2023 Financial Assurance Estimate Form

(with pre-plat construction)

			PROJEC	T INF	ORMATIO	N					
Hwy. 105 / Jackson Creek Pkwy. Int. Im	ps. (East of Int. only)			7/5	5/2023					CDR-2	237
Project Name				Da	ate				PCD File No.		
	1				11-2				6	Dict 0	• • • • • • • • • • • •
Description	0"	antity	Unite		Unit Cost			Total	(with Pre-	-Plat C	Pemaining
SECTION 1 - GRADING AND FROS		nstruction	and Perm	anent	BMPs)		-	iotai	70 complete		Kananing
Earthwork					. 5111 5)						
less than 1,000; \$5,300 min			CY	\$	8.00	=	\$	-		\$	-
1,000-5,000; \$8,000 min		2,000	CY	\$	6.00	=	\$	12,000.00		\$	12,000.00
5,001-20,000; \$30,000 min			CY	\$	5.00	=	\$	-		\$	-
20,001-50,000; \$100,000 min			CY	\$	3.50	=	\$	-		\$	-
50,001-200,000; \$175,000 min			CY	\$	2.50	=	\$	-		\$	-
greater than 200,000; \$500,000 mi	in		CY	\$	2.00	=	\$	-		\$	-
Permanent Erosion Control Blanket		650.0	SY	\$	8.00	=	\$	5,200.00		\$	5,200.00
Permanent Seeding (inc. noxious weed mg	mnt.) & Mulching	0.2	AC	\$	1,875.00	=	\$	375.00		\$	375.00
Permanent Pond/BMP (provide engineer's	estimate)		EA			=	\$	-		\$	-
Concrete Washout Basin			EA	\$	1,089.00	=	\$	-		\$	-
Inlet Protection		1	EA	\$	202.00	=	\$	202.00		\$	202.00
Rock Check Dam			EA	\$	605.00	=	\$	-		\$	-
Safety Fence				\$	3.00	=	\$	-		\$	-
Sediment Trap			EA	¢	2,132.00	=	\$	-		\$ *	-
Silt Fence		375		¢	3.00	_	\$ \$	1 125 00		ф ф	1 125 00
Slope Drain		375		¢ ¢	3.00 /10.00	_	۹ \$	1,125.00		≁ \$	1,123.00
Straw Bale			FA	\$	31.00	=	\$	-		≁ \$	-
Straw Wattle/Rock Sock		45	LF	\$	7.00	=	\$	315.00		\$	315.00
Surface Roughening			AC	\$	250.00		\$	-		\$	-
Temporary Erosion Control Blanket			SY	\$	3.00	=	\$	-		\$	-
Temporary Seeding and Mulching			AC	\$	1,666.00	=	\$	-		\$	-
Vehicle Tracking Control		1	EA	\$	2,867.00	=	\$	2,867.00		\$	2,867.00
						=	\$	-		\$	-
[insert items not listed but part of construction	ion plans]					=	\$	-		\$	-
	MAINTE	NANCE (3	5% of Con	nstruct	tion BMPs)	=	\$	1,578.15		\$	1,578.15
* - Subject to defect warranty financial assurance. A minim	num of 20% shall be		Sor	otion	1 Subtotal	_		22 662 15		*	22 662 15
retained until final acceptance (MAXIMON OF 80% COMP	LETE ALLOWED)		000	Stion	i oublotai	_	J.	23,002.15		₽	23,002.13
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SECTION 2 - PUBLIC IMPROVEME	NTS *							-			,
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS	NTS *			_							•
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control	NTS *	1.0	LS	\$	5,000.00	=	\$	5,000.00		\$	5,000.00
SECTION 2 - PUBLIC IMPROVEME <u>ROADWAY IMPROVEMENTS</u> Construction Traffic Control Aggregate Base Course (135 lbs/cf)	NTS *	1.0	LS Tons	\$	5,000.00 34.00	=	\$	5,000.00		\$ \$	5,000.00 -
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf)	NTS *	1.0	LS Tons CY	\$\$\$	5,000.00 34.00 61.00	=	\$ \$ \$	5,000.00 - -		\$ \$ \$	5,000.00 - -
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asgnalt Pavement (3" thick) Applied Pavement (4" thick)	NTS *	1.0	LS Tons CY SY	\$ \$ \$ \$	5,000.00 34.00 61.00 17.00	=	\$ \$ \$ \$	5,000.00 - - -		\$ \$ \$ \$	5,000.00 - - -
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick)	NTS *	1.0	LS Tons CY SY SY	\$ \$ \$ \$ \$	5,000.00 34.00 61.00 17.00 23.00	=	\$ \$ \$ \$ \$	5,000.00 - - - -		\$ \$ \$ \$ \$ \$	5,000.00 - - - -
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SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Epoxy Pavement Marking Delineator - Type 1 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (6" thick, 6' wide to include	e return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY SY Tons SF Nents Were	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 0.00 364.00 241.00 241.00 241.00 29.00 35.00 37.00 35.00 35.00 37.00 37.00 35.00		* *	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$, 5,000.00 - - - - - - - - - - - - - - - - -
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SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking pr Barricade - Type 3 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (6" thick, 6' wide to include Curb Opening with Drainage Chase	e return)	1.0 proven te that v review , signs, ngs, sto	LS Tons CY SY SY Tons SF nents were orm LF SY SY SY SY SY SY LF LF LF LF	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 10.00 10.00 28.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 72.00 87.00 116.00 1,390.00 1,390.00		. \$ <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td>, 5,000.00 - - - - - - - - - - - - - - - - -</td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$, 5,000.00 - - - - - - - - - - - - - - - - -
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Curb and Gutter, Type A (6" Vertica Pé Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, Iccal (6" thick, 6' wide to include Cross Pan, Iccal (6" thick, 6' wide to include Curb Opening with Drainage Chase Guardrail Type 3 (W-Beam)	e return) clude return)	1.0 proven te that v review , signs, ngs, sto	LS Tons CY SY SY Tons SF nents were orm LF SY SY SY SY SY SY LF LF LF LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 10.00 364.00 28.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 72.00 87.00 116.00 1,390.00 73.00 111.00 1,790.00 60.00		. \$ <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td>, 5,000.00 - - - - - - - - - - - - - - - - -</td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$, 5,000.00 - - - - - - - - - - - - - - - - -
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Barricade - Type 3 Curb and Gutter, Type A (6" Vertica Barricade - Type 1 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk 9 Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete)	e return) clude return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY SY Tons SF nents were orm LF SY SY SY SY SY EA LF LF EA LF	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 10.00 364.00 28.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 72.00 87.00 116.00 1,390.00 73.00 75		. \$ <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>* * * * * * * * * * * * * * * * * * * *</td><td></td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		* * * * * * * * * * * * * * * * * * * *	
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Barricade - Type 3 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 9 Cross Pan, local (8" thick, 6' wide to include Curb Opening with Drainage Chase Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete) Guardrail End Anchorage	e return) clude return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY Tons SF nents were brm LF SY SY SY SY SY EA LF LF EA	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 10.00 364.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 72.00 87.00 116.00 1,390.00 73.00 111.00 1,790.00 60.00 87.00 2,538.00		. . <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td></td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
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SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Delineator - Type 1 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (6" thick, 6' wide to include Cross Pan, collector (9" thick, 8' wide to include Cross Pan, collector (9" thick, 6' wide to include Cross Pan, collector (9" thick, 6' wide to include Cross Pan, collector (9" thick, 6' wide to include Cross Pan, collector (9" thick, 8' wide to include Cross Pan, collector (9" thick, 6' wide to include Curb Opening with Drainage Chase Guardrail Type 7 (Concrete) Guardrail Type 7 (Concrete) Guardrail Inpact Attenuator Sound Barrier Fence (CMU block, 6' high)	e return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY Tons SF nents were orm LF SY SY SY SY SY EA LF LF EA LF EA LF	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 28.00 241.00 28.00 241.00 29.00 35.000 35.00 35.00		. . <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td></td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Delineator - Type 1 Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type A (6" Vertica Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 9 Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include Cross Pan, local (8" thick, 8' wide to include Cross Pan, local (8" thick, 6' wide to include Curdrail Type 7 (Concrete) Guardrail Impact Attenuator Sound Barrier Fence (CMU block, 6' high) Sound Barrier Fence (panels, 6' high)	e return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY SY Tons SF Dents Were OT SY SY SY SY SY SY SY SY SY EA LF EA LF EA LF EA LF EA LF	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 10.00 364.00 28.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 35.00 35.00 35.00 116.00 1,390.00 72.00 87.00 111.00 1,790.00 60.00 87.00 87.00 95.00 95.00		. . <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td></td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
SECTION 2 - PUBLIC IMPROVEME ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Pf Barricade - Type 3 Curb and Gutter, Type A (6" Vertica Pf Curb and Gutter, Type B (Median) f Curb and Gutter, Type B (Median) Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk 9 Cross Pan, local (8" thick, 6' wide to include Cross Pan, local (8" thick, 6' wide to include Curb and Ramp Cross Pan, local (8" thick, 6' wide to include Curb Opening with Drainage Chase Guardrail Type 3 (W-Beam) Guardrail End Anchorage Guardrail End Anch	e return)	1.0 proven te that y review , signs, ngs, sto	LS Tons CY SY SY Tons SF nents were orm LF SY SY SY SY SY SY SY EA LF LF EA LF LF EA LF LF	\$ \$	5,000.00 34.00 61.00 17.00 23.00 35.00 106.00 10.00 28.00 241.00 29.00 35.00 35.00 35.00 35.00 35.00 35.00 35.00 116.00 87.00 1,390.00 73.00 1,190.00 60.00 87.00 2,538.00 95.00 95.00 97.00 2,000		. . <t< td=""><td>5,000.00 - - - - - - - - - - - - - - - - -</td><td></td><td>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</td><td></td></t<>	5,000.00 - - - - - - - - - - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	

Updated: 12/8/2022

		PROJECT	INFORMATIO	N				
Hwy. 105 / Jackson Creek Pkwy. Int. Imps. (East of Int	. only)		7/5/2023					CDR-237
Project Name			Date		_		PCD File No.	
			Unit				(with Pre	-Plat Construction)
Description	Quantity	Units	Cost			Total	% Complete	Remaining
	quantity	0		_	¢			¢ _
lineart items not listed but nort of construction plane?					Þ			- -
				=	>	-		Þ -
STORM DRAIN IMPROVEMENTS					<i>*</i>			*
Concrete Box Culvert (M Standard), Size (W X H)		LF		=	\$	-		\$ -
18" Reinforced Concrete Pipe		LF	\$ 76.00	=	\$	-		\$ -
24" Reinforced Concrete Pipe	8	LF	\$ 91.00	=	\$	728.00		\$ 728.00
30" Reinforced Concrete Pipe		LF	\$ 114.00	=	\$	-		\$ -
36" Reinforced Concrete Pipe		LF	\$ 140.00	=	\$	-		\$-
42" Reinforced Concrete Pipe		LF	\$ 187.00	=	\$	-		\$-
48" Reinforced Concrete Pipe		LF	\$ 228.00	=	\$	-		\$-
54" Reinforced Concrete Pipe		LF	\$ 297.00	=	\$	-		\$-
60" Reinforced Concrete Pipe		LF	\$ 348.00	=	\$	-		\$-
66" Reinforced Concrete Pipe		LF	\$ 402.00	=	\$	-		\$-
72" Reinforced Concrete Pipe		LF	\$ 460.00	=	\$	-		\$-
18" Corrugated Steel Pipe		LF	\$ 98.00	=	\$	-		\$ -
24" Corrugated Steel Pipe		LF	\$ 112.00	=	\$	-		\$ -
30" Corrugated Steel Pipe		LF	\$ 143.00	=	\$	-		\$ -
36" Corrugated Steel Pipe		LF	\$ 171.00	=	\$	-		\$ -
42" Corrugated Steel Pipe		LE	\$ 197.00	=	\$	-		¢ -
42 Corrugated Steel Pipe		L.	\$ 207.00	_	\$	-		÷ -
54" Corrugated Steel Pipe		LI	\$ 304.00	_	4	-		¢ _
60" Corrugated Steel Pipe			\$ 304.00	_	¢			
60 Confugated Steel Pipe			\$ 328.00	_	\$ \$			- -
56° Corrugated Steel Pipe			\$ 397.00	=	\$	-		⇒ -
72" Corrugated Steel Pipe		LF	\$ 467.00	=	\$	-		\$ -
78" Corrugated Steel Pipe		LF	\$ 537.00	=	\$	-		\$ -
84" Corrugated Steel Pipe		LF	\$ 642.00	=	\$	-		\$ -
(unit cost = 6x pipe unit cost)		FA		=	\$	-		\$-
Flared End Section (FES) CSP Size =		27.						
(unit cost = 6x pipe unit cost)		EA		=	\$	-		ş -
End Treatment- Headwall		EA		=	\$	-		\$ -
End Treatment- Wingwall		EA		=	\$	-		\$-
End Treatment - Cutoff Wall		EA		=	\$	-		\$-
Curb Inlet (Type R) L=5'. Depth < 5'		EA	\$ 6.703.00	=	\$	-		\$ -
Curb Inlet (Type R) L=5'. 5' ≤ Depth < 10'		EA	\$ 8.715.00	=	\$	-		\$ -
Curb Inlet (Type R) $ _{=5}'$ 10' < Depth < 15'		FA	\$ 10,092,00	=	\$	-		\$ -
Curb Inlet (Type R) $I = 10'$ Depth < 5'		FA	\$ 9,224,00	=	\$	-		\$ -
Curb Inlet (Type R) $L = 10'$, $5' \leq Depth \leq 10'$		EA	\$ 9,507,00	=	\$	-		¢ ¢ -
Curb Inlet (Type R) $L = 10'$, $3' = Depth < 10'$		EA	\$ 11,901,00	_	4	_		¢ _
Curb Inlet (Type R) $L = 15$, $10 = Deptit < 10$		EA	\$ 11,001.00	_	φ 4			φ
Curb Inlet (Type P) $L = 15'$, $Depth < 3'$		EA	\$ 12,555.00	_	4			Ψ
Curb Inlet (Type R) L = 15, $5 \le \text{Depth} < 10^{\circ}$		EA	\$ 12,050.00	_	\$ \$			- - -
Curb Iniei (Type R) L = 15, $10 \le \text{Depth} < 15$		EA	\$ 14,061.00	=	\$	-		э - *
Curb Inlet (Type R) L = 20', Depth $< 5'$		EA	\$ 12,783.00	=	\$	-		\$ -
Curb Inlet (Type R) L = 20', $5' \le \text{Depth} < 10'$		EA	\$ 14,109.00	=	\$	-		\$ -
Grated Inlet (Type C), Depth < 5		EA	\$ 5,611.00	=	\$	-		\$ -
Grated Inlet (Type D), Depth < 5'		EA	\$ 6,931.00	=	\$	-		\$ -
Storm Sewer Manhole, Box Base		EA	\$ 14,061.00	=	\$	-		\$ -
Storm Sewer Manhole, Slab Base	1	EA	\$ 7,734.00	=	\$	7,734.00		\$ 7,734.00
Geotextile (Erosion Control)		SY	\$ 8.00	=	\$	-		\$ -
Rip Rap, d50 size from 6" to 24"		Tons	\$ 97.00	-	\$	-		\$ -
Rip Rap, Grouted		Tons	\$ 115.00	=	\$	-		\$-
Drainage Channel Construction, Size (W x H)		LF	\$ -	=	\$	-		\$-
Drainage Channel Lining, Concrete		CY	\$ 689.00	=	\$	-		\$ -
Drainage Channel Lining, Rip Rap		CY	\$ 135.00	=	\$	-		\$-
Drainage Channel Lining, Grass		AC	\$ 1,776.00	=	\$	-		\$ -
Drainage Channel Lining, Other Stabilization				=	\$	-		\$ -
				=	\$	-		\$ -
[insert items not listed but part of construction plans]				=	\$	-		\$-
* - Subject to defect warranty financial assurance. A minimum of 20% shall be								
retained until final acceptance (MAXIMUM OF 80% COMPLETE ALLOWED)		Sect	ion 2 Subtotal	=	\$	13,462.00		\$ 13,462.00

		PROJECT	INF	ORMATIO	N					
Hwy. 105 / Jackson Creek Pkwy. Int. Imps. (East of I	nt. only)		7/5	/2023					CDR-	237
Project Name			Da	te		_		PCD File No.		
				Unit				(with Pre	-Plat (Construction)
Description	Quantity	Units		Cost			Total	% Complete		Remaining
SECTION 3 - COMMON DEVELOPMENT IMPR	OVEMENTS (Pri	vate or Di	stric	t and NOT	Maintair	ied by	EPC)**		_	
ROADWAY IMPROVEMENTS										
Retaining Wall (Adjacent to Hwy. 105)	1	EA	\$	200,000.00	=	\$	200,000.00		\$	200,000.00
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
STORM DRAIN IMPROVEMENTS (Exce	otion: Permanent Por	nd/BMP shall	be ite	mized under	Section 1)					
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
WATER SYSTEM IMPROVEMENTS										
Water Main Pipe (PVC), Size 8"		LF	\$	78.00	=	\$	-		\$	-
Water Main Pipe (Ductile Iron), Size 8"		LF	\$	91.00	=	\$	-		\$	-
Gate Valves, 8"		EA	\$	2,247.00	=	\$	-		\$	-
Fire Hydrant Assembly, w/ all valves		EA	\$	7,978.00	=	\$	-		\$	-
Water Service Line Installation, inc. tap and valves		EA	\$	1,601.00	=	\$	-		\$	-
Fire Cistern Installation, complete		EA			=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
SANITARY SEWER IMPROVEMENTS										
Sewer Main Pipe (PVC), Size 8"		LF	\$	78.00	=	\$	-		\$	-
Sanitary Sewer Manhole, Depth < 15 feet		EA	\$	5,305.00	=	\$	-		\$	-
Sanitary Service Line Installation, complete		EA	\$	1,696.00	=	\$	-		\$	-
Sanitary Sewer Lift Station, complete		EA			=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
LANDSCAPING IMPROVEMENTS	(For subdivision sp	ecific conditio	n of a	pproval, or Pl	JD)					
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
tt. Casting 2 is not achieved a defend warmach as a vice and		EA			=	\$	-		\$	
 Section 3 is not subject to detect warranty requirements 		Sect	ion 3	s Subtotal	=	\$	200.000.00		\$	200.000.00

		PROJECT	INFORMATIO	DN				
Hwy. 105 / Jackson Creek Pkwy. Int. Imps. (East of In	t. only)		7/5/2023					CDR-237
Project Name			Date				PCD File No.	
			Unit				(with Pre-	Plat Construction)
Description	Quantity	Units	Cost		То	tal	% Complete	Remaining
AS-BUILT PLANS (Public Improvements inc. Permanent W	QCV BMPs)	LS		=	\$	-		\$-
POND/BMP CERTIFICATION (inc. elevations and volume c	alculations)	LS		=	\$	-		\$-
				lota	Constructio	n Financia	al Assurance _	\$ 237,124.1
			(Sum of all se	ction subtot	als plus as-built	s and pond/B	MP certification)	
	Total Rom	aining Con	struction Fina	ncial Acc	uranco (with	Dro Diat C	onstruction)	e 227 124 1
							MD contification)	\$ 237,124.1
	(Sum of	all section tota	als less credit lor	terns comple	ete plus as-builts	s and pond/b	we certification)	
				Total D	efect Warran	ty Financia	al Assurance	\$ 6 207 4
		(20% of all ite	ms identified as (lateralized at tin	of prelimin	arv accentance)	\$ 0,207.4
		(2070 01 811 110). 10 00 001				
Annuala								
Approvais								
I hereby certify that this is an accurate and complete estimate	of costs for the wo	ork as shown o	n the Grading and	d Erosion Co	ntrol Plan and C	onstruction D	rawings associated	d with the Project.
		_						
Engineer (P.E. Seal Required)								
Approved by Owner (Applicant		-	Data					
Approved by Owner / Applicant			Date					



FINAL DRAINAGE REPORT FOR MONUMENT JUNCTION DEVELOPMENT HIGHWAY 105 CORRIDOR & JACKSON CREEK PARKWAY INTERSECTION IMPROVEMENTS

July 2023

Prepared for: ELITE PROPERTIES OF AMERICA, INC 2138 FLYING HORSE CLUB DR. COLORADO SPRINGS, CO 80921

Prepared by: CLASSIC CONSULTING 619 N. CASCADE AVE., SUITE 200 COLORADO SPRINGS CO 80903 (719) 785-0790

Job no. 1302.22



619 N. Cascade Ave, Suite 200 | Colorado Springs, CO 80903 | (719) 785-0790

ClassicConsulting.net

FINAL DRAINAGE REPORT FOR MONUMENT JUNCTION DEVELOPMENT – HIGHWAY 105 CORRIDOR & JACKSON CREEK PARKWAY INTERSECTION IMPROVEMENTS

DRAINAGE REPORT STATEMENT

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the Town for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

	Marc A. Whorton. Colorado P.E. #37155	 Date	
--	---------------------------------------	----------	--

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:	ELITE PROPERTIES OF AMERICA, INC.
By:	
Title:	
Address:	2138 FLYING HORSE CLUB DR.

COLORADO SPRINGS, CO 80921

TOWN OF MONUMENT:

Filed in accordance with Sections 12.13.010 of the Subdivision Ordinance for the Town of Monument, revised 1997 and 13.11.160 of the Zoning Ordinance for the Town of Monument, revised 1997.

For Town of Monument

Date

EL PASO COUNTY:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E. Date County Engineer, / ECM Administrator (Review only for Hwy. 105 intersection design east of Jackson Creek Pkwy.)

> CLASSIC CONSULTING ENGINEERS & SURVEYORS

FINAL DRAINAGE REPORT FOR MONUMENT JUNCTION DEVELOPMENT – HIGHWAY 105 CORRIDOR & JACKSON CREEK PARKWAY INTERSECTION IMPROVEMENTS

TABLE OF CONTENTS:

PURPOSE	Page	1
GENERAL DESCRIPTION	Page	1
EXISTING DRAINAGE CONDITIONS	Page	1
PROPOSED DRAINAGE CHARACTERISTICS	Page	4
DRAINAGE CRITERIA	Page	8
FLOODPLAIN STATEMENT	Page	8
SUMMARY	Page	8
REFERENCES	Page 2	10

APPENDICES

VICINITY MAP SOILS MAP (S.C.S. SURVEY) F.E.M.A. MAP JURISDICTIONAL DETERMINATION HYDROLOGIC / HYDRAULIC CALCULATIONS STORMWATER QUALITY / DETENTION CALCULATIONS DRAINAGE MAPS



PURPOSE

This document is the Final Drainage Report for the Monument Junction Development and the associated adjacent off-site improvements to Highway 105 and the intersection with Jackson Creek Parkway. The purpose of this report is to identify the existing drainage patterns in this corridor, define and detail practical solutions for the conveyance and attenuation of developed flows to minimize drainage impacts further downstream resulting from these regional roadway improvements as required by Town of Monument, El Paso County and CDOT. Two separate reports cover the on-site aspects of the Monument Junction Development. Please reference "Monument Junction East – Phase 1 PD Site Plan" and "Monument Junction West Filing No. 1", both prepared by Classic Consulting. These reports have been approved by the Town of Monument and detail and describe all the on-site drainage design for the development.

GENERAL DESCRIPTION

This report covers the Highway 105 corridor from the I-25 off-ramp to the Knollwood Drive intersection and the Jackson Creek Parkway improvements from Highway 105 to the high point in the road approximately 750 feet south of Highway 105. This area lies within Section 14, township 11 south, range 67 west of the 6th principal meridian, in El Paso County. This corridor is bounded on the north by CDOT property and private rural residential property, to the south by Monument Junction development and various commercial developments along Highway 105, to the east by existing Village Center at Woodmoor development and to the west by existing CDOT Right-of-way (Interstate-25).

The average soil condition reflects Hydrologic Group "D" (Alamosa Loam) as determined by the "Web Soil Survey of El Paso County Area," prepared by the Soil Conservation Service (see map in Appendix).

EXISTING DRAINAGE CONDITIONS

This corridor is entirely within the Dirty Woman Creek drainage basin. Existing slopes range from 1% to 33% and ground cover is predominantly paved roadway with native grass sideroad ditches with some trees and wetlands within the corridor. The current drainage pattern flows generally in a westerly direction towards the intersection of Highway 105 and the I-25 off-ramp where an existing 36" RCP culvert crosses the I-25 off-ramp. This natural drainageway just upstream of this facility contains wetland area within the natural channel behind the sidewalk along the south side of Highway 105. Please reference the Jurisdictional Determination (JD) Action No. SPA-2022-00180 that finds these wetlands to be non-jurisdictional. (See Appendix) The corridor east of Jackson Creek



Parkway contains an existing storm system collecting the developed street flows and the adjacent property along the south side of Highway 105.

The following off-site basins (OS-10 thru OS-18) are all along this stretch of the Highway 105 corridor east to Knollwood Drive including the intersection with Jackson Creek Parkway:

Basin OS-10 (Q_5 = 3 cfs, Q_{100} = 10 cfs) consists of the off-site property within the existing Right-of-Way for Highway 105 and the I-25 off-ramp. These flows travel as sheet flow in a northerly direction directly into the sideroad ditch along the south side of Highway 105 and the east side of the I-25 off-ramp. The flows then travel as ditch flow towards the intersection with the I-25 off-ramp. The total flows at this location are described later as Design Point H10.

Basin OS-16 ($Q_5 = 2 \text{ cfs}$, $Q_{100} = 5 \text{ cfs}$) consists of the off-site fully developed properties east of Jackson Creek Parkway and south of Highway 105. This basin consists of existing buildings, parking lot, drive aisle and landscape area. These developed flows travel into a landscape sediment area adjacent to the buildings and then directly into Basin OS-11. **Basin OS-11** ($Q_5 = 3 \text{ cfs}$, $Q_{100} = 6 \text{ cfs}$) consists of the off-site partially developed property due east of Jackson Creek Parkway just south of Highway 105. This basin consists of an existing building, parking lot, driveway and native planted slope adjacent to Jackson Creek Parkway. The combined developed flows travel in a westerly direction and directly into the sideroad ditch along Jackson Creek Parkway. However, the ditch on the east side of the road seems to end and these flows appear to spillover to the westerly side of the roadway (Design Point H7) as the northbound approach to the intersection with Highway 105 is superelevated due to the grade on Highway 105. At **Design Point H7** ($Q_5 = 5 \text{ cfs}$, $Q_{100} = 10 \text{ cfs}$) these combined flows are partially collected by an existing 10' Type R at-grade inlet ($Q_5 = 4.9 \text{ cfs}$, $Q_{100} = 7.7 \text{ cfs}$) with a flow-by of ($Q_5 = 0.1 \text{ cfs}$, $Q_{100} = 2.3 \text{ cfs}$). This minor flow-by continues around the corner and then in a westerly direction down the street within Basin OS-17. The collected flows along with the upstream flows are conveyed in an existing 30'' RCP storm pipe and daylight into the sideroad ditch along the south side of Highway 105.

Basin OS-12 (Q_5 **= 1.2 cfs,** Q_{100} **= 3 cfs)** consists of the most easterly portion of Highway 105 at the Knollwood Drive intersection. Portions of this basin include the existing paved roadway and naturally landscaped area within the ROW. It has been assumed that the upstream facilities (east of Knollwood Dr.) capture 100% of the minor flows but approximately 0.85 cfs bypass those facilities in the major event. (Information taken from recent "Preliminary Drainage Report Highway 105 Project A", prepared by HDR for El Paso County, dated November 2021) Thus, the



total flows are conveyed via curb and gutter in a westerly direction towards **Design Point H4 (Q₅= 1 cfs, Q₁₀₀= 3.8 cfs)**. At this location, an existing 5' Type R at-grade inlet collects a portion of these flows (Q_5 = 1 cfs, Q_{100} = 2.5 cfs) with a flow-by of (Q_5 = 0 cfs, Q_{100} = 1.3 cfs). This minor flow-by continues in a westerly direction down the street within Basin OS-13. The collected flows are conveyed in an existing 15" RCP storm pipe in a westerly direction under Highway 105.

Basin OS-13 (Q_5 **= 2 cfs, Q**₁₀₀**= 4 cfs)** consists of a portion of Highway 105 west of Knollwood Drive. Portions of this basin include the existing paved roadway and naturally landscaped area within the ROW. These flows along with the minor 100 yr. flow-by from Design Point H4 are conveyed via curb and gutter in a westerly direction towards **Design Point H5**. At this location, an existing 10' Type R at-grade inlet collects a portion of these flows (Q_5 **= 2 cfs, Q**₁₀₀**= 4.9 cfs**) with a flow-by of (Q_5 **= 0 cfs, Q**₁₀₀**= 0.4 cfs**). This minor flow-by continues in a westerly direction down the street within Basin OS-14. The collected flows combine with the upstream system and are conveyed in an existing 15" RCP storm pipe in a westerly direction.

Basin OS-14 (Q_5 **= 0.8 cfs, Q**₁₀₀**= 2 cfs)** consists of a portion of Highway 105 just east of Jackson Creek Parkway. Portions of this basin include the existing paved roadway and naturally landscaped area within the ROW. These flows along with the 100 yr. flow-by from Design Point H5 are conveyed via curb and gutter in a westerly direction towards **Design Point H6**. At this location, an existing 10' Type R at-grade inlet completely collects these flows with no flow-by. The total collected flows are then conveyed in an existing 24" RCP storm pipe in a southwesterly direction.

Basin OS-15 (Q_5 **= 4 cfs, Q**₁₀₀**= 8 cfs)** consists of the off-site partially developed property due east of Jackson Creek Parkway just south of Highway 105. This basin consists of existing buildings, parking lots, drive aisles and native undeveloped areas. These developed flows generally travel in a westerly direction towards a sediment basin up on top of the slope at the intersection with Jackson Creek Parkway. This facility does not seem to have any formal stormwater quality features but rather just a rip-rap basin with and existing 18" ADS storm outfall. This outfall conveys the flows directly into a grated inlet behind the curb along the east side of Jackson Creek Parkway. The flows are then conveyed under the roadway within an existing 30" RCP storm system. This system daylights into the sideroad ditch at the SW corner of Highway 105 and Jackson Creek Parkway.

Basin OS-17 (Q₅= 2 cfs, Q_{100} = 4 cfs) consists of a portion of Highway 105 within the intersection with Jackson Creek Parkway. The majority of this basin includes the existing paved roadway along with an area naturally landscaped



slope at the SE corner of the intersection. These flows along with the by-pass flows from Design Point H7 described above are conveyed via curb and gutter in a westerly direction towards **Design Point H8 (Q**₅= **2.1 cfs, Q**₁₀₀= **6.3 cfs)**. At this location, an existing 10' Type R at-grade inlet collects a portion of these flows (Q₅= **2.1 cfs, Q**₁₀₀= **5.5 cfs)** with a flow-by of (Q₅= **0 cfs, Q**₁₀₀= **0.8 cfs)**. This minor flow-by continues in a westerly direction down the street within Basin OS-18. The collected flows are conveyed out of the back of the inlet via a 24" RCP directly into the sideroad ditch along the south side of Highway 105.

Basin OS-18 (Q₅= **1.3 cfs, Q**₁₀₀= **2 cfs)** consists of a portion of Highway 105 just east of the intersection with the I-25 off-ramp. All of this basin includes the existing paved roadway. These flows along with the by-pass flows from Design Point H8 described above are conveyed via curb and gutter in a westerly direction towards **Design Point H9 (Q**₅= **1 cfs, Q**₁₀₀= **3 cfs)**. At this location, an existing 10' Type R sump inlet completely collects these flows. The collected flows are conveyed out of the back of the inlet via a 24" RCP directly into the sideroad ditch along the south side of Highway 105.

Design Point H10 (Q_5 **= 14 cfs,** Q_{100} **= 36 cfs)** consists of the total combined flows from all the tributary upstream basins described above. At this location, the natural ditch within CDOT ROW conveys the flows to an existing 36" RCP culvert under the I-25 off-ramp. This facility seems to adequately handle these current developed flows.

PROPOSED DRAINAGE CONDITIONS

Developed runoff from the proposed off-site public roadway improvements within the Highway 105 and Jackson Creek Parkway ROW corridors will be conveyed via surface drainage and public storm sewer systems to a proposed permanent storm water quality facility located at the SE corner of the intersection of the I-25 off-ramp and Highway 105. Given that these improvements span multiple jurisdictions, the proposed facilities will be designed and installed per the latest El Paso County ECM and Town of Monument drainage criteria and detailed in this report. See the following general descriptions of the anticipated developed design points and how all the developed flows will be mitigated:

Design Point D4 (Q₅= **1.4 cfs, Q**₁₀₀= **3.9 cfs)** consists of the most easterly portion of Highway 105 at the Knollwood Drive intersection within Basin OS12D. Portions of this basin include the existing paved roadway and naturally landscaped area within the ROW and new roadway improvements proposed by El Paso County. These developed flows include the minor 100 yr. flow-by of 0.85 cfs as described in the "Preliminary Drainage Report Highway 105



Project A", prepared by HDR for El Paso County, dated November 2021. The total flows are conveyed via curb and gutter in a westerly direction towards Design Point H4. At this location, a proposed 5' Type R at-grade inlet collects a portion of these flows (Q_5 = 1.4 cfs, Q_{100} = 2.5 cfs) with a flow-by of (Q_5 = 0 cfs, Q_{100} = 1.3 cfs). This minor flow-by continues in a westerly direction down the street within Basin OS13D. The collected flows are conveyed in a proposed 18" RCP storm pipe in a westerly direction under Highway 105. This proposed inlet and 18" RCP storm will be constructed as a part of the El Paso County Highway 105 Project A.

