

Updated geotech report to provide recommendations for the permanent detention/wqcv facilities per Drainage Criteria Manual Chapter 11 Section 11.2.2 and 11.3.3

FRONT RANGE GEOTECHN

Unresolved. This can be resolved by providing an addendum letter if you are unable to edit the original geotech report.

11.3.3 Embankment Structures

The width of the top of the embankment structure shall be a minimum of 12 feet for embankments less than 25 feet in height. Also, side slopes on embankment structures will vary with materials types used and shall be designed to produce a stable and easily maintained structure. A slope stability analysis shall be required on all Class 1 structures.

An allowance for settlement shall also be factored into the design for all embankment structures. Consideration shall also be given to limiting excessive seepage through the embankment and foundation that may lead to embankment erosion and structure instability for all Class 1 structures.

A geotechnical analysis and report prepared by a Colorado Professional Engineer with recommendations for the foundation preparation and embankment construction shall be submitted to the City/County Engineer with the complete design analysis for all permanent detention facilities.

11.2.2 Detention Facility Construction

The construction of detention facilities which multi-use benefits can provide significant benefits when properly planned and designed. Controlled outlets for flood surcharge storage should be provided, and it is required that such outlets be designed to release at a rate that does not exceed the peak rate estimated under natural conditions for the design storms, or other discharge established by policy and/or the drainage basin planning study.

Adequate safety measures shall be provided with all detention facilities. A minimum 15-foot maintenance easement shall be provided around the perimeter of the impoundment and embankment areas. Access to the bottom of the pond from a public road shall be provided via a minimum 15-foot wide ramp at a slope no greater than twelve (12) percent.

The geologic conditions of the site shall be investigated in sufficient detail to determine the suitability for impoundment of surface water. Ground water level increases downstream of the structure and the complexity of the local site geology.

Guidelines for conducting geotechnical investigations for State of Colorado jurisdictional dams are presented in the draft "Design Review Manual" for dams and dam safety (Colorado Office of the State Engineer, July 31, 1986).

A design engineer check list for State of Colorado jurisdictional dams is included as Attachment A of this chapter. For non-jurisdictional dams i.e., those that do not or would not fall under State of Colorado purview, the designer must evaluate the appropriate factors identified, in the engineer check list, for the hazard rating presented as Attachment A and as otherwise required by the City/County.

8/20/00

AMENDED June 25, 2022

- REVISED FIG 2 – PRELIMINARY GEOLOGIC
- REVISED FIG 3 – SEWAGE DISPOSAL CHAR
- LETTER REQUEST TO PCD DIRECTOR

June 25, 2022

Mr. Kevin Mastin, Interim Executive Director
El Paso County Planning & Community Development Department
2880 International Circle, Suite 110
Colorado Springs, CO. 80910

Re: Walden Preserve Subdivision 2, Fil 5 Final Plat Application – SF2211

Dear Mr. Mastin,

On April 14, 2022 PCD staff reviewed the Front Range Geotechnical Preliminary Geology, Surface Soils and Sewage Disposal Evaluation dated Aug 29, 2004 for the Walden Preserve 2, Filing 5 final plat application SF2211. The PCD review required that the Geotechnical Engineering Study be updated as “staff has concerns with evaluating the geologic constraints and hazards which may be present within the subdivision due to the significant difference to the plan layout since the report was prepared.” The review went on to say “Staff may consider using an older report if an exhibit is provided depicting the geologic hazards and constraints with the revised lot and street layout. It will be the determination of the PCD Director on whether this will be acceptable, pursuant to LDC Sec. 8.4.9.A.2.”

I am writing to request that PCD recognize the adequacy of the previously submitted and approved Front Range Geotechnical report as amended consistent with *LDC Sec. 8.4.9.A.2 - where a geology and soils report has been completed and reviewed at an earlier stage of the subdivision process, a new report may not be required if in the determination of the PCD Director the existing report provides the level of site-specific detail necessary to review the subdivision application, and the recommendations of the report and the Colorado Geological Survey (CGS) have been followed in the preparation of the preliminary plan.*

The following statements are offered in support of this application:

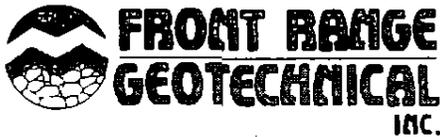
- Figures 2 & 3 within the report have been updated to reflect Front Range Geotechnical’s identified constraints on the current lot and roadway layout.
- No geologic hazards or constraints have been identified within Filing 5’s lots or roadways.
- The subdivision will be served by both central water and sewer eliminating geologic concerns and constraints related to onsite septic systems.
- The report has been utilized in obtaining numerous land use approvals including; Preliminary Plan, PUD Development Plan and Final Plat approvals for Filings 1 through 4.
- The Filing 5 Final Plat approval is the last of the Walden Preserve 2 development applications.

- Jonathan R. Lovekin, P.G. Senior Engineering Geologist, Colorado Geological Survey stated in his 4/5/2022 application review;
 - CGS has no objection to approval of the Final Plat as submitted.
 - Our previous review (8.15.14) remains valid. “Provided Front Range Geotechnical’s recommendations are adhered to, and lot-specific investigations and analyses are conducted for use in design of individual foundations and subsurface drainage systems,”
 - I agree that the site appears to be suitable for the proposed use and density.

Your time in consideration of this request is greatly appreciated. Should you have any questions or require additional documentation, please contact my office.

Respectfully submitted,

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August 29, 2004

Subject: Preliminary Geology, Surface Soils, and Sewage Disposal Evaluation
Walden Preserve Subdivision
El Paso County, Colorado

INTRODUCTION

The following report presents the results of a Preliminary Geologic, Surface Soils, and Sewage Disposal Evaluation for the proposed Walden Preserve Subdivision in El Paso County, Colorado. The report presents discussions of site geology and surface soils and our opinions of the potential effect of these conditions on development and sewage disposal. The information included in this report has been compiled from analysis of aerial photographs, a field reconnaissance and mapping of the site, review of studies on sites in close proximity, geologic research and analysis, and our experience in the area. Geologic conditions were mapped and evaluated by John Himmelreich & Associates. Front Range Geotechnical, Inc. (Front Range) performed 20 percolation tests on the site. In addition, Front Range drilled three test borings in an area of small lot development proposed in the southeast portion of the site. Conditions disclosed by additional surface, subsurface investigations and/or laboratory analysis might make revisions of the conclusions of this report appropriate.

PROPOSED DEVELOPMENT

The site is proposed for construction of a residential subdivision, with 87 residential lots with sizes of about 2.5 acres, and 73 smaller lots (see Figure 2). The larger (2.5-acre) lots will be served by individual wells and individual sewage disposal systems. The smaller lots will be served by both central water and wastewater systems.

SITE DESCRIPTION

The proposed Walden Preserve subdivision is located southeast of Walker Road and Highway 83 (see Figure 1). The site is an irregular-shaped parcel located in portions of Sections 14, 15, 22, and 23 Township 11 South, Range 66 West of the Sixth Principal Meridian. The Wastewater Treatment Plant for the Walden Development lies to the north of the site. Property to the east and west is currently rural residential. The property to the south is currently vacant.

Topographically, the site consists of a series of low ridges separated by swales and drainageways. Most of the slopes on the site range from about 3 to 20 percent with some small areas of slopes in excess of 30%. The site has numerous 'contour terraces' that parallel the contours of the land. A major drainageway runs through and borders the eastern part of the site. Two sizable ponds are located in this drainageway. The site is located in the West Cherry Creek drainage basin.

The majority of the site is dominated by grassland or prairie-type vegetation. Areas of dense to scattered ponderosa pine dominate the northeast part of the site. A few areas of lush grass are located in some of the smaller swales and drainageways, and in numerous locations in the larger drainageway. The site appears to have been used for grazing in the past with a few areas of disturbed ground and fill.

SITE GEOLOGY

The site is underlain by bedrock consisting of the Dawson Arkose (Figure 2). This formation consists primarily of discontinuous and lenticular beds of arkosic sandstone and claystone. Although the Dawson sandstones are commonly only slightly to moderately cemented, they are typically very dense. Few good outcrops (bedrock exposures) were observed on-site. The regional dip of the strata is very gentle to the north. Our experience in this area indicates the rocks are not highly fractured.

Overlying the bedrock are residual soils (weathered in-place), alluvium (water transported materials), and colluvium (slopewash). Some of the finer grained colluvial soils may be of wind-blown origin.

SITE GEOLOGY (CONTINUED)

Alluvial deposits are continuing to form to this day in the swales and drainageways. The alluvium and colluvium consists of poorly sorted silty to clayey sand and gravel, sandy silt, and sandy/silty clay. Based on the profile holes drilled for the percolation tests, the alluvium and colluvium ranges from a few feet to greater than 10 feet thick on the site.

The site is located in the Dawson Arkose (bedrock aquifer) in the Denver groundwater basin. This aquifer serves as the water supply for most wells in the immediate area. A perched water table is also often encountered in the alluvial deposits in the swales and drainageways, at least on a seasonal basis. The Soil Conservation Service (SCS) indicates that four mapping units are present on the subject site (71-Pring coarse sandy loam, 21-Cruckton sandy loam, 25-Elbeth sandy loam, and 92-Tomah-Crowfoot loamy sands). The SCS map is included as Figure 5.

RECOVERABLE RESOURCES

Under the provision of House Bill 1529, it was made a policy of the State of Colorado to preserve for extraction any commercial mineral resource located in a populous county. The El Paso County Aggregate Resource Evaluation (Map 1) October 1995 indicates that potential sand and gravel aggregate resources are located on the site; however, site observations and gradation test results of selected samples of the soil materials indicate these deposits are not likely to be an economic resource.

GEOLOGIC HAZARDS AND CONSTRAINTS

We believe that the subject site is relatively free from serious geologic hazards. The more significant geologic hazards recognized on the site are: 1) potential expansive soils/bedrock, 2) the potential for erosion, 3) and the potential for flooding. Other potential hazards include the stability of cut slopes, potential settlement of the surficial deposits, and the presence of corrosive minerals.

GEOLOGIC HAZARDS & CONSTRAINTS (CONTINUED)

Certain regional conditions (seismicity and radiation) also affect the site. The geologic hazards identified on this site are relatively common to the region and are mitigated by employing proper planning, investigation, design, and construction practices.

Geologic characteristics and constraints that will influence the location and design of individual sewage disposal systems include percolation rate, shallow bedrock, shallow groundwater, and slope. These constraints can be mitigated with engineered designed systems.

Construction and Development Considerations

There are geotechnical conditions that will influence development and construction on this site. While none of the conditions are believe to present an unacceptable risk, they should be considered. The following sections discuss our opinions of the conditions.

Trenching/Slopes

The sandy and silty soils underlying the site generally lack cohesion and therefore are prone to caving and sloughing on steep slopes and in excavations. Permanent cut slopes should either be laid back or supported with a retaining structure. Excavations in the surficial soils or areas where seepage is encountered may expose material which is poorly consolidated and which may be wet at least on a seasonal basis. Cuts in these soils should be treated with caution, especially in utility trenches.

Soil and Geotechnical Considerations

The surficial soils that underlie the site will have variable properties with regard to foundation support. The surficial soils are commonly of low-density and prone to settlement if heavily loaded. Hence low foundation bearing pressures are typically appropriate. Comparatively low bearing pressures normally are not a major concern for relatively light residential and commercial structures.

Soil and Geological Considerations (continued)

The silt and clay soils may be subject to hydrocompaction if heavily loaded or if they become saturated. Heavy concentrated loads may need to utilize deep foundations founded in the underlying bedrock. These factors are normally addressed in site-specific soil and foundation studies for each structure.

Some of the soils on the site are clay and probably possess expansion potential. The Dawson Arkose also contains lenses and layers of claystone. When in the presence of water, the clay minerals absorb the water and expand in volume. Pressures resulting from this expansion are commonly of a magnitude they could damage foundations or flatwork. Expansive soils are rather common in the Front Range of Colorado and techniques for mitigation are fairly well developed. It is therefore important that each structure be analyzed individually so the potential problem can be assessed and individual design measures taken to mitigate the hazard.

Corrosive minerals may be present in the soils, bedrock, or groundwater. Corrosive minerals can have detrimental effects on concrete and buried metals. This condition is normally addressed in a soils and foundation study for each structure.

Flooding and Erosion

As shown on the Preliminary Geologic Map (Figure 2), alluvium/colluvium is found in a band paralleling the swales and drainageways on site. Although the smaller drainageways do not appear to carry surface water most of the time, it appears that erosion and flooding from thunderstorm runoff occasionally occurs. It should be noted that no drainage study was performed as part of this report and the flood plain and hazard zone should be defined by a more detailed drainage report. The simplest mitigation for flooding is avoidance, although channelization or elevation of structures may be appropriate in some areas. The larger drainageway on the site is being avoided by development except for two road crossings.

Flooding and Erosion

The soils on the site are susceptible to erosion by both wind and water because the sandy and silty soils commonly have low cohesion. The potential for erosion should be addressed in an erosion control plan, which was not part of our scope of work. Disturbed areas should be re-vegetated as soon as possible after construction. The existing 'contour terraces' serve to reduce the potential for erosion. These features should be retained where possible.

Subsurface Drainage

The swales and drainageways on the site sometimes exhibit problems with subsurface drainage. The variable permeability characteristics of the surficial soils are such that the cleaner sands carry water, perched on lower permeability layers. Subsurface seepage will move laterally along the top of the lower permeability layers (commonly clay layers or bedrock) and either daylight on a slope (or in a foundation excavation), or follow the buried bedrock in the swales. Swales and drainageways are the areas where subsurface drainage is likely to be concentrated.

For individual structures, mitigation of subsurface drainage problems usually takes the form of perimeter drains around foundations. A gravity daylight for the perimeter drains is recommended if possible. The need for and capacity of these individual subsurface drainage systems should be based on an individual site analysis for each specific structure. The observation of the subsurface soil and moisture conditions in excavations for foundations should take seasonal variations and permeability characteristics of the subsurface materials into account.

Seismic Activity

This area, like most of central Colorado, is subject to a degree of seismic risk. The Colorado Geological Survey considers this area of Colorado to be in Seismic Risk Zone 2. We understand design for seismic forces is not required for residential structures in this zone. Wind loading may govern structural design.

Radiation Activity

There is not believed to be any unusual hazard from naturally occurring sources of radioactivity on this site. Most of Colorado is located in a geologic setting that is considered 'high' and all rocks contain some natural radioactive minerals. Small bodies of uranium-bearing rock have been found within the lower part of the Dawson Arkose in the southern portion of the Black Forest in Northgate, Kettle Creek Ranch, Briargate, and Wolf Ranch areas (Himmelreich, 1996 and 1997, and Himmelreich and Flynn, 1994). When encountered these deposits are usually small and of relatively low grade.

The principle hazard produced by soil and bedrock of the types that underlie the site are usually associated with radon gas, build-ups of which can be mitigated by providing increased ventilation of perimeter drains, basements and crawl spaces, and sealing of joints. Radon hazards are best mitigated at the building design and construction phases.

SEWAGE DISPOSAL

It is planned to use individual treatment systems for sewage disposal on the larger (2.5-acre) lots on this site. In areas that are unacceptable for standard soil absorption systems, alternate systems such as self contained systems, raised systems, or mounded systems may be used. There don't appear to be situations where an alternate disposal system cannot be utilized for lot sizes on the order of those proposed for this subdivision.

In order to evaluate site characteristics geologic mapping was performed and 20 percolation tests were performed (22% of the 87 lots). Drill Hole and test locations are shown on the attached Figure 2. Visual logs of the profile holes, a summary of percolation test results, and soil laboratory testing data can be found in Appendix A. Figure 3 is "Sewage Disposal Characteristics Map" and also shows slopes of 30% and greater.

Percolation Testing Procedure and Regulations:

The procedure for percolation testing for each hole location was to drill one four inch diameter profile hole to a maximum depth of 10 feet, and to drill an adjacent hole to a depth of approximately 30 inches for percolation testing. To aid in identifying site conditions, two additional soil profile borings were also drilled in the small lot area, but without performing percolation tests. Holes were drilled by a power driven auger drill rig. Visual logs of soil and bedrock profiles were obtained from drill cuttings, and Standard Penetration Tests (ASTM D-1586) were performed to obtain samples for visual examination and to verify bedrock depths. Selected samples were also tested in the laboratory (see Gradation Test Results with the Drill Logs).

The percolation test holes were filled with water and saturated prior to testing. The test procedure consisted of filling the hole with approximately six inches of water and measuring the drop in water level and corresponding time interval until the percolation rate stabilized. This type of percolation test is for the purpose of defining the overall general, but typical, percolation characteristics. Three-hole tests must be made on each lot prior to construction of the individual sewage disposal systems.

The Health Department regulations indicate that certain conditions must be satisfied for installation of soil absorption systems without special design. These are:

- The minimum depth allowed by the El Paso County Health Department is 21 inches from the ground surface to the bottom of a seepage bed or absorption trench. Bedrock or water tables must be at least four feet deeper. Therefore, bedrock or groundwater within approximately six feet of the surface constitutes unacceptable conditions for a standard absorption system.
- Unless designed by a Registered Professional Engineer and approved by the Health Department, no soil absorption system is permitted where the ground slope is in excess of 30%.
- Colorado State and El Paso County Health Department Regulations indicate that percolation rates faster than five minutes per inch or slower than sixty minutes per inch are unacceptable for soil absorption systems without special design.

Percolation Testing Procedures & Regulations (continued)

Percolation rates are controlled by soil characteristics that include grain size and gradation, amount of silt and clay, and density. Coarse, clean soils with little or no fine particles have fast percolation rates. Clayey sands, clays, silts and dense materials such as bedrock commonly have slower percolation rates.

Soil Conditions:

Based upon the geologic characteristics and constraints as observed, profile holes, and experience, sewage disposal characteristics and limitations have been analyzed. These various areas and limitations are shown on Figure 2 and 3, and a discussion of these follows.

Area I (Qc-Tda): Area I consists of that portion of the site characterized by thin to thicker surficial deposits and variable (but generally acceptable) percolation rates. These areas has been mapped as Qc-Tda on the enclosed Figure2 and are characterized by colluvial soils over the Dawson Arkose. With some exploration, it is felt that in most cases it will be possible to locate an acceptable soil absorption system in the Area I lots, although local slow percolation rates or shallow soils may be encountered in these areas and thus will require some form of alternate system.

Area II (Tda): Area II consists of that portion of the site interpreted to be underlain by shallow soils over weathered bedrock (mapped as Tda on Figure 2). In most of this area it is felt that bedrock may be too shallow and/or too impermeable for conventional soil absorption systems, and alternate systems will be required.

Area III (Qac), (sw): Area III consists of that portion of the site identified as being underlain by deeper soils (Qac on Figure 2), but might be characterized by seasonally wet conditions (sw) or shallow ground water, at least on a seasonal basis. In areas that are found to be outside the flood plain and possess shallow ground water, alternate systems will be required. Percolation rates are likely to be variable. The seasonally wet areas were mapped based on analysis of aerial photographs and

field observations. Additional areas of shallow groundwater may also be encountered on the site. The percolation rate measurements and depth to weathered bedrock are summarized on Table I (below). The results of the profile holes are also summarized below. No ground water was encountered in any of the profile holes.

TABLE I

Percolation Test Number	Percolation Rate	Depth to Weathered Bedrock
TH-1	53.3 minutes per inch	Greater than 10 feet
TH-2	26.7 minutes per inch	Greater than 10 feet
TH-3	22.9 minutes per inch	Greater than 10 feet
TH-4	14.5 minutes per inch	Greater than 10 feet
TH-5	160 minutes per inch	Greater than 10 feet
TH-6	22.9 minutes per inch	Greater than 10 feet
TH-7	32 minutes per inch	Greater than 10 feet
TH-8	20 minutes per inch	4 feet
TH-9	32 minutes per inch	Greater than 10 feet
TH-10	13.3 minutes per inch	Greater than 10 feet
TH-11	17.8 minutes per inch	Greater than 10 feet
TH-12	17.8 minutes per inch	Greater than 10 feet
TH-13	53.3 minutes per inch	2 feet
TH-14	53.3 minutes per inch	Greater than 10 feet
TH-15	20 minutes per inch	1 foot
TH-16	16 minutes per inch	2 feet
TH-17	26.7 minutes per inch	4 feet
TH-18	17.8 minutes per inch	8 feet
TH-19	13.3 minutes per inch	4 feet
TH-20	17.8 minutes per inch	Greater than 10 feet
TH-21	16 minutes per inch	3.5 feet

Only one percolation rate was measured as greater than 60 minutes per inch. The subsurface materials encountered in the profile holes consisted of deep to shallow surficial and residually weathered soils ranging from 1 to greater than 10 feet deep. Soil and residually weathered material consisted of silty to clayey sands, silts, and sandy clays. The underlying bedrock materials consisted of sandstones. No groundwater was encountered during drilling in any of the profile holes.

Slopes

Slopes in excess of 30% are shown on the attached Figure 3. Proper performance of conventional soil absorption systems requires that they be constructed on relatively shallow slopes. The El Paso County Health Department "Individual Sewage Disposal System Regulations" (1996) consider that on slopes in excess of 30%, soil absorption systems require special design in order to take into account the effect of the steeper topography. Few slopes in excess of 30% exist on the site. The El Paso County Subdivision Regulations (Interim Performance Guidelines) classify slopes in excess of 10% as being unique topographic conditions. Where acceptable percolation rate and depth to bedrock are found in these areas of steeper slopes (greater than 30%), disposal fields using special designs will be required.

Relationship to Surrounding Areas

The site's relationship to surrounding areas is shown on Figure 1. The Wastewater Treatment Plant for the Walden Development lies to the north of the site. West Cherry Creek is located about one-quarter to one-half miles to the west of the site. Two surface water ponds are located along the larger drainageway on the site. The developed portions of the Walden subdivision are located adjacent to the north and east of the site. A school lies adjacent to the smaller lot area in the northeast. The Walden III subdivision lies west of the site. Streams, lakes and other features in the area of the site are shown on Figure 1.

The closest proposed residence to the larger lot portion of the site will likely be a single family dwelling approximately 150 feet away. Potential leach fields across this subdivision would probably be located no closer than about 100 feet from proposed residences or existing residences. Adequate separation between wells and septic systems needs to be provided.

Since the underlying topography is largely controlled by the bedrock, sewage effluent is likely to flow in the subsurface toward the swales and drainageways, then off site in the subsurface soils. The individual sewage disposal systems constructed on the site will add effluent ('water') to the shallow

Relationships to Surrounding Area (continued)

subsurface. This shallow subsurface water (which includes the seasonally wet areas) is considered to be "surface water" and/or tributary to surface streams (West Cherry Creek). The seasonally wet areas are likely to increase in extent and duration on and down gradient from the site. It is not thought that with proper design, installation, and operation/maintenance of these systems that there will be adverse effects on or off the site.

Relationship to On-site Wells

Individual wells are proposed for the larger lots in the subdivision. The smaller lots will be served by a central water supply from wells within the area. The locations of listed wells in the immediate area are shown on Figure 4. The well data for these wells indicates that most (if not all) of the wells withdraw water from the bedrock aquifer. Our experience indicates that the Dawson is not recharged by surface waters (like sewage effluent). As long as adequate surface seals are (were) provided during well design and construction to prevent surface water from impacting the bedrock aquifers, and required setbacks are maintained, it appears that the potential for sewage effluent to contaminate the bedrock aquifers is low. As indicated previously, sewage effluent is likely to impact surface water and/or shallow groundwater. If any domestic-use wells in the immediate area withdraw from the alluvial aquifer, the water may have to be treated for parameters such as nitrates and phosphates.

