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Update as accordingly for the OWTS report

SOIL, GEOLOGY, GEOLOGIC HAZARD, AND WASTEWATER STUDY MOUNTAINS TO VIEW ESTATES 11150 NORTH ELLICOTT HIGHWAY EL PASO COUNTY, COLORADO

Prepared for

Avalar Real Estate 7495 McLaughlin Road, Suite 101 Falcon, Colorado 80831

Attn: Craig McConnell

April 16, 2018

Respectfully Submitted,

ENTECH ENGINEERING, INC.

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Logan L. Langford Geologist

LLL/m

Encl.

Entech Job No. 180343 AAprojects/2018/180343 countysoll/geo/wastewater Reviewed by:

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1.0 SUMMARY

Project Location

The project lies in a portion of the SE¼ of the NE¼ of Section 24, Township 12 South, Range 63 West of the 6th Principal Meridian in El Paso County, Colorado. The site is located approximately 5½ miles southeast of Peyton, Colorado. More specifically the site is located southwest of Scott Road and North Ellicott Highway.

Project Description

Total acreage involved in the project is approximately forty acres. The proposed site development consists of three rural residential lots. The development will utilize individual water wells and on-site wastewater treatment systems. The existing house is located on Lot 1 will remain.

Scope of Report

This report presents the results of our geologic evaluation and treatment of engineering geologic hazard study.

Land Use and Engineering Geology

This site was found to be suitable for the proposed development. Areas were encountered where the geologic conditions will impose some constraints on development and land use. These include artificial fill, hydrocompaction, loose or collapsible soils, floodplain, and potentially seasonally shallow groundwater areas. Based on the proposed development plan, the floodplain areas have been designated as a no build area. These conditions will be discussed in greater detail in the report.

In general, it is our opinion that the development can be achieved if the observed geologic conditions on site are either avoided or properly mitigated. All recommendations are subject to the limitations discussed in the report.

2.0 GENERAL SITE CONDITIONS AND PROJECT DESCRIPTION

The site is located in a portion of the SE¼ of the NE¼ of Section 24, Township 12 South, Range 63 West of the 6th Principal Meridian in El Paso County, Colorado. The site is located approximately 5½ miles southeast of Peyton, Colorado. More specifically the site is located southwest of Scott Road and North Ellicott Highway. The location of the site is as shown on the Vicinity Map, Figure 1.

The topography of the site is generally gently sloping to the southeast. The drainages on site flow in a southeasterly direction through the central portion of the site. Water was not observed in the drainages on-site at the time of this investigation. The site boundaries are indicated on the USGS Map, Figure 2. Previous land uses have included grazing and pasture land. The site contains primarily field grasses, weeds, cacti, and yuccas, and scattered trees along the southern portion of the site. Site photographs, taken March 10, 2018, are included in Appendix A.

Total acreage involved in the proposed development is approximately forty acres. Three singlefamily rural residential lots are proposed. The proposed lots will be approximately 13 acres. The area will be serviced individual water wells and on-site wastewater treatment systems. The proposed Development Plan is presented in Figure 3.

3.0 SCOPE OF THE REPORT

The scope of the report will include the following:

- A general geologic analysis utilizing published geologic data. Detailed site-specific mapping will be conducted to obtain general information in respect to major geographic and geologic features, geologic descriptions and their effects on the development of the property.
- The site will be evaluated for on-site wastewater treatment systems in accordance with El Paso Land Development Code.

4.0 FIELD INVESTIGATION

Our field investigation consisted of the preparation of a geologic map of any bedrock features and significant surficial deposits. The Natural Resource Conservation Service (NRCS), previously the Soil Conservation Service (SCS) survey was also reviewed to evaluate the site. The position of mappable units within the subject property are shown on the Geologic Map. Our mapping procedures involved both field reconnaissance and measurements and air photo reconnaissance and interpretation. The same mapping procedures have also been utilized to produce the Geology/Engineering Geology Map which identified pertinent geologic conditions affecting development. The field mapping was performed by personnel of Entech Engineering, Inc. on March 10, 2018.

Two tactile test pits for On-site Wastewater Treatment Systems (OWTS) were excavated on the site to determine general soil and bedrock characteristics. The locations of the test pits are indicated on the Site Plan/Test Boring Location Map, Figure 4. The Test Pit Logs are presented in Appendix B. Results of this testing will be discussed later in this report.

Laboratory testing was also performed on some of the soils to classify and determine the soils engineering characteristics. Laboratory tests included grain-size analysis. Results of the laboratory testing are included in Appendix C.

A Soils Report which included two test borings on the southern lot (Lot 3) by Geoquest, LLC (Reference 1, Appendix D) was also used in evaluating the site.

5.0 SOIL, GEOLOGY AND ENGINEERING GEOLOGY

5.1 General Geology

Physiographically, the site lies in the western portion of the Great Plains Physiographic Province. Approximately 26 miles to the west is a major structural feature known as the Rampart Range Fault. This fault marks the boundary between the Great Plains Physiographic Province and the Southern Rocky Mountain Province. The site exists within the southeastern edge of a large structural feature known as the Denver Basin. Bedrock in the area tends to be very gently dipping in a northwesterly direction (Reference 2). The rocks in the area of the site are sedimentary in nature and typically Upper Cretaceous in age. The bedrock underlying the

site consists of the Dawson Formation. Overlying this formation are unconsolidated deposits of alluvial and eolian soils of Quaternary Age. The alluvial soils were deposited by water on-site and as stream terrace deposits along the drainages on-site. The site's stratigraphy will be discussed in more detail in Section 5.3.

5.2 Soil Conservation Survey

The Natural Resource Conservation Service (Reference 3), previously the Soil Conservation Service (Reference 4) has mapped four soil types on the site (Figure 4). In general, the soils classify as loamy sand and sandy loam. The soils are described as follows:

Туре	Description
8	Blakeland Loamy Sand, 1 to 9% slopes
10	Blendon Sandy Loam, 0 to 3% slopes
28	Ellicott Loamy Coarse Sand, 0 to 5% slopes
96	Truckton Sandy Loam, 0 to 3% slopes

Complete descriptions of each soil type are presented in Appendix E. The soils have generally been described to have moderately rapid to rapid permeability. Possible hazards with soil erosion are present on the site. The erosion potential can be controlled with vegetation. The majority of the soils have been described to have moderate to high erosion hazards (Reference 4).

5.3 Site Stratigraphy

The Pueblo 1°x2° Quadrangle Geology Map showing the site is presented in Figure 5 (Reference 5). The Geology Map prepared for the site is presented in Figure 6. Four mappable units were identified on this site which are described as follows:

- Qal Recent Alluvium of Holocene Age: These are recent deposits that have been deposited along the drainages on-site.
- **Qaf** Artificial Fill of Holocene Age: These are man-made fill deposits associated with the small earthen dam that is located in the southeastern portion of Lot 2.

- **Qp Piney Creek Alluvium of Holocene Age:** This material is a water-deposited alluvium, typically classified as a silt to well-graded sand, brown to dark brown in color and of moderate density. The Piney Creek Alluvium can sometimes be very highly stratified containing layers of very silty and clayey soil.
- Qes Eolian Sand of Quaternary Age: These deposits are fine to medium grained soils deposited on the site by action of the prevailing winds from the west and northwest. They typically occur as large dune deposits or narrow ridges. These soil types are typically tan to brown in color and tend to have very uniform or well-sorted gradation. These materials tend to have a relatively high permeability and low density.

The soils listed above were mapped from site-specific mapping, and the *Geologic Map of the Pueblo 1° x 2° Quadrangle South-Central Colorado* distributed by the US Geological Survey in 1976 (Reference 5). The Test Pits and Test Holes (Geoquest) were also used in evaluating the site and are included in Appendices B and D. The Geology Map prepared for the site is presented in Figure 6.

5.4 Soil Conditions

The soils encountered in the Test Holes and Test Pits can be grouped into one general soil types. The soils were classified using the Unified Soil Classification System (USCS). The test pit soils were classified using the USDA Textural Soil Classification.

<u>Soil Type 1</u> silty sand (SM), encountered in both of test holes and test pits at the existing ground surface and extending to depths ranging from 8 feet to 15 feet bgs. These soils were encountered at loose to medium dense states and at moist conditions. Samples tested had 10 to 18 percent passing the No. 200 Sieve.

The Test Pit Logs are presented in Appendix B. Laboratory Test Results are presented in Appendix C. A Summary of Tactile Test Pit Results is presented in Table 1. Test Hole Logs and Laboratory Test Results from the Soils Report performed by Geoquest, LLC (Reference 1) are included in Appendix D.

5.5 Groundwater

Groundwater was not encountered in the test pits or test holes. Areas of potential seasonal shallow groundwater have been mapped along the drainages on-site. These areas are discussed in the following section. Fluctuation in groundwater conditions may occur due to variations in rainfall and other factors not readily apparent at this time.

It should be noted that in the sandy materials on site, some groundwater conditions might be encountered due to the variability in the soil profile. Isolated sand and gravel layers within the soils, sometimes only a few feet in thickness and width, can carry water in the subsurface. Groundwater may also flow on top of the underlying bedrock. Builders and planners should be cognizant of the potential for the occurrence of such subsurface water features during construction on-site and deal with each individual problem as necessary at the time of construction.

6.0 ENGINEERING GEOLOGY – IDENTIFICATION AND MITIGATION OF GEOLOGIC HAZARDS

As mentioned previously, detailed mapping has been performed on this site to produce an Engineering Geology Map Figure 6. This map shows the location of various geologic conditions of which the developers should be cognizant during the planning, design and construction stages of the project. These hazards and the recommended mitigation techniques are as follows:

Artificial Fill

These are man-made fill deposits associated with erosion berms and the earthen dam on-site.

<u>Mitigation:</u> The earthen dam will be avoided by the development, and the small erosion berms can easily be removed or penetrated by foundations. Should any uncontrolled fill be encountered beneath foundations, removal and recompaction at 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 will be required.

Hydrocompaction

Areas in which hydrocompaction have been identified are acceptable as building sites. In areas identified for this hazard classification, however, we anticipate a potential for settlement movements upon saturation of these surficial soils. The low density, uniform grain sized, windblown sand deposits are particularly susceptible to this type of phenomenon. Additionally, loose or collapsible soils may be encountered on this site.

<u>Mitigation:</u> The potential for settlement movement is directly related to saturation of the soils below the foundation areas. Therefore, good surface and subsurface drainage is extremely critical in these areas in order to minimize the potential for saturation of these soils. The ground surface around all permanent structures should be positively sloped away from the structure to all points, and water must not be allowed to stand or pond anywhere on the site. We recommend that the ground surface within 10 feet of the structures be sloped away with a minimum gradient of five percent. If this is not possible on the upslope side of the structures, then a well-defined swale should be created to intercept the surface water and carry it quickly and safely around and away from the structures. Roof drains should be made to discharge well away from the structures and into areas of positive drainage. Where several structures are involved, the overall drainage design should be such that water directed away from one structure is not directed against an adjacent building. Planting and watering in the immediate vicinity of the structures, as well as general lawn irrigation, should be minimized.

