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PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT

FALCON STORAGE SUBDIVISION

PART OF THE SW1/4 SECTION 1, T.13S.. R.65W. OF THE 6TH P.M.

EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

PCD File No. PPR2232

Please also add PCD File No. MS232

Prepared for

Falcon Storage Partners LLLP

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

Due to the type and quantity of comments provided additional comments may be generated on the resubmittal.

OLIVER E. WATTS, PE-LS

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Celebrating over 41 years in business

November 23, 2022

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report

Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments.

Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

Oliver E. Watts, President

BY:

FALCON STORAGE SUBDIVISION DRAINAGE REPORT TABLE OF CONTENTS

Drainage Report 5 pages
Computations, 7 pages
Vicinity Map
FEMA Panel No. 08041C0553 G
SCS Soils Map and Interpretation Sheet
Backup Information, 4 sheets
Falcon DBPS Map
Drainage Plan, Falcon Meadows at Bent Grass
Drainage Plan, Latigo Business Center
Drainage Plan, Dwg 02-5523-04

FALCON STORAGE SUBDIVISION DRAINAGE REPORT REFERENCES

City-County Drainage Criteria, current edition
Fema Firm Insurance Rate Map
El Paso County Soils Survey, SCS
Falcon Drainage Basin Planning Study
Drainage Report, Falcon Meadows at Bent Grass
Drainage Report, Latigo Business Center, Lot 1

1. ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

	s or omissions on my part in p	repairing this report.	
Oliver E. Watts, Co	nsulting Engineer, Inc.		
Oliver E. Watts	Colo. PE-LS No. 9853	date	
2. OWNERS / DE	VELOPER'S STATEMENT		
I the owner / develo drainage report and	per have read and will comply plan.	with all of the requirement	s specified i
Falcon Storage Part	ners LLLP		
Ву:			
Richard Graham 4615 Northpark Dri	vo.	Date	
Colorado Springs, C			
3. EL PASO COU	NTTV.		
S. EL PASO COU	ur.		
Filed in accordance	with the requirements of the H	l Paso Land Development (Code, Draina
Criteria Manual Vol	umes 1 and 2, and the Engine	ering Criteria Manual, as an	nended.
		io .	
		147	
Joshua Palmer, P.E. County Engineer / E		date	
		date	

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-Manual, using the rational method for areas of the size of the deve enclosed for reference and review. Pertinent portions of the criter

The soils in the subdivision have been mapped by the local USDA interpretation sheet are enclosed for reference. All soils in this are within the development area.

Please see comments on the drainage plan regarding the conveyance of flows from the basins into the pond as portions of each of the basins do not reach the pond. Elaborate in your description of each of the basins and how the flow is conveyed to the pond and/or subsequent basin that will convey the flow to the pond.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary, and it indicates the historic undeveloped runoff of the site, totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Minor grading is indicated which is intended to contain the runoff into the interior drive isle street network. The site will be graded to route and contain all runoff within the private north-south streets, terminating at the south boundary. The westerly street (Basin A) will develop 4.1 cfs \ 11.8 cfs (5-year / 100-year runoffs) near the in the southwest corner of the plat. Basins B, C, and D will develop 5.9 cfs / 11.9 cfs in the easterly street near the southeast corner. The total outfall into full spectrum detention is required per criteria.

C. Detention Storage: At the proposed outfall point a detention pond is proposed Please state that. sized for sedimentation basins to be used during the construction period and converted into a sand filter basins upon completion. The basin will contain 13320 CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One

Please identify these as basins O-1 and AH in the narrative as shown on the drainage plan.

Temporary Sediment

Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling

throughout (example:

"Pond A" or

"Pond 1").

singular

18-inch (minimum) filter layer

Falcon Storage Subdivision Rreliminary and Final Drainage Plan and Report 4.1 cfs per the excerpt provided. revise accordingly

The underdrain system should be Temporary Sediment placed within an 5-inch-thick section of CDOT Class C filter

fool of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be modified to a sand filter basin, with one foot of sand in the bottom. A 4-inch underdrain will drain into the grated inlet outlet structures set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice sized for the installation. Detention basin stage-storage tables are included for each basin. slotted

C. Outfall Point: Discharge from the subdivision will be into existing north-south street of Lot 1 of the Latigo Business Center. Some minor construction is shown along the north boundary of Lot 1. The two properties are under common ownership. The drainage plan for this property is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 6.7 cfs / 10.1 cfs over the remaining south frontage.

WATER QUALITY

Water quality facilities will be provided as described above.

FOUR STEP PROCESS

outfall is and where the developments The following process has been followed to minimize adversation will be ultimately conveyed to.

Runoff Reduction: The scope of the development has been minimized consistent with zoning requirements to present the minimum footprint in providing a RV Storage development. The undisturbed portions are to be landscaped to reduce the impervious percent. Show these locations on the

Treat and Slowly Release: Detention storage is being provided downstream by others with sub regional facilities.

Identify that detention/WQCV is being provided by the sand filter detention pond as identified above.

for industrial and Commercial BMPs).

Per the drainage plan the spillway is

located in the landscape strip along

Bentgrass. The outfall pipe is not shown on the plan. Please clarify where the

Channel Stabilizing: \The site will be graded to route the runoff over improve provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision

Source Controls: This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of the revise the 4-step headings to match ECM Appendix I.7.2, (Runoff reduction, stabilize mitigate erosive problems. drainage ways, provide WQCV, Consider need

8 COST ESTIMATE.

o, COST Ex	TIMATE.	madoma and co	minorolal Bitt	. 6/1
Item No.	Description	Quantity	Unit Cost	Cost
1	Sand Filter Basin	1 ea	\$ 4000.00	\$ 4000.00
2	Grated inlet	1 ea	1800.00	1800.00
3	24" CMP drainage pipe	105 lf	40.00	4200.00
	Subtotal Construction Cost			\$ 10,000.00
	Engineering	10%		1,000.00

Please show on the drainage plan

These costs do not match the FAE please revise.

As the subdivision was submitted in Total Estimate 2023, the site is subject to the 2023 drainage basin fees (\$37,256 drainage & \$5,118 bridge). Please revise

\$11,000.00

9. FEES: At plat recording.

2021 Falcon Basin Fees: 5.004 acres @80% Impervious = 4.0032 Impervious acres

Drainage fees @ \$34,117 per acre = \$136,577.17

Bridge fees @ \$4,687 per acre = \$10,762.99

Total Fees: \$ 155,340.17

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

> Please identify and analyze whether the downstream facilities are adequate to accept the developments flows.