Discussion:

At the time of house siting on each individual lot, it is extremely important that the engineer performing the percolation tests properly identifies all the geologic and soil related design factors that influence sewage disposal (percolation rate, depth to bedrock, and depth to groundwater). It is this combination of factors that determines the general type of individual sewage disposal system best suited for the site. It is also the responsibility of the testing engineer to evaluate soil properties and continuity of the materials for the total depth of the profile hole (and within the area of the proposed system).

Discussion (continued)

In most cases where sandstone bedrock was encountered in the profile holes, it was weathered and contained low to no cementation. Under these conditions, it is uncommon for open fractures to develop in bedrock of this type. Observed excavations in bedrock in other areas of the Black Forest confirm this.

In the context of this report, the term "weathered bedrock" denotes that this material has been derived from the weathering (in place) of the underlying bedrock formation (the Dawson Arkose). That is, the materials have not been transported to their position by geologically recent erosional and depositional processes like the surficial soil deposits have. Although soil-like in appearance, from the standpoint of sewage disposal characteristics, the weathered bedrock is different than the surficial soil deposits because it is usually found at a higher in-place density. Although easily drillable with commonly used drilling equipment, this higher density commonly results in slower percolation rates than the overlying surficial deposits. Cemented bedrock (the type of bedrock that would contain open fractures, and hence, not treat the effluent) was not encountered in any of the profile holes drilled on-site. Since the weathered bedrock is soil-like in terms of most of its physical properties, it is judged to be a suitable stratum for disposal of sewage effluent (assuming it exhibits acceptable percolation rates).

The El Paso County Regulations do not specifically prohibit absorption systems in weathered bedrock (assuming all other conditions are acceptable) and historically the Health Department has permitted absorption systems under these conditions.

Our experience has shown that unless a) one is very familiar with the geologic units; b) utilizes and analyzes fugitive drilling information (ease of drilling, etc.); c) observes and analyzes color and other physical material changes during drilling; d) verifies interpretations with standard penetration or other types of tests; and/or e) performs deeper percolation tests; the presence, position, and sewage disposal characteristics of weathered bedrock can be misinterpreted. This misinterpretation could

Discussion (continued)

Have a significant impact on the sewage disposal system designed and ultimately, the performance. As part of the percolation testing (as with all other tests in other subdivisions), the testing engineer needs to provide an evaluation of the weathered bedrock's acceptability for sewage disposal. Acceptable percolation rates in weathered bedrock materials were measured on this site and have been observed in similar geologic settings. Depth to weathered bedrock has been indicated on Table 1 and on the Drill Logs (Appendix A).

Sewage Disposal Conclusions:

In general, all the lots within the proposed development are suitable for installation of some type of on-site wastewater system. However, because of local areas of shallow bedrock and isolated slow percolation rates, many lots will require engineer-designed systems.

Based upon our experience in the Black Forest area, it is our opinion that the Walden Preserve property is similar to and typical of many developed subdivision regions in the Black Forest. The task of the engineers and builders in the Black Forest region has become one of matching the disposal process and approved systems with prevalent field conditions. With knowledgeable builders, proper siting and testing techniques, and some exploration on each lot, it is felt that on all lots two disposal fields can be located and will be able to utilize soil absorption type systems for individual sewage disposal in this subdivision. In all cases methods are available for an individual sewage disposal system on each and every lot in the subdivision. **It should be emphasized that due to the geologic characteristics and other constraints on this site many systems are likely to consist of an engineer-designed system.**

Potential buyers and builders of lots within the subdivision should be provided with a copy of this report so that they can be apprised of site conditions, constraints and recommendations.

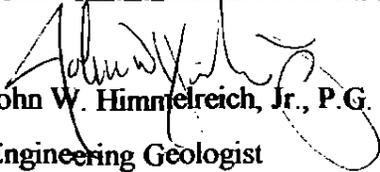
LIMITATIONS

The opinions presented in this report were developed from review of aerial photographs, topographic and geologic maps, site reconnaissance, profile holes and percolation tests, and research of published and unpublished information. Should additional surface or subsurface data become available, the conclusions and recommendations contained in this report shall not be considered valid unless the data are reviewed and the conclusions of this report are modified or approved in writing. If you have questions or require additional information, please contact us.

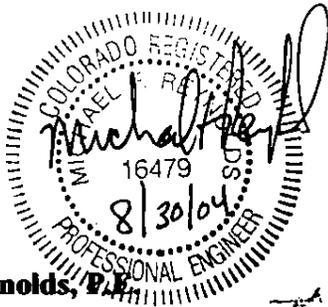
Respectfully,

FRONT RANGE GEOTECHNICAL, INC. &

JOHN HIMMELREICH & ASSOCIATES


John W. Himmelreich, Jr., P.G.
Engineering Geologist


Jeff Houchin
Geologist

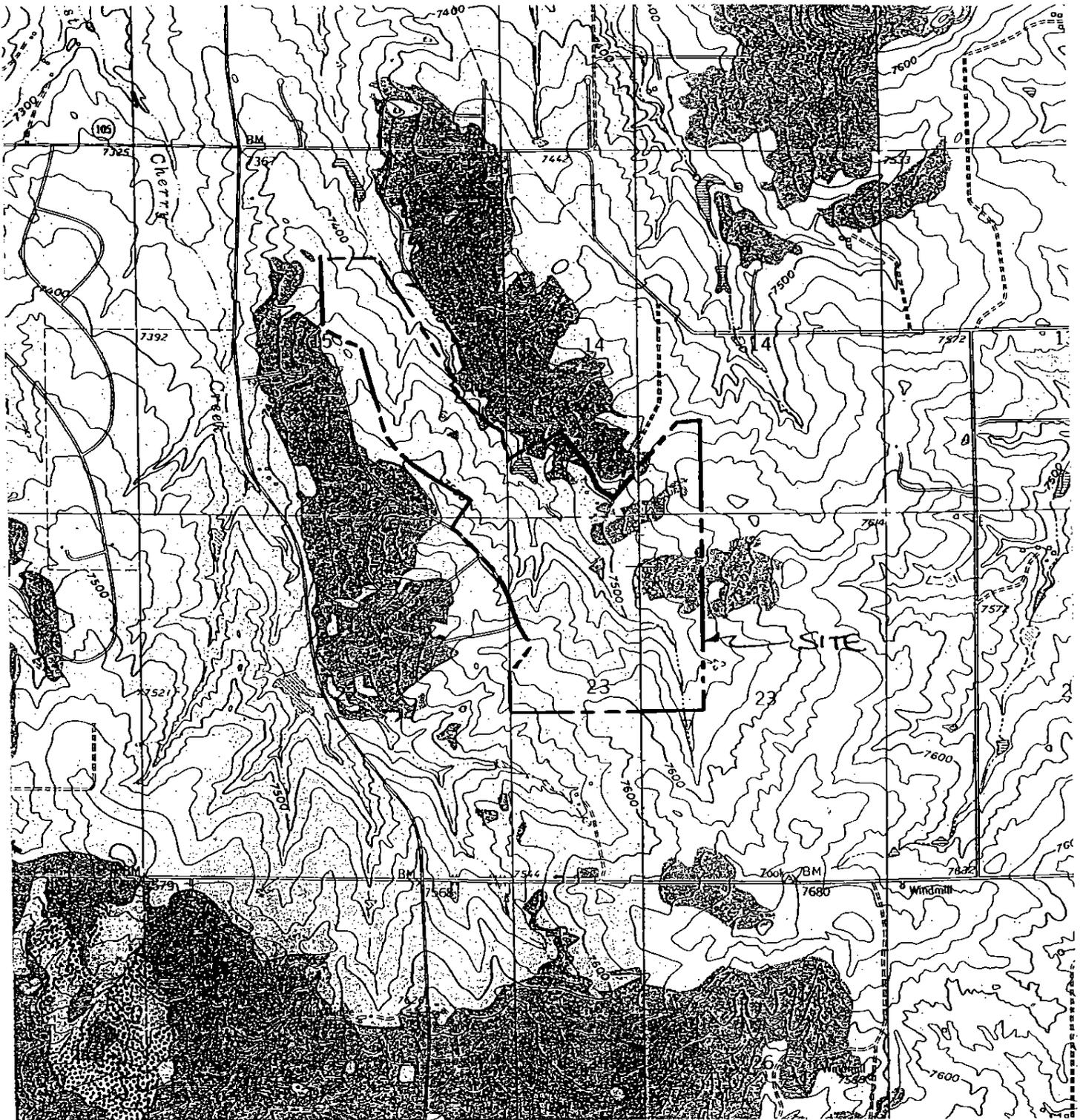


Michael F. Reynolds, P.E.
Civil Engineer

PARTIAL LIST OF REFERENCES

1. Himmelreich, J. W., Jr. (4-22-97). "Reconnaissance Geologic Hazards Study, Wolf Ranch Master Plan Area, Colorado Springs, Colorado". CTL/Thompson, Inc. Job No. CS-7272.
2. Himmelreich, J. W., Jr. (12-10-96). "Reconnaissance Geologic Hazards Study, Briargate Master Plan Area, Colorado Springs, Colorado". CTL/Thompson, Inc. Job No. CS-7040.
3. Himmelreich, J. W., Jr. and Flynn, A. B. (12-15-94). "Naturally Occurring Radioactive Materials, Briargate Master Plan Area, Colorado Springs, Colorado". CTL/Thompson, Inc. Job No. CS-5126.
4. El Paso County (10-11-96). "Individual Sewage Disposal System Regulations".
5. Colorado Geological Survey (1991). "Results of the 1987-88. EPA Supported Radon Study in Colorado". Colorado Geological Survey, Open-File Report 91-4.
6. Gazette Telegraph Articles: a. February 20, 1998 "Researchers Refine Range of Radon Risks". b. June 22, 1997 "Radon Found in Half of Tested Homes".
7. Johnson, E. J. and Himmelreich, J.W., Jr. (1998). "Geologic Hazards Avoidance or Mitigation: A Comprehensive Guide to State Statutes, Land Use Issues and Professional Practice in Colorado". Colorado Geological Survey Information Series 47.
8. El Paso County Land Use Department (1980). "Sourcebook, El Paso County, Colorado, Planning Information Base".
9. Trimble, D.E. and Machette, M.N. (1979). "Geologic Map of the Colorado Springs- Castle Rock Area; Front Range Urban Corridor, Colorado". U.S. Geological Survey, Miscellaneous Investigations Series, Map I-857-F.
10. Kirkham, R.M. and Rogers, W.P. (1981). "Earthquake Potential in Colorado, A Preliminary Evaluation". Colorado Geological Survey, Bulletin 43.
11. Frankel, A. and others (1996). "National Seismic-Hazard Maps: Documentation June 1996". U. S. Geological Survey Open-File Report 96-532.
12. Cochran, D. M. (1977). "El Paso County, Colorado: Potential Geologic Hazards and Surficial Deposits, Environmental and Engineering Geologic Maps and Tables for Land Use". Charles S. Robinson & Associates, Inc.

13. Himmelreich, J. W., Jr. and Noe, D. C. (1999). "Map of Areas Susceptible to Differential Heave in Steeply Dipping Bedrock, City of Colorado Springs, Colorado". Colorado Geological Survey Map Series 32.
14. Hill, J. J. (1974). "Environmental Resources Study for Teller and El Paso Counties Colorado, Part B: Geology". Resource Planning Associates, Inc.
15. Scott, G. R. and Wobus, R. A. (1973). "Reconnaissance Geologic Map of Colorado Springs and Vicinity, Colorado". U. S. Geological Survey Map MF-482.
16. Rogers, W. P., and others (1974). "Guidelines and Criteria for Identification and Land-Use Controls of Geologic Hazard and Mineral Resource Areas". Colorado Geological Survey, Special Publication 6.
17. Noe, D. C. (1999). "Geologic Hazards, Land-Use Laws, and Professional Standards of Practice in Colorado". Colorado Geological Survey, September 1999.
18. United States Department of Agriculture, Soil Conservation Service (1981). "Soil Survey of El Paso County, Colorado".
19. El Paso County Planning Department (October 1995). "El Paso County Aggregate Resource Evaluation, Map 1".



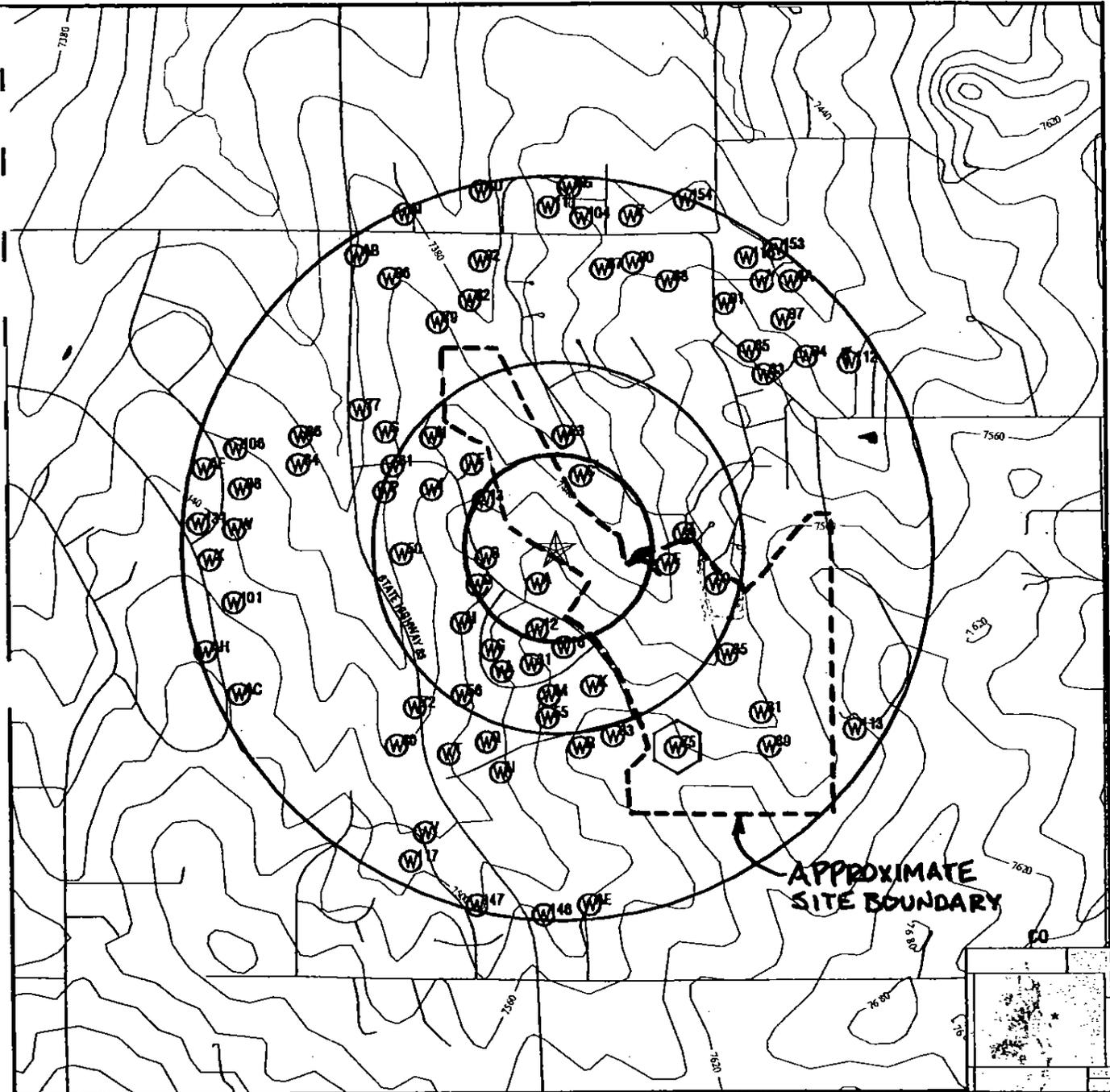
VICINITY MAP
FIGURE I

FIGURE # 2

FIGURE # 3

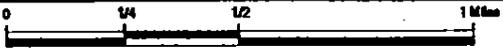
Are located in the rear pocket of this
folder.

PHYSICAL SETTING SOURCE MAP - 1018694.1s



- ↘ County Boundary
- ↘ Major Roads
- ↘ Contour Lines
- ⊙ Earthquake epicenter, Richter 5 or greater
- ⊙ Water Wells
- ⊙ Public Water Supply Wells
- Cluster of Multiple Icons

- ↓ Groundwater Flow Direction
- (GI) Indeterminate Groundwater Flow at Location
- (GY) Groundwater Flow Varies at Location
- Oil, gas or related wells

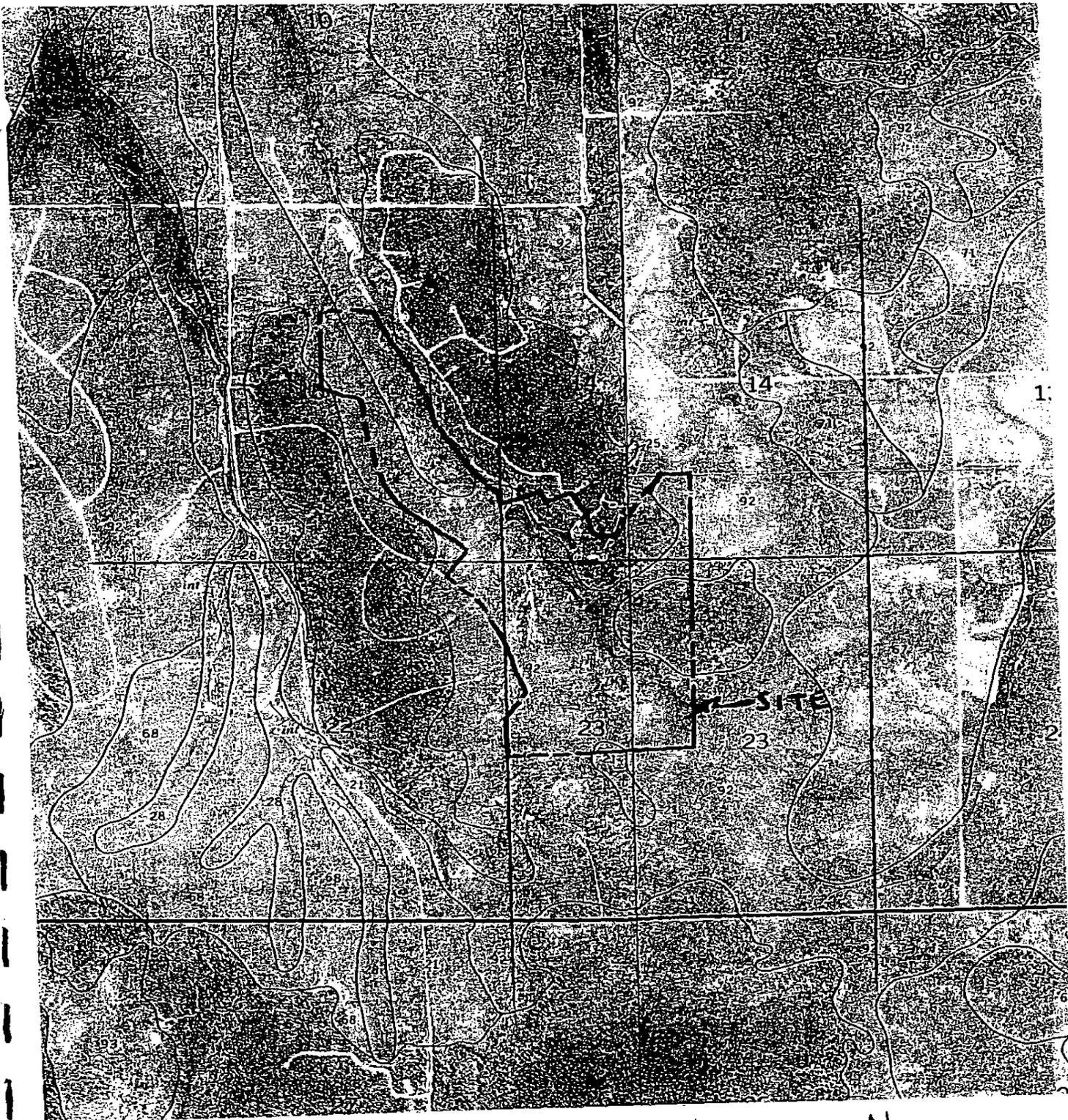


TARGET PROPERTY: Walden Village
ADDRESS: Pond View Place
CITY/STATE/ZIP: Colorado Springs CO 80908
LAT/LONG: 39.0876 / 104.7605

CUSTOMER: John Himmelreich & Associates
CONTACT: John Himmelreich
INQUIRY #: 1018694.1s
DATE: July 25, 2003 1:09 pm

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FIGURE 4



LEGEND

- 21 - CRUCKTON SANDY LOAM, 1-9% SLOPES
- 25 - ELBETH SANDY LOAM, 3-8% SLOPES
- 71 - PRING COARSE SANDY LOAM, 3-8% SLOPES
- 92 - TOMAH - LOAMY SANDS, 3-8% SLOPES

N
1" = 2000'

SCS SOILS MAP
FIGURE 5

21—Cruckton sandy loam, 1 to 9 percent slopes. This deep, well drained soil formed in arkosic sandy loam deposits on uplands. Elevation ranges from 7,200 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 115 days.

Typically, the surface layer is dark grayish brown sandy loam about 4 inches thick. The subsoil is grayish brown sandy loam about 24 inches thick. The substratum is pale brown loamy coarse sand.

Included with this soil in mapping are small areas of Peyton sandy loam, 1 to 5 percent slopes, Peyton sandy loam, 5 to 9 percent slopes, and Pring coarse sandy loam, 3 to 8 percent slopes.

Permeability of this Cruckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate to high. Surface runoff is slow to medium, and the hazard of erosion is moderate. In places runoff from snowmelt in spring causes rills and small gullies to form in cultivated fields.

Most of this soil is in native grass that is used for grazing livestock. A small acreage on some of the more gentle slopes is used for small grain and corn for silage.

Native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. The soil is subject to invasion by Kentucky bluegrass and Gambel oak. Noticeable forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Proper location of livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. Special design of roads and streets is needed because of frost action. Installation of drains helps to control surface runoff and keeps soil losses to a minimum. Capability subclass VIe.

25—Elbeth sandy loam, 3 to 8 percent slopes. This deep, well drained soil formed in material transported from arkose deposits on uplands. Elevation ranges from 7,300 to 7,600 feet. The average annual precipitation is about 18 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 120 days.

Typically the surface layer is very dark grayish brown sandy loam about 3 inches thick. The subsurface layer is light gray loamy sand about 20 inches thick. The subsoil is brown sandy clay loam about 45 inches thick. The substratum is light brown sandy clay loam.

Included with this soil in mapping are small areas of Tomah-Crowfoot loamy sands, 3 to 8 percent slopes; Kettle gravelly loamy sand, 3 to 8 percent slopes; and Peyton-Pring complex, 3 to 8 percent slopes.

Permeability of this Elbeth soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is high. Surface runoff is slow to medium, and the hazard of erosion is moderate.

This soil is used for woodland, limited livestock grazing, recreation, wildlife habitat, and homesites.

This soil is suited to the production of ponderosa pine. It is capable of producing about 2,240 cubic feet, or 4,900 board feet (International rule), of merchantable timber per acre from a fully stocked, even-aged stand of 80-year-old trees. Conventional methods can be used for harvesting, but operations may be restricted during wet periods. Reforestation, after harvesting, must be carefully managed to reduce competition of undesirable understory plants.