Loose or Collapsible Soils

Some of the sandy soils encountered on site exhibit low density and may be subject to settlement under a load. The potential for loose or collapsible soils exists anywhere in areas mapped as Eolian Sand (Qes) and may also exist in areas mapped as Piney Creek Alluvium (Qp).

<u>Mitigation:</u> Should loose collapsible soils be encountered beneath foundations, removal and recompaction of the upper 2 feet with thorough moisture conditioning at 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 will be necessary. Specific recommendations should be made after additional investigation of each building site.

Groundwater and Floodplain Areas

Areas within the drainages on-site have been identified as areas of potentially seasonally high groundwater areas. Water was not flowing in the any of the drainages at the time of this investigation. Areas of the site are mapped within a floodplain zone according to the FEMA Map No. 08041C0575F, Figure 7 (Reference 6). These areas are located within the no-build area and will be avoided by development. Finished floor levels must be a minimum of on foot above floodplain levels. Specific floodplain locations and drainage studies are beyond the scope of this report.

Potentially Seasonal Shallow Groundwater Area

In these areas, we would anticipate the potential for periodically high subsurface moisture conditions, frost heave potential and highly organic soils. The majority of these areas lie within defined drainages which can likely be avoided by the proposed development.

<u>Mitigation:</u> Foundations must have a minimum 30-inch depth for frost protection. In areas where high subsurface moisture conditions are anticipated periodically, subsurface perimeter drains are recommended to help prevent the intrusion of water into areas below grade. Typical drain details are presented in Figure 8. Any grading in these areas should be done to direct surface flow around construction to avoid areas of ponded water. Structures should not block drainages. All organic material should be completely removed prior to any fill placement.

6.1 RELEVANCE OF GEOLOGIC CONDITIONS TO LAND USE PLANNING

The proposed development will be three single family rural residential lots. It is our opinion that the existing geologic and engineering geologic conditions will impose some constraints on the proposed development and construction. The most significant issues affecting development will be those associated with the artificial fill, hydrocompaction, loose or collapsible soils, floodplain, and potentially seasonally shallow groundwater areas on site that can be properly mitigated or avoided. Other hazards on site may be satisfactorily mitigated through proper engineering design and construction practices.

The upper materials are typically at loose to medium dense states. The medium dense granular soils encountered in the upper soil profiles of the test holes and test pits should provide good support for foundations. Loose soils, if encountered at foundation depth will require mitigation. Foundations anticipated for the site are standard spread footings possibly in conjunction with overexcavation in areas of loose soils. Excavation is anticipated to be moderately easy with rubber-tired equipment for the site sand materials. Expansive layers may also be encountered in the soil on this site. Areas of expansive soils encountered on site are sporadic; therefore, none have been indicated on the maps. Expansive soils, if encountered, will require special foundation design and/or overexcavation. These soils will not prohibit development.

Areas of potentially seasonal shallow groundwater, and an earthen dam exist on this site. Due to lot size, it is anticipated these areas can be avoided by development. All surface drainage should be directed around proposed structures.

A floodplain exists in the western portion of the site. This area is designated as a no-build area and will be avoided by development. Finished floors must be a minimum of one foot above the floodplain level. Specific floodplain locations and drainage studies are beyond the scope of this report.

In summary, development of the site can be achieved if the items mentioned above are mitigated. These items can be mitigated through proper design and construction or through avoidance. Investigation on each lot is recommended prior to construction.

7.0 ECONOMIC MINERAL RESOURCES

Some of the sandy materials on-site could be considered a low-grade sand resource. According to the *El Paso County Aggregate Resource Evaluation Map* (Reference 7), the area is not mapped with any aggregate deposits. According to the *Atlas of Sand, Gravel and Quarry Aggregate Resources, Colorado Front Range Counties* distributed by the Colorado Geological Survey (Reference 8), areas of the site are not mapped with any resources. According to the *Evaluation of Mineral and Mineral Fuel Potential* (Reference 9), the area of the site has been mapped as "Good" for industrial minerals. However, considering the silty nature of much of these materials and abundance of similar materials through the region and the close proximity to developed land, they would be considered to have little significance as an economic resource.

According to the Evaluation of Mineral and Mineral Fuel Potential of El Paso County State Mineral Lands (Reference 9), the site is mapped within the Denver Basin Coal Region. However, the area of the site has been mapped as "Poor" for coal resources. No active or inactive mines have been mapped in the area of the site. No metallic mineral resources have been mapped on-site (Reference 9).

The site has been mapped as "Fair" for oil and gas resources (Reference 9). No oil or gas fields have been discovered in the area of the site. The sedimentary rocks in the area may lack the geologic structure for trapping oil or gas; therefore, it may not be considered a significant resource. Hydraulic fracturing is a new method that is being used to extract oil and gas from rocks. It utilizes pressurized fluid to extract oil and gas from rocks that would not normally be productive. The area of the site has not been explored to determine if the rocks underlying the site would be commercially viable utilizing hydraulic fracturing. The practice of hydraulic fracturing has come under review due to concerns about environmental impacts, health and safety.

8.0 ON-SITE WASTEWATER TREATMENT

The site was evaluated for On-site Wastewater Treatment Systems (OWTS) for the proposed lots in accordance with El Paso Land Development Code. Two (2) tactile test pits were performed on the site. Tactile test pits were located in anticipated locations of proposed on-site wastewater treatment system (OWTS) for the development. The approximate locations of the test pits are indicated on Figure 3 and 6, and on the Septic Suitability Map, Figure 9. The locations were chosen to determine a general understanding of the soil and bedrock conditions across the site. The results of the tactile test pits are presented in Table 1. An existing mobile home and septic system are located on Lot 1 and will remain. Septic records for Lot 1 are presented in Appendix F. An infiltrator system installed in 2002 is presently located on the site.

The Natural Resource Conservation Service (Reference 3), previously the Soil Conservation Service (Reference 4) has been mapped with four soil descriptions. The Soil Survey Map (Reference 3) is presented in Figure 4, and the Soil Survey Descriptions are presented in Appendix E. The soils are described as having moderately rapid to rapid percolation rates.

Soils encountered in the tactile test pits consisted of sandy loam to loamy sand. The limiting layers encountered in the test pits are the sandy loam, which corresponds to an LTAR value of 0.50 gallons per day per square foot. The conditions encountered in test pits are suitable for a conventional OWTS. Signs of seasonal shallow groundwater or bedrock were not observed in the test pits, which were excavated to 8 feet.

In summary, it is our opinion the site is suitable for individual on-site wastewater treatment systems and that contamination of surface and subsurface water resources should not occur provided the OWTS sites are evaluated and installed according to El Paso County Guidelines and properly maintained. A Septic Suitability Map is presented in Figure 9. Absorption fields must be located a minimum of 100 feet from any well, including those on adjacent properties. Absorption fields must also be located a minimum of 50 feet from any ponded areas and 25 feet from dry gulches. It should be noted that additional testing will be required for the individual lots prior to construction on each lot.

9.0 EROSION CONTROL

The soil types observed on the site are mildly to highly susceptible to wind erosion, and moderately to highly susceptible to water erosion. A minor wind erosion and dust problem may be created for a short time during and immediately after construction. Should the problem be considered severe enough during this time, watering of the cut areas or the use of chemical palliative may be required to control dust. However, once construction has been completed and vegetation re-established, the potential for wind erosion should be considerably reduced.

With regard to water erosion, loosely compacted soils will be the most susceptible to water erosion, residually weathered soils become increasingly less susceptible to water erosion. For the typical soils observed on-site, allowable velocities or unvegetated and unlined earth channels would be on the order of 3 to 4 feet/second, depending upon the sediment load carried by the water. Permissible velocities may be increased through the use of vegetation to something on the order of 4 to 7 feet/second, depending upon the type of vegetation established. Should the anticipated velocities exceed these values, some form of channel lining material may be required to reduce erosion potential. These might consist of some of the synthetic channel lining materials on the market or conventional riprap. In cases where ditch-lining materials are still insufficient to control erosion, small check dams or sediment traps may be required. The check dams will serve to reduce flow velocities, as well as provide small traps for containing sediment. The determination of the amount, location and placement of ditch linings, check dams and of the special erosion control features should be performed by or in conjunction with the drainage engineer who is more familiar with the flow quantities and velocities.

Cut and fill slope areas will be subjected primarily to sheetwash and rill erosion. Unchecked rill erosion can eventually lead to concentrated flows of water and gully erosion. The best means to combat this type of erosion is, where possible, the adequate re-vegetation of cut and fill slopes. Cut and fill slopes having gradients more than three (3) horizontal to one (1) vertical become increasingly more difficult to revegetate successfully. Therefore, recommendations pertaining to the vegetation of the cut and fill slopes may require input from a qualified landscape architect and/or the Soil Conservation Service.

10.0 CLOSURE

It is our opinion that the existing geologic engineering and geologic conditions will impose some constraints on development and construction of the site. The majority of these conditions can be mitigated through proper engineering design and construction practices. The proposed development and use is consistent with anticipated geologic and engineering geologic conditions.

It should be pointed out that because of the nature of data obtained by random sampling of such variable and non-homogeneous materials as soil and rock, it is important that we be informed of any differences observed between surface and subsurface conditions encountered in construction and those assumed in the body of this report. Individual investigations for building sites will be required prior to construction. Construction and design personnel should be made familiar with the contents of this report. Reporting such discrepancies to Entech Engineering, Inc. soon after they are discovered would be greatly appreciated and could possibly help avoid construction and development problems.

This report has been prepared for Avalar Real Estate for application to the proposed project in accordance with generally accepted geologic soil and engineering practices. No other warranty expressed or implied is made.

We trust that this report has provided you with all the information that you required. Should you require additional information, please do not hesitate to contact Entech Engineering, Inc.

