

MASTER DEVELOPMENT DRAINAGE PLAN

FOR

**LORSON RANCH EAST
EAST OF THE EAST TRIBUTARY
OF JIMMY CAMP CREEK**

PUDSP-16-003

JUNE 30, 2017

Prepared for:

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ENGINEERING GROUP

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ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Richard L. Schindler, P.E. #33997

Date

OWNER'S STATEMENT

I, the Owner, have read and will comply with all the requirements specified in the drainage report and plan.

Lorson, LLC

Business Name

Date

By

Jeff Mark, Manager

Title

212 North Wahsatch Avenue, Suite 301

Address

Colorado Springs, Colorado 80903

FLOODPLAIN STATEMENT

To the best of my knowledge and belief, this development is located within a designated floodplain as shown on Flood Insurance Rate Map Panel No. 08041C0957 F and 08041C1000 F, dated March 17, 1997 and modified by modified per LOMR Case No. 14-08-0534P. (See Appendix A, FEMA FIRM Exhibit)

Richard L. Schindler, #33997

Date

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volume 1 and 2, and Engineering Criteria Manual, As Amended.

Jennifer Irvine

Date

County Engineer/ECM Administrator

1.0 INTRODUCTION

Purpose and Scope

The purpose of this Master Development Drainage Plan (MDDP) is to provide an overview of the overall drainage impacts/mitigation due to development in the proposed Lorson Ranch East development located to the east of the East Tributary of Jimmy Camp Creek (hereafter referred to as the East Tributary). The study area of this report is approximately 790 acres. See **Appendix A** for vicinity map.

A Drainage Basin Planning Study (DBPS) has been approved by the City of Colorado Springs and partially approved for the entire Jimmy Camp Creek Basin, including the East Tributary prepared by Kiowa Engineering [7]. Lorson Ranch East will meet the requirements of the Kiowa DBPS. See the East Tributary section of this report for discussion on the status of the East Tributary.

There is an existing (unapproved) DBPS for Jimmy Camp Creek prepared by Wilson & Company in 1987 [3], which is referenced in this report but the use of the report has been limited since it was never officially adopted and has been superseded by the Kiowa Engineering DPBS partially adopted by El Paso County.

There is very little offsite runoff from the north which will be routed through this site to the East Tributary as in existing conditions. On site runoff will be conveyed to the East Tributary through a system of swales, constructed streets, ponds, inlets, culverts, and storm sewers. Detention basins are strategically located to reduce developed runoff into the East Tributary at a rate equal to or less than existing conditions. Detention ponds will comply with current county requirements which include full spectrum detention.

Other than flows actually conveyed by the East Tributary...

A few small sub basins flow offsite on the south side of Lorson Ranch will be detained in individual ponds and released offsite at a rate equal to or less than existing conditions and at the historic location. For these basins that flow offsite there is a possibility of extending storm sewer to intercept the runoff which will be discussed in this report.

in a historic manner

Property Location and Description

The proposed 790 acre portion of the Lorson Ranch development herein referred to as Lorson Ranch East is located east of the East Tributary of Jimmy Camp Creek (hereafter referred to as the East Tributary), which flows from the north in a southwesterly direction through the property. The portion of the property addressed with this report is bounded on the west by East Tributary and on the east by existing ranch land and the future Meridian Road. The property is bounded on the north by Banning Lewis Ranch, Rolling Hills Ranch and on the south by Peaceful Valley Estates (a residential subdivision and golf course within El Paso County and an undeveloped land which is currently used for farming and ranching).

by the developer

A previous Master Development Drainage Plan was created and approved by El Paso County (November 2006) for the portion of the Lorson Ranch development that exists between the main channel of Jimmy Camp Creek and the East Tributary.

The East Tributary of Jimmy Camp Creek enters the site at the center of the northern boundary and flows south. In the southern portion of the site it turns west then turns south again before it connects to the main channel of Jimmy Camp Creek, approximately 1,300 feet south of Peaceful Valley Road. The confluence of the East Tributary with the main channel is south of and offsite the Lorson Ranch.

delete or reword (not partially adopted, but allowed for concept)

The legal description for the Lorson Ranch property is:

The Lorson Ranch Development is located within portions of the north half of Section 23, the north half of Section 24, the south half of Section 13, the south half of Section 14 and the northeast quarter of Section 22, all in Township 15 South, Range 65 West of the 6th Principal Meridian, east of the county road known as Marksheffel Road, except any portion of said northeast quarter within the plat of Brownsville Subdivision No. 2 as recorded in plat book H-6 at page 81 of the County of El Paso, State of Colorado Records. The total site consists of 1,361.4 acres, more or less all in Township 15 South, Range 65 West of the 6th Principal Meridian, County of El Paso, State of Colorado. This report addresses only 790 acres east of the East Tributary of Jimmy Camp Creek (Lorson Ranch East).

(fees were not calculated for El Paso County)

Conformance with applicable Drainage Basin Planning Studies

There is an existing (unapproved) DBPS for Jimmy Camp Creek prepared by Wilson & Company in 1987, adopted by El Paso County, and is referenced in this report. The only major drainage improvements for this study area according to the 1987 Wilson study was the reconstruction of the East Tributary of Jimmy Camp Creek (East Tributary). In 2014 a portion of the East Tributary was reconstructed from Fontaine Boulevard south 2,800 feet in accordance with the 1987 study. This section of the East Tributary included a trapezoidal channel section with 6:1 side slopes and a sand bottom. On March 9, 2015 a new DBPS for Jimmy Camp Creek and the East Tributary was completed by Kiowa Engineering. The Kiowa Engineering DBPS has been adopted by the City of Colorado Springs and partially adopted by El Paso County for the entire Jimmy Camp Creek Basin, including the East Tributary and the full spectrum detention pond requirements. El Paso county has not approved the drainage fees detailed in the Kiowa DBPS so current county drainage/bridge fees apply to this development. Per the Kiowa DBPS the preferred channel improvements include selective channel armoring with a low flow channel for the East Tributary. All remaining channel improvements are reimbursable against drainage fees for future development within the study area. The only major infrastructure not shown in the Kiowa DBPS is the future bridge for Fontaine Boulevard and Lorson Boulevard on the East Tributary. The Fontaine Boulevard bridge is considered to be reimbursable since it is shown on the El Paso County 2060 Major Thoroughfare Plan as a Principal Arterial roadway. Lorson Boulevard bridge is not considered reimbursable.

see below

Reconstruction of the East Tributary of Jimmy Camp Creek

The Kiowa DBPS shows the East Tributary to be protected using selective armoring (soil rip rap) at the outside stream bends (500' minimum radius) and a stabilized low flow channel. The East Tributary can be divided into three different sections, south, middle, and north. The first section (south) is from the south property line east and north to design point ET-3 (see drainage map) and is roughly 2,900 feet in length. The south section does not have any development located next to it at this time and will be armored per the Kiowa DBPS in the future as development occurs. During site visits with ACOE (Van Truan) and El Paso County Staff (Rich Harvey) it was discussed that the south section may be a good candidate to eliminate the stabilized low flow channel because of the large amounts of existing vegetation have already stabilized the low flow channel. The vegetation in this section is much more robust than the northern sections since it is supported by a higher groundwater table. The final design plans will further evaluate the low flow channel alternate. The 100-year flow rate for design is 5,500cfs. A CLOMR is not necessary for constructing the improvements in the south section

because there are no proposed bridge crossings or channel re-alignment. The middle section is from Design Point ET-3 north 2,800 feet to the future extension of Fontaine Boulevard. The channel for this section was reconstructed and stabilized in 2014 in accordance with the 1987 Wilson DBPS. The only infrastructure left to construct are the bridges over the creek at Fontaine Boulevard and Lorson Boulevard. LOMR Case No. 14-08-0534P was approved by FEMA for this middle section. The northern section is from Fontaine Boulevard and extends north to the north property line. The north section will be protected per the Kiowa DBPS during the first phase of development east of the East Tributary. The channel consists of a stabilized low flow channel and soil rip rap armored outer bends. Kiowa Engineering has submitted construction plans to El Paso County for this section of creek including bridges for Lorson Boulevard and Fontaine Boulevard. A CLOMR for the creek and bridge construction is currently submitted to FEMA. The 100-year flow rate for design is 4,750cfs for this section.

in conformance with (?)

2.0 DRAINAGE DESIGN CRITERIA

The supporting drainage design and calculations were performed in accordance with the City of Colorado Springs/El Paso County Drainage Criteria Manual DCM dated 1994; and Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014.

The proposed improvements to the Lorson Ranch Development will be in substantial compliance with the “Jimmy Camp Creek Drainage Basin Planning Study”, dated March 9, 2014 prepared by Kiowa Engineering, which has been adopted by El Paso County excluding the drainage fees.

see previous comments

The Rational Method as outlined in Section 3.2.7.F of the El Paso County “Engineering Criteria Manual” [5] was used for basins less than 100 acres to determine the rainfall and runoff conditions for the proposed development of the site. The soil Conservation Service (SCS) Hydrograph Procedure as outlined in the same section was used for basins larger than 100 acres to determine the rainfall and runoff conditions for the proposed development of the site. The runoff rates for the 5-year initial storm and 100-year major design storm were calculated.

Current updates to the Drainage Criteria manual for El Paso County states when detention is necessary, Full Spectrum Detention will be included in the design. Based on this criteria, Full Spectrum Detention will be required for this development

3.0 EXISTING HYDROLOGICAL CONDITIONS

The site is located within the Jimmy Camp Creek Drainage Basin. The roughly 43,000-acre (66.9 square miles) basin is located within unincorporated El Paso County, the City of Colorado Springs, and the City of Fountain, Colorado. The “Jimmy Camp Creek Drainage Basin Planning Study” [7] establishes drainage guidelines and mitigation for development within the Jimmy Camp Creek Drainage Basin. This report has been adopted by the City of Colorado Springs, and by El Paso County excluding drainage fees. El Paso County has yet to adopt the drainage fee portions of the DBPS.

see previous comments

The area that is the subject of this Master Development Drainage Plan covers approximately 808 acres of undeveloped land (790 acres onsite) that has recently been used for agriculture and grazing, and is currently zoned as RRS (rural residential district). The land east and south of the East Tributary consists of hilly terrain with slopes up to 12%.

bedrock

The Soil Conservation Service (SCS) classifies the soils within the Lorson Ranch East property as Ascalon sandy loam; Manzanola clay loam; Nelson-Tassel fine Sandy loam; Razor clay loam; and Wiley silt loam (13%) [3]. The sandy and silty loams are considered hydrologic soil group B soils with moderate to moderately rapid permeability. The Razor clay loams are considered hydrologic soil group C soils with slow permeability. All of these soils are susceptible to erosion by wind and water, have low bearing strength, moderate shrink-swell potential, and high frost heave potential (see table 3.1 below). The clay loams are difficult to vegetate and comprise of a small portion of the study area. These soils can be mitigated easily by limiting their use as topsoil since they comprise of a small portion of the study area. Weathered will be encountered beneath some of the site but it can be excavated using conventional techniques.

Table 3.1: SCS Soils Survey

Soil	Hydro. Group	Shrink/Swell Potential	Permeability	Surface Runoff Potential	Erosion Hazard
2-Ascalon Sandy Loam - (4%)	B	Moderate	Moderate	Slow to Medium	Moderate
3-Ascalon Sandy Loam - (9%)	B	Moderate	Moderate	Slow to Medium	Moderate
52-Manzanola Clay Loam (17%)	C	High	Slow	Medium	Moderate
54-Midway Clay Loam (3%)	D	High	Slow	Medium	Moderate
56-Nelson – Tassel Fine Sandy Loam (50%)	B	Moderate	Moderately Rapid	Slow	Moderate
75-Razor Clay Loam (10%)	C	High	Slow	Medium	Moderate
104-Vona Sandy Loam (1%)	B	Low	Moderate	Slow	Moderate
108-Wiley Silt Loam (13%)	B	Moderate	Moderate	Medium	Moderate

Excerpts from the SCS “Soil Survey of El Paso County Area, Colorado” [2] are provided in **Appendix A** for further reference.

For the purpose of preparing hydrologic calculations for this report, the soil of each basin are assumed to be wholly comprised of the majority soil hydrologic group.

An existing electrical easement, within existing transmission towers, runs through the center of this portion of the development and will be set aside as open space in the future. It is the intent of this drainage plans to utilize some of the open space under the towers for detention of developed storm flows.

The FMIC (irrigation canal) that runs parallel with the East Tributary through this site was decommissioned in 2006 and for the purpose of existing drainage calculations the canal was ignored and all flow was assumed to flow to the East Tributary.

Portions of the site are located within the delineated 100-year floodplain of the East Tributary of Jimmy Camp Creek per the Federal Emergency Management Agency (FEMA) Flood Rate Insurance Map (FIRM) number 08041C0957 F & 08041C1000 F, effective 17 March 1997 [2]. Floodplain along the East Tributary middle section was modified per LOMR Case No. 14-08-0534P (see appendix). Floodplain designations include Zone AE and Zone X within the property boundary. A portion of this map is provided in **Appendix A** for reference.

The existing drainage area of this MDDP has been divided into major basins and numerous smaller sub basins. The majority of the area drains naturally to the East Tributary, with some smaller basins flowing offsite to the east and south, and north. See the map pocket in the rear of this report for the existing conditions map. The rational method was used to estimate the runoff from each basin for both 5-year and 100-year storm events except for the three (3) basins which are larger than 100 acres where the SCS method was utilized (see **Appendix B** for calculation and break out of the sub basins). Following is a description of the Existing Major Basins:

Basin EX-A1

This 4.28 acre basin is in the northwest corner of the site and includes part of the East Tributary. Under existing conditions, this area contributes 1.1 cfs and 8.0 cfs to the East Tributary for 5-year and 100-year events respectively. This basin comprises of the East Tributary and will not be developed in the future.

Overall Basin EX-B flows to Design Point 1

This 20.06 acre basin is the northeast corner of the site and includes off-site flows from the east (Basin OS-B1), on-site flows (Basin B1.1). All runoff flows overland to the northwest to the East Tributary. The calculated existing flows are 10.5 cfs and 58.8 cfs for the 5-year and 100-year storm events respectively and drain overland.

Overall Basin EX-C flows to Design Point 2

This is the largest existing basin at 452.97 acres which includes approximately the northern half of the site. This basin is an overall existing basin including Basins EX-C1 to EX-C10. There are two offsite basins (OS-C6.1 and OS-C5.1) which flow onto the site from the north and east and are included in the flow at Design Point 2. Under existing conditions, this basin contributes 141.0 cfs and 458.0 cfs for the 5-year and 100-year events respectively at Design Point 2. Design Point 2 is located at the East Tributary and all flow is routed to the East Tributary in an existing swale that is eroded and is not armored.

Overall Basin EX-D flows to Design Point 3

Overall Basin EX-D is located adjacent to and southwest of Basin Ex-C and is 109.55 acres in size. This basin is an overall existing on-site basin. The existing runoff of 29.7cfs and 166.5cfs for the 5-year and 100-year events at Design Point 3 respectively and flows directly overland into the East Tributary.

Overall Basin EX-E flows to Design Point 4

Overall Basin EX-E is located adjacent to and southwest of Basin Ex-D and is 186.30 acres in size. Overall Basin EX-E is the second largest historic basin at 186.30 acres and includes on-site flow (Basins EX-E1 to EX-E3) and offsite flows (Basin OS-E1.1 and OS-E2.1) from the Peaceful Valley Estates subdivision to the south. Under existing conditions, this overall basin contributes 104.0 cfs and 286.0 cfs for the 5-year and 100-year events respectively at Design Point 4 and flows directly overland into the East Tributary.

100 and 280?

Basin EX-F flows to Design Point 5

This 39.85 acre basin flows offsite to the east toward the future Meridian Road. This basin is an overall existing on-site basin including Basins EX-F1 to EX-F2. The existing runoff is 19.3 cfs and 113.7 cfs for the 5-year and 100-year events respectively.

Basin EX-G-Design Point 6

Basin Ex-G is relatively small basin of 14.91 acres in the southeast portion of the site and flow south overland offsite to the Peaceful Valley Lake Estates subdivision. The existing flows are 7.9cfs and 44.1cfs for the 5-year and 100-year storm events respectively.

Basin EX-H-Design Point 7

This 28.13 acre basin flows offsite overland to the south onto the adjacent subdivision. The existing flows are 12.3cfs and 73.2cfs for 5-year and 100-year events respectively.

Overall Basin EX-I flows to Design Point 8

This 32.92 acre overall basin includes on-site flow (Basins EX-I1) and offsite flows (Basin OS-I1.1) and flows directly into the East Tributary. Under existing conditions, this overall basin contributes 12.4cfs and 74.1cfs for the 5-year and 100-year events respectively at Design Point 8.

Overall Basin EX-J flows to Design Point 9

This 25.78 acre overall basin includes on-site flow (Basins EX-J1) and offsite flows (Basin OS-J1.1) and flows directly into the East Tributary. Under existing conditions, this basin contributes 9.0cfs and 55.9cfs for the 5-year and 100-year events respectively at Design Point 9.

Overall Basin EX-K flows to Design Point 10

This 7.57 acre overall basin is located in the southwest corner of the site and includes on-site flow (Basins EX-K1) and offsite flows (Basin OS-K1.1) and flows directly into the East Tributary. The existing flows are 2.1cfs and 15.2 cfs for 5-year and 100-year storm events respectively at Design Point 10.

4.0 DEVELOPED HYDROLOGICAL CONDITIONS

Under developed conditions, there will essentially be seven (7) drainage basins that will drain directly into the East Tributary and for (4) basins that could drain offsite unless directed back on-site via storm sewer. These basins closely mimic the existing drainage patterns and locations and flow rates.

The site will be divided into multiple phases with total build out in the year 2033. The proposed total build out of this portion of the development will include residential development and a school site.

The runoff coefficient of 0.49 (5-year) and 0.65 (100-year) were used to calculate developed runoff.

Fontaine Boulevard and Lorson Boulevard will extend through the development from the west as major roadways. There will also be several local and collector roads that will be constructed for access throughout the site. Only the arterial and collector streets have been shown on the plans. The proposed detention ponds, storm sewer, drainage channels, and diversion swales shown on the plan are schematic in nature and shown for information only. As more of the development is designed in greater detail, localized, detailed drainage plans will need to be created that follow the general plan set forth in this document.

As summary table of design point developed flow rates can be found on the Developed Conditions map in the back pocket of this report. The following is a description of the Developed basins and Design Points:

discuss pond concept
and design

Basin A

This 2.6 acre basin is in the northwest corner of the site and includes the East Tributary. This basin consists of open space contributes 1.4 cfs and 7.7 cfs to the East Tributary for 5-year and 100-year events respectively. This basin comprises of the East Tributary and will not be developed.

Basin OS-B1

Offsite Basin OS-B1 is 5.64 acres and will flow overland onto Basin B2. Meridian Road may be constructed along the eastern border of Lorson Ranch in the future which will intercept the flows going to Basin B2. For this report the flows are assumed to flow overland to Basin B2. Assuming the runoff does reach the development it will flow onto Basin B2 and can be expected to be approximately 3.4 cfs and 19.0 cfs for the 5-year and 100-year design storms respectively.

Basin B2

This basin is located in the northeast corner of the site and consists of residential development. It is 3.9 acres and flows offsite to the northwest. The runoff for Basin B2 under developed conditions is estimated at 6.4 cfs and 14.3 cfs for the 5-year and 100-year storm events.

Overall Basin B at Design Point 1

Overall Basin B is located at the northeast corner of the site and receives offsite flow from Basin OS-B1 and Basin B2. The total flow for the basin is 8.5 cfs and 28.0 cfs for the 5-year and 100-year storm events which is less than the existing runoff. (see Design Pt. 1 in existing conditions). Developed runoff will flow offsite to the northwest as in

existing conditions. These developed flows will not need to be detained but will require water quality treatment.

Basin C1

Basin C1 consists of residential development and is located in the upstream portion of Overall Basin C. This basin is 23.2 acres and flows downstream to a low point in Lorson Boulevard and into Basin C2. The runoff under developed conditions is estimated at 34.9 cfs and 77.7cfs for the 5-year and 100-year storm events. A 36" storm sewer will be necessary to convey runoff under Lorson Boulevard into Basin C2.

Basin C2 and Design Point 2

Basin C2 consists of residential development and is located in the upstream portion of Overall Basin C. This basin is 34.5 acres and flows downstream into Pond C1. Detention Pond C1 is proposed at the downstream portion of this basin within the existing electrical transmission easement. The runoff for Basin C2 under developed conditions is estimated at 66.6cfs and 148.4 cfs for the 5-year and 100-year storm events.

The total combined flow reaching Pond C1 at Design Point 2 is from Basin C1 and C2 and is 80.1 cfs and 171 cfs for the 5-year and 100-year storm events respectively. It is estimated that a 48" storm will be necessary to convey runoff into Pond C1.

Basin C3

This is small sub basin of 8.3 acres and flows downstream north into Basin C4 at Design Point 3a. The runoff for Basin C3 under developed conditions is estimated at 13.9 cfs and 31.0 cfs for the 5-year and 100-year storm events. Runoff from this basin will be collected in storm sewer at Lorson Boulevard and will be directed west to Detention Pond C2.1.

Basin C4

This relatively large sub basin is located in the upstream portion of Basin C. The 57.5 acre basin contributes 79.7 cfs and 177.4 cfs for the 5-year and 100-year storm events. Runoff from this basin will be collected in storm sewer at Lorson Boulevard and will be directed west to Detention Pond C2.1.

Basin C5

Basin C5 is located in the upstream portion of Basin C in the northeast corner of Fontaine and Lorson Boulevards. The 25.0 acre basin contributes 42.4 cfs and 94.4 cfs for the 5-year and 100-year storm events to Design Point 3d. Runoff from this basin will be collected in storm sewer at Lorson Boulevard/Fontaine and will be directed west in Fontaine Boulevard to Detention Pond C2.2.

Basin C6

Basin C6 is located south of Fontaine Boulevard and is in the upstream portion of Basin C. Basin C6 is 18.7 acres and under developed conditions the flow is estimated to be 31.7cfs and 70.5 cfs for the 5-year and 100-year storm events respectively. Runoff will be directed to Pond C2.3. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 3a

This design point is the total outflow flow from Pond C2.1. The total developed flow is 11.0cfs and 65.0 cfs for the 5-year and 100-year storm events. **flowing to Pond C2.3?**

Design Point 3b

This design point is the total inflow to Pond C2.3. Runoff at this design point is from Design Point 3a and Basin C6. The total developed flow is 46.3cfs and 111.0 cfs for the 5-year and 100-year storm events at Design Point 3b. Runoff from this basin will be collected in storm sewer and will be directed to Detention Pond C2.3. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 3c

This design point is the total outflow flow from Pond C2.3. The total developed flow is 4.0cfs and 46.0 cfs for the 5-year and 100-year storm events. **Is Pond C2.1 release (65 cfs) flowing through this pond?**

Basin C7

Basin C7 is located north of Fontaine Boulevard and is in the upstream portion of Basin C. Basin C7 is 14.5 acres and under developed conditions the flow is estimated to be 26.4 cfs and 58.9 cfs for the 5-year and 100-year storm events respectively. Runoff will be directed to Pond C2.2.

Basin OS-C9.1

Offsite Basin OS-C9.1 is 3.59 acres and will flow overland onto Basin C8. Meridian Road may be constructed along the eastern border of Lorson Ranch in the future which will intercept the flows going to Basin C8. For this report the flows are assumed to flow overland to Basin C8. Assuming the runoff does reach the development it will flow onto Basin C8 and can be expected to be approximately 4.0 cfs and 10.6 cfs for the 5-year and 100-year design storms respectively.

Basin C8

Basin C8 is located north of Fontaine Boulevard and is in the northeast portion of Basin C. Portions of the northeast corner of this basin will be graded so the runoff flows southwest instead of north to Basin B. This grading will reduce the runoff flowing offsite into Basin B. Basin C8 is 74.5 acres and under developed conditions the flow is estimated to be 119.3 cfs and 265.5 cfs for the 5-year and 100-year storm events respectively at Design Point 5 flowing into Pond C4. **← add Pond C4 outflow rates**

Basin C8a

Basin C8a is located east of Pond C3. Basin C8a is 11.7acres and under developed conditions the flow is estimated to be 22.0 cfs and 49.0 cfs for the 5-year and 100-year storm events respectively. Runoff will be directed to Pond C3.

Basin OS-C9

Sub Basin OS-C9 is 5.2 acres and will flow into Basin C10 and Lorson Boulevard. The runoff for sub Basin OS-C9 is estimated at 10.1 cfs and 22.4 cfs for the 5-year and 100-year storms respectively.

Basin C10

Basin C10 is a 13.0 acre basin is located in the north portion of Basin C and accepts offsite flow from Basin OS-C9. Runoff flows south to Lorson Boulevard and then to a

low point in Lorson Boulevard at Design Point 4. The on-site developed flows this basin are 22.8 cfs and 50.7 cfs for the 5-year and 100-year events respectively.

Design Point 4

This design point is located at a low point in Lorson Boulevard (north of Fontaine Blvd.) and is the total flow into Pond C3. Runoff at this design point is from Basin C8a, OS-C9, C10, and from Pond C4. The total developed flow is 51.6cfs and 134.0 cfs for the 5-year and 100-year storm events into Detention Pond C3. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

add the inflow values

discuss overflow path for developed flows

Design Point 3d

This design point is the total flow into Pond C2.2 (24" storm sewer outfall) from Basin C5, C7, and Pond C3. The total developed flow is 70.0cfs and 138.0cfs for the 5-year and 100-year storm events. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

add the inflow values

Design Point 3e

This design point is the total outflow flow from Pond C2.2. The total developed outflow is 6.0cfs and 40.0 cfs for the 5-year and 100-year storm events.

Discuss pond designs and modeling ponds in series.

Design Point 3f

This design point is the total flow in a storm sewer in Fontaine Boulevard consisting of Pond C2.3 outflow, Pond C2.2 outflow, and Pond C1 outflow. The total developed flow is 14.0cfs and 104.0cfs for the 5-year and 100-year storm events in the pipe.

Basin C12

Basin C12 is a 19.6 acre basin is located to the east of the school site and south of Lamprey Drive (collector road). The developed flows from this basin are 33.0cfs and 73.5cfs for the 5-year and 100-year events respectively. Flows will be directed north in streets/storm sewer to Lamprey Drive. A 30" storm sewer at 1% will flow west in Lamprey Drive to Design Point 6a. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Basin C13

Basin C13 is a 21.2 acre basin is the majority of the school site. The school site will be required to detain developed flows within the basin. Stormwater quality will be provided for this basin in Pond C5. The allowable runoff from this basin is limited to existing conditions and is 7.6 cfs and 40.5 cfs for the 5-year and 100-year events respectively. Flows will be directed west within the basin to Design Point 6b where a 30" storm sewer stub will be located.

Basin C14

Basin C14 is a 11.1acre basin that contains a portion of the school site and Fontaine Boulevard that drains south to Fontaine Boulevard. Approximately 4.0acres of the school site is allowed to direct runoff to Fontaine Boulevard but must be detained to existing flows within the school site. The allowed runoff from Basin C14 is 16.6cfs and 37.0 cfs for the 5-year and 100-year events respectively.

Basin C15

Basin C15 is a 40.2 acre basin is located south of Fontaine Boulevard, east of Lamprey Drive, and west of Pond C1. The developed flows from this basin are 57.6 cfs and 128.3cfs for the 5-year and 100-year events respectively. Flows from this basin will be directed north to Design Point 7 in a 42" storm sewer at 2.4% slope. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Basin OS-C11

Offsite Basin OS-C11 is 5.6 acres and will flow overland west directly to the East Tributary of Jimmy Camp Creek in a swale. The runoff for sub Basin OS-C11 is estimated at 10.2 cfs and 22.7 cfs for the 5-year and 100-year storms.

show on plan

Basin C16a

Basin C16a is a 21.29 acre basin is located north of Lamprey Drive and flows to Design Point 6a. The developed flows from this basin are 35.1 cfs and 78.3 cfs for the 5-year and 100-year events respectively. Flows from this basin will be directed south to Design Point 6a. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 6a

Design Point 6a is located in the southwest corner of Basin C16a and flows are from Basin C16a Basin C12. The developed flows are 68.1cfs and 151.8cfs for the 5-year and 100-year events respectively. Flows will be directed west in Lamprey Drive via streets/storm sewer to Design Point 6c located next to Pond C5. A 42" storm sewer at 1.0% will flow west in Lamprey Drive to Design Point 6c. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 6b

Design Point 6b is located on Lamprey Drive and flows are from Design Point 6a and Basin C12. The developed flows are 75.7cfs and 192.3cfs for the 5-year and 100-year events respectively. Flows will be directed west in Lamprey Drive via streets/storm sewer to Design Point 6c located next to Pond C5. A 54" storm sewer at 1.0% will flow west in Lamprey Drive to Design Point 6c. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

from Lamprey Dr.?

Basin C16b

Basin C16b is a 32.23 acre basin is located north of Fontaine Boulevard, east of Pond C5, and west of Lamprey Drive and flows to Design Point 6c. The developed flows from this basin are 55.6cfs and 123.8cfs for the 5-year and 100-year events respectively. Flows from this basin will be directed to Design Point 6c. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 6c

Design Point 6c is located east of Pond C5 and is the flow from the C16 basins, C12, and C13. The developed flows are 90.0cfs and 222.0cfs for the 5-year and 100-year events respectively. Flows will be directed west into Pond C5 in a 66" storm sewer. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 7

This design point is the total flow in a storm sewer in a low point in Lamprey Drive and Fontaine Boulevard. The total developed flow is 88.0cfs and 270.0cfs for the 5-year and 100-year storm events and flows west in Fontaine Boulevard to Design Point 7a in a 60” storm sewer at a 1.0% grade. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Basin C17

Basin C17 is a 22.7acre basin that contains portions of Fontaine Boulevard, and residential areas south of Fontaine Boulevard. The developed flows from this basin are 31.7cfs and 70.6cfs for the 5-year and 100-year events respectively. Flows from this basin will be directed north to Design Point 7a.

Design Point 7a

Design Point 7a is located on Fontaine Boulevard south of Pond C5. Flows at this design Point are from Design Point 7 and Basin C17 and is the flow into Pond C5 from the south. The developed flows are 114.0 cfs and 337.0 cfs for the 5-year and 100-year events respectively. A 60” storm sewer at 1.0% will flow north to Pond C5. When the future preliminary drainage report for this area is prepared the actual street flows and storm sewer capacities will need to be verified.

Design Point 7b

Design Point 7b is the total inflow into Pond C5. The developed flows are 204 cfs and 484 cfs for the 5-year and 100-year events respectively.

Discuss pond design, add contributing acreage

Design Point 7c

Design Point 7c is the total outflow from Pond C5. The developed flows are 121.0 cfs and 420.0 cfs for the 5-year and 100-year events respectively and flow west into the East Tributary. These flows closely mimic the existing conditions flows into the East Tributary. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

====="D" BASINS=====

Basin D1

This 17.0 acre basin consists of residential development and Lorson Boulevard that flows to Pond D1 south of Lorson Boulevard. The developed flows from this basin are 32.0 cfs and 71.1cfs for the 5-year and 100-year events respectively.

Basin D2

This 8.0 acre basin consists of residential development and flows south to Design Point 8 in Lorson Boulevard. The developed flows from this basin are 16.0 cfs and 35.5cfs for the 5-year and 100-year events respectively.

← Discuss pond D1 design

Design Point 8

This design point is in Lorson Boulevard just east of Lamprey Drive. Flows are from Basin D2 and Pond D1 outflow. The developed flows from this basin are 18.0cfs and 46.0cfs for the 5-year and 100-year events respectively. A 30” storm sewer is needed to convey flows to Pond D2

Basin D3 - Design Point 9a

This 23 acre basin consists of residential development and flows north to Pond D2. The developed flows from this basin are 38.0cfs and 84.5 cfs for the 5-year and 100-year events respectively.

Basin D4 - Design Point 9b

This 36.4 acre basin consists of residential development and flows west to Design Point 9b just east of Pond D2. The developed flows from this basin are 61.7 cfs and 137.5 cfs for the 5-year and 100-year events respectively.

Basin D5

Basin D5 is a 4.6 acre basin that contains Pond D2, portions of Lorson Boulevard, and residential areas. The developed flows from this basin are 7.5cfs and 20.6 cfs for the 5-year and 100-year events respectively. Flows from this basin will be directed to Pond D2.

Design Point 10a

This design point is the total flow into Pond D2 from Design Points 8, 9a, 9b and Basin D5. The developed flow at this design point is 106.0 cfs and 243.0cfs for the 5-year and 100-year events respectively.

← Discuss pond D2 design

Design Point 10b

This design point is the outfall of Pond D2 into the East Tributary. The developed flows at this design point are 67.0cfs and 131.2cfs for the 5-year and 100-year events respectively. These flows closely mimic the existing conditions flows into the East Tributary. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

====="E" BASINS=====

Basin OS-E3

Offsite Basin OS-E3 is 9.90 acres and consists of runoff from the Peaceful Valley Lake Estates 1st Filing which is an existing residential large lot subdivision consisting of 2.5acre to 5acre lots. The runoff will flow overland onto Lorson Ranch into Basin E4 where it will be conveyed to Pond E3 and the East Tributary. Runoff from Basin OS-E3 is 9.2cfs and 32.7cfs respectively for the 5-year and 100-year storm events.

Basin OS-E6

Offsite Basin OS-E6 is 21.1 acres and consists of runoff from the Peaceful Valley Lake Estates 1st Filing which is an existing residential large lot subdivision consisting of 2.5acre to 5acre lots. The runoff will flow overland onto Lorson Ranch into Basin E7 where it will be conveyed to Pond E3 and the East Tributary. Runoff from Basin OS-E6 is 18.4cfs and 65.3cfs respectively for the 5-year and 100-year storm events.

Basin OS-E9

Offsite Basin OS-E9 is 46.9 acres and consists of runoff from the Peaceful Valley Lake Estates 1st Filing which is an existing residential large lot subdivision consisting of 2.5acre to 5acre lots. The runoff will flow overland onto Lorson Ranch into Basin E10-E11 where it will be conveyed to Pond E3 and the East Tributary. Runoff from Basin OS-E9 is 15.2 cfs and 102.0 cfs respectively for the 5-year and 100-year storm events.

Basin E1

This 10.2 acre basin is located in the upstream portion of Basin E. The developed flows from this basin are 18.5cfs and 41.1 cfs for the 5-year and 100-year events respectively. Flows from both Basins E1 will be directed to Pond E1 via storm sewer.

Basin E2

This 10.3 acre basin is located directly north of Basin E1. The developed flows from this basin are 19.9cfs and 44.3cfs for the 5-year and 100-year events respectively. Detention Pond E1 is proposed downstream of this basin within the existing electrical transmission easement.

Basin E4

This 12.8 acre basin is located just to the west of Basin E1 and flows north to Trappe Drive and then to Pond E1. The developed flows from this basin are 23.6cfs and 52.5cfs for the 5-year and 100-year events respectively.

Basin E5

This 13.3 acre basin is located directly east of Pond E1. The developed flows from this basin are 24.4cfs and 54.3 cfs for the 5-year and 100-year events respectively.

Basins E1-E5 at Design Point 12

The total flows reaching Pond E1 at Design Point 12 from basins E1-E5 is 88.7 cfs and 209.5 cfs for the 5-year and 100-year storm events respectively.

← Discuss pond E1 design

Basin E7

This 6.7acre basin is located directly south of Basin OS-E6 and flows west to Trappe Drive where a storm sewer will convey the flow west to Design Point 13. The developed flows from this basin are 12.5cfs and 27.9cfs for the 5-year and 100-year events respectively.

← DP11?

Design Point 11

This design point is located on Trappe Drive where a 48" storm sewer will convey the flow west to Design Point 13. The developed flows from this basin are 26.2cfs and 89.8cfs for the 5-year and 100-year events respectively.

Basin E8

This 21.6acre basin is located directly north of Basin E7 and flows south and west to Trappe Drive where a storm sewer will convey the flow west to Design Point 13. The developed flows from this basin are 35.4cfs and 78.8 cfs for the 5-year and 100-year events respectively.

Design Point 13

This design point is located at a low point on Trappe Drive where a 48" storm sewer will convey the flow south to Design Point 14 and Pond E2 The developed flows at this design point are 78.0cfs and 205.0cfs for the 5-year and 100-year events respectively.

Design Point 14

This design point is the total inflow to Pond E2 including the significant offsite areas in Basin OS-E6 and OS-E9. The developed flows at this design point are 190.0cfs and 423.0 cfs for the 5-year and 100-year events respectively.

← Discuss pond E2 design

Design Point 14a

This design point is the total outflow from Pond E2 into the East Tributary. The pond outflow at this design point is 97.0cfs and 260.0cfs for the 5-year and 100-year events respectively. These flows closely mimic the existing conditions flows into the East Tributary. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary. This pond will only include water quality for development within Lorson Ranch.

=====“ F, G, H, I, J, K ” BASINS=====

full-spectrum sizing is based on contributing impervious area

Basin F at Design Point 15

This 33.0 acre basin is located on the very east portion of the site and discharges into Pond F to the east where the future proposed Meridian Road will be constructed. The total flows reaching Pond F at Design Point 15 are 50 cfs and 111.3cfs for the 5-year and 100-year storm events respectively. These flows closely mimic the existing conditions flows offsite to the east. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

← Discuss pond F design

Design Point 15a

Design Point 15a is the total outflow from Pond F. The developed flows are 3.5 cfs and 41.0 cfs for the 5-year and 100-year events respectively and flow west into the East Tributary. These flows closely mimic the existing conditions flowing east. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

where?

Basin G-Design Point 16

This basin is located in the southeast corner of the study areas. It is 20.05 acres in size and contributes flows offsite. Detention Pond G is proposed near the southern boundary of the property and will be utilized to reduce the runoff to less than pre-development rates. The total flows reaching Pond G at Design Point 16 are 36 cfs and 80.2cfs for the 5-year and 100-year storm events respectively.

← Discuss pond G design

Design Point 16a

Design Point 16a is the total outflow from Pond G. The developed flows are 2.0 cfs and 33.0 cfs for the 5-year and 100-year events respectively and flow south offsite. These flows closely mimic the existing conditions flowing south. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary. Since this flow is offsite is should also be designed to spread the flow onto the adjacent property and not concentrate the flow which can be accomplished using a rip rap berm. It may be possible to route the pond flow west into Pond H which should be evaluated in the preliminary design phase.

?

Basin H-Design Point 17

This basin is located in the southeast corner of the study areas. It is 22.3 acres in size and contributes flows offsite. The total flows reaching Pond H at Design Point 17 are 38.7 cfs and 86.3cfs for the 5-year and 100-year storm events respectively.

Design Point 17a

Design Point 17a is the total outflow from Pond H. The developed flows are 2.0 cfs and 35.3 cfs for the 5-year and 100-year events respectively and flow south offsite. These flows closely mimic the existing conditions flowing south. See Table 6.2 for a comparison of existing versus develop runoff to the East Tributary. Since this flow is offsite it should also be designed to spread the flow onto the adjacent property and not concentrate the flow which can be accomplished using a rip rap berm. It may be possible to route the pond flow west into Pond H which should be evaluated in the preliminary design phase.

Basin OS-I1

Offsite Basin OS-I1 is 15.96 acres and consists of runoff from the Peaceful Valley Lake Estates 1st Filing which is an existing residential large lot subdivision consisting of 2.5acre to 5acre lots. The runoff will flow overland onto Lorson Ranch into Basin I2 where it will be conveyed to Pond I and the East Tributary. Runoff from Basin OS-I1 is 14.1 cfs and 50.0 cfs respectively for the 5-year and 100-year storm events.

Basin I2

Basin I2 is located south of the East Tributary and north of Basin OS-I1. This basin accepts runoff from Basin OS-I1 and flows north to the East Tributary. Runoff from Basin I2 is 25.2cfs and 56.1 cfs respectively for the 5-year and 100-year storm events.

consisting of future residential lots?

Design Point 18a

Design Point 18a is the flow from Pond I and is located adjacent to the East Tributary. This pond accepts runoff from Basin I2, detains, treats runoff, and discharges it north to the East Tributary. The pond outflow is 1.0cfs and 21.1cfs respectively for the 5-year and 100-year storm events. Runoff from Basin OS-I1 is routed around Pond I and will not be detained or treated for water quality.

how? by swale?

Design Point 18

Design Point 18 is located at the southwest corner of the site, is adjacent to the East Tributary, and receives flows from Pond I and basin OS-I1. The developed flow is 15.1 cfs and 71.0cfs for the 5-year and 100-year event and flows. These flows closely mimic the existing conditions flowing to the East Tributary. Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

Basin OS-J1

Offsite Basin OS-J1 is 12.36 acres and consists of runoff from the Peaceful Valley Lake Estates 1st Filing which is an existing residential large lot subdivision consisting of 2.5acre to 5acre lots and Apple Ridge Subdivision. The runoff will flow overland onto Lorson Ranch into Basin J2 where it will be conveyed to Pond J and the East Tributary. Runoff from Basin OS-E9 is 10.8 cfs and 38.3 cfs respectively for the 5-year and 100-year storm events.

Basin J2

Basin J2 is located south of the East Tributary and north of Basin OS-J1. This basin accepts runoff from Basin OS-J1 and flows north to the East Tributary. Runoff from Basin J2 is 22.0cfs and 49.1cfs respectively for the 5-year and 100-year storm events.

Design Point 19a

Design Point 19a is the flow from Pond J and is located adjacent to the East Tributary. This pond accepts runoff from Basin J2, detains, treats runoff, and discharges it north to

the East Tributary. The pond outflow is 0.4cfs and 20.3cfs respectively for the 5-year and 100-year storm events. Runoff from Basin OS-J1 is routed around Pond J and will not be detained or treated for water quality.

how? by swale?

Design Point 19

Design Point 19 is located at the southwest corner of the site, is adjacent to the East Tributary, and receives flows from Pond J and basin OS-J1. The developed flow is 11.2 cfs and 58.6cfs for the 5-year and 100-year event and flows. These flows closely mimic the existing conditions flowing to the East Tributary. Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

Basin OS-K1

Offsite Basin OS-K1 is 1.98 acres and consists of runoff from the Apple Tree Golf Course. The runoff will flow overland onto Lorson Ranch into Basin K2 where it will be conveyed to Pond K and the East Tributary. Runoff from Basin OS-K1 is 2.0 cfs and 7.3 cfs respectively for the 5-year and 100-year storm events.

Basin K2

Basin K2 is located south of the East Tributary and north of Basin OS-K1. Runoff from Basin K2 is 7.3cfs and 16.3cfs respectively for the 5-year and 100-year storm events.

consisting of future residential lots?

Design Point 20a

Design Point 20a is the flow from Pond K and is located adjacent to the East Tributary. This pond accepts runoff from Basin K2, detains, treats runoff, and discharges it north to the East Tributary. The pond outflow is 0.1cfs and 5.6cfs respectively for the 5-year and 100-year storm events. Runoff from Basin OS-K1 is routed around Pond K and will not be detained or treated for water quality.

how? by swale?

Design Point 20

Design Point 20 is located at the southwest corner of the site, is adjacent to the East Tributary, and receives flows from Pond K and basin OS-K1. The developed flow is 2.1 cfs and 12.9cfs for the 5-year and 100-year event and flows. These flows closely mimic the existing conditions flowing to the East Tributary. Table 6.2 for a comparison of existing versus develop runoff to the East Tributary.

5.0 DRAINAGE AND BRIDGE FEES

Lorson Ranch is located within the Jimmy Camp Creek drainage basin which is currently a fee basin in El Paso County. Current El Paso County regulations require drainage and bridge fees to be paid for platting of land. Fees will be paid according to the fee at the time of platting. Construction of the major drainage improvements on the East Tributary to be completed as part of development will be eligible for reimbursement.

There will be two creek crossings associated with the construction of the East Tributary to serve this development. The two crossings will be at Fontaine Boulevard and Lorson Boulevard as they cross the East Tributary. At each crossing, a Conspan will be used to span the creek. The arches will be secured with engineered footer and the channel bottom will consist of natural material. Only the Fontaine Boulevard crossing will be eligible for reimbursement since it is a principal arterial in the 2060 Major Thoroughfare Plan.

Reword that reimbursement may be requested through the DCM and Drainage Board process.

6.0 DETENTION AND WATER QUALITY POND

The purpose of this MDDP is to provide an overview of the overall drainage impacts/mitigation due to development in the proposed Lorson Ranch Development on the East side of the East Tributary. It is recommended to construct larger (semi-regional off-line) on-site detention ponds to reduce the developed runoff at or below pre-development runoff rates. This approach to detention ponds is in compliance with the Jimmy Camp DBPS. Also included within the detention ponds are provisions for storm water quality as required by El Paso County DCM, Volume 2 [4].

There is existing 325 foot electrical transmission line easement that runs diagonally through the middle of the site in a north-south direction. It is the intention of this report to utilize this area for detention ponding, thereby decreasing the runoff further downstream and resulting in smaller storm sewer sizes. The detention ponds within the easement shall not adversely affect the existing power poles and should be at existing grade or lower as to not raise the grade under the power lines.

The detention ponds will be Full Spectrum have been preliminary sized using the Full Spectrum Detention Pond excel spreadsheets from Denver Urban Drainage for ponds that are not in series (no upstream ponds tributary). For ponds in series, the WQ portion of the pond was calculated by the excel spreadsheets and the 5-year/100-year sizing/outflows were determined using hydrologic modeling software called Hydraflow Hydrographs by Intellisolve. See Table 6.1 below for the required volumes of the 5-year, 100-year, and the allowable release rates of each pond. Please see the plan in the back pocket of this report for the location. The detention ponds shown are schematic and will need to be designed with greater detail when the localized plans are designed. All ponds will include WQCV and full spectrum detention design as part of the preliminary plan drainage design.

Table 6.1: Detention Pond Data (full-spectrum (?))

Pond	5-year Volume (Ac-ft)	100-year Volume (Ac-ft)	Release Rate 5-year (cfs)	Release Rate 100-year (cfs)
Pond C1	5.98	10.22	3.0	17.7
Pond C2.1	4.83	8.33	11.0	65.0
Pond C2.2	3.72	6.38	6.0	40.0
Pond C2.3	1.48	4.32	4.0	46.0
Pond C3	1.73	6.33	4.6	17.8
Pond C4	5.69	10.72	12.4	38.3
Pond C5	13.01	15.56	121.0	420.0
Pond D1	1.25	2.48	2.0	10.5
Pond D2	5.61	8.53	31.2	131.2
Pond E1	3.60	6.57	9.4	32.0
Pond E2	5.94	9.67	97.0	260.0
Pond F	2.42	3.48	3.5	41.0
Pond G	1.41	2.20	1.1	33.0

This needs to be clarified.

Pond H	1.57	2.35	1.7	35.3
Pond I	0.91	1.38	1.0	21.0
Pond J	0.86	1.25	0.4	20.3
Pond K	0.26	0.47	0.1	5.6

The detention ponds within Basins G and H , which historically flow onto the subdivision to the south will not only need to release at the pre-development rate and location, but shall be designed as to not concentrate the flow onto the adjacent property, but rather spread it by using a rip rap berm. There is a possibility that the pond outflow may be routed west in storm sewer which should be analyzed in the preliminary drainage reports.

Table 6.2: Existing versus Developed Runoff Summary at Outfall Points

Existing Runoff			Developed Runoff			Outfall
Design Point	Runoff 5-yr (cfs)	Runoff 100-yr (cfs)	Corresponding Developed Design Point	Runoff 5-yr (cfs)	Runoff 100-yr (cfs)	
1	10.5	58.8	1	8.5	28.0	"B" basins to north
2	141.0	458.0	7c	121.0	420.0	"C" basins to Etrib
3	29.7	166.5	10b	31.2	131.2	"D" basins to Etrib
4	104.0	286.0	14a	97.0	260.0	"E" basins to Etrib
5	19.3	113.7	15a	3.5	41.0	Basin F to east
6	7.9	44.1	16	2.0	33.0	Basin G to south
7	12.3	73.2	17	2.0	35.3	Basin H to south
8	12.4	74.1	18	15.1	71.0	Basin I to Etrib
9	9.0	55.9	19	11.2	58.6	Basin J to Etrib
10	2.1	15.2	20	2.1	12.9	Basin K to Etrib

7.0 CONCLUSIONS

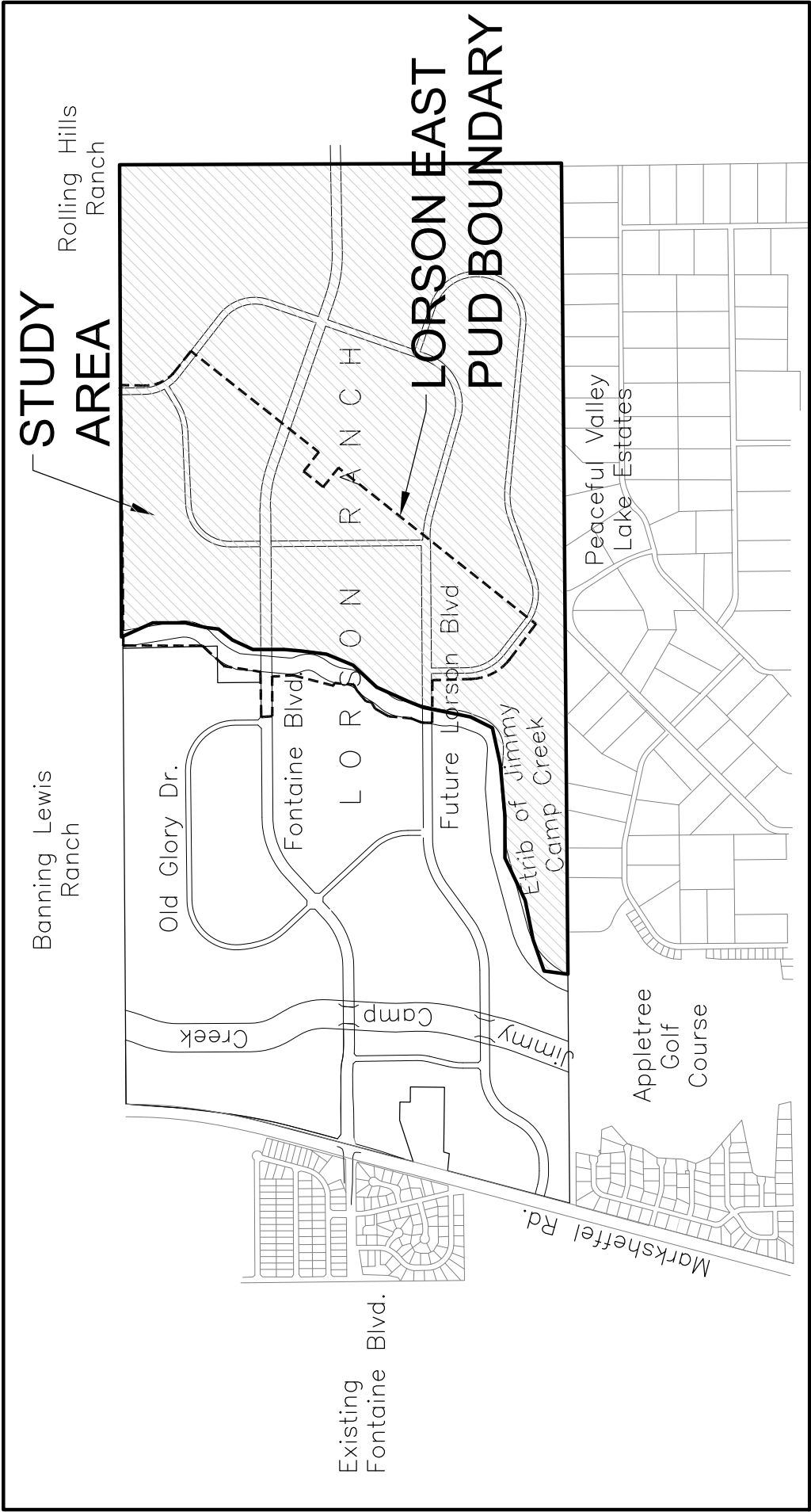
This drainage report has been prepared in accordance with the City of Colorado Springs/El Paso County Drainage Criteria Manual. The proposed development and drainage infrastructure will not cause adverse impacts to adjacent properties or properties located downstream. Several key aspects of the development discussed above are summarized as follows:

- Developed runoff will be conveyed via curb/gutter and storm sewer facilities
- Full Spectrum Detention is provided in all ponds
- Water Quality Capture Volume will be provided in all ponds

8.0 REFERENCES

1. City of Colorado Springs/El Paso County Drainage Criteria Manual DCM
2. Soil Survey of El Paso County Area, Colorado by USDA, SCS
3. Jimmy Camp Creek Drainage Basin Planning Study, 1987, Wilson & Co.
4. City of Colorado Springs "Drainage Criteria Manual, Volume 2
5. El Paso County "Engineering Criteria Manual"
6. Final Drainage Report for Fontaine Boulevard, Old Glory Drive, and Marksheffel Road Phase 1 Improvements, Dated February 6, 2006, Revised September 7, 2006, by Pentacor Engineering.
7. Drainage Basin Planning Study, Dated March 9, 2015, by Kiowa Engineering Corporation
8. El Paso County Resolution #15-042, El Paso County adoption of Chapter 6 and Section 3.2.1 of the City of Colorado Springs Drainage Criteria Manual dated May, 2014.

APPENDIX A – VICINTIY MAP, SOILS MAP, FEMA MAP



VICINITY MAP
NO SCALE



CORE
ENGINEERING GROUP

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LORSON RANCH EAST-MDDP
VICINITY MAP

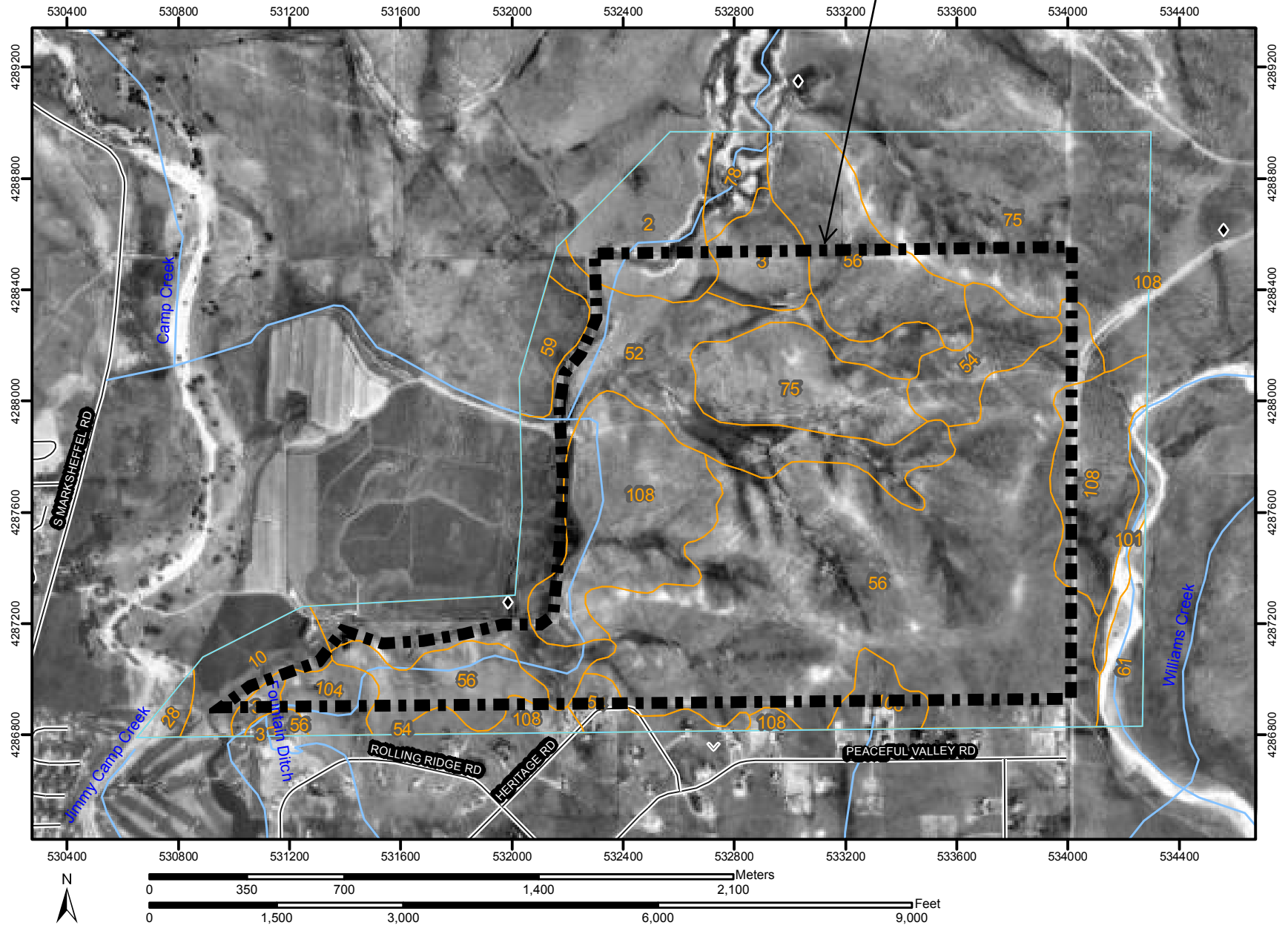
SCALE:
NTS

DATE:
JUNE, 2017

FIGURE NO.

Soil Map—El Paso County Area, Colorado
(LORSON RANCH EAST)


STUDY AREA



Soil Map—El Paso County Area, Colorado
(LORSON RANCH EAST)

MAP LEGEND






















Area of Interest (AOI)




 Area of Interest (AOI)

Soils




 Soil Map Units

Special Point Features

-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot
-  Spoil Area
-  Stony Spot



-  Very Stony Spot
-  Wet Spot
-  Other

Special Line Features



-  Gully
-  Short Steep Slope
-  Other

Political Features

Municipalities

-  Cities
-  Urban Areas






Water Features

-  Oceans
-  Streams and Canals

Transportation

-  Rails

Roads

-  Interstate Highways
-  US Routes
-  State Highways
-  Local Roads
-  Other Roads

MAP INFORMATION

Original soil survey map sheets were prepared at publication scale. Viewing scale and printing scale, however, may vary from the original. Please rely on the bar scale on each map sheet for proper map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
Coordinate System: UTM Zone 13N

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

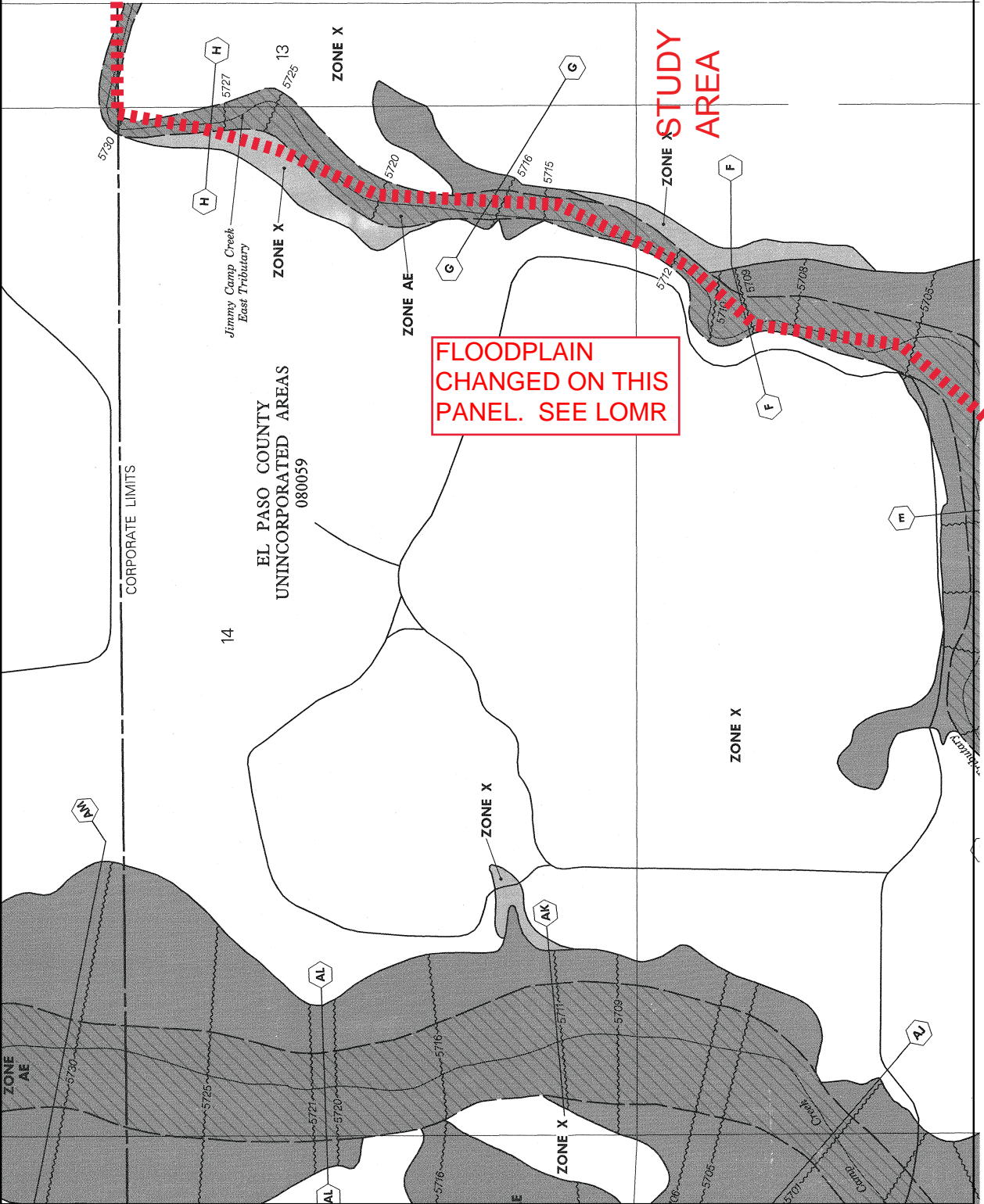
Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 5, Jan 15, 2008

Date(s) aerial images were photographed: 1999

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

El Paso County Area, Colorado (CO625)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
2	Ascalon sandy loam, 1 to 3 percent slopes	54.4	4.2%
3	Ascalon sandy loam, 3 to 9 percent slopes	32.6	2.5%
10	Blendon sandy loam, 0 to 3 percent slopes	29.0	2.2%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	5.5	0.4%
52	Manzanola clay loam, 1 to 3 percent slopes	180.3	14.0%
54	Midway clay loam, 3 to 25 percent slopes	46.2	3.6%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	476.6	37.0%
59	Nunn clay loam, 0 to 3 percent slopes	16.8	1.3%
61	Olney sandy loam, 3 to 5 percent slopes	18.8	1.5%
75	Razor-Midway complex	213.9	16.6%
78	Sampson loam, 0 to 3 percent slopes	16.4	1.3%
101	Ustic Torrifluvents, loamy	11.3	0.9%
104	Vona sandy loam, 1 to 3 percent slopes	17.4	1.4%
108	Wiley silt loam, 3 to 9 percent slopes	170.2	13.2%
Totals for Area of Interest (AOI)		1,289.3	100.0%



APPROXIMATE SCALE IN FEET

500
0
500

NATIONAL FLOOD INSURANCE PROGRAM

FIRM FLOOD INSURANCE RATE MAP

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 957 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:	COMMUNITY	NUMBER	PANEL	SUFFIX
	COLORADO SPRINGS, CITY OF	080050	0987	F
	EL PASO COUNTY UNINCORPORATED AREAS	080059	0987	F
	FOUNTAIN, CITY OF	080061	0987	F

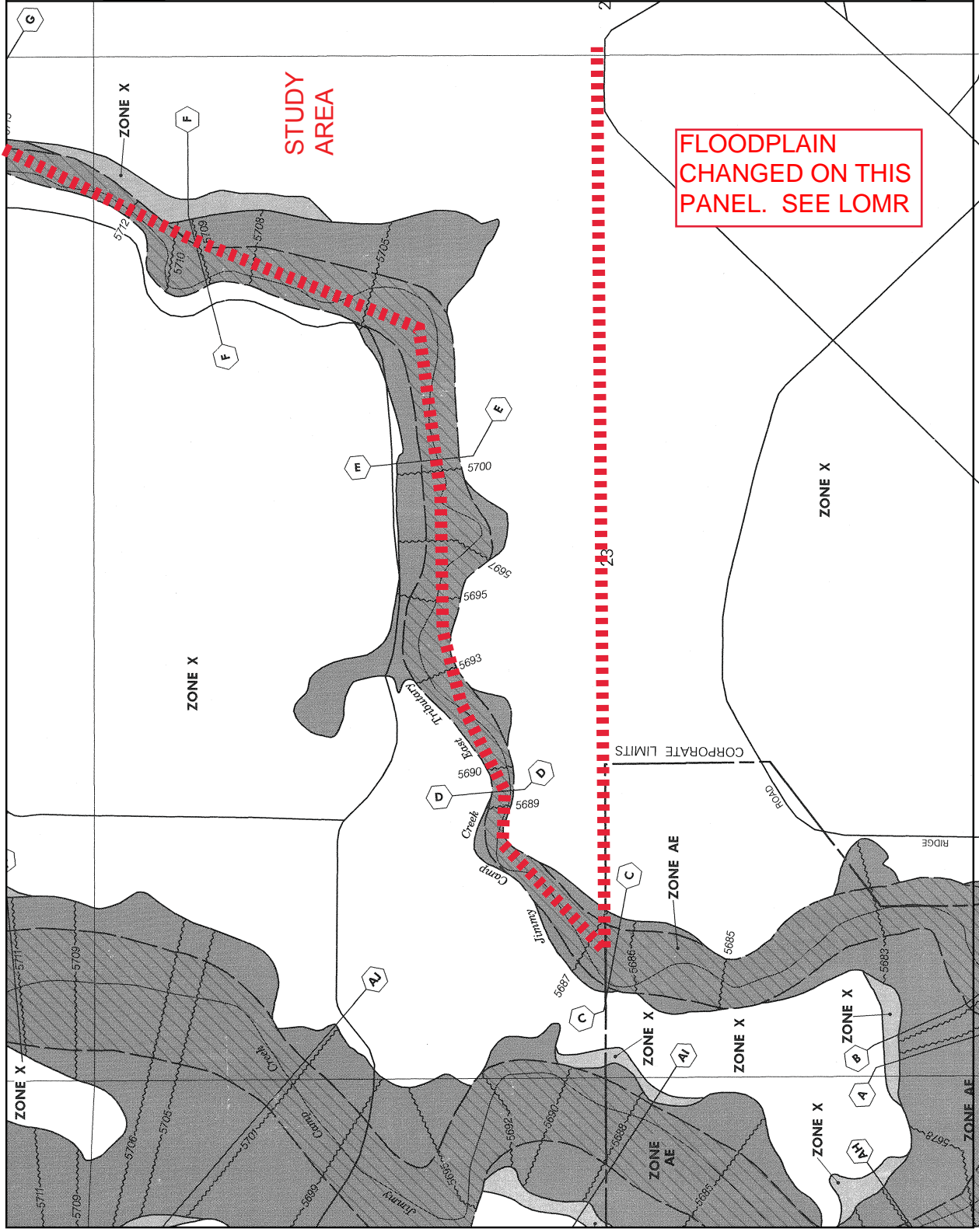
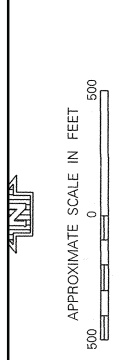
MAP NUMBER 08041C0957 F

EFFECTIVE DATE: MARCH 17, 1997

Federal Emergency Management Agency

This is an official copy of a portion of the above referenced flood map. It was extracted using the National Flood Insurance Program's software. One should not use this map for any other purpose. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at www.nas.fema.gov

JOINS PANEL 1000



NATIONAL FLOOD INSURANCE PROGRAM


FIRM FLOOD INSURANCE RATE MAP

EL PASO COUNTY,
COLORADO AND
INCORPORATED AREAS

PANEL 957 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS	COMMUNITY	NUMBER	PANEL	SUFFIX
	COLORADO SPRINGS, CITY OF	080080	0987	F
	EL PASO COUNTY UNINCORPORATED AREAS	080089	0987	F
	FOUNTAIN, CITY OF	080081	0987	F




MAP NUMBER 08041C0957 F
EFFECTIVE DATE: MARCH 17, 1997



Federal Emergency Management Agency

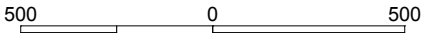
This is an official copy of a portion of the above referenced flood map. It was created using a firm's data. This map does not represent a change in the flood insurance rate map. Changes may be made to the flood insurance rate map without notice. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at www.nas.fema.gov

Legend

-  1% annual chance (100-Year) Floodplain
-  1% annual chance (100-Year) Floodway
-  0.2% annual chance (500-Year) Floodplain



APPROXIMATE SCALE IN FEET



NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

EL PASO COUNTY,
COLORADO AND
INCORPORATED AREAS

**REVISED TO
REFLECT LOMR
EFFECTIVE: January 29, 2015**

PANEL 957 OF 1300

(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0957	F
EL PASO COUNTY UNINCORPORATED AREAS	080059	0957	F
FOUNTAIN, CITY OF	080061	0957	F

MAP NUMBER
08041C0957 F

EFFECTIVE DATE:
MARCH 17, 1997



Federal Emergency Management Agency

JOINS PANEL 0769

104°37'30"
38°45'00"

NOTE: MAP AREA SHOWN ON THIS
PANEL IS LOCATED WITHIN TOWNSHIP
15 SOUTH, RANGE 65 WEST.

