



## **Falcon Highlands**

### **Final Drainage Report**

Owner/Developer

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Contact: Jim Byers

Engineer

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Contact: Kevin Blumhardt, PE

Atwell Project Number

24004308

PCD File Number

SF1418

***Submitted by: Atwell, LLC***

December 20, 2024

**Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

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Kevin Blumhardt, PE 54413	Date	Seal:
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**Developer's Statement:**

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Challenger Homes

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By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_

**El Paso County Approval:**

Filed in accordance with requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code.

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County Engineer, Conditions:	Date
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## INTRODUCTION

This Final Drainage Report (FDR) has been completed for Challenger Homes in order to present an effective storm water management plan for the Falcon Highlands South Filing 1 development, hereinafter referred to as the Site. This report is intended to guide the development of the Site and recommend general drainage concepts that can be implemented as development progresses. Included within this report is a proposed drainage plan for the Site along with reference information for drainage basins and storm water conveyance facilities.

The Site was most recently studied in the Preliminary Drainage Report (PDR) level in the *Falcon Highlands South PUDSP Preliminary Drainage Report* by Atwell, LLC, approved May 17, 2024.

The Site for Falcon Highlands South Filing 1 is approximately 19.66 acres and will include a total of approximately 24 single-family residential units.

Proposed herein is a network of storm infrastructure, permanent water quality and detention facilities, and swales that will meet relevant drainage criteria.

## GENERAL LOCATION AND DESCRIPTION

The Site is located within Section 12, Township 13 South, Range 65 West of the Sixth Principal Meridian, County of El Paso, State of Colorado. The Site is bounded by Antelope Meadows to the south, Bridal Vail Way to the west. Falcon Highlands Filing No. 2 is located to the north of the Site.

The overall area consists of approximately 19.66 acres that is proposed to be developed into 24 single-family residential units, roadways, and open space. In addition to the Site development, two off-site water quality and detention will be constructed to detain runoff from the Site and other areas of the overall Falcon Highlands development.

The Site is within the Sand Creek Drainage Basin.

A vicinity map showing the location of the Site is included in appendix A.

The Site is within the Falcon Highlands MDDP by Atwell, LLC, dated March 2022.

## SOILS AND EXISTING CONDITIONS

Much of the Site is currently undeveloped. Of the development within the Site, there are existing dirt roadways and sanitary sewer infrastructure installed per the Construction Drawings for Falcon Highlands Filing No. 2 prepared by Terra Nova Engineering, most recent revised date of September 7, 2010. The ALTA survey conducted by Atwell, LLC., shows the existing conditions of Falcon Highlands and adjacent development of Filing No. 2. The Site is comprised of existing

natural grass vegetation typical of the eastern plains with sparse vegetative cover at its outer limits to the south and southeast. There is an existing detention pond south of the Site, from Falcon Highlands Filing No.2 and the future development of Falcon Highlands Filing No. 3. The on-Site slopes range from 0 percent to 10 percent and generally sheet flows from west to east. An Existing Conditions Drainage Map is included in Appendix G showing the delineated drainage basins.

The Site is compromised of Blakeland-Fluvaquentic Haplaquolls soil, a loamy sand, and hydraulic soils group A. The Natural Resources Conservation Service of the United State Department of Agriculture Web Soil Survey has been included in Appendix B for reference.

Based on a Geotechnical Report done by Rocky Mountain Group, dated October 8, 2021, three bore holes were drilled within the Site, TB-1, TB-2, TB-3. From these bore holes it was noted that ground water was hit at 16.0', 14.6', and 11.4' respectively. A copy of this report can be found in Appendix F.

## DRAINAGE DESIGN CRITERIA

The El Paso County Drainage Manual (EPC DCM) and El Paso County Engineering Criteria Manual (EPC ECM) were used in conjunction with the Colorado Springs Drainage Criteria Manual (DCM) Mile High Flood District (MHFD) Criteria Manual. The rational method was used for a drainage basin less than 100-acres. The 5-year design frequency was used for the minor storm and a 100-year design frequency was used for the major storm in calculation on-Site storm hydraulics. The City of Colorado Springs IDF Curve has used for calculating the rainfall intensity of 1.50 inches for the 5-year and 2.52 inches for the 100-year.

## EXISTING ONSITE AND OFFSITE DRAINAGE BASINS

Off-Site drainage basin runoff data and calculations have been updated per current codes and standards. The developments of Falcon Highlands Filings No. 1 and 2 remain consistent with the Master Drainage Development Plan, MDDP (EDARP project number SF05033) and therefore off Site basin descriptions are delineations provided are based on previous County approved reports.

The Site has been broken down into several major existing drainage basins. An Existing Conditions Drainage Map is in appendix F.

### **Off-Site Basins (Existing):**

Filing No. 2:

**OS-1 (6.38 ac,  $Q_5 = 5.58$  cfs,  $Q_{100} = 16.11$  cfs)** is an off-Site basin located on the northwestern part of Falcon Highlands Filing No. 2 and consists of the rear yard areas of PUD residential zoned lots.

The historic drainage pattern sheet flows southwesterly where it is captured by basin OS-5 at **Design Point 7** and ultimately outfalls into existing Pond 1 through the public 60" RCP storm pipe that runs through Falcon Highlands South.

**OS-2 (3.12 ac,  $Q_5 = 2.29$  cfs,  $Q_{100} = 6.06$  cfs)** is an off-Site sub-basin within the developed area of Filing No. 1 for quarter-acre lots and is an off-Site basin that was included in the MDDP for Filing No. 2. The basin's runoff sheet flows due south in Filing No. 2 and is captured by the roadways and storm system in Filing No. 2 that runs through Falcon Highlands South, and ultimately outfalls into the existing Pond 1. The basin flows to OS-5.

**OS-3 (1.14 ac,  $Q_5 = 4.06$  cfs,  $Q_{100} = 7.04$  cfs)** is an off-Site basin within Filing No. 1 that includes the developed right-of-way of Rolling Thunder Way. This sub-basin was included in the previous MDDP as an off-Site basin and represents a portion of the landscaped right-of-way on the south side of Rolling Thunder Way that sheet flows due south into the developed areas of Filing No. 2 and ultimately into the public storm system shared with Falcon Highlands South, outfalling to existing Detention Pond 2.

**OS-4 (13.09 ac,  $Q_5 = 4.44$  cfs,  $Q_{100} = 15.98$  cfs)** is an off-Site basin located on the southwestern part of Falcon Highlands Filing No. 2 and consists of mostly Tract A and portions of PUD residential zoned lots rear yard areas. The historic drainage pattern sheet flows south where it is captured by basin A, and per existing drainage patterns is not tributary to on-Site detention ponds and drains directly offSite via overland sheet flow.

**OS-5 (59.62 ac,  $Q_5 = 51.26$  cfs,  $Q_{100} = 135.39$  cfs)** is an off-Site basin that stretches from the eastern border of basin OS-4 to the eastern edge of Bridal Vail Way within Filing No. 2. The basin is zoned as PUD residential lots of about quarter-acre size. Runoff is carried in the public rights-of-way where the flow travels south through a series of public curb and gutters, sump inlets and storm infrastructure within Filing No. 2. The flow outfalls into the existing Pond 1 through the public 60" RCP storm pipe that runs through Falcon Highlands South. No surface flow from this basin enters the Site.

**OS-6 (35.75 ac,  $Q_5 = 14.22$  cfs,  $Q_{100} = 49.60$  cfs)** is off-Site basin located between Bridal Vail Way and Antelope Meadows Circle within Filing 2. This basin includes PUD residential zoned lots of half-acre size and contains drainage tracts. The basin is captured by a series of public curb and gutter systems in the rights-of-way where public storm infrastructure conveys storm water to the end of the cul-de-sac of Wagon Track Drive where the public storm system of Filing No. 2 connects and daylight to Falcon Highlands South within future Antelope Meadows Circle right-of-way. Flows continue through Falcon Highlands South via an existing diversion ditch to Pond 2.

**OS-7 (6.47 ac,  $Q_5 = 2.29$  cfs,  $Q_{100} = 7.97$  cfs)** is the off-Site basin located within Filing 2, just north of Basin D of Filing 3. The basin includes PUD residential zoned lots of half-acre size with right of way. The basin runoff is captured in the public right-of-way curb and gutter where it travels south and is released at the road end, where it continues south through Antelope Meadows Circle and then due east through Falcon Highlands South's Basin D in the existing access path where it outfalls to Pond WU.

#### Future Falcon Highlands Phases:

**OS-8 (3.74 ac,  $Q_5 = 0.15$  cfs,  $Q_{100} = 2.03$  cfs)** is the basin located southwest of Antelope Meadow Circle, just below basin OS-4, and west of basin OS-11. The storm water runoff from this basin sheet flows south and off-Site at with the combined flow of OS-4, and per existing drainage patterns is not tributary to on-Site detention ponds.

**OS-9 (3.14 ac,  $Q_5 = .20$  cfs,  $Q_{100} = 2.62$  cfs)** is the undeveloped, natural landscaped area between Tamlin Road and the existing Pond 1. Runoff from Basin E is directed by a ditch section to a low point between the future Dublin Road and Highway 24. This drainage concept and its associated storm infrastructure is presented in the previous master plan and is to remain as the intended plan. The 2005 PDR suggested that an inline grate inlet be installed but there is no evidence that this was installed. The existing drainage pattern consists of pooling within the local low point of the ditch that surcharges and is directed south through the grassland swale.

**OS-10 (3.67 ac,  $Q_5 = 0.18$  cfs,  $Q_{100} = 2.42$  cfs)** is the undeveloped area between Tamlin Road and the existing Detention Pond 2. The runoff from Basin F is directed to the low point in the downstream grasslined swale between the Site and Tamlin Road. This drainage concept and its associated storm infrastructure is presented in the previous master plan and is to remain as the intended plan. The 2005 PDR suggested that a 4'x4' area inlet be constructed but there is no evidence that this was installed. The existing drainage pattern consists of pooling within the local low point of the ditch that surcharges and is directed south through the grassland swale.

**OS-11 (35.55 ac,  $Q_5 = 1.32$  cfs,  $Q_{100} = 17.58$  cfs)** is located south of Antelope Meadow Circle, adjacent to basin A. The Site is covered in native grasses with limited grading work from a previous development. Runoff from the Site sheet flows southwesterly overland to existing Pond 1). The private 42" RCP outlet pipe from the outlet structure of the pond daylights at the grassland swale south of the abandoned future Tamlin Road right-of-way.

**OS-12 (39.29 ac,  $Q_5 = 1.57$  cfs,  $Q_{100} = 20.90$  cfs)** is located adjacent to Basin B and covered in native grasses and weeds. The Site has limited grading due to work from a previous development that did not finish. Runoff from the Site sheet flows southwesterly overland to an existing diversion ditch that spans from an existing public 24" RCP storm sewer main that daylights within Falcon Highlands South south of Wagon Track Way. The diversion ditch flows directly to existing Pond 2. The private 42" RCP outlet pipe from the outlet structure of the pond daylights at the grassland swale south of the project Site.

**OS-13 (10.54 ac,  $Q_5 = 0.44$  cfs,  $Q_{100} = 5.86$  cfs)** is located to the northeast of the Filing and consists of undeveloped area with native grasses. The basin's runoff drains directly to existing Pond WU.

**OS-14 (8.84 ac,  $Q_5 = 0.39$  cfs,  $Q_{100} = 5.14$  cfs)** is the area east of Basin C that is not to be disturbed and remain as open, natural landscape. The runoff from Basin G is collected in a local

topographic low point and when overtopping the low point, the runoff continues southeast to the low point in the grasslined swale along Highway 24.

### On-Site Basins (Existing):

This Site has been broken down into three major existing drainage basins. An existing drainage map can be found in Appendix F.

**EX-1 (3.38 ac,  $Q_5= 0.12$  cfs,  $Q_{100}= 1.60$  cfs )** is located in the west portion of the Site, and consists of undeveloped land. Stormwater flows south and west into the existing Bridal Vail Way then continues south via curb and gutter to a cross pan at the intersection of Bridal Vail Way and Antelope Meadows Circle and flows west to an existing inlet (Design point C1), flow from this inlet is then conveyed west and then south through existing storm infrastructure where it is then released into the existing detention pond 1 built with Falcon Highlands Filing No. 2 & No. 3 File No. SF05033 .

**EX-2 (9.38 ac,  $Q_5= 0.36$  cfs,  $Q_{100}= 4.85$  cfs )** is located in the northern part of the Site, and consists of undeveloped land. Stormwater flows southwest to a natural swale and continues off-Site and into an existing detention pond 2, built with Falcon Highlands Filing No. 2 & No. 3 File No. SF05033.

**EX-3 (9.14 ac,  $Q_5= 0.42$  cfs,  $Q_{100}= 5.53$  cfs)** is located in the south portion of the Site and consists of undeveloped land. Stormwater flows south to a low point in the basin then continues south to existing detention pond 2, built with Falcon Highlands Filing No. 2 & No. 3 File No. SF05033.

## PROPOSED DRAINAGE BASINS

Preliminary grading design on the Site has been completed to include right-of-way design and assignment of lot type A, B, and Transition (T). The assigned lots drain per a typical lot template, into roadways where on-grade sump inlets are located to capture and convey stormwater through public storm system and outfall to a permanent water quality and detention facility.

The overarching premise of the drainage design is to route overland flow from residential lots to adjacent right-of-ways where public storm infrastructure will be installed and ultimately convey the stormwater to the downstream permanent water quality and detention facility to provide water quality treatment as well as flow attenuation and detention. Previous drainage reports designed ponds 1 and 2 in order to provide detention for existing Filings 2 and 3. The analysis in this report provides a detailed and defined design of these ponds to account for drainage requirement changes as well as a design to account for full spectrum detention. This report will redesign these existing ponds to meet current standards and provide full-spectrum detention.



There is a proposed grass-lined swale to capture flows in the open space behind the northern lots, The design of this swale is included in the report in Appendix E, to accurately access the width and depth of the drainage way for the minor and major storm events.

HLG calculations for both the 5-year and 100-year storms are provided in Appendix E.

### On-Site Basins (Proposed):

**A-1 (4.49 ac,  $Q_5= 0.12$  cfs,  $Q_{100}= 1.64$  cfs )** is located in the north portion of the Site along the back of the existing lots and the proposed lots, and consists of open space. Stormwater flows to a proposed swale in the open space and flows to an existing outlet (Design point A1). The existing Design point discharges to a natural swale that flows southwest to proposed pond 2.

**A-2 (4.83 ac,  $Q_5= 2.89$  cfs,  $Q_{100}= 8.24$  cfs)** is located in the north portion of the Site south of Basin A-1 and consists of large lots (greater than 19,000 sf) public right-of-way, curb and gutter, and attached sidewalk. Stormwater sheet flows from the lots toward the public right-of-way, and is conveyed south via curb and gutter to a local low point in the roadway where it is then captured by a proposed 10' Type R sump inlet (Design point B1) and enters the proposed public storm infrastructure and is released into a proposed temporary water quality pond (Design point P.1). Emergency overflow from the inlet will overtop the crown in the roadway and continue to flow south and will be picked up by future inlets in Antelope Meadows Circle (Design Point B4) and will be released into proposed pond 2.

**A-3 (2.46 ac,  $Q_5= 1.48$  cfs,  $Q_{100}= 4.22$  cfs)** is located on the west side on the Site south of Basin B-1 and consists of large lots (greater than 19,000 sf) public right-of-way, curb and gutter, and attached sidewalk. Stormwater sheet flows from the lots toward the public right-of-way, and is conveyed south via curb and gutter to a local low point in the roadway where it is then captured by a proposed 10' Type R sump inlet (Design point A2) and enters the proposed public storm infrastructure and is released into a proposed temporary water quality pond (Design point P.1). Emergency overflow from the inlet will overtop the crown in the roadway and continue to flow south and will be picked up by future inlets in Antelope Meadows Circle (Design Point C2) and will be released into proposed pond 2.

**A-4 (1.98 ac,  $Q_5= 1.54$  cfs,  $Q_{100}= 4.38$  cfs)** is located on the southwest side on the Site south of Basin B-2 and consists of large lots (greater than 19,000 sf) public right-of-way, curb and gutter, and attached sidewalk. Stormwater sheet flows from the lots toward the public right-of-way, and is conveyed east via curb and gutter to a local low point in the roadway where it is then captured by a proposed 5' Type R sump inlet (Design point B3) and enters the proposed public storm infrastructure and is released into a proposed temporary water quality pond (Design point P.1) and will be released into proposed pond 2.

**A-5 (3.52 ac,  $Q_5= 2.35$  cfs,  $Q_{100}= 6.7$  cfs)** is located on the southeast side on the Site south of Basin B-1 and consists of large lots (greater than 19,000 sf) public right-of-way, curb and gutter, and attached sidewalk. Stormwater sheet flows from the lots toward the public right-of-way, and is conveyed west via curb and gutter to a local low point in the roadway where it is then captured by a proposed 10' Type R sump inlet (Design point B4) and enters the proposed public storm

infrastructure and is released into a proposed temporary water quality pond (Design point P.1) and will be released into proposed pond 2.

**A-6 (1.63 ac,  $Q_5= 1.61$  cfs,  $Q_{100}= 4.59$  cfs)** is located on the western boundary of the Site and consists of large lots (greater than 19,000 sf) public right-of-way, curb and gutter, and attached sidewalk. Stormwater sheet flows west toward the public right-of-way, and is conveyed south via curb and gutter to a local low point in the roadway where it is captured by an existing 20' inlet (Design point C1), where it will enter existing storm infrastructure and be release into the proposed pond 1.

**Major Basin B (40.12 ac,  $Q_5= 18.65$  cfs,  $Q_{100}= 53.18$  cfs)** is located south-west of the proposed Site. It is modeled as a future Falcon Highlands development and will consist of lots, public right-of-way, curb and gutter, and attached sidewalk. Stormwater will be conveyed via storm infrastructure into proposed pond 1.

**Major Basin C (41.08 ac,  $Q_5= 25.69$  cfs,  $Q_{100}= 73.24$  cfs)** is located south of the proposed Site. It is modeled as a future Falcon Highlands development and will consist of lots, public right-of-way, curb and gutter, and attached sidewalk. Stormwater will be conveyed via storm infrastructure into proposed pond 2.

**Major Basin D (8.26 ac,  $Q_5= 12.79$  cfs,  $Q_{100}= 26.67$  cfs)** is located east of the proposed Site. It is modeled as a future Falcon Highlands development and will consist of lots, public right-of-way, curb and gutter, and attached sidewalk. Stormwater will be conveyed via storm infrastructure into proposed pond 2.

**Major Basin E (1.41 ac,  $Q_5= 0.08$  cfs,  $Q_{100}= 1.03$  cfs)** is located south of pond 1. It is undisturbed area and is planned to remain undisturbed. Stormwater sheets flows off the basin south into Sand Creek.

**Major Basin F (5.91 ac,  $Q_5= 0.26$  cfs,  $Q_{100}= 1.41$  cfs)** is located east of pond 1 and west of pond 2. It is undisturbed area and is planned to remain undisturbed. Stormwater sheets flows off the basin south into Sand Creek.

**Major Basin G (8.38 ac,  $Q_5= 0.37$  cfs,  $Q_{100}= 4.93$  cfs)** is located north east of pond 2. It is undisturbed area and is planned to remain undisturbed. Stormwater sheets flows off the basin south into Sand Creek.

## STORMWATER CONVEYANCE AND STORAGE FACILITIES

The proposed on-Site conveyance facilities will consist of a combination of storm pipe, swales/channels, curb and gutter, and inlets, and has been designed using runoff data from the calculations shown in Appendix D. Proposed drainage patterns will generally follow historic drainage patterns outlined in the previous section of this report. At sump conditions, inlets will be sized to collect 100-year flows. Runoff entering the inlets will be conveyed within the public storm sewer system to proposed pond 2.

The Site will send storm water runoff to both proposed ponds 1 and 2. These proposed ponds have been redesigned to meet current standards and provide full spectrum detention.

Proposed Flows to Proposed Ponds for Entire Development				
	WQCV	EURV-WQCV	100-year - EURV-WQCV	Total Volume Required
<b>Proposed Pond 1</b>	2.411 ac-ft	6.711 ac-ft	4.500 ac-ft	13.683 ac-ft
<b>Proposed Pond 2</b>	2.033 ac-ft	5.710 ac-ft	3.795 ac-ft	11.539 ac-ft

Both ponds were designed using Mile High Flood District Detention Spread Sheets for volume and outlet structures.

Both ponds are designed to release into Sand Creek at or below the peak existing flows.

MHFD-Inlet\_v5.03 software was used to analyze and design the street and inlet capacities throughout the Site. The results of the software is included in the appendices for reference. Chapter 7 of the City of Colorado Springs Drainage Criteria Manual, Volume 1 was used for street flow design criteria.

A proposed grass lined swale is designed to convey stormwater to an outfall point for tributary areas within the northern open space portion of the Site. This swale is to be designed to El Paso County and Colorado Springs Drainage standards with one foot of freeboard. Design calculations and cross sections are included within the appendix.

## FOUR STEP PROCESS

The Four Step Process focuses on reducing runoff volumes, treating the WQCV, stabilizing drainageways, and implementing long-term source controls. The Four Step Process pertains to management of smaller, frequently occurring events, as opposed to larger storms for which drainage and flood control infrastructure are sized. The Four Step Process is summarized below, and elements of the designed development are presented as a means to address and follow this process.

### 1. Step 1: Employ Runoff Reduction Practices

The Site is developed to capture runoff from impervious areas at sump locations and local low points within the public storm system. Impervious area is avoided where functional hardscape is not needed and open space is provided within the subdivision and remains undisturbed where developed lots are not laid out. Pervious landscaped areas are proposed where feasible in order to reduce runoff. Typical lot layouts will include pervious landscape areas surrounding the residences including front yards, rear yards, and side yard swales for drainage. The exact future ratio of pervious to impervious area per lot may vary depending on future homebuilding activity. In order

to calculate estimated runoff reduction for each lot for this project, lots were assumed to have 35% imperviousness as specified by the DCM Volume 1, Table 6-6 for residential lots sized as 0-3 dwelling per acre.

Runoff calculations were completed for three two separate areas, the basins tributary to the permanent water quality and detention facilities 1 and 2, and the basins that flow off Site. The 2 permanent water quality and detention facilities are responsible for all water quality treatment for the Site.

Runoff reduction calculations and results are included in Appendix D. Runoff reduction areas are shown and can be found in the Green Infrastructure Maps, included in Appendix G.

## 2. Step 2: Implement Control Measures That Provide a Water Quality Capture Volume with Slow Release.

Runoff from this development is treated through the capture and timed release of the WQCV via the 2 proposed detention ponds on Site. Proposed ponds 1 and 2 provide the required and necessary WQCV for their respective tributary basins. A drainage map can be found in appendix F.

Basin ID	Total Area (ac)	Total Proposed Disturbed Area (ac)	Area Tributary to Pond 1 (ac)	Area Tributary to Pond 2 (ac)	Disturbed Area Treated (ac)	Un-Disturbed Area un-Treated (ac)
A-1	4.49	4.49	0	4.49	4.49	
A-2	4.83	4.83	4.83		4.83	
A-3	2.46	2.46	2.46		2.46	
A-4	2.55	2.55	2.55		2.55	
A-5	3.52	3.52	3.52		3.52	
A-6	2.75	2.75	2.75		2.75	
B	40.12	0		40.12		
C	41.08	0	41.08			
D	8.26	0	8.26			
E	1.41	0				1.41
F	5.91	0				5.91
G	8.38	0				8.38
TOTAL	125.76	20.6	65.45	44.61	20.6	15.7

## 3. Step 3: Stabilized Drainageways

The Site utilizes concrete curb and gutter to channel stormwater from impervious runoff, mostly paved roadways, and residential lots. Landscaped areas are to be permanently stabilized with

native seeding and mulching as well as trees and shrubbery according to the landscaping plans. Sloped landscaped areas will not exceed 3H:1V grades. The proposed grass lined swale follows El Paso County and City of Colorado Springs drainage criteria. The Site will outfall into the Existing Detention Pond 2.