BIBLIOGRAPHY

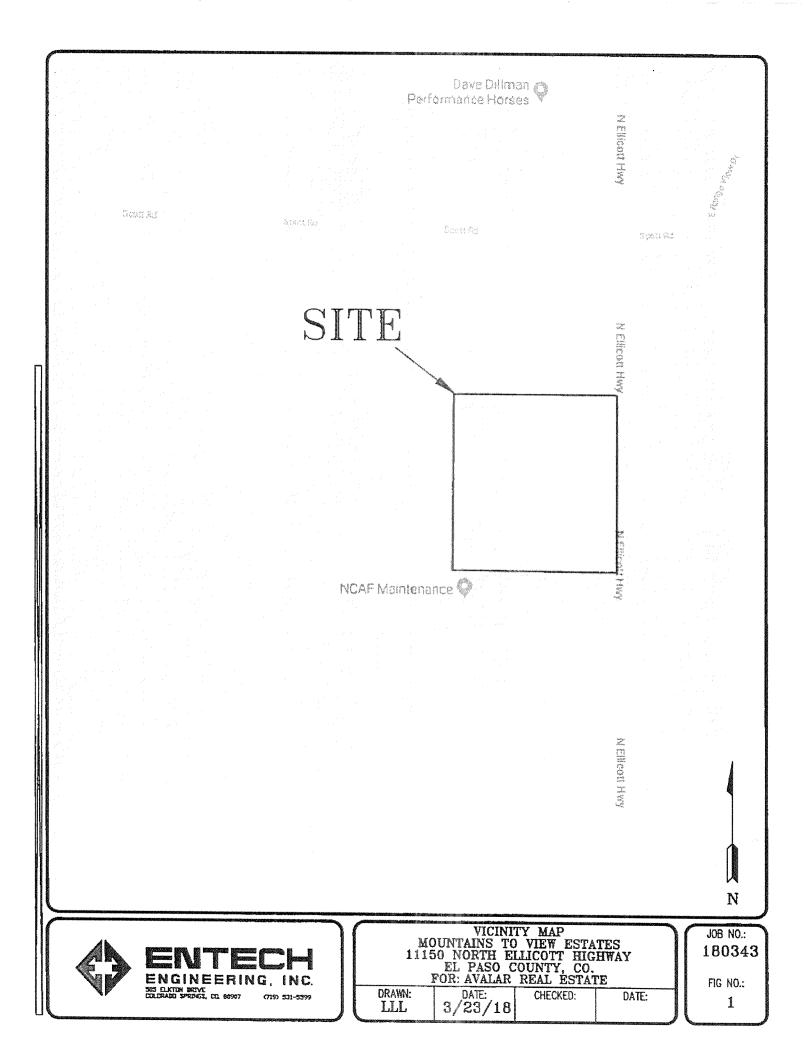
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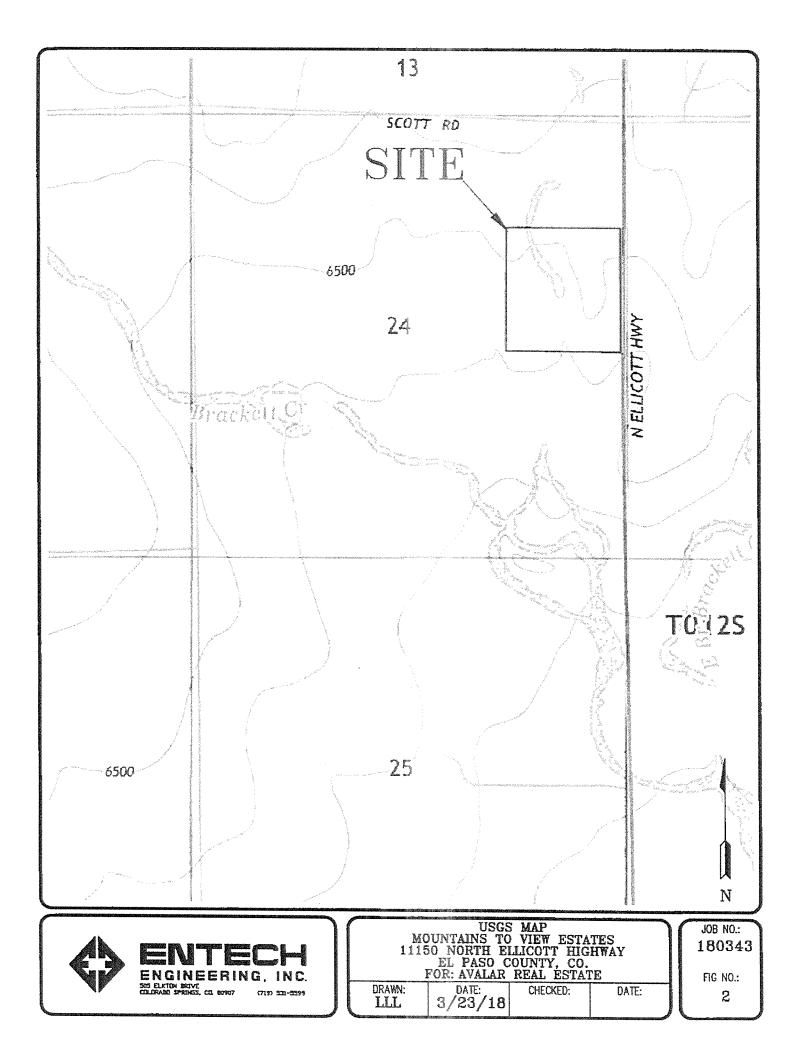
TABLE

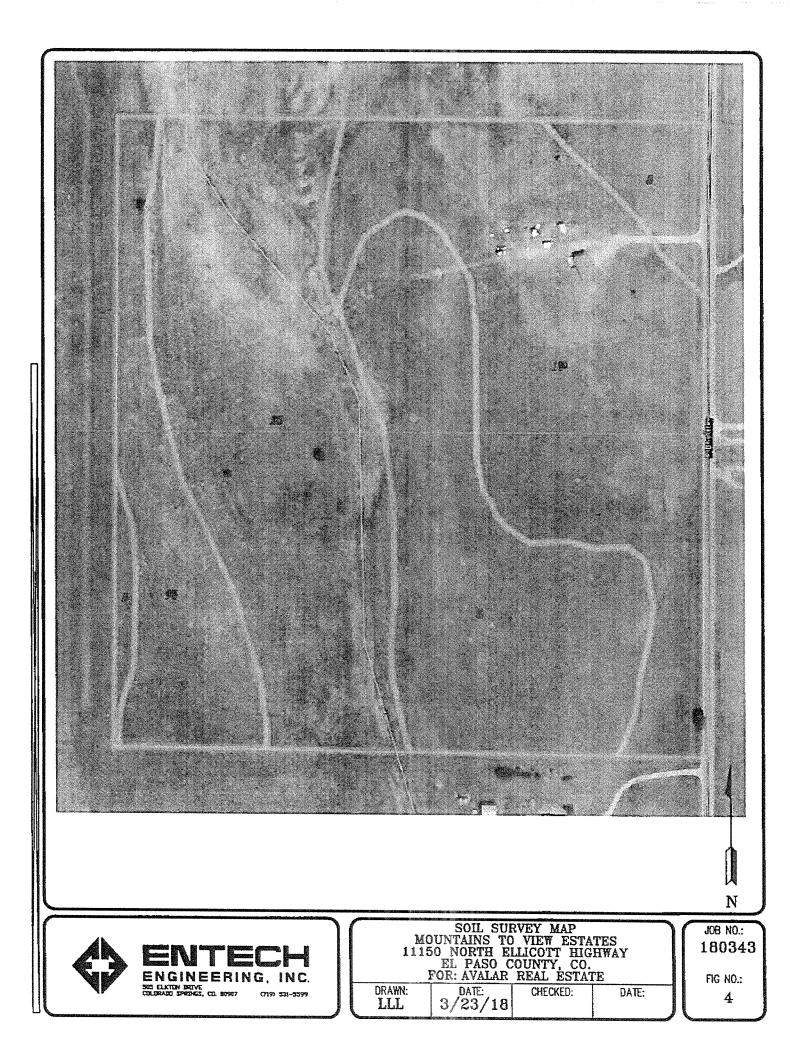
Table 1: Summary of Percolation Test and Tactile Test Pit Results

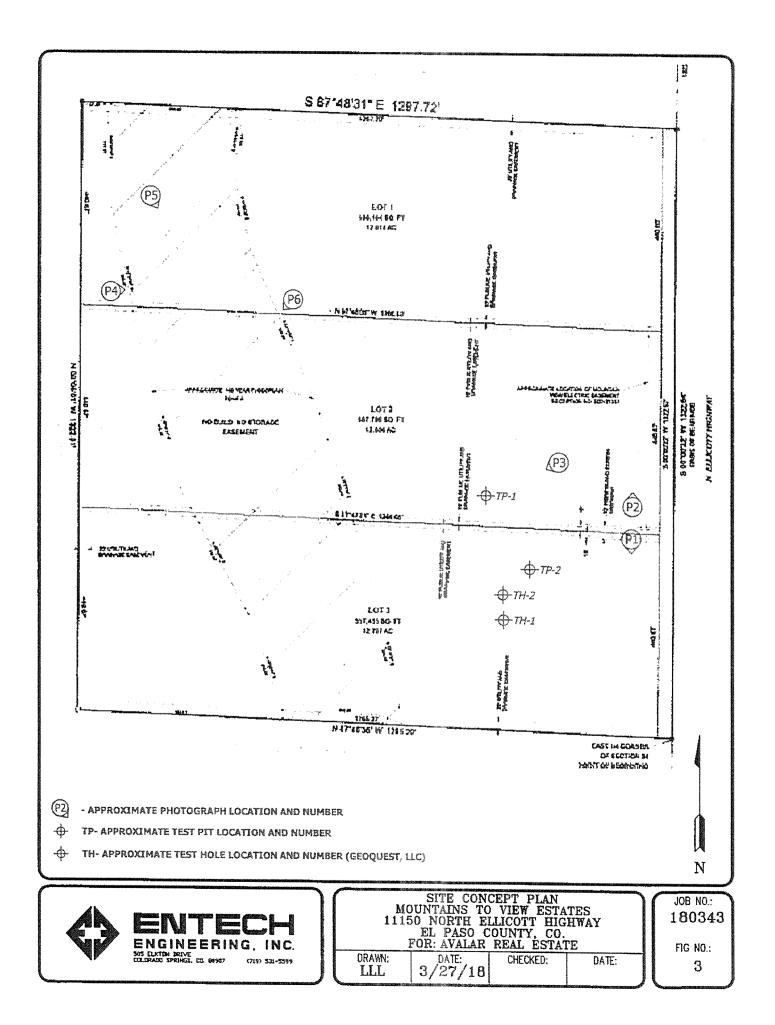
Test Pit No.	USDA Soil Type	LTAR	Depth to	Depth to Seasonally
	Limiting Layer	Value	Bedrock (ft.)	Occurring Groundwater
				(ft.)
1	2A	0.50	N/A	N/A
2	2A	0.50	N/A	N/A