Woodland wildlife, such as mule deer and wild turkey, is attracted to this soil because of its potential to produce ponderosa pine, Gambel oak, and various grasses and shrubs. Water developments, such as guzzlers, would enhance populations of wild turkey as well as other kinds of wildlife. Where wildlife and livestock share the same range, proper grazing management is needed to prevent overuse and to reduce competition. Livestock watering facilities would also benefit wildlife on this soil.

This soil has good potential for homesites. The main limitation is the moderate shrink-swell potential in the subsoil. Special road design is necessary on this soil to overcome the limitations of shrink-swell potential and frost action. Special planning is needed on this soil to minimize site disturbance and tree and seedling damage. During seasons of low precipitation, fire may become a hazard to homesites on this soil. The hazard can be minimized by installing firebreaks and reducing the amount of potential fuel on the forest floor. Capability subclass VIe.

71—Pring coarse sandy loam, 3 to 8 percent slopes. This deep, noncalcareous, well drained soil formed in sandy sediment derived from arkosic sedimentary rock on valley side slopes and on uplands. Elevation ranges from 6,800 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 120 days.

Typically, the surface layer is dark grayish brown coarse sandy loam about 4 inches thick. The substratum is dark grayish brown coarse sandy loam about 10 inches thick over pale brown gravelly sandy loam that extends to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Alamosa loam, 1 to 3 percent slopes, along drainageways; Cruckton sandy loam, 1 to 9 percent slopes; Peyton sandy loam, 1 to 5 percent slopes; Peyton sandy loam, 5 to 9 percent slopes; and Tomah-Crowfoot loamy sands, 3 to 8 percent slopes. In some places arkose beds of sandstone and shale are at a depth of 0 to 40 inches.

Permeability of this Pring soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is medium, and the hazard of erosion is moderate.

Almost all areas of this soil are used as rangeland. Some areas previously cultivated have been reseeded to grass. This soil is also used for wildlife habitat and homesites.

This soil is well suited to the production of native vegetation suitable for grazing by cattle and sheep. Rangeland vegetation is mainly mountain muhly, little bluestem, needleandthread, Parry oatgrass, and junegrass.

Deferment of grazing in spring helps to maintain vigor and production of the cool-season bunchgrasses. Fencing and properly locating livestock watering facilities help to control grazing.

Windbreaks and environmental plantings generally are suited to this soil. The hazard of soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil is well suited for use as homesites. Erosion control practices are needed to control soil blowing and water erosion on construction sites where the ground cover has been removed. Capability subclass IVe.

92—Tomah-Crowfoot loamy sands, 3 to 8 percent slopes. These gently sloping to moderately sloping soils are on alluvial fans, hills, and ridges in the uplands. Elevation ranges from about 7,300 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 42 degrees F, and the average frost-free period is about 120 days.

The Tomah soil makes up about 50 percent of the complex, the Crowfoot soil about 30 percent, and other soils about 20 percent.

Included with these soils in mapping are areas of Elbeth sandy loam, 3 to 8 percent slopes; Kettle gravelly loamy sand, 3 to 8 percent slopes; and Pring coarse sandy loam, 3 to 8 percent slopes.

The Tomah soil is deep and well drained. It formed in alluvium or residuum derived from arkose beds. Typically, the surface layer is dark grayish brown loamy sand about 10 inches thick. The subsurface layer is very pale brown coarse sand about 12 inches thick. The subsoil, about 26 inches thick, is a matrix of very pale brown coarse sand in which are embedded many thin bands and lamellae of pale brown coarse sandy clay loam. The substratum is very pale brown coarse sand to a depth of 60 inches or more.

Permeability of the Tomah soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate.

The Crowfoot soil is deep and well drained. It formed in sediment weathered from arkosic sandstone. Typically, the surface layer is grayish brown loamy sand about 12 inches thick. The subsurface layer is very pale brown sand about 11 inches thick. The subsoil is light yellowish brown sandy clay loam about 13 inches thick. The substratum is very pale brown coarse sand to a depth of about 68 inches.

Permeability of the Crowfoot soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate.

This complex is used as rangeland, for wildlife habitat, and as homesites.

Native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. These soils are subject to invasion by Kentucky bluegrass and Gambel oak. Noticeable forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Properly locating livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings are fairly well suited to these soils. Blowing sand and moderate available water capacity are the principal limitations for the

establishment of trees and shrubs. The soils are so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

These soils are best suited to habitat for openland wildlife such as pronghorn antelope and sharp-tailed grouse. Although sharp-tailed grouse are not plentiful, they could be encouraged on these soils, especially where brush species are interspersed with grasses and forbs. If these soils are used as rangeland, wildlife production can be increased by managing livestock grazing to preclude overuse of the more desirable grass species and depletion of the various brush species.

These soils have good potential for use as homesites. The main limitation of the Crowfoot soil is frost-action potential. Roads and streets need to be designed to minimize frost-heave damage. Maintaining the existing vegetation on building sites during construction helps to control erosion. Capability subclass IVe.

APPENDIX A



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

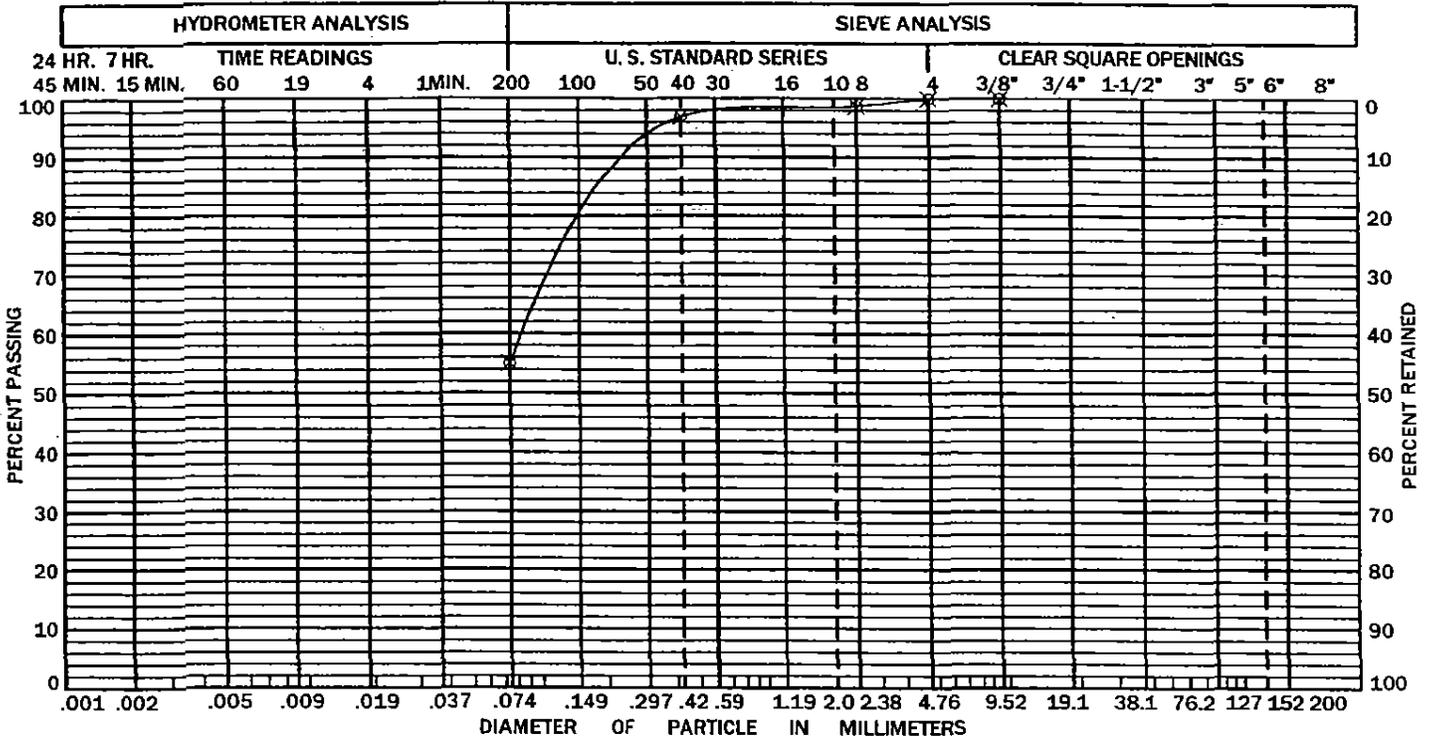
JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
11411						
TEST BORING NO.: TH-1						
DATE: 05/12/2003						
0-6" <u>TOPSOIL</u>	0-6	XXXX				
6"-10' <u>SILT</u>	6-10					
fine grained						
moderate density						
moderate-high moisture content				40 12"	11.7	
moderate sand content						
low plasticity						
dark grey color						
density decreases w/depth						
	10			20 12"	6.0	ML
	12					
	14					
	16					
	18					
	20					

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	
CLASSIFICATION <u>ML</u>	NOTES: <u>6.0 % Moisture content</u>					
GRAVEL <u>0.0 %</u>	<u>LL = 23.6 %</u>					
SAND <u>45.5 %</u>	<u>PL = 20.7 %</u>					
FINES <u>54.5 %</u>	<u>PI = 2.9 %</u>					
SAMPLE# <u>1</u> HOLE# <u>TH-1</u> DEPTH <u>10</u> FEET	<u>Job #: 11411 By: KO 05/13/2003</u>					



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-2

DATE: 05/12/2003

0-6" TOPSOIL

6"-10' SAND

fine grained

moderate density

moderate-high
moisture content

moderate clay content

moderate plasticity

tan color

density decreases
w/depth

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
6-10'	Diagonal lines				
4.0		26 12"	13.4		SM/ SC
10.0		10 12"	12.7		
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					

JOB#:

TEST BORING
NO.:

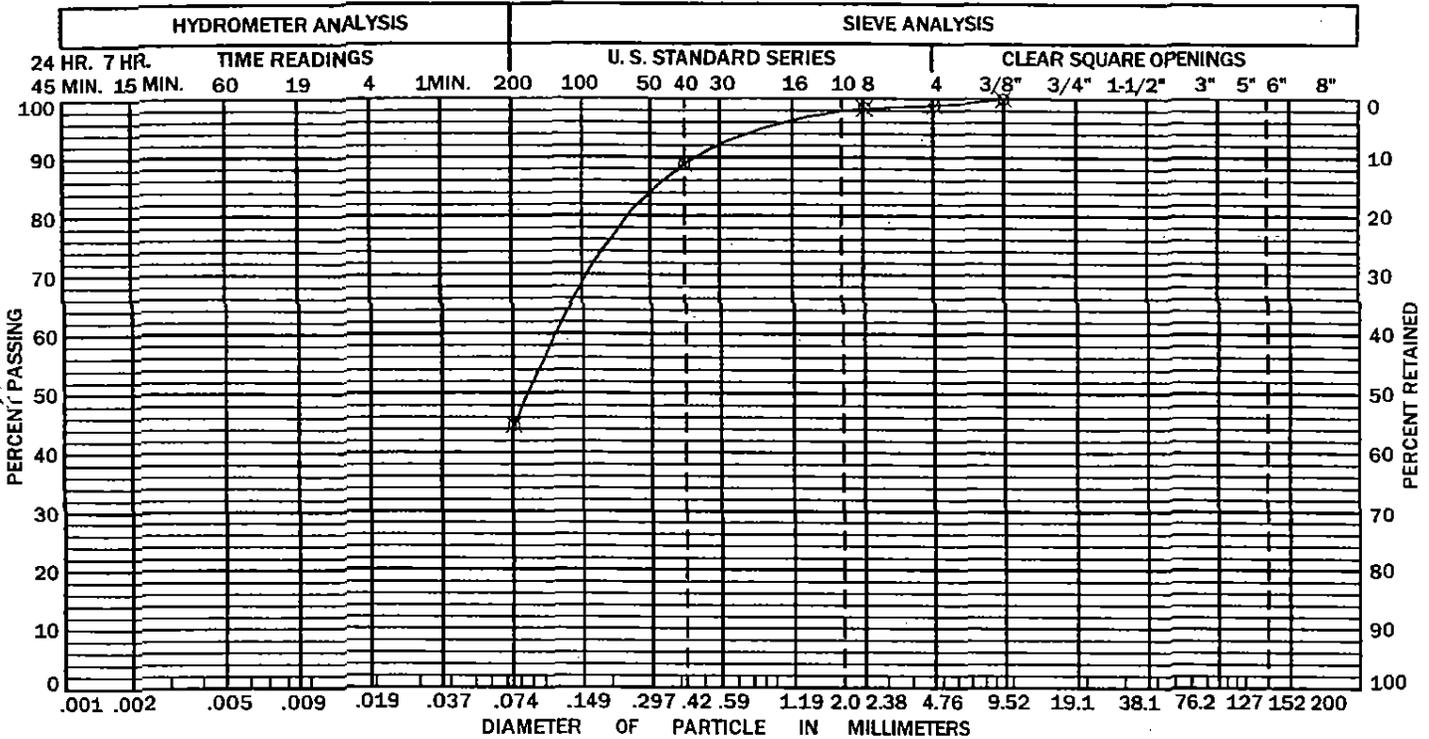
DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS

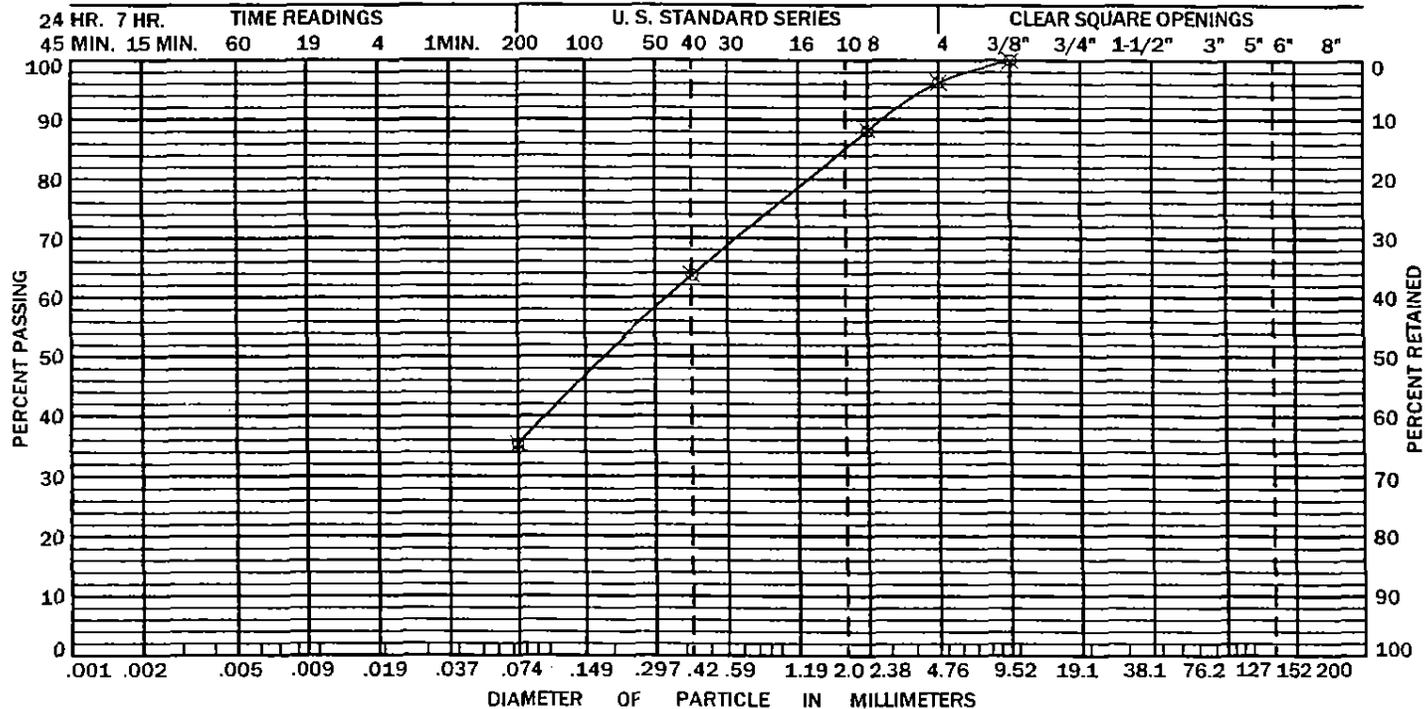
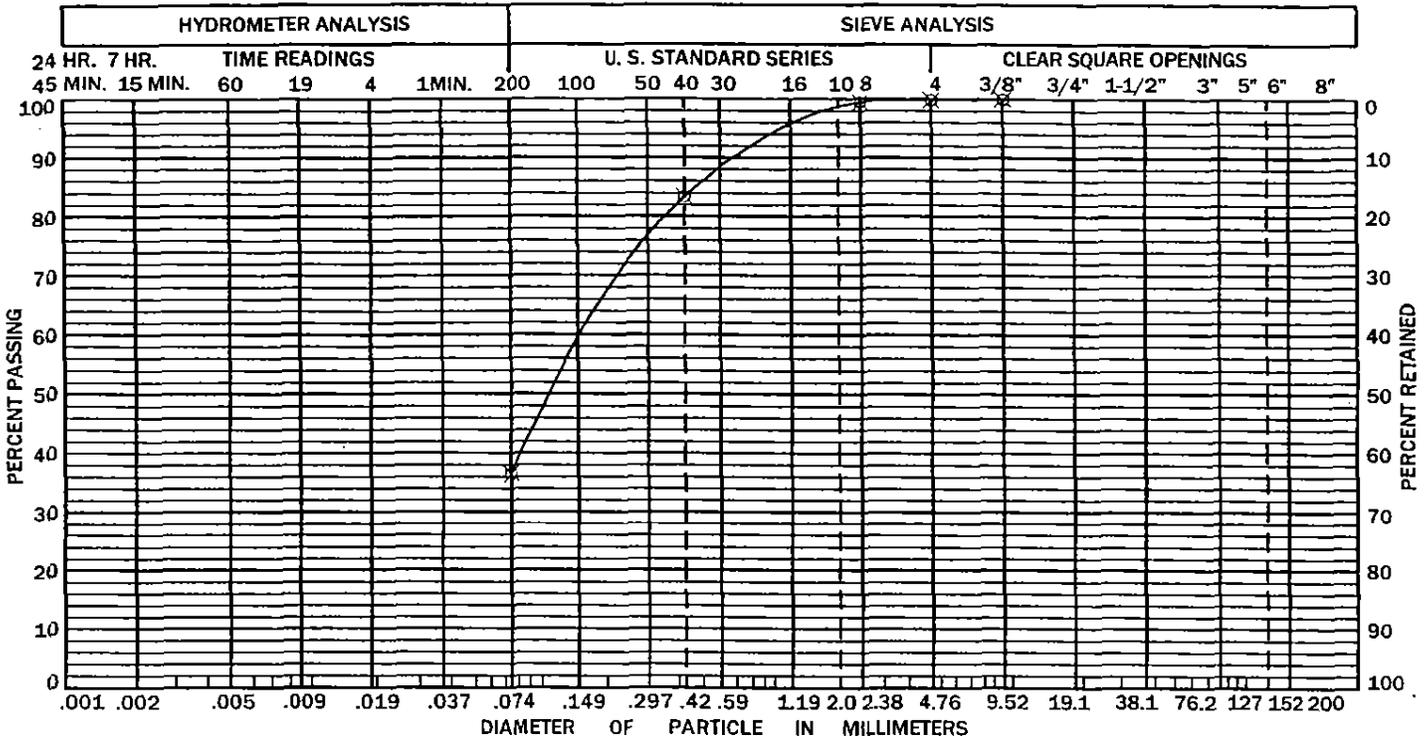


CLASSIFICATION	SM/SC	SAND			GRAVEL		COBBLES
		FINE	MEDIUM	COARSE	FINE	COARSE	
GRAVEL	0.2 %						
SAND	55.3 %						
FINES	44.5 %						
SAMPLE# <u>1</u> HOLE# <u>TH-2</u> DEPTH <u>4</u> FEET		NOTES: <u>13.4 % Moisture content</u>					
		<u>LL = 23.4 %</u>					
		<u>PL = 18.6 %</u>					
		<u>PI = 4.8 %</u>					
		<u>Job #: 11411</u>		<u>By: KO</u>		<u>05/13/2003</u>	



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS





**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

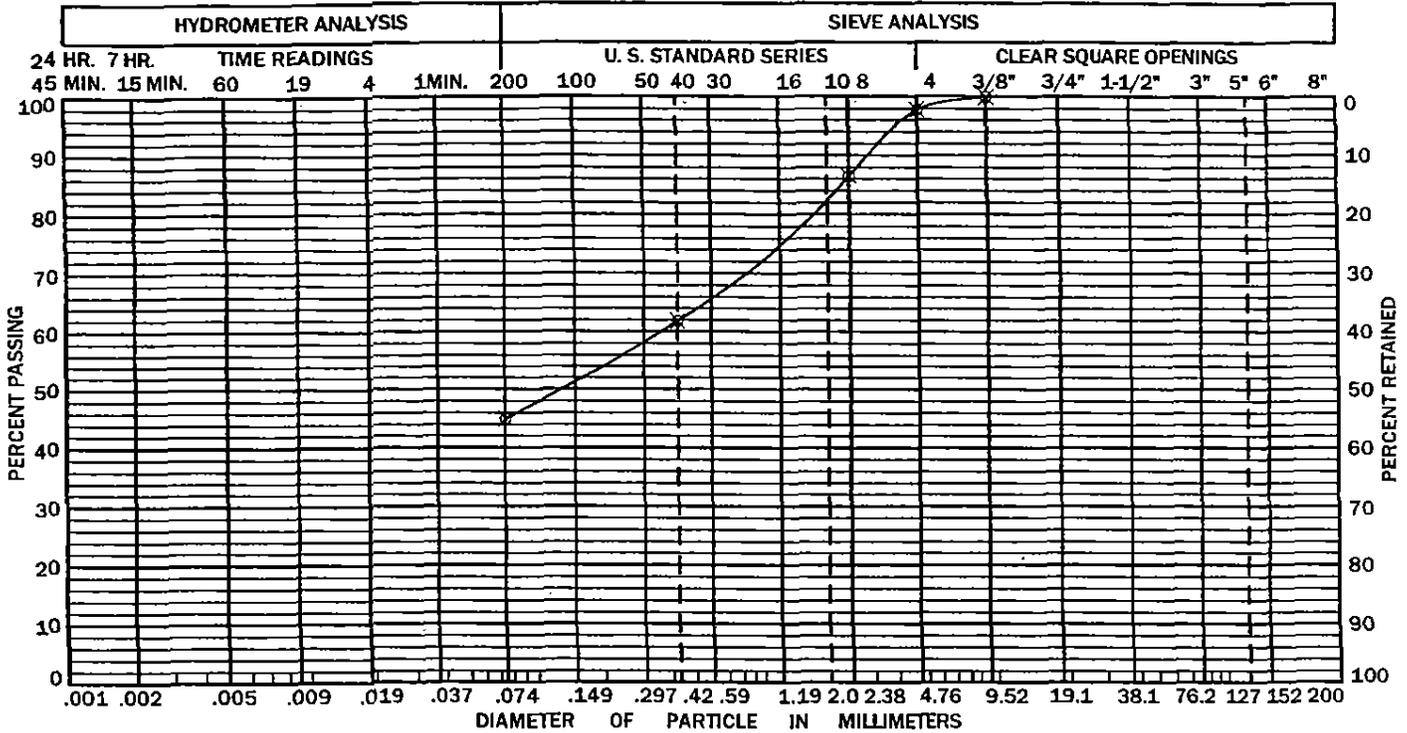
JOB#: 11411	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING JO.: TH-4						
DATE: 05/12/2003						
0-6" <u>TOPSOIL</u>	0-6	XXXX				
6"-10' <u>SAND</u>	6-10	Diagonal lines				
fine grained						
high density						
moderate moisture content				$\frac{39}{12}$	7.2	SC
moderate clay content						
moderate plasticity						
tan color						
density decreases w/depth				$\frac{18}{12}$	10.0	
	20					