#### 4. Step 4: Implement Site Specific and Other Control Measures

Site construction is to follow a Stormwater Management Report and Grading and Erosion Control Plan that includes non-structural control measures during the initial, interim, and final phases of construction. As the development is multifamily residential land use, there are no anticipated Site-specific permanent source control measures required for the Site.

### WATER QUALITY ENHANCEMENT CONTROL MEASURES

The proposed ponds 1 and 2 discussed in previous sections shall have infrastructure in place that meets El Paso County and MHFD Urban Storm Drainage Criteria Manuals. The proposed permanent water quality and detention facility is designed to treat the WQCV and detain the EURV and the 100-year detention volumes as well as meet release rate criteria. Runoff from the upstream tributary areas will be conveyed to the permanent water quality and detention facility via storm sewer. A developed drainage plan showing developed areas and their drainage patterns to the permanent water quality and detention facility is included in Appendix G.

Non-structural Best Management Practices that will be incorporated into the project are anticipated to include grass swales. Water quality is provided via side yard grass swales between lots in developed areas throughout the subdivision. It is provided for basins that drain directly offSite and are not tributary to the ponds by way of grass-lined swales, and by having minimal grading with no developed imperviousness in these areas as either open space or permanently seeded and landscaped rear yard areas.

Structural Best Management Practices that are incorporated in the Site design include storm infrastructure within the extended detention basins such as outlet structures and spillways.

### MAINTENANCE

The proposed permanent water quality and detention facility will be maintained by El Paso County. The proposed storm sewer system in the internal streets will be owned and maintained by El Paso County.

## FLOODPLAIN MODIFICATION

There are no floodplain modifications required or proposed for the Site, see Appendix C for the FEMA Flood Zone Map.

## DRAINAGE/BRIDGE FEES AND COST ESTIMATES

The Site lies within the Sand Creek Drainage Basin. The El Paso County Drainage Basin Fees were last updated in 2024 and were used.

The project Site has a total area of 19.66 acres. The following calculations for the imperviousness of the development is shown below.

Average Housing Footprint: =3,400 sf

Total Housing Footprint Area: 3,400 x 24 =21,600 sf

Total ROW Area: =155,700 sf

ROW and Housing Footprint areas are 100% impervious.

Total Impervious Area:  $(21,600 + 155,700) / 43,560 = 4.07$  ac

### **Drainage Fees:**

$\$25,632 \times 4.07$  Imp. Acres = \$104,322.24

### **Bridge Fees:**

$\$10,484 \times 4.07$  Imp. Acres = \$42,669.88

The table below summarizes these costs.

Drainage Basin	Area Impervious (acres)	2024 Drainage Fee (per impervious acre \$)	2024 Bridge Fee (per impervious acre)	Drainage fees (\$)	Bridge Fees (\$)	Total (\$)
Sand Creek	4.07	\$ 25,632.00	\$ 10,484.00	\$ 104,322.24	\$ 42,669.88	\$ 146,992.50

Below is a cost estimate for the proposed storm infrastructure proposed within the filing.

Item	Quantity	Unit	Unit Cost	Cost
<b>Storm Infrastructure</b>				
5' CDOT Type R Inlet	1	EA	\$ 9,200.00	\$ 9,200.00
10' CDOT Type R Inlet	3	EA	\$ 12,800.00	\$ 38,400.00
24" RCP	72	LF	\$ 130.00	\$ 9,360.00
30" RCP	240	LF	\$ 155.00	\$ 37,200.00
36" RCP	504	LF	\$ 212.00	\$ 106,848.00
48" RCP	421	LF	\$ 275.00	\$ 115,775.00
54" RCP	170	LF	\$ 325.00	\$ 55,250.00
5' Manhole	4	EA	\$ 8,200.00	\$ 32,800.00
6' Manhole	3	EA	\$ 10,000.00	\$ 30,000.00
7' Manhole	1	EA	\$ 12,000.00	\$ 12,000.00
<b>PBMPs</b>				
Forebay	5	EA	\$ 15,000.00	\$ 75,000.00
Trickle Channel	1400	LF	\$ 15.00	\$ 21,000.00
Outlet Structure	2	EA	\$ 15,000.00	\$ 30,000.00
Outlet Pipe (36")	115	LF	\$ 212.00	\$ 24,380.00
Outlet Pipe (54")	130	LF	\$ 325.00	\$ 42,250.00
<b>Subtotal</b>				\$ 597,213.00
<b>Contingency (15%)</b>				\$ 89,581.95
<b>Total</b>				\$ 686,794.95

## CONCLUSION

This Final Drainage Plan report describes the proposed storm water management plan for the Falcon Highlands South development Filing 1. This Plan will improve the existing ponds 1 and 2 on Site to current El Paso County standards and will provide water quality treatment and detention of storm water. This document will provide guidance so that the drainage infrastructure constructed throughout the Falcon Highlands South Filing 1 development will function efficiently and effectively. This report follows all standard criteria set forth by the El Paso County Drainage Criteria Manual, El Paso County Engineering Criteria Manual, the City of Colorado Springs Drainage Criteria Manuals Volumes 1, 2, and 3, and the Mile High Flood District Urban Storm Drainage Criteria Manual, with no requested variances. Downstream drainage facilities will not be negatively affected, as existing drainage patterns and allowable release rates shall be maintained. It has been concluded that the proposed Falcon Highlands South Filing 1 development will have no negative impact to infrastructure and development.



## REFERENCES

- 1) Urban Storm Drainage Criteria Manuals; Mile High Flood District; latest edition
- 2) El Paso County Engineering Criteria Manual (ECM), latest revision October 14, 2020
- 3) El Paso County Drainage Criteria Manual (DCM), October 1991; latest revision October 31, 2018
- 4) City of Colorado Springs Drainage Criteria Manuals, Volumes 1, 2, and 3, latest revision May 2014 (Not Adopted by El Paso County)
- 5) Flood Insurance Rate Map of El Paso County Colorado, Federal Emergency Management Agency, Flood Insurance Rate Map No. 08041C0561G and 08041C0545G dated December 7, 2018.
- 6) Hydrologic Soil Group – El Paso County, Colorado, Web Soil Survey, National Cooperative Soils Survey, May 21, 2021
- 7) *Falcon Highlands Filing No. 2 & 3 Final Drainage Report* by Terra Nova Engineering, Inc., latest revision August 2010.
- 8) *Falcon Highlands Phase 2, Filing No. 2 & 3 Master Development Drainage Plan and Preliminary Drainage Report* by Terra Nova Engineering, Inc. latest revision September 2005
- 9) *Bent Grass Residential Subdivision Filing No. 2 (SF-19-014) Final Drainage Report*, latest revision March 2020.
- 10) URS Section for Regional Detention Pond WU, developed by Galloway & Company
- 11) Sand Creek DBPS, developed by Stantec, HDR, and Dewberry dated January 2021 (Not Adopted by El Paso County)
- 12) Falcon DBS, developed by Matrix Design Group dated September 2015

# Appendix B

## Soils Report



United States  
Department of  
Agriculture

**NRCS**

Natural  
Resources  
Conservation  
Service

A product of the National  
Cooperative Soil Survey,  
a joint effort of the United  
States Department of  
Agriculture and other  
Federal agencies, State  
agencies including the  
Agricultural Experiment  
Stations, and local  
participants

# Custom Soil Resource Report for El Paso County Area, Colorado



# Preface

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Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist ([http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\\_053951](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951)).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# How Soil Surveys Are Made

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Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

## Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and



## Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

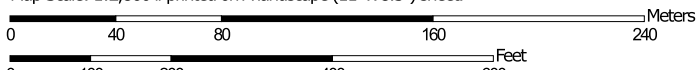
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The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report Soil Map



Map Scale: 1:2,860 if printed on A landscape (11" x 8.5") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84





### MAP LEGEND


**Area of Interest (AOI)**

 Area of Interest (AOI)




















**Soils**







 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

**Special Point Features**






-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 21, Aug 24, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Oct 20, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
9	Blakeland-Fluvaquentic Haplaquolls	19.0	100.0%
<b>Totals for Area of Interest</b>		<b>19.0</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

## Custom Soil Resource Report

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## El Paso County Area, Colorado

### 9—Blakeland-Fluvaquentic Haplaquolls

#### Map Unit Setting

*National map unit symbol:* 36b6  
*Elevation:* 3,500 to 5,800 feet  
*Mean annual precipitation:* 13 to 17 inches  
*Mean annual air temperature:* 46 to 55 degrees F  
*Frost-free period:* 110 to 165 days  
*Farmland classification:* Not prime farmland

#### Map Unit Composition

*Blakeland and similar soils:* 60 percent  
*Fluvaquentic haplaquolls and similar soils:* 38 percent  
*Minor components:* 2 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Blakeland

##### Setting

*Landform:* Hills, flats  
*Landform position (three-dimensional):* Side slope, talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Sandy alluvium derived from arkose and/or eolian deposits derived from arkose

##### Typical profile

*A - 0 to 11 inches:* loamy sand  
*AC - 11 to 27 inches:* loamy sand  
*C - 27 to 60 inches:* sand

##### Properties and qualities

*Slope:* 1 to 9 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Somewhat excessively drained  
*Runoff class:* Low  
*Capacity of the most limiting layer to transmit water (Ksat):* High to very high (5.95 to 19.98 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 5 percent  
*Available water supply, 0 to 60 inches:* Low (about 4.5 inches)

##### Interpretive groups

*Land capability classification (irrigated):* 3e  
*Land capability classification (nonirrigated):* 6e  
*Hydrologic Soil Group:* A  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

## Description of Fluvaquentic Haplaquolls

### Setting

*Landform:* Swales  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Alluvium

### Typical profile

*H1 - 0 to 12 inches:* variable  
*H2 - 12 to 60 inches:* stratified very gravelly sand to loam

### Properties and qualities

*Slope:* 1 to 2 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Poorly drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high  
(0.20 to 6.00 in/hr)  
*Depth to water table:* About 0 to 24 inches  
*Frequency of flooding:* Occasional  
*Frequency of ponding:* None  
*Maximum salinity:* Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Moderate (about 6.2 inches)

### Interpretive groups

*Land capability classification (irrigated):* 6w  
*Land capability classification (nonirrigated):* 6w  
*Hydrologic Soil Group:* D  
*Ecological site:* R048AY241CO - Mountain Meadow  
*Hydric soil rating:* Yes

## Minor Components

### Other soils

*Percent of map unit:* 1 percent  
*Hydric soil rating:* No

### Pleasant

*Percent of map unit:* 1 percent  
*Landform:* Depressions  
*Hydric soil rating:* Yes



# Soil Information for All Uses

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## Soil Reports

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

## Water Features

This folder contains tabular reports that present soil hydrology information. The reports (tables) include all selected map units and components for each map unit. Water Features include ponding frequency, flooding frequency, and depth to water table.

## Hydrologic Soil Group and Surface Runoff

This table gives estimates of various soil water features. The estimates are used in land use planning that involves engineering considerations.

*Hydrologic soil groups* are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The four hydrologic soil groups are:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or

## Custom Soil Resource Report

soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas.

*Surface runoff* refers to the loss of water from an area by flow over the land surface. Surface runoff classes are based on slope, climate, and vegetative cover. The concept indicates relative runoff for very specific conditions. It is assumed that the surface of the soil is bare and that the retention of surface water resulting from irregularities in the ground surface is minimal. The classes are negligible, very low, low, medium, high, and very high.

### Report—Hydrologic Soil Group and Surface Runoff

Absence of an entry indicates that the data were not estimated. The dash indicates no documented presence.

Hydrologic Soil Group and Surface Runoff—El Paso County Area, Colorado			
Map symbol and soil name	Pct. of map unit	Surface Runoff	Hydrologic Soil Group
9—Blakeland-Fluvaquentic Haplaquolls			
Blakeland	60	Low	A
Fluvaquentic haplaquolls	38	Very high	D

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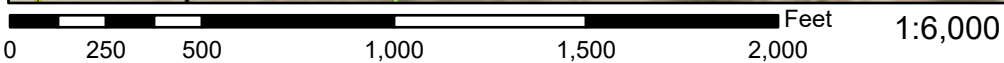
# Appendix C

FEMA Map

# National Flood Hazard Layer FIRMMette



104°37'40"W 38°56'3"N



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

104°37'3"W 38°55'35"N

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

- |                                    |  |  |
|------------------------------------|--|--|
| <b>SPECIAL FLOOD HAZARD AREAS</b>  |  | Without Base Flood Elevation (BFE)<br><i>Zone A, V, A99</i>  |
|                                    |  | With BFE or Depth <i>Zone AE, AO, AH, VE, AR</i>   |
|                                    |  | Regulatory Floodway  |
| <b>OTHER AREAS OF FLOOD HAZARD</b> |  | 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile <i>Zone X</i> |
|                                    |  | Future Conditions 1% Annual Chance Flood Hazard <i>Zone X</i>  |
|                                    |  | Area with Reduced Flood Risk due to Levee. See Notes. <i>Zone X</i>  |
|                                    |  | Area with Flood Risk due to Levee <i>Zone D</i>  |
| <b>OTHER AREAS</b>                 |  | NO SCREEN Area of Minimal Flood Hazard <i>Zone X</i>   |
|                                    |  | Effective LOMRs  |
| <b>GENERAL STRUCTURES</b>          |  | Area of Undetermined Flood Hazard <i>Zone D</i>  |
|                                    |  | Channel, Culvert, or Storm Sewer   |
|                                    |  | Levee, Dike, or Floodwall  |
| <b>OTHER FEATURES</b>              |  | 20.2 Cross Sections with 1% Annual Chance  |
|                                    |  | 17.5 Water Surface Elevation   |
|                                    |  | Coastal Transect   |
|                                    |  | Base Flood Elevation Line (BFE)  |
|                                    |  | Limit of Study   |
| <b>MAP PANELS</b>                  |  | Jurisdiction Boundary  |
|                                    |  | Coastal Transect Baseline  |
|                                    |  | Profile Baseline   |
|                                    |  | Hydrographic Feature   |
|                                    |  | Digital Data Available   |
|                                    |  | No Digital Data Available  |
|                                    |  | Unmapped   |
|                                    |  | The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.                                     |



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **5/21/2021 at 11:21 AM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

# Appendix D

## Hydrologic Calculations

**Calculation of Peak Runoff using Rational Method**

Designer: LMS  
 Company: Atwell, LLC  
 Date: 12/5/2024  
 Project: Falcon Highlands  
 Location:

Version 2.00 released May 2017

Cells of this color are for required user-input  
 Cells of this color are for optional override values  
 Cells of this color are for calculated results based on overrides

$$t_t = \frac{0.395(1.1 - C_s)\sqrt{L_t}}{S_t^{0.333}}$$

$$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$$

Computed  $t_c = t_t + t_t$

Regional  $t_c = (26 - 17t) + \frac{L_t}{60(14t + 9)\sqrt{S_t}}$

$t_{\text{minimum}} = 5$  (urban)  
 $t_{\text{minimum}} = 10$  (non-urban)

Selected  $t_c = \max\{t_{\text{minimum}}, \min(\text{Computed } t_c, \text{Regional } t_c)\}$

Select UDFCD location for NOAA Atlas 14 Rainfall Depths from the pulldown list OR enter your own depths obtained from the NOAA website (click this link)

1-hour rainfall depth, P1 (in) =	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr
	1.16	1.44	1.68	1.92	2.16	2.42	
Rainfall Intensity Equation Coefficients =	a	b	c	$I(\text{in/hr}) = \frac{a * P_t}{(b + t_c)^c}$			
	28.50	10.00	0.786				

$Q(\text{cfs}) = CIA$

Subcatchment Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	Runoff Coefficient, C							Overland (Initial) Flow Time							Channelized (Travel) Flow Time							Time of Concentration			Rainfall Intensity, I (in/hr)							Peak Flow, Q (cfs)						
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	Overland Flow Length L <sub>t</sub> (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S <sub>t</sub> (ft/ft)	Overland Flow Time t <sub>t</sub> (min)	Channelized Flow Length L <sub>t</sub> (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S <sub>t</sub> (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V <sub>t</sub> (ft/sec)	Channelized Flow Time t <sub>t</sub> (min)	Computed t <sub>c</sub> (min)	Regional t <sub>c</sub> (min)	Selected t <sub>c</sub> (min)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr		
EX-1	3.38	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.050	19.88	1250.00			0.020	5	0.71	29.46	49.34	40.34	40.34	1.52	1.89	2.20	2.51	2.83	3.17		0.09	0.12	0.16	0.26	0.65	1.60			
EX-2	9.38	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.090	16.37	975.00			0.030	5	0.87	18.76	35.14	34.82	34.82	1.66	2.07	2.41	2.75	3.10	3.47		0.27	0.36	0.49	0.79	1.97	4.85			
EX-3	9.14	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.090	16.37	440.00			0.020	5	0.71	10.37	26.74	30.50	26.74	1.95	2.42	2.82	3.22	3.62	4.06		0.30	0.42	0.56	0.90	2.24	5.53			
OS-1	6.38	A	34.3	0.21	0.22	0.23	0.27	0.32	0.38	0.48	25.00			0.020	6.32	650.00			0.030	20	3.46	3.13	9.45	24.70	9.45	3.21	3.98	4.65	5.31	5.97	6.69		4.27	5.58	6.92	9.00	12.12	16.11			
OS-2	3.12	A	40.0	0.25	0.27	0.28	0.32	0.37	0.42	0.51	50.00			0.020	8.46	2180.00			0.020	20	2.83	12.85	21.30	36.80	21.30	2.21	2.74	3.20	3.65	4.11	4.60		1.75	2.29	2.82	3.60	4.70	6.06			
OS-3	1.14	A	100.0	0.84	0.86	0.87	0.88	0.88	0.89	0.90	20.00			0.020	1.54	1190.00			0.020	20	2.83	7.01	8.55	15.10	8.55	3.33	4.13	4.82	5.51	6.20	6.95		3.19	4.06	4.80	5.55	6.21	7.04			
OS-4	13.09	A	23.8	0.13	0.14	0.15	0.18	0.23	0.30	0.41	80.00			0.020	12.36	2300.00			0.020	20	2.83	13.55	25.91	43.93	25.91	1.98	2.46	2.87	3.28	3.69	4.13		3.36	4.44	5.59	7.56	11.02	15.98			
OS-5	59.62	A	40.0	0.25	0.27	0.28	0.32	0.37	0.42	0.51	100.00			0.020	11.96	608.00			0.020	20	2.83	3.58	15.54	24.11	15.54	2.59	3.21	3.75	4.29	4.82	5.40		39.33	51.26	63.13	80.65	105.39	135.79			
OS-6	35.75	A	25.0	0.14	0.15	0.16	0.19	0.24	0.30	0.42	300.00			0.020	23.71	0.00			0.006	20	1.55	0.00	23.71	21.75	21.75	2.18	2.71	3.16	3.61	4.06	4.55		10.78	14.22	17.88	24.03	34.65	49.60			
OS-7	6.47	A	25.0	0.14	0.15	0.16	0.19	0.24	0.30	0.42	300.00			0.020	23.71	300.00			0.006	20	1.55	3.23	26.94	26.91	26.91	1.94	2.41	2.81	3.21	3.61	4.04		1.73	2.29	2.87	3.86	5.57	7.97			
OS-8	3.74	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	202.00			0.020	22.07	910.00			0.010	15	1.50	10.11	32.18	40.79	32.18	1.75	2.17	2.53	2.89	3.25	3.64		0.11	0.15	0.21	0.33	0.82	2.03			
OS-9	3.14	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	75.00			0.020	13.45	150.00			0.030	15	2.60	0.96	14.41	26.64	14.41	2.68	3.33	3.89	4.44	5.00	5.60		0.14	0.20	0.27	0.43	1.06	2.62			
OS-10	3.67	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	125.00			0.020	17.36	630.00			0.016	15	1.90	5.53	22.90	33.71	22.90	2.12	2.63	3.07	3.51	3.95	4.43		0.13	0.18	0.25	0.39	0.98	2.42			
OS-11	35.55	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.020	26.90	950.00			0.010	15	1.50	10.56	37.45	41.47	37.45	1.59	1.98	2.30	2.63	2.96	3.32		0.96	1.32	1.78	2.85	7.13	17.58			
OS-12	39.29	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.020	26.90	570.00			0.010	15	1.50	6.33	33.23	34.94	33.23	1.71	2.13	2.48	2.83	3.19	3.57		1.14	1.57	2.12	3.39	8.48	20.90			
OS-13	10.54	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.020	26.90	360.00			0.010	15	1.50	4.00	30.90	31.34	30.90	1.79	2.22	2.59	2.96	3.33	3.73		0.32	0.44	0.59	0.95	2.38	5.86			
OS-14	8.84	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	200.00			0.020	21.96	630.00			0.011	15	1.57	6.67	28.64	35.47	28.64	1.87	2.32	2.71	3.10	3.48	3.90		0.28	0.39	0.52	0.83	2.08	5.14			



### Calculation of Peak Runoff using Rational Method

Designer: LMS  
 Company: Atwell, LLC  
 Date: 1/2/2025  
 Project: Falcon Highlands  
 Location:

Version 2.00 released May 2017

Cells of this color are for required user-input  
 Cells of this color are for optional override values  
 Cells of this color are for calculated results based on overrides

$$t_t = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_i^{0.333}}$$

$$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$$

Computed  $t_c = t_t + t_t$

$$\text{Regional } t_c = (26 - 17t) + \frac{L_t}{60(14t + 9)\sqrt{S_t}}$$

$t_{\text{minimum}} = 5$  (urban)  
 $t_{\text{minimum}} = 10$  (non-urban)

Selected  $t_c = \max\{t_{\text{minimum}}, \min(\text{Computed } t_c, \text{Regional } t_c)\}$

Select UDFCD location for NOAA Atlas 14 Rainfall Depths from the pulldown list OR enter your own depths obtained from the NOAA website (click this link)

1-hour rainfall depth, P1 (in) =

2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr
1.16	1.44	1.68	1.92	2.16	2.42	