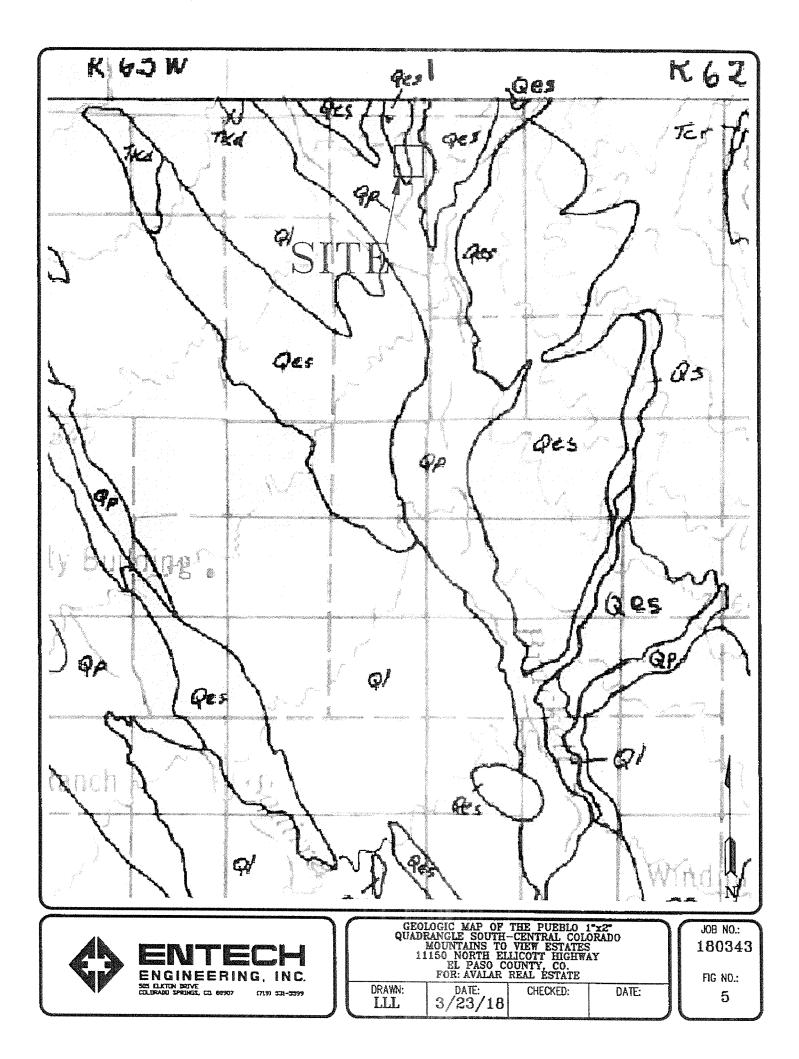
FIGURES

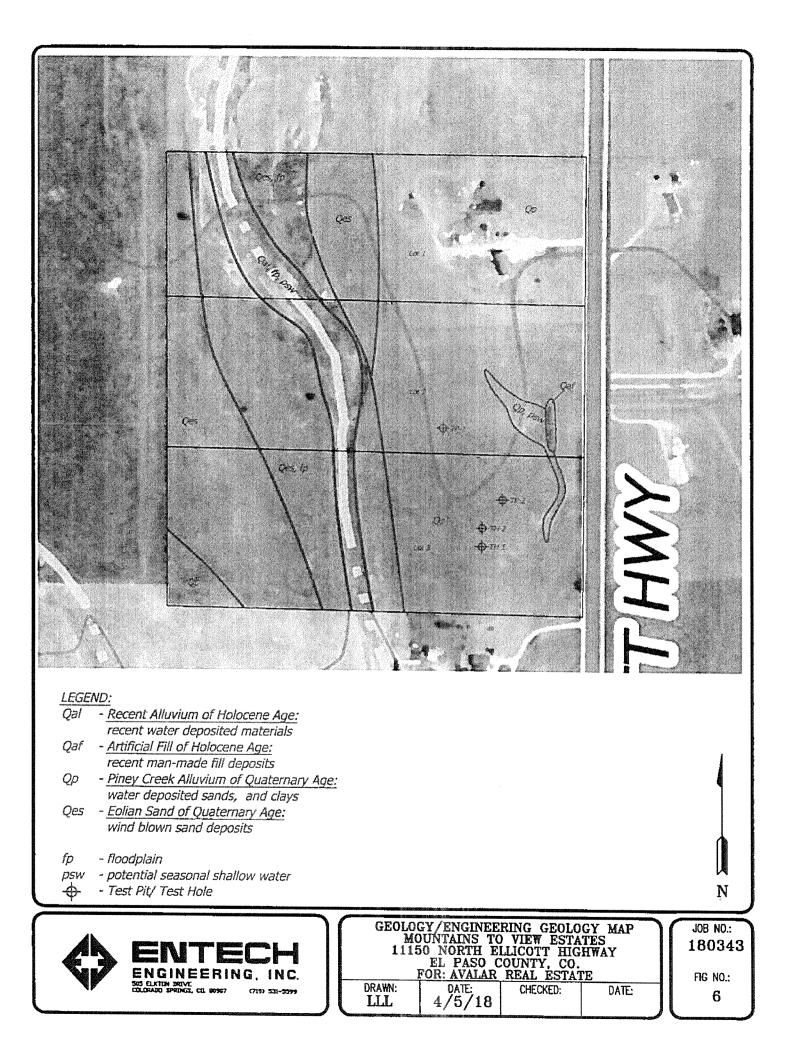


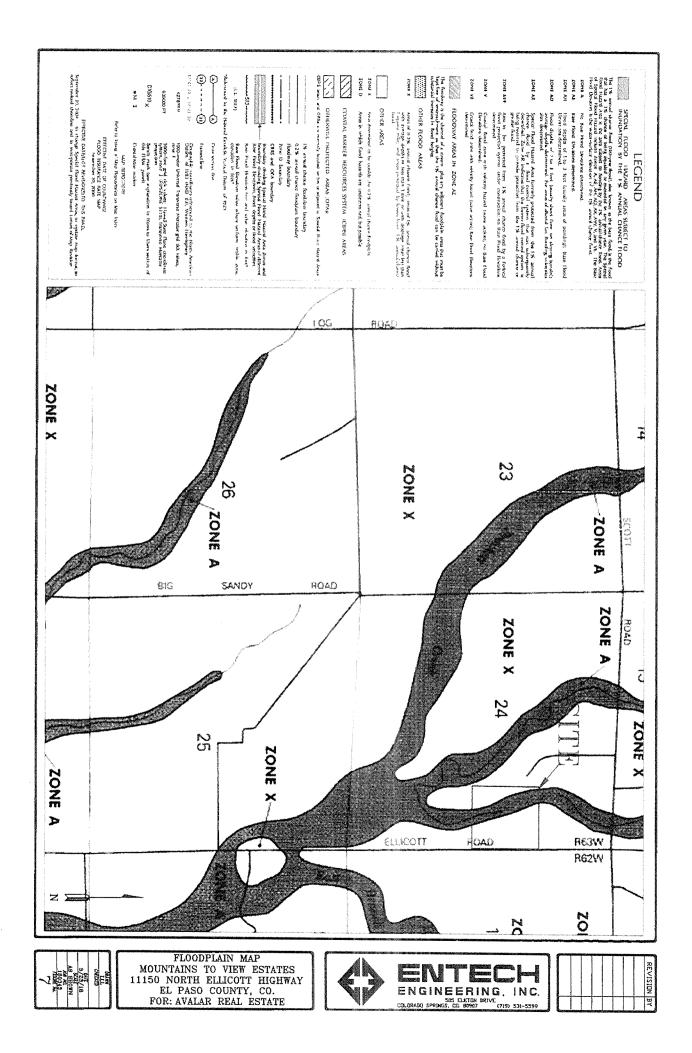


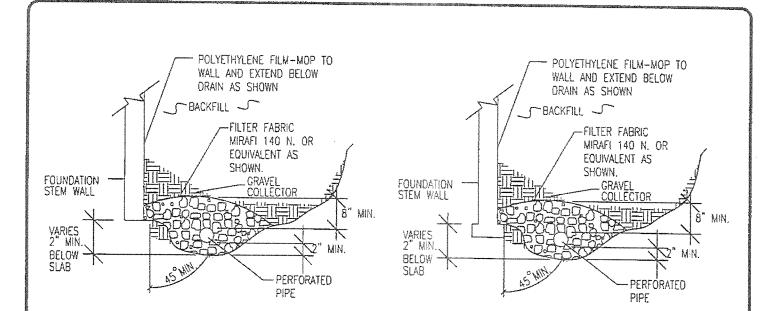












NOTES:

-GRAVEL SIZE IS RELATED TO DIAMETER OF PIPE PERFORATIONS-85% GRAVEL GREATER THAN 2x PERFORATION DIAMETER.

-PIPE DIAMETER DEPENDS UPON EXPECTED SEEPAGE. 4-INCH DIAMETER IS MOST OFTEN USED.

-ALL PIPE SHALL BE PERFORATED PLASTIC. THE DISCHARGE PORTION OF THE PIPE SHOULD BE NON-PERFORATED PIPE.

-FLEXIBLE PIPE MAY BE USED UP TO 8 FEET IN DEPTH, IF SUCH PIPE IS DESIGNED TO WITHSTAND THE PRESSURES. RIGID PLASTIC PIPE WOULD OTHERWISE BE REQUIRED.

-MINIMUM GRADE FOR DRAIN PIPE TO BE 1% OR 3 INCHES OF FALL IN 25 FEET.

-DRAIN TO BE PROVIDED WITH A FREE GRAVITY OUTFALL, IF POSSIBLE. A SUMP AND PUMP MAY BE USED IF GRAVITY OUT FALL IS NOT AVAILABLE.

