

ENTECH ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

SOIL, GEOLOGY, GEOLOGIC HAZARD, AND WASTEWATER STUDY, JUDGE ORR ROAD RV PARK AND STORAGE 14010 JUDGE ORR ROAD PARCEL NO. 42330-00-027 EL PASO COUNTY, COLORADO

Prepared for

WILLIAM GUMAN AND ASSOCIATIES, LTD.

731 North Weber Street, Suite 10 Colorado Springs, Colorado 80903

Attn: Bill Guman

Per Chapter 11 Section 11.3.3 of the El Paso County Drainage Criteria Manual recommendations for the foundation preparation and embankment construction shall be submitted with the complete design analysis for all permanent detention facilities.

December 12, 2016

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Logan L. Langford Geologist

LLL/rm

Encl.

Entech Job No. 160533 AAprojects/2016/160533 countysoil/geo/ww Reviewed by:

Add "PCD File No. PPR-16-040"

Entech Engineering, Inc.

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SOIL, GEOLOGY, GEOLOGIC HAZARD, AND WASTEWATER STUDY, JUDGE ORR ROAD RV PARK AND STORAGE 14010 JUDGE ORR ROAD PARCEL NO. 42330-00-027 EL PASO COUNTY, COLORADO

1.0 INTRODUCTION

Project Location

The project lies in a portion of the SW ¼ of Section 33, Township 12 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado at 14010 Judge Orr Road, Parcel No. 42330-00-027. The site is located approximately 2½ miles northeast of Falcon, Colorado.

Project Description

Total acreage involved in the project is approximately 40 acres. The proposed site development consists of six hundred and thirty-one (631) boat/trailer storage bays, forty (40) RV camp spaces, and associated site improvements. The RV Park is anticipated to be serviced by an individual well and on-site wastewater treatment system. Future phases will include additional RV camp spaces.

Scope of Report

This report presents the results of our geologic evaluation, treatment of engineering geologic hazard study and wastewater study for an on-site wastewater treatment system.

Land Use and Engineering Geology

This site was found to be suitable for the proposed development. Areas were encountered where the geologic conditions will impose some constraints on development and land use. These include areas of seasonal shallow groundwater areas, potentially seasonal shallow groundwater, ponded water, drainage areas, flood plain, and artificial fill. Based on the proposed development plan, it appears that these areas will have some impact on the development. These conditions will be discussed in greater detail in the report.

In general, it is our opinion that the development can be achieved if the observed geologic conditions on site are either avoided or properly mitigated. All recommendations are subject to the limitations discussed in the report.

2.0 GENERAL SITE CONDITIONS AND PROJECT DESCRIPTION

The site is located in a portion of the SW ¼ of Section 33, Township 12 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado. The site is located approximately 2½ miles northeast of Falcon, Colorado, on Judge Orr Road, east of Highway 24. The location of the site is as shown on the Vicinity Map, Figure 1.

The topography of the site is gently sloping generally to the southeast. The drainages on site flow in southerly and easterly direction through the property, and easterly in the flood plain located in the northeast corner of the site. Water was not observed flowing in drainages at the time of this investigation, a small pool of water was observed in the pond located in the southeast portion of the site. A single-story house and barn are present in the southwest portion the property and are to remain. Several travel trailers are currently parked in the southwest portion of the property in the area of the existing house and barn. The site boundaries are indicated on the USGS Map, Figure 2. Previous land uses have included grazing and pasture land. The site contains primarily field grasses, weeds, yuccas, cacti, scattered shrubs, and scattered trees along the southern portion of the property and around the existing house and barn. Site photographs, taken December 5, 2016, are included in Appendix A.

Total acreage involved in the proposed development is approximately 40 acres. The proposed site development consists of six hundred and thirty-one (631) boat/trailer storage bays, forty (40) RV camp spaces, and associated site improvements. The RV Park is anticipated to be serviced by an individual well and on-site wastewater treatment system. The proposed Development Plan is presented in Figure 3. Future phases will have additional RV camp spaces.

3.0 SCOPE OF THE REPORT

The scope of the report will include the following:

- A general geologic analysis utilizing published geologic data. Detailed site-specific mapping
 will be conducted to obtain general information in respect to major geographic and geologic
 features, geologic descriptions and their effects on the development of the property.
- The site will be evaluated for an on-site wastewater treatment system in accordance with El Paso Land Development Code.

4.0 FIELD INVESTIGATION

Our field investigation consisted of the preparation of a geologic map of any bedrock features and significant surficial deposits. The Natural Resource Conservation Service (NRCS), previously the Soil Conservation Service (SCS) survey was also reviewed to evaluate the site. The position of mappable units within the subject property are shown on the Geologic Map. Our mapping procedures involved both field reconnaissance and measurements and air photo reconnaissance and interpretation. The same mapping procedures have also been utilized to produce the Engineering Geology Map which identified pertinent geologic conditions affecting development. The field mapping was performed by personnel of Entech Engineering, Inc. on December 5, 2016.

One (1) percolation test, and four (4) tactile test pits were performed on the site to determine general suitability of the site for the use of an on-site wastewater treatment system. The locations of the profile hole boring, and test pits are indicated on the Development Plan/Test Boring Location Map, Figure 3. Percolation test holes were placed adjacent to the test pits. The Profile Hole and Test Pit Logs are presented in Appendix B. Results of this testing will be discussed later in this report.

Laboratory testing was also performed on some of the soils to classify and determine the soils engineering characteristics. Laboratory tests included grain-size analysis, ASTM D-422, and Atterberg Limits, ASTM D-4318. Results of the laboratory testing are included in Appendix C. A Summary of Laboratory Test Results is presented in Table 1.

5.0 SOIL, GEOLOGY AND ENGINEERING GEOLOGY

5.1 General Geology

Physiographically, the site lies in the western portion of the Great Plains Physiographic Province. Approximately 16 miles to the west is a major structural feature known as the Rampart Range Fault. This fault marks the boundary between the Great Plains Physiographic Province and the Southern Rocky Mountain Province. The site exists within the southeastern edge of a large structural feature known as the Denver Basin. Bedrock in the area tends to be very gently dipping in a northeasterly direction (Reference 1). The rocks in the area of the site are sedimentary in nature and typically Tertiary to Upper Cretaceous in age. The bedrock underlying the site consists of the Dawson Arkose Formation. Overlying this formation are unconsolidated deposits of residual, man-made fill, and alluvial soils of the Quaternary Age. The residual soils are produced by the in-situ action of weathering of the bedrock on site. The alluvial soils were deposited by water in the major drainages on site and as stream terraces on some of the ridge lines. Man-made soils exist as earthen dams and erosion berms. The site's stratigraphy will be discussed in more detail in Section 5.3.

5.2 Soil Conservation Survey

The Natural Resource Conservation Service (Reference 2), previously the Soil Conservation Service (Reference 3) has mapped two soil types on the site (Figure 4). In general, they vary from gravelly sandy loam to very gravelly loamy sand. The soils are described as follows:

<u>Type</u>	<u>Description</u>
19	Columbine Gravelly Sandy Loam, 0-3% slopes

Complete description of the soil type is presented in Appendix D. The soils have generally been described to have moderate to moderately rapid permeabilities. Roads may need to be designed to minimize frost-heave potential. Possible hazards with soil erosion are present on the site. The erosion potential can be controlled with vegetation. The majority of the soils have been described to have slight to moderate erosion hazards.

5.3 Site Stratigraphy

The Falcon Quadrangle Geology Map showing the site is presented in Figure 5 (Reference 4). The Geology Map prepared for the site is presented in Figure 6. Four mappable units were identified on this site, which are described as follows:

- **Qal Alluvium of recent Holocene Age:** These are recent deposits that have been deposited along the drainages that exist on-site. These materials typically consist of silty to clayey sands and sandy clays. Some of these alluviums contain highly organic soils.
- Qaf Artificial Fill of Holocene Age: These are man-made fill deposits associated with erosion berms and earthen dam on-site.
- Qp Piney Creek Alluvium of Holocene Age: This material is a water-deposited alluvium, typically classified as a silty to well-graded sand, brown to dark brown in color and of moderate density. The Piney Creek Alluvium can sometimes be very highly stratified containing thin layers of very silty and clayey soil.
- Broadway Alluvium of Late Pleistocene Age: These materials consist of lower stream terrace deposits. The Broadway Alluvium typically consists of silty to clayey gravelly sands. This deposit is usually highly stratified and may contain lenses of silt, clay or cobbles.

