

BARGHAUSEN



Drainage Report Dutch Bros Coffee (CO0907)

PREPARED BY

Barghausen Consulting Engineers, Inc.

PREPARED FOR

Dutch Bros Coffee

CLIENT ADDRESS

110 S.W. 4th Street, Grants Pass, OR 97526



This drainage report is very brief. See Chapter 4 of the El Paso County DCM Volume 1 for the required components for the drainage report.

ENGINEER'S STATEMENT:

Design Engineer's Statement:		under
The attached drainage plan and report were supervision and are correct to the best of my drainage report has been prepared according County for drainage reports and said report is master plan of the drainage basin. I accept r by any negligent acts, errors or omissions on	prepared under my direction and knowledge and belief. Said g to the criteria established by the s in conformity with the applicable responsibility for any liability cause my part in preparing this report.	al and lorado accept part in
[Name, P.E. #]	Date	
Anthony E. Merlino, PE#60820	Seal	E NO L
DEVELOPER'S STATEMENT:	-	04/10/202
Dutch Bros LLC hereby certifies that the drainad Owner/Developer's Statement: I, the owner/developer have read and will co specified in this drainage report and plan.	ie facilities for Dutch Bros CO0907 shall	be Colorado ertified by ction nal ns of not imply
[Name, Title] [Business Name] [Address]	Date	
Title:	Address:	_
		_
El Paso County:		
Filed in accordance with the requirements of Manual, Volumes 1 and 2, El Paso County E and Land Development Code as amended.	ngs} 200 the Drainage Criteria ngineering Criteria Manual	01, as
Joshua Palmer, P.E. County Engineer / ECM Administrator	Date	
Conditions:	WATR C	onformance

PROJECT OVERVIEW

What does this mean? What predetermined storm basin requirements? The proposed redevelopment will need to follow all El Paso County Standards.

This document is the Drainage Report for 5810 Omaha Boulevard, Colorado Springs, CO 80915. This report is intended to demonstrate that the drainage requirements for the proposed Dutch Bros. Coffee development is in conformance with the predetermined storm basin requirements for the existing commercial development.

This project is located in the northwest corner of Powers Boulevard and Omaha Boulevard, Colorado Springs, Colorado and is currently an existing gas station. The parcel is approximately $0.62\pm$ ac or $26,869\pm$ square feet and is bounded by Powers Boulevard to the west, existing commercial development on the east and north, and Omaha Boulevard to the south. The disturbed area consists of approximately $0.62\pm$ ac or $26,869\pm$ square feet. Overall, the site slopes from the northeast to the southwest. Refer to Appendix A for the Vicinity Map.

The property is zoned as Commercial Regional. The proposed development includes a building footprint of 950 square feet and a 272-square-foot trash enclosure. The planned site improvements include paved asphalt driving area, reinforced concrete driving area, on-site sidewalk area, and landscaping. These values give the site an overall impervious percentage of approximately 59%±.

SOILS

Per the Natural Resources Conservation Service web soils survey, soils for this project, delineated on the Soils Map within Appendix B of this report, are classified as Blendon Sandy Loam. Blendon Sandy Loam has been classified as Hydrologic Soil Type "B". The study area consists of undeveloped land with sparse, grassy vegetation.

FLOODPLAN STATEMENT

The subject property is located in Zone "X" (Area determined to be outside the 0.2% annual chance floodplain) per the Flood Insurance Rate Map for County of El Paso, Colorado Map Number 08041C0751G, revised December 7, 2018.

EXISTING DRAINAGE

Discuss in more detail, how many inlets? What size storm drains etc.

The existing site is currently an existing gas station with existing drainage inlets near the south side of the site. There is an existing storm drain system located near the south end of the site. In general, the site typically sheet flows from the northeast to the southwest towards the existing inlets. Refer to Appendix B for the Existing Conditions Drainage Map.

In existing conditions, Basin A-1 is approximately 0.62 acres in size and approximately 90% impervious. The runoff coefficient for the 5-year and 100-year storm event is 0.81 and 0.88, respectively. The flow rate was calculated using a minimum time of concentration of 5 minutes. The runoff is approximately 2.61 cfs for the 5-year and 4.76 cfs for the 100-year storm event. The runoff is conveyed and collected by the existing drainage inlets located near the south end of the site and is conveyed to the existing storm drain.

