FINAL DRAINAGE PLAN SF 24X

VILLAGE AT LORSON RANCH

APRIL, 2024

Prepared for:

Lorson, LLC 212 N. Wahsatch Ave, Suite 301 Colorado Springs, Colorado 80903 (719) 635-3200

Prepared by:

Core Engineering Group, LLC 15004 1ST Avenue South Burnsville, MN 55306 (719) 570-1100

Project No. 100.070



TABLE OF CONTENTS

ENGINEER'S STATEMENT1
OWNER'S STATEMENT1
FLOODPLAIN STATEMENT
1.0 LOCATION and DESCRIPTION
2.0 DRAINAGE CRITERIA
3.0 EXISTING HYDROLOGICAL CONDITIONS
4.0 DEVELOPED HYDROLOGICAL CONDITIONS
5.0 HYDRAULIC SUMMARY
6.0 DETENTION and WATER QUALITY PONDS
7.0 DRAINAGE and BRIDGE FEES
8.0 FOUR STEP PROCESS
9.0 CONCLUSIONS
10.0 REFERENCES

APPENDIX A

VICINITY MAP, SCS SOILS INFORMATION, FEMA FIRM MAP

APPENDIX B

HYDROLOGY CALCULATIONS

APPENDIX C

HYDRAULIC CALCULATIONS

APPENDIX D

POND G1/G2

APPENDIX E

DRAINAGE BOARD MEETING MINUTES FOR BASINCLOSURE STORM SEWER SCHEMATIC and HYDRAFLOW STORM SEWER CALCS

BACK POCKET

EXISTING CONDITIONS DRAINAGE MAP DEVELOPED CONDITIONS DRAINAGE MAPS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Richard L. Schindler, P.E. #33997 For and on Behalf of Core Engineering Group, LLC

OWNER'S STATEMENT

I, the Owner, have read and will comply with all the requirements specified in the drainage report and plan.

Lorson, LLC

By Jeff Mark

Title

Manager

Address

212 N. Wahsatch Avenue, Suite 301, Colorado Springs, CO 80903

FLOODPLAIN STATEMENT

To the best of my knowledge and belief, this development is not located within a designated floodplain as shown on Flood Insurance Rate Map Panel No. and 08041C0957 G, dated December 7, 2018. (See Appendix A, FEMA FIRM Exhibit)

Richard L. Schindler, #33997

Date

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volume 1 and 2, and Engineering Criteria Manual, As Amended.

Date

County Engineer/ECM Administrator

Conditions:

Date

Date

1.0 LOCATION and DESCRIPTION

Village at Lorson Ranch is located west of Jimmy Camp Creek. The site is located on approximately 9.722 acres of vacant land. This project will develop this site into a commercial development. The land for the commercial lots is currently owned by Cradlan, LLC.

The site is located in the Southeast 1/4 of Section 15, Township 15 South and Range 65 West of the 6th Principal Meridian. The site is bounded on the north by Carriage Meadows North Filing No. 1, on the west by Marksheffel Road, on the east by Carriage Meadows Drive, and the south by Fontaine Boulevard. For reference, a vicinity map is included in Appendix A of this report.

Conformance with applicable Drainage Basin Planning Studies

There is an existing (unapproved) DBPS for Jimmy Camp Creek prepared by Wilson & Company in 1987, and is referenced in this report. The only major drainage improvements for this study area according to the 1987 Wilson study was the reconstruction of the main stem of Jimmy Camp Creek. In 2006 the main stem of Jimmy Camp Creek was reconstructed in accordance with the 1987 study. There are no further improvements to be made on Jimmy Camp Creek.

<u>Conformance with Lorson Ranch MDDP1 by Pentacor Engineering (approved November 7, 2006) and</u> <u>Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 (approved September</u> 7, 2017)

Core Engineering Group has an approved MDDP for Lorson Ranch, which covers this study area for major infrastructure. The major infrastructure in the MDDP includes storm sewer in Fontaine Boulevard and relocation of the FMIC irrigation ditch which was constructed in 2006 conforming to the MDDP for Lorson Ranch. Other major infrastructure improvements constructed to serve this site include Pond G1/G2 constructed as part of Carriage Meadows South at Lorson Ranch Filing No. 1. Pond G1/G2 is an offsite full spectrum detention pond constructed in 2017 and included detention and water quality provisions that serve Village at Lorson Ranch.

The Village at Lorson Ranch is located within the *"Jimmy Camp Creek Drainage Basin"*, which is a fee basin in El Paso County. Jimmy Camp Drainage Basin has recently been updated to be a closed basin within Lorson Ranch which is further discussed in the drainage fee section of this report.

2.0 DRAINAGE CRITERIA

The supporting drainage design and calculations were performed in accordance with the City of Colorado Springs and El Paso County "Drainage Criteria Manual (DCM)", dated November, 1991, the El Paso County "Engineering Criteria Manual", Chapter 6 and Section 3.2.1 Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014, and the UDFCD "Urban Storm Drainage Criteria Manual" Volumes 1, 2 and 3 for inlet sizing and full spectrum ponds. No deviations from these published criteria are requested for this site.

The Rational Method as outlined in Section 6.3.0 of the May 2014 "Drainage Criteria Manual" and in Section 3.2.8.F of the El Paso County "Engineering Criteria Manual" was used for basins less than 130 acres to determine the rainfall and runoff conditions for the proposed development of the site. The runoff rates for the 5-year initial storm and 100-year major design storm were calculated.

Current updates to the Drainage Criteria manual for El Paso County states the if detention is necessary, Full Spectrum Detention will be included in the design, based on this criteria, Full Spectrum Detention will not be required for this development.

3.0 EXISTING HYDROLOGICAL CONDITIONS

This site is currently undeveloped with native vegetation (grass with no shrubs) and gentle slopes in a southerly direction to the north side of Fontaine Boulevard.

The Soil Conservation Service (SCS) classifies the soils within the Village at Lorson Ranch property as Manzanst clay loam and Ellicot loamy coarse sand. The clay loam is considered to be hydrologic soil group C and the sandy loams are considered hydrologic soil group A (see table 3.1 below). The clay loams are difficult to vegetate and comprise of the majority of the study area. These soils can be mitigated easily by limiting their use as topsoil since they this is a commercial site and most areas will be paved or landscaped with rock bedding.

Soil No.	Soil	Hydro. Group	Shrink/Swell Potential	Permeability	Surface Runoff Potential	Erosion Hazard
28	Ellicott Loamy Coarse Sand (0.8%)	А	Low	Moderate	Medium	Moderate
52	Manzanst Clay Loam (2.2%)	С	High	Slow	Medium	Moderate

Table 3.1: SCS Soils Survey for the Study Area

Excerpts from the SCS "Soil Survey of El Paso County Area, Colorado" are provided in **Appendix A** for further reference.

For the purpose of preparing hydrologic calculations for this report, the soils of each basin are assumed to be wholly comprised of the majority soil hydrologic group.

This site is not located within the delineated 100-year floodplain of the East Tributary of Jimmy Camp Creek per the Federal Emergency Management Agency (FEMA) Flood Rate Insurance Map (FIRM) number 08041C10957 G, effective December 7, 2018.

Basin EX1

This existing basin consists primarily of flows from the existing FMIC channel, a majority of these flows are from the offsite area west of the channel. Runoff from basin EX1 flows to the existing FMIC channel, then continues west toward Carriage Meadows Drive. The existing runoff from this 0.95 acre basin is 0.3cfs and 1.6cfs for the 5-year and 100-year events. No other runoff is directed to this basin.

The FMIC historically consisted of an open channel from Cottonwood Meadows to Jimmy Camp Creek (culvert under Marksheffel). Upon development of Lorson Ranch in 2007, a 48" pipe was installed from Cottonwood Meadows west and under Marksheffel Road. The 48" pipe carries FMIC water (50cfs) and stormwater to the east side of Marksheffel Road where a reconstructed open channel directs water east to Carriage Meadows Drive. In addition, this open channel section is designed to handle runoff from the full buildout of Marksheffel Road which is carried in a 30" RCP under Marksheffel Road. The 30" RCP is located directly north of the 48" FMIC pipe. Stormwater and FMIC water (113cfs & 214cfs in 5/100 year storm) travels east to Carriage Meadows Drive where a diversion structure and a box culvert effectively separate stormwater from FMIC water. The diversion structure is a 25' D-10-R inlet with a 1.5' opening and the box culvert is a 3x4 culvert with a gate to regulate or shut off flow. During times of FMIC operation, the gate is adjusted so that only the FMIC water is allowed to pass east in the FMIC channel. Additional runoff at this gate will pond up and flow into the 25' diversion structure. During times the FMIC is not operating, the gate is closed which forces all runoff into the 25' diversion structure. The outlet structure is drained by a 48" RCP that flows east under Carriage Meadows Drive. A 60" RCP at 0.95% slope continues east and outlets directly into Jimmy Camp Creek with a capacity of 270cfs. Just north of the 60" RCP, a 36" stub has been constructed to accept flows from a WQ basin in the Carriage

Meadows residential areas. This entire system is in place and has been fully operational since August, 2006.