The soils listed above were mapped from site-specific mapping, the *Geologic Map of the Falcon Quadrangle* distributed by the Colorado Geological Survey in 2012 (Reference 4), the *Geologic Map of the Colorado Springs-Castle Rock Area*, distributed by the US Geological Survey in 1979 (Reference 5), and the *Geologic Map of the Denver 1º x 2º Quadrangle*, distributed by the US Geological Survey in 1981 (Reference 6). The Test Borings and Profile Holes were also used in evaluating the site and are included in Appendix B. The Geology Map prepared for the site is presented in Figure 6.

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5.4 Soil Conditions

The soils encountered in the Profile Hole and Tactile Test Pits can be grouped into four general

soil and rock types. The profile hole soils were classified using the Unified Soil Classification

System (USCS). The test pit soils were classified using the USDA Textural Soil Classification.

Soil Type 1 is a clayey sand (SC), was encountered in the upper soil profile in the profile hole

and test pits. These soils were encountered at medium dense states and at moist conditions.

An expansion pressure of 430 psf was determined from a sample of the clayey sand, which

indicates a low expansion potential. Samples tested had 19 to 34 percent passing the No. 200

Sieve.

Soil Type 2 is a sandy clay and clay (CL), was encountered in the profile hole and it Test Pit

Nos. 1 and 2. The soils were encountered at firm consistencies and moist conditions. Samples

tested had 66 to 90 percent passing the No. 200. Sieve.

Soil Type 3 is a sandy claystone (CL), was encountered in all of the test pits at depths ranging

from 1 to 8 feet below the surface. The claystone was encountered at hard to consistencies and

moist conditions.

Soil Type 4 is a very clayey sandstone (SC), was encountered in the profile hole at depths

ranging from 8 feet below the surface and extended to the termination of the boring (20 feet).

The claystone was encountered at hard to very hard consistencies and moist conditions. The

sample tested had 46 percent passing the No. 200 sieve.

The Test Boring Logs and the Profile Hole Logs are presented in Appendix B. Laboratory Test

Results are presented in Appendix C. A Summary of Laboratory Test Results is presented in

Table 1.

5.5 Groundwater

Groundwater was not encountered in the profile hole or test pits which was drilled to 20 feet and

excavated to 8 feet. Signs of seasonally shallow groundwater were observed in the test pits at

depths ranging from 31/2 to 6 feet. Areas of seasonal shallow groundwater and ponded water

have been mapped in the pond, low-lying areas and in the drainages on-site. These areas are

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discussed in the following section. Fluctuation in groundwater conditions may occur due to variations in rainfall and other factors not readily apparent at this time.

It should be noted that in the sandy materials on site, some groundwater conditions might be encountered due to the variability in the soil profile. Isolated sand and gravel layers within the soils, sometimes only a few feet in thickness and width, can carry water in the subsurface. Groundwater may also flow on top of the underlying bedrock. Planners should be cognizant of the potential for the occurrence of such subsurface water features during construction on-site and deal with each individual problem as necessary at the time of construction.

6.0 ENGINEERING GEOLOGY – IDENTIFICATION AND MITIGATION OF GEOLOGIC HAZARDS

As mentioned previously, detailed mapping has been performed on this site to produce an Engineering Geology Map (Figure 6). This map shows the location of various geologic conditions of which the developers should be cognizant during the planning, design and construction stages of the project. These hazards and the recommended mitigation techniques are as follows:

Groundwater and Floodplain Areas

Areas within the drainages on-site have been identified as areas of seasonally high groundwater areas, potentially seasonally high groundwater areas and floodplains. Additionally, areas of ponded water also exist on-site. Water was not flowing in the any of the drainages at the time of this investigation. The drainage located in the northeast corner of the property has been mapped as a floodplain zone according to the FEMA Map No. 08041CO575F Figure 7 (Reference 7). These areas are discussed as follows:

Floodplain: It is anticipated that the proposed improvements will not be within the floodplain zone at the northeast corner of the site. Development within the floodplain would require approval of the Drainage Plan prior to construction. Building areas within the floodplain will require filling to raise the building area above floodplain and seasonally high groundwater levels. Mitigation for Seasonally High Groundwater levels discussed in the following sections is recommended for construction in the floodplain zone. Finished floor levels must

be one foot above the floodplain level. Exact floodplain locations and drainage studies are beyond the scope of this report.

<u>Potentially Seasonal High Groundwater:</u> In these areas, we would anticipate the potential for periodically high subsurface moisture conditions and possible frost heave potential, depending on the soil conditions. It is our understanding that the areas will be regraded.

Mitigation: Due to the proposed use as RV Storage and camp sites the regrading will mitigate these areas. Foundations if installed in these areas are subject to severe frost heave potential should penetrate sufficient depth so as to discourage the formation of ice lenses beneath foundations. At this location and elevation, a foundation depth for frost protection of 30-inch is recommended. In areas where high subsurface moisture conditions are anticipated periodically, a subsurface perimeter drain will be necessary to help prevent the intrusion of water into areas located below grade. A typical perimeter drain detail is presented in Figure 8. Additionally, swales should be created to intercept surface runoff and carry it safely around and away from structures. It is anticipated that the site grading may mitigate the drainages on the property. The water table may be of sufficient depth to minimize the effects on buildings in some areas.

<u>Seasonally High Groundwater Area</u>: In these areas, high subsurface moisture condition, frost heave potential and highly organic soils may exist, particularly on a seasonal basis. The majority of the areas will be mitigated with site grading.

Mitigation: In areas where development is planned, overlot grading will mitigate the drainages. All organic material, soft or wet soils should be removed prior to any filling. The same mitigation recommendations for potentially high groundwater areas as discussed previously should be followed in these areas of seasonally high groundwater. In some areas, it may be necessary to dewater the excavation. Any grading should be done in a manner that directs surface flow around construction to avoid areas of ponded water. Structures should not block drainages, but swales should be created to intercept surfacerunoff and carry it safely around and away from structures. Additional investigation will be necessary to determine the water depth and its affect on development. Other areas than those mapped could encounter groundwater that could affect shallow foundations onsite.

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Areas of Ponded Water: This the area where water is ponded behind earthen dam on-site. This area will likely be removed during site grading. Should construction be considered in these areas, regrading will be necessary in order to fill the area above the groundwater level. All soft or organic soils should be removed prior to filling. The same mitigation techniques for seasonally high groundwater areas are recommended for these ponded

areas as well.

6.1 Relevance of Geologic Conditions to Land Use Planning

As mentioned earlier in this report, we understand that the development will be recreational vehicle park and storage. It is our opinion that the existing geologic and engineering geologic conditions will impose some constraints on the proposed development and construction. The most significant problems affecting development will be those associated with the drainages on site that may be satisfactorily mitigated through site grading, engineering design, and construction practices.

The upper materials are typically at medium dense states. The granular soils encountered in the upper soil profiles of the profile hole and tactile test pits should provide good support for foundations. Expansive soils were encountered in the area tested for the on-site wastewater treatment system. It is anticipated that overlot grading will be used to mitigate the drainage area where the expansive soils were encountered. Expansive layers may also be encountered in the soils in other areas on this site. Areas of expansive soils encountered on site are sporadic; therefore, none have been indicated on the maps. These soils will not prohibit development.

Areas of seasonal shallow groundwater and areas of ponded water were encountered on site. These areas will require overlot grading to mitigate the drainage areas and the pond located on this site. Absorption fields should not be located in these areas without site grading due to the potential for periodic high groundwater conditions.

In summary, development of the site can be achieved if the items mentioned above are mitigated. These items can be mitigated through proper design and construction or through avoidance.