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SC
 GRAVEL 2.3 %
 SAND 52.8 %
 FINES 44.9 %
 SAMPLE# 1 HOLE# TH-4 DEPTH 10 FEET

NOTES: 10.0 % Moisture content
LL = 28.2 %
PL = 20.0 %
PI = 8.2 %
 Job #: 11411 By: KO 5/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

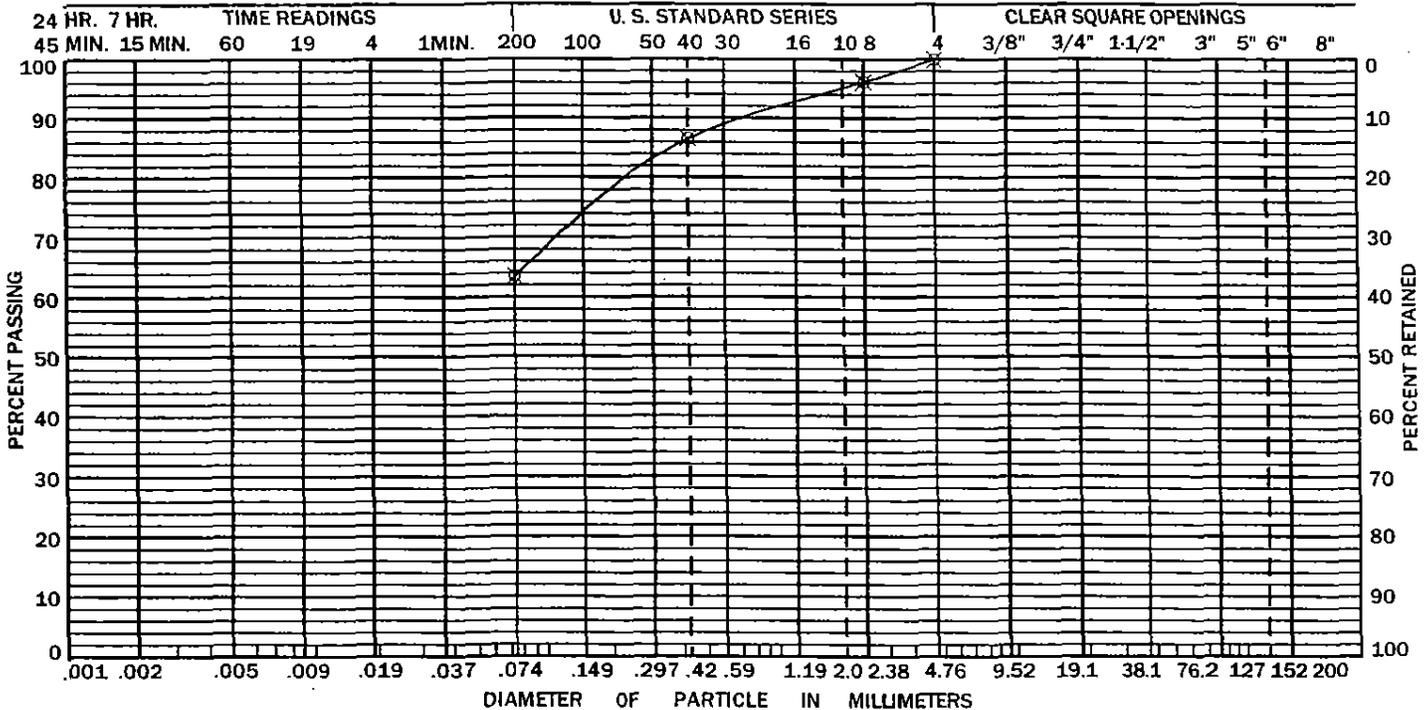
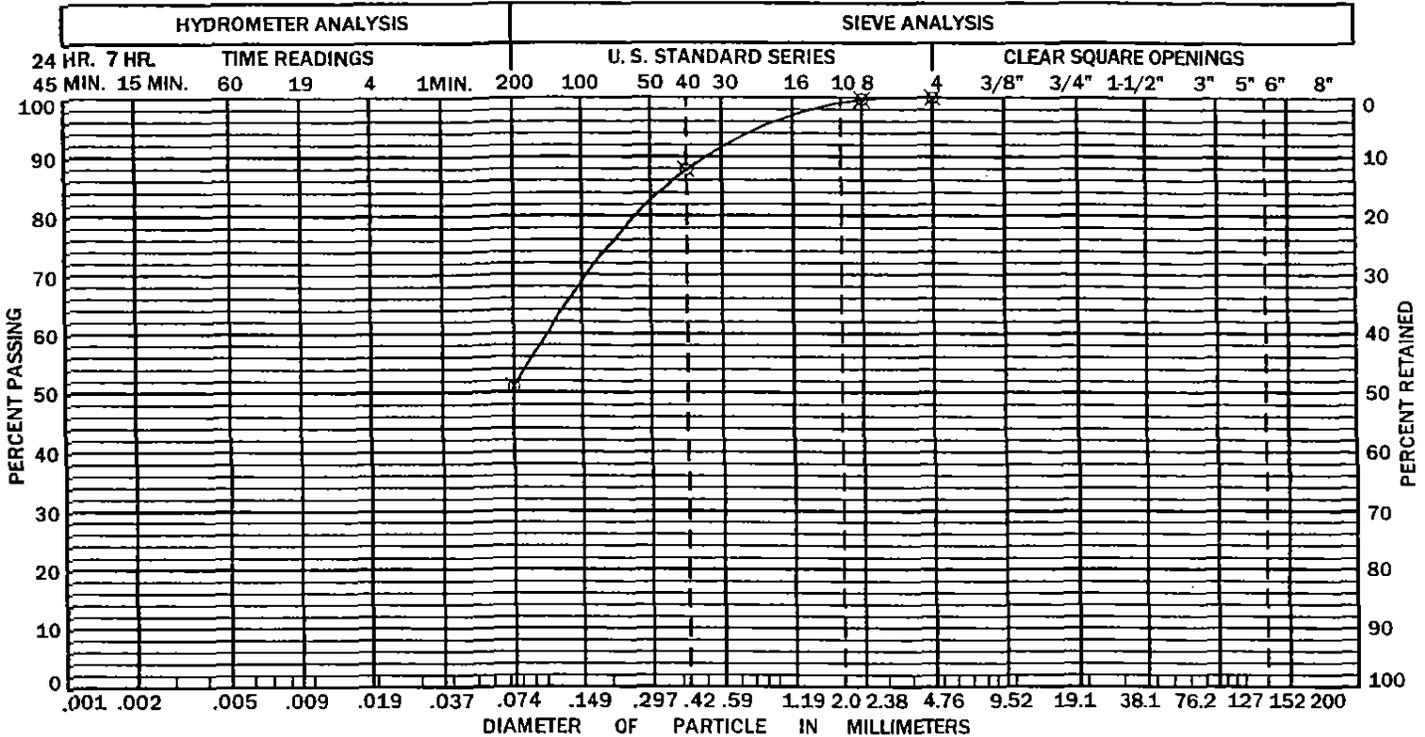
JOB#: 11411	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.: TH-5						
DATE: 05/12/2003						
0-6" <u>TOPSOIL</u>	0-6"	XXXX				
6"-5' <u>SILT</u>	6-11'					
fine grained	2			$\frac{10}{12}$ "	13.7	ML
low-moderate density	4			$\frac{13}{12}$ "	7.4	
moderate moisture content	6					
moderate sand content	8					
low plasticity	10			$\frac{11}{12}$ "	14.5	CL/ML
tan color	12					
5'-10' <u>SILTY/CLAY</u>	14					
fine grained	16					
low-moderate density	18					
moderate-high moisture content	20					
moderate sand content						
moderate plasticity						
olive brown color						

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



Job #: 11411 By: KO 5/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

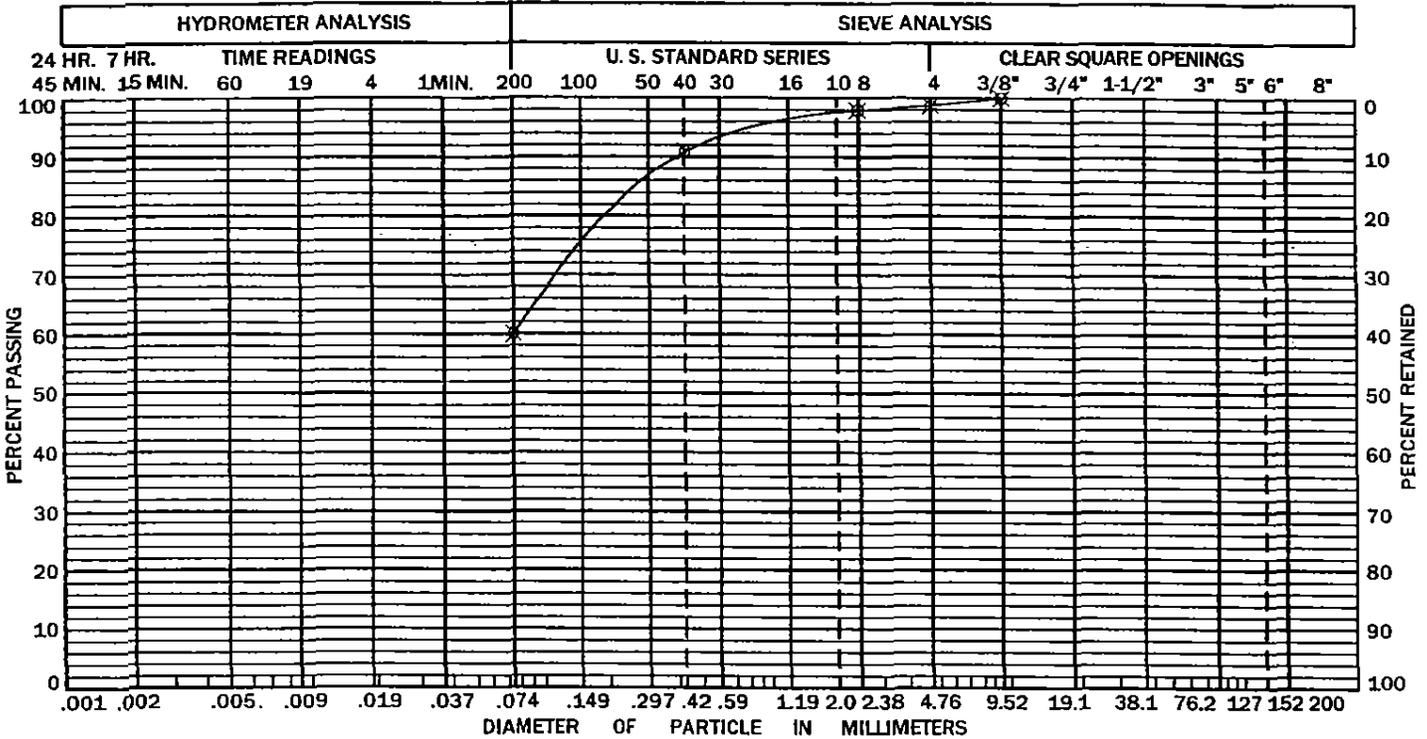
JOB#: 11411	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.: TH-6						
DATE: 05/12/2003						
0-6" <u>TOPSOIL</u>	0-6	XXXX				
6"-10' <u>CLAY</u>	6-10	Diagonal lines				
fine grained						
moderate density						
moderate moisture content				13 12"	12.7	
low sand content						
moderate plasticity						
tan color						
density decreases w/depth						
	10			8 12"	14.4	CL
	12					
	14					
	16					
	18					
	20					

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION CL
 GRAVEL 0.3 %
 SAND 39.5 %
 FINES 60.2 %
 SAMPLE# 1 HOLE# TH-6 DEPTH 10 FEET

NOTES: 14.4 % Moisture content
LL = 26.3 %
PL = 17.9 %
PI = 8.4 %
 Job #: 11411 By: KO 05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
11411						
TEST BORING NO.: TH-7						
DATE: 05/12/2003						
0-6" <u>TOPSOIL</u>	0	xxx				
6"-10' <u>SILT</u>	6					
fine grained						
moderate densitiy						
moderate moisture content				$\frac{21}{12}$	9.7	ML
low sand content						
low plasticity						
tan color				$\frac{18}{12}$	6.8	
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-8

DATE: 05/12/2003

0-6" TOPSOIL
6"-4' SAND
fine grained
moderate density
moderate moisture
content
low clay content
low plasticity
tan color
4'-10' SANDSTONE
fine-medium grained
very-high density
moderate moisture
content
low clay content
low plasticity
buff color

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
6"-4'					
46 12"		■	46 12"	6.5	SM
54 12"		■	54 12"	7.3	

JOB#:

TEST BORING
NO.:

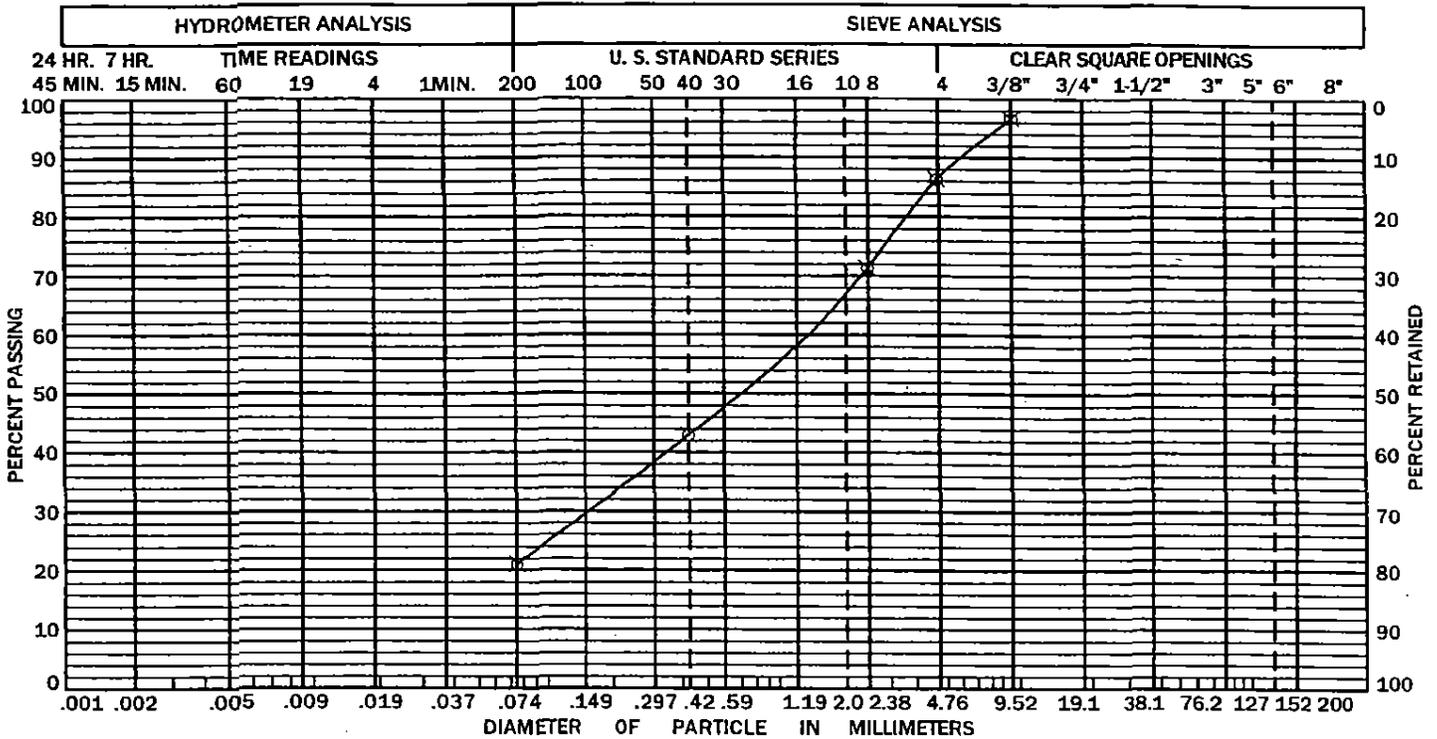
DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SM
 GRAVEL 14.3 %
 SAND 64.7 %
 FINES 21.0 %
 SAMPLE# 1 HOLE# TH-8 DEPTH 4 FEET

NOTES: 6.5 % Moisture content
LL = 20.6 %
PL = 17.9 %
PI = 2.7 %
 Job #: 11411 By: KO 05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-9

DATE: 05/12/2003

0-6" TOPSOIL

6"-10' CLAY

very-fine grained

moderate density

moderate-high
moisture content

low sand content

moderate plasticity

tan color

DEPTH (in ft.)

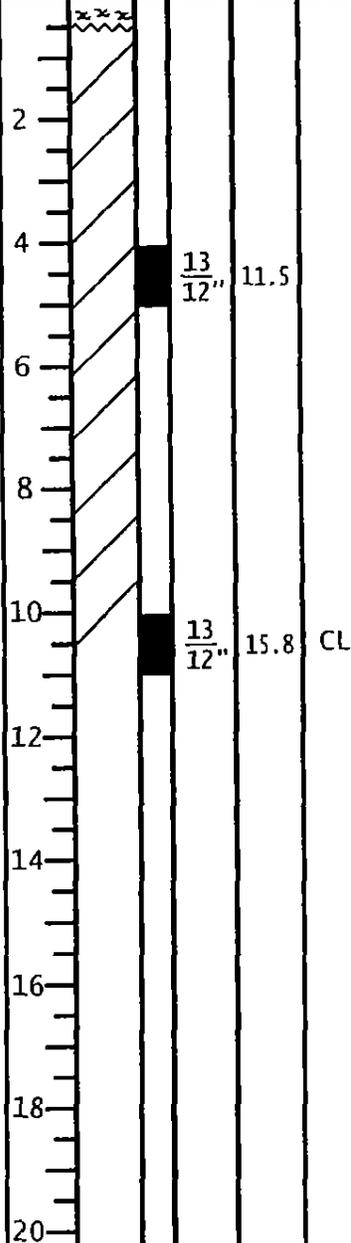
SYMBOL

SAMPLES

BLOW COUNT

WATER %

SOIL TYPE



JOB#:

TEST BORING
NO.:

DATE:

DEPTH (in ft.)

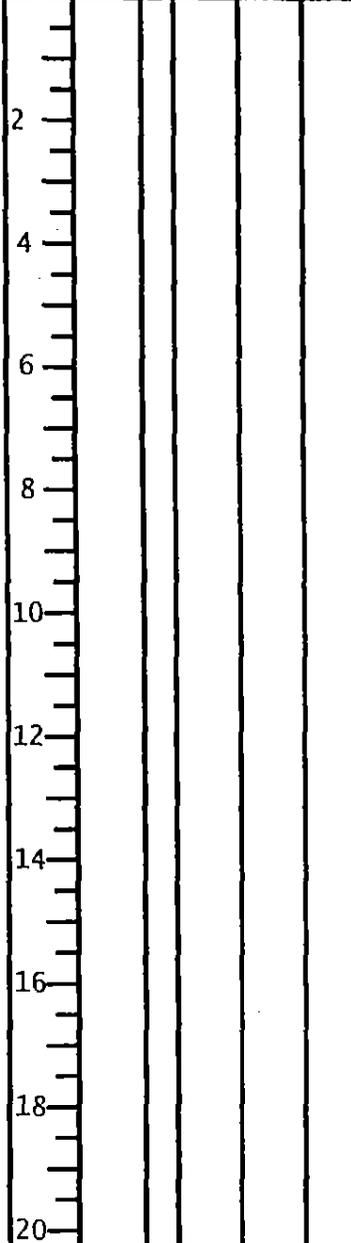
SYMBOL

SAMPLES

BLOW COUNT

WATER %

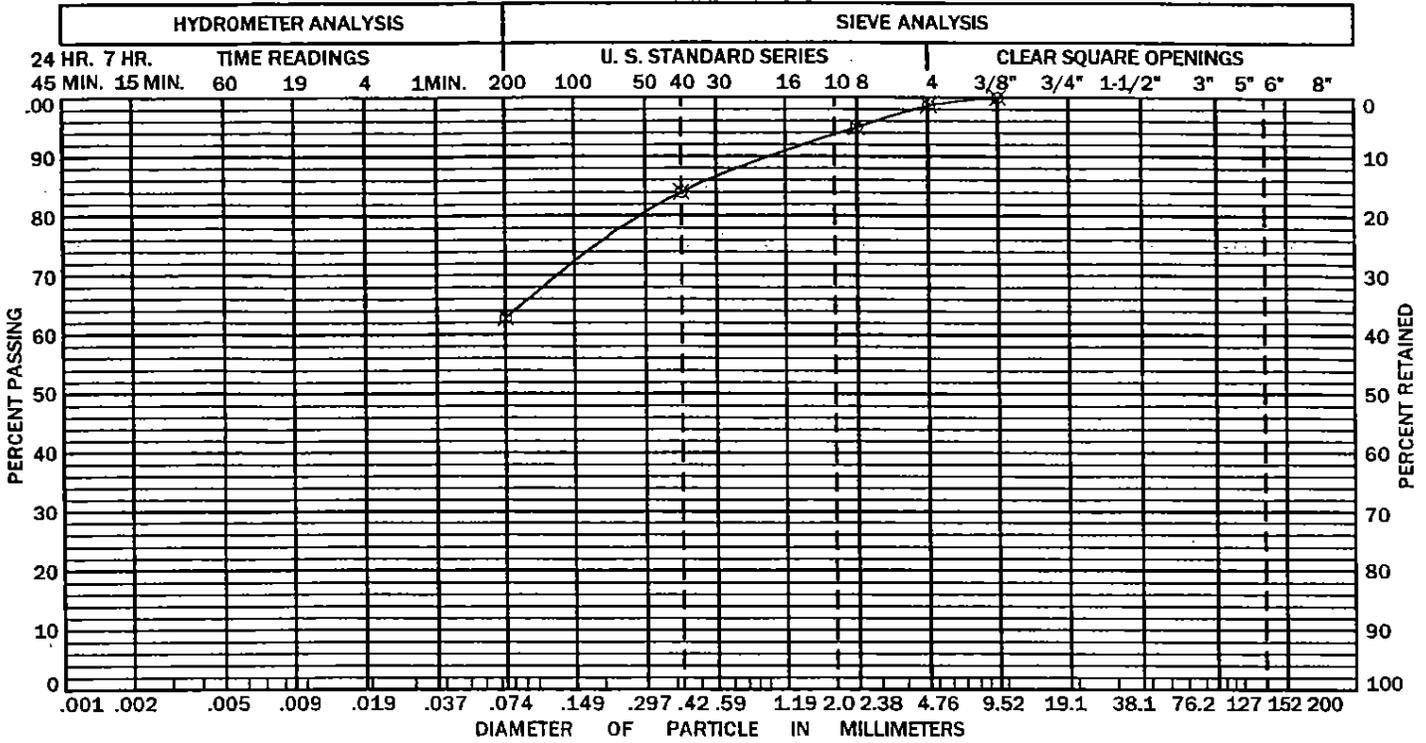
SOIL TYPE





FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLASSIFICATION	CLAY TO SILT	SAND			GRAVEL		COBBLES
		FINE	MEDIUM	COARSE	FINE	COARSE	
CL							
GRAVEL	1.0 %						
SAND	36.2 %						
FINES	62.8 %						
SAMPLE#	1	HOLE#	TH-9	DEPTH	10	FEET	