Additionally, compare the detained flows and the historical flow leaving the site. Indicate whether or not the sites flow is at or below historic flows leaving the site.

MAJOR BASIN	SUB BASIN	Al	REA	BA	SIN	Tc MIN	4	I /hr.	SOIL GRP	DEV. TYPE	(5-ry	OW 100-yr		TURN RIOD
		PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT								qp -CFS-	qp -CFS-	-years-	
FALCON	0-1	9.75	2.47	300	4.5	27			A	SF 5AC.	0.12	0.39				
			V=0.82	+480	1.3	+10										
		H TT				37	2.1	3.6			7		0.62	3.5	5	100
HISTORIC	A	COGO	5.00	+525	9	+13	100					*:				
			V=0.65			50	1.8	2.8	A	R/L	0.08	0.35				
	TOTAL		7.47			. 61				MIX	0.093	0.362	1.25	7.6	5	100
DEVELOPED	A	COGO	1.68	300	2.5	15.2		10-11	A	GRAVEL	0.59	0.70			5	100
			V=3.06	+300	7	+1.6										
						16.8	3.2	5.5	11 27 11				3.2	6.5	5	100
	01 + A	(DP-1)	4.15	=400	8	+2	3.2	5.5	A	MIX	0.310	0.516				
		1	V=2.82			52	1.7	2.9			1		2.1	6.2	5	100
	В	cogo	0.66	370	2.4	16.4			A	GRAVEL	0.59	0.70	1.3	2.5	5 -	100
	C	COGO	2.30	300	4	14.5			A	GRAVEL	0.59	0.70				14
		0000	V=2.66	+340	6	+2.1				1						
			1			16.6	3.3	5.5	7.5.5.7		1.18		4.5	8.9	5	100
	B+C			+360	8	+2.7		1							1111	
		(DP-2)	2.96			19.3	3.0	5.1	Α	GRAVEL	0.59	0.70	5.2	10.4	5	100
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	Α	GRAVEL	0.59	0.70	0.8	1.6	5	100
	B+C+D		V=2.22	+50		+0.4	100	11			200					
	7	(DP-3)	3.32			19.7	3.0	5.1	A	GRAVEL	0.59	0.70	5.9	11.9	5	100
	+0-1+A		7.47	+240	2.4	+2	761	+ -1			11:39:E					
						54	1.7	2.8	A	MIX	0.434	0.598	5.5	12.5	5	100
	1		UTATION					1-14							DA	GE 1

HYDROLOGICAL COMPUTATION – BASIC DATA LCON STORAGE SUB BY: O.E. WATTS

PROJ: FALCON STORAGE SUB RATIONAL METHOD

DATE: 2/4/21 10/17/22 11-21-21

OLIVER E. WATTS, CONSULTING ENGINEER, INC.
614 ELKTON DRIVE COLORADO SPRINGS, CO 80907

Flows for DP1 do not match the drainage plan nor the table on the drainage plan for DP1. Revise accordingly.

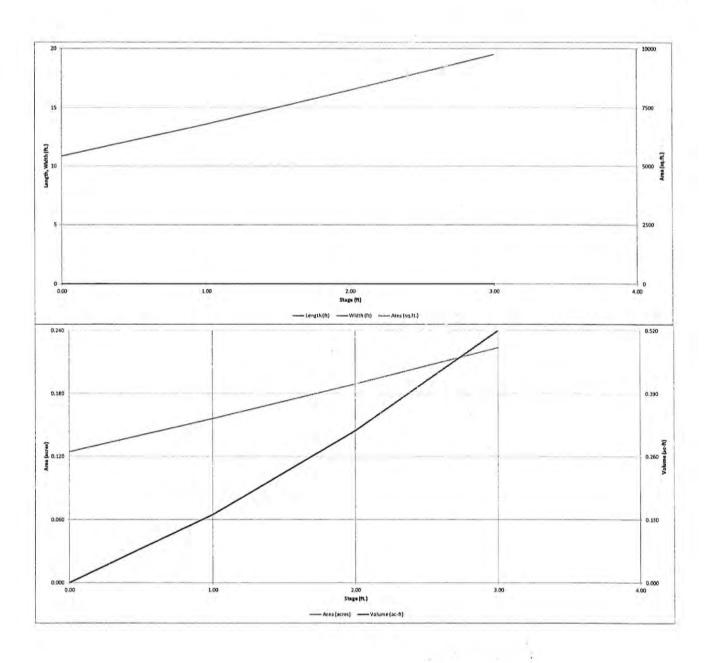
see comment on drainage map regarding total flow at the pond and revise accordingly.

OF >

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022) Project: Falcon Storage Sub. provide calculation as Basin ID: Basins O-1 AND A-D to how this was determined Optional Example Zone Configuration (Retention Pend) Length Volume Description (ft) Stage (ft) (ft) (ft) (ft 1) Area (ft 1 (acre) (R3) (ac-ft) Watershed Information Media Surface 5,432 0.125 Selected BMP Type = Note: L / W Patto > 8 1.00 6,800 0.156 6,116 0.140 L / W Batlo = 8.27 Watershed Area -7.47 2.00 8,240 0.189 13,636 0.313 Watershed Length 1,640 3.00 9,752 0.224 22,632 0.520 Watershed Length to Centrold = 790 Watershed Slope Watershed Imperviousness = 64,00% Percentage Hydrologic Soil Group A = 100.0% percent Percentage Hydrologic Soil Group B • 0.0% ercent Percentage Hydrologic Soil Groups C/D = ercent Target WQCV Drain Time = 12.0 Location for 1-hr Rainfall Depths - User Inpu After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure. Optional User Overrides Water Quality Capture Volume (WQCV) = 0.125 acre-feet Excess Urban Runoff Volume (EURV) = acre-feet 2-yr Runoff Volume (P1 = 1.19 in.) = 0.438 1.19 5-yr Runoff Volume (P1 = 1.5 in.) = 0.575 scre-feet 1.50 inches 10-yr Runoff Volume (P1 = 1.75 in.) = 0.685 scre-feet 1.75 inches 25-yr Runoff Volume (P1 = 2 in.) = acre-feet inches 0.829 2.00 50-yr Runoff Volume (P1 = 2.25 in.) = 0.971 Inches acre-feet 2.25 100-yr Runoff Volume (P1 = 2.52 in.) = 1.145 2.52 500-yr Runoff Volume (P1 = 3.14 in.) = 1.523 acre-feet inches Approximate 2-yr Detention Volume = 0.384 acre-feet Approximate 5-yr Detention Volume = 0.502 acre-feet Approximate 10-yr Detention Volume = 0.606 ocre-feet Approximate 25-yr Detention Volume = acre-feet Approximate 50-yr Detention Volume = 0.605 acre-feet Approximate 100-yr Detention Volume = 0.883 acre-feet Define Zones and Basin Geometry Select Zone 1 Storage Volume (legulred) Select Zone 2 Storage Volume (Optional) acre-feet Select Zone 3 Storage Volume (Optional) = acre-feet Total Detention Basin Volume acre-fee Initial Surcharge Volume (ISV) N/A Initial Surcharge Depth (ISD) NYA Total Available Detention Depth (Hussi) Depth of Trickle Channel (Hrc) N/A Slope of Trickle Channel (STC) N/A n/n Slopes of Main Basin Sides (Sman) user Basin Length-to-Width Ratio (Ruw) Please fill out the user Initial Surcharge Area (Attv) = Surcharge Volume Length (Lsv) = zones (i.e. WQCV, Surcharge Volume Width (Way) = user Depth of Basin Floor (H_{FLOOR}) : user user EURV-zone 1, Length of Basin Floor (L_{FLDOR}) Width of Basin Floor (W_{FLOOR}) user 100yr-Zones 1 & 2) Area of Basin Floor (AFLOOR) = user Volume of Basin Floor (VFLOOR) User Depth of Main Basin (H_{MAIN}) user Length of Main Basin (L_{MAIN}) = Width of Main Basin (W_{MAIN}) Area of Main Basin (Amain) = user Volume of Main Basin (VHAIN) user Calculated Total Basin Volume (Visit) =