7.0 ON-SITE WASTEWATER TREATMENT

The site was evaluated for an on-site wastewater treatment system for the RV camp area in accordance with El Paso Land Development Code. Due to the commercial project a designed system will be required. One (1) percolation test and four (4) tactile test pits were performed on the property. Percolation test and tactile test pits were located in anticipated location of the proposed on-site wastewater treatment system (OWTS) for the RV Park at the southeast corner of the site. The approximate locations of the test pits are indicated on Figure 3 and on the Septic Suitability Map, Figure 9. It should be noted that other areas of the site are likely suitable for OWTS systems. The proposed location was to maintain gravity flow. A table showing the results of the test pits and percolation test is presented in Table 2. The specific test results are presented in Appendix E of this report

The Natural Resource Conservation Service (Reference 2), previously the Soil Conservation Service (Reference 3) has been mapped with one soil descriptions. The Soil Survey Map (Reference 2) is presented in Figure 4, and the Soil Survey Descriptions are presented in Appendix D. The soils are described as having moderate to moderately rapid percolation rates.

The percolation rate was 80 minutes per inch. The percolation rate is not suitable for conventional on-site wastewater treatment systems. The percolation rate is slower than 60 minutes per inch which will require designed systems. Shallow bedrock was also encountered in the profile holes and test pits, and will also required a designed system. Additional drilling may identify areas where faster rates are encountered that are suitable for conventional systems.

Standard penetration testing, ASTM D-1586, was performed in each profile hole to evaluate the density of the soil and the presence of bedrock. Bedrock was encountered in The Profile Hole at 8 feet. Designed systems are required in areas of shallow bedrock.

Soils encountered in the tactile test pits consisted of sandy loam to gravelly sandy loam, gravelly sandy clay loam, sandy clay and clay with underlying sandy claystone. The limiting layer encountered in the test pits is the clay and sandy claystone, which corresponds to an LTAR value of 0.10 gallons per day per square foot. The bedrock was encountered at 3½ to 6½ feet in the test pits. The conditions encountered in the test pits will require a designed system.

Signs of seasonal shallow groundwater were observed at depths ranging from 3½ to 6 feet in the test pits.

Absorption fields must be maintained a minimum of 4 feet above groundwater or bedrock. Groundwater was encountered at 17 feet in the profile hole which was drilled to 20 feet. Signs of seasonally shallow groundwater were observed in Test Pit Nos. 1, 3, and 4 at depths ranging from 3½ to 6 feet. Shallow bedrock was encountered in the profile holes and test pits at depths ranging from 3½ to 6 feet.

The percolation rates measured are not suitable for conventional systems. Both tests had rates of slower than 60 minutes per inch. El Paso County guidelines require designed systems for percolation rates exceed 60 minutes per inch. Additional drilling may identify areas where conventional systems can be used. Bedrock was encountered in the profile hole and test pits at depths that would affect conventional systems. Due to the commercial use a designed system will be required.

In summary, it is our opinion the site is suitable for a on-site wastewater treatment system (OWTS) and that contamination of surface and subsurface water resources should not occur provided the OWTS sites are evaluated and installed according to El Paso County and State Guidelines and properly maintained. It is anticipated that a low pressure drip system, may be appropriate for this site. In addition, some pretreatment to lower BOD and nitrogen levels may be warranted. Based on the testing performed as part of this investigation and the type of project a designed system will be required. For design purposes a LTAR value of 0.10 gallons per day per square foot should be used. A Septic Suitability Map is presented in Figure 9. Absorption fields must be located a minimum of 180 feet from any well for the proposed design flow, including those on adjacent properties. Absorption fields must also be located a minimum of 130 feet from any ponded areas and 25 feet from dry gulches. It should be noted that additional testing will be required once overlot grading is completed.

8.0 ECONOMIC MINERAL RESOURCES

Some of the sandy materials on-site could be considered a low grade sand resource. According to the *El Paso County Aggregate Resource Evaluation Map* (Reference 8), the area is not mapped with any aggregate deposits. According to the *Atlas of Sand, Gravel and Quarry Aggregate Resources, Colorado Front Range Counties* distributed by the Colorado Geological Survey (Reference 9), areas of the site are not mapped with any resources. According to the *Evaluation of Mineral and Mineral Fuel Potential* (Reference 10), the area of the site has been mapped as "Good" for industrial minerals. However, considering the silty nature of much of these materials and abundance of similar materials through the region and the close proximity to developed land, they would be considered to have little significance as an economic resource.

According to the Evaluation of Mineral and Mineral Fuel Potential of El Paso County State Mineral Lands (Reference 10), the site is mapped within the Denver Basin Coal Region. However, the area of the site has been mapped as "Poor" for coal resources. No active or inactive mines have been mapped in the area of the site. No metallic mineral resources have been mapped on the site (Reference 10).

The site has been mapped as "Fair" for oil and gas resources (Reference 10). No oil or gas fields have been discovered in the area of the site. The sedimentary rocks in the area may lack the geologic structure for trapping oil or gas; therefore, it may not be considered a significant resource. Hydraulic fracturing is a new method that is being used to extract oil and gas from rocks. It utilizes pressurized fluid to extract oil and gas from rocks that would not normally be productive. The area of the site has not been explored to determine if the rocks underlying the site would be commercially viable utilizing hydraulic fracturing. The practice of hydraulic fracturing has come under review due to concerns about environmental impacts, health and safety.

9.0 EROSION CONTROL

The soil types observed on the site are mildly to highly susceptible to wind erosion, and moderately to highly susceptible to water erosion. A minor wind erosion and dust problem may be created for a short time during and immediately after construction. Should the problem be considered severe enough during this time, watering of the cut areas or the use of chemical palliative may be required to control dust. However, once construction has been completed and vegetation re-established, the potential for wind erosion should be considerably reduced.

With regard to water erosion, loosely compacted soils will be the most susceptible to water erosion, residually weathered soils and weathered bedrock materials become increasingly less susceptible to water erosion. For the typical soils observed on site, allowable velocities or unvegetated and unlined earth channels would be on the order of 3 to 4 feet/second, depending upon the sediment load carried by the water. Permissible velocities may be increased through the use of vegetation to something on the order of 4 to 7 feet/second, depending upon the type of vegetation established. Should the anticipated velocities exceed these values, some form of channel lining material may be required to reduce erosion potential. These might consist of some of the synthetic channel lining materials on the market or conventional riprap. In cases where ditch-lining materials are still insufficient to control erosion, small check dams or sediment traps may be required. The check dams will serve to reduce flow velocities, as well as provide small traps for containing sediment. The determination of the amount, location and placement of ditch linings, check dams and of the special erosion control features should be performed by or in conjunction with the drainage engineer who is more familiar with the flow quantities and velocities.

Cut and fill slope areas will be subjected primarily to sheetwash and rill erosion. Unchecked rill erosion can eventually lead to concentrated flows of water and gully erosion. The best means to combat this type of erosion is, where possible, the adequate re-vegetation of cut and fill slopes. Cut and fill slopes having gradients more than three (3) horizontal to one (1) vertical become increasingly more difficult to revegetate successfully. Therefore, recommendations pertaining to the vegetation of the cut and fill slopes may require input from a qualified landscape architect and/or the Soil Conservation Service.

10.0 CLOSURE

It is our opinion that the existing geologic engineering and geologic conditions will impose some constraints on development and construction of the site. The majority of these conditions can be mitigated through site grading, proper engineering design and construction practices. The proposed development and use is consistent with anticipated geologic and engineering geologic conditions.

It should be pointed out that because of the nature of data obtained by random sampling of such variable and non-homogeneous materials as soil and rock, it is important that we be informed of any differences observed between surface and subsurface conditions encountered in construction and those assumed in the body of this report. Additional investigations for OWTS systems will be required after the anticipated overlot grading is completed. Construction and design personnel should be made familiar with the contents of this report. Reporting such discrepancies to Entech Engineering, Inc. soon after they are discovered would be greatly appreciated and could possibly help avoid construction and development problems.

This report has been prepared for William Guman and Associates, LTD. for application to the proposed project in accordance with generally accepted geologic soil and engineering practices. No other warranty expressed or implied is made.