Basin EX2

This existing basin consists of on-site undeveloped basin located approximately 100' east of Marksheffel Road, south of and adjacent to the existing FMIC channel, and north of Fontaine Boulevard. This basin has moderate slopes and flows overland south downstream to Fontaine Boulevard, then to an existing 34"x53" HERCP storm sewer that routes runoff southerly under Fontaine Boulevard. The total pre-developed flow from this 8.44 acre basin is 3.4cfs and 19.0cfs in the 5 and 100-year storm events.

Basin EX3

Basin EX3 is a self-contained basin and does not accept any offsite flows. Surface flows are FROM Marksheffel Road and are directed to an existing drainage swale that flows in a southerly-southwesterly direction to an existing 18" RCP, these flows are then routed within this existing 18" RCP to the aforementioned existing 34"x53" HERCP that flows southerly under Fountain Boulevard. The existing runoff from this 0.73 acre site is 0.4cfs and 2.4cfs for the 5-year and 100-year events.

Basin EX4

Basin EX4 consists of the west half of Carriage Meadows Drive, a developed north-south road. Flow is directed westerly to the existing curb and gutter, then continues southerly to an existing 5' Type "R" inlet. This inlet is located on west side of Carriage Meadows Drive, at the northwest corner of Fountaine Boulevard and Carriage Meadows Drive. Flow is routed westerly from this inlet to the aforementioned 34"x53" HERCP via an existing 30" RCP. The existing runoff from this 0.57 acre site is 2.6cfs and 4.7cfs for the 5-year and 100-year events.

4.0 DEVELOPED HYDROLOGICAL CONDITIONS

Hydrology for **Village at Lorson Ranch** drainage report was based on the City of Colorado Springs/El Paso County Drainage Criteria. Sub-basins that lie within this project were determined and the 5-year and 100-year peak discharges for the developed conditions have been presented in this report. Based on these flows, storm inlets will be added when the street capacity is exceeded.

Soil types A/B & C/D have been assumed for the developed hydrologic conditions. See Appendix A for SCS Soils Map.

The time of concentration for each basin and sub-basin was developed using an overland, ditch, street and pipe flow components. The maximum overland flow length for developed conditions was limited to 100 feet. Travel time velocities ranged from 2 to 6 feet per second. The travel time calculations are included in the back of this report.

Runoff coefficients for the various land uses were obtained from Table 6-6 dated May 2014 from the updated City of Colorado Springs/El Paso County Drainage Criteria Manual. See Appendix B.

Drainage for the site was divided into 8 proposed basins and 3 existing basins. Runoff coefficients for the 5/100-year events are 0.83 and 0.90 respectively. This is a commercial site, and most areas will be paved or landscaped with rock bedding. Analysis for each of the basins are briefly discussed as follows:

Basins EX1, EX3 & EX4

These offsite basins have been discussed in the existing Hydrological Conditions portion of this report, any additional discussion is not required.

<u>Basin PR1</u>

This basin consists of a commercial area, surface runoff will be directed to a future 10' Type "R" inlet in a sump condition at the southwest corner of this basin. Runoff from this inlet, (design point #7) will be conveyed westerly via proposed 18" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 1.24 acre basin is 5.3cfs for the 5-year storm event and 9.7cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR2

This basin consists of a commercial area, surface runoff will be directed to a proposed 20' Type "R" inlet in a sump condition at the south-center part of this basin. Runoff from this inlet, (design point #1) will be conveyed southerly by a proposed 24" RCP, then easterly via proposed 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 2.41 acre basin is 9.4cfs for the 5-year storm event and 17.0cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR3

This basin consists of a commercial area and street, surface runoff will be directed to a proposed 5' Type "R" inlet in a sump condition at the south-center portion of this basin. Runoff from this inlet, (design point #1a) will be conveyed southerly by a proposed 24" RCP, then easterly via proposed 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 0.11 acre basin is 0.5cfs for the 5-year storm event and 0.9cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR4

This basin consists of a commercial area, surface runoff will be directed to a proposed continuous ongrade 10' Type "R" inlet at the southeast corner of this basin. Runoff from this inlet, (design point #4) will be conveyed easterly via proposed 24" and 36" RCP to the previously mentioned existing 34"x53" HERCP. Developed flow from this 1.68 acre basin is 7.2cfs for the 5-year storm event and 13.1cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR5

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed southerly, then easterly to a proposed 5' Type "R" inlet in a sump condition at the southeast corner of this basin. Runoff from this inlet, (design point #5) is routed by a proposed 24" RCP to the previously discussed proposed 36" RCP then continues easterly to the previously mentioned existing 34"x53" HERCP. Developed flow from this 0.39 acre basin is 1.7cfs for the 5-year storm event and 3.0cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR6

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed easterly and southerly to a proposed 10' Type "R" inlet in a sump condition at the southeast corner of this basin. Runoff from this inlet, (design point #3) is routed southeasterly by a proposed 24" RCP to the previously discussed proposed 36" RCP then continues easterly to the existing 34"x53" HERCP. Developed flow from this 0.72 acre basin is 3.1cfs for the 5-year storm event and 5.6cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR7

This basin consists of a fast-food type of commercial area, surface runoff from this basin is directed southerly to a future 10' Type "R" inlet in a sump condition at the south-center portion of this basin. Runoff from this inlet, (design point #8a) is routed by proposed 24" RCP's southwesterly and westerly to the existing 34"x53" HERCP. Developed flow from this 1.41 acre basin is 6.0cfs for the 5-year storm event and 11.0cfs for the 100-year storm event. See the appendix for detailed calculations.

Basin PR8

This basin consists of parking for a fast-food type of commercial area, surface flow from this basin is directed northerly to a proposed 5' Type "R" inlet in a sump condition at the north-center portion of this basin. Runoff from this inlet, (design point #8) is routed westerly by proposed 24" RCP to the existing 34"x53" HERCP. Developed flow from this 0.22 acre basin is 0.9cfs for the 5-year storm event and 1.7cfs for the 100-year storm event. See the appendix for detailed calculations.

See the Developed Conditions Hydrology Calculations in the back of this report and the Developed Conditions Drainage Map (Map Pocket) for the 5-year and 100-year storm event amounts.

5.0 HYDRAULIC SUMMARY

The sizing of the hydraulic structures was prepared by using the *StormSewers* software programs developed by Intellisolve, which conforms to the methods outlined in the "City of Colorado Springs/El Paso County Drainage Criteria Manual". Street capacities and Inlets were sized by Denver Urban Drainage's xcel spreadsheet UD-Inlet.

It is the intent of this drainage report to use the proposed parking area curb/gutter and storm sewer to convey runoff to an existing storm sewer system, then to the existing detention and water quality pond, this pond has been adequately sized to accept the developed flow from this development. Flows will then outlet to the East Tributary of Jimmy Camp Creek. Inlet size and location are shown on the storm sewer layout in the appendix. See the appendix for detailed calculations and the storm sewer model.

	Residen	tial Local	Residential Collector		Principal Arterial	
Street Slope	5-year	100-year	5-year	100-year	5-year	100-year
0.5%	6.3	26.4	9.7	29.3	9.5	28.5
0.6%	6.9	28.9	10.6	32.1	10.4	31.2
0.7%	7.5	31.2	11.5	34.6	11.2	33.7
0.8%	8.0	33.4	12.3	37.0	12.0	36.0
0.9%	8.5	35.4	13.0	39.3	12.7	38.2
1.0%	9.0	37.3	13.7	41.4	13.4	40.2
1.4%	10.5	44.1	16.2	49.0	15.9	47.6
1.8%	12.0	45.4	18.4	50.4	18.0	50.4
2.2%	13.3	42.8	19.4	47.5	19.5	47.5
2.6%	14.4	40.7	18.5	45.1	18.5	45.1
2.7%	14.7	40.6	18.4	45.0	18.4	45.0
3.0%	15.5	39.0	17.7	43.2	17.8	43.2
3.5%	16.7	37.2	16.9	41.3	17.0	41.3
4.0%	17.9	35.7	16.2	39.7	16.3	39.7
4.5%	19.0	34.5	15.7	38.3	15.7	38.3
5.0%	19.9	33.4	15.2	37.1	15.2	37.1

Table 1: Street Capacities (100-year capacity is only $\frac{1}{2}$ of street)

Note: all flows are in cfs (cubic feet per second).

Design Point 1 is located on the north side of Street B and accepts developed flows from Basin PR2. The runoff will be conveyed to Design Point 1 via curb/gutter. The street capacity of Street B (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR2 Upstream flowby:	Inlet/MH Number: Inlet DP1 Total Street Flow: 9.4cfs				
Flow Intercepted: 9.4cfs Inlet Size: 20' type R, sump	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, capa	acity = 8.0cfs, okay half flow from each side				
<u>(100-year storm)</u> Tributary Basins: PR2 Upstream flowby:	Inlet/MH Number: Inlet DP1 Total Street Flow: 17.0cfs				
Flow Intercepted: 17.0cfs Inlet Size: 20' type R, SUMP	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay					

Design Point 1a

Design Point 1a is located on the south side of Street B and accepts developed flows from Basin PR3. The runoff will be conveyed to Design Point 1a via curb/gutter. The street capacity of Street B (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR3 Upstream flowby:	Inlet/MH Number: Inlet DP1a Total Street Flow: 0.5cfs				
Flow Intercepted: 0.5cfs Inlet Size: 5' type R, sump	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, cap	acity = 8.0cfs, okay half flow from each side				
<u>(100-year storm)</u> Tributary Basins: PR3 Upstream flowby:	Inlet/MH Number: Inlet DP1a Total Street Flow: 0.9cfs				
Flow Intercepted: 0.9cfs Inlet Size: 5' type R, SUMP	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay					

Design Point 2

Design Point 2 is located on the south side of Street B and is the total pipe flow from Des. Pts 1 & 1a. The runoff will be conveyed to Design Point 3 via a 24" storm sewer. The total pipe flow is 9.8cfs/17.8cfs in the 5/100-year storm events.