Rainfall Intensity Equation Coefficients =

a	b	c
28.50	10.00	0.786

$$I(\text{in/hr}) = \frac{a \cdot P_t}{(b + t_c)^c}$$

Q(cfs) = CIA

Subcatchment Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	Runoff Coefficient, C							Overland (Initial) Flow Time				Channelized (Travel) Flow Time				Time of Concentration			Rainfall Intensity, I (in/hr)							Peak Flow, Q (cfs)									
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	Overland Flow Length L <sub>i</sub> (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S <sub>i</sub> (ft/ft)	Overland Flow Time t <sub>t</sub> (min)	Channelized Flow Length L <sub>i</sub> (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S <sub>i</sub> (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V <sub>i</sub> (ft/sec)	Channelized Flow Time t <sub>t</sub> (min)	Computed t <sub>c</sub> (min)	Regional t <sub>c</sub> (min)	Selected t <sub>c</sub> (min)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
A-1	4.49	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	200.00			0.020	21.96	1600.00			0.005	10	0.71	37.71	59.67	64.03	59.67	1.18	1.46	1.70	1.95	2.19	2.45		0.09	0.12	0.17	0.27	0.67	1.64
A-2	4.83	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	200.00			0.020	17.76	650.00			0.013	20	2.24	4.84	22.61	27.02	22.61	2.14	2.65	3.10	3.54	3.98	4.46		2.21	2.89	3.58	4.64	6.23	8.24
A-3	2.46	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	200.00			0.020	17.76	625.00			0.013	20	2.24	4.66	22.42	26.75	22.42	2.15	2.66	3.11	3.55	4.00	4.48		1.13	1.48	1.83	2.37	3.19	4.22
A-6	2.75	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	200.00			0.020	17.76	975.00			0.020	20	2.83	5.75	23.51	28.32	23.51	2.09	2.60	3.03	3.46	3.90	4.36		1.23	1.61	2.00	2.59	3.47	4.59
A-4	2.55	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	200.00			0.020	17.76	550.00			0.010	20	2.00	4.58	22.35	26.64	22.35	2.15	2.67	3.11	3.56	4.00	4.49		1.17	1.54	1.90	2.47	3.31	4.38
A-5	3.52	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	100.00			0.020	12.56	700.00			0.010	20	2.00	5.83	18.39	28.44	18.39	2.38	2.96	3.45	3.94	4.44	4.97		1.80	2.35	2.91	3.77	5.06	6.70
B	40.12	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	100.00			0.020	12.56	1900.00			0.005	20	1.41	22.39	34.95	52.27	34.95	1.66	2.06	2.40	2.75	3.09	3.46		14.26	18.65	23.11	29.95	40.18	53.18
C	41.08	A	35.0	0.21	0.23	0.24	0.27	0.32	0.38	0.48	120.00			0.020	13.76	600.00			0.005	20	1.41	7.07	20.83	30.22	20.83	2.23	2.77	3.23	3.70	4.16	4.66		19.65	25.69	31.82	41.25	55.34	73.24
D	8.26	A	65.0	0.48	0.50	0.51	0.54	0.58	0.62	0.67	120.00			0.020	9.49	600.00			0.020	10	1.41	7.07	16.56	18.86	16.56	2.51	3.12	3.64	4.16	4.68	5.24		9.94	12.79	15.42	18.70	22.40	26.67
E	1.41	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	150.00			0.020	19.02	0.00			0.020	10	1.41	0.00	19.02	25.15	19.02	2.34	2.91	3.39	3.88	4.36	4.89		0.06	0.08	0.10	0.17	0.42	1.03
F	5.91	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.020	26.90	240.00			0.020	20	2.83	1.41	28.31	28.07	28.07	1.89	2.35	2.74	3.13	3.52	3.95		0.19	0.26	0.35	0.56	1.41	3.48
G	8.38	A	5.0	0.02	0.02	0.02	0.03	0.07	0.15	0.29	300.00			0.020	26.90	240.00			0.020	20	2.83	1.41	28.31	28.07	28.07	1.89	2.35	2.74	3.13	3.52	3.95		0.27	0.37	0.50	0.80	2.00	4.93
OS-1	6.38	A	34.3	0.21	0.22	0.23	0.27	0.32	0.38	0.48	25.00			0.020	6.32	650.00			0.020	20	2.83	3.83	10.15	25.72	10.15	3.12	3.87	4.52	5.16	5.81	6.51		4.15	5.43	6.73	8.75	11.78	15.66
OS-2	3.12	A	40.0	0.25	0.27	0.28	0.32	0.37	0.42	0.51	50.00			0.020	8.46	2180.00			0.020	20	2.83	12.85	21.30	36.80	21.30	2.21	2.74	3.20	3.65	4.11	4.60		1.75	2.29	2.82	3.60	4.70	6.06
OS-3	1.14	A	100.0	0.84	0.86	0.87	0.88	0.88	0.89	0.90	20.00			0.020	1.54	1190.00			0.020	20	2.83	7.01	8.55	15.10	8.55	3.33	4.13	4.82	5.51	6.20	6.95		3.19	4.06	4.80	5.55	6.21	7.04
OS-4	13.09	A	23.8	0.13	0.14	0.15	0.18	0.23	0.30	0.41	80.00			0.020	12.36	2300.00			0.020	20	2.83	13.55	25.91	43.93	25.91	1.98	2.46	2.87	3.28	3.69	4.13		3.36	4.44	5.59	7.56	11.02	15.98
OS-5	59.62	A	40.0	0.25	0.27	0.28	0.32	0.37	0.42	0.51	100.00			0.020	11.96	608.00			0.006	20	1.55	6.54	18.50	28.16	18.50	2.38	2.95	3.44	3.93	4.42	4.96		36.09	47.03	57.92	74.00	96.69	124.58
OS-6	35.75	A	25.0	0.14	0.15	0.16	0.19	0.24	0.30	0.42	300.00			0.020	23.71	0.00			0.006	20	1.55	0.00	23.71	23.71	23.71	2.18	2.71	3.16	3.61	4.06	4.55		10.78	14.22	17.88	24.03	34.65	49.60
OS-7	6.47	A	25.0	0.14	0.15	0.16	0.19	0.24	0.30	0.42	300.00			0.020	23.71	300.00			0.020	20	2.83	1.77	25.48	24.58	24.58	2.04	2.53	2.96	3.38	3.80	4.26		1.82	2.41	3.03	4.07	5.86	8.39

# Appendix E

## Hydraulic Calculations

# INLET MANAGEMENT

Worksheet Protected

INLET NAME	A-2	A-3	A-4	A-5
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET
Hydraulic Condition	On Grade	On Grade	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

## USER-DEFINED INPUT

User-Defined Design Flows				
Minor $Q_{known}$ (cfs)	2.9	1.5	1.5	2.4
Major $Q_{known}$ (cfs)	8.2	4.2	4.4	6.7

Bypass (Carry-Over) Flow from Upstream <span style="color: blue;">Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.</span>				
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	A-3	A-2
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.2	2.1

Watershed Characteristics				
Subcatchment Area (acres)				
Percent Impervious				
NRCS Soil Type				

Watershed Profile				
Overland Slope (ft/ft)				
Overland Length (ft)				
Channel Slope (ft/ft)				
Channel Length (ft)				

Minor Storm Rainfall Input				
Design Storm Return Period, $T_r$ (years)				
One-Hour Precipitation, $P_1$ (inches)				

Major Storm Rainfall Input				
Design Storm Return Period, $T_r$ (years)				
One-Hour Precipitation, $P_1$ (inches)				

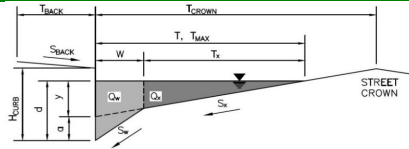
## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>2.9</b>	<b>1.5</b>	<b>1.5</b>	<b>2.4</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>8.2</b>	<b>4.2</b>	<b>4.6</b>	<b>8.8</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	0.0	0.0	N/A	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	2.1	0.2	N/A	N/A

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID: **A-2**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 5.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.013$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.7$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_0 = 0.020$  ft/ft  
 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	7.2	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Spread Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

$Q_{allow} =$ 

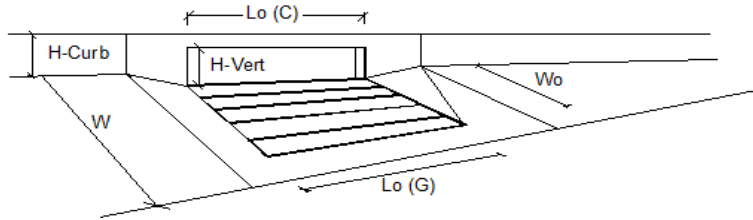
Minor Storm	Major Storm
18.9	18.9

 cfs

**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 2.90 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.20 cfs on sheet 'Inlet Management'**

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.03 (August 2023)

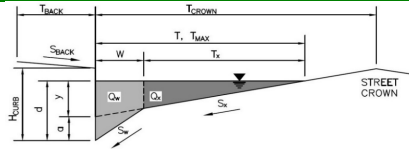


Design Information (Input)	MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening			
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_u =$	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_u =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f (G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f (C) =$	0.10	0.10	
Street Hydraulics: OK - $Q <$ Allowable Street Capacity				
Total Inlet Interception Capacity	$Q =$	2.9	6.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	2.1	cfs
Capture Percentage = $Q_c/Q_s$	$C\% =$	100	74	%

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:**  
**Inlet ID:** A-3



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$ =	5.0	ft
$S_{BACK}$ =	0.020	ft/ft
$n_{BACK}$ =	0.013	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$ =	6.00	inches
$T_{CROWN}$ =	17.7	ft
$W$ =	2.00	ft
$S_x$ =	0.020	ft/ft
$S_w$ =	0.083	ft/ft
$S_0$ =	0.020	ft/ft
$n_{STREET}$ =	0.013	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX}$ =	17.0	17.0	ft
$d_{MAX}$ =	6.0	7.2	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

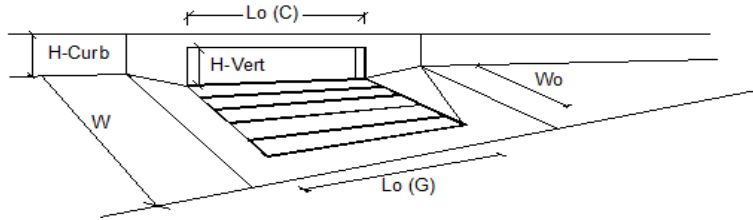
MINOR STORM Allowable Capacity is based on Spread Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

	Minor Storm	Major Storm	
$Q_{allow}$ =	18.9	18.9	cfs

**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 1.50 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 4.20 cfs on sheet 'Inlet Management'**

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.03 (August 2023)

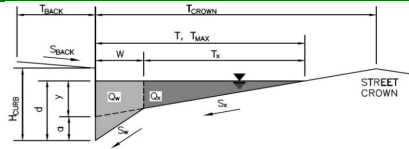


Design Information (Input)	MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening			
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_u =$	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_u =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f (G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f (C) =$	0.10	0.10	
Street Hydraulics: OK - $Q <$ Allowable Street Capacity				
Total Inlet Interception Capacity	$Q =$	1.5	4.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_o =$	0.0	0.2	cfs
Capture Percentage = $Q_i/Q_o$	$C\% =$	100	95	%

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:**  
**Inlet ID:** A-4



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 5.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.013$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.7$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	7.2	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

$Q_{allow} =$ 

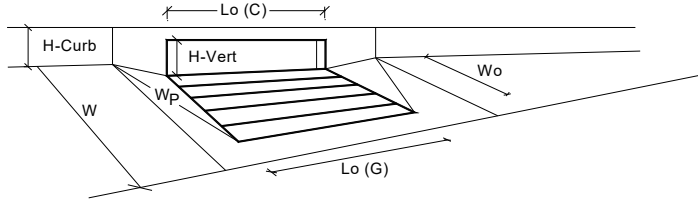
Minor Storm	Major Storm
<b>SUMP</b>	<b>SUMP</b>

 cfs



# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

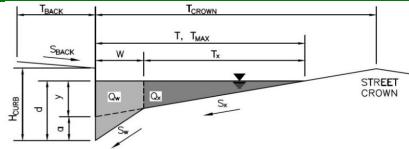


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	5.6	7.2	inches
<b>Grate Information</b>	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
<b>Curb Opening Information</b>	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.30	0.43	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>	MINOR	MAJOR	
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;0 Peak)</b>	4.6	8.0	cfs
<b>Q<sub>PEAK</sub> REQUIRED</b>	1.5	4.6	cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:**  
**Inlet ID:** A-5



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 5.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.013$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.7$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	7.2	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

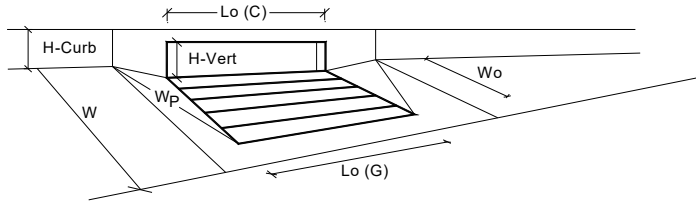
$Q_{allow} =$ 

Minor Storm	Major Storm
<b>SUMP</b>	<b>SUMP</b>

 cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

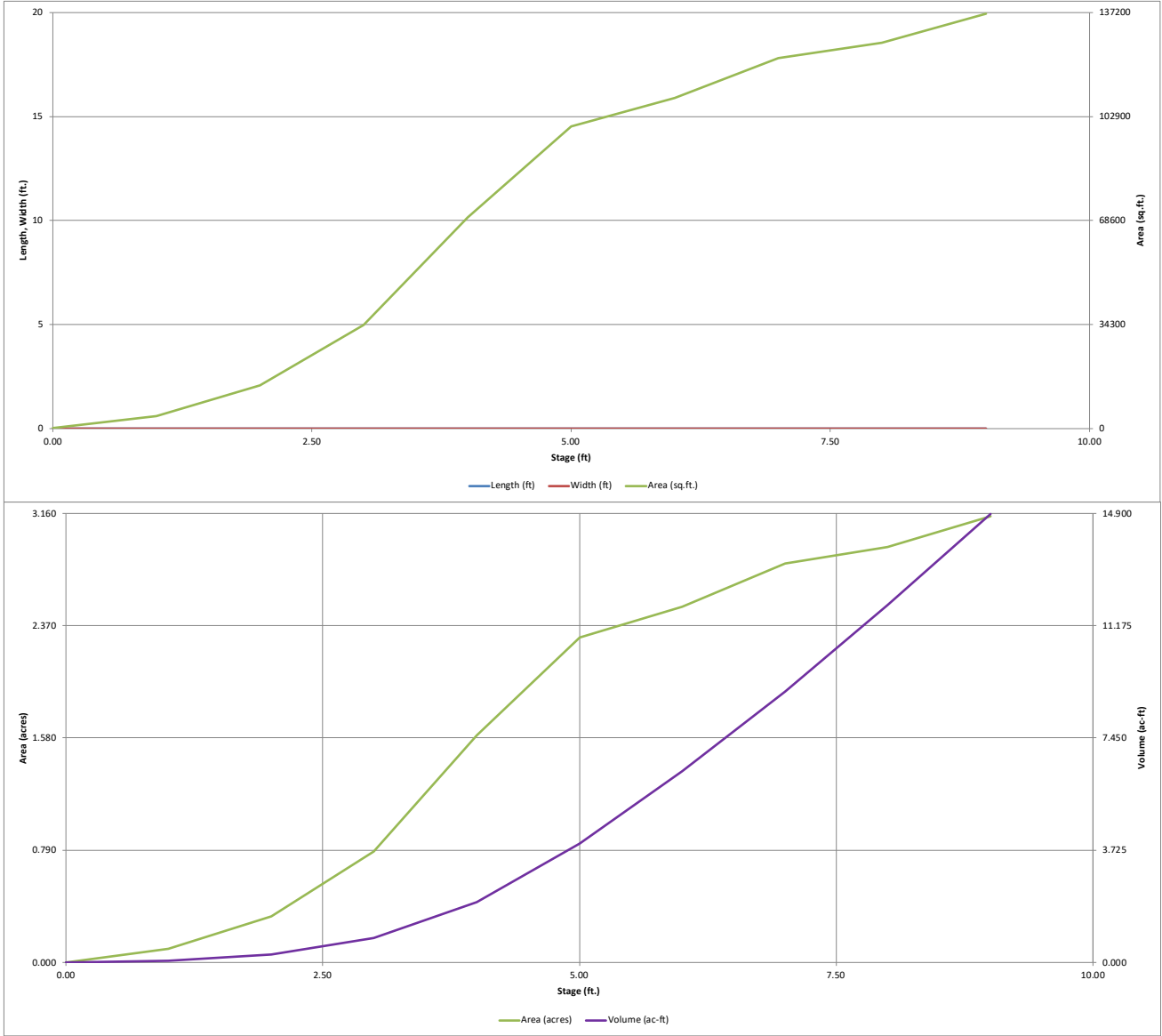


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	5.6	7.2	inches
<b>Grate Information</b>	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
<b>Curb Opening Information</b>	MINOR	MAJOR	
Length of a Unit Curb Opening	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.30	0.43	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	0.91	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>	MINOR	MAJOR	
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;0 Peak)</b>	6.9	13.1	cfs
<b>Q<sub>PEAK REQUIRED</sub></b>	2.4	8.8	cfs



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

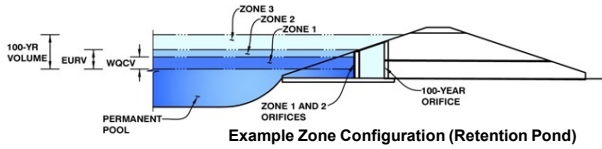
*MHFD-Detention, Version 4.06 (July 2022)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.06 (July 2022)

**Project: Falcon Highlands**  
**Basin ID: Pond 1**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.25	2.411	Orifice Plate
Zone 2 (EURV)	7.07	6.771	Orifice Plate
Zone 3 (100-year)	8.62	4.500	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>13.683</b>	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain		
Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	7.10	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate		
WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.40	4.80	6.00				
Orifice Area (sq. inches)	9.15	9.15	34.00	34.00				
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orif		
Vertical Orifice Area =	N/A	N/A
Vertical Orifice Centroid =	N/A	N/A

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.10	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	23.00	N/A	feet
Overflow Weir Gate Slope =	5.00	N/A	H:V
Horiz. Length of Weir Sides =	5.82	N/A	feet
Overflow Gate Type =	Close Mesh Gate	N/A	
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir		
Height of Gate Upper Edge, H <sub>t</sub> =	8.26	N/A
Overflow Weir Slope Length =	5.94	N/A
Gate Open Area / 100-yr Orifice Area =	23.89	N/A
Overflow Gate Open Area w/o Debris =	107.98	N/A
Overflow Gate Open Area w/ Debris =	53.99	N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	26.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate		
Outlet Orifice Area =	4.52	N/A
Outlet Orifice Centroid =	1.16	N/A
Half-Central Angle of Restrictor Plate on Pipe =	2.39	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	9.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	110.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway		
Spillway Design Flow Depth =	0.98	feet
Stage at Top of Freeboard =	10.98	feet
Basin Area at Top of Freeboard =	3.14	acres
Basin Volume at Top of Freeboard =	14.89	acre-ft

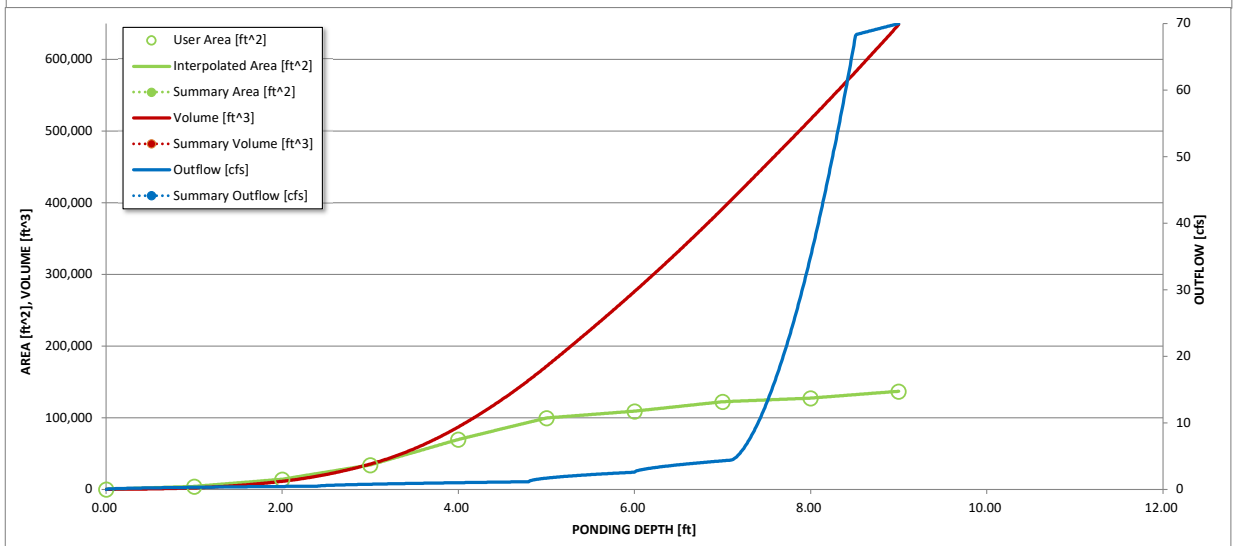
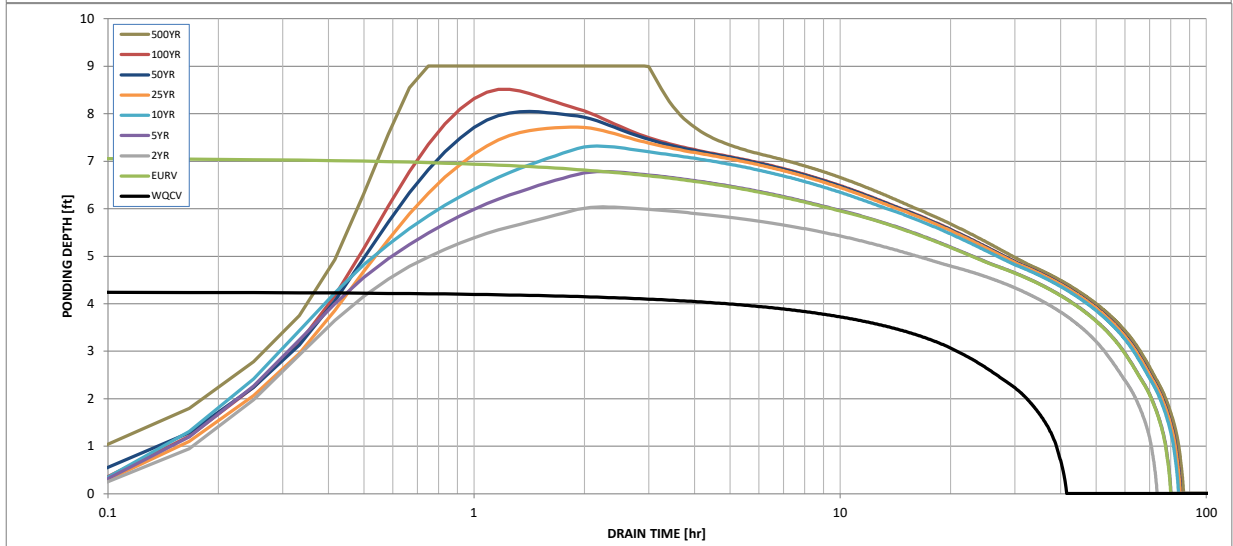
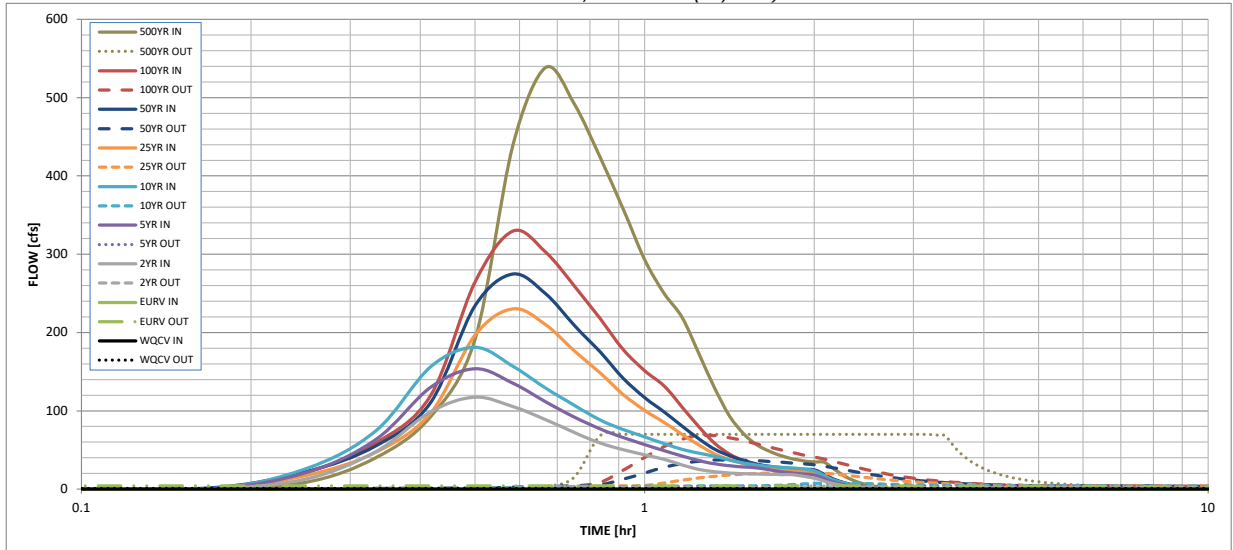
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AA)