We trust that this report has provided you with all the information that you required. Should you require additional information, please do not hesitate to contact Entech Engineering, Inc.

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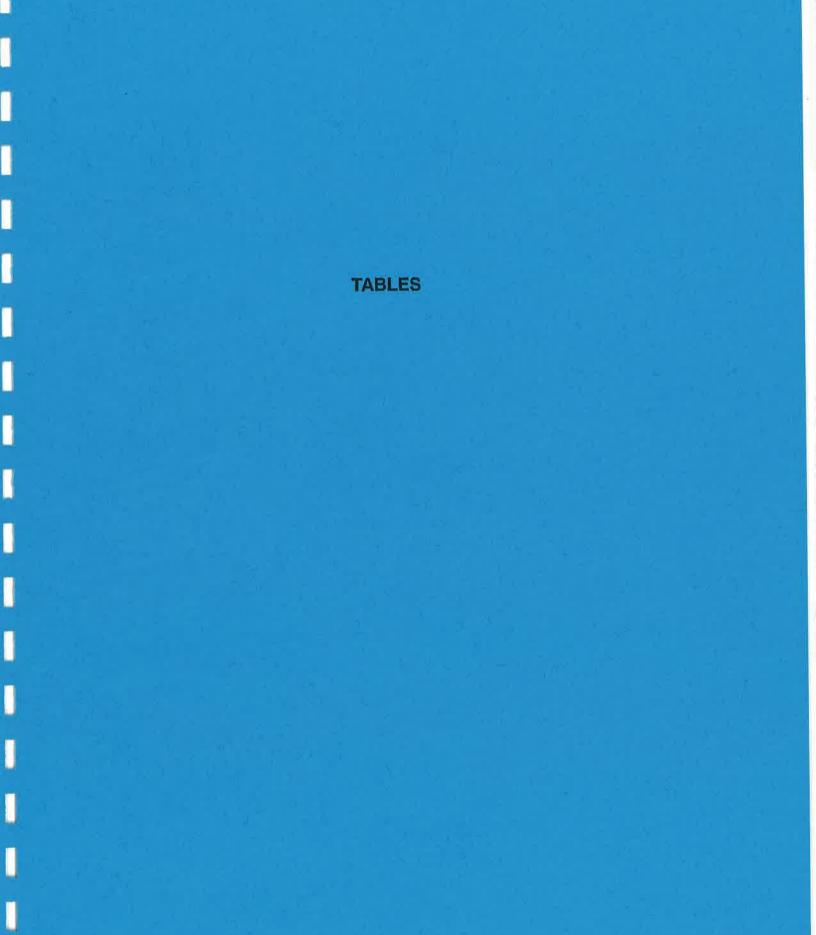


TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

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SOIL DESCRIPTION	SAND, CLAYEY	CLAY, SANDY	CLAY, SANDY	SANDSTONE, VERY CLAYEY				
UNIFIED	SC	SC	SC	SC	SC	ರ	ರ	SC
SWELL/ CONSOL (%)								
FHA SWELL (PSF)	430		=1					
SULFATE (WT %)								
PLASTIC INDEX (%)								
LIQUID LIMIT (%)								
PASSING NO. 200 SIEVE (%)	34.1	27.0	29.9	18.5	16.0	66.2	90.3	46.3
DRY F DENSITY NO (PCF)								
DEPTH WATER (FT)								
	2	GRAB	GRAB	GRAB	GRAB	5-6	2-3	15
TEST BORING NO.	-	P-4	P.9	P.3	P-4	TP-1	TP-2	-
SOIL	-		-		-			4

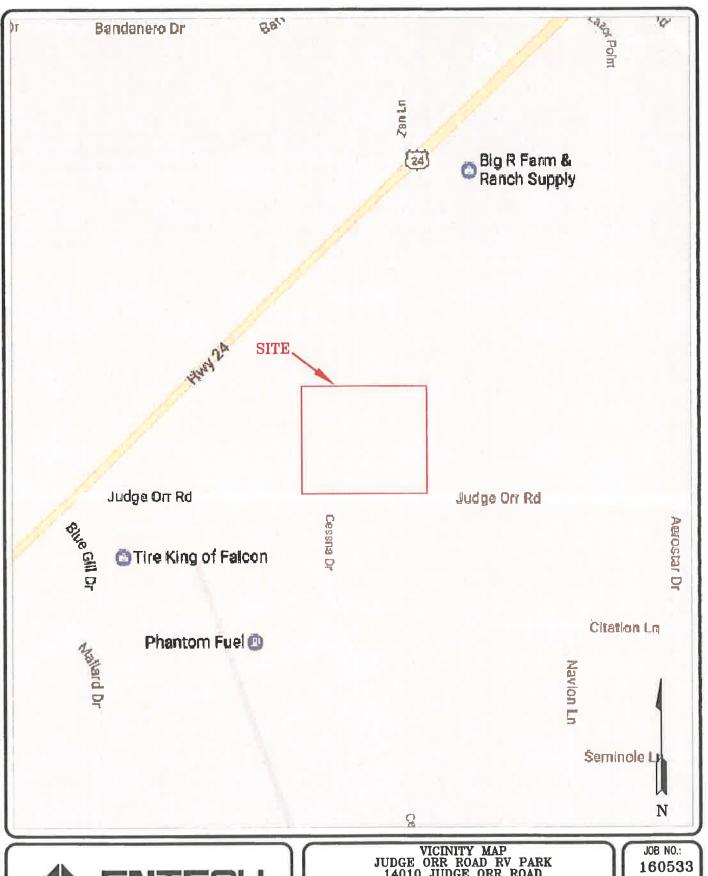
Table 2: Summary of Test Pits and Percolation Test Results

Test Pit No.	USDA Soil Type of	LTAR	Depth to	
	Limiting Layer	Value (1)	Bedrock (ft.)	
1	5	0.10	5	
2	5	0.10	6	
3	5	0.10	5.5	
4	5	0.10	3.5	

Profile Hole	Average	Depth	Depth to		
No.	Percolation	to	Groundwater		
	Rate (1)	Bedrock (ft.)	(ft.)		
	(min/in)				
1	70	8	17		

^{(1) -} Designed system required due to soil conditions and commercial use.

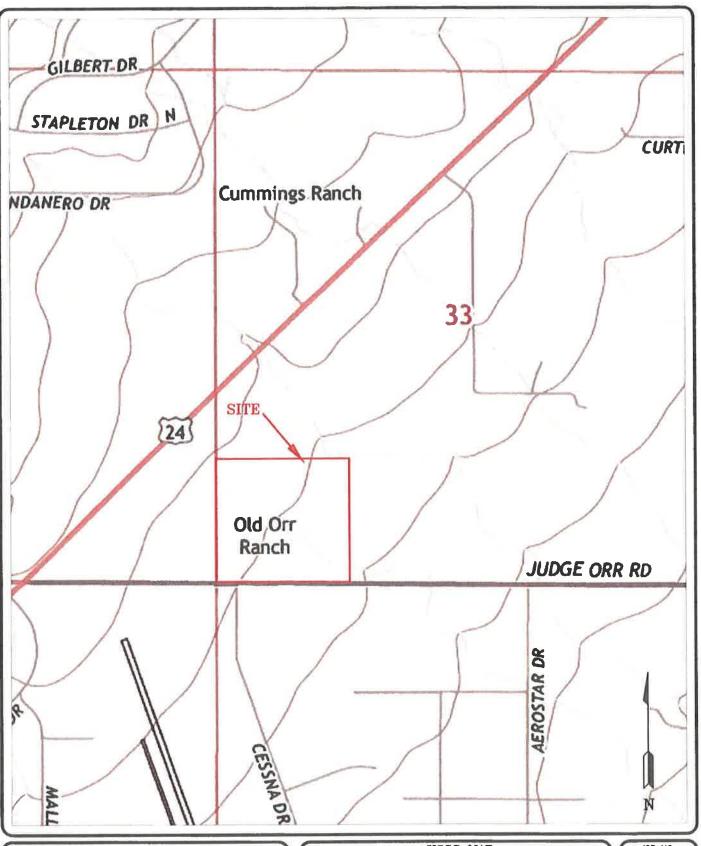
FIGURES





	VICINI	I'Y MAP					
J.	UDGE ORR I	ROAD RV PA	R K				
	14010 JUDG	E ORR ROAL	D				
EI	PASO COU	NTY, COLORA	VDO OCT				
FOR: WILLIAM GUMAN & ASSOCIATES, LTD							
DRAWN-	DATE:	CHECKED:	DATE:				