NOTES: 15.8 % Moisture content

LL = 28.6 %

PL = 21.1 %

PI = 7.5 %

Job #: 11411 By: KO 05/11/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

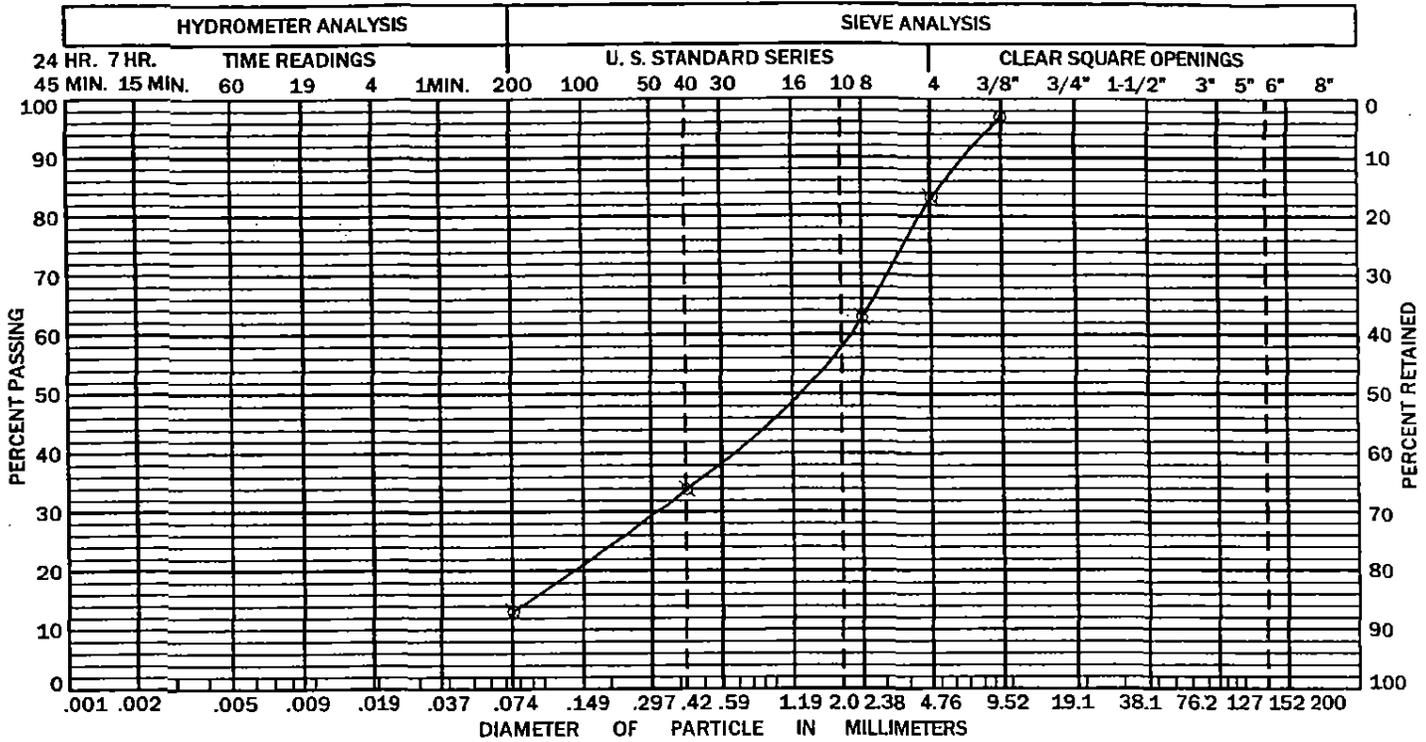
JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
11411	0-6"	XXXX				
TEST BORING NO.: TH-10	6"-10'	Diagonal lines				
DATE: 05/12/2003	2					
0-6" <u>TOPSOIL</u>	4			20	7.3	
6"-10' <u>SAND</u>	6					
fine-medium grained	8					
moderate density	10			22	9.7	SC
moderate moisture content	12					
moderate clay content	14					
moderate plasticity	16					
tan color	18					
	20					

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
	2					
	4					
	6					
	8					
	10					
	12					
	14					
	16					
	18					
	20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SC
 GRAVEL 16.9 %
 SAND 60.3 %
 FINES 22.8 %

SAMPLE# 1 HOLE# TH-10 DEPTH 10 FEET

NOTES: 9.7 % Moisture content

LL = 26.4 %

PL = 19.2 %

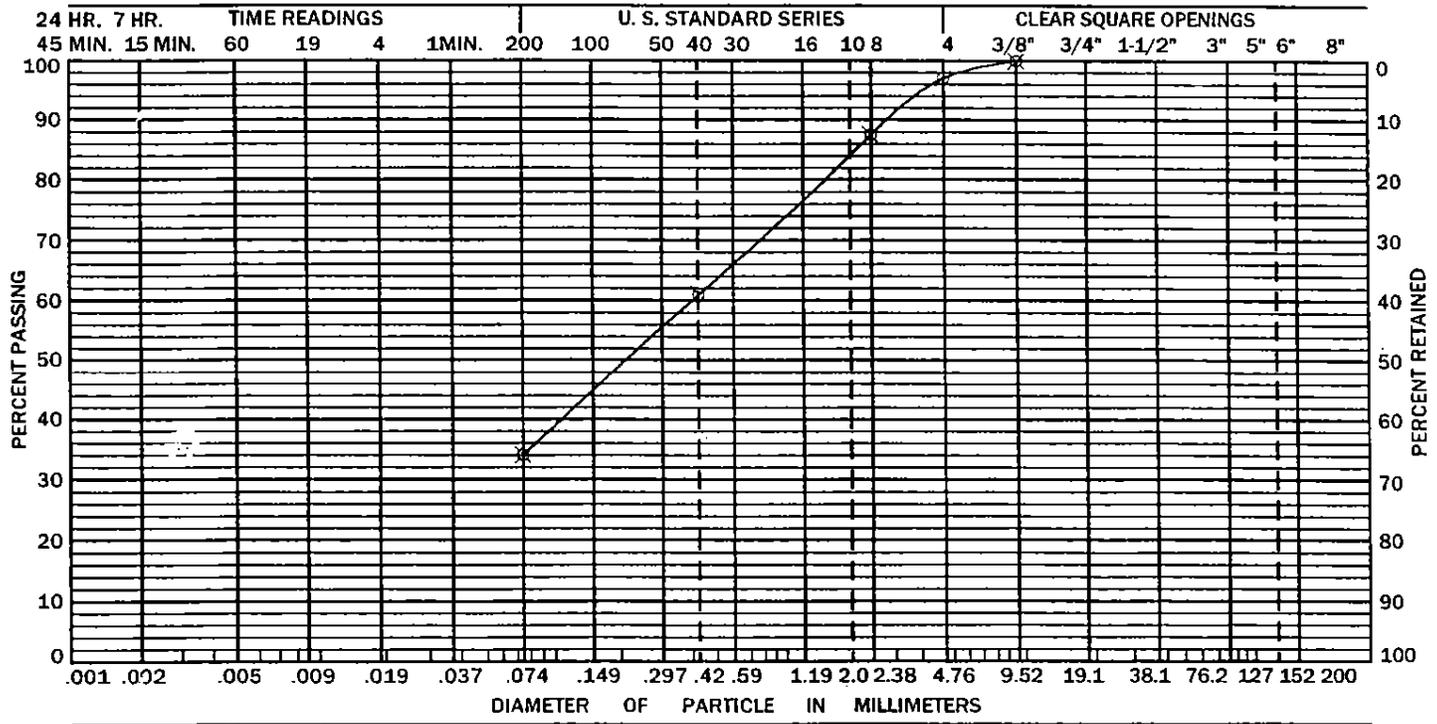
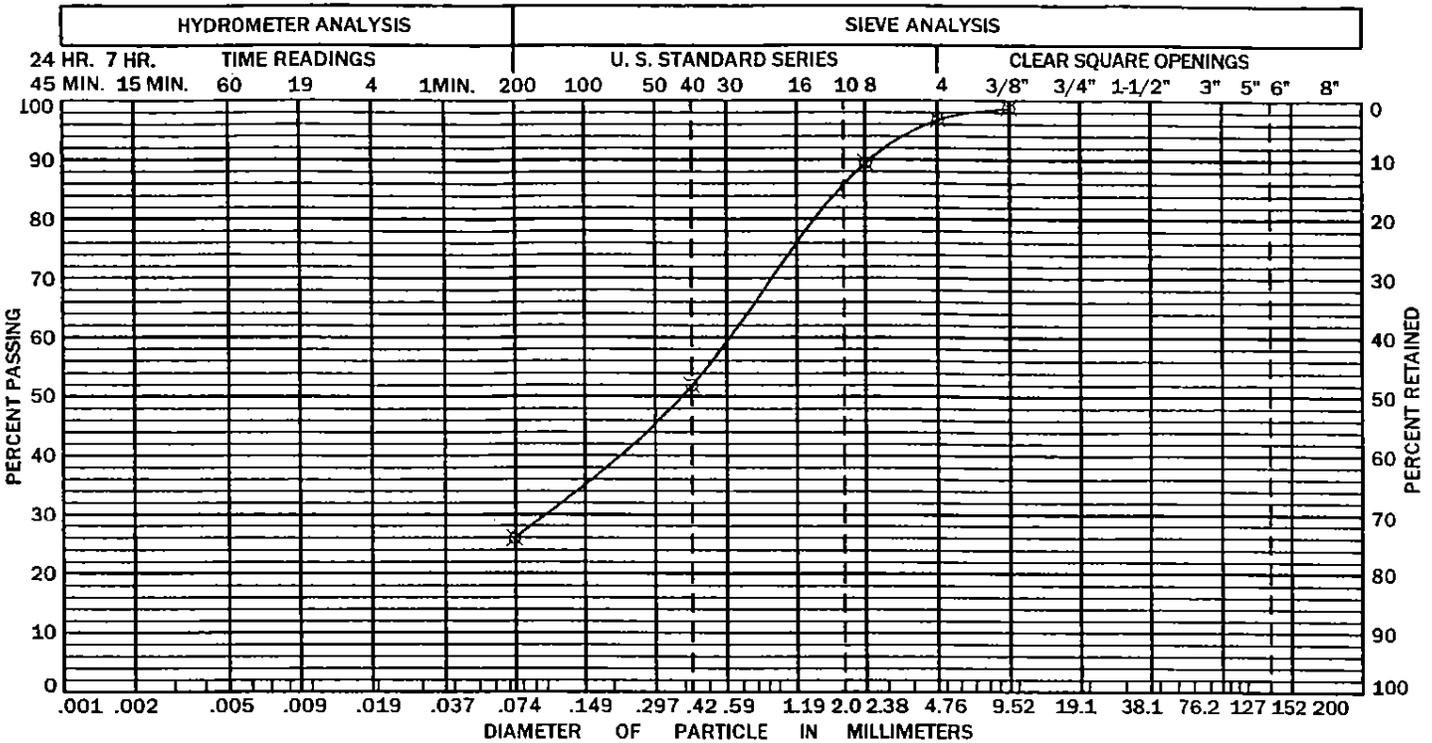
PI = 7.2 %

Job #: 11411 By: KO 05/13/2003



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS





**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411
TEST BORING
NO.: TH-12
DATE: 05/12/2003

JOB#:
TEST BORING
NO.:
DATE:

0-6" TOPSOIL
6"-10' SILTY/CLAY
very-fine grained
moderate density
moderate-high
moisture content
low sand content
moderate plasticity
dark brown color

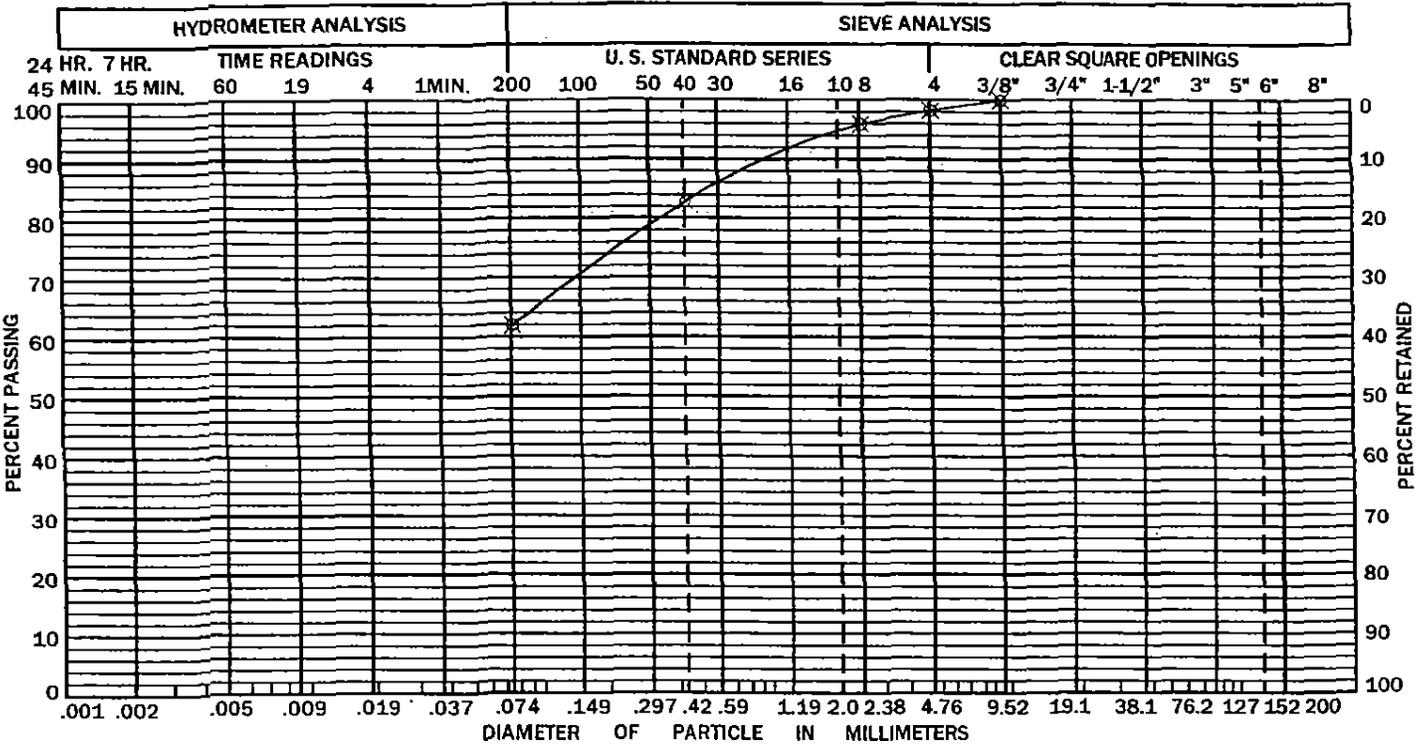
DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
6"-10'					
4			14 12"	12.5	CL/ ML
10			18 12"	11.3	

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"					
6"-10'					
4					
10					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS





**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-13

DATE: 05/12/2003

0-6" TOPSOIL

6"-2' SAND

fine grained

moderate density

moderate moisture
content

low clay content

low plasticity

tan

2'-10' SANDSTONE

fine-medium grained

very-high density

moderate moisture
content

low clay content

low plasticity

tan color

density increases
w/depth

DEPTH (in ft.)

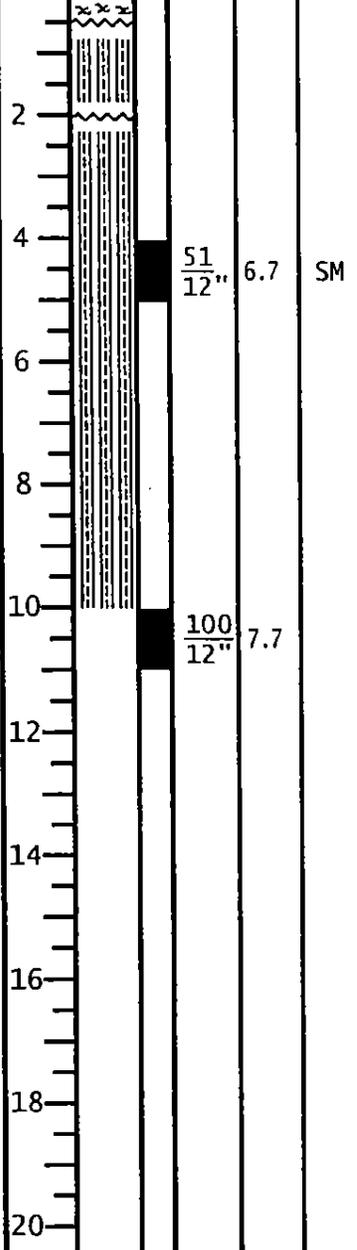
SYMBOL

SAMPLES

BLOW COUNT

WATER %

SOIL TYPE



JOB#:

TEST BORING
NO.:

DATE:

DEPTH (in ft.)

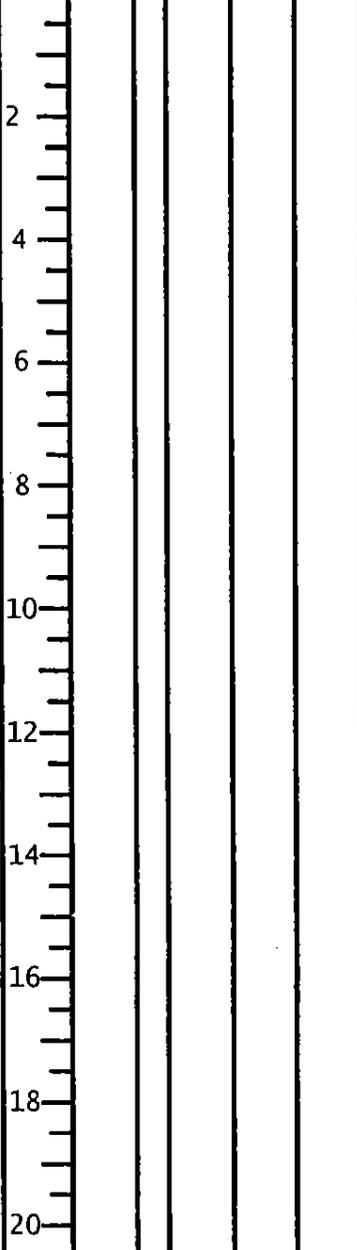
SYMBOL

SAMPLES

BLOW COUNT

WATER %

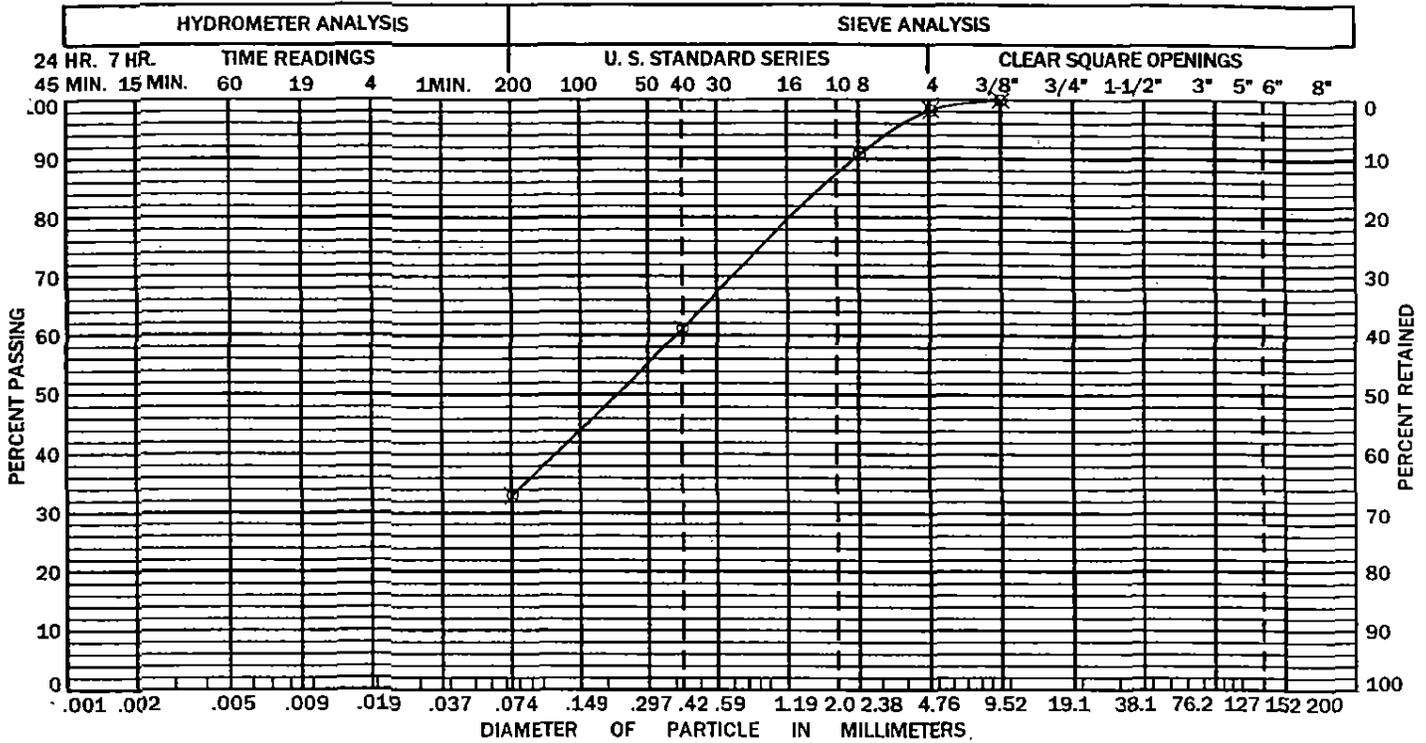
SOIL TYPE





FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLASSIFICATION	SM	SAND			GRAVEL		COBBLES
		FINE	MEDIUM	COARSE	FINE	COARSE	
GRAVEL	1.5 %						
SAND	65.3 %						
FINES	33.2 %						
SAMPLE#	1	HOLE# TH-13		DEPTH 4 FEET			

NOTES:	6.7 % Moisture content
	LL = 15.8 %
	PL = 15.5 %
	PI = 0.3 %
Job #:	11411
By:	KO
	05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-14

DATE: 05/12/2003

0-6" TOPSOIL

6"-10' CLAY

fine grained

moderate density

moderate-highmoisture
moisture content

low sand content

moderate plasticity

red-brown color

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
6-10'	Diagonal lines				
4		14 12"	13.1		
10		16 12"	14.3		CL

JOB#:

TEST BORING
NO.:

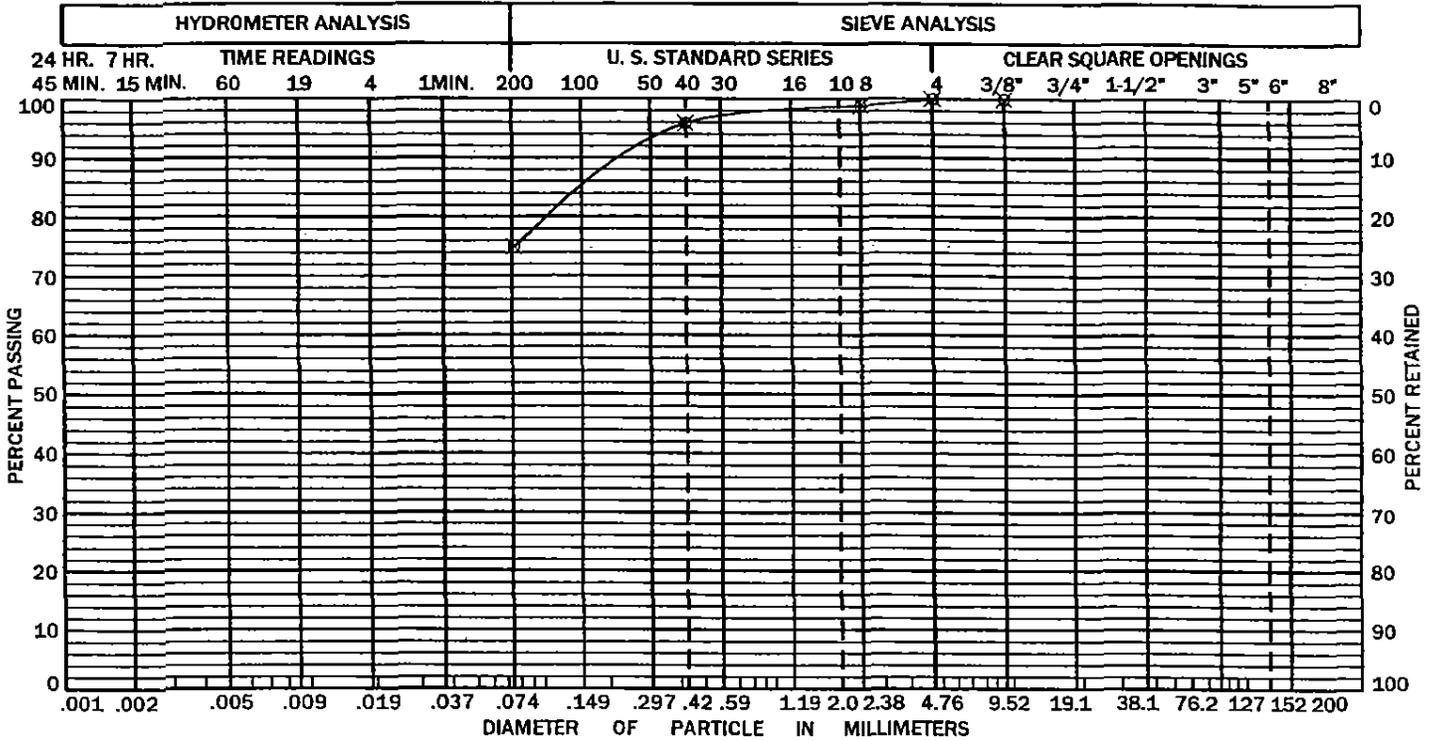
DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-20'					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION CL
 GRAVEL 0.0 %
 SAND 25.0 %
 FINES 75.0 %
 SAMPLE# 1 HOLE# TH-14 DEPTH 10 FEET

NOTES: 14.3 % Moisture content
LL = 27.7 %
PL = 19.2 %
PI = 8.5 %
 Job #: 11411 By: KO 05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

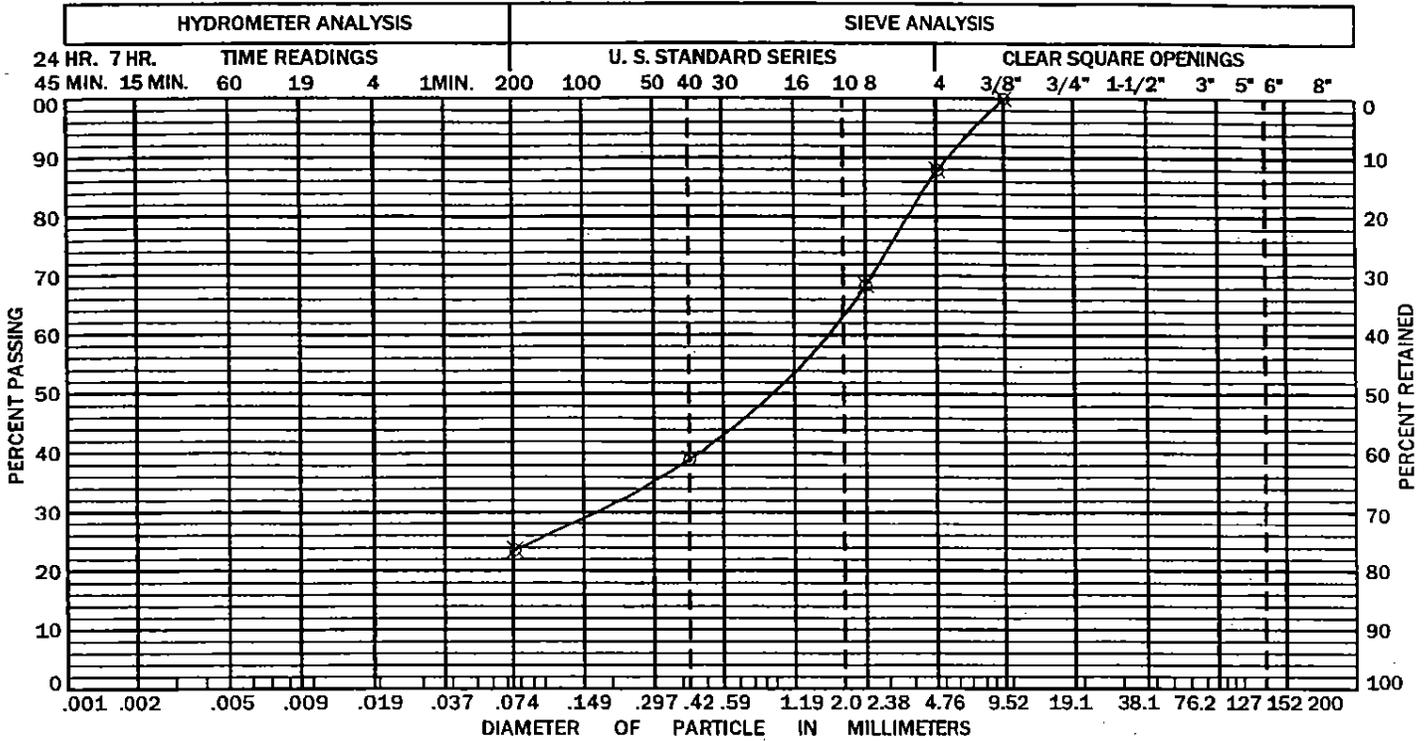
OB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
11411						
TEST BORING NO.: TH-15						
DATE: 05/12/2003						
0-6" TOPSOIL	0-6	XXXXXX				
6"-12" SAND	6-12	Diagonal lines				
fine grained						
low density						
moderate moisture content				40 12"	6.9	
low clay content						
low plasticity						
buff color						
12"-10' SANDSTONE	12-10'	Diagonal lines				
fine-medium grained						
high density				70 12"	8.2	SC
moderate moisture content						
moderate clay content						
moderate plasticity						
buff color						
oxidized soil						
density increases w/depth						

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SC
 GRAVEL 12.2 %
 SAND 64.3 %
 FINES 23.5 %

NOTES: 8.2 % Moisture content
LL = 33.6 %
PL = 21.5 %
PI = 12.1 %
 Job #: 11411 By: KO 05/13/2003

SAMPLE# 1 HOLE# TH-15 DEPTH 10 FEET



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-16

DATE: 05/12/2003

0-6" TOPSOIL

6"-2' SAND

fine-coarse grained
moderate density

moderate moisture
content

low clay content

low plasticity

tan color

2'-10' SANDSTONE

fine-coarse grained

high density

moderate moisture
content

moderate sand content

moderate plasticity

buff color

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
2					
4			45 12"	4.9	SC
6					
8					
10			40 12"	9.1	SC
12					
14					
16					
18					
20					

JOB#:

TEST BORING
NO.:

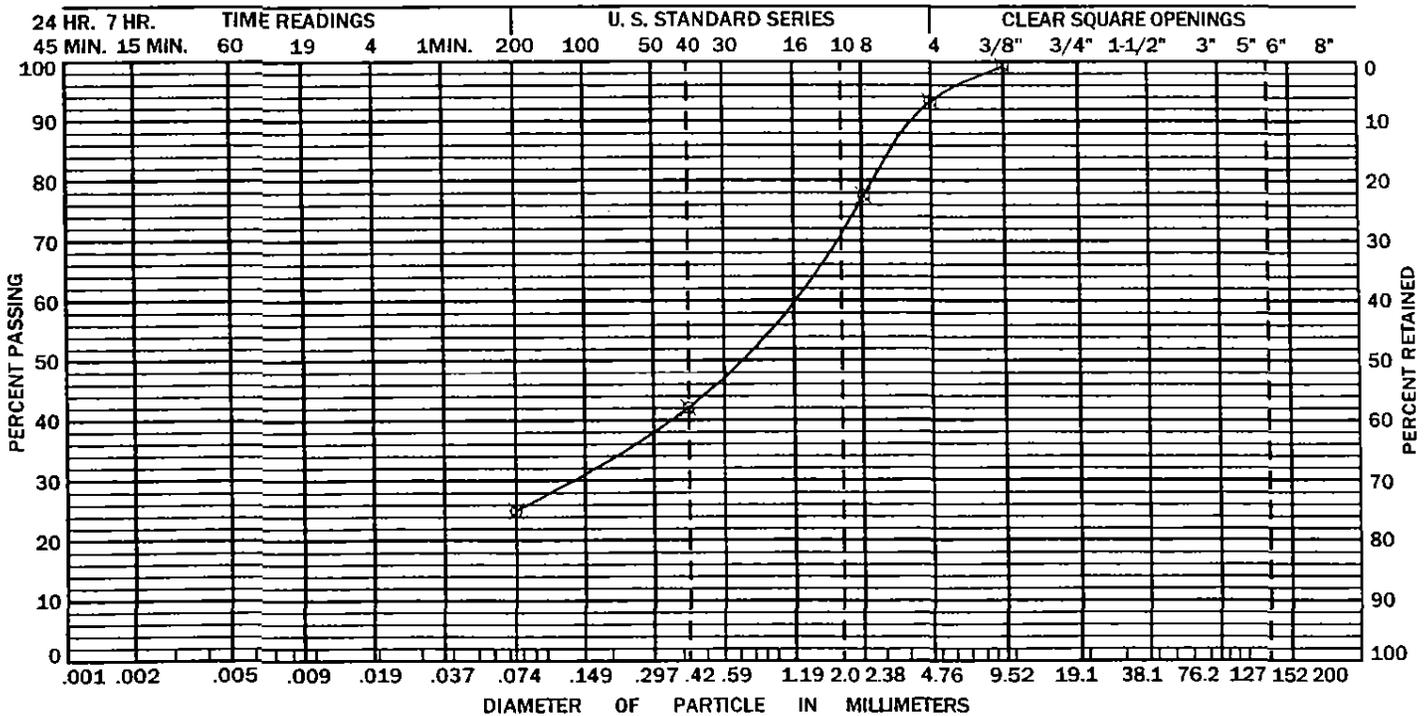
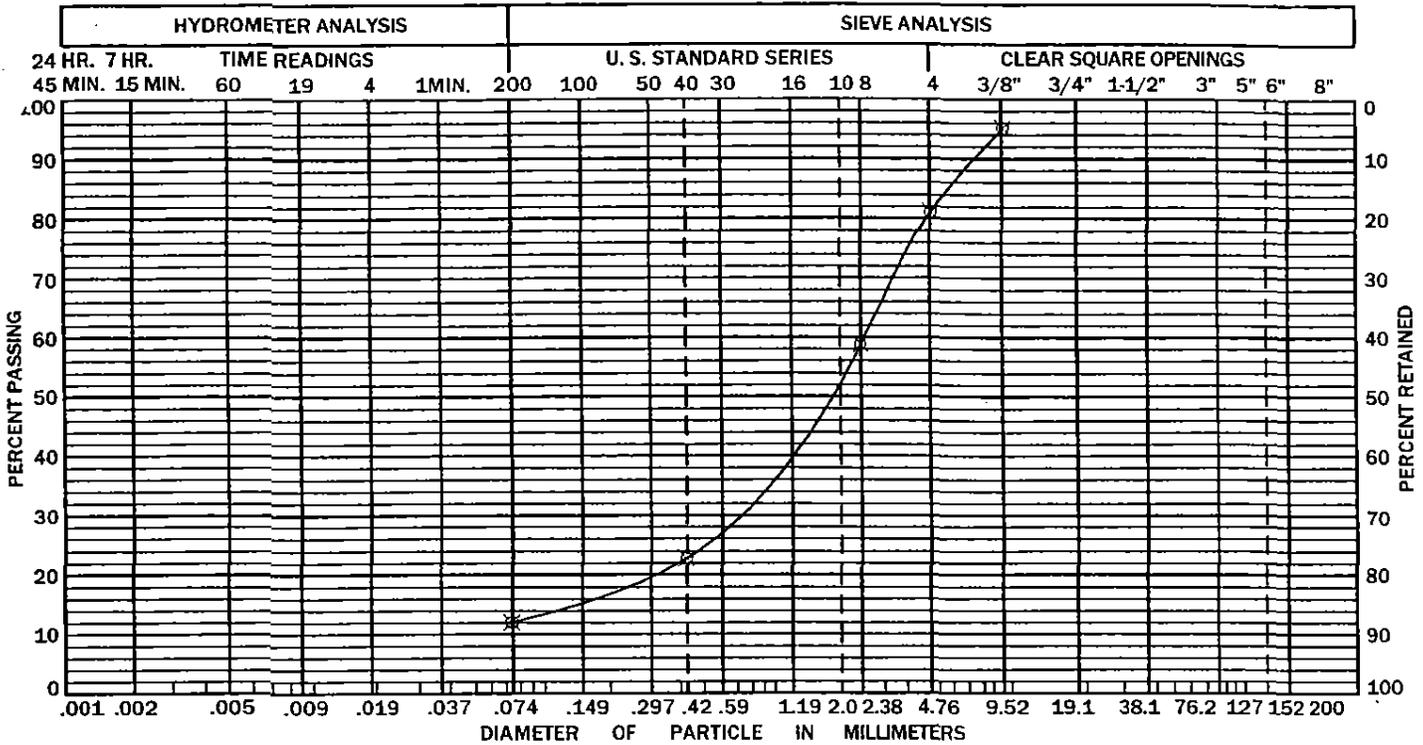
DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS

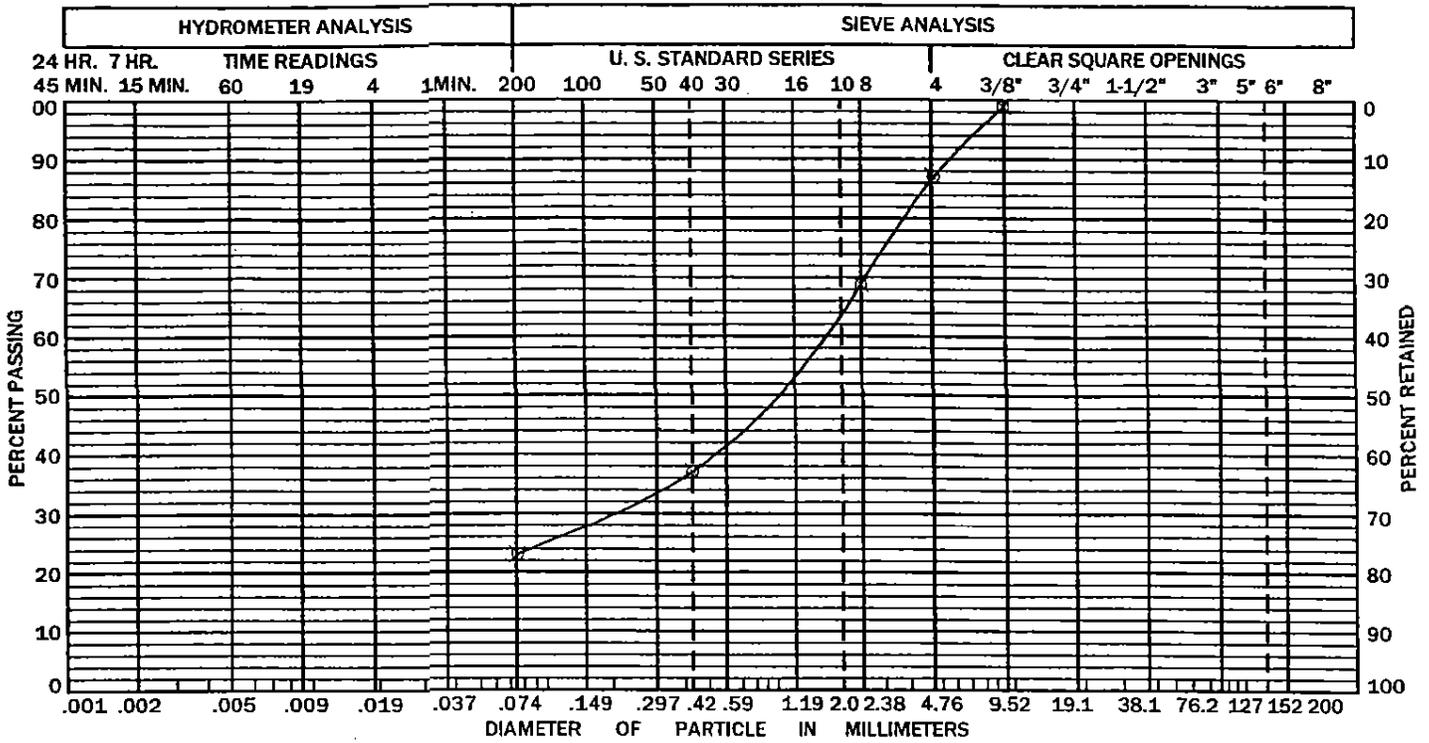


CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	
CLASSIFICATION	SC					
GRAVEL	6.4 %					
SAND	68.6 %					
FINES	25.0 %					
SAMPLE#	1 HOLE# TH-16 DEPTH 10 FEET					
NOTES:	9.1 % Moisture content					
	LL = 30.9 %					
	PL = 20.8 %					
	PI = 10.1 %					
	Job #: 11411 By: KO 05/13/2003					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION	SC
GRAVEL	13.3 %
SAND	63.8 %
FINES	22.9 %
SAMPLE#	1 HOLE# TH-17 DEPTH 10 FEET

NOTES:	7.6 % Moisture content
	LL = 31.3 %
	PL = 20.3 %
	PI = 11.0 %
Job #:	11411
By:	KO
	05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

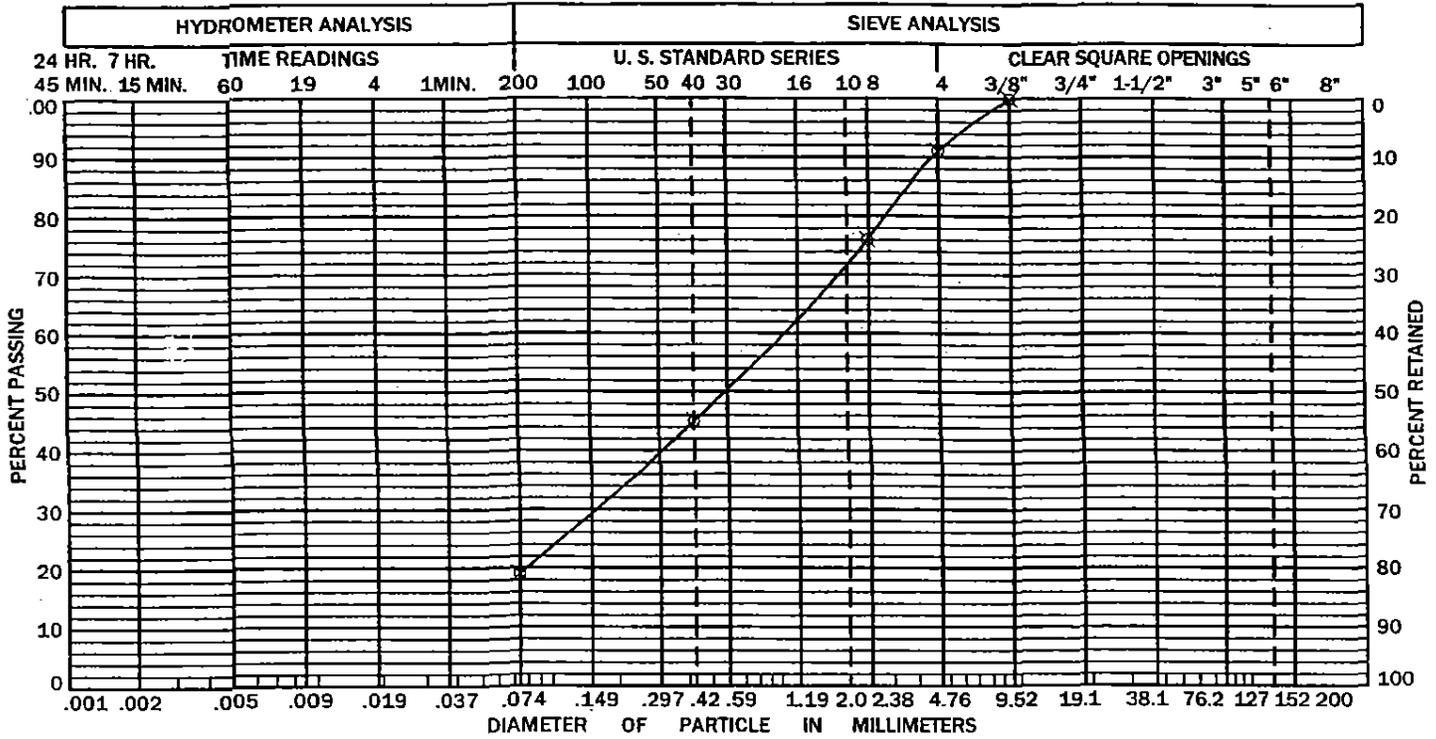
JOB#: 11411	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.: TH-18						
DATE: 05/12/2003						
0-4" <u>TOPSOIL</u>	0-4					
4"-8' <u>SAND</u>	4-8					
fine-medium grained						
moderate density						
low-moderate moisture content				13 12"	4.5	SM
moderate clay content						
moderate plasticity						
tan color						
8'-12' <u>SANDSTONE</u>	8-12					
fine-medium grained						
moderate-high density				58 12"	6.0	
moderate moisture content						
low clay content						
low plasticity						
brown color						
density increases w/depth						

JOB#:	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
TEST BORING NO.:						
DATE:						
	0-2					
	2-4					
	4-6					
	6-8					
	8-10					
	10-12					
	12-14					
	14-16					
	16-18					
	18-20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	
CLASSIFICATION <u>SM</u>	NOTES: <u>4.5 % Moisture content</u>					
GRAVEL <u>8.8 %</u>	<u>LL = 24.3 %</u>					
SAND <u>72.5 %</u>	<u>PL = 21.2 %</u>					
FINES <u>18.7 %</u>	<u>PI = 3.1 %</u>					
SAMPLE# <u>1</u> HOLE# <u>TH-18</u> DEPTH <u>4</u> FEET	<u>Job #: 11411 By: KO 05/13/2003</u>					



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-19

DATE: 05/12/2003

0-6" TOPSOIL

6"-4' SAND

fine-medium grained
moderate density

moderate moisture
content

moderate clay content

moderate plasticity

tan color

4'-10' SANDSTONE

fine-medium grained
moderate density

moderate moisture
content

moderate clay content

moderate plasticity

buff color

density increases
w/depth

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-6"	XXXX				
6"-4'	Diagonal lines				
33 12"		33 12"	8.5		SC
60 12"		60 12"	9.7		

JOB#:

TEST BORING
NO.:

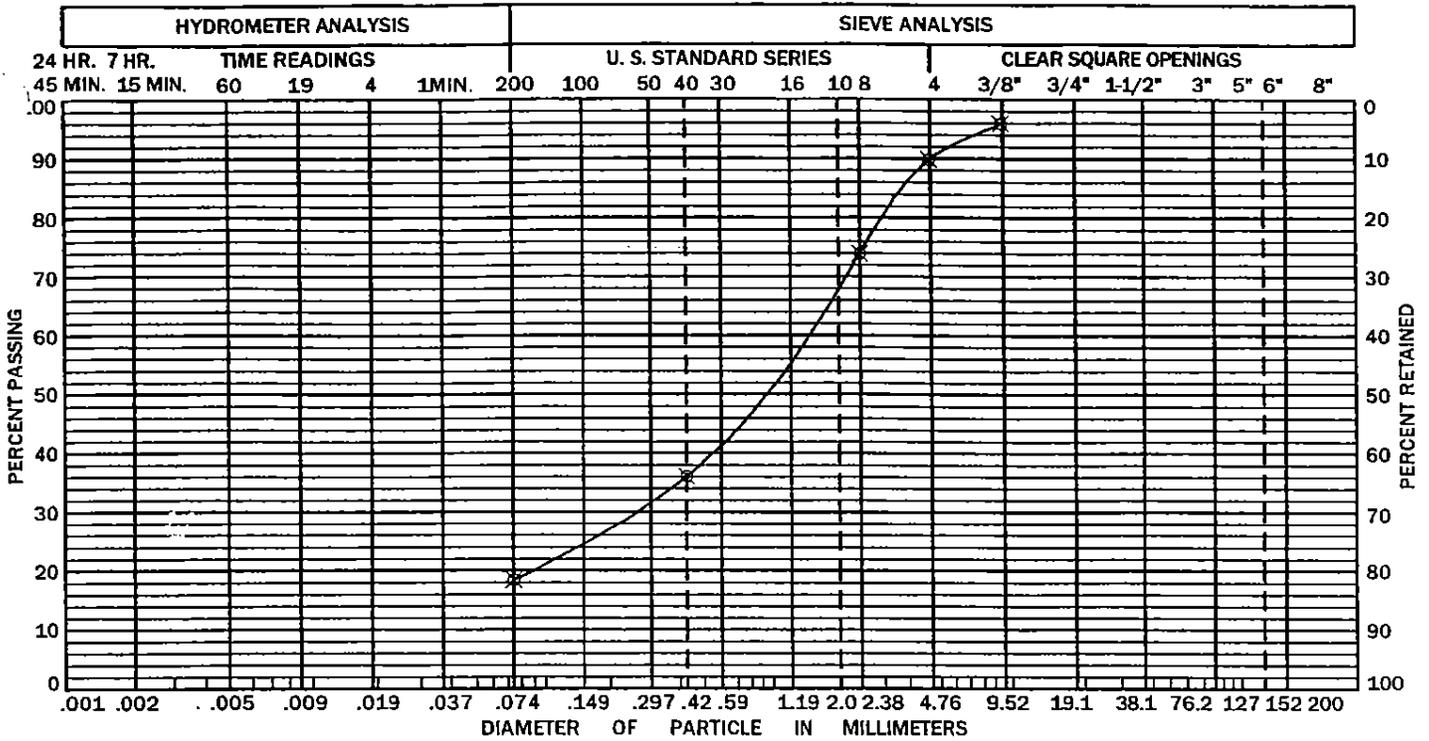
DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SC
 GRAVEL 10.2 %
 SAND 71.2 %
 FINES 18.6 %
 SAMPLE# 1 HOLE# TH-19 DEPTH 4 FEET

NOTES: 8.5 % Moisture content
LL = 30.3 %
PL = 21.1 %
PI = 9.2 %
 Job #: 11411 By: KO 05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-20

DATE: 05/12/2003

0-6" TOPSOIL

6"-3' SILT

very fine grained

low density

moderate moisture
content

moderate clay content

moderate plasticity

buff color

3'-12' SAND

fine-medium grained

moderate density

moderate-high
moisture content

moderate clay content

moderate plasticity

buff-brown color

DEPTH (in ft.)

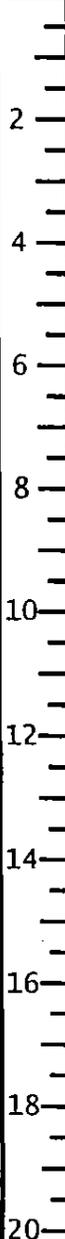
SYMBOL

SAMPLES

BLOW COUNT

WATER %

SOIL TYPE



$\frac{19}{12}$ "

13.2

SM

$\frac{18}{12}$ "

7.5

JOB#:

TEST BORING
NO.:

DATE:

DEPTH (in ft.)

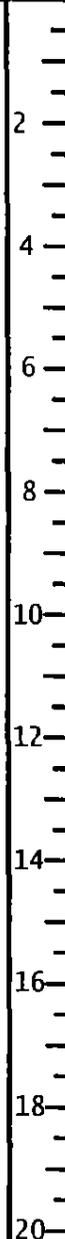
SYMBOL

SAMPLES

BLOW COUNT

WATER %

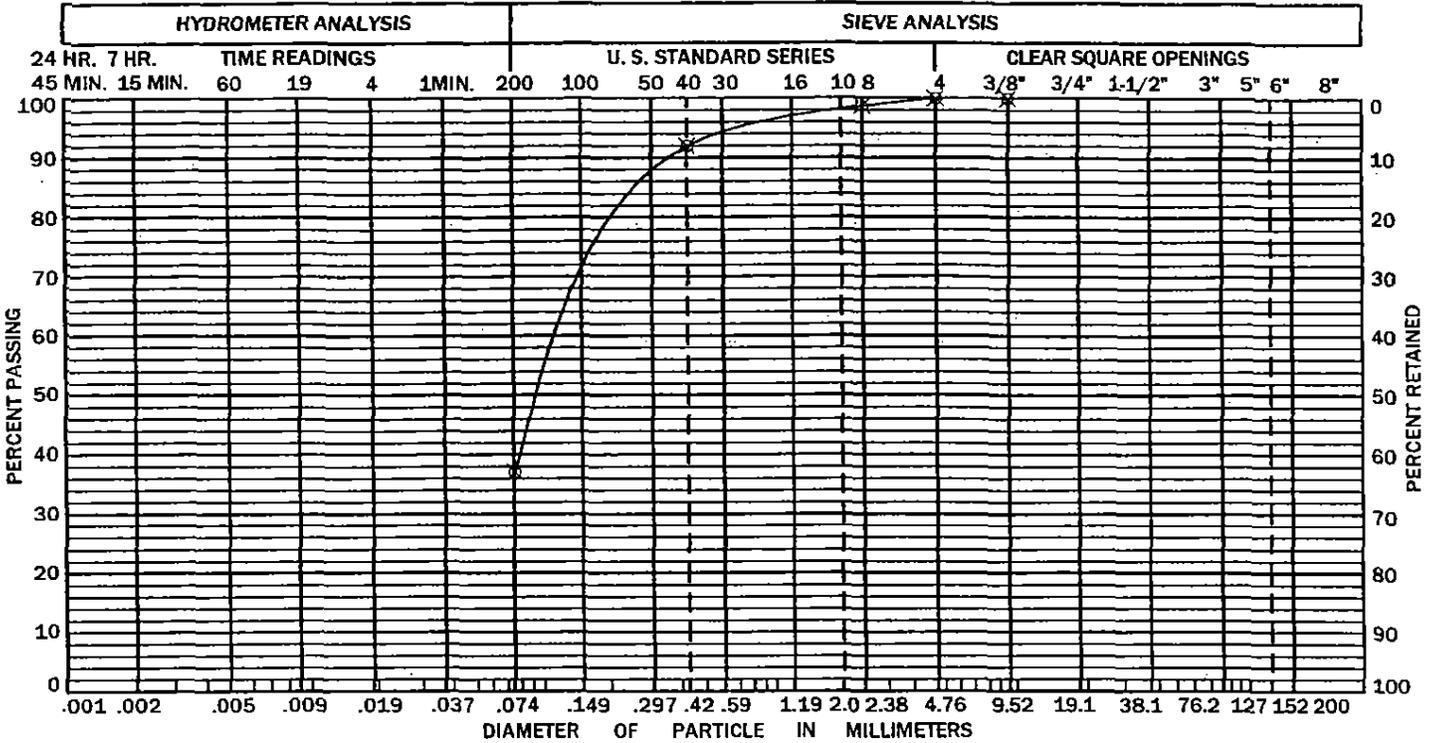
SOIL TYPE





FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

CLASSIFICATION SM
 GRAVEL 0.0 %
 SAND 62.3 %
 FINES 37.7 %

NOTES: 13.2 % Moisture content
LL = Could Not Be Determined
PL = Non-Plastic

SAMPLE# 1 HOLE# TH-20 DEPTH 4 FEET

Job #: 11411 By: KO 05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-21

DATE: 05/12/2003

0-6" TOPSOIL

6"-3'6" SAND

fine-medium grained

moderate density

low moisture
content

low clay content

low plasticity

buff color

3'6"-12' SANDSTONE

fine-medium grained

moderate-high density

moderate moisture
content

low clay content

non-plastic

buff/weathered color

density increases
w/depth

DEPTH (in ft.)

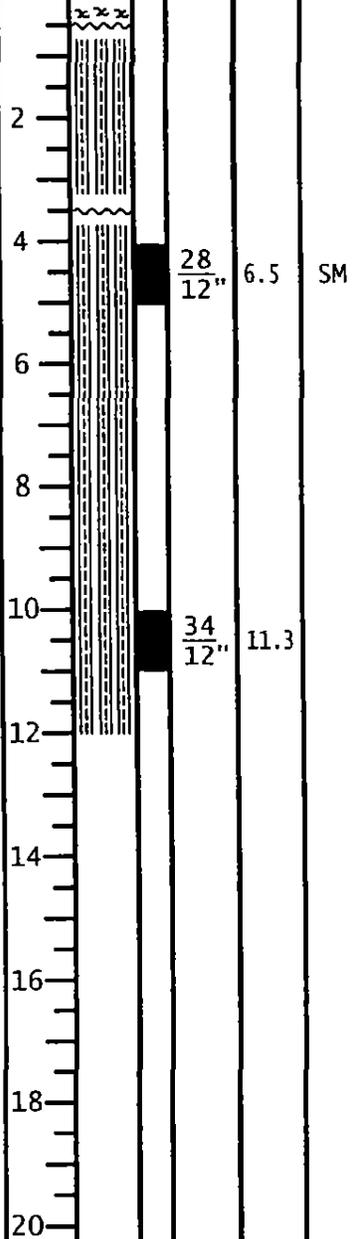
SYMBOL

SAMPLES

BLOW COUNT

WATER %

SOIL TYPE



JOB#:

TEST BORING
NO.:

DATE:

DEPTH (in ft.)

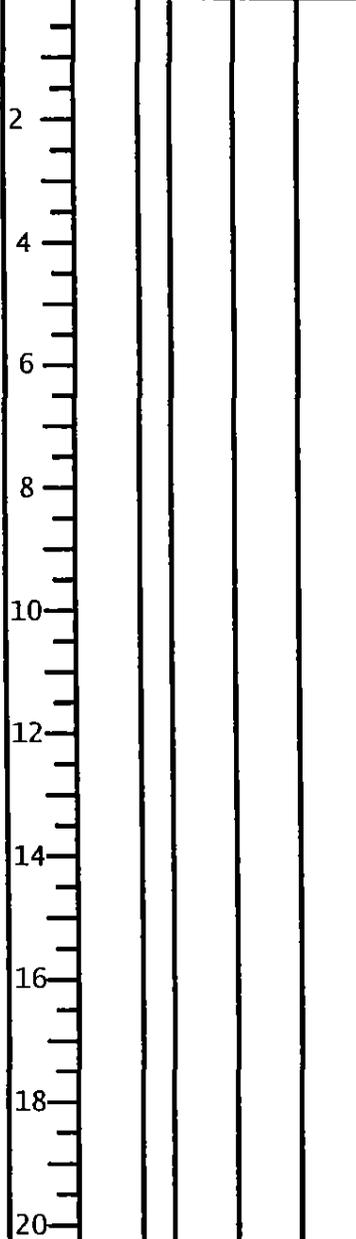
SYMBOL

SAMPLES

BLOW COUNT

WATER %

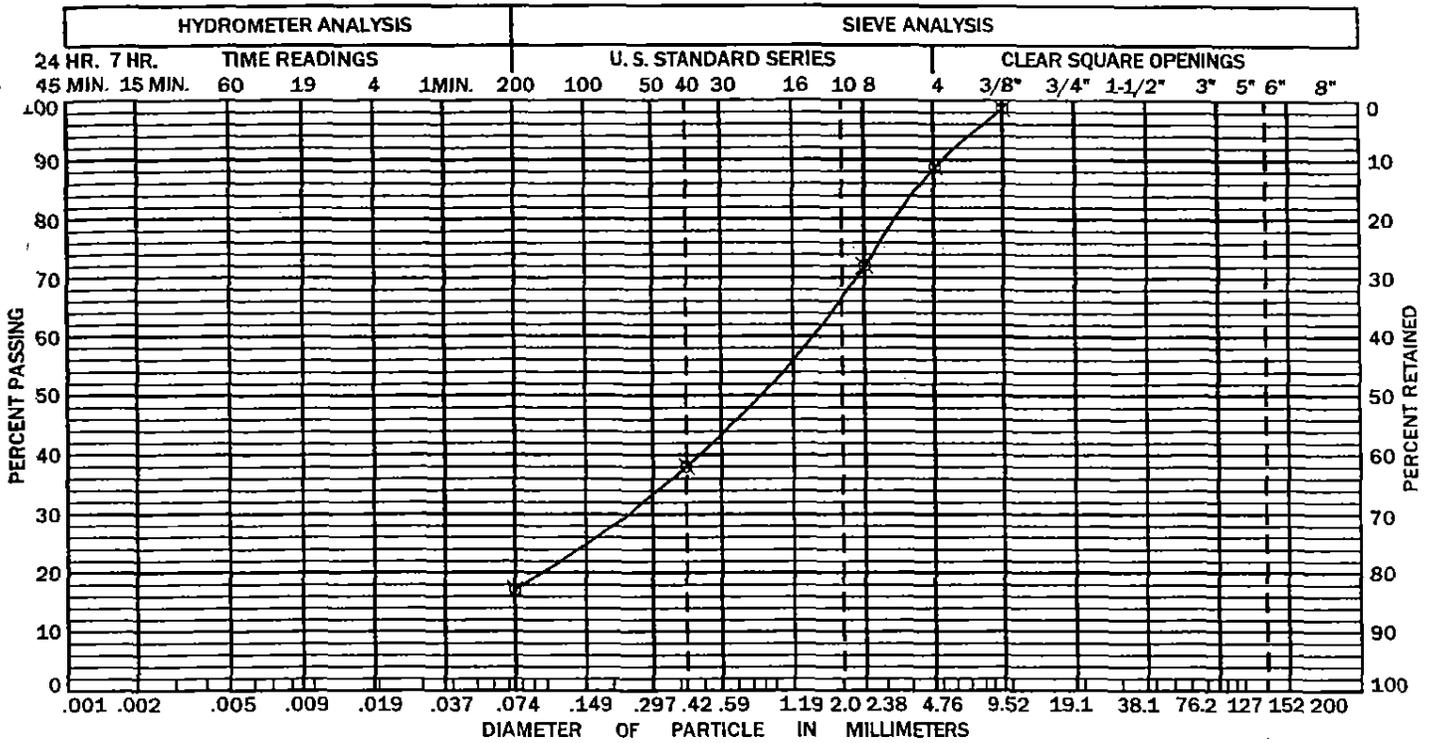
SOIL TYPE





FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	

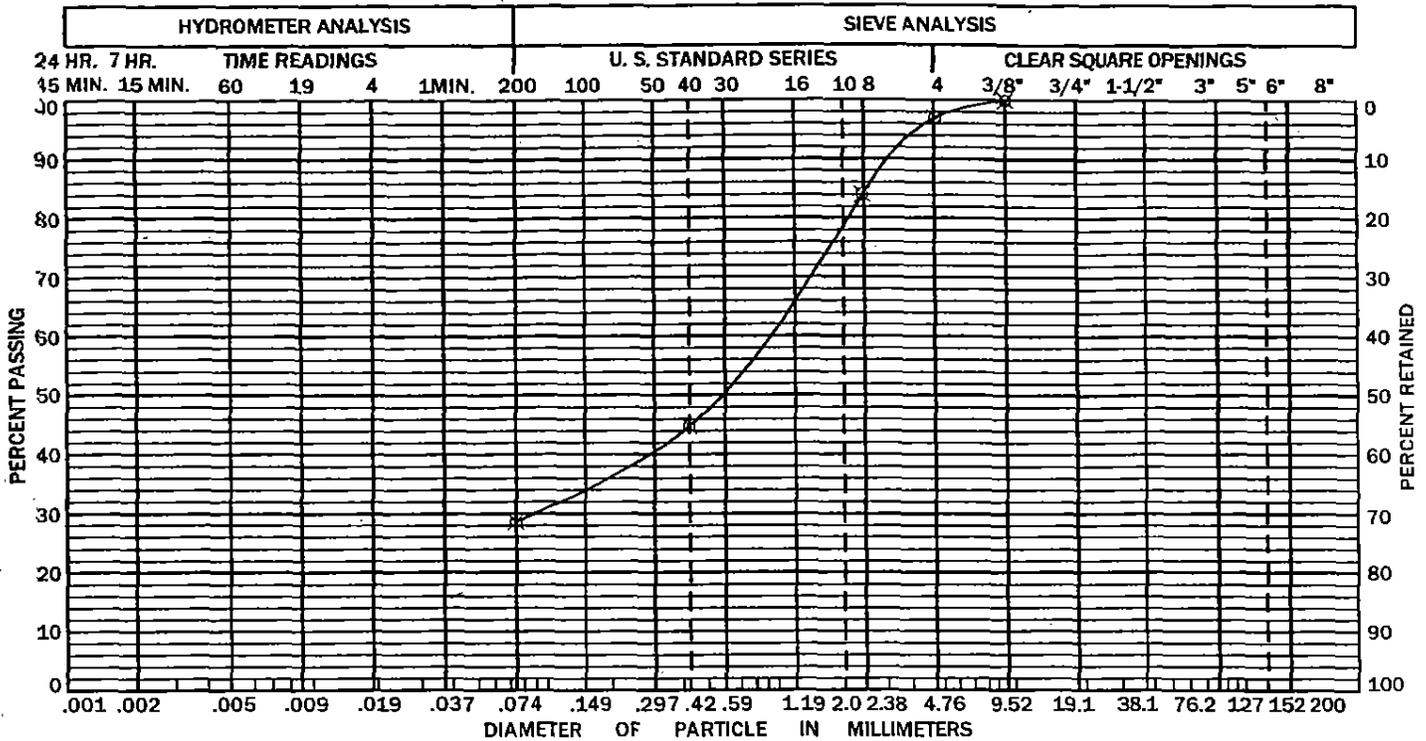
CLASSIFICATION SM
 GRAVEL 10.6 %
 SAND 72.2 %
 FINES 17.2 %
 SAMPLE# 1 HOLE# TH-21 DEPTH 4 FEET

NOTES: 6.5 % Moisture content
LL = Could Not Be Determined
PL = Non-Plastic
 Job #: 11411 By: KO 05/13/2003



FRONT RANGE GEOTECHNICAL INC.

GRADATION TEST RESULTS



CLAY TO SILT	SAND			GRAVEL		COBBLES
	FINE	MEDIUM	COARSE	FINE	COARSE	
CLASSIFICATION	SC					
GRAVEL	3.0 %					
SAND	68.6 %					
FINES	28.4 %					
SAMPLE#	1 HOLE# TH-22 DEPTH 4 FEET					

NOTES:	12.0 % Moisture content
	LL = 29.4 %
	PL = 18.4 %
	PI = 11.0 %
Job #:	11411
By:	KO
	05/13/2003



**FRONT RANGE
GEOTECHNICAL
INC.**

DRILL LOGS

JOB#: 11411

TEST BORING
NO.: TH-23

DATE: 05/12/2003

0-24" TOPSOIL

24"-36" SAND

fine grained

moderate density

moderate moisture
content

moderate clay content

moderate plasticity

tan color

36"-15' SANDSTONE

fine-medium grained

very-high density

moderate moisture
content

moderate clay content

moderate plasticity

rust-oxidized color

density increases
w/depth

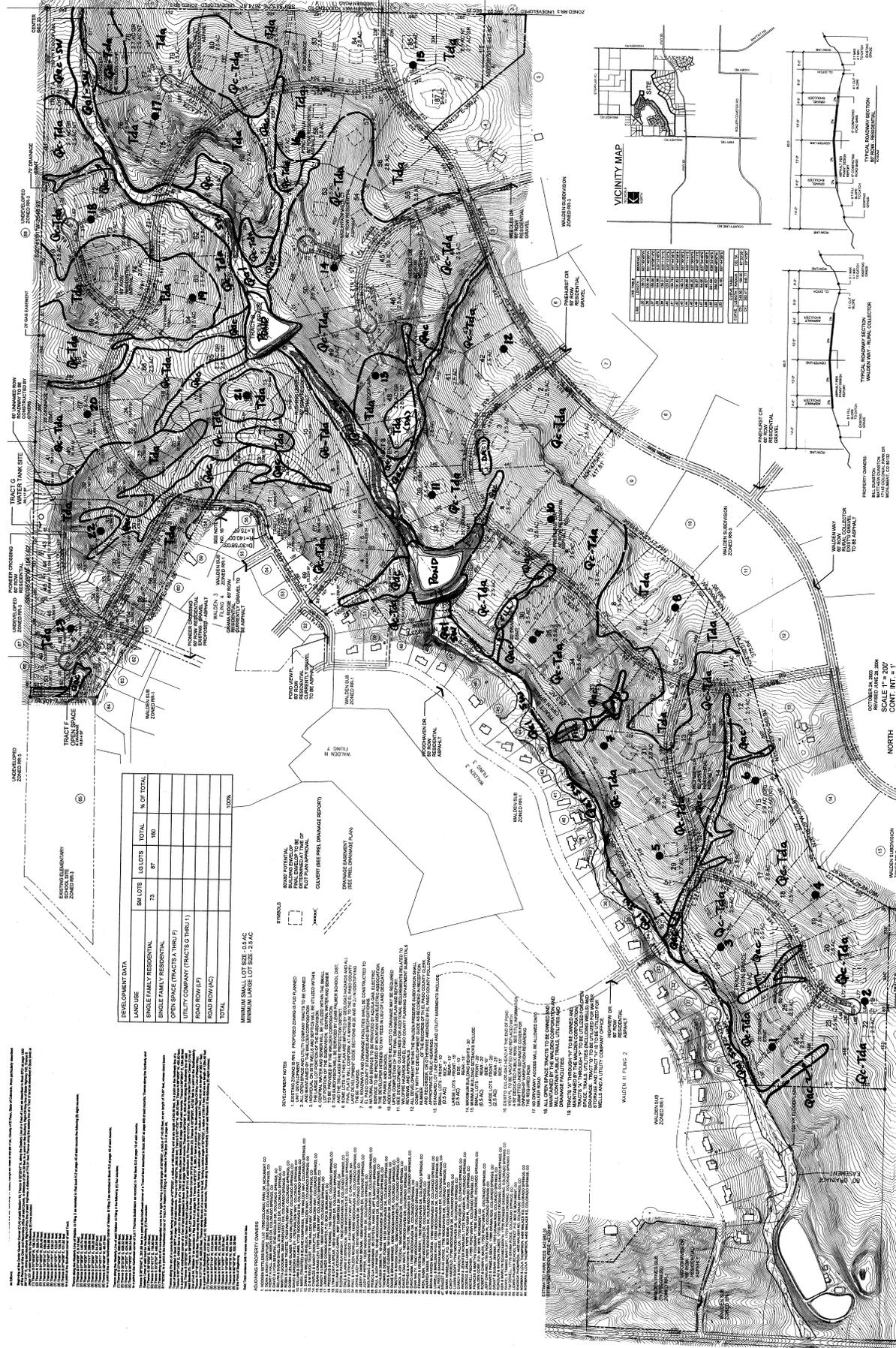
DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
0-24"	XXXXXX				
24"-36"	XXXXXX				
2					
4			41 12"	9.1	SC
6					
8					
10			72 12"	6.9	
12					
14					
16					
18					
20					