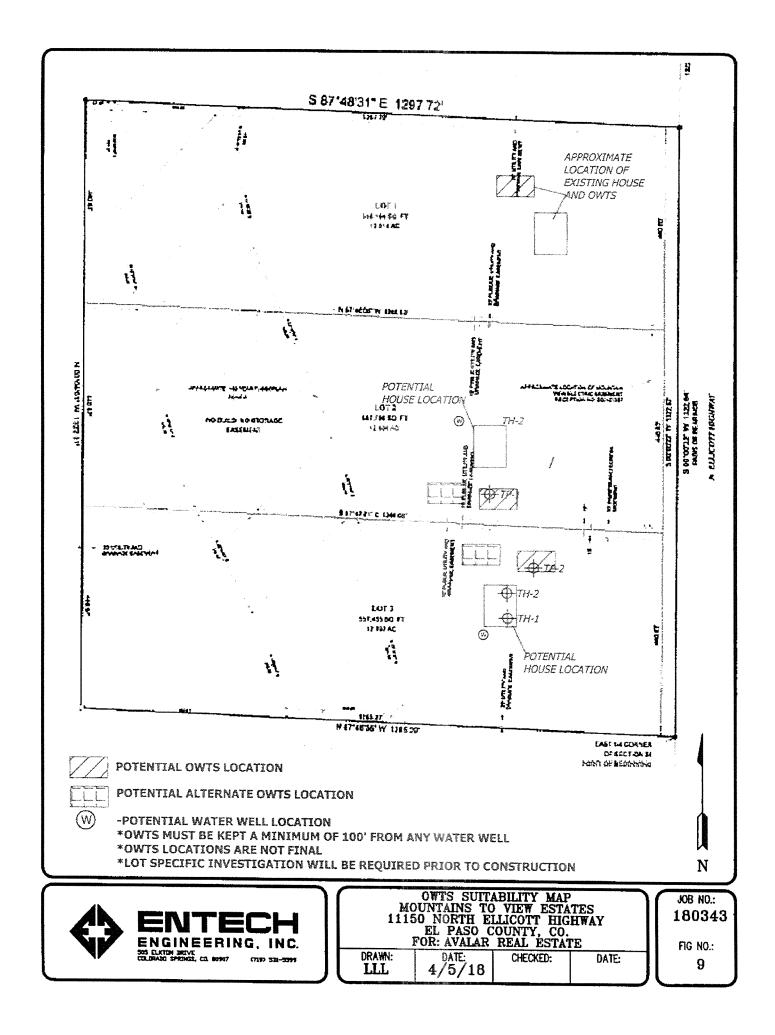


PERIMETER DRAIN DETAIL

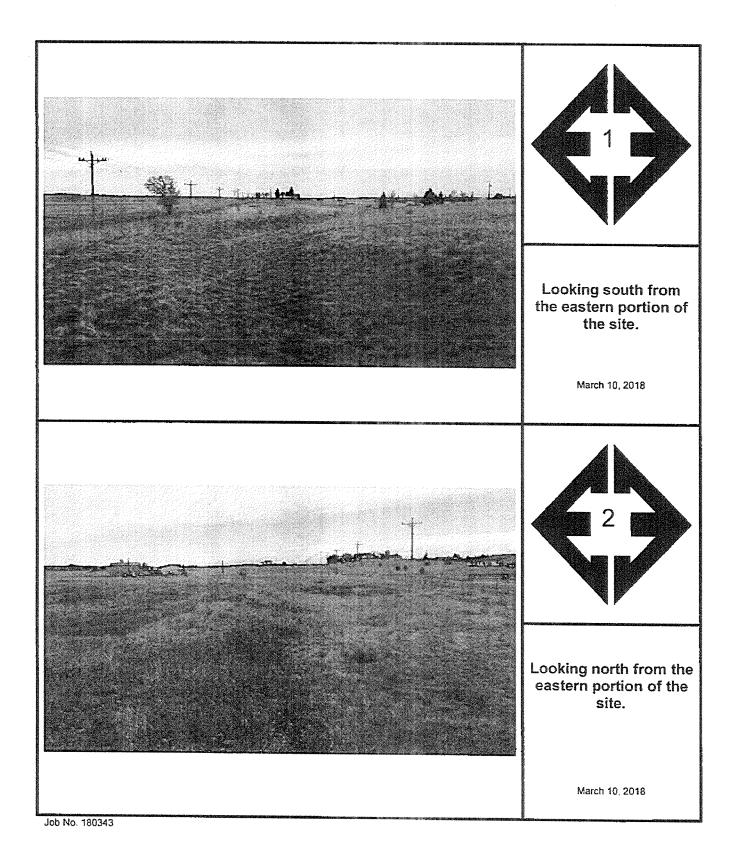
DATE

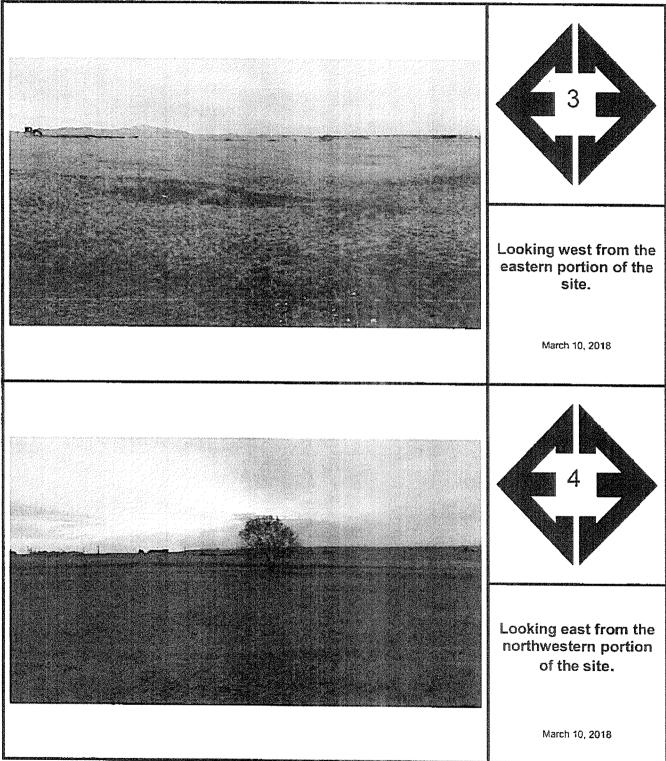
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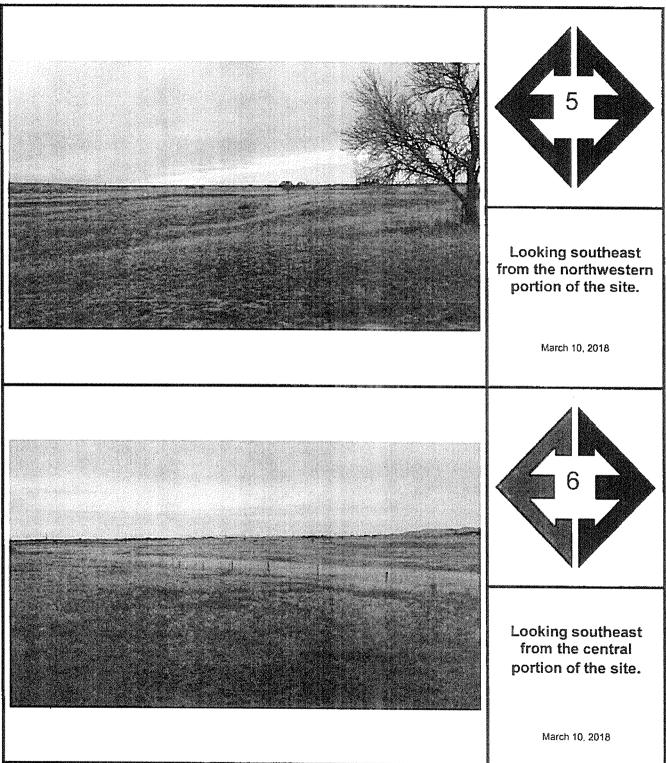


APPENDIX A: Site Photographs





Job No. 180343



Job No. 180343

APPENDIX B: Test Pit Logs

TEST PIT NO. 1 DATE EXCAVATED 3/10/2018 Job # 180343 REMARKS Image: Constraint of the second secon					TEST PIT NO. 2 DATE EXCAVATED 3/10/2018 CLIENT AVALAR REAL ESTATE LOCATION 11150 N. ELLICOTT HWY REMARKS I				
	Depth (ft)	Symbol	Samples	Soil Structure Shape	Soil Structure Grade	USDA Soil Type	Depth (tt) Symbol Samples Soil Structure Shape Soil Structure Grade		
topsoil, sandy loam, brown sandy loam, fine to medium grained, light brown				gr	W	2A	topsoil, sandy loam, brown sandy loam, fine to medium grained, light brown 2 3 		
loamy sand, fine to coarse grained, tan	4 - 5 - 6 - 7 - 8 - 9 - 10 -			sg			loamy sand, fine to coarse grained, tan		
<u>Soil Structure Shape</u> granular - gr platy - pl blocky - bl prismatic - pr single grain - sg massive - ma							<u>Soil Structure Grade</u> weak - w moderate - m strong - s loose - l		

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	ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907			JOB NO.: 180343			
		DRAWN	DATE:	CHECKED	DATE 4/51/9		FIG NO.: G - 1
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APPENDIX C: Laboratory Test Results

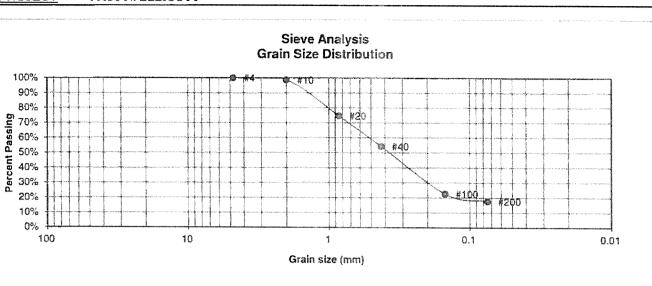
BORING NO.TP-1DEPTH(ft)2-3CLIENTAVAPROJECT11150

2-3 AVALAR REAL ESTATE 11150 N. ELLICOTT

UNIFIED CLASSIFICATION AASHTO CLASSIFICATION

TEST BY BL JOB NO. 180343

SM



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	Swell
10	98.7%	Moisture at start
20	74.7%	Moisture at finish
40	54.3%	Moisture increase
100 200	22.6% 17.8%	Initial <mark>dry density (pcf</mark>) Swell (psf)

.