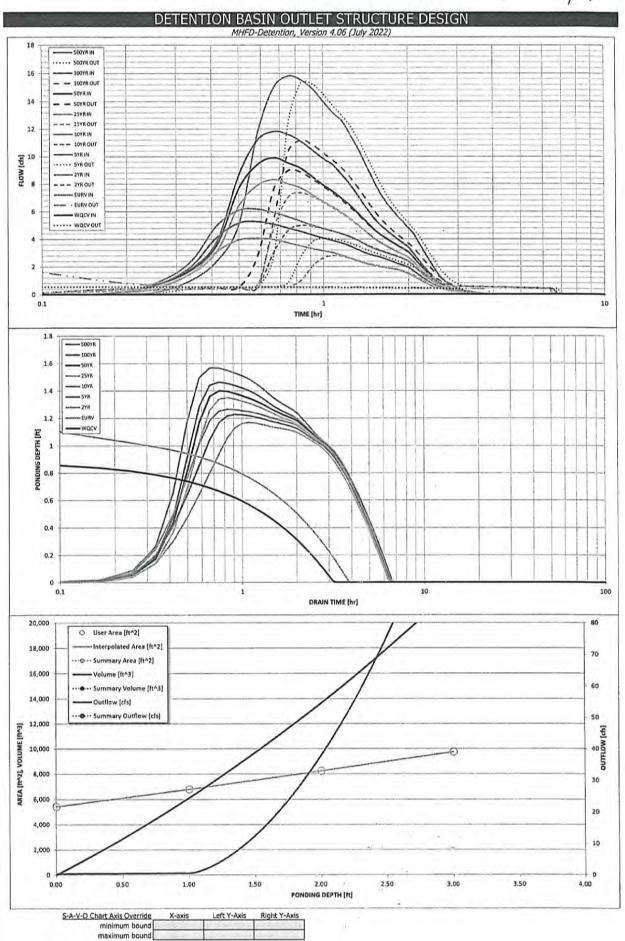




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	Falcon Storage Su		ectrum de						
Basin ID:	Basins O-1 AND A-	-D	ease also	provide t	he UD-BN	1P			
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20HE I AND 2	ORIFICE	fu	rther revie	w and po	ssible cor	nments			
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User Input: Orifice Plate with one or more orific	es or Elliptical Slot		the second secon	Charles and a second of the case	imentation BMP)	COLUMN C	Calculated Parame		
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Depth at top of Zone using Orifice Plate =			n bottom at Stage =	= 0 ft)	Inches India	ptical Half-Width =		feet	
Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =		inches sq. Inches				cal Slot Centroid = Iliptical Slot Area =	N/A N/A	feet ft ²	
Office Plate. Office Area per Now =		lad. menea				ilipucai siot Area –	190	iic.	
User Input: Stage and Total Area of Each Orific	e Row (numbered f	from lowest to high	nest)						
	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centrold (ft)		F-15-5-							
Orifice Area (sq. inches)	2						S V V	2000	1
The second second second	2 2 (X		T 200 11 (0000000)		Dec. 12 (-0-0-0)	Daniel Stanfords	Day of the street	Day 15 toutour	1
Stage of Orifice Centroid (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	-
Orifice Area (sq. inches)	7 - 1								1
User Input: Vertical Orifice (Circular or Rectang	The second secon		-	015			Calculated Parame	ters for Vertical Or	ifice
Martin and Alia when	Not Selected	Not Selected	100.750		19 C. 1		Not Selected	Not Selected	1
Invert of Vertical Orifice =				n bottom at Stage	- 20 Carl Att. 1 Carl Att.	tical Orifice Area =			ft²
Depth at top of Zone using Vertical Orifice = Vertical Orifice Diameter =			inches	n bottom at Stage	= 0 rt) Vertical	Orifice Centroid =			feet
vertical Offlice Diameter =	-		Jinches						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Re	ctangular/Trapezoid	tal Weir and No Ou	tlet Pipe)		Calculated Parame	eters for Overflow \	Weir
	Not Selected	Not Selected	F 195 LST 17				Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =			The first court of the state of the state of the	bottom at Stage = 0		Upper Edge, H ₁ =	- 10		feet
Overflow Welr Front Edge Length =			feet			eir Slope Length =			feet
Overflow Weir Grate Slope =			HIV		rate Open Area / 10				
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Debris Clogging % =			96		overnow orace oper	in race my bearing -			Tire
	1-1-0-2-1								
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, F	Restrictor Plate, or	Rectangular Orifice)		Ca	iculated Parameter	s for Outlet Pipe w	Flow Restriction F	Plate
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Depth to Invert of Outlet Pipe =				asin bottom at Stage		utlet Orifice Area =			ft ²
Circular Orifice Diameter =		10 10 100	Inches	Half-Can	tral Angle of Restric	t Orifice Centroid =	N/A	N/A	feet
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User Input: Emergency Spillway (Rectangular or	Trapezoidal)						Calculated Parame	eters for Spillway	
Spillway Invert Stage=		ft (relative to bas	in bottom at Stage	= 0 ft)	Spillway D	esign Flow Depth=	0.53	feet	
Spillway Crest Length =	10.00	feet prov	vide spillway	riprap	Stage at 1	Top of Freeboard =	2.53	feet	
Spillway End Slopes =	3.00		culations. Sho	ow detail		Top of Freeboard =		acres	
Freeboard above Max Water Surface =	1.00	Jfeet and	riprap grada	tion on	Basin Volume at 1	Top of Freeboard =	0.42	acre-ft	
			C Plans						
Routed Hydrograph Results	The user can over	ride the default CL	JHP hydrographs an	d runoff volumes b	y entering new valu	es in the Inflow Hy	rdrographs table (C	olumns W through	AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	N/A 0.125	0.591	1.19 0.438	0.575	1.75 0.685	2,00 0.829	2.25 0.971	2.52 1.145	3.14 1.523
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.438	0,575	0.685	0.829	0.971	1.145	1.523
CUHP Predevelopment Feak Q (cfs) =	N/A	N/A	0.0	0.0	0.1	0.6	1.3	2.2	4.1
OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A N/A	N/A N/A	0.00	0.01	0.01	0.09	0.17	0.29	0.54
Peak Inflow Q (cfs) =	N/A	N/A	4.1	Y 5.X Y	6.2	8.3	1.9	11.8	15.8
Peak Outflow Q (cfs) =	0.6	61.8	2.8	4.1	5.0	7.4	9.0	11.2	15.3

Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = N/A Filtration Media N/A N/A Spillway 11.4 Spillway N/A 6.9 Spillway N/A N/A Spillway Spillway Spillway N/A Spillway N/A Spillway N/A N/A Max Velocity through Grate 1 (fps) = N/A N/A N/A Max Velocity through Grate 2 (fps) = N/A N/A 3 Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = 4 6 6 1.27 0.16 0.182 1.35 0.17 0.195 0.91 0.15 0.126 1.12 0.16 0.158 1.40 0.17 0.205 1.46 0.17 0.216 1.57 0.17 0.233 Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =

revise so that peak outflow is less than predevelopment flow. Design must comply for the full spectrum of storms.





DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.00	0.14
	0:15:00	0.00	0.00	0.40	0.65	0.80	0.54	0.68	0.66	0.96
	0:20:00	0.00	0.00	1.46	1.93	2.28	1.44	1.70	1.80	2.38
	0:25:00	0.00	0.00	3.10	4.12	4.97	3.10	3.55	3.81	5.08
1	0:30:00	0.00	0.00	3.94	5.18	6.11	6.41	7.66	8.63	11.65
	0:35:00	0.00	0.00	4.07	5.28	6.19	7.90	9.41	11.18	14.97
9	0:40:00	0.00	0.00	3.97	5.08	5.93	8.31	9.91	11.82	15.81
	0:45:00	0.00	0.00	3.73	4.80	5.62	8.01	9.52	11.60	15.55
	0:50:00	0.00	0.00	3.50	4.55	5.29	7.70	9.13	11.09	14.90
	1:00:00	0.00	0.00	3.29	4.29	5.00 4.77	7.19 6.71	8.50 7.91	9.84	13.20
	1:05:00	0.00	0.00	2.99	3.88	4.57	6.32	7.43	9.36	12.58
	1:10:00	0.00	0.00	2.79	3.70	4.37	5.89	6.90	8.62	11.55
	1:15:00	0.00	0.00	2.58	3.46	4.16	5.47	6.39	7.88	10.53
	1:20:00	0.00	0.00	2.38	3.21	3.88	4.99	5.82	7.06	9.40
	1:25:00	0.00	0.00	2.21	2.98	3.58	4.55	5.29	6.29	8.35
	1:30:00	0.00	0.00	2.08	2.82	3.34	4.10	4.76	5.59	7.41
	1:35:00	0.00	0.00	1.99	2.70	3.16	3.76	4.36	5.07	6.70
	1:40:00	0.00	0.00	1.91	2.54	3.01	3.49	4.04	4.66	6,15
	1:45:00	0.00	0.00	1.84	2.38	2.86	3.26	3.77	4.31	5.66
	1:50:00	0.00	0.00	1.76	2.23	2.72	3.05	3.52	3,98	5.22
	1:55:00	0.00	0.00	1.63	2.09	2.57	2.85	3.29	3.68	4.81
	2:00:00	0.00	0.00	1.49	1.94	2.38	2.66	3.06	3.39 2.94	4.41
	2:05:00	0.00	0.00	1.29	1,69	2.06 1.75	2,32 1.98	2.66	2.50	3.82
	2:15:00	0.00	0.00	0.92	1.20	1.46	1.65	1.89	2.08	2.69
	2:20:00	0.00	0.00	0.75	0.98	1.20	1.35	1.54	1.69	2.18
	2:25:00	0.00	0.00	0.61	0.79	0.98	1.08	1.23	1.34	1.71
	2:30:00	0.00	0.00	0.50	0.65	0.80	0.85	0.96	1.02	1.30
	2:35:00	0.00	0.00	0.41	0.54	0.68	0.68	0.76	0.80	1.01
	2:40:00	0.00	0.00	0.34	0.45	0.57	0.55	0.62	0.64	0.80
	2:45:00	0.00	0.00	0.29	0.38	0.47	0.45	0.51	0.51	0.64
	2:50:00	0.00	0.00	0.24	0.32	0.39	0.37	0.41	0.41	0.51
	2:55:00	0.00	0.00	0.20	0.26	0.33	0.30	0.34	0.32	0.40
	3:00:00	0.00	0.00	0.17	0.21	0.27	0.24	0.27	0.26	0.32
	3:05:00	0.00	0.00	0.14	0.18	0.22	0.20	0.22	0.21	0.26
	3:15:00	0.00	0.00	0.09	0.14	0.14	0.13	0.15	0.14	0.17
	3:20:00	0.00	0.00	0.07	0.09	0.11	0.11	0.12	0.11	0.14
	3:25:00	0.00	0.00	0.06	0.07	0.09	0.08	0.09	0.09	0.11
	3:30:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.07	0.08
	3:35:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	3:40:00	0.00	0.00	0.02	0.03	0.03	0.03	0.03	0.03	0.04
	3:45:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.02
	3:50:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0,00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Required Area per Row (in²)

					Depth at	Outlet (ft)			
	-	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73
	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87
€	0.6	4.51	2.31	1.53	1.13	0.89	0.72	0.61	0.52
(acre-ft)	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35
100	0.2	1.50	0.77	0.51	0.38	0.30	0.24	0.20	0.17
Volume	0.1	0.75~	0.39	0.26	0.19	0.15	0.12	0.10	0.09
믕	0.06	0.45	0.23	0.15	0.11	0.09	0.07	0.06	0.05
2	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03
Design	0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02
ŏ	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01