CITY OF
COLORADO SPRINGS
080060

Jimmy Camp Creek
East Tributary

REVISED
AREA

ZONE AE

EL PASO COUNTY
UNINCORPORATED AREAS
080059

AREA REVISED BY LOMR
DATED AUGUST 29, 2007.

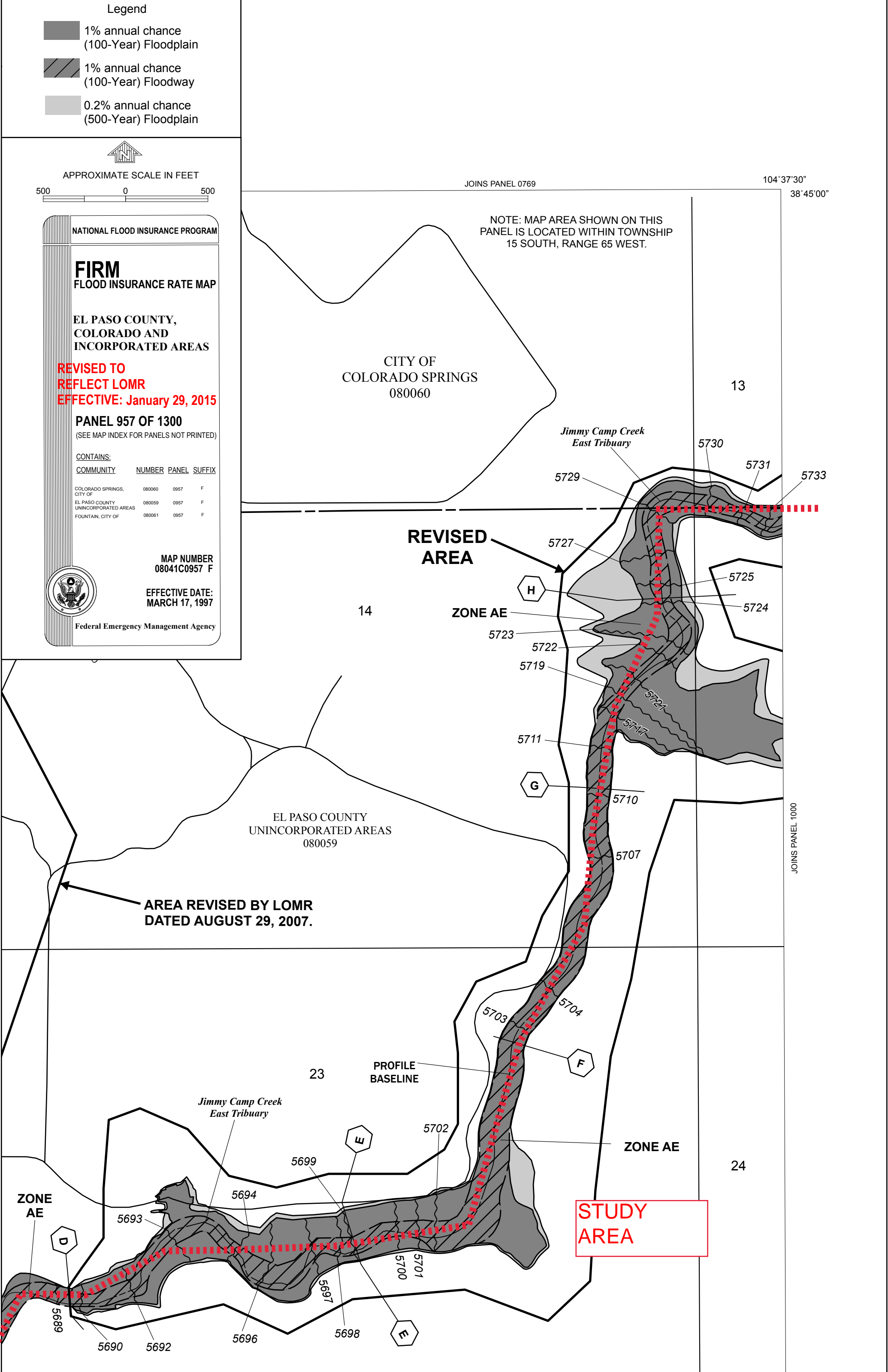
PROFILE
BASELINE

Jimmy Camp Creek
East Tributary




ZONE AE

STUDY
AREA

JOINS PANEL 1000



Legend

-  1% annual chance (100-Year) Floodplain
-  1% annual chance (100-Year) Floodway
-  0.2% annual chance (500-Year) Floodplain



NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO AND
INCORPORATED AREAS

PANEL 1000 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:

COMMUNITY	NUMBER	PANEL SUFFIX
COLORADO SPRINGS, CITY OF	080060	1000 F
EL PASO COUNTY, UNINCORPORATED AREAS	080059	1000 F

REVISED TO REFLECT LOMR EFFECTIVE: January 29, 2015

MAP NUMBER
08041C1000 F

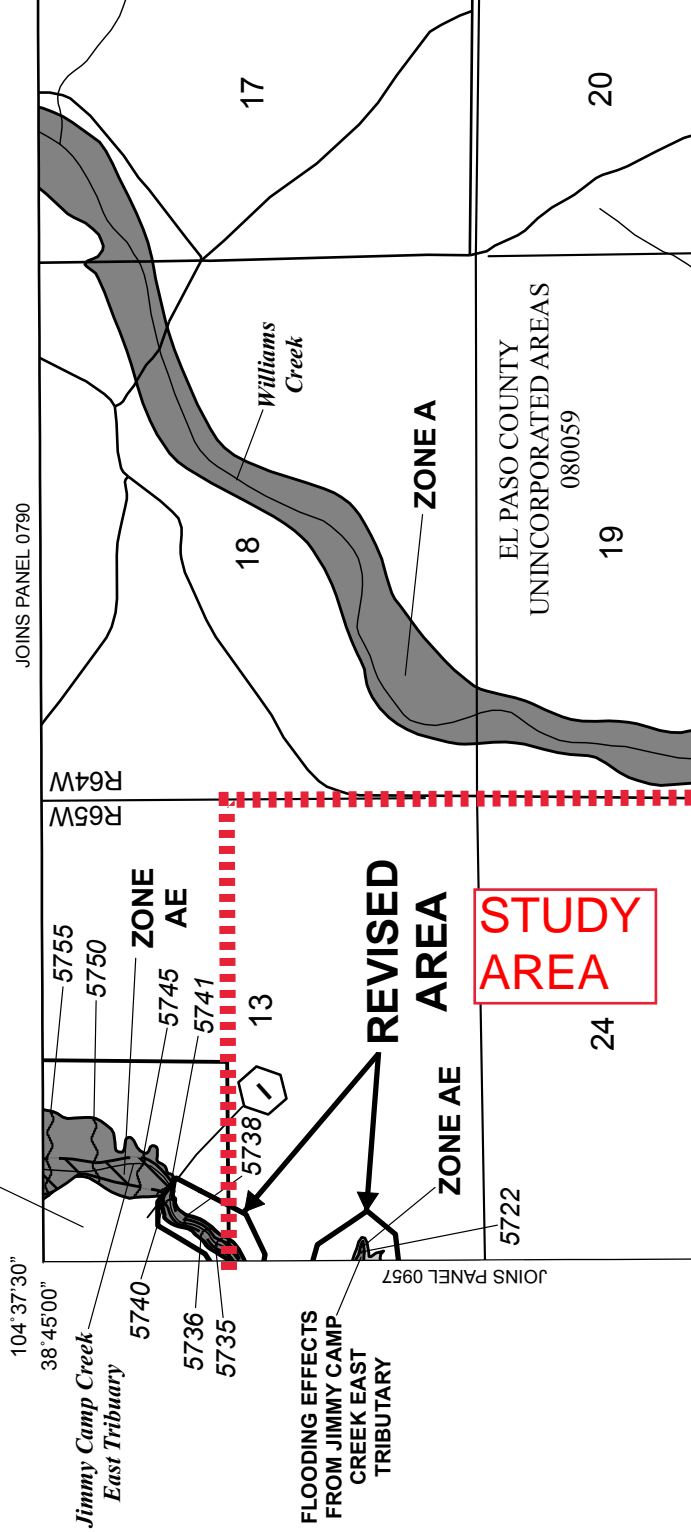
EFFECTIVE DATE:
MARCH 17, 1997



Federal Emergency Management Agency

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 64 WEST AND TOWNSHIP 16 SOUTH, RANGE 65 WEST.

CITY OF
COLORADO SPRINGS
0800060



APPENDIX B – HYDROLOGY & HYDRAULIC CALCULATIONS



15004 1st Avenue South
Burnsville, MN 55306

PROJECT NAME: Lorson Ranch East MDDP
PROJECT NUMBER: 100.032
ENGINEER: LAB
DATE: April 27, 2016

Master Development Drainage Plan
EXISTING CONDITIONS RUNOFF COEFFICIENTS

BASIN	Soil No.	Hydro Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Type of Cover
EX-C1	108	B	0.10	0.09%	0.08	0.00	0.35	0.00	61	0.1	
	56	C	107.02	97.32%	0.15	0.15	0.50	0.49	74	72.0	
	54	D	2.85	2.59%	0.15	0.00	0.50	0.01	80	2.1	
			109.97	100.00%		0.15		0.50		74.1	
EX-C2	75	C	9.84	92.22%	0.15	0.14	0.50	0.46	74	68.2	
	54	D	0.83	7.78%	0.15	0.01	0.50	0.04	80	6.2	
			10.67	100.00%		0.15		0.50		74.5	
EX-C3	108	B	4.22	5.67%	0.08	0.00	0.35	0.02	61	3.5	
	52 & 56	C	70.18	94.33%	0.15	0.14	0.50	0.47	74	69.8	
			74.40	100.00%		0.15		0.49		73.3	
EX-C5	108	B	1.46	1.43%	0.08	0.00	0.35	0.01	61	0.9	
	56	C	71.84	70.30%	0.15	0.11	0.50	0.35	74	52.0	
	54	D	28.89	28.27%	0.15	0.04	0.50	0.14	80	22.6	
			102.19	100.00%		0.15		0.50		75.5	
EX-C6	3	B	1.02	8.94%	0.08	0.01	0.35	0.03	61	5.5	
	56	C	10.39	91.06%	0.15	0.14	0.50	0.46	74	67.4	
			11.41	100.00%		0.14		0.49		72.8	
EX-C7	3	B	6.24	15.99%	0.08	0.01	0.35	0.06	61	9.8	
	75	C	32.78	84.01%	0.15	0.13	0.50	0.42	74	62.2	
			39.02	100.00%		0.14		0.48		71.9	
EX-C8	108	B	3.90	30.90%	0.08	0.02	0.35	0.11	61	18.9	
	75	C	8.72	69.10%	0.15	0.10	0.50	0.35	74	51.1	
			12.62	100.00%		0.13		0.45		70.0	
EX-C9	2 & 3	B	15.57	37.81%	0.08	0.03	0.35	0.13	61	23.1	
	52	C	25.61	62.19%	0.15	0.09	0.50	0.31	74	46.0	
			41.18	100.00%		0.12		0.44		69.1	



15004 1st Avenue South
Burnsville, MN 55306

PROJECT NAME: Lorson Ranch East MDDP

PROJECT NUMBER: 100.032

ENGINEER: LAB

DATE: April 27, 2016

Master Development Drainage Plan

EXISTING CONDITIONS RUNOFF COEFFICIENTS

BASIN	Soil No.	Hydro Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Type of Cover
EX-C10	108	B	7.51	68.96%	0.08	0.06	0.35	0.24	61	42.1	
	52	C	3.38	31.04%	0.15	0.05	0.50	0.16	74	23.0	
			10.89	100.00%		0.10		0.40		65.0	
EX-C	108	B	40.02	8.84%	0.08	0.01	0.35	0.03	40	3.5	
	56	C	380.38	83.97%	0.15	0.13	0.50	0.42	54	45.3	
	54	D	32.57	7.19%	0.15	0.01	0.50	0.04	63	4.5	
			452.97	100.00%		0.14		0.49		53.4	
EX-D1	108	B	18.79	93.95%	0.08	0.08	0.35	0.33	61	57.3	
	56	C	1.21	6.05%	0.15	0.01	0.50	0.03	74	4.5	
			20.00	100.00%		0.08		0.36		61.8	
EX-D2	108	B	50.90	56.84%	0.08	0.05	0.35	0.20	61	34.7	
	56	C	38.65	43.16%	0.15	0.06	0.50	0.22	74	31.9	
			89.55	100.00%		0.11		0.41		66.6	
EX-D	108	B	69.69	63.61%	0.08	0.05	0.35	0.22	61	38.8	
	56	C	39.86	36.39%	0.15	0.05	0.50	0.18	74	26.9	
			109.55	100.00%		0.11		0.40		65.7	
EX-E1	108	B	5.47	6.88%	0.08	0.01	0.35	0.02	61	4.2	
	56	C	73.88	92.86%	0.15	0.14	0.50	0.46	74	68.7	
	54	D	0.21	0.26%	0.15	0.00	0.50	0.00	80	0.2	
			79.56	100.00%		0.15		0.49		73.1	
EX-E2	108	B	0.44	2.56%	0.08	0.00	0.35	0.01	61	1.6	
	56	C	13.55	78.73%	0.15	0.12	0.50	0.39	74	58.3	
	54	D	3.22	18.71%	0.15	0.03	0.50	0.09	80	15.0	
			17.21	100.00%		0.15		0.50		74.8	



15004 1st Avenue South
Burnsville, MN 55306

PROJECT NAME: Lorson Ranch East MDDP
PROJECT NUMBER: 100.032
ENGINEER: LAB
DATE: April 27, 2016

Master Development Drainage Plan
EXISTING CONDITIONS RUNOFF COEFFICIENTS

BASIN	Soil No.	Hydro Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Type of Cover
OS-E1.1	108	B	4.76	15.50%	0.08	0.01	0.35	0.05	61	9.5	
	56	C	7.72	25.15%	0.15	0.04	0.50	0.13	74	18.6	
	54	D	18.22	59.35%	0.15	0.09	0.50	0.30	80	47.5	
			30.70	100.00%		0.14		0.48		75.5	
OS-E2.1	108	B	32.76	69.84%	0.08	0.06	0.35	0.24	61	42.6	
	56	C	0.89	1.90%	0.15	0.00	0.50	0.01	74	1.4	
	54	D	13.26	28.27%	0.15	0.04	0.50	0.14	80	22.6	
			46.91	100.00%		0.10		0.40		66.6	
EX-E	108	B	43.43	23.31%	0.08	0.02	0.35	0.08	40	9.3	
	56	C	107.96	57.95%	0.15	0.09	0.50	0.29	54	31.3	
	54	D	34.91	18.74%	0.15	0.03	0.50	0.09	63	11.8	
			186.30	100.00%		0.13		0.47		52.4	
EX-F1	108	B	8.74	39.09%	0.08	0.03	0.35	0.14	61	23.8	
	56	C	13.62	60.91%	0.15	0.09	0.50	0.30	74	45.1	
			22.36	100.00%		0.12		0.44		68.9	
EX-F2	108	B	0.23	1.32%	0.08	0.00	0.35	0.00	61	0.8	
	56	C	17.26	98.68%	0.15	0.15	0.50	0.49	74	73.0	
			17.49	100.00%		0.15		0.50		73.8	
EX-F	108	B	8.97	22.51%	0.08	0.02	0.35	0.08	61	13.7	
	56	C	30.88	77.49%	0.15	0.12	0.50	0.39	74	57.3	
			39.85	100.00%		0.13		0.47		71.1	
EX-H1	108	B	7.70	27.37%	0.08	0.02	0.35	0.10	61	16.7	
	56	C	20.43	72.63%	0.15	0.11	0.50	0.36	74	53.7	
			28.13	100.00%		0.13		0.46		70.4	
OS-I1.1	108	B	11.51	72.12%	0.08	0.06	0.35	0.25	61	44.0	
	56	C	4.45	27.88%	0.15	0.04	0.50	0.14	74	20.6	
			15.96	100.00%		0.10		0.39		64.6	

These seem high for existing. Provide land use/impervious table and coefficients tables.



15004 1st Avenue South
Burnsville, MN 55306

Master Development Drainage Plan
EXISTING CONDITIONS RUNOFF COEFFICIENTS

PROJECT NAME: Lorson Ranch East MDDP
PROJECT NUMBER: 100.032
ENGINEER: LAB
DATE: April 27, 2016

BASIN	Soil No.	Hydro Group	Area	Cover (%)	C5	Wtd. C5	C100	Wtd. C100	CN	Wtd. CN	Type of Cover
EX-I	108	B	11.51	34.96%	0.08	0.03	0.35	0.12	61	21.3	
	56	C	21.41	65.04%	0.15	0.10	0.50	0.33	74	48.1	
			32.92	100.00%		0.13		0.45		69.5	
EX-J1	104	B	9.20	68.55%	0.08	0.05	0.35	0.24	61	41.8	
	56	C	4.22	31.45%	0.15	0.05	0.50	0.16	74	23.3	
			13.42	100.00%		0.10		0.40		65.1	
OS-J1.1	104	B	3.84	31.07%	0.08	0.02	0.35	0.11	61	19.0	
	56	C	8.52	68.93%	0.15	0.10	0.50	0.34	74	51.0	
			12.36	100.00%		0.13		0.45		70.0	
EX-J	104	B	13.08	50.74%	0.08	0.04	0.35	0.18	61	30.9	
	56	C	12.70	49.26%	0.15	0.07	0.50	0.25	74	36.5	
			25.78	100.00%		0.11		0.42		67.4	



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: June, 2017
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP
 Design Storm: **5 - Year Event, Existing Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff			Street		Pipe			Travel Time			Remarks	
		Area Design	Area (A)	Runoff Coeff. (C)	t_c	CA	i	Q	t_c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity		t_t
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec		min
EX-A1			4.28	0.08	18.6	0.34	3.20	1.1													
EX-B1			14.42	0.15	16.9	2.16	3.34	7.2													
OS-B1.1			5.64	0.15	14.7	0.85	3.55	3.0													
EX-B	DP-1		20.06	0.15					15.3	3.01	3.49	10.5									
EX-C1			109.97	0.15	29.6	16.50	2.50	41.3													
EX-C2			10.67	0.15	14.7	1.60	3.55	5.7													
EX-C3			74.40	0.15	30.2	11.16	2.47	27.6													
EX-C4			27.13	0.15	19.6	4.07	3.12	12.7													
OS-C5.1			3.59	0.15	12.6	0.54	3.78	2.0													
EX-C5			102.19	0.15	30.4	15.33	2.46	37.7													
OS-C6.1			9.96	0.15	14.1	1.49	3.61	5.4													
EX-C6			11.47	0.14	19.5	1.61	3.13	5.0													
EX-C7			39.02	0.14	22.7	5.46	2.90	15.8													
EX-C8			12.62	0.13	19.8	1.64	3.10	5.1													
EX-C9			41.18	0.12	21.7	4.94	2.97	14.7													
EX-C10			10.89	0.10	18.1	1.09	3.24	3.5													
EX-C	DP-2		452.97	CN = 67						SCS =		141.0									
EX-D	DP-3		109.55	0.12	34.7	13.15	2.26	29.7													
OS-E1.1			31.10	0.25	17.0	7.78	3.33	25.9													
EX-E1			79.50	0.15	33.0	11.93	2.34	27.9													
OS-E2.1			46.90	0.25	18.1	11.73	3.24	38.0													
EX-E2			30.40	0.15	17.0	4.56	3.33	15.2													
EX-E	DP-4		187.30	CN = 73						SCS =		100.0									
EX-F1			22.36	0.12	13.8	2.68	3.65	9.8													
EX-F2			17.49	0.15	13.5	2.62	3.68	9.7													
EX-F	DP-5		39.85	0.13					13.8	5.31	3.65	19.3									
EX-G			14.91	0.15	15.0	2.24	3.52	7.9													
EX-H			28.13	0.13	16.6	3.66	3.37	12.3													
OS-I1.1			15.96	0.10	16.4	1.60	3.39	5.4													



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: June, 2017
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP
 Design Storm: **5 - Year Event, Existing Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe		Travel Time			Remarks	
		Area Design	Area (A)	Runoff Coeff. (C)	t _c	CA	i	Q	t _c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity		t _t
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec		min
EX-I1			16.96	0.15	15.7	2.54	3.45	8.8													
EX-I	DP-8		32.92	0.13					21.2	4.14	3.00	12.4									
OS-J1.1			12.36	0.13	17.0	1.61	3.33	5.4													
EX-J1			13.42	0.10	15.3	1.34	3.49	4.7													
EX-J	DP-9		25.78	0.11					20.6	2.95	3.05	9.0									
OS-K1.1			1.98	0.08	16.0	0.16	3.42	0.5													
EX-K1			5.59	0.08	15.3	0.45	3.49	1.6													
EX-K	DP-10		7.57	0.08					16.0	0.61	3.42	2.1									

Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: April 28, 2016
 Checked By: Leonard Beasley

Job No: 100.032
 Project: Lorson Ranch East MDDP
 Design Storm: **100 - Year Event, Existing Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t_c	CA	i	Q	t_c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t_t	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX-A1			4.28	0.35	18.6	1.50	5.37	8.0													
EX-B1			14.42	0.50	16.9	7.21	5.61	40.4													
OS-B1.1			5.64	0.50	14.7	2.82	5.96	16.8													
EX-B	DP-1		20.06	0.50					15.3	10.03	5.86	58.8									
EX-C1			109.97	0.50	29.6	54.99	4.20	230.8													
EX-C2			10.67	0.50	14.7	5.34	5.96	31.8													
EX-C3			74.40	0.49	30.2	36.46	4.15	151.2													
EX-C4			27.13	0.50	19.6	13.57	5.24	71.0													
OS-C5.1			3.59	0.50	12.6	1.80	6.35	11.4													
EX-C5			102.19	0.50	30.4	51.10	4.13	211.1													
OS-C6.1			9.96	0.50	14.1	4.98	6.07	30.2													
EX-C6			11.47	0.49	19.5	5.62	5.25	29.5													
EX-C7			39.02	0.48	22.7	18.73	4.87	91.2													
EX-C8			12.62	0.45	19.8	5.68	5.21	29.6													
EX-C9			41.18	0.44	21.7	18.12	4.98	90.2													
EX-C10			10.89	0.40	18.1	4.36	5.44	23.7													
EX-C	DP-2		452.97	CN = 67						SCS =		458.0									
EX-D	DP-3		109.55	0.40	34.7	43.82	3.80	166.5													
OS-E1.1			31.10	0.48	17.0	14.93	5.60	83.5													
EX-E1			79.50	0.49	33.0	38.96	3.92	152.9													
OS-E2.1			46.90	0.40	18.1	18.76	5.44	102.0													
EX-E2			30.40	0.50	17.0	15.20	5.60	85.0													
EX-E	DP-4		187.30	CN = 73						SCS =		280.0									
EX-F1			22.36	0.44	13.8	9.84	6.12	60.2													
EX-F2			17.49	0.50	13.5	8.75	6.18	54.0													
EX-F	DP-5		39.85	0.47					13.8	18.58	6.12	113.7									
EX-G			14.91	0.50	15.0	7.46	5.91	44.1													
EX-H			28.13	0.46	16.6	12.94	5.66	73.2													
OS-I1.1			15.96	0.39	16.4	6.22	5.69	35.4													



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: April 28, 2016
 Checked By: Leonard Beasley

Job No: 100.032
 Project: Lorson Ranch East MDDP
 Design Storm: **100 - Year Event, Existing Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t_c	CA	i	Q	t_c	$\Sigma(CA)$	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t_t	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
EX-I1			16.96	0.50	15.7	8.48	5.80	49.1													
EX-I	DP-8		32.92	0.45					21.2	14.70	5.04	74.1									
OS-J1.1			12.36	0.45	17.0	5.56	5.60	31.1													
EX-J1			13.42	0.40	15.3	5.37	5.86	31.5													
EX-J	DP-9		25.78	0.42					20.6	10.93	5.11	55.9									
OS-K1.1			1.98	0.35	16.0	0.69	5.75	4.0													
EX-K1			5.59	0.35	15.3	1.96	5.86	11.5													
EX-K	DP-10		7.57	0.35					16.0	2.65	5.75	15.2									

Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 4:1 PM

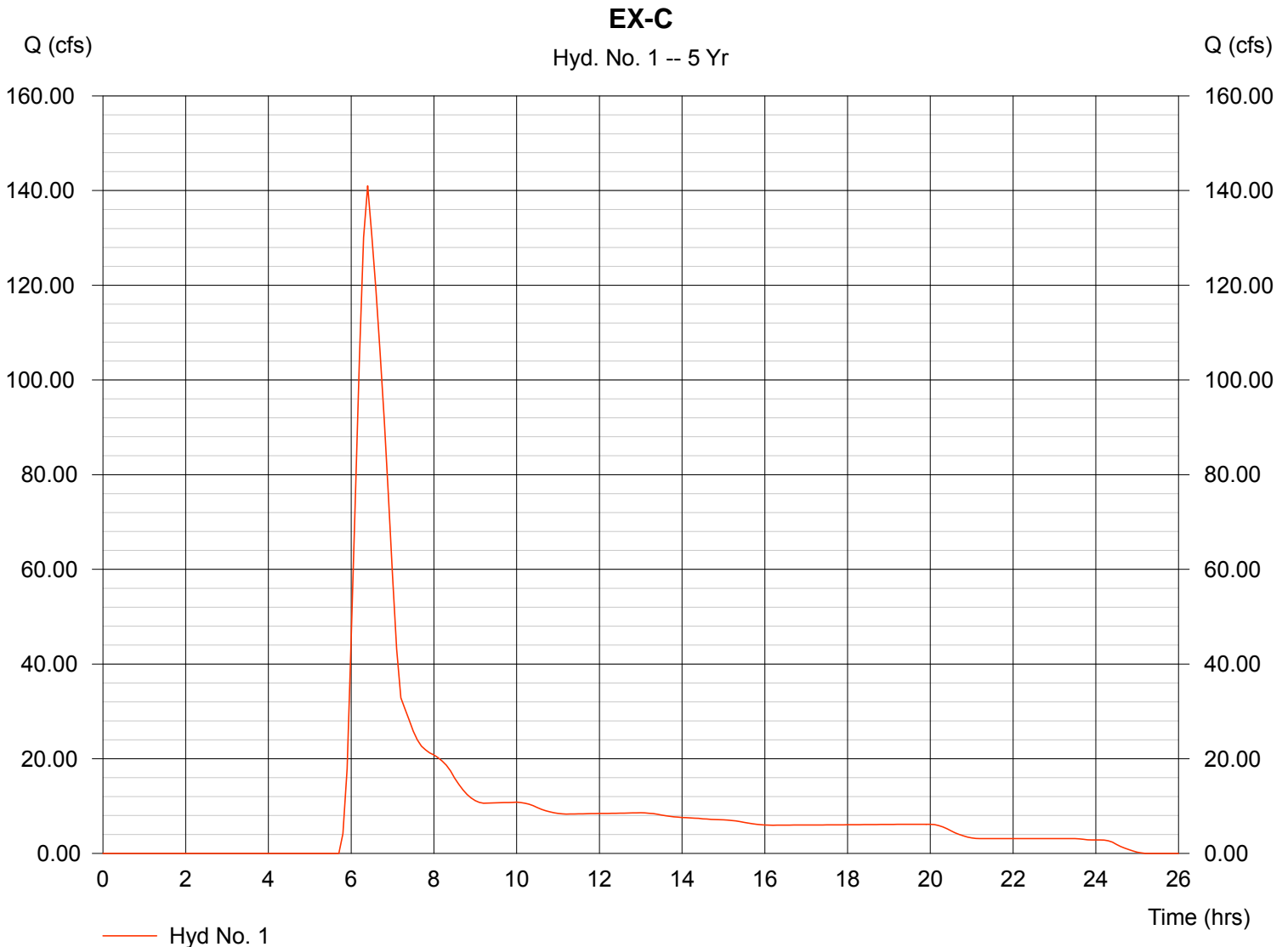
Hyd. No. 1

EX-C

Hydrograph type = SCS Runoff
Storm frequency = 5 yrs
Drainage area = 452.970 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 2.80 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 140.99 cfs
Time interval = 6 min
Curve number = 69
Hydraulic length = 7400 ft
Time of conc. (Tc) = 49.50 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 905,484 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 4:1 PM

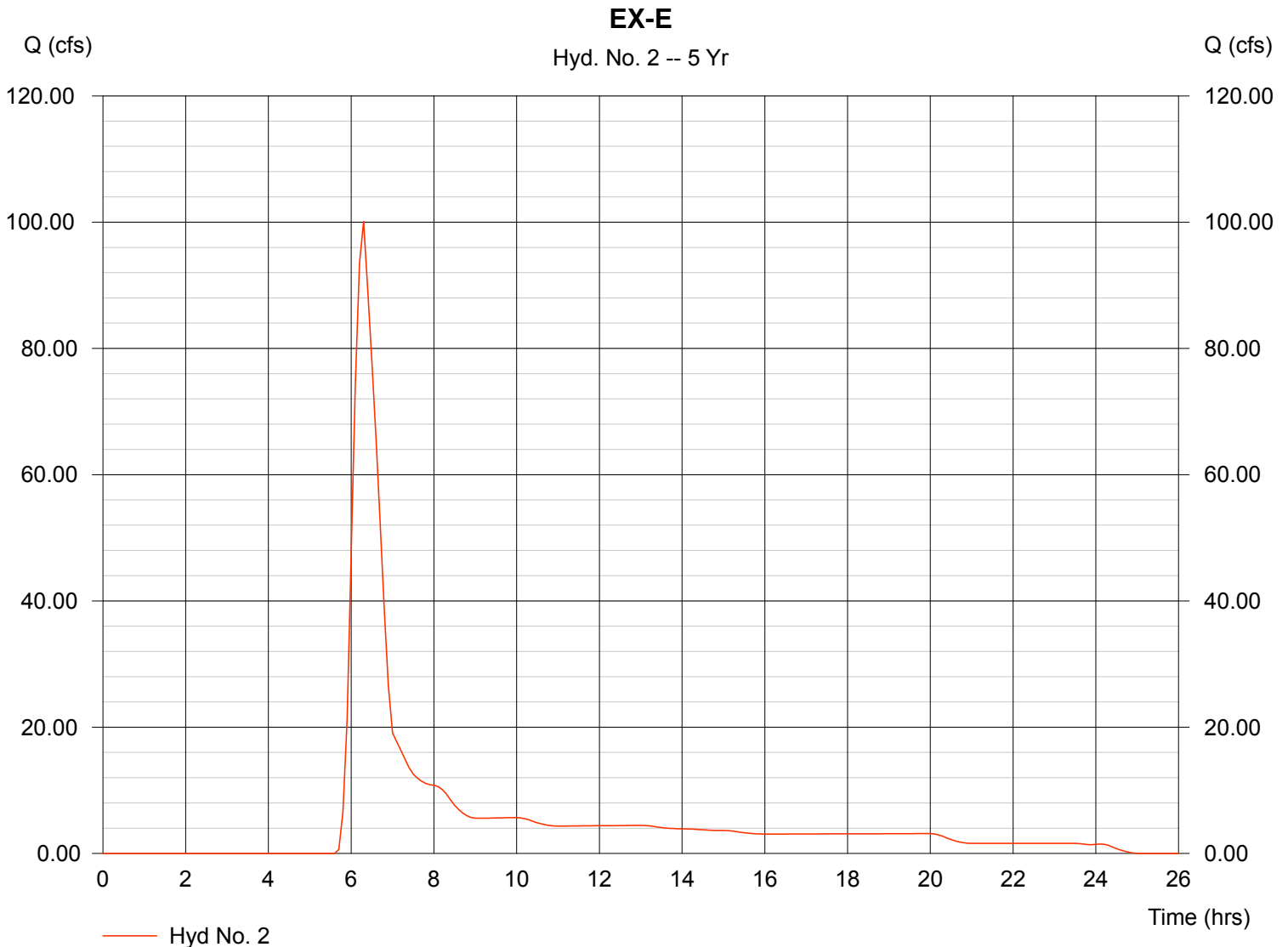
Hyd. No. 2

EX-E

Hydrograph type = SCS Runoff
Storm frequency = 5 yrs
Drainage area = 187.300 ac
Basin Slope = 3.0 %
Tc method = USER
Total precip. = 2.80 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 100.11 cfs
Time interval = 6 min
Curve number = 73
Hydraulic length = 4150 ft
Time of conc. (Tc) = 33.00 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 513,793 cuft



Hydrograph Plot

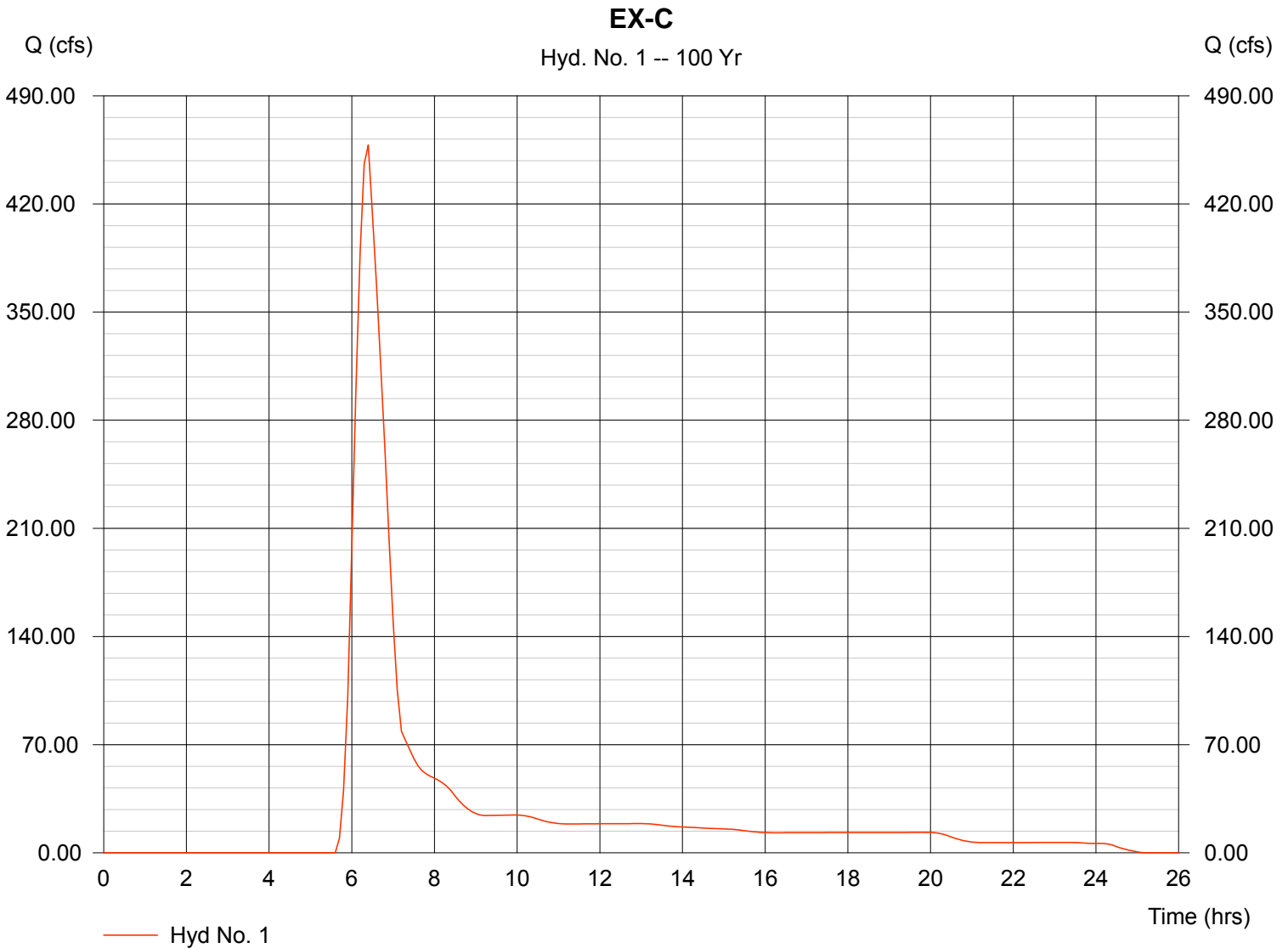
Hyd. No. 1

EX-C

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 452.970 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 4.40 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 458.13 cfs
Time interval = 6 min
Curve number = 69
Hydraulic length = 7400 ft
Time of conc. (Tc) = 49.50 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 2,456,980 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 4:1 PM

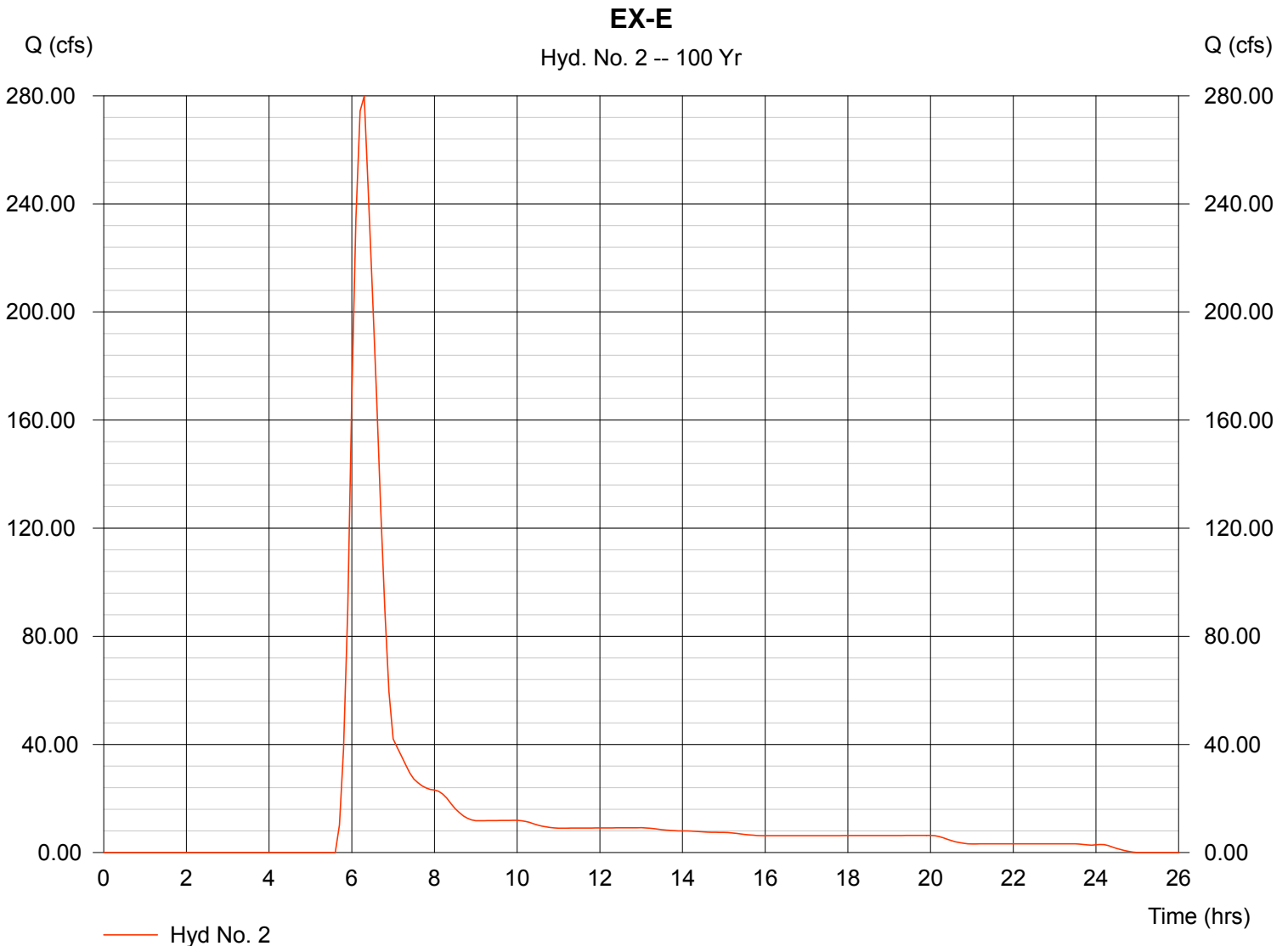
Hyd. No. 2

EX-E

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 187.300 ac
Basin Slope = 3.0 %
Tc method = USER
Total precip. = 4.40 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 279.84 cfs
Time interval = 6 min
Curve number = 73
Hydraulic length = 4150 ft
Time of conc. (Tc) = 33.00 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 1,267,200 cuft



Standard Form SF-1. Time of Concentration-Proposed

Calculated By: Leonard Beasley

Job No: 100.013

Date: September, 2016

Project: Lorson Ranch East MDDP

Checked By: Leonard Beasley

Sub-Basin Data				Initial Overland Time (t _i)				Travel Time (t _t)					t _c Check (urbanized Basins)		Final t _c
BASIN or DESIGN	C _s	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _i minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _t minutes	Computed t _c Minutes	TOTAL LENGTH (L) feet	Regional t _c =(L/180)+10 minutes	USDCM Recommended t _c =t _i +t _t (min)
A	0.08	2.6	7.0	100.00	8.00%	0.18	9.27	928.00	0.54%	0.51	30.07	39.34	1028.00	15.71	15.71
OS-B1	0.15	5.6	20.0	100.00	7.00%	0.18	9.02	435.00	4.25%	4.12	1.76	10.78	535.00	12.97	10.78
B2	0.49	3.9	20.0	100.00	3.60%	0.23	7.22	1652.00	2.08%	2.88	9.55	16.76	1752.00	19.73	16.76
B	0.15	9.5	20.0	100.00	7.00%	0.18	9.02	2119.00	2.55%	3.19	11.06	20.08	2219.00	22.33	20.08
C1	0.49	23.2	15.0	100.00	1.30%	0.17	10.10	900.00	3.30%	2.72	5.50				
			20.0					1000.00	3.20%	3.58	4.66	20.26	2000.00	21.11	20.26
C2	0.49	34.5	15.0	75.00	2.00%	0.16	7.59	5.00	0.72%	1.27	0.07				
			20.0					510.00	3.70%	3.85	2.21				
			pipe					1385.00	2.70%	15.63	1.48	11.34	1975.00	20.97	11.34
DP-2	0.49	57.7	15.0	100.00	0.90%	0.15	11.40	1105.00	3.19%	2.68	6.87				
			20.0					547.00	4.02%	4.01	2.27				
			pipe					1494.00	1.00%	15.63	1.59	22.14	3246.00	28.03	22.14
C3	0.49	8.3	15.0	100.00	2.70%	0.21	7.94	200.00	2.70%	2.46	1.35				
			20.0					1161.00	2.07%	2.88	6.72	16.01	1461.00	18.12	16.01
C4	0.49	57.5	15.0	100.00	1.87%	0.19	8.96	755.00	1.87%	2.05	6.13				
			20.0					1318.00	2.28%	3.02	7.27				
			pipe					1230.00	2.93%	14.30	1.43	23.80	3403.00	28.91	23.80
C5	0.49	25.0	15.0	100.00	4.20%	0.24	6.86	200.00	4.15%	3.06	1.09				
			15.0					498.00	5.12%	3.39	2.45				
			20.0					1328.00	4.52%	4.25	5.21	15.60	1428.00	17.93	15.60
C6	0.49	18.7	20.0	100.00	1.00%	0.15	11.01	885.00	3.62%	3.81	3.88				
			pipe					831.00	2.41%	17.73	0.78	15.67	1816.00	20.09	15.67
C7	0.49	14.5	20.0	100.00	2.00%	0.19	8.76	681.00	2.50%	3.16	3.59				
			pipe					831.00	2.41%	17.73	0.78	13.13	1612.00	18.96	13.13
DP-4	0.49	124.0	15.0	100.00	1.87%	0.19	8.96	755.00	1.87%	2.05	6.13				
			20.0					1318.00	2.28%	3.02	7.27				
			24"					1230.00	2.93%	14.30	1.43				
			48"					831.00	2.41%	17.73	0.78				
			54"					200.00	2.50%	19.55	0.17	24.75	4434.00	34.63	24.75
C8	0.49	74.5	15.0	100.00	5.30%	0.26	6.35	1415.00	5.40%	3.49	6.77				
			20.0					883.00	2.50%	3.16	4.65	17.77	2398.00	23.32	17.77
C8a	0.49	11.7	15.0	100.00	2.00%	0.19	8.76	100.00	2.00%	2.12	0.79				
			20.0					715.00	5.17%	4.55	2.62	12.17	915.00	15.08	12.17
OS-C9	0.49	5.2	15.0	100.00	4.18%	0.24	6.87	810.00	4.18%	3.07	4.40	11.27	910.00	15.06	11.27
C10	0.49	13.0	15.0	100.00	3.00%	0.22	7.66	100.00	3.00%	2.60	0.64				

Standard Form SF-1. Time of Concentration-Proposed

Calculated By: Leonard Beasley
 Date: September, 2016
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP

Sub-Basin Data				Initial Overland Time (t _i)				Travel Time (t _t)					t _c Check (urbanized Basins)		Final t _c
BASIN or DESIGN	C _s	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _i minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _t minutes	Computed t _c Minutes	TOTAL LENGTH (L) feet	Regional t _c =(L/180)+10 minutes	USDCM Recommended t _c =t _i +t _t (min)
			20.0					957.00	2.60%	3.22	4.95				
			pipe					653.00	1.50%	8.91	1.22	14.47	1810.00	20.06	14.47
OS-C11	0.49	5.6	15.0	100.00	3.00%	0.22	7.66	100.00	3.00%	2.60	0.64				
			20.0					957.00	2.60%	3.22	4.95	13.25	1157.00	16.43	13.25
DP-5	0.49	5.2	15.0	100.00	4.18%	0.24	6.87	810.00	4.18%	3.07	4.40				
			20.0					1758.00	2.39%	3.09	9.48	20.75	2668.00	24.82	20.75
C12	0.49	19.6	15.0	100.00	3.00%	0.22	7.66	969.00	1.34%	1.74	9.30				
			20.0					292.00	0.60%	1.55	3.14	20.11	1361.00	17.56	17.56
C13	0.16	21.2	15.0	100.00	3.17%	0.14	11.60	595.00	3.17%	2.67	3.71				
			20.0					2968.00	1.00%	2.00	24.73	40.04	3663.00	30.35	30.35
DP-6	0.49	40.8	15.0	100.00	3.00%	0.22	7.66	969.00	1.34%	1.41	11.45				
			20.0					3280.00	0.82%	1.81	30.18	49.30	4349.00	34.16	34.16
C14	0.16	7.6	15.0	100.00	4.82%	0.17	10.10	382.00	4.82%	1.41	4.52				
			20.0					1404.00	4.50%	4.24	5.52	20.13	1886.00	20.48	20.48
C15	0.49	44.0	15.0	100.00	1.00%	0.15	11.01	238.00	2.10%	2.17	1.82				
			20.0					1758.00	2.39%	3.09	9.48	22.31	2096.00	21.64	22.31
C16	0.49	69.0	15.0	100.00	5.00%	0.26	6.48	100.00	5.00%	3.35	0.50				
			20.0					596.00	3.40%	3.69	2.69				
			pipe					2801.00	1.20%	7.93	5.89	15.55	3597.00	29.98	15.55
C17	0.49	18.8	15.0	100.00	4.00%	0.24	6.97	1462.00	3.42%	2.77	8.78				
			pipe					95.00	6.30%	18.10	0.09	15.84	1657.00	19.21	15.84
Basin C	0.49	464.9	15.0	100.00	4.18%	0.24	6.87	865.00	4.18%	3.07	4.70				
			20.0					4150.00	1.40%	2.37	29.23	40.80	5115.00	38.42	38.42
D1	0.49	17.0	15.0	100.00	3.30%	0.22	7.43	200.00	3.30%	2.72	1.22				
			20.0					909.00	4.50%	4.24	3.57	12.22	1209.00	16.72	12.22
D2	0.49	8.0	15.0	100.00	4.00%	0.24	6.97	600.00	3.69%	2.88	3.47	10.44	700.00	13.89	10.44
D3	0.49	23.0	15.0	100.00	3.00%	0.22	7.66	700.00	1.00%	1.50	7.78				
			20.0					400.00	3.00%	3.46	1.92	17.37	1200.00	16.67	16.67
D4	0.49	36.4	15.0	100.00	2.50%	0.20	8.14	100.00	3.50%	2.81	0.59				
			20.0					1400.00	2.90%	3.41	6.85	15.58	1600.00	18.89	15.58
D5	0.40	4.6	20.0	70.00	4.00%	0.17	6.69	300.00	0.50%	1.41	3.54				
								0.00	2.60%	15.17	0.00	10.23	370.00	12.06	10.23

Standard Form SF-1. Time of Concentration-Proposed

Calculated By: Leonard Beasley
 Date: September, 2016
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP

Sub-Basin Data				Initial Overland Time (t _i)				Travel Time (t _t)					t _c Check (urbanized Basins)		Final t _c
BASIN or DESIGN	C _s	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _i minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _t minutes	Computed t _c Minutes	TOTAL LENGTH (L) feet	Regional t _c =(L/180)+10 minutes	USDCM Recommended t _c =t _i +t _t (min)
DP-10	0.49	92.5	15.0	100.00	3.30%	0.22	7.43	200.00	3.30%	2.72	1.22				
			20.0						909.00	4.50%	4.24	3.57			
			20.0					1865.00	2.68%	3.27	9.49	21.71	1965.00	20.92	20.92
E1	0.49	10.2	15.0	100.00	2.30%	0.20	8.37	120.00	2.30%	2.27	0.88				
			20.0						1098.00	4.90%	4.43	4.13	13.38	1318.00	17.32
E2	0.49	10.3	15.0	100.00	4.90%	0.26	6.52	43.00	4.90%	3.32	0.22				
			20.0						1186.00	4.60%	4.29	4.61	11.34	1329.00	17.38
OS-E3	0.26	9.9	15.0	100.00	2.90%	0.16	10.67	200.00	2.90%	2.55	1.30				
			15.0						500.00	3.50%	2.81	2.97	14.95	800.00	14.44
E4	0.49	12.8	15.0	100.00	3.00%	0.22	7.66	900.00	4.70%	3.25	4.61				
			20.0						100.00	2.50%	3.16	0.53	12.80	1100.00	16.11
E5	0.49	13.3	15.0	100.00	3.00%	0.22	7.66	391.00	6.14%	3.72	1.75				
			20.0						657.00	2.40%	3.10	3.53	12.95	1148.00	16.38
DP-12	0.49	43.4	15.0	100.00	2.90%	0.22	7.75	200.00	2.90%	2.55	1.30				
			20.0						1400.00	3.50%	3.74	6.24	15.29	1700.00	19.44
OS-E6	0.26	20.8	15.0	100.00	2.70%	0.15	10.93	200.00	2.70%	2.46	1.35				
			20.0						920.00	1.70%	2.61	5.88	18.16	1220.00	16.78
E7	0.49	8.8	15.0	100.00	3.50%	0.23	7.28	900.00	4.05%	3.02	4.97	12.25	1000.00	15.56	12.25
E8	0.49	21.6	15.0	100.00	6.00%	0.27	6.10	600.00	6.00%	3.67	2.72				
			20.0						1300.00	1.80%	2.68	8.07	16.89	2000.00	21.11
OS-E9	0.26	46.9	15.0	100.00	3.00%	0.16	10.55	200.00	3.00%	2.60	1.28				
			20.0						1160.00	1.70%	2.61	7.41	19.25	1460.00	18.11
E10	0.49	20.0	15.0	100.00	2.00%	0.19	8.76	1411.00	2.83%	2.52	9.32	18.08	1511.00	18.39	18.08
E11	0.49	14.5	15.0	100.00	2.82%	0.21	7.82	965.00	2.82%	2.52	6.38	14.21	1065.00	15.92	14.21
E9-E11	0.36	81.4	15.0	100.00	3.00%	0.18	9.30	200.00	3.00%	2.60	1.28				
			20.0						2000.00	2.80%	3.35	9.96	20.54	2300.00	22.78
F1	0.49	5.1	15.0	100.00	4.00%	0.24	6.97	654.00	5.05%	3.37	3.23				
			20.0						175.00	0.60%	1.55	1.88	12.09	929.00	15.16
F2	0.49	28.0	15.0	100.00	5.70%	0.27	6.20	1704.00	1.84%	2.03	13.96	20.16	1804.00	20.02	20.02
G	0.49	20.1	15.0	100.00	2.70%	0.21	7.94	862.00	2.82%	2.52	5.70	13.64	962.00	15.34	13.64
H1	0.49	4.3	15.0	100.00	1.00%	0.15	11.01	46.00	1.00%	1.50	0.51				
			20.0						863.00	4.90%	4.43	3.25	14.77	1009.00	15.61
H2	0.49	18.0	15.0	100.00	4.00%	0.24	6.97	1132.00	4.42%	3.15	5.98	12.95	1232.00	16.84	12.95

Standard Form SF-1. Time of Concentration-Proposed

Calculated By: Leonard Beasley

Job No: 100.013

Date: September, 2016

Project: Lorson Ranch East MDDP

Checked By: Leonard Beasley

Sub-Basin Data				Initial Overland Time (t _i)				Travel Time (t _t)					t _c Check (urbanized Basins)		Final t _c
BASIN or DESIGN	C _s	AREA (A) acres	NRCS Convey.	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _i minutes	LENGTH (L) feet	SLOPE (S) %	VELOCITY (V) ft/sec	t _t minutes	Computed t _c Minutes	TOTAL LENGTH (L) feet	Regional t _c =(L/180)+10 minutes	USDCM Recommended t _c =t _i +t _t (min)
OS-I1	0.26	16.0	15.0	100.00	2.00%	0.14	12.07	200.00	2.00%	2.12	1.57				
			20.0					845.00	3.20%	3.58	3.94	17.57	1145.00	16.36	16.36
I2	0.49	13.0	15.0	100.00	3.50%	0.23	7.28	762.00	4.53%	3.19	3.98	11.26	862.00	14.79	11.26
I	0.38	29.0	15.0	100.00	2.00%	0.16	10.34	200.00	3.00%	2.60	1.28				
			20.0					1470.00	1.70%	2.61	9.40	21.02	1770.00	19.83	19.83
OS-J1	0.26	12.4	15.0	100.00	3.00%	0.16	10.55	200.00	3.00%	2.60	1.28				
			20.0					965.00	2.70%	3.29	4.89	16.73	1265.00	17.03	16.73
J2	0.49	12.0	15.0	100.00	2.00%	0.19	8.76	737.00	3.93%	2.97	4.13	12.89	837.00	14.65	12.89
J	0.38	24.4	15.0	100.00	3.00%	0.18	9.05	200.00	3.00%	2.60	1.28				
			20.0					1802.00	3.17%	3.56	8.43	18.76	2102.00	21.68	18.76
OS-K1	0.26	2.0	15.0	100.00	4.00%	0.17	9.60	200.00	6.97%	3.96	0.84				
			20.0					216.00	6.97%	5.28	0.68	11.12	516.00	12.87	11.12
K2	0.49	3.7	15.0	100.00	3.64%	0.23	7.19	586.00	3.64%	2.86	3.41	10.60	686.00	13.81	10.60
K	0.43	5.7	15.0	100.00	8.00%	0.27	6.09	750.00	2.27%	2.26	5.53	11.62	850.00	14.72	11.62



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: September, 2016
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP
 Design Storm: **5 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t _c	CA	i	Q	t _c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t	
A			2.59	0.16	15.7	0.41	3.45	1.4													
OS-B1			5.64	0.15	10.8	0.85	4.02	3.4													
B2			3.90	0.49	16.8	1.91	3.35	6.4													
Basin B	DP-1	9.54							20.1	2.76	3.08	8.5									
C1			23.20	0.49	20.3	11.37	3.07	34.9													
C2			34.50	0.49	11.3	16.91	3.94	66.6													
	DP-2	57.70							22.1			80.1									
C3			8.30	0.49	16.0	4.07	3.42	13.9													
C4			57.50	0.49	23.8	28.18	2.83	79.7													
C5			25.00	0.49	15.6	12.25	3.46	42.4													
C6			18.70	0.49	15.7	9.16	3.46	31.7													
C7			14.50	0.49	13.1	7.11	3.72	26.4													
C8a			11.70	0.49	12.2	5.73	3.83	22.0													
C8			74.50	0.49	17.8	36.51	3.27	119.3													
OS-C9			5.20	0.49	11.3	2.55	3.95	10.1													
C10			13.00	0.49	14.5	6.37	3.57	22.8													
OS-C11			5.60	0.49	13.3	2.74	3.71	10.2													
C12			20.50	0.49	17.6	10.05	3.28	33.0													
C13			19.20	0.16	30.4	3.07	2.46	7.6													
	DP-6c	93.22							34.2	39.34	2.29	90.0									
C14			11.10	0.49	20.5	5.44	3.05	16.6													
C15			40.20	0.49	22.3	19.70	2.93	57.6													
C16a			21.29	0.49	16.6	10.43	3.37	35.1													
C16b			32.23	0.49	15.0	15.79	3.52	55.6													
Overall C16			53.52	0.49	16.6	26.22	3.37	88.3													
C17			18.80	0.49	15.8	9.21	3.44	31.7													
C17a			7.50	0.16	8.0	1.20	4.46	5.4													
D1			17.00	0.49	12.2	8.33	3.83	31.9													
D2			8.00	0.49	10.4	3.92	4.07	16.0													



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: September, 2016
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP
 Design Storm: **5 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time		Remarks	
		Area Design	Area (A)	Runoff Coeff. (C)	t _c	CA	i	Q	t _c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity		t _t
D3			23.00	0.49	16.6	11.27	3.37	38.0													
D4			36.40	0.49	15.6	17.84	3.46	61.7													
D5			4.60	0.40	10.2	1.84	4.10	7.5													
Basin D		89.00							20.9	43.20	3.02	130.5									
E1			10.20	0.49	13.4	5.00	3.69	18.5													
E2			10.30	0.49	11.3	5.05	3.94	19.9													
OS-E3			9.90	0.26	14.4	2.57	3.58	9.2													
E4			12.80	0.49	12.8	6.27	3.76	23.6													
E5			13.30	0.49	13.0	6.52	3.74	24.4													
	DP-12	56.50							15.3	25.41	3.49	88.7									
OS-E6			21.10	0.22	16.8	4.54	3.35	15.2													
E7			6.70	0.49	12.3	3.28	3.82	12.5													
	DP-11	27.80							16.8	7.82	3.35	26.2									
E8			21.60	0.49	16.9	10.58	3.34	35.4													
OS-E9			46.90	0.26	18.1	12.19	3.24	39.5													
E10			20.00	0.49	18.1	9.80	3.24	31.8													
E11			14.50	0.49	14.2	7.11	3.60	25.6													
	E9-E11	81.40							20.5	29.10	3.05	88.8									
Basin E		187.30																			
F1			5.06	0.49	12.1	2.48	3.84	9.5													
F2			27.97	0.49	20.0	13.71	3.09	42.3													
Basin F		33.03							20.0	16.18	3.09	50.0									
G			20.05	0.49	13.6	9.82	3.66	36.0													
H1			4.27	0.49	14.8	2.09	3.54	7.4													
H2			18.04	0.49	13.0	8.84	3.74	33.1													
Basin H		22.31							14.8	10.93	3.54	38.7									
OS-I1			15.96	0.26	16.4	4.15	3.39	14.1													
I2			13.00	0.49	11.3	6.37	3.95	25.2													



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley
 Date: September, 2016
 Checked By: Leonard Beasley

Job No: 100.013
 Project: Lorson Ranch East MDDP
 Design Storm: **5 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff			Street		Pipe			Travel Time			Remarks	
		Area Design	Area (A)	Runoff Coeff. (C)	t _c	CA	i	Q	t _c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity		t _t
OS-J1			12.36	0.26	16.7	3.21	3.36	10.8													
J2			12.00	0.49	12.9	5.88	3.75	22.0													
OS-K1			1.98	0.26	11.1	0.51	3.97	2.0													
K2			3.70	0.49	10.6	1.81	4.04	7.3													

Calculated By: Leonard Beasley

Job No: 100.013

Date: September, 2016

Project: Lorson Ranch East MDDP

Checked By: Leonard Beasley

Design Storm: **100 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t _c	CA	i	Q	t _c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t _t	
			ac.			min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	
A			2.59	0.51	15.7	1.32	5.79	7.7													
OS-B1			5.64	0.50	10.8	2.82	6.74	19.0													
B2			3.90	0.65	16.8	2.54	5.63	14.3													
Basin B	DP-1	9.54							20.1	5.36	5.18	27.7									
C1			23.20	0.65	20.3	15.08	5.15	77.7													
C2			34.50	0.65	11.3	22.43	6.62	148.4													
	DP-2	57.70							22.1			171.0									
C3			8.30	0.65	16.0	5.40	5.75	31.0													
C4			57.50	0.65	23.8	37.38	4.75	177.4													
C5			25.00	0.65	15.6	16.25	5.81	94.4													
C6			18.70	0.65	15.7	12.16	5.80	70.5													
C7			14.50	0.65	13.1	9.43	6.25	58.9													
C8a			11.70	0.65	12.2	7.61	6.44	49.0													
C8			74.50	0.65	17.8	48.43	5.48	265.5													
OS-C9			5.20	0.65	11.3	3.38	6.63	22.4													
C10			13.00	0.65	14.5	8.45	6.00	50.7													
OS-C11			5.60	0.65	13.3	3.64	6.22	22.7													
C12			20.50	0.65	17.6	13.33	5.51	73.5													
C13			19.20	0.51	30.4	9.79	4.13	40.5													
	DP-6c	93.22							34.2	57.91	3.84	222.2									
C14			11.10	0.65	20.5	7.22	5.13	37.0													
C15			40.20	0.65	22.3	26.13	4.91	128.3													
C16a			21.29	0.65	16.6	13.84	5.66	78.3													
C16b			32.23	0.65	15.0	20.95	5.91	123.8													
Overall C16			53.52	0.65	16.6	34.79	5.66	196.7													
C17			18.80	0.65	15.8	12.22	5.77	70.6													
C17a			7.50	0.51	8.0	3.83	7.49	28.7													

Calculated By: Leonard Beasley

Job No: 100.013

Date: September, 2016

Project: Lorson Ranch East MDDP

Checked By: Leonard Beasley

Design Storm: **100 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe		Travel Time			Remarks	
		Area Design	Area (A)	Runoff Coeff. (C)	t_c	CA	i	Q	t_c	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity		tt
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec		min
D1			17.00	0.65	12.2	11.05	6.43	71.1													
D2			8.00	0.65	10.4	5.20	6.83	35.5													
D3			23.00	0.65	16.6	14.95	5.66	84.5													
D4			36.40	0.65	15.6	23.66	5.81	137.5													
D5			4.60	0.65	10.2	2.99	6.88	20.6													
E1			10.20	0.65	13.4	6.63	6.20	41.1													
E2			10.30	0.65	11.3	6.70	6.62	44.3													
OS-E3			9.90	0.55	14.4	5.45	6.01	32.7													
E4			12.80	0.65	12.8	8.32	6.31	52.5													
E5			13.30	0.65	13.0	8.65	6.28	54.3													
	DP-12	56.50							15.3	35.74	5.86	209.5									
OS-E6			21.10	0.55	16.8	11.61	5.63	65.3													
E7			6.70	0.65	12.3	4.36	6.41	27.9													
	DP-11	27.80							16.8	15.96	5.63	89.8									
E8			21.60	0.65	16.9	14.04	5.61	78.8													
	E6-E8	49.40							21.6	30.00	5.61	168.3									
OS-E9			46.90	0.40	18.1	18.76	5.44	102.0													
E10			20.00	0.65	18.1	13.00	5.44	70.7													
E11			14.50	0.65	14.2	9.43	6.05	57.0													
	E9-E11	81.40							22.0	41.19	4.95	203.9									
Basin E		187.30																			
F1			5.06	0.65	12.1	3.29	6.45	21.2													
F2			27.97	0.65	20.0	18.18	5.18	94.2													



Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)

Calculated By: Leonard Beasley

Job No: 100.013

Date: September, 2016

Project: Lorson Ranch East MDDP

Checked By: Leonard Beasley

Design Storm: **100 - Year Event, Proposed Conditions**

Street or Basin	Design Point	Direct Runoff						Total Runoff				Street		Pipe		Travel Time			Remarks		
		Area Design	Area (A)	Runoff Coeff. (C)	tc	CA	i	Q	tc	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length		Velocity	tt
Basin F		33.03						20.0	21.47	5.18	111.3										
G			20.05	0.65	13.6	13.03	6.15	80.2													
H1			4.27	0.65	14.8	2.78	5.95	16.5													
H2			18.04	0.65	13.0	11.73	6.28	73.7													
Basin H		22.31						14.8	14.50	5.95	86.3										
OS-I1			15.96	0.55	16.4	8.78	5.69	50.0													
I2			13.00	0.65	11.3	8.45	6.63	56.1													
OS-J1			12.36	0.55	16.7	6.80	5.64	38.3													
J2			12.00	0.65	12.9	7.80	6.29	49.1													
OS-K1			1.98	0.55	11.1	1.09	6.66	7.3													
K2			3.70	0.65	10.6	2.41	6.79	16.3													

Channel Report

Hydraflow Express by Intelisolve

Sunday, Aug 7 2016, 10:17 AM

36-inch from Basin C1 under Lorson Blvd.