In the above paragraph inlets is plural. The basins for the project site should have one discharge point each. If there are multiple inlets there should be multiple sub-basins. Ensure that these values are based on DCM table 5-1

PROPOSED DRAINAGE

The project proposes to construct a new Dutch Bros Coffee building, drive aisles, parking stalls, landscaping, and utilities. In proposed conditions, the project proposes more landscaping than existing conditions, which reduces the amount of runoff to the tributary drainage inlets.

In proposed conditions, Basin A-1 is the proposed Dutch Bros Coffee site. The basin is approximately 0.63 acres in size and approximately 73% impervious. The runoff coefficient for the 5-year and 100-year storm event is 0.68 and 0.80, respectively. The flow rate was calculated using a minimum time of concentration of 5 minutes. The runoff is approximately 2.22 cfs for the 5-year and 4.35 cfs for the 100-year storm event, which is less than the existing conditions. The runoff is conveyed to curb cuts, is collected by the drainage inlets located near the south end of the site, and is conveyed to the existing storm drain.

Refer to Appendix B for the Proposed Conditions Drainage Map and Appendix C for the Hydrology Calculations for Basin A-1 Ensure that these

SUMMARY

values are based on DCM table 5-1

It has been concluded that the proposed project and the constructed improvements will maintain the thresholds of the existing conditions. The proposed project is less than one (1) acre in size, reduces the amount of the existing impervious area from 90% impervious to 73% impervious, and reduces the amount of runoff from 2.61 cfs to 2.22 cfs for the 5-year storm event and from 4.76 cfs to 4.35 cfs for the 100-year storm event. The proposed site also maintains the existing drainage patterns; because the site reduces the amount of runoff tributary to the existing inlets, the existing storm drains/appurtenances will not adversely affect the downstream and surrounding developments. Therefore, the proposed site is in conformance with the City of Colorado Springs and El Paso County standards and requirements.

Water quality/exemption from water quality needs to be discussed in the report.

Provide hydraulic calculations for proposed drainage features and how they will interact with existing drainage features. Ensure modifications to the site are hydraulically working with no negative impacts. See comments on the drainage map.

APPENDIX A

VICINITY MAP



APPENDIX B

EXISTING CONDITIONS DRAINAGE MAP
 PROPOSED CONDITIONS DRAINAGE MAP



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DRAINAGE SUMMARY TABLE

	EXISTING	CONDITIONS			
C (min)	i (2-YR) (in/hr)	PEAK Q ₂ (cfs)	Tc (min)	i (2-YR) (in/hr)	1 HR Q ₂ (cfs)
5	4.12	2.05	60	1.16	0.58
C (min)	i (5-YR) (in/hr)	PEAK Q ₅ (cfs)	Tc (min)	i (5-YR) (in/hr)	1 HR Q ₅ (cfs)
5	5.17	2.62	60	1.44	0.73
C (min)	i (100-YR) (in/hr)	PEAK Q ₁₀₀ (cfs)	Tc (min)	i (100-YR) (in/hr)	1 HR Q ₁₀₀ (cfs)
5	8.68	4.85	60	2.42	1.35

This column is the second Tc column and 60 minutes is an unreasonable Tc for the site. What Tc was actually used?



Revision	AINAGE PLAN HA BLVD RINGS, CO 80915	
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	Scale: Horizontal 1" = 10' Vertical N/A	
	Designed <u>EMM</u> Drawn <u>EMM</u> Checked <u>AEM</u> Approved <u>AEM</u> Date 04/08/24	I EMIGUEL
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DRAINAGE SUMMARY TABLE

	PROPOSED	CONDITIONS			
C (min)	i (2-YR) (in/hr)	PEAK Q ₂ (cfs)	Tc (min)	i (2-YR) (in/hr)	1 HR Q ₂ (cfs)
5	4.12	1.71	60	0.48	0.58
C (min)	i (5-YR) (in/hr)	PEAK Q ₅ (cfs)	Tc (min)	i (5-YR) (in/hr)	1 HR Q ₅ (cfs)
5	5.17	2.22	60	0.62	0.73
C (min)	i (100-YR) (in/hr)	PEAK Q ₁₀₀ (cfs)	Tc (min)	i (100-YR) (in/hr)	1 HR Q ₁₀₀ (cfs)
5	8.68	4.35	60	1.21	1.34
	•				

This column is the second Tc column and 60 minutes is an unreasonable Tc for the site. What Tc was actually used?