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
Design Storm Return Period =								
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	2.411	9.182	6.802	8.919	10.620	12.843	15.025	17.675
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	6.802	8.919	10.620	12.843	15.025	17.675
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.9	1.7	2.4	21.9	43.6	72.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.02	0.19	0.38	0.64
Peak Inflow Q (cfs) =	N/A	N/A	117.6	153.8	181.1	230.3	274.6	329.5
Peak Outflow Q (cfs) =	1.0	4.4	2.8	4.0	7.8	21.1	37.4	68.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.3	3.2	1.0	0.9	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.2	0.3	0.6
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	70	66	71	73	72	71	69
Time to Drain 99% of Inflow Volume (hours) =	40	76	70	76	79	80	79	78
Maximum Ponding Depth (ft) =	4.25	7.07	6.03	6.78	7.32	7.72	8.04	8.51
Area at Maximum Ponding Depth (acres) =	1.77	2.81	2.51	2.74	2.84	2.89	2.93	3.03
Maximum Volume Stored (acre-ft) =	2.420	9.187	6.411	8.353	9.866	11.012	11.971	13.373

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	1.46	0.15	8.66
	0:15:00	0.00	0.00	12.85	20.88	25.90	17.42	21.99	21.29	40.05
	0:20:00	0.00	0.00	47.77	63.25	74.60	47.26	55.15	58.92	92.26
	0:25:00	0.00	0.00	98.59	129.86	156.05	96.97	110.60	119.25	191.29
	0:30:00	0.00	0.00	117.56	153.76	181.06	196.57	234.13	264.36	438.42
	0:35:00	0.00	0.00	105.39	135.30	157.08	230.35	274.64	329.46	538.20
	0:40:00	0.00	0.00	88.89	111.59	129.16	209.99	249.61	302.87	492.00
	0:45:00	0.00	0.00	72.20	91.97	107.09	176.45	209.19	259.57	423.87
	0:50:00	0.00	0.00	58.77	76.86	88.34	148.58	175.28	217.74	357.49
	0:55:00	0.00	0.00	50.32	65.89	76.18	120.79	141.44	178.08	292.91
	1:00:00	0.00	0.00	43.91	57.00	66.77	100.43	116.92	151.28	249.75
	1:05:00	0.00	0.00	38.00	48.99	58.01	85.17	98.70	131.83	218.72
	1:10:00	0.00	0.00	30.86	42.25	50.61	69.68	80.30	104.48	171.80
	1:15:00	0.00	0.00	25.18	36.27	45.73	55.98	63.96	79.10	127.98
	1:20:00	0.00	0.00	22.25	32.22	41.77	44.64	50.61	58.05	92.86
	1:25:00	0.00	0.00	20.70	29.81	37.03	37.72	42.62	44.50	70.23
	1:30:00	0.00	0.00	19.77	28.26	33.28	32.32	36.41	36.47	56.52
	1:35:00	0.00	0.00	19.28	27.23	30.77	28.46	32.03	31.57	48.12
	1:40:00	0.00	0.00	18.89	24.68	29.02	25.91	29.15	28.23	42.37
	1:45:00	0.00	0.00	18.61	22.26	27.83	24.31	27.34	26.04	38.58
	1:50:00	0.00	0.00	18.43	20.61	27.01	23.17	26.06	24.54	36.01
	1:55:00	0.00	0.00	16.21	19.43	25.74	22.46	25.26	23.74	34.69
	2:00:00	0.00	0.00	13.96	18.09	23.38	22.02	24.77	23.44	34.24
	2:05:00	0.00	0.00	10.31	13.55	17.26	16.68	18.75	17.81	25.97
	2:10:00	0.00	0.00	6.98	9.14	11.68	11.25	12.63	12.06	17.55
	2:15:00	0.00	0.00	4.70	6.15	7.94	7.66	8.59	8.23	11.96
	2:20:00	0.00	0.00	3.12	4.02	5.27	5.11	5.73	5.48	7.94
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	2:30:00	0.00	0.00	1.19	1.66	2.15	2.15	2.40	2.29	3.30
	2:35:00	0.00	0.00	0.62	0.95	1.19	1.24	1.38	1.32	1.88
	2:40:00	0.00	0.00	0.26	0.44	0.53	0.58	0.64	0.61	0.86
	2:45:00	0.00	0.00	0.08	0.13	0.14	0.17	0.18	0.17	0.23
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
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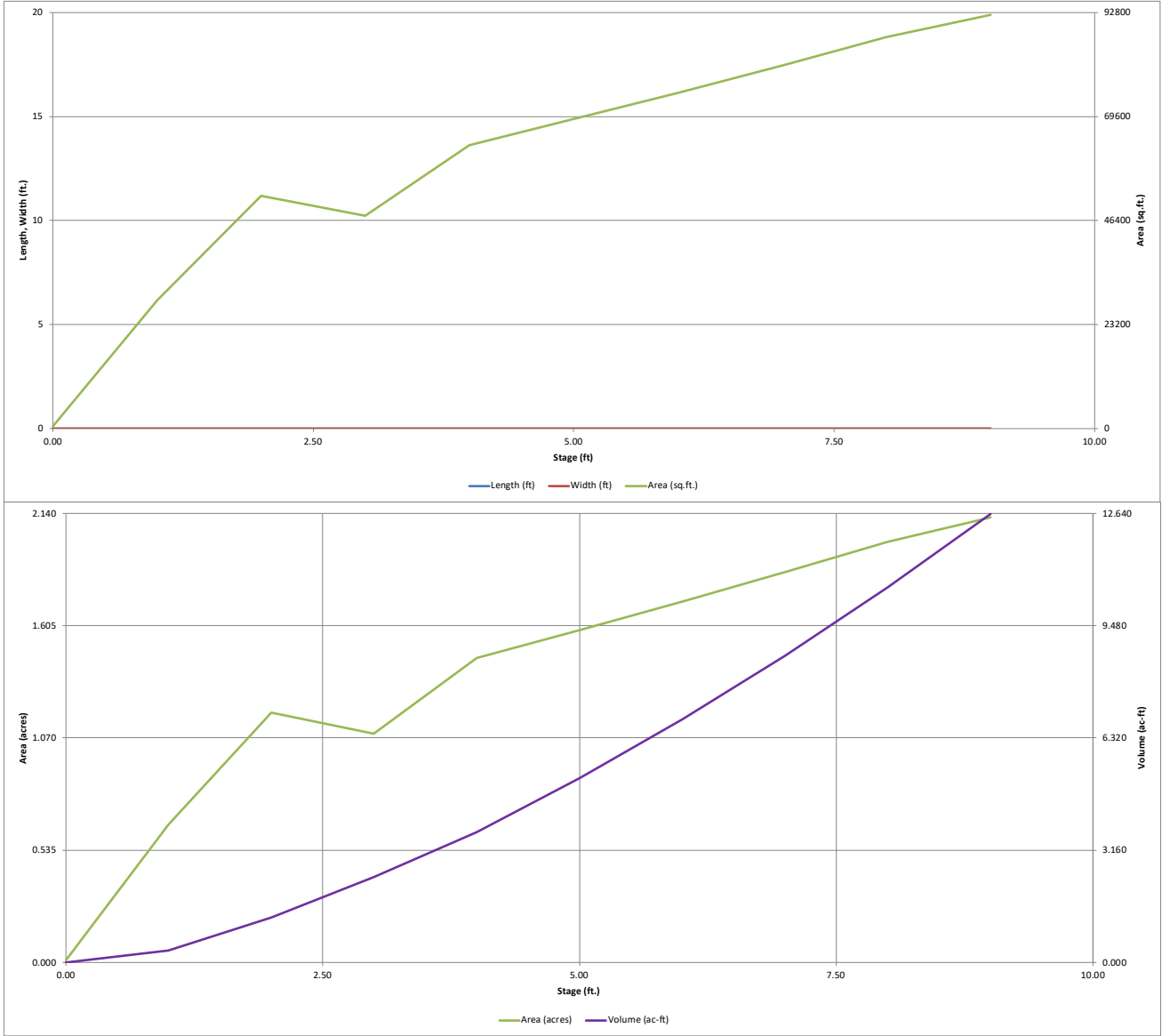






# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.06 (July 2022)*

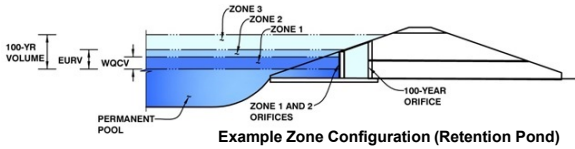


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention*, Version 4.06 (July 2022)

**Project:** Falcon Highlands

**Basin ID:** Pond 2



**Example Zone Configuration (Retention Pond)**

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.68	2.033	Orifice Plate
Zone 2 (EURV)	6.52	5.710	Orifice Plate
Zone 3 (100-year)	8.49	3.795	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>11.539</b>	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	N/A ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	6.60	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate	
WQ Orifice Area per Row =	N/A ft <sup>2</sup>
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.20	4.40					
Orifice Area (sq. inches)	14.00	18.00	18.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice	
Vertical Orifice Area =	N/A ft <sup>2</sup>
Vertical Orifice Centroid =	N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	6.60	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.67	N/A	feet
Overflow Weir Gate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	2.91	N/A	feet
Overflow Gate Type =	Close Mesh Gate	N/A	
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir	
Height of Gate Upper Edge, H <sub>u</sub> =	7.33 feet
Overflow Weir Slope Length =	3.00 feet
Grate Open Area / 100-yr Orifice Area =	8.56
Overflow Gate Open Area w/o Debris =	13.45 ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	6.73 ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	12.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate	
Outlet Orifice Area =	1.57 ft <sup>2</sup>
Outlet Orifice Centroid =	0.58 feet
Half-Central Angle of Restrictor Plate on Pipe =	1.57 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	8.90	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	95.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway	
Spillway Design Flow Depth =	0.97 feet
Stage at Top of Freeboard =	10.87 feet
Basin Area at Top of Freeboard =	2.12 acres
Basin Volume at Top of Freeboard =	12.62 acre-ft

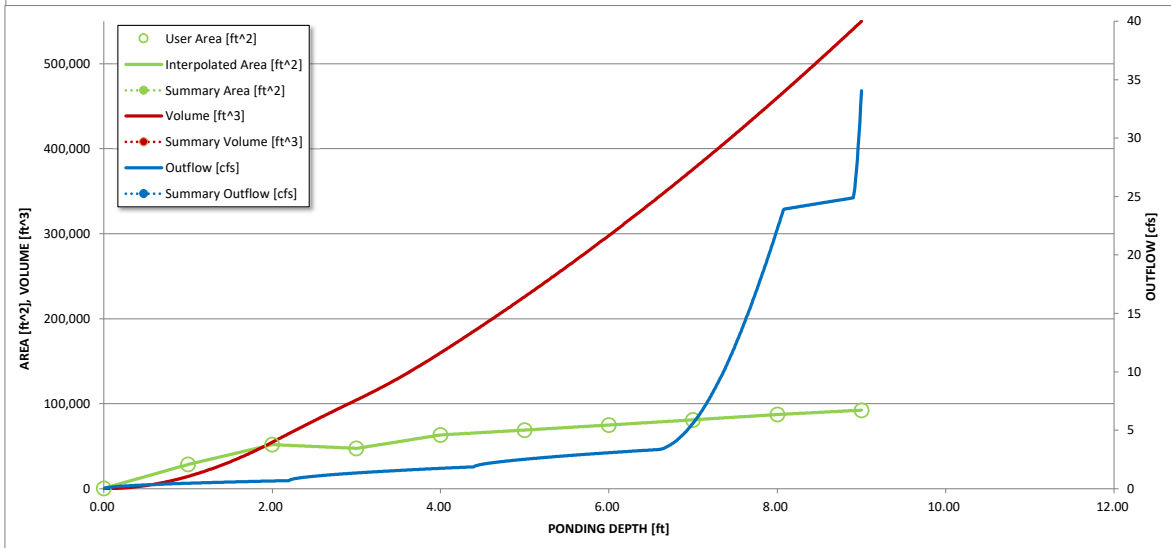
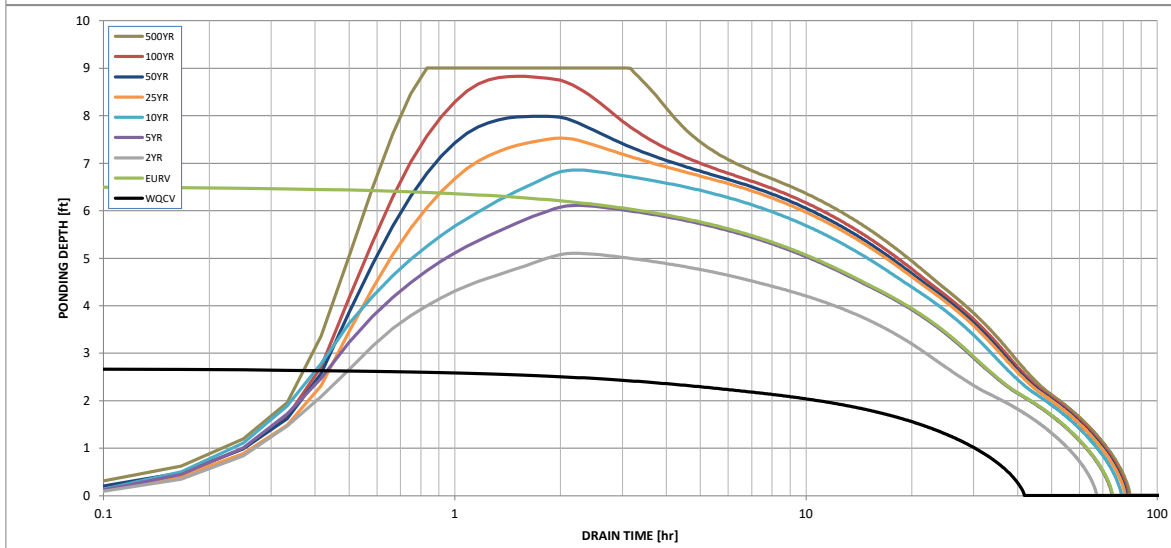
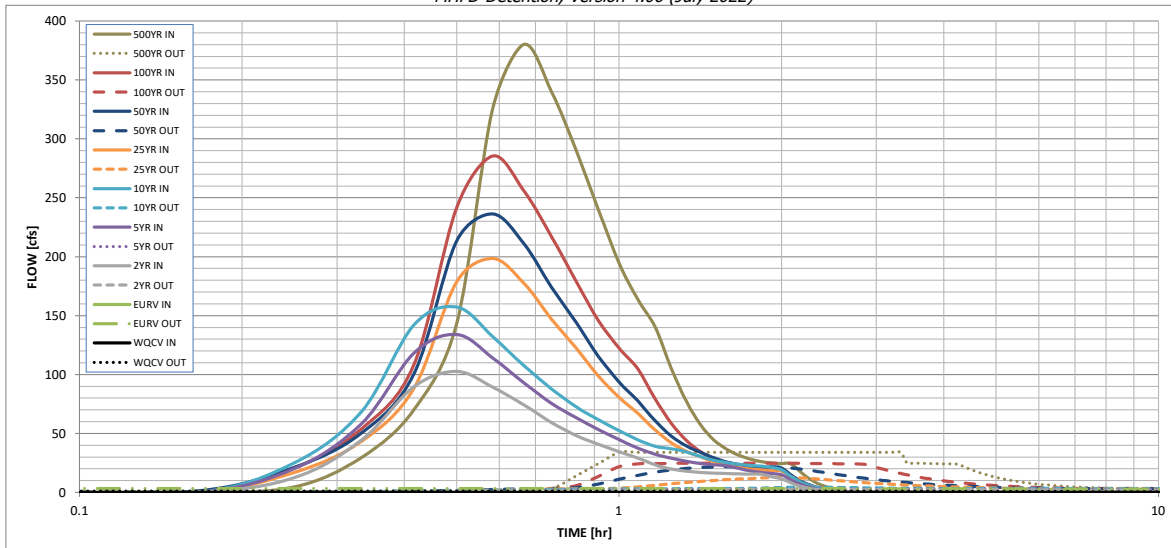
**Routed Hydrograph Results**

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
One-Hour Rainfall Depth (in) =	2.033	7.743	5.700	7.474	8.895	10.744	12.566	14.781	19.627
CUHP Runoff Volume (acre-ft) =	N/A	N/A	5.700	7.474	8.895	10.744	12.566	14.781	19.627
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.8	1.6	2.2	20.0	39.8	64.9	116.6
OPTIONAL CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.02	0.21	0.41	0.68	1.21
Peak Inflow Q (cfs) =	N/A	N/A	102.6	134.0	157.3	198.5	236.4	285.5	380.1
Peak Outflow Q (cfs) =	1.2	3.3	2.6	3.1	4.5	12.8	21.9	24.8	34.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.0	2.0	0.6	0.5	0.4	0.3
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	N/A
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.7	1.3	1.5	1.5
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	66	60	66	69	70	69	68	66
Time to Drain 99% of Inflow Volume (hours) =	40	71	64	71	75	76	76	76	76
Maximum Ponding Depth (ft) =	2.68	6.52	5.10	6.11	6.86	7.53	7.98	8.83	9.00
Area at Maximum Ponding Depth (acres) =	1.12	1.79	1.60	1.73	1.84	1.93	2.00	2.10	2.12
Maximum Volume Stored (acre-ft) =	2.044	7.753	5.346	7.012	8.352	9.616	10.521	12.244	12.624

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*Outflow Hydrograph Workbook Filename:* \_\_\_\_\_

### Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	1.42	0.14	4.55
	0:15:00	0.00	0.00	12.40	20.15	24.99	16.94	21.16	20.68	29.74
	0:20:00	0.00	0.00	44.53	58.49	68.80	43.38	50.43	54.13	70.18
	0:25:00	0.00	0.00	89.68	118.19	142.15	88.17	100.43	108.25	143.30
	0:30:00	0.00	0.00	102.59	134.03	157.30	178.74	213.47	241.76	325.40
	0:35:00	0.00	0.00	89.22	114.19	132.27	198.45	236.37	285.45	380.07
	0:40:00	0.00	0.00	74.27	93.02	107.54	177.46	210.89	255.75	340.06
	0:45:00	0.00	0.00	59.25	75.52	87.82	146.89	174.04	217.08	289.77
	0:50:00	0.00	0.00	48.13	63.16	72.40	122.21	143.87	178.76	239.41
	0:55:00	0.00	0.00	40.73	53.32	61.59	98.55	115.24	145.59	194.64
	1:00:00	0.00	0.00	34.52	44.75	52.44	80.64	93.73	122.43	163.72
	1:05:00	0.00	0.00	29.19	37.62	44.67	67.07	77.58	104.76	140.50
	1:10:00	0.00	0.00	23.33	32.41	39.08	52.96	60.79	79.39	105.49
	1:15:00	0.00	0.00	19.80	28.99	37.08	42.11	47.84	58.68	77.08
	1:20:00	0.00	0.00	18.04	26.33	34.36	34.73	39.30	43.95	57.30
	1:25:00	0.00	0.00	16.96	24.50	30.32	30.05	33.88	34.42	44.39
	1:30:00	0.00	0.00	16.37	23.32	27.27	25.95	29.21	28.67	36.59
	1:35:00	0.00	0.00	15.97	22.54	25.26	22.93	25.79	24.99	31.62
	1:40:00	0.00	0.00	15.67	20.25	23.87	21.10	23.74	22.56	28.34
	1:45:00	0.00	0.00	15.47	18.22	22.95	19.84	22.31	20.93	26.14
	1:50:00	0.00	0.00	15.38	16.89	22.29	19.02	21.39	19.99	24.89
	1:55:00	0.00	0.00	13.31	15.97	21.22	18.56	20.87	19.66	24.49
	2:00:00	0.00	0.00	11.40	14.89	19.17	18.26	20.54	19.51	24.30
	2:05:00	0.00	0.00	8.09	10.67	13.63	13.19	14.82	14.15	17.60
	2:10:00	0.00	0.00	5.29	6.96	8.98	8.71	9.78	9.37	11.64
	2:15:00	0.00	0.00	3.46	4.53	5.91	5.79	6.50	6.23	7.73
	2:20:00	0.00	0.00	2.17	2.84	3.75	3.70	4.14	3.96	4.91
	2:25:00	0.00	0.00	1.28	1.77	2.31	2.32	2.60	2.48	3.07
	2:30:00	0.00	0.00	0.69	1.04	1.31	1.38	1.54	1.47	1.81
	2:35:00	0.00	0.00	0.29	0.50	0.60	0.68	0.75	0.72	0.88
	2:40:00	0.00	0.00	0.10	0.16	0.18	0.22	0.24	0.23	0.28
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