Design Point 3 is located on the north side of an access street and accepts developed flows from Basin PR6. The runoff will be conveyed to Design Point 3 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR6 Upstream flowby:	Inlet/MH Number: Inlet DP3 Total Street Flow: 3.1cfs				
Flow Intercepted: 3.1cfs Inlet Size: 10' type R, sump	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, capa	acity = 8.0cfs, okay				
<u>(100-year storm)</u> Tributary Basins: PR6 Upstream flowby:	Inlet/MH Number: Inlet DP3 Total Street Flow: 5.6cfs				
Flow Intercepted: 5.6cfs Inlet Size: 10' type R, SUMP	Flow Bypassed: 0.0cfs				
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay					

<u>Design Point 3a</u>

Design Point 3a is located on the north side of an access street and is the total pipe flow from Des. Pts 2 & 3. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 12.5cfs/22.8cfs in the 5/100-year storm events.

Design Point 4

Design Point 4 is located on the south side of an access street and accepts developed flows from Basin PR4. The runoff will be conveyed to Design Point 4 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR4 Upstream flowby:	Inlet/MH Number: Inlet DP4 Total Street Flow: 7.2cfs					
Flow Intercepted: 5.9cfs Inlet Size: 10' type R, on-grade	Flow Bypassed: 1.3cfs					
Street Capacity: Street slope = 0.9%, capa	Street Capacity: Street slope = 0.9%, capacity = 8.0cfs, okay					
(100-year storm) Tributary Basins: PR4 Upstream flowby:	Inlet/MH Number: Inlet DP4 Total Street Flow: 13.1cfs					
Flow Intercepted: 8.1cfs Inlet Size: 10' type R, on-grade	Flow Bypassed: 5.0cfs					
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay						

Design Point 5 is located on the south side of an access street and accepts developed flows from Basin PR5. The runoff will be conveyed to Design Point 5 via curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: Upstream flowby:	PR5 1.3cfs from DP4	Inlet/MH Number: Inlet DP5 Total Street Flow: 1.7+1.3=3.0cfs				
Flow Intercepted:3.0cfsFlow Bypassed:0.0cfsInlet Size:5' type R, sump						
Street Capacity: Str	eet slope = 0.9%, cap	acity = 8.0cfs, okay				
<u>(100-year storm)</u> Tributary Basins: Upstream flowby:	PR5 5.0cfs from DP4	Inlet/MH Number: Inlet DP5 Total Street Flow: 5.0+3.0=8.0cfs				
Flow Intercepted:8.0cfsFlow Bypassed:0.0cfsInlet Size:5' type R, sump						
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay						

<u>Design Point 5a</u>

Design Point 5a is located on the south side of an access street and is the total pipe flow from Des. Pts 4 & 5. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 8.9cfs/16.1cfs in the 5/100-year storm events.

Design Point 6

Design Point 6 is located on the south side of an access street and is the total pipe flow from Des. Pts 3a & 5a. The runoff will be conveyed to Design Point 6 via a 24" storm sewer. The total pipe flow is 20.5cfs/37.3cfs in the 5/100-year storm events.

Design Point 7 is located on the east end of an access street and accepts developed flows from Basin PR1 which will be developed in the future. The runoff will be conveyed to Design Point 7 via future curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded. A future inlet will be constructed at this design point when the adjacent lot is developed.

<u>(5-year storm)</u> Tributary Basins: PR1 Upstream flowby:	Inlet/MH Number: future Inlet DP7 Total Street Flow: 5.3cfs			
Flow Intercepted: 5.3cfs Inlet Size: future 10' type R, sump	Flow Bypassed: 0.0cfs			
Street Capacity: Street slope = 0.9%, capa	acity = 8.0cfs, okay			
(100-year storm) Tributary Basins: PR1 Upstream flowby:	Inlet/MH Number: future Inlet DP7 Total Street Flow: 9.7cfs			
Flow Intercepted: 9.7cfs Inlet Size: future 10' type R, SUMP	Flow Bypassed: 0.0cfs			
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay				

Design Point 8

Design Point 8 is located on the east end of an access street and accepts developed flows from Basin PR8 which will be developed in the future. The runoff will be conveyed to Design Point 8 via future curb/gutter. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded.

<u>(5-year storm)</u> Tributary Basins: PR8 Upstream flowby:	Inlet/MH Number: Inlet DP8 Total Street Flow: 0.9cfs					
Flow Intercepted: 0.9cfs Inlet Size: 5' type R, sump	Flow Bypassed: 0.0cfs					
Street Capacity: Street slope = 0.9%, capa	Street Capacity: Street slope = 0.9%, capacity = 8.0cfs, okay					
<u>(100-year storm)</u> Tributary Basins: PR8 Upstream flowby:	Inlet/MH Number: Inlet DP8 Total Street Flow: 1.7cfs					
Flow Intercepted: 1.7cfs Inlet Size: 5' type R, SUMP	Flow Bypassed: 0.0cfs					
Street Capacity: Street slope = 0.9%, capacity = 35.4cfs (half street) is okay						

<u>Design Point 8a</u>

Design Point 8a is located on the east end of an access street and accepts developed flows from Basin PR7 which will be developed in the future. The runoff will be conveyed to Design Point 8a via future curb/gutter. The total surface flow is 6.0cfs/11.0cfs in the 5/100-year storm events. The street capacity of the access street (Res. Local, 8.5/35.4cfs at 0.9% slope) is not exceeded. A future inlet will be constructed at this design point when the adjacent lot is developed.

Design Point 9

Design Point 9 is located on the south side of an access street and is the total pipe flow from Des. Pts 7, 8 & 8a. The runoff will be conveyed to Design Point 10 via a 24" storm sewer. The total pipe flow is 12.2cfs/22.4cfs in the 5/100-year storm events.

Design Point 10

Design Point 10 is located on the south side of an access street and is the total pipe flow from Des. Pts 6 & 9. The runoff will be conveyed to an existing 34"x53" HERCP. The total pipe flow is 31.5cfs/57.3cfs in the 5/100-year storm events. The allowable flow into the existing HERCP is 32.2cfs/59.0cfs per the Carriage Meadows North FDR and the Fontaine Blvd. Phase 1 FDR.

6.0 DETENTION AND WATER QUALITY PONDS

Detention and Storm Water Quality for Village at Lorson Ranch will be provided for in existing Pond G1/G2 located south of Fontaine Boulevard. Pond G1/G2 is an existing full spectrum detention pond constructed in 2017 as part of the Carriage Meadows South at Lorson Ranch Filing No. 1 subdivision (SF 1711) per El Paso County criteria. Pond G1/G2 was as-builted and certified on June 27, 2023 by Core Engineering Group. A copy of the certification letter, as-builts, and a pond drainage area map are located in the appendix of this report.

For additional information, see the approved Final Drainage Report and Plan for "Carriage Meadows South at Lorson Ranch Filing No. 1, SF 1711, dated 08/10/2017.

The following text was taken from the Carriage Meadows South final drainage report:

Detention Pond G1/G2 (Full Spectrum Design), (District Facility, SF1711)

This is an on-site permanent full spectrum detention pond that includes water quality. Pond G1/G2 is designed as a single pond in the UDCF Full Spectrum spreadsheets. The full spectrum print outs are in the appendix of this report. See map in appendix for watershed areas. This pond is sized to provide full spectrum and water quality for the Brownsville Subdivision No. 2 should it become a part of Lorson Ranch.

- Watershed Ares: 96 acres
- Watershed Imperviousness: 79%
- Hydrologic Soils Group A, B, C/D
- Zone 1 WQCV: 2.301 ac-ft, WSEL: 5683.93
- Zone 2 EURV: 8.104 ac-ft, WSEL: 5686.29
- Zone 3 (100-yr): 12.881ac-ft, WSEL: 5687.93
- Pipe Outlet: 36" RCP at 0.4%
- 5-yr outflow = 4.2cfs, 100-yr outflow = 55.6cfs

7.0 DRAINAGE AND BRIDGE FEES

Village at Lorson Ranch is located within the Jimmy Camp Creek drainage basin which is currently a fee basin in El Paso County. Current El Paso County regulations require drainage and bridge fees to be paid for platting of land as part of the plat recordation process. Lorson Ranch initiated the closure of Jimmy Camp Creek drainage basin for drainage/bridge fees a few years ago and was recently approved by El Paso County and the Pikes Peak Drainage Board. Therefore, no drainage fees or bridge fees are required to be paid at this time. A copy of the drainage board meeting minutes is in the appendix of this report.