Circular

Diameter (ft) = 3.00

Invert Elev (ft) = 100.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 2.70

Q (cfs) = 71.10

Area (sqft) = 6.70

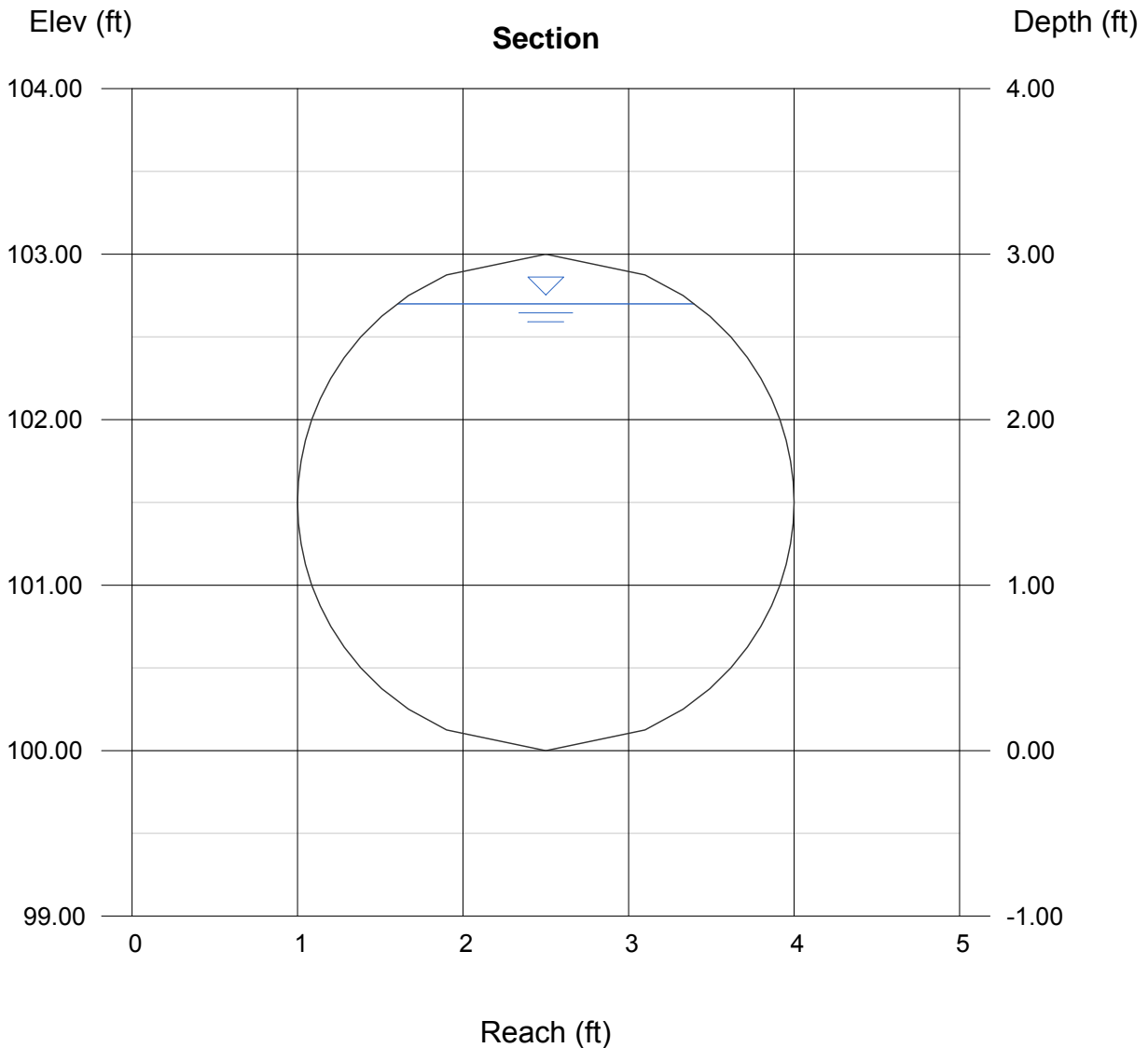
Velocity (ft/s) = 10.61

Wetted Perim (ft) = 7.50

Crit Depth, Y_c (ft) = 2.59

Top Width (ft) = 1.80

EGL (ft) = 4.45



Channel Report

48-inch at Des. Pt. 2 into Pond C1

Circular

Diameter (ft) = 4.00

Invert Elev (ft) = 100.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 3.60

Q (cfs) = 153.14

Area (sqft) = 11.92

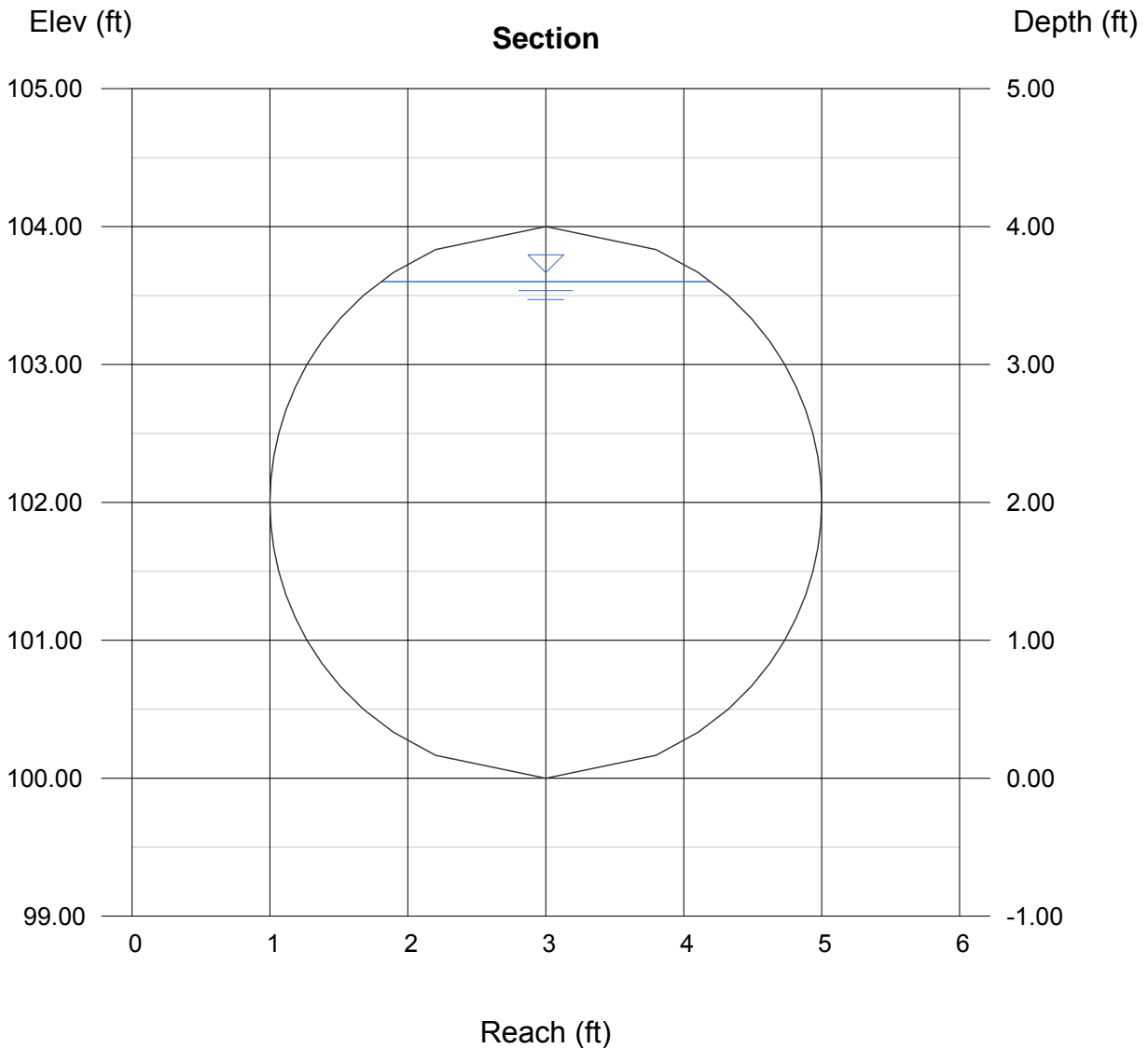
Velocity (ft/s) = 12.85

Wetted Perim (ft) = 10.00

Crit Depth, Y_c (ft) = 3.52

Top Width (ft) = 2.39

EGL (ft) = 6.17



Channel Report

Hydraflow Express by Intelisolve

Sunday, Aug 7 2016, 2:34 PM

42-inch from Design Pt. 3e to Design Pt. 7

Circular

Diameter (ft) = 3.50

Invert Elev (ft) = 100.00

Slope (%) = 1.30

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 3.15

Q (cfs) = 122.29

Area (sqft) = 9.12

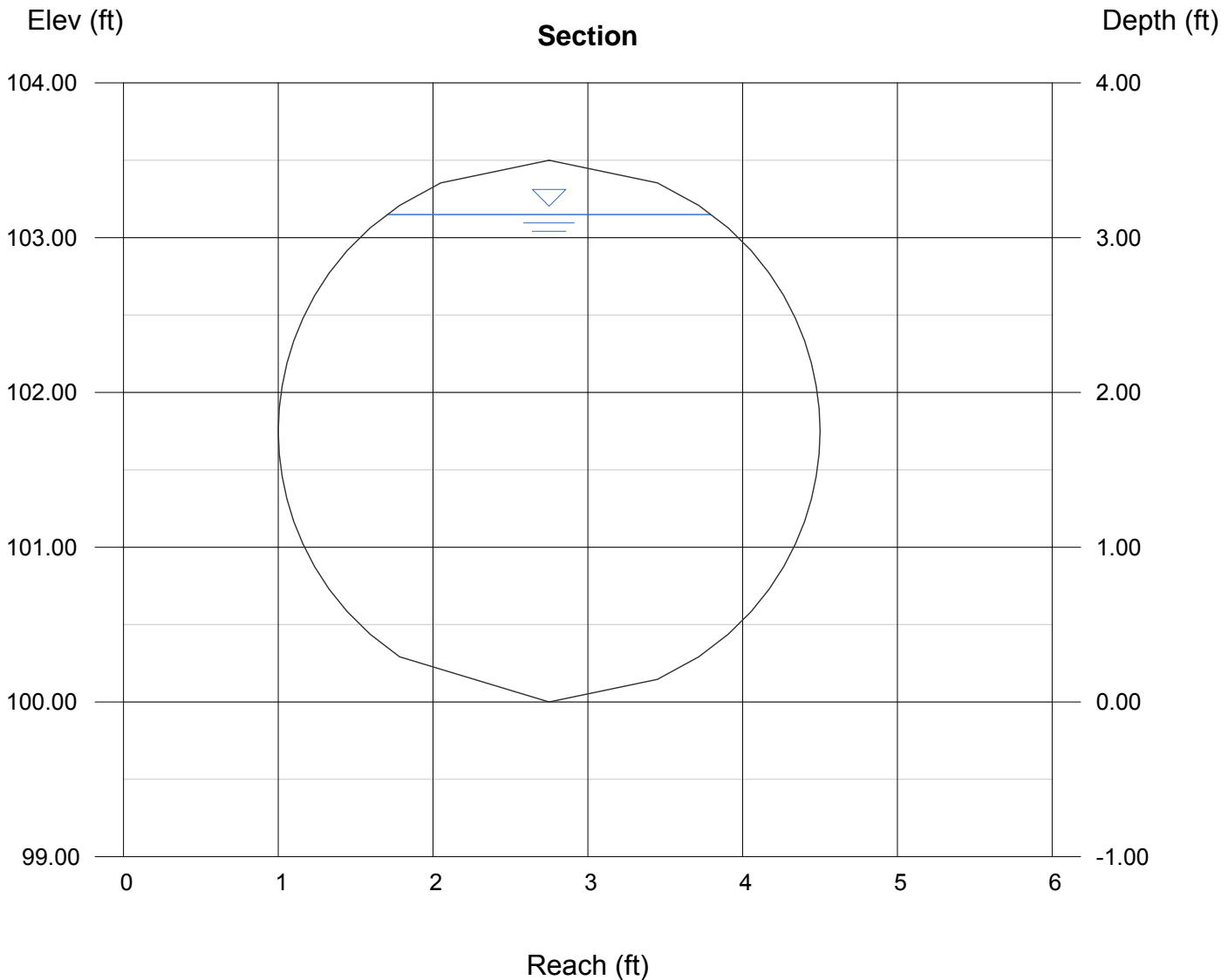
Velocity (ft/s) = 13.40

Wetted Perim (ft) = 8.75

Crit Depth, Y_c (ft) = 3.19

Top Width (ft) = 2.09

EGL (ft) = 5.94



Channel Report

Hydraflow Express by Intelisolve

Friday, Sep 2 2016, 10:37 PM

Design Pt. 6a to 6c

42"
RCP

Circular

Diameter (ft) = 3.50

Invert Elev (ft) = 100.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 3.15

Q (cfs) = 107.26

Area (sqft) = 9.12

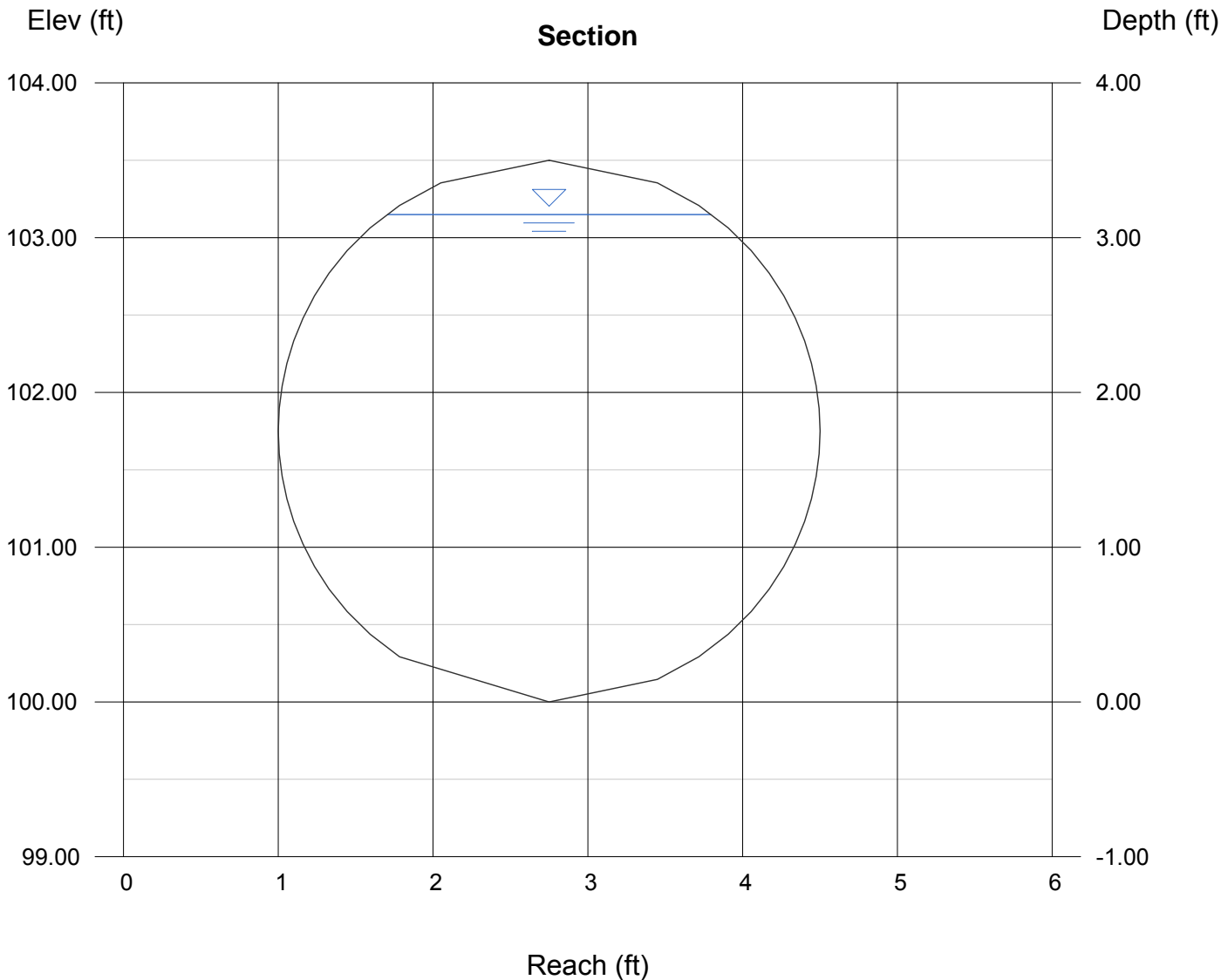
Velocity (ft/s) = 11.75

Wetted Perim (ft) = 8.75

Crit Depth, Yc (ft) = 3.05

Top Width (ft) = 2.09

EGL (ft) = 5.30



Channel Report

48-inch from Design Pt.6c to Design Point 6

Circular

Diameter (ft) = 4.00

Invert Elev (ft) = 100.00

Slope (%) = 0.70

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 3.60

Q (cfs) = 128.13

Area (sqft) = 11.92

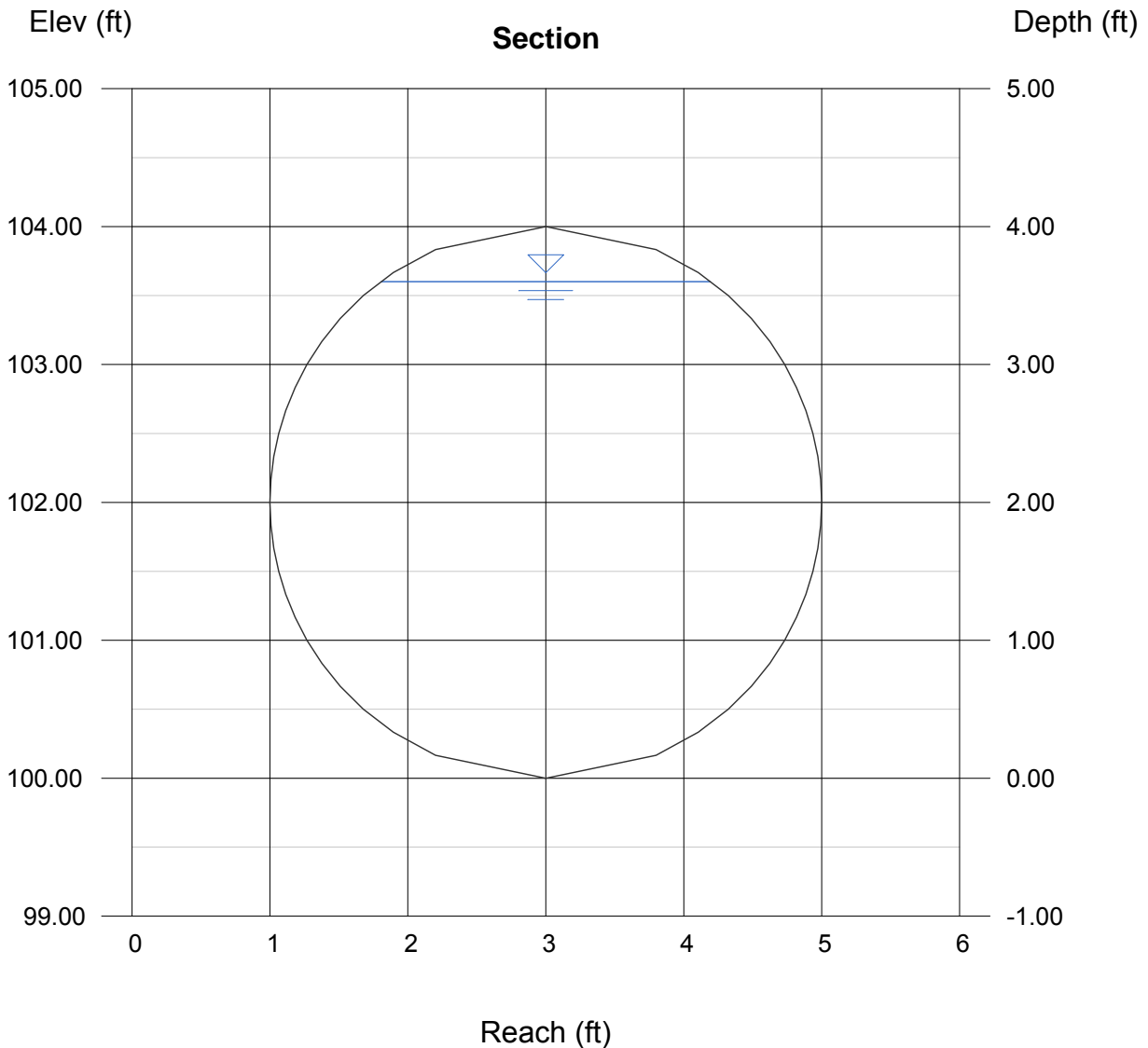
Velocity (ft/s) = 10.75

Wetted Perim (ft) = 10.00

Crit Depth, Y_c (ft) = 3.27

Top Width (ft) = 2.39

EGL (ft) = 5.40



Channel Report

66-inch cmp from Design Pt. 6 to Pond C5

Circular

Diameter (ft) = 5.50

Invert Elev (ft) = 100.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 4.95

Q (cfs) = 358.06

Area (sqft) = 22.53

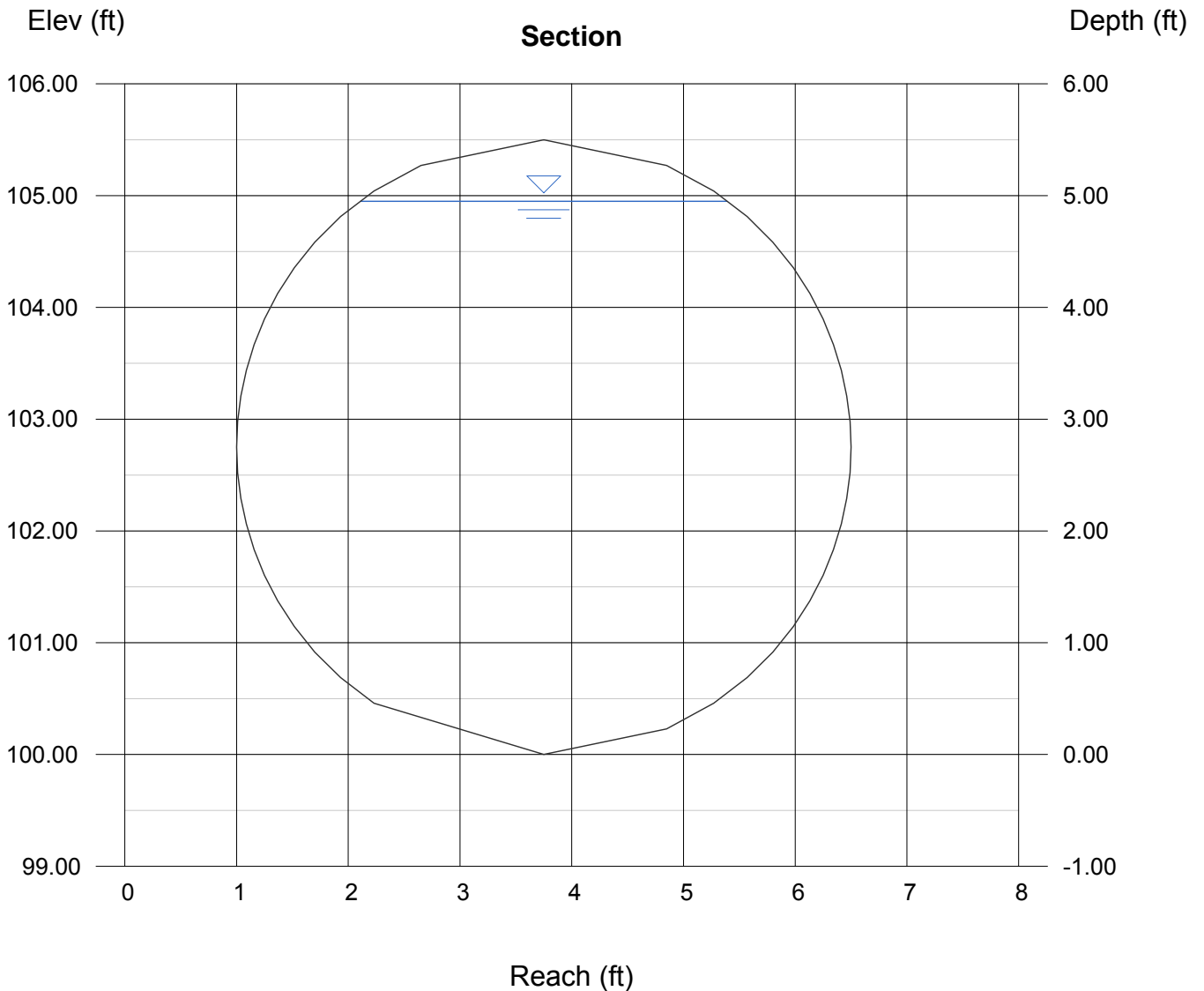
Velocity (ft/s) = 15.89

Wetted Perim (ft) = 13.75

Crit Depth, Y_c (ft) = 4.92

Top Width (ft) = 3.29

EGL (ft) = 8.88



APPENDIX C – HYDRAFLOW CALCULATIONS

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	140.99	6	384	905,484	---	-----	-----	EX-C
2	SCS Runoff	104.56	6	378	530,876	---	-----	-----	EX-E

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	458.13	6	384	2,456,980	---	-----	-----	EX-C
2	SCS Runoff	286.52	6	378	1,291,638	---	-----	-----	EX-E

Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, May 23 2017, 7:39 AM

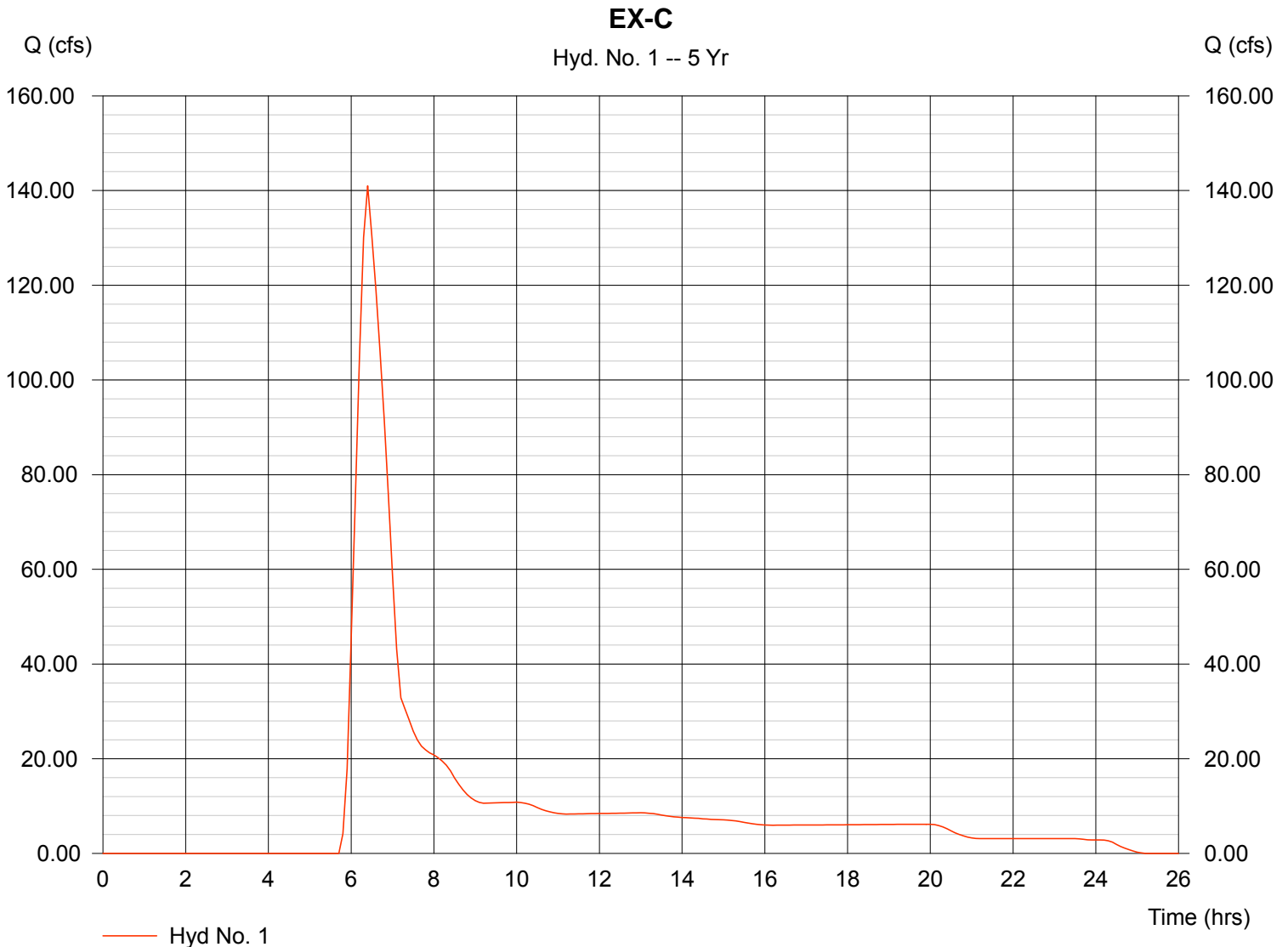
Hyd. No. 1

EX-C

Hydrograph type = SCS Runoff
Storm frequency = 5 yrs
Drainage area = 452.970 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 2.80 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 140.99 cfs
Time interval = 6 min
Curve number = 69
Hydraulic length = 7400 ft
Time of conc. (Tc) = 49.50 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 905,484 cuft



Hydrograph Plot

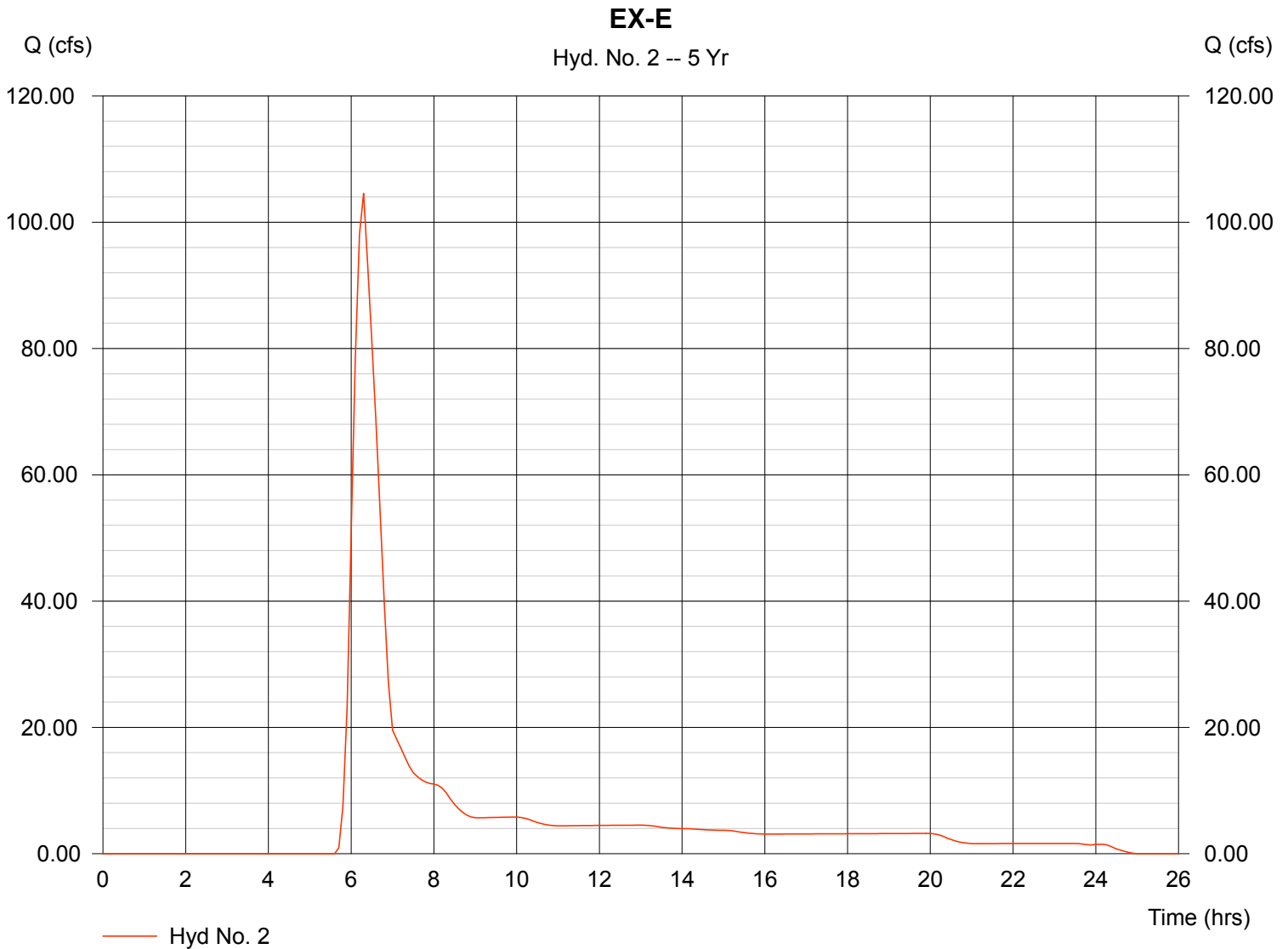
Hyd. No. 2

EX-E

Hydrograph type = SCS Runoff
Storm frequency = 5 yrs
Drainage area = 187.300 ac
Basin Slope = 3.0 %
Tc method = USER
Total precip. = 2.80 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 104.56 cfs
Time interval = 6 min
Curve number = 73.5
Hydraulic length = 4150 ft
Time of conc. (Tc) = 33.00 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 530,876 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, May 23 2017, 7:39 AM

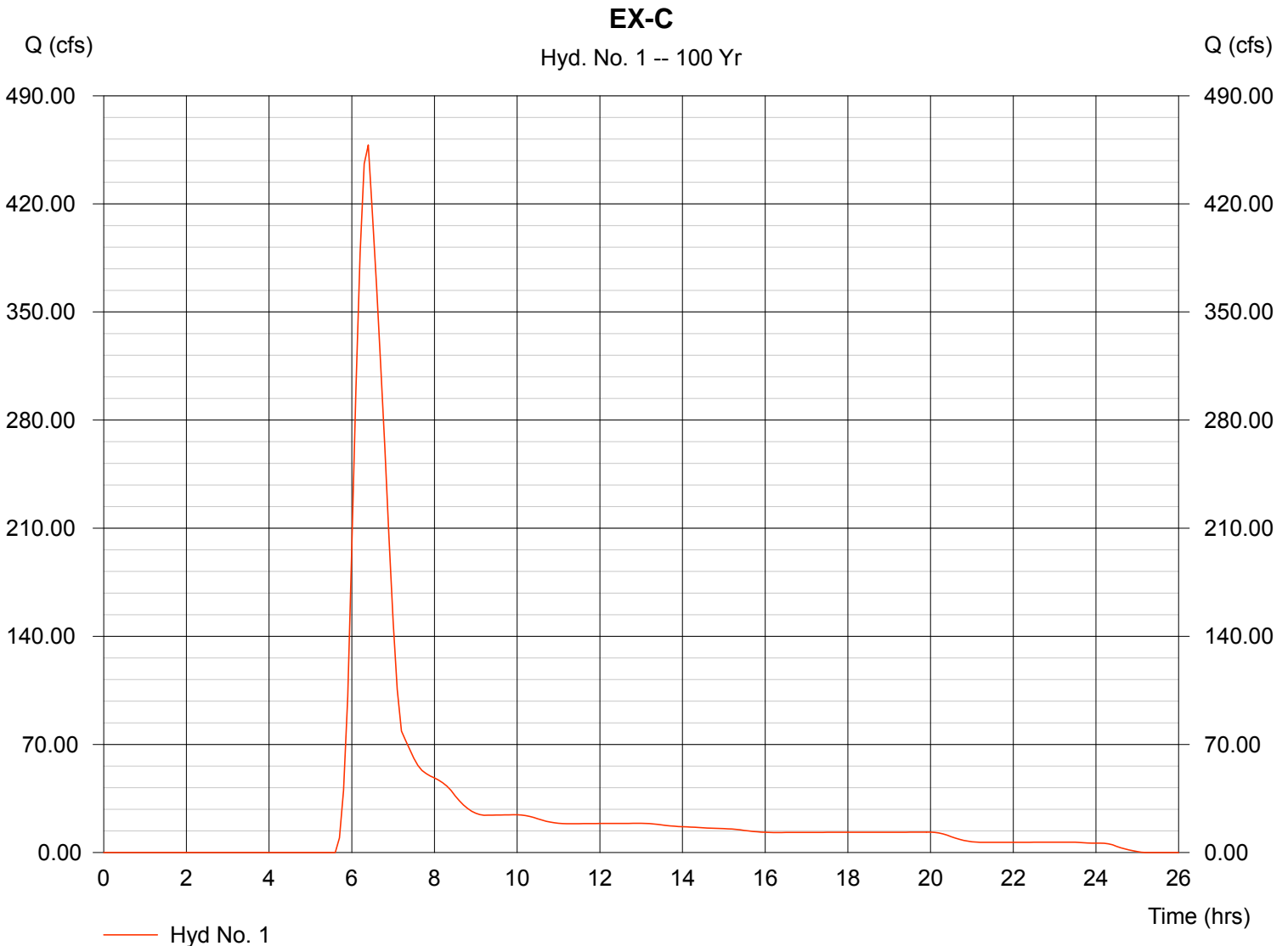
Hyd. No. 1

EX-C

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 452.970 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 4.40 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 458.13 cfs
Time interval = 6 min
Curve number = 69
Hydraulic length = 7400 ft
Time of conc. (Tc) = 49.50 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 2,456,980 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, May 23 2017, 7:13 AM

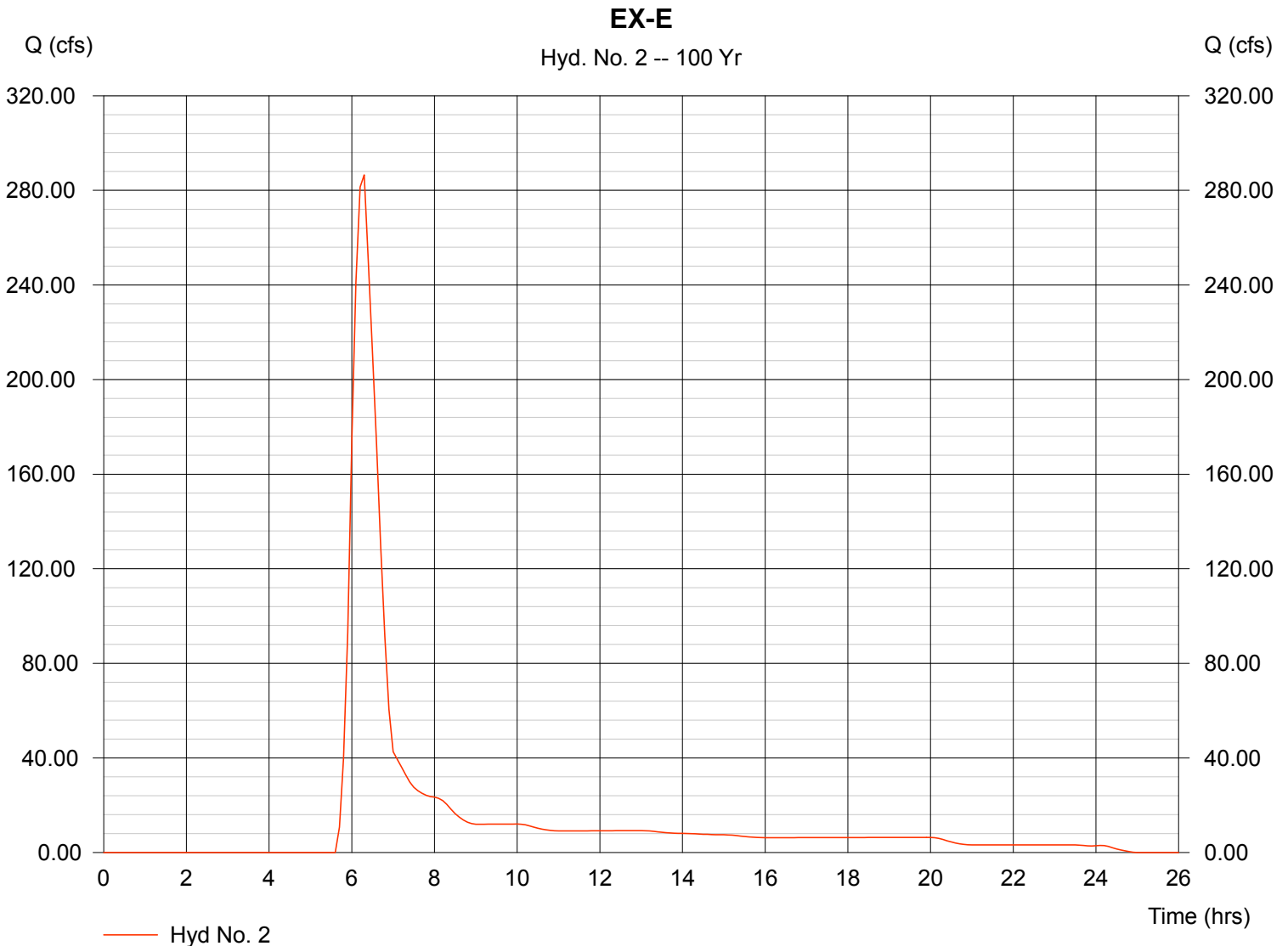
Hyd. No. 2

EX-E

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 187.300 ac
Basin Slope = 3.0 %
Tc method = USER
Total precip. = 4.40 in
Storm duration = CSpring_IIA-6min.cds

Peak discharge = 286.52 cfs
Time interval = 6 min
Curve number = 73.5
Hydraulic length = 4150 ft
Time of conc. (Tc) = 33.00 min
Distribution = Custom
Shape factor = 484

Hydrograph Volume = 1,291,638 cuft



APPENDIX D – POND CALCULATIONS

Detention Basin Outlet Structure Design

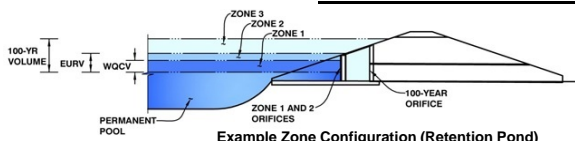
UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Basin C1, C2 & C3, Pond "C1"

Project:

Basin ID:



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.02	1.222	Orifice Plate
Zone 2 (EURV)	3.83	2.401	Rectangular Orifice
Zone 3 (100-year)	5.46	2.423	Weir&Pipe (Restrict)
		6.046	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.77	1.55					
Orifice Area (sq. inches)	7.20	7.20	7.20					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="2.02"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="3.83"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="5.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="10.49"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.36"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.21"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="5.47"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="25%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="5.47"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="11.39"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="16.80"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="12.60"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="18.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="14.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="1.47"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="0.64"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="2.16"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	1.222	3.623	3.370	4.678	5.763	7.356	8.625	10.193	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.223	3.625	3.372	4.680	5.765	7.355	8.621	10.194	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.13	0.35	0.81	1.07	1.39	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.9	7.4	20.2	46.7	61.6	80.2	0.0
Peak Inflow Q (cfs) =	21.3	62.4	58.1	80.1	98.2	124.6	145.4	171.0	#N/A
Peak Outflow Q (cfs) =	0.7	3.2	3.1	3.8	4.4	12.6	16.8	17.9	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.2	0.3	0.3	0.2	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.5	0.7	0.7	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	37	46	46	47	48	48	47	46	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	54	56	58	57	57	#N/A
Maximum Ponding Depth (ft) =	1.93	3.56	3.40	4.25	4.93	5.71	6.23	6.98	#N/A
Area at Maximum Ponding Depth (acres) =	1.19	1.38	1.37	1.45	1.51	1.59	1.64	1.72	#N/A
Maximum Volume Stored (acre-ft) =	1.122	3.250	3.017	4.212	5.218	6.443	7.267	8.526	#N/A

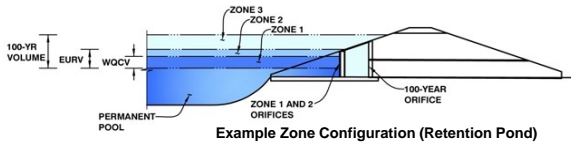
Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: _____

Basin C3 & C4, Pond C2.1



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.18	1.440	Orifice Plate
Zone 2 (EURV)	5.78	2.830	Rectangular Orifice
Zone 3 (100-year)	8.04	2.855	Weir&Pipe (Restrict)
		7.126	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.00	3.00				
Orifice Area (sq. inches)	4.66	4.66	4.66	4.66				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	3.18	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.78	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	4.00	N/A	inches
Vertical Orifice Width =	13.86		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.39	N/A	ft ²
Vertical Orifice Centroid =	0.17	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	12.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	% grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	6.00	N/A	feet
Over Flow Weir Slope Length =	12.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	6.84	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	33.60	N/A	ft ²
Overflow Grate Open Area w/ Debris =	16.80	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	48.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	4.91	N/A	ft ²
Outlet Orifice Centroid =	1.25	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

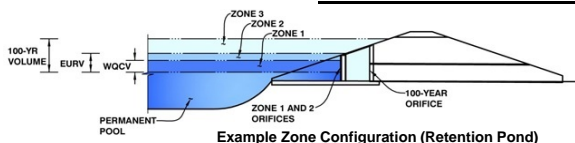
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	1.440	4.270	3.972	5.513	6.792	8.669	10.164	12.013	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.440	4.271	3.972	5.513	6.784	8.669	10.161	12.008	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.13	0.36	0.83	1.09	1.42	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	1.1	8.9	24.4	56.2	74.2	96.5	0.0
Peak Inflow Q (cfs) =	25.6	74.7	69.6	95.9	117.4	149.0	173.8	204.2	#N/A
Peak Outflow Q (cfs) =	0.7	3.9	3.7	10.8	33.5	56.6	59.4	63.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.2	1.4	1.0	0.8	0.7	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.9	1.5	1.6	1.7	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	48	47	49	47	45	44	42	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	54	53	52	52	51	#N/A
Maximum Ponding Depth (ft) =	3.08	5.40	5.16	6.20	6.56	6.99	7.58	8.42	#N/A
Area at Maximum Ponding Depth (acres) =	1.00	1.15	1.14	1.21	1.23	1.27	1.31	1.37	#N/A
Maximum Volume Stored (acre-ft) =	1.341	3.834	3.559	4.779	5.207	5.745	6.504	7.641	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Basin ID: Basin C5 & C7, Pond C2.2



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.93	0.847	Orifice Plate
Zone 2 (EURV)	5.49	1.665	Rectangular Orifice
Zone 3 (100-year)	7.67	1.680	Weir&Pipe (Restrict)
		4.191	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-15/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.00	3.00				
Orifice Area (sq. inches)	2.90	2.90	2.90	2.90				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="3.10"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="5.50"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.11"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.17"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="5.80"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="10.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="5.80"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="10.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="8.91"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="28.00"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="14.00"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="24.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="48.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="3.14"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="1.00"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="3.14"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.847	2.512	2.336	3.243	3.995	5.100	5.979	7.066	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.846	2.509	2.334	3.240	3.991	5.087	5.967	7.056	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.11	0.29	0.69	0.91	1.19	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.5	4.2	11.7	27.5	36.3	47.6	0.0
Peak Inflow Q (cfs) =	13.1	38.3	35.7	49.3	60.5	76.7	89.6	105.5	#N/A
Peak Outflow Q (cfs) =	0.4	1.5	1.4	5.4	19.1	35.5	36.8	39.1	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.3	1.6	1.3	1.0	0.8	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.6	1.2	1.2	1.3	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	56	55	58	57	55	53	52	#N/A
Time to Drain 99% of Inflow Volume (hours) =	41	60	59	63	63	62	61	60	#N/A
Maximum Ponding Depth (ft) =	2.82	5.20	4.96	5.96	6.24	6.51	6.93	7.67	#N/A
Area at Maximum Ponding Depth (acres) =	0.58	0.70	0.69	0.74	0.75	0.77	0.79	0.83	#N/A
Maximum Volume Stored (acre-ft) =	0.784	2.301	2.135	2.847	3.055	3.261	3.597	4.198	#N/A

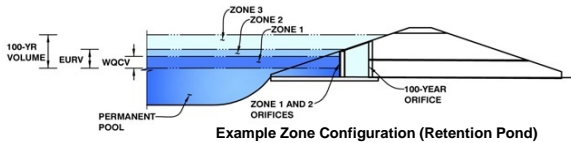
Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: _____

Basin C6, Pond C2.3



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.43	0.396	Orifice Plate
Zone 2 (EURV)	2.81	0.778	Rectangular Orifice
Zone 3 (100-year)	4.05	0.785	Weir&Pipe (Restrict)
		1.960	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-13/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.70	1.40					
Orifice Area (sq. inches)	2.61	2.61	2.61					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="1.50"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="2.81"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="7.39"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.21"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.17"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="4.23"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="16.80"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="8.40"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="27.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="27.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="3.98"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="1.13"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="3.14"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

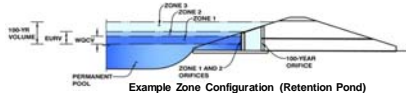
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.396	1.174	1.092	1.516	1.868	2.384	2.795	3.304	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.396	1.174	1.092	1.516	1.867	2.383	2.794	3.302	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.4	3.4	9.2	20.5	27.0	34.7	0.0
Peak Inflow Q (cfs) =	9.4	27.4	25.5	35.3	43.4	55.2	64.5	76.1	#N/A
Peak Outflow Q (cfs) =	0.2	1.3	1.2	2.7	9.8	20.6	29.0	32.5	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.8	1.1	1.0	1.1	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.5	1.1	1.6	1.8	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	49	49	50	48	46	44	43	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	54	53	55	55	54	53	52	#N/A
Maximum Ponding Depth (ft) =	1.39	2.62	2.49	3.09	3.33	3.58	3.73	4.00	#N/A
Area at Maximum Ponding Depth (acres) =	0.53	0.59	0.58	0.62	0.63	0.64	0.65	0.67	#N/A
Maximum Volume Stored (acre-ft) =	0.373	1.060	0.989	1.343	1.492	1.651	1.754	1.932	#N/A

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: _____ Basin C8a & C10, Pond "C3"



Required Volume Calculation

Selected BMP Type =	EDB	
Watershed Area =	24.70	acres
Watershed Length =	1,250	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	65.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	30.0%	percent
Percentage Hydrologic Soil Groups C/D =	70.0%	percent
Desired WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	
Water Quality Capture Volume (WQCV) =	0.523	acre-feet
Excess Urban Runoff Volume (EURV) =	1.612	acre-feet
2-yr Runoff Volume (P1 = 1.16 in.) =	1.434	acre-feet
5-yr Runoff Volume (P1 = 1.44 in.) =	1.960	acre-feet
10-yr Runoff Volume (P1 = 1.68 in.) =	2.445	acre-feet
25-yr Runoff Volume (P1 = 1.92 in.) =	3.128	acre-feet
50-yr Runoff Volume (P1 = 2.16 in.) =	3.658	acre-feet
100-yr Runoff Volume (P1 = 2.42 in.) =	4.326	acre-feet
500-yr Runoff Volume (P1 = 0 in.) =	0.000	acre-feet
Approximate 2-yr Detention Volume =	1.345	acre-feet
Approximate 5-yr Detention Volume =	1.845	acre-feet
Approximate 10-yr Detention Volume =	2.179	acre-feet
Approximate 25-yr Detention Volume =	2.331	acre-feet
Approximate 50-yr Detention Volume =	2.408	acre-feet
Approximate 100-yr Detention Volume =	2.623	acre-feet

Optional User Override 1-hr Precipitation	1.16	inches
	1.44	inches
	1.68	inches
	1.92	inches
	2.16	inches
	2.42	inches

Stage-Storage Calculation

Zone 1 Volume (WQCV) =	0.523	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.089	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.012	acre-feet
Total Detention Basin Volume =	2.623	acre-feet
Initial Surcharge Volume (SV) =	user	ft³
Initial Surcharge Depth (SD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{tc}) =	user	ft
Slope of Trickle Channel (S _{tc}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{l:w}) =	user	
Initial Surcharge Area (A _{sv}) =	user	ft²
Surcharge Volume Length (L _{sv}) =	user	ft
Surcharge Volume Width (W _{sv}) =	user	ft
Depth of Basin Floor (H _{bottom}) =	user	ft
Length of Basin Floor (L _{bottom}) =	user	ft
Width of Basin Floor (W _{bottom}) =	user	ft
Area of Basin Floor (A _{bottom}) =	user	ft²
Volume of Basin Floor (V _{bottom}) =	user	ft³
Depth of Main Basin (H _{main}) =	user	ft
Length of Main Basin (L _{main}) =	user	ft
Width of Main Basin (W _{main}) =	user	ft
Area of Main Basin (A _{main}) =	user	ft²
Volume of Main Basin (V _{main}) =	user	ft³
Calculated Total Basin Volume (V _{total}) =	user	acre-feet

Depth Increment = 0.2 ft

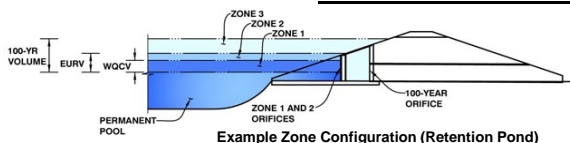
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft²)	Area (acre)	Volume (ft³)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	262	0.006		
5757.33	--	0.33	--	--	--	4,657	0.107	786	0.018
5758	--	1.00	--	--	--	13,580	0.312	6,786	0.156
5759	--	2.00	--	--	--	33,254	0.763	30,006	0.689
5760	--	3.00	--	--	--	46,803	1.074	70,366	1.615
5761	--	4.00	--	--	--	50,425	1.158	118,980	2.731
5762	--	5.00	--	--	--	54,123	1.242	171,254	3.931
5763	--	6.00	--	--	--	57,909	1.329	227,270	5.217
5764	--	7.00	--	--	--	61,796	1.419	287,123	6.591

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Basin ID: Basin C8a & C10, Pond "C3"



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.76	0.523	Orifice Plate
Zone 2 (EURV)	3.00	1.089	Rectangular Orifice
Zone 3 (100-year)	3.91	1.012	Weir&Pipe (Restrict)
		2.623	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-15/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.70	1.40					
Orifice Area (sq. inches)	3.00	3.00	3.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="1.80"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.06"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.13"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="3.10"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="8.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="3.10"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="8.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="12.68"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="22.40"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="11.20"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="18.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="18.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="1.77"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="0.75"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="3.14"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

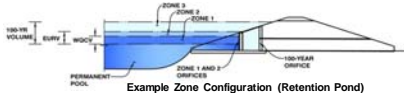
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.523	1.612	1.434	1.960	2.445	3.128	3.658	4.326	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.523	1.612	1.434	1.960	2.445	3.129	3.659	4.327	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.12	0.37	0.91	1.22	1.59	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.4	2.9	9.2	22.5	30.1	39.3	0.0
Peak Inflow Q (cfs) =	10.6	32.3	28.8	39.2	48.7	62.1	72.5	85.4	#N/A
Peak Outflow Q (cfs) =	0.3	0.7	0.7	2.1	8.8	14.5	15.3	16.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.7	1.0	0.6	0.5	0.4	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.6	0.6	0.7	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	39	58	56	60	58	56	54	53	#N/A
Time to Drain 99% of Inflow Volume (hours) =	42	64	61	67	66	65	64	64	#N/A
Maximum Ponding Depth (ft) =	1.70	2.91	2.75	3.19	3.39	3.67	3.98	4.40	#N/A
Area at Maximum Ponding Depth (acres) =	0.63	1.05	0.99	1.09	1.11	1.13	1.16	1.19	#N/A
Maximum Volume Stored (acre-ft) =	0.488	1.520	1.347	1.810	2.030	2.354	2.708	3.189	#N/A