DRAWN: 12/7/16 FIG NO.: 1





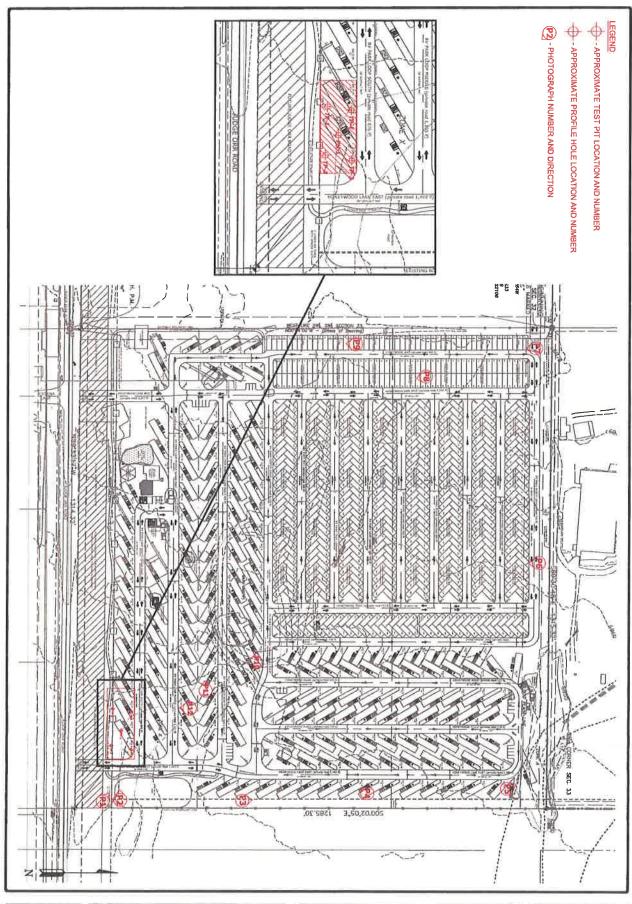
USGS MAP
JUDGE ORR ROAD RV PARK
14010 JUDGE ORR ROAD
EL PASO COUNTY, COLORADO
FOR: WILLIAM GUMAN & ASSOCIATES, LTD

DRAWN: DATE: 12/7/16 CHECKED: DATE:

JOB NO.: 160533

FIG NO.:

2





DEVELOPMENT MAP
JUDGE ORR ROAD RV PARK
14010 JUDGE ORR ROAD
EL PASO COUNTY, COLORADO
FOR: WILLIAM GUMAN' & ASSOCIATES, LTD









SCS MAP

JUDGE ORR ROAD RV PARK

14010 JUDGE ORR ROAD

EL PASO COUNTY, COLORADO

FOR: WILLIAM GUMAN & ASSOCIATES, LTD

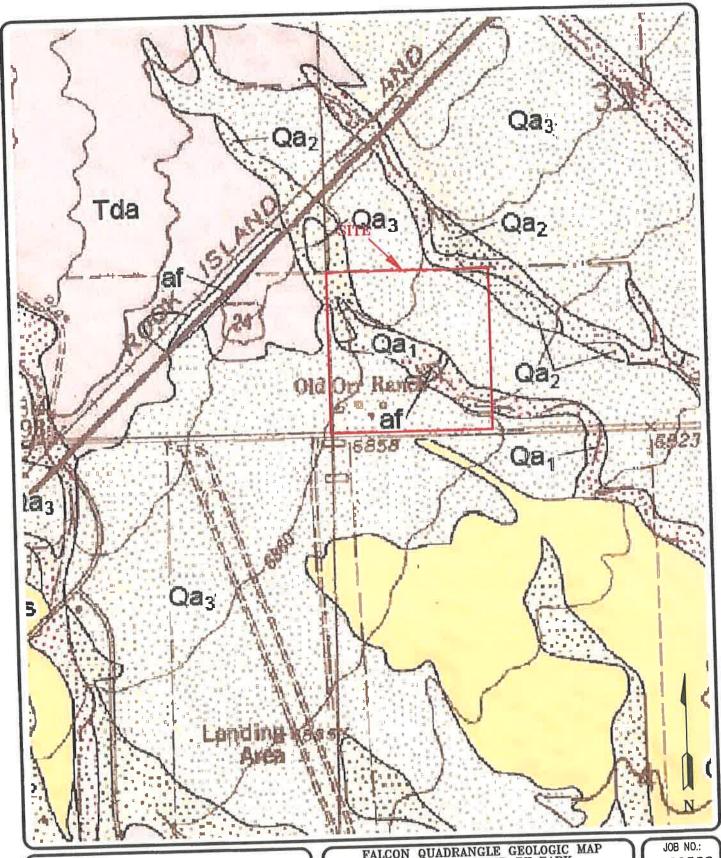
DRAWN: DATE: CHECKED: DATE:
LLL 12/7/16

JOB NO.: 160533

N

FIG NO.:

4





FALCON QUADRANGLE GEOLOGIC MAP
JUDGE ORR ROAD RV PARK
14010 JUDGE ORR ROAD
EL PASO COUNTY, COLORADO
FOR: WILLIAM GUMAN & ASSOCIATES, LTD

DRAWN: DATE: CHECKED: DATE:
LLL 12/7/16

JOB NO.: 160533 FIG NO.: 5

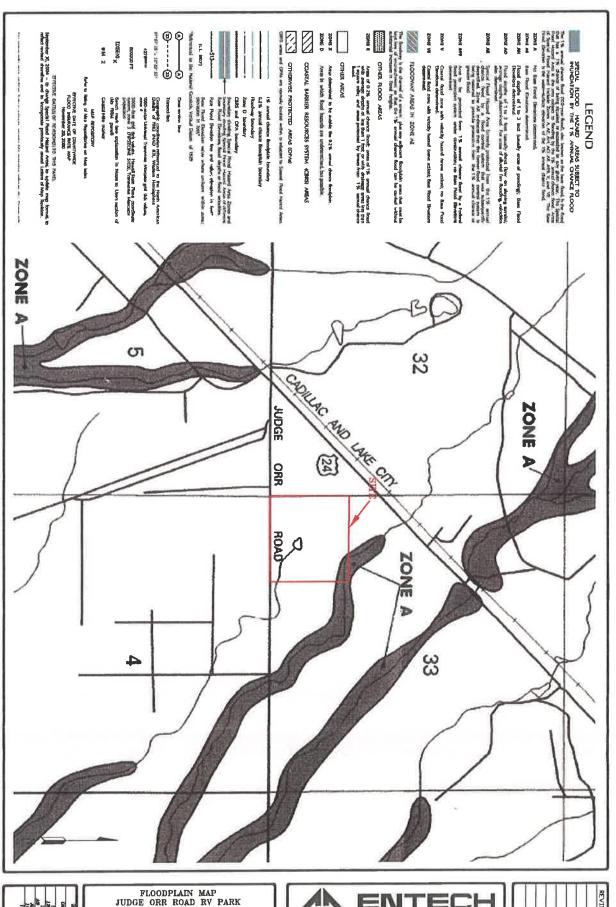




GEOLOGY/ENGINEERING GEOLOGY MAP JUDGE ORR ROAD RV PARK 14010 JUDGE ORR ROAD EL PASO COUNTY, COLORADO FOR: WILLIAM GUMAN & ASSOCIATES, LTD