Item	Quantity	Unit	Unit Cost	Item Total
5' Inlet	3	EA	\$5,000/EA	\$15,000
10' Inlet	4	EA	\$8,000/EA	\$32,000
20' Inlet	1	EA	\$12,000/EA	\$12,000
18" Storm	206	LF	\$180	\$37,080
24" Storm	351	LF	\$240	\$84,240
36" Storm	73	LF	\$360	\$26,280
Manholes	2	EA	\$10,000	\$20,000
			Subtotal	\$226,600
			Eng/Cont (10%)	\$22,660
			Total Est. Cost	\$249,260

 Table 7.1: Private Drainage Facility Costs (non-reimbursable)

8.0 FOUR STEP PROCESS

The site has been developed to minimize wherever possible the rate of developed runoff that will leave the site and to provide water quality management for the runoff produced by the site as proposed on the development plan. The following four step process should be considered and incorporated into the storm water collection system and storage facilities where applicable.

Step 1: Employ Runoff Reduction Practices

Village at Lorson Ranch has employed several methods of reducing runoff.

- The street configuration was laid out to minimize the length of streets. Many streets are straight and perpendicular resulting in lots with less wasted space. Landscape buffers are provided for adjacent residential development
- Construct one Full Spectrum Detention Outlet Structure (Pond G1/G2). The full spectrum detention mimics existing storm discharges and includes water quality.

Step 2: Stabilize Drainageways

Jimmy Camp Creek is a major drainageway located east of this site. In 2006 Jimmy Camp Creek was reconstructed and stabilized per county criteria. The design included a natural sand bottom and armored sides.

Step 3: Provide Water Quality Capture Volume

Treatment of the water quality capture volume (WQCV) is required for all new developments. Village at Lorson Ranch utilizes an existing full spectrum stormwater extended detention basin outlet structure within existing Pond G1/G2 which include Water Quality Volumes and WQ outlet structures.

Step 4: Consider Need for Industrial and Commercial BMP's

There are no industrial areas within this site. This site is commercial but will be mostly light use commercial areas such as restaurants, gas station, mini storage, etc which does not need specific BMP's.

9.0 CONCLUSIONS

This drainage report has been prepared in accordance with the City of Colorado Springs/El Paso County Drainage Criteria Manual. The proposed development and drainage infrastructure will not cause adverse impacts to adjacent properties or properties located downstream. Several key aspects of the development discussed above are summarized as follows:

- Developed runoff will be conveyed via curb/gutter and storm sewer facilities
- Jimmy Camp Creek has been reconstructed east of this study area
- Detention and water quality for this site will be provided.

10.0 REFERENCES

- 1. City of Colorado Springs/El Paso County Drainage Criteria Manual DCM, dated November, 1991
- 2. Soil Survey of El Paso County Area, Colorado by USDA, SCS
- 3. Jimmy Camp Creek Drainage Basin Planning Study, Dated March 9, 2015, by Kiowa Engineering Corporation
- 4. City of Colorado Springs "Drainage Criteria Manual, Volume 2
- 5. El Paso County "Engineering Criteria Manual"
- 6. Lorson Ranch MDDP 1, November 7, 2006 by Pentacor.
- 7. El Paso County Resolution #15-042, El Paso County adoption of Chapter 6 and Section 3.2.1 of the City of Colorado Springs Drainage Criteria Manual dated May, 2014.
- 8. Final Drainage Report for Fontaine Boulevard Phase 1 Improvements prepared by Pentacor, dated November, 2006
- 9. Final Drainage Report for Carriage Meadows South at Lorson Ranch Filing No. 1 prepared by Core Engineering Group, Reference SF1711, approved September 7, 2017
- 10. Final Drainage Report for Carriage Meadows North prepared by Core Engineering Group, Reference SF1723, approved April 12, 2018

APPENDIX A – VICINTIY MAP, SOILS MAP, FEMA MAP



National Flood Hazard Layer FIRMette



Legend



Basemap Imagery Source: USGS National Map 2023



Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

El Paso County Area, Colorado

28—Ellicott loamy coarse sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 3680 Elevation: 5,500 to 6,500 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 47 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Ellicott and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ellicott

Setting

Landform: Stream terraces, flood plains Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium

Typical profile

A - 0 to 4 inches: loamy coarse sand C - 4 to 60 inches: stratified coarse sand to sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: NoneFrequent
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A Ecological site: R069XY031CO - Sandy Bottomland Other vegetative classification: SANDY BOTTOMLAND (069AY031CO) Hydric soil rating: No

USDA

Minor Components

Fluvaquentic haplaquoll

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

Other soils

Percent of map unit: 1 percent Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022



El Paso County Area, Colorado

52—Manzanst clay loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2w4nr Elevation: 4,060 to 6,660 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 50 to 54 degrees F Frost-free period: 130 to 170 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Manzanst and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Manzanst

Setting

Landform: Drainageways, terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave, linear Parent material: Clayey alluvium derived from shale

Typical profile

A - 0 to 3 inches: clay loam Bt - 3 to 12 inches: clay Btk - 12 to 37 inches: clay Bk1 - 37 to 52 inches: clay Bk2 - 52 to 79 inches: clay

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Gypsum, maximum content: 3 percent
Maximum salinity: Slightly saline (4.0 to 7.0 mmhos/cm)
Sodium adsorption ratio, maximum: 10.0
Available water supply, 0 to 60 inches: High (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4c

USDA

Hydrologic Soil Group: C *Ecological site:* R067BY037CO - Saline Overflow *Hydric soil rating:* No

Minor Components

Ritoazul

Percent of map unit: 7 percent Landform: Interfluves, drainageways Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY042CO - Clayey Plains Hydric soil rating: No

Arvada

Percent of map unit: 6 percent Landform: Interfluves, drainageways Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY033CO - Salt Flat Hydric soil rating: No

Wiley

Percent of map unit: 2 percent Landform: Interfluves Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY002CO - Loamy Plains Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022





Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	0.1	1.2%
52	Manzanst clay loam, 0 to 3 percent slopes	8.5	98.8%
Totals for Area of Interest		8.6	100.0%



CORE
ENGINEERING GROUP

Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

			UP	Calcula Date: A Checke	ated By: April <u>, 20</u> ed By: <u>L</u> ect Run	: <u>Leonar</u> 24 eonard	d Beasl Beasley	<u>ey</u> <u>/</u>	1	Total	Runoff		Job No Project Design	o: <u>100.0</u> t: Village <u>i Storm:</u> reet	70 e at Lors <u>5 - Yea</u>	on Ran <u>r Event</u> Pipe	nch FDF t (Curre	ং • <u>nt)</u> । ⊤	ravel Tir	ne	
Street or Basin	Jesign Point	ea Design	Area (A)	Runoff Coeff. (C)	tc t	CA		Ø	tc	Σ (CA)	. <u> </u>	a	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length .	Velocity	tt	Remarks
		Ā	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX1			0.95	0.15	40.3	0.14	2.04	0.3													
EX2			8.44	0.15	26.4	1.27	2.68	3.4													
EX3			0.73	0.15	11.1	0.11	3.98	0.4													
EX4			0.57	0.90	5.0	0.51	5.17	2.6													
													-								
													-								
													-								
													-								
													-								
													-								
1		1	1	1	1		1	1	1		1	1					1	1	1		



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

ENG	INEERIN	IG GROL	JP	Calcula	ated By:	Leonar	d Beasle	<u>ey</u>					Job No	o: 100.0)70						
				Date: A	pril <u>, 20</u>	24		-					Projec	t: Villag	e at Lo	rson Ra	anch FI	DR			
				Checke	ed By: <u>L</u> ect Run	<u>eonard</u>	Beasley	<u> </u>		Total R	unoff		Desigr Sti	<u>n Storm</u> reet	: <u>100-Y</u>	Pipe	ent (Cu	u rrent) ⊤r	avel Tir	ne	
Street or Basin	Design Point	ea Design	Area (A)	Runoff Coeff. (C)	tc	CA		Ø	tc	Σ (CA)		Ø	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	tt	Remarks
		Ar	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX1			0.95	0.50	40.3	0.48	3.42	1.6													
EX2			8.44	0.50	26.4	4.22	4.49	19.0													
EX3			0.73	0.50	11.1	0.37	6.68	2.4													
EX4			0.57	0.96	5.0	0.55	8.68	4.7													
														I							

	ORE GINEERIN	G GROUP					PROJECT N PROJECT N ENGINEER: DATE: April	AME: Village at J MBER: 100.07 LAB 2024	Lorson Ranch '0	FDR		
	Burnsville,	MN 55306	nage Plan				 , ryon,					
	CURRENT	CONDITION	NS COEFFICIE	NT "C" CALCUI	ATIONS	1	1		I	1	1	1
BASIN	Soil No.	Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Impervious	Type of Cover
EX1	52	С	0.95	100.00%	0.15		0.50		51		0%	Pasture/Meadow
EX2	52	С	8.44	100.00%	0.15		0.50		51		0%	Pasture/Meadow
EX3	52	С	0.76	100.00%	0.15		0.50		51		0%	Pasture/Meadow
EX4	52	С	0.66	100.00%	0.90		0.96		51		100%	Paved Road
J		1	1			1	1	1		1	1	