TABLE SB-1

0-1+ A-D wacr 0.125 AF = 5445CF 0.3225 1112 100 6"

Circular Perforation Sizing

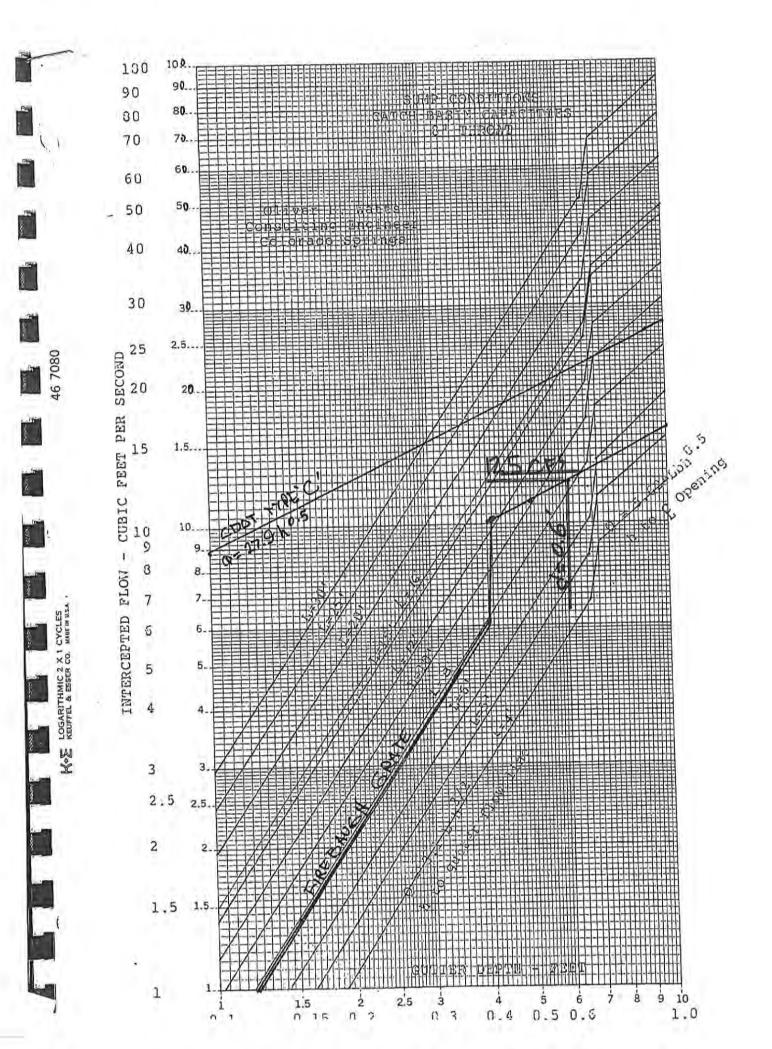
Hole Diameter	Hole Diameter	Are	a per Row (in 2)	
(in)	(in)	n = 1	n = 2	n=3
1/4	0.250	0.05	0.10	0.15
5/16	0.313	0.08	0.15	0,23
3/8	0.375	0.11	0.22	0.33
7/16	0.438	0.15 :	0.30	0.45
1/2	0.500	0.20	0.39	0.59
9/16	0.563	0.25	0.50	0.75
5/8	0.625	0.31	0.61	0.92
11/16	0.688	(032)	0.74	1.11
3/4	0.750	0.44	0.88	1.33
7/8	0.875	0.60	1.20	1.80
1.1	1.000	0.79	1.57	2.36
1 1/8	1,125	0.99	1.99	2.98
1 1/4	1.250	1.23	2.45	3.68
1 3/8	1.375	1.48	2.97	4.45
1 1/2	1.500	1.77	3.53	5.30
1 5/8	1.625	2.07	4.15	6.22
1 3/4	1.750	2.41	4.81	7.22
1 7/8	1.875	2.76	5.52	8.28
2	2.000	3.14	6.28	9.42
	n = Numbe	er of columns of perfo	rations	
Minimum steel	plate thickness	1/4"	5/16"	3/8"