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: Basin C8, Pond "C4"



Example Zone Configuration (Retention Pond)

Required Volume Calculation

Selected BMP Type =	EDB		
Watershed Area =	75.00	acres	
Watershed Length =	2,300	ft	
Watershed Slope =	0.055	ft/ft	
Watershed Imperviousness =	65.00%	percent	
Percentage Hydrologic Soil Group A =	0.0%	percent	
Percentage Hydrologic Soil Group B =	0.0%	percent	
Percentage Hydrologic Soil Groups C/D =	100.0%	percent	
Desired WCCV Drain Time =	40.0	hours	
Location for 1-hr Rainfall Depths =	User Input		
Water Quality Capture Volume (WQCV) =	1,588	acre-feet	Optional User Override 1-hr Precipitation
Excess Urban Runoff Volume (EURV) =	4,710	acre-feet	
2-yr Runoff Volume (P1 = 1.16 in.) =	4,381	acre-feet	1.16 inches
5-yr Runoff Volume (P1 = 1.44 in.) =	6,080	acre-feet	1.44 inches
10-yr Runoff Volume (P1 = 1.68 in.) =	7,491	acre-feet	1.68 inches
25-yr Runoff Volume (P1 = 1.92 in.) =	9,562	acre-feet	1.92 inches
50-yr Runoff Volume (P1 = 2.16 in.) =	11,210	acre-feet	2.16 inches
100-yr Runoff Volume (P1 = 2.42 in.) =	13,290	acre-feet	2.42 inches
500-yr Runoff Volume (P1 = 0 in.) =	0,000	acre-feet	
Approximate 2-yr Detention Volume =	4,110	acre-feet	
Approximate 5-yr Detention Volume =	5,727	acre-feet	
Approximate 10-yr Detention Volume =	6,549	acre-feet	
Approximate 25-yr Detention Volume =	6,987	acre-feet	
Approximate 50-yr Detention Volume =	7,191	acre-feet	
Approximate 100-yr Detention Volume =	7,859	acre-feet	

Stage-Storage Calculation

Zone 1 Volume (WQCV) =	1,588	acre-feet	
Zone 2 Volume (EURV - Zone 1) =	3,122	acre-feet	
Zone 3 Volume (100-year - Zones 1 & 2) =	3,149	acre-feet	
Total Detention Basin Volume =	7,859	acre-feet	
Initial Surcharge Volume (SV) =	user	ft ³	
Initial Surcharge Depth (SD) =	user	ft	
Total Available Detention Depth (H _{total}) =	user	ft	
Depth of Trickle Channel (H _{TC}) =	user	ft	
Slope of Trickle Channel (S _{TC}) =	user	ft/ft	
Slopes of Main Basin Sides (S _{main}) =	user	F:V	
Basin Length-to-Width Ratio (R _{LW}) =	user		
Initial Surcharge Area (A _{sv}) =	user	ft ²	
Surcharge Volume Length (L _{sv}) =	user	ft	
Surcharge Volume Width (W _{sv}) =	user	ft	
Depth of Basin Floor (H _{floor}) =	user	ft	
Length of Basin Floor (L _{floor}) =	user	ft	
Width of Basin Floor (W _{floor}) =	user	ft	
Area of Basin Floor (A _{floor}) =	user	ft ²	
Volume of Basin Floor (V _{floor}) =	user	ft ³	
Depth of Main Basin (H _{main}) =	user	ft	
Length of Main Basin (L _{main}) =	user	ft	
Width of Main Basin (W _{main}) =	user	ft	
Area of Main Basin (A _{main}) =	user	ft ²	
Volume of Main Basin (V _{main}) =	user	ft ³	
Calculated Total Basin Volume (V _{total}) =	user	acre-feet	

Depth increment = 0.2 ft

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	500	0.011	858	0.020
5767.33	--	0.33	--	--	--				
5768	--	1.00	--	--	--	48,694	1.118	18,411	0.423
5769	--	2.00	--	--	--	51,543	1.183	68,497	1.572
5770	--	3.00	--	--	--	54,460	1.250	122,014	2.801
5771	--	4.00	--	--	--	57,445	1.319	177,967	4.086
5772	--	5.00	--	--	--	60,499	1.389	236,939	5.439
5773	--	6.00	--	--	--	63,620	1.461	298,998	6.864
5774	--	7.00	--	--	--	66,809	1.534	364,213	8.361
5775	--	8.00	--	--	--	70,066	1.608	432,650	9.932
5776	--	9.00	--	--	--	73,392	1.685	504,379	11.579
5777	--	10.00	--	--	--	76,785	1.763	579,468	13.303
5778	--	11.00	--	--	--	80,246	1.842	657,983	15.105
5779	--	12.00	--	--	--	83,760	1.923	739,986	16.988

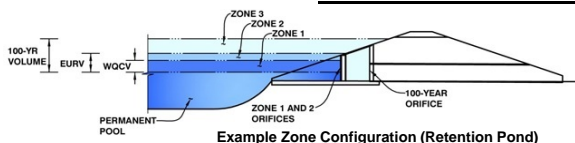
Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: _____

Basin C8, Pond C4



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.01	1.588	Orifice Plate
Zone 2 (EURV)	4.47	3.122	Rectangular Orifice
Zone 3 (100-year)	6.68	3.149	Weir&Pipe (Restrict)
Total		7.859	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.70	1.40					
Orifice Area (sq. inches)	8.00	8.00	8.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.30	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.70	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	8.00		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.11	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.70	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	12.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	% grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	4.70	N/A	feet
Over Flow Weir Slope Length =	12.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	10.70	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	33.60	N/A	ft ²
Overflow Grate Open Area w/ Debris =	16.80	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	48.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	3.14	N/A	ft ²
Outlet Orifice Centroid =	1.00	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

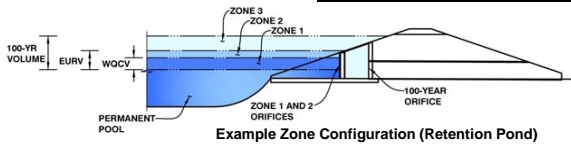
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	1.588	4.710	4.381	6.080	7.491	9.562	11.210	13.250	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.587	4.707	4.378	6.068	7.486	9.546	11.194	13.239	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.15	0.40	0.92	1.21	1.57	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	1.3	11.1	30.2	68.9	90.9	117.7	0.0
Peak Inflow Q (cfs) =	31.9	93.2	86.8	119.5	146.6	185.6	216.5	254.5	#N/A
Peak Outflow Q (cfs) =	0.9	2.2	2.1	12.4	31.7	34.9	37.5	40.5	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.1	1.0	0.5	0.4	0.3	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.3	0.9	1.0	1.0	1.1	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	40	58	57	60	58	56	55	54	#N/A
Time to Drain 99% of Inflow Volume (hours) =	42	64	62	67	66	65	65	64	#N/A
Maximum Ponding Depth (ft) =	1.92	4.27	4.04	4.97	5.38	6.32	7.14	8.16	#N/A
Area at Maximum Ponding Depth (acres) =	1.18	1.34	1.32	1.39	1.42	1.48	1.54	1.62	#N/A
Maximum Volume Stored (acre-ft) =	1.478	4.444	4.125	5.398	5.972	7.335	8.561	10.174	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP (100.013)**

Basin ID: **Pond C5 (only used for WQCV and EURV) Do not use for 100-yr Storm Event!!!!!!**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.01	3.515	Orifice Plate
Zone 2 (EURV)	6.57	6.868	Rectangular Orifice
Zone 3 (100-year)	8.95	7.126	Weir&Pipe (Restrict)
Total		17.508	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.34	2.67					
Orifice Area (sq. inches)	9.21	9.21	9.21					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="4.01"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="6.57"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="18.68"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.78"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.25"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="6.60"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="18.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="6.60"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope Length =	<input type="text" value="3.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="3.01"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="37.80"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="18.90"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="48.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="48.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="12.57"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="2.00"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="3.14"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

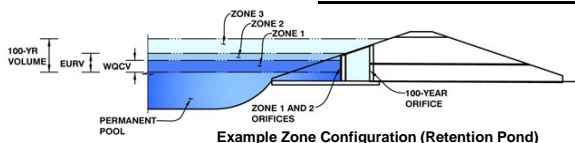
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	3.14
Calculated Runoff Volume (acre-ft) =	3.515	10.382	9.641	13.459	16.659	21.433	25.205	29.878	41.092
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	3.517	10.386	9.640	13.467	16.663	21.449	25.222	29.902	41.123
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.14	0.37	0.85	1.12	1.46	2.19
Predevelopment Peak Q (cfs) =	0.0	0.0	2.8	23.2	63.2	145.3	191.8	249.0	374.8
Peak Inflow Q (cfs) =	63.1	181.4	168.8	233.0	286.9	364.1	424.6	497.8	660.8
Peak Outflow Q (cfs) =	1.4	7.3	7.0	30.7	77.5	132.6	154.2	163.7	171.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.3	1.2	0.9	0.8	0.7	0.5
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.6	1.8	3.3	3.8	4.0	4.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	54	53	55	54	52	50	48	45
Time to Drain 99% of Inflow Volume (hours) =	40	58	57	60	59	58	58	57	56
Maximum Ponding Depth (ft) =	3.92	6.27	6.02	6.99	7.43	7.99	8.50	9.32	10.00
Area at Maximum Ponding Depth (acres) =	2.47	2.80	2.77	2.89	2.95	3.02	3.08	3.18	3.26
Maximum Volume Stored (acre-ft) =	3.298	9.524	8.827	11.603	12.888	14.530	16.086	18.682	20.870

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Project: _____
Basin ID: _____ Basin D1, Pond "D1"



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.74	0.360	Orifice Plate
Zone 2 (EURV)	3.27	0.708	Rectangular Orifice
Zone 3 (100-year)	4.61	0.714	Weir&Pipe (Restrict)
		1.781	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.60	1.20					
Orifice Area (sq. inches)	2.09	2.09	2.09					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="1.74"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="3.27"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	<input type="text" value="2.00"/>	<input type="text" value="N/A"/>	inches
Vertical Orifice Width =	<input type="text" value="7.51"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	<input type="text" value="0.10"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="0.08"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="3.50"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="6.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	%, grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="4.50"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="6.08"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="16.89"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="17.03"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="8.52"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="18.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="10.00"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="1.01"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="0.48"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="1.68"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

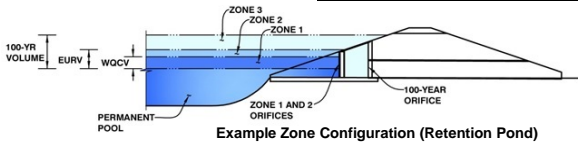
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.360	1.068	0.993	1.378	1.698	2.167	2.541	3.003	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.360	1.068	0.993	1.379	1.700	2.170	2.543	3.006	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.4	3.1	8.3	18.6	24.6	31.6	0.0
Peak Inflow Q (cfs) =	8.8	25.8	24.0	33.2	40.8	51.9	60.7	71.6	#N/A
Peak Outflow Q (cfs) =	0.2	0.9	0.9	1.6	5.2	9.7	10.3	10.9	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.6	0.5	0.4	0.3	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.2	0.5	0.5	0.6	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	37	46	46	47	46	44	43	41	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	54	54	53	52	52	#N/A
Maximum Ponding Depth (ft) =	1.68	3.10	2.96	3.66	4.01	4.47	4.94	5.54	#N/A
Area at Maximum Ponding Depth (acres) =	0.38	0.49	0.49	0.52	0.54	0.56	0.58	0.61	#N/A
Maximum Volume Stored (acre-ft) =	0.337	0.987	0.913	1.265	1.456	1.707	1.970	2.334	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson Ranch East MDDP**

Basin ID: **Pond D2 - Lorson Blvd at East Tributary of JCC**



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.72	1.502	Orifice Plate
Zone 2 (EURV)	3.44	2.944	Rectangular Orifice
Zone 3 (100-year)	5.05	3.012	Weir&Pipe (Restrict)
		7.458	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	1.72	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	6.70	inches
Orifice Plate: Orifice Area per Row =	8.95	sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row =	6.215E-02	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.60	1.20					
Orifice Area (sq. inches)	8.95	8.95	8.95					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	1.72	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.44	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	6.00	N/A	inches
Vertical Orifice Width =	12.22		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.51	N/A	ft ²
Vertical Orifice Centroid =	0.25	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.50	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	14.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	% grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	3.50	N/A	feet
Over Flow Weir Slope Length =	14.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	3.12	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	39.20	N/A	ft ²
Overflow Grate Open Area w/ Debris =	19.60	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	48.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	60.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	12.57	N/A	ft ²
Outlet Orifice Centroid =	2.00	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	6.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	30.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	3.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	1.64	feet
Stage at Top of Freeboard =	10.64	feet
Basin Area at Top of Freeboard =	2.43	acres

Routed Hydrograph Results

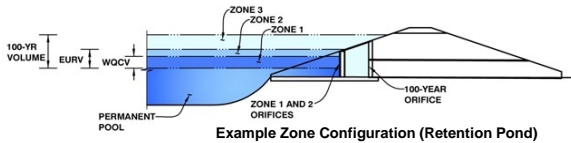
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	3.14
Calculated Runoff Volume (acre-ft) =	1.502	4.446	4.132	5.752	7.103	9.102	10.687	12.650	17.372
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.503	4.450	4.137	5.758	7.109	9.104	10.696	12.654	17.382
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.14	0.38	0.86	1.14	1.48	2.22
Predevelopment Peak Q (cfs) =	0.0	0.0	1.2	9.9	27.0	62.1	81.9	106.3	160.0
Peak Inflow Q (cfs) =	27.6	80.5	75.0	103.6	127.2	161.8	189.2	222.5	303.4
Peak Outflow Q (cfs) =	0.9	4.1	3.9	12.7	33.6	64.7	89.1	102.8	125.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.3	1.2	1.0	1.1	1.0	0.8
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.7	1.5	2.1	2.5	2.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	47	46	46	45	42	41	39	36
Time to Drain 99% of Inflow Volume (hours) =	40	52	52	53	53	51	50	49	47
Maximum Ponding Depth (ft) =	1.65	3.19	3.03	3.72	4.01	4.34	4.55	4.89	6.10
Area at Maximum Ponding Depth (acres) =	1.47	1.78	1.76	1.82	1.85	1.88	1.90	1.93	2.04
Maximum Volume Stored (acre-ft) =	1.385	4.002	3.719	4.938	5.488	6.084	6.481	7.131	9.533

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Lorson Ranch East, MDDP Prelim. Full Spectrum Design, #100.013

Basin ID: _____ Basin E1 - E5, Pond "E1"



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.17	1.128	Orifice Plate
Zone 2 (EURV)	5.90	2.211	Rectangular Orifice
Zone 3 (100-year)	8.30	2.325	Weir&Pipe (Restrict)
Total		5.664	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.10	2.20					
Orifice Area (sq. inches)	3.90	3.90	3.90					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	3.17	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	6.00	N/A	inches
Vertical Orifice Width =	8.56		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.36	N/A	ft ²
Vertical Orifice Centroid =	0.25	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	6.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	10.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	6.00	N/A	feet
Over Flow Weir Slope Length =	10.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	11.08	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	28.00	N/A	ft ²
Overflow Grate Open Area w/ Debris =	14.00	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	18.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	2.53	N/A	ft ²
Outlet Orifice Centroid =	0.83	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.09	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

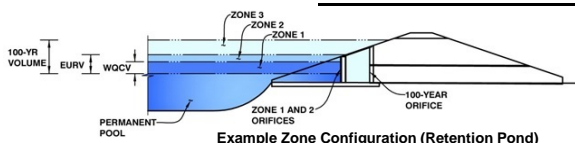
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	1.128	3.339	3.067	4.293	5.354	6.949	8.194	9.743	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.126	3.334	3.063	4.287	5.344	6.933	8.178	9.728	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.17	0.47	1.06	1.40	1.81	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	1.2	9.5	26.3	59.9	79.2	102.1	0.0
Peak Inflow Q (cfs) =	25.0	72.9	67.0	93.3	115.8	149.2	175.2	207.3	#N/A
Peak Outflow Q (cfs) =	0.5	3.3	3.1	12.7	29.5	32.0	34.0	36.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.3	1.1	0.5	0.4	0.4	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.3	0.9	1.0	1.0	1.1	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	48	47	48	47	45	44	42	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	53	52	52	51	51	#N/A
Maximum Ponding Depth (ft) =	3.08	5.55	5.26	6.28	6.71	7.74	8.62	9.73	#N/A
Area at Maximum Ponding Depth (acres) =	0.72	0.87	0.85	0.91	0.94	1.01	1.07	1.14	#N/A
Maximum Volume Stored (acre-ft) =	1.060	3.026	2.776	3.677	4.076	5.089	6.002	7.226	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson Ranch East MDDP**

Basin ID: **Pond E2**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.48	1.254	Orifice Plate
Zone 2 (EURV)	3.21	2.429	Rectangular Orifice
Zone 3 (100-year)	4.90	2.597	Weir&Pipe (Restrict)
		6.280	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.50	1.00					
Orifice Area (sq. inches)	7.67	7.67	7.67					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	1.48	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.21	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	6.00	N/A	inches
Vertical Orifice Width =	11.16		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.47	N/A	ft ²
Vertical Orifice Centroid =	0.25	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	16.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	3.00	N/A	feet
Over Flow Weir Slope Length =	16.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	3.57	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	44.80	N/A	ft ²
Overflow Grate Open Area w/ Debris =	22.40	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	48.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	60.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	12.57	N/A	ft ²
Outlet Orifice Centroid =	2.00	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

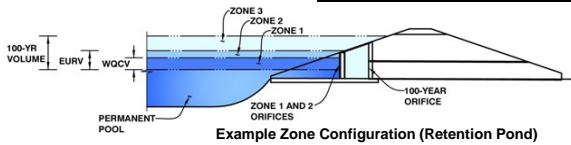
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	3.14
Calculated Runoff Volume (acre-ft) =	1.254	3.682	3.414	4.795	5.964	7.736	9.126	10.851	14.969
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.254	3.685	3.416	4.798	5.967	7.737	9.132	10.853	14.977
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.15	0.40	0.91	1.20	1.55	2.33
Predevelopment Peak Q (cfs) =	0.0	0.0	1.1	9.2	25.0	57.0	75.2	97.4	146.4
Peak Inflow Q (cfs) =	24.1	69.9	64.9	90.5	112.1	144.3	169.5	200.4	273.1
Peak Outflow Q (cfs) =	0.7	3.7	3.5	20.0	40.6	70.7	86.8	95.8	118.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.2	1.6	1.2	1.2	1.0	0.8
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.3	0.8	1.5	1.8	2.0	2.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	46	46	45	43	41	39	38	34
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	52	51	50	49	47	45
Maximum Ponding Depth (ft) =	1.42	2.95	2.78	3.32	3.56	3.84	4.06	4.50	5.80
Area at Maximum Ponding Depth (acres) =	1.35	1.45	1.44	1.48	1.50	1.51	1.53	1.56	1.66
Maximum Volume Stored (acre-ft) =	1.160	3.300	3.069	3.857	4.213	4.620	4.955	5.651	7.745

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**

Basin ID: **Pond F**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.05	0.699	Orifice Plate
Zone 2 (EURV)	6.18	1.373	Rectangular Orifice
Zone 3 (100-year)	8.84	1.386	Weir&Pipe (Restrict)
		3.458	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-7/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.02	2.03					
Orifice Area (sq. inches)	2.81	2.81	2.81					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	3.05	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	6.18	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	2.22		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.03	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.50	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	6.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	12.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	8.50	N/A	feet
Over Flow Weir Slope Length =	12.17	N/A	feet
Grate Open Area / 100-yr Orifice Area =	11.29	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	34.06	N/A	ft ²
Overflow Grate Open Area w/ Debris =	17.03	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	22.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	3.02	N/A	ft ²
Outlet Orifice Centroid =	0.96	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.56	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

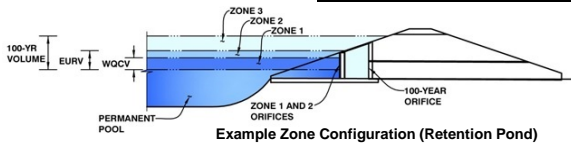
Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	3.14
Calculated Runoff Volume (acre-ft) =	0.699	2.072	1.928	2.675	3.296	4.207	4.933	5.830	7.994
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.699	2.073	1.927	2.675	3.296	4.208	4.934	5.824	7.991
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.13	0.37	0.84	1.11	1.45	2.18
Predevelopment Peak Q (cfs) =	0.0	0.0	0.5	4.4	12.1	27.8	36.7	47.7	71.8
Peak Inflow Q (cfs) =	12.7	37.3	34.7	48.0	58.9	74.9	87.5	102.9	140.1
Peak Outflow Q (cfs) =	0.4	0.9	0.8	3.5	13.2	29.7	39.0	40.9	43.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.8	1.1	1.1	1.1	0.9	0.6
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.1	1.2	1.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	56	55	60	58	56	55	53	49
Time to Drain 99% of Inflow Volume (hours) =	40	62	60	66	65	64	63	62	60
Maximum Ponding Depth (ft) =	2.92	5.94	5.64	6.90	7.39	7.85	8.16	8.89	10.00
Area at Maximum Ponding Depth (acres) =	0.39	0.48	0.47	0.50	0.52	0.53	0.54	0.56	0.59
Maximum Volume Stored (acre-ft) =	0.649	1.955	1.814	2.425	2.679	2.921	3.087	3.484	4.131

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**
Basin ID: **Pond G**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.19	0.394	Orifice Plate
Zone 2 (EURV)	5.17	0.758	Rectangular Orifice
Zone 3 (100-year)	8.10	0.824	Weir&Pipe (Restrict)
		1.976	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-11/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.73	1.46					
Orifice Area (sq. inches)	2.24	2.24	2.24					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.19	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.17	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	4.00	N/A	inches
Vertical Orifice Width =	2.34		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.07	N/A	ft ²
Vertical Orifice Centroid =	0.17	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.20	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	5.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	10.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	8.20	N/A	feet
Over Flow Weir Slope Length =	10.20	N/A	feet
Grate Open Area / 100-yr Orifice Area =	12.00	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	28.55	N/A	ft ²
Overflow Grate Open Area w/ Debris =	14.28	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	17.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	2.38	N/A	ft ²
Outlet Orifice Centroid =	0.79	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.00	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

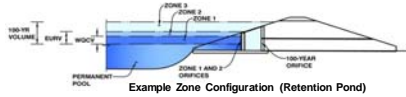
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.394	1.152	1.067	1.503	1.875	2.442	2.886	3.436	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.393	1.152	1.068	1.505	1.876	2.445	2.889	3.440	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.4	3.7	9.8	21.9	28.9	37.1	0.0
Peak Inflow Q (cfs) =	11.4	32.9	30.5	42.8	53.2	69.1	81.5	96.8	#N/A
Peak Outflow Q (cfs) =	0.3	1.0	0.9	1.1	1.1	2.37	30.6	32.6	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.8	1.1	1.1	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.2	0.8	1.0	1.1	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	46	46	48	47	44	42	40	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	51	55	55	54	53	51	#N/A
Maximum Ponding Depth (ft) =	2.09	4.89	4.59	6.13	6.87	7.48	7.94	8.87	#N/A
Area at Maximum Ponding Depth (acres) =	0.24	0.27	0.26	0.28	0.28	0.29	0.29	0.30	#N/A
Maximum Volume Stored (acre-ft) =	0.371	1.078	0.999	1.414	1.618	1.796	1.927	2.203	#N/A

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Project: Lorson East MDDP

Basin ID: Pond G



Example Zone Configuration (Retention Pond)

Required Volume Calculation

Selected BMP Type =	EDB	
Watershed Area =	20.00	acres
Watershed Length =	650	ft
Watershed Slope =	0.043	ft/ft
Watershed Imperviousness =	60.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	100.0%	percent
Desired WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	
Water Quality Capture Volume (WQCV) =	0.394	acre-feet
Excess Urban Runoff Volume (EURV) =	1.152	acre-feet
2-yr Runoff Volume (P1 = 1.16 in.) =	1.067	acre-feet
5-yr Runoff Volume (P1 = 1.44 in.) =	1.503	acre-feet
10-yr Runoff Volume (P1 = 1.68 in.) =	1.875	acre-feet
25-yr Runoff Volume (P1 = 1.92 in.) =	2.442	acre-feet
50-yr Runoff Volume (P1 = 2.16 in.) =	2.886	acre-feet
100-yr Runoff Volume (P1 = 2.42 in.) =	3.436	acre-feet
500-yr Runoff Volume (P1 = 0 in.) =	0.000	acre-feet
Approximate 2-yr Detention Volume =	1.001	acre-feet
Approximate 5-yr Detention Volume =	1.416	acre-feet
Approximate 10-yr Detention Volume =	1.617	acre-feet
Approximate 25-yr Detention Volume =	1.731	acre-feet
Approximate 50-yr Detention Volume =	1.786	acre-feet
Approximate 100-yr Detention Volume =	1.976	acre-feet

Note: L / W Ratio < 1
L / W Ratio = 0.5

Optional User Override 1-hr Precipitation	1.16	inches
	1.44	inches
	1.68	inches
	1.92	inches
	2.16	inches
	2.42	inches

Stage-Storage Calculation

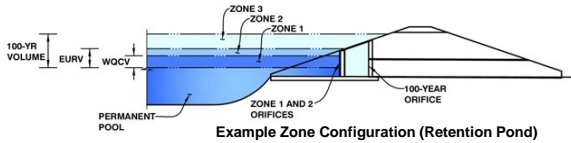
Zone 1 Volume (WQCV) =	0.394	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.758	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.824	acre-feet
Total Detention Basin Volume =	1.976	acre-feet
Initial Surcharge Volume (SV) =	user	ft³
Initial Surcharge Depth (SD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	F:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
Initial Surcharge Area (A _{sv}) =	user	ft²
Surcharge Volume Length (L _{sv}) =	user	ft
Surcharge Volume Width (W _{sv}) =	user	ft
Depth of Basin Floor (H _{bottom}) =	user	ft
Length of Basin Floor (L _{bottom}) =	user	ft
Width of Basin Floor (W _{bottom}) =	user	ft
Area of Basin Floor (A _{bottom}) =	user	ft²
Volume of Basin Floor (V _{bottom}) =	user	ft³
Depth of Main Basin (H _{main}) =	user	ft
Length of Main Basin (L _{main}) =	user	ft
Width of Main Basin (W _{main}) =	user	ft
Area of Main Basin (A _{main}) =	user	ft²
Volume of Main Basin (V _{main}) =	user	ft³
Calculated Total Basin Volume (V _{total}) =	user	acre-feet

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft²)	Area (acre)	Volume (ft³)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	50	0.001		
	--	1.00	--	--	--	10,000	0.230	4,925	0.113
	--	2.00	--	--	--	10,400	0.239	15,121	0.347
	--	3.00	--	--	--	10,800	0.248	25,825	0.593
	--	4.00	--	--	--	11,200	0.257	36,825	0.845
	--	5.00	--	--	--	11,600	0.266	48,225	1.107
	--	6.00	--	--	--	12,000	0.275	60,025	1.378
	--	7.00	--	--	--	12,400	0.285	72,225	1.658
	--	8.00	--	--	--	12,800	0.294	84,825	1.947
	--	9.00	--	--	--	13,200	0.303	97,825	2.246
	--	10.00	--	--	--	13,600	0.312	111,225	2.553

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**
Basin ID: **Pond H**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.44	0.439	Orifice Plate
Zone 2 (EURV)	4.92	0.846	Rectangular Orifice
Zone 3 (100-year)	7.41	0.919	Weir&Pipe (Restrict)
		2.203	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.81	1.63					
Orifice Area (sq. inches)	2.03	2.03	2.03					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.44	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.92	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	2.84		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.04	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.50	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	6.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	12.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	7.50	N/A	feet
Over Flow Weir Slope Length =	12.17	N/A	feet
Grate Open Area / 100-yr Orifice Area =	12.18	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	34.06	N/A	ft ²
Overflow Grate Open Area w/ Debris =	17.03	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	20.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	2.80	N/A	ft ²
Outlet Orifice Centroid =	0.90	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.30	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

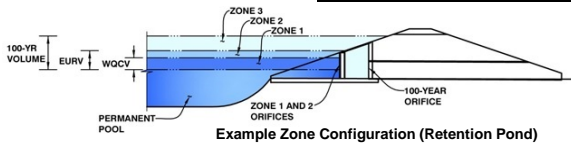
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.439	1.284	1.190	1.676	2.090	2.723	3.218	3.832	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.438	1.285	1.190	1.677	2.092	2.725	3.220	3.835	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.5	4.1	10.9	24.4	32.2	41.4	0.0
Peak Inflow Q (cfs) =	10.9	31.7	29.4	41.2	51.3	66.5	78.4	93.2	#N/A
Peak Outflow Q (cfs) =	0.2	0.7	0.7	1.7	9.1	24.5	33.4	35.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.8	1.0	1.0	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.2	0.7	1.0	1.0	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	37	52	51	55	54	52	50	48	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	58	57	62	62	60	59	58	#N/A
Maximum Ponding Depth (ft) =	2.36	4.73	4.47	5.72	6.23	6.74	7.04	7.78	#N/A
Area at Maximum Ponding Depth (acres) =	0.33	0.35	0.35	0.36	0.37	0.38	0.38	0.39	#N/A
Maximum Volume Stored (acre-ft) =	0.412	1.219	1.128	1.574	1.761	1.948	2.065	2.348	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**

Basin ID: **Pond i**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.64	0.256	Orifice Plate
Zone 2 (EURV)	5.02	0.493	Rectangular Orifice
Zone 3 (100-year)	7.34	0.536	Weir&Pipe (Restrict)
		1.284	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-1/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.88	1.76					
Orifice Area (sq. inches)	1.03	1.03	1.03					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.64	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.02	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	2.00		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.03	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.60	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	5.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	10.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	7.60	N/A	feet
Over Flow Weir Slope Length =	10.20	N/A	feet
Grate Open Area / 100-yr Orifice Area =	17.20	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	28.55	N/A	ft ²
Overflow Grate Open Area w/ Debris =	14.28	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	16.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.66	N/A	ft ²
Outlet Orifice Centroid =	0.71	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.46	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

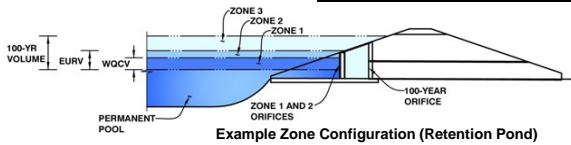
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.256	0.749	0.694	0.977	1.219	1.587	1.876	2.234	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.255	0.749	0.693	0.977	1.219	1.588	1.877	2.235	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.3	2.4	6.4	14.2	18.8	24.1	0.0
Peak Inflow Q (cfs) =	6.3	18.4	17.0	23.9	29.7	38.6	45.5	54.1	#N/A
Peak Outflow Q (cfs) =	0.1	0.4	0.4	1.0	5.7	15.1	19.9	21.0	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.9	1.1	1.1	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.2	0.5	0.7	0.7	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	37	53	52	57	55	53	52	50	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	59	57	63	62	61	60	59	#N/A
Maximum Ponding Depth (ft) =	2.56	4.85	4.60	5.77	6.21	6.64	6.92	7.60	#N/A
Area at Maximum Ponding Depth (acres) =	0.19	0.22	0.22	0.23	0.23	0.24	0.24	0.24	#N/A
Maximum Volume Stored (acre-ft) =	0.241	0.709	0.657	0.917	1.018	1.116	1.182	1.348	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**

Basin ID: **Pond J**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.53	0.236	Orifice Plate
Zone 2 (EURV)	4.76	0.455	Rectangular Orifice
Zone 3 (100-year)	6.93	0.494	Weir&Pipe (Restrict)
		1.186	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-1/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.88	1.76					
Orifice Area (sq. inches)	0.99	0.99	0.99					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.53	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.76	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	2.00		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.03	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.60	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	5.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	10.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	7.60	N/A	feet
Over Flow Weir Slope Length =	10.20	N/A	feet
Grate Open Area / 100-yr Orifice Area =	17.20	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	28.55	N/A	ft ²
Overflow Grate Open Area w/ Debris =	14.28	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	16.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.66	N/A	ft ²
Outlet Orifice Centroid =	0.71	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.46	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

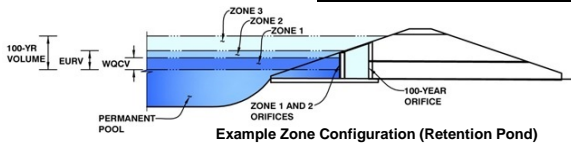
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	0.00
Calculated Runoff Volume (acre-ft) =	0.236	0.691	0.640	0.902	1.125	1.465	1.731	2.062	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.236	0.690	0.639	0.900	1.123	1.463	1.729	2.059	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.18	0.49	1.09	1.44	1.86	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.3	2.2	5.9	13.1	17.3	22.3	0.0
Peak Inflow Q (cfs) =	5.7	16.5	15.3	21.5	26.8	34.8	41.0	48.7	#N/A
Peak Outflow Q (cfs) =	0.1	0.4	0.4	0.4	3.4	11.7	18.3	20.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.6	0.9	1.1	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.4	0.6	0.7	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	37	52	51	57	56	54	53	51	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	58	57	63	63	62	61	60	#N/A
Maximum Ponding Depth (ft) =	2.46	4.58	4.35	5.50	6.05	6.51	6.75	7.19	#N/A
Area at Maximum Ponding Depth (acres) =	0.19	0.22	0.21	0.22	0.23	0.23	0.24	0.24	#N/A
Maximum Volume Stored (acre-ft) =	0.222	0.653	0.603	0.856	0.981	1.085	1.142	1.247	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Lorson East MDDP**

Basin ID: **Pond K**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.49	0.073	Orifice Plate
Zone 2 (EURV)	4.43	0.140	Rectangular Orifice
Zone 3 (100-year)	6.42	0.152	Weir&Pipe (Restrict)
		0.366	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 9/16 inch)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.80	1.60	2.40				
Orifice Area (sq. inches)	0.25	0.25	0.25	0.25				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.49	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.43	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	0.73		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.01	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Slope =	4.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	8.00	N/A	feet
Overflow Weir Slope Length =	4.12	N/A	feet
Grate Open Area / 100-yr Orifice Area =	15.21	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	11.54	N/A	ft ²
Overflow Grate Open Area w/ Debris =	5.77	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	8.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.76	N/A	ft ²
Outlet Orifice Centroid =	0.39	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.46	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

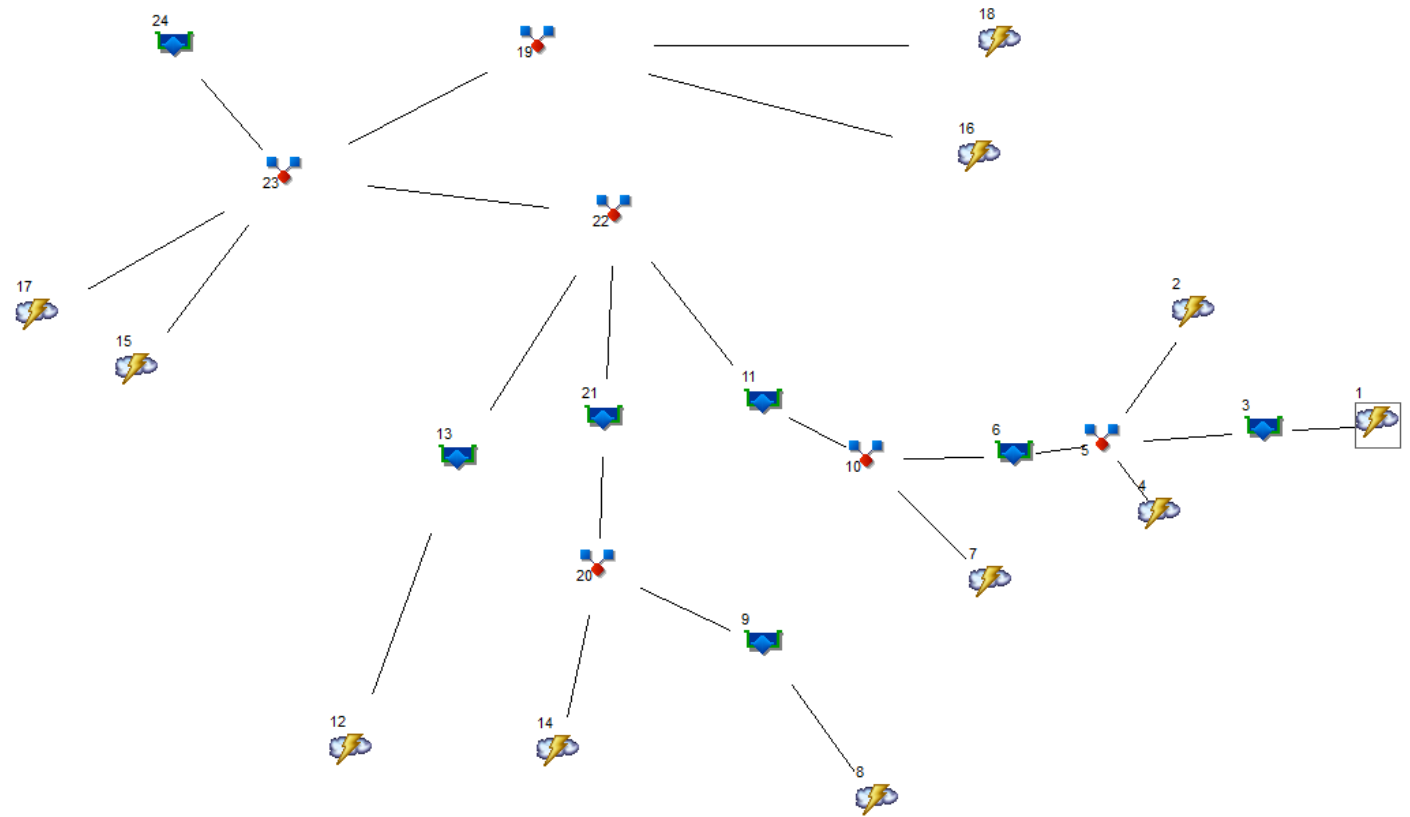
Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.16	1.44	1.68	1.92	2.16	2.42	3.14
Calculated Runoff Volume (acre-ft) =	0.073	0.213	0.197	0.278	0.347	0.452	0.534	0.636	0.878
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.072	0.213	0.197	0.277	0.347	0.452	0.534	0.636	0.878
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.17	0.45	1.01	1.33	1.71	2.57
Predevelopment Peak Q (cfs) =	0.0	0.0	0.1	0.6	1.7	3.7	4.9	6.3	9.5
Peak Inflow Q (cfs) =	1.7	4.9	4.5	6.4	7.9	10.3	12.1	14.4	19.9
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.2	0.5	2.7	5.6	10.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.1	0.1	0.5	0.9	1.1
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.0	0.2	0.5	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	54	53	59	62	66	65	63	59
Time to Drain 99% of Inflow Volume (hours) =	39	58	57	63	68	73	72	72	70
Maximum Ponding Depth (ft) =	2.42	4.26	4.05	5.09	5.96	7.13	7.43	7.66	8.11
Area at Maximum Ponding Depth (acres) =	0.07	0.07	0.07	0.08	0.08	0.08	0.08	0.08	0.08
Maximum Volume Stored (acre-ft) =	0.068	0.201	0.185	0.262	0.329	0.423	0.446	0.466	0.503

APPENDIX E – HYDROGRAPHS



Legend

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	Rational	C8
2	Rational	Basins OS-C9 & C10
3	Reservoir	Pond C4 outflow
4	Rational	Basin C8a
5	Combine	Inflow Pond C3
6	Reservoir	Pond C3 outflow
7	Rational	Basins C5 & C7
8	Rational	Basin C3 & C4
9	Reservoir	Pond C2.1 outflow
10	Combine	Inflow Pond C2.2
11	Reservoir	Pond C2.2 outflow
12	Rational	Basins C1 & C2
13	Reservoir	Pond C1 outflow
14	Rational	Basin C6
15	Rational	Basin C14+C15
16	Rational	Basin C13
17	Rational	C17
18	Rational	Basins C16 & C12
19	Combine	Des.Pt.6c to Pond C5
20	Combine	inflow Pond C2.3
21	Reservoir	Pond C2.3 outflow
22	Combine	Des. Pt 3f
23	Combine	Inflow Pond C5
24	Reservoir	Pond C5 outflow

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	Rational	106.80	1	19	121,752	---	-----	-----	C8
2	Rational	29.21	1	15	26,289	---	-----	-----	Basins OS-C9 & C10
3	Reservoir	12.40	1	36	24,518	1	5772.03	247,806	Pond C4 outflow
4	Rational	20.81	1	12	14,982	---	-----	-----	Basin C8a
5	Combine	44.82	1	15	65,789	2, 3, 4	-----	-----	Inflow Pond C3
6	Reservoir	4.568	1	58	20,897	5	5760.24	75,308	Pond C3 outflow
7	Rational	48.92	1	25	73,387	---	-----	-----	Basins C5 & C7
8	Rational	83.17	1	25	124,758	---	-----	-----	Basin C3 & C4
9	Reservoir	11.73	1	46	17,691	8	5771.23	210,648	Pond C2.1 outflow
10	Combine	48.92	1	25	94,284	6, 7,	-----	-----	Inflow Pond C2.2
11	Reservoir	6.735	1	49	28,966	10	5750.97	162,116	Pond C2.2 outflow
12	Rational	70.57	1	25	105,861	---	-----	-----	Basins C1 & C2- Pond C1 inflow
13	Reservoir	2.952	1	49	14,392	12	5750.59	260,656	Pond C1 outflow
14	Rational	31.01	1	14	26,052	---	-----	-----	Basin C6
15	Rational	65.81	1	23	90,814	---	-----	-----	Basin C14+C15
16	Rational	6.881	1	30	12,386	---	-----	-----	Basin C13
17	Rational	46.96	1	16	45,084	---	-----	-----	C17
18	Rational	79.61	1	31	148,075	---	-----	-----	Basins C16 & C12
19	Combine	86.26	1	31	160,462	16, 18	-----	-----	Des.Pt.6c to Pond C5
20	Combine	31.01	1	14	43,743	9, 14,	-----	-----	inflow Pond C2.3
21	Reservoir	4.548	1	61	13,634	20	5749.16	64,350	Pond C2.3 outflow
22	Combine	12.37	1	57	56,992	11, 13, 21	-----	-----	Des. Pt 3f
23	Combine	156.57	1	23	353,350	15, 17, 19, 22	-----	-----	Inflow Pond C5
24	Reservoir	121.19	1	32	341,003	23	5713.47	566,932	Pond C5 outflow

5yr ponds C1 C2, C3, C4 & C5.gpw Return Period: 5 Year Wednesday, May 24 2017, 5:39 AM

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	Rational	266.64	1	19	303,974	---	-----	-----	C8
2	Rational	63.71	1	15	57,341	---	-----	-----	Basins OS-C9 & C10
3	Reservoir	38.34	1	35	298,076	1	5775.34	467,055	Pond C4 outflow
4	Rational	51.32	1	12	36,953	---	-----	-----	Basin C8a
5	Combine	133.89	1	15	392,370	2, 3, 4	-----	-----	Inflow Pond C3
6	Reservoir	17.79	1	144	367,493	5	5763.93	275,851	Pond C3 outflow
7	Rational	121.62	1	25	182,430	---	-----	-----	Basins C5 & C7
8	Rational	206.75	1	25	310,131	---	-----	-----	Basin C3 & C4
9	Reservoir	65.13	1	42	279,789	8	5773.91	363,096	Pond C2.1 outflow
10	Combine	137.71	1	25	549,923	6, 7,	-----	-----	Inflow Pond C2.2
11	Reservoir	40.34	1	45	530,339	10	5753.55	278,207	Pond C2.2 outflow
12	Rational	175.44	1	25	263,155	---	-----	-----	Basins C1 & C2
13	Reservoir	17.68	1	47	222,974	12	5753.09	445,161	Pond C1 outflow
14	Rational	76.98	1	14	64,659	---	-----	-----	Basin C6
15	Rational	163.99	1	23	226,299	---	-----	-----	Basin C14+C15
16	Rational	40.73	1	30	73,322	---	-----	-----	Basin C13
17	Rational	108.00	1	16	103,681	---	-----	-----	C17
18	Rational	195.70	1	31	363,995	---	-----	-----	Basins C16 & C12
19	Combine	235.07	1	31	437,317	16, 18	-----	-----	Des.Pt.6c to Pond C5
20	Combine	110.99	1	17	344,448	9, 14,	-----	-----	inflow Pond C2.3
21	Reservoir	45.83	1	84	334,262	20	5753.06	188,378	Pond C2.3 outflow
22	Combine	99.75	1	48	1,087,511	11, 13, 21	-----	-----	Des. Pt 3f
23	Combine	484.24	1	23	1,854,809	15, 17, 19, 22	-----	-----	Inflow Pond C5
24	Reservoir	419.90	1	32	1,757,155	23	5714.32	677,645	Pond C5 outflow

100yr ponds C1 C2, C3, C4 & C5.gpw Return Period: 100 Year Tuesday, May 23 2017, 7:33 AM

Pond Report

Pond No. 4 - Pond C1

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5746.00	26,303	0	0
1.00	5747.00	53,900	40,102	40,102
2.00	5748.00	57,925	55,913	96,014
3.00	5749.00	62,019	59,972	155,986
4.00	5750.00	66,200	64,110	220,096
5.00	5751.00	70,500	68,350	288,446
6.00	5752.00	74,920	72,710	361,156
7.00	5753.00	78,760	76,840	437,996
8.00	5754.00	80,000	79,380	517,376
9.00	5755.00	82,000	81,000	598,376
10.00	5756.00	85,000	83,500	681,876

Culvert / Orifice Structures

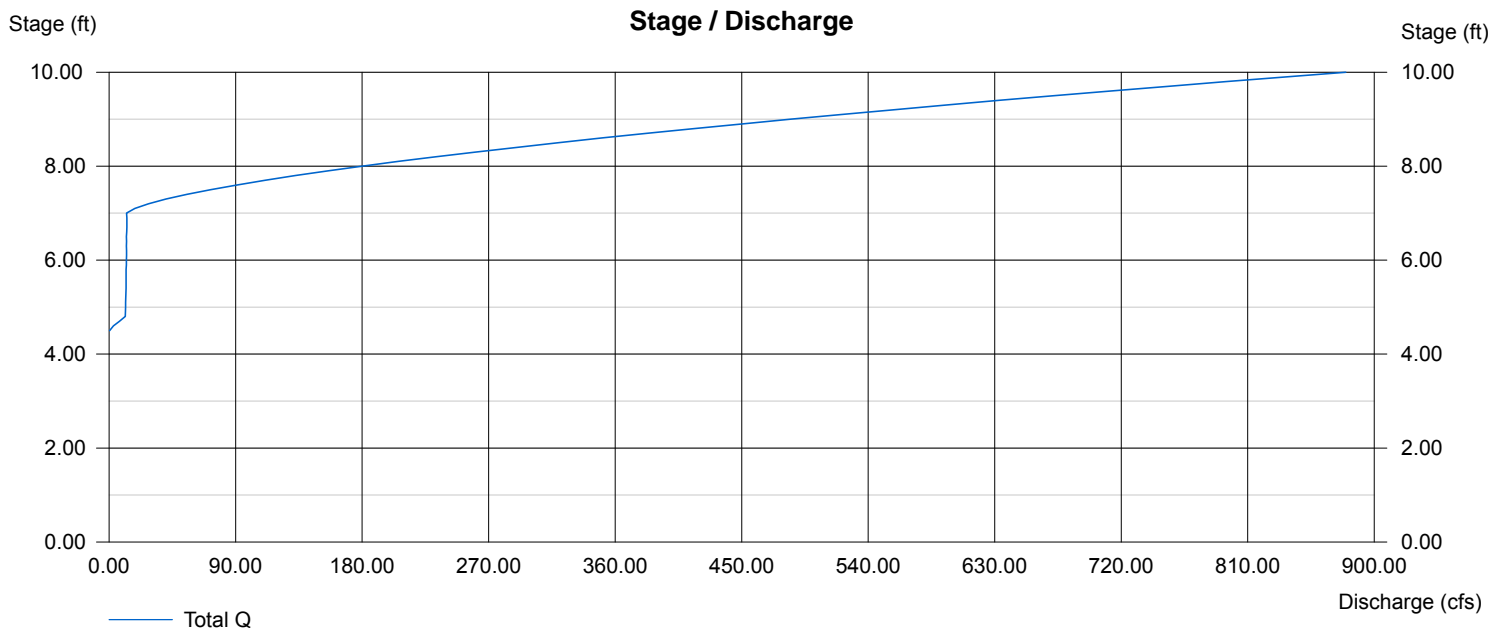
	[A]	[B]	[C]	[D]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5743.50	0.00	0.00	0.00
Length (ft)	= 675.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 20.00	50.00	0.00	0.00
Crest El. (ft)	= 5750.47	5753.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Pond Report

Pond No. 7 - Pond C2.1

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5765.00	50	0	0
1.00	5766.00	5,012	2,531	2,531
2.00	5767.00	29,041	17,027	19,558
3.00	5768.00	43,198	36,120	55,677
4.00	5769.00	46,089	44,644	100,321
5.00	5770.00	49,051	47,570	147,891
6.00	5771.00	52,082	50,567	198,457
7.00	5772.00	55,183	53,633	252,090
8.00	5773.00	58,358	56,771	308,860
9.00	5774.00	61,000	59,679	368,539

Culvert / Orifice Structures

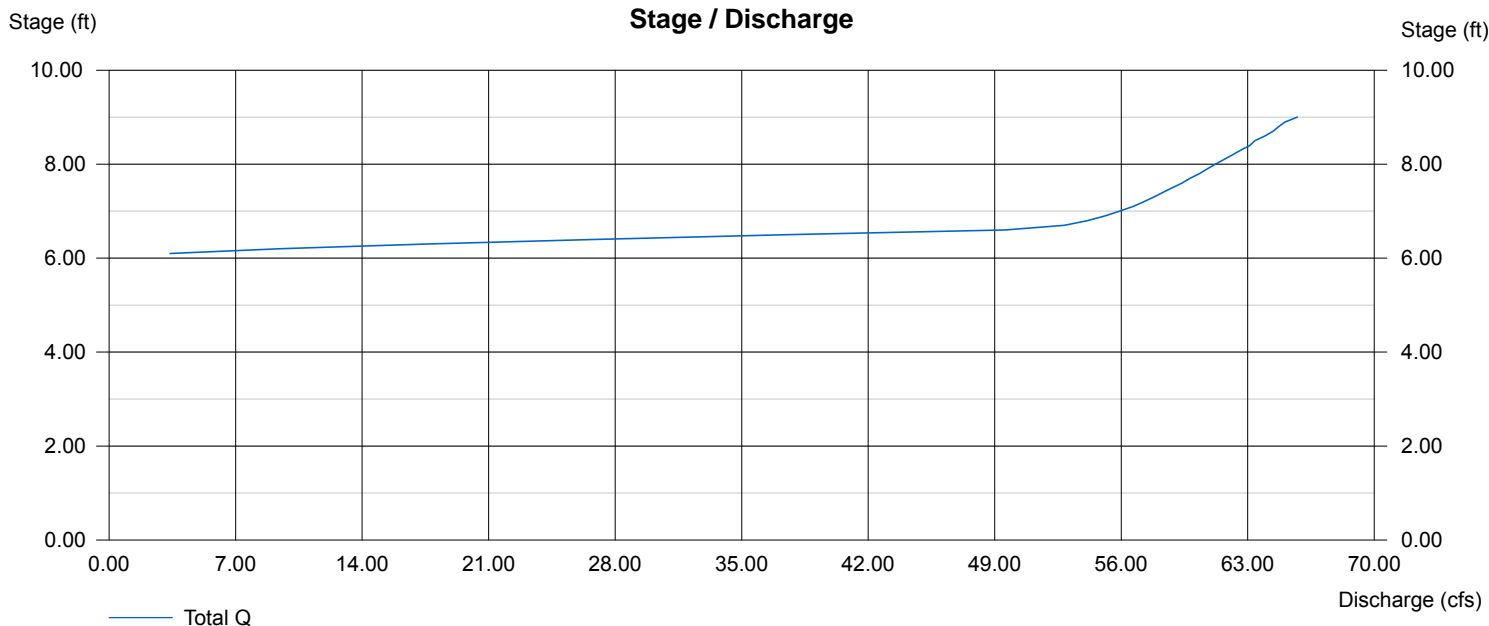
	[A]	[B]	[C]	[D]
Rise (in)	= 30.00	0.00	0.00	0.00
Span (in)	= 30.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5765.00	0.00	0.00	0.00
Length (ft)	= 100.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.000	.000	.000
Orif. Coeff.	= 0.60	0.00	0.00	0.00
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 32.00	50.00	0.00	0.00
Crest El. (ft)	= 5771.00	5774.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Pond Report

Pond No. 3 - Pond C2.2

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5745.00	10	0	0
1.00	5746.00	2,363	1,187	1,187
2.00	5747.00	31,533	16,948	18,135
3.00	5748.00	33,850	32,692	50,826
4.00	5749.00	36,237	35,044	85,870
5.00	5750.00	38,701	37,469	123,339
6.00	5751.00	41,268	39,985	163,323
7.00	5752.00	44,081	42,675	205,998
8.00	5753.00	47,000	45,541	251,538
9.00	5754.00	50,000	48,500	300,038
10.00	5755.00	53,000	51,500	351,538
11.00	5756.00	56,000	54,500	406,038

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5745.00	0.00	0.00	0.00
Length (ft)	= 100.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

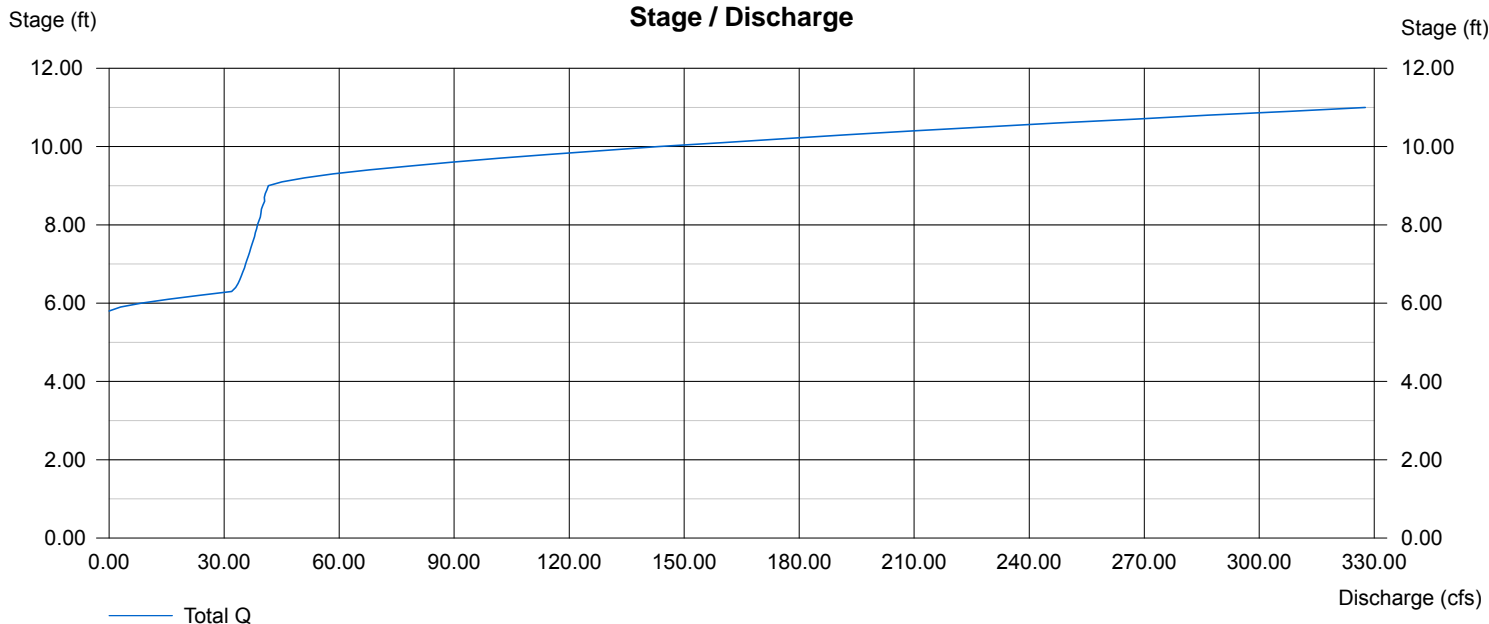
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 28.00	30.00	0.00	0.00
Crest El. (ft)	= 5750.80	5754.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



Pond Report

Pond No. 6 - Pond C2.3

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5746.00	100	0	0
1.00	5747.00	22,141	11,121	11,121
2.00	5748.00	24,321	23,231	34,352
3.00	5749.00	26,601	25,461	59,813
4.00	5750.00	28,983	27,792	87,605
5.00	5751.00	31,466	30,225	117,829
6.00	5752.00	34,050	32,758	150,587
7.00	5753.00	36,742	35,396	185,983
8.00	5754.00	38,000	37,371	223,354

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 27.00	0.00	0.00	0.00
Span (in)	= 27.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5746.00	0.00	0.00	0.00
Length (ft)	= 100.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.000	.000	.000
Orif. Coeff.	= 0.60	0.00	0.00	0.00
Multi-Stage	= n/a	No	No	No

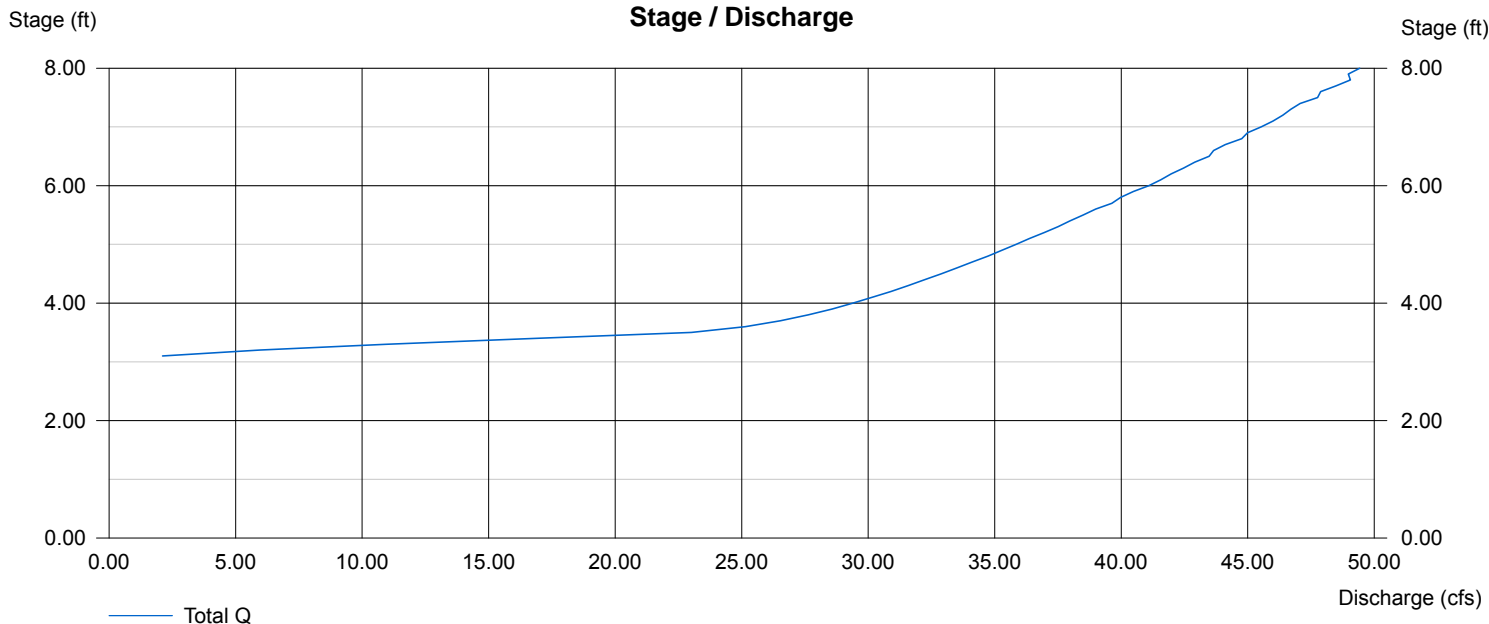
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 20.00	30.00	0.00	0.00
Crest El. (ft)	= 5749.00	5754.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



Pond Report

Pond No. 2 - Pond C3

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5758.00	13,580	0	0
1.00	5759.00	33,254	23,417	23,417
2.00	5760.00	46,803	40,029	63,446
3.00	5761.00	50,425	48,614	112,060
4.00	5762.00	54,123	52,274	164,334
5.00	5763.00	57,909	56,016	220,350
6.00	5764.00	61,796	59,853	280,202
7.00	5765.00	70,319	66,058	346,260
8.00	5766.00	74,258	72,289	418,548
9.00	5767.00	78,270	76,264	494,812
10.00	5768.00	82,343	80,307	575,119

Culvert / Orifice Structures

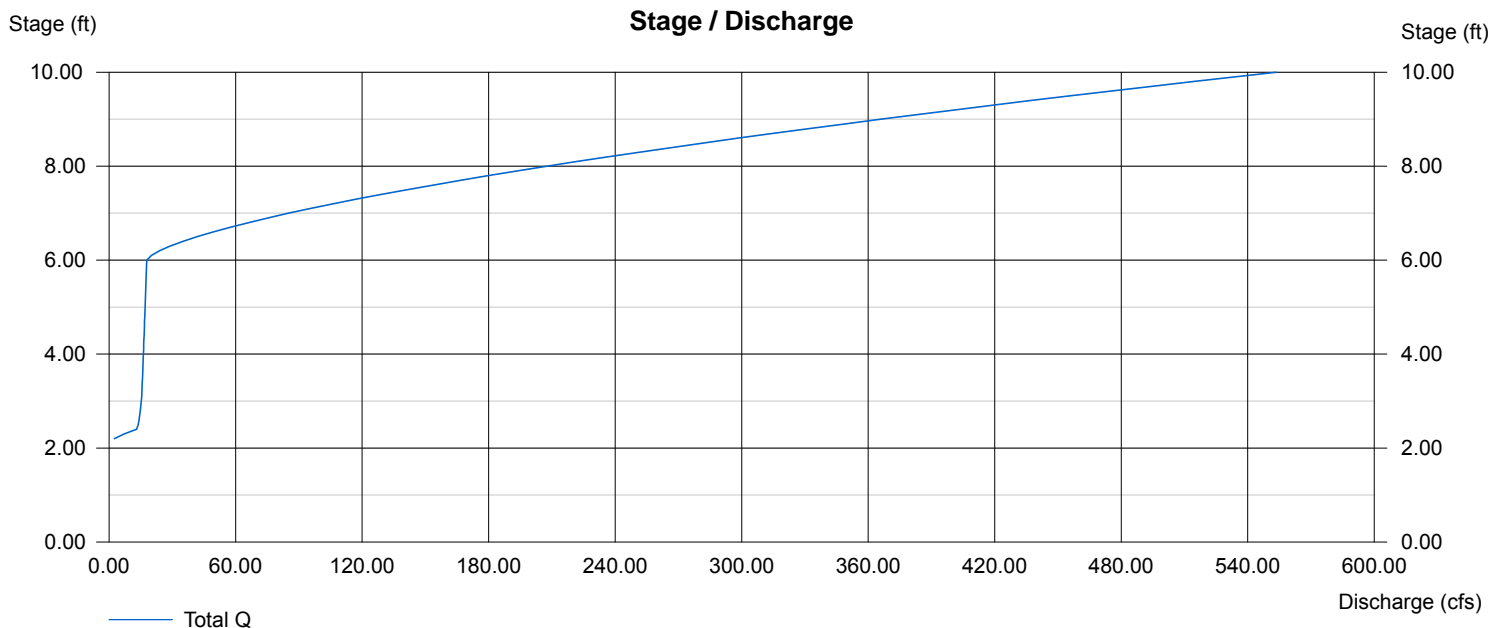
	[A]	[B]	[C]	[D]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5757.00	0.00	0.00	0.00
Length (ft)	= 325.00	0.00	0.00	0.00
Slope (%)	= 1.90	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 24.00	20.00	0.00	0.00
Crest El. (ft)	= 5760.10	5764.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Pond Report