**FlexTable: Conduit Table**

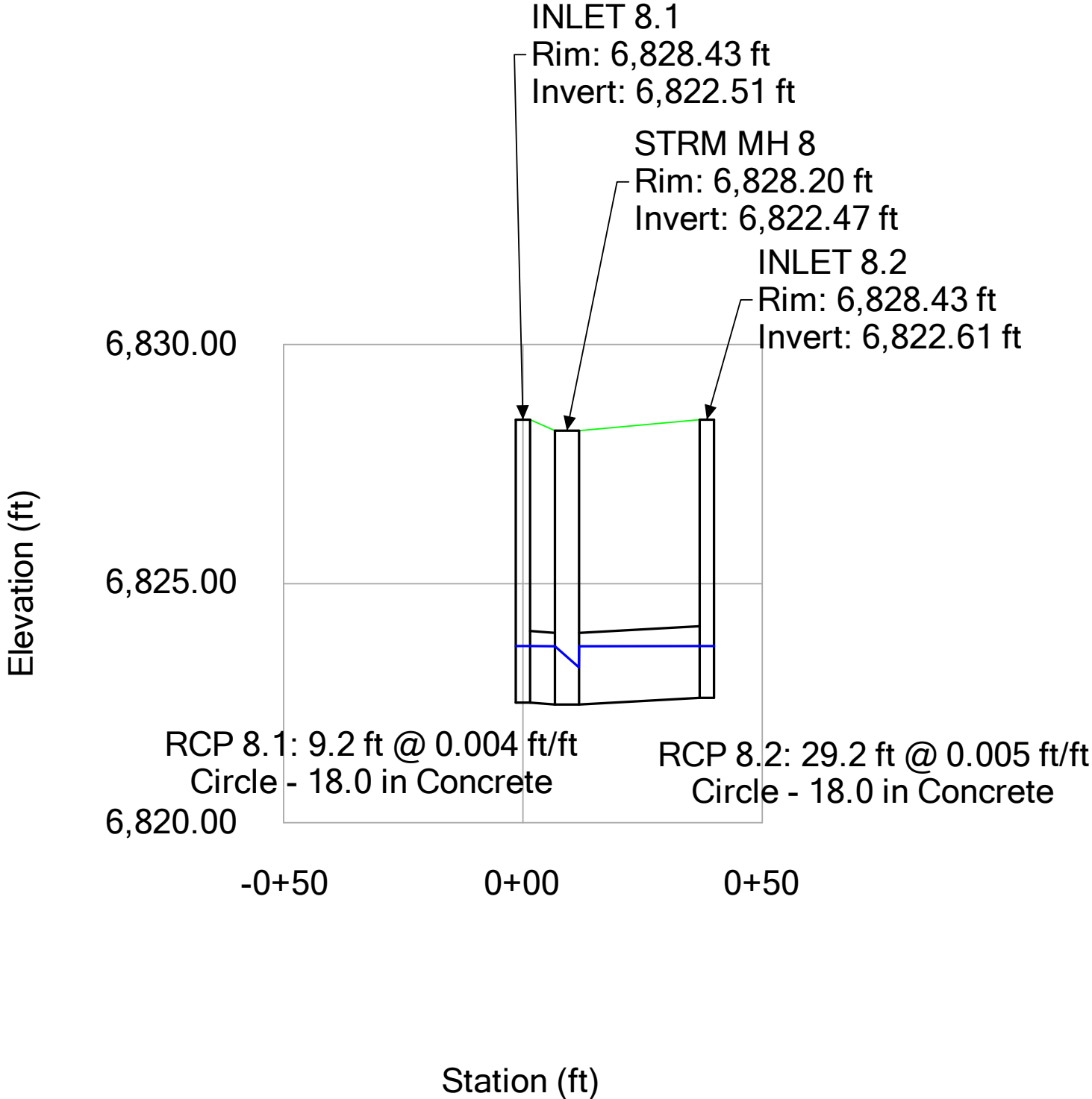
**Active Scenario: 5-year**

Label	Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Flow (cfs)	Length (3D) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Capacity (Design) (cfs)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Area (Flow) (ft <sup>2</sup> )
RCP 4	STRM MH 8	STRM MH 7	6,822.47	6,820.06	4.91	239.1	0.010	24.0	0.013	5.75	22.62	21.7	6,823.25	6,821.08	22.62	6,823.54	6,821.22	0.9
RCP 6	INLET 7.2	STRM MH 7	6,820.70	6,820.56	2.39	23.8	0.005	18.0	0.013	3.69	7.28	32.8	6,821.29	6,821.14	7.28	6,821.50	6,821.36	0.6
RCP 5	INLET 7.1	STRM MH 7	6,820.60	6,820.56	1.68	11.8	0.004	18.0	0.013	3.24	6.94	24.3	6,821.11	6,821.08	6.94	6,821.27	6,821.23	0.5
RCP 10	STRM MH 7	STRM MH 8	6,815.15	6,814.68	8.50	94.9	0.005	48.0	0.013	4.90	101.51	8.4	6,816.00	6,815.46	101.51	6,816.30	6,815.84	1.7
RCP 11	STRM MH 8	STRM MH 9	6,814.48	6,813.21	8.45	254.8	0.005	48.0	0.013	4.89	101.29	8.3	6,815.33	6,814.08	101.29	6,815.62	6,814.35	1.7
RCP 12	STRM MH 9	STRM MH 10	6,813.21	6,812.85	8.30	71.7	0.005	48.0	0.013	4.89	101.99	8.1	6,814.05	6,813.62	101.99	6,814.34	6,813.99	1.7
RCP 13	STRM MH 10	P2 OUTFALL 1	6,812.35	6,811.52	8.26	192.4	0.005	54.0	0.013	4.84	140.75	5.9	6,813.16	6,812.26	140.75	6,813.44	6,812.62	1.7
CO-9	MH-8	P1 OUTFALL 1	6,811.70	6,811.00	0.00	63.4	0.011	36.0	0.013	0.00	70.09	0.0	6,811.70	6,811.00	70.09	6,811.70	6,811.00	0.0
CO-10	MH-10	P1 OUTFALL 3	6,814.96	6,814.00	0.00	191.7	0.005	36.0	0.013	0.00	47.20	0.0	6,814.96	6,814.00	47.20	6,814.96	6,814.00	0.0
CO-11	CB-7	MH-8	6,813.50	6,811.70	0.00	155.3	0.012	36.0	0.013	0.00	71.81	0.0	6,813.50	6,811.70	71.81	6,813.50	6,811.70	0.0
CO-12	CB-8	MH-10	6,816.20	6,814.96	0.00	173.9	0.007	36.0	0.013	0.00	56.32	0.0	6,816.20	6,814.96	56.32	6,816.20	6,814.96	0.0
CO-13	MH-12	P2 OUTFALL 2	6,814.00	6,812.70	0.00	93.8	0.014	36.0	0.013	0.00	78.54	0.0	6,814.00	6,812.70	78.54	6,814.00	6,812.70	0.0
RCP 7	STRM MH 7	STRM MH 5	6,819.53	6,818.33	8.81	206.7	0.006	30.0	0.013	5.51	31.53	27.9	6,820.52	6,819.23	31.53	6,820.89	6,819.71	1.6
RCP 8.1	INLET 8.1	STRM MH 8	6,822.51	6,822.47	3.25	7.9	0.004	18.0	0.013	3.86	6.93	47.0	6,823.70	6,823.69	6.93	6,823.77	6,823.76	0.8
RCP 8.2	INLET 8.2	STRM MH 8	6,822.61	6,822.47	1.66	30.3	0.005	18.0	0.013	3.34	7.27	22.9	6,823.70	6,823.69	7.27	6,823.72	6,823.71	0.5
CO-16	STRM MH 5	STRM MH 7	6,817.84	6,816.15	8.69	297.0	0.006	36.0	0.013	5.33	50.32	17.3	6,818.77	6,816.99	50.32	6,819.11	6,817.44	1.6

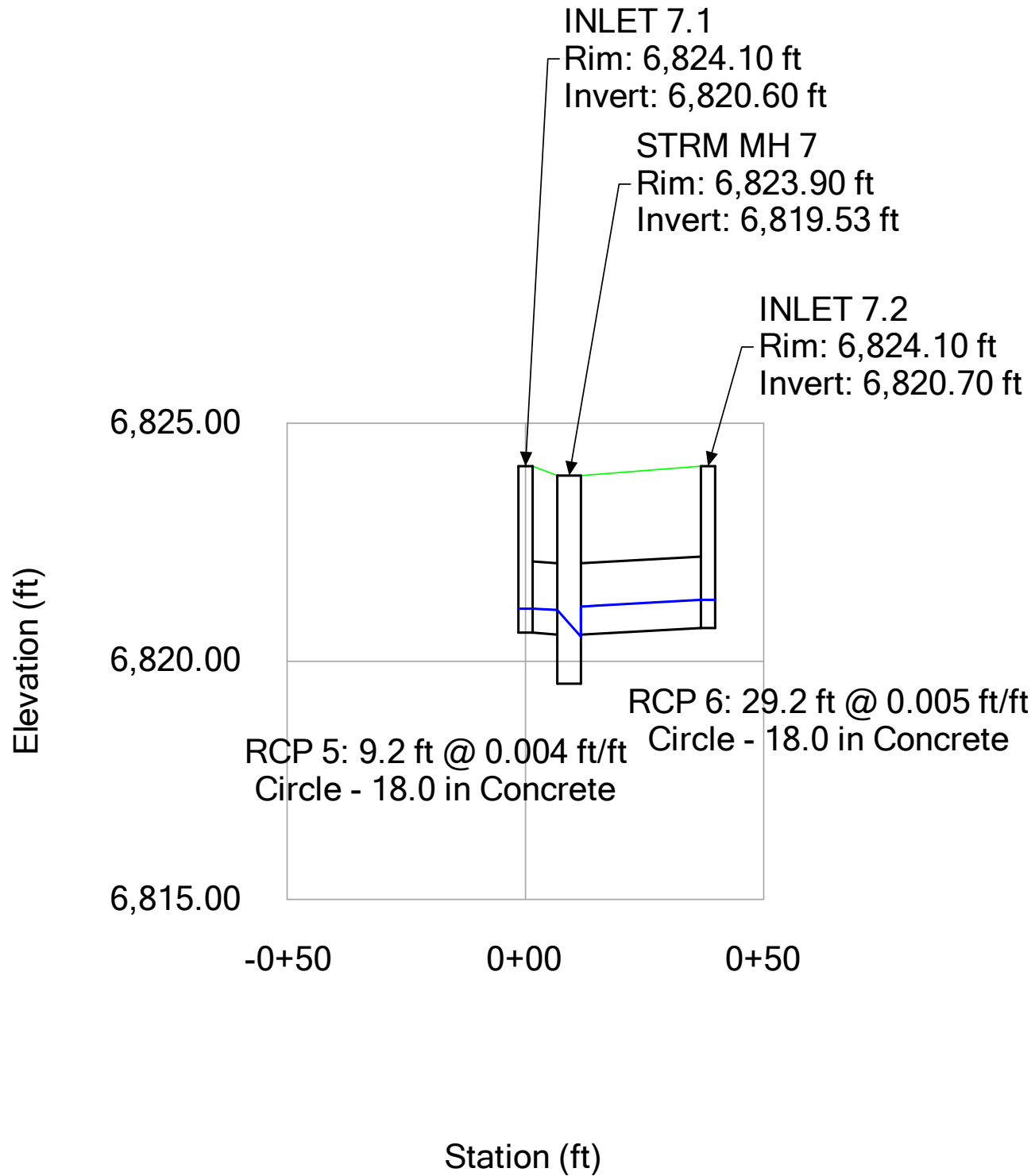


**Profile Report**  
**Engineering Profile - STORM RUN 1.1 (24004308-StormCAD-2024-12-11.stsw)**

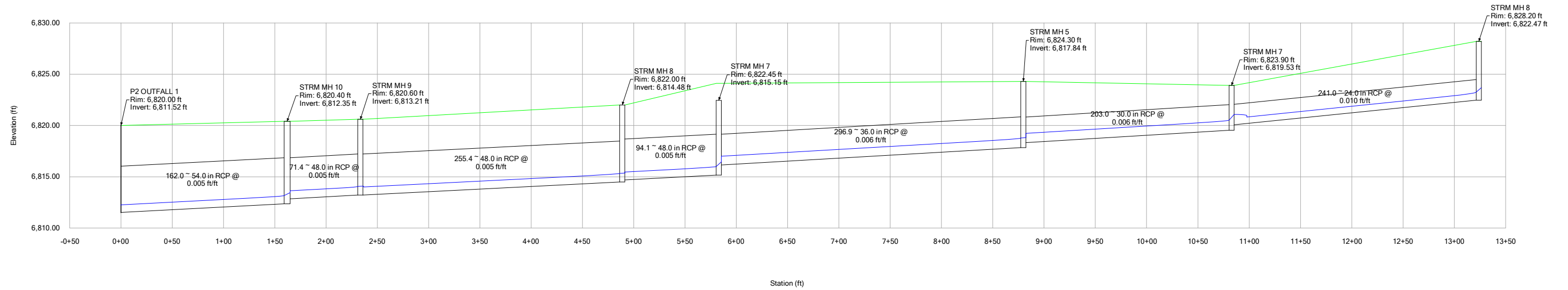
**Active Scenario: 5-year**



**Profile Report**  
**Engineering Profile - STORM RUN 1.2 (24004308-StormCAD-2024-12-11.stsw)**  
**Active Scenario: 5-year**



**Profile Report**  
**Engineering Profile - STORM RUN 1 (24004308-StormCAD-2024-12-11.stsw)**  
**Active Scenario: 5-year**

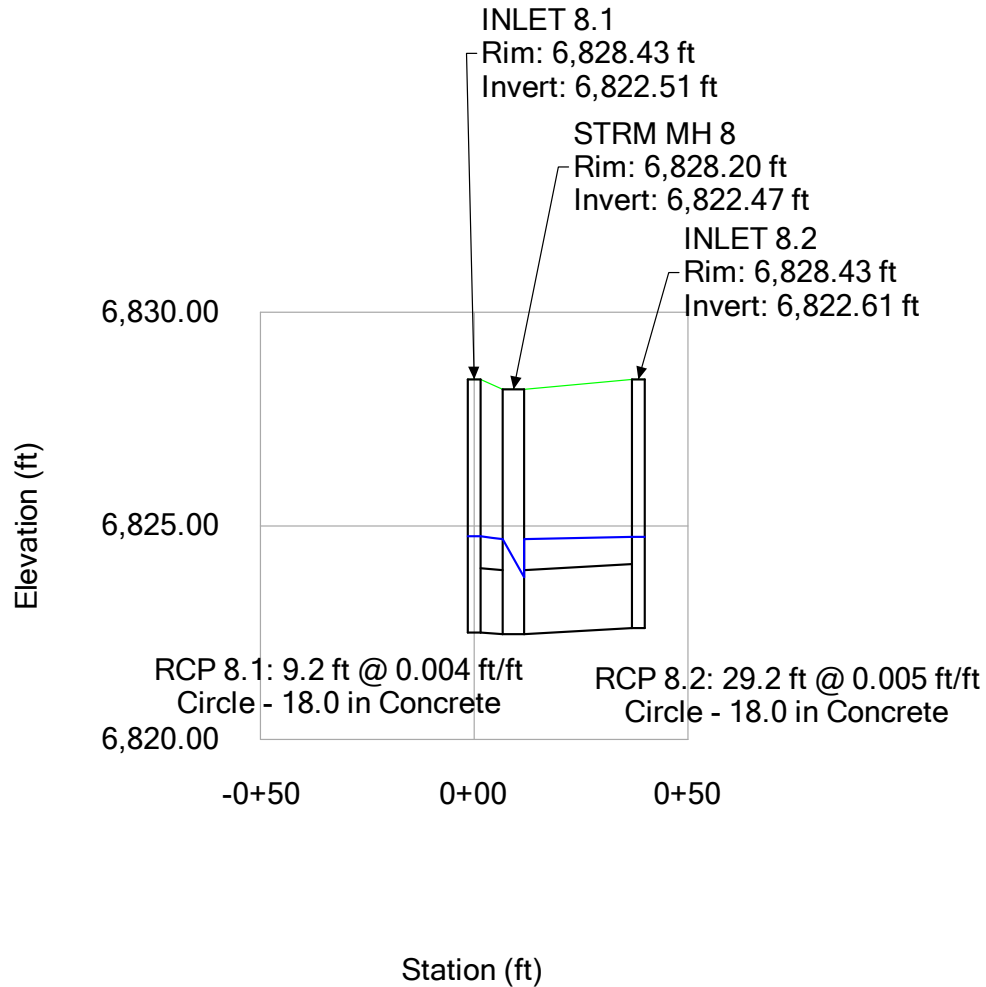


**FlexTable: Conduit Table**

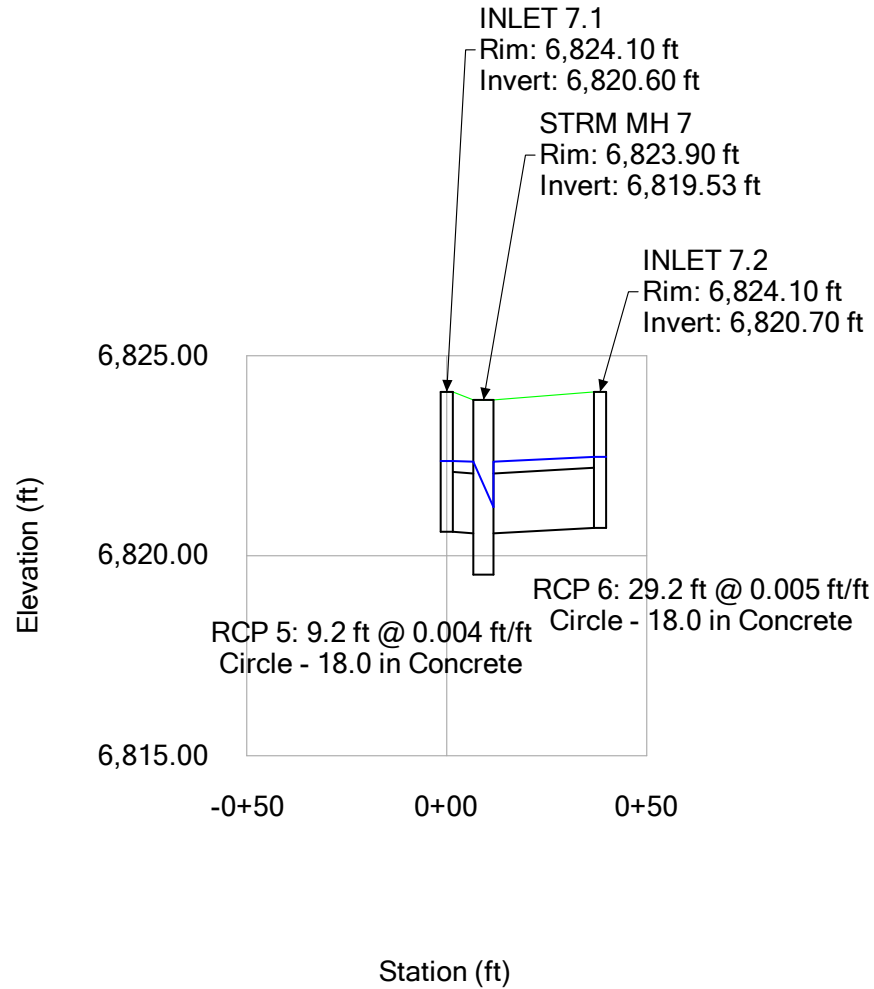
**Active Scenario: 100-year**

Label	Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Flow (cfs)	Length (3D) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Capacity (Design) (cfs)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Area (Flow) (ft <sup>2</sup> )
RCP 4	STRM MH 8	STRM MH 7	6,822.47	6,820.06	13.62	239.1	0.010	24.0	0.013	7.53	22.62	60.2	6,823.80	6,822.35	22.62	6,824.39	6,822.65	1.8
RCP 6	INLET 7.2	STRM MH 7	6,820.70	6,820.56	6.62	23.8	0.005	18.0	0.013	3.75	7.28	91.0	6,822.47	6,822.35	7.28	6,822.69	6,822.57	1.4
RCP 5	INLET 7.1	STRM MH 7	6,820.60	6,820.56	4.67	11.8	0.004	18.0	0.013	2.64	6.94	67.3	6,822.37	6,822.35	6.94	6,822.48	6,822.46	1.1
RCP 10	STRM MH 7	STRM MH 8	6,815.15	6,814.68	51.42	94.9	0.005	48.0	0.013	4.09	101.51	50.7	6,819.88	6,819.76	101.51	6,820.14	6,820.02	6.3
RCP 11	STRM MH 8	STRM MH 9	6,814.48	6,813.21	51.22	254.8	0.005	48.0	0.013	4.08	101.29	50.6	6,819.74	6,819.41	101.29	6,819.99	6,819.67	6.3
RCP 12	STRM MH 9	STRM MH 10	6,813.21	6,812.85	50.72	71.7	0.005	48.0	0.013	4.04	101.99	49.7	6,819.39	6,819.30	101.99	6,819.64	6,819.55	6.3
RCP 13	STRM MH 10	P2 OUTFALL 1	6,812.35	6,811.52	66.85	192.4	0.005	54.0	0.013	4.20	140.75	47.5	6,819.02	6,818.83	140.75	6,819.29	6,819.10	7.7
CO-9	MH-8	P1 OUTFALL 1	6,811.70	6,811.00	47.45	63.4	0.011	36.0	0.013	6.71	70.09	67.7	6,816.71	6,816.39	70.09	6,817.41	6,817.09	4.5
CO-10	MH-10	P1 OUTFALL 3	6,814.96	6,814.00	64.88	191.7	0.005	36.0	0.013	9.18	47.20	137.5	6,818.60	6,816.58	47.20	6,819.91	6,818.14	7.1
CO-11	CB-7	MH-8	6,813.50	6,811.70	47.45	155.3	0.012	36.0	0.013	6.71	71.81	66.1	6,817.50	6,816.71	71.81	6,818.20	6,817.41	4.4
CO-12	CB-8	MH-10	6,816.20	6,814.96	64.88	173.9	0.007	36.0	0.013	9.18	56.32	115.2	6,820.25	6,818.60	56.32	6,821.56	6,819.91	7.1
CO-13	MH-12	P2 OUTFALL 2	6,814.00	6,812.70	50.49	93.8	0.014	36.0	0.013	7.14	78.54	64.3	6,819.37	6,818.83	78.54	6,820.16	6,819.62	4.3
RCP 7	STRM MH 7	STRM MH 5	6,819.53	6,818.33	24.45	206.7	0.006	30.0	0.013	7.10	31.53	77.5	6,821.21	6,820.67	31.53	6,821.96	6,821.08	3.4
RCP 8.1	INLET 8.1	STRM MH 8	6,822.51	6,822.47	9.03	7.9	0.004	18.0	0.013	5.11	6.93	130.4	6,824.76	6,824.69	6.93	6,825.16	6,825.10	1.8
RCP 8.2	INLET 8.2	STRM MH 8	6,822.61	6,822.47	4.62	30.3	0.005	18.0	0.013	2.61	7.27	63.5	6,824.75	6,824.69	7.27	6,824.85	6,824.80	1.1
CO-16	STRM MH 5	STRM MH 7	6,817.84	6,816.15	24.18	297.0	0.006	36.0	0.013	7.05	50.32	48.1	6,820.66	6,820.28	50.32	6,820.85	6,820.46	3.4

**Profile Report**  
**Engineering Profile - STORM RUN 1.1 (24004308-StormCAD-2024-12-11.stsw)**  
**Active Scenario: 100-year**



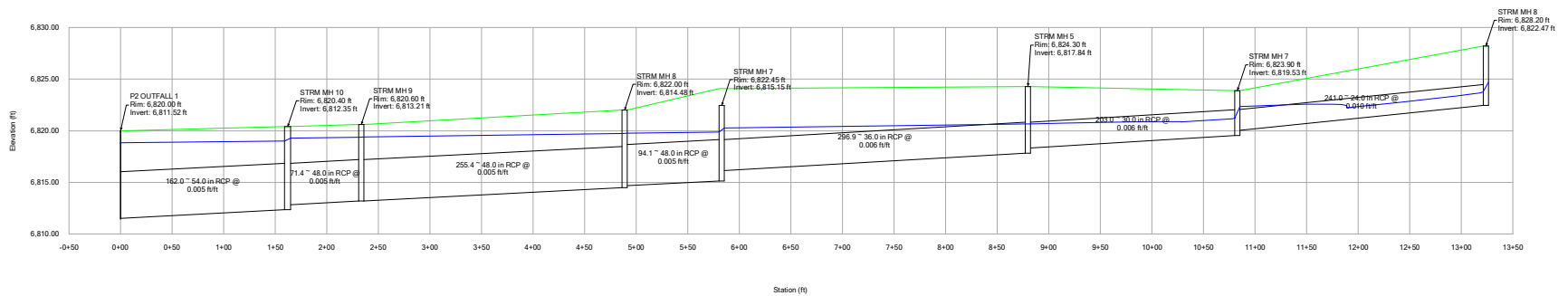
**Profile Report**  
**Engineering Profile - STORM RUN 1.2 (24004308-StormCAD-2024-12-11.stsw)**  
**Active Scenario: 100-year**