Design Point D5 (Q_5 **= 2 cfs, Q**₁₀₀**= 5 cfs)** consists of a portion of the redeveloped Highway 105 by El Paso County. At this location, a proposed 10' Type R at-grade inlet collects a portion of these flows (Q_5 **= 2 cfs, Q**₁₀₀**= 4.9 cfs)** with a flow-by of (Q_5 **= 0 cfs, Q**₁₀₀**= 0.4 cfs)**. This minor flow-by continues in a westerly direction down the street within Basin OS14D. The collected flows combine with the upstream system and are conveyed in a proposed 18" RCP storm pipe in a westerly direction. This proposed inlet and 24" RCP storm will be constructed as a part of the El Paso County Highway 105 Project A.

Design Point D6 (Q_5 **= 4 cfs, Q**₁₀₀**= 8 cfs)** consists of the off-site partially developed property due east of Jackson Creek Parkway just south of Highway 105. Basin OS-15D is the upstream basin that consists of existing buildings, parking lots, drive aisles and native undeveloped areas. These developed flows generally travel in a westerly direction and will continue to be captured by a proposed CDOT Type C inlet within their property, located behind the proposed retaining wall. Appropriate easement documents and agreements will need to be granted prior to construction. The collected flows will then be routed via a proposed 18" RCP pipe routed towards the proposed storm system within Highway 105. These flows then combine with the upstream flows described earlier and are conveyed further downstream in a westerly direction.

Design Point D7 (Q_5 **= 6 cfs, Q**₁₀₀**= 12 cfs)** consists of a portion of the proposed Jackson Creek Parkway road improvements and a few off-site basins to the east that are tributary to this location (Basins OS-16 and OS11D). Developed flows from these basins sheet flow towards Jackson Creek Parkway and enter the roadway. This portion of the road will remain superelevated and the flows sheet flow towards the median and a proposed 10' Type R at-grade inlet. This facility collects a portion of these flows (Q_5 = 5.4 cfs, Q_{100} = 8.2 cfs) with a flow-by of (Q_5 = 0.6 cfs, Q_{100} = 3.8 cfs). This flow-by continues in a northerly direction down the street within Basin OS14D. The collected flows are conveyed in a proposed 18" RCP storm pipe in a northerly direction.



Design Point D8 (Q_5 **= 3 cfs,** Q_{100} **= 8 cfs)** consists of a portion of the intersection including both proposed Jackson Creek Parkway and Highway 105 road improvements. Developed flow from this basin along with the flow-by described above sheet flow towards the intersection and a proposed 10' Type R sump inlet within the median. This facility completely collects these flows with a maximum ponding elevation of 6". The collected flows combine with the routed upstream flows and are conveyed in a proposed 24" RCP storm pipe in a westerly direction.

Design Point D9 (Q_5 **= 2 cfs, Q**₁₀₀**= 5 cfs)** consists of a portion of the proposed Jackson Creek Parkway road improvements (Basin JPC7) and the on-site basin G. Developed flows from these basins sheet flow towards Jackson Creek Parkway and enter the roadway as curb and gutter flow towards a proposed 10' Type R at-grade inlet. This facility collects a portion of these flows (Q_5 = 2 cfs, Q_{100} = 4.8 cfs) with a flow-by of (Q_5 = 0 cfs, Q_{100} = 0.2 cfs). This flow-by continues in a westerly direction down the street within Basin OS17D. The collected flows are conveyed in a proposed 18" RCP storm pipe in a northerly direction.

Design Point D10 (Q_5 **= 3 cfs, Q**₁₀₀**= 6 cfs)** consists of a portion of the proposed Highway 105 road improvements within Basin OS17D. Developed flows from this basin along with the upstream flow-by sheet flow towards Highway 105. At this location a proposed 10' Type R at-grade inlet is proposed. This facility collects a portion of these flows (Q_5 **= 3 cfs, Q**₁₀₀**= 5.4 cfs)** with a flow-by of (Q_5 **= 0 cfs, Q**₁₀₀**= 0.8 cfs)**. This flow-by continues in a westerly direction down the street within Basin OS18D. The collected flows are conveyed in a proposed 18" RCP storm pipe towards the proposed storm system behind the curb.

Design Point D11 (Q_5 **= 2 cfs, Q**₁₀₀**= 4 cfs)** consists of a portion of the proposed Highway 105 road improvements within Basin OS18D. Developed flows from this basin along with the minor upstream flow-by sheet flow towards Highway 105. At this location, an existing 10' Type R sump inlet completely collects these flows. The collected flows are conveyed out of the back of the inlet via an existing 24'' RCP directly into the proposed SWQ facility.

Basin H (Q₅= **0.4 cfs, Q**₁₀₀= **1.8 cfs)** consists of a small portion of the proposed commercial development that will likely be landscape area and continue to sheet flow directly into Basin OS10D. **Basin OS10D (Q**₅= **0.8 cfs, Q**₁₀₀= **4 cfs)** consists of the existing vegetated slope within CDOT ROW that sheet flows to the sideroad ditch along the east side of the I-25 off-ramp. The combined flows will continue to travel as ditch flow directly into the proposed SWQ facility.



Design Point 13 (Q₅= **18 cfs, Q**₁₀₀= **40 cfs)** consists of the total combined developed flows from all the tributary upstream basins within the Highway 105 corridor and Jackson Creek Parkway intersection described above. These developed flows compare to the pre-development flows as follows:

Developed Flows at exist. 36" RCP at I-25 off-ramp: $(Q_5 = 18 \text{ cfs}, Q_{100} = 40 \text{ cfs})$ Pre-developed flows at exist. 36" RCP at I-25 off-ramp: $(Q_5 = 14 \text{ cfs}, Q_{100} = 36 \text{ cfs})$

A proposed SWQ/detention facility is planned within CDOT Right-of-way to help manage the additional impervious area introduced within this roadway corridor created by the public roadway improvements. This facility is designed as an Extended Detention Basin (EDB) storm water quality facility with a full spectrum outlet box and associated forebay, micro pool, well screen, orifice plate, and 100-year outlet conveyance per the current drainage criteria manual. An IGA between CDOT and the Town of Monument will describe the ownership and maintenance responsibilities. The pond design allows for the required Water Quality Capture Volume with release though an orifice plate (Top of Micropool = 7004.50) and then the other storm events up to the 100 yr. event will be handled through a 6'x3' concrete outlet box (Top of box = 7010.00).

The following represents the required design for this facility (See Appendix):

SWQ Pond

Total tributary area:	11.84 ac.		
Effective Imperviousne	53.6%		
	Estimated		<u>Provided</u>
Zone 1 (WQCV)	0.21 Acft.		0.21 Acft
Zone 2 (EURV)	0.39 Acft.		0.39 Acft
Zone 3 (100-yr.)	0.52 Acft.		0.24 Acft
Total	1.12 Acft.		0.84 Acft

Top of Micropool elev:7004.506'x3' Conc. Outlet box with top of box height of 5.5' and exist. 36" RCP outfall pipeOrifice Plate design:Four holes = 1-3/16" dia. spaced 16.5"Calculations per MHFD-Detention_v4.05 spreadsheet:Pond Peak Design Release: $(Q_2 = 0.5 cfs, Q_5 = 4.6 cfs, Q_{100} = 25.2 cfs)$ Pre-developed Release: $(Q_2 = 10 cfs, Q_5 = 14 cfs, Q_{100} = 36 cfs)$

Please reference the IGA between CDOT and the Town of Monument for details on ownership and maintenance.



DRAINAGE CRITERIA

Hydrologic calculations were performed using the Town of Monument Standards, which follow the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in May 2014. The Rational Method was used to estimate storm water runoff anticipated from design storms for the 5 year and 100-year recurrence interval for local storm inlet and pipe facility sizing. Runoff Coefficients are based on the imperviousness of the particular land use and the hydrologic soil type in accordance with Table 6-6. The average rainfall intensity, by recurrence interval found in the Intensity-Duration-Frequency (IDF) curves in Figure 6-5. (See Appendix)

The UD-BMP spreadsheet (ver. 3.07) along with the MHFD-Detention spreadsheet (ver. 4.05) were used to calculate the required volume for the EURV and 100-year release. User input 1-hour precipitation values in the UD-Detention spreadsheet were taken from Table 6-2 Volume 1 Colorado Springs Drainage Criteria Manual.

FLOODPLAIN STATEMENT

No portion of this site is located within a floodplain as determined by the Flood Insurance Rate Maps (F.I.R.M.) Map Number 08041C0278G effective date, December 7, 2018 (See Appendix).

SUMMARY

Construction of these proposed public roadway improvements will not adversely affect the surrounding developments. All drainage facilities were sized using the current Drainage Criteria and will safely discharge storm water runoff to adequate outfalls. Developed flows will be routed to the proposed SWQ/detention facility within CDOT ROW and slowly released at historic rates. All existing downstream facilities will not be significantly affected upon the construction of these public improvements.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC

Marc A. Whorton, P.E. Project Manager

maw/130222/Reports/FDR - MJ West Hwy 105-JCP.doc



REFERENCES

- 1. City of Colorado Springs/County of El Paso Drainage Criteria Manual dated May 2014.
- 2. "Drainage Analysis Addendum No. 2 Village Center at Woodmoor", Classic Consulting Engineers and Surveyors, dated June 2009.
- 3. "Drainage Letter Amendment for the Drainage Analysis Addendum Village Center at Woodmoor", Classic Consulting Engineers and Surveyors, dated October 2010.
- 4. "Village Center @ Woodmoor Filing No.1" Berge-Brewer and Associates, Inc., dated January 2005.
- 5. "Drainage Basin Planning Study Dirty Woman Creek and Crystal Creek El Paso County," Kiowa Engineering Corporation, dated September 1993.
- 6. "MDDP for The Village" Classic Consulting, dated February 2020
- 7. "Final Drainage Report for Monument Junction East (Phase 1 PD Site Plan)", Classic Consulting, dated January 2022.
- 8. "Final Drainage Report for Monument Junction West Filing No. 1", Classic Consulting, dated March 2022.
- 9. "Preliminary Drainage Report Highway 105 Project A for El Paso County", HDR, Inc., dated November 2021.



APPENDIX



VICINITY MAP



MONUMENT JUNCTION DEVELOPMENT HIGHWAY 105 / JACKSON CREEK PKWY. INTERSECTION IMPROVEMENTS VICINITY MAP





SOILS MAP (S.C.S SURVEY)



USDA Natural Resources

Conservation Service

MAP	LEGEND	MAP INFORMATION			
Area of Interest (AOI) Area of Interest (AOI)	Spoil Area	The soil surveys that comprise your AOI were mapped at 1:24,000.			
Soils Soil Map Unit Polygons	Very Stony Spot Wet Spot	Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cau			
Soil Map Unit Lines		misunderstanding of the detail of mapping and accuracy of line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detain			
Special Point Features () Blowout	Water Features	scale.			
Borrow Pit	Streams and Canals Transportation	Please rely on the bar scale on each map sheet for map measurements.			
Clay Spot	Rails	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)			
Gravel Pit	US Routes	Maps from the Web Soil Survey are based on the Web Mer			
Candfill	Major Roads	distance and area. A projection that preserves area, such a Albers equal-area conic projection, should be used if more			
▲ Lava Flow ▲ Marsh or swamp	Background Aerial Photography	accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified da of the version date(s) listed below			
Mine or QuarryMiscellaneous Water		Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021			
Perennial Water Rock Outcrop		Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.			
Saline Spot		Date(s) aerial images were photographed: Aug 19, 2018– 23, 2018			
Sandy Spot		The orthophoto or other base map on which the soil lines w compiled and digitized probably differs from the background imagery displayed on these maps. As a result. some minor			
 Sinkhole Slide or Slip 		shifting of map unit boundaries may be evident.			
💋 Sodic Spot					



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Alamosa loam, 1 to 3 percent slopes	13.3	41.7%
92	Tomah-Crowfoot loamy sands, 3 to 8 percent slopes	18.6	58.3%
Totals for Area of Interest		32.0	100.0%



El Paso County Area, Colorado

1—Alamosa loam, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 3670 Elevation: 7,200 to 7,700 feet Farmland classification: Prime farmland if irrigated and reclaimed of excess salts and sodium

Map Unit Composition

Alamosa and similar soils: 85 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Alamosa

Setting

Landform: Flood plains, fans Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

A - 0 to 6 inches: loam Bt - 6 to 14 inches: clay loam Btk - 14 to 33 inches: clay loam Cg1 - 33 to 53 inches: sandy clay loam Cg2 - 53 to 60 inches: sandy loam

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water
(Ksat): Moderately high (0.20 to 0.60 in/hr)
Depth to water table: About 12 to 18 inches
Frequency of flooding: FrequentNone
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Very slightly saline to strongly saline (2.0 to 16.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: D Ecological site: R048AY241CO - Mountain Meadow Hydric soil rating: Yes

USDA

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021

El Paso County Area, Colorado

92—Tomah-Crowfoot loamy sands, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 36b9 Elevation: 7,300 to 7,600 feet Farmland classification: Not prime farmland

Map Unit Composition

Tomah and similar soils: 50 percent Crowfoot and similar soils: 30 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Tomah

Setting

Landform: Hills, alluvial fans Landform position (three-dimensional): Side slope, crest Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from arkose and/or residuum weathered from arkose

Typical profile

A - 0 to 10 inches: loamy sand

E - 10 to 22 inches: coarse sand

- Bt 22 to 48 inches: stratified coarse sand to sandy clay loam
- C 48 to 60 inches: coarse sand

Properties and qualities

Slope: 3 to 8 percent Depth to restrictive feature: More than 80 inches Drainage class: Well drained Runoff class: Medium Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Low (about 4.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: B Ecological site: R049XY216CO - Sandy Divide Hydric soil rating: No

USDA

Description of Crowfoot

Setting

Landform: Alluvial fans, hills Landform position (three-dimensional): Side slope, crest Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

A - 0 to 12 inches: loamy sand

- E 12 to 23 inches: sand
- Bt 23 to 36 inches: sandy clay loam
- C 36 to 60 inches: coarse sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: B Ecological site: R049XY216CO - Sandy Divide Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021 F.E.M.A. MAP



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile aselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website a http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table Vertical Datum Flooding Source Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NUMBER PANEL SUFFIX 080059 0278 080064 0278 Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details. Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the MAP NUMBER 08041C0278G MAP REVISED **DECEMBER 7, 2018**

JURISDICTIONAL DETERMINATION





DEPARTMENT OF THE ARMY CORPS OF ENGINEERS, ALBUQUERQUE DISTRICT SOUTHERN COLORADO REGULATORY BRANCH 201 WEST 8TH STREET, SUITE 350 PUEBLO, COLORADO 81003

June 23, 2022

Regulatory Division

SUBJECT: Jurisdictional Determination- Action No.SPA-2022-00180

Classic Communities Attn: Steve Schlosser 2138 Flying Horse Club Drive Colorado Springs, Colorado 80921 <u>sschlosser@classichomes.com</u>

Dear Mr. Schlosser:

This letter responds to your request for a jurisdictional determination (JD) for multiple aquatic resources associated with the Monument Junction-Highway 105 improvement Project. The project site is located near Dirty Woman Creek, centered at latitude 39.092991°, longitude -104.856431°, Colorado Springs, El Paso County, Colorado. We have assigned Action No. SPA-2022-00180 to your request. Please reference this number in all future correspondence concerning the site.

Based on the information provided, we concur with your aquatic resource delineation for the site, as depicted on the enclosed drawing labeled, *SPA-2022-00180, Figure 1*, prepared by Core Consultants, Inc. (enclosure 1). We have determined that the site does not contain waters of the United States that are subject to regulation under Section 404 of the Clean Water Act. The aquatic resources identified as *WT-A1 (0.169 acres), WT-A2 (0.006 acre), ST-A1 (0.003 acre), ST-A2 (0.001 acre), ST-A3 (0.001 acre), and ST-A4 (0.001 acre),* on the above drawing are man-made wetland and ditch features that were constructed in uplands, drain only uplands, and do not have relatively permanent flow. As such, these aquatic resources are not regulated by the U.S. Army Corps of Engineers. This disclaimer of jurisdiction is only for Section 404 of the Federal Clean Water Act.

We are enclosing a copy of the *Approved Jurisdictional Determination Form* for your site (enclosure 2). A copy of this JD is also available at <u>http://www.spa.usace.army.mil/reg/JD</u>. This approved JD is valid for five years unless new information warrants revision of the determination before the expiration date.

You may accept or appeal this approved JD or provide new information in accordance with the attached Notification of Administration Appeal Options and Process and Request for Appeal (NAAOP-RFA) (enclosure 3). If you elect to appeal this approved JD, you must complete Section II of the form and return it to the Army Engineer Division, South Pacific, CESPD-PDS-O, Attn: Tom Cavanaugh, Administrative

Appeal Review Officer, P.O. Box 36023, 450 Golden Gate Ave, San Francisco, CA 94102 within 60 days of the date of this notice. Failure to notify the Corps within 60 days of the date of this notice means that you accept the approved JD in its entirety and waive all rights to appeal the approved JD.

If you have any questions, please contact Senior Project Manager Kyle Zibung by email at <u>kyle.d.zibung@usace.army.mil</u>, or telephone at (651) 290-5877. For program information or to complete our Customer Survey, visit our website at <u>https://www.spa.usace.army.mil/Missions/Regulatory-Program-and-Permits/.</u>

Sincerely,

Kyle Zibung Senior Project Manager Southern Colorado Branch

Enclosures

CC:

Natalie Graves, Core Consultants, Inc. (ngraves@liveyourcore.com)





Figure 4.4 Potential WOTUS Location Map

REQUEST	FOR APPEAL	COCESS AND
Applicant: Classic Communities c/o Steve Schlosser	File No.: SPA-2022-00180	Date: June 23, 2022
Attached is:	I	See Section below
INITIAL PROFFERED PERMIT (Standard Perr	nit or Letter of permission)	Α
PROFFERED PERMIT (Standard Permit o	r Letter of permission)	В
PERMIT DENIAL		С
→ APPROVED JURISDICTIONAL DETERMIN	NATION	D
PRELIMINARY JURISDICTIONAL DETER	MINATION	E
SECTION I - The following identifies your rights and options Additional information may be found at <i>http://www.usace.arr</i> CFR Part 331.	regarding an administrative appeal ny.mil/cecw/pages/reg_materials.as	of the above decision. <i>px</i> or Corps regulations at 33
A: INITIAL PROFFERED PERMIT: You may accept or obje	ect to the permit.	
 ACCEPT: If you received a Standard Permit, you may s final authorization. If you received a Letter of Permissio Your signature on the Standard Permit or acceptance of waive all rights to appeal the permit, including its terms associated with the permit. 	sign the permit document and return n (LOP), you may accept the LOP a the LOP means that you accept the and conditions, and approved jurisd	it to the district engineer for nd your work is authorized. e permit in its entirety, and ictional determinations
 OBJECT: If you object to the permit (Standard or LOP) that the permit be modified accordingly. You must comp engineer. Your objections must be received by the distr forfeit your right to appeal the permit in the future. Upor objections and may: (a) modify the permit to address all objections, or (c) not modify the permit having determine evaluating your objections, the district engineer will send Section B below. 	because of certain terms and condi lete Section II of this form and return ict engineer within 60 days of the da receipt of your letter, the district en of your concerns, (b) modify the pe ed that the permit should be issued d you a proffered permit for your rec	tions therein, you may request in the form to the district ate of this notice, or you will gineer will evaluate your rmit to address some of your as previously written. After onsideration, as indicated in
B: PROFFERED PERMIT: You may accept or appeal the p	ermit	
 ACCEPT: If you received a Standard Permit, you may s final authorization. If you received a Letter of Permissio Your signature on the Standard Permit or acceptance of waive all rights to appeal the permit, including its terms associated with the permit. 	sign the permit document and return n (LOP), you may accept the LOP a f the LOP means that you accept the and conditions, and approved jurisd	it to the district engineer for nd your work is authorized. e permit in its entirety, and ictional determinations
• APPEAL: If you choose to decline the proffered permit therein, you may appeal the declined permit under the O Section II of this form and sending the form to the divisio the division engineer within 60 days of the date of this n	(Standard or LOP) because of certa Corps of Engineers Administrative A on engineer (address on reverse). T otice.	in terms and conditions opeal Process by completing his form must be received by
C: PERMIT DENIAL: You may appeal the denial of a perm by completing Section II of this form and sending the form to received by the division engineer within 60 days of the date	hit under the Corps of Engineers Ad the division engineer (address on r of this notice.	ninistrative Appeal Process everse). This form must be
D: APPROVED JURISDICTIONAL DETERMINATION: You information.	a may accept or appeal the approve	d JD or provide new
 ACCEPT: You do not need to notify the Corps to accept the date of this notice, means that you accept the appro- JD. 	t an approved JD. Failure to notify to be a solution to be all be an its entirety, and waive all be all be all be able to be a solution of the	he Corps within 60 days of rights to appeal the approved
• APPEAL: If you disagree with the approved JD, you mand Administrative Appeal Process by completing Section II (address on reverse). This form must be received by the	y appeal the approved JD under the of this form and sending the form to e division engineer within 60 days o	e Corps of Engineers the division engineer f the date of this notice.
E: PRELIMINARY JURISDICTIONAL DETERMINATION: ` JD. The Preliminary JD is not appealable. If you wish, you	You do not need to respond to the C may request an approved JD (which	orps regarding the preliminary nay be appealed), by

contacting the Corps district for further instruction. Also you may provide new information for further consideration by the Corps to reevaluate the JD.

SECTION II - REQUEST FOR APPEAL or OBJECTIONS TO AN INITIAL PROFFERED PERMIT

REASONS FOR APPEAL OR OBJECTIONS: (Describe your reasons for appealing the decision or your objections to an initial proffered permit in clear concise statements. You may attach additional information to this form to clarify where your reasons or objections are addressed in the administrative record.)

ADDITIONAL INFORMATION: The appeal is limited to a review of the administrative record, the Corps memorandum for the
record of the appeal conference or meeting, and any supplemental information that the review officer has determined is
needed to clarify the administrative record. Neither the appellant nor the Corps may add new information or analyses to the
record. However, you may provide additional information to clarify the location of information that is already in the
administrative record.
POINT OF CONTACT FOR QUESTIONS OR INFORMATION:

If you only have questions regarding the appeal process you may		
also contact:		
Thomas J. Cavanaugh		
Administrative Appeal Review Officer		
U.S. Army Corps of Engineers		
South Pacific Division		
P.O. Box 36023, 450 Golden Gate Ave		
San Francisco, California 94102		
Phone: 415-503-6574, FAX:415-503-6646		
Email: Thomas.J.Cavanaugh@usace.army.mil		
RIGHT OF ENTRY: Your signature below grants the right of entry to Corps of Engineers personnel, and any government		
consultants, to conduct investigations of the project site during the course of the appeal process. You will be provided a 15		
day notice of any site investigation and will have the opportunity to participate in all site investigations.		

	Date [.]	Telenhone number [.]
	Date.	reiephone number.
Circulations of encoderation except		
Signature of appellant of agent.		
5 11 5		

APPROVED JURISDICTIONAL DETERMINATION FORM U.S. Army Corps of Engineers

This form should be completed by following the instructions provided in Section IV of the JD Form Instructional Guidebook.

SECTION I: BACKGROUND INFORMATION

A. REPORT COMPLETION DATE FOR APPROVED JURISDICTIONAL DETERMINATION (JD): June 23, 2022

B. ST PAUL, MN DISTRICT OFFICE, FILE NAME, AND NUMBER: SPA-2022-00180, Classic Communities Highway 105 AJD

C. PROJECT LOCATION AND BACKGROUND INFORMATION:

State: Colorado County/parish/borough: El Paso County City: Monument

Center coordinates of site (lat/long in degree decimal format): Lat. 39.092991° N, Long. -104.856431° W.

Universal Transverse Mercator: 15

Name of nearest waterbody:

Name of watershed or Hydrologic Unit Code (HUC): 07020007

Check if map/diagram of review area and/or potential jurisdictional areas is/are available upon request.

Check if other sites (e.g., offsite mitigation sites, disposal sites, etc...) are associated with this action and are recorded on a different JD form.

D. <u>REVIEW PERFORMED FOR SITE EVALUATION (CHECK ALL THAT APPLY):</u>

- Office (Desk) Determination. Date: June 22, 2022
- Field Determination. Date(s): June 8, 2022

SECTION II: SUMMARY OF FINDINGS A. RHA SECTION 10 DETERMINATION OF JURISDICTION.

There are no "nonvigable waters of the US" within Divers and Herbers A of (DHA) invisition (as defined by 22

There are no "navigable waters of the U.S." within Rivers and Harbors Act (RHA) jurisdiction (as defined by 33 CFR part 329) in the review area.

B. CWA SECTION 404 DETERMINATION OF JURISDICTION.

There are no"waters of the U.S." within Clean Water Act (CWA) jurisdiction (as defined by 33 CFR part 328) in the review area.

- 1. Waters of the U.S.: N/A
- 2. Non-regulated waters/wetlands (check if applicable):¹

Potentially jurisdictional waters and/or wetlands were assessed within the review area and determined to be not jurisdictional. Explain: The review area for this determination is comprised of two linear wetlands labeled as WT-A1 (0.169 acres) and WT-A2 (0.006 acre) and four linear stream segments labeled as ST-A1 (0.003 acre), ST-A2 (0.001 acre), ST-A3 (0.001 acre), and ST-A4 (0.001 acre) in the February 2022, Core Consultants, Inc. Wetland Delineation Report. In 2005, the entire review area was graded for roadway improvements to Highway 105 and the I-25 interchange, thereby creating all six linear aquatic resources evaluated by this determination. Based on an analysis of multiple years of aerial photography, USDA web soil survey data, USGS topographic maps, USGS NHD, NWI mapping, February 2022, Core Consultants, Inc. Wetland Delineation Report, and a June 22, 2002 site visit, the Corps has determined that all six aquatic resources are linear roadside drainage features constructed in uplands during grading for the Highway 105 and the I-25 interchange projects. In accordance with Corps Regulations at 33 CFR Part 328.3(b) and associated Rapanos Guidance, the aformentioned aquatic features are not within the Corps jurisdiction because they were constructed in uplands, drain only uplands, and do not have relatively permanent flow.

SECTION III: CWA ANALYSIS

A. TNWs AND WETLANDS ADJACENT TO TNWs: N/A

- B. CHARACTERISTICS OF TRIBUTARY (THAT IS NOT A TNW) AND ITS ADJACENT WETLANDS (IF ANY): N/A
- C. SIGNIFICANT NEXUS DETERMINATION: N/A
- D. DETERMINATIONS OF JURISDICTIONAL FINDINGS. THE SUBJECT WATERS/WETLANDS ARE (CHECK ALL THAT APPLY): N/A

¹ Supporting documentation is presented in Section III.F.
E. ISOLATED [INTERSTATE OR INTRA-STATE] WATERS, INCLUDING ISOLATED WETLANDS, THE USE, DEGRADATION OR DESTRUCTION OF WHICH COULD AFFECT INTERSTATE COMMERCE, INCLUDING ANY SUCH WATERS (CHECK ALL THAT APPLY): N/A

F. NON-JURISDICTIONAL WATERS, INCLUDING WETLANDS (CHECK ALL THAT APPLY):

- If potential wetlands were assessed within the review area, these areas did not meet the criteria in the 1987 Corps of Engineers Wetland Delineation Manual and/or appropriate Regional Supplements.
- Review area included isolated waters with no substantial nexus to interstate (or foreign) commerce.
 - Prior to the Jan 2001 Supreme Court decision in "SWANCC," the review area would have been regulated based solely on the "Migratory Bird Rule" (MBR).
 - Waters do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction. Explain:
 - Other (explain, if not covered above):

Provide acreage estimates for non-jurisdictional waters in the review area, where the sole potential basis of jurisdiction is the MBR factors (i.e., presence of migratory birds, presence of endangered species, use of water for irrigated agriculture), using best professional judgment (check all that apply):

Non-wetland waters (i.e., rivers, streams): linear feet width (ft).

Lakes/ponds: acres.

Other non-wetland waters: acres. List type of aquatic resource:

Wetlands: acres.

Provide acreage estimates for non-jurisdictional waters in the review area that do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction (check all that apply):

- Non-wetland waters (i.e., rivers, streams): linear feet, width (ft).
- Lakes/ponds: acres.
- Other non-wetland waters: acres. List type of aquatic resource:
- Wetlands: acres.

SECTION IV: DATA SOURCES.

A. SUPPORTING DATA. Data reviewed for JD (check all that apply - checked items shall be included in case file and, where checked and requested, appropriately reference sources below):

- Maps, plans, plots or plat submitted by or on behalf of the applicant/consultant: February 2022, Core Consultants, Inc.
- Wetland Delineation Report
- Data sheets prepared/submitted by or on behalf of the applicant/consultant. Office concurs with data sheets/delineation report.
 - Office does not concur with data sheets/delineation report.
 - Data sheets prepared by the Corps:
 - Corps navigable waters' study:
- \square U.S. Geological Survey Hydrologic Atlas:
 - USGS NHD data. USGS 8 and 12 digit HUC maps.
- U.S. Geological Survey map(s). Cite scale & quad name: 1:24k-Monument
- USDA Natural Resources Conservation Service Soil Survey. Citation: Web Soil Survey
- \boxtimes National wetlands inventory map(s). Cite name: National Wetland Inventory
- State/Local wetland inventory map(s):
- FEMA/FIRM maps:
- (National Geodectic Vertical Datum of 1929) 100-year Floodplain Elevation is:
- Photographs: 🖂 Aerial (Name & Date): Site Photos contained in Feb 2022 Core Consultants, Inc. Wetland

Delineation Report

- or 🛛 Other (Name & Date):Google Earth- 1999, 2004, 2005, 2006, 2008, 2010, 2011, 2015,
- 2017, 2019, 2020
- Previous determination(s). File no. and date of response letter:
- Applicable/supporting case law:
- Applicable/supporting scientific literature:
- Other information (please specify):

B. ADDITIONAL COMMENTS TO SUPPORT JD:

HYDROLOGIC / HYDRAULIC CALCULATIONS



For Colorado Springs and much of the Fountain Creek watershed, the 1-hour depths are fairly uniform and are summarized in Table 6-2. Depending on the location of the project, rainfall depths may be calculated using the described method and the NOAA Atlas maps shown in Figures 6-6 through 6-17.

Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth
2	1.19	1.70	2.10
5	1.50	2.10	2.70
10	1.75	2.40	3.20
25	2.00	2.90	3.60
50	2.25	3.20	4.20
100	2.52	3.50	4.60
<u>ر</u> ۲	Where Z=	6.840 ft/10)0

Table 6-2. Rainfall Depths for Colorado Springs

These depths can be applied to the design storms or converted to intensities (inches/hour) for the Rational Method as described below. However, as the basin area increases, it is unlikely that the reported point rainfalls will occur uniformly over the entire basin. To account for this characteristic of rain storms an adjustment factor, the Depth Area Reduction Factor (DARF) is applied. This adjustment to rainfall depth and its effect on design storms is also described below. The UDFCD UD-Rain spreadsheet, available on UDFCD's website, also provides tools to calculate point rainfall depths and Intensity-Duration-Frequency curves² and should produce similar depth calculation results.

2.2 Design Storms

Design storms are used as input into rainfall/runoff models and provide a representation of the typical temporal distribution of rainfall events when the creation or routing of runoff hydrographs is required. It has long been observed that rainstorms in the Front Range of Colorado tend to occur as either shortduration, high-intensity, localized, convective thunderstorms (cloud bursts) or longer-duration, lowerintensity, broader, frontal (general) storms. The significance of these two types of events is primarily determined by the size of the drainage basin being studied. Thunderstorms can create high rates of runoff within a relatively small area, quickly, but their influence may not be significant very far downstream. Frontal storms may not create high rates of runoff within smaller drainage basins due to their lower intensity, but tend to produce larger flood flows that can be hazardous over a broader area and extend further downstream.

• **Thunderstorms**: Based on the extensive evaluation of rain storms completed in the Carlton study (Carlton 2011), it was determined that typical thunderstorms have a duration of about 2 hours. The study evaluated over 300,000 storm cells using gage-adjusted NEXRAD data, collected over a 14-year period (1994 to 2008). Storms lasting longer than 3 hours were rarely found. Therefore, the results of the Carlton study have been used to define the shorter duration design storms.

To determine the temporal distribution of thunderstorms, 22 gage-adjusted NEXRAD storm cells were studied in detail. Through a process described in a technical memorandum prepared by the City of Colorado Springs (City of Colorado Springs 2012), the results of this analysis were interpreted and normalized to the 1-hour rainfall depth to create the distribution shown in Table 6-3 with a 5 minute time interval for drainage basins up to 1 square mile in size. This distribution represents the rainfall

Land Lice or Surface	Percent	Runoff Coefficients												
Characteristics	Impervious	2-γ	ear	5-γ	ear	10-1	/ear	25-1	<i>y</i> ear	50- ۲	/ear	100-	year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	H\$G A&B	H\$G C&D	
Business														
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89	
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68	
Residential														
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65	
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57	
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56	
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55	
Industrial														
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52	
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54	
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
Undeveloped Areas				• • • • •	-									
Historic Flow Analysis	2				•									
Greenbelts, Agriculture		0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51	
Pasture/Meadow	0	0.0Z	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	D.94	0.95	0.95	0.96	0.96	
Offsite Flow Analysis (when	45													
landuse is undefined)		0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59	
Streets				[}			
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0,70	0.74	
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Type of Land Surface	C _v
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Table 6-7.	Conveyance	Coefficient, C_{ν}
------------	------------	------------------------

For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_t) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of



Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations $I_{100} = -2.52 \ln(D) + 12.735$ $I_{50} = -2.25 \ln(D) + 11.375$ $I_{25} = -2.00 \ln(D) + 10.111$ $I_{10} = -1.75 \ln(D) + 8.847$ $I_5 = -1.50 \ln(D) + 7.583$ $I_2 = -1.19 \ln(D) + 6.035$ Note: Values calculated by
equations may not precisely
duplicate values read from figure.