Pond No. 1 - Pond C4

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5766.50	500	0	0
0.50	5767.00	5,000	1,375	1,375
1.50	5768.00	48,694	26,847	28,222
2.50	5769.00	51,543	50,119	78,341
3.50	5770.00	54,460	53,002	131,342
4.50	5771.00	57,445	55,953	187,295
5.50	5772.00	60,499	58,972	246,267
6.50	5773.00	63,620	62,060	308,326
7.50	5774.00	66,809	65,215	373,541
8.50	5775.00	70,666	68,738	442,278
9.50	5776.00	73,392	72,029	514,307
10.50	5777.00	76,785	75,089	589,396
11.50	5778.00	80,246	78,516	667,911

Culvert / Orifice Structures

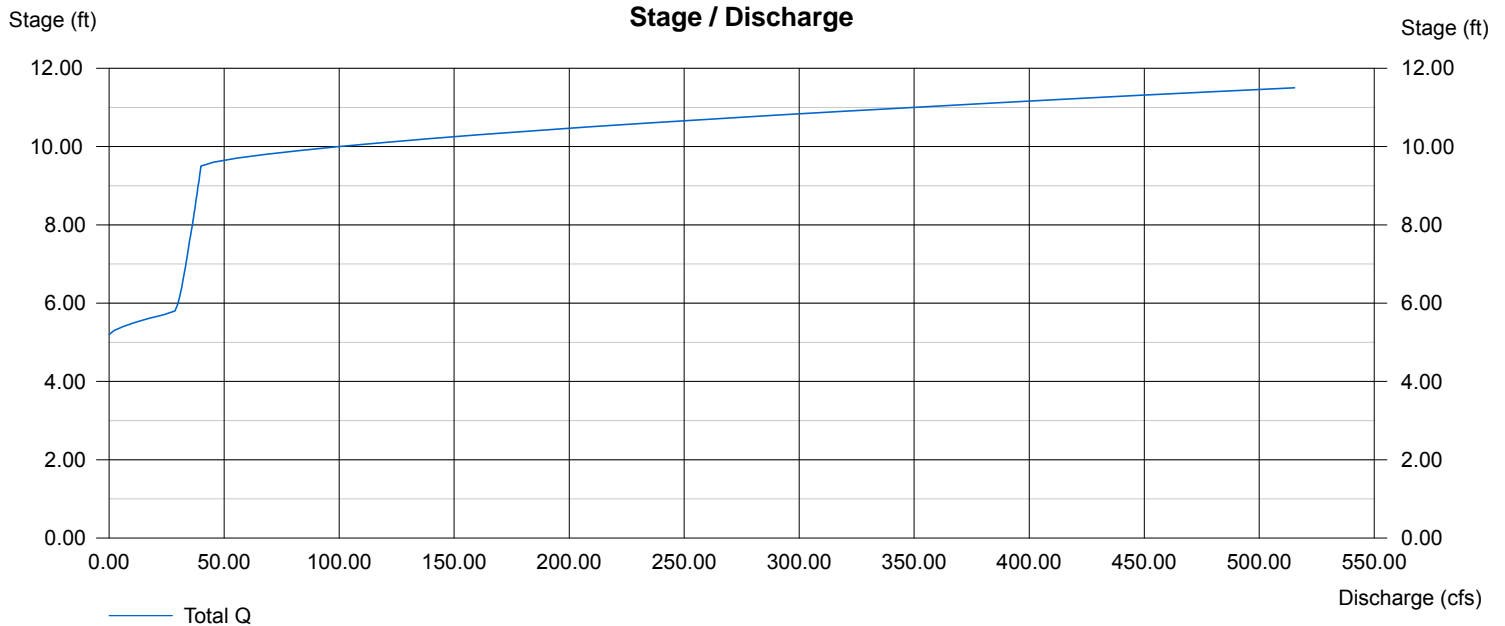
	[A]	[B]	[C]	[D]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5766.50	0.00	0.00	0.00
Length (ft)	= 150.00	0.00	0.00	0.00
Slope (%)	= 0.60	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 20.00	50.00	0.00	0.00
Crest El. (ft)	= 5771.70	5776.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Pond Report

Pond No. 5 - Pond C5

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5707.00	1,000	0	0
1.00	5708.00	18,898	9,949	9,949
2.00	5709.00	77,432	48,165	58,114
3.00	5710.00	110,270	93,851	151,965
4.00	5711.00	115,455	112,863	264,828
5.00	5712.00	120,720	118,088	382,915
6.00	5713.00	126,045	123,383	506,298
7.00	5714.00	131,696	128,871	635,168
8.00	5715.00	136,745	134,221	769,389
9.00	5716.00	141,857	139,301	908,690

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 48.00	0.00	0.00	0.00
Span (in)	= 48.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5704.50	0.00	0.00	0.00
Length (ft)	= 120.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

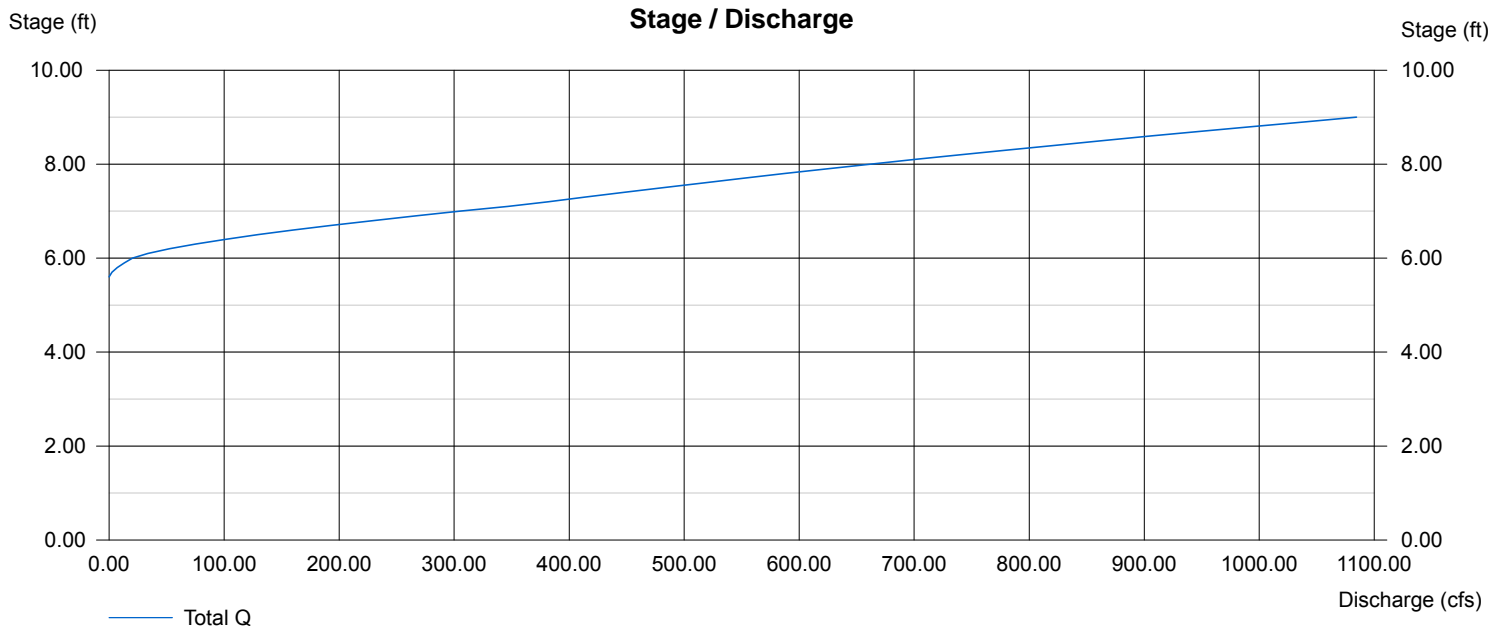
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 24.00	52.00	0.00	0.00
Crest El. (ft)	= 5712.60	5713.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

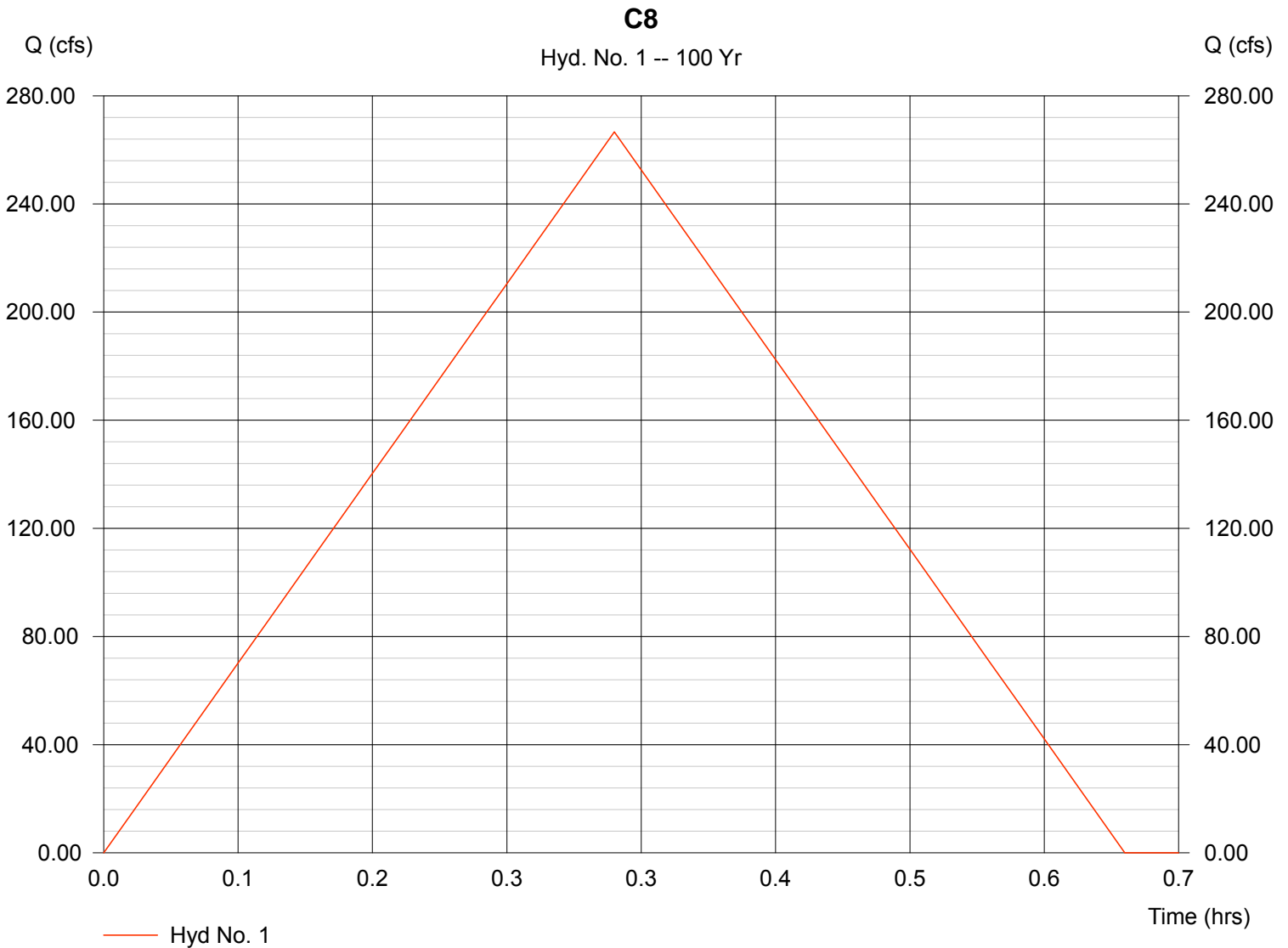
Hyd. No. 1

C8

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 75.000 ac
Intensity = 5.470 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 266.64 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 19.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 303,974 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

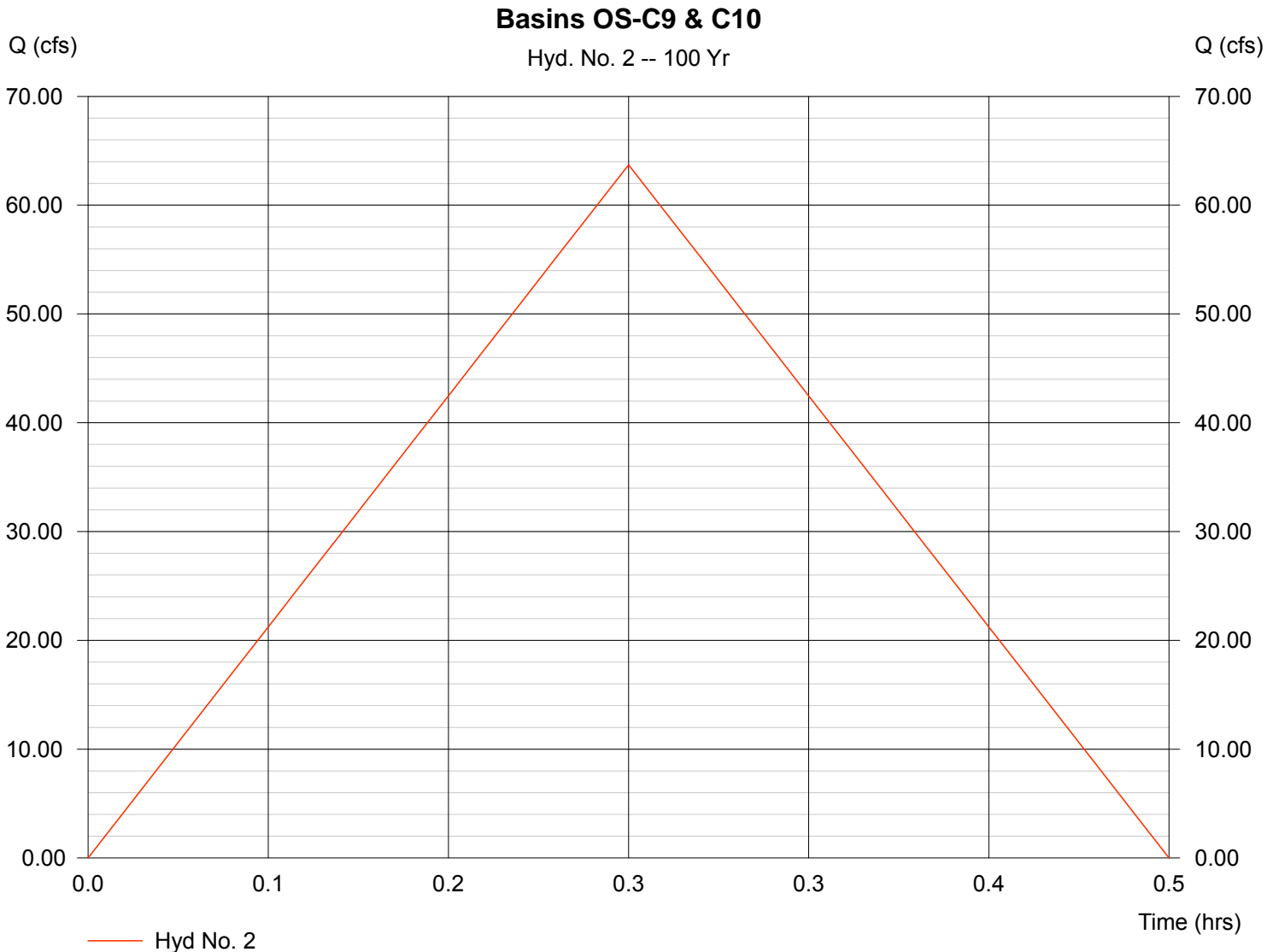
Hyd. No. 2

Basins OS-C9 & C10

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 18.200 ac
Intensity = 6.142 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 63.71 cfs
Time interval = 1 min
Runoff coeff. = 0.57
Tc by User = 15.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 57,341 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 3

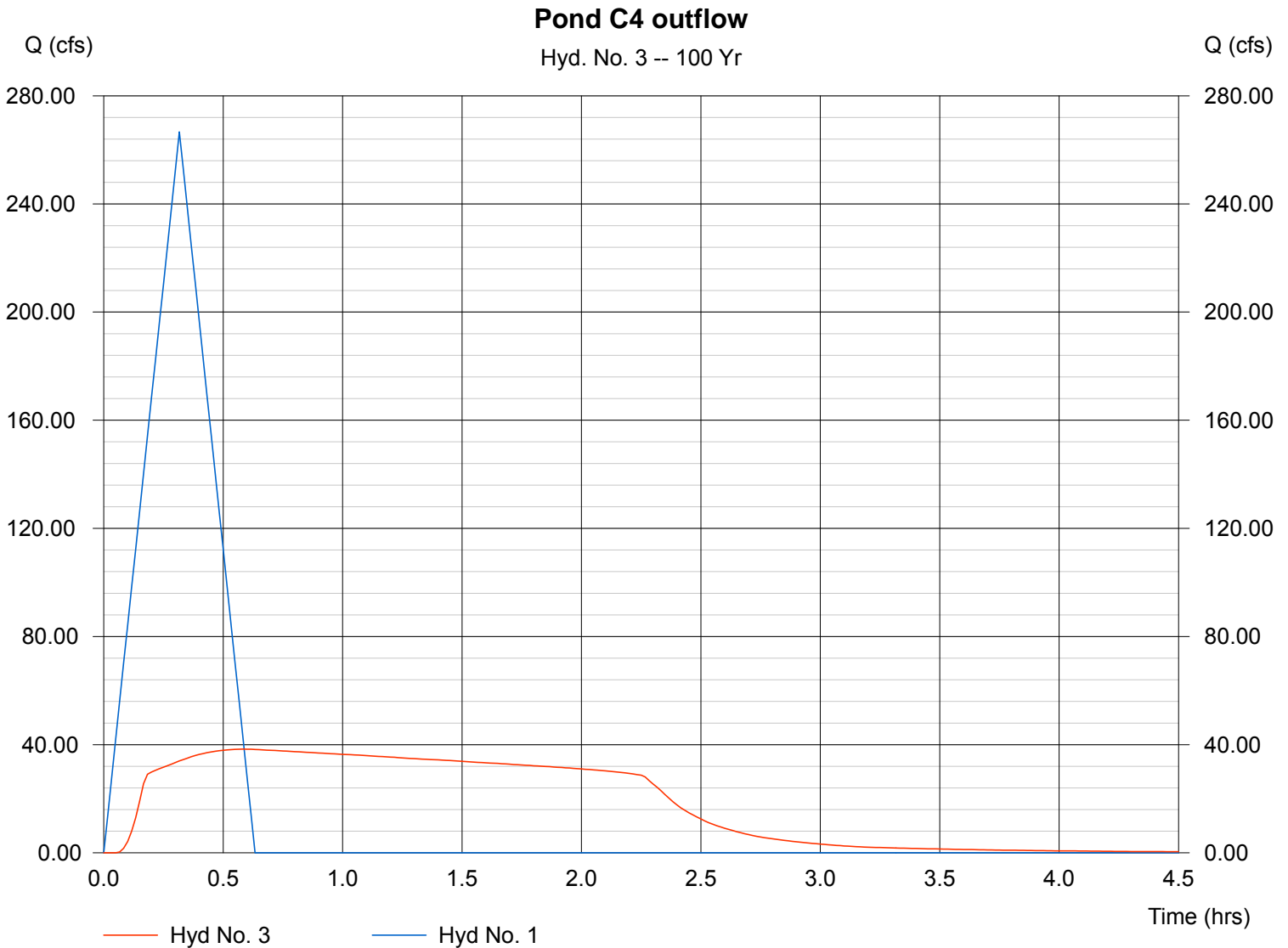
Pond C4 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 1
Reservoir name = Pond C4

Peak discharge = 38.34 cfs
Time interval = 1 min
Max. Elevation = 5775.34 ft
Max. Storage = 467,055 cuft

Storage Indication method used. Wet pond routing start elevation = 5771.60 ft.

Hydrograph Volume = 298,076 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

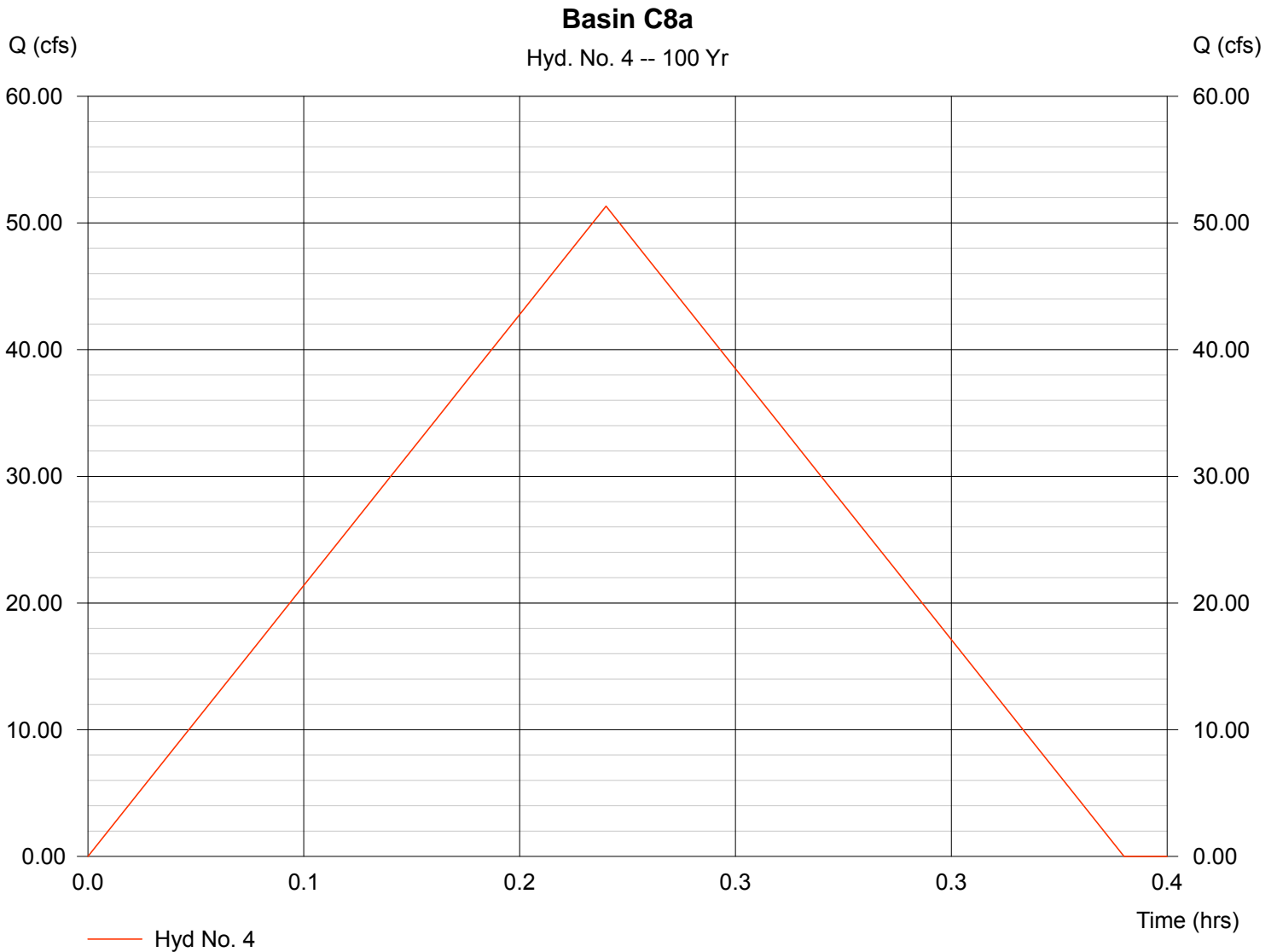
Hyd. No. 4

Basin C8a

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 11.700 ac
Intensity = 6.749 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 51.32 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 12.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 36,953 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

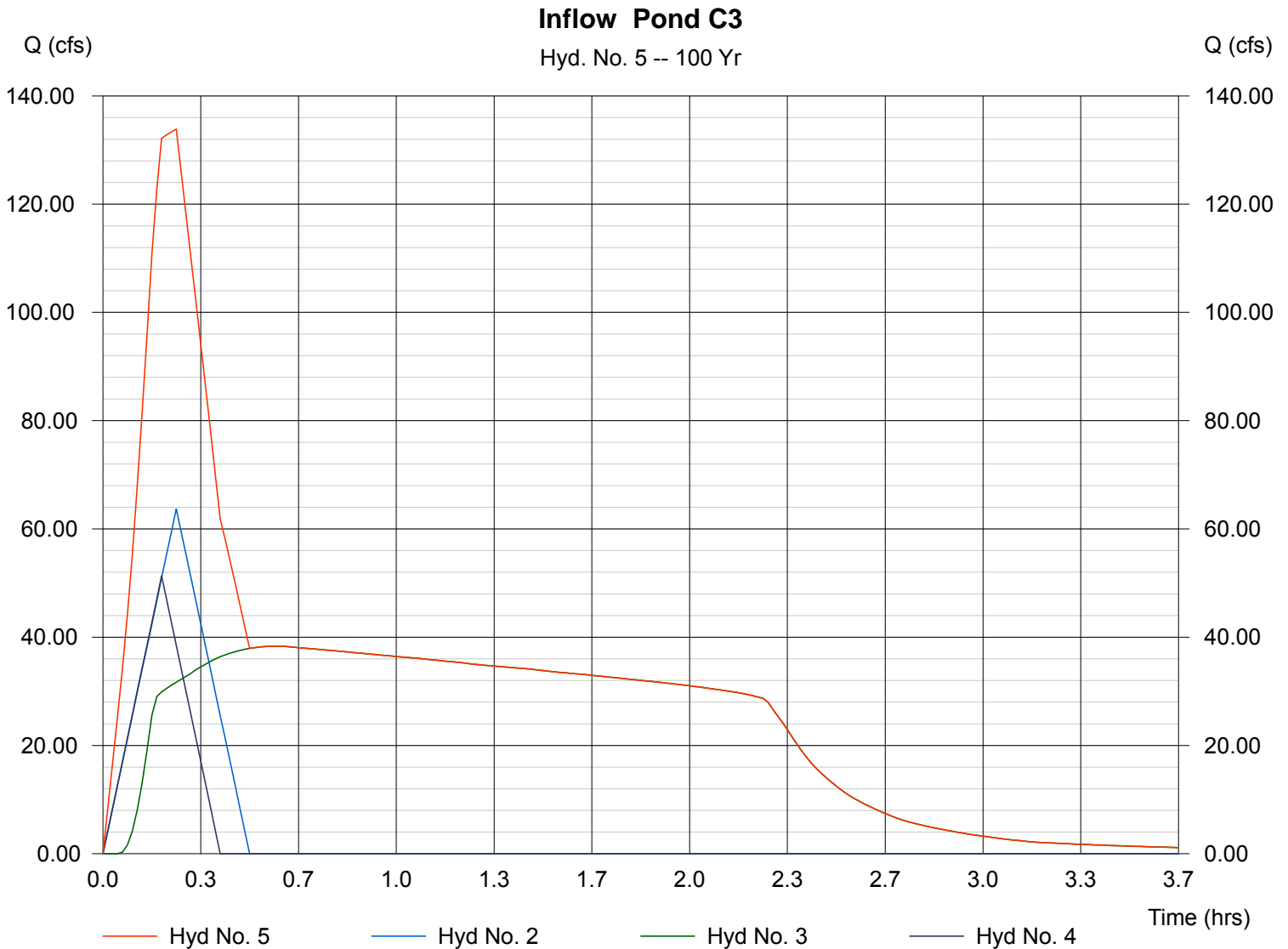
Hyd. No. 5

Inflow Pond C3

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 2, 3, 4

Peak discharge = 133.89 cfs
Time interval = 1 min

Hydrograph Volume = 392,370 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 6

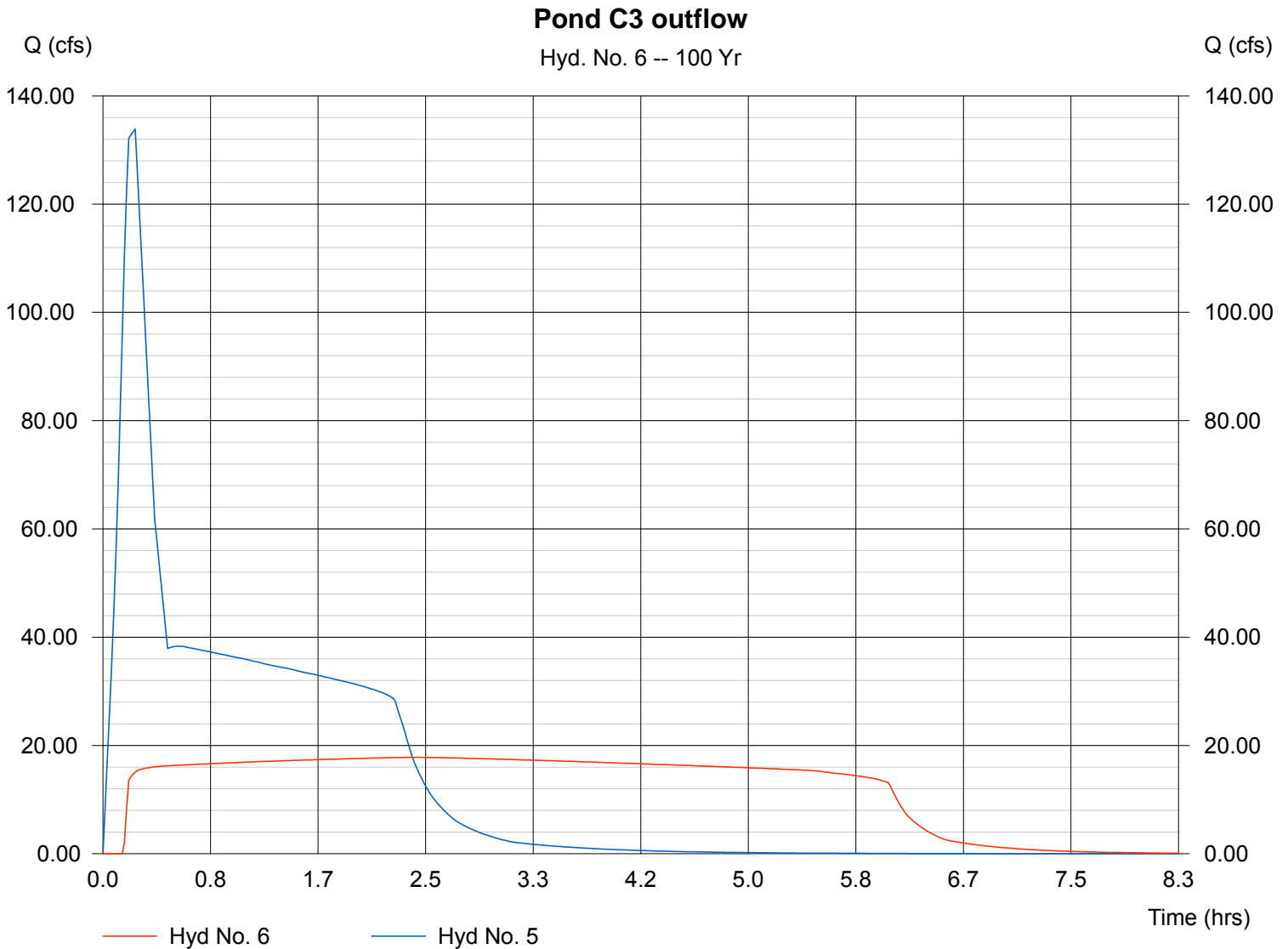
Pond C3 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 5
Reservoir name = Pond C3

Peak discharge = 17.79 cfs
Time interval = 1 min
Max. Elevation = 5763.93 ft
Max. Storage = 275,851 cuft

Storage Indication method used. Wet pond routing start elevation = 5759.50 ft.

Hydrograph Volume = 367,493 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

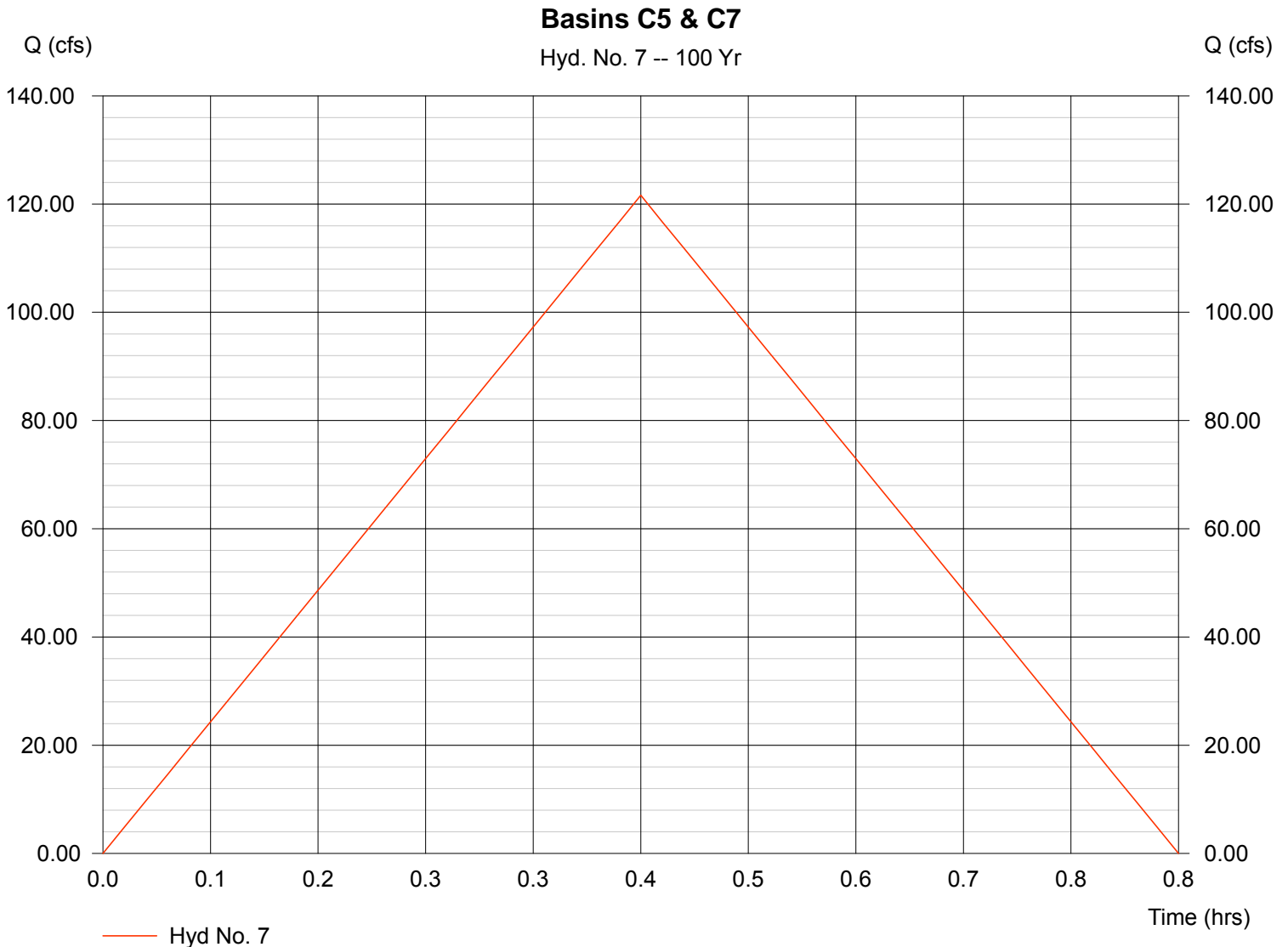
Hyd. No. 7

Basins C5 & C7

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 40.000 ac
Intensity = 4.678 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 121.62 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 25.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 182,430 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

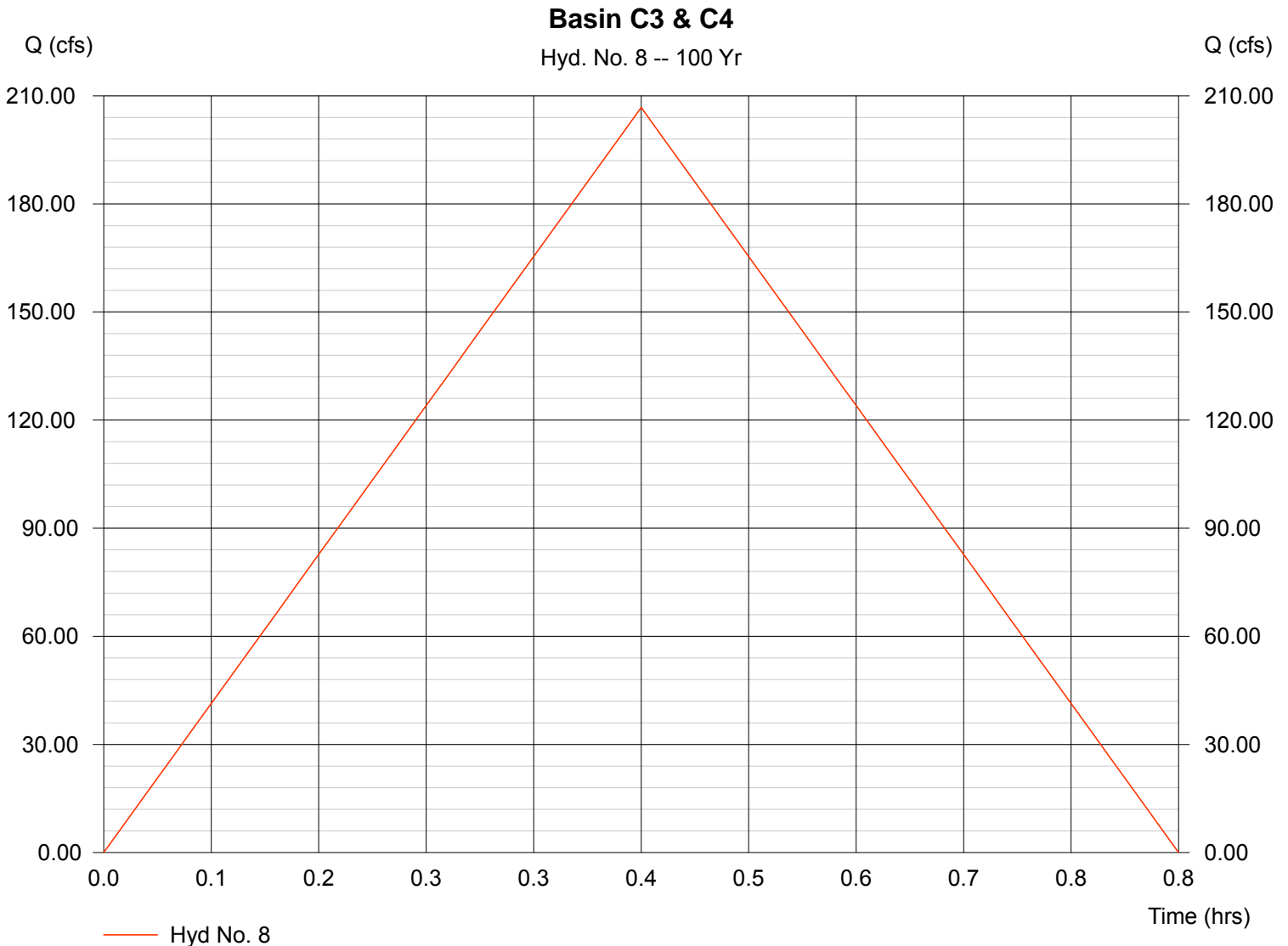
Hyd. No. 8

Basin C3 & C4

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 68.000 ac
Intensity = 4.678 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 206.75 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 25.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 310,131 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 9

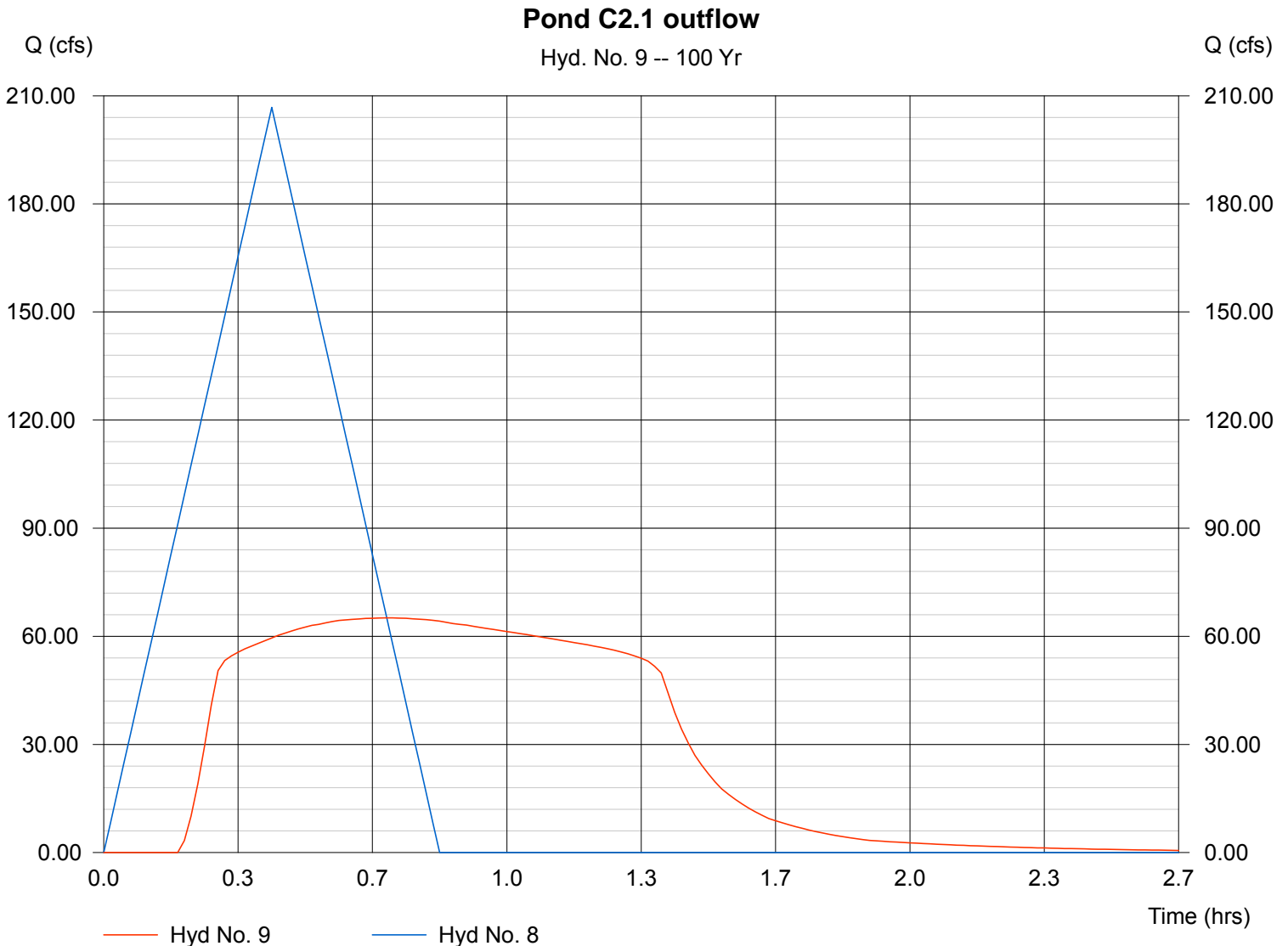
Pond C2.1 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 8
Reservoir name = Pond C2.1

Peak discharge = 65.13 cfs
Time interval = 1 min
Max. Elevation = 5773.91 ft
Max. Storage = 363,096 cuft

Storage Indication method used. Wet pond routing start elevation = 5770.40 ft.

Hydrograph Volume = 279,789 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

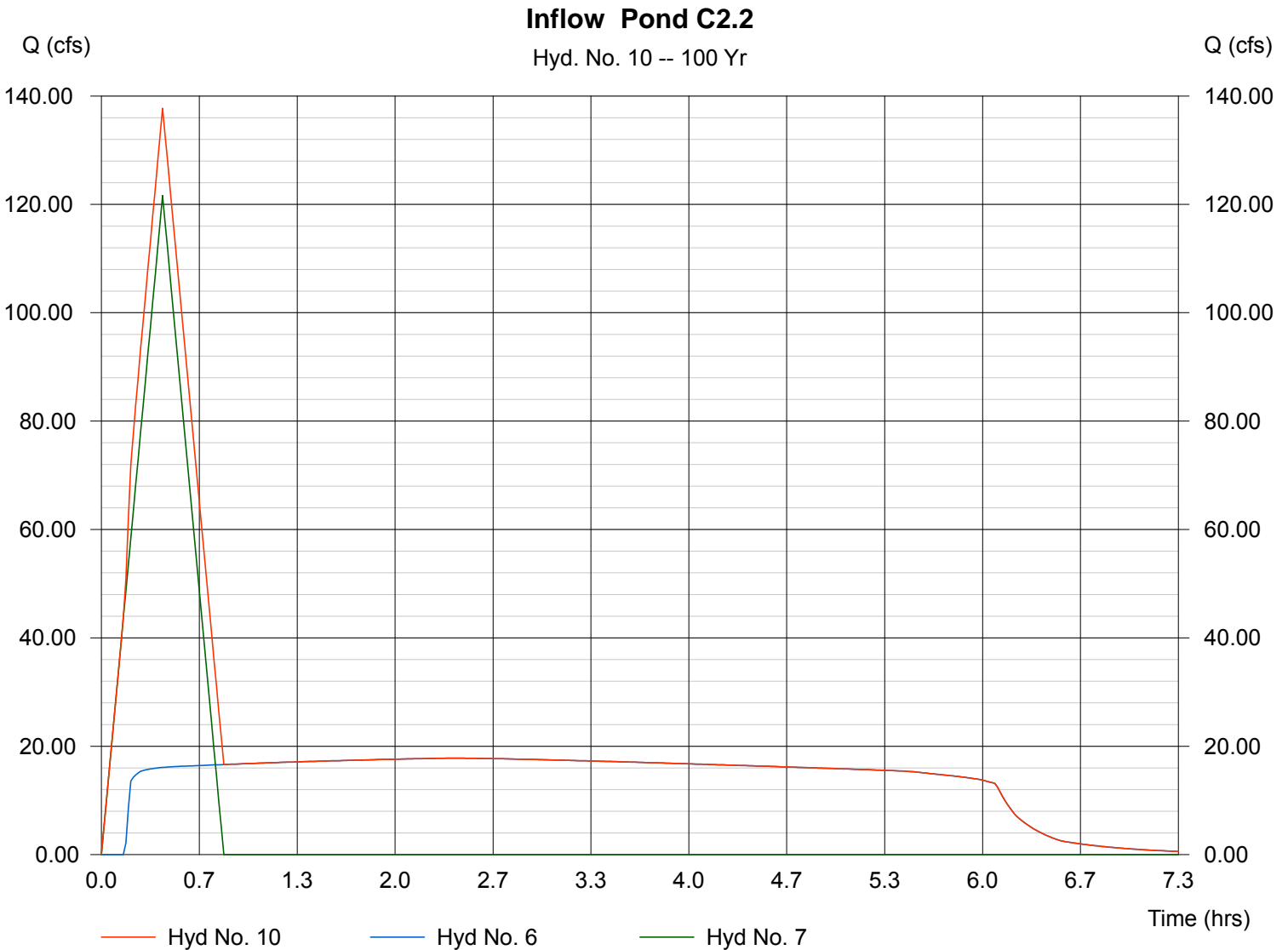
Hyd. No. 10

Inflow Pond C2.2

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 6, 7

Peak discharge = 137.71 cfs
Time interval = 1 min

Hydrograph Volume = 549,923 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 11

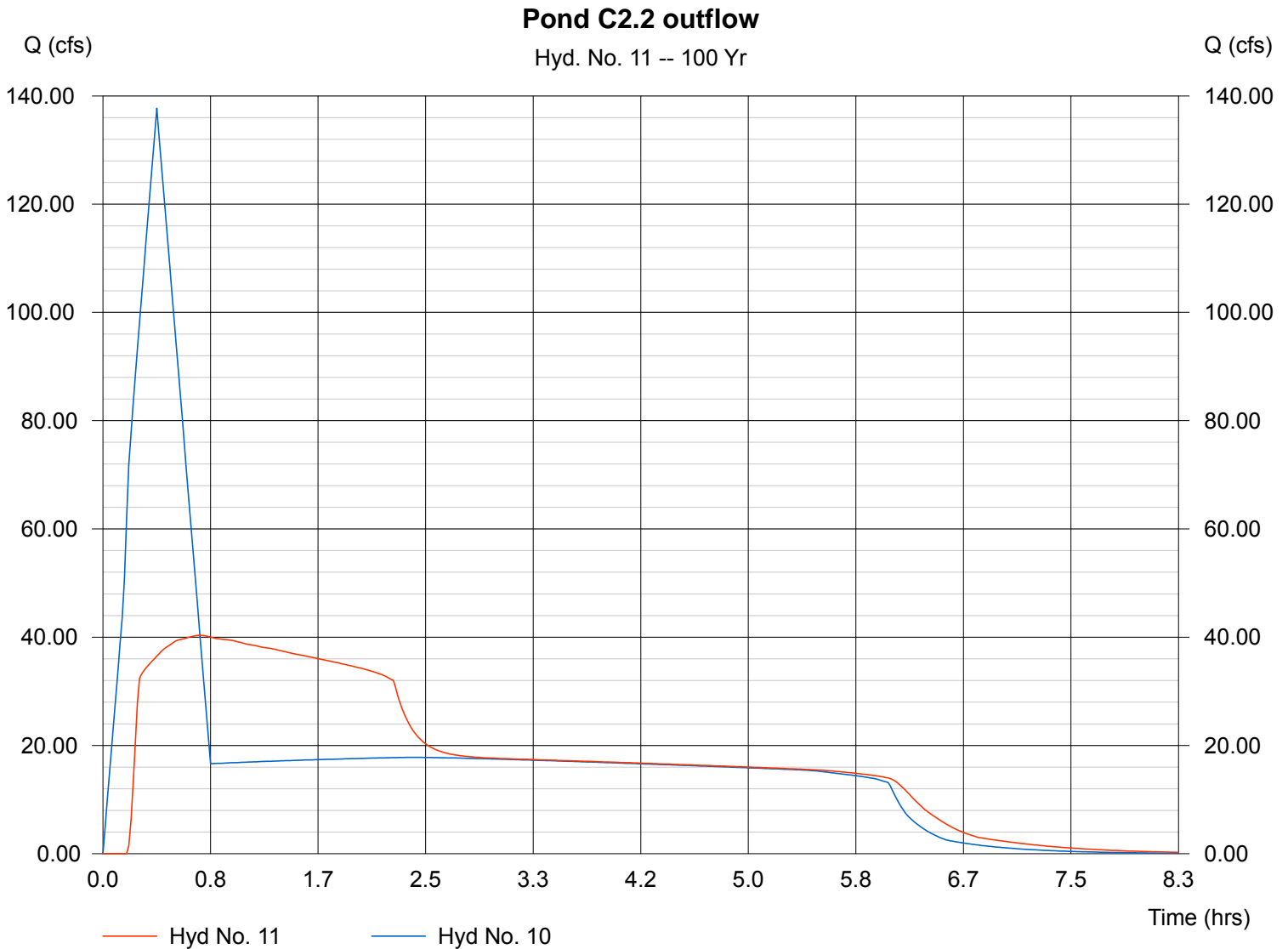
Pond C2.2 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 10
Reservoir name = Pond C2.2

Peak discharge = 40.34 cfs
Time interval = 1 min
Max. Elevation = 5753.55 ft
Max. Storage = 278,207 cuft

Storage Indication method used. Wet pond routing start elevation = 5750.30 ft.

Hydrograph Volume = 530,339 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

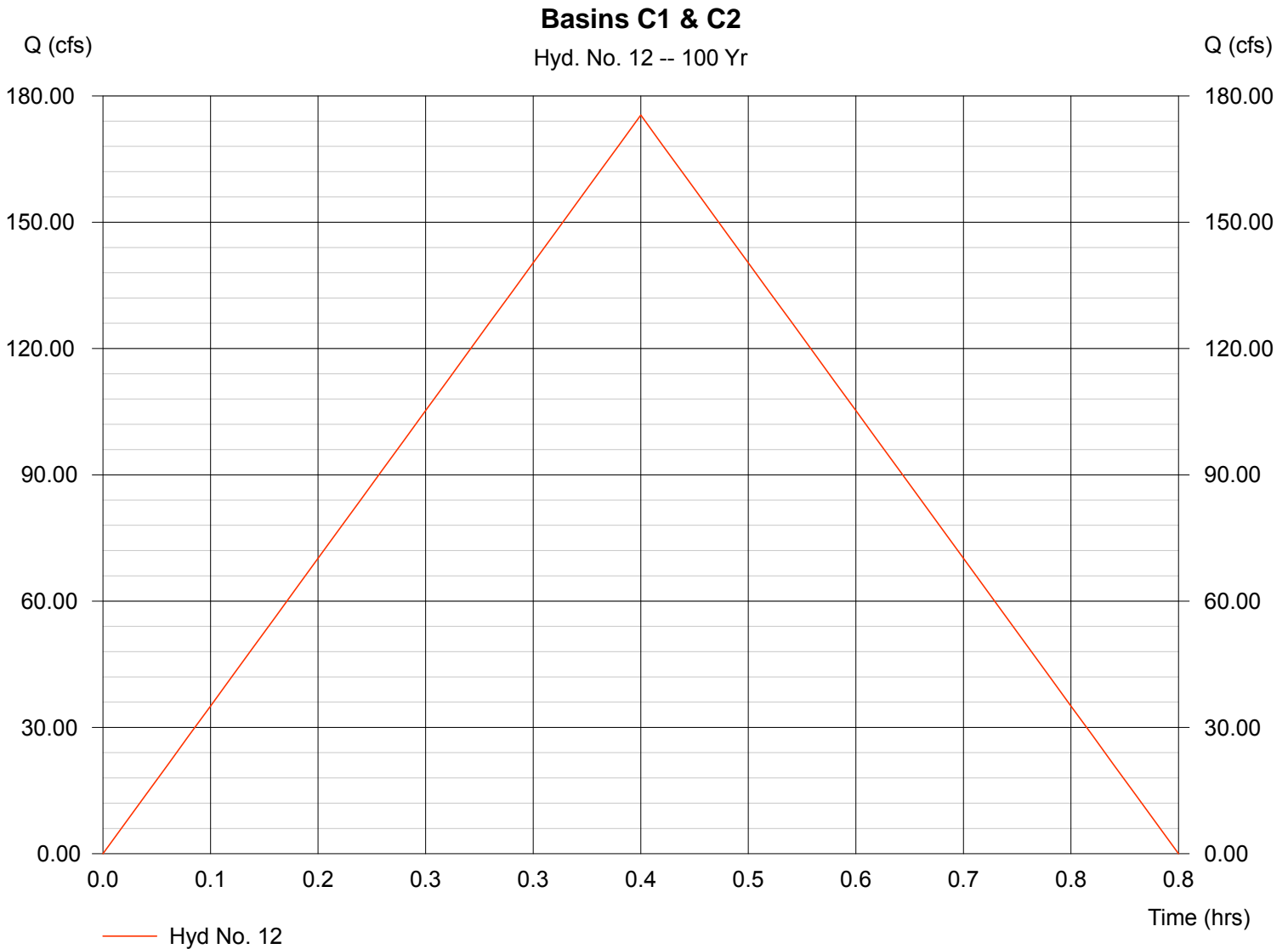
Hyd. No. 12

Basins C1 & C2

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 57.700 ac
Intensity = 4.678 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 175.44 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 25.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 263,155 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 13

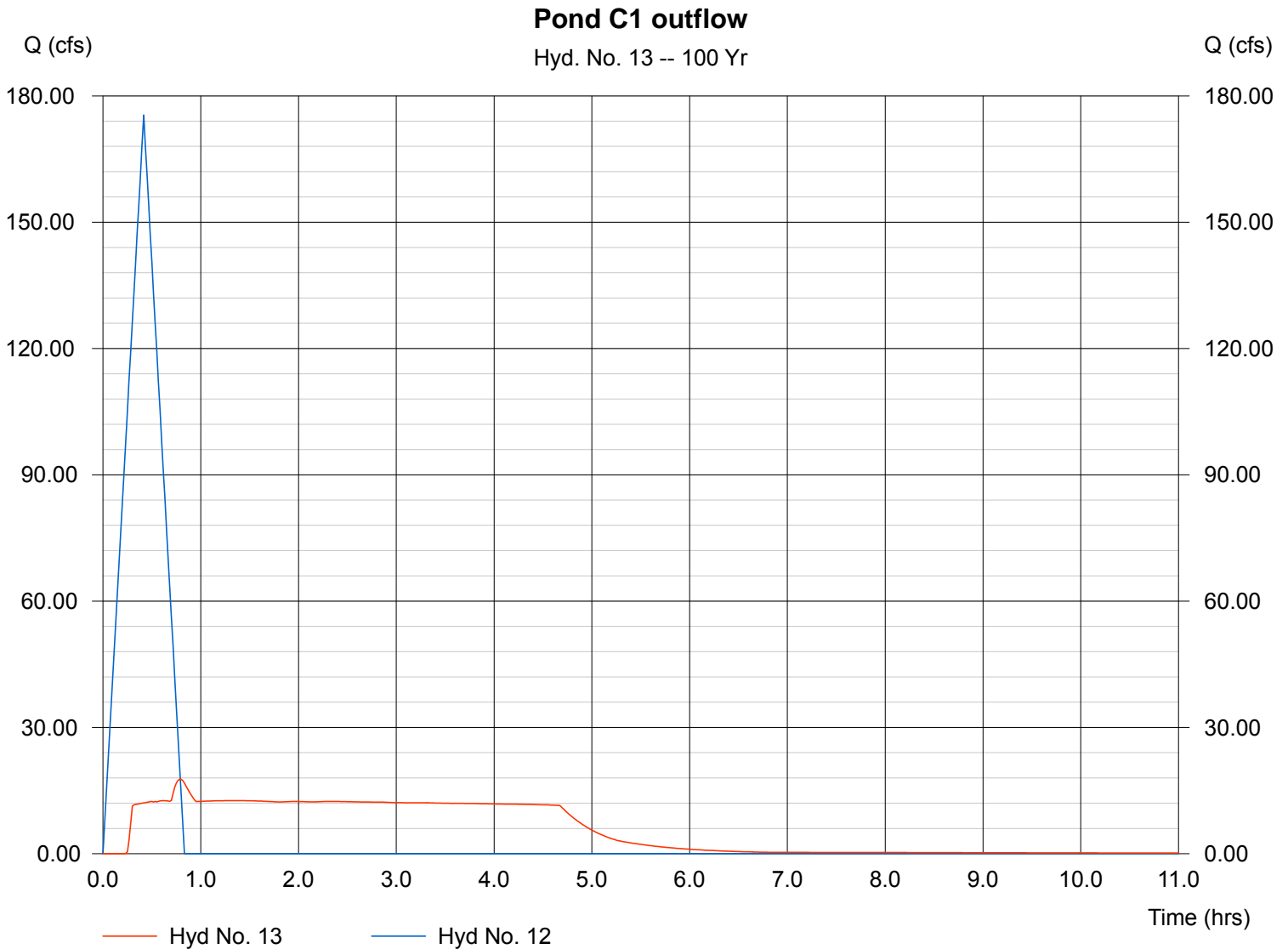
Pond C1 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 12
Reservoir name = Pond C1

Peak discharge = 17.68 cfs
Time interval = 1 min
Max. Elevation = 5753.09 ft
Max. Storage = 445,161 cuft

Storage Indication method used. Wet pond routing start elevation = 5749.80 ft.

