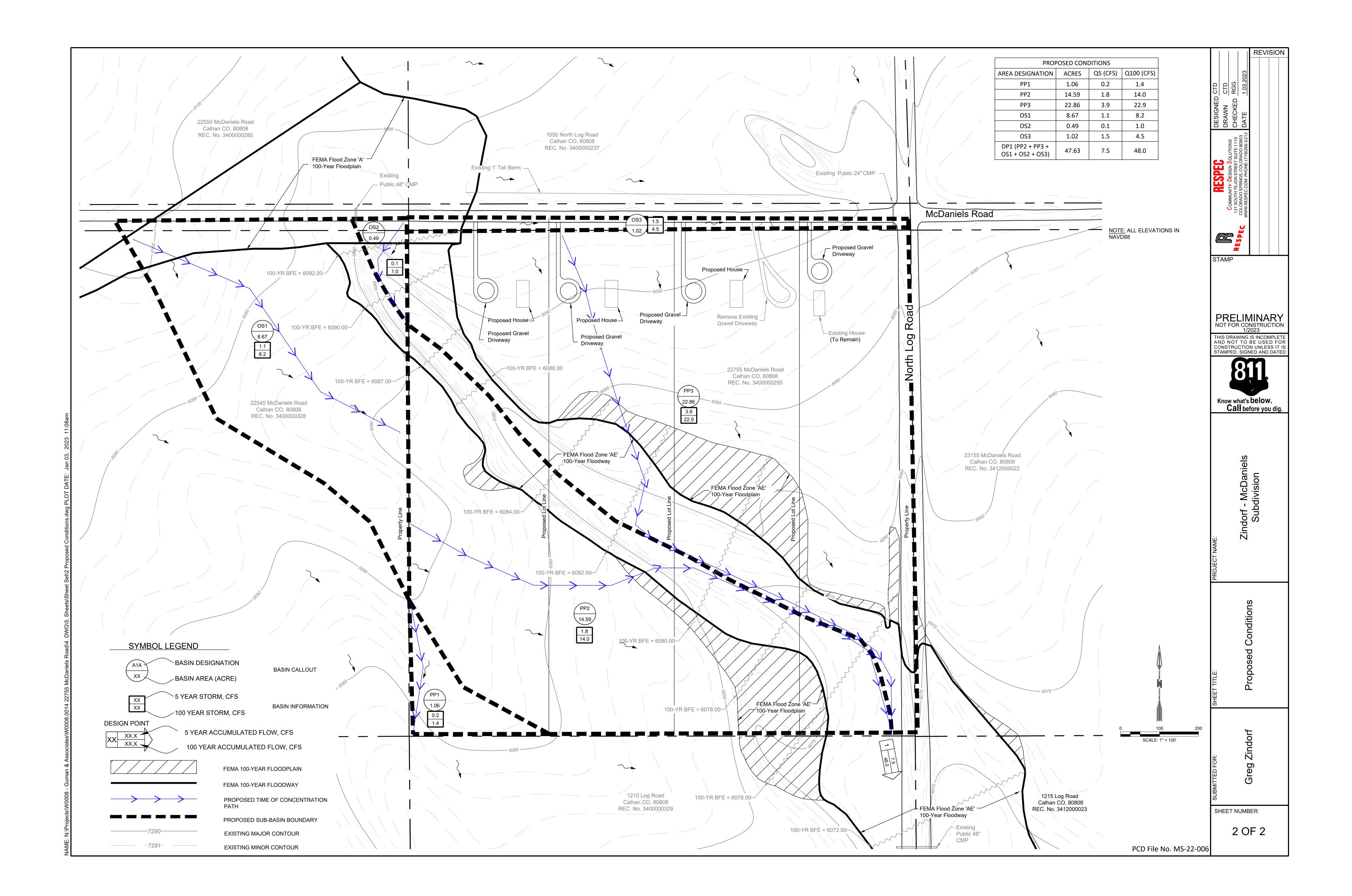
O. USACE (1997).

E. Gray, D.H., and Sotir, R.B. (1996). J. Schoklitsch, A. (1937).



## **BACK POCKET**





### v4\_Drainage Report - Final.pdf Markup Summary

#### CDurham (3)



Subject: Text Box Page Label: 9 Author: CDurham

Date: 7/31/2023 4:34:39 PM

Color:

Indicate what flows were used in the analysis (FEMA lists 7019 cfs but HEC-RAS shows 3200 cfs). Indicate what velocity, FR # and how these all

meet channel requirements from DCM.



Subject: Text Box Page Label: 22 Author: CDurham

Date: 7/31/2023 4:32:21 PM

Color:

Label sections. Be sure to show and label sections that correspond to those shown on FEMA floodplain map.



Subject: Callout Page Label: 23 Author: CDurham

Date: 7/31/2023 4:29:36 PM

Color:

FEMA flow in channel is 7019 cfs. Where was

3200 cfs obtained?