JOB NAME:	MONUMENT JUNCTION DEVELOPMENT (HWY. 105 & JCP INT. IMPS.)
JOB NUMBER:	1302.22
DATE:	02/24/23
CALCULATED BY:	MAW

			F	INAL DR	AINAGE	REPORT	~ BASIN	RUNOFI	COEFFIC	IENT SUM	MARY					
		DEVEL	OPED AREA	/IMPERVIOU	S AREA	LAND	SCAPE/UNI	DEVELOPED	AREAS	I	NEIGHTED			WEIGHTED C	A	IMPERVIOUSNESS
	TOTAL															
BASIN	AREA (AC)	AREA (AC)	C(2)	C(5)	C(100)	AREA (AC)	C(2)	C(5)	C(100)	C(2)	C(5)	C(100)	CA(2)	CA(5)	CA(100)	%
G	0.20	0.05	0.79	0.81	0.88	0.15	0.03	0.09	0.36	0.22	0.27	0.49	0.04	0.05	0.10	25%
Н	0.57	0.05	0.79	0.81	0.88	0.52	0.03	0.09	0.36	0.10	0.15	0.41	0.06	0.09	0.23	10%
OS-10	4.10	0.60	0.89	0.90	0.96	3.50	0.03	0.09	0.36	0.16	0.21	0.45	0.64	0.86	1.84	16%
OS10D	2.00	0.10	0.89	0.90	0.96	1.90	0.03	0.09	0.36	0.07	0.13	0.39	0.15	0.26	0.78	7%
OS-11	1.70	0.80	0.89	0.90	0.96	0.90	0.02	0.08	0.35	0.43	0.47	0.64	0.73	0.79	1.08	45%
OS11D	1.70	1.20	0.89	0.90	0.96	0.50	0.03	0.09	0.36	0.64	0.66	0.78	1.08	1.13	1.33	71%
OS-12	0.51	0.27	0.89	0.90	0.96	0.24	0.03	0.09	0.36	0.49	0.52	0.68	0.25	0.26	0.35	54%
OS12D	0.58	0.31	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.49	0.52	0.68	0.28	0.30	0.39	54%
OS-13	0.67	0.40	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.54	0.57	0.72	0.36	0.38	0.48	61%
OS13D	0.67	0.40	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.54	0.57	0.72	0.36	0.38	0.48	61%
OS-14	0.28	0.15	0.89	0.90	0.96	0.13	0.03	0.09	0.36	0.49	0.52	0.68	0.14	0.15	0.19	55%
OS14D	0.86	0.72	0.89	0.90	0.96	0.14	0.03	0.09	0.36	0.75	0.77	0.86	0.65	0.66	0.74	84%
OS-15	1.60	1.20	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.68	0.70	0.81	1.08	1.12	1.30	76%
OS15D	1.60	1.20	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.68	0.70	0.81	1.08	1.12	1.30	76%
OS-16	1.00	0.70	0.89	0.90	0.96	0.30	0.02	0.08	0.35	0.63	0.65	0.78	0.63	0.65	0.78	67%
OS-17	0.53	0.43	0.89	0.90	0.96	0.10	0.03	0.09	0.36	0.73	0.75	0.85	0.39	0.40	0.45	82%
OS17D	1.00	0.60	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.55	0.58	0.72	0.55	0.58	0.72	61%
OS-18	0.30	0.30	0.89	0.90	0.96	0.00	0.03	0.09	0.36	0.89	0.90	0.96	0.27	0.27	0.29	100%
OS18D	0.78	0.43	0.89	0.90	0.96	0.35	0.03	0.09	0.36	0.50	0.54	0.69	0.39	0.42	0.54	56%
OS-19	0.18	0.00	0.89	0.90	0.96	0.18	0.03	0.09	0.36	0.03	0.09	0.36	0.01	0.02	0.06	2%
OS-20	0.11	0.01	0.89	0.90	0.96	0.10	0.03	0.09	0.36	0.11	0.16	0.41	0.01	0.02	0.05	10%
JCP7	0.59	0.50	0.89	0.90	0.96	0.09	0.03	0.09	0.36	0.76	0.78	0.87	0.45	0.46	0.51	85%
EX2	0.56	0.56	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.02	0.05	0.20	2%
EX3	1.80	1.80	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.05	0.16	0.65	2%
						ļ										
Exist. Trib. to Pond	13.05					┨────┤										37.5%
Dev. Trib. to Pond	11.84					 										53.6%
						 										
Dev. Trib. to Forebay	8.49					 										67.2%
				1		• •					1				1	

JOB NA	ME:	MONUME	ENT JUNCT	TION D	EVELO	PMEN'	T (HWY	. 105 &	JCP IN	NT. IMP	PS.)							
JOB NU	MBER:	1302.22						-					Table 6	-7. Cor	iveyance	e Coeffi	cient, C	v
DATE:		02/24/23											Trm	often	d Surfac	~		C
CALC'D	BY:	MAW										Heav	r yp	e of Lan	a Surfac	e	_	2.5
Ret	um 1-Hour							-				Tillad	y meado re/field	w		r		5
Per	iod Depth											Ripra	p (not b)	rried)*	$t_{c} = \frac{1}{15}$	$\frac{5}{20} + 10$		6.5
2	1.19	1			0 205(1	1 0	\ TT					Short	pasture	and lawn	. 10		_	7
	1.50	4		$t_i = -$	0.395(1	-1-C5	WL	1	$V = C_v \lambda$	$S_{w}^{0.5}$	Tc=L/V	Nearl	y bare gr	round				10
1	0 1.75	4				Seaso						Grass	sed water	way				15
2	2.00	4										Paveo	d areas ar	nd shallo	w paved	swales	1	20
2	0 2.25	4										For bu	ried riprap	, select C _v	value base	d on type o	f vegetativ	e cover.
10	2.52	1	FI	NAL D	RAIN	AGE F	REPOF	RT ~ B	ASIN	RUNC)FF Sl	JMMA	RY					
		WEIGHTEI	D		OVER	RLAND		STRE	ET / CH	ANNEL	FLOW	Tc		NTENSI	ΓY	TOT	AL FLC	JWS
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length	Height	Tc	Length	Slope	Velocity	Tc	TOTAL	I(2)	l(5)	I(100)	Q(2)	Q(5)	Q(100
	()			. ,	(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(in/hr)	(cfs)	(cfs)	(cfs)
G	0.04	0.05	0.10	0.09	30	1.5	5.9					5.9	3.93	4.93	8.27	0.17	0.3	0.8
Н	0.06	0.09	0.23	0.09	40	2	6.8					6.8	3.76	4.71	7.91	0.2	0.4	1.8
											1							
OS-10	0.64	0.86	1.84	0.09	65	2	10.1	950	3.5%	1.9	8.5	18.6	2.56	3.20	5.37	2	3	10
OS10D	0.15	0.26	0.78	0.09	65	2	10.1	950	3.5%	1.9	8.5	18.6	2.56	3.20	5.37	0.4	0.8	4
OS-11	0.73	0.79	1.08	0.08	100	2	14.7	500	4.0%	2.0	4.2	18.8	2.54	3.18	5.34	1.9	3	6
OS11D	1.08	1.13	1.33	0.09	100	2	14.5	300	4.0%	2.0	2.5	17.0	2.66	3.33	5.59	3	4	7
OS-12	0.25	0.26	0.35	0.09	40	2	6.8	200	3.5%	3.7	0.9	7.7	3.61	4.53	7.60	0.9	1.2	3
OS12D	0.28	0.30	0.39	0.09	40	2	6.8	200	3.5%	3.7	0.9	7.7	3.61	4.53	7.60	1.0	1.4	3.0
OS-13	0.36	0.38	0.48	0.09	25	3	4.0	240	5.5%	4.7	0.9	5.0	4.12	5.17	8.68	1.5	2	4
OS13D	0.36	0.38	0.48	0.09	25	3	4.0	250	3.5%	3.7	1.1	5.1	4.09	5.13	8.61	1.5	2	4
OS-14	0.14	0.15	0.19	0.09	30	10	3.1	170	5.5%	4.7	0.6	5.0	4.12	5.17	8.68	0.6	0.8	2
OS14D	0.65	0.66	0.74	0.09	30	10	3.1	190	5.5%	4.7	0.7	5.0	4.12	5.17	8.68	3	3	6
OS-15	1.08	1.12	1.30	0.09	180	12	13.1	100	3.0%	1.7	1.0	14.0	2.89	3.62	6.08	3	4	8
OS15D	1.08	1.12	1.30	0.09	180	12	13.1	80	3.0%	3.5	0.4	13.5	2.94	3.68	6.18	3	4	8
OS-16	0.63	0.65	0.78	0.08	100	4	11.7	130	1.5%	1.2	1.8	13.4	2.94	3.69	6.19	1.9	2	5

JOB NAM JOB NU	ME: MBER:	MONUME 1302.22	ENT JUNCI	TION D	evelo	PMEN	T (HWY	<u>.</u> 105 &	JCP IN	T. IMP	S.)		Table 6	-7. Con	veyance	Coeffi	cient, <i>C</i>	y.
DATE:		02/24/23						-					Type	e of Lan	d Surfac	e		C_v
CALC'D	BY:	MAW						-				Heav	y meadow	N			1	2.5
Ret	un 1-Hour	T										Tillag	e/field		. 1	. 10		5
Pen	od Depth	+										Ripra	p (not bu	ried)*	$r_{c} = -\frac{1}{18}$	$\frac{-}{0}$ + 10	(5.5
5	1.50	+		(0.395(1	1 - C	VI			~ 0.5		Short	pasture a	and lawn	5			7
10	1.75	+		$t_i = -$		c ^{0.33}	/ -	L	$=C_{v}$	w	I C=L/V	Nearl	y bare gr	ound				10
2	2.00	+				,						Grass	ed water	way				15
50	2.25	+										Paveo	l areas ar	nd shallo	w paved	swales		20
10	0 2.52	+										For bu	ried riprap	select C _v	value based	i on type o	t vegetativ	e cover.
		1	FII	NAL D	RAIN	AGE R	REPOF	RT ~ B	ASIN	RUNO	FF SL	JMMA	RY					
		WEIGHTE	כ		OVER	LAND		STRE	ET / CH	ANNEL	FLOW	Tc	INTENSITY		Y	TOTAL FLOW		OWS
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length	Height	Тс	Length	Slope	Velocity	Тс	TOTAL	I(2)	l(5)	I(100)	Q(2)	Q(5)	Q(100)
	()		· · · ·	()	(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(in/hr)	(cfs)	(cfs)	(cfs)
OS-17	0.39	0.40	0.45	0.09	60	14	5.0	380	5.0%	4.5	1.4	6.4	3.82	4.80	8.05	1.5	2	4
OS17D	0.55	0.58	0.72	0.09	60	14	5.0	380	5.0%	4.5	1.4	6.4	3.82	4.80	8.05	2	3	6
OS-18	0.27	0.27	0.29	0.09	15	0.5	4.7	280	2.0%	2.8	1.6	6.4	3.83	4.80	8.06	1.0	1.3	2
OS18D	0.39	0.42	0.54	0.09	90	4	10.6	260	2.0%	2.8	1.5	12.1	3.07	3.84	6.45	1.2	1.6	3
OS-19	0.01	0.02	0.06	0.09	80	3.2	10.3	380	5.0%	4.5	1.4	11.7	3.10	3.89	6.53	0.02	0.1	0.4
OS-20	0.01	0.02	0.05	0.09	50	3	7.1					7.1	3.70	4.63	7.78	0.0	0.1	0.4
JCP7	0.45	0.46	0.51	0.09	20	0.6	5.7	300	4.5%	4.2	1.2	6.9	3.74	4.70	7.88	2	2	4
EX2	0.02	0.05	0.20	0.09	50	2	8.2					8.2	3.54	4.43	7.44	0.1	0.2	1.5
EX3	0.05	0.16	0.65	0.09	260	5	23.7					23.7	2.27	2.84	4.76	0.1	0.5	3

(PS.)
1

JOB NUMBER: 1302.22

DATE: 07/20/23

CALCULATED BY: MAW

FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY

					Inten	sity	Fl	ow	
Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	l(5)	l(100)	Q(5)	Q(100)	Inlet Size
H1	OS-1 thru OS-8	6.48	15.46	33.4	2.32	3.89	15	60	EXIST. 60" RCP CULVERT
H2	DP H1, OS-9, EX-1	9.17	25.43	39.4	2.07	3.48	19	88	EXIST. CDOT OUTFALL
H3	EX4	1.49	5.98	35.7	2.22	3.73	3	22	EXIST. SIDE ROAD DITCH
H4	OS-12	0.26	0.46	7.7	4.53	7.60	1	3	EXIST. 5' TYPE R AT- GRADE INLET
H5	OS-13, Flow-by from H4	0.38	0.63	5.0	5.17	8.68	2	5	EXIST. 10' TYPE R AT-GRADE INLET
H6	OS-14, Flow-by from H5	0.15	0.24	5.0	5.17	8.68	1	2	EXIST. 10' TYPE R AT-GRADE INLET
H7	OS-11 and OS-16	1.45	1.86	18.8	3.18	5.34	5	10	EXIST. 10' TYPE R AT-GRADE INLET
H8	OS-17, Flow-by from H7	0.42	0.73	6.4	4.80	8.05	2	6	EXIST. 10' TYPE R AT-GRADE INLET
H9	OS-18, Flow-by from H8	0.27	0.41	6.4	4.80	8.06	1	3	EXIST. 10' TYPE R AT-GRADE INLET
H10	EX2, EX3, OS-10 thru OS-18	5.09	7.60	23.7	2.84	4.76	14	36	EXIST. 36" RCP CDOT CULVERT

JOB NAME: MONUMENT JUNCTIC	N DEVELOPMENT (HWY. 105 & JCP INT. IMPS.)
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JOB NUMBER: 1302.22

DATE: 07/20/23 CALCULATED BY: MAW

FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY

				Inten	sity	Fl	ow		
Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	l(5)	l(100)	Q(5)	Q(100)	Inlet Size
D4	OS12D, 0.85 CFS 100Yr Flow-by from upstream	0.30	0.51	7.7	4.53	7.60	1.4	3.9	PROP. 5' TYPE R AT- GRADE INLET
D5	OS13D, Flow-by from D4	0.38	0.63	5.0	5.17	8.68	2	5	PROP. 10' TYPE R AT-GRADE INLET
D6	OS15D	1.12	1.30	13.5	3.68	6.18	4	8	PROP. CDOT TYPE C INLET
D7	OS11D, OS-16, OS-19, OS-20	1.81	2.22	17.0	3.33	5.59	6	12	PROP. 10' TYPE R AT-GRADE INLET
D8	OS14D, Flow-by from D5&D7	0.84	1.47	17.0	3.33	5.59	3	8	PROP. 10' TYPE R SUMP INLET
D9	JCP7, G	0.51	0.61	6.9	4.70	7.88	2	5	PROP. 10' TYPE R AT-GRADE INLET
D10	OS17D, Flow-by from D9	0.58	0.74	6.4	4.80	8.05	3	6	PROP. 10' TYPE R AT-GRADE INLET
D11	OS18D, Flow-by from D10	0.42	0.64	12.1	3.84	6.45	2	4	EXIST. 10' TYPE R SUMP INLET
13	G, H, JCP7, OS10D thru OS15D, OS-16, OS17D, OS18D, OS-19, OS-20	5.87	8.01	21.1	3.01	5.05	18	40	SWQ FACILITY in CDOT ROW

JOB NUMBER: 1302.22 DATE: 07/20/23	JOB NAME:	MONUMENT JUNCTION DEVELOPMENT	. (HWY. 105 &	JCP INT. IMPS
DATE: 07/20/23	JOB NUMBER:	1302.22		
	DATE:	07/20/23		
CALCULATED BY: <u>MAW</u>	CALCULATED BY:	MAW		

* PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE. REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

					Inten	sity	Fl	ow	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	l(5)	l(100)	Q(5)	Q(100)	Pipe Size*
H1	Inlet Capture at DP-H4	0.26	0.24	7.7	4.53	7.60	1	2	Exist. 15" RCP
H2	PR-H1, Inlet Capture at DP-H5	0.65	0.77	7.8	4.51	7.57	3	6	Exist. 15" RCP
H3	PR-H2, Inlet Capture at DP-H6	0.80	1.01	7.9	4.49	7.54	4	8	Exist. 24" RCP
H4	OS-15	1.12	1.30	14.0	3.62	6.08	4	8	Exist. 18" ADS
H5	PR-H3, PR-H4, Portion of OS-11 and OS-16	3.20	3.95	18.8	3.18	5.34	10	21	Exist. 30" RCP
H6	Inlet Capture at DP-H8	0.42	0.64	6.4	4.80	8.05	2	5	Exist. 24" RCP
H7	Inlet Capture at DP-H9	0.27	0.41	6.4	4.80	8.06	1	3	Exist. 24" RCP

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY

JOB NAME:	MONUMENT JUNCTION DEVELOPMENT	T (HWY. 1	105 & JCP	INT. IMPS.)
JOB NUMBER:	1302.22			
DATE:	07/20/23			
CALCULATED BY:	MAW			

* PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE. REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

					Inten	sity	Fle	ow	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	l(5)	l(100)	Q(5)	Q(100)	Pipe Size*
1	Inlet Capture at D4	0.30	0.33	7.7	4.53	7.60	1.4	2.5	PROP. 18" RCP
2	PR-1, Inlet Capture at D5	0.69	0.92	7.7	4.53	7.60	3	7	PROP. 24" RCP
3	CDOT Type C Inlet Capture at D6	1.12	1.30	13.5	3.68	6.18	4	8	PROP. 18" RCP
4	PR-2, PR-3	1.80	2.22	13.7	3.66	6.15	7	14	PROP. 24" RCP
5	Inlet Capture at D7	1.63	1.51	17.0	3.33	5.59	5	8	PROP. 18" RCP
6	PR-5, Inlet Capture at D8	2.47	2.98	17.0	3.33	5.59	8	17	PROP. 24" RCP
7	PR-6, Inlet Capture at D9	2.98	3.56	17.0	3.33	5.59	10	20	PROP. 24" RCP
8	PR-4, PR-7	4.79	5.77	17.2	3.32	5.56	16	32	PROP. 30" RCP
9	Inlet Capture at D10	0.58	0.66	6.4	4.80	8.05	3	5	PROP. 18" RCP
10	PR-8, PR9	5.36	6.43	17.4	3.30	5.54	18	36	PROP. 30" RCP
11	Inlet Capture at D11	0.42	0.64	12.1	3.84	6.45	2	4	EXIST. 18" RCP

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY



Unresolved:

Include calculation for drainage swale along top of retaining wall to show that it is sized to handle the flow.







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.0	2.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	66	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.0	4.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	93	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.0	2.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q₂/Q₀ =	C% =	100	100	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.9	7.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	97	77	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.1	5.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	87	%



INLET IN A SUMP OR SAG LOCATION





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening]
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	3.8	6.0	inches
Grate Information		MINOR	MAJOR	🥅 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	•
Length of a Unit Curb Opening	L _o (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Poduction (Coloulated)	-	MINOR	MAIOR	-
Depth for Grate Midwidth	da . =	N/A	N/A	Tft
Depth for Curb Opening Weir Equation	d _{Grate} =	0.15	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	REcombination =	0.36	0.50	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{curb} =	0.77	0.93	1
Grated Inlet Performance Reduction Factor for Long Inlets	RFGrate =	N/A	N/A	1
· · · · · · · · · · · · · · · · · · ·	Giale			
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	2.1	8.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.0	2.8	cfs









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.4	2.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	97	66	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.0	4.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	93	%

Version 4.06 Released August 2018

AREA INLET IN A SWALE



Version 4.06 Released August 2018

AREA INLET IN A SWALE



Warning 04: Froude No. exceeds USDCM Volume I recommendation.









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STORM	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	5.4	8.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.6	3.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	90	68	%



INLET IN A SUMP OR SAG LOCATION





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Type = CDOT Type R Curb Opening		1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information		MINOR	MAJOR	🥅 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	•
Length of a Unit Curb Opening	L _o (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	1.00	1.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C ₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.42	0.42	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	0.57	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	0.93	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.0	10.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.6	9.8	cfs








Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.0	4.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	95	%









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.0	5.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	88	%



INLET IN A SUMP OR SAG LOCATION





Design Information (Input)		т	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	1
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L _o (G) =	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical val	lue 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical v	ralue 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		L _o (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in	n Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in In	ches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	C _f (C) =	0.10	0.10]
Curb Opening Weir Coefficient (ty	/pical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduct	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d _{Curb} =	0.33	0.33	ft
Combination Inlet Performance R	eduction Factor for Long Inlets	RF _{Combination} =	0.57	0.57	1
Curb Opening Performance Redu	ction Factor for Long Inlets	RF _{Curb} =	0.93	0.93	
Grated Inlet Performance Reducti	on Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
			MINOR	MAJOR	
Total Inlet Interception Ca	apacity (assumes clogged condition)	Q _a =	8.3	8.3	cfs
Inlet Capacity IS GOOD for Mine	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.6	3.8	cfs

	T _c How angle Area) ↓Y	
Design Information (Input)			
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	18.00	inches
Design discharge	Q =	2.50	cfs
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	1.77	sa ft
Full-flow wetted perimeter	Pf =	4.71	ft.
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Of =	10.53	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number Calculation of Critical Flow Condition Half Central Angle (0CThetacc 3.14)</theta<3.14) 	Theta = $An = Tn = Pn = Pn = Pn = Pn = Pn = Pn = P$	1.23 0.51 1.41 1.84 0.50 4.88 2.50 23.7% 1.43	radians sq ft ft ft ft fps cfs of full flow supercritical
Critical flow area		1.3/	
Critical top width		1.47	
Critical top Width Critical flow donth		1.4/	
		2 00.00	
Critical Now Velocity		3.80	
		1.00	

	T _c How Area D	↓v ↓	
Design Information (Input)			
Pipe Invert Slope	So =	0.0536	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	18.00	linches
Design discharge	Q =	2.50	cfs
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	1.77	sq ft
Full-flow wetted perimeter	Pf =	4.71	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	24.38	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number Calculation of Critical Flow Condition Half Central Angle (0<theta-c<3.14) Critical flow area Critical top width</theta-c<3.14) </theta<3.14) 	Theta = $An = An = An = An = An = An = An = A$	0.97 0.28 1.24 1.45 0.32 8.89 2.50 10.3% 3.28 1.37 0.66 1.47	radians sq ft ft ft ft fps cfs of full flow supercritical radians sq ft ft
Critical flow depth	Yc =	0.60	ft
Critical flow velocity Critical Depth Froude Number	Vc =	3.80 1.00	fps
	с <u> </u>		

Flow	Tc D angle D	Ŷ	
Design Information (Input)			_
Pipe Invert Slope	So =	0.0568	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	24.00	inches
Design discharge	Q =	7.00	cfs
Eull-Elow Capacity (Calculated)			
Full-flow area	Δf =	3 14	lsa ft
Full-flow wetted perimeter	Pf =	6.28	
Half Central Angle	Theta =	3 14	Iradians
Full-flow canacity		54.06	
Calculation of Normal Flow Condition	۰ <u>۲</u>	5 1100	
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.03</td><td>radians</td></theta<3.14)<>	Theta =	1.03	radians
Flow area	An =	0.59	sq ft
Top width	Tn =	1.72	ft
Wetted perimeter	Pn =	2.06	ft
Flow depth	Yn =	0.49	ft
Flow velocity	Vn =	11.86	fps
Discharge	Qn =	7.00	cfs
Percent of Full Flow	Flow =	12.9%	of full flow
Normal Depth Froude Number	Fr _n =	3.56	supercritical
Calculation of Critical Flow Condition			
Hair Central Angle (U <ineta-c<3.14)< td=""><td>i neta-c =</td><td>1.51</td><td></td></ineta-c<3.14)<>	i neta-c =	1.51	
	AC =	1.45	
	[c =	2.00	$-\pi$
Critical flow depth	Yc =	0.94	$-\prod_{r=1}^{n}$
Critical flow velocity	Vc =	4.83	tps
Critical Depth Froude Number	$r_{c} = $	1.00	

+	T ₀ How Area	
Design Information (Input)		
Pipe Invert Slope	So = 0.0100	ft/ft
Pipe Manning's n-value	n = 0.0130	
Pipe Diameter	D = 18.00	inches
Design discharge	Q = 8.00	cfs
Full-Flow Capacity (Calculated)		
Full-flow area	Af = 1.77	sq ft
Full-flow wetted perimeter	Pf = 4.71	ft l
Half Central Angle	Theta = 3.14	radians
Full-flow capacity	Of = 10.53	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number Calculation of Critical Flow Condition Half Central Angle (0<theta-c<3.14) Critical flow area</theta-c<3.14) </theta<3.14) 	$\begin{array}{c} \text{Theta} = & 1.88 \\ \text{An} = & 1.22 \\ \text{Tn} = & 1.43 \\ \text{Pn} = & 2.82 \\ \text{Yn} = & 0.98 \\ \text{Vn} = & 6.56 \\ \text{Qn} = & 8.00 \\ \text{Flow} = & 76.0\% \\ \text{Fr}_{n} = & 1.25 \\ \end{array}$	radians sq ft ft ft ft fps cfs of full flow supercritical radians sq ft
Critical top width	Tc = 1.33	ft
Critical flow depth	Yc = 1.10	ft
Critical flow velocity	Vc = 5.78	fps
Critical Depth Froude Number	Fr _c = 1.00	

CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

MHFD-Culvert, Version 4.00 (May 2020) Project: MONUMENT JUNCTION DEVELOPMENT - HWY. 105 & JCP INT. IMPS. Pipe ID: Pipe Run 4

> Тc θ angle How Y Ател D Design Information (Input) Pipe Invert Slope 0.0763 ft/ft So = Pipe Manning's n-value 0.0130 n = Pipe Diameter D = 24.00 inches Design discharge 14.00 Q = cfs Full-Flow Capacity (Calculated) Full-flow area Af =3.14 sq ft Pf = Full-flow wetted perimeter 6.28 ft Half Central Angle 3.14 radians Theta = Full-flow capacity 62.66 Qf = cfs Calculation of Normal Flow Condition Half Central Angle (0<Theta<3.14) Theta = 1.21 radians Flow area An = 0.87 sq ft ft Top width Tn = 1.87 Wetted perimeter Pn =2.41 ft ft Flow depth 0.64 Yn =Flow velocity 16.07 Vn = fps Discharge Qn = 14.00 cfs Percent of Full Flow Flow = 22.3% of full flow Normal Depth Froude Number $Fr_n =$ 4.15 supercritical Calculation of Critical Flow Condition Half Central Angle (0<Theta-c<3.14) Theta-c = 1.93 radians Critical flow area Ac = 2.25 sq ft Critical top width Tc = 1.88 ft Critical flow depth Yc = 1.35 ft Critical flow velocity 6.22 Vc = fps Critical Depth Froude Number 1.00 $Fr_c =$

r.	Tc How Aren	↓¥	
· · · · · · · · · · · · · · · · · · ·	U	2	
Design Information (Input)			_
Pipe Invert Slope	So =	0.0448	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	18.00	inches
Design discharge	Q =	8.00	cfs
Eull-Flow Capacity (Calculated)			
Full-flow area	Δf =	1 77	lsa ft
Full-flow wetted perimeter	Pf =	4 71	
Half Central Angle	Theta =	3 14	
Full-flow capacity	Qf =	22.29	cfs
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.40</td><td>radians</td></theta<3.14)<>	Theta =	1.40	radians
Flow area	An =	0.69	sq ft
Top width	Tn =	1.48	ft
Wetted perimeter	Pn =	2.10	ft
Flow depth	Yn =	0.62	ft
Flow velocity	Vn =	11.58	fps
Discharge	Qn =	8.00	cfs
Percent of Full Flow	Flow =	35.9%	of full flow
Normal Depth Froude Number	Fr _n =	2.98	supercritical
Calculation of Critical Flow Condition			
Half Central Angle (0 <theta-c<3 14)<="" td=""><td>Theta-c =</td><td>2 05</td><td></td></theta-c<3>	Theta-c =	2 05	
Critical flow area		1 38	
Critical top width		1 33	
Critical flow depth		1 10	
Critical flow velocity		5 78	
Critical Depth Froude Number	Fr. =	1.00	
	··c L	2.00]

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	T _C How angle Y Area V	
Design Information (Input)		
Pipe Invert Slope	So = <u>0.0307</u>	ft/ft
Pipe Manning's n-value	n = 0.0130	
Pipe Diameter	D = 24.00	inches
Design discharge	Q = 17.00	cfs
Full-Flow Capacity (Calculated)		
Full-flow area	Af = 3.14	lsa ft
Full-flow wetted perimeter	Pf = 6.28	
Half Central Angle	Theta = 3.14	radians
Full-flow capacity	Of = 39.74	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number Calculation of Critical Flow Condition Half Central Angle (0<theta-c<3.14) Critical flow area</theta-c<3.14) </theta<3.14) 	Theta = 1.48 An = 1.40 Tn = 1.99 Pn = 2.97 Yn = 0.91 Vn = 12.16 Qn = 17.00 Flow = 42.8% Fr _n = 2.56 Theta-c = 2.08 Ac = 2.50 Tc = 1.75	radians sq ft ft ft ft fps cfs of full flow supercritical radians sq ft
Critical flow depth	IC = 1.75	
	10 = 1.49	
Critical Depth Froude Number	VC = 6.79 $Fr_c = 1.00$	
F		

t	Tc Flow Area D	Ì) ↓ ↓		
Design Information (Input)	_		_	
Pipe Invert Slope	So =	0.1140	ft/ft	
Pipe Manning's n-value	n =	0.0130		
Pipe Diameter	D =	24.00	inches	
Design discharge	Q =[20.00	cfs	
Full-Flow Capacity (Calculated)				
Full-flow area	Af =	3.14	lsa ft	
Full-flow wetted perimeter	Pf =	6.28	lft	
Half Central Angle	Theta =	3.14	radians	
Full-flow capacity	Qf =	76.59	cfs	
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area</theta<3.14) 	Theta = An =	1.26 0.98	radians sq ft	
Top width	Tn =	1.91	ft	
Wetted perimeter	Pn =	2.53	ft Per FCN	I section 3.3.1.1.8
Flow depth	Yn =[0.70]ft maximu	m storm sower
Flow velocity	Vn =	20.51	tips volocity	is 18 fre Ploseo
Discharge	Qn =	20.00	cfs review	is to ips. Flease
Percent of Full Flow	Flow =	26.1%	of full flerevise	1
Normal Depth Froude Number	Fr _n =[5.05	supercritical	
Calculation of Critical Flow Condition	[2.22	7	
Hair Central Angle (U <theta-c<3.14)< td=""><td>Ineta-c =</td><td>2.22</td><td>Iradians</td><td></td></theta-c<3.14)<>	Ineta-c =	2.22	Iradians	
Critical flow area	AC =	2./0	ISY IC	
Critical flow dopth		1.59		
Critical flow velocity		1.01	fnc	
Critical Depth Froude Number		1.40		
	п _с – [1.00	1	

	\frown		
	Flow Area	↓¥	
Decign Information (Input)	.5.0		
Design Information (Input)	so -	0.0065	
Pipe Manning's n-value	50 =	0.0005	
Pipe Maining's n-value		30.00	linchos
Pipe Didifielei Design discharge		32.00	cfc
	Q -	52.00	
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	4.91	sa ft
Full-flow wetted perimeter	Pf =	7.85	
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	33.16	cfs
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>2.19</td><td>radians</td></theta<3.14)<>	Theta =	2.19	radians
Flow area	An =	4.16	sq ft
Top width	Tn =	2.04	ft
Wetted perimeter	Pn =	5.47	ft
Flow depth	Yn =	1.97	ft
Flow velocity	Vn =	7.69	fps
Discharge	Qn =	32.00	cfs
Percent of Full Flow	Flow =	96.5%	of full flow
Normal Depth Froude Number	Fr _n =	0.95	subcritical
Calculation of Critical Flow Condition			
Half Central Angle (0 <theta-c<3 14)<="" td=""><td>Theta-c -</td><td>2 14</td><td>Iradians</td></theta-c<3>	Theta-c -	2 14	Iradians
Critical flow area		4 06	
Critical ton width		2 10	
Critical flow denth		1 93	
Critical flow velocity		7.88	
Critical Depth Froude Number	Fr. =	1 00	
	· · c =	1100	

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E	Te Te Te Te	4	
\ ←	Plow ange Area	V V	
Design Information (Input)			
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	18.00	inches
Design discharge	0 =	5.00	cfs
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	1.77	sq ft
Full-flow wetted perimeter	Pf =	4.71	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	10.53	cfs
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.54</td><td>radians</td></theta<3.14)<>	Theta =	1.54	radians
Flow area	An =	0.85	sq ft
Top width	Tn =	1.50	ft
Wetted perimeter	Pn =	2.31	ft
Flow depth	Yn =	0.73	ft
Flow velocity	Vn =	5.88	fps
Discharge	Qn =	5.00	cfs
Percent of Full Flow	Flow =	47.5%	of full flow
Normal Depth Froude Number	Fr _n =	1.38	supercritical
Calculation of Critical Flow Condition			
Half Central Angle (0 <theta-c<3.14)< td=""><td>Theta-c =</td><td>1.72</td><td>radians</td></theta-c<3.14)<>	Theta-c =	1.72	radians
Critical flow area	Ac =	1.05	sq ft
Critical top width	Tc =	1.48	ft
Critical flow depth	Yc =	0.86	ft
Critical flow velocity	Vc =	4.77	fps
Critical Depth Froude Number	Fr _c =	1.00	