Hydrograph Volume = 222,974 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

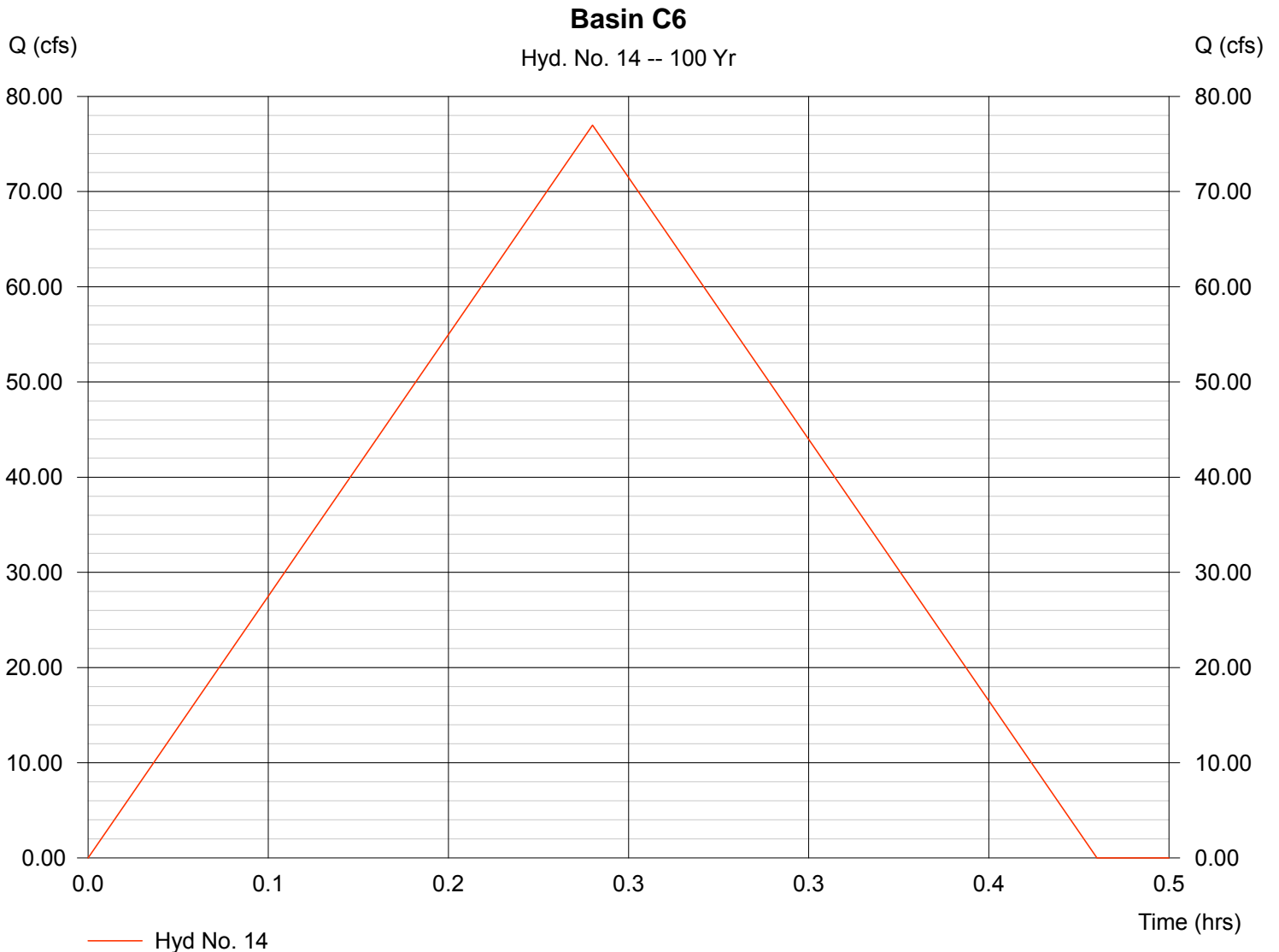
Hyd. No. 14

Basin C6

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 18.700 ac
Intensity = 6.333 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 76.98 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 14.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 64,659 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

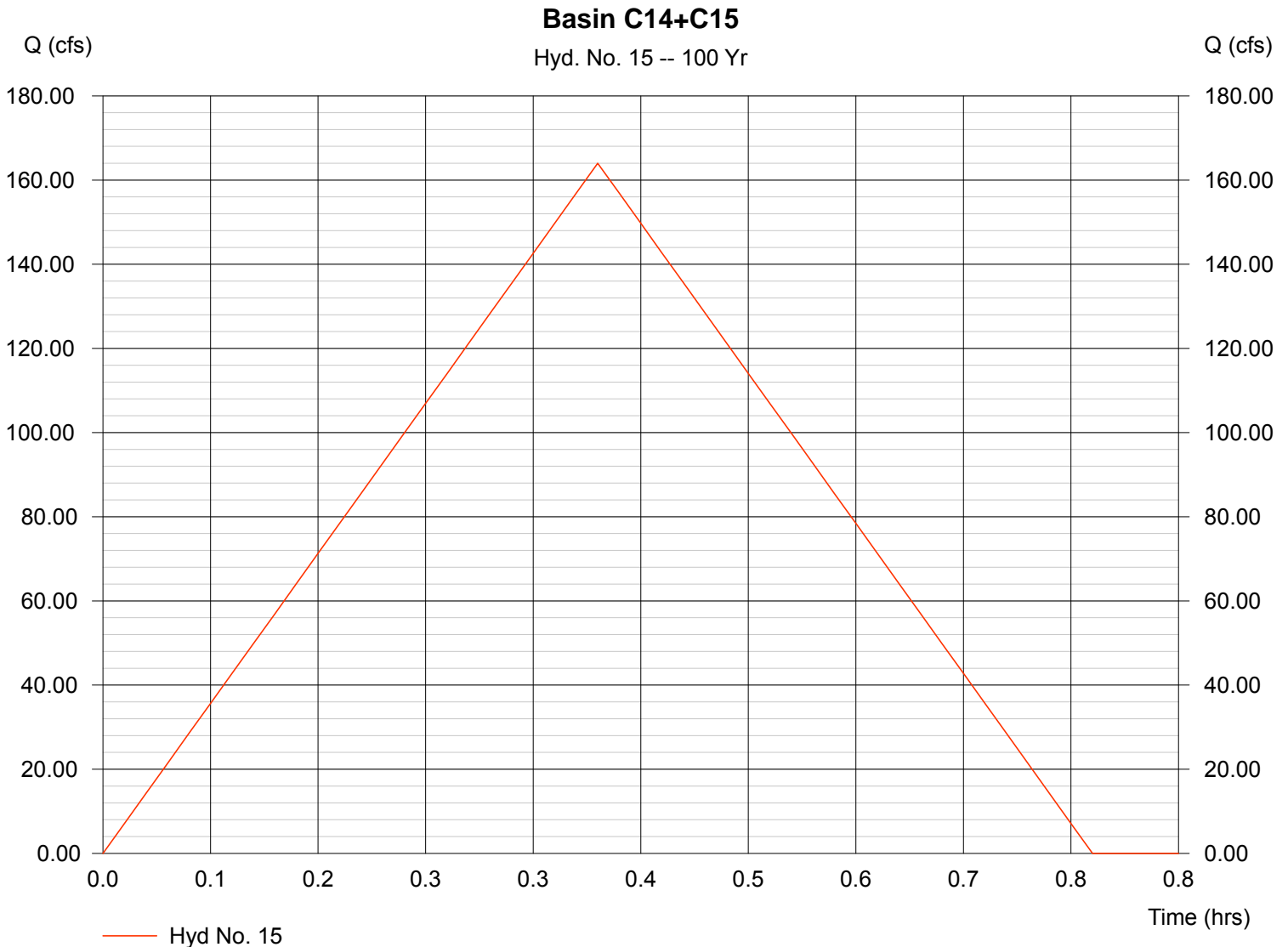
Hyd. No. 15

Basin C14+C15

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 51.300 ac
Intensity = 4.918 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 163.99 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 23.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 226,299 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

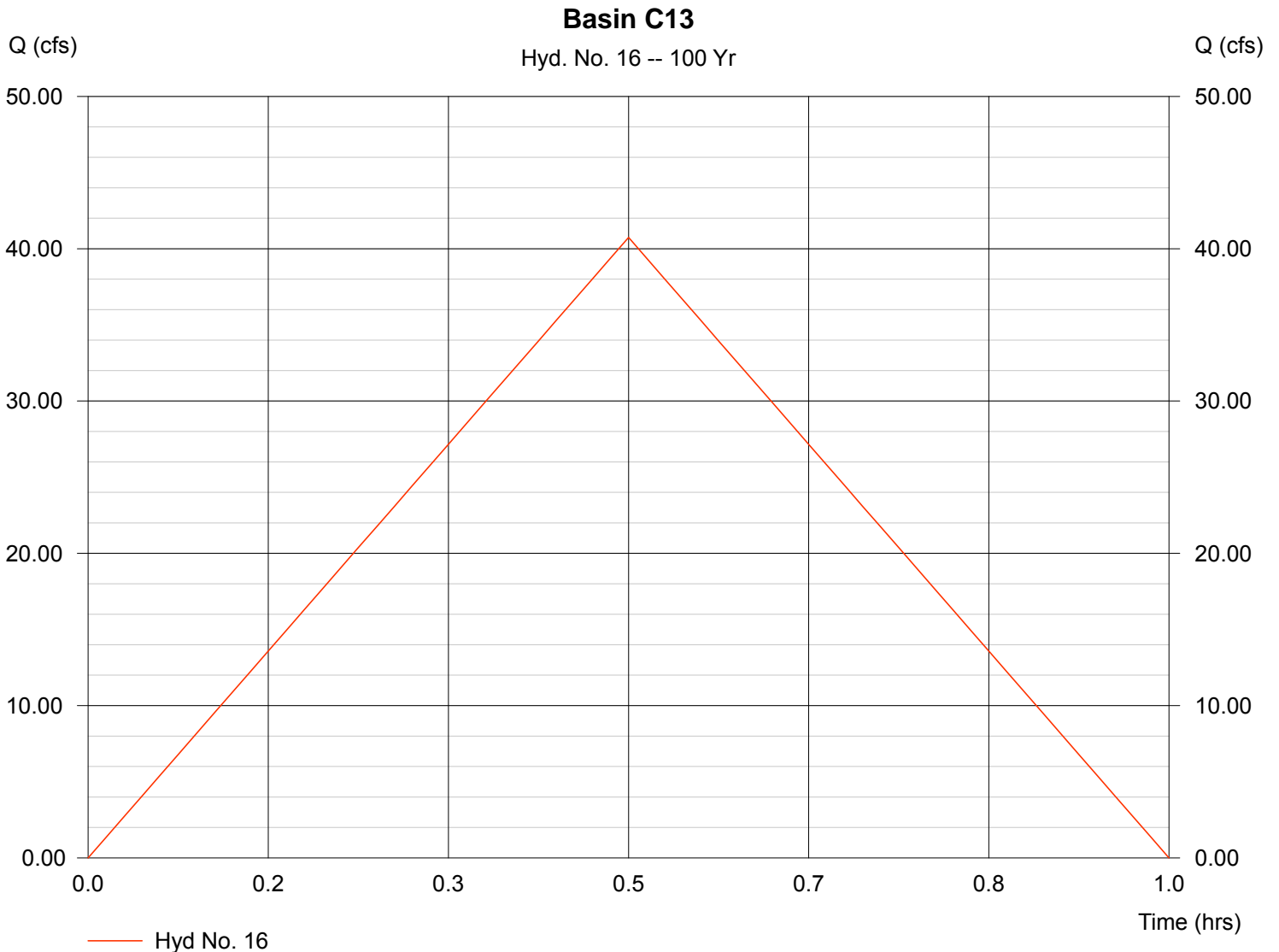
Hyd. No. 16

Basin C13

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 19.200 ac
Intensity = 4.160 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 40.73 cfs
Time interval = 1 min
Runoff coeff. = 0.51
Tc by User = 30.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 73,322 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

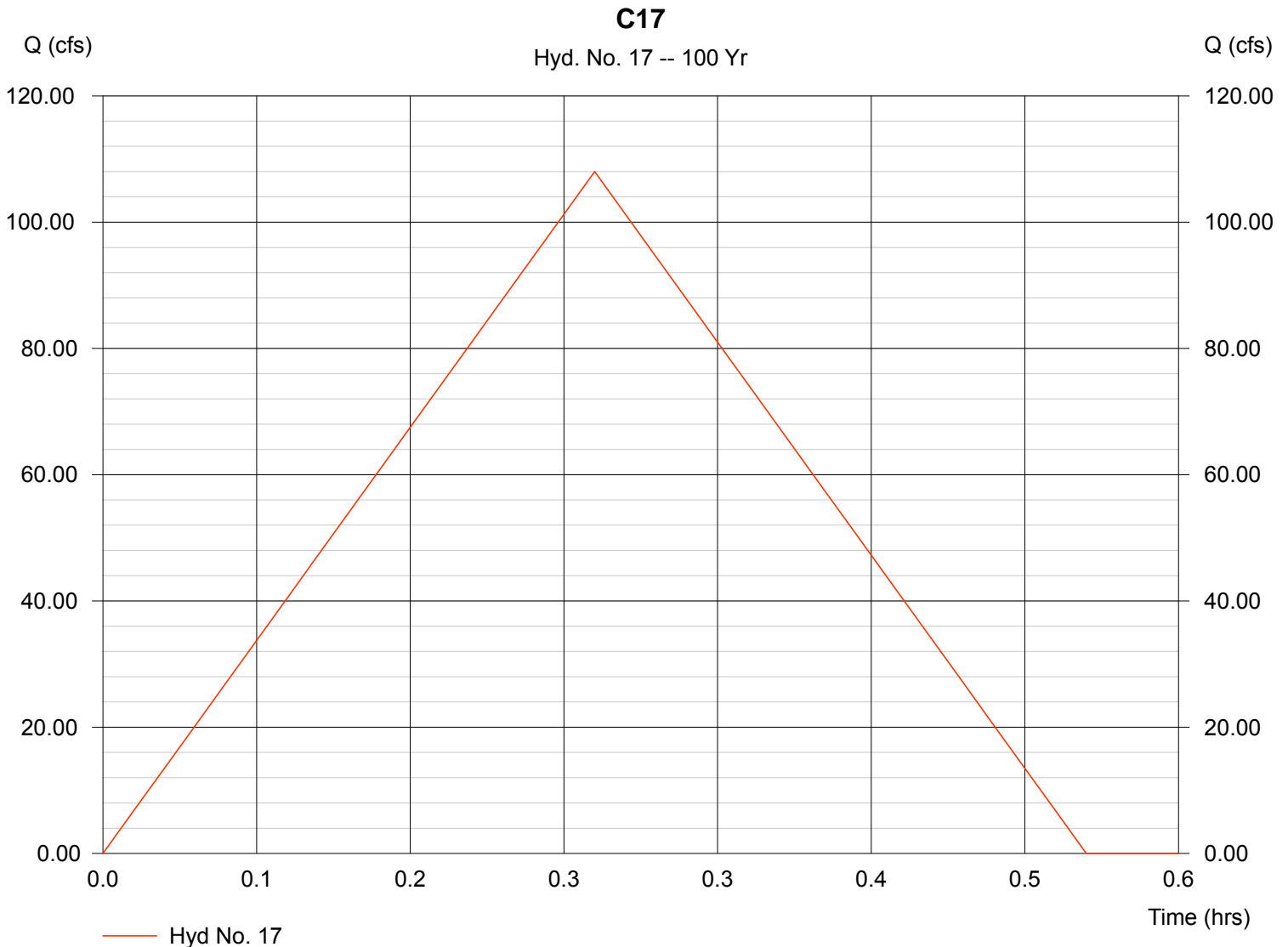
Hyd. No. 17

C17

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 30.200 ac
Intensity = 5.960 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 108.00 cfs
Time interval = 1 min
Runoff coeff. = 0.6
Tc by User = 16.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 103,681 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

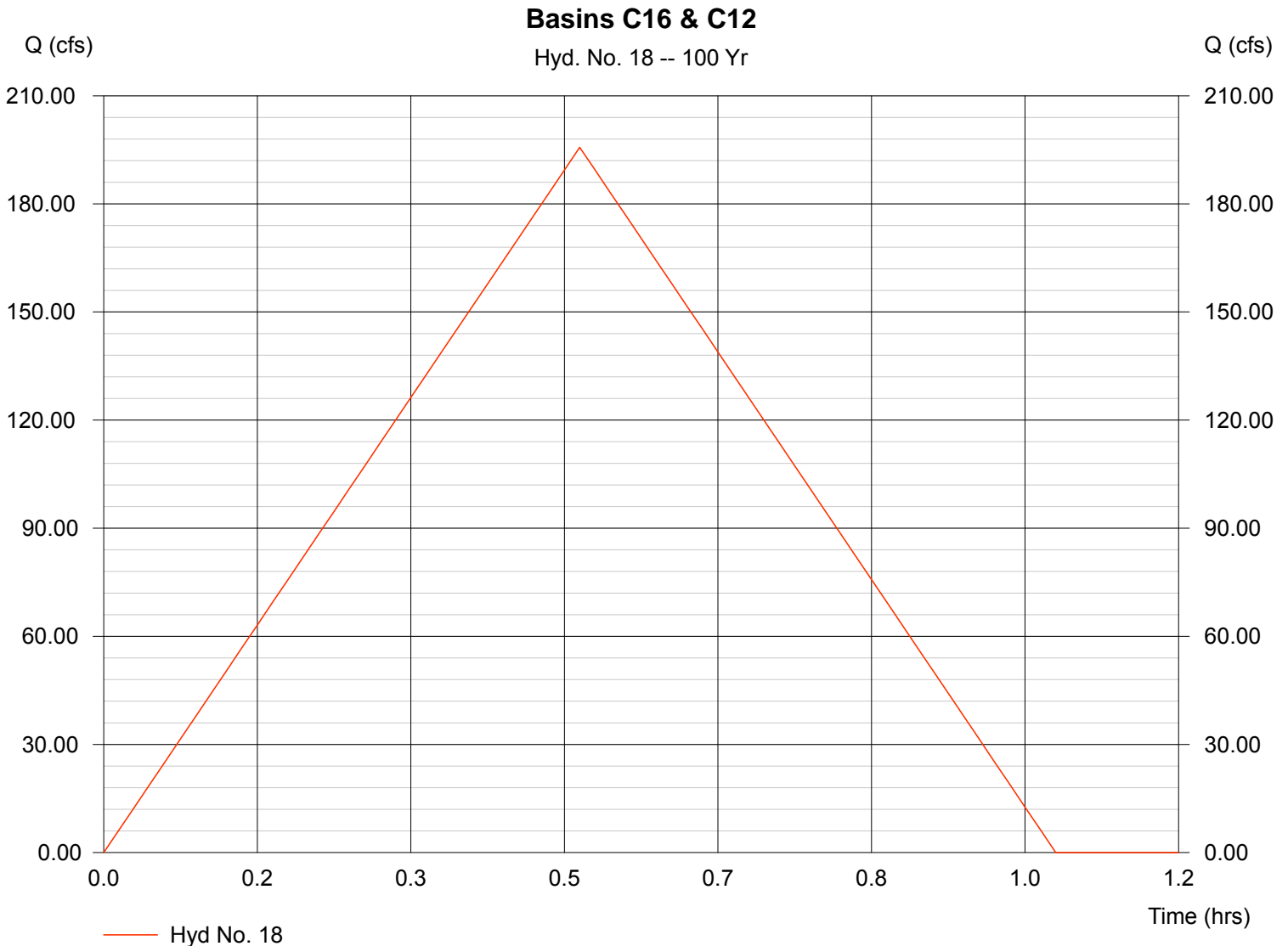
Hyd. No. 18

Basins C16 & C12

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 74.000 ac
Intensity = 4.069 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 195.70 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 31.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 363,995 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

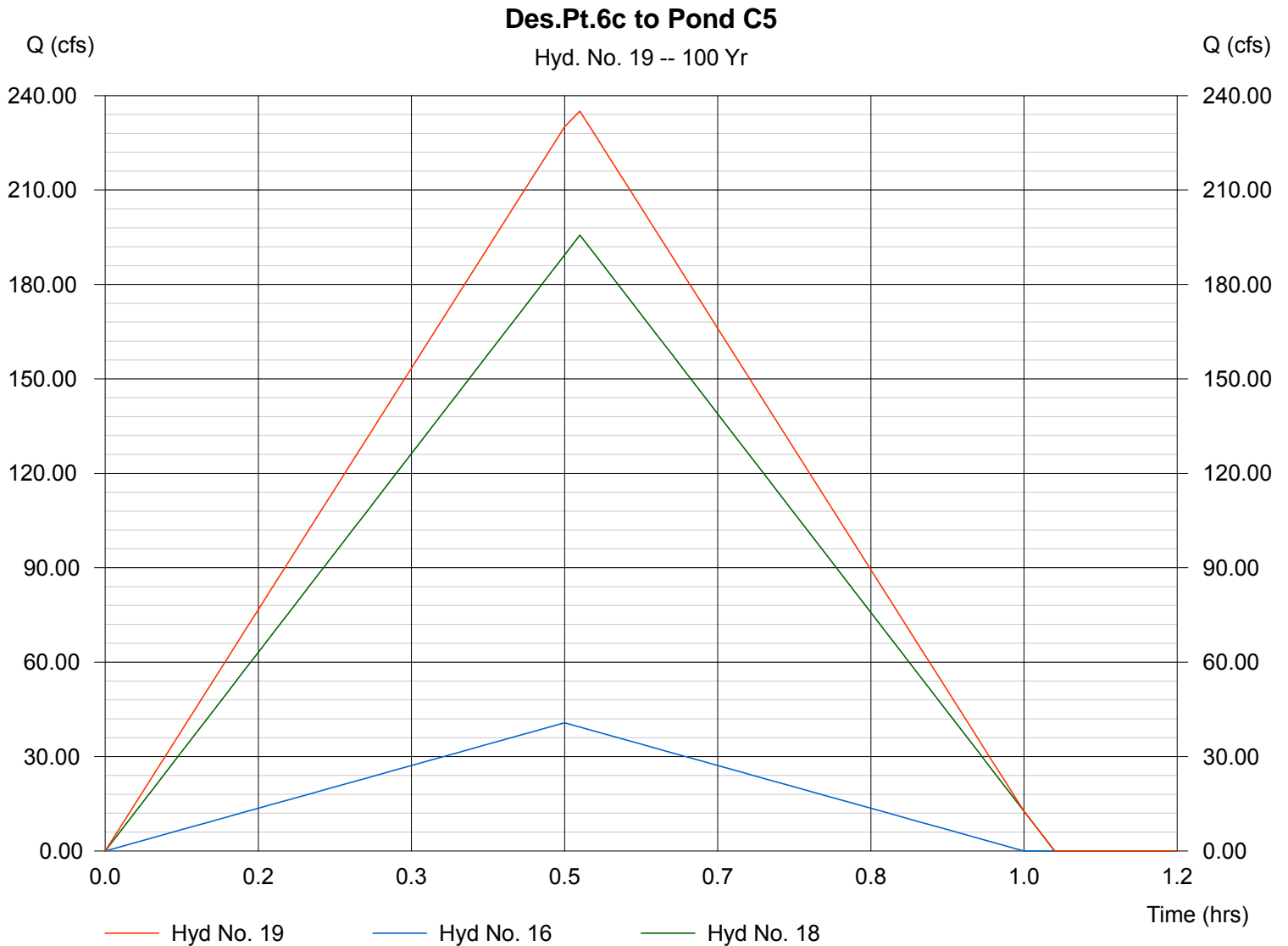
Hyd. No. 19

Des.Pt.6c to Pond C5

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 16, 18

Peak discharge = 235.07 cfs
Time interval = 1 min

Hydrograph Volume = 437,317 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

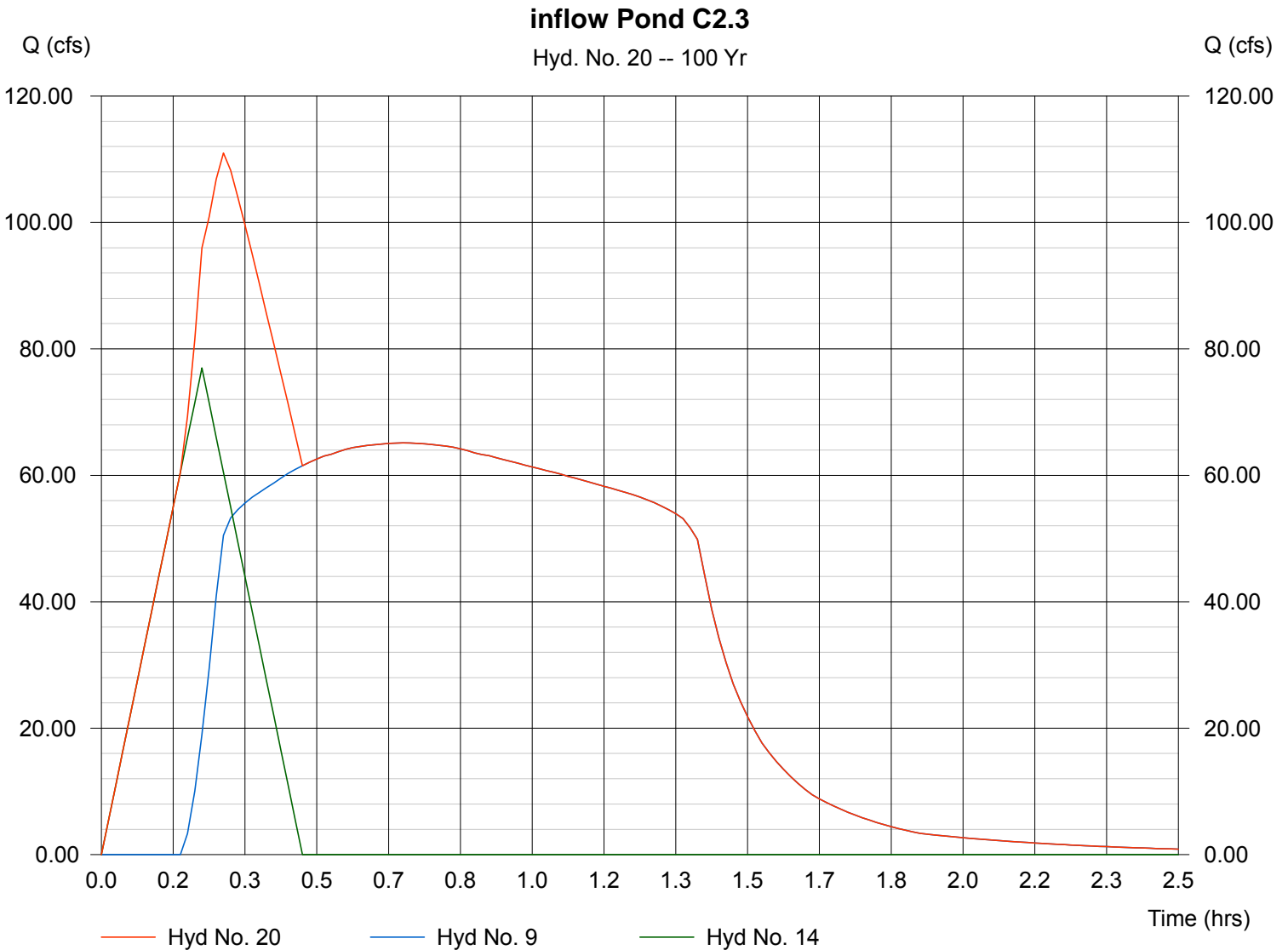
Hyd. No. 20

inflow Pond C2.3

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 9, 14

Peak discharge = 110.99 cfs
Time interval = 1 min

Hydrograph Volume = 344,448 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

Hyd. No. 21

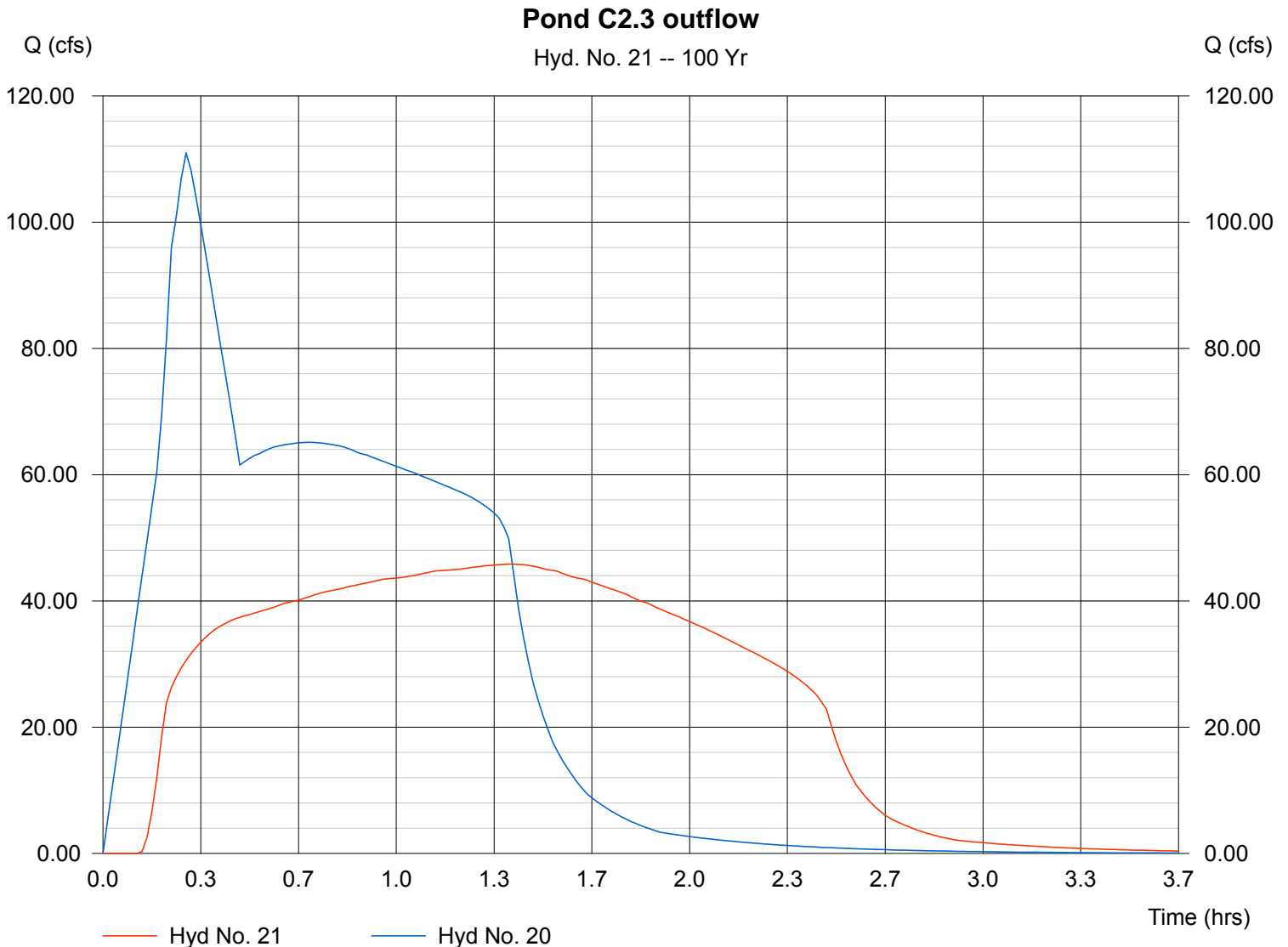
Pond C2.3 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 20
Reservoir name = Pond C2.3

Peak discharge = 45.83 cfs
Time interval = 1 min
Max. Elevation = 5753.06 ft
Max. Storage = 188,378 cuft

Storage Indication method used. Wet pond routing start elevation = 5748.60 ft.

Hydrograph Volume = 334,262 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

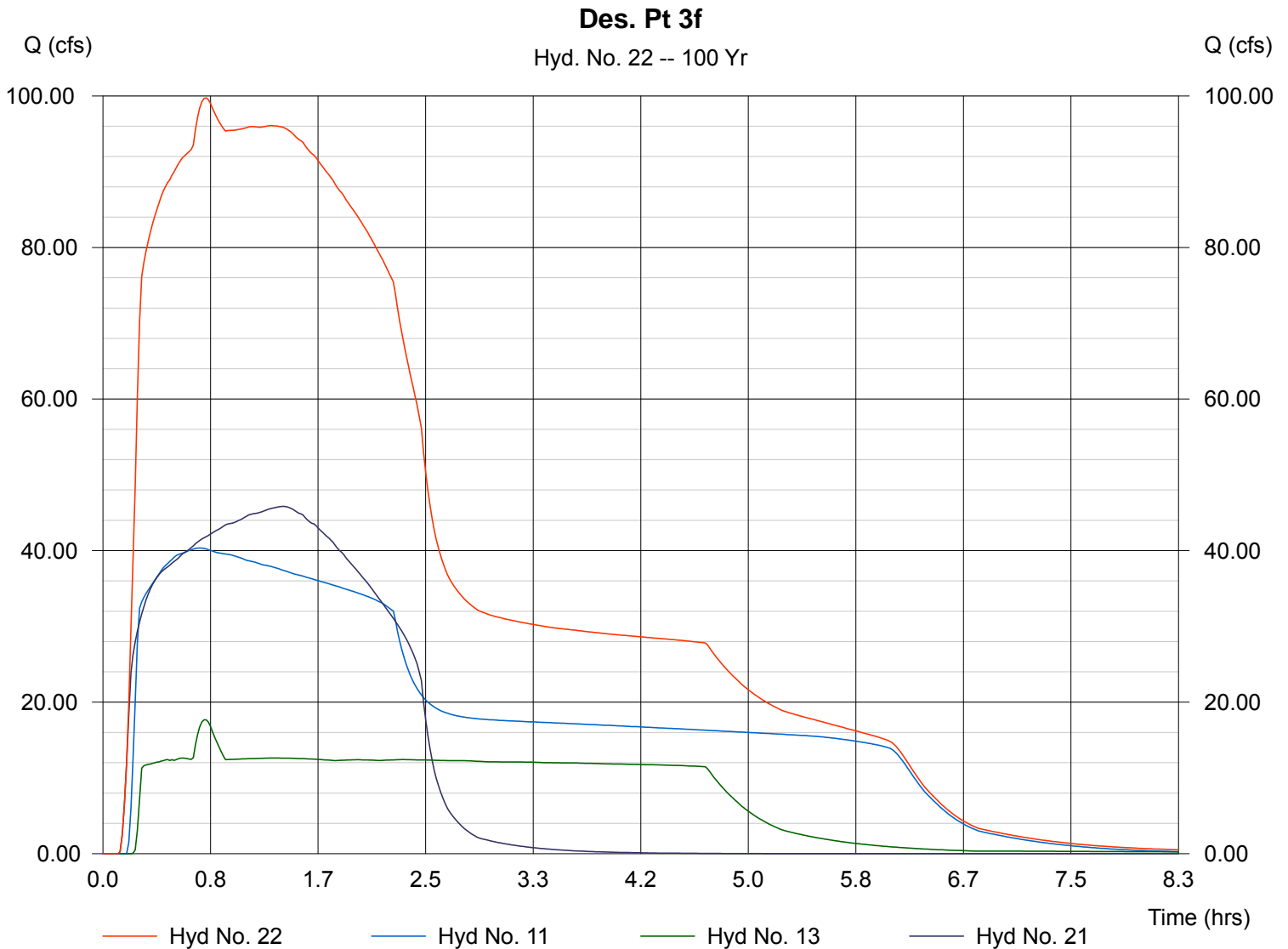
Hyd. No. 22

Des. Pt 3f

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 11, 13, 21

Peak discharge = 99.75 cfs
Time interval = 1 min

Hydrograph Volume = 1,087,511 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Friday, May 19 2017, 6:32 AM

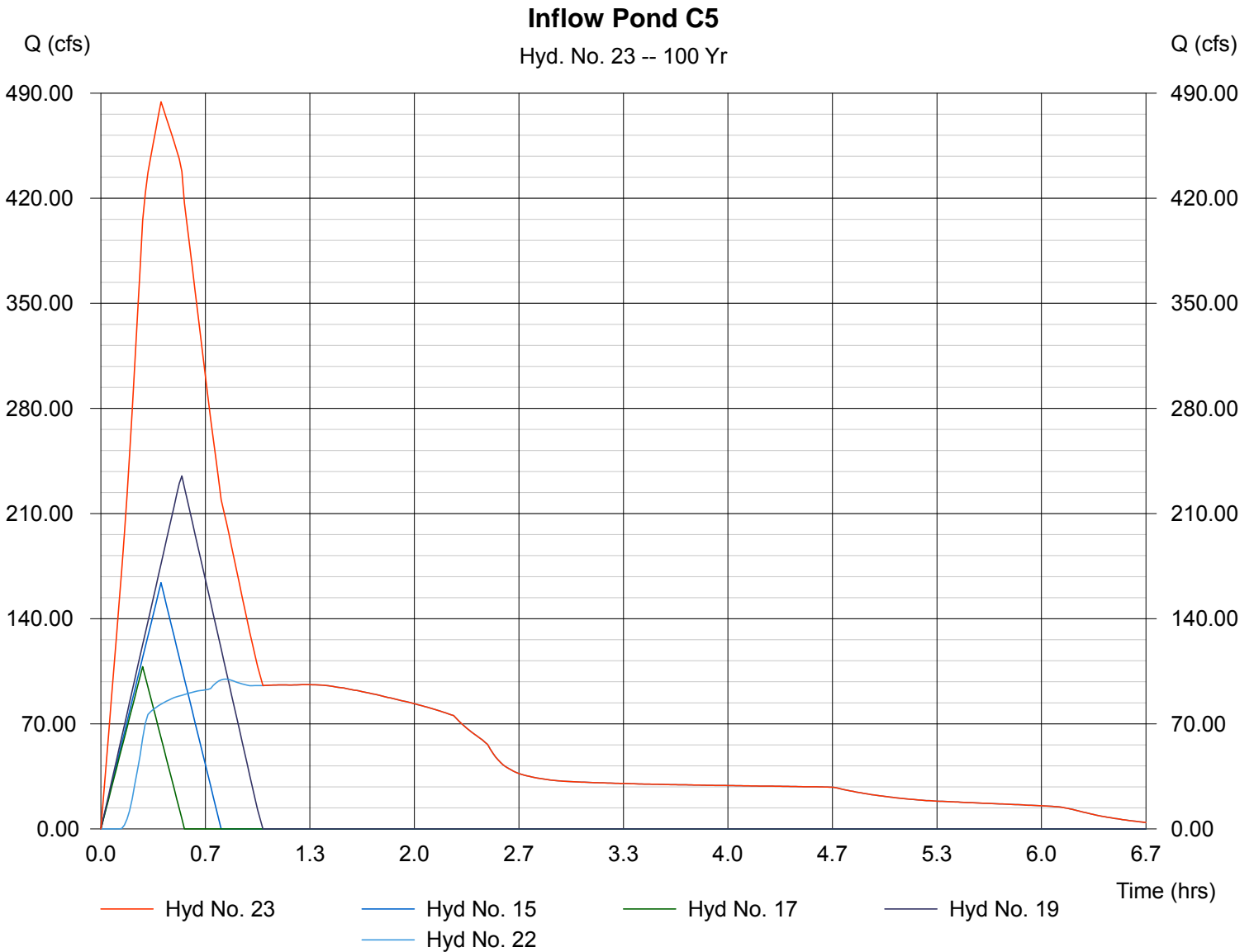
Hyd. No. 23

Inflow Pond C5

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 15, 17, 19, 22

Peak discharge = 484.24 cfs
Time interval = 1 min

Hydrograph Volume = 1,854,809 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Tuesday, May 23 2017, 7:33 AM

Hyd. No. 24

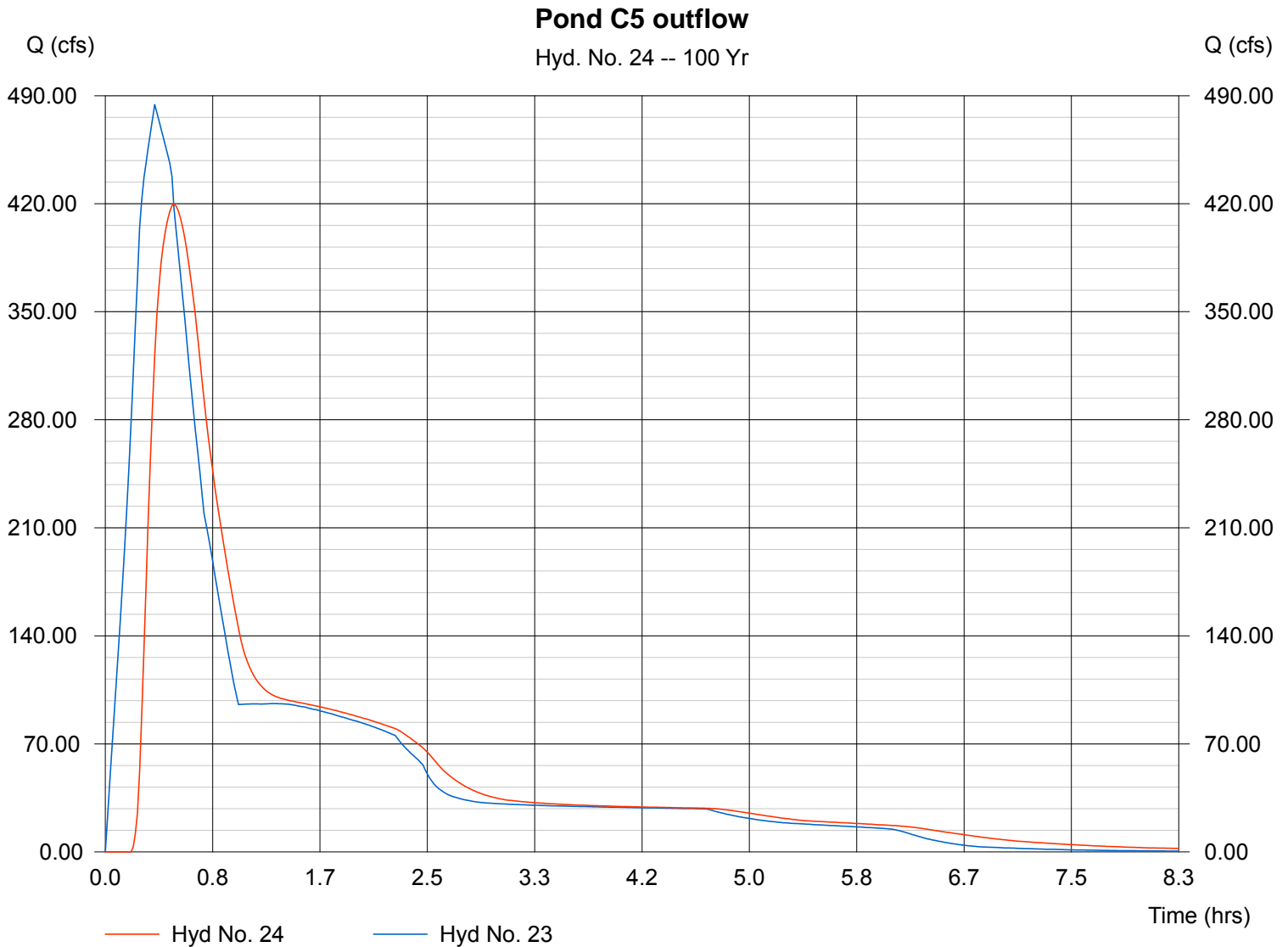
Pond C5 outflow

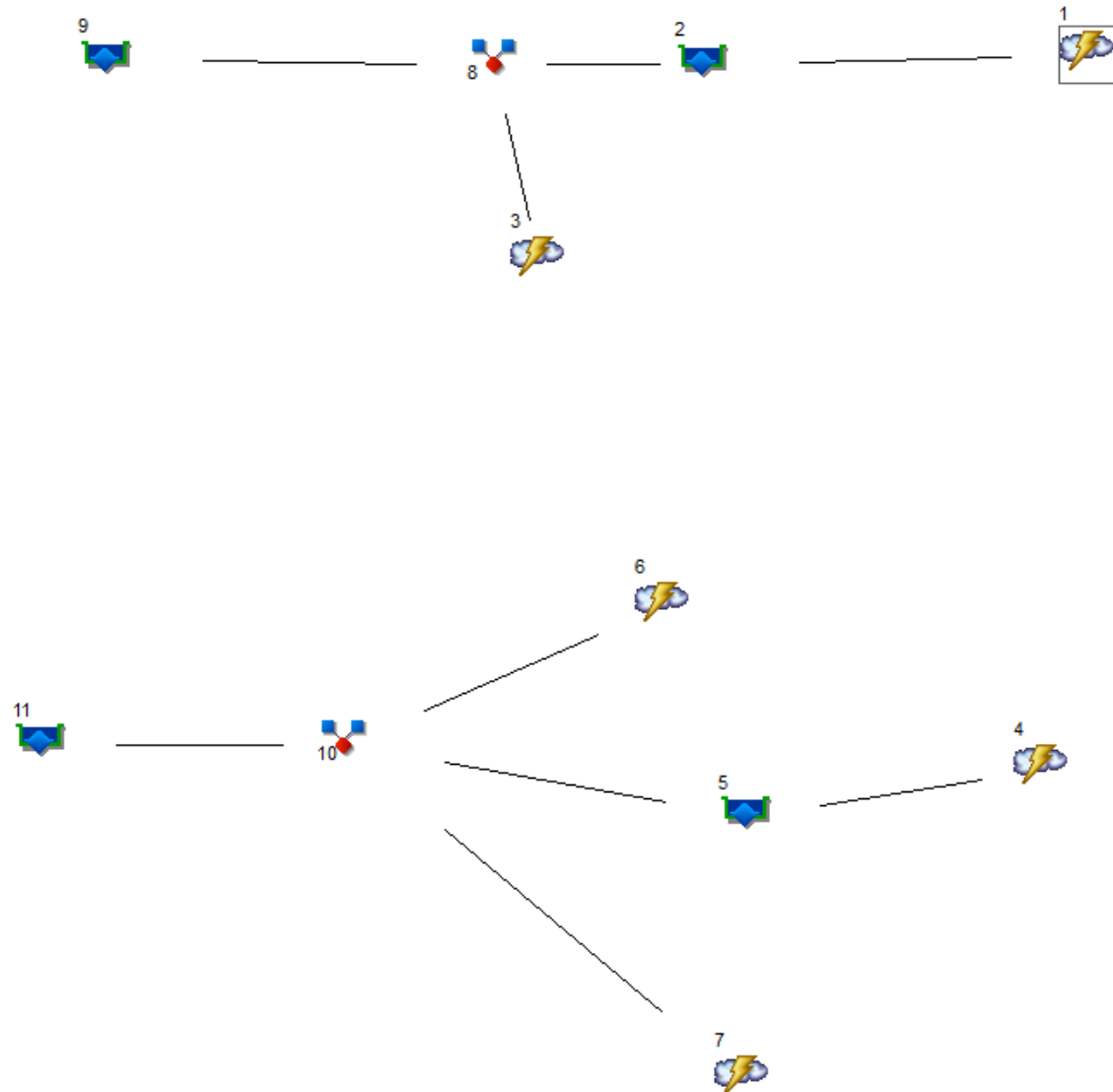
Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 23
Reservoir name = Pond C5

Peak discharge = 419.90 cfs
Time interval = 1 min
Max. Elevation = 5714.32 ft
Max. Storage = 677,645 cuft

Storage Indication method used. Wet pond routing start elevation = 5711.80 ft.

Hydrograph Volume = 1,757,155 cuft





Legend

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	Rational	Basin D1
2	Reservoir	Pond D1 outflow
3	Rational	Basin D2-D5
4	Rational	Pond E1 Inflow
5	Reservoir	Pond E1 Outflow
6	Rational	Basin E6-E8
7	Rational	Basin E9-E11
8	Combine	Pond D2 Inflow
9	Reservoir	Pond D2 Outflow
10	Combine	Pond E2 Inflow
11	Reservoir	Pond E2 Outflow

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	Rational	33.48	1	12	36,160	---	-----	-----	Basin D1
2	Reservoir	1.915	1	35	3,207	1	5754.62	54,571	Pond D1 outflow
3	Rational	106.13	1	22	210,141	---	-----	-----	Basin D2-D5
4	Rational	97.18	1	15	87,458	---	-----	-----	Pond E1 Inflow
5	Reservoir	9.385	1	29	11,277	4	5734.22	157,054	Pond E1 Outflow
6	Rational	76.79	1	20	92,144	---	-----	-----	Basin E6-E8
7	Rational	119.99	1	22	158,384	---	-----	-----	Basin E9-E11
8	Combine	106.13	1	22	213,348	2, 3,	-----	-----	Pond D2 Inflow
9	Reservoir	31.20	1	53	81,085	8	5700.07	244,557	Pond D2 Outflow
10	Combine	189.10	1	22	261,805	5, 6, 7,	-----	-----	Pond E2 Inflow
11	Reservoir	96.43	1	33	224,662	10	5698.66	259,062	Pond E2 Outflow

Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description	
1	Rational	74.60	1	12	80,573	---	-----	-----	Basin D1	
2	Reservoir	10.52	1	33	71,644	1	5756.78	108,212	Pond D1 outflow	
3	Rational	232.67	1	22	460,692	---	-----	-----	Basin D2-D5	
4	Rational	208.33	1	15	187,500	---	-----	-----	Pond E1 Inflow	
5	Reservoir	31.62	1	28	187,499	4	5737.32	293,609	Pond E1 Outflow	
6	Rational	165.73	1	20	198,882	---	-----	-----	Basin E6-E8	
7	Rational	242.50	1	22	320,099	---	-----	-----	Basin E9-E11	
8	Combine	242.93	1	22	532,337	2, 3,	-----	-----	Pond D2 Inflow	
9	Reservoir	131.19	1	43	508,771	8	5701.75	386,691	Pond D2 Outflow	
10	Combine	422.93	1	22	706,480	5, 6, 7,	-----	-----	Pond E2 Inflow	
11	Reservoir	257.97	1	31	669,336	10	5700.91	421,789	Pond E2 Outflow	
100-yr; D-E basins.gpw					Return Period: 100 Year			Monday, Jun 5 2017, 6:15 AM		

Pond Report

Pond No. 1 - Pond D1

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5751.00	00	0	0
1.00	5752.00	10,904	5,452	5,452
2.00	5753.00	19,275	15,090	20,542
3.00	5754.00	21,293	20,284	40,826
4.00	5755.00	23,346	22,320	63,145
5.00	5756.00	25,482	24,414	87,559
6.00	5757.00	27,711	26,597	114,156
7.00	5758.00	30,034	28,873	143,028
8.00	5759.00	32,451	31,243	174,271
9.00	5760.00	37,565	35,008	209,279
10.00	5761.00	40,000	38,783	248,061
11.00	5762.00	43,000	41,500	289,561

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 10.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5750.50	0.00	0.00	0.00
Length (ft)	= 140.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.013	.013
Orif. Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

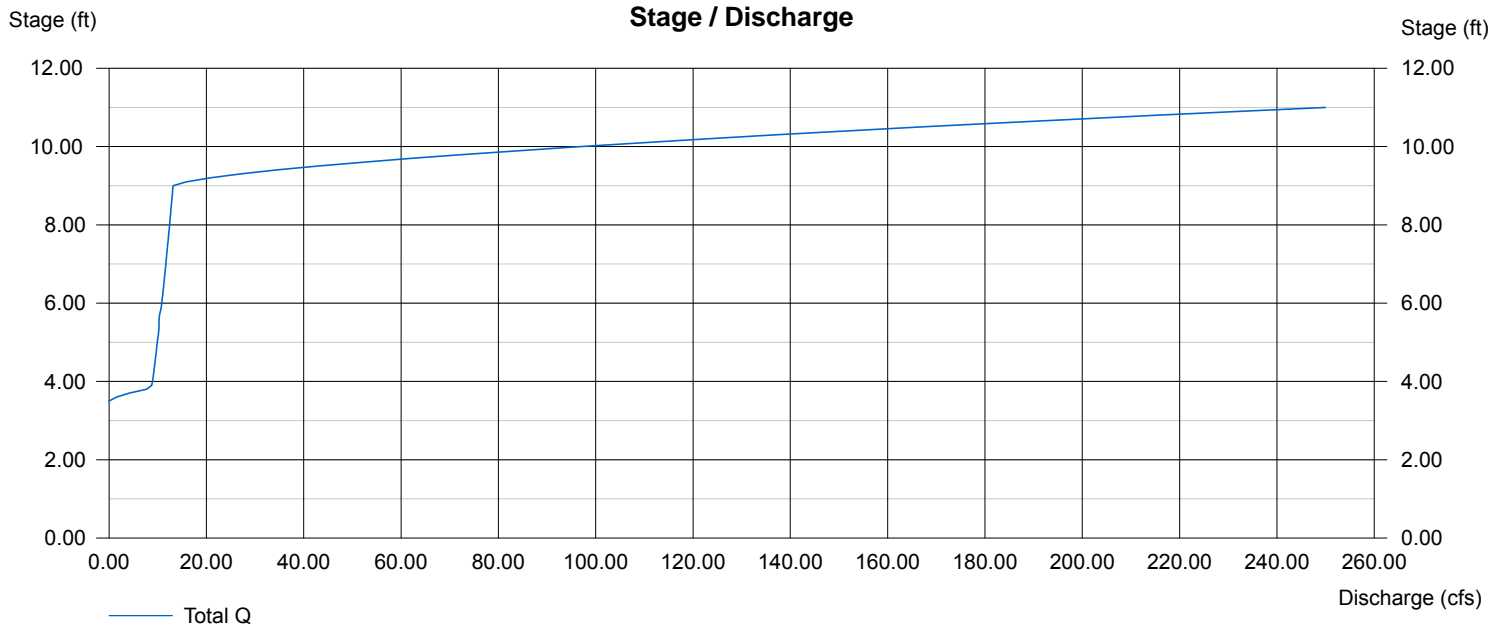
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 14.00	25.00	0.00	0.00
Crest El. (ft)	= 5754.50	5760.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



Pond Report

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

Pond No. 2 - Pond D2

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5696.00	1,068	0	0
1.00	5697.00	48,988	25,028	25,028
2.00	5698.00	72,821	60,905	85,933
3.00	5699.00	76,610	74,716	160,648
4.00	5700.00	80,490	78,550	239,198
5.00	5701.00	84,486	82,488	321,686
6.00	5702.00	88,582	86,534	408,220
7.00	5703.00	92,768	90,675	498,895
8.00	5704.00	97,074	94,921	593,816
9.00	5705.00	102,033	99,554	693,370
10.00	5706.00	106,000	104,017	797,386

Culvert / Orifice Structures

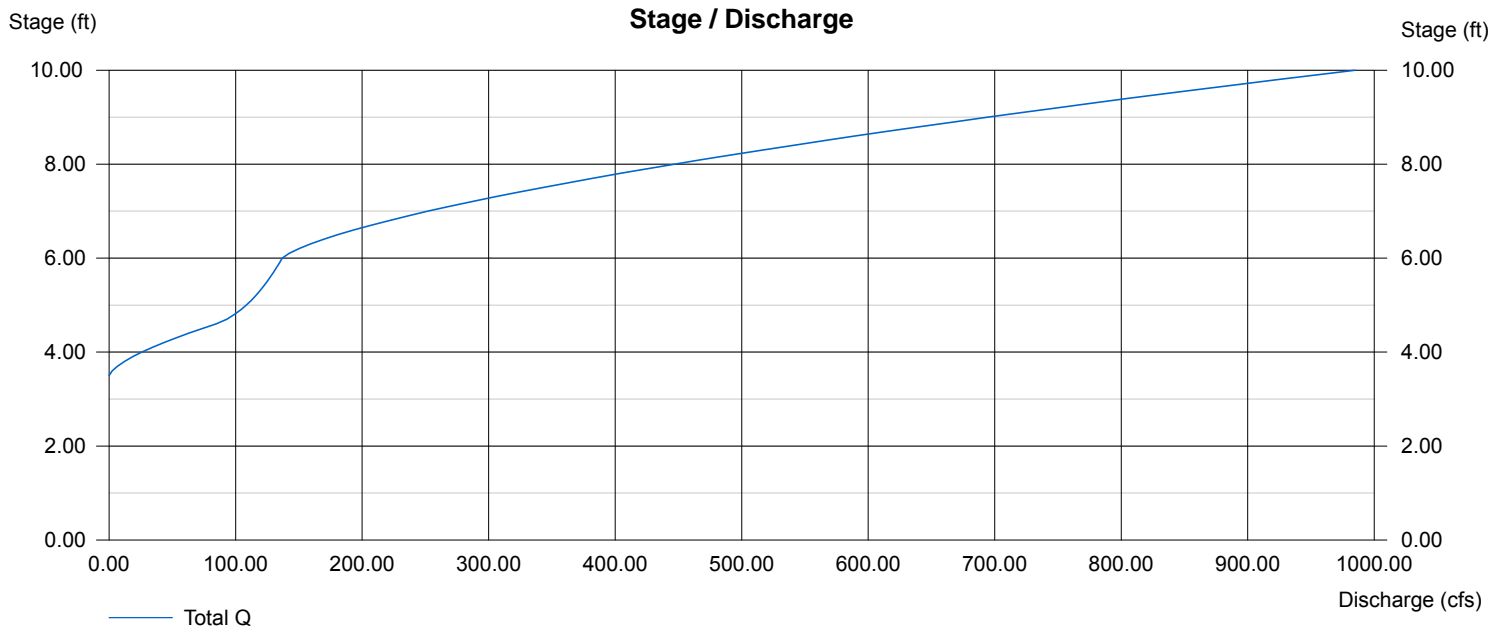
	[A]	[B]	[C]	[D]
Rise (in)	= 48.00	0.00	0.00	0.00
Span (in)	= 48.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5694.55	0.00	0.00	0.00
Length (ft)	= 110.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.013	.013
Orif. Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 22.00	30.00	0.00	0.00
Crest El. (ft)	= 5699.50	5702.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Pond Report

Pond No. 3 - Pond E1

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5729.00	2,550	0	0
1.00	5730.00	25,900	14,225	14,225
2.00	5731.00	31,341	28,621	42,846
3.00	5732.00	33,851	32,596	75,442
4.00	5733.00	36,442	35,147	110,588
5.00	5734.00	39,105	37,774	148,362
6.00	5735.00	41,838	40,472	188,833
7.00	5736.00	44,644	43,241	232,074
8.00	5737.00	47,527	46,086	278,160
9.00	5738.00	50,487	49,007	327,167
10.00	5739.00	52,120	51,304	378,470
11.00	5740.00	55,072	53,596	432,066

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 20.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5727.50	0.00	0.00	0.00
Length (ft)	= 400.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.000	.000
Orif. Coeff.	= 0.60	0.60	0.00	0.00
Multi-Stage	= n/a	No	No	No

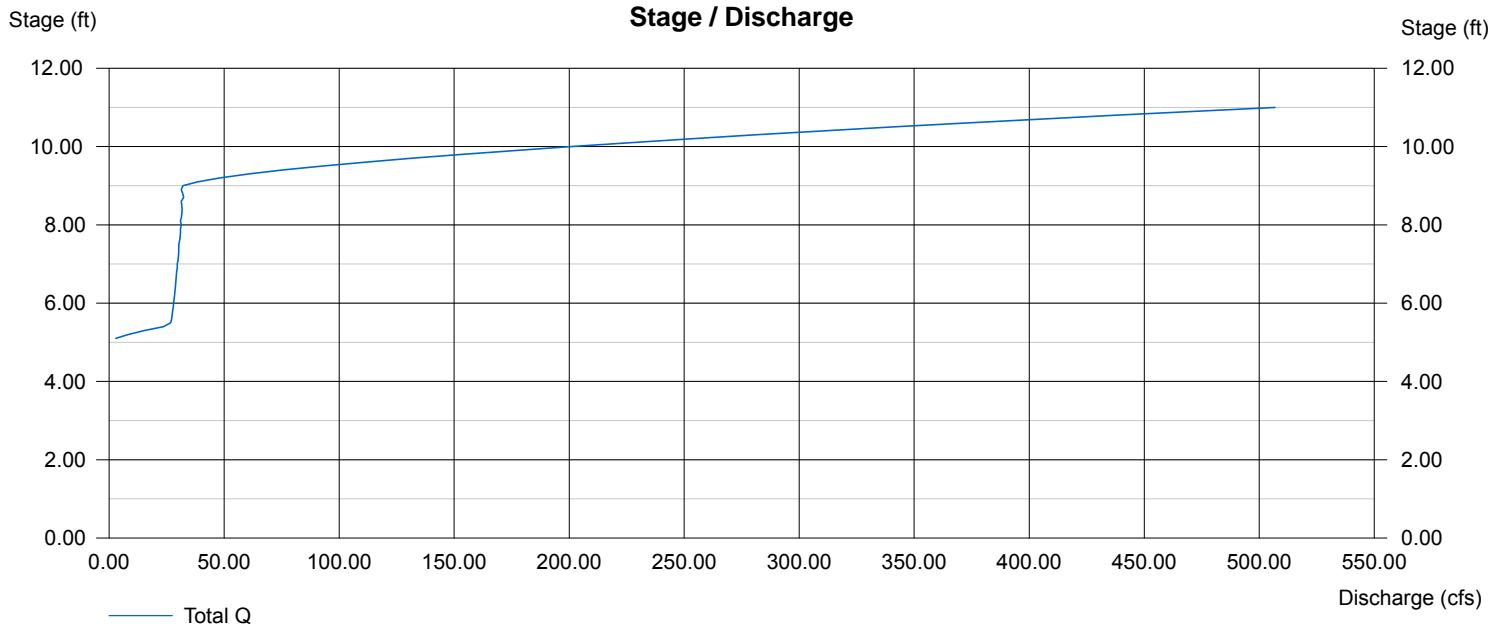
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 28.00	50.00	0.00	0.00
Crest El. (ft)	= 5734.00	5738.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



Pond Report

Pond No. 4 - Pond E2

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	5694.00	00	0	0
1.00	5695.00	57,500	28,750	28,750
2.00	5696.00	60,400	58,950	87,700
3.00	5697.00	63,400	61,900	149,600
4.00	5698.00	66,500	64,950	214,550
5.00	5699.00	69,700	68,100	282,650
6.00	5700.00	72,900	71,300	353,950
7.00	5701.00	76,300	74,600	428,550
8.00	5702.00	79,600	77,950	506,500

Culvert / Orifice Structures

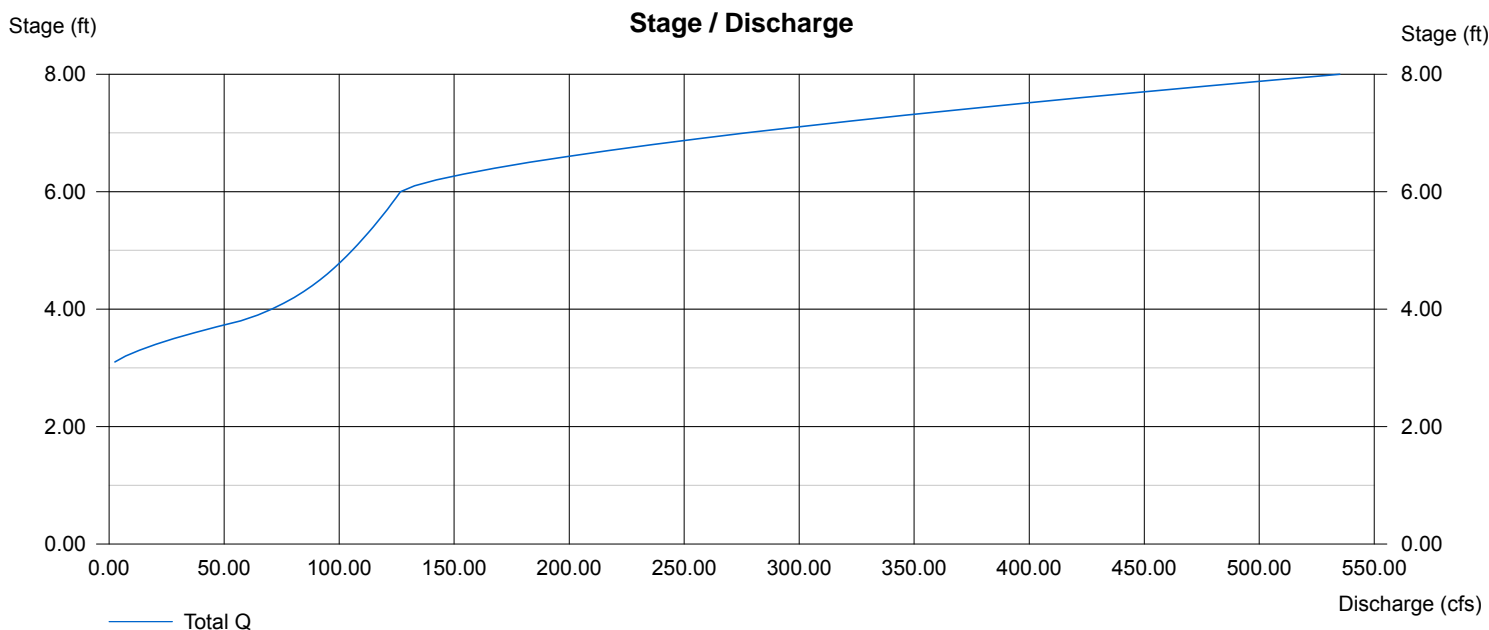
	[A]	[B]	[C]	[D]
Rise (in)	= 48.00	0.00	0.00	0.00
Span (in)	= 48.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 5693.10	0.00	0.00	0.00
Length (ft)	= 160.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	0.00
N-Value	= .013	.013	.013	.013
Orif. Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 24.00	40.00	0.00	0.00
Crest El. (ft)	= 5697.00	5700.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

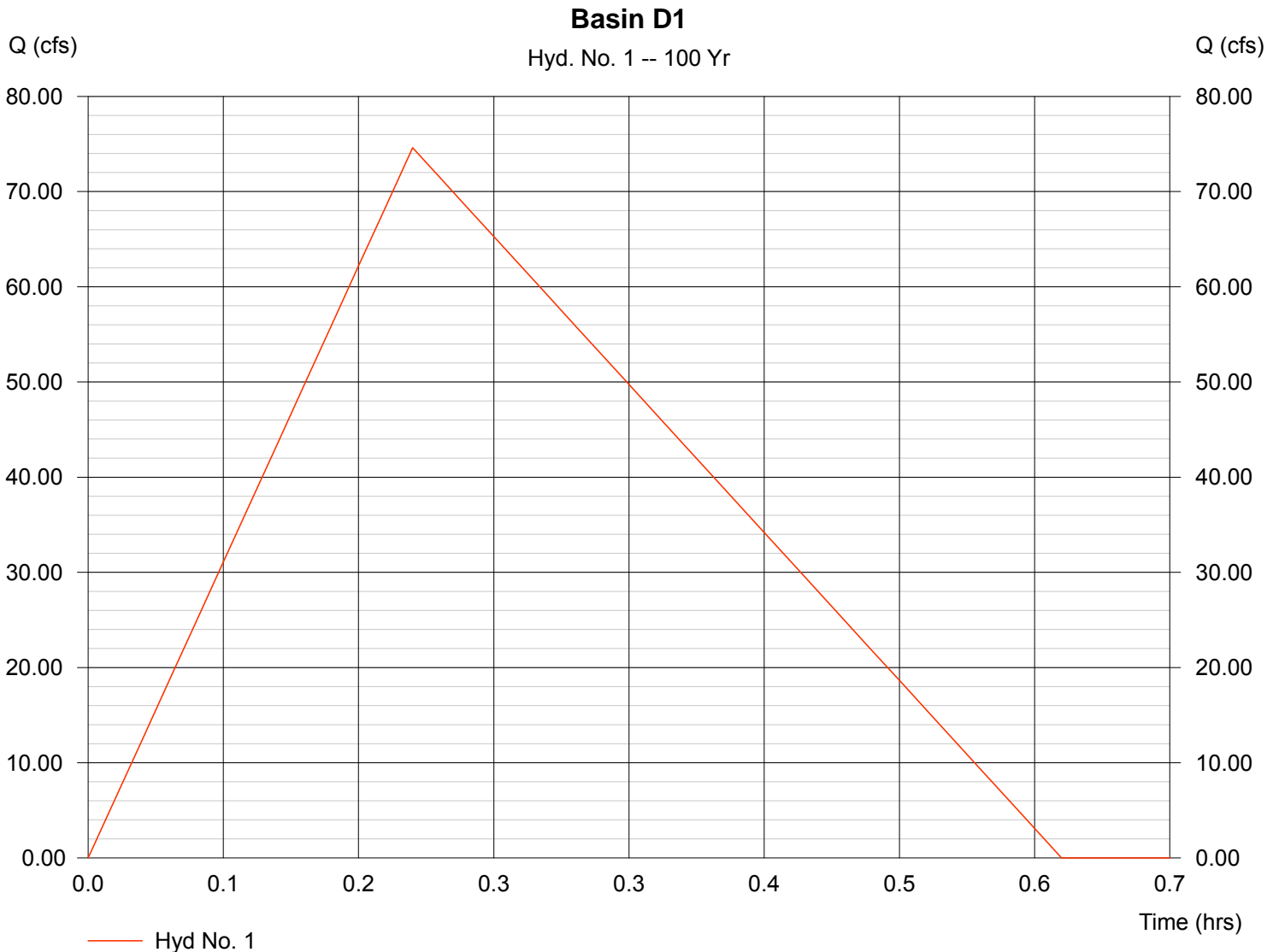
Hyd. No. 1

Basin D1

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 17.000 ac
Intensity = 6.752 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 74.60 cfs
Time interval = 1 min
Runoff coeff. = 0.65
Tc by User = 12.00 min
Asc/Rec limb fact = 1/2

Hydrograph Volume = 80,573 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

Hyd. No. 2

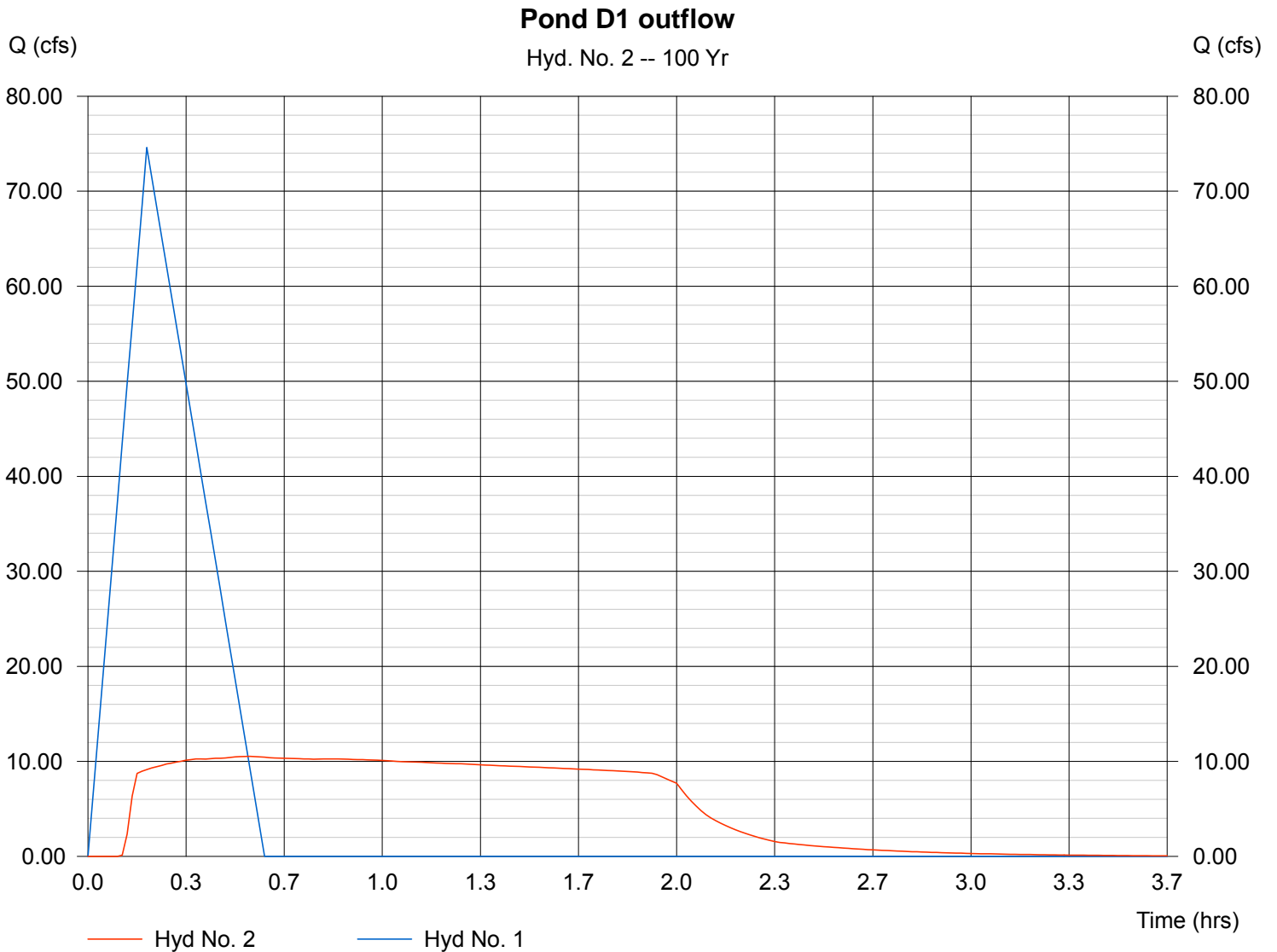
Pond D1 outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 1
Reservoir name = Pond D1

Peak discharge = 10.52 cfs
Time interval = 1 min
Max. Elevation = 5756.78 ft
Max. Storage = 108,212 cuft

Storage Indication method used. Wet pond routing start elevation = 5754.10 ft.