# Profile Report

## Engineering Profile - STORM RUN 1 (24004308-StormCAD-2024-12-11.stsw)

### Active Scenario: 100-year

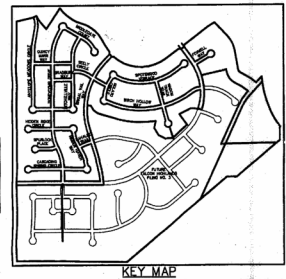
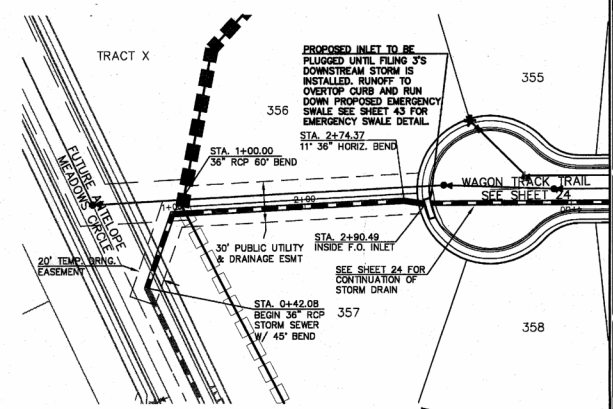
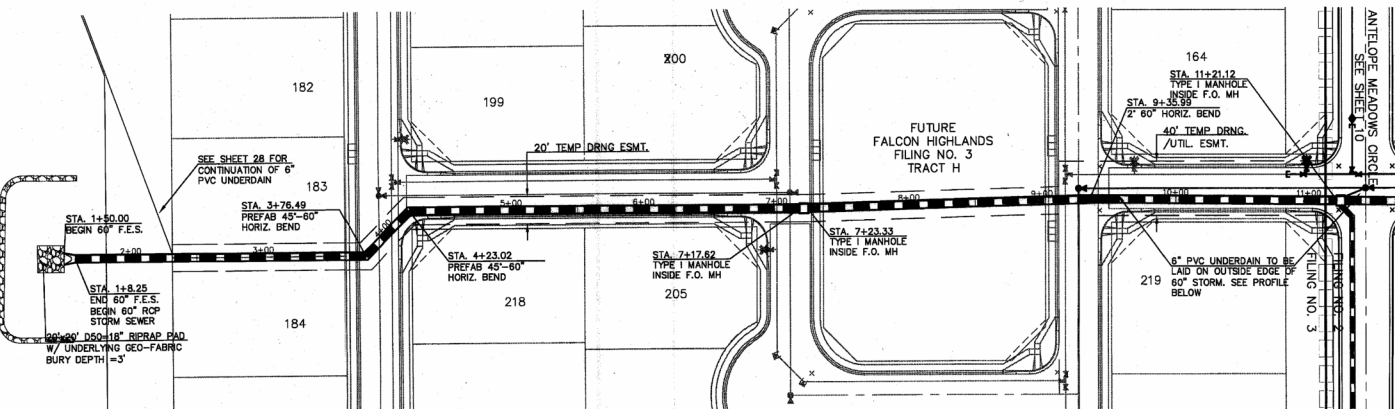


# Appendix F

Reference Material



Pages from Falcon Highlands Filing  
NO. 2 & 3 Final Drainage Report  
Revised November 2005  
SF-05-033



**60" RCP STORM SEWER**  
STA. 1+50.00 ~ STA. 11+21.12

**36" RCP STORM SEWER**  
STA. 1+00.00 ~ STA. 2+90.49 50'

NOTE: THESE PLANS FOR STORM SEWER PLAN AND PROFILE ONLY.

NOTE:  
SEE CONSTRUCTION DRAWINGS FOR FALCON HIGHLANDS FILING NO. 3 BY TERRA NOVA ENGINEERING FOR EXISTING SANITARY AND STORM SEWER INFORMATION

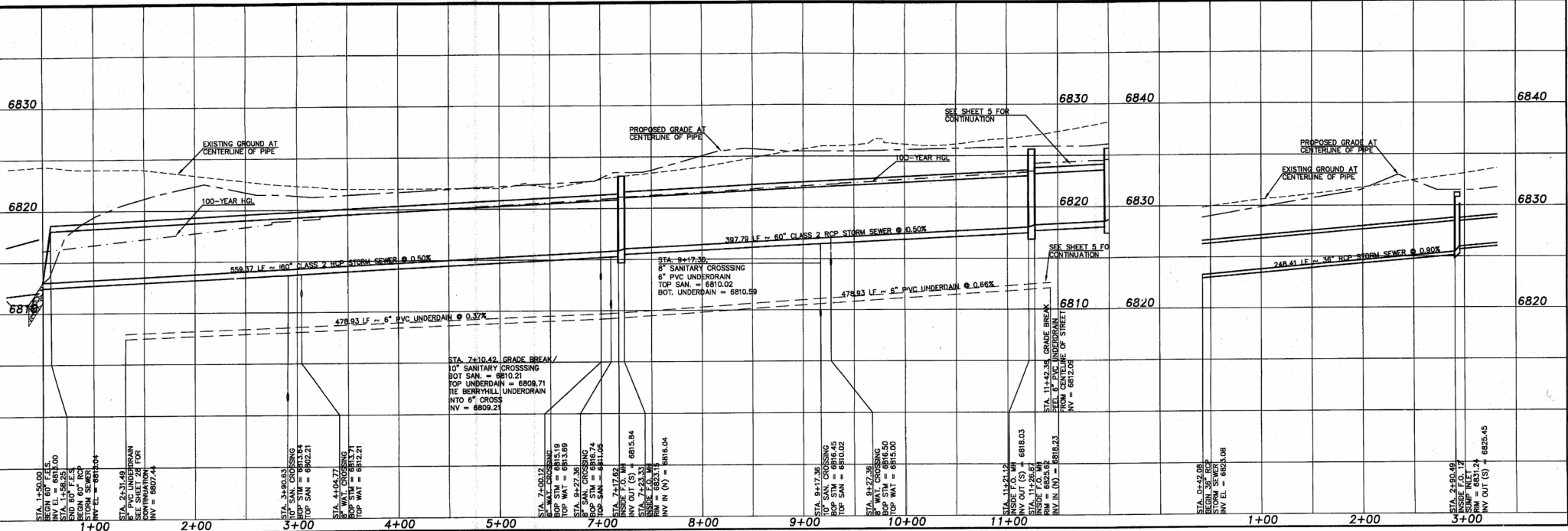
NOTE:  
SEE SHEET 35-39 FOR SANITARY, WATER, STORM AND CURB RETURN LINE TABLES

EL PASO COUNTY RECOGNIZES THE DESIGN ENGINEER AS HAVING RESPONSIBILITY FOR THE DESIGN. THE COUNTY HAS LIMITED ITS SCOPE OF REVIEW ACCORDINGLY.  
RESUBMITTAL REQUIRED IF CONSTRUCTION HAS NOT COMMENCED WITHIN 180 DAYS AFTER REVIEW DATE.

ASPHALT DATA FOR:	ALT. 2:
ASPHALT THICKNESS:	
AC SURFACE:	
AC BASE:	
AGGREGATE BASE THICKNESS:	ALT. 1:
CLASS 6:	ALT. 2:
CLASS 5:	
CLASS 4:	

THIS DESIGN WAS PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF TERRA NOVA ENGINEERING, INC.

QUENTIN N. ARMSTRONG, P.E. REGISTERED PROFESSIONAL ENGINEER  
COLORADO P.E. NO. 10000



DATE: 10/17/05  
DESCRIPTION: 1. PER COUNTY/HOUSE COMMENTS 2. PER WOODMAN DIST. COMMENTS  
NO. 10/21/05  
REVISIONS:  
DATE: 10/21/05  
DESCRIPTION: 1. PER COUNTY/HOUSE COMMENTS 2. PER WOODMAN DIST. COMMENTS  
NO. 10/21/05  
PREPARED FOR: TAMLIN VENTURES, LLC  
DRAWN BY: MR. MIKE SCOTT  
CHECKED BY: MR. MIKE SCOTT  
DATE ISSUED: 10/21/05  
SHEET NO. 2  
FALCON HIGHLANDS FILING NO. 2  
DESIGNED BY: [Signature]  
DRAWN BY: [Signature]  
CHECKED BY: [Signature]  
H-SCALE: [Blank]  
V-SCALE: [Blank]  
JOB NO. 04  
DATE ISSUED: 10/21/05  
SHEET NO. 2

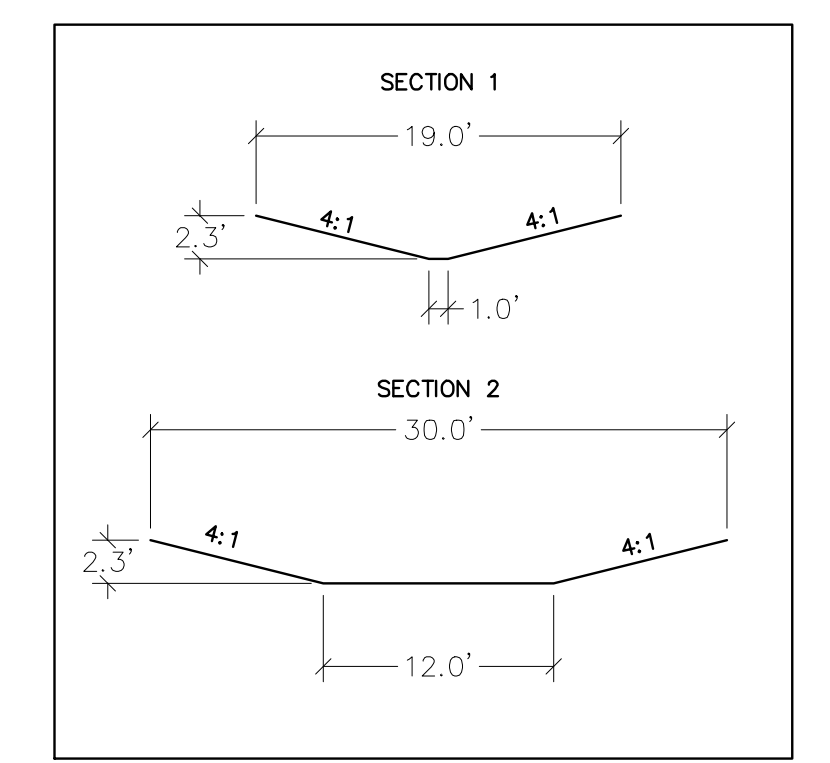
# 60" Storm Main

## HYDRAULIC GRADE LINE CALCULATIONS

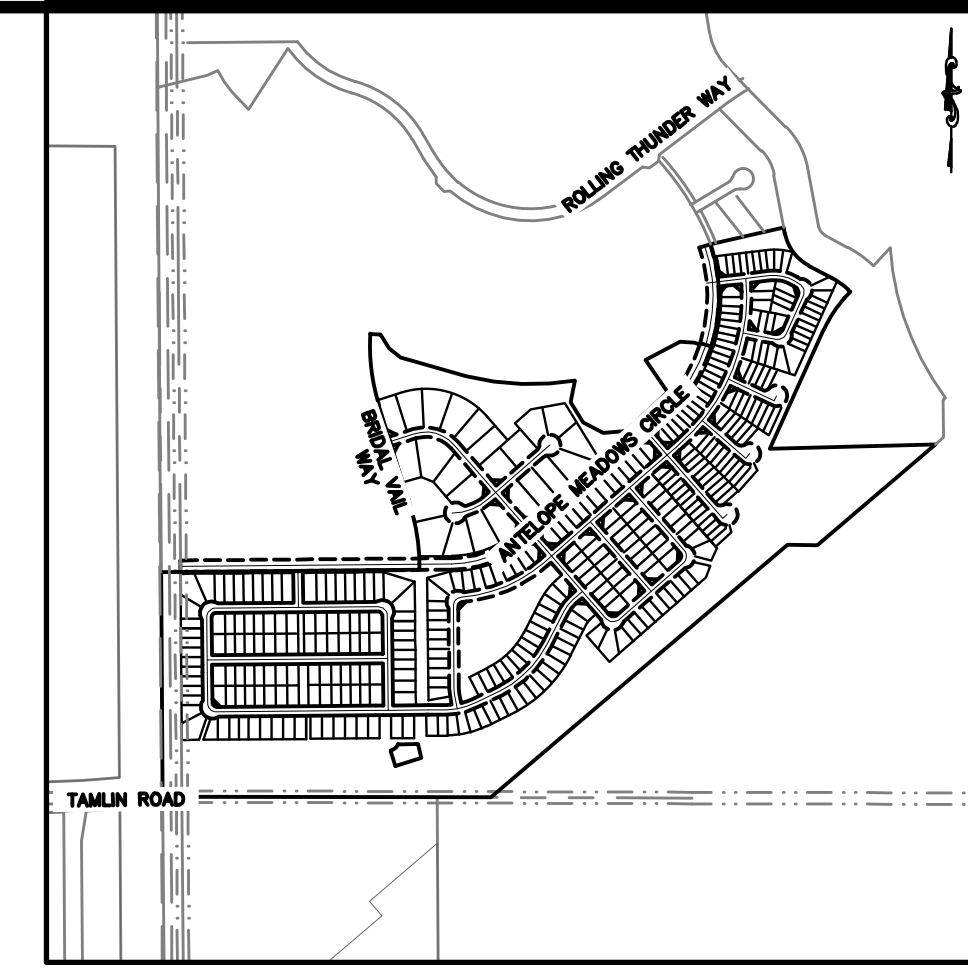
From Station	To Station	Loss Type	Start Inv. [ft]	Dia. [ft]			Flow [cfs]			Slope S <sub>1</sub> [%]	Horiz Bend [°]	Manning n Coeff.	Friction Slope [%]		H.G.L. Elev. [ft]	Head Loss [ft]	Velocity fps
				D <sub>1</sub>	D <sub>2</sub>	D <sub>3</sub>	Q <sub>1</sub>	Q <sub>2</sub>	Q <sub>3</sub>				S <sub>f-1</sub>	S <sub>f-3</sub>			
1+50.00	3+76.49	1	6813.04	5			196			0.50%		0.013	0.57%	--	6816.10	0.00	9.98
3+76.49	3+76.49	2	6814.17	5			196			0.50%	45	0.013	0.57%	--	6818.62	0.22	9.98
3+76.49	4+23.02	1	6814.17	5			196			0.50%		0.013	0.57%	--	6818.84	0.26	9.98
4+23.02	4+23.02	2	6814.40	5			196			0.50%	45	0.013	0.57%	--	6819.10	0.22	9.98
4+23.02	7+17.62	1	6814.40	5			196			0.50%		0.013	0.57%	--	6819.32	1.67	9.98
7+17.62	7+17.62	3	6815.84	5			196			0.50%		0.013	0.57%	--	6820.99	0.08	9.98
7+17.62	7+23.33	1	6815.84	5			196			0.50%		0.013	0.57%	--	6821.07	0.03	9.98
7+23.33	9+35.99	1	6816.04	5			196			0.50%		0.013	0.57%	--	6821.10	1.20	9.98
9+35.99	9+35.99	2	6817.10	5			196			0.50%	2	0.013	0.57%	--	6822.30	0.05	9.98
9+35.99	11+21.12	1	6817.10	5			196			0.50%		0.013	0.57%	--	6822.35	1.05	9.98
11+21.12	11+21.12	3	6818.03	5			196			0.50%		0.013	0.57%	--	6823.39	0.08	9.98
11+21.12	11+26.87	1	6818.03	5			196			0.50%		0.013	0.57%	--	6823.47	0.03	9.98
11+26.87	11+26.87	6	6818.23	5	3	3	166	196	30	0.50%	45	0.013	0.41%	0.57%	6823.50	0.73	8.45
11+26.87	11+95.80	1	6818.23	5			166			0.50%		0.013	0.41%	--	6824.24	0.28	8.45
11+95.80	11+95.80	3	6818.57	5			166			0.50%		0.013	0.41%	--	6824.52	0.06	8.45
11+95.80	12+01.55	1	6818.57	5			166			0.50%		0.013	0.41%	--	6824.57	0.02	8.45
12+01.55	12+01.55	6	6820.07	3.5	5	3	84	166	41	0.50%	45	0.013	0.70%	0.41%	6824.60	1.07	8.73
12+01.55	16+79.95	1	6820.07	3.5			84			1.00%		0.013	0.70%	--	6825.66	3.33	8.73
16+79.95	16+79.95	3	6824.87	3.5			84			1.00%		0.013	0.70%	--	6828.99	0.06	8.73
16+79.95	16+84.86	1	6824.87	3.5			84			1.00%		0.013	0.70%	--	6829.05	0.03	8.73
16+84.86	19+24.03	1	6825.07	3.5			84			0.90%		0.013	0.70%	--	6829.09	1.67	8.73
19+24.03	19+24.03	6	6827.23	3.5	3.5	1.5	63	84	11	0.90%	45	0.013	0.39%	0.70%	6830.75	0.88	6.55
19+24.03	19+28.53	1	6827.23	3.5			63			0.90%		0.013	0.39%	--	6831.63	0.02	6.55
19+28.53	22+22.51	1	6827.73	3.5			63			1.93%		0.013	0.39%	--	6831.65	1.15	6.55
22+22.51	22+22.51	6	6833.40	2.5	3.5	2.5	33	63	30	1.93%	45	0.013	0.65%	0.39%	6835.05	0.26	6.72
22+22.51	22+42.51	1	6833.40	2.5			33			1.93%		0.013	0.65%	--	6835.31	0.13	6.72
22+42.51	22+42.51	2	6833.79	2.5			33			1.93%	45	0.013	0.65%	--	6835.44	0.10	6.72
22+42.51	22+53.36	1	6833.79	2.5			33			1.93%		0.013	0.65%	--	6835.53	0.07	6.72
22+53.36			6781.90									0.013	--	--	6835.60	--	--

Pages from Falcon Highlands  
South Preliminary Drainage Report  
Dated March 2024  
PUDSP-22-005

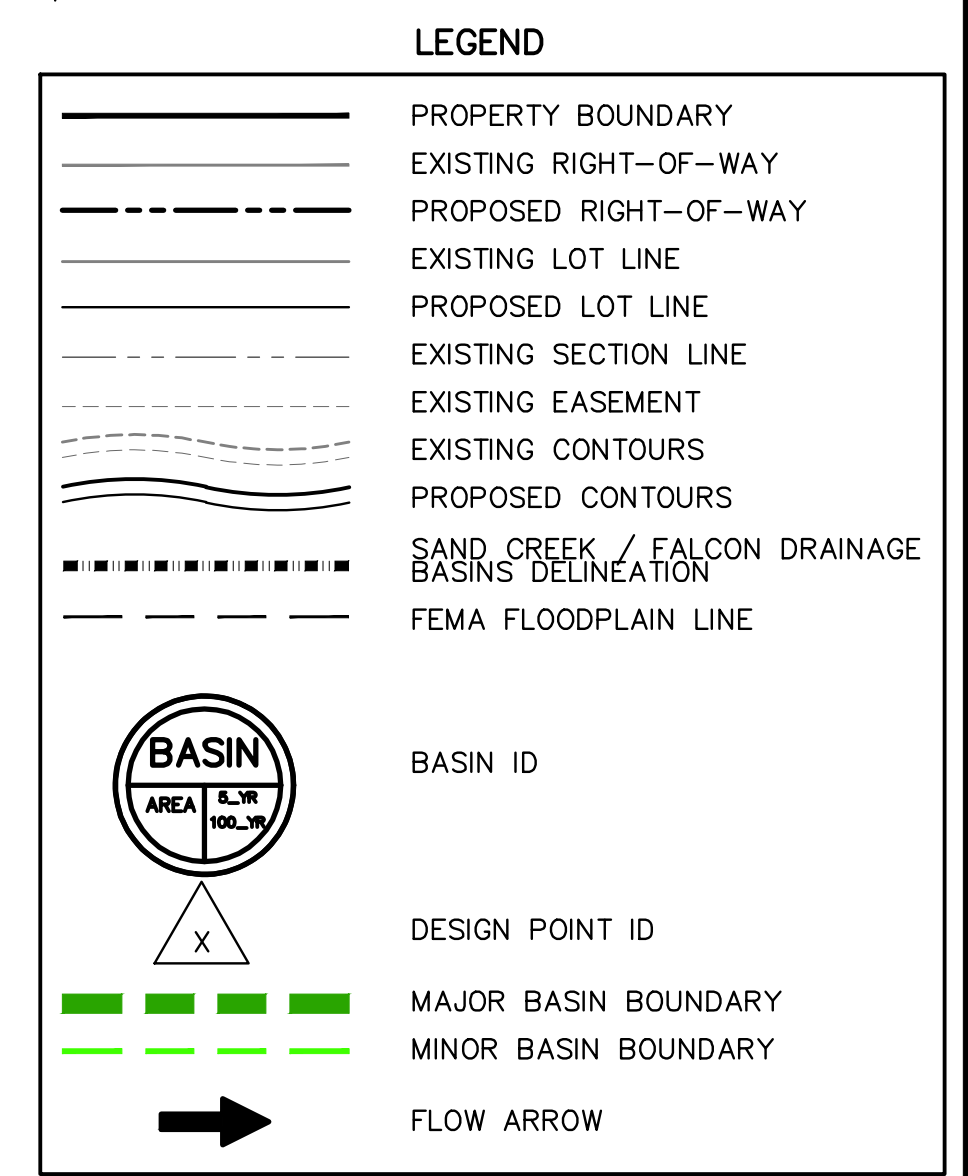
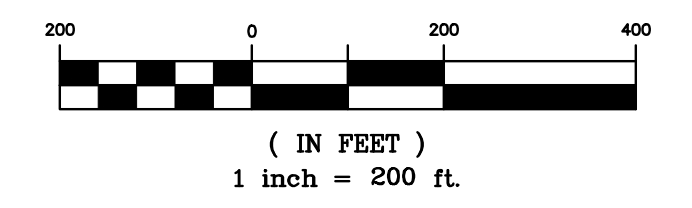
NOTE: SEE SHEETS DR-3 THRU DR-5 FOR SUB-BASINS B, C, & D



GRASS LINED SWALE SECTIONS  
N.T.S.