	T _c How Area) ↓ →	
Design Information (Input)			
Pipe Invert Slope	So =	0.0080	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	30.00	inches
Design discharge	Q =	36.00	cfs
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	4.91	sq ft
Full-flow wetted perimeter	Pf =	7.85	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Of =	36.79	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number Calculation of Critical Flow Condition Half Central Angle (0<theta-c<3.14) Critical flow area Critical top width</theta-c<3.14) </theta<3.14) 	Theta = An = Tn = Pn = Yn = Yn = Vn = Qn = Flow = Fr _n = Theta-c = Ac = Tc =	2.22 4.21 2.00 5.54 2.00 8.54 36.00 97.9% 1.04 2.25 4.28 1.95	radians sq ft ft ft ft fps cfs of full flow supercritical radians sq ft
Critical flow depth	Yc =	2.03	ft
Critical flow velocity	Vc =	8.41	fps
Critical Depth Froude Number	Fr _c =	1.00	

DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.00 (May 2020) Project: MONUMENT JUNCTION - HWY. 105 / JCP INT. IMPROVEMENTS ID: 30" RCP STORMWATER QUALITY OUTFALL CIRCLE Soil Type: Choose One: Sandy Non-Sandy Design Information: cfs Design Discharge Q = 36 Circular Culvert: Barrel Diameter in Inches D = 30 inches Inlet Edge Type (Choose from pull-down list) Square Edge Projecting OR: Box Culvert: OR Barrel Height (Rise) in Feet H (Rise) = ft Barrel Width (Span) in Feet W (Span) = ft Inlet Edge Type (Choose from pull-down list) Number of Barrels # Barrels = 1 Inlet Elevation Elev IN = 7013.25 ft Outlet Elevation OR Slope Elev OUT = 7012.75 ft Culvert Lenath 1 = 100 ft Manning's Roughness n = 0.013 Bend Loss Coefficient k_b = 0 Exit Loss Coefficient k_x = 1 Tailwater Surface Elevation ft $Y_{t, Elevation} =$ Max Allowable Channel Velocity 7 V = ft/s Calculated Results: lft² Culvert Cross Sectional Area Available A = 4.91 Culvert Normal Depth $Y_n =$ 2.50 ft Culvert Critical Depth $Y_c =$ 2.03 ft Froude Number Fr = Pressure flow! Entrance Loss Coefficient 0.20 k_e = Friction Loss Coefficient k_f = 0.92 Sum of All Loss Coefficients 2.12 ft k_s = Headwater: Inlet Control Headwater $HW_{I} =$ 3.85 ft Outlet Control Headwater $HW_0 =$ 3.54 ft **Design Headwater Elevation** HW = 7017.10 ft HW/D > 1.5! Headwater/Diameter OR Headwater/Rise Ratio HW/D =1.54 Outlet Protection: ft^{0.5}/s Flow/(Diameter^2.5) $Q/D^{2.5} =$ 3.64 Tailwater Surface Height $Y_t =$ 1.00 ft Tailwater/Diameter Yt/D = 0.40 Expansion Factor 1/(2*tan(O)) = 3.82 Flow Area at Max Channel Velocity $A_t =$ 5.14 ft² Width of Equivalent Conduit for Multiple Barrels $W_{eq} =$ ft Length of Riprap Protection 11 ft L₀ = Width of Riprap Protection at Downstream End T = 6 ft Adjusted Diameter for Supercritical Flow Da = ft Minimum Theoretical Riprap Size d₅₀ min= 8 in Nominal Riprap Size d₅₀ nominal= 9 lin MHFD Riprap Type Type = L

	T _c How angle	↓ V	
Design Information (Input)			
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	18.00	inches
Design discharge	 0 =	4.00	cfs
	τ		
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	1.77	lsa ft
Full-flow wetted perimeter	Pf =	4.71	ft ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Of =	10.53	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) Flow area Top width Wetted perimeter Flow depth Flow velocity Discharge Percent of Full Flow Normal Depth Froude Number <u>Calculation of Critical Flow Condition</u> Half Central Angle (0<theta-c<3.14)< td=""><td>Theta = $\ An = \ Tn = \ Pn = \ Yn = \ Yn = \ Qn = \ Flow = \ Fr_n = \ Fr_n = \ Theta-c = \ Theta-c = \ Freta-c =$</td><td>1.42 0.72 1.48 2.14 0.64 5.55 4.00 38.0% 1.40</td><td>radians sq ft ft ft ft fps cfs of full flow supercritical</td></theta-c<3.14)<></theta<3.14) 	Theta = $\ An = \ Tn = \ Pn = \ Yn = \ Yn = \ Qn = \ Flow = \ Fr_n = \ Fr_n = \ Theta-c = \ Theta-c = \ Freta-c =$	1.42 0.72 1.48 2.14 0.64 5.55 4.00 38.0% 1.40	radians sq ft ft ft ft fps cfs of full flow supercritical
Critical flow area		0.91	
Critical top width		1 50	
Critical flow depth		0.77	
Critical flow velocity		4 41	
Critical Depth Froude Number	$Fr_c =$	1.00	

CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

Project: MONUMENT JUNCTION DEVELOPMENT - HWY. 105 & JCP INT. IMPS. Pipe ID: EXIST. 36" RCP CULVERT

	Tc How angle Area	↓ Y	
	17-13		
Design Information (Input)			
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	36.00	inches
Design discharge	Q =	40.00	cfs
Full-Flow Capacity (Calculated)	·		
Full-flow area	Af =	7.07	sq ft
Full-flow wetted perimeter	Pf =	9.42	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	66.88	cfs
Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.69</td><td>radians</td></theta<3.14)<>	Theta =	1.69	radians
Flow alea		2.05	
Notted perimeter		2.96	
		3.00	
		1.67	
	vn =	9.88	ips
Discharge	Qn =	40.00	
Percent of Full Flow		59.8%	
Normal Depth Froude Number	$r_n = $	1.49	supercritical
Calculation of Critical Flow Condition	Theta-c =	1 95	radians
Critical flow area		5 17	
Critical top width		2 78	
Critical flow depth		2.70	
		2.00	
Critical Depth Froude Number		1.00	
		1.00	

DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.00 (May 2020)
Project: MONUMENT JUNCTION - HWY. 105 / JCP INT. IMPROVEMENTS





System Input Summary

Rainfall Parameters

Rainfall Return Period: 100 **Rainfall Calculation Method:** Table

Time	Intensity
5	8.68
10	6.93
20	5.19
30	4.16
40	3.44
60	2.42
120	0.67

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20 Maximum Rural Overland Len. (ft): 500 Maximum Urban Overland Len. (ft): 300 Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00 Maximum Depth to Rise Ratio: 0.90 Maximum Flow Velocity (fps): 18.0 Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 7013.75

Manhole Input Summary:

		Giv	en Flow	Sub Basin Information								
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)		
OUTFALL 1	7016.92	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 1 SWR 1 - 1	7020.91	36.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 5 SWR 5 - 1	7017.60	5.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 2 SWR 2 - 1	7026.36	32.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 3 SWR 3 - 1	7036.03	14.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 4 SWR 4 - 1	7044.17	7.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 9 SWR 9 - 1	7059.12	2.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 10 SWR 10 - 1	7059.50	2.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 6 SWR 6 - 1	7026.36	20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 7 SWR 7 - 1	7030.00	17.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
MH 8 SWR 8 - 1	7037.20	8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		

Manhole Output Summary:

		Loc	al Contribu	ıtion			Total D	esign Flow		
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
OUTFALL 1	0.00	0.00	0.00	0.00	0.00	54.92	0.66	0.38	36.00	
MH 1 SWR 1 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	36.00	
MH 5 SWR 5 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5.00	
MH 2 SWR 2 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	32.00	
MH 3 SWR 3 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	14.00	
MH 4 SWR 4 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	7.00	
MH 9 SWR 9 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.50	
MH 10 SWR 10 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.50	
MH 6 SWR 6 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	20.00	
MH 7 SWR 7 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	17.00	
MH 8 SWR 8 - 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	8.00	

Sewer Input Summary:

		Ele	evation		Loss C	oeffici	ents	Given Dimensions			
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)	
MH 1 SWR 1 - 1	166.16	7012.75	0.5	7013.58	0.013	0.03	1.00	CIRCULAR	30.00 in	30.00 in	

MH 5 SWR 5 - 1	3.17	7014.58	1.0	7014.61	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in
MH 2 SWR 2 - 1	256.17	7014.08	0.5	7015.36	0.013	0.05	1.00	CIRCULAR	30.00 in	30.00 in
MH 3 SWR 3 - 1	187.50	7015.87	7.6	7030.16	0.013	0.05	1.00	CIRCULAR	24.00 in	24.00 in
MH 4 SWR 4 - 1	145.36	7030.66	5.7	7038.92	0.013	0.05	1.00	CIRCULAR	18.00 in	18.00 in
MH 9 SWR 9 - 1	275.71	7039.42	5.4	7054.20	0.013	0.83	0.00	CIRCULAR	18.00 in	18.00 in
MH 10 SWR 10 - 1	7.53	7054.70	1.1	7054.78	0.013	0.38	1.00	CIRCULAR	18.00 in	18.00 in
MH 6 SWR 6 - 1	41.85	7015.86	11.4	7020.63	0.013	0.83	1.00	CIRCULAR	24.00 in	24.00 in
MH 7 SWR 7 - 1	69.88	7021.13	3.1	7023.28	0.013	0.94	1.00	CIRCULAR	24.00 in	24.00 in
MH 8 SWR 8 - 1	200.00	7023.78	4.5	7032.73	0.013	0.05	1.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Fu Ca	ll Flow pacity	Critic	cal Flow		Normal Flow					
Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
MH 1 SWR 1 - 1	29.08	5.92	30.00	7.33	30.00	7.33	0.00	Pressurized	36.00	166.16	
MH 5 SWR 5 - 1	10.53	5.96	10.32	4.77	8.73	5.88	1.38	Pressurized	5.00	3.17	
MH 2 SWR 2 - 1	29.08	5.92	30.00	6.52	30.00	6.52	0.00	Pressurized	32.00	256.17	

Unresolved: Per storm profiles in CD set, pipe size is 24".

MH 3 SWR 3 - 1	62.62	19.93	16.17	6.22	7.71	16.06	4.14	Supercritical Jump	14.00	18.03	
MH 4 SWR 4 - 1	25.11	14.21	12.29	5.45	6.50	12.17	3.40	Supercritical	7.00	0.00	
MH 9 SWR 9 - 1	24.39	13.80	7.18	3.80	3.89	8.89	3.28	Supercritical	2.50	0.00	
MH 10 SWR 10 - 1	10.83	6.13	7.18	3.80	5.88	4.98	1.47	Supercritical	2.50	0.00	
MH 6 SWR 6 - 1	76.58	24.38	19.27	7.40	8.37	20.51	5.05	Supercritical Jump	20.00	11.11	Velocity is Too High
MH 7 SWR 7 - 1	39.79	12.66	17.83	6.79	10.96	12.17	2.56	Supercritical	17.00	0.00	
MH 8 SWR 8 - 1	22.28	12.61	13.15	5.78	7.46	11.57	2.98	Supercritical	8.00	0.00	

• A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe maximum storm sewer

• If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer. velocity is 18 fps. Please revise

• If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft^2)	Comment
MH 1 SWR 1 - 1	36.00	CIRCULAR	30.00 in	30.00 in	33.00 in	33.00 in	30.00 in	30.00 in	4.91	Existing height is smaller than the suggested height.

										Existing width is smaller than the suggested width. Exceeds max. Depth/Rise
MH 5 SWR 5 - 1	5.00	CIRCULAR	18.00 in	1.77						
MH 2 SWR 2 - 1	32.00	CIRCULAR	30.00 in	30.00 in	33.00 in	33.00 in	30.00 in	30.00 in	4.91	Existing height is smaller than the suggested height. Existing width is smaller than the suggested width. Exceeds max. Depth/Rise
MH 3 SWR 3 - 1	14.00	CIRCULAR	24.00 in	24.00 in	18.00 in	18.00 in	24.00 in	24.00 in	3.14	
MH 4 SWR 4 - 1	7.00	CIRCULAR	18.00 in	1.77						
MH 9 SWR 9 - 1	2.50	CIRCULAR	18.00 in	1.77						
MH 10 SWR 10 - 1	2.50	CIRCULAR	18.00 in	1.77						
MH 6 SWR 6 - 1	20.00	CIRCULAR	24.00 in	24.00 in	18.00 in	18.00 in	24.00 in	24.00 in	3.14	
MH 7 SWR 7 - 1	17.00	CIRCULAR	24.00 in	24.00 in	18.00 in	18.00 in	24.00 in	24.00 in	3.14	
MH 8 SWR 8 - 1	8.00	CIRCULAR	18.00 in	1.77						

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics where calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 7013.75

	Invert]	Elev.	Downstre L	eam Manhole osses	HG	L		EGL	
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
MH 1 SWR 1 - 1	7012.75	7013.58	0.00	0.00	7015.25	7016.52	7016.08	1.27	7017.36
MH 5 SWR 5 - 1	7014.58	7014.61	0.16	0.00	7017.40	7017.40	7017.52	0.01	7017.53
MH 2 SWR 2 - 1	7014.08	7015.36	0.03	0.18	7016.91	7018.46	7017.57	1.55	7019.12
MH 3 SWR 3 - 1	7015.87	7030.16	0.02	0.35	7019.18	7031.51	7019.48	12.62	7032.11
MH 4 SWR 4 - 1	7030.66	7038.92	0.01	0.06	7031.58	7039.94	7033.50	6.90	7040.40
MH 9 SWR 9 - 1	7039.42	7054.20	0.03	0.00	7039.97	7054.80	7040.97	14.05	7055.02
MH 10 SWR 10 - 1	7054.70	7054.78	0.01	0.00	7055.19	7055.38	7055.58	0.03	7055.60
MH 6 SWR 6 - 1	7015.86	7020.63	0.52	0.03	7019.04	7022.24	7019.67	3.42	7023.09
MH 7 SWR 7 - 1	7021.13	7023.28	0.43	0.17	7022.84	7024.77	7024.34	1.14	7025.48
MH 8 SWR 8 - 1	7023.78	7032.73	0.02	0.14	7024.92	7033.83	7026.48	7.87	7034.35

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * $V_{fi} ^ 2/(2*g)$
- Lateral loss = $V_{fo} \wedge 2/(2*g)$ Junction Loss K * $V_{fi} \wedge 2/(2*g)$.
- Friction loss is always Upstream EGL Downstream EGL.

STORMWATER QUALITY CALCULATIONS



	Design Procedure Form:	Extended Detention Basin (EDB)
	UD-BMP	(Version 3.07, March 2018) Sheet 1 of 3
Designer:	Marc A. Whorton, P.E.	
Company:	Classic Consulting	
Date:	July 20, 2023	
Project:	SWQ Facility in CDOT ROW	
Location.		
1. Basin Storage \	/olume	
A) Ellective imp	erviousness of Tributary Area, I _a	$I_a = 53.0$ %
B) Tributary Are	a's Imperviousness Ratio (i = $I_a/100$)	i = 0.536
C) Contributing	Watershed Area	Area = <u>11.840</u> ac
D) For Watersł	neds Outside of the Denver Region, Depth of Average	d ₆ = 0.42 in
Runoff Prod	ucing Storm	
E) Design Con	cept	Water Quality Canture Volume (WQQV)
(Select EUR	V when also designing for flood control)	Excess Urban Runoff Volume (EURV)
F) Design Volu	me (WQCV) Based on 40-hour Drain Time	V _{DESIGN} = ac-ft
(V _{DESIGN} = (1.0 * (0.91 * i ³ - 1.19 * i ² + 0.78 * i) / 12 * Area)	
G) For Waters	neds Outside of the Denver Region,	V _{DESIGN OTHER} =ac-ft
Water Quali (Vwocy other	ty Capture Volume (WQCV) Design Volume ₂ = (d _e *(V _{DESIGN} /0.43))	
(Only if a dif	ferent WQCV Design Volume (WQCV) Design Volume	V _{DESIGN USER} = 0.121 aC-π
I) NRCS Hydro	logic Soil Groups of Tributary Watershed	
i) Percenta	ge of Watershed consisting of Type A Soils	HSG _A = %
ii) Percenta iii) Percent	age of Watershed consisting of Type B Soils age of Watershed consisting of Type C/D Soils	HSG _B =%
J) Excess Urba For HSG A	in Runoπ Volume (EURV) Design Volume : EURV _A = 1.68 * i ^{1.28}	EURV _{design} =ac-f t
For HSG B	$EURV_{\rm B} = 1.36 * i^{1.08}$	
K) User Input o (Only if a dif	f Excess Urban Runoff Volume (EURV) Design Volume ferent EURV Design Volume is desired)	EURV _{design user} =
2. Basin Shape: L	ength to Width Ratio	L : W = 2.0 : 1
(A basin length	to width ratio of at least 2:1 will improve TSS reduction.)	
3. Basin Side Slop	es	
A) Basin Maxin (Horizontal	hum Side Slopes distance per unit vertical, 4:1 or flatter preferred)	Z = 3.00 ft / ft DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE
-		
4. Inlet		Concrete Forebay
A) Describe me	eans of providing energy dissipation at concentrated	
ínflow locati	ons:	
5. Forebay		
A) Minimum Fo	rebay Volume	V _{FMIN} = 0.004 ac-ft
(V _{FMIN}	= <u>3%</u> of the WQCV)	
B) Actual Forel	bay Volume	$V_F = 0.004$ ac-ft
C) Forebay Dep	th	
(D _F	= <u>18</u> inch maximum)	$D_{\rm F} = 18.0$ in
D) Forebay Dis	charge	
i) Undetain	ed 100-year Peak Discharge	Q ₁₀₀ = <u>36.00</u> cfs
ii) Forebav	Discharge Design Flow	Q _F = 0.72 cfs
(Q _F = 0.0	2 * Q ₁₀₀)	
E) Forebay Disc	charge Design	[Choose One
		Berm With Pipe Flow too small for berm w/ pipe
		Wall with Rect. Notch Wall with V-Notch Weir
F) Discharge Pi	pe Size (minimum 8-inches)	Calculated D _P =in
G) Rectangular	Notch Width	Calculated W _N =5.0 in

	Design Procedure Form:	Extended Detention Basin (EDB)	
Designer: Company: Date: Project: Location:	Marc A. Whorton, P.E. Classic Consulting July 20, 2023 Monument Junction Development - Hwy. 105 & JCP Int. Imps. SWQ Facility in CDOT ROW		Sheet 2 of 3
		C Churry Day	
 6. Trickle Channel A) Type of Tric 	l kle Channel	Choose One Concrete © Soft Bottom	PROVIDE A CONSISTENT LONGITUDINAL SLOPE FROM FOREBAY TO MICROPOOL WITH NO MEANDERING. RIPRAP AND SOIL RIPRAP LINED CHANNELS ARE
F) Slope of Trie	ckle Channel	S = 0.0200 ft / ft	NOT RECOMMENDED. MINIMUM DEPTH OF 1.5 FEET
7. Micropool and (Dutlet Structure		
A) Depth of Mi	cropool (2.5-feet minimum)	D _M = ft	
B) Surface Are	a of Micropool (10 ft ² minimum)	A _M = <u>48</u> sq ft	
C) Outlet Type		Choose One Orifice Plate Other (Describe):]
D) Smallest Dir (Use UD-Deten	mension of Orifice Opening Based on Hydrograph Routing tion)	D _{orffice} = 1.19 inches	
E) Total Outlet	Area	A _{ot} = <u>4.36</u> square	inches
8. Initial Surcharge	e Volume		
A) Depth of Init (Minimum re	tial Surcharge Volume commended depth is 4 inches)	D _{IS} = <u>6</u> in	
B) Minimum Init (Minimum vo	ial Surcharge Volume lume of 0.3% of the WQCV)	V _{IS} = <u>16</u> cu ft	
C) Initial Surcha	arge Provided Above Micropool	V _s = 24.0 cu ft	
9. Trash Rack			
A) Water Quali	ity Screen Open Area: A _t = A _{ot} * 38.5*(e ^{-0.095D})	A _t = <u>150</u> square	inches
B) Type of Scre in the USDCM, total screen are	een (If specifying an alternative to the materials recommended indicate "other" and enter the ratio of the total open are to the for the material specified.)	S.S. Well Screen with 60% Ope	in Area
	Other (Y/N): N		
C) Ratio of Tota	al Open Area to Total Area (only for type 'Other')	User Ratio =	
D) Total Water	Quality Screen Area (based on screen type)	A _{total} =sq. in.	
E) Depth of Des (Based on	sign Volume (EURV or WQCV) design concept chosen under 1E)	H= <u>5.5</u> feet	
F) Height of Wa	ater Quality Screen (H_{TR})	H _{TR} = 94 inches	
G) Width of Wa (Minimum of 12	ter Quality Screen Opening (W _{opening}) inches is recommended)	W _{opening} = <u>12.0</u> inches	VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.

	Design Procedure Form:	Extended Detention Basin (EDB)
Designer: Company: Date: Project: Location:	Marc A. Whorton, P.E. Classic Consulting July 20, 2023 Monument Junction Development - Hwy. 105 & JCP Int. Imps. SWQ Facility in CDOT ROW	Sheet 3 of 3
 Overflow Emb A) Describe of B) Slope of C (Horizonta) 	pankment embankment protection for 100-year and greater overtopping: Overflow Embankment al distance per unit vertical, 4:1 or flatter preferred)	Buried Rip-Rap Ze = 50.00 ft / ft
11. Vegetation		Choose One O Irrigated Not Irrigated
12. Access A) Describes	Sediment Removal Procedures	
Notes:		

Design Procedure Form: Extended Detention Basin (EDB)					
	UD-BMP	(Version 3.07, March 2018) Sheet 1 of 3			
Designer:	Marc A. Whorton, P.E.				
Company:	Classic Consulting				
Date:	July 20, 2023				
Project:	Monument Junction Development - Hwy. 105 & JCP Int. Imps.				
Location:	SWQ Facility - Forebay Sizing				
1 Pasin Storage \	(olumo				
1. Dasin otorage v					
A) Effective Imp	erviousness of Tributary Area, I _a	$I_a = \frac{67.2}{\%}$ %			
B) Tributary Are	a's Imperviousness Ratio (i = l _a / 100)	i =			
C) Contributing	Watershed Area	Area = 8.490 ac			
D) For Watersh	neds Outside of the Denver Region. Depth of Average	d _e = 0.42 in			
Runoff Prod	ucing Storm				
E) Design Con	cept	Choose One			
(Select EUR	V when also designing for flood control)	water Quality Capture Volume (WQCV) Evident Linher Durieff Volume (FUDV)			
E) Design Volu	me (WOCV) Resed on 40-bour Drain Time	V			
(V _{DESIGN} = (1	$1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$				
G) For Watersh	neds Outside of the Denver Region.	Vorsion oture=			
Water Quali	ty Capture Volume (WQCV) Design Volume				
(Vwqcv other	$R = (d_6^*(V_{\text{DESIGN}}/0.43))$				
H) User Input o	f Water Quality Capture Volume (WQCV) Design Volume	V _{DESIGN USER} = 0.121 ac-ft			
(Only if a dif	terent wQCV Design volume is desired)				
I) NRCS Hydro	logic Soil Groups of Tributary Watershed				
ii) Percenta	ige of Watershed consisting of Type A Soils age of Watershed consisting of Type B Soils	$HSG_A = \frac{1}{2}$			
iii) Percent	age of Watershed consisting of Type C/D Soils	HSG _{C/D} = %			
J) Excess Urba	n Runoff Volume (EURV) Design Volume				
For HSG A	$EURV_{A} = 1.68 * i^{1.28}$	EURV _{DESIGN} =ac-f t			
For HSG C	$D: EURV_{B} = 1.30^{\circ} I$				
K) User Input o	f Excess Urban Runoff Volume (EURV) Design Volume	EURV _{DESIGN LISEP} = ac-ft			
(Only if a dif	ferent EURV Design Volume is desired)				
2. Basin Shape: Le (A basin length	to width ratio of at least 2:1 will improve TSS reduction.)	L : W = <u>2.0</u> : 1			
Basin Side Slop	es				
A) Basin Maxin	num Side Slopes	Z = 3.00 ft / ft			
(Horizontal o	distance per unit vertical, 4:1 or flatter preferred)	DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE			
4 Inlet		Concrete Forebay			
4. Inici					
 A) Describe me inflow location 	eans of providing energy dissipation at concentrated				
5. Forebay					
A) Minimum Fo	rehav Volume	Vous.= 0.004 ac.ft			
(V _{FMIN}	= <u>3%</u> of the WQCV)				
B) Actual Foret	pay Volume	V _F = 0.004 ac-ft			
, () Earrhau Dar	46				
(D _F	= <u>18</u> inch maximum)	D _F = 18.0 in			
D) Forebay Dise	charge				
	or and 400 years Deals Discharge	0 - 2600 - 4			
I) Undetaine	au Iuu-year Peak Discharge	$u_{100} = 36.00$ cts			
ii) Forebay (Q _F = 0.0	Discharge Design Flow 2 * Q ₁₀₀)	Q _F =			
E) Forebay Disc	charge Design				
		Choose One Berm With Pipe Flow too small for berm w/ pipe			
		Wall with Rect. Notch			
		O Wall with V-Notch Weir			
F) Discharge Pi	pe Size (minimum 8-inches)	Calculated D _P =in			
G) Rectangular	Notch Width	Calculated $W_N = 5.0$ in			
Ginecialigular					

	Design Procedure Form:	Extended Detention Basin (EDB)	
Designer: Company: Date: Project: Location:	Marc A. Whorton, P.E. Classic Consulting July 20, 2023 Monument Junction Development - Hwy. 105 & JCP Int. Imps. SWQ Facility - Forebay Sizing		Sheet 2 of 3
 6. Trickle Channel A) Type of Trick F) Slope of Trick 	de Channel kle Channel	Choose One Concrete Soft Bottom S = 0.0200 ft / ft	PROVIDE A CONSISTENT LONGITUDINAL SLOPE FROM FOREBAY TO MICROPOOL WITH NO MEANDERING. RIPRAP AND SOIL RIPRAP LINED CHANNELS ARE NOT RECOMMENDED. MINIMUM DEPTH OF 1.5 FEET
 7. Micropool and C A) Depth of Mic B) Surface Area C) Outlet Type 	Dutlet Structure ropool (2.5-feet minimum) a of Micropool (10 ft ² minimum)	D _M = ft A _M = sq ft Choose One O orifice Plate O Other (Describe):]
D) Smallest Din (Use UD-Detent E) Total Outlet A	nension of Orifice Opening Based on Hydrograph Routing ion) \rea	D _{onfice} =inches A _{ot} =square	inches
 8. Initial Surcharge A) Depth of Initi (Minimum rec B) Minimum Initii (Minimum volu C) Initial Surchard 	Volume al Surcharge Volume commended depth is 4 inches) al Surcharge Volume ume of 0.3% of the WQCV) rge Provided Above Micropool	$D_{1S} =$ in $V_{1S} =$ 16 cu ft $V_s =$ cu ft	
 9. Trash Rack A) Water Qualit B) Type of Screet in the USDCM, it total screen are 	y Screen Open Area: $A_t = A_{ct} * 38.5*(e^{-0.095D})$ en (If specifying an alternative to the materials recommended ndicate "other" and enter the ratio of the total open are to the for the material specified.) Other (Y/N):	A _t =square	inches
C) Ratio of Total D) Total Water C E) Depth of Des (Based on d F) Height of Wat G) Width of Wat (Minimum of 12	l Open Area to Total Area (only for type 'Other') Quality Screen Area (based on screen type) ign Volume (EURV or WQCV) lesign concept chosen under 1E) ter Quality Screen (H _{TR}) ter Quality Screen Opening (W _{opening}) inches is recommended)	User Ratio =	

	Design Procedure Form:	Extended Detention Basin (EDB)	
Designer: Company: Date: Project: Location:	Marc A. Whorton, P.E. Classic Consulting July 20, 2023 Monument Junction Development - Hwy. 105 & JCP Int. Imps. SWQ Facility - Forebay Sizing	Sheet	: 3 of 3
 Overflow Emba A) Describe er B) Slope of Ov (Horizontal 	ankment mbankment protection for 100-year and greater overtopping: /erflow Embankment distance per unit vertical, 4:1 or flatter preferred)	Buried Rip-Rap Ze = 4.00 ft / ft	
11. Vegetation		Choose One Irrigated Not Irrigated	
12. Access A) Describe Si	ediment Removal Procedures		
Notes:			

DETENTION FACILITY CALCULATIONS


DETENTION BASIN STAGE-STORAGE TABLE BUILDER

1.00

ft

MHFD-Detention, Version 4.05 (January 2022)

Depth Increment =

Project: Monument Junction Development - Hwy. 105 & JCP Int. Imps.