TABLE SB-2

City of Colorado Springs Stormwater Quality

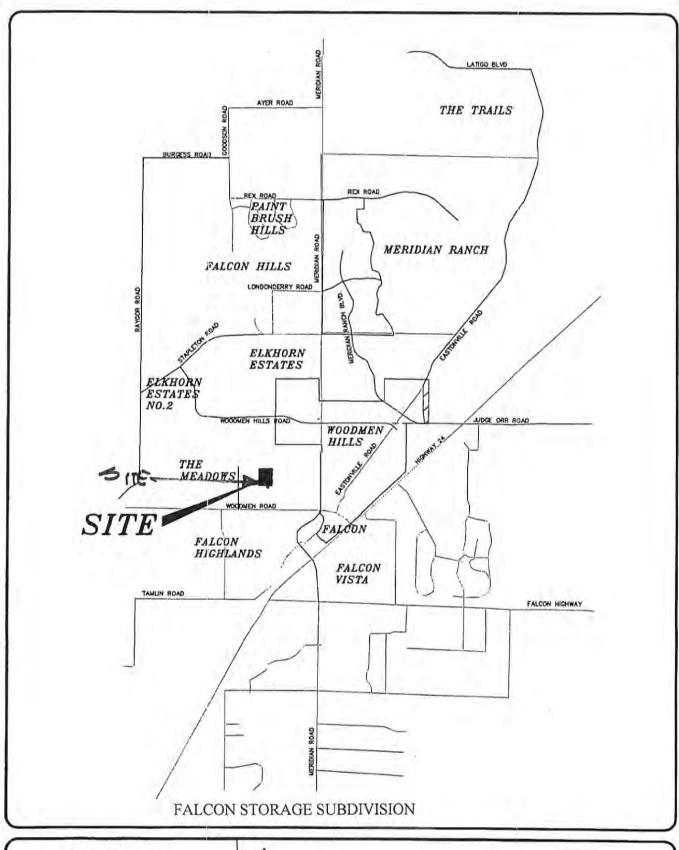
Figure SB-2 **Outlet Sizing**

Application Techniques and Maintenance Requirements



AMETER	AREA	D 8/3		K	C. C	
-IN	-FT2-	-FT-	N=0.010	N=0.013	N=0.024	N=0.026
1						
2	0.02182	0.008413	0.3895			
4	0.08727	0.053420	2.4733			1099-1
6	0.19630	0.157500	7.2922	5.609	4.24	
8	0.34910	0.339200	15.7050	12.081		
10	0.54540	0.615000	28.4745	21.903	4.64	5.55
12	0.78540	1.000000	46.3000	35,615	F. 4. 4	
15	1.22720	1.813100	83.9465	64.574		50.5
18	1.76710	2.948300	136,5100	105.000	56.88	52.5
21	2.40530	4.447400	205.9100	158.400	85.80	79.2
24	3.14160	6.349600	293.9900	226.140	122.49	113.0
27	3.97610	8.692700	402.4700	309.590	167.70	154.7
30	4.90870	11.512600	533.0300	410.030	222.10	205.0
33	5.93960	14.844100	- Callering Street	528.680		
36	7.06860	18,720800	866.7700	666.700	361.20	333.3
39	8.29580	23,175100		825.400		
42	9,62110	28.238900		1005.000	544.80	502.
48	12.56640	40.317500		1436.000	777.80	718.
54	15.90430	55.195000		1966.000	1065.00	983.
60	19.63500	73.100400		2604.000	1410.00	1302.
66	23.75830	94.254200		3357.000	1818.00	1678.
72	28.27430	118.869400		4234.000	2293.00	2117.
78	33.18310	147.152900		5241.000	2839.00	2620.
84	38.48450	179.306000		6386.000	3459.00	3193.
90	44.17860	215.524500		7676.000	4158.00	3838.
	50.26550	256.000000		9118.000	4939.00	4559.
96	63.61730	350.466600	100	12480.000	6761.00	6140.
108	78.53980	464.158900	THE PARTY OF	16530.000	8954.00	8265.
120	78.53980	404.130300		1 1 100 100 100 100		
						11000

Oliver E. Watts Consulting Engine Colorado Springs



VICINITY MAP LATIGO

Δ.

(719) 380-1090

Colorado Design Concepts

3578 Hartsel Drive E323 Colorado Springs, CO 80920

FIGURE.1

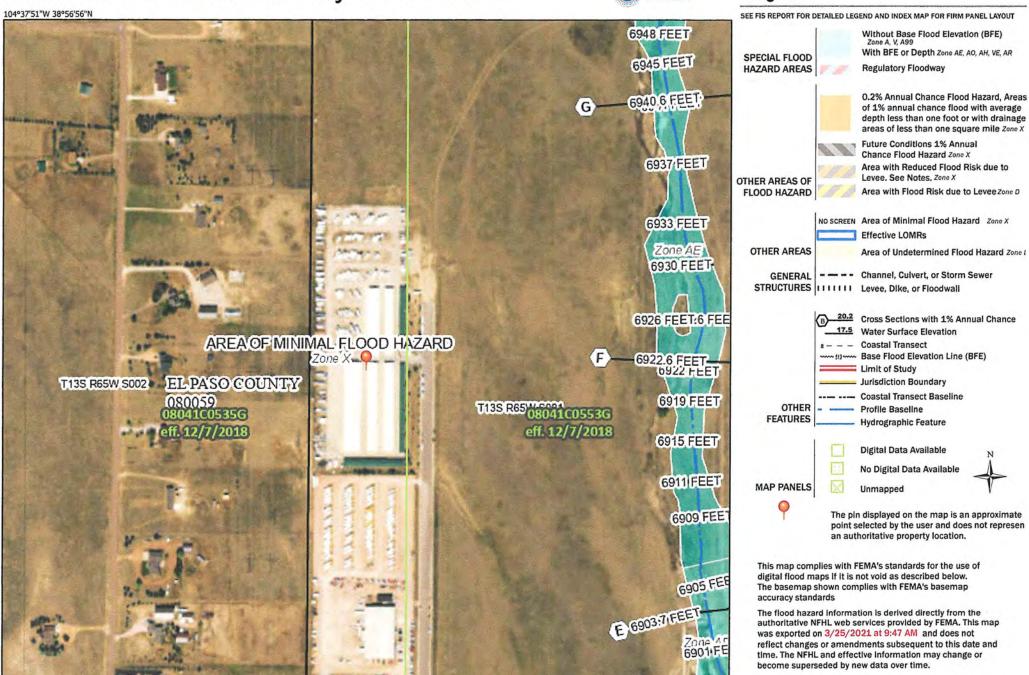
PROJECT NO. 200401

National Flood Hazard Layer FIRMette



104°37'13"W 38°56'28"N

Legend



Feet

2,000

1.500

1.000

250

500

1:6,000

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

NOTES TO USERS

i map is for use in administering the National Flood Insurance Program. It d necessarily identify all areas subject to flooding, particularly from local drain cas of small size. The community map repository should be consulted tible updated or additional flood the particular in the program of the program

obtain more detailed information in areas where Base Flood Elevations (RFF o obtain more detailed information in areas where Base Flood Elevations (BFEs) dollor floodways have been determined, users are encouraged to consult the Flood following the flood of the flood flood flood of the flood of the flood of the flood of the flood flood of the flood of the flood of the flood of the flood levations. These BFEs are intended for flood intermediate flood flood of the flood of t

oastal Base Flood Elevations shown on this map apply only landward of 0,0 nth American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be view that cleastal flood elevations are also provided in the Summary of Sillwhate varied had ceastal flood elevations are also provided in the Summary of Sillwhater elevations table in the Flood insurance Study report for this jurisdiction. Elevations down in the Summary of Sillwhater Elevations table should be used for construction.

pundaries of the floodways were computed at cross sections and interpolate tween cross sections. The floodways were based on hydraulic considerations wi agard to requirements of the National Flood Insurance Program. Floodway wild not other pertinent floodway data are provided in the Flood Insurance Study repo

Certain areas not in Special Flood Hazard Areas may be protected by flood con structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insura Study report for Information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NADB3, GRS80 spheroid Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positions differences in may features across jurisdiction boundaries. These differences do no effect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAV088). These flood elevations must be compared to structure and pround elevations referenced to the same vertical datum, for information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1986, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey st the following activess:

o obtain current elevation, description, and/or location information for bench marks hown on this map, please contact the Information Services Branch of the Nationa seedetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Past County, Colorado Springs Utilities, Cily of Fountain, Bureau of Land Management vational Oceanic and Atmospheric Administration, United States Geological Survey and Anderson Consulting Engineers, Inc. These data are current as of 2006.