KEY MAP  
1" = 1000'



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COLORADO SPRINGS, CO 80920  
(719) 598-5192  
JIM BYERS

CHALLENGER HOMES  
FALCON HIGHLANDS FILING NO. 3  
EL PASO COUNTY, COLORADO  
DRAINAGE MAP  
MAJOR BASINS PROPOSED CONDITIONS

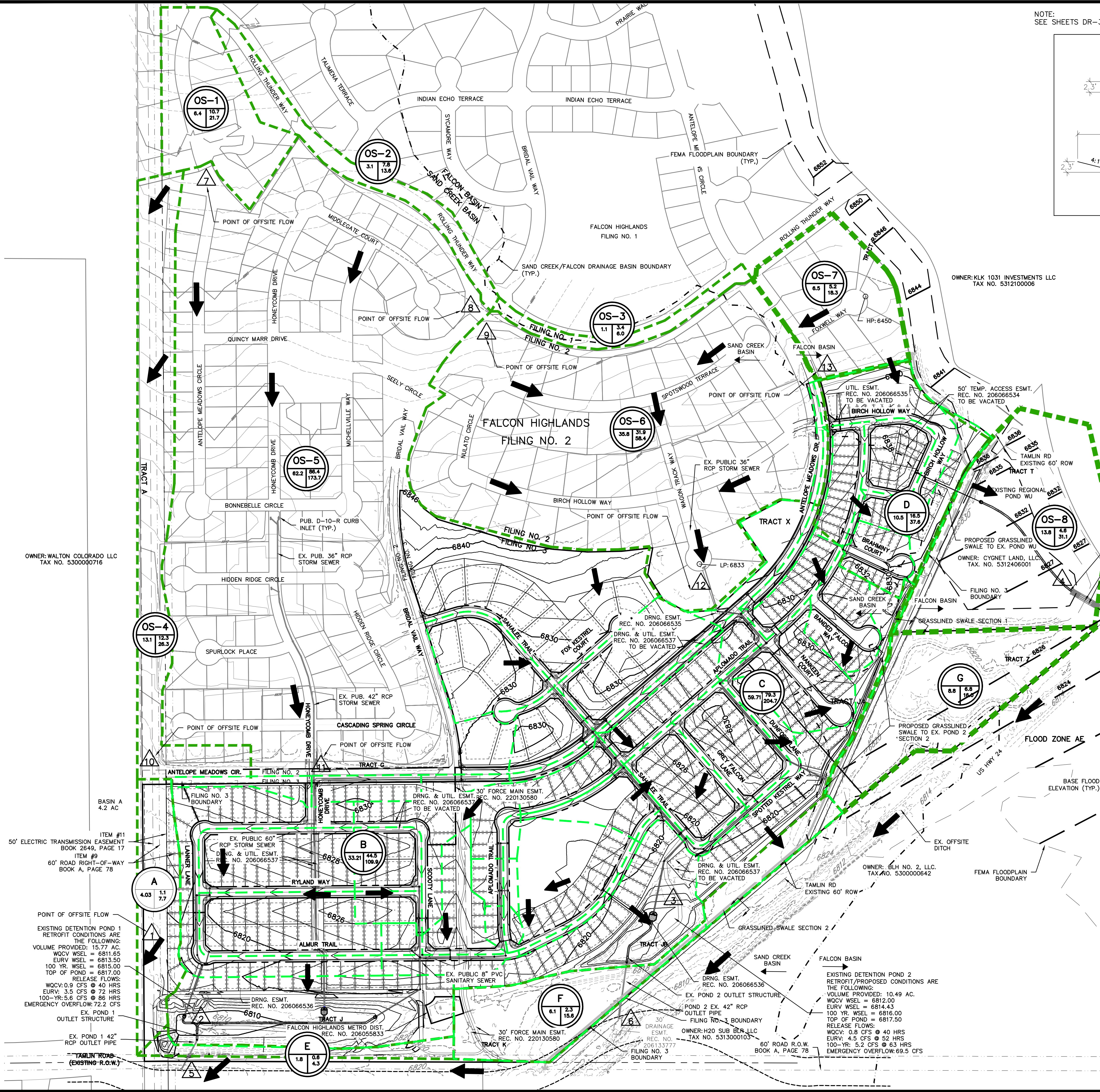
CLIENT: CHALLENGER HOMES  
DATE: 08/26/2022

REVISIONS	DATE	DESCRIPTION
A	07/31/2022	SUBMITTAL TO EPIC
B	08/26/2022	SUBMITTAL TO EPIC
C	08/26/2022	SUBMITTAL TO EPIC
D	07/21/2023	SUBMITTAL TO EPIC

DR: SLP CH: DJM  
P.M: DJM  
JOB: 21002568  
SHEET NO. 1  
DR-02

PROPOSED CONDITIONS CUMULATIVE DRAINAGE BASIN SUMMARY

Basin	Design Point	Area (acres)	WEIGHTED C <sub>5</sub>	WEIGHTED C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
A	1	4.03	0.08	0.33	1.1	7.7
B	2	33.21	0.36	0.54	45.4	112.3
C	3	62.88	0.34	0.53	87.0	222.9
D	4	7.36	0.42	0.57	11.5	26.7
E	5	1.77	0.09	0.36	0.6	4.3
F	6	6.06	0.10	0.41	2.3	15.6
G	6	8.84	0.09	0.36	6.8	16.0
OS-1	7	6.38	0.27	0.48	10.7	21.7
OS-2	8	3.12	0.30	0.50	7.8	13.6
OS-3	9	1.14	0.90	0.96	3.4	6.0
OS-4	10	13.09	0.34	0.44	12.3	26.3
OS-5	11	62.20	0.34	0.55	86.4	173.7
OS-6	12	35.75	0.22	0.46	31.9	58.4
OS-7	13	6.47	0.22	0.46	5.4	19.1
OS-8	4	13.79	0.09	0.36	4.8	32.5
<b>TOTAL</b>		<b>266.09</b>			<b>317.6</b>	<b>756.8</b>



OWNER: WALTON COLORADO LLC  
TAX NO. 530000716

ITEM #11  
50' ELECTRIC TRANSMISSION EASEMENT  
BOOK 2549, PAGE 17

ITEM #9  
60' ROAD RIGHT-OF-WAY  
BOOK A, PAGE 78

POINT OF OFFSITE FLOW

EXISTING DETENTION POND 1  
RETROFIT CONDITIONS ARE  
THE FOLLOWING:  
VOLUME PROVIDED: 15.77 AC.  
WQCV WSEL = 6811.65  
EURV WSEL = 6813.50  
100 YR. WSEL = 6815.00  
TOP OF POND = 6817.00  
RELEASE FLOWS:  
WQCV: 0.9 CFS @ 40 HRS  
EURV: 3.5 CFS @ 72 HRS  
100-YR: 5.6 CFS @ 85 HRS  
EMERGENCY OVERFLOW: 72.2 CFS

EX. POND 1  
OUTLET STRUCTURE

EX. POND 1 42"  
RCP OUTLET PIPE

TAMLIN ROAD  
(EXISTING R.O.W.)

EXISTING DETENTION POND 2  
RETROFIT/PROPOSED CONDITIONS ARE  
THE FOLLOWING:  
VOLUME PROVIDED: 10.49 AC.  
WQCV WSEL = 6812.00  
EURV WSEL = 6814.43  
100 YR. WSEL = 6816.00  
TOP OF POND = 6817.50  
RELEASE FLOWS:  
WQCV: 0.8 CFS @ 40 HRS  
EURV: 4.5 CFS @ 52 HRS  
100-YR: 5.2 CFS @ 63 HRS  
EMERGENCY OVERFLOW: 69.5 CFS

OWNER: H2O SUB BLR LLC  
TAX NO. 5313000103

OWNER: ELH NO. 2, LLC  
TAX NO. 530000642

OWNER: H2O SUB BLR LLC  
TAX NO. 5313000103

OWNER: H2O SUB BLR LLC  
TAX NO. 5313000103

OWNER: H2O SUB BLR LLC  
TAX NO. 5313000103

## On-site Basins (Falcon Highlands South, Undeveloped):

The site has been broken down into seven major on-site basins upstream within the limits of Falcon Highlands South. A drainage map is in the appendix.

**Basin A (3.74 ac,  $Q_5 = 1.15$  cfs,  $Q_{100} = 7.7$  cfs)** is the basin located southwest of Antelope Meadow Circle, just below basin OS-4, west of Basin B. The majority of the basin is comprised of Tract F and consists of some rear yard runoff from the PUD lots at the western edge of Basin B. The storm water runoff from this basin sheet flows south and off-site at **Design Point 1** with the combined flow of OS-4, and per existing drainage patterns is not tributary to on-site detention ponds.

**Basin B (38.93 ac,  $Q_5 = 11.65$  cfs,  $Q_{100} = 78.20$  cfs)** is located south of Antelope Meadow Circle, adjacent to basin A. The site is covered in native grasses with limited grading work from a previous development. Runoff from the site sheet flows southwesterly overland to existing Pond 1 (**Design Point 2**). The private 42" RCP outlet pipe from the outlet structure of the pond daylights at the grassland swale south of the abandoned future Tamlin Road right-of-way at **Design Point 5**.

**Basin C (57.81 ac,  $Q_5 = 18.4$  cfs,  $Q_{100} = 123.57$  cfs)** is located adjacent to Basin B and covered in native grasses and weeds. The site has limited grading due to work from a previous development that did not finish. Runoff from the site sheet flows southwesterly overland to an existing diversion ditch that spans from an existing public 24" RCP storm sewer main that daylights within Falcon Highlands South south of Wagon Track Way. The diversion ditch flows directly to existing Pond 2 (**Design Point 3**). The private 42" RCP outlet pipe from the outlet structure of the pond daylights at the grassland swale south of the project site at **Design Point 6**.

**Basin D (10.54 ac,  $Q_5 = 3.47$  cfs,  $Q_{100} = 23.31$  cfs)** is located to the northeast of the Filing and consists of undeveloped area with native grasses. The basin's runoff drains directly to existing Pond WU (**Design Point 4**).

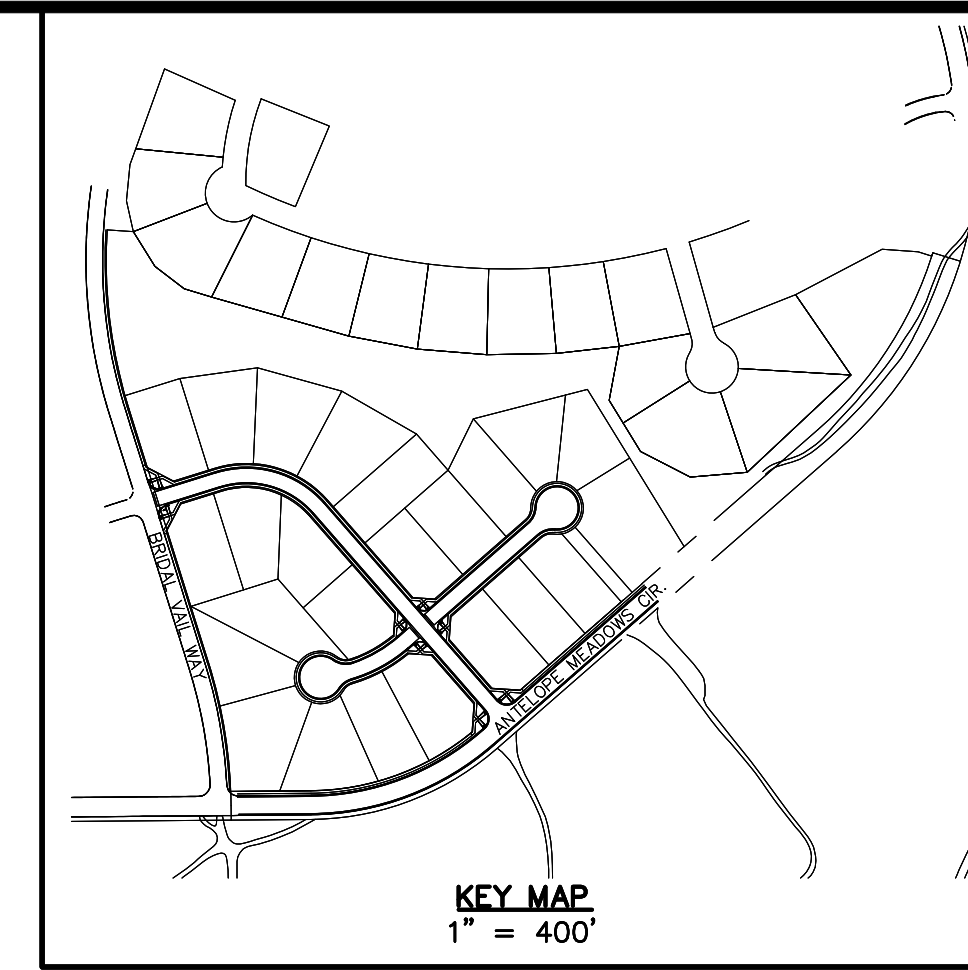
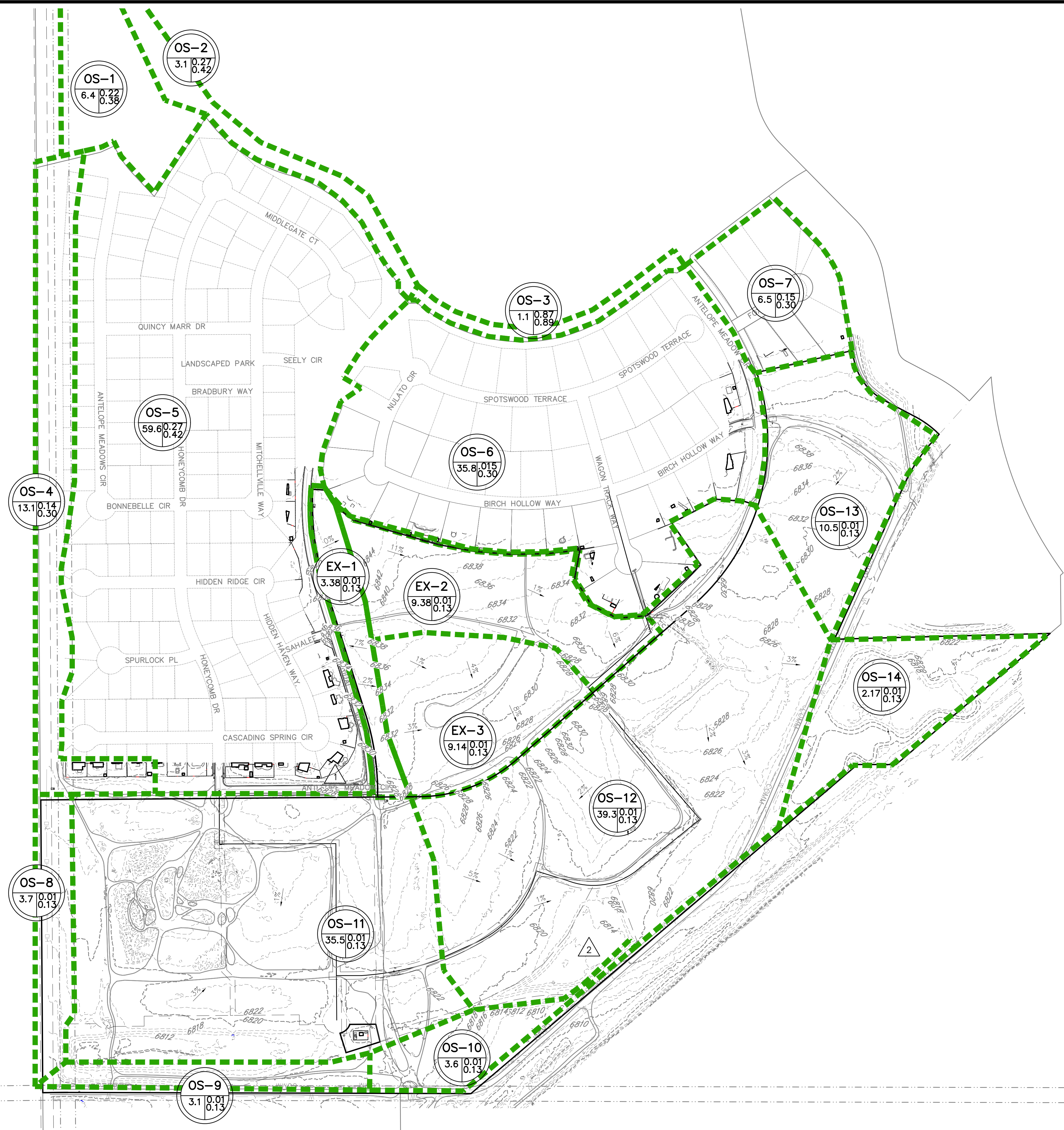
**Basin E (3.14 ac,  $Q_5 = 1.12$  cfs,  $Q_{100} = 7.5$  cfs)** is the undeveloped, natural landscaped area between Tamlin Road and the existing Pond 1. Runoff from Basin E is directed by a ditch section to a low point between the future Dublin Road and Highway 24 (**Design Point 5**). This drainage concept and its associated storm infrastructure is presented in the previous master plan and is to remain as the intended plan. The 2005 PDR suggested that an inline grate inlet be installed but there is no evidence that this was installed. The existing drainage pattern consists of pooling within the local low point of the ditch that surcharges and is directed south through the grassland swale.

**Basin F (3.67 ac,  $Q_5 = 1.19$  cfs,  $Q_{100} = 7.99$  cfs)** is the undeveloped area between Tamlin Road and the existing Detention Pond 2. The runoff from Basin F is directed to the low point in the downstream grasslined swale between the Site and Tamlin Road (**Design Point 6**). This drainage concept and its associated storm infrastructure is presented in the previous master plan and is to remain as the intended plan. The 2005 PDR suggested that a 4'x4' area inlet be constructed but

Only a portion of the described drainage patterns remain unchanged during this planning.

# Appendix G

## Drainage Maps



**EXISTING CONDITIONS DRAINAGE BASIN SUMMARY**

Basin	Design Point	Area (acres)	C <sub>s</sub>	C <sub>100</sub>	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
EX-1	1	3.38	0.01	0.13	0.04	1.32
EX-2	2	9.38	0.01	0.13	0.11	4.05
EX-3	2	9.14	0.01	0.13	0.13	4.64
OS-1	2	2.17	0.01	0.13	0.03	0.93
OS-2	2	1.28	0.01	0.13	0.02	0.66
<b>Total</b>		<b>25.35</b>			<b>0.33</b>	<b>11.6</b>

**Existing Conditions Design Point Summary**

Design Point	Contributing Basins	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
1	EX-1	0.04	1.32
2	EX-2, EX-3, OS-1, OS-2	0.29	10.28

**LEGEND**

- PROPERTY BOUNDARY
- EXISTING RIGHT-OF-WAY
- PROPOSED RIGHT-OF-WAY
- EXISTING LOT LINE
- PROPOSED LOT LINE
- EXISTING SECTION LINE
- EXISTING EASEMENT
- EXISTING CONTOURS
- PROPOSED CONTOURS

**BASIN SIZE IN ACRES**

**DESIGN POINT ID**

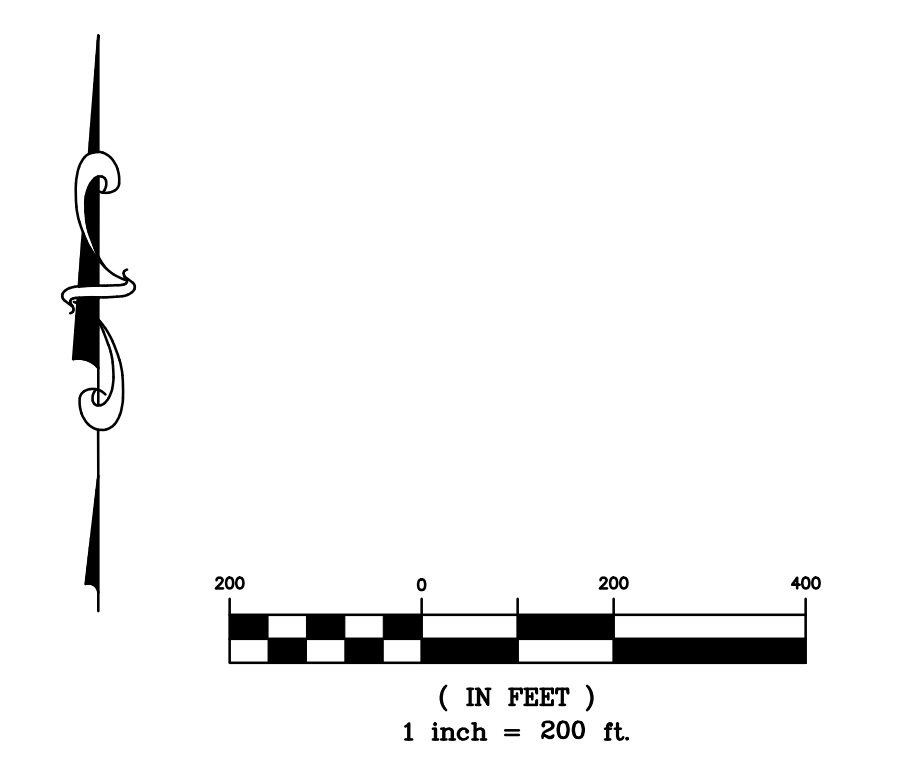
**MAJOR BASIN BOUNDARY**

**FLOW ARROW**

**BASIN ID**

**5-YR RATIONAL C COEFFICIENT**

**5-YR RATIONAL C COEFFICIENT**



**BENCHMARK:**  
ELEVATIONS ARE BASED UPON SW COR SEC. 12, T13S, R65W, 6TH PM, FND. 3.25" ALUM. CAP. (ELEVATION: 6810.43=NAVD88).

**BASIS OF BEARINGS:**  
BEARINGS ARE BASED UPON THE WEST LINE OF THE SOUTHWEST QUARTER OF SECTION 12, TOWNSHIP 13 SOUTH, RANGE 65 WEST OF THE SIXTH PRINCIPAL MERIDIAN, MONUMENTED AT THE SOUTH END BY A FOUND-3-1/4" ALUMINUM CAP STAMPED "AZTEC CONSULTANTS PLS 38256" AND AT THE NORTH END BY A FOUND 3-1/4" ALUMINUM CAP STAMPED "PLS 4842".