JOB#:

TEST BORING
NO.:

DATE:

DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					



PRELIMINARY PLAN WALDEN PRESERVE SUBDIVISION
 EL PASO COUNTY, COLORADO
 DEVELOPED BY CUSTOM CASTLE, INC. 1145 COLONIAL PARK DR. MONUMENT, CO. 80132

SCALE 1" = 200'
 CONT. INT. = 1'
 NORTH

ACRES	FEET
0.0000	0.0000
0.0001	3.5131
0.0002	7.0262
0.0003	10.5393
0.0004	14.0524
0.0005	17.5655
0.0006	21.0786
0.0007	24.5917
0.0008	28.1048
0.0009	31.6179
0.0010	35.1310
0.0011	38.6441
0.0012	42.1572
0.0013	45.6703
0.0014	49.1834
0.0015	52.6965
0.0016	56.2096
0.0017	59.7227
0.0018	63.2358
0.0019	66.7489
0.0020	70.2620
0.0021	73.7751
0.0022	77.2882
0.0023	80.8013
0.0024	84.3144
0.0025	87.8275
0.0026	91.3406
0.0027	94.8537
0.0028	98.3668
0.0029	101.8799
0.0030	105.3930
0.0031	108.9061
0.0032	112.4192
0.0033	115.9323
0.0034	119.4454
0.0035	122.9585
0.0036	126.4716
0.0037	130.0847
0.0038	133.5978
0.0039	137.1109
0.0040	140.6240
0.0041	144.1371
0.0042	147.6502
0.0043	151.1633
0.0044	154.6764
0.0045	158.1895
0.0046	161.7026
0.0047	165.2157
0.0048	168.7288
0.0049	172.2419
0.0050	175.7550
0.0051	179.2681
0.0052	182.7812
0.0053	186.2943
0.0054	189.8074
0.0055	193.3205
0.0056	196.8336
0.0057	200.3467
0.0058	203.8598
0.0059	207.3729
0.0060	210.8860
0.0061	214.3991
0.0062	217.9122
0.0063	221.4253
0.0064	224.9384
0.0065	228.4515
0.0066	231.9646
0.0067	235.4777
0.0068	238.9908
0.0069	242.5039
0.0070	246.0170
0.0071	249.5301
0.0072	253.0432
0.0073	256.5563
0.0074	260.0694
0.0075	263.5825
0.0076	267.0956
0.0077	270.6087
0.0078	274.1218
0.0079	277.6349
0.0080	281.1480
0.0081	284.6611
0.0082	288.1742
0.0083	291.6873
0.0084	295.2004
0.0085	298.7135
0.0086	302.2266
0.0087	305.7397
0.0088	309.2528
0.0089	312.7659
0.0090	316.2790
0.0091	319.7921
0.0092	323.3052
0.0093	326.8183
0.0094	330.3314
0.0095	333.8445
0.0096	337.3576
0.0097	340.8707
0.0098	344.3838
0.0099	347.8969
0.0100	351.4100

PRELIMINARY GEOLOGIC MAP

LEGEND

Q₁ - RECENT ALLUVIUM IN FLOODPLAIN
 Q₂ - CALCIUM (SERRANUS)
 Q₃ - MIXED ALLUVIUM AND CALCIUM
 T_{1a} - DANSON AEGEUS FORMATION
 SW - SUBSMALL MT. AREAS
 DA - DISTURBED AREA
 FILL - MAN-PLACED FILL

● - LOCATION AND NUMBER OF RECOGNITION TEST

DEVELOPMENT DATA

LAND USE	SM. LOTS	LG. LOTS	TOTAL	% OF TOTAL
SINGLE FAMILY RESIDENTIAL	73	87	160	
SINGLE FAMILY RESIDENTIAL				
OPEN SPACE (TRACTS A THRU F)				
UTILITY COMPANY (TRACTS G THRU I)				
ROAD (ROADS)				
TOTAL				100%

MINIMUM SMALL LOT SIZE: 0.5 AC
 MINIMUM LARGE LOT SIZE: 2.5 AC

NOTES

1. DEVELOPMENT NOTES

2. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

3. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

4. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

5. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

6. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

7. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

8. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

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10. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

11. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

12. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

13. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

14. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

15. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

16. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

17. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

18. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

19. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

20. ALL UTILITIES SHALL BE DEEPENED TO A MINIMUM OF 4 FEET BELOW FINISHED GRADE.

FIGURE 2

LAND DESCRIPTION

1. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 2. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 3. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 4. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 5. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 6. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 7. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
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 18. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 19. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 20. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.

LAND USE	SM LOTS	LG LOTS	TOTAL	% OF TOTAL
SINGLE FAMILY RESIDENTIAL	73	87	160	100%
OPEN SPACE (TRACTS A THRU F)				
UTILITY COMPANY (TRACTS G THRU I)				
ROAD ROW (J)				
ROAD ROW (K)				
TOTAL				

MINIMUM LOT SIZE: 5,000 SQ. FT.
 MINIMUM LARGE LOT SIZE: 2.5 AC.

SYMBOLS
 BOUNDARY OF TRACTS
 CENTERLINE OF TRACTS
 CENTERLINE OF ROAD ROWS
 CENTERLINE OF UTILITY LINES
 CENTERLINE OF FENCE LINES
 CENTERLINE OF DRIVEWAYS
 CENTERLINE OF SIDEWALKS
 CENTERLINE OF CURBS
 CENTERLINE OF GUTTERS
 CENTERLINE OF DRAINAGE CANALS
 CENTERLINE OF EROSION CONTROL STRUCTURES
 CENTERLINE OF OTHER STRUCTURES

DEVELOPMENT NOTES
 1. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 2. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 3. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 4. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
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 17. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 18. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 19. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.
 20. ALL TRACTS ARE TO BE DEVELOPED AS SINGLE-FAMILY RESIDENTIAL UNLESS OTHERWISE SPECIFIED.

SEWAGE DISPOSAL CHARACTERISTICS MAP

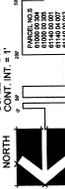
LEGEND

- I - THIN TO THICK SURFICIAL DEPOSITS OVER DANVON RANGE BEDROCK.
- II - THIN SANDS OVER DANVON RANGE BEDROCK.
- III - THICKER SANDS IN SINKS AND DRAINAGES.
- SM - SEASONALLY WET AREAS.
- DA - DISTURBED AREAS.
- FILL - MAN-MADE FILL.
- SLOPES OF 30% AND GREATER.

FIGURE 3



PRELIMINARY PLAN WALDEN PRESERVE SUBDIVISION
 EL PASO COUNTY, COLORADO
 DEVELOPED BY CANTON CATTLE, INC., 1745 COLONIAL PARK DR., BUCKNIGHT, CO. 80532



DATE: OCTOBER 14, 2003
 SHEET NO. 1 OF 1
 TOTAL SHEETS: 1
 TOTAL ACRES: 160.00
 TOTAL LOTS: 160
 TOTAL ACRES: 160.00
 TOTAL LOTS: 160
 TOTAL ACRES: 160.00
 TOTAL LOTS: 160
 TOTAL ACRES: 160.00

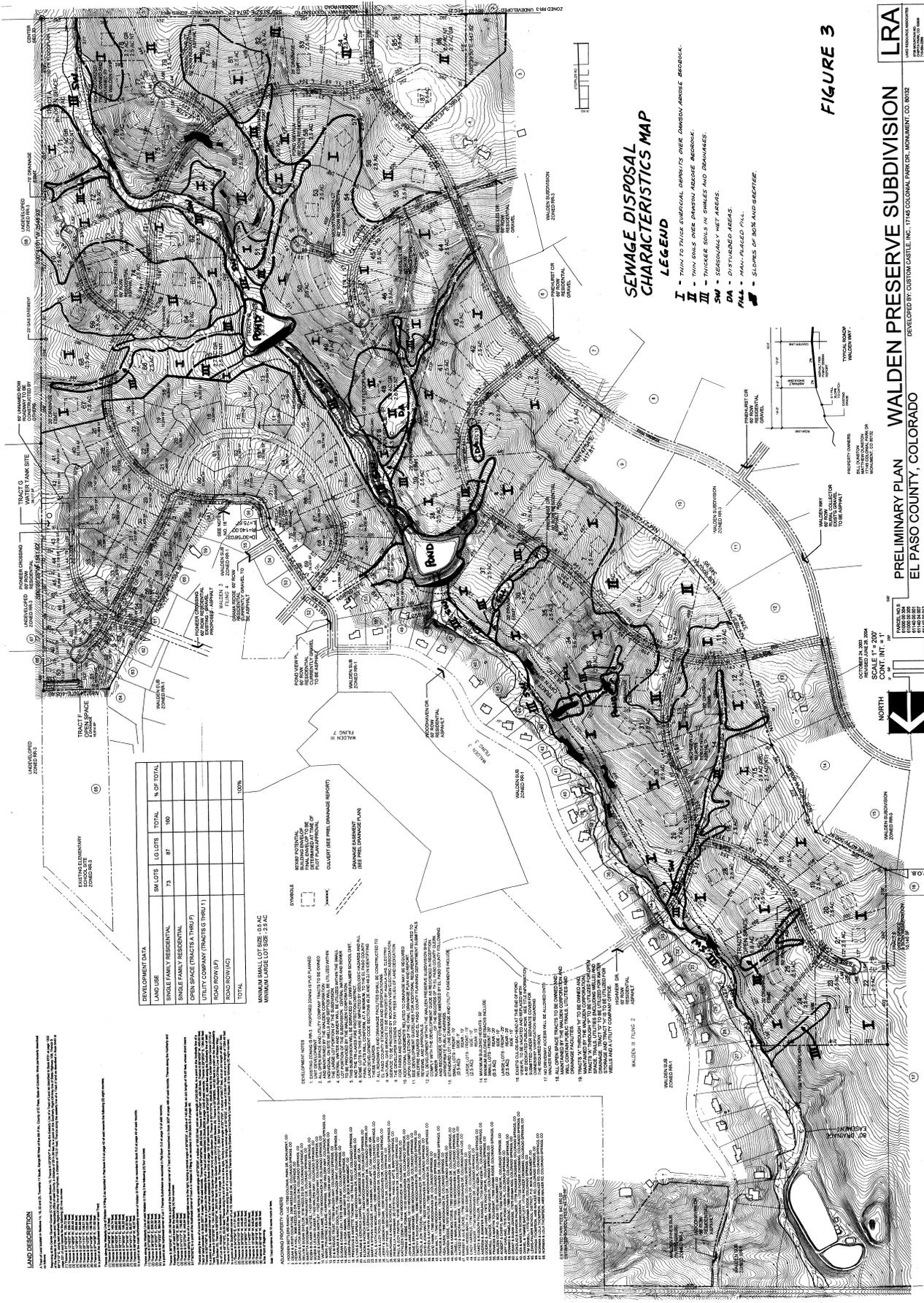
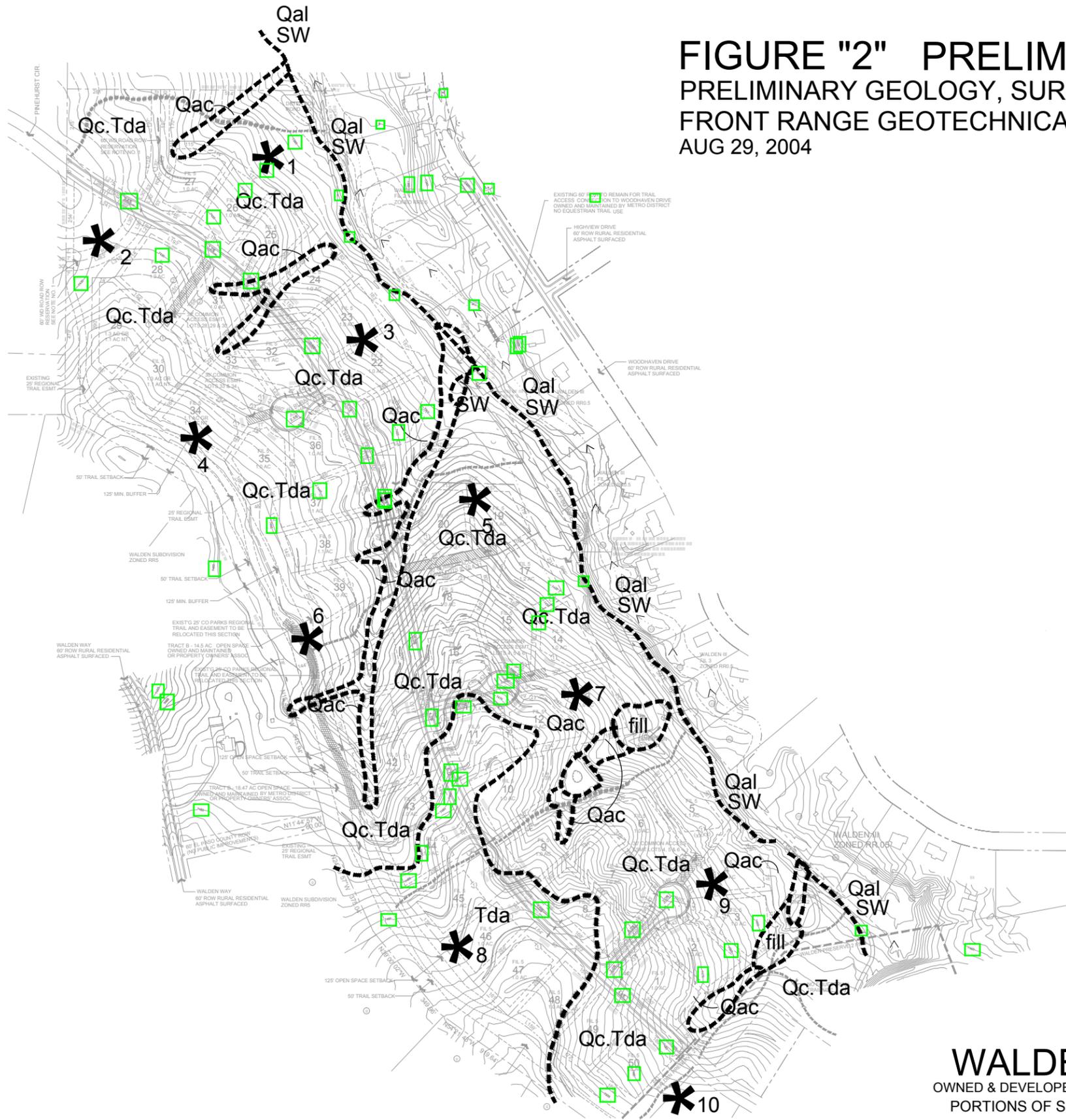


FIGURE "2" PRELIMINARY GEOLOGIC MAP

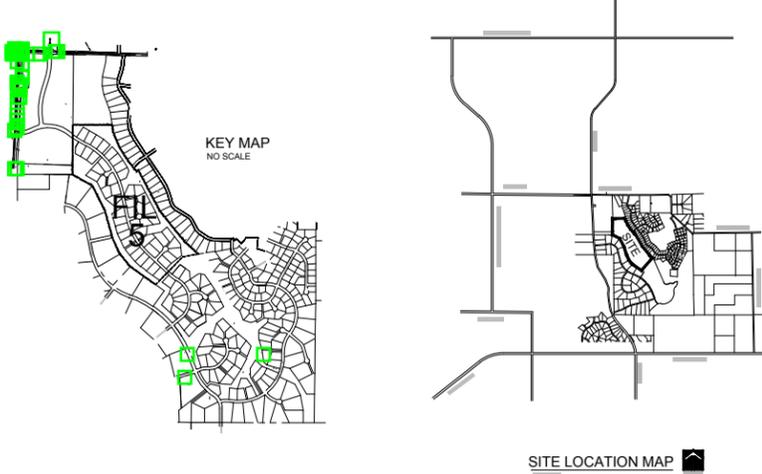
PRELIMINARY GEOLOGY, SURFACE SOILS, AND SEWAGE DISPOSAL EVALUATION

FRONT RANGE GEOTECHNICAL, INC
AUG 29, 2004



LEGEND

- Qal - RECENT ALLUVIUM IN FLOODPLAIN
- Qc - COLLUVIUM (SLOPEWASH)
- Qac - MIXED ALLUVIUM AND COLLUVIUM
- Tda - DAWSON ARKOSE FORMATION
- SW - SEASONALLY WET AREAS
- DA - DISTURBED AREAS
- fill - MAN-PLACED FILL
- 2 * - LOCATION AND NUMBER OF PERCOLATION TEST



WALDEN PRESERVE 2 - FILING NO. 5
 OWNED & DEVELOPED BY: WALDEN HOLDINGS I LLC, 17145 COLONIAL PARK DR, MONUMENT, CO 80132
 PORTIONS OF SEC 14, 15, 22 & 23, T11S, R66W, 6TH PM IN EL PASO COUNTY COLORADO

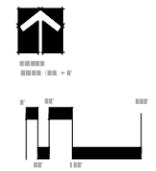
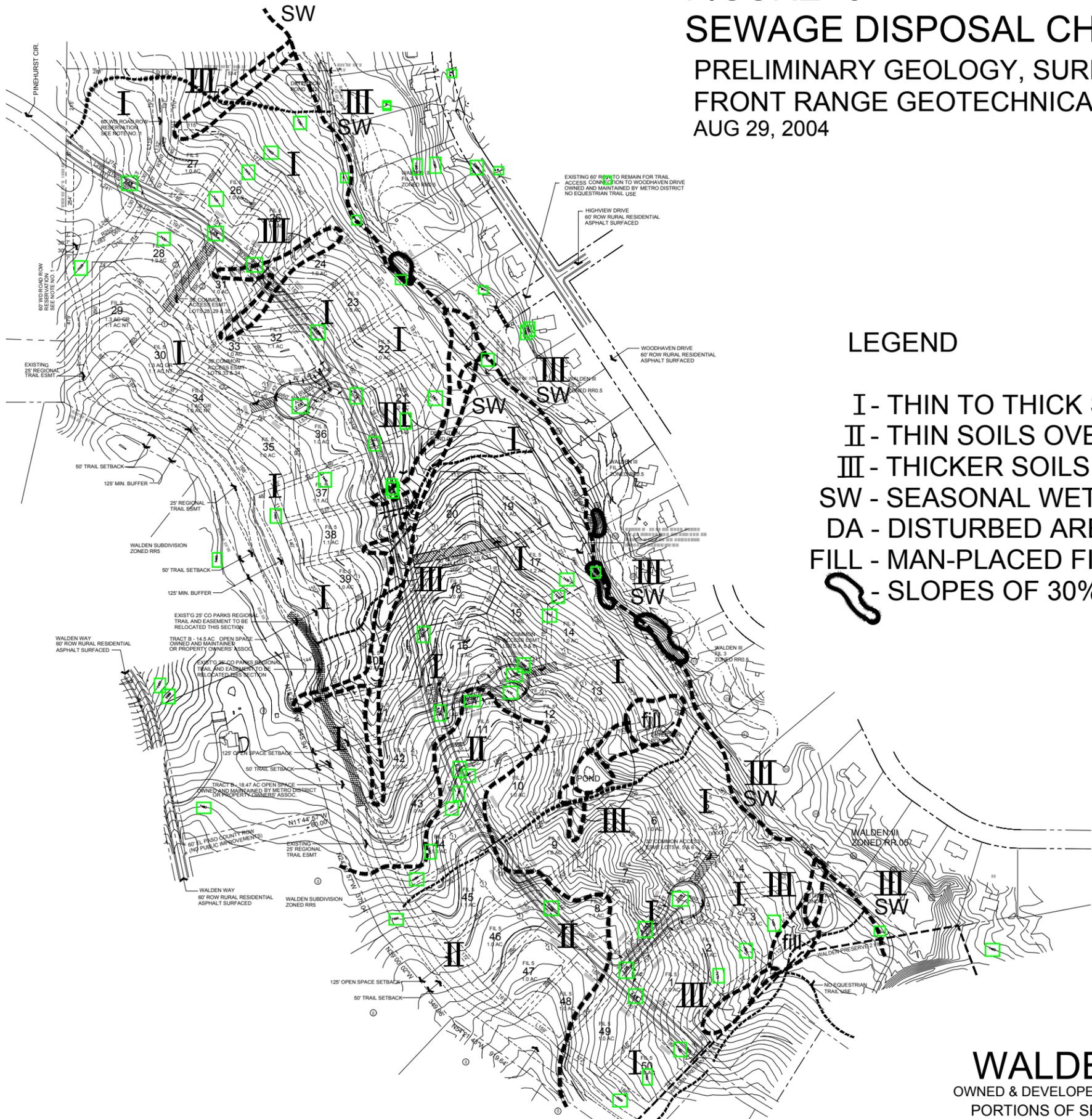


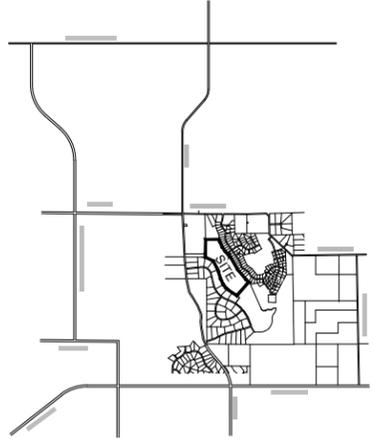
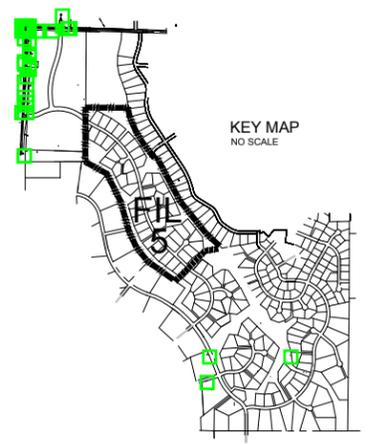
FIGURE "3" SEWAGE DISPOSAL CHARACTERISTICS MAP

PRELIMINARY GEOLOGY, SURFACE SOILS, AND SEWAGE DISPOSAL EVALUATION
FRONT RANGE GEOTECHNICAL, INC
AUG 29, 2004



LEGEND

- I - THIN TO THICK SURFICIAL EPOSITS OVR AWSON ARKOSE BEDROCK
- II - THIN SOILS OVER DAWSON ARKOSE BEDROCK
- III - THICKER SOILS IN SWAILS AND DRAINAGES
- SW - SEASONAL WET AREAS
- DA - DISTURBED AREAS
- FILL - MAN-PLACED FILL
- SLOPES OF 30% OR GREATER



WALDEN PRESERVE 2 - FILING NO. 5
OWNED & DEVELOPED BY: WALDEN HOLDINGS I LLC, 17145 COLONIAL PARK DR, MONUMENT, CO 80132
PORTIONS OF SEC 14, 15, 22 & 23, T11S, R66W, 6TH PM IN EL PASO COUNTY COLORADO