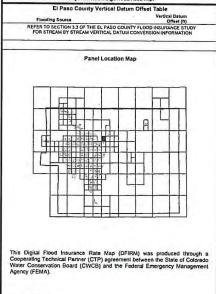
This map reflects more detailed and up-to-date stream channel configurations an floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM map have been adjusted to conform to these new stream channel configurations. As result, the Flood Profiles and Floodway Data tables in the Flood Insurance SMA Report (which contains authoritative hydraulic data) may reflect stream channe distances that office from what is shown on this map. The profile beselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables it applicable, in the FIS report. As a result, the profiles of Floodway Data Tables it applicable, in the FIS report. As a result, the profiles may deviate significantly from the new base map channel representation and yappear suiside of the floodglain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should confact appropriate

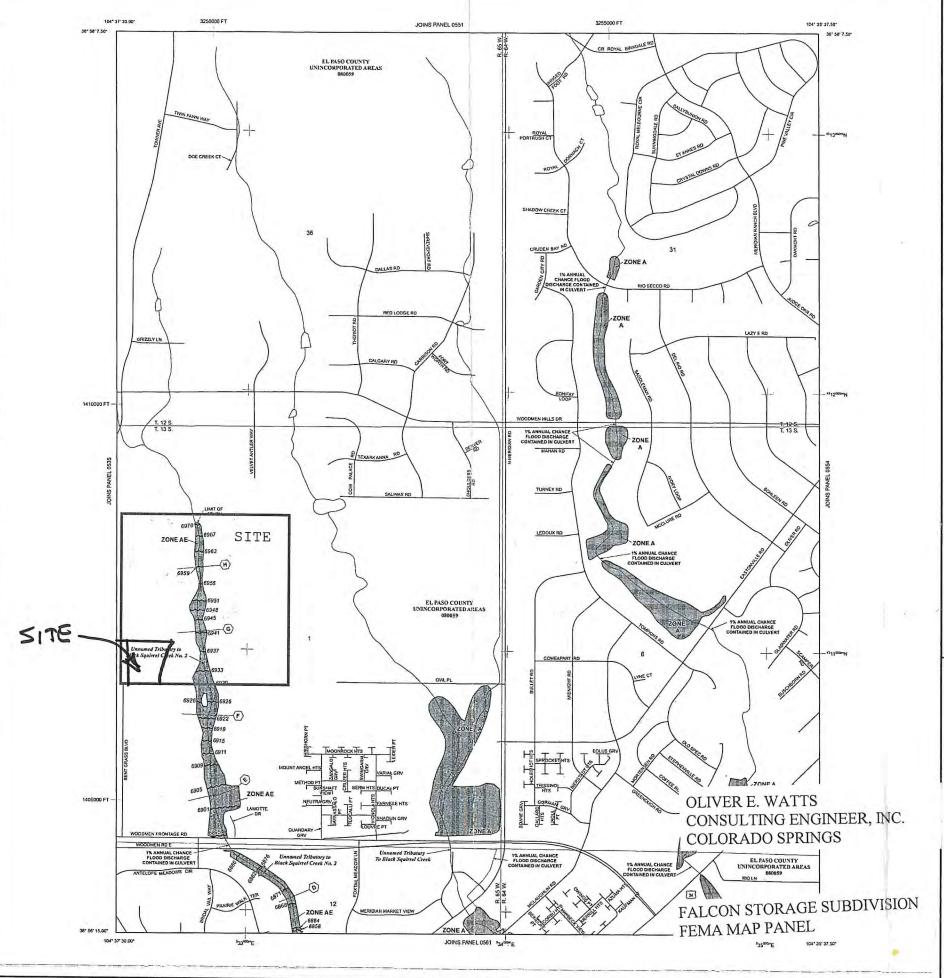
Please refer to the separately printed Map Index for an overview map of the countriowing the layout of map panels; community map repository addresses; and usting of Communities table containing National Flood Insurance Program dates if each community as well as a listing of the panels on which each community

Contact FEMA Map Service Center (MSC) via the FEMA Map Information exchang (FMIX) 1-077-336-2627 for information on available products associated with the FIRM. Available products may fluxude previously issued Letters of Map Change. Flood Insurance Study Report, and/or digital versions of this map. The MSC madis be reached by Fax at 1-600-358-9620 and its website http://www.msc.ci.ema.gov/.

If you have questions about this map or questions concerning the National Floor insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) o wisk the FEMA website at http://www.fema.gov/business/nfip.



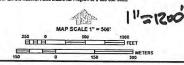
available from local communities and the Colors Water Conservation Board.

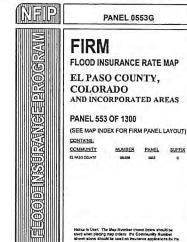


LEGEND SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equated or excreted in any piven year. The Special Flood hazard Ares is the erea subject to floodingly by the 1% annual chance flood, Avess of Special Flood hazard area is AM, AM, AM, AM, AM, AM, AM VE. The Base Flood Beaction is the water-surface developed of the 1% annual chance flood. ZONE A No Base Flood Elevations determined. ZONE AE Base Flood Elevations determined. ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. ZONE AO Flood depths of to 3 feet (usually sheet flow on sloping terroin); overage depths determined. For press of alkahel fan flooding, velocities also determined. Special Rood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently eccrrified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined. Coastal flood zone with velocity hazard (wave accon); no Base Flood ZONE VE Ceastal flood zone with velocity hazard (wave action); Base Flood Bevations determined. FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplein areas that must be kept free of encroactment so that the 1% annual chance flood can be carried without substantial increases in flood heights. OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drafnage areas less than 1 square mile; and areas protected by leves from 1% annual chance flood. OTHER AREAS Areas in which flood hezards are undetermined, but possible, COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAS) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Area ____ Floodway houndar CERS and OPA boundar Philosophia and a second ~~ 513 ~~ (EL 987) Base Flood Elevation value where uniform within zone; clevation in feet* (A)—(A) Cross section line 23-------23 97° 07° 30.00° 32° 22° 30.00° Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 47500mN 5000-foot grid ticks: Colorado State Plane coordinal system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection 5000000 FT DX5510 Bench mark (see explanation in Notes to Users section of EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANE DECEMBER 7, 2018 - to update corporate limits, to change Base Floor Special Flood Hazard Areas, to update may formal, to add roads and roads incorporate previously issued Letters of Man Revision

For community map revision history prior to countywide mapping, refer to the Co Map History Table located in the Flood Insurance Study report for this jurisdiction