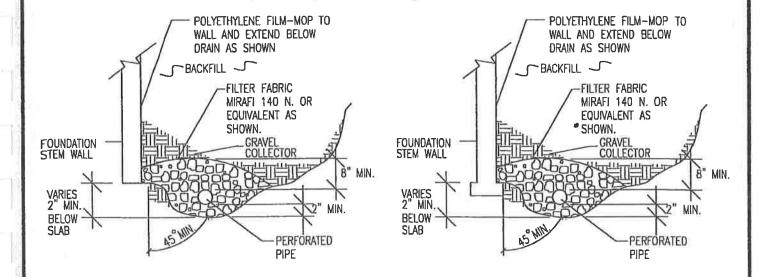




FLOODPLAIN MAP JUDGE ORR ROAD RV PARK 14010 JUDGE ORR ROAD EL PASO COUNTY, COLORADO FOR: WILLIAM GUMAN & ASSOCIATES, LTD







NOTES:

- -GRAVEL SIZE IS RELATED TO DIAMETER OF PIPE PERFORATIONS-85% GRAVEL GREATER THAN 2x PERFORATION DIAMETER.
- -PIPE DIAMETER DEPENDS UPON EXPECTED SEEPAGE. 4-INCH DIAMETER IS MOST OFTEN USED.
- -ALL PIPE SHALL BE PERFORATED PLASTIC. THE DISCHARGE PORTION OF THE PIPE SHOULD BE NON-PERFORATED PIPE.
- -FLEXIBLE PIPE MAY BE USED UP TO 8 FEET IN DEPTH, IF SUCH PIPE IS DESIGNED TO WITHSTAND THE PRESSURES. RIGID PLASTIC PIPE WOULD OTHERWISE BE REQUIRED.
- -MINIMUM GRADE FOR DRAIN PIPE TO BE 1% OR 3 INCHES OF FALL IN 25 FEET.
- -DRAIN TO BE PROVIDED WITH A FREE GRAVITY OUTFALL, IF POSSIBLE. A SUMP AND PUMP MAY BE USED IF GRAVITY OUT FALL IS NOT AVAILABLE.

DRAWN:



PERIMETER DRAIN DETAIL

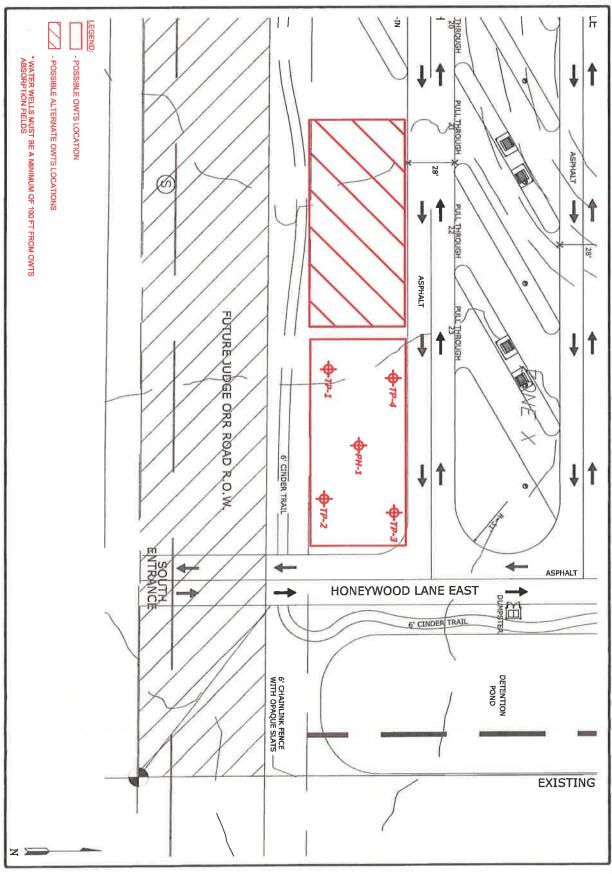
DATE: DESIGNED: CHEC

05

CHECKED:

JOB NO.: (60533 FIG NO.:

8





SEPTIC SUITABILITY MAP JUDGE ORR ROAD RV PARK 14010 JUDGE ORR ROAD EL PASO COUNTY, COLORADO FOR: WILLIAM GUMAN & ASSOCIATES, LTD





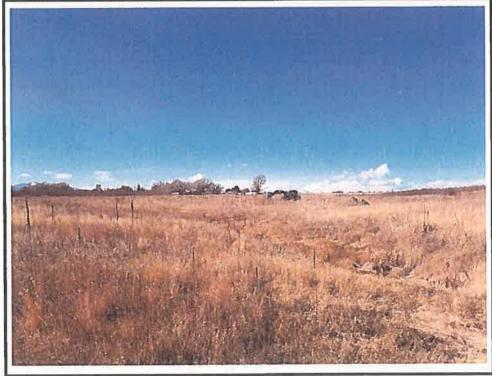
APPENDIX A: Site Photographs





Looking northwest from the southeast portion of the property.

December 5, 2016





Looking west towards proposed OWTS area along drainage.

December 5, 2016

Job No. 160533





Looking north from the eastern portion of the property.

December 5, 2016

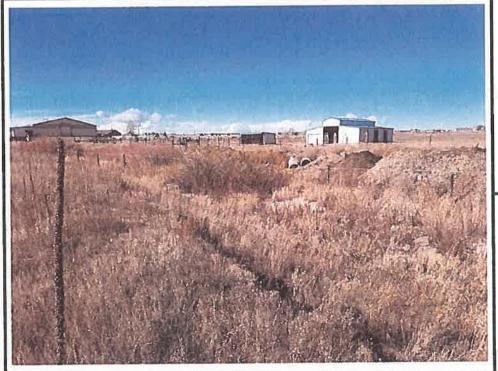




Looking west from the eastern portion of the property.

December 5, 2016

Job No. 160533





Flood zone and drainage northeast corner of the property.

December 5, 2016





Looking south from northern portion of the property.

December 5, 2016

Job No. 160533





Looking south along the berm and drainage from the northwest corner of the property.

December 5, 2016





Looking south from the northwest portion of the property.

December 5, 2016

Job No. 160533





Looking south along berm and drainage on the west side of the property.

December 5, 2016

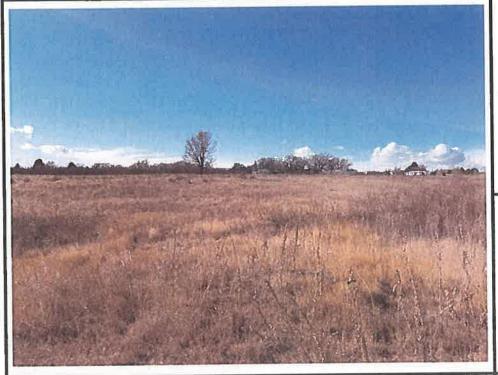




Looking west from the dam towards the pond.

December 5, 2016

Job No. 160533





Looking southwest from the east side of the dam towards existing house and travel trailers.

December 5, 2016





Looking southeast from the east side of the dam towards the proposed OWTS area.