0.66

0.68

0.80

APPENDIX C

HYDROLOGY CALCULATIONS

Project:Dutch Bros - CO0907Location:5810 Omaha Blvd, Colorado Springs, COBCE#23098

Rational Method

EXISTING	3						
Basin:	A-1						
Total Area (sf)	27,124						
Total Area (ac)	0.62						
Impervious Area (sf)	24,308						
Pervious Area (sf)	2,816						
Total Area (sf)	27,124						
%Impervious (i)	0.90						
Runoff Coefficient, c				(per Table 6-6 Ru	noff Coefficient	- Commercial)	
Soil Type	В			(per NRCS Web S	oil Survey)		
	2 YR	5 YR	100 YR				
Impervious	0.89	0.9	0.96				
Pervious	0.02	0.08	0.35				
	A-1						
2 Year	0.79						
5 Year	0.81						
100 year	0.88						
Rainfall Intensity, i (in/	'nr)			(per Figure 6-5 - (Colorado Springs	Rainfall Intensity Dur	ration Frequency)
		5 (min)	60 (min)				
	i2 (in/hr) =	4.12	1.16				
	i5 (in/hr) =	5.17	1.44				
	i100 (in/hr) =	8.68	2.42				
Runoff, Q (cfs), assume	e min Tc = 5 min		Q = C * i * A	R	unoff, Q (cfs), as	sume min Tc = 1 hr	Q = C * i * A
	A-1					A-1	
Q2 (cfs) =	2.03				Q2 (cfs) =	0.57	
Q5 (cfs) =	2.61	\mathbf{X}			Q5 (cfs) =	0.73	
Q100 (cfs) =	4.76				Q100 (cfs) =	1.32	
		\backslash	Drainage	mans show			
			different	Tc			

Project:Dutch Bros - CO0907Location:5810 Omaha Blvd, Colorado Springs, COBCE#23098

Rational Method

PROPOSE	D					
asin:	A-1					
otal Area (sf)	27,405					
tal Area (ac)	0.63					
npervious Area (sf)	20,095					
ervious Area (sf)	7,310					
otal Area (sf)	27,405					
mpervious (i)	0.73					
inoff Coefficient, c				(per Table 6-6 Runoff Coefficient -	- Commercial)	
oil Type	В			(per NRCS Web Soil Survey)		
	2 YR	5 YR	100 YR			
pervious	0.89	0.9	0.96			
rvious	0.02	0.08	0.35			
	A-1					
<i>l</i> ear	0.66					
/ear	0.68					
)0 year	0.80					
ainfall Intensity, i (in/	hr)			(per Figure 6-5 - Colorado Springs	Rainfall Intensi	ty Dı
		5 (min)	60 (min)			
	i2 (in/hr) =	4.12	1.16			
	i5 (in/hr) =	5.17	1.44			
	i100 (in/hr) =	8.68	2.42			
unoff, Q (cfs), assume	min Tc = 5 min		Q = C * i * A	Runoff, Q (cfs), as	sume min Tc = 1	L hr
	A-1				A-1	
Q2 (cfs) =	1.71			Q2 (cfs) =	0.48	
Q5 (cfs) =	2.22			Q5 (cfs) =	0.62	
Q100 (cfs) =	4.35			Q100 (cfs) =	1.21	

APPENDIX D

REFERENCES



Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations								
$I_{100} = -2.52 \ln(D) + 12.735$								
$I_{50} = -2.25 \ln(D) + 11.375$								
$I_{25} = -2.00 \ln(D) + 10.111$								
$I_{10} = -1.75 \ln(D) + 8.847$								
$I_5 = -1.50 \ln(D) + 7.583$								
$I_2 = -1.19 \ln(D) + 6.035$								
Note: Values calculated by equations may not precisely duplicate values read from figure.								

Please use DCM table 5-1 for runoff coefficients

Land Line on Cunface	Demonst	Runoff Coefficients											
Characteristics	Impervious	2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis													
Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when													
landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
o													
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.