Watershed Information

	EDB	Selected BMP Type =
acres	11.84	Watershed Area =
ft	1,200	Watershed Length =
ft	600	Watershed Length to Centroid =
ft/ft	0.050	Watershed Slope =
percent	53.60%	Watershed Imperviousness =
percen	0.0%	Percentage Hydrologic Soil Group A =
percent	0.0%	Percentage Hydrologic Soil Group B =
percent	100.0%	Percentage Hydrologic Soil Groups C/D =
hours	40.0	Target WQCV Drain Time =
-	User Input	Location for 1-hr Rainfall Depths =

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	ire.	Optional User	r Overri
Water Quality Capture Volume (WQCV) =	0.213	acre-feet		acre-fe
Excess Urban Runoff Volume (EURV) =	0.604	acre-feet		acre-fe
2-yr Runoff Volume (P1 = 1.19 in.) =	0.673	acre-feet	1.19	inches
5-yr Runoff Volume (P1 = 1.5 in.) =	0.955	acre-feet	1.50	inches
10-yr Runoff Volume (P1 = 1.75 in.) =	1.195	acre-feet	1.75	inches
25-yr Runoff Volume (P1 = 2 in.) =	1.472	acre-feet	2.00	inches
50-yr Runoff Volume (P1 = 2.25 in.) =	1.723	acre-feet	2.25	inches
100-yr Runoff Volume (P1 = 2.52 in.) =	2.026	acre-feet	2.52	inches
500-yr Runoff Volume (P1 = 3.85 in.) =	3.392	acre-feet	3.85	inches
Approximate 2-yr Detention Volume =	0.535	acre-feet		
Approximate 5-yr Detention Volume =	0.786	acre-feet		
Approximate 10-yr Detention Volume =	0.896	acre-feet		
Approximate 25-yr Detention Volume =	0.965	acre-feet		
Approximate 50-yr Detention Volume =	0.998	acre-feet		
Approximate 100-yr Detention Volume =	1.124	acre-feet		

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.213	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.390	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.520	acre-feet
Total Detention Basin Volume =	1.124	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft

Width of Main Basin (W_{MAIN}) =

Area of Main Basin (A_{MAIN}) =

Volume of Main Basin (V_{MAIN}) =

Calculated Total Basin Volume (V_{total}) =

user lft. ĥ

user

user ft

user

acre-feet

Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
I OP OT MICROPOOI		0.00				48	0.001		
7006		1.50				3,347	0.077	2,546	0.058
7008		3.50				5,688	0.131	11,581	0.266
7010		5.50				9,690	0.222	26,959	0.619
7012		7.50				14,548	0.334	51,197	1.175
								1	
								T	
									-
								-	
								<u> </u>	<u> </u>
								1	
								<u> </u>	<u> </u>
								1	
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								1	
								<u> </u>	<u> </u>
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.05 (January 2022) Project: Monument Junction Development - Hwy. 105 & JCP Int. Imps Basin ID: SWQ Facility in CDOT ROW Estimated Estimated ZONE 1 Stage (ft) Volume (ac-ft) Outlet Type VOLUME EURV WQCV Zone 1 (WQCV) 3.09 0.213 Orifice Plate 100-YEAR Zone 2 (EURV) 5.44 0.390 Orifice Plate ZONE 1 AND 2 Zone 3 (100-year) 7.35 0.520 Weir&Pipe (Restrict) PERMANENT Example Zone Configuration (Retention Pond) Total (all zones) 1.124 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area Underdrain Orifice Invert Depth = N/A N/A ft² Underdrain Orifice Centroid = Underdrain Orifice Diameter = N/A inches N/A feet Calculated Parameters for Plate User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) WO Orifice Area per Row = 7.569E-03 0.00 lft² Depth at top of Zone using Orifice Plate = 5.50 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = N/A feet Orifice Plate: Orifice Vertical Spacing = 16.50 inches Elliptical Slot Centroid = N/A feet Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-3/16 inches) Elliptical Slot Area =]ft² 1.09 N/A User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) 2.80 Stage of Orifice Centroid (ft) 0.00 1.40 4.20 Orifice Area (sq. inches) 1.09 1.09 1.09 1.09 Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sg. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected lft² Invert of Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A Depth at top of Zone using Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A N/A feet inches Vertical Orifice Diameter = N/A N/A User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho = 5.50 ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t = N/A 5.50 N/A feet Overflow Weir Slope Length = Overflow Weir Front Edge Length = 6.00 N/A feet 3.00 N/A feet Overflow Weir Grate Slope = 0.00 N/A H:V Grate Open Area / 100-yr Orifice Area = 1.77 N/A Horiz. Length of Weir Sides = Overflow Grate Open Area w/o Debris = 12.53 ft² 3.00 N/A feet N/A Overflow Grate Open Area w/ Debris = Overflow Grate Type = Type C Grate N/A 6.26 N/A fť Debris Clogging % = 50% N/A % User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe = Outlet Orifice Area = ft² 0.70 N/A ft (distance below basin bottom at Stage = 0 ft) 7.07 N/A Outlet Pipe Diameter = 36.00 N/A inches Outlet Orifice Centroid : 1.50 N/A feet Restrictor Plate Height Above Pipe Invert = 36.00 . inches Half-Central Angle of Restrictor Plate on Pipe = 3.14 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= 6.50 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.51 feet Spillway Crest Length = Stage at Top of Freeboard = 30.00 feet 8.01 feet Spillway End Slopes = 3.00 H:V Basin Area at Top of Freeboard 0.33 acres Freeboard above Max Water Surface = 1.00 feet Basin Volume at Top of Freeboard = 1.18 acre-ft Routed Hydrograph Results in the Inflow H ohs table ns W throu The user can override the c ring new val EURV Design Storm Return Period = WQCV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year One-Hour Rainfall Depth (in) = 1.50 N/A N/A 1.19 1.75 2.00 2.25 2.52 3.85 0.955 3.392 CUHP Runoff Volume (acre-ft) 0.213 0.604 0.673 1.195 1.472 1.723 2.026 Inflow Hydrograph Volume (acre-ft) = N/A N/A 0.673 0.955 1.195 1.472 1.723 2.026 3.392 CUHP Predevelopment Peak O (cfs) : N/A N/A 14.2 31.7 2.6 5.4 7.5 11.5 17.5 OPTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A 10.0 14.0 20.0 27.0 30.0 36.0 Predevelopment Unit Peak Flow, g (cfs/acre) : 2.28 25.4 N/A N/A 0.84 1.18 1.69 2.53 3.04 2.68 Peak Inflow Q (cfs) 20.2 29.7 57.6 11.9 16.8 35.1 N/A N/A 51.2 Peak Outflow Q (cfs) : 0.1 0.3 4.6 7.8 14.8 19.2 25.2 0.5 Ratio Peak Outflow to Predevelopment Q = N/A N/A N/A 0.3 0.4 0.5 0.6 0.7 Structure Controlling Flow : Plate Plate Overflow Weir 1 Ôv erflow Weir 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Spillway Max Velocity through Grate 1 (fps) = N/A N/A 0.02 0.3 0.6 1.2 1.5 2.0 Max Velocity through Grate 2 (fps) = N/A N/A N/A N/A N/A N/A N/A N/A N/A 58 Time to Drain 97% of Inflow Volume (hours) = 42 61 56 53 Time to Drain 99% of Inflow Volume (hours) 40 63 66 65 64 63 62 61 56 Maximum Ponding Depth (ft) = 3.08 5.44 5.54 5.78 5.91 6.13 6.25 6.40 6.79

0.24

0.683

0.26

0.24

0 712

Area at Maximum Ponding Depth (acres)

Maximum Volume Stored (acre-ft) =

0.12

0.22

0.606

0.22

0.626

0.29

0.949

0.27

0.26

0.80



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate progra

1										01.11.15
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00 min	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.01	0.85
	0:15:00	0.00	0.00	1.11	1.81	2.23	1.50	1.86	1.83	3.46
	0:20:00	0.00	0.00	3.84	5.19	6.38	3.70	4.30	4.62	8.62
	0:25:00	0.00	0.00	9.05	13.93	17.60	8.81	10.91	12.17	23.92
	0:30:00	0.00	0.00	11.92	16.76	20.16	22.94	27.05	30.39	51.17
	0:35:00	0.00	0.00	10.04	15.00	17.02	25.45	20.66	25.12	57.60
	0:40:00	0.00	0.00	10.94	13.00	17.92	23.43	23.00	33.13	57.00
	0.40.00	0.00	0.00	9.50	12.83	15.35	24.05	27.92	32.89	53.00
	0:45:00	0.00	0.00	7.81	10.80	13.12	20.93	24.30	29.53	48.00
	0:50:00	0.00	0.00	6.41	9.13	10.90	18.49	21.42	25.87	41.94
	0:55:00	0.00	0.00	5.38	7.67	9.37	15.18	17.62	21.91	35.64
	1:00:00	0.00	0.00	4.69	6.67	8.35	12.86	14.96	19.17	31.30
	1:05:00	0.00	0.00	4.13	5.84	7.48	11.21	13.06	17.26	28.20
	1:10:00	0.00	0.00	3.36	5.07	6.62	9.29	10.87	13.89	22.87
	1:15:00	0.00	0.00	2.68	4.16	5.84	7.61	8.94	11.01	18.28
	1:20:00	0.00	0.00	2.13	3.32	4.80	5.85	6.85	8.06	13.45
	1:25:00	0.00	0.00	1.81	2.87	3.97	4,46	5,23	5,78	9,81
	1:30:00	0.00	0.00	1.67	2.64	3 44	3 51	4 13	4 30	7 57
	1.35.00	0.00	0.00	1.07	2.01	2.07	2.00	2 42	2.54	6.10
	1.35.00	0.00	0.00	1.59	2.40	3.07	2.90	3.42	3.54	5.19
	1.45.00	0.00	0.00	1.54	2.1/	2.80	2.51	2.95	2.97	5.24
	1.40:00	0.00	0.00	1.51	1.94	2.62	2.24	2.63	2.58	4.60
	1:50:00	0.00	0.00	1.48	1.77	2.49	2.06	2.42	2.31	4.15
	1:55:00	0.00	0.00	1.28	1.65	2.31	1.94	2.27	2.12	3.83
	2:00:00	0.00	0.00	1.13	1.50	2.04	1.85	2.17	2.01	3.65
	2:05:00	0.00	0.00	0.83	1.10	1.48	1.36	1.59	1.47	2.67
	2:10:00	0.00	0.00	0.60	0.79	1.05	0.97	1.13	1.05	1.91
	2:15:00	0.00	0.00	0.43	0.56	0.75	0.69	0.81	0.76	1.37
	2:20:00	0.00	0.00	0.30	0.39	0.52	0.49	0.57	0.54	0.97
	2:25:00	0.00	0.00	0.21	0.26	0.36	0.33	0.39	0.37	0.67
	2:30:00	0.00	0.00	0.14	0.17	0.24	0.23	0.27	0.26	0.46
	2:35:00	0.00	0.00	0.08	0.11	0.16	0.15	0.18	0.17	0.30
	2:40:00	0.00	0.00	0.05	0.07	0.09	0.09	0.11	0.10	0.18
	2:45:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.09
	2:50:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.03
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow]
Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
Micropool Elev.	4.50	7,689	0.177	18,270	0.419	0.21	For best results, include the
EURV	5.44	9,570	0.220	26,381	0.606	0.26	stages of all grade slope
	5.50	9,690	0.222	26,959	0.619	0.26	changes (e.g. ISV and Floor)
5-yr.	5.54	9,787	0.225	27,349	0.628	0.49	Sheet 'Basin'.
100-yr.	6.40	11,876	0.273	36,664	0.842	25.05	
	7.50	14,548	0.334	51,197	1.175	147.73	Also include the inverts of all
							overflow grate, and spillway,
							where applicable).
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							4



DRAINAGE MAPS



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Unresolved: On both maps, indicate what facilities are public and/or private

	FINAL DRAINAGE REPORT ~ BASIN RUNUFF CUEFFICIENT SUMIMART															
		DEVELOPED AREA/IMPERVIOUS AREA			IS AREA	LANDSCAPE/UNDEVELOPED AREAS			WEIGHTED			WEIGHTED CA			IMPERVIOUSNESS	
BASIN	TOTAL AREA (AC)	AREA (AC)	C(2)	C(5)	C(100)	AREA (AC)	C(2)	C(5)	C(100)	C(2)	C(5)	C(100)	CA(2)	CA(5)	CA(100)	%
OS-10	4.10	0.60	0.89	0.90	0.96	3.50	0.03	0.09	0.36	0.16	0.21	0.45	0.64	0.86	1.84	16%
OS-11	1.70	0.80	0.89	0.90	0.96	0.90	0.02	0.08	0.35	0.43	0.47	0.64	0.73	0.79	1.08	45%
OS-12	0.51	0.27	0.89	0.90	0.96	0.24	0.03	0.09	0.36	0.49	0.52	0.68	0.25	0.26	0.35	54%
OS-13	0.67	0.40	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.54	0.57	0.72	0.36	0.38	0.48	61%
OS-14	0.28	0.15	0.89	0.90	0.96	0.13	0.03	0.09	0.36	0.49	0.52	0.68	0.14	0.15	0.19	55%
OS-15	1.60	1.20	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.68	0.70	0.81	1.08	1.12	1.30	76%
OS-16	1.00	0.70	0.89	0.90	0.96	0.30	0.02	0.08	0.35	0.63	0.65	0.78	0.63	0.65	0.78	67%
OS-17	0.53	0.43	0.89	0.90	0.96	0.10	0.03	0.09	0.36	0.73	0.75	0.85	0.39	0.40	0.45	82%
OS-18	0.30	0.30	0.89	0.90	0.96	0.00	0.03	0.09	0.36	0.89	0.90	0.96	0.27	0.27	0.29	100%
EX2	0.56	0.56	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.02	0.05	0.20	2%
EX3	1.80	1.80	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.05	0.16	0.65	2%
Exist. Trib. to Pond	13.05															

	FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY																	
		WEIGHTE	D		OVER	RLAND		STREE	et / Ch	ANNEL	FLOW	Tc INTENSITY			TY	TOTAL FLOWS		
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length <i>(ft)</i>	Height <i>(ft)</i>	Tc (<i>min</i>)	Length <i>(ft)</i>	Slope (%)	Velocity <i>(fps)</i>	Tc (<i>min</i>)	TOTAL (<i>min</i>)	l(2) (in/hr)	l(5) (in/hr)	l(100) (in/hr)	Q(2) (cfs)	Q(5) <i>(cfs)</i>	Q(100) <i>(cfs)</i>
OS-10	0.64	0.86	1.84	0.09	65	2	10.1	950	3.5%	1.9	8.5	18.6	2.56	3.20	5.37	2	3	10
OS-11	0.73	0.79	1.08	0.08	100	2	14.7	500	4.0%	2.0	4.2	18.8	2.54	3.18	5.34	1.9	3	6
OS-12	0.25	0.26	0.35	0.09	40	2	6.8	200	3.5%	3.7	0.9	7.7	3.61	4.53	7.60	0.9	1.2	3
OS-13	0.36	0.38	0.48	0.09	25	3	4.0	240	5.5%	4.7	0.9	5.0	4.12	5.17	8.68	1.5	2	4
OS-14	0.14	0.15	0.19	0.09	30	10	3.1	170	5.5%	4.7	0.6	5.0	4.12	5.17	8.68	0.6	0.8	2
OS-15	1.08	1.12	1.30	0.09	180	12	13.1	100	3.0%	1.7	1.0	14.0	2.89	3.62	6.08	3	4	8
OS-16	0.63	0.65	0.78	0.08	100	4	11.7	130	1.5%	1.2	1.8	13.4	2.94	3.69	6.19	1.9	2	5
OS-17	0.39	0.40	0.45	0.09	60	14	5.0	380	5.0%	4.5	1.4	6.4	3.82	4.80	8.05	1.5	2	4
OS-18	0.27	0.27	0.29	0.09	15	0.5	4.7	280	2.0%	2.8	1.6	6.4	3.83	4.80	8.06	1.0	1.3	2
EX2	0.02	0.05	0.20	0.09	50	2	8.2					8.2	3.54	4.43	7.44	0.1	0.2	1.5
EX3	0.05	0.16	0.65	0.09	260	5	23.7					23.7	2.27	2.84	4.76	0.1	0.5	3

	FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY										
					Inten	sity	Fl	ow			
Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Inlet Size		
H4	OS-12	0.26	0.46	7.7	4.53	7.60	1	3	EXIST. 5' TYPE R AT-GRADE INLET		
H5	OS-13, Flow-by from H4	0.38	0.63	5.0	5.17	8.68	2	5	EXIST. 10' TYPE R AT-GRADE INLET		
H6	OS-14, Flow-by from H5	0.15	0.24	5.0	5.17	8.68	1	2	EXIST. 10' TYPE R AT-GRADE INLET		
H7	OS-11 and OS-16	1.45	1.86	18.8	3.18	5.34	5	10	EXIST. 10' TYPE R AT-GRADE INLET		
H8	OS-17, Flow-by from H7	0.42	0.73	6.4	4.80	8.05	2	6	EXIST. 10' TYPE R AT-GRADE INLET		
Н9	OS-18, Flow-by from H8	0.27	0.41	6.4	4.80	8.06	1	3	EXIST. 10' TYPE R AT-GRADE INLET		
H10	EX2, EX3, OS-10 thru OS-18	5.09	7.60	23.7	2.84	4.76	14	36	EXIST. 36" RCP CDOT CULVERT		

	FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY										
					Inten	sity	FI	ow			
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Pipe Size*		
H1	Inlet Capture at DP-H4	0.26	0.24	7.7	4.53	7.60	1	2	Exist 15" RCP		
H2	PR-H1, Inlet Capture at DP-H5	0.65	0.77	7.8	4.51	7.57	3	6	Exist 15" RCP		
Н3	PR-H2, Inlet Capture at DP-H6	0.80	1.01	7.9	4.49	7.54	4	8	Exist 24" RCP		
H4	OS-15	1.12	1.30	14.0	3.62	6.08	4	8	Exist 18" ADS		
H5	PR-H3, PR-H4, Portion of OS-11 and OS-16	3.20	3.95	18.8	3.18	5.34	10	21	Exist 30" RCP		
H6	Inlet Capture at DP-H8	0.42	0.64	6.4	4.80	8.05	2	5	Exist 24" RCP		
H7	Inlet Capture at DP-H9	0.27	0.41	6.4	4.80	8.06	1	3	Exist 24" RCP		

<u>LEGEND</u> **DESCRIPTION** <u>SYMBOL</u> 6910 _____ EXISTING GROUND CONTOUR PROPOSED FINISHED CONTOUR ----- 6910 -----BASIN BOUNDARY $\langle 3 \rangle$ DESIGN POINT BB 10.0 BASIN IDENTIFIER -----AREA IN ACRES -EXISTING DIRECTION OF FLOW \sim EXIST. STORM SEWER TRIBUTARY AREA TO 36" CULVERT



FINAL DRAINAGE REPORT ~ BASIN RUNOFE COFFEICIENT SUMMARY

0	100	200
SCALE:	1" = 100'	



ONUMENT JUNCTION DEVELOPMENT									
WY. 105 &	: JACKS	SON CREEK I	NT. IMPS.	SS]					
NAL DRAINAGE REPORT RE-DEVELOPED DRAINAGE MAP									
ESIGNED BY	MAW	SCALE	DATE	03/16/					

٦		<i>r</i>)	WS
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IED BY	MAW	SCALE	DATE	0	3/16/	/22
I BY	MAW	(H) 1"= 100'	SHEET	1	OF	2
ED BY		(V) 1"= N/A	JOB NO.		1302.2	22



			FI	NAL DRA		REPORT [,]	~ BASIN	RUNOF		CIENT SUI	MMARY							
		DEVELOPED AREA/IMPERVIOUS AREA LANDSCAPE/UNDEVELOPED AREAS WEIGHTED													WEIGHTED CA			
	τοται																	
BASIN	AREA (AC)	AREA (AC)	C(2)	C(5)	C(100)	AREA (AC)	C(2)	C(5)	C(100)	C(2)	C(5)	C(100)	CA(2)	CA(5)	CA(100)	%		
G	0.20	0.05	0.79	0.81	0.88	0.15	0.03	0.09	0.36	0.22	0.27	0.49	0.04	0.05	0.10	25%		
Н	0.57	0.05	0.79	0.81	0.88	0.52	0.03	0.09	0.36	0.10	0.15	0.41	0.06	0.09	0.23	10%		
OS-10	4.10	0.60	0.89	0.90	0.96	3.50	0.03	0.09	0.36	0.16	0.21	0.45	0.64	0.86	1.84	16%		
OS10D	2.00	0.10	0.89	0.90	0.96	1.90	0.03	0.09	0.36	0.07	0.13	0.39	0.15	0.26	0.78	7%		
OS-11	1.70	0.80	0.89	0.90	0.96	0.90	0.02	0.08	0.35	0.43	0.47	0.64	0.73	0.79	1.08	45%		
OS11D	1.70	1.20	0.89	0.90	0.96	0.50	0.03	0.09	0.36	0.64	0.66	0.78	1.08	1.13	1.33	71%		
OS-12	0.51	0.27	0.89	0.90	0.96	0.24	0.03	0.09	0.36	0.49	0.52	0.68	0.25	0.26	0.35	54%		
OS12D	0.58	0.31	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.49	0.52	0.68	0.28	0.30	0.39	54%		
OS-13	0.67	0.40	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.54	0.57	0.72	0.36	0.38	0.48	61%		
OS13D	0.67	0.40	0.89	0.90	0.96	0.27	0.03	0.09	0.36	0.54	0.57	0.72	0.36	0.38	0.48	61%		
OS-14	0.28	0.15	0.89	0.90	0.96	0.13	0.03	0.09	0.36	0.49	0.52	0.68	0.14	0.15	0.19	55%		
OS14D	0.86	0.72	0.89	0.90	0.96	0.14	0.03	0.09	0.36	0.75	0.77	0.86	0.65	0.66	0.74	84%		
OS-15	1.60	1.20	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.68	0.70	0.81	1.08	1.12	1.30	76%		
OS15D	1.60	1.20	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.68	0.70	0.81	1.08	1.12	1.30	76%		
OS-16	1.00	0.70	0.89	0.90	0.96	0.30	0.02	0.08	0.35	0.63	0.65	0.78	0.63	0.65	0.78	67%		
OS-17	0.53	0.43	0.89	0.90	0.96	0.10	0.03	0.09	0.36	0.73	0.75	0.85	0.39	0.40	0.45	82%		
OS17D	1.00	0.60	0.89	0.90	0.96	0.40	0.03	0.09	0.36	0.55	0.58	0.72	0.55	0.58	0.72	61%		
OS-18	0.30	0.30	0.89	0.90	0.96	0.00	0.03	0.09	0.36	0.89	0.90	0.96	0.27	0.27	0.29	100%		
OS18D	0.78	0.43	0.89	0.90	0.96	0.35	0.03	0.09	0.36	0.50	0.54	0.69	0.39	0.42	0.54	56%		
OS-19	0.18	0.00	0.89	0.90	0.96	0.18	0.03	0.09	0.36	0.03	0.09	0.36	0.01	0.02	0.06	2%		
OS-20	0.11	0.01	0.89	0.90	0.96	0.10	0.03	0.09	0.36	0.11	0.16	0.41	0.01	0.02	0.05	10%		
JCP7	0.59	0.50	0.89	0.90	0.96	0.09	0.03	0.09	0.36	0.76	0.78	0.87	0.45	0.46	0.51	85%		
EX2	0.56	0.56	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.02	0.05	0.20	2%		
EX3	1.80	1.80	0.03	0.09	0.36	0.00	0.03	0.09	0.36	0.03	0.09	0.36	0.05	0.16	0.65	2%		
Exist. Trib. to Pond	13.05															37.5%		
Dev. Trib. to Pond	11.84															53.6%		
Dev. Trib. to Forebay	8.49															67.2%		

EXISTING POND #3				FIN	AL DRAI	NAGE	REPO	RT ~ B/	ASIN F	RUNOF	FF SU	MMA	RY															
	and the		WEIGHTE	D	0	VERLAND)	STREE	T / CHA	NNEL FI	LOW	Тс	INTEN	ISITY	тс	TAL FL	.OWS											
	BASIN	CA(2)	CA(5)	CA(100)	C(5) Ler	ngth Heig	ht Tc	Length	Slope \	Velocity (fno)	Tc T	OTAL	(2) (5	5) I(10 hr) (in/h	0) Q(2)	Q(5)	Q(100))										
05=2	G	0.04	0.05	0.10	0.09 3	1) (11) 10 1.5	5.9	(11)	(%)	<u>(ips)</u>	<i></i>	5.9	3.93 4.9		7 0.17	0.3	0.8	-										
0,33 (þ902)	н	0.06	0.09	0.23	0.09 4	0 2	6.8					6.8	3.76 4.7	71 7.9	1 0.2	0.4	1.8	-										
MONUMENT	OS-10	0.64	0.86	1.84	0.09 6	5 2	10.1	950	3.5%	1.9	8.5	18.6	2.56 3.2	20 5.3	7 2	3	10			FINAL D	RAINAGE	REPORT ~	SURFACE	ROUTIN	G SUMMA	RY		
EAST DEVELOPMENT	OS10D	0.15	0.26	0.78	0.09 6	5 2	10.1	950	3.5%	1.9	8.5	18.6	2.56 3.2	20 5.3	0.4	0.8	4							Inter	sity	Fl	w	
(REFERENCE MONUMENT	OS-11	0.73	0.79	1.08	0.08 10	0 2	14.7	500	4.0%	2.0	4.2	18.8	2.54 3.1	18 5.3	4 1.9	3	6	Desi	gn	Contributing Basins	Equivalent	Equivalent	Maximum	1(5)	1(100)	Q(5)	Q(100)	
PLAN FINAL DRAINAGE REPORT	OS11D	1.08	1.13	1.33	0.09 10	0 2	14.5	300	4.0%	2.0	2.5	17.0	2.66 3.3	33 5.5	93	4	7	Poin	:(s)		CA(5)	CA(100)	Tc	.(0)		۹(۵)	۵(۱۰۰۰)	Inlet Size
	OS-12	0.25	0.26	0.35	0.09 4	0 2	6.8	200	3.5%	3.7	0.9	7.7	3.61 4.5	53 7.6	0 0.9	1.2	3	13		G, H, JCP7, OS10D thru	5.84	7 90	21.1	3.01	5.05	18	40	CDOT SWQ
	OS12D	0.28	0.30	0.39	0.09 4	0 2	6.8	200	3.5%	3.7	0.9	7.7	3.61 4.5	53 7.6	0 1.0	1.4	3.0			OS18D	5.04	7.50	21.1	5.01	0.00	10	40	FACILITY
P P P P P P P P P P P P P P P P P P P	OS-13	0.36	0.38	0.48	0.09 2	5 3	4.0	240	5.5%	4.7	0.9	5.0	4.12 5.1	17 8.6	8 1.5	2	4	D4		OS12D, 0.85 CFS 100Yr	0.30	0.51	7.7	4.53	7.60	1.4	3.9	PROP. 5' TYPE R
	OS13D	0.36	0.38	0.48	0.09 2	5 3	4.0	250	3.5%	3.7	1.1	5.1	4.09 5.1	13 8.6	1 1.5	2	4			CS12D Flow by from D4	0.29	0.62	5.0	5 17	0.60	0	5	PROP. 10' TYPE R
	OS-14	0.14	0.15	0.19	0.09 3	0 10	3.1	170	5.5%	4.7	0.6	5.0	4.12 5.1	17 8.6	8 0.6	0.8	2				0.50	0.05	5.0	5.17	0.00	2	5	AT-GRADE INLET
<u>05-21</u> 0.36	OS14D	0.65	0.66	0.74	0.09 3	0 10	3.1	190	5.5%	4.7	0.7	5.0	4.12 5.1	17 8.6	8 3	3	6	D6		OS15D	1.12	1.30	13.5	3.68	6.18	4	8	TYPE C INLET
	OS-15	1.08	1.12	1.30	0.09 18	30 12	13.1	100	3.0%	1.7	1.0	14.0	2.89 3.6	6.0	8 3	4	8	D7		OS11D, OS-16, OS-19, OS-20	1.81	2.22	17.0	3.33	5.59	6	12	PROP. 10' TYPE R AT-GRADE INI ET
JCP2	OS15D	1.08	1.12	1.30	0.09 18	30 12	13.1	80	3.0%	3.5	0.4	13.5	2.94 3.6	6.1	8 3	4	8	DE		OS14D, Flow-by from D5&D7	0.84	1.47	17.0	3.33	5.59	3	8	PROP. 10' TYPE R
0.28	OS-16	0.63	0.65	0.78	0.08 10	0 4	11.7	130	1.5%	1.2	1.8	13.4	2.94 3.6	6.1	9 1.9	2	5				0.51	0.61	6.0	4 70	7.00		F	SUMP INLET PROP. 10' TYPE R
Re PR	OS-17	0.39	0.40	0.45	0.09 6	0 14	5.0	380	5.0%	4.5	1.4	6.4	3.82 4.8	8.0	5 1.5	2	4	D:		JCP7, G	0.51	0.01	0.9	4.70	7.00	2	5	
	OS17D	0.55	0.58	0.72	0.09 6	0 14	5.0	380	5.0%	4.5	1.4	6.4	3.82 4.8	30 8.0	¹⁵ 2	3	6	D1)	OS17D, Flow-by from D8	0.58	0.74	6.4	4.80	8.05	3	6	AT-GRADE INLET
	05-18	0.27	0.27	0.29	0.09 1	5 0.5	4.7	280	2.0%	2.8	1.6	6.4	3.83 4.8	30 8.0	6 1.0	1.3	2	D1	1	OS18D, Flow-by from D9	0.42	0.64	12.1	3.84	6.45	2	4	EXIST. 10' TYPE R SUMP INLET
	05180	0.39	0.42	0.04	0.09 9	0 32	10.0	200	Z.0%	2.0	1.5	12.1	3.07 3.0	0,4 0,65	0 02	1.0	3	-		I		11	I		L			
PE ER IZ	05-20	0.01	0.02	0.00	0.09 0	i0 3.2	7 1	300	5.0 %	4.0	1.4	7.1	3.70 / 6	33 7 7	8 0.02	0.1	0.4	-										
1 Jake The The The The The The The The The Th	JCP7	0.45	0.46	0.51	0.09 2	0 0.6	5.7	300	4.5%	4.2	1.2	6.9	3.74 4.7	70 7.8	8 2	2	4											
The F																		-										
R 1.1	EX2	0.02	0.05	0.20	0.09 5	0 2	8.2					8.2	3.54 4.4	43 7.4	4 0.1	0.2	1.5	4		FINA			T ~ PIPF R		SI IMMAR'	v		
NLET	EX3	0.05	0.16	0.65	0.09 26	50 5	23.7					23.7	2.27 2.8	34 4.7	6 0.1	0.5	3								ensity	' I F	low	
PE DE LE		1	1		<u> </u>	I		<u> </u>			I		I	I	L		1	⊐ Pipe	Run	Contributing Basins	Equivaler	nt Equivalent	Maximum	I(5)	I(100)	Q(5)	Q(100)	Ding Size*
	ited)																			Inlet Capture at D4	0.30	0.33	7.7	4.53	7.60	1.4	2.5	PROP. 15" RCP
S" PCD	1-2-)	PR-1, Inlet Capture at D5	0.69	0.92	7.7	4.53	7.60	3	7	PROP. 18" RCP
TORM PIPE																												



30' DRAINAGE ESMT.

36" RCP STORM PIPE



					Inten	sity	Fl	ow	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Pipe Size*
1	Inlet Capture at D4	0.30	0.33	7.7	4.53	7.60	1.4	2.5	PROP. 15" RCP
2	PR-1, Inlet Capture at D5	0.69	0.92	7.7	4.53	7.60	3	7	PROP. 18" RCP
3	CDOT Type C InletCapture at D6	1.12	1.30	13.5	3.68	6.18	4	8	PROP. 18" RCP
4	PR-2, PR-3	1.80	2.22	13.7	3.66	6.15	7	14	PROP. 24" RCP
5	Inlet Capture at D7	1.63	1.51	17.0	3.33	5.59	5	8	PROP. 18" RCP
6	PR-5, InletCapture at D8	2.47	2.98	17.0	3.33	5.59	8	17	PROP. 24" RCP
7	PR-6, Inlet Capture at D9	2.98	3.56	17.0	3.33	5.59	10	20	PROP. 24" RCP
8	PR-4, PR-7	4.79	5.77	17.2	3.32	5.56	16	32	PROP. 30" RCP
9	Inlet Capture at D10	0.58	0.66	6.4	4.80	8.05	3	5	PROP. 18" RCP
10	PR-8, PR9	5.36	6.43	17.4	3.30	5.54	18	36	PROP. 30" RCP
11	Inlet Capture at D11	0.42	0.64	12.1	3.84	6.45	2	4	EXIST. 18" RCP

100 SCALE: 1" = 100'

200



MONUMENT JUNCTION DEVELOPMENT	
HWY. 105 & JACKSON CREEK INT. IMPS.	5
FINAL DRAINAGE REPORT	
DEVELOPED DRAINAGE MAP	Įζ

DESIGNED BY	MAW	SCALE	DATE C	3/16/22
DRAWN BY	MAW	(H) 1"= 100'	SHEET 2	OF 2
CHECKED BY		(V) 1"= N/A	JOB NO.	1302.22

EL PASO COUNTY GENERAL CONSTRUCTION NOTES:

- 1. THE LOCATION OF EXISTING UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND MAY NOT INCLUDE ALL UTILITIES. THE EXCAVATION CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE OCCASIONED BY HIS FAILURE TO EXACTLY LOCATED AND PRESERVE ANY AND ALL UTILITIES.
- 2. BEFORE COMMENCING ANY EXCAVATION, CALL 1-800-922-1987 FOR EXISTING UTILITY LOCATIONS.
- 3. THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE UTILITIES WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- 4. ALL BACKFILL, SUB-BASE AND/OR BASE COURSE (CLASS 6) MATERIAL SHALL BE COMPACTED TO THE SOILS ENGINEER'S RECOMMENDATIONS, AND APPROVED BY EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT (PCD).
- 5. ALL STATIONING IS CENTERLINE UNLESS OTHERWISE INDICATED. ALL ELEVATIONS ARE CENTERLINE UNLESS OTHERWISE INDICATED.
- 6. THE CONTRACTOR SHALL REVEGETATE ALL DISTURBED AREAS AS SOON AS POSSIBLE AND EROSION CONTROL SHALL BE INSTALLED AND MAINTAINED IN A FUNCTIONAL MANNER AT ALL TIMES. DEVELOPER RESPONSIBLE FOR MAINTAINING DISTURBED AREAS UNTIL REVEGETATION IS COMPLETE.
- 7. ALL DISTURBED PAVEMENT EDGES SHALL BE CUT TO NEAT LINES. REPAIR SHALL CONFORM TO THE EPC ECM APPENDIX K 1.2C.
- 8. ADDITIONAL EROSION CONTROL STRUCTURES MAY BE REQUIRED AT THE TIME OF CONSTRUCTION.

BY PLANNING AND COMMUNITY DEVELOPMENT PRIOR TO CONSTRUCTION.

- 9. BUILDING CONTRACTORS WILL BE RESPONSIBLE FOR CONSTRUCTING POSITIVE DRAINAGE AWAY FROM ALL STRUCTURES. 10. ASPHALT THICKNESS AND BASE COURSE THICKNESS (COMPACTED) FOR ROADS SHALL BE PER DESIGN REPORT BY OWNER'S GEOTECHNICAL ENGINEER. OWNER'S GEOTECHNICAL ENGINEER TO BE ON SITE AT TIME OF ROAD CONSTRUCTION TO EVALUATE SOIL CONDITIONS AND DETERMINE IF ADDITIONAL MEASURES ARE NECESSARY TO ASSURE STABILITY OF THE NEW ROADS. PAVEMENT DESIGN SHALL BE APPROVED
- 11. THE CONTRACTOR SHALL REVEGETATE ALL DISTURBED AREAS WITHIN 21 DAYS OF SUBSTANTIAL GRADING COMPLETION. EROSION CONTROL SHALL BE INSTALLED AND MAINTAINED IN A FUNCTIONAL MANNER AT ALL TIMES. DEVELOPER IS RESPONSIBLE FOR MAINTAINING DISTURBED AREAS UNTIL REVEGETATION IS COMPLETE.
- 12. TYPE M RIP-RAP WITH 4" OF TYPE II GRANULAR BEDDING AND MIRAFI 180N OR EQUAL MAY BE SUBSTITUTED WHERE TYPE L RIP-RAP WITH MIRAFI FW 700 OR EQUAL IS SPECIFIED
- 13. ALL MATERIALS AND INSTALLATION PROCEDURES SHALL BE IN COMPLIANCE WITH ANY AND ALL APPLICABLE EL PASO COUNTY STANDARDS

STANDARD NOTES FOR EL PASO COUNTY CONSTRUCTION PLANS:

- 1. ALL DRAINAGE AND ROADWAY CONSTRUCTION SHALL MEET THE STANDARDS AND SPECIFICATIONS OF THE CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2, AND THE EL PASO COUNTY ENGINEERING CRITERIA MANUAL.
- 2. CONTRACTOR SHALL BE RESPONSIBLE FOR THE NOTIFICATION AND FIELD NOTIFICATION OF ALL EXISTING UTILITIES, WHETHER SHOWN ON THE PLANS OR NOT. BEFORE BEGINNING CONSTRUCTION. LOCATION OF EXISTING UTILITIES SHALL BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. CALL 811 TO CONTACT THE UTILITY NOTIFICATION CENTER OF COLORADO (UNCC).
- 3. CONTRACTOR SHALL KEEP A COPY OF THESE APPROVED PLANS, THE GRADING AND EROSION CONTROL PLAN, THE STORMWATER MANAGEMENT PLAN (SWMP), THE SOILS AND GEOTECHNICAL REPORT, AND THE APPROPRIATE DESIGN AND CONSTRUCTION STANDARDS AND SPECIFICATIONS AT THE JOB SITE AT ALL TIMES, INCLUDING THE FOLLOWING: a. EL PASO COUNTY ENGINEERING CRITERIA MANUAL (ECM) b. CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2
- C. COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION d. CDOT M & S STANDARDS
- 4. NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS. INCLUDING THE LAND DEVELOPMENT CODE. THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING. ANY MODIFICATIONS NECESSARY TO MEET CRITERIA AFTER-THE-FACT WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- 5. IT IS THE DESIGN ENGINEER'S RESPONSIBILITY TO ACCURATELY SHOW EXISTING CONDITIONS, BOTH ONSITE AND OFFSITE, ON THE CONSTRUCTION PLANS. ANY MODIFICATIONS NECESSARY DUE TO CONFLICTS, OMISSIONS, OR CHANGED CONDITIONS WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- 6. CONTRACTOR SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT -INSPECTIONS, PRIOR TO STARTING CONSTRUCTION.
- 7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO UNDERSTAND THE REQUIREMENTS OF ALL JURISDICTIONAL AGENCIES AND TO OBTAIN ALL REQUIRED PERMITS, INCLUDING BUT NOT LIMITED TO EL PASO COUNTY EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP) REGIONAL BUILDING FLOODPLAIN DEVELOPMENT PERMIT, U.S. ARMY CORPS OF ENGINEERS-ISSUED 401 AND/OR 404 PERMITS, AND COUNTY AND STATE FUGITIVE DUST PERMITS.
- 8. CONTRACTOR SHALL NOT DEVIATE FROM THE PLANS WITHOUT FIRST OBTAINING WRITTEN APPROVAL FROM THE DESIGN ENGINEER AND PCD. CONTRACTOR SHALL NOTIFY THE DESIGN ENGINEER IMMEDIATELY UPON DISCOVERY OF ANY ERRORS OR INCONSISTENCIES.
- 9. ALL STORM DRAIN PIPE SHALL BE CLASS III RCP OR CLASS IV WITH WATER TIGHT JOINTS WHERE CALLED OUT, UNLESS OTHERWISE NOTED AND APPROVED BY PCD.
- 10. CONTRACTOR SHALL COORDINATE GEOTECHNICAL TESTING PER ECM STANDARDS. PAVEMENT DESIGN SHALL BE APPROVED BY EL PASO COUNTY PCD PRIOR TO PLACEMENT OF CURB AND GUTTER AND PAVEMENT.
- 11. ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE AT APPROVED CONSTRUCTION ACCESS POINTS.
- 12. SIGHT VISIBILITY TRIANGLES AS IDENTIFIED IN THE PLANS SHALL BE PROVIDED AT ALL INTERSECTIONS. OBSTRUCTIONS GREATER THAN 18 INCHES ABOVE FLOWLINE ARE NOT ALLOWED WITHIN SIGHT TRIANGLES.
- 13. SIGNING AND STRIPING SHALL COMPLY WITH EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS AND MUTCD CRITERIA.
- 14. CONTRACTOR SHALL OBTAIN ANY PERMITS REQUIRED BY EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS, INCLUDING WORK WITHIN THE RIGHT-OF-WAY AND SPECIAL TRANSPORT PERMITS.
- 15. THE LIMITS OF CONSTRUCTION SHALL REMAIN WITHIN THE PROPERTY LINE UNLESS OTHERWISE NOTED. THE OWNER/DEVELOPER SHALL OBTAIN WRITTEN PERMISSION AND EASEMENTS, WHERE REQUIRED, FROM ADJOINING PROPERTY OWNER(S) PRIOR TO ANY OFF-SITE DISTURBANCE, GRADING, OR CONSTRUCTION.