December 5, 2016

Job No. 160533

APPENDIX B: Test Pit Logs and Test Boring Log from the Profile Hole

TEST PIT NO. 1 DATE EXCAVATED 12/5/2016 Job # TEST PIT NO. 2 DATE EXCAVATED 12/5/2016

CLIENT WILLIAM GUMAN & ASSOCIATES, LTD LOCATION JUDGE ORR ROAD RV PARK

305 "							LOCATION JUDGE O	RR R	OAD	RV	PAF	RK	
REMARKS	Depth (ft)	Symbol	Samples	Soil Structure Shape	Soil Structure Grade	USDA Soil Type	REMARKS	Depth (ft)	Symbol	Samples	Soil Structure Shape	Soil Structure Grade	N USDA Soil Type
topsoil, sandy loam, dark brown	1	*		gr	m	2	topsoil, sandy loam, dark brown	1 -	*		gr	m	2
gravelly sandy loam, fine to coarse grained, brown	2 3	بعر		gr	m	2	gravelly sandy clay loam, fine to coarse grained, brown, with 1 - 2" sand lenses	2 - 3	بر		gr	m	3
sandy clay, black-brown	4			gr	w	ЗА	clay, olive gray	4			ma		4A
weathered to formational sandy claystone, light gray brown	5_ 6 7 8		***************************************	pl	S	5	weathered to formational sandy claystone	5 6 7			pf	s	5
	9							9			11.52		
	10	7		1		I	1	10		1	1	1	1

Soil Structure Shape granular - gr platy - pl blocky - bl

prismatic - pr single grain - sg massive - ma Soil Structure Grade

weak - w moderate - m strong - s loose - l

<>	ENTECH ENGINEERING, INC.
N/	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

	TEST	PIT LOG	
DRAWN:	DATE:	CHECKED:	DATE: 12/8/16

JOB NO.; \UO533 FIG NO.; TEST PIT NO. 3
DATE EXCAVATED 12/5/2016
Job # 161944

TEST PIT NO. 4
DATE EXCAVATED 12/5/2016

CLIENT WILLIAM GUMAN & ASSOCIATES, LTD LOCATION JUDGE ORR ROAD RV PARK

						LOCATION JUDGE C	RR R	OAD	RV	PAI	RK	
REMARKS	Depth (ft) Symbol	Samples	Soil Structure Shape	Soil Structure Grade	USDA Soil Type	REMARKS	Depth (ft)	Symbol	Samples	Soil Structure Shape	Soil Structure Grade	USDA Soil Type
topsoil, sandy loam, dark brown	1 2		gr	m	2	topsoil, sandy loam, dark brown	1	×				
gravelly sandy loam, fine to coarse grained, brown	2 3	4	gr	m	2	gravelly sandy loam, fine to coarse grained, brown	3	/		gr	m	2
	4 5					weathered to formational sandy claystone, light gray brown	4 5_		*****	p!	s	5
weathered to formational sandy claystone, light gray brown	6 7 8	XXXXXXX	pl	S	5		6 7 8		××××××	8		
	9 -						9					

Soil Structure Shape

granular - gr platy - pl blocky - bl prismatic - pr single grain - sg massive - ma Soil Structure Grade

weak - w moderate - m strong - s loose - l



	TEST	PIT LOG	
DRAWN:	DATE:	CHECKED:	DATE:

JOB NO.:

(60533
FIGNO.:

B-2

TEST BORING NO. TEST BORING NO. DATE DRILLED DATE DRILLED 12/5/2016 WILLIAM GUMAN & ASSOC. CLIENT 160533 Job# JUDGE ORR ROAD RV PARK LOCATION REMARKS REMARKS Watercontent % Blows per foot Blows per foot Watercontent Soil Type Soil Type Samples Depth (ft) Depth (ft) Symbol Samples Symbol WATER @ 17', 12/6/16 SAND, CLAYEY, FINE GRAINED, BROWN, MEDIUM DENSE TO 1 8.4 26 DENSE, MOIST 5 35 11.5 1 5 <u>50</u> 11.3 10 10 SANDSTONE, VERY CLAYEY. FINE GRAINED, BROWN, VERY DENSE, MOIST 15 12.5 4 <u>50</u> 15 <u>50</u> 9.8 6"



ENTECH ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907 **TEST BORING LOG**

DRAWN: DATE: CHECKED: DATE:

LLL 12/13//6

JOB NO.:

160533

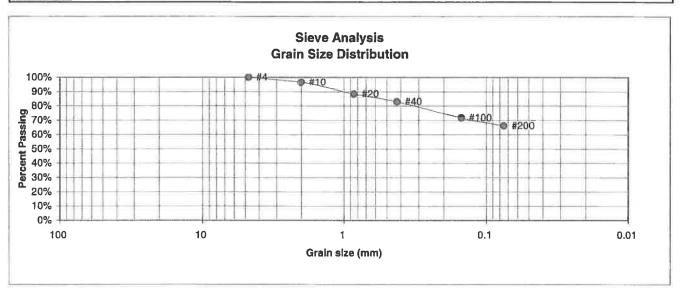
FIG NO.;

B-3

APPENDIX C: Laboratory Test Results

BORING NO. TP-1 UNIFIED CLASSIFICATION CL
DEPTH(ft) 5-6 AASHTO CLASSIFICATION

CLIENT WILLIAM GUMAN & ASSOC.
PROJECT JUDGE ORR ROAD RV PARK



TEST BY

JOB NO.

BL

160533

U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	96.5%	Moisture at start
20 40	88.3% 83.0%	Moisture at start Moisture at finish Moisture increase
100	71.6%	Initial dry density (pcf)
200	66.2%	Swell (psf)



LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 160533 FIG NO.:

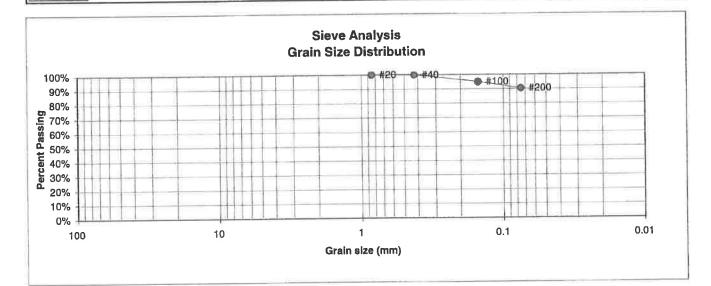
C-1

BORING NO. TP-2 UNIFIED CLASSIFICATION AASHTO CLASSIFICATION TEST BY BL JOB NO.

CL

160533

DEPTH(ft) CLIENT **PROJECT** 3-4 WILLIAM GUMAN & ASSOC. JUDGE ORR ROAD RV PARK



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"		Swell
4 10		Moisture at start
20 40	100.0% 99.8%	Moisture at finish Moisture increase
100 200	94.8% 90.3%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST	
RESULTS	

DRAWN: CHECKED: DATE: DATE: 12/13/16

JOB NO.: 160533 FIG NO.: 6-2

BORING NO.

UNIFIED CLASSIFICATION **AASHTO CLASSIFICATION** TEŞT BY JOB NO.

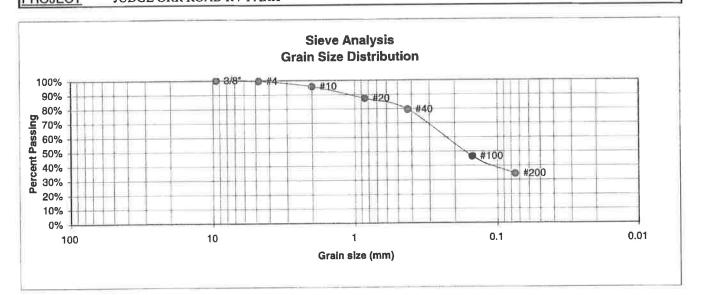
SC

BL

160533

DEPTH(ft) CLIENT PROJECT

WILLIAM GUMAN & ASSOC. JUDGE ORR ROAD RV PARK



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	99.6%	<u>Swell</u>
10	95.7%	Moisture at start 7.7%
20	87.3%	Moisture at finish 22.0%
40	79.4%	Moisture increase 14.3%
100	46.4%	Initial dry density (pcf) 103
200	34.1%	Swell (psf) 430



LABORATORY	TEST
RESULTS	

DRAWN: DATE: DATE: CHECKED: 12/13/16 LLL

JOB NO.: 160533 FIG NO.: 6-3

BORING NO.

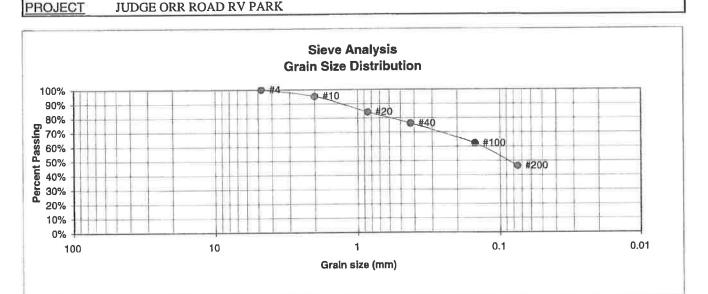
UNIFIED CLASSIFICATION AASHTO CLASSIFICATION TEST BY JOB NO.