Hydrograph Volume = 71,644 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

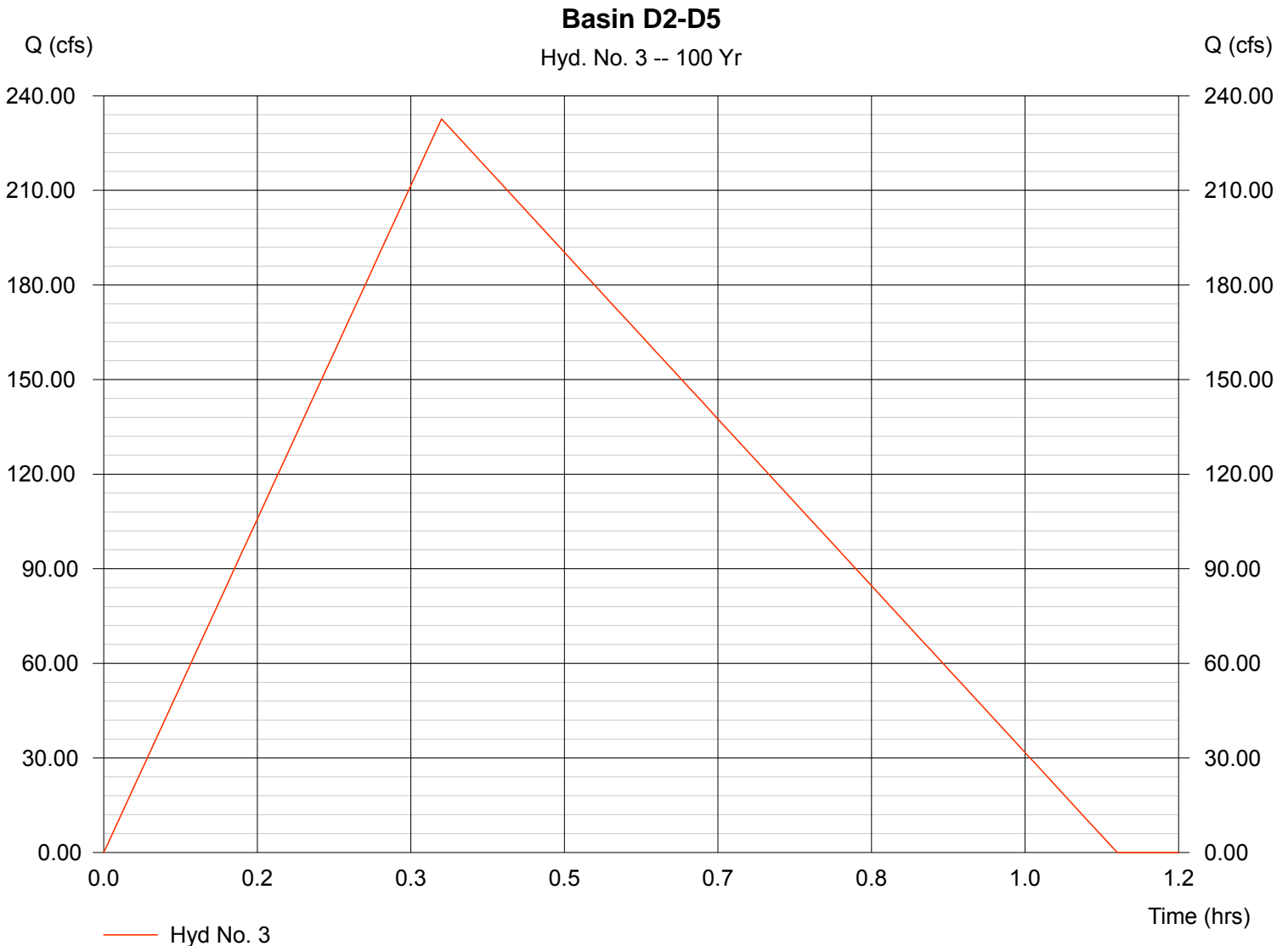
Hyd. No. 3

Basin D2-D5

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 72.000 ac
Intensity = 5.049 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 232.67 cfs
Time interval = 1 min
Runoff coeff. = 0.64
Tc by User = 22.00 min
Asc/Rec limb fact = 1/2

Hydrograph Volume = 460,692 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

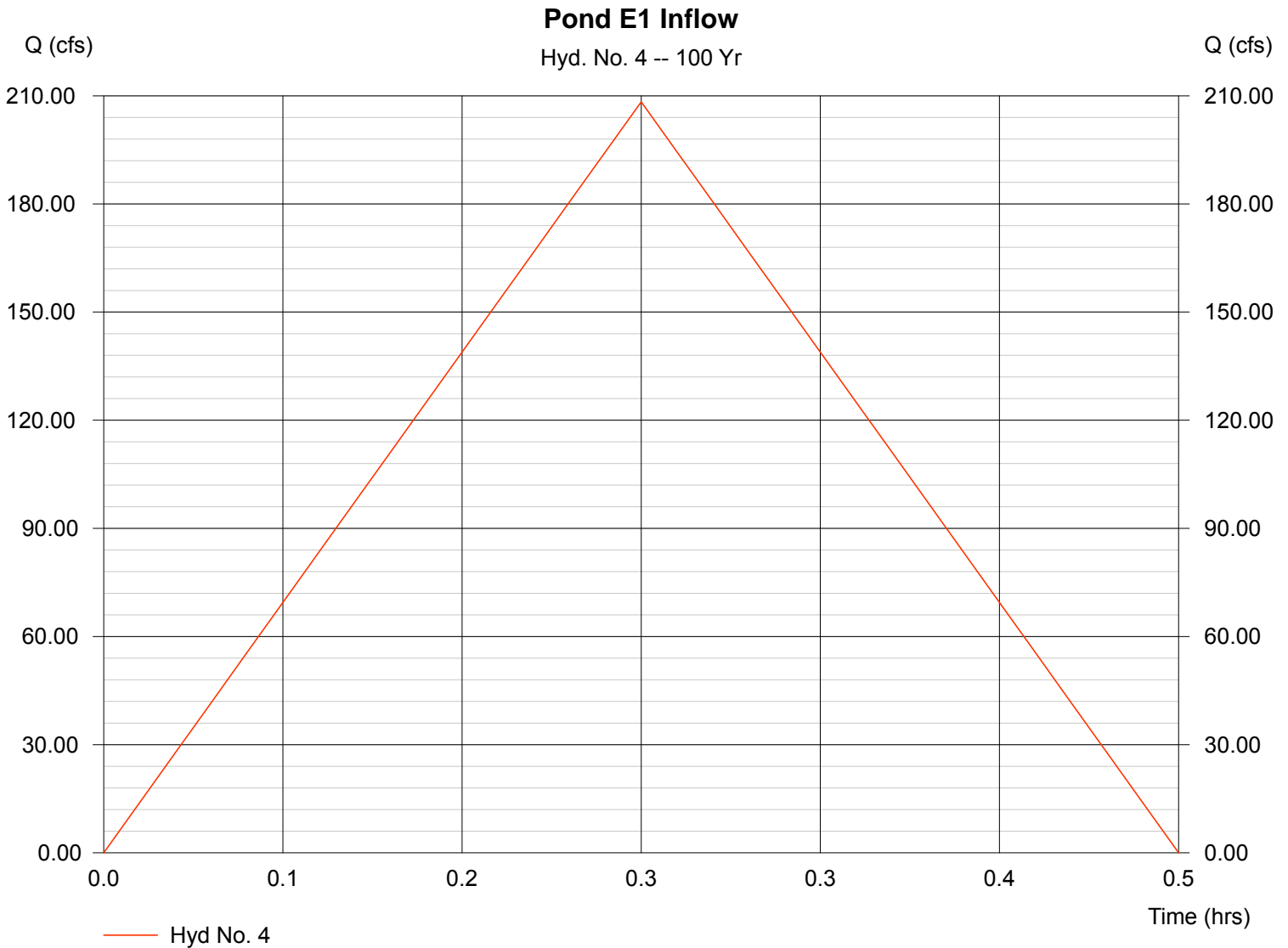
Hyd. No. 4

Pond E1 Inflow

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 56.500 ac
Intensity = 6.146 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 208.33 cfs
Time interval = 1 min
Runoff coeff. = 0.6
Tc by User = 15.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 187,500 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

Hyd. No. 5

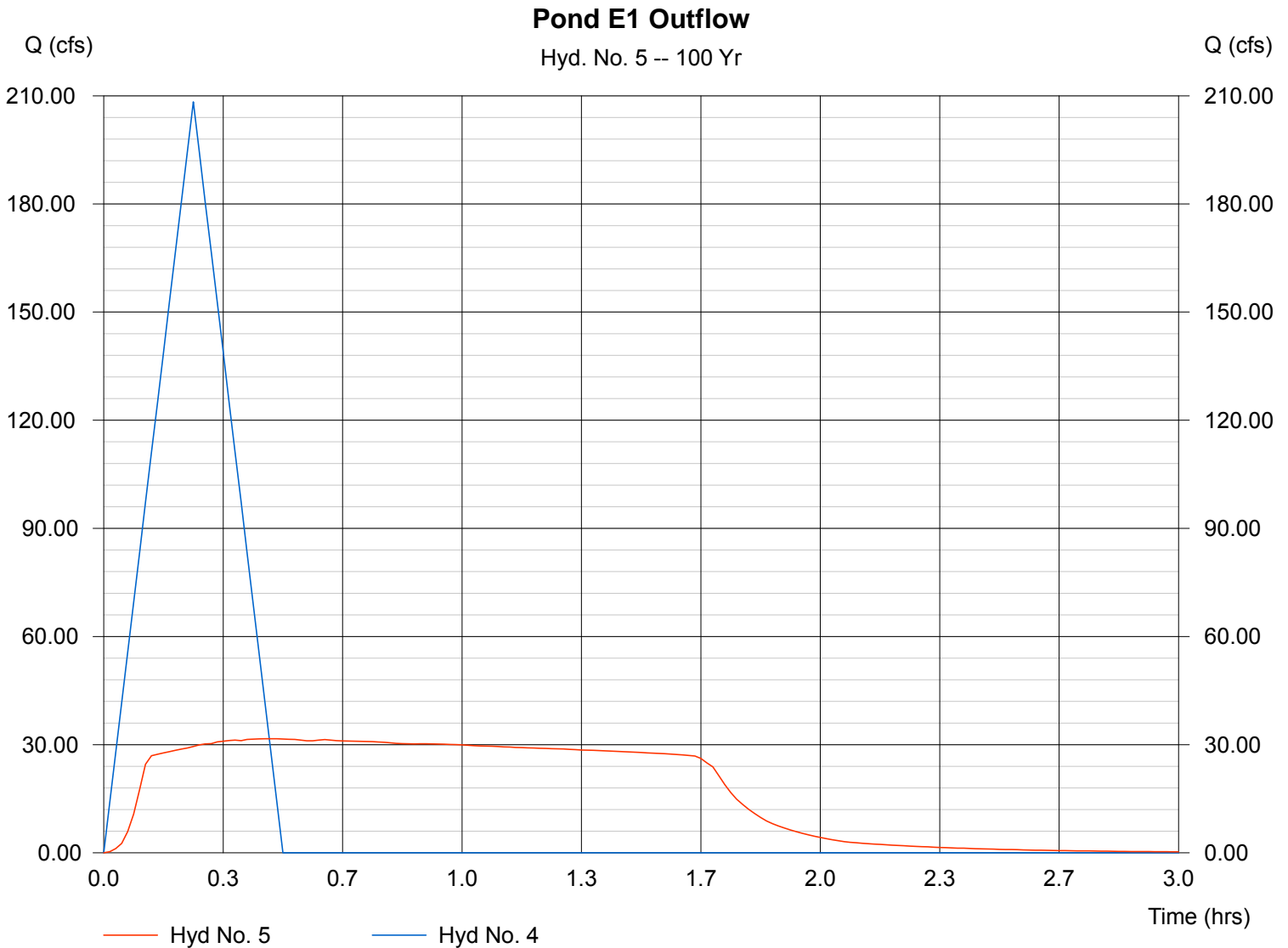
Pond E1 Outflow

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 4
Reservoir name = Pond E1

Peak discharge = 31.62 cfs
Time interval = 1 min
Max. Elevation = 5737.32 ft
Max. Storage = 293,609 cuft

Storage Indication method used. Wet pond routing start elevation = 5734.00 ft.

Hydrograph Volume = 187,499 cuft



Hydrograph Plot

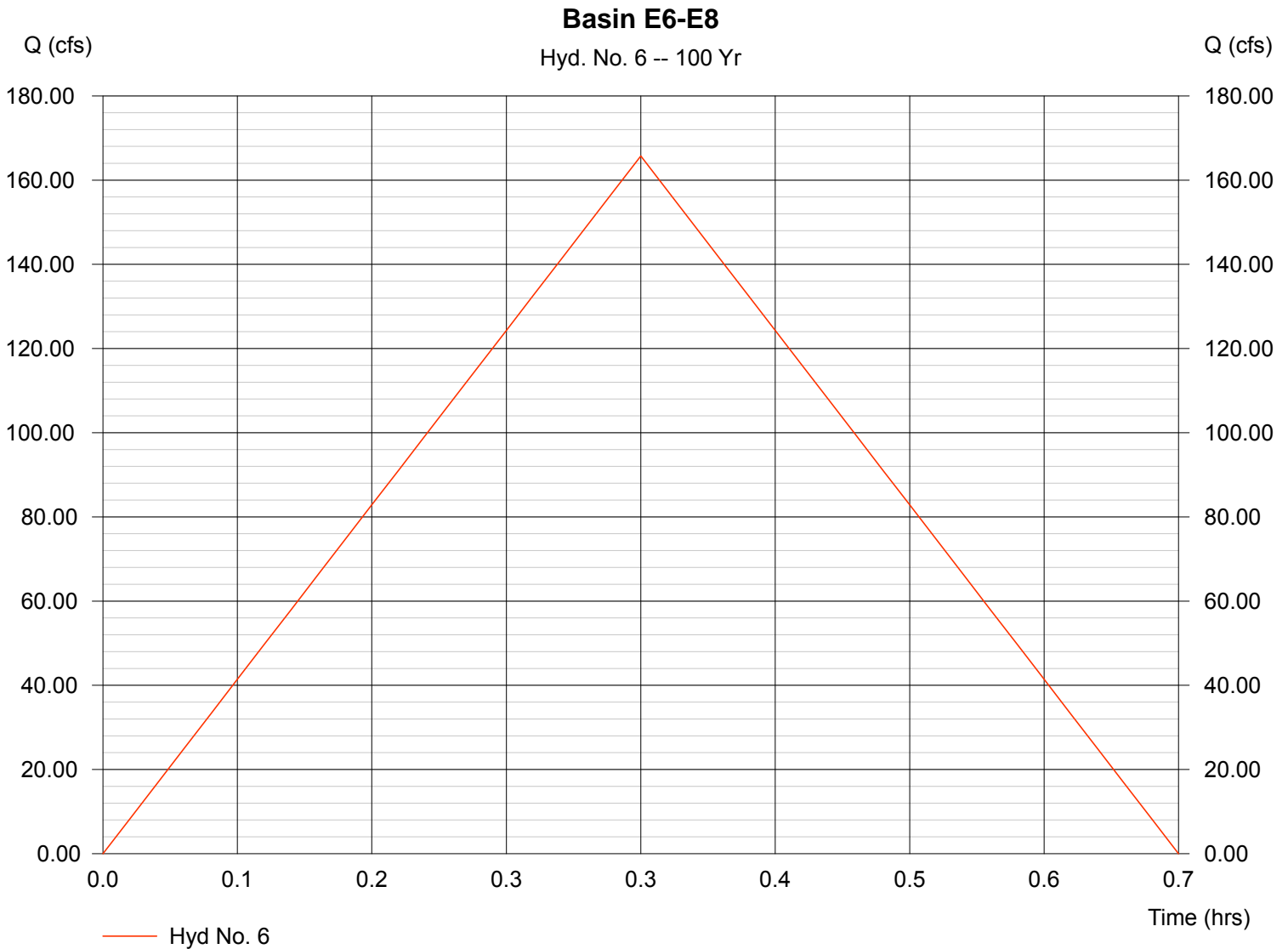
Hyd. No. 6

Basin E6-E8

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 49.400 ac
Intensity = 5.325 in/hr
IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 165.73 cfs
Time interval = 1 min
Runoff coeff. = 0.63
Tc by User = 20.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 198,882 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

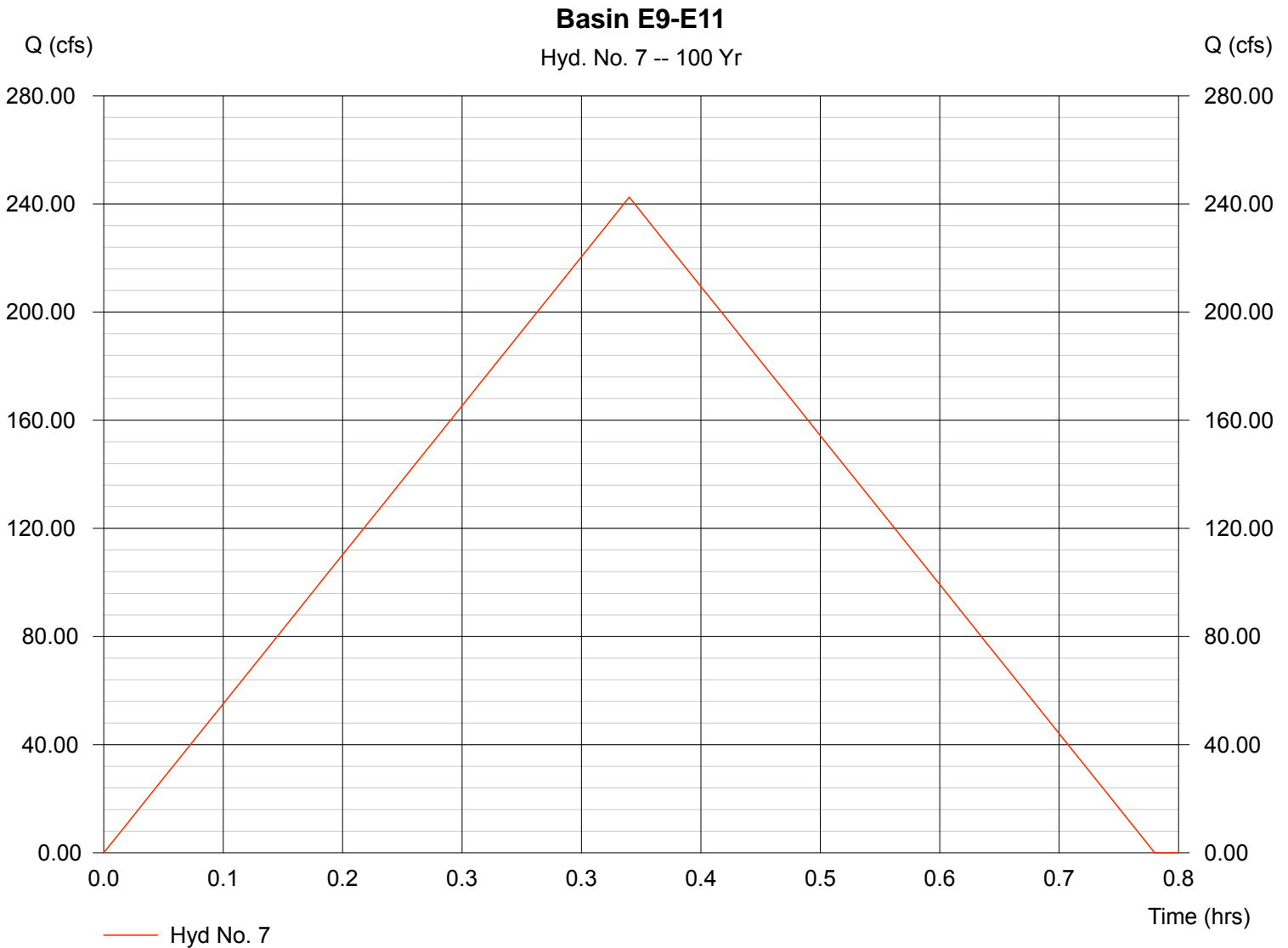
Hyd. No. 7

Basin E9-E11

Hydrograph type = Rational
 Storm frequency = 100 yrs
 Drainage area = 81.400 ac
 Intensity = 5.049 in/hr
 IDF Curve = 2016-idf curves-rls.IDF

Peak discharge = 242.50 cfs
 Time interval = 1 min
 Runoff coeff. = 0.59
 Tc by User = 22.00 min
 Asc/Rec limb fact = 1/1

Hydrograph Volume = 320,099 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

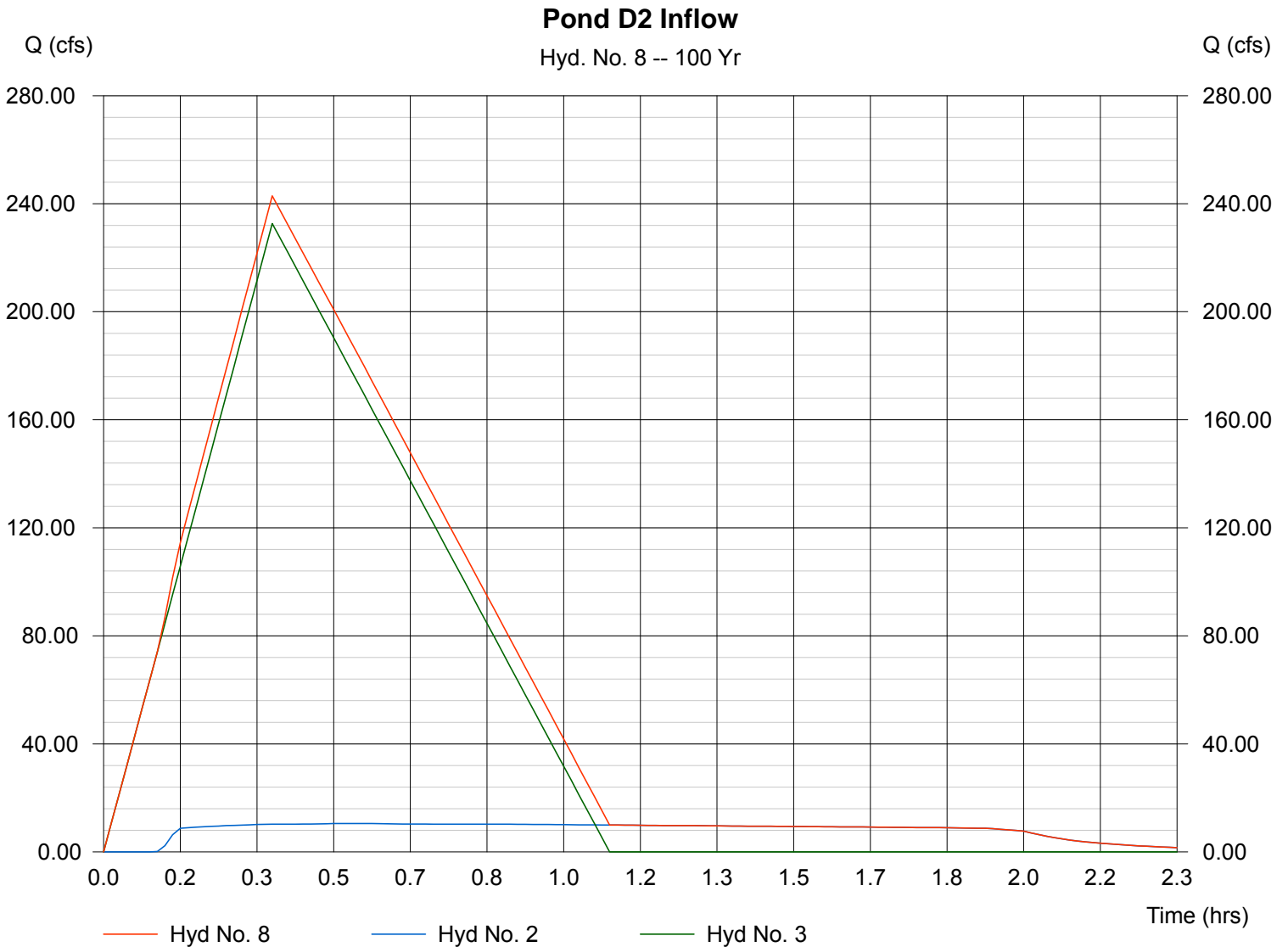
Hyd. No. 8

Pond D2 Inflow

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 2, 3

Peak discharge = 242.93 cfs
Time interval = 1 min

Hydrograph Volume = 532,337 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

Hyd. No. 9

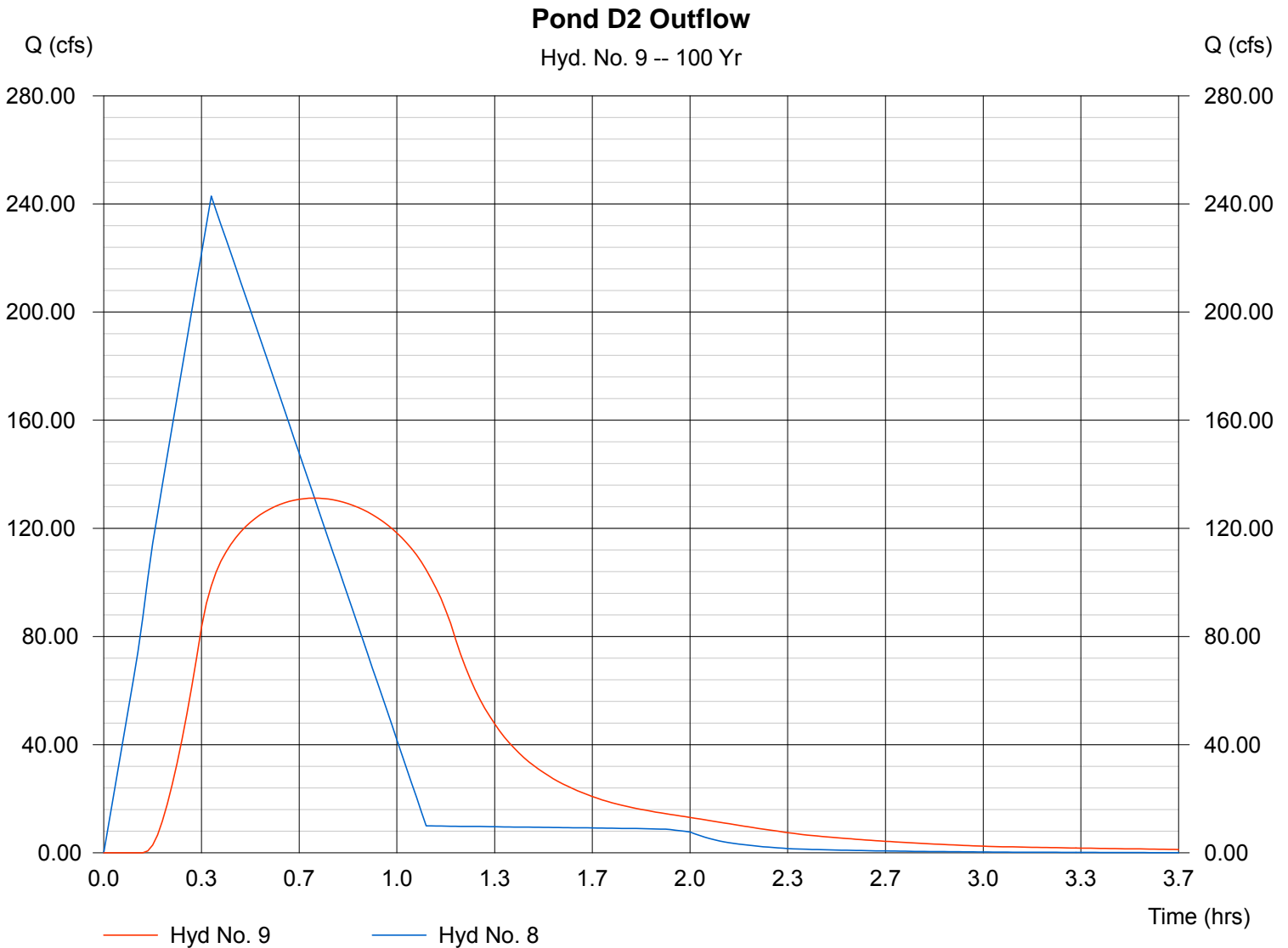
Pond D2 Outflow

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 8
 Reservoir name = Pond D2

Peak discharge = 131.19 cfs
 Time interval = 1 min
 Max. Elevation = 5701.75 ft
 Max. Storage = 386,691 cuft

Storage Indication method used. Wet pond routing start elevation = 5699.20 ft.

Hydrograph Volume = 508,771 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

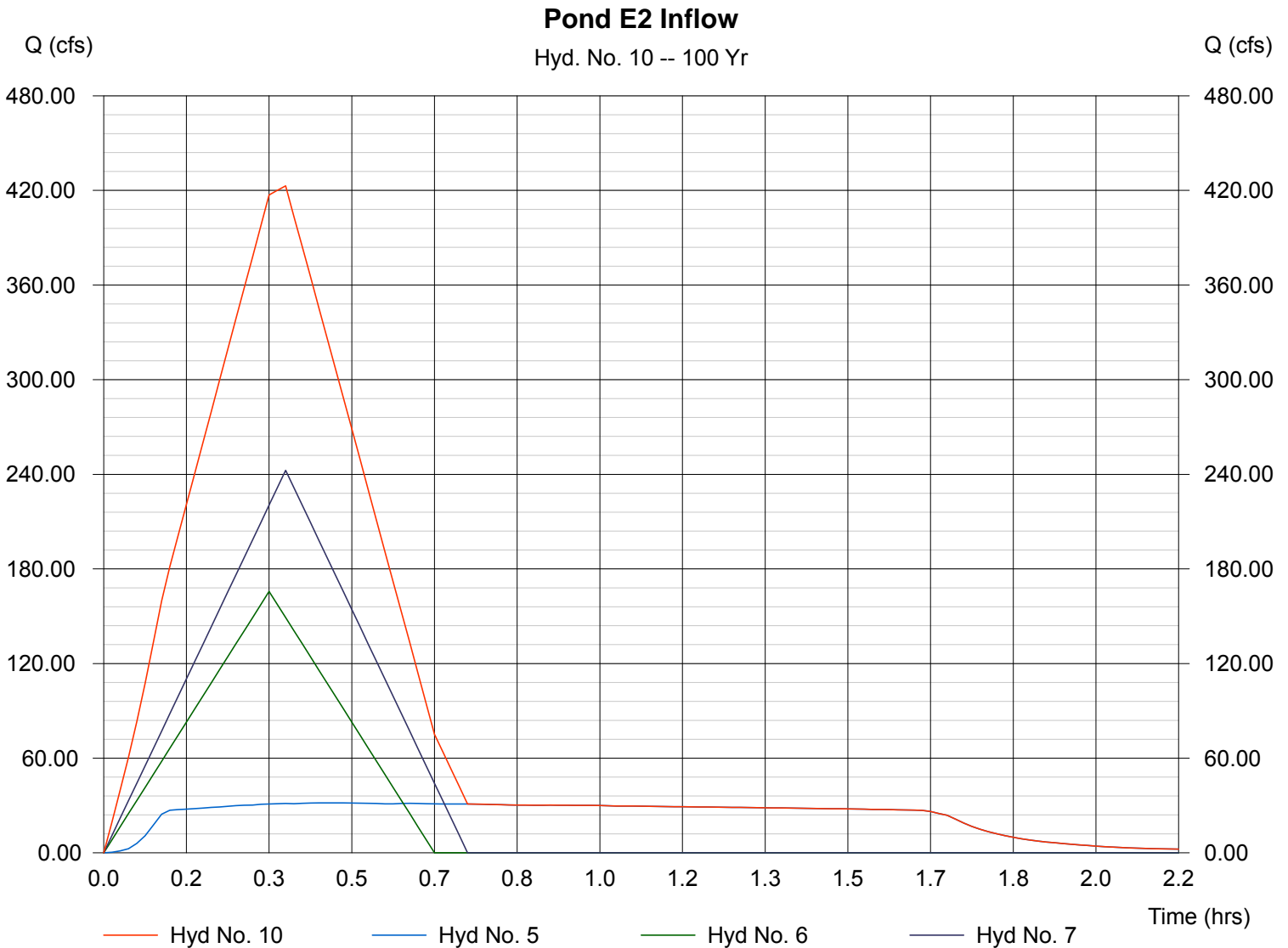
Hyd. No. 10

Pond E2 Inflow

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 5, 6, 7

Peak discharge = 422.93 cfs
Time interval = 1 min

Hydrograph Volume = 706,480 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jun 5 2017, 6:15 AM

Hyd. No. 11

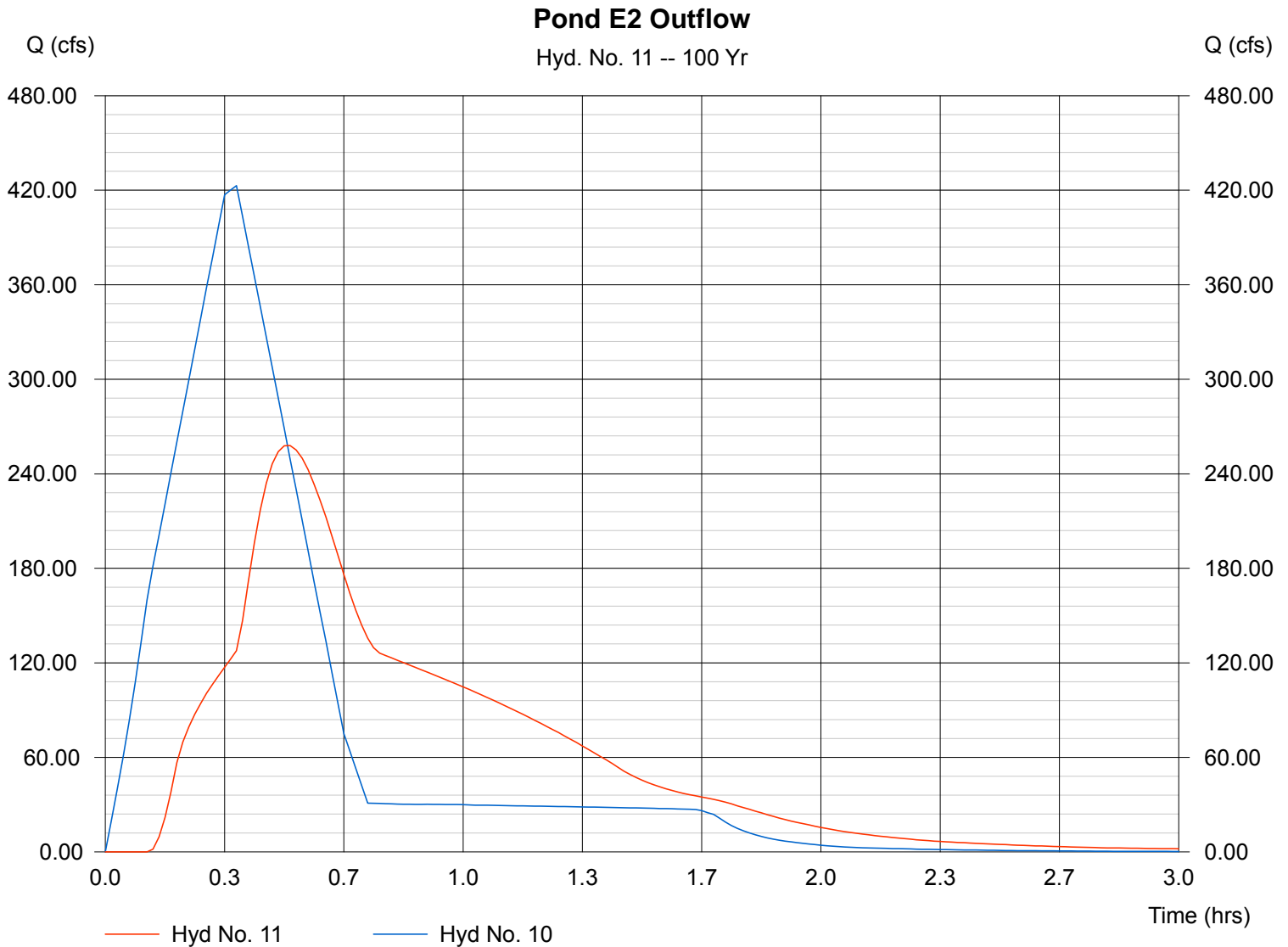
Pond E2 Outflow

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 10
 Reservoir name = Pond E2

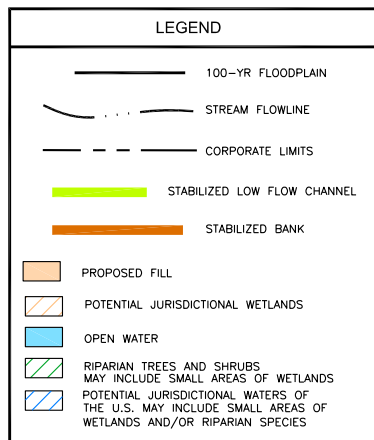
Peak discharge = 257.97 cfs
 Time interval = 1 min
 Max. Elevation = 5700.91 ft
 Max. Storage = 421,789 cuft

Storage Indication method used. Wet pond routing start elevation = 5696.40 ft.

Hydrograph Volume = 669,336 cuft



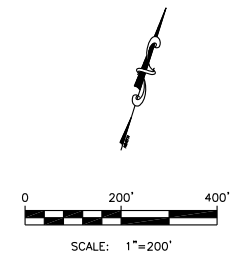
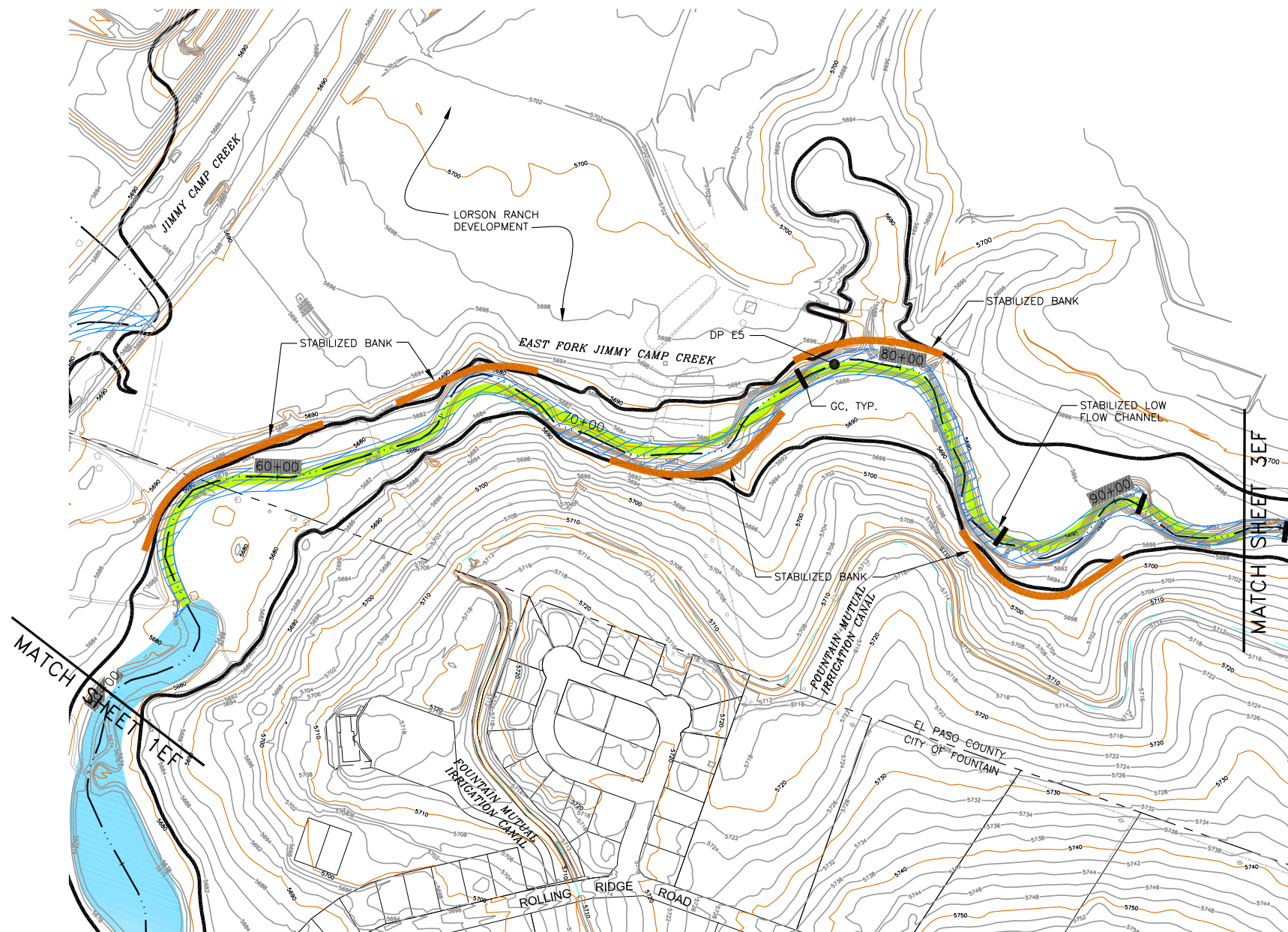
APPENDIX F – JIMMY CAMP CREEK DBPS – KIOWA ENGINEERING



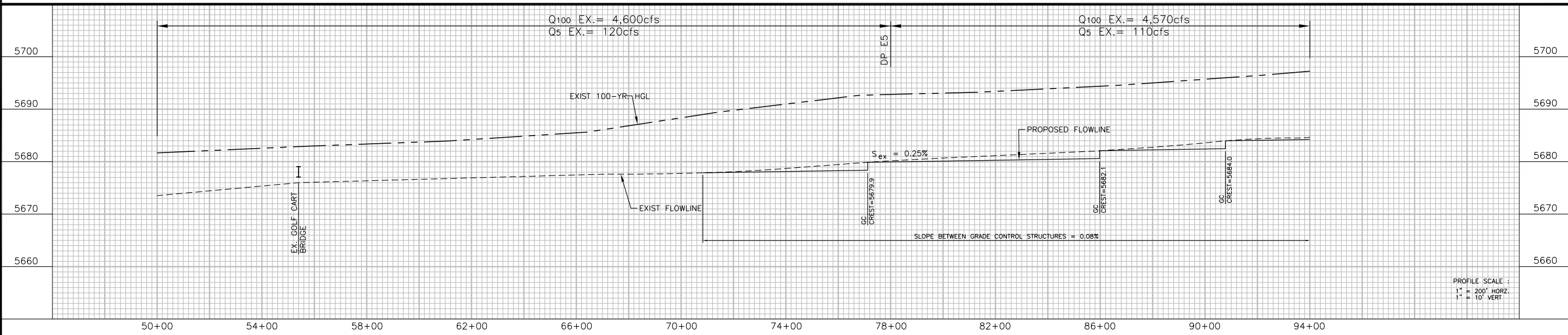
FLOODPLAIN BOUNDARIES ARE FOR PLANNING INFORMATION ONLY AND ARE NOT INTENDED TO BE USED FOR FLOODPLAIN REGULATION OR MANAGEMENT.

THIS DRAWING IS A PLANNING EXHIBIT REPRESENTING CONCEPTUAL ENGINEERING AND IS SUBJECT TO REFINEMENT. THIS DRAWING SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

DISCHARGES UPSTREAM OF DP E1 HAD NO AREA ADJUSTMENT APPLIED



REACH E1



PROFILE SCALE :
1" = 200' HORZ.
1" = 10' VERT.

Project No.:	14008
Date:	OCTOBER 2014
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	

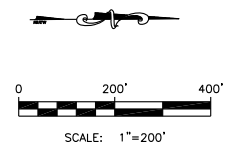
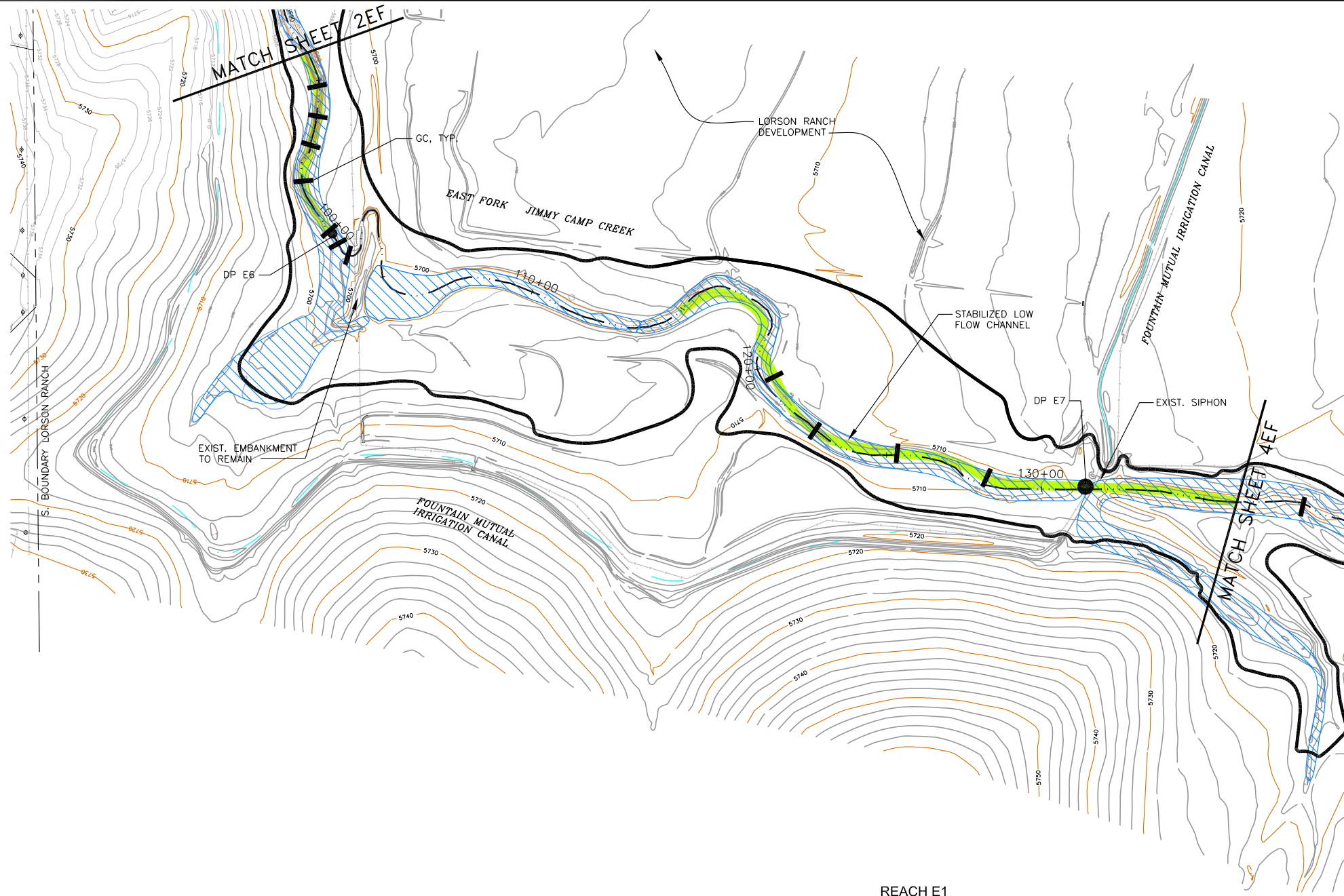
LEGEND

- 100-YR FLOODPLAIN
- STREAM FLOWLINE
- CORPORATE LIMITS
- STABILIZED LOW FLOW CHANNEL
- STABILIZED BANK
- PROPOSED FILL
- POTENTIAL JURISDICTIONAL WETLANDS
- OPEN WATER
- RIPARIAN TREES AND SHRUBS
MAY INCLUDE SMALL AREAS OF WETLANDS
- POTENTIAL JURISDICTIONAL WATERS OF THE U.S. MAY INCLUDE SMALL AREAS OF WETLANDS AND/OR RIPARIAN SPECIES

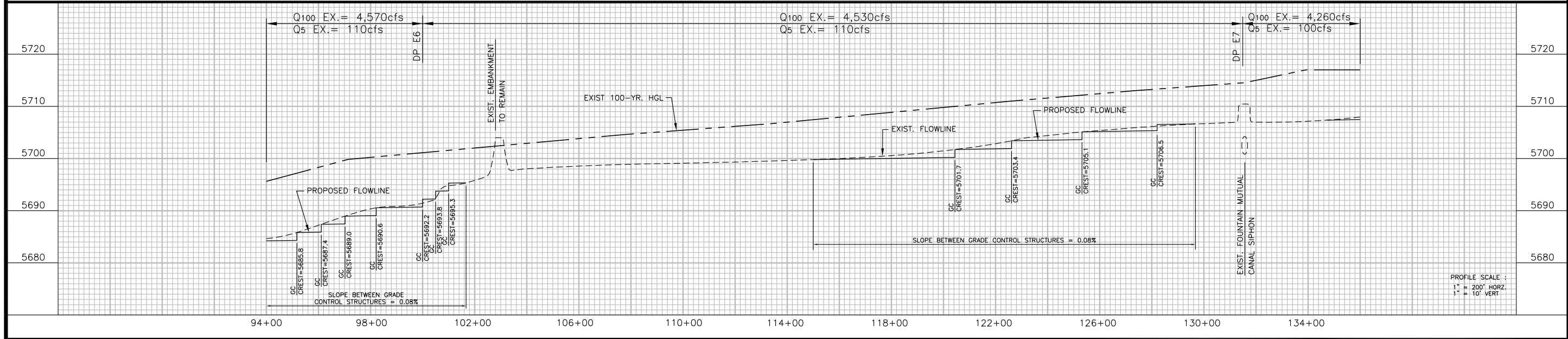
FLOODPLAIN BOUNDARIES ARE FOR PLANNING INFORMATION ONLY AND ARE NOT INTENDED TO BE USED FOR FLOODPLAIN REGULATION OR MANAGEMENT.

THIS DRAWING IS A PLANNING EXHIBIT REPRESENTING CONCEPTUAL ENGINEERING AND IS SUBJECT TO REFINEMENT. THIS DRAWING SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

DISCHARGES UPSTREAM OF DP E1 HAD NO AREA ADJUSTMENT APPLIED



REACH E1

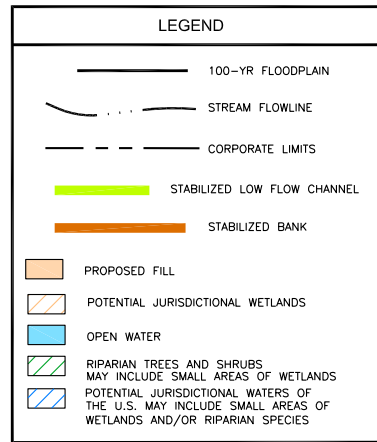


PROFILE SCALE :
1" = 200' HORZ
1" = 10' VERT

JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY
EAST FORK JIMMY CAMP CREEK
 CONCEPTUAL DESIGN PLAN & PROFILE
 CITY OF COLORADO SPRINGS, COLORADO

Project No.:	14008
Date:	OCTOBER 2014
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	

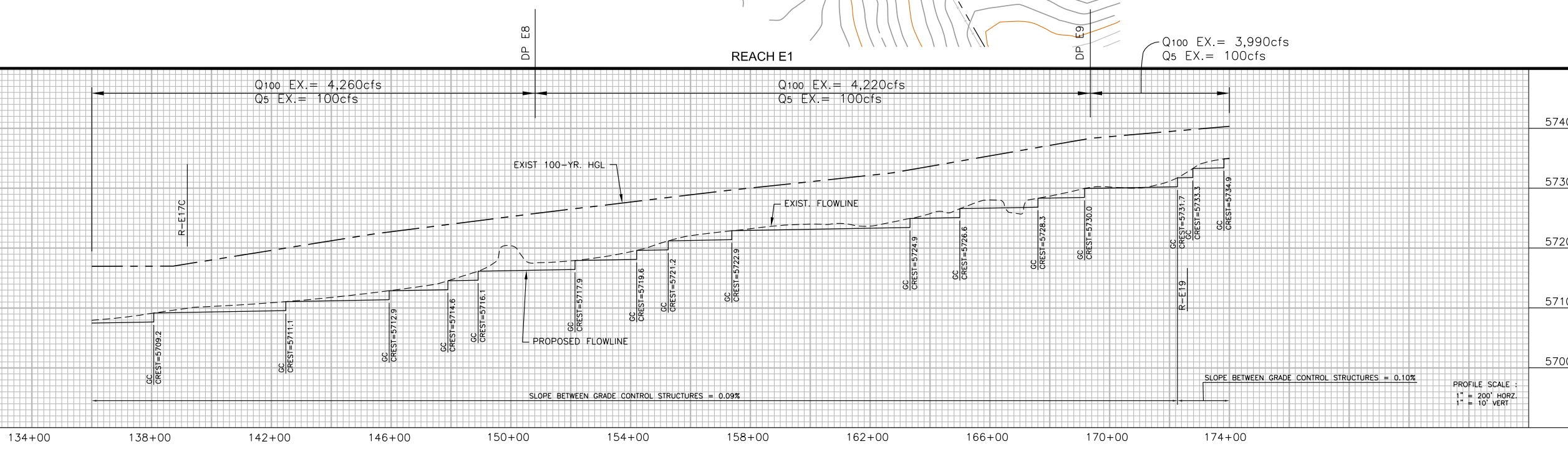
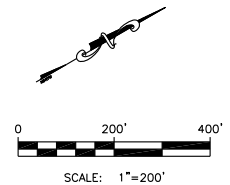
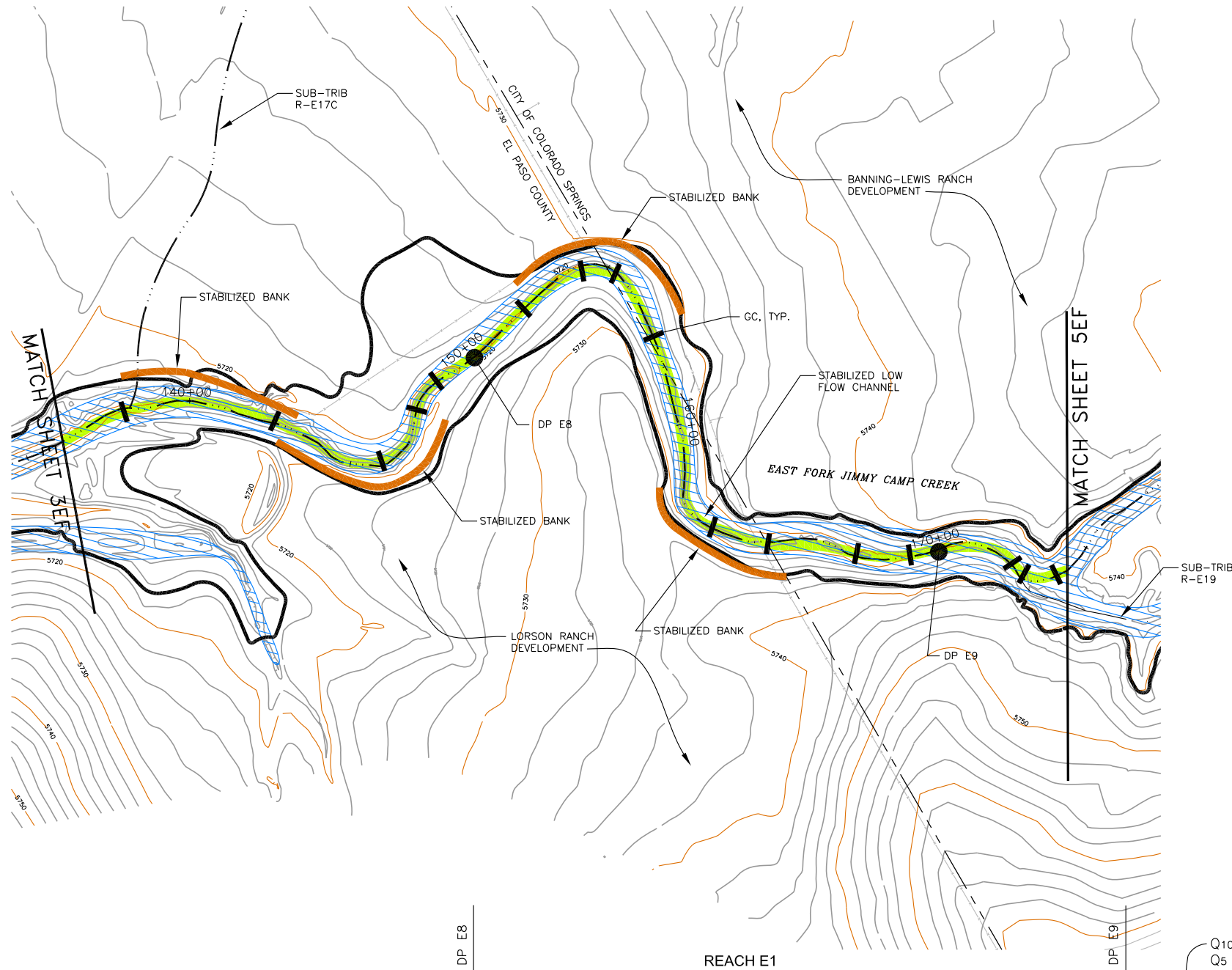
3EF



FLOODPLAIN BOUNDARIES ARE FOR PLANNING INFORMATION ONLY AND ARE NOT INTENDED TO BE USED FOR FLOODPLAIN REGULATION OR MANAGEMENT.