EL PASO COUNTY SIGNING AND STRIPING NOTES:

- 1. ALL SIGNS AND PAVEMENT MARKINGS SHALL BE IN COMPLIANCE WITH THE CURRENT MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD).
- 2. REMOVAL OF EXISTING PAVEMENT MARKINGS SHALL BE ACCOMPLISHED BY A METHOD THAT DOES NOT MATERIALLY DAMAGE THE PAVEMENT. THE PAVEMENT MARKINGS SHALL BE REMOVED TO THE EXTENT THAT THEY WILL NOT BE VISIBLE UNDER DAY OR NIGHT CONDITIONS. AT NO TIME WILL IT BE ACCEPTABLE TO PAINT OVER EXISTING PAVEMENT MARKINGS.
- 3. ANY DEVIATION FROM THE STRIPING AND SIGNING PLAN SHALL BE APPROVED BY EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT
- 4. ALL SIGNS SHOWN ON THE SIGNING AND STRIPING PLAN SHALL BE NEW SIGNS. EXISTING SIGNS MAY REMAIN OR BE REUSED IF THEY MEET CURRENT EL PASO COUNTY AND MUTCD STANDARDS.
- 5. STREET NAME AND REGULATORY STOP SIGNS SHALL BE ON THE SAME POST AT INTERSECTIONS.
- 6. ALL REMOVED SIGNS SHALL BE DISPOSED OF IN A PROPER MANNER BY THE CONTRACTOR.
- 7. ALL STREET NAME SIGNS SHALL HAVE "D" SERIES LETTERS, WITH LOCAL ROADWAY SIGNS BEING 4" UPPER-LOWER CASE LETTERING ON 8" BLANK AND NON-LOCAL ROADWAY SIGNS BEING 6" LETTERING, UPPER-LOWER CASE ON 12" BLANK, WITH A WHITE BORDER THAT IS NOT RECESSED. MULTI-LANE ROADWAYS WITH SPEED LIMITS OF 40 MPH OR HIGHER SHALL HAVE 8" UPPER-LOWER CASE LETTERING ON 18" BLANK WITH A WHITE BORDER THAT IS NOT RECESSED. THE WIDTH OF THE NON-RECESSED WHITE BORDERS SHALL MATCH PAGE 255 OF THE 2012 MUTCD "STANDARD HIGHWAY SIGNS.
- 8. ALL TRAFFIC SIGNS SHALL HAVE A MINIMUM HIGH INTENSITY PRISMATIC GRADE SHEETING.
- 9. ALL LOCAL RESIDENTIAL STREET SIGNS SHALL BE MOUNTED ON A 1.75" X 1.75" SQUARE TUBE SIGN POST AND STUB POST BASE. FOR OTHER APPLICATIONS, REFER TO THE CDOT STANDARD S-614-8 REGARDING USE OF THE P2 TUBULAR STEEL POST SLIPBASE DESIGN. 10. ALL SIGNS SHALL BE SINGLE SHEET ALUMINUM WITH 0.100" MINIMUM THICKNESS.
- 11. ALL LIMIT LINES/STOP LINES, CROSSWALK LINES, PAVEMENT LEGENDS, AND ARROWS SHALL BE A MINIMUM 125 MIL THICKNESS PREFORMED THERMOPLASTIC PAVEMENT MARKINGS WITH TAPERED LEADING EDGES PER CDOT STANDARD S-627-1. WORD AND SYMBOL MARKINGS SHALL BE THE NARROW TYPE. STOP BARS SHALL BE 24" IN WIDTH. CROSSWALKS LINES SHALL BE 24" WIDE AND 9' LONG.
- 12. ALL LONGITUDINAL LINES SHALL BE A MINIMUM 15MIL THICKNESS EPOXY PAINT. ALL NON-LOCAL RESIDENTIAL ROADWAYS SHALL INCLUDE BOTH RIGHT AND LEFT EDGE LINE STRIPING AND ANY ADDITIONAL STRIPING AS REQUIRED BY CDOT S-627-1
- 13. THE CONTRACTOR SHALL NOTIFY EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT (719) 520-6819 PRIOR TO AND UPON COMPLETION OF SIGNING AND STRIPING.
- 14. THE CONTRACTOR SHALL OBTAIN A WORK IN THE RIGHT OF WAY PERMIT FROM THE EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS (DPW) PRIOR TO ANY SIGNAGE OR STRIPING WORK WITHIN AN EXISTING EL PASO COUNTY ROADWAY.

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AGENCIES

DEVELOPER:

CIVIL ENGINEER:

COLORADO DEPARTMENT OF TRANSPORTATION, PERMIT REVIEW:

COLORADO DEPARTMENT OF TRANSPORTATION, NORTH PROGRAM

COLORADO DEPARTMENT OF TRANSPORTATION, ENVIRONMENTAL / ROW

COUNTY ENGINEERING:

GAS COMPANY:

ELECTRIC COMPANY:

TELEPHONE COMPANY:

APPROVALS:

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DESIGN ENGINEER'S STATEMENT:

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR DETAILED ROADWAY, DRAINAGE, GRADING AND EROSION CONTROL PLANS AND SPECIFICATIONS, AND SAID PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH APPLICABLE MASTER DRAINAGE PLANS AND MASTER TRANSPORTATION PLANS, SAID PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR ROADWAY AND DRAINAGE FACILITIES ARE DESIGNED AND ARE CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY DIRECTLY CAUSED BY THE NEGLIGENT ACTS, ERRORS, OR OMISSIONS ON MY PART IN PREPARATION OF THESE DETAILED PLANS AND SPECIFICATIONS.

ELITE PROPERTIES OF AMERICA, INC.

MR. STEVE SCHLOSSER, (719) 592-9333

619 N. CASCADE AVENUE. SUITE 200

COLORADO SPRINGS, COLORADO 80903

MS. MICHELLE REGALDO (719) 546-5416

1480 QUAIL LAKE LOOP ROAD, SUITE A

COLORADO SPRINGS, COLORADO 80906

2880 INTERNATIONAL CIRCLE, SUITE 110

MR. GILBERT LAFORCE (719) 520-7945

MR. GEORGE M. PETERSON, (719) 392-3491

COLORADO SPRINGS, COLORADO 80910

MR. ANDY STECKLEIN, P.E. (719) 227-3264

MR. GABRIEL COSYLEON (719) 562-5528 (ENV. MANAGER) MR. AMBER BILLINGS (719) 227-5725 (ROW MANAGER)

EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT

MR. MARC A. WHORTON, P.E. (719) 785–2802

2138 FLYING HORSE CLUB DR COLORADO SPRINGS, CO 80921

CLASSIC CONSULTING

REGION 2 - ACCESS

REGION 2 - ACCESS

BLACKHILLS ENERGY

P.O. BOX 1600

37 WIDEFIELD BOULEVARD WIDEFIELD, COLORADO 80911

MOUNTAIN VIEW ELECTRIC

LIMON, COLORADO 80828

U.S. WEST COMMUNICATIONS

(LOCATORS) (800) 922-1987

MR. LES ULFERS, (719) 495-2283

5615 WILLS BOULEVARD

PUEBLO, COLORADO 81008

5615 WILLS BOULEVARD

PUEBLO, COLORADO 81008

REGION 2 - NORTH PROGRAM

MARC A WHORTON, COLORADO P.E. #37155 FOR AND ON THE BEHALF OF CLASSIC CONSULTING ENGINEERS & SURVEYORS

<u>OWNER/DEVELOPER'S STATEMENT:</u>

THE OWNER/DEVELOPER HAVE READ AND WILL COMPLY WITH THE REQUIREMENTS OF THE GRADING AND EROSION CONTROL PLAN AND ALL OF THE REQUIREMENTS SPECIFIED IN THESE DETAILED PLANS AND SPECIFICATIONS.

STEVE SCHLOSSER

TOWN OF MONUMENT APPROVAL:

THESE PLANS HAVE BEEN REVIEWED BY TOWN OF MONUMENT STAFF AND FOUND TO BE IN GENERAL COMPLIANCE WITH TOWN STANDARDS. IT IS THE RESPONSIBILITY OF THE SITE ENGINEER AND GENERAL CONTRACTOR TO ENSURE CONSTRUCTION IS IN COMPLIANCE WITH THESE PLANS AND IN CONFORMANCE WITH THE TOWN OF MONUMENT ORDINANCES AND REGULATIONS. THE SPECIFICATIONS, STANDARDS, AND INTENT OF THE TOWN OF MONUMENT ORDINANCES, REGULATIONS AND THE CITY OF COLORADO SPRINGS DRAINAGE CRITERIA MANUALS VOLUMES 1 AND 2 SHALL PREVAIL IN ANY INSTANCES WHERE THESE PLANS DIFFER FROM THOSE REQUIREMENTS. THE DEVELOPMENT SERVICES DEPARTMENT SHALL BE NOTIFIED IF ANY CHANGES NEED TO BE MADE.

THIS REVIEW IS ONLY FOR THE PROPOSED CONSTRUCTION ON JACKSON CREEK PARKWAY

SIGNED TOWN OF MONUMENT

EL PASO COUNTY

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

FILED IN ACCORDANCE WITH THE REQUIREMENTS OF THE EL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2 AND ENGINEERING CRITERIA MANUAL AS AMENDED.

IN ACCORDANCE WITH WITH ECM SECTION 1.12, THESE CONSTRUCTION DOCUMENTS WILL BE VALID FOR CONSTRUCTION FOR A PERIOD OF 2 YEARS FROM THE DATE SIGNED BY THE EL PASO COUNTY ENGINEER. IF CONSTRUCTION HAS NOT STARTED WITHIN THOSE 2 YEARS, THE PLANS WILL NEED TO BE RESUBMITTED FOR APPROVAL, INCLUDING PAYMENT OF REVIEW FEES AT THE PLANNING AND COMMUNITY DEVELOPMENT DIRECTOR'S DISCRETION.

THIS REVIEW IS ONLY FOR THE PROPOSED CONSTRUCTION IN HIGHWAY 105, EAST OF JACKSON CREEK PARKWAY.

(719)785-0799(F

JOSHUA PALMER, P. COUNTY ENGINEER / ECM ADMINISTRATOR

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF CONSULTING DATE 619 N. Cascade Avenue, Suite 200

Colorado Springs, Colorado 80903

DATE

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DATE

DATE

DATE

CDOT GENERAL NOTES

- 1. ALL CONSTRUCTION MATERIALS, TECHNIQUES, AND PROCEDURES WITHIN THE HIGHWAY LIMITS SHALL BE IN CONFORMANCE WITH THE COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) STANDARD SPECIFICATIONS FOR ROAD CONSTRUCTION AS SET FORTH IN THE LATEST "M & S" STANDARDS MANUAL.
- 2. A FULLY EXECUTED COMPLETE COPY OF THE ACCESS PERMITS AND A VALID NOTICE TO PROCEED TO CONSTRUCTION MUST BE ON THE JOB SITE WITH THE CONTRACTOR AT ALL TIMES DURING CONSTRUCTION.
- 3. ANY ADDITIONAL PERMITS AND CLEARANCES REQUIRED BY OTHER FEDERAL, STATE, AND LOCAL GOVERNMENT AGENCIES IS THE RESPONSIBILITY OF THE OWNER/DEVELOPER.
- 4. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL UNDERGROUND UTILITIES ALONG THE ROUTE OF HIGHWAY CONSTRUCTION. THE OMISSION FROM OR THE INCLUSION OF UTILITY LOCATIONS ON THE PLANS IS NOT TO BE CONSIDERED AS THE NONEXISTENCE OF OR A DEFINITE LOCATION OF EXISTING UNDERGROUND UTILITIES.
- 5. THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE UTILITIES WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- 6. ALL STATIONING IS CENTERLINE UNLESS OTHERWISE INDICATED. ALL ELEVATIONS ARE CENTERLINE UNLESS OTHERWISE INDICATED.
- 7. FIVE WORKING DAYS PRIOR TO BEGINNING CONSTRUCTION, THE OWNER/CONTRACTOR MUST CONTACT MR. RON YOUNG (719) 289-8718. CDOT ACCESS/TRAFFIC MANAGER, TO COORDINATE CONSTRUCTION.
- 8. WORK SHALL BEGIN AFTER 8:30 AM AND ALL EQUIPMENT SHALL BE OUT OF THE RIGHT-OF-WAY BEFORE 3:00 PM DURING SCHOOL HOURS/DAYS. NO WORK IS ALLOWED WITHIN THE HIGHWAY RIGHT-OF-WAY ON WEEKENDS OR STATE/FEDERAL HOLIDAYS. NO CONSTRUCTION VEHICLES SHALL BE PARKED, OR CONSTRUCTION MATERIALS STOCKPILED IN THE HIGHWAY RIGHT-OF-WAY OVERNIGHT. NO PRIVATE VEHICLES MAY BE PARKED IN THE HIGHWAY RIGHT-OF-WAY AT ANY TIME DURING CONSTRUCTION.
- 9. TWO WAY TRAFFIC SHALL BE MAINTAINED THROUGHOUT THE WORK AREA AT ALL TIMES.
- 10. ALL SIGNS SHALL BE MANUFACTURED IN ACCORDANCE WITH THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (M.U.T.C.D.). THE SHEETING FOR THE SIGNS BE HIGHWAY INTENSITY SHEETING (ASTM TYPE IV RETRO REFLECTIVE SHEETING).
- 11. ALL DISTURBED PAVEMENT EDGES SHALL BE CUT TO NEAT LINES 1' FROM EXISTING EDGE OF PAVEMENT. NEW SURFACING FOR THE ACCESS AND THE HIGHWAY WIDENING SHALL BE A FULL DEPTH TOTAL OF 7 INCHES OF COMPACTED HOT MIX ASPHALT (HMA), GRAD-S(100), PG. 58-28 OR PG. 64-22 (WITH 1% LIME) PLACED IN 3 LIFTS. OVER 12 INCHES OF CEMENT TREATED SUBGRADE, OVER COMPACTED RANDOM FILL SUBGRADE WITH A MINIMUM R-VALUE OF 17 CONFIRMED WITH R2 MATERIALS.
- 12. PLACEMENT AND COMPACTION OF HOT MIX ASPHALT (HMA) SHALL COMPLY WITH SECTION 401 OF THE 2005 CDOT STANDARD SPECIFICATIONS AS WELL AS THE LATEST CDOT STANDARD SPECIAL PROVISIONS.
- 13. PLACEMENT AND COMPACTION OF SUB-GRADE, EMBANKMENTS, AND BACKFILLS SHALL COMPLY WITH SECTION 203 OF THE CDOT STANDARD SPECIFICATIONS AS WELL AS THE LATEST CDOT STANDARD SPECIAL PROVISIONS.
- 14. SOIL PREPARATION INCLUDING TOPSOIL, SEEDING, AND MULCHING IS REQUIRED WITHIN THE HIGHWAY RIGHT-OF-WAY ON ALL DISTURBED AREAS NOT SURFACED AND THOSE AREAS BEYOND THE HIGHWAY THAT MAY ERODE AND SEND DEBRIS INTO THE HIGHWAY RIGHT-OF-WAY.
- 15. ADDITIONAL EROSION CONTROL STRUCTURES MAY BE REQUIRED AT THE TIME OF CONSTRUCTION.
- 16. WIDENED AREAS OF THE ROADWAY SHALL BE A MINIMUM OF 20-YEAR DESIGN LIFE.
- 17. OVERLAY OF EXISTING PAVEMENT SHALL ALSO BE A MINIMUM OF 20-YEAR DESIGN LIFE TO AVOID DIFFERING MAINTENANCE ISSUES BETWEEN THE OVERLAY SECTION AN THE NEW PAVEMENT WIDENING.
- 18. WATER SHALL BE USED AS A DUST PALLIATIVE WHERE REQUIRED. COST OF WATER SHALL BE INCLUDED IN THE WORK.
- 19. THIS DESIGN IS IN FULL COMPLIANCE WITH SECTION 4 OF THE STATE HIGHWAY ACCESS CODE, 2 CCR 601-1 EXCEPT FOR THE FOLLOWING APPROVED VARIANCES: NONE
- 20. THIS DESIGN IS IN FULL COMPLIANCE WITH TITLE II ADA ACCESSIBILITY REQUIREMENTS EXCEPT FOR THE FOLLOWING APPROVED VARIANCES: NONE

COLORADO DEPARTMENT OF TRANSPORTATION:

CDOT PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH THE CDOT DESIGN CRITERIA. CDOT IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. CDOT THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

EL PASO COUNTY TRAFFIC SIGNAL NOTES

- THE PROJECT.
- SHOWN ON THESE PLANS.
- EQUIPMENT
- CONTAINED IN THE PROJECT PLAN.
- MOUNTING ASSEMBLY.
- ARRANGEMENTS FOR PICKING UP THE SIGNAL CONTROLLER.
- RIGHT.
- ENCLOSURES SHALL BE PROVIDED AT THE CONNECTION POINT OF EACH POWER SOURCE OR POINT OF SERVICE AS DIRECTED
- BY THE ENGINEER. THE FUNCTIONALITY OF ALL TRAFFIC SIGNAL EQUIPMENT.
- ALL WORK ECESSARY TO COMPLETE THE CONSTRUCTION SHOWN ON THESE PLANS.
- WORK NECESSARY FOR PROPER SIGNAL OPERATION HAS BEEN COMPLETED.
- SIGNAL INSTALLATION BE VISIBLE
- ρι δης
- HAS BEEN COMPLETED.
- PROVIDE ADDITIONAL INFORMATION AS DIRECTED BY THE ENGINEER.

- FOUNDATION AND 24 INCH X 36 INCH X 18 INCH FOR THE REMAINING PULL BOXES.

MIGHT

1. THE CONTRACTOR HALL PROVIDE, FOR REVIEW, BY THE ENGINEER, A COMPLETE TRAFFIC SIGNAL MATERIAL SUBMITTAL PACKAGE THAT CONTAINS, ALL OF THE PROPOSED TRAFFIC SIGNAL EQUIPMENT. INCLUDING MATERIAL SPECIFICATIONS AND DESCRIPTIONS THAT WILL BE NECESSARY TO COMPLETE THE TRAFFIC SIGNAL WORK. THE CONTRACTOR SHALL ALLOW FOR A MINIMUM THREE-WEEK SUBMITTAL REVIEW PERIOD AND SHALL NOT ORDER ANY SIGNAL EQUIPMENT UNTIL AFTER A REVIEW OF ALL SUBMITTALS HAVE BEEN COMPLETED BY THE ENGINEER AND VERIFIED BY THE CONTRACTOR.

FUNCTIONAL AND OPERATIONAL RESPONSIBILITY FOR ALL NEWLY INSTALLED AND EXISTING TRAFFIC SIGNAL EQUIPMENT WILL BECOME THE RESPONSIBILITY OF THE CONTRACTOR UNTIL FINAL ACCEPTANCE OF THE PROJECT. THE CONTRACTOR SHALL CONSIDER THIS WORK INCIDENTAL TO THE OVERALL WORK BEING PERFORMED AND SHALL BE INCLUDED AS PART OF

3. SEE COLORADO DEPARTMENT OF TRANSPORTATION SIGNAL DETAILS FOR CONSTRUCTION/ INSTALLATION DETAILS NOT

4. ALL SIGNAL EQUIPMENT REMOVED BY THE CONTRACTOR SHALL BE SALVAGED AND BECOME THE PROPERTY OF EL PASO COUNTY. THE SALVAGED EQUIPMENT SHALL BE DELIVERED AS DIRECTED BY THE ENGINEER. DELIVERY OF THE SIGNAL EQUIPMENT WILL NOT BE PAID FOR SEPARATELY, BUT WILL BE INCLUDED IN THE WORK FOR REMOVAL OF TRAFFIC SIGNAL

5. OVERHEAD STREET NAME SIGN DESIGN AND LAYOUT INFORMATION SHALL BE PER THE STREET MANE SIGN DETAIL

6. TRAFFIC SIGNS MOUNTED ON SIGNAL POLES, MAST ARMS, AND PEDESTALS SHALL BE MOUNTED USING BANDING, ALUMINUM CHANNELS, AND BACKING ZEES PER APPLICABLE COOT STANDARD PLANS, OR SIMILAR RIGID SIGN BRACING

7. ONCE THE PROFESSIONAL ENGINEERING CONSULTANT HAS COMPLETED ALL TRAFFIC SIGNAL CONTROLLER TIMING DEVELOPMENT AND CONTROLLER PROGRAMMING, THE CONTRACTOR WILL COORDINATE THE DELIVERY DATE OF THE PROGRAMMED TRAFFIC SIGNAL CONTROLLER FOR REVIEW OF EPC DEPARTMENT OF PUBLIC WORKS, HIGHWAY DIVISION SIGNAL SHOP AND ALLOW FOR A MINIMUM TWO-WEEK REVIEW PERIOD, AFTER WHICH TIME THE CONTRACTOR MAY MAKE

8. CONTROLLER CABINET SHALL BE FURNISHED WITH A "BEST" DOOR LOCK KIT LOCK AND CODE IS "BEST": 5L6R LEFT AND

9. CONDUIT IS TO BE REPLACED IN THE EVENT THAT EXISTING CONDUIT IS DAMAGED AND AS DIRECTED BY THE ENGINEER. 10. ELECTRICAL SERVICE DISCONNECT BOXES SHALL BE LOCKABLE AND WEATHER PROOF WITH NEMA TYPE CIRCUIT BREAKER.

11. THE CONTRACTOR SHALL FURNISH AND INSTALL ALL WIRING REQUIRED TO COMPLETE THE INSTALLATION AND ESTABLISH

12. ALL INCIDENTAL ITEMS NOT SHOWN IN THE SUMMARY OF APPROXIMATE QUANTITIES OR TABULATION OF SIGNAL EQUIPMENT SHALL BE CONSIDERED TO BE INCLUDED AS PART OF THE TRAFFIC SIGNAL INSTALLATION AND WILL NOT BE MEASURED AND PAID FOR SEPARATELY. ALL QUANTITIES ARE APPROXIMATE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR

13. THE SIGNAL SHALL NOT BE TURNED ON OR STARTED UNTIL DIRECTED BY THE ENGINEER. PRIOR TO SIGNAL ACTIVATION, THE ENGINEER SHALL CONFIRM THAT THE APPROPRIATE PAVEMENT MARKINGS AND SIGNING ARE IN PLACE AND THAT ALL

14. THE SIGNAL CONTROLLER SHALL BE A MACCAIN 2070 FLEX ATC CONTROLLER AND THE CONFLICT MONITOR SHALL BE MODEL 2010 ECLIP W/ ETHERNET PORT (EDI). THE CONTROLLER CABINET SHALL BE A COOT SPECIFICATION MODEL 332D WITH BATTERY BACKUP AND AUX RACK AND SHALL CONTAIN ANTI-GRAFFITI SILVER FINISH COATING. THE CABINET SHALL BE MOUNTED ON A CAST-IN-PLACE CONCRETE FOUNDATION PER APPLICABLE COOT'S STANDARDS STANDARD PLAN AND THE CABINET SHALL BE POSITIONED SUCH THAT, WITH THE FRONT DOOR OPEN, BOTH THE CONTROLLER DISPLAY AND THE

15. LUMINAIRES SHALL CONSIST OF AN ASSEMBLY THAT UTILIZES LEDS AS THE LIGHT SOURCE. IN ADDITION, A COMPLETE LUMINAIRE SHALL CONSIST OF A HOUSING, LED ARRAY, AND ELECTRONIC DRIVER (POWER SUPPLY). ALL LUMINAIRES SHALL BE WIRED 120 VOLTS AC WITH MULTI-TAP HEADS. THE LED FIXTURE MUST HAVE A COLOR TEMPERATURE OF 4100K (+/-SOOK), MUST BE DESIGNED TO OPERATE AT A TEMPERATURE RANGE OF -40"F TO 105"F (-40"C TO 40° C), AND PROVIDE A MINIMUM OF 70,000 HOURS OF OPERATION. LUMINAIRES SHALL BE E-LIGHT-STAR LED STREET LIGHT, OR APPROVED EQUAL. THE CONTRACTOR SHALL PROVIDE A RECOMMENDATION FOR TYPE OF THE STREET LIGHT BASED ON THE CONSTRUCTION PLANS AND MANUFACTURER'S SPECIFICATIONS, TO BE APPROVED BY THE ENGINEER. THE FIXTURE MUST BE CAST ALUMINUM, PROVIDED WITH FUSING, SURGE SUPPRESSION AND MUST BE UL LISTED FOR WET LOCATIONS. THE FIXTURE MUST HAVE AN INTERNAL, WEATHER-TIGHT LED DRIVE. NO ACTIVE COOLING FEATURES (FANS, ETC.) WILL BE ALLOWED. THE FINISHED SHALL MATCH THE EXTENSION ARM SHAFTS. THE LUMINAIRES WILL BE INSTALLED ON 15 FOOT EXTENSION ARM SHAFTS AT NOMINAL HEIGHT OF 40 FEET AND SHALL BE WELDED TO THE SIGNAL POLE PER CDOT TYPICAL TRAFFIC SIGNAL INSTALLATION DETAILS STANDARD PLAN S-614-40. LUMINAIRE ARM SHAFT SHALL BE IN ACCORDANCE WITH THE PROJECT

16. THE INTERSECTION DETECTION SYSTEM {MICROWAVE RADAR} CONTRACT ITEM INCLUDES DEVICE INSTALLATION (I.E., DETECTOR UNIT, HARDWARE, WIRING, PROCESSOR MODULE, ETC.), AND VERIFICATION OF SUCCESSFUL IN-FIELD DETECTION ZONE OPERATION BASED ON SEVERAL VEHICLE ACTUATIONS IN ALL DETECTION ZONES.

17. THE CONTRACTOR SHALL COORDINATE THE SCHEDULES OF THE CONTRACTED PROFESSIONAL ENGINEERING CONSULTANT AND THE EPC DEPARTMENT OF PUBLIC WORKS, HIGHWAY DIVISION TRAFFIC SIGNAL STAFF FOR SCHEDULING THE ON-SITE FIELD IMPLEMENTATION OF ALL TRAFFIC SIGNAL TIMING AND OPERATIONAL PROGRAMMING, VEHICLE DETECTION ZONE PLACEMENT, AND DETECTION EQUIPMENT POSITIONING. THIS WORK SHALL BE SCHEDULED NEAR THE END OF THE PROJECT, PRIOR TO PROJECT ACCEPTANCE, AND ONLY AFTER ALL FINAL PAVEMENT MARKINGS, SIGNING, AND TRAFFIC SIGNAL WORK

18. THE MICROWAVE RADAR DETECTION SYSTEM SHALL UTILIZE MS SEDCO INTERSECTOR TC-CK1-SBE WITH INTERFACE BOARD. 19. PEDESTRIAN SIGNAL HEAD INSTALLATION SHALL INCLUDE ALUMINUM AND POWDER COATED GLOSS BLACK SIGNAL HEAD WITH APPROVED LED COUNTDOWN DISPLAY, ALUMINUM OPEN VISOR WITH THE OUTSIDE POWDER COATED GLOSS BLACK. PUSHBUTTON, AND INSTRUCTIONAL R10-3E COUNTDOWN PEDESTRIAN ACTUATION SIGN. PUSHBUTTONS SHALL BE POLERA NAVIGATOR S 2-WIRE PUSH BUTTONS, SPECIFIED AS INS2 5 UN 1-B-BD-ES, OR APPROVED EQUIVALENT. CUSTOM MESSAGING SHALL NOT INTERFERE WITH TRADITIONAL NON-VISUAL FORMATS SPECIFIED IN 4E OF THE MUTCD AND SHALL ONLY

20. ALL TRAFFIC SIGNAL POLES, MAST ARMS, PEDESTALS, AND LUMINAIRE ARMS SHALL HAVE A GLOSS BLACK COAT FINISH OVER HOT DIP GALVANIZED BASE COAT. INSTALLED IN ACCORDANCE WITH THE PAINT MANUFACTURER'S INSTRUCTIONS.

21. ALL SIGNAL POLE AND CONTROLLER LOCATIONS SHOWN ARE APPROXIMATE ONLY. MAST ARMS SHALL BE OF SUFFICIENT LENGTH AND DESIGN TO ALLOW PROPER PLACEMENT OF SIGNAL HEADS AND OVERHEAD SIGNING PER THE PLANS. ACTUAL LOCATIONS SHALL BE STAKED IN THE FIELD AND FIELD VERIFIED BY THE ENGINEER PRIOR TO DRILLING, EXCAVATION, AND ORDERING THE SIGNAL EQUIPMENT AND MAST ARMS. THE LOCATION OF EACH SIGNAL POLE FOUNDATION SHALL BE POTHOLED PRIOR TO DRILLING TO CONFIRM WHETHER OR NOT ANY UTILITY CONFLICTS EXIST.

22. LATERAL OFFSETS FROM THE NEAR EDGE OF TRAFFIC SIGNAL POLES, PEDESTALS, AND CABINETS TO THE FACE OF CURB OR EDGE OF PAVED SHOULDER SHOULD BE AT LEAST SIX FEET, HOWEVER, A MINIMUM LATERAL OFFSET OF AT LEAST FOUR FEET MAY BE PROVIDED FOR CURB OFFSETS. IF NO PAVED SHOULDER EXISTS, A MINIMUM LATERAL OFFSET OF AT LEAST EIGHT FEET SHOULD BE PROVIDED FROM THE EDGE OF PAVEMENT FOR AN AUXILIARY LANE AND A MINIMUM LATERAL OFFSET OF AT LEAST TWELVE FEET SHOULD BE PROVIDED FROM THE EDGE OF PAVEMENT FOR A THROUGH LANE.

23. SHOULD THE CONTRACTOR ENCOUNTER WATER IN THE CAISSON, ANY DE-WATERING METHODS AND NECESSARY PERMITS SHALL BE INCLUDED IN THE COST OF THE CAISSON AND WILL BE CONSIDERED INCIDENTAL TO THE WORK.

24. ALL TRAFFIC SIGNAL COMPONENT PULL BOXES SHALL BE PRE-CAST HIGH DENSITY POLYMER CONCRETE (HDPC) MATERIAL WITH THE FOLLOWING SIZES: 36 INCH X 48 INCH X 18 INCH FOR THE PULL BOX ADJACENT TO THE CONTROLLER CABINET

25. TRAFFIC PULL BOX LOCATIONS SHOWN IN THE PROJECT PLANS ARE APPROXIMATE. ACTUAL LOCATIONS SHALL BE VERIFIED IN THE FIELD BY THE ENGINEER. PULL BOXES SHALL BE FLUSH WITH THE FINISHED GROUND SURFACE AND SHALL NOT BE PLACED IN AREAS THAT ARE SUSCEPTIBLE TO WATER RUNOFF OR STANDING WATER. CONDUIT RUNS BETWEEN PULL BOXES SHALL NOT EXCEED APPROXIMATELY 200 FEET AND PULL BOXES SHALL NOT BE LOCATED IN HANDICAP RAMPS, PEDESTRIAN LANDING AREAS, SIDEWALKS, PRIMARY SIDEWALK PATHS, OR ROADWAY PAVEMENT AREAS.