10 15

Œ			IG GROL	IP	Standard F Calculated Date: Feb. Checked B	F orm SF-1. By: <u>Leonar</u> <u>15, 2024</u> y: <u>Leonard</u>	Time of Co d Beasley Beasley	oncentration	<u>-Current</u>	Job No: <u>100.</u> Project: <u>Villa</u>	. <u>070</u> ge at Lorson	Ranch FDR	
	Sub-Ba	asin Data		li	nitial Overla	nd Time (t i)		-	Fravel Time (t	it)		Final t _c
BASIN or DESIGN	C₅	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	τi minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	Т t minutes	Computed tC Minutes	USDCM Recommended tc=ti+tt (min)
EX1	0.15	0.95	15.0	51.00	10.78%	0.15	5.59	1398.00	0.20%	0.67	34.73	40.32	40.32
EX2	0.15	8.44	7.0	226.00	3.10%	0.21	17.81	229.00	1.31%	0.80	4.76		
			15.0					284.00	0.70%	1.25	3.77	26.35	26.35
													-
EX3	0.15	0.73	15.0	37.00	4.05%	0.09	6.58	442.00	1.20%	1.64	4.48	11.06	11.06
EX4	0.90	0.66	20.0	22.00	2.00%	0.27	1.35	462.00	1.75%	2.65	2.91	4.26	4.26
													-
													-
													-

г

					<u>Standa</u>	ard For	<u>m SF-2.</u>	Storm	Draina	ge Syst	em Des	sign (Ra	ational	Method	Proce	<u>dure)</u>					
	INEERI	NG GRO	UP	Calcula	ated Bv	Leonar	rd Beasl	ev					Job No	• 100 0 [°]	70						
				Date: A	April <u>, 20</u>	<u>24</u>	<u>u Douoi</u>	<u>oy</u>					Project	t: Village	e at Lor	son Rar	nch FDF	R			
				Checke	ed By: <u>L</u>	eonard	Beasley	4					Design	Storm:	<u>5 - Yea</u>	r Even	t (Devel	oped)			
	It			Dire	ect Run	off				Total I	Runoff			Str	reet			1	Pipe		
Street or Basin	Design Poir	rea Design	Area (A)	Runoff Coeff. (C)	tc	CA		Ø	ţc	Σ (CA)		σ	Slope / Pipe Slope	Full Street Max Flow	Max Allow street flow	Street Velocity	Design Pipe Flow	Slope	Pipe Size	Min Pipe Flow	Pipe Velocity
		Ā	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	min	cfs	%	in	cfs	fps
EX1			0.95	0.15	40.3	0.14	2.04	0.3													
EX3			0.73	0.15	11.1	0.11	3.98	0.4													
EX4			0.57	0.90	5.0	0.51	5.17	2.6													
PR1	7		1.24	0.83	5.0	1.03	5.17	5.3													
PR2	1		2.41	0.83	6.9	2.00	4.68	9.4													
PR3	1a		0.11	0.83	5.0	0.09	5.17	0.5													
(PR2-PR3)	2	2.52		0.83					6.9	2.09	4.68	9.8									
PR4	4		1.68	0.83	5.0	1.39	5.17	7.2													
PR5			0.39	0.83	5.0	0.32	5.17	1.7													
(PR4-PR5)	5a	2.07		0.83					5.0	1.72	5.17	8.9									
PR6 (PR2,PR3&PR6)	3a		0.72	0.83	5.0	0.60	5.17	3.1	7.0	2.69	4.66	12.5									
(PR2-PR6)	6	5.31		0.83					7.1	4.41	4.65	20.5									
PR7	8a		1.41	0.83	5.0	1.17	5.17	6.0													
PR8	8		0.22	0.83	5.0	0.18	5.17	0.9													
(PR1,PR7&PR8)	9	2.87							5.1	2.38	5.14	12.2									
(PR1-PR8)	10	8.18							7.1	6.79	4.64	31.5								+	
																				+	

	DE				<u>Standa</u>	ard For	<u>m SF-2</u>	. Storm	Draina	<u>ge Syst</u>	em Des	sign (Ra	tional I	Method	Proced	<u>dure)</u>					
			JP	Calcul	ated By:		d Roas	امر					Job No	· 100 0	70						
				Date: A	April 20	24	u Deas						Project	t: Villag	<u>atlor</u>	son Rar	hch EDE	? Desia	n		
				Check	ed Bv: L	eonard	Beasle	v					Storm:	100 - Y	ear Eve	ent (De	veloped	(200ig 1)			
	<u> </u>			Dir	ect Run	off		1		Total	Runoff			St	reet			- /	Pipe		
Street or Basin)esign Poin	ea Design	Area (A)	Runoff Coeff. (C)	ţc	CA		a	tc	Σ (CA)		Ø	Slope / Pipe Slope	Full Street Max Flow	Max Allow street flow	Street Velocity	Design Pipe Flow	Slope	Pipe Size	Min Pipe Flow	Pipe Velocity
		Ar	ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	min	cfs	%	ft	cfs	fps
EX1			0.95	0.50	40.3	0.48	3.42	1.6													
EX3			0.73	0.50	11 1	0.37	6 68	24													
			0.70	0.00	5.0	0.07	0.00	4.7													
EX4			0.57	0.96	5.0	0.55	8.08	4.7													
PR1	7		1.24	0.90	5.0	1.12	8.68	9.7													
PR2	1		2.41	0.90	6.9	2.17	7.85	17.0													
PR3	1a		0.11	0.90	5.0	0.10	8.68	0.9													
(PR2-PR3)	2	2.52		0.90					7.0	2.27	7.83	17.8									
PR4	4		1.68	0.90	5.0	1.51	8.68	13.1													
PR 5			0.39	0.90	5.0	0.35	8 68	3.0													-
	5.	0.07	0.00	0.00	0.0	0.00	0.00	0.0	5.0	4.00	0.00	10.1									
(PR4-PR5)	5a	2.07		0.90					5.0	1.86	8.66	16.1									
(PR2,PR3&PR6)	3a		0.72	0.90	5.0	0.65	8.68	5.6	7.0	2.92	7.83	22.8	-				-				
(PR2-PR6)	6	5.31		0.90					7.1	4.78	7.81	37.3									
PR7	8a		1.41	0.90	5.0	1.27	8.68	11.0													
PR8	8		0.22	0.90	5.0	0.20	8.68	1.7													
(PR1,PR7&PR8)	9	2.87							5.0	2.58	8.68	22.4									
(PR1-PR8)	10	8 18	8 18	0.90	71	7 36	7 79	57.3	71	7 36	7 79	57.3									
(0.10		0.00															<u> </u>		
																			<u> </u>		<u> </u>
																			<u> </u>		<u> </u>

Œ		DRE			<u>Standarc</u>	l Form SF	-1. Time (of Concen	tration-Pr	roposed					
	ENG	INEER	ING GR	OUP	Calculate Date: <u>Apr</u> Checked	ed By: <u>Leor</u> ril, 2024 By: <u>Leona</u>	nard Beas rd Beasle	<u>ley</u> Y			Job No: <u>1</u> Project: <u>V</u>	<u>00.070</u> ′illage at Lo	rson Ranch		
	Sub-Ba	sin Data		In	itial Overla	and Time (ti)		Tr	avel Time ((tt)		tc Check	(urbanized	Final tc
BASIN or DESIGN	C ₅	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	T i minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	T t minutes	Computed tC Minutes	TOTAL LENGTH (L) feet	Regional tc tc=(L/180)+10 minutes	USDCM Recommended Tc=Tı+Tt (mın)
EX1	0.15	0.95	15.0	51.00	10.78%	0.15	5.59	1398.00	0.20%	0.67	34.73	40.32			40.32
EX3	0.15	0.73	15.0	37.00	4.05%	0.09	6.58	442.00	1.20%	1.64	4.48	11.06			11.06
EX4	0.90	0.66	20.0	22.00	2.00%	0.27	1.35	462.00	1.75%	2.65	2.91	4.26			4.26
PR1	0.90	1.24	20.0	15.00	2.00%	0.22	1.12	410.00	1.22%	2.21	3.09	4.21	425.00	12.36	4.21
PR2	0.90	2.41	7.0	36.00	2.00%	0.35	1.73	114.00	1.00%	0.70	2.71				
			20.0					300.00	1.00%	2.00	2.50	6.94	450.00	12.50	6.94
PR3	0.90	0.11	20.0	22.00	2.00%	0.27	1.35	128.00	1.00%	2.00	1.07	2.42	150.00	10.83	2.42
PR4	0.90	1.68	20.0	10.00	2.00%	0.18	0.91	597.00	1.60%	2.53	3.93	4.85	607.00	13.37	4.85
PR5	0.90	0.39	20.0	10.00	1.96%	0.18	0.92	353.00	1.60%	2.53	2.33	3.24	363.00	12.02	3.24
PR6	0.90	0.72	20.0	10.00	2.00%	0.18	0.91	368.00	1.34%	2.32	2.65	3.56	378.00	12.10	3.56
PR7	0.90	1.41	20.0	15.00	2.20%	0.23	1.08	320.00	1.56%	2.50	2.14	3.22	335.00	11.86	3.22
PR8	0.90	0.22	20.0	25.00	2.00%	0.29	1.44	108.00	1.56%	2.50	0.72	2.16	133.00	10.74	2.16



INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	6.9	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) =$	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
	_			_
Low Head Performance Reduction (Calculated)	-	MINOR	MAJOR	_
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.41	ft
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.75	0.84	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	-	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	9.8	18.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	9.4	17.0	cfs






Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	-			-
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.4	4.6	cts
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{\text{PEAK REQUIRED}} =$	0.5	0.9	CTS







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_{w} (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.90	0.91	
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{Combination} =$	N/A	N/A	
		MINOR	MAIOR	
Total Inlet Interception Capacity (assumes clogged condition)	0, =	6.6	6.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	3.1	5.6	cfs



INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	10	10.10	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.9	8.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	1.3	5.0	cfs
Capture Percentage = Q_a/Q_o	C% =	81	61	%







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	7.2	inches
Grate Information		MINOR	MAJOR	 Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.43	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
		MINOD	MAJOR	
Tatal Jalat Intercention Conscilu (accumes alogged condition)	o – I			cfe
I otal Inter Interception Capacity (assumes clogged condition)	Q _a =	4.4	8.0	cfs
WARNING: INIET Capacity < Q Peak for Major Storm	✓ PEAK REQUIRED -	5.0	0.0	CI S







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	6.5	inches
Grate Information		MINOR	MAJOR	 Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_{w} (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information	=	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.38	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{curb} =	0.90	0.96	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{combination} =	N/A	N/A	
		MINOR	MAIOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q ₂ =	6.6	10.2	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	5.3	9.7	cfs







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	5.6	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{o}(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.29	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
_	-			
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.4	4.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	0.9	1.7	cfs





June 27, 2023

El Paso County Planning and Community Development 2880 International Circle, Suite 110 Colorado Springs, CO 80910

RE: Carriage Meadows South Filing No. 1 (SF 17-011) Certification Letter

Dear El Paso County PCD,

Based upon information gathered from as-built surveys and periodic visits to the project, Core Engineering Group is of the opinion that the subdivision improvements have been constructed in general conformance with the approved design plans as filed with El Paso County.

The site and adjacent properties (as affected by work performed under the County permit) appear to be stable with respect to settlement and subsidence, sloughing of cut and fill slopes, revegetation or other ground cover, and the improvements (public improvements, common development improvements, site grading and paving) visually appear to meet or exceed the minimum design requirements. There have been some service line utility trench settlements but that is currently being addressed as part of the punchlist process.

The sanitary and watermain located in the public ROW has also been completed in accordance with Widefield Water and Sanitation Districts criteria.

In addition, Core Engineering Group has verified that the Extended Detention Basin/WQ Pond G1, G2, and G3 have been constructed and certified and meet the volume and elevation requirements and have been constructed in general compliance with the approved construction plans. The outlet structure for Pond G3 did change slightly from the design so the full spectrum spreadsheet was updated for this pond and it meets the design output as shown in the approved final drainage report.

Based on information gathered during construction and post-construction, Core Engineering Group is of the opinion that the public streets and storm sewer have been constructed in general accordance with the approved construction documents.



Pond G1/G2, G3 As-builts Street/storm As-builts

DETENTION BASIN STAGE-STORAGE TABLE BUILDER														
UD-Detention, Version 3.07 (February 2017)														
Project: Basin ID:	Carriage Me Full Spectru	adows Sou Im Pond G3	th at Lorson Rai - asbuilt	nch										
	2 DNE 1	1												
VOLUMET EURY WOCY	14102	100-YE ORIFIC	AR CE	\geq	Depth Increment =	0.1	ft	asblt orifice	=82.94					
POOL Example Zone	Configurat	tion (Rete	ntion Pond)		Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft*2)	Optional Override Area (ft*2)	Area (acre)	Volume (ft*3)	Volume (ac-ft)
Required Volume Calculation Selected BMP Type =	EDB	1			Top of Micropool 5684	-	0.00				50 1.284	0.001	694	0.016
Watershed Area =	6.02	acres			5685	-	2.06				5,841	0.134	4,269	0.098
Watershed Length = Watershed Slope =	790 0.016	ft/ft			5687	-	3.06				8,575	0.197	21,034	0.263
Watershed Imperviousness = Percentage Hydrologic Soil Group A =	55.00% 0.0%	percent percent			5yr=5687.22 100yr=5687.81	-	4.28 4.87			-	10,921 11,948	0.251 0.274	23,395 30,141	0.537 0.692
Percentage Hydrologic Soil Group B = Percentage Hydrologic Soil Groups C/D =	100.0% 0.0%	percent percent			5688 5689	-	5.06 6.06				12,279 14,100	0.282	32,443 45,632	0.745
Desired WQCV Drain Time = Location for 1-hr Rainfall Depths =	40.0 User Input	hours				-			-	-				
Water Quality Capture Volume (WQCV) =	0.111	acre-feet	Optional User	Override		-			-					
2-yr Runoff Volume (P1 = 1.16 in.) =	0.357	acre-feet	1.16 i	nches		-			-	-				
5-yr Runoff Volume (P1 = 1.44 in.) = 10-yr Runoff Volume (P1 = 1.68 in.) =	0.378	acre-feet acre-feet	1.44 i 1.68 i	nches nches		-			-	-				
25-yr Runoff Volume (P1 = 1.92 in.) = 50-yr Runoff Volume (P1 = 2.16 in.) =	0.678	acre-feet acre-feet	1.92 i 2.16 i	nches nches		-				-				
100-yr Runoff Volume (P1 = 2.42 in.) = 500-yr Runoff Volume (P1 = 0 in) =	0.966	acre-feet	2.42 i	nches nches										
Approximate 2-yr Detention Volume =	0.265	acre-feet	L1			-								
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	0.355	acre-feet				-			-	-				
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	0.503	acre-feet acre-feet				-								
Approximate 100-yr Detention Volume =	0.580	acre-feet				-				-				
Stage-Storage Calculation						-			-					
Zone 1 Volume (WQCV) = Zone 2 Volume (EURV - Zone 1) =	0.111 0.246	acre-feet acre-feet				-			-	-				
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	0.223	acre-feet				-								
Initial Surcharge Volume (ISV) =	user	ft^3				-								
Total Available Detention Depth (H _{total}) =	user	ft				-			-	-				
Slope of Trickle Channel (B _{TC}) =	user	ft ft/ft				-			-	-				
Slopes of Main Basin Sides (S _{main}) = Basin Length-to-Width Ratio (R _{LW}) =	user user	H:V				-			-	-				
Initial Surcharge Area (A) =	10.00													
Surcharge Volume Length (L _{ISV}) =	user	ft				-			-	-				
Surcharge Volume Width (W _{ISV}) = Depth of Basin Floor (H _{FLOOR}) =	user	ft ft				-			-	-				
Length of Basin Floor (L _{FLOOR}) = Width of Basin Floor (W _{FLOOR}) =	user	ft ft				-				-				
Area of Basin Floor (A _{FLOOR}) =	user	ft*2				-								
Depth of Main Basin (H _{MAIN}) =	user	ft				-		-	-	-				
Length of Main Basin (L _{MAIN}) = Width of Main Basin (W _{MAIN}) =	user	ft ft				-								
Area of Main Basin (A _{MAIN}) = Volume of Main Basin (V _{MAIN}) =	user	ft*2 ft*3				-								
Calculated Total Basin Volume (V _{total}) =	user	acre-feet				-								
						-			-	-				
						-			-	-				
						-								
						-			-					
						-			-	-				
						-			-	-				
						-			-	-				
						-			-	-				
						-								
						-			-	-				
						-								
						-						_		
						-								
						-								
						-			-					
						-	-						-	