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

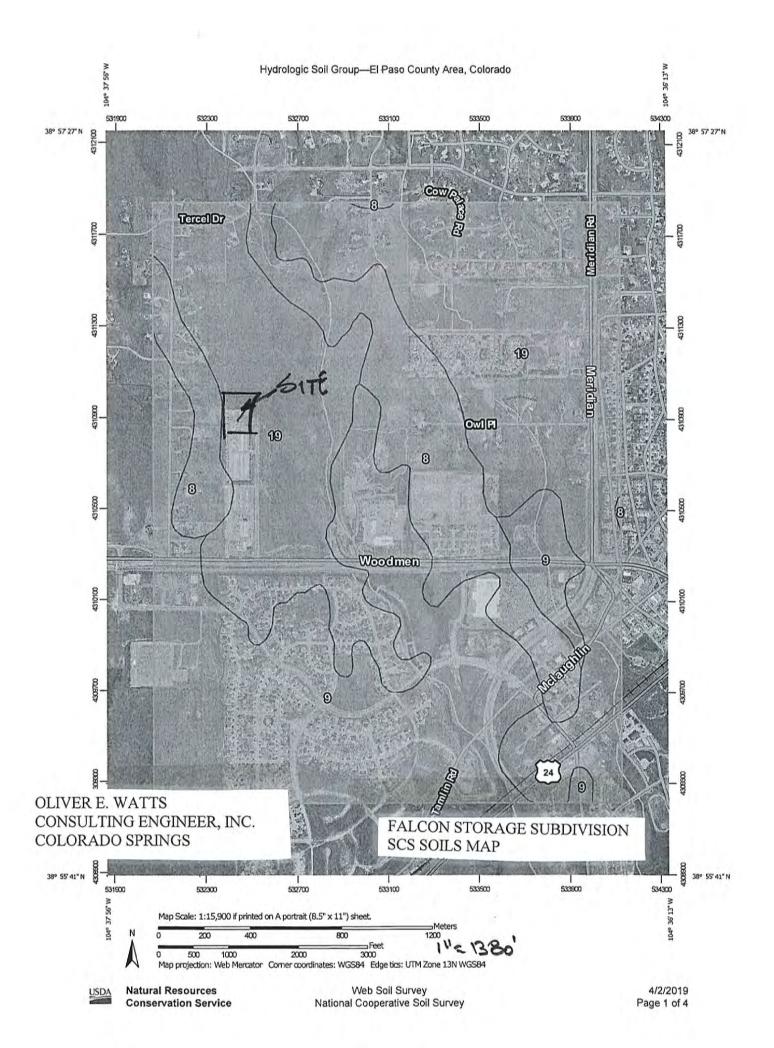






MAP NUMBER 08041C0553G MAP REVISED

DECEMBER 7, 2018 Federal Emergency Management Agency



EL PASO COUNTY AREA, COLORADO

TABLE 16. -- SOIL AND WATER FEATURES

[Absence of an entry indicates the feature is not a concern. See "flooding" in Glossaly for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

	New York	1	Flooding		l Bed	drock	-1	
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	Potential frost action	
Alamosa:				100	In			
1	c	Frequent	Brief	May-Jun	>60		High.	
Ascalon: 2, 3	В	None		177	>60		Moderate:	
Badland: 4	D			777				
Bijou: 5, 6, 7	В	None		47-	>60		Low.	
Blakeland: 8	A	None		444	>60		Low.	
19: Blakeland part-	A	None			>60		Low.	
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60		High:	
Blendon: 10	В	None		444	>60		Moderate.	
Bresser: 11, 12, 13	В	None		3-3-1	>60		Low.	
Brussett: 14, 15	В	None			>60		Moderate.	
Chaseville: 16, 17	A	None		1000	>60		Low.	
118: Chaseville part	A	None		-5-	>60		Low.	
Midway part	D	None	1 1	16-60	10-20	Rippable	Moderate.	
Columbine:		None to rare		1983	>60		Low.	
Connerton: 120: Connerton part-	В	None			>60		High.	
Rock outcrop	D							
Cruckton: 21	В	None			>60		Moderate.	
Cushman: 22, 23	c	None			20-40	Rippable	Moderate.	
124: Cushman part	c	None		1.5	20-40	Rippable	Moderate.	
Kutch part	C	None			20-40	Rippable	Moderate.	
Elbeth: 25, 26	В	None		444	>60		Moderate.	
127: Elbeth part	В	None		(>60		Moderate.	

See footnote at end of table.

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent			_			Runoff Co	efficients					
Characteristics	Impervious	2-1	rear	5-1	ear	10-	year	25-	year	50-	year	100-	-year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG CAO
Business			100				USA SER	100,000	THE COL	HOUNGE	Had Cold	HJG Mail	H3G CAU
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0,88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0,53	0.53	0,57	0.58	0.62	0.60	0.65	0.62	0.68
Residential			7 00 0		-		_		-		-		
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.50	
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.59	0.65
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43		0.50	0.58
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0,46	0.41	0.52	0.47	0.57
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.46	0,56
Industrial		-	1		-	-			10.	_			
Light Areas	80	0.57	0.50	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.70	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0,23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.54
Undeveloped Areas		-					-						
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	.0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0,37	0.38	0.44	0,44	0.51	0.48	0.55	0.51	0.59
Streets	\$7.00 T									-		-	
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0,63	0.63	0,66	0,66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0,94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$t_c = t_1 + t_1 \tag{Eq. 6-7}$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
 (Eq. 6-8)

Where:

t_i = overland (initial) flow time (min)

 C_5 = runoff coefficient for 5-year frequency (see Table 6-6)

L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_i , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_{\nu} S_{\nu}^{0.5}$$
 (Eq. 6-9)

Where:

V = velocity (ft/s)

 $C_v = \text{conveyance coefficient (from Table 6-7)}$

 $S_w = \text{watercourse slope (ft/ft)}$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	. 7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

* For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_i) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L =waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

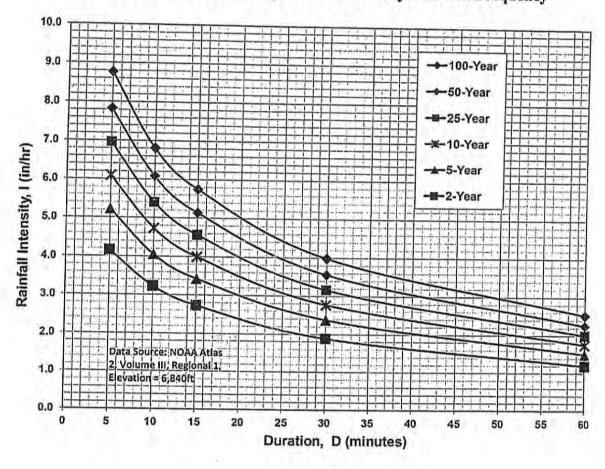


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