THIS DRAWING IS A PLANNING EXHIBIT REPRESENTING CONCEPTUAL ENGINEERING AND IS SUBJECT TO REFINEMENT. THIS DRAWING SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

DISCHARGES UPSTREAM OF DP E1 HAD NO AREA ADJUSTMENT APPLIED

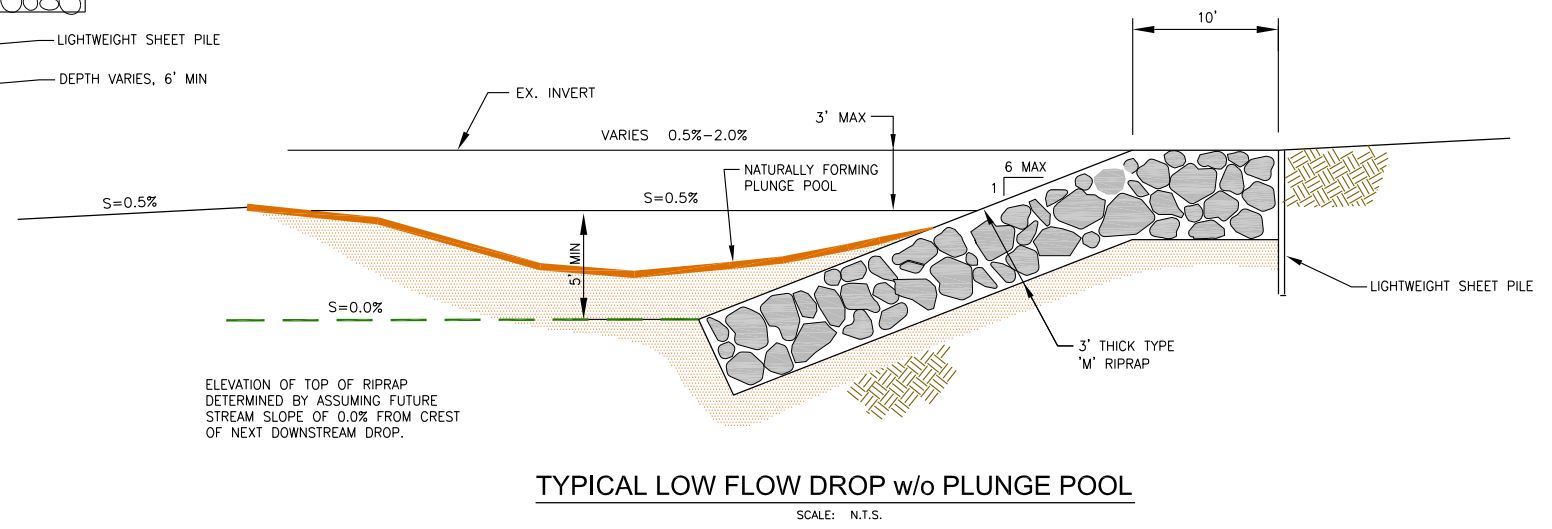
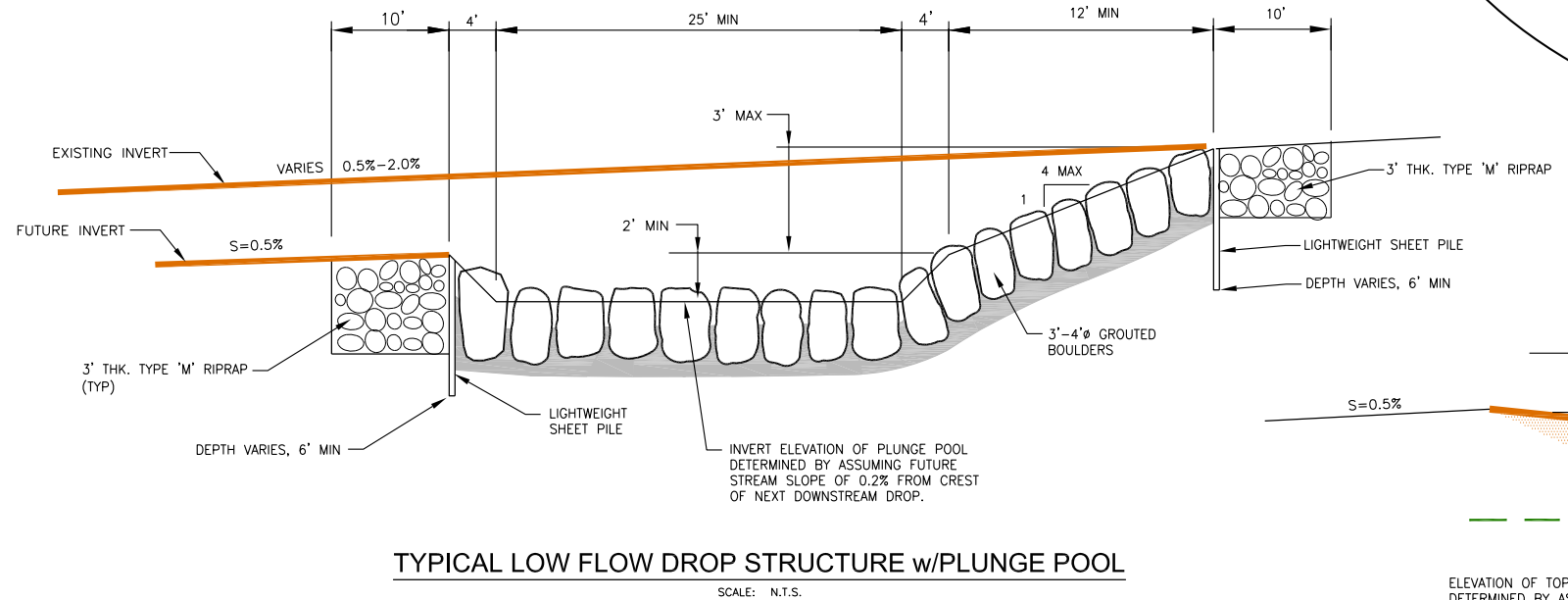
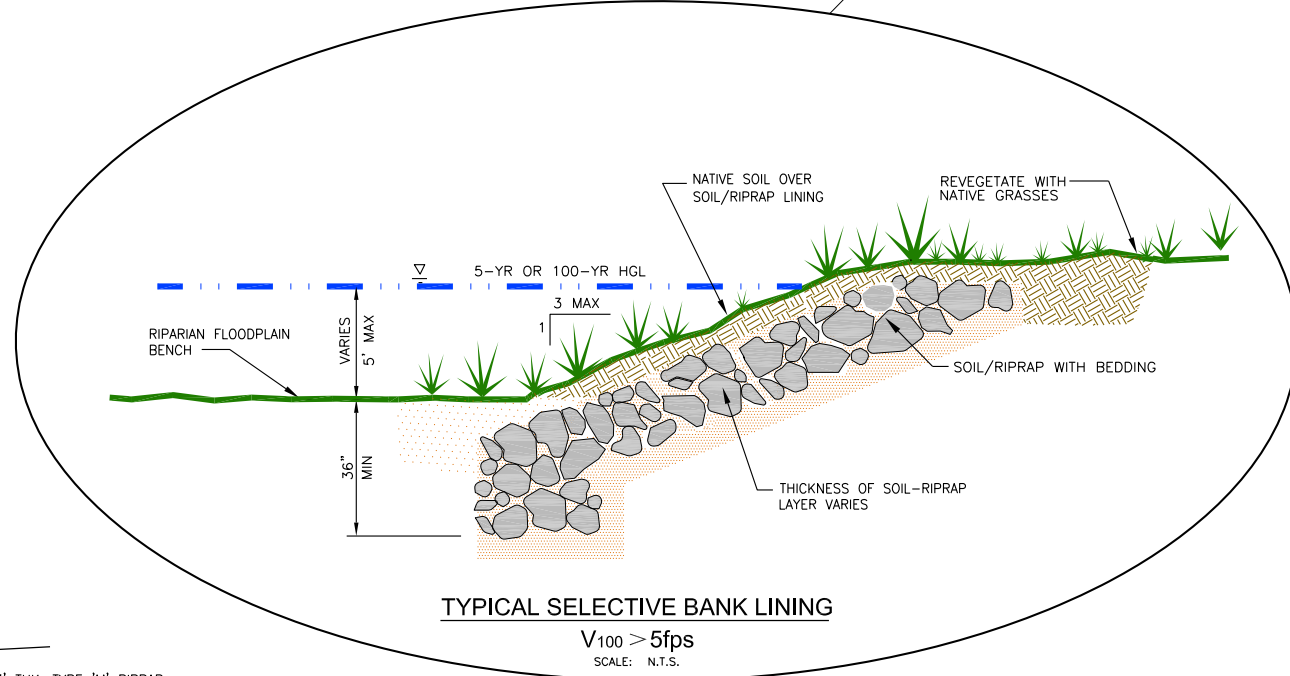
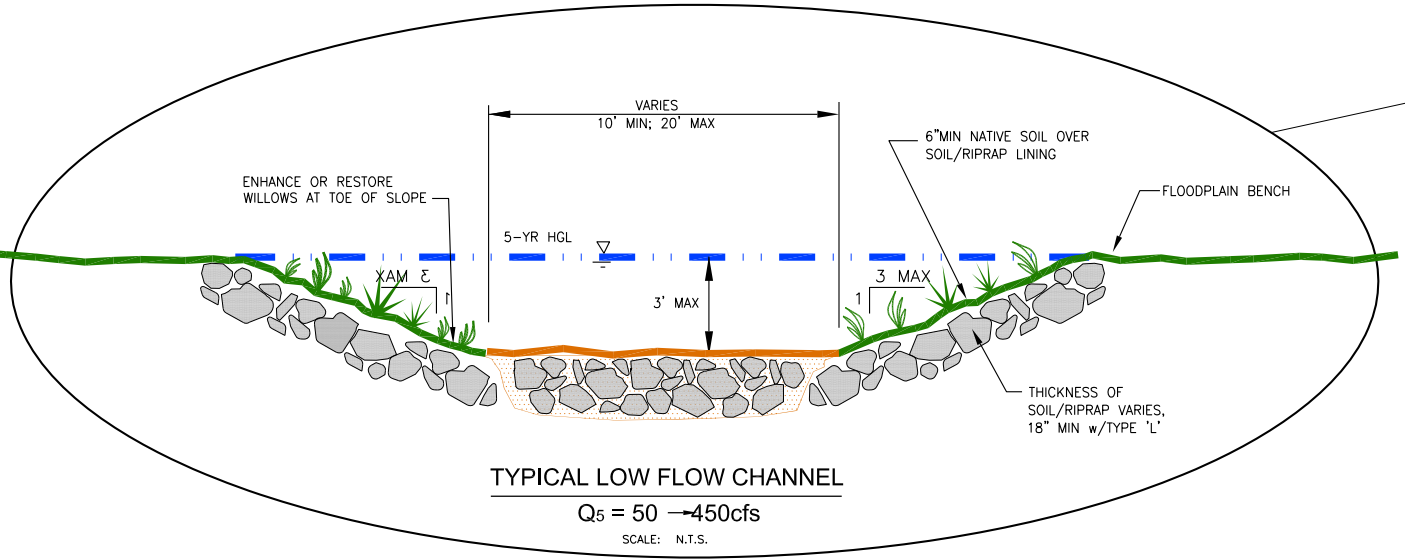
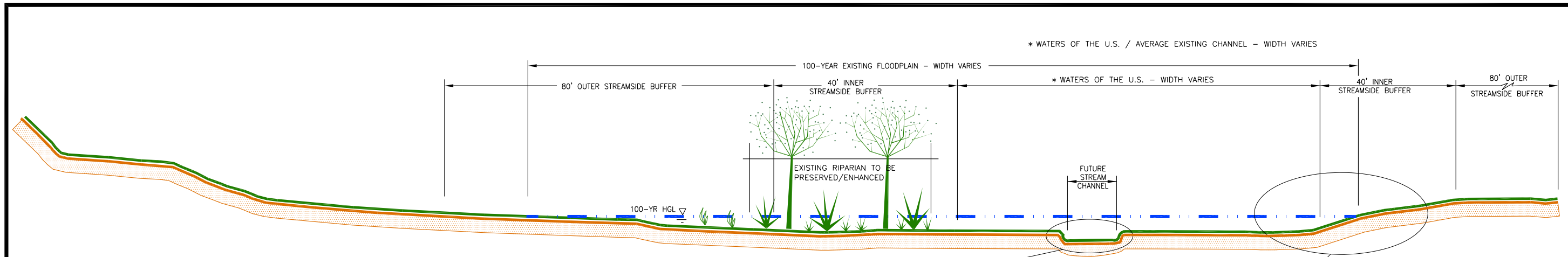


JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY
 EAST FORK JIMMY CAMP CREEK
 CONCEPTUAL DESIGN PLAN & PROFILE
 CITY OF COLORADO SPRINGS, COLORADO

Project No.: 14008
 Date: OCTOBER 2014
 Design: RNW
 Drawn: JLN
 Check: RNW
 Revisions:

4EF

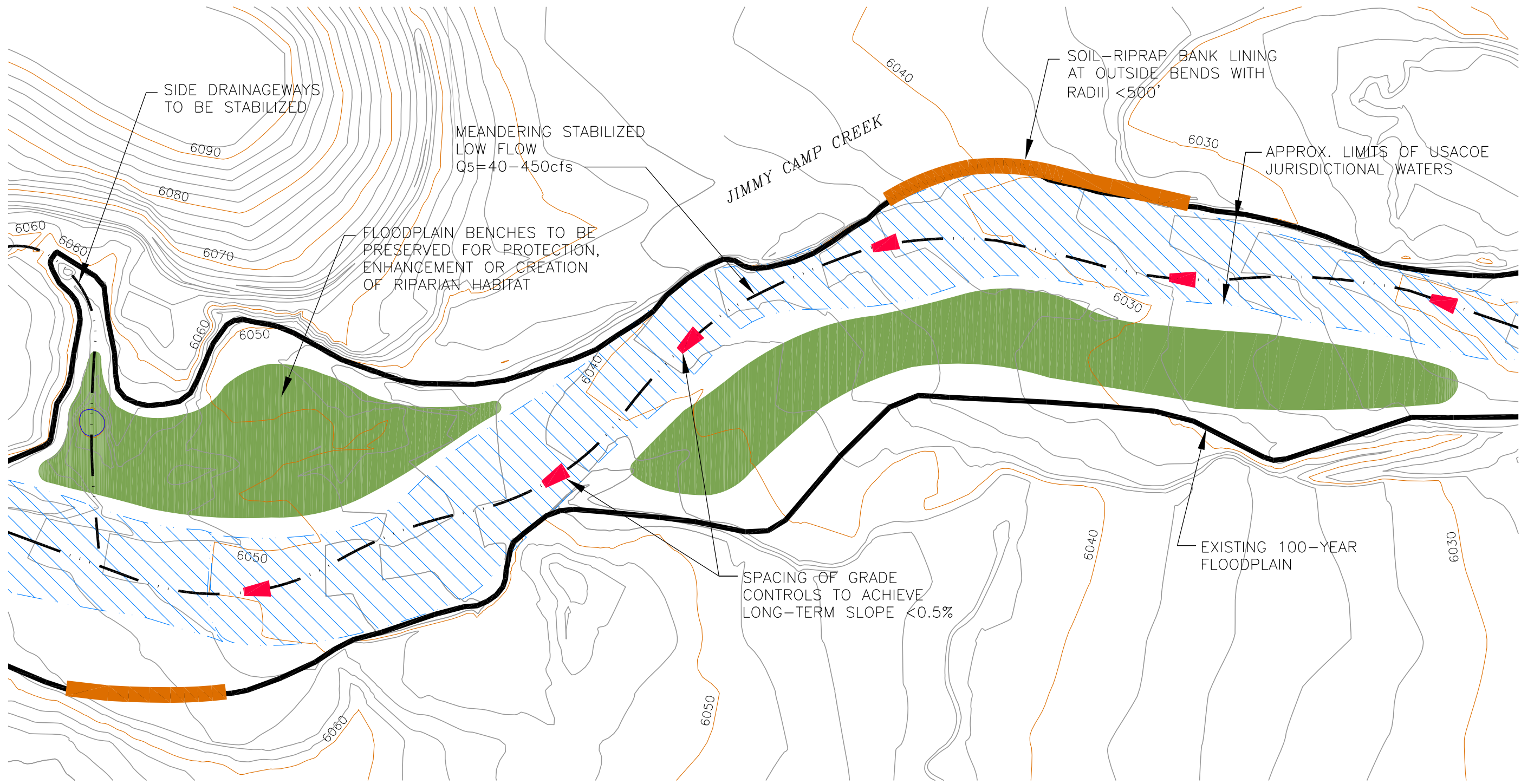
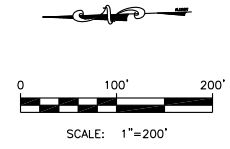
Kiowa
 Engineering Corporation
 1604 South 21st Street
 Colorado Springs, Colorado 80904
 (719) 630-7342



Project No.:	14008
Date:	OCTOBER 2014
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	

JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY
JIMMY CAMP CREEK
TYPICAL FLOODPLAIN PRESERVATION PLAN
CITY OF COLORADO SPRINGS, COLORADO

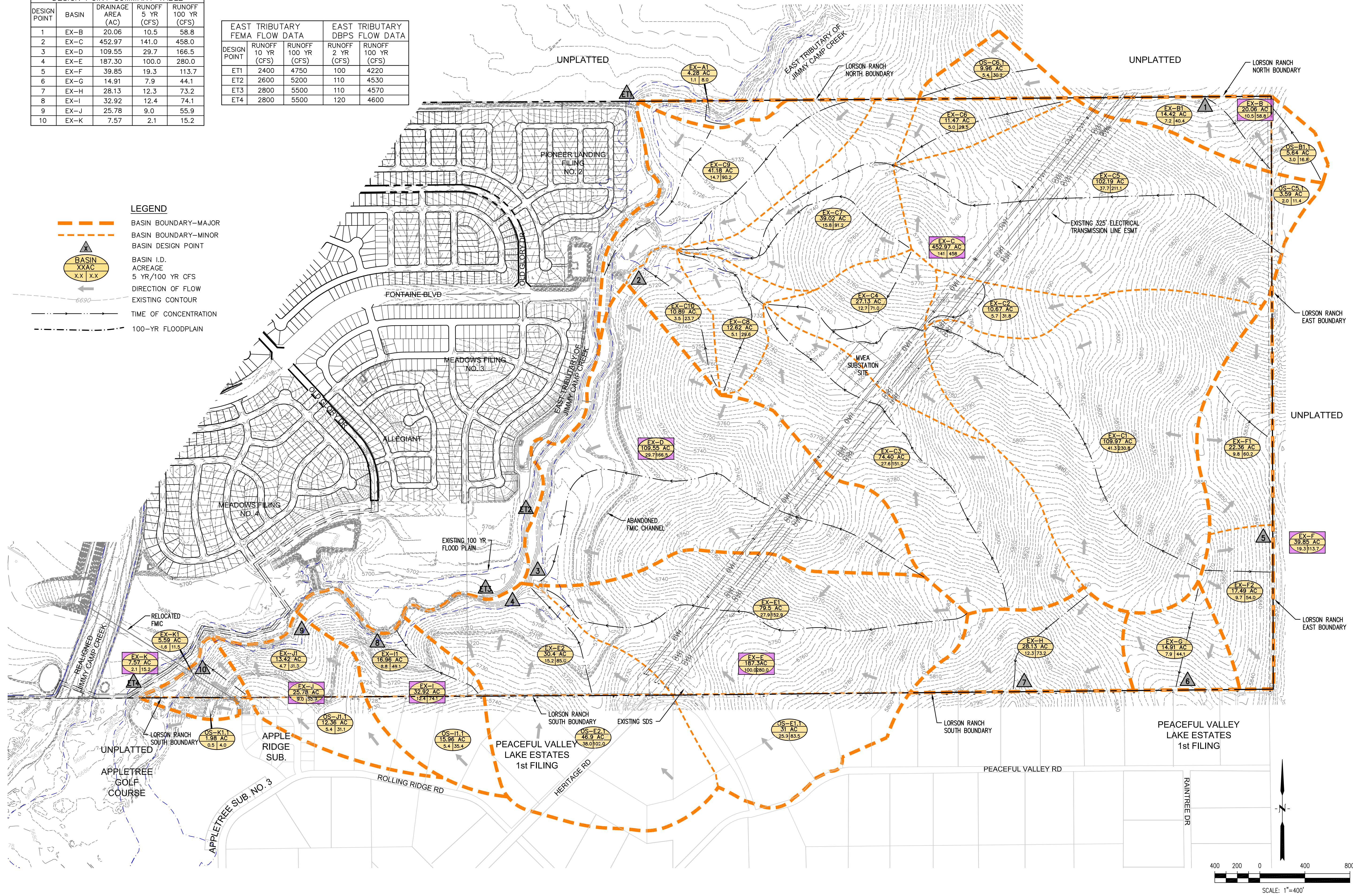
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Date:	OCTOBER 2014
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Drawn:	JLN
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Revisions:	



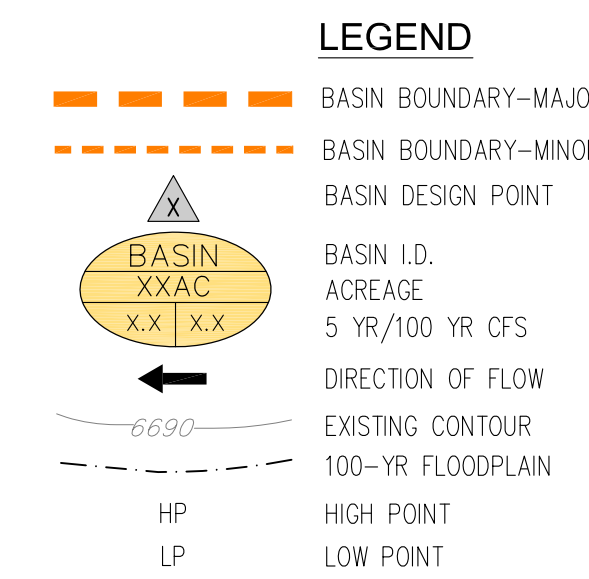
DESIGN POINT SUMMARY TABLE				
DESIGN POINT	Basin	Drainage Area (AC)	Runoff 5 Yr (CFS)	Runoff 100 Yr (CFS)
1	EX-B	20.06	10.5	58.8
2	EX-C	452.97	141.0	458.0
3	EX-D	109.55	29.7	166.5
4	EX-E	187.30	100.0	280.0
5	EX-F	39.85	19.3	113.7
6	EX-G	14.91	7.9	44.1
7	EX-H	28.13	12.3	73.2
8	EX-I	32.92	12.4	74.1
9	EX-J	25.78	9.0	55.9
10	EX-K	7.57	2.1	15.2

EAST TRIBUTARY FEMA FLOW DATA		EAST TRIBUTARY DBPS FLOW DATA	
DESIGN POINT	Runoff 10 Yr (CFS)	Runoff 100 Yr (CFS)	Runoff 100 Yr (CFS)
ET1	2400	4750	100
ET2	2600	5200	110
ET3	2800	5500	110
ET4	2800	5500	120

- LEGEND**
- BASIN BOUNDARY-MAJOR
 - BASIN BOUNDARY-MINOR
 - BASIN DESIGN POINT
 - BASIN I.D. ACREAGE
 - 5 YR/100 YR CFS
 - DIRECTION OF FLOW
 - EXISTING CONTOUR
 - TIME OF CONCENTRATION
 - 100-YR FLOODPLAIN



DESIGN POINT SUMMARY TABLE				
DESIGN POINT	DRAINAGE AREA	RUNOFF 5 YR (CFS)	RUNOFF 100 YR (CFS)	COMMENTS
1	9.54ac	8.5	28	
2	57.7ac	80.1	171.0	INFLOW POND C1
3a		11.0	65.0	POND C2.1 OUTFLOW
3b		46.3	111.0	INFLOW POND C2.3
3c		4.0	46.0	POND C2.3 OUTFLOW
3d		70.0	138.0	INFLOW POND C2.2
3e		6.0	40.0	POND C2.2 OUTFLOW
3f		14.0	104.0	FLOW IN PIPE
4		51.6	134.0	INFLOW POND C3
5		74.5	265.5	INFLOW POND C4
6a		68.1	151.8	
6b		75.7	192.3	
6c		93.2	222	INFLOW C16+C12+C13
7		88	270	
7a		114	337	INFLOW FROM FONTAINE
7b		204	484	INFLOW POND C5
7c		121	420	POND C5 OUTFLOW
8		18.0	46.0	
9a		23.0	38.0	84.5
9b		36.4	61.7	137.5
10a		106.0	243.0	INFLOW POND D2
10b		31.2	131.2	FROM POND D2
11		26.2	89.8	
12		88.7	209.5	INFLOW POND E1
13		78.0	205.0	
14		190.0	423.0	INFLOW POND E2
14a		97.0	260.0	FROM POND E2
15		33.0	50.0	111.3
15a		3.5	41.0	FROM POND F
16		20.05	36.0	80.2
16a		2.0	33.0	FROM POND G
17		22.3	38.7	86.3
17a		2.0	35.3	FROM POND H
18		15.1	71.0	POND I + OS-I
18a		1.0	21.0	FROM POND I
19		11.2	58.6	POND J + OS-J1
19a		0.4	20.3	FROM POND J
20		2.1	12.9	POND K + OS-K1
20a		0.1	5.6	FROM POND K



NOTES:

- ALL DETENTION PONDS, RIGHTS-OF-WAY AND STORM SEWERS PRESENTED HERE ARE SCHEMATIC IN NATURE, AND ARE SHOWN FOR INFORMATION ONLY. FINAL DESIGN OF DRAINAGE SYSTEM WILL OCCUR WITH THE DESIGN OF THE ROADS AND SUBDIVISIONS.
- PROPOSED DETENTION PONDS WITHIN THE EXISTING 325' ELECTRICAL TRANSMISSION LINE EASEMENT WILL NEED TO BE DESIGNED WITH A 40' BUFFER FROM EXISTING POWER POLES.

EAST TRIBUTARY FEMA FLOW DATA			EXISTING FLOW DATA FROM JCC DBPS		
DESIGN POINT	RUNOFF 10 YR (CFS)	RUNOFF 100 YR (CFS)	RUNOFF 2 YR (CFS)	RUNOFF 100 YR (CFS)	
ET1	2400	4750	100	4220	
ET2	2600	5200	110	4530	
ET3	2800	5500	110	4570	
ET4	2800	5500	120	4600	

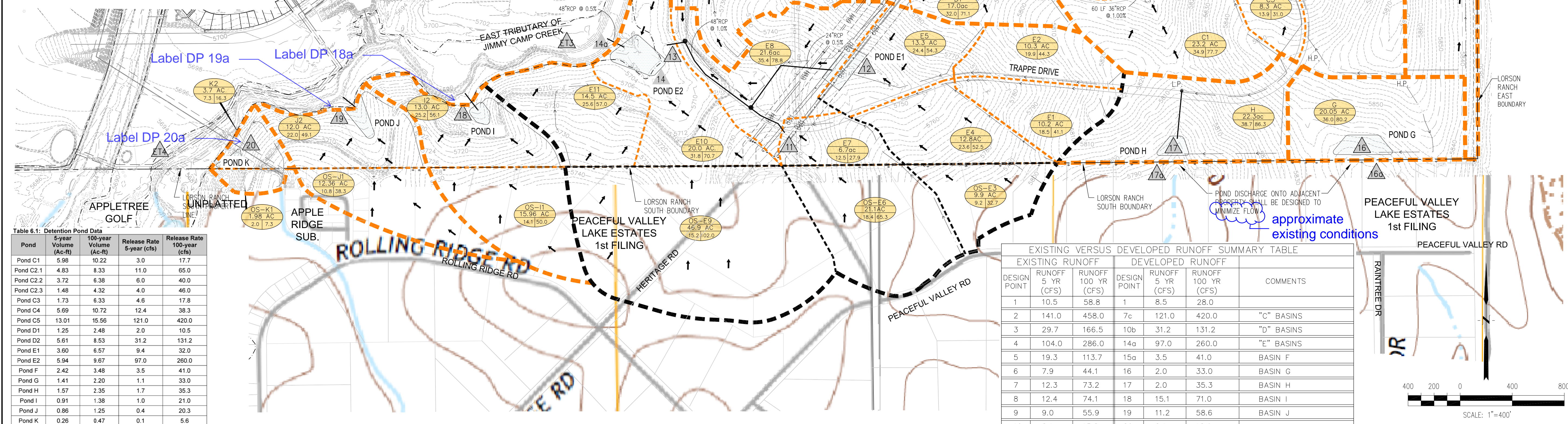


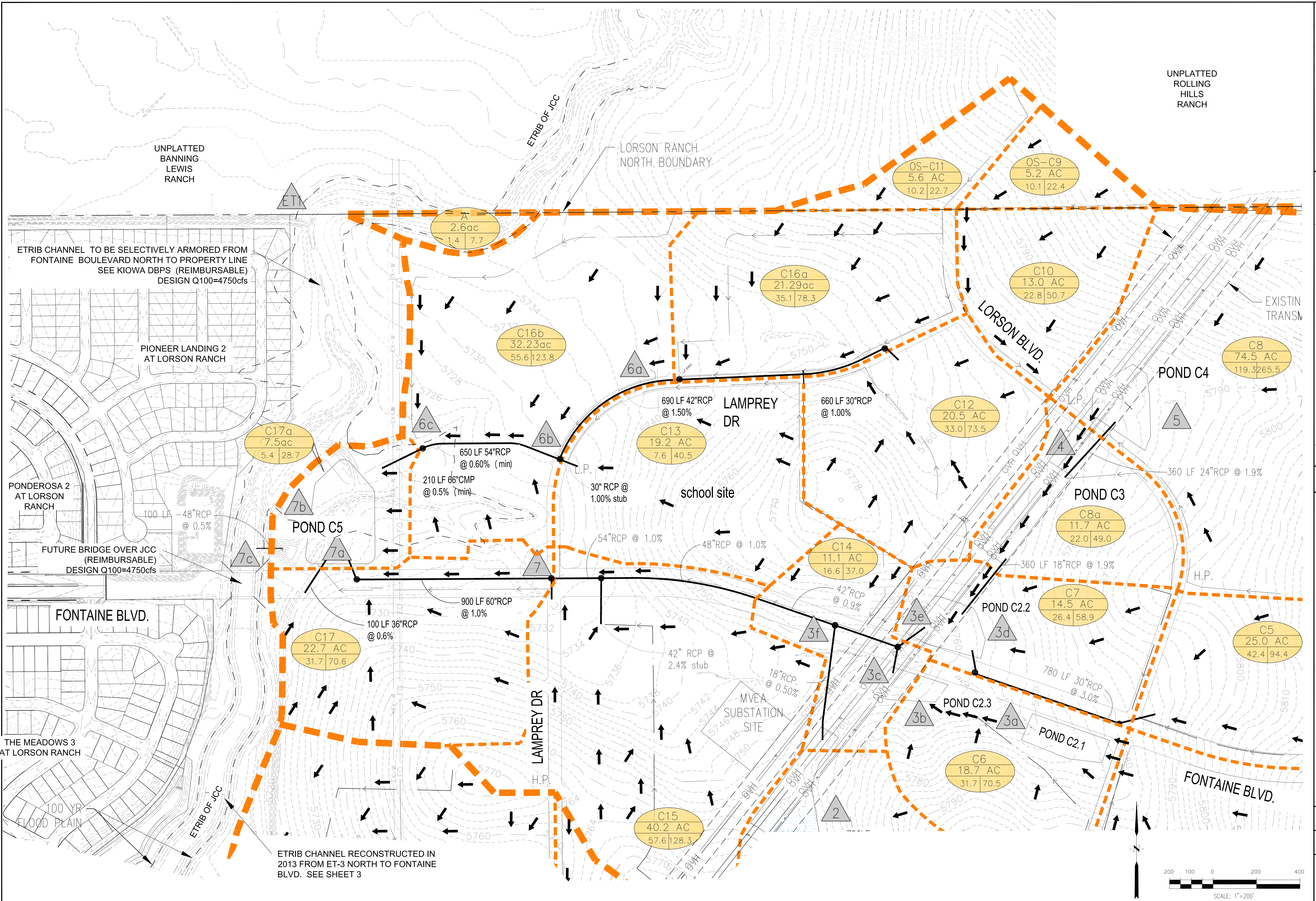
Table 6.1: Detention Pond Data

Pond	5-year Volume (Ac-ft)	100-year Volume (Ac-ft)	Release Rate 5-year (cfs)	Release Rate 100-year (cfs)
Pond C1	5.98	10.22	3.0	17.7
Pond C2.1	4.83	8.33	11.0	65.0
Pond C2.2	3.72	6.38	6.0	40.0
Pond C2.3	1.48	4.32	4.0	46.0
Pond C3	1.73	6.33	4.6	17.8
Pond C4	5.69	10.72	12.4	38.3
Pond C5	13.01	15.56	121.0	420.0
Pond D1	1.25	2.48	2.0	10.5
Pond D2	5.61	8.53	31.2	131.2
Pond E1	3.60	6.57	9.4	32.0
Pond E2	5.94	9.67	97.0	260.0
Pond F	2.42	3.48	3.5	41.0
Pond G	1.41	2.20	1.1	33.0
Pond H	1.57	2.35	1.7	35.3
Pond I	0.91	1.38	1.0	21.0
Pond J	0.86	1.25	0.4	20.3
Pond K	0.26	0.47	0.1	5.6

EXISTING VERSUS DEVELOPED RUNOFF SUMMARY TABLE

DESIGN POINT	EXISTING RUNOFF		DESIGN POINT	DEVELOPED RUNOFF		COMMENTS
	5 YR (CFS)	100 YR (CFS)		5 YR (CFS)	100 YR (CFS)	
1	10.5	58.8	1	8.5	28.0	
2	141.0	458.0	7c	121.0	420.0	"C" BASINS
3	29.7	166.5	10b	31.2	131.2	"D" BASINS
4	104.0	286.0	14a	97.0	260.0	"E" BASINS
5	19.3	113.7	15a	3.5	41.0	BASIN F
6	7.9	44.1	16	2.0	33.0	BASIN G
7	12.3	73.2	17	2.0	35.3	BASIN H
8	12.4	74.1	18	15.1	71.0	BASIN I
9	9.0	55.9	19	11.2	58.6	BASIN J
10	2.1	15.2	20	2.1	12.9	BASIN K





UNPLATTED ROLLING HILLS RANCH

ETRIB CHANNEL TO BE SELECTIVELY ARMORED FROM FONTAINE BOULEVARD NORTH TO PROPERTY LINE SEE KIOWA DBPS (REIMBURSABLE) DESIGN Q100=4750cfs

FUTURE BRIDGE OVER JCC (REIMBURSABLE) DESIGN Q100=4750cfs

ETRIB CHANNEL RECONSTRUCTED IN 2013 FROM ET-3 NORTH TO FONTAINE BLVD. SEE SHEET 3

CORE ENGINEERING GROUP
 15004 1ST AVENUE S
 PH: 719.570.1100
 CONTACT: RICHARD L. SCHINDLER, P.E.
 EMAIL: Rich@cegi.com

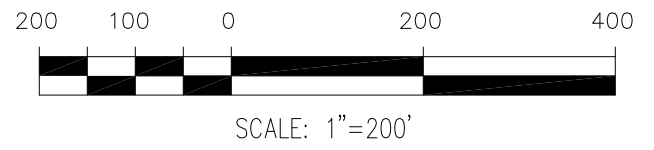
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 DESCRIPTION: _____
 NO: _____
 DRAWN: RLS
 DESIGNED: LAB
 CHECKED: RLS

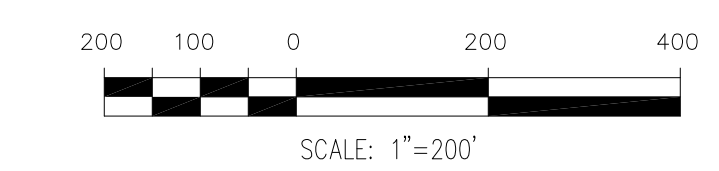
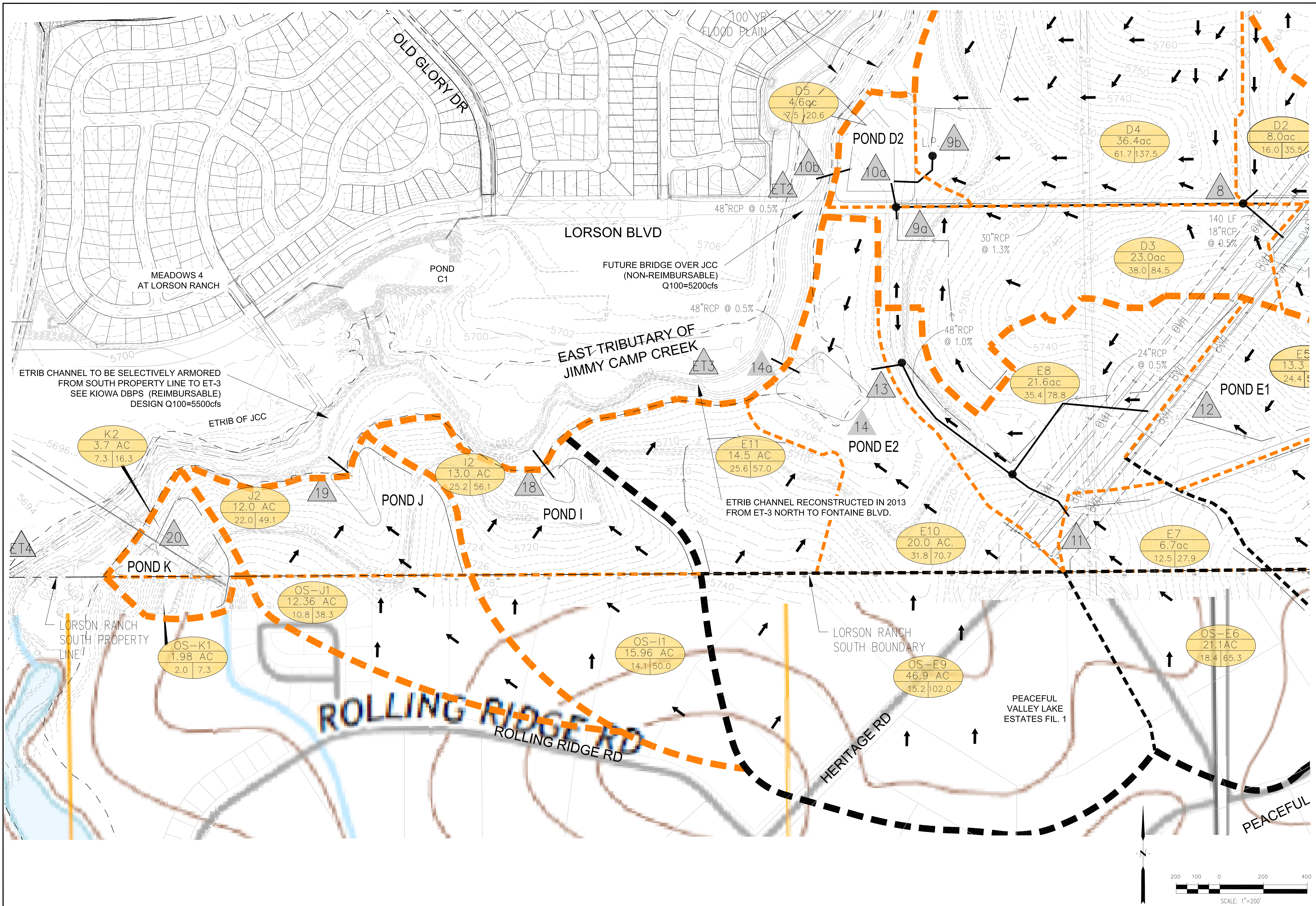
PREPARED FOR: LORSON LLC
 212 NORTH WAHSATCH AVE, SUITE 301
 COLORADO SPRINGS, COLORADO 80903 (719) 635-5200
 CONTACT: DAVE COCCINI

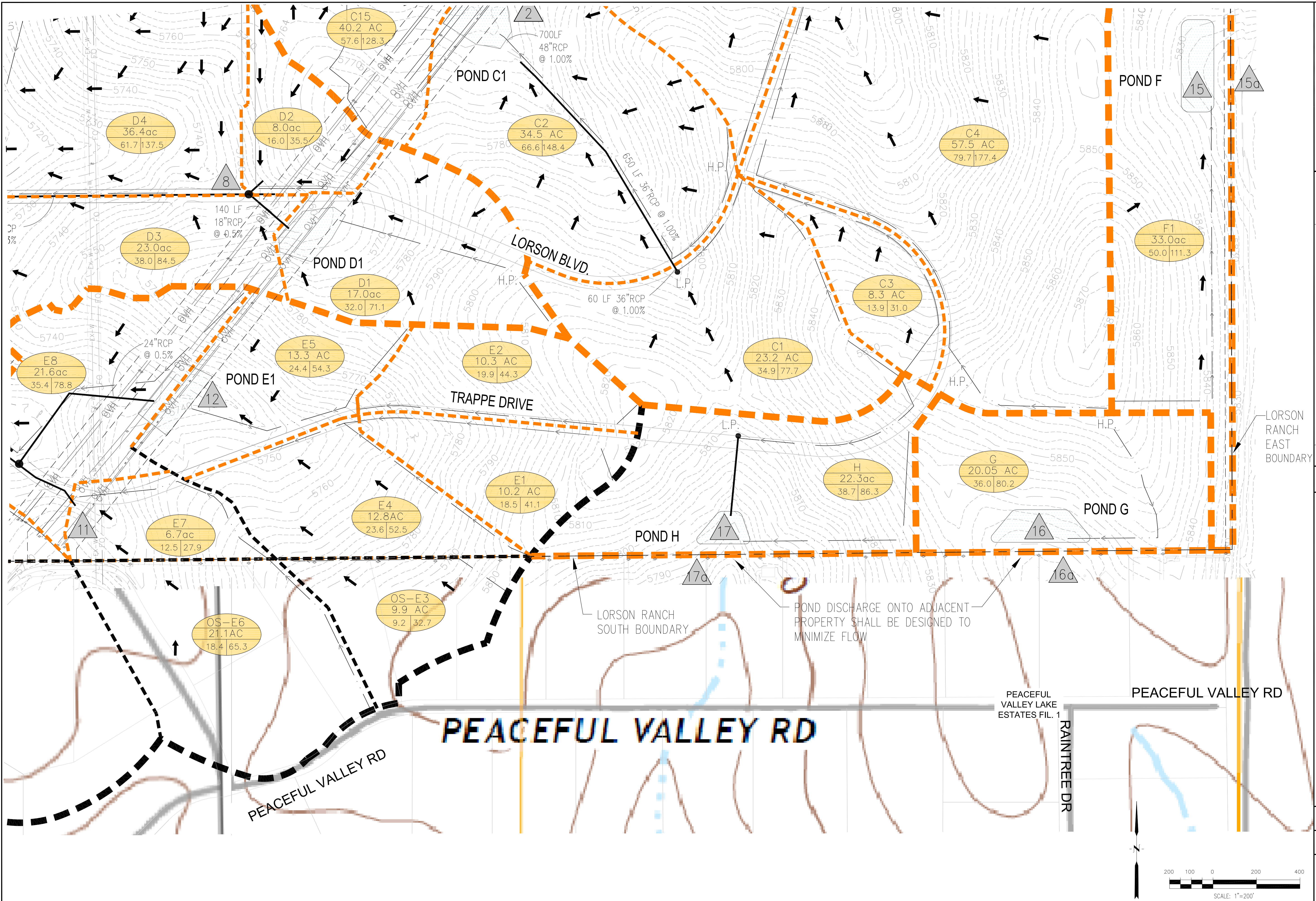
PROJECT: LORSON RANCH EAST MDDP
 EAST OF THE EAST TRIBUTARY
 EL PASO COUNTY, COLORADO

DEVELOPED CONDITIONS
LORSON RANCH EAST MDDP
NORTHWEST AREA

DATE: JUNE, 2017
 PROJECT NO. 100.013
 SHEET NUMBER 2
 TOTAL SHEETS: 5

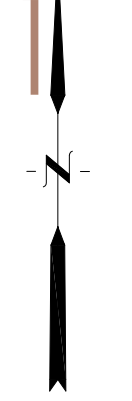
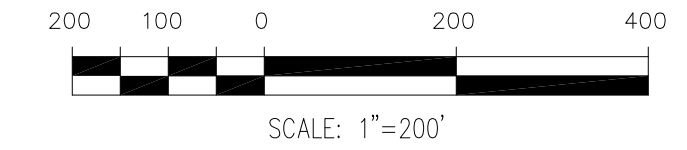


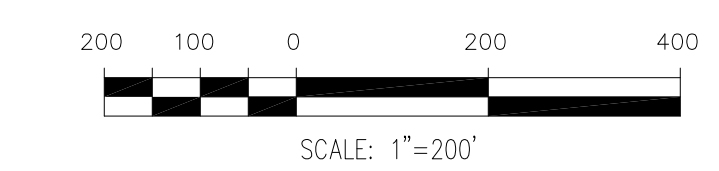
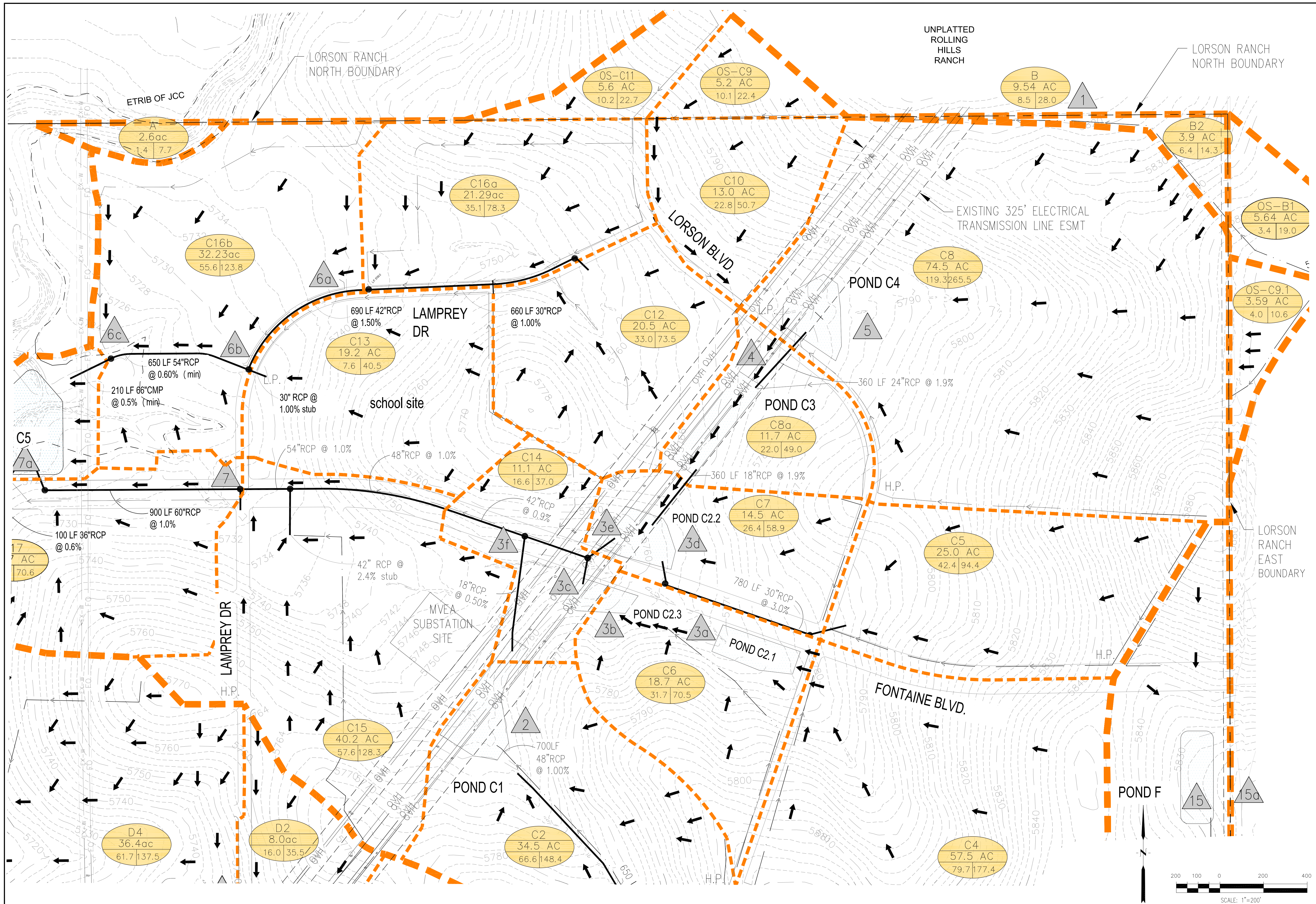




DATE	
DESCRIPTION	
NO.	
PREPARED FOR:	LORSON LLC 212 NORTH WATCH AVE. SUITE 301 COLORADO SPRINGS, COLORADO 80903 (719) 635-3200 CONTACT: DAVE COCCINI
PROJECT:	LORSON RANCH EAST MDDP EAST OF THE EAST TRIBUTARY EL PASO COUNTY, COLORADO
DRAWN:	RLS
DESIGNED:	LAB
CHECKED:	RLS

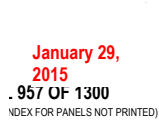
DEVELOPED CONDITIONS
LORSON RANCH EAST MDDP
SOUTHEAST AREA





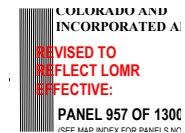
Markup Summary

alex.dabdub (4)

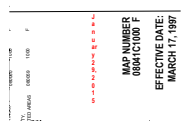


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January 29, 2015

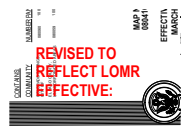


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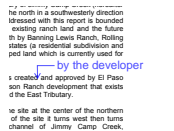
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January 29, 2015



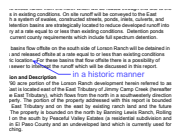
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dsdrice (56)



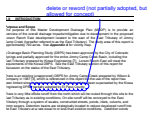
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Author: dsdrice
Date: 8/14/2017 8:29:04 AM
Color: ■

by the developer



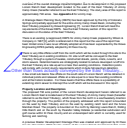
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Author: dsdrice
Date: 8/14/2017 8:27:39 AM
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in a historic manner



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Page Label: 4
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Author: dsdrice
Date: 8/2/2017 2:45:41 PM
Color: ■

delete or reword (not partially adopted, but allowed for concept)



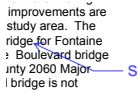
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Other than flows actually conveyed by the East Tributary...



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Checkmark: Unchecked
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Date: 8/2/2017 2:45:49 PM
Color: ■

delete or reword (not partially adopted, but allowed for concept)



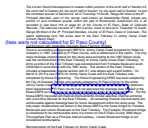
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Date: 8/2/2017 2:55:29 PM
Color: ■

s



Subject: Cloud+
Page Label: 5
Lock: Unlocked
Status:
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Author: dsdrice
Date: 8/2/2017 2:54:52 PM
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reimbursable in accordance with adopted DBPS -- improvements from the new DBPS need to go through the process



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Page Label: 5
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Date: 8/2/2017 2:48:00 PM
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(fees were not calculated for El Paso County)

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Date: 8/2/2017 2:57:03 PM
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see below

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Author: dsdrice
Date: 8/14/2017 8:33:55 AM
Color: ■

in conformance with (?)

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Author: dsdrice
Date: 8/2/2017 3:03:34 PM
Color: ■

see previous comments

Subject: Cloud+
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Author: dsdrice
Date: 8/2/2017 3:02:22 PM
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see previous comments

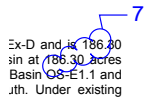
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Author: dsdrice
Date: 8/2/2017 3:09:05 PM
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bedrock

Subject: Cloud+
Page Label: 9
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Status:
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Author: dsdrice
Date: 8/2/2017 3:19:10 PM
Color: ■

100 and 280?

Point 3 respectively



Subject: Cloud+
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Status:
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Date: 8/2/2017 3:18:00 PM
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7

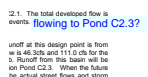
5.2 cfs for



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Date: 8/2/2017 3:29:28 PM
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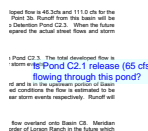


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Date: 8/14/2017 10:27:02 AM
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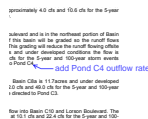
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Author: dsdrice
Date: 8/14/2017 10:02:43 AM
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flowing to Pond C2.3?



Subject: Text Box
Page Label: 12
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:02:04 AM
Color: ■

Is Pond C2.1 release (65 cfs) flowing through this pond?



Subject: Callout
Page Label: 12
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:16:31 AM
Color: ■

add Pond C4 outflow rates

add the inflow values

Subject: Callout
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:13:59 AM
Color: ■

add the inflow values

discuss overflow path for developed flows

Subject: Callout
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:13:32 AM
Color: ■

discuss overflow path for developed flows

add the inflow values

Subject: Callout
Page Label: 13
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:12:49 AM
Color: ■

add the inflow values

Discuss pond designs and modeling ponds in series.

Subject: Text Box
Page Label: 13
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:32:41 AM
Color: ■

Discuss pond designs and modeling ponds in series.

from Lamprey Dr.?

Subject: Cloud+
Page Label: 14
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:23:09 AM
Color: ■

from Lamprey Dr.?

show on plan

Subject: Callout
Page Label: 14
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:20:15 AM
Color: ■

show on plan

an C17 and in the flow into Pond C5 from
east 200 S ds for the 5-year and 100-year
OR will flow north to Pond C5. When the
is prepared the actual extent from area 1.
CS The developed flows are 204 cfs and
westward. Discuss pond design,
add contributing acreage
of CS. The developed flows are 115 cfs
westward and flow west into the
the existing conditions flow into the Basin
handling which develop north to the Basin

Subject: Callout
Page Label: 15
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:32:05 AM
Color: ■

Discuss pond design, add contributing acreage

an C17 and in the flow into Pond C5 from
east 200 S ds for the 5-year and 100-year
OR will flow north to Pond C5. When the
is prepared the actual extent from area 1.
CS The developed flows are 204 cfs and
westward. Discuss pond design,
add contributing acreage
of CS. The developed flows are 115 cfs
westward and flow west into the
the existing conditions flow into the Basin
handling which develop north to the Basin

Subject: Callout
Page Label: 15
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:29:52 AM
Color: ■

Discuss pond D1 design

an C17 and in the flow into Pond C5 from
east 200 S ds for the 5-year and 100-year
OR will flow north to Pond C5. When the
is prepared the actual extent from area 1.
CS The developed flows are 204 cfs and
westward. Discuss pond design,
add contributing acreage
of CS. The developed flows are 115 cfs
westward and flow west into the
the existing conditions flow into the Basin
handling which develop north to the Basin

Subject: Callout
Page Label: 16
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:31:33 AM
Color: ■

Discuss pond D2 design

an C17 and in the flow into Pond C5 from
east 200 S ds for the 5-year and 100-year
OR will flow north to Pond C5. When the
is prepared the actual extent from area 1.
CS The developed flows are 204 cfs and
westward. Discuss pond design,
add contributing acreage
of CS. The developed flows are 115 cfs
westward and flow west into the
the existing conditions flow into the Basin
handling which develop north to the Basin

Subject: Callout
Page Label: 17
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:36:33 AM
Color: ■

Discuss pond E2 design

Basin E4-E5 at Design Point 12
The local flows reaching Point 12 at Design Point 12 from
200 S ds for the 5-year and 100-year storm events respec
Basin E2
This E2 basin is located directly south of Basin C5
Down where a storm sewer will convey the flow west to D
Basin. This basin area is 12.5 acres and 27.5 cfs for the
respectively. DP11?
Design Point 11
This DP11 is located on Trappa Drive where a 48
flow reach to Design Point 13. The developed flows are
89 cfs for the 5-year and 100-year events respectively.
Basin E6
This E6 basin is located directly north of Basin E7

Subject: Callout
Page Label: 17
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:35:49 AM
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DP11?

Basin E1-E3 at Design Point 13
The local flows reaching Point 13 at Design Point 13 from
200 S ds for the 5-year and 100-year storm events respec
Basin E1
This E1 basin is located directly north of Point E1. The developed flows from the
are 204 cfs for the 5-year and 100-year events respectively.
Design Point 14
This DP14 is located on Trappa Drive where a 48
flow reach to Design Point 15. The developed flows are
89 cfs for the 5-year and 100-year events respectively.
Basin E7
This E7 basin is located directly north of Basin E7

Subject: Callout
Page Label: 17
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:34:24 AM
Color: ■

Discuss pond E1 design

west corner of the study area. It is 20.05 acres in size and is proposed to be developed with a residential density of 10 units per acre. The site is bounded by the southern boundary and to the east by the site boundary. The site is bounded by the southern boundary and to the east by the site boundary. The site is bounded by the southern boundary and to the east by the site boundary.

Subject: Cloud+
Page Label: 18
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:39:41 AM
Color: ■

?

property
erm. It i
evaluatec

Subject: Highlight
Page Label: 18
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:39:47 AM
Color: ■

... ..

Subject: Callout
Page Label: 18
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Author: dsdrice
Date: 8/14/2017 10:37:41 AM
Color: ■

Discuss pond F design

... ..
y.
where?
is 20.05 acres in size
the southern boundary

Subject: Cloud+
Page Label: 18
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:38:29 AM
Color: ■

where?

... ..

Subject: Callout
Page Label: 18
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:39:02 AM
Color: ■

Discuss pond G design

... ..

Subject: Cloud+
Page Label: 18
Lock: Unlocked
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Author: dsdrice
Date: 8/11/2017 4:21:11 PM
Color: ■

full-spectrum sizing is based on contributing
impervious area

... and is located adjacent to the East Tributary. It detains, treats runoff, and discharges it north to ... 1.0cfs and 21.1cfs respectively for the 5-year storm. Basin OS-11 is routed around Pond J and will ...

Subject: Callout
Page Label: 19
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:43:25 AM
Color: ■

how? by swale?

... the southwest corner of the site, is adjacent to the East Tributary and basin OS-11. The developed flow is 18.1 cfs for the 100-year event and flows. These flows closely mimic the East Tributary. Table 6.2 for a comparison of ...

Subject: Callout
Page Label: 19
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:41:47 AM
Color: ■

consisting of future residential lots?

... the southwest corner of the site, is adjacent to the East Tributary and basin OS-11. The developed flow is 18.1 cfs for the 100-year event and flows. These flows closely mimic the East Tributary. Table 6.2 for a comparison of ...

Subject: Callout
Page Label: 20
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:47:58 AM
Color: ■

consisting of future residential lots?

... and is located adjacent to the East Tributary. It detains, treats runoff, and discharges it north to ... 0.4cfs and 20.3cfs respectively for the 5-year storm. Basin OS-11 is routed around Pond J and will ...

Subject: Callout
Page Label: 20
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Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:48:54 AM
Color: ■

how? by swale?

... the southwest corner of the site, is adjacent to the East Tributary and basin OS-11. The developed flow is 18.1 cfs for the 100-year event and flows. These flows closely mimic the East Tributary. Table 6.2 for a comparison of ...

Subject: Callout
Page Label: 20
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:49:00 AM
Color: ■

how? by swale?

... the southwest corner of the site, is adjacent to the East Tributary and basin OS-11. The developed flow is 18.1 cfs for the 100-year event and flows. These flows closely mimic the East Tributary. Table 6.2 for a comparison of ...

Subject: Cloud+
Page Label: 20
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/14/2017 10:52:30 AM
Color: ■

Reword that reimbursement may be requested through the DCM and Drainage Board process.

red volumes of the 5-year, e see the plan in the back are schematic. All plans are designed. All as part of the preliminary.

This needs to be clarified.

Release Rate	100-year	5-year	100-year
	17.7	3.0	17.7
	65.0	11.0	65.0

Subject: Cloud+
Page Label: 21
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Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/15/2017 12:55:13 PM
Color: ■

This needs to be clarified.

Subject: Callout
Page Label: 21
Lock: Unlocked
Status:
Checkmark: Unchecked
Author: dsdrice
Date: 8/15/2017 12:57:08 PM
Color: ■

Add contributing area column

See Table 6.1 below for the required volumes of the release rates of each pond. Please see the plan in 1 location. The detention ponds shown are schematic; greater detail when the localized plans are design and full spectrum detention design as part of the pre

of Data (full-spectrum (?))

100-year Volume (Ac-ft)	Release Rate 5-year (cfs)	Release Rate 100-year (cfs)
10.23	3.0	17.7
8.20	11.0	65.0

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Date: 8/15/2017 12:56:02 PM
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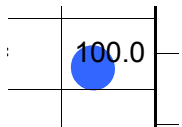
(full-spectrum (?))

These seem high for existing. Provide land use/impervious table and coefficients tables.

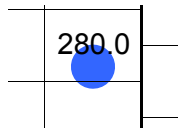
100-year Volume (Ac-ft)	Release Rate 5-year (cfs)	Release Rate 100-year (cfs)
10.23	3.0	17.7
8.20	11.0	65.0

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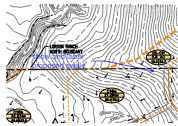
These seem high for existing. Provide land use/impervious table and coefficients tables.



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Date: 8/2/2017 3:20:11 PM
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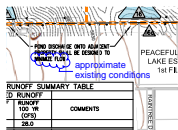
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Date: 8/14/2017 10:20:57 AM
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show and label proposed swale



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Date: 8/14/2017 10:47:24 AM
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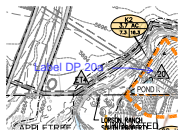
Label DP 19a



REVISION SUMMARY TABLE	
NO.	COMMENTS
1	
2	
3	

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Author: dsdrice
Date: 8/11/2017 2:15:09 PM
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approximate existing conditions



Subject: Callout
Page Label: 166
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Date: 8/14/2017 10:48:20 AM
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Label DP 20a



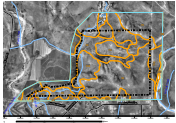
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Label DP 18a

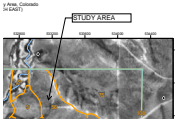


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Show proposed grading on sheets 2-5

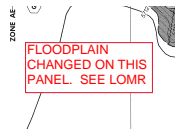


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STUDY AREA



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FLOODPLAIN CHANGED ON THIS PANEL. SEE LOMR



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Date: 6/5/2017 11:38:41 AM
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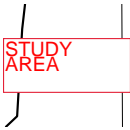


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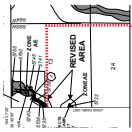


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Date: 6/5/2017 11:42:11 AM
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STUDY
AREA



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STUDY
AREA

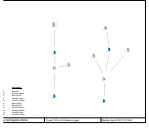


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42" RCP



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Date: 5/19/2017 5:19:42 AM
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