			IABLE						IABLE			
		NORTHING	EASTING	ELEVATION	POND ROTTOM			NORTHING	EASTING	ELEVATION	POND ROTTOM	
	2	20426.91	20580.07	5683.19	POND BOTTOM			20008.20	20084.49	JUOJ.UU	FUND DUTIUM	
	3	20508.55	20484.61	5683.80	POND BOTTOM							
	4	20562.75	20440.18	5684.00	POND BOTTOM							
	5	20556.24	20428.64	5684.00	POND BOTTOM							
	6	20473.78	20380.35	5684.00	POND BOTTOM					5007.55		
							16	20558.92	20432.02	5683.55	INVERT 48″ RCP	
	9	20360.30	20583.01	5683.00	POND BOTTOM							
,										,	, , ,	
							1		/			
							,2 ^{.30}		,			
	RCP	(LATERAL D)	ANS			, SIMC	OE DR.					
	SEE STRE	EIVS				1						
=5691.5	\langle											
										\times		
		\backslash				A						
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~												
× 5691.02												
											$\sim$	
$\langle / / \rangle /$												
146832		.92										
	+563											
- Aster	$\backslash /$	$\langle \times$	3:1 SLOPE	/	$\boldsymbol{\times}$							
	12				5693~							
3) - Se	83:	$\langle X \rangle$	19 ¹	, /								
		$\langle \rangle \rangle \rangle$	+569		FG=5692.3							
- 81											FG=5692.1 —	
682.					Š							
			$\langle \rangle \rangle \rangle$	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>							X	
	CONCRETE RICKLE				- 01.65				FG=36			
	CHANNEL				+563		56 ^{91.19}		01			
			6	5684 5686 5686			+3		+5691.9	- 91.0 ⁴		
468	,2.43		11 0	3.12						+565	S^A	
TX A	X	+ 568	3. ⁵ ' 560								+\$691.	
		,		5683.9	+ 12	±5683	13					
				2	56 ^{83.'}	1		2.26+				
· · · · · · · · · · · · · · · · · · ·				+ 5683.	<i>.</i>		568	1		+)»°		
				ć	$\neg$	-7. ⁰¹		15	+ + + + + + + + + +		, 56 ^{91,16}	
		0.4		•	4 7	+ 5685	×56 ⁸²		$\begin{pmatrix} + & + & + & + \\ + & + & + & + \\ + & + &$			
		+ 9682.40			4	33						
					560	~		TLET		+ + + + + + + + + + + + + + + + + + +		
							Z					
	<			/			N		5682.			
14									32.03			
<u>1</u> 62. ¹¹		<u> </u>		<u>, 63.09</u>	<u> </u>			-5682.0	-+++		5681	AS-BL
	4:1 SL	.ope		9			(	10		$\begin{pmatrix} & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & $		DATE:APRII
/				$\bigcirc$					× 50,5		1600	
/												
												Ŧ
	89				08.19		-69 ^{1.}	56	905			- M
+ 20			+. ⁹		+ 30		+3-		+569(·· )		$\begin{array}{c} & & & & & & & & & & & & & & & & & & &$	
			-				N					
											* * * * * * * * * * * * * * * * * * *	
								 FG=569	2.2 —			
										56	589 × ×	SCALE: 1
										1 1 1		JUALE. I







## DOINT TADIE

PUINT	TABLE		
RTHING	EASTING	ELEVATION	NOTES
714.71	20158.47	5684.80	INV 48" RCP (LINE B)
786.15	20197.19	5685.54	POND BOTTOM
312.62	20159.51	5685.65	POND BOTTOM
327.21	20164.67	5685.70	POND BOTTOM
341.64	20138.20	5685.74	POND BOTTOM
395.71	20061.76	5686.10	POND BOTTOM
943.87	20009.80	5686.20	POND BOTTOM
395.38	19997.02	5686.11	POND BOTTOM
373.70	19970.67	5686.17	POND BOTTOM
373.69	19949.53	5686.21	POND BOTTOM
389.83	19884.81	5686.30	POND BOTTOM
356.85	19874.86	5686.55	POND BOTTOM
70.85	19852.26	5686.28	POND BOTTOM
730.51	19999.53	5685.88	POND BOTTOM
65.63	20129.13	5685.60	POND BOTTOM
300.21	19976.50	5685.40	TRICKLE CHANNEL INVERT
361.06	19916.81	5685.66	TRICKLE CHANNEL INVERT
378.04	19882.51	5685.80	INV 48" RCP (LINE C)
45.23	20093.52	568501	TRICKLE CHANNEL INVERT
355.30	20113.66	5685.45	TRICKLE CHANNEL INVERT



TOTAL SHEETS: 12

SCALE: 1"=20'

**AS-BUILT** 

DATE: <u>APRIL 6, 2018</u>





APPLE TREE GOLF COURSE

AS DATE:

				CORE ENGINEERING GROUP 15004 15T AVE. S BURNSVILLE, MN 55306	PH: 719.570.1100 CONTACT: RICHARD L. SCHINDLER, P.E. EMAIL: Rich@ceg1.com
OINT	TABLE	ELEVATION	NOTES	NO.     DESCRIPTION       NO.     DESCRIPTION       DEMOLECT:     PREPARED FOR:	ATRIAGE MEADOWS SOUTH 212 N. WARSATCH AVE., SUITE 301 AT LORSON RANCH FIL. NO. 1 212 N. WAHSATCH AVE., SUITE 301 FONTAINE BLVD CARRIAGE MEADOWS DR COLORADO SPRINGS, COLORADO 80903 EL PASO COUNTY, COLORADO (719) 635-3200 EL PASO COUNTY, COLORADO CONTACT: JEFF MARK
.70 .79 .08 .43 .53 .57 .57 .0VED WER STORM ATERA	20951.65 20901.93 20876.39 20843.88 20866.94 20880.42	5684 5684 5684.20 5685 5685 5685	POND BOTTOM POND BOTTOM POND BOTTOM POND BOTTOM POND BOTTOM POND BOTTOM	DESIGNED: RLS CHECKED: RLS (LOINTON DOND G3 (DISTRICT)	CARRIAGE MEADOWS SOUTH
<b>S−E</b> :	<b>3UIL</b> April 6, 20	<b>F</b> 18_	-N- 20 10 0 20 40 SCALE: 1"=20'	DATE AUGUST 10 PROJECT N 100.03 SHEET NUM C4.8 TOTAL SHEETS:	, 2017 ^{IO.} D BER 12







WALL SECTION A-A 1"=10'

	POINT	TABLE	
NUMBER	NORTHING	EASTING	ELEVAT
1	20560.79	20433.55	5683.5
2	20561.80	20438.53	5683.5
3	20530.94	20464.35	5683.5
4	20514.32	20456.47	5683.3
5	20524.93	20450.92	5683.3
6	20517.12	20437.44	5683.5
7	20529.87	20415.52	5683.5
8	20546.23	20451.50	5683.5
9	20545.54	20450.19	5683.5
10	20539.98	20439.55	5683.4
11	20535.97	20434.28	5683.4
12	20553.38	20438.13	5683.5







LE	ING	ТΗ
Α	=	1/2
C	=	1 —

	POINT	TABLE		
NUMBER	NORTHING	EASTING	ELEVATION	NOTES
1	20365.82	20318.86	5683.65	FOREBAY BOTTOM
2	20365.52	20329.30	5683.60	FOREBAY BOTTOM
3	20359.71	20333.16	5683.57	FOREBAY BOTTOM
4	20359.74	20345.96	5683.50	FOREBAY BOTTOM
5	20368.80	20321.19	5683.67	FOREBAY BOTTOM
6	20380.69	20328.16	5683.67	FOREBAY BOTTOM
7	20376.85	20334.70	5683.66	FOREBAY BOTTOM
8	20361.75	20335.03	5683.58	FOREBAY BOTTOM
9	20357.71	20332.26	5683.58	FOREBAY BOTTOM
10	20363.46	20319.53	5683.67	FOREBAY BOTTOM

CORRERING GROUP ENGINEERING GROUP 15004 1ST AVE. S. BURNSVILLE, MN 55306 PH: 719.570.1100 CONTACT: RICHARD L. SCHINDLER, P.E. EMAL: Rich@ceg1.com
LLC LLC SUITE 301 S200 FF MARK
PREPARED FOR: LORSON, 212 N. WAHSATCH AV COLORADO SPRINGS, CC (719) 635- CONTACT: JEF
AGE MEADOWS SOUTH DRSON RANCH FIL. NO. 1 BLVD CARRIAGE MEADOWS DR
DRAWN: RLS DESIGNED: RLS CHECKED: RLS
POND G1/G2 (DISTRICT) G2 SIDE OF POND TRICKLE AND FOREBAY DETAILS
 DATE AUGUST 28, 2017 PROJECT NO. 100.030
C9.2



BAR SIZE	#4	#5	#6
MIN. SPLICE LENGTH	1'-3"	1'-7"	2'-0"







## APPENDIX E- DRAINAGE BOARD MINUTES, STORM SEWER SCHEMATIC AND HYDRAFLOW STORM SEWER CALCS

## Minutes City of Colorado Springs/ El Paso County Drainage Board Meeting Summary January 23, 2024

The City of Colorado Springs/ El Paso County Drainage Board held its meeting at 1:30 PM, Tuesday, January 23, 2024, at Pikes Peak Regional Building in the Pikes Peak Hearing Room.

**MEMBERS PRESENT:** Tim McConnell (Chair), Marc Whorton (Vice Chair), Grant Petik, Brett Louk, Mark Sherwood, Scott Smith

OTHERS PRESENT: Christina Aragon (City), Erin Powers (City), Erica Schmitz (City), Amy Tuten (City), Rebecca Greenberg (City), Daniel Torres (El Paso County), Carlos Hernandez (El Paso County), Jeff Rice (El Paso County), Greg Shaner (Matrix), Jesse Sullivan (Matrix), Tina Buschar (View Homes), JM Turley (View Homes), Jeff Mark (Landhuis), Rich Wray (Kiowa), Dave Gorman (MVE)

Item 1: Meeting called to order by *Tim McConnell* at 1:31 PM.

## Item 2:

a) Approval of the November 14, 2023, Drainage Board minutes

Approval of the minutes from the November 14, 2023, Drainage Board Meeting. Motion was made by *Scott Smith* to approve the minutes of November 14, 2023, *with the amendment to remove Marc Whorton's duplicate naming in the "Members Present"*. Motion was seconded by *Mark Sherwood*.