SC

BL

160533

DEPTH(ft) CLIENT PROJECT 15 WILLIAM GUMAN & ASSOC.



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	95.3%	Moisture at start
20	84.1%	Moisture at finish
40	76.2%	Moisture increase
100	62.0%	Initial dry density (pcf)
200	46.3%	Swell (psf)



LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE: LLL /2//3//6

JOB NO.: 160533 FIG NO.: C-4

P-1

GRAB

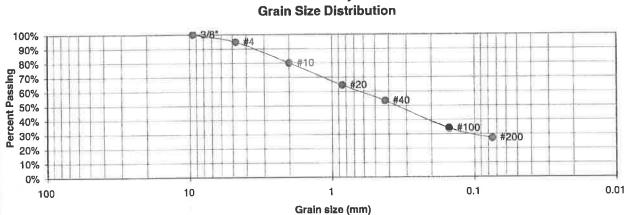
UNIFIED CLASSIFICATION **AASHTO CLASSIFICATION** SC

TEST BY JOB NO.

BL 160533

CLIENT PROJECT WILLIAM GUMAN & ASSOC. JUDGE ORR ROAD RV PARK





Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
100.0%	
94.8%	<u>Swell</u>
80.0%	Moisture at start
64.4%	Moisture at finish
53.4%	Moisture increase
33.9% 27.0%	Initial dry density (pcf) Swell (psf)
	100.0% 94.8% 80.0% 64.4% 53.4%



L	ABORATORY	TEST
R	ESULTS	

DRAWN: DATE: CHECKED: DATE: 444 12/13/16 JOB NO.:

160533 FIG NO.: C-5

P-2 GRAB UNIFIED CLASSIFICATION
AASHTO CLASSIFICATION

TEST BY JOB NO.

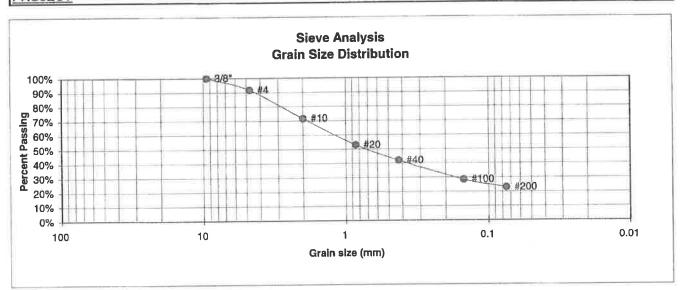
SC

BL 160533

CLIENT

WILLIAM GUMAN & ASSOC.

PROJECT JUDGE ORR ROAD RV PARK



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	Swell
4 10	91.7% 71.5%	Moisture at start
20	52.9%	Moisture at finish
20 40	42.0%	Moisture increase
100 200	28.4% 22.9%	Initial dry density (pcf) Swell (psf)



LABORATORY 7	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 160533 FIG NO.:

P-3

GRAB

UNIFIED CLASSIFICATION AASHTO CLASSIFICATION SC

TEST BY JOB NO.

BL 160533

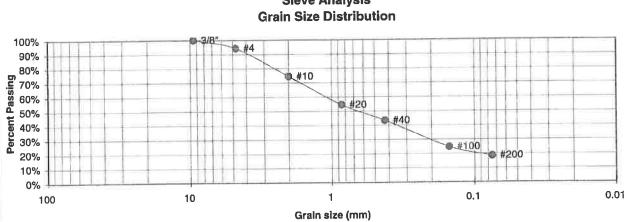
CLIENT

WILLIAM GUMAN & ASSOC.

PROJECT

JUDGE ORR ROAD RV PARK





U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	94.1%	<u>Swell</u>
10	74.4%	Moisture at start
20	54.5%	Moisture at finish
40	43.4%	Moisture increase
100 200	24.7% 18.5%	Initial dry density (pcf) Swell (psf)



LABORATORY	TEST
RESULTS	

DRAWN:

DATE:

CHECKED: LLL

12/13/16

JOB NO.:

160533

FIG NO.:

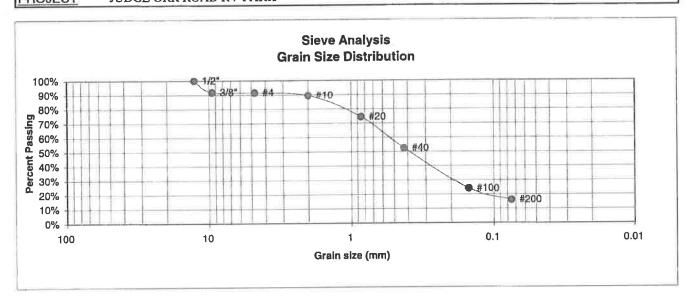
6.7

P-4 GRAB UNIFIED CLASSIFICATION AASHTO CLASSIFICATION JOB NO.

SC

BL 160533

CLIENT PROJECT WILLIAM GUMAN & ASSOC.
JUDGE ORR ROAD RV PARK



U.S. <u>Sieve #</u> 3" 1 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit
3/4"		Plastic Index
1/2"	100.0%	
3/8"	91.8%	
4	91.5%	<u>Swell</u>
10	89.3%	Moisture at start
20	74.4%	Moisture at finish
40	52.3%	Moisture increase
100 200	23.8% 16.0%	Initial dry density (pcf) Swell (psf)



	LABORAT RESULTS	ORY TEST	
DRAWN:	DATE:	CHECKED:	DATE: /2/13//6

JOB NO.: 160533 FIG NO.: ___ S APPENDIX D: Soil Survey Descriptions

El Paso County Area, Colorado

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the

mapunit.

Description of Columbine

Setting

Landform: Flood plains, fan terraces, fans

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam
C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to

very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.5 Inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Gravelly Foothill (R049BY214CO)

Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: Landform: Swales Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 14, Sep 23, 2016 **APPENDIX E: Percolation Test Results**

Client:

William Guman and Associates

Test Location:

Judge Orr Road RV Park

Job Number:

160533

PERCOLATION HOLES

Time

(min.)

10

10

10

Date Holes Prepared:

12/5/2016

Date Hole Completed:

12/6/2016

Hole No. 1

Hole No. 2

Trial Trial

1

2

3

Depth:

38" Depth:

	Dopuii	. –	
Water			Water
Level		Time	Level
Change (in.)	<u>Trial</u>	(min.)	Change (in.)
1/8	1	10	1/8
0	2	10	1/8

Perc Rate (min./in.):

80

1/8

Perc Rate (min./in.);

42"

10

80

1/8

Hole No. 3

Depth:

Hole No. 4

3

42" Depth:

Level Time (min.) Change (in.) **Trial** 10 1/8 1 2 10 0 1/8 3 10

Water Water Time Level Change (in.) **Trial** (min.) 1/4 10 1 2 10 3/8 1/4 3 10

Perc Rate (min./in.):

80

Perc Rate (min./in.):

40

Average Perc Rate (min./in.)

70

Date Profile Hole Completed:

PROFILE HOLE

Visual Classification

Depth 0-8

8-20'

Sand, clayey, fine grained, brown Sandstone, very clayey, fine grained, brown

Remarks

Sandstone Bedrock at 8'

12/5/2016

Groundwater at 17'

26 Blows / ft. @ 2'

35 Blows / ft. @ 4'

50 Blows / 7" @ 9'

LTAR = 0.20 gallons per square foot per day.

Designed system required due soil conditions and commercial use.

Observer:

Graham Espenlaub



PERCOLATION TEST RESULTS

DRAWN:

DATE:

CHECKED:

DATE:

JOB NO.: 1605 33 FIG NO.: E-1

Markup Summary

dsdlaforce (2)



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Add "PCD File No. PPR-16-040"



Subject: Text Box Page Label: 1 Author: dsdlaforce

Date: 6/28/2018 4:28:03 PM

Color:

Per Chapter 11 Section 11.3.3 of the El Paso County Drainage Criteria Manual recommendations for the foundation preparation and embankment construction shall be submitted with the complete design analysis for all

permanent detention facilities.