EL PASO COUNTY TRAFFIC SIGNAL NOTES (CONT.)

- 26. THE CONDUIT NUMBER AND SIZES FOR TYPICAL CONDUIT RUNS INCLUDE THE FOLLOWING FOR A PREEMINENT MAST ARM SIGNAL INSTALLATION.
- A. BETWEEN THE SIGNAL POLE FOUNDATION AND ADJACENT SIGNAL POLE PULL BOX: TWO (2) 2 INCH AND ONE (1) 3 INCH.
- B. BETWEEN SIGNAL PULL BOXES: TWO (2) 2 INCH AND THREE (3) 3 INCH.
- C. BETWEEN THE CONTROLLER CABINET FOUNDATION AND ADJACENT PULL BOX: THREE (3) 2 INCH AND FOUR (4) 3 INCH. D. BETWEEN THE SECONDARY SERVICE PEDESTAL METER FOUNDATION AND THE CONTROLLER CABINET FOUNDATION ONE (1) 2 INCH FOR THE ELECTRICAL SERVICE FEED.
- 27. ALL CONDUIT AND FITTINGS SHALL BE SCHEDULE 80 PVC AND ALL CONDUIT SHALL HAVE A PULL ROPE LEFT IN THEM WHEN CONSTRUCTION IS COMPLETED. ALL CONDUIT ENTERING THE CABINET FOUNDATION AND PULL BOXES SHALL HAVE BELL END STYLE COUPLINGS ON ALL CONDUIT ENDS.
- 28. ALL CONDUIT THAT IS DIRECTIONALLY BORED SHALL BE A MINIMUM OF THREE FEET BELOW THE EXISTING PAVEMENT. THIS WORK SHALL AVOID DISTURBING OR DAMAGING EXISTING FACILITIES AND THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROMPT RECONSTRUCTION, ALTERATION, REPAIR OR MAINTENANCE OF HIGHWAY PROPERTY, AS NECESSARY, TO REPAIR DAMAGE CAUSED BY THE ACCOMMODATION OF THE UTILITY, AND TO RESTORE THE HIGHWAY TO PRE-EXISTING OR BETTER CONDITIONS.
- 29. ALL SIGNAL CABLE SHALL BE CONTINUOUS FROM CONNECTIONS MADE IN THE HANDHOLE COMPARTMENT OF THE SIGNAL POLE BASE TO THE TERMINAL COMPARTMENT OF THE CONTROLLER CABINET AND SHALL CONTAIN NO SPLICES. EACH SIGNAL HEAD SHALL CONTAIN SEPARATE AND CONTINUOUS SIGNAL CABLE FROM THE SIGNAL HEAD TO THE ABOVE GROUND HANDHOLE AT THE BASE OF THE SIGNAL POLE AND SHALL CONTAIN NO SPLICES.
- 30. A SEPARATE AND CONTINUOUS 21 CONDUCTOR CABLE SHALL RUN FROM THE CONTROLLER CABINET TO THE HANDHOLE AT EACH SIGNAL POLE AND SHALL CONTAIN NO SPLICES.
- 31. ALL SIGNS MOUNTED ON SIGNAL POLES, MAST ARMS, AND PEDESTALS SHALL BE MOUNTED USING BANDING ALUMINUM CHANNELS, AND BACKING ZEES PER CDOT TYPICAL POLE MOUNT SIGN INSTALLATIONS STANDARD PLAN S-614-20, OR SIMILAR RIGID SIGN BRACING MOUNTING ASSEMBLY. AS DIRECTED BY THE ENGINEER. MAST ARM SIGNS THAT REQUIRE Z-BRACKETS SHALL BE MOUNTED ON ASTRO-STYLE BRACKETS AND RISERS. THE COST OF ALL HARDWARE FITTINGS, TOOLS, AND EQUIPMENT NECESSARY FOR A COMPLETE INSTALLATION OF MAST ARM SIGNS WILL NOT BE MEASURED AND PAID FOR SEPARATELY BUT SHALL BE INCLUDED IN THE COST OF THE WORK.
- 32. ALL CONDUCTORS AND CABINET WIRING SHALL BE COLOR CODED AND PERMANENTLY TAGGED PER ENGINEER DIRECTION AND IN ACCORDANCE WITH THE SIGNAL PHASE NUMBERING AND DETECTION ZONE PHASE NUMBERING INFORMATION CONTAINED IN THE PROJECT PLANS.
- 33. ALL VEHICLE SIGNAL HEADS SHALL HAVE APPROVED 12 INCH LED INDICATIONS AND SHALL BE ALUMINUM WITH POWDER COATED GLOSS BLACK FINISH AND SHALL CONTAIN 12 INCH ALUMINUM TUNNEL VISORS WITH THE OUTSIDE POWDER COATED GLOSS BLACK. ALL VEHICLE SIGNAL HEADS SHALL HAVE ALUMINUM LOUVERED BACK PLATES WITH POWDER COATED GLOSS BLACK FINISH AND YELLOW RETRO REFLECTIVE BORDER. MAST ARM SIGNAL HEADS SHALL USE ASTRO- TYPE MOUNTING ASSEMBLIES AND SHALL BE INSTALLED APPROXIMATELY LEVEL WITH ONE ANOTHER AT A 17 TO 19 FOOT VERTICAL CLEARANCE ABOVE THE HIGH POINT OF THE PAVEMENT GRADE.
- 33. FINAL VEHICLE DIRECTION ZONE PLACEMENT AND DIMENSIONS, IN ACCORDANCE WITH THE PROJECT PLAN, AND FINAL SIGNAL PROGRAMMING SHALL BE COMPLETED IN THE FIELD AND THE CONTRACTOR SHALL CONTACT THE ENGINEER FOR COORDINATING AND SCHEDULING THIS WORK.
- 34. ALL VEHICLE AND PEDESTRIAN SIGNAL HEADS THAT HAVE NOT BEEN PLACED IN SERVICE SHALL BE COVERED WITH PREFABRICATED WEATHER RESISTANT NYLON FORM FITTING SIGNAL FACE COVER MATERIAL. THE SIGNAL FACE SHALL REMAIN COMPLETELY COVERED UNTIL THE SIGNAL HEAD IS PLACED IN SERVICE AND IS FULLY FUNCTIONAL AND OPERATIONAL
- 35. ALL DETECTION EQUIPMENT, DETECTION ZONES, AND SIGNAL TIMING OPERATION SHALL BE CONFIRMED IN THE FIELD BY THE PROFESSIONAL ENGINEERING CONSULTANT TO BE ACHIEVING SATISFACTORY TRAFFIC SIGNAL OPERATION. 36. COMMUNICATION SYSTEM SHALL BE A DYMEC ETHERNET SWITCH KY-3170EMX AND CELLULAR MODEM MICROHARD
- BULLET LTE, WITH CITEL SURGE SUPPRESSION ON ALL THESE COMPONENTS. 38. THE CONTRACTED PROFESSIONAL ENGINEERING TRAFFIC SIGNAL TIMING, CONTROLLER PROGRAMMING AND OPERATION
- AND OVERALL TRAFFIC SIGNAL OPERATIONAL CONSULTANT SERVICES THAT ARE TO BE RETAINED BY THE OWNER/ DEVELOPER/ DISTRICT SHALL INCLUDE, BUT NOT BE LIMITED TO:
- A. DEVELOPING ALL TRAFFIC SIGNAL TIMING AND ALL OPERATIONAL PARAMETERS FOR ACHIEVING ISOLATED, FULL-ACTUATED VEHICLE AND PEDESTRIAN INTERSECTION OPERATION AND, WHEN DOCUMENTED TO BE NECESSARY, COORDINATED SIGNAL SYSTEM TIMING PLAN OPERATION DURING VARIOUS TIMES OF THE DAY.
- B. PROGRAMMING ALL SIGNAL TIMING PARAMETERS INTO THE TRAFFIC SIGNAL CONTROLLER. C. FIELD IMPLEMENTING AND FINE-TUNING/ ADJUSTING ALL TRAFFIC SIGNAL TIMING PARAMETERS, INCLUDING FOLLOW-UP FIELD REVIEWS AS MAY BE NECESSARY.
- D. DEVELOPING, PROGRAMMING, FIELD IMPLEMENTING, AND FINE-TUNING ALL VEHICLE DETECTION ZONE DIMENSIONS, ZONE LOCATIONS, AND OPERATIONAL PARAMETERS.

ALL OF THE AFOREMENTIONED CONTRACTED PROFESSIONAL ENGINEERING TRAFFIC SIGNAL OPERATIONAL CONSULTANT SERVICED DELIVERABLES SHALL BE CONSISTENT WITH NATIONAL PUBLICATIONS, INCLUDING BUT NOT LIMITED TO: MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD) LATEST EDITION/ REVISION. FHWA-HOP-08-024 "TRAFFIC SIGNAL TIMING MANUAL" (JUNE 2008), FHWA-HRT-04-091 "SIGNALIZED INTERSECTIONS: INFORMATIONS GUIDE" (AUGUST 2004), FHWA-HOP-06-006 "TRAFFIC CONTROL SYSTEMS HANDBOOK" (OCTOBER 2005), FHWA-DTFH61-01-C-00183 "SIGNAL TIMING PROCESS FINAL REPORT" (DECEMBER 2003), NCHRP REPORT 731 "GUIDELINES FOR TIMING YELLOW AND ALL-RED INTERVALS AT SIGNALIZED INTERSECTIONS" (2012), NCHRP REPORT 812 "SIGNAL TIMING MANUAL SECOND EDITION" (2015)

48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811	1	REVISED PER CDOT/COUNTY COMMENTS	5/12/23	PREPARED UNDER MY DIRECT S
UTILITY NOTIFICATION CENTER OF COLORADO				CLASSIC CONSULTING ENGINEERS
IT'S THE LAW				
THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR				
SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL				
BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND				MARC A. WHORTON, COLORADO
PRESERVE ANY AND ALL UNDERGROUND UTILITIES.				······································

TOWN OF MONUMENT GENERAL NOTES:

- 1. ALL MATERIALS, WORKMANSHIP, AND CONSTRUCTION OF SITE IMPROVEMENTS SHALL MEET OR EXCEED THE SITE WORK STANDARDS AND SPECIFICATIONS AND THE STANDARDS AND SPECIFICATIONS SET FORTH IN THE TOWN OF MONUMENT MUNICIPAL CODE CRITERIA, AND APPLICABLE STANDARDS, AND APPLICABLE LOCAL, STATE, AND FEDERAL REGULATIONS. WHERE THERE IS CONFLICT BETWEEN THESE PLANS AND THE SPECIFICATIONS, OR ANY APPLICABLE STANDARDS. THE HIGHER QUALITY STANDARD SHALL APPLY. ALL WORK WITHIN PUBLIC R.O.W. OR EASEMENTS SHALL BE INSPECTED AND APPROVED BY THE TOWN OF MONUMENT INSPECTOR. THE TOWN WILL ALSO INSPECT ALL WORK ON PRIVATE PROPERTY.
- 2. THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES, AS SHOWN ON THESE PLANS, IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED UPON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE LOCAL UTILITY LOCATION CENTER AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATIONS OF THE UTILITIES. PRIOR TO CONSTRUCTION. THE CONTRACTOR SHALL VERIFY PERTINENT LOCATIONS AND ELEVATIONS, ESPECIALLY AT THE CONNECTION POINTS AND AT POTENTIAL UTILITY CONFLICTS. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES THAT CONFLICT WITH THE PROPOSED IMPROVEMENTS SHOWN ON THESE PLANS.
- 3. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS FROM THE TOWN OF MONUMENT AND ALL APPLICABLE AGENCIES. THE CONTRACTOR SHALL NOTIFY THE TOWN INSPECTOR AT LEAST 48 HOURS PRIOR TO THE START OF ANY EARTH DISTURBING ACTIVITY, OR CONSTRUCTION ON ANY AND ALL PUBLIC IMPROVEMENTS.
- 4. THE CONTRACTOR SHALL COORDINATE AND COOPERATE WITH THE TOWN AND ALL UTILITY COMPANIES INVOLVED WITH REGARD TO RELOCATIONS OR ADJUSTMENTS OF EXISTING UTILITIES DURING CONSTRUCTION AND TO ASSURE THAT THE WORK IS ACCOMPLISHED IN A TIMELY FASHION AND WITH THE MINIMUM DISRUPTION OF SERVICE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONTACTING ALL PARTIES AFFECTED BY ANY DISRUPTION OF ANY UTILITY SERVICE.
- 5. THE CONTRACTOR SHALL HAVE ONE (1) SIGNED COPY OF THE APPROVED PLANS, ONE (1) COPY OF THE APPROPRIATE STANDARDS AND SPECIFICATIONS, AND A COPY OF ALL PERMITS NEEDED FOR THE JOB, ON-SITE AT ALL TIMES.
- 6. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ASPECTS OF SAFETY INCLUDING, BUT NOT LIMITED TO, EXCAVATION, TRENCHING, SHORING, TRAFFIC CONTROL, AND SECURITY.
- 7. IF, DURING THE CONSTRUCTION PROCESS, CONDITIONS ARE ENCOUNTERED WHICH COULD INDICATE A SITUATION THAT IS NOT IDENTIFIED IN THE PLANS OR SPECIFICATIONS, THE CONTRACTOR SHALL CONTACT THE ENGINEER OF RECORD AND THE TOWN INSPECTOR IMMEDIATELY
- 8. ALL REFERENCES TO ANY PUBLISHED STANDARDS SHALL REFER TO THE LATEST REVISION OF SAID STANDARD, UNLESS SPECIFICALLY STATED OTHERWISE.
- 9. THE CONTRACTOR SHALL SUBMIT A TRAFFIC CONTROL PLAN, IN ACCORDANCE WITH M.U.T.C.D. TO THE TOWN OF MONUMENT FOR APPROVAL. PRIOR TO ANY CONSTRUCTION ACTIVITIES WITHIN, OR AFFECTING, THE RIGHT-OF-WAY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING ANY AND ALL TRAFFIC CONTROL DEVICES AS MAY BE REQUIRED BY THE CONSTRUCTION ACTIVITIES.
- 10. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING ALL LABOR AND MATERIALS NECESSARY FOR THE COMPLETION OF THE INTENDED IMPROVEMENTS SHOWN ON THESE DRAWINGS OR DESIGNATED TO BE PROVIDED, INSTALLED, OR CONSTRUCTED, UNLESS SPECIFICALLY NOTED OTHERWISE.
- 11. THE CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING ROADWAYS FREE AND CLEAR OF ALL CONSTRUCTION DEBRIS AND DIRT TRACKED FROM THE SITE.
- 12. THE CONTRACTOR SHALL BE RESPONSIBLE FOR RECORDING AS-BUILT INFORMATION ON A SET OF RECORD DRAWINGS KEPT AT THE CONSTRUCTION SITE, WHICH SHALL BE AVAILABLE TO THE TOWN OF MONUMENT DEVELOPMENT SERVICES DEPARTMENT INSPECTOR AT ALL TIMES. A REPRODUCIBLE SET OF AS-BUILT DRAWINGS MUST BE FURNISHED TO THE TOWN OF MONUMENT AT THE COMPLETION OF THE PROJECT, PRIOR TO FINAL APPROVAL BY THE TOWN AND AS A CONDITION FOR OBTAINING A CERTIFICATE OF OCCUPANCY.
- 13. DIMENSIONS FOR LAYOUT AND CONSTRUCTION ARE NOT TO BE SCALED FROM ANY DRAWING. IF PERTINENT DIMENSIONS ARE NOT SHOWN, CONTACT THE ENGINEER-OF-RECORD FOR CLARIFICATION, AND ANNOTATE THE DIMENSION ON THE AS-BUILT RECORD DRAWINGS
- 14. ALL STRUCTURAL EROSION CONTROL MEASURES SHALL BE INSTALLED, AT THE LIMITS OF CONSTRUCTION, PRIOR TO ANY OTHER GROUND DISTURBING ACTIVITY. ALL EROSION CONTROL MEASURES SHALL BE MAINTAINED IN GOOD REPAIR BY THE CONTRACTOR, UNTIL SUCH TIME AS THE ENTIRE DISTURBED AREAS ARE STABILIZED WITH HARD SURFACE OR LANDSCAPING.
- 15. THE CONTRACTOR SHALL SEQUENCE THE INSTALLATION OF UTILITIES IN SUCH A MANNER AS TO MINIMIZE POTENTIAL UTILITY CONFLICTS. IN GENERAL, STORM SEWER AND SANITARY SEWER SHOULD BE CONSTRUCTED PRIOR TO INSTALLATION OF WATER LINES AND DRY UTILITIES
- 16. NO SITE-RELATED IMPROVEMENTS MAY COMMENCE UNTIL A PRE-CONSTRUCTION MEETING IS HELD WITH THE TOWN OF MONUMENT AND ALL APPLICABLE PERMITS ARE OBTAINED.
- 17. THE DEVELOPER MUST IDENTIFY TO THE TOWN OF MONUMENT, PRIOR TO THE START OF ANY WORK, A QUALIFIED PLAN PERSON RESPONSIBLE FOR REVIEWING AND MONITORING ALL OPERATIONS IN ORDER TO PREVENT OR MINIMIZE THE IMPACT OF VIBRATION, NOISE, DUST, DRAINAGE, AND EROSION DAMAGE, AND OTHER FORMS OF POLLUTION ON NEARBY PROPERTY AND THE PUBLIC AS A WHOLE. THE DEVELOPER MUST WRITE TO THE OWNERS/OCCUPANTS OF PROPERTIES WITHIN AT LEAST 100 YARDS OF THE LIMITS OF THE WORKSITE, INFORMING THEM OF THE NATURE AND TIMING OF THE PROJECT AND PROVIDING CONTACT DETAILS FOR COMPLAINTS. THE TOWN, PRIOR TO THE COMMENCEMENT OF THE PROJECT, MUST APPROVE A COPY OF THE LETTER, MAILING LIST, AND DELIVERY DATES.
- 18. ***TOWN OF MONUMENT DISCLAIMER*** APPROVAL OF THESE SITE CONSTRUCTION PLANS PRIOR TO SITE PLAN APPROVAL DOES NOT IN ANY WAY OBLIGATE THE TOWN TO APPROVE SUBSEQUENT SUBMITTALS (I.E., SITE PLANS AND PLATS), AND THE TOWN HAS NO LIABILITY IN ANY FORM DUE TO ITS ACTIONS IN THE APPROVAL OF THESE SITE CONSTRUCTION PLANS.

TOWN OF MONUMENT CONSTRUCTION NOTES:

- 1. THE TOWN OF MONUMENT DESIGN CRITERIA & CONSTRUCTION SPECIFICATIONS MANUAL IS CONSIDERED PART OF THIS CONSTRUCTION DRAWING SET. THIS DESIGN AND PLAN SET IS INCOMPLETE WITHOUT THIS SPECIFICATIONS MANUAL. THE CONTRACTOR SHALL OBTAIN A COPY OF THIS MANUAL AND BE FAMILIAR WITH IT FOR ALL CONSTRUCTION ACTIVITIES. A COPY CAN BE OBTAINED FROM THE TOWN BY CALLING (719)-499-3375.
- 2. ALL MATERIALS AND WORKMANSHIP SHALL BE IN COMPLIANCE WITH THE TOWN CRITERIA AND CONSTRUCTION SPECIFICATION MANUAL AND TOWN OF MONUMENT MUNICIPAL CODE AND SHALL BE SUBJECT TO INSPECTION BY THE TOWN OF MONUMENT INSPECTOR.
- 3. THE CONTRACTOR SHALL VERIFY THE LOCATION OF ALL EXISTING UTILITIES PRIOR TO ACTUAL CONSTRUCTION. ALL EXISTING UTILITIES SHOWN ARE BASED ON INFORMATION OF RECORD. THE CONTRACTOR IS RESPONSIBLE TO TAKE PRECAUTIONARY MEASURES TO PROTECT THE EXISTING UTILITIES SHOWN HEREON AND ANY OTHER EXISTING UTILITIES NOT OF RECORD OR NOT SHOWN ON THESE PLANS AND AGREES TO ACCEPT FULL RESPONSIBILITY FOR FAILURE TO LOCATE AND PRESERVE ANY AND ALL EXISTING UTILITIES.
- 4. THE HORIZONTAL AND VERTICAL LOCATION OF EXISTING IMPROVEMENTS TO BE MET BY THE PROPOSED IMPROVEMENTS SHOWN ON THESE PLANS SHALL BE CONFIRMED BY FIELD MEASUREMENTS PRIOR TO CONSTRUCTION. ANY SIGNIFICANT DISCREPANCIES FOUND BETWEEN THIS PLAN SET AND ACTUAL FIELD CONDITIONS SHALL BE IMMEDIATELY REPORTED TO THE ENGINEER OF RECORD FOR APPROPRIATE ACTION.
- 5. THE CONTRACTOR IS ADVISED THAT ALL EXISTING CONDITIONS OUTSIDE THE AREA OF WORK SHALL BE PROTECTED, IF DAMAGE OCCURS DURING CONSTRUCTION, IT WILL BE REPLACED IN THE ORIGINAL EXISTING CONDITION AT THE CONTRACTOR'S EXPENSE.
- 6. CONCRETE USED FOR CONSTRUCTION OF CURB AND GUTTER, SIDEWALK, AND CROSSPANS SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 4,000 P.S.I. AFTER 28 DAYS.
- 7. ALL DISTURBED PAVEMENT EDGES WILL BE CUT TO NEAT LINES. THE THICKNESS OF ANY REPLACED ASPHALT AND BASE COURSE SHALL EQUAL OR EXCEED THE EXISTING THICKNESS.
- 8. WHEN ABUTTING NEW PAVEMENT TO EXISTING, OR TO REMOVE ANY BROKEN OR CRACKED PAVEMENT, SAWCUT EXISTING PAVEMENT TO A STRAIGHT EDGE AND AT A RIGHT ANGLE, OR AS APPROVED BY THE TOWN INSPECTOR.
- 9. FINAL GRADING OF CURBS AND PAVING SHALL PROVIDE POSITIVE DRAINAGE. STANDING WATER POCKETS OR PONDING WILL NOT BE ACCEPTABLE.
- 10. WHERE REMOVAL OF EXISTING CURB, GUTTER, SIDEWALK, OR PAVEMENT IS REQUIRED, THE CONTRACTOR SHALL SAWCUT AND/OR REMOVE TO THE NEAREST JOINT. CURB, GUTTER, AND SIDEWALK SHOWN AS EXISTING ON THESE PLANS IS NOT TO BE REMOVED UNLESS OTHERWISE NOTED. IF ANY OF THE EXISTING CURB, GUTTER, OR SIDEWALK IS DAMAGED BY THE CONTRACTOR, THEN IT SHALL BE REPLACED AT THE CONTRACTOR'S EXPENSE.
- 11. CONTRACTOR SHALL PROVIDE TRAFFIC CONTROL AND ROUTING DURING CONSTRUCTION, IF REQUIRED. TWO-WAY TRAFFIC SHALL BE MAINTAINED THROUGH THE WORK AREA AT ALL TIMES.
- 12. ALL DISTURBED AREAS THAT ARE TO REMAIN UNCOVERED FOR A PERIOD GREATER THAN 2 MONTHS SHALL BE RESEEDED AND WATERED UNTIL STABLE VEGETATION IS ESTABLISHED.
- 13. AT LEAST ONE SIGNED AND STAMPED SET OF THESE CONSTRUCTION DRAWINGS SHALL BE KEPT ON-SITE AT ALL TIMES.

SUPERVISION FOR AND ON BEHALF OF RS AND SURVEYORS, LLC

DATE

P.E. #37155

.		STATE HIGH PKWY. – PH	WAY 10 HASE 2)5 / JACKSO CONSTRUCTI	N CREEP	K NS		
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	Colorado Springs, Colorado 80903 (719)/85–0790 (719)785–0799(Fax)	CHECKED BY		(V) 1"= N/A	JOB NO.		1302.	22

PLAN NUMBER	M STANDARD
<u>M-100-1</u>	STANDARD SYMBOLS (3 SHEETS)
<u> </u>	ACRONYMS AND ABBREVIATIONS (4 SHEETS)
□ M-203-1	APPROACH ROADS
□ M-203-2	DITCH TYPES
□ M-203-11	SUPERELEVATION CROWNED AND DIVIDED HIGHWAYS (3 SHEETS)
🔀 M-203-12	SUPERELEVATION STREETS (2 SHEETS)
M-206-1	EXCAVATION AND BACKFILL FOR STRUCTURES (2 SHEETS)
□ M-206-2	EXCAVATION AND BACKFILL FOR BRIDGES (2 SHEET
₩-208-1	TEMPORARY EROSION CONTROL (11 SHEETS)
□ M-210-1	MAILBOX SUPPORTS (2 SHEETS)
□ M-214-1	NURSERY STOCK DETAILS
₩ M-216-1	SOIL RETENTION COVERING (2 SHEETS)
□ M-412-1	CONCRETE PAVEMENT JDINTS (9 SHEETS) (REVISED DN JANUARY 31, 2022)
□ M-412-2	CONCRETE PAVEMENT CRACK REPAIR (6 SHEETS) <i>(REVISED ON SEPTEMBER 6, 2022)</i>
□ M-510-1	STRUCTURAL PLATE PIPE H-20 LOADING
□ M-601-1	SINGLE CONCRETE BOX CULVERT (CAST-IN-PLACE). (2 SHEETS)
□ M-601-2	DOUBLE CONCRETE BOX CULVERT (CAST-IN-PLACE) (2 SHEETS)
□ M-601-3	TRIPLE CONCRETE BOX CULVERT (CAST-IN-PLACE). (2 SHEETS)
₩-601-10	HEADWALL FOR PIPES
□ M-601-11	TYPE "S" SADDLE HEADWALLS FOR PIPE
□ M-601-12	HEADWALLS AND PIPE OUTLET PAVING
□ M-601-20	WINGWALLS FUR PIPE OR BUX CULVERIS (2 SHEE)
□ M-603-1	METAL PIPE (4 SHEETS)
M-603-2	REINFURCED CONCRETE PIPE
□ M-603-3	(REVISED ON SEPTEMBER 10, 2020)
∟ M-603-4	CORRUGATED POLYETHYLENE PIPE (AASHTO M294) CORRUGATED POLYPROPYLENE PIPE (AASHTO M330) <i>(REVISED ON MARCH 7, 2022)</i>
□ M-603-5	POLYVINYL CHLORIDE (PVC) PIPE (AASHTO M304)
□ M-603-6	STEEL REINFORCED POLYETHYLENE RIBBED PIPE (AASHTO MP 20)
□ M-603-10	CONCRETE AND METAL END SECTIONS
□ M-603-12	TRAVERSABLE END SECTIONS AND SAFETY GRATES (3 SHEETS)
🔀 M-604-10	INLET, TYPE C
□ M-604-11	INLET, TYPE D
₩-604-12	CURB INLET TYPE R (2 SHEETS)
□ M-604-13	CONCRETE INLET TYPE 13
₩ M-604-20	MANHOLES (3 SHEETS)
□ M-604-25	VANE GRATE INLET (5 SHEETS) (REVISED ON FEBRUARY 3, 2023)
₩-605-1	SUBSURFACE DRAINS

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Designer Initials: JBK	R-X		
Last Modification Date: 04/14/23	R-X		
Detailer Initials: LTA	R-X		
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PAGE <u>NUMBER</u>	PLAN <u>NUMBER</u>	M STANDARD <u>TITLE</u> <u>NU</u>	PAGE PLAN <u>JMBER</u> <u>NUMBER</u>
1–3	□ M-606-1	MIDWEST GUARDRAIL SYSTEM TYPE 3 W-BEAM	.79-97 🗖 S-612-1
	□ M-606-13	GUARDRAIL TYPE 7 F-SHAPE BARRIER (4 SHEETS)	98-101
10-12		(REVISED ON FEBRUARY 9, 2023)	□ S-613-2
10-12	□ M-606-15	GUARDRAIL TYPE 9 SINGLE SLOPE BARRIER	.105-115 🔀 S-614-1
	□ M-607-1	WIRE FENCES AND GATES (3 SHEETS)	. 116-118 🔀 S-614-2
15–16	□ M-607-2	CHAIN LINK FENCE (3 SHEETS)	. 119-121 🔀 S-614-3
TS) 17-18	□ M-607-3	BARRIER FENCE	122 🗖 S-614-4
19-29	□ M-607-4	DEER FENCE, GATES, AND GAME RAMPS (7 SHEETS) · <i>(REVISED ON JULY 13, 2020)</i>	123-127
	□ M-607-10	PICKET SNOW FENCE	128 🗖 S-614-6
	□ M-607-15	RDAD CLOSURE GATE (9 SHEETS)	129-137 S -614-8
	₩-608-1	CURB RAMPS (10 SHEETS)	138-147
	₩ M-609-1	CURBS, GUTTERS, AND SIDEWALKS (4 SHEETS)	.148-151 <u>S-614-9</u>
	□ M-611-1	CATTLE GUARD (2 SHEETS)	152-153
4.0	M 611-2	DEER GUARD (2 SHEETS)	$154 - 155$ \Box $5 - 614 - 10$
	M = 614 = 1	RUMBLE STRIPS (J SHEETS)	$150-150$ \Box $5-614-12$
	M = 614 = 2	EMBANKMENT PROTECTOR TYPE 3	161 D S-614-14
43-44	□ M-615-2	EMBANKMENT PROTECTOR TYPE 5	162 X S-614-20
	□ M-616-1	INVERTED SIPHON	
45-46	□ M-620-1	FIELD LABORATORY CLASS 1	164
	□ M-620-2	FIELD LABORATORY CLASS 2 (2 SHEETS)	.165-166 🛛 🖾 S-614-22
48	□ M-620-11	FIELD OFFICE CLASS 1	167 🗖 S-614-40
	□ M-620-12	FIELD OFFICE CLASS 2	168
TS) 50-51	□ M-629-1	SURVEY MONUMENTS (2 SHEETS)	169-170 🔀 S-614-40
52-55			~1
56			□ S-614-41
57			S-614-42
AND 58 -		DEPARIMENT OF TRANSPORTATION	□ S-614-43
) (2 sheets)	١	M&S STANDARDS PLANS LIST	□ S-614-44
		UUV 31 2010 UPDATE THIS	SHEET S-614-45
60		AS APPLICAB	LE D S-614-50
61		Revised on April 14 2023	□ S-614-60
S 62–64		Revised on April 7, 2020	X 5-627-1
65	P		<u>」</u> 区 S-630-1
	ALL	OF THE M&S STANDARD PLANS, AS SUPPLEMENTED	⊠ S-630-2
	AND	REVISED, APPLY TO THIS PROJECT WHEN USED	
	BY	DESIGNATED PAY ITEM UR SUBSIDIARY ITEM.	□ S-630-3
73-77			□ S-630-4
	THE M&S ST	TANDARD PLANS USED TO DESIGN THIS PROJECT ARE	□ S-630-5
78	INDICATED	BY A MARKED BOX \blacksquare , and will be attached to 1	THE 🗖 S-630-6
	PLANS. ALL	OTHER M&S STANDARD PLANS ARE STILL ELIGIBLE F	OR USE S-630-7
	IN CONSTRU	ICTIUN IF APPRUVED BY AN APPROPRIATE CDOT ENG	INEER.
heet Revision			
Comment	s (Colorado Department of Transportation	STAN
e en monte		CDDT HQ, 3rd Floor	
	7	Denver, CD 80204	PLAN
		Construction Engineering Services	Issued by the Project Day
			issued by the Project Dev

48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811	1	REVISED PER CDOT COMMENTS	5/18/23	PREPARED UNDER MY DIRECT S
UTILITY NOTIFICATION CENTER OF COLORADO				CLASSIC CONSULTING ENGINEERS
IT'S THE LAW				
CATIONS OF EXISTING UNDERGROUND UTILITIES ARE				
DETERMINE THE EXACT LOCATION OF ALL EXISTING				
LY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH				
RVE ANY AND ALL UNDERGROUND UTILITIES.				MARC A. WHORION, COLORADO

S STAI TIT	NDARD I F	NUMBER
DELINEATOR INSTALLATIONS	(8 SHEETS)) 171–178
(REVISED ON JANUARY 19, 2 RDADWAY LIGHTING (6 SHEE	2 023) ETS)	.179-186-
ALTERNATIVE ROADWAY LIG	u, 2020) hting (4 se	HEETS)
(NEW, ISSUED ON SEPTEMBE	R 30, 2020)	
GROUND SIGN PLACEMENT (2	2 SHEETS)	
CLASS I SIGNS		
CLASS II SIGNS (3 SHEETS	;)	191–19.3
BREAK-AWAY SIGN SUPPORT	DETAILS	
CONCRETE FOOTINGS AND S	IGN ISLANDS	S 196–197
TUBULAR STEEL SIGN SUPPORT	DRT DETAILS	S (7 SHEETS)198-204
PEDESTRIAN PUSH BUTTON	, <i>2020)</i> Post Assea	181 Y (2 SHEETS) 205-206-
(SUPERSEDED ON JANUARY	23, 2020 B	Y S-614-45)
MARKER ASSEMBLY INSTALL	ATIONS	
MILEPOST SIGN DETAIL FOR	HIGH SNOW	/ AREAS 208
STRUCTURE NUMBER INSTAL	LATION (2 S	SHEETS) 209-210
FLASHING BEACON AND SIGN	N INSTALLAT	IONS (4 SHEETS). 211-214
TYPICAL POLE MOUNT SIGN	INSTALLATI	ONS
(2 SHEETS) (REVISED ON S	EPTEMBER 2	216–217 21, 2020)
TYPICAL MULTI-SIGN INSTAL	LATIONS	
TYPICAL TRAFFIC SIGNAL 3 65'-75' SINGLE MAST ARMS (REVISED ON JULY 22, 202)	0'-75'DUUBL (5 SHEETS) 2)	.E MAST ARMS219-223
ALTERNATIVE TRAFFIC SIGN 25'-55' SINGLE MAST ARMS (REVISED DN JULY 22.202	AL (4 SHEETS) 2)	
TEMPORARY SPAN WIRE SIG	 NALS (13 SH	HEETS)
CABINET FOUNDATION DETAI	L (4 SHEET	S)241–244
TRAFFIC LOOP AND MISCELL (8 SHEETS)	ANEDUS SIG	NAL DETAILS245-252
PEDESTAL POLE SIGNALS (2	SHEETS)	253–254
PEDESTRIAN PUSH BUTTON (REVISED ON DECEMBER 3, 2	POST ASSEN 2020)	BLY DETAILS (6 SHEETS)
STATIC SIGN MONOTUBE STR	RUCTURES (12 SHEETS)255-266
DYNAMIC SIGN MONOTUBE S	TRUCTURES	(14 SHEETS)267-280
PAVEMENT MARKINGS (11 SHE (REVISED ON APRIL 14, 202	EETS) 3)	
TRAFFIC CONTROLS FOR HIC (26 SHEETS) <i>(REVISED ON</i>	GHWAY CONS <i>January 20</i>	STRUCTION
BARRICADES, DRUMS, CONCRE AND VERTICAL PANELS	TE BARRIER	S (TEMP)314
FLASHING BEACON (PORTABL	E) DETAILS	
STEEL SIGN SUPPORT (TEMF DETAILS (2 SHEETS)	ORARY) INS	TALLATION
PORTABLE RUMBLE STRIPS ((TEMPORARY))(2 SHEETS)318-319
EMERGENCY PULL-OFF AREA	(TEMPORAR	Y)320
ROLLING ROADBLOCKS FOR (3 SHEETS)	TRAFFIC CO	NTROL
	STAN	ΝΠΑΡΠΡΙ ΔΝΙΝΟ
JAKD	STAN	ADDE DI ANE I ICT
TIT	STANL	
	Stand	ard Sheet No. 1 of 1

Issued by the Project Development Branch: July 31, 2019

Project Sheet Number:

STATE HIGHWAY 105 / JACKSON CREEK PRWY. – PHASE 2 CONSTRUCTION PLANS CDOT STANDARD PLAN SHEET <u>_</u> CLASSIC T SUPERVISION FOR AND ON BEHALF OF EERS AND SURVEYORS, LLC CONSULTING DESIGNED BY PRA SCALE DATE 02-23-23 PRA (H) 1"= N/A SHEET 3 OF 26 DRAWN BY 0 P.E. #37155 DATE
 619 N. Cascade Avenue, Suite 200
 (719)785-0790

 Colorado Springs, Colorado 80903
 (719)785-0799(Fax)
 (V) 1"= N/A JOB NO. 1302.22









48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811				PREPARED UNDER MY DIRECT SU
UTILITY NOTIFICATION CENTER OF COLORADO IT'S THE LAW				CLASSIC CONSULTING ENGINEERS
CATIONS OF EXISTING UNDERGROUND UTILITIES ARE				
IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR DETERMINE THE EXACT LOCATION OF ALL EXISTING S REFORE COMMENCING WORK THE CONTRACTOR SHALL				
Y RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH E CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND				MARC. A. WHORTON, COLORADO
/E ANY AND ALL UNDERGROUND UTILITIES.				