ENTECH		JOB NO. 180343						
ENGINEERING, INC.		RESULTS			FIG NO :			
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN	DATE:	CHECKED:	DATE. 3/19/18	L-1			

BORING NO. T DEPTH(ft) 5 CLIENT A PROJECT 1

TP-1 5-6 AVALAR REAL ESTATE 11150 N. ELLICOTT

UNIFIED CLASSIFICATION AASHTO CLASSIFICATION

<u>TEST BY</u> BL JOB NO. 180343

SM-SW

Sieve Analysis Grain Size Distribution 100% ¢ #10 90% 80% 80% 60% 50% 40% 30% 20% \$ \$20 #40 * #TOU #240 20% 10% 0% 100 10 0.1 0.01 1 Grain size (mm)

U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	Swell
10	95.3%	Moisture at start
20	75.9%	Moisture at finish
40	54.2%	Moisture increase
100	18.0%	Initial dry density (pcf)
200	11.6%	Swell (psf)

ENTECH ENGINEERING, INC.		LABORATC RESULTS	RY TEST		JOB NO 5 180343 FIG NO 1
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE	CHECKED	DATE: 3//a//8	6-2

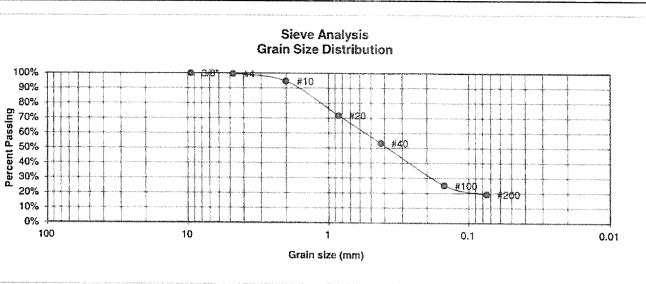
BORING NO. TP-2 DEPTH(ft) 2-3 CLIENT AVAL PROJECT 11150

2-3 AVALAR REAL ESTATE 11150 N. ELLICOTT

UNIFIED CLASSIFICATION AASHTO CLASSIFICATION

TEST BY BL JOB NO. 180343

SM



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	99.6%	Swell
10	94.6%	Moisture at start
20	71.7%	Moisture at finish
40	53.2%	Moisture increase
100	25.2%	Initial dry density (pcf)
200	19.3%	Swell (psf)

ENTECH ENGINEERING, INC.		LABORAT RESULTS	ORY TEST	
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE	CHECKED:	DATE:
			lan lan Sonia. Anter Care Sonia	5/19/

JOB NO. 180343 FIG NO (2-3) BORING NO. TP-2 UNIFIED CLASSIFICATION SM-SW TEST BY BL DEPTH(ft) 5-6 AASHTO CLASSIFICATION JOB NO. 180343 CLIENT PROJECT AVALAR REAL ESTATE 11150 N. ELLICOTT Sieve Analysis Grain Size Distribution 100% 90% **1** 80% b0% 70% 60% 50% 40% 30% 20% W #40

1

Grain size (mm)

₩100 H

0.1

500

0.01

U.S. <u>Sieve #</u> 3" 1 1/2" 3/4* 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	99.5%	Moisture at start
20	84.7%	Moisture at finish
40	58.0%	Moisture increase
100	15.7%	Initial dry density (pcf)
200	10.1%	Swell (psf)

10

505 ELKTON DRIVE DATE DATE DATE	ENTECH ENGINEERING, INC.		LABORAT(RESULTS	ORY TEST		JOB NO.: 180343 FIG NO :
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE		DATE 31/9/18	6-4

20%

10%

0% 100 APPENDIX D: Geoquest, LLC, Soils Report,

February 13, 2018, Job No. 18-0058



6825 Silver Ponds Heights #101 Colorado Springs, CO 80908 (719) 481-4560

SOILS REPORT

FOR

APEX CONSTRUCTION

JOB #18-0058

11150 North Ellicott Highway, El Paso County, Colorado

Respectfully submitted,

Charles E. Millgan, P.E. Civil Engineer



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INTRODUCTION

The owners must be made aware of the contents of this report. If there are any questions or concerns regarding the information in this report please contact us. This is to ensure that the recommendations and requirements of the report, especially regarding the surface drainage, are acknowledged and followed. This report is prepared for Apex Construction on 11150 North Ellicott Highway, El Paso County, Colorado. It is my understanding that a single-family residence is planned for this site. The site is currently vacant.

CONCLUSIONS

A satisfactory foundation for this structure is a properly designed shallow foundation system consisting of foundation components resting directly on undisturbed materials. Foundation components resting directly on undisturbed materials shall be designed for a loading of not greater than 1,000 pounds per square foot. Any design by any engineer is subject to revision based on the results of the open hole observation. The compressibility of this material is low. This bearing capacity is calculated with a safety factor of three. The type of foundation configuration used depends on the building loads applied. The depth of foundation elements shall be determined by the foundation engineer, but should be at least as deep as the minimum depth required by the governing building authority. The laboratory testing revealed that the on-site soil is silty sand (U.S.C. Classification Symbol SM). The unit weight of equivalent fluid soil pressure of this material is 40 (SM) pounds per cubic foot. The owners shall be made aware that movement will occur if surface or subsurface water is allowed to collect around the foundation wall.

GENERAL

The investigation was made to reveal important characteristics of the soils and of the site influencing the foundation design. Also evaluated during the investigation were subsurface conditions that affect the depth of the foundation and subsequent loading design, such as ground water levels, soil types, and other factors which affect the bearing capacity of the soils. Design loadings are based on soils characteristics and represent the maximum permissible loads for these conditions.

FIELD AND LABORATORY INVESTIGATION

Two exploratory holes were drilled on January 22, 2018, at the location shown on the enclosed site map. The location of these test holes were determined by Apex Construction. The test holes was drilled with a 4-inch diameter auger. At intervals anticipated to be the foundation depths, and as determined by the soils conditions, the drill tools were removed and samples were taken by the use of a 2-inch split barrel sampler connected to a 140-pound drop-hammer. This hammer is dropped 30 inches to drive the penetration sampler into the soil (ASTM D-1586). The depths and descriptions of the materials encountered in each test boring at which the samples were taken are shown on the enclosed log sheets. All samples were classified both in the field and in the laboratory to evaluate the physical and mechanical properties of the materials encountered.

TOPOGRAPHY

The topography of this site is that of an incline sloping down towards the southeast at 3%.

WEATHER

The weather at the time of the soil examination consisted of clear skies with cold temperatures.

DESIGN AND CONSTRUCTION CONSIDERATIONS

Residential basement slabs-on-grade may move and crack. Vertical slab movement of one to three inches is considered normal for soils of low to moderate expansion potential and for compacted structural fill after removal of highly expansive soils. In some cases, vertical movement may exceed this range. If movement and associated damage to basement floors and finish cannot be tolerated, a structural floor system should be installed. If compaction is not performed, settlement may occur causing cracking of foundation walls and floors. Soil located beneath concrete walls shall be compacted to at least 95% Modified Proctor density. Soil located beneath concrete floors shall be compacted to at least 85% Modified Proctor density. Special care is to be taken to re-compact the material above utility lines to a minimum of 85% Modified Proctor density. During construction, conditions that could cause settlement shall be eliminated. Interior non-bearing partition walls shall be constructed such that they do not transmit floor slab movement to the roof or overlying floor. The gap or void (1.5" min.) installed in these non-bearing partitions may require re-construction over the life of the structure to re-establish the gap or void to allow for vertical slab movement. Stairwells, doorways and sheeted walls should be designed for this movement. The following are general recommendations of on-grade slabs:

- Slabs shall be placed on well-compacted, non-expansive materials, and all soft spots shall be thoroughly excavated and replaced with non-expansive fill materials as stated above.
- Separate the slab from all foundation walls, load bearing members, and utility lines.
- 3. At intervals not to exceed 12 feet in each direction, provide control joints to reduce problems with shrinkage and curling as recommended by the American Concrete Institute (ACI). Moisten the ground beneath the slab prior to placement of concrete.
- 4. All concrete placed must be cured properly as recommended by the American Concrete Institute (ACI). Separate load bearing members from slabs, as discussed above. Care must be exercised to prevent excess moisture from entering the soil under the structure, both during and after construction.

DESIGN AND CONSTRUCTION CONSIDERATIONS (CONTINUED)

- 5. Due to the exposure of exterior concrete to variations in moisture fluctuations, heaving and cracking of exterior slabs-on-grade should be expected. Placement of at least 3 feet of non-expansive fill beneath the slabs can help to reduce the impact of differential movement and cracking but may not eliminate movement.
- 6. The soil has been analyzed for its expansion and/or consolidation potential. Basement slabs, garage slabs, and all concrete floor slabs, however, exert a very low dead-load pressure on the soil. Since this soil contains at least a small amount of expansion potential, slabs will crack and heave or settle if excess water is allowed to penetrate the sub-grade. For example, column openings to pads below the placed slab, if exposed to precipitation during construction, will conduct water to the sub-grade, possibly causing it to expand. Also, if the slab is placed with concrete too wet, expansion may occur. We recommend 3,000 psi concrete placed at a maximum slump of 4 inches.

RECOMMENDATION REMARKS

The recommendations provided in this report are based upon the observed soil parameters, anticipated foundation loads, and accepted engineering procedures. The recommendations are intended to minimize differential movement resulting from the heaving of expansive soil or from the settlement induced by the application of loads. It must be recognized that the foundation will undergo some movement on all soil types. In addition, concrete floor slabs will move vertically, therefore, adherence to those recommendations which isolate floor slabs from columns, walls, partitions or other structural components is extremely important, if damage to the superstructure is to be minimized. Any subsequent owners should be apprised of the soil conditions and advised to maintain good practice in the future with regard to surface and subsurface drainage and partition framing, drywall and finish work above floor slabs.

Geoquest, LLC does not assure that the contractor and/or homeowner will comply with the recommendations provided in this report. Geoquest, LLC provides recommendations and requirements only and does not supervise, direct or control the implementation of such.

COLD TEMPERATURE CONSIDERATIONS

- 1. Concrete shall not be placed upon frozen soil.
- 2. Concrete shall be protected from freezing until it has been allowed to cure for at least 7 days after placement in forms.
- 3. Snow or other frozen water shall not be allowed in the forms during placement of concrete.

COLD TEMPERATURES CONSIDERATIONS (CONTINUED)

- 4. Concrete shall be cured in forms for at least 72 hours.
- 5. The site shall be kept well drained at all times.

SURFACE DRAINAGE

After construction of foundation walls, the backfill material shall be well compacted to 80% Modified Proctor density, to prevent future settlement. Any areas that settle after construction shall be filled to eliminate ponding of water adjacent to the foundation walls. The finished grade shall have a positive slope away from the structure with an initial slope of 6" in the first 10'. If a 10' zone is not possible on the upslope site of the structure, then a well-defined swale should be created a minimum of 5' from the foundation and sloped parallel with the wall at a 2% grade to intercept the surface water and carry it around and away from the structure. Homeowners shall maintain the surface grading and drainage installed by the builder to prevent water directed in the wrong direction. All downspouts shall have splash blocks that will remove runoff to outside the foundation area and carried across backfill zones. No irrigation devices shall be placed within 7' of the foundation. Shrubs and plants requiring minimal watering shall be established in this area. Irrigated grass shall not be located within 5' of the foundation. Sprinklers shall not discharge water within 5' of the foundation. Irrigation should be limited to the minimum amount sufficient to maintain vegetation. Application of more water will increase likelihood of floor slab and foundation movement.

SUBSURFACE DRAINAGE

The necessity for perimeter drains will be determined at the time of the Open Hole Observation.

REINFORCING

The concrete foundation walls shall be properly reinforced as per the specific design for this foundation by a Professional Engineer. Exact requirements are a function of the design of the structure. Questions concerning the specific design requirements shall be referred to the design engineer.

FOOTING DESIGN

The design for footings for this structure is determined by applying the dead load and full live load to the foundation walls.