## **Motion Passed 6-0**

Item 3: Old Business - None.

## Item 4: New Business

# a) Partial Closure of Jimmy Camp Creek for Bull Hill/Rolling Meadows (County) – presented by Jeff Rice (County), Jeff Mark (Landhuis), and Rich Wray (Kiowa)

Jeff Rice introduces the request for the closure of a portion of Jimmy Camp Creek Basin for Bull Hill, Rolling Meadows, and the remaining unplatted portions of Lorson Ranch development in unincorporated El Paso County. El Paso County supports the approval of the partial closure, but they are still reviewing to ensure this action will not significantly increase the drainage fee for the remaining parcels in the basin. *Tim McConnell* asks if this item will need to come back to Drainage Board once the determinations are made, or will it be approved administratively. *Jeff Rice* responds that could be decided by the Board whether or not they would like to have the item come back to the Board. *Jeff Mark* then states it would be preferred if the Item could be settled administratively, but agrees it is the Board's decision. *Jeff Rice* displays the map of Lorson Ranch to show the area of concern for this Item. *Jeff Mark* continues to describe the area in question and explain the background of the improvements already installed and future installments. Jeff explains this request is being brought to the Board because the cost of the improvements is anticipated to far exceed what the basin fees would be based on the analysis. Mark Sherwood asks if they are fairly confident about the required improvements to be installed in the area. Jeff Rice answers that they are confident about the final design and associated fees. Rich Wray arrives and offers further details on the calculations of the drainage fees for the area. He then continues to explain justifications to support this request. Scott Smith asks Jeff Mark about the current status of this portion of Lorson Ranch in terms of the fees and reimbursable cost and if it's in balance. Jeff Rice responds by explaining the current status of this portion of Lorson Ranch discussing the fees and credits for the basin. Marc Whorton asks if the channel improvements have been accepted by the County. Jeff Rice confirms that the channels have been completed and accepted, and the metro district maintains it. Marc Whorton then asks when the updated DBPS will be completed, and Jeff Rice responds that it is anticipated to be completed within the year.

*Marc Whorton* asks if Jeff Mark would be ok with splitting up the request to close the portion of the basin with completed improvements while the County finishes their review and completes the updated DBPS. Jeff agrees the would be acceptable if the Board agrees.

*Marc Whorton* moves to approve the partial closure of Jimmy Camp Creek just for the remaining Lorson developments, pending confirmation that this action will not significantly raise the resulting drainage fees for the remaining parcels in the basin with the expectation that the applicant will bring the same request back to the Board for Rolling Meadows/ Bull Hill. *Scott Smith* seconds the motion.

#### **Motion Passed 6-0**

## b) Sand Creek Channel Stabilization Reimbursement Request (City) – presented by Erica Schmitz (City) and Gregory Shaner (Matrix)

*Erica Schmitz* introduces the request for reimbursement for Sand Creek channel improvements. Erica continues providing a bit of background for the request and states that City staff is remaining neutral on this request because the reimbursement request is greater than the 10% allotted by code. *Gregory Shaner* is introduced and continues to provide background on the project and history of the site. Gregory describes the difficulties and obstacles with the project, which helps to justify why they are requesting a larger reimbursement. Grant Petik asks for clarification on some of the additional costs shown in their analysis. Gregory explains the costs depicted and discusses more details about the project. Board members and applicant discuss the cost breakdown, and Tim McConnell mentions an analysis to determine whether a fee increase is warranted. There is further discussion amongst the Board.

*Tim McConnell* moves to approve the \$553,188.31 channel improvements reimbursement request. *Mark Sherwood* seconds the motion.

#### **Motion Passed 6-0**

## c) Sand Creek Request to Designate Reimbursable Infrastructure (City) – presented by Erica Schmitz (City)

*Erica Schmitz* introduces the request for channel improvements associated with the Final Plat for The Crossing at Palmer Park Filing No. 5 be designated as reimbursable. Erica adds that City staff is remaining neutral on this request but offers options for possible motions. Erica introduces *Dave Gorman*, who takes the stand to explain the background of their improvements and the reason for their request. Dave explains there has been no improved or stabilization of the channel in this area previously. *Mike Turley* asks about drainage fees in association with platting the area. *Erin Powers* 

addresses Mike's question with City policy. *Scott Smith* then asks if these improvements are installed already, and Dave responds that they have not. Dave explains that plans have been reviewed by the City and this is just an estimated cost for the improvements. *Scott Smith* confirms that this is a request to improvement costs to be considered reimbursable and Dave confirms. There is further discussion between the Board and applicant describing the project and development for The Crossing at Palmer Park Filing No. 5.

*Scott Smith* moves to approve the request to add this reimbursable amount to the Sand Creek Drainage Basin with a request for a fee analysis of the Sand Creek Basin upon request for reimbursement. *Marc Whorton* seconds the motion.

#### **Motion Passed 6-0**

#### e) Housekeeping

## a. February meeting cancellation

*Mark Sherwood* moves to approve the cancellation of the schedule meeting in February 2024. *Marc Whorton* seconds the motion.

#### **Motion Passed 6-0**

## f) Open Discussion

*Tim McConnell* asks about Gary's vacancy and the upcoming vacancies when his and Marc's terms expire in May 2024. *Erin Powers* responds explaining that the vacancies are posted and reviews the process for hiring.

*Tim McConnell* then asks about the financial update from the County and requests they could provide an update at the next meeting.

*Tim McConnell* asked about Amy's financial update and the unclaimed reimbursements, wanting more details on where the additional unclaimed funds were reallocated to. *Erin Powers* responds that she will speak with Amy to find out if the unclaimed funds will be reallocated to each individual basin versus the Interest fund.

Item 5: Tim McConnell - Meeting adjourned at 3:43 PM.





## Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor Ioss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	1	31.50	34x53	Ell	28.90	5701.86	5702.05	0.657	5704.47	5703.75	0.38	5703.75	End	Manhole
2	2	20.50	36	Cir	72.76	5702.15	5702.51	0.495	5703.75	5703.96	n/a	5703.96	1	Manhole
3	3	12.50	24	Cir	26.00	5703.26	5703.52	1.001	5704.32	5704.79	0.23	5704.79	2	Manhole
4	4	9.80	24	Cir	239.29	5703.62	5706.01	0.999	5704.79	5707.13	n/a	5707.13 j	3	Manhole
5	5	9.40	24	Cir	35.00	5706.11	5706.46	1.000	5707.13	5707.56	0.44	5707.56	4	Manhole
6	6	8.90	24	Cir	22.46	5703.26	5703.38	0.535	5704.31	5704.44	n/a	5704.44	2	Manhole
7	7	5.90	18	Cir	151.60	5703.88	5704.63	0.495	5704.89	5705.64	0.34	5705.98	6	Manhole
8	8	12.20	24	Cir	28.65	5702.90	5703.19	1.012	5703.94	5704.44	0.51	5704.44	1	Manhole
9	9	5.30	18	Cir	125.20	5703.69	5704.94	0.998	5704.44	5705.83	n/a	5705.83	8	None
10	10	6.00	18	Cir	29.57	5703.69	5703.99	1.016	5704.50	5704.94	0.41	5704.94	8	None
Village 5yr									Number o	f lines: 10		Run E	Date: 3/28/2	2024
NOTES:	NOTES: Return period = 5 Yrs. ; j - Line contains hyd. jump.													

## Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	1	57.30	34x53	EII	29.00	5701.86	5702.05	0.655	5704.41	5704.32	n/a	5704.32	End	Manhole
2	2	37.30	36	Cir	72.76	5702.15	5702.51	0.495	5704.32	5704.52	0.81	5705.32	1	Manhole
3	3	22.80	24	Cir	26.00	5703.26	5703.52	1.001	5705.32*	5705.59*	0.34	5705.93	2	Manhole
4	4	17.80	24	Cir	239.29	5703.62	5706.01	0.999	5705.93	5707.53	n/a	5707.53 j	3	Manhole
5	5	17.00	24	Cir	35.00	5706.11	5706.46	1.000	5707.53	5707.95	0.72	5707.95	4	Manhole
6	6	16.10	24	Cir	22.46	5703.26	5703.38	0.535	5705.32*	5705.44*	0.06	5705.50	2	Manhole
7	7	8.10	18	Cir	151.60	5703.88	5704.63	0.495	5705.50*	5706.40*	0.33	5706.73	6	Manhole
8	8	22.40	24	Cir	29.00	5702.90	5703.19	1.000	5704.52	5704.88	0.92	5704.88	1	Manhole
9	9	9.70	18	Cir	125.20	5703.69	5704.94	0.998	5704.88	5706.14	0.64	5706.14	8	None
10	10	11.00	18	Cir	29.57	5703.69	5703.99	1.016	5704.98	5705.28	0.72	5706.00	8	None
									Number of	l f lines: 10	<u></u>	ј Run Г	) Date: 3/28/2	2024
NOTES														
	Return penou – 100 Yrs. ; "Surch	arged (HG		i)., j - Lin	e contains	nya. jump.								

# MAP POCKET