48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811	1	ADDED SECTION SHEET PER CDOT COMMENTS	7/10/23	PREPARED UNDER MY DIRECT SU
UTILITY NOTIFICATION CENTER OF COLORADO				CLASSIC CONSULTING ENGINEERS
CATIONS OF EXISTING UNDERGROUND UTILITIES ARE				
IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR DETERMINE THE EXACT LOCATION OF ALL EXISTING				
Y RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH				MARC A. WHORTON, COLORADO
/E ANY AND ALL UNDERGROUND UTILITIES.				,

TOTAL HOT MIX ASPHALT DE	EPTH	6.0"
# OF LIFTS		3
HOT MIX ASPHALT	LIFT 1	2.0"
GRAD-S(75) (PG 64-22)	LIFT 2	2.0"
HOT MIX ASPHALT SURFACE COURSE GRAD-SX(75) (PG 64-28)	LIFT 3	2.0"

48 HOURS BEFORE YOU DIG,	NO	. REVISION	DATE	REVIEW:
UTILITY LOCATORS 811 UTILITY NOTIFICATION CENTER OF COLORADO IT'S THE LAW	1	REVISED PER JACOBS COMMENTS	5/17/23	PREPARED UNDER MY DIRECT SU CLASSIC CONSULTING ENGINEERS
CATIONS OF EXISTING UNDERGROUND UTILITIES ARE IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR DETERMINE THE EXACT LOCATION OF ALL EXISTING S BEFORE COMMENCING WORK. THE CONTRACTOR SHALL LY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND				MARC A. WHORTON, COLORADO

48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811	1	REVISED PER JACOBS COMMENTS	5/17/23	PREPARED UNDER MY DIRECT S
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IT'S THE LAW				
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ETERMINE THE EXACT LOCATION OF ALL EXISTING				
BEFORE COMMENCING WORK. THE CONTRACTOR SHALL Y RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH				
E CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND E ANY AND ALL UNDERGROUND UTILITIES.				MARC A. WHORTON, COLORADO
			1	

						H-		
			GHW AV 105		50	25 0 SCALE	50 E: 1" = 50'	100
27+10.22, 36.50' LT (JCP) = 7+41.97 (HYW 105) OF REVERSE CURVE EL = 7031.61			29-bd					
C19 C20	SEE SHEET CREEK PAR 105 CON		15 FOR JACK STATE HIGH TO THE NOR	SON WAY TH				
8	STA. 27-	-10.22, 41.50 [°]	RT (JCP) =			EL PASO C "HIGHWAY 1 IMPROVEMEN	OUNTY 105 PROJECT A NT LIMIT LINE	Ā"
$\frac{1000}{1000} PT STA. 25+53.92$ $\frac{1000}{1000} PT STA. 25+53.92, 41.50' RT$	STA. 0+0 RT_FL_EL PROP. RETAINI PROP. 8' SIDEWAL	0.00 (HYW 10 = 7034.82 <u>7' HIGH MAX</u> NG WALL <u>ATTACHED</u>			5-1-1-00 +	HIGH		
The EL = 7041.20 $\frac{25+12.71, 42.78' \text{ RT}}{= 7042.45}$ $\frac{10E}{87.19, 000}$ 1000	PROPOSED S (SEE SHEETS PROP. CDOT TY C&G SECTION III (MODIFIED SPILL UNPLATTED IOUNTAIN STA TELEPHONE	TES				WAY 105		
								/ //
+66.00 0.39.66 35% -3 00 							7050	
HCL EL: 703	Image: Constraint of the sector of	PVI STA PVI ELEV	=28+09.33 / =7028.69 =6.51%				7040	
	28.98 8.98.3 28.36.1 28.36.1 28.36.1 20.31.96 4.51% -4	K = L = LP STA: LP ELE PROP	=22.28 145.00 28+37.27 /: 7029.70 OSED HCL GRA	ल VT: 28+81.83 ↓ L EL: 7030.14	29+09.09 НСL PROFILE EL = 7030.69 СН НМҮ 105)			
Image: sector	EK PARKWAY BEGIN HWY BY CCES)	AND	PIVOT POINT				7030	
TINUE 4% ROADWAY CROSS PE TO ACHIEVE SMOOTH NSITION INTO STATE HWAY 105 EXISTING GRADE	STA. 27+10.22 HCL EL = 7033.16 (END JACKSON CRE STREET PLANS AND 105 STREET PLANS			AT HCL			7020	
RT TRAVEL WAY e = +4.0%								
CENTERLINE & PIVOT POINT								
LT TRAVEL WAY e = -4.0%	+00	28+	00	29+	-00			
PERVISION FOR AND ON BEHALF OF AND SURVEYORS, LLC		AS NSULTIN		SM STATE PKWY. ROADW JACKSO	HIGHWAY - PHASE AY IMPROVEM ON CREEK PK	105 / JACH 2 CONSTRU ENT PLANS WY. PLAN &	KSON CREEK JCTION PLAN PROFILE	
P.E. #37155 DATE	ENGINEE	KS & SU	(719)785-0790	DRAWN	BY PRA	(H) 1"= 5	50' SHEET 13	3 OF 26

9.50' LT 32.78	SEE SHEET CREEK PAI 105 CON	5 12 AND 15 RKWAY AND ST TINUATION TO 27+10.22, 2.50' L EL = 7033.02	FOR JACKSO TATE HIGHWA THE NORTH		50 EL PA: "HIGHV IMPRO"	25 0 SCALE: SO COUNTY VAY 105 PRO- VEMENT LIMIT	50 1" = 50'	100
VPROP. CDOT TYPE 2		ų						
C&G SECTION IB (MODIFIED CARRY)	PROP. 8	<u>17' HIGH MAX</u> ING WALL 3' ATTACHED	N			HIG		
$\frac{251.02}{54} = 7039.40$	SIDEWAL PROPOSED S (SEE SHEETS	K TORM SEWER 5 21-22)		$\backslash \backslash$		AN PL		
		(١			105		
	MOUNTAIN S - TELEPHO	eu) Tates / Ne~ /					\ \	
				\mathcal{A}			١	
				X	\ \			
+66.00							7050	
359,66 35% 3 00								
1035.72								
		PVI STA =2 PVI ELEV =	8+09.33 7028.69				7040	
	200 200 200 200 200 200 200 200 200 200	K =22 L =145 LP STA: 28	.28 .00 3+37.27	<u>8</u> 33	<u>ه</u>			
	3'92' 92'+2' -4.51% 2' ;;	LP ELEV: 7	7029.70	28+81.6	09.09 PROFILE 1 7030.6 HWY 105.6			
	HCL EL	PROPOSE AND PIVO	D HCL GRADE DT POINT	PVT: HCL EL	MATCH = 29+			
	ES)			2.00			7030	
			E	XISTING GR	ADE			
	0.22 7033.16 ANS AN CR PLANS		,					
TINUE 4% ROADWAY CROSS PE TO ACHIEVE SMOOTH	TA. 27+1 CL EL = CL EL = CND JACH IREET PI							
NSITION INTO STATE							7020	
RT TRAVEL WAY e = +4.0%								
CENTERLINE & PIVOT POINT								
LT TRAVEL WAY e = -4.0%								
26+00 27	+00	28+00		29-1	-00			
				STATE PKWY	HIGHWAY – PHASE	105 / JACK 2 CONSTRU	SON CREEK	
PERVISION FOR AND ON BEHALF OF AND SURVEYORS, LLC	CL	ASS	I	ROADW	AY IMPROVEN	IENT PLANS		
		DNSULTING			UN CREEK PK	WY. RAISED N	DATE	U 2 02−23−23
P.E. #37155 DATE	619 N. Cascade Avenu	e, Suite 200 (7	719)785-0790		BY PRA	(H) $1" = 5($)' SHEET 14	4 OF 26 1302.22

48 HOURS BEFORE YOU DIG,	NO.	REVISION	DATE	REVIEW:
811	1	REVISED PER CDOT/COUNTY/TOWN OF MONUMENT COMMENTS	7/10/23	PREPARED UNDER MY DIRECT S
TILITY NOTIFICATION CENTER OF COLORADO IT'S THE LAW				CLASSIC CONSULTING ENGINEER
TONS OF EXISTING UNDERGROUND UTILITIES ARE AN APPROXIMATE WAY ONLY. THE CONTRACTOR				
ERMINE THE EXACT LOCATION OF ALL EXISTING				
RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND ANY AND ALL UNDERGROUND UTILITIES.				MARC. A. WHORTON, COLORADO

CHECKED BY

Colorado Springs, Colorado 80903 (719)785–0799(Fax)

(V) 1"= 5' JOB NO. 1302.22

48 HOURS BEFORE YOU DIG,	NO.	REVISION		DATE	REVIEW:
811	1	ADDED PEDRAMP DETAIL SHEET TO PLAN	6	5-23-23	PREPARED UNDER MY DIRECT SU
UTILITY NOTIFICATION CENTER OF COLORADO IT'S THE LAW	-				CLASSIC CONSULTING ENGINEERS
CATIONS OF EXISTING UNDERGROUND UTILITIES ARE					
DETERMINE THE EXACT LOCATION OF ALL EXISTING ES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL					
BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND RVE ANY AND ALL UNDERGROUND UTILITIES.					MARC A. WHORTON, COLORADO

	-			
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BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND				MARC A. WHORTON, COLORADO
PRESERVE ANY AND ALL UNDERGROUND UTILITIES.				

(V) 1"= N/A JOB NO. 1302.22

CHECKED BY

(719)785-0799(Fax)

Colorado Springs, Colorado 80903

LITY DIS TE RELO IITARY A ACILITIES	THE UNDER DIFFERENT AND DOES N PROJECT. FU THE HWY 10 TO CONSIDE DETERMINA TRICT CATIONS _{OP} ND	GROUND ST THAN PREV IOT TIE INTO JRTHER CO 5 PROJECT RATION OF TION OF RE TION OF RE FOP FOP FOP	ORM LAYOU IOUSLY DISC O THE HWY 10 ORDINATION IS REQUIRED THIS LAYOU SPONSIBILITI	T IS VERY USSED D5A WITH D PRIOR T AND ES!!	Wx N	W _X W _X PW FOP FOP	V NPW FOP	50 25		50 1" = 50'	100
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₩ <u>x</u>	₩,			F F	OP FOP	FOP FOP	FOP	FOP	— FOP — F(0 V	
PROP. R RETAININ	EDI-RÔĈKSP - G	AS			85 —	SS SS	SS	SS		_	
				<u>GAS</u> <u>GAS</u> JGE UGE	OP GAS G, UGE UGE	AS - GAS		<u> </u>	- FOP FC AS GAS - UGE	- DF	
UNPL WOOI RINAR	ATTED DMOOR Y HOSPITA	L	- SS - S	VALLE ESTATES F LC	Y VISTA FILING NO. ()T 3	 	VA ESTATE	LLEY VI ES FILIN LOT 4	STA G NO. 3,		
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			× -								
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		7060									
/		2050 87.73 94.73 87.73									
/u24.20											
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+ 52.90	4 UIA. IN(S) = ST/ ST/ SEF										
STA. 10	18" INV 18" INV	7040									
				7020			3.17 L.F	F. ~ 18" R(SEWER @ 1	CP	7020	
								IA. 0+06.80 (. COMMUN			
		7030						(. COMMUNIC	CATION T, COMM.		
								0+05.67			
				7010 <u>§</u> ₽	TA. 0+02.50 ISTALL 5' DIA. 1 IM = 7020.91	YPE II MANHO	LE AT-G	LL 10' TYPI RADE INLET PLAN VIEW	E R FOR TOP	7010	
				1 	8" INV IN(N) = 0" INV IN(E) = 0" INV OUT(W) =	7014.58 7014.08 = 7013.58	OF B(18" ⊪	UX ELEVATION VV OUT(N)	UNS = 7014.61		
		7020		C	UT = 7.33'						
				7000	STOR	STATE HI M SEWER	GHWAY RUN 1	105 — LAT	1	7000	
						0	+00 IF HICH	WAY 105			Sa Sa
IPERVISI AND SI	ON FOR AND ON JRVEYORS, LLC	N BEHALF OF		AS	SIC	PKW	Y. – PH	HASE 2	PROFILE	ICTION PLAN	$\frac{\overline{O}}{\frac{1}{10000000000000000000000000000000$
			FNGIN	CONSULTI	NG JRVFVORS	SM DESIG	NED BY	PRAS	SCALE	DATE	02-23-23
P.E.	#37155	DATE	619 N. Cascade Av Colorado Springs	enue, Suite 200 colorado 8090.3	(719)785–0790 (719)785–0790	DRAW DORAW DORAW DRAW	N BY	PRA ((H) 1" = 50 (V) 1" = 5	0' SHEET 2 5' JOB NO.	1 OF 26 1302.22

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			1	1				

CURB AND GUTTER TYPE 2 (SECTION IB) (6 IN. BARRIER – 1 FT. GUTTER)

CURB AND GUTTER TYPE 2

(SECTION IM)

(6 IN. MOUNTABLE - 1 FT. GUTTER)

· Δ · · Δ ·

(SECTION IIB)

Computer File Information			Sheet Revisions
Creation Date: 07/31/19		Date:	Comments
Designer Initials: JBK	(R-X)		
Last Modification Date: 07/31/19	(R-X)		
Detailer Initials: LTA	(R-X)		
CAD Ver.: MicroStation V8 Scale: Not to Scale Units: English	(R-X)		

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48 HOURS BEFORE YOU DIG,	NO. REVISION	DATE	REVIEW:
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Y RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH			
BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND VE ANY AND ALL UNDERGROUND UTILITIES.			MARC. A. WHORTON, COLORADO

CDOT ITEM NO.	ITEM DESCRIPTION	UNITS	TOTAL	NOTES
202-00828	REMOVAL OF TRAFFIC SIGNAL EQUIPMENT	LS	1	REFER TO THE REMOVAL ITEMS AND QUANTITIES BELOW
	REMOVAL OF TRAFFIC SIGNAL POLE	EACH	4	
-	REMOVAL OF TRAFFIC SIGNAL HEAD	EACH	12	
FOR	REMOVAL OF TRAFFIC SIGNAL CONTROLLER AND CABINET	EACH	1	
INFORMATION	REMOVAL OF LUMINAIRE	EACH	4	RETURN TO EL PASO COUNTY
ONLY	REMOVAL OF STREET NAME SIGN	EACH	3	
	REMOVAL OF LANE USE/OPERATION SIGN	EACH	2	
	REMOVAL OF SPAN WIRE CABLE	LF	320	
210-00479	RESET RADIO COMMUNICATION ANTENNA	EACH	1	
503-00036	DRILLED SHAFT (36 INCH)	LF	60	CDOT STD. S-614-40A FOOTING
613-00206	2 INCH ELECTRICAL CONDUIT (BORED)	LF	400	SCHEDULE 80
613-00306	3 INCH ELECTRICAL CONDUIT (BORED)	LF	800	SCHEDULE 80
613-01200	2 INCH ELECTRICAL CONDUIT (PLASTIC)	LF	155	SCHEDULE 80
613-01300	3 INCH ELECTRICAL CONDUIT (PLASTIC)	LF	190	SCHEDULE 80
613-07003	TYPE THREE PULL BOX	EACH	4	SIGNAL POLE AND CONTROLLER PULL BOXES
613-07004	TYPE FOUR PULL BOX	EACH	1	HOME RUN PULL BOX
613-10000	WIRING	LS	1	SIGNAL AND LIGHTING
613-13004	LUMINAIRE (LED) (4,000 LUMENS)	EACH	4	
613-50109	METER POWER PEDESTAL	EACH	1	
614-00011	SIGN PANEL (CLASS I)	SF	40	
614-70150	PEDESTRIAN SIGNAL FACE (16) (COUNTDOWN)	EACH	2	LED TYPE, POLYCARBONATE, YELLOW INCOLOR
614-70336	TRAFFIC SIGNAL FACE (12-12-12)	EACH	15	LED TYPE, POLYCARBONATE, YELLOW INCOLOR
614-72855	TRAFFIC SIGNAL CONTROLLER CABINET	EACH	1	
614-72860	PEDESTRIAN PUSH BUTTON	EACH	1	PUSH BUTTON STATION, R10-3e SIGN AND ANY NECESSARY EXTE
614-72863	PEDESTRIAN PUSH BUTTON POST ASSEMBLY	EACH	2	CDOT STD. S-614-45, INCLUDES R10-3e SIGNS
614-72866	FIRE PREEMPTION UNIT AND TIMER	EACH	1	INCLUDES 2 PREEMPTION UNITS
614-72886	INTERSECTION DETECTION SYSTEM (CAMERA)	EACH	2	
614-81000	TRAFFIC SIGNAL-LIGHT POLE STEEL	EACH	1	
614-81125	TRAFFIC SIGNAL-LIGHT POLE STEEL $(1-25$ foot mast arm)	EACH	1	CDOT STD. S-614-40A
614-81145	TRAFFIC SIGNAL-LIGHT POLE STEEL $(1-45$ foot mast arm)	EACH	1	CDOT STD. S-614-40A
614-81155	TRAFFIC SIGNAL-LIGHT POLE STEEL (1-55 FOOT MAST ARM)	EACH	1	CDOT STD. S-614-40A
614-86248	TRAFFIC SIGNAL CONTROLLER (TYPE 2070LC)	EACH	1	

- Jack	PRINT DATE: 05/5/2023 11:26 AM	_		SHEET REVISION	S	EST. 1879	AS CONSTRUCTED) _
4-01	FILE NAME: T121234-01SIG-TAB01.DWGHORIZ. SCALE:N/AVERT. SCALE:N/A	- $(R-X)$	DATE	COMMENTS	INITIALS		NO. REVISIONS:	-
121234	FELSBURG 3 South Tejon Street, Suite 300 Colorado Springs, CO 80903					NONUMENT	REVISED:	DESIGNER:
S:/	HOLI & Phone: 719.314.1800 ULLEVIG www.FHUENG.com					COLORADO	VOID:	- DETAILER: Sheet subs

JACKSON CR	PROJECT NO./CODE	
STATE HIG	HWAY 105	121234-01
BJH	STRUCTURE	
BEN.HARMS	NUMBERS	
ET: TRAFFIC	SHEET SUBSET: TT-01 OF	1

TRAFFIC SIGNAL POLE AND MAST ARM
PEDESTRIAN PUSH BUTTON POLE
LUMINAIRE
TRAFFIC SIGNAL HEAD
TRAFFIC SIGNAL HEAD & BACKPLATE
PEDESTRIAN SIGNAL HEAD
SIGNAL CONTROLLER CABINET
PULL BOX
SIGNAL CONDUITS
VEHICLE DETECTOR CAMERA
PED PUSH BUTTON & SIGN
FIRE PREEMPTION UNIT
RADIO COMMUNICATION ANTENNA

F			
l			

)U	0	lg.
		~

JACKSON CREEK	PROJECT NO./CODE	
INALLIC SIGNAL		
STATE HIGHWAY	121234-01	
BJH STRUC	TURE	
BEN.HARMS NUME	ERS	
ET: TRAFFIC SHEET	SUBSET: TS-01 OF 2	

LEGEND (PBS-R/L = PED PUSH BUTTION STATION WITHR10-3e RIGHT OR LEFT SIGN PULL BOX (TYPE 4) (24"X36"X24") PULL BOX (TYPE 3) (17"X30"X12") ------ TR ------ TRAFFIC SIGNAL CONDUIT STREET CROSSINGS - TRAFFIC SIGNAL CONDUIT PULL BOX CONNECTIONS SIGNAL CONDUITS 1-2" (TRENCHED) POWER METER: 1-2" AND 4-3" (TRENCHED) CONTROLLER SIGNAL POLES 1-2" AND 2-3" (TRENCHED) PUSH BUTTON POST

STREET CROSSINGS

2-2" 1-2" AND 2-3" (TRENCHED) (BORED)

PULL BOX AND CONDUIT LOCATIONS ARE APPROXIMATE ONLY. TO THE EXTENT POSSIBLE, THE CONTRACTOR SHALL INSTALL PULL BOXES OUTSIDE OF SIDEWALK AREAS; HOWEVER, IF PULL BOXES NEED TO BE PLACED WITHIN SIDEWALKS, THEY SHALL BE INSTALLED FLUSH WITH THE FINISHED SURFACE AND THE LIDS SHALL HAVE AN ANTI-SKID SURFACE TREATMENT. PULL BOXES SHALL NOT BE INSTALLED IN ANY CURB RAMPS.

<u>SCHEDULE OF TRAFFIC SIGNAL POLES</u>

C SIGN	VAL POLE	STAKING LOCATION AND CAISSON DETAILS			
r arm	LUMMINAIRE ARM	NORTHING	EASTING	DIAMETER	DEPTH
) FT	15 FT ARM	1459419.60	3183115.91	36 IN	15 FT
_	15 FT ARM	1459418.55	3183021.45	36 IN	15 FT
) FT	15 FT ARM	1459515.01	3182989.04	36 IN	15 FT
FT	15 FT ARM	1459514.13	3183107.67	36 IN	15 FT

JACKSON CR	PROJECT NO./CODE		
STATE HIG	121234-01		
BJH	STRUCTURE		
BEN.HARMS NUMBERS			
ET: TRAFFIC	SHEET SUBSET:	TS-02 OF 2	

Document1.pdf Markup Summary

8/11/2023 1:03:19 PM (1)

Subject: Callout Page Label: 97 Author: CDurham Date: 8/11/2023 1:03:19 PM Status: Color: Color: Color: Space:

8/11/2023 1:09:23 PM (1)

Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/11/2023 1:09:23 PM Status: Color: Layer: Space:

Unresolved:

Unresolved:

Verify pipe size-Appendix calculations say 18" and CD's say 24". Update so same size is referenced through all documents

Per storm profiles in CD set, pipe size is 24".
8/11/2023 1:09:46 PM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/11/2023 1:09:46 PM Status: Color: Layer: Space:

8/11/2023 1:10:53 PM (1)

Unresolved: On both maps, indicate what facilities are public and/or private Subject: Text Box Page Label: [1] Layout1 Author: CDurham Date: 8/11/2023 1:10:53 PM Status: Color: Layer: Space:

8/11/2023 1:13:26 PM (1)

Unresolved: Include calculation for drainage swale along too of retaining wall to show that it is sized to handle the flow. Subject: Text Box Page Label: 50 Author: CDurham Date: 8/11/2023 1:13:26 PM Status: Color: Layer: Space:

8/11/2023 1:30:46 PM (1)

Subject: Text Box Page Label: [1] Layout1 Author: EPCDPW-Werre Date: 8/11/2023 1:30:46 PM Status: Color: ■ Layer: Space:

8/11/2023 1:37:22 PM (1)

SOUTH SID	Subject: Line
PKWY. AND	Page Label: [1] LAYOUT1
-SECOND QL	Author: EPCDPW-Werre
	Date: 8/11/2023 1:37:22 PM
	Status:
	Color: 📕
	Layer:
	Space:

8/11/2023 1:37:48 PM (1)



Subject: Callout Page Label: [1] LAYOUT1 Author: EPCDPW-Werre Date: 8/11/2023 1:37:48 PM Status: Color: Layer: Space: Unresolved: Label ROW & any easements along SH 105

Unresolved: On both maps, indicate what facilities are public and/or private

Unresolved: Include calculation for drainage swale along top of retaining wall to show that it is sized to handle the flow.

UPDATE THIS SHEET AS APPLICABLE

THIRD

8/11/2023 1:56:42 PM (1)



Subject: Callout Page Label: [1] LAYOUT1 Author: EPCDPW-Werre Date: 8/11/2023 1:56:42 PM Status: Color: Layer: Space:

THIS INLET NEEDS TO BE INSTALLED BEFORE THE WALL IS BUILT AND IDEALLY BY THE DEVELOPER

8/11/2023 1:57:05 PM (1)



8/11/2023 2:25:03 PM (1)

SCALI FIX PAGE NUMBERS BY THE CONTRACTOR FOR A PLEASING APP 10 AND 17) FOR ADDITIONAL INFORMAT EAS OF RECONSTRUCTION AND/OR RE-STRI Subject: Callout Page Label: [1] Layout1 Author: EPCDPW-Werre Date: 8/11/2023 2:25:03 PM Status: Color: Laver: Space:

8/11/2023 2:30:17 PM (1)



Subject: Callout Page Label: [1] LAYOUT1 Author: EPCDPW-Werre Date: 8/11/2023 2:30:17 PM Status: Color: Layer: Space:

8/11/2023 2:30:56 PM (1)



Subject: Callout Page Label: [1] LAYOUT1 Author: EPCDPW-Werre Date: 8/11/2023 2:30:56 PM Status: Color: Layer: Space:

PAGE SHOWS A COMPLETELY DIFFERENT LAYOUT THAN PAGE 5- GEC PLAN.

8/11/2023 2:32:05 PM (1)



Subject: Callout Page Label: [1] SI-01 Author: EPCDPW-Werre Date: 8/11/2023 2:32:05 PM Status: Color: Laver: Space:

THE UNDERGROUND STORM LAYOUT IS VERY DIFFERENT THAN PREVIOUSLY DISCUSSED AND DOES NOT TIE INTO THE HWY 105A PROJECT. FURTHER COORDINATION WITH THE HWY 105 PROJECT IS REQUIRED PRIOR TO CONSIDERATION OF THIS LAYOUT AND DETERMINATION OF **RESPONSIBILITIES!!**

FIX PAGE NUMBERS

THE UNDERGROUND STORM LAYOUT IS VERY DIFFERENT THAN PREVIOUSLY DISCUSSED AND DOES NOT TIE INTO THE HWY 105A PROJECT. FURTHER COORDINATION WITH THE HWY 105 PROJECT IS REQUIRED PRIOR TO CONSIDERATION OF THIS LAYOUT!!

THE UNDERGROUND STORM SHOWN ON THIS

8/11/2023 2:38:36 PM (1)



Subject: Callout Page Label: [1] STORM-1 Author: EPCDPW-Werre Date: 8/11/2023 2:38:36 PM Status: Color: Layer: Space:

8/14/2023 8:28:34 AM (1)

RKWAY - PHA
S Contron ADD Projects
SHEET INDEX

Subject: Text Box Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 8:28:34 AM Status: Color: ■ Layer: Space:

8/14/2023 8:28:46 AM (1)



Subject: Text Box Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 8:28:46 AM Status: Color: Layer: Space:

8/14/2023 9:21:12 AM (1)

Subject: Callout Page Label: [1] LAYOUT2 Author: CDurham Date: 8/14/2023 9:21:12 AM Status: Color: Layer: Space:

8/14/2023 9:25:46 AM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:25:46 AM Status: Color: Color: Color: Space:

8/14/2023 9:27:14 AM (1)

°AVEMENT TAIL<mark>⊂TO_LEFT)</mark> Subject: Highlight Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:27:14 AM Status: Color: Layer: Space: THE UNDERGROUND STORM LAYOUT IS VERY DIFFERENT THAN PREVIOUSLY DISCUSSED AND DOES NOT TIE INTO THE HWY 105A PROJECT. FURTHER COORDINATION WITH THE HWY 105 PROJECT IS REQUIRED PRIOR TO CONSIDERATION OF THIS LAYOUT AND DETERMINATION OF RESPONSIBILITIES!!

Comments provided by DPW Capital Projects

Comments provided by DPW Development Services

Unresolved: Include calculation in drainage report to show that swale is sized to adequately handle flow

Pavement section detail calls for 6" of asphalt but pavement section lift detail only adds up to 5". Please revise so details show same information.

8/14/2023 9:27:39 AM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:27:39 AM Status: Color: Layer: Space:

8/14/2023 9:29:31 AM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:29:31 AM Status: Color: Layer: Space:

8/14/2023 9:29:50 AM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:29:50 AM Status: Color: Layer: Space:

8/14/2023 9:32:29 AM (1)



Subject: Text Box Page Label: [1] SI-01 Author: CDurham Date: 8/14/2023 9:32:29 AM Status: Color: Layer: Space:

8/14/2023 9:39:09 AM (1)



Subject: Highlight Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:39:09 AM Status: Color: Layer: Space:

8/14/2023 9:40:17 AM (1)



Subject: Callout Page Label: [1] Layout1 Author: CDurham Date: 8/14/2023 9:40:17 AM Status: Color: Layer: Space: Pavement section detail calls for 6" of asphalt but pavement section lift detail only adds up to 5". Please revise so details show same information.

Asphalt lift is different than previous sheets. Please revise to same detail or clearly state where different lift sections are happening within plan.

Asphalt lift is different than previous sheets. Please revise to same detail or clearly state where different lift sections are happening within plan.

Unresolved: Show underground utility crossings

Per Std Dtl SD_2-41 in the ECM, landing area of a pedestrian ramp shall not exceed 2% in any direction. Please revise

8/14/2023 9:41:38 AM (1)



Subject: Callout Page Label: [1] SI-04 Author: CDurham Date: 8/14/2023 9:41:38 AM Status: Color: Layer: Space:

8/14/2023 9:58:30 AM (1)



Subject: Callout Page Label: [1] STORM-1 Author: CDurham Date: 8/14/2023 9:58:30 AM Status: Color: Layer: Space:

8/14/2023 9:59:29 AM (1)



Subject: Callout Page Label: [1] STORM-1 Author: CDurham Date: 8/14/2023 9:59:29 AM Status: Color: Layer: Space:

8/14/2023 9:59:46 AM (1)

Maang HGL Ing

Subject: Callout Page Label: [1] STORM-1 Author: CDurham Date: 8/14/2023 9:59:46 AM Status: Color: Layer: Space:

8/14/2023 10:56:31 AM (1)



Subject: Callout Page Label: 62 Author: CDurham Date: 8/14/2023 10:56:31 AM Status: Color: Layer: Space:

StormCAD in FDR appendix shows pipe size as

18". Please coordinate between 2 documents to

Missing HGL line

Unresolved: Per road profiles in CD set, street slope is approximately 5.5%

8/14/2023 11:01:42 AM (1)



Subject: Text Box Page Label: 1 Author: CDurham Date: 8/14/2023 11:01:42 AM Status: Color: Layer: Space:

Include public improvements back into estimate that were provided on first review (ABC, pavement, signs, pavement markings, storm pipe, inlets, etc)

Unresolved: Label c&g type

show same pipe size.

Fix overlapping text