CONSTRUCTION DETAILS

It is necessary with any soils investigation to assume that the materials from the test holes are representative of the materials in the area. On occasion variations in the subsurface materials do occur, therefore, should such variations become apparent during construction, the owner is advised to contact this office for a determination as to whether these variations will affect the design of the structure's foundation. If clay layers are observed during the excavation for the dwelling, this office should be contacted to determine whether the layers will adversely affect the design.

MINIMUM MATERIALS SPECIFICATIONS

- 1. Minimum materials specifications of the concrete, reinforcing, etc., shall be determined by the Professional Engineer.
- Compact beneath foundation walls a minimum of 95% Modified Proctor density to prevent settlement.
- 3. Compact all back-fill material located around the perimeter of the foundation to a minimum of 80% Modified Proctor density.
- 4. Concrete shall be vibrated or rodded in forms to avoid segregation and cold joints.
- 5. The site shall be kept well drained at all times.

OPEN HOLE OBSERVATION (added cost)

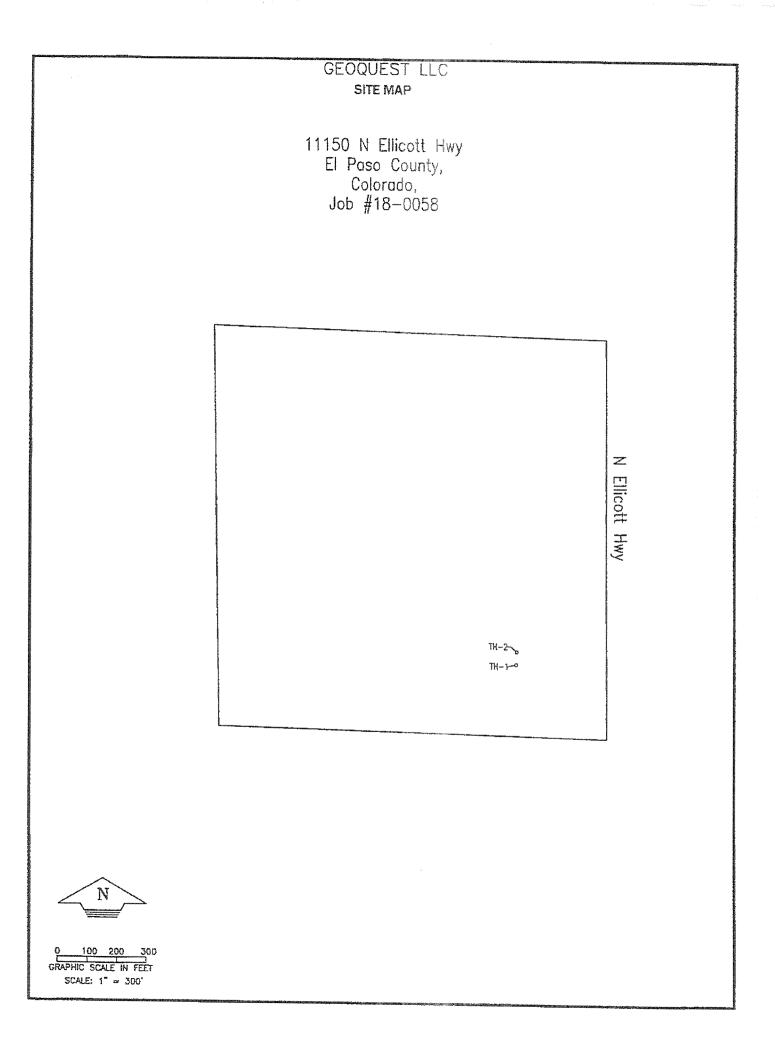
If anyone other than Geoquest performs the Open Hole Observation, that person/company assumes liability for the soils, and any possible changes to the foundation design.

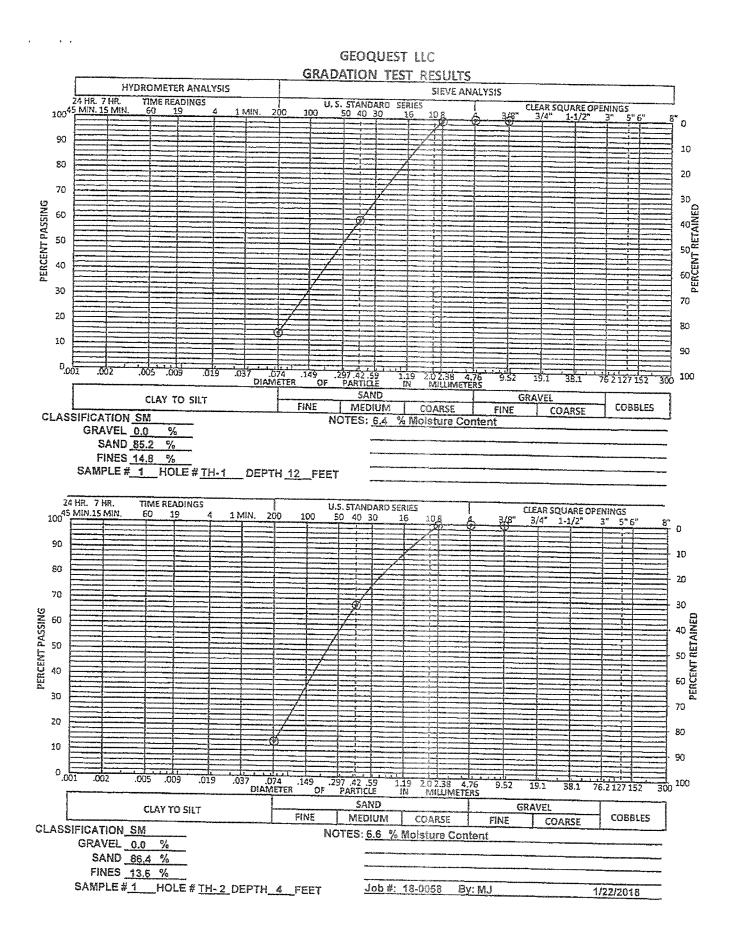
The owner, or a representative of the construction company shall contact Geoquest, LLC. a minimum of 24 hours prior to excavating for the foundation. An Open Hole Observation must be performed on each individual structure prior to the placement of concrete, and preferably prior to the placement of forms in the excavated area. The failure to request or obtain an Open Hole Observation prior to the placement of foundation components may result in this Soils Report being declared null and void. This is to ensure that soft areas, anomalies, etc., are not present in the foundation region. At the time of the open hole observation the foundation type recommendations, maximum allowable bearing capacity may be revised according to soil conditions found at that time. If revisions are made to the Soils Report Due to the soil conditions of the excavation, the Foundation Design Engineer must be notified of all revisions.



DRILL LOGS

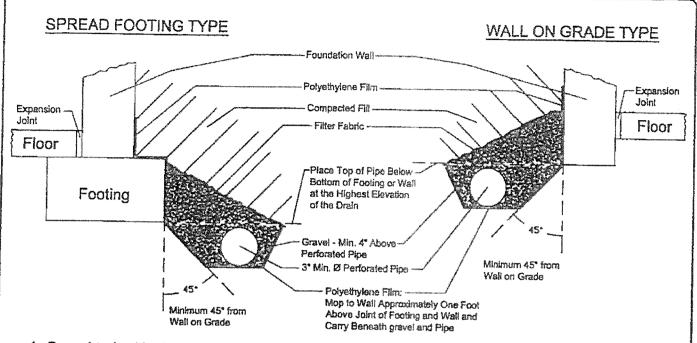
JOB #: 18-0058 TEST BORING NO.: TH-1 DATE: 1/22/2018	DEPTH (in ft.)	TOBMYS	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE	TEST B NO.: T	 #: 18-0058 ORING H-2 1/22/2018 	DEPTH (in ft.)	SYMBOL	SAMPLES	BLOW COUNT	WATER %	SOIL TYPE
<u>O"-6" Topsoil</u> <u>6"-15' Sand (SM)</u> Fine-coarse grained Low-moderate density Low-moderate moisture content Low clay content Low plasticity Brown color	2 -			8 12"	3.8		Fine-cc Low-m Low-m conten Low cla	Sand (SM) parse grained oderate density oderate moisture t ay content asticity	2 -			<u>9</u> 12"	6.6	SM
	10- 12- 14- 16- 18-			<u>15</u> 12"	6.4	SM			10-			<u>15</u> 12"	4.9	
	20-								18- 20-					







EXTERIOR DRAIN DETAIL



1. Gravel to be Not More Than 1-1/2" and Not Less Than 1/2" Diameter.

2. Perforated Pipe Diameter Varies With Expected Seepage. 3"Ø and 4"Ø are Most Common. ABS and PVC are Most Common Materials for Pipe.

3. Pipe to be Laid out in a Minimum Slope of 1" in 10'.

4. Gravity Outfall is Desired if Possible. Portion of Pipe in Area Not Drained Shall be Non-Perforated. Daylight Must be Maintained Clear of Debris in Order to Function Properly.

5. If Gravity Outfall is Not Possible, Provide a Sump With Operational Pump. Pump May Not Connect to Any Sanitary or Storm Sewer.

6. Soil Backfill Should be Compacted to at Least 80% of the Modified Proctor Denisty in the Upper Three Feet of Fill.

7. Filter Fabric to be Mirafi 140s or Approved Equivalent. Roofing Felt and Sheet Plastic are Not Acceptable.

8. Drain Pipe Shall be Laid Below Protected Area, as Shown in The Detail Above.

9. Mop Polyethylene Film to Wall Approximately One Foot Above Joint of Footing and Wall and Carry Beneath Gravel and Pipe.

10. The Polyethylene Film Shall be Continued to the Edge of the Excavation.

LIMITATIONS

This report is issued based on the understanding that the owner or his representative will bring the information, data, and recommendations contained in this report to the attention of the project engineer and architect, in order that they may be incorporated into the plans for the structure. It is also the owner's responsibility to ensure that all contractors and sub-contractors carry out these recommendations during the construction phase.

This report was prepared in accordance with generally accepted professional geotechnical/engineering methods. However, Geoquest, LLC makes no other warranty, express or implied, as to the findings, data, specifications, or professional advice rendered hereunder.

This report is considered valid as of the present date. The owner acknowledges, however, that changes in the conditions of the property might occur with the passage of time, such as those caused by natural effects or man-made changes, both on this land and on abutting properties. Further, changes in acceptable tolerances or standards might arise as the result of new legislative actions, new engineering advances, or the broadening of geotechnical knowledge. Thus certain developments beyond our control may invalidate this report, in whole or in part.

This report and its recommendations do not apply to any other site than the one described herein and are predicated on the assumption that the soil conditions do not deviate from those described. In the event that any variations or undesirable conditions should be detected during the construction phase or if the proposed construction varies from that planned as of this report date, the owner shall immediately notify Geoquest, LLC in order that supplemental recommendations can be provided, if so required. APPENDIX E: Soil Survey Descriptions

El Paso County Area, Colorado

8-Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 85 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Flats, hills Landform position (three-dimensional): Side slope, talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 5 percent
Available water storage in profile: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: Sandy Foothill (R049BY210CO) Hydric soil rating: No **Minor Components**

Other soils Percent of map unit: Hydric soil rating: No

Pleasant Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017



El Paso County Area, Colorado

10-Blendon sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 3671 Elevation: 6,000 to 6,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Blendon and similar soils: 85 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blendon

Setting

Landform: Alluvial fans, terraces Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium derived from arkose

Typical profile

A - 0 to 10 inches: sandy loam Bw - 10 to 36 inches: sandy loam C - 36 to 60 inches: gravelly sandy loam

Properties and qualities

Slope: 0 to 3 percent Depth to restrictive feature: More than 80 inches Natural drainage class: Well drained Runoff class: Low Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Frequency of ponding: None Calcium carbonate, maximum in profile: 2 percent Available water storage in profile: Moderate (about 6.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: B Ecological site: Sandy Foothill (R049BY210CO) Hydric soil rating: No **Minor Components**

Other soils Percent of map unit: Hydric soil rating: No

Pleasant Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017



El Paso County Area, Colorado

28—Ellicott loamy coarse sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 3680 Elevation: 5,500 to 6,500 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 47 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Ellicott and similar soils: 85 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ellicott

Setting

Landform: Flood plains, stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium

Typical profile

A - 0 to 4 inches: loamy coarse sand C - 4 to 60 inches: stratified coarse sand to sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Frequent
Frequency of ponding: None
Available water storage in profile: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A Ecological site: Sandy Bottomland LRU's A & B (R069XY031CO) Other vegetative classification: SANDY BOTTOMLAND (069AY031CO) Hydric soil rating: No Map Unit Description: Ellicott loamy coarse sand, 0 to 5 percent slopes—El Paso County Area, Colorado

Minor Components

Fluvaquentic haplaquoll

Percent of map unit: Landform: Swales Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017



El Paso County Area, Colorado

96-Truckton sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 36bf Elevation: 6,000 to 7,000 feet Mean annual precipitation: 14 to 15 inches Mean annual air temperature: 46 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Prime farmland if irrigated and the product of I (soil erodibility) x C (climate factor) does not exceed 60

Map Unit Composition

Truckton and similar soils: 85 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Truckton

Setting

Landform: Flats Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Arkosic alluvium derived from sedimentary rock and/or arkosic residuum weathered from sedimentary rock

Typical profile

A - 0 to 8 inches: sandy loam Bt - 8 to 24 inches: sandy loam C - 24 to 60 inches: coarse sandy loam

Properties and qualities

Slope: 0 to 3 percent Depth to restrictive feature: More than 80 inches -Natural drainage class: Well drained Runoff class: Very low Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water storage in profile: Low (about 5.7 inches)

Interpretive groups

Land capability classification (irrigated): 2e Land capability classification (nonirrigated): 3e Hydrologic Soil Group: A Ecological site: Sandy Foothill (R049BY210CO) Hydric soil rating: No Map Unit Description: Truckton sandy loam, 0 to 3 percent slopes-El Paso County Area, Colorado

Minor Components

Other solls Percent of map unit: Hydric soil rating: No

Pleasant Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017 APPENDIX F: El Paso County Health Department Septic Records

3200000143 EL PASO COUNTY DEPARIMENT OF HEALTH AND ENVIRONMENT Permit # 4379 TNDIVIT THIL SEWAGE DISPOSAL SYSTEM INSPECTION FORM Date 8/22/02 APPROVED: YES ____ NO ____ (Repair/Addition) ENVIRONMENTALIST D. Ficky___ Address 11150 Ellicott HWY Owner Alysia Baing Legal Description <u>Sivily of NE 1/4</u> Sec. 24 TW 12 R 63 W of the 6th P.M. Residence , # of bedrooms 7; Commercial ; System Installer <u>Rudge</u> SEPTIC TANK: Commercial : Noncommercial , L , W , WD Construction Material _______ Precast concrete , capacity ______ gallons. DISPOSAL FIELD: Rock Systems:

 Rock systems.

 Trench: depth _____, width _____, total length _____, sq. feet ______

 Bed: depth ______, length _____, width _____, sq. feet ______

 Rock type ______, depth _____, under PVC _____, over PVC ______

 Seepage Pits: # of pits ______, total # of rings ______, working depth(s) ______

 size of pit(s) L X W ______, lining material ______, total sq. feet ______

 Rockless Systems: Rockless Systems: Chamber: Type <u>Milleritation</u>, number of chambers <u>44</u>, bed <u>trequired</u>, trench <u>sq. ft./section</u>, reduction allowed <u>40 %</u>, sq. ft required <u>1127</u> total sq. ft. installed <u>1136</u>, depth of installation <u>36"-40"</u> Engineer Design Y or (N), Designing Engineer Approval letter provided? Y or N Well 50 feet from tank (f) or N 100 feet from leach field Oor N Well installed at time of septic system inspection (f) or N Public Water *Approval will be revoked if in the future the well is found to be within 50 feet of the sentic tank and/or 100 feet of the disposal field. feet of the septic tank and/or 100 feet of the disposal field. NOTES: pipe= 4"SDR 35, 4" Well (asing specified on drawing * Existing leach field was abandoned. New leach field installed in same low from C UJJLL Sang. Act of the bien mounte SH_ Witch white mobile SH Wneil Blue Mobile DEEVERIA मुग र्षसी Bank SHED Mobile which & Olice 13 Mubile ųĽ 741 4C .1 s:" 101 Uz

		1 % W
INTERVIDUAL SEWAGE DISPOSAL SYSTEM PERMIT OWNER NAME: ASSA BONGL ADDRESS: HIGHLICOTT HWY OWNER NAME: HIGHLICOTT HWY BYSTALLED BY: HIGHLICOTT HWY BYSTALLED BY: Marchine and the control of the second processing of the second procesent of the second procesecond processing of the second processing	DEPARTMENT OF HEALTH AN	• • •
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	THIS PERMIT DOES NOT DENOTE APPROVAL OF ZONING	AND ACREAGE REQUIREMENTS.
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	DIRECTOR, EL PASO COUN	ITY DEPARTMENT OF HEALTH AND ENVIRONMENT
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	FOR ADMINISTRATIVE Permit Ready 6102 24 K Called Final Inspection Requested: BY: J. Chica Dally Date	Called In: 42102 2:1-102
	FOR ADMINISTRATIVE Permit Ready 6102 24 K Called Final Inspection Requested: BY: J. Chica Dally Date	Called In: 42102 2:1-102

A17
Inspector JANET UID Record I.D. <u>A379</u>
EL PASO COUNTY ENVIRONMENTAL HEALTH SERVICES
301 South Union Boulevard • Colorado Springs, CO • 80910-3123 • (719) 578-3126 • Fax: (719) 578-3188
RC FOLLS VIES 1801
APPLICATION FOR AN ON-SITE TREATMENT SYSTEM:
Wher <u>MIUSITE</u> DOING OF BIEGERICA Dayame Phone <u>S.V.C. doubs</u>
Address of Property 11150 ElliCott Hur City'& Zip Calilan's 80805
Legal Description 56 1/4 of NE 1/4 Sec. 24, TU 12 Range 63'W: 6th PM
Owner's MAILING Address <u>11150 Ellicott</u> Hur City, State & Zip Calhan CO 80808
Lot Size <u>40 HCR</u> Tax Schedule # <u>3200000/43</u> -Mark 337-6882
Septic Contractor <u>KUNACL</u> Daytime Phone # <u>663-3730</u>
Type of Building: Frame Modular Mobile Commercial Manufactured Oother
Water Supply: Well or Spring Cistern Public Inside City Limits: No Yes-City
MAIL PERMIT OR PERMIT THERE IS AN ADDITIONAL RESIDENCE ON THIS PROPERTY
MAXIMUM POTENTIAL BEDROOMS
Percolation Test Attached N Garbage Disposa Y N Basement Y N Clothes Washer Y N
represented to be true and correct to the best of my knowledge and belief, and are designed to be relied on by the El Páso County Department of Health and Environment in evaluating the same for purposes of issuing the permit applied for herein. I further understand any falsification or misrepresentation may result in the denial of the application or revocation of any permit granted based upon said application and in legal action for perjury as provided by law. <u>OWNER'S SIGNATURE</u> <u>Determined and Kathur</u> Determined and State Signed Determined and State Signed Determined Determi
DEPARTMENT OF HEALTH USE ONLY
See Belon Existing 1250 gelon 2A-g. 200 2 Minimum Abscription Area Minimum Tank Capacity Date of Site Inspection
REMARKS Owner wonts to size for future 7 bedroom, -
- 5 mobile hemer 3 are fixed in I does not have alumbar
- beach field was dry pool of septic master water of top
at septic tank,
<u> </u>
EHS INSPECTOR Junet (Mustersen DATE 08/02/02 (APPROVED) DENIED
FEE AS OF 8/1/00: NEW CONSTRUCTION \$315. + County Surcharge of \$30. = \$345.00
MAJOR REPAIR/ADDITION \$150 -DATE TO PLANNING / WASTEWATER- MINOR REPAIR/ADDITION \$75 DATE TO FLOODPLAIN:

1) We require an original of your <u>PERCOLATION (PERC) TEST</u> with an original professional engineer's (PE) stamp and signature as well as a plot of the percolation test holes. 2) PROPERT NUMBER MUST BE POSTED AND CLEARLY VISIBLE FROM ROAD. PE STATES 3) A **PLOT P** FIU HEALTH INCLINE to scale) on an 8 ½ x 11 sheet of paper. The plot plan must include: uildings (proposed or existing) 7) driveway (proposed or 2) property in the second osed septic system site existing and name of 3) property in Alasta nate septic system site adjoining street) 4) Initial any astronomy that apply to your property and **INCLUDE** them on your **PLOT** DATE 08.01 PLAN. T Well djacent property well(s) MDA-ADD H ____ Subsoil drain - -3165 Ciste 1505 150 \$150:00 Vater line 5) Initial any c50000111 \$150.00 thin 100 feet of your proposed septic system and INCLUDE on your PLOT PL TOTAL \$150.00 CHECK \$150.00 Lake(s) BRENDA MD. 000019 Stream(s) Natural drainage course(s) 6) GIVE COMPLETE DIRECTIONS TO THE PROPERTY FROM A MAIN HIGHWAY Highway 24 To Ellicott Hur South 3 miles 2nd right south of scott Rol. Highway SI S'I YOSIX 714 2211 \$.40L 512,512,05 P9L