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719-598-5192  
JIM BYERS

**CHALLENGER HOMES**  
FALCON HIGHLANDS SOUTH - FILING 1  
EL PASO COUNTY, COLORADO  
DRAINAGE MAPS  
EXISTING DRAINAGE MAP

CLIENT: CHALLENGER HOMES

DATE: 07/08/2024

REVISIONS:

NO.	DESCRIPTION

COUNTY FILE NO.:

DR: TN CH: KB  
P.M. DM

JOB: 24004308  
SHEET NO.:

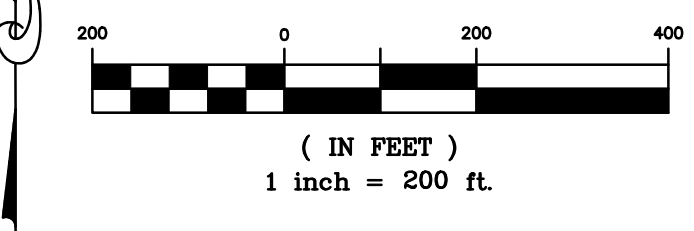
CAD FILE: 24004308-EX-DRAINAGE MAPS.DWG





### Proposed Basin Summary

Basin	Area (acres)	C <sub>5</sub>	C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
A	20.60	0.23	0.38	9.99	29.77
B	40.12	0.23	0.38	18.65	53.18
C	41.08	0.23	0.38	25.69	73.24
D	8.26	0.50	0.62	12.79	26.67
E	1.41	0.02	0.15	0.08	1.03
F	5.91	0.02	0.15	0.26	3.48
G	8.38	0.02	0.15	0.37	4.93
OS-1	6.38	0.22	0.38	5.43	15.66
OS-2	3.12	0.27	0.42	2.29	6.06
OS-3	1.14	0.86	0.89	4.06	7.04
OS-4	13.09	0.14	0.30	4.44	15.98
OS-5	59.62	0.27	0.42	47.03	124.58
OS-6	35.75	0.15	0.30	14.22	49.60
OS-7	6.47	0.15	0.30	2.41	8.39



#### LEGEND

	PROPERTY BOUNDARY
	EXISTING RIGHT-OF-WAY
	PROPOSED RIGHT-OF-WAY
	EXISTING LOT LINE
	PROPOSED LOT LINE
	EXISTING SECTION LINE
	EXISTING EASEMENT
	EXISTING CONTOURS
	PROPOSED CONTOURS

	BASIN ID
	5-YR RATIONAL C COEFFICIENT
	5-YR RATIONAL C COEFFICIENT

	DESIGN POINT ID
	MAJOR BASIN BOUNDARY
	FLOW ARROW

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<b>CHALLENGER HOMES</b>	719-598-5192 JIM BYERS
<b>CHALLENGER HOMES</b>	FALCON HIGHLANDS SOUTH - FILING 1 EL PASO COUNTY, COLORADO DRAINAGE MAPS OVERALL MAP
CLIENT	
DATE	
REVISIONS	
COUNTY FILE NO.:	
DR. TN	CH. KB
P.M. DM	
JOB	24004308
SHEET NO.	02

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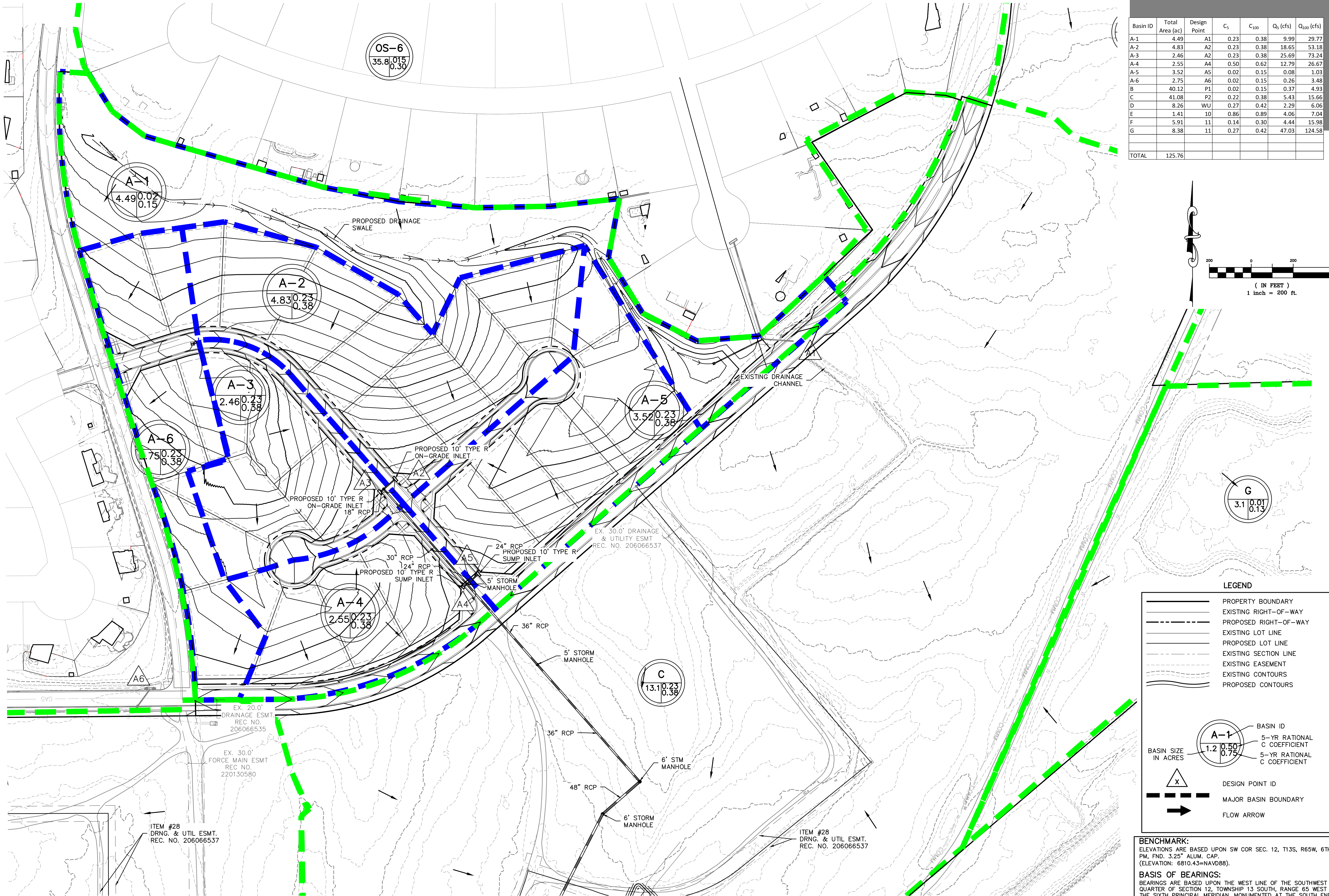
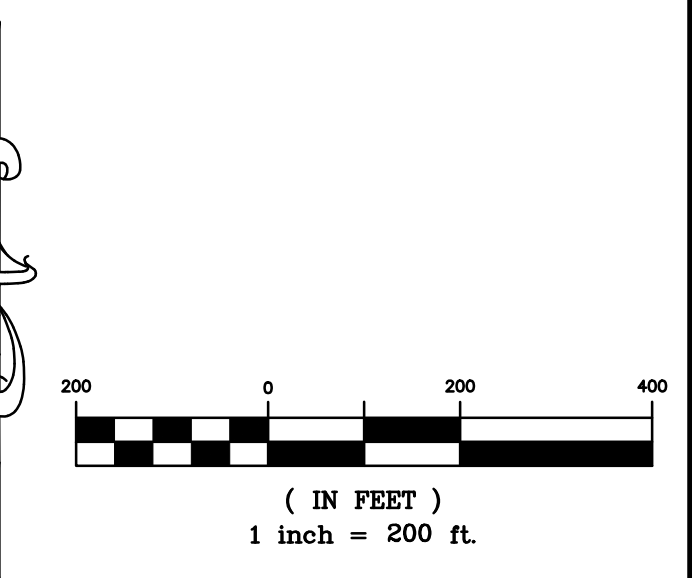
CHALLENGER HOMES  
FALCON HIGHLANDS SOUTH - FILING 1  
EL PASO COUNTY, COLORADO  
DRAINAGE MAPS  
PROPOSED MAP

CLIENT: CHALLENGER HOMES  
DATE: 07/28/2024

REVISIONS

COUNTY FILE NO.:  
DR. TN CH. KB  
P.M. DM  
JOB 24004308  
SHEET NO. 03

Basin ID	Total Area (ac)	Design Point	C <sub>s</sub>	C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
A-1	4.49	A1	0.23	0.38	9.99	29.77
A-2	4.83	A2	0.23	0.38	18.65	53.18
A-3	2.46	A2	0.23	0.38	25.69	73.24
A-4	2.55	A4	0.50	0.62	12.79	26.67
A-5	3.52	A5	0.02	0.15	0.08	1.03
A-6	2.75	A6	0.02	0.15	0.26	3.48
B	40.12	P1	0.02	0.15	0.37	4.93
C	41.08	P2	0.22	0.38	5.43	15.66
D	8.26	WU	0.27	0.42	2.29	6.06
E	1.41	10	0.86	0.89	4.06	7.04
F	5.91	11	0.14	0.30	4.44	15.98
G	8.38	11	0.27	0.42	47.03	124.58
TOTAL	125.76					



**LEGEND**

- PROPERTY BOUNDARY
- EXISTING RIGHT-OF-WAY
- PROPOSED RIGHT-OF-WAY
- EXISTING LOT LINE
- PROPOSED LOT LINE
- EXISTING SECTION LINE
- EXISTING EASEMENT
- EXISTING CONTOURS
- PROPOSED CONTOURS

**BENCHMARK:**  
ELEVATIONS ARE BASED UPON SW COR SEC. 12, T13S, R65W, 6TH PM, FND. 3.25" ALUM. CAP. (ELEVATION: 6810.43=NAVD88).

**BASIS OF BEARINGS:**  
BEARINGS ARE BASED UPON THE WEST LINE OF THE SOUTHWEST QUARTER OF SECTION 12, TOWNSHIP 13 SOUTH, RANGE 65 WEST OF THE SIXTH PRINCIPAL MERIDIAN, MONUMENTED AT THE SOUTH END BY A FOUND-3-1/4" ALUMINUM CAP STAMPED "AZTEC CONSULTANTS PLS 38256" AND AT THE NORTH END BY A FOUND 3-1/4" ALUMINUM CAP STAMPED "PLS 4842".

**Basin Size Legend:**  
 A-1: BASIN ID, 5-YR RATIONAL C COEFFICIENT (1.2, 0.50, 0.75)  
 X: DESIGN POINT ID  
 ---: MAJOR BASIN BOUNDARY  
 →: FLOW ARROW

ITEM #28  
DRNG. & UTIL ESMT.  
REC. NO. 206066537

ITEM #28  
DRNG. & UTIL ESMT.  
REC. NO. 206066537

EX. 20.0' DRAINAGE ESMT.  
REC. NO. 206066535

EX. 30.0' FORCE MAIN ESMT.  
REC. NO. 220130580

EX. 30.0' DRAINAGE & UTILITY ESMT.  
REC. NO. 206066537



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Basin ID	Total Area (ac)	Design Point	C <sub>s</sub>	C <sub>100</sub>	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
A-1	4.49	A1	0.23	0.38	9.99	29.77
A-2	4.83	A2	0.23	0.38	18.65	53.18
A-3	2.46	A2	0.23	0.38	25.69	73.24
A-4	2.55	A4	0.50	0.62	12.79	26.67
A-5	3.52	A5	0.02	0.15	0.08	1.03
A-6	2.75	A6	0.02	0.15	0.26	3.48
B	40.12	P1	0.02	0.15	0.37	4.93
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D	8.26	WU	0.27	0.42	2.29	6.06
E	1.41	10	0.86	0.89	4.06	7.04
F	5.91	11	0.14	0.30	4.44	15.98
G	8.38	11	0.27	0.42	47.03	124.58
TOTAL	125.76					

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 8605 EXPLORER DRIVE  
 SUITE 250  
 COLORADO SPRINGS, CO 80920  
 719-598-5192  
 JIM BYERS

**CHALLENGER HOMES**  
 FALCON HIGHLANDS SOUTH - FILING 1  
 EL PASO COUNTY, COLORADO  
 DRAINAGE MAPS  
 PROPOSED MAP

CLIENT: CHALLENGER HOMES  
 DATE: 07/08/2024

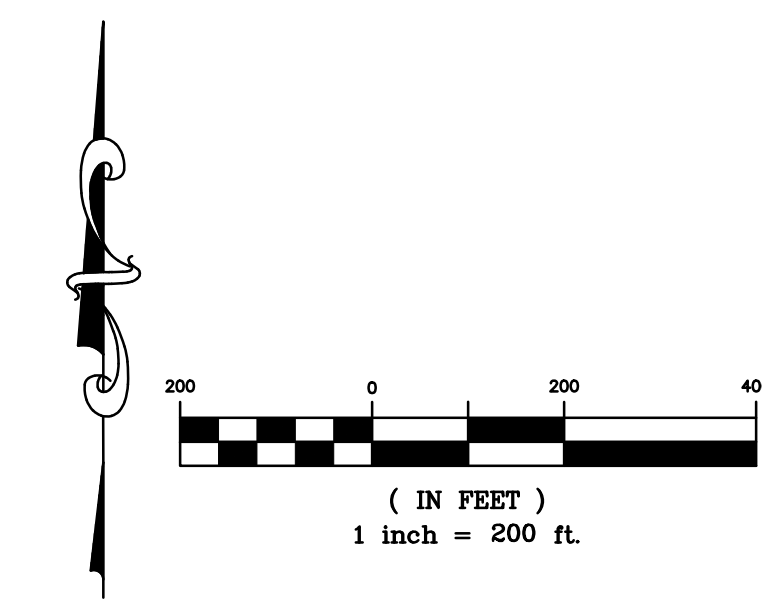
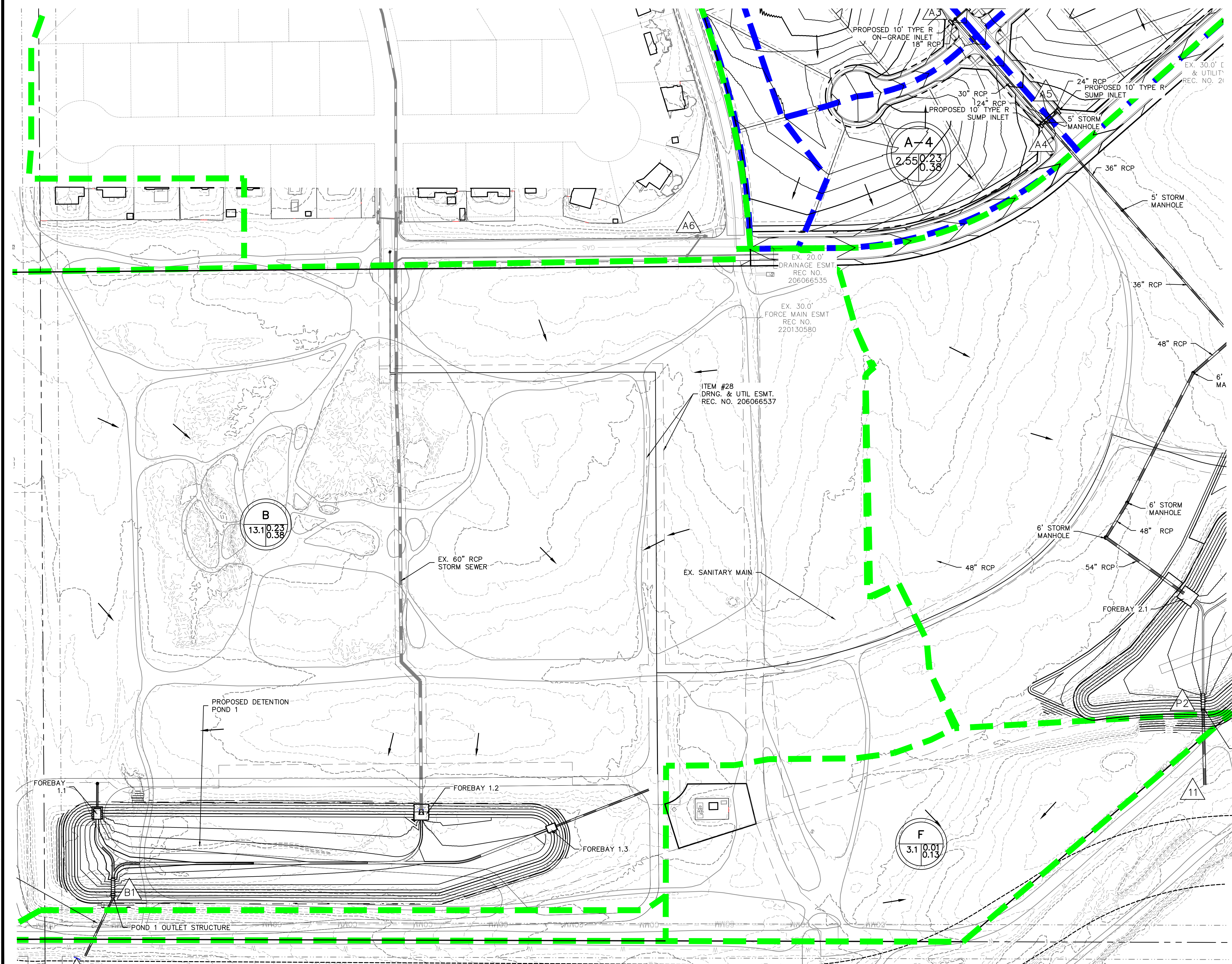
REVISIONS

COUNTY FILE NO.:

DR: TN CH: KB  
 P.M. DM

JOB: 24004308  
 SHEET NO. 04

CAD FILE: 24004308-PROPOSED DRAINAGE MAP-OVERALL.DWG



**LEGEND**

- PROPERTY BOUNDARY
- EXISTING RIGHT-OF-WAY
- PROPOSED RIGHT-OF-WAY
- EXISTING LOT LINE
- PROPOSED LOT LINE
- EXISTING SECTION LINE
- EXISTING EASEMENT
- EXISTING CONTOURS
- PROPOSED CONTOURS

**Basin Size in Acres**

Basin ID: A-1  
 5-YR RATIONAL C COEFFICIENT: 0.50  
 5-YR RATIONAL C COEFFICIENT: 0.75

Design Point ID: X

MAJOR BASIN BOUNDARY (Green dashed line)

MINOR BASIN BOUNDARY (Blue dashed line)

FLOW ARROW

**BENCHMARK:**  
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8605 EXPLORER DRIVE  
SUITE 250  
COLORADO SPRINGS, CO 80920  
719-598-5192  
JIM BYERS

**CHALLENGER HOMES**  
FALCON HIGHLANDS SOUTH - FILING 1  
EL PASO COUNTY, COLORADO  
DRAINAGE MAPS  
PROPOSED MAP

CLIENT: CHALLENGER HOMES  
DATE: --

REVISIONS

1st SUBMITTAL TO JURISDICTION  
07/08/2024 - KME

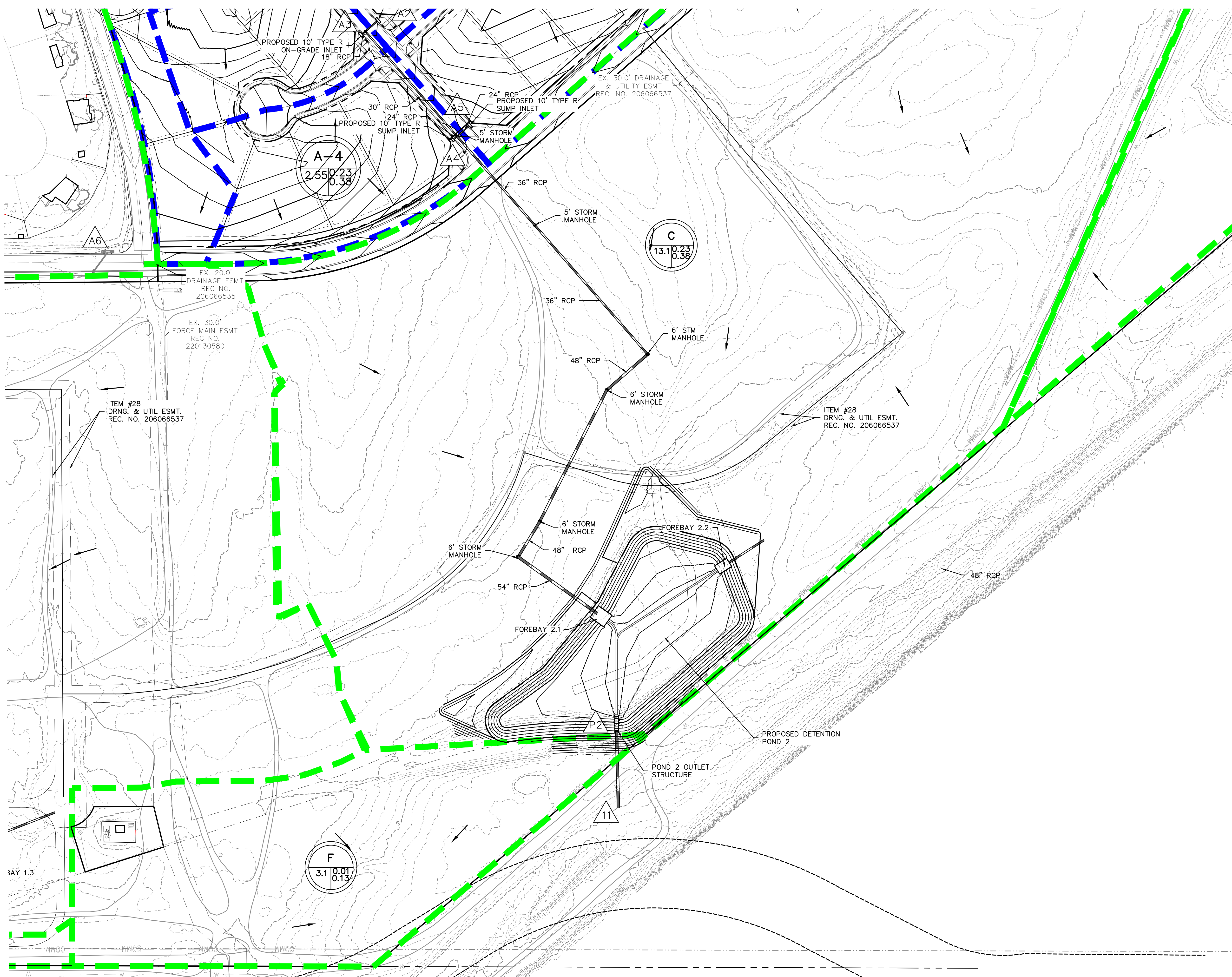
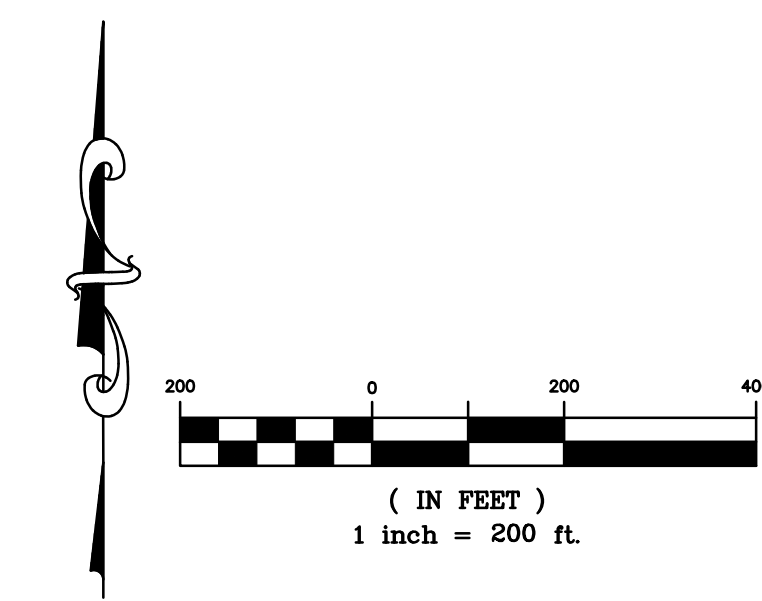
COUNTY FILE NO.:

DR. TN CH. KB  
P.M. DM

JOB: 24004308  
SHEET NO. 05

CAD FILE: 24004308-PROPOSED DRAINAGE MAP-OVERALL.DWG

Basin ID	Total Area (ac)	Design Point	C <sub>s</sub>	C <sub>100</sub>	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
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**LEGEND**

- PROPERTY BOUNDARY
- EXISTING RIGHT-OF-WAY
- PROPOSED RIGHT-OF-WAY
- EXISTING LOT LINE
- PROPOSED LOT LINE
- EXISTING SECTION LINE
- EXISTING EASEMENT
- EXISTING CONTOURS
- PROPOSED CONTOURS

**BASIN SIZE IN ACRES**

**DESIGN POINT ID**

**MAJOR BASIN BOUNDARY**

**FLOW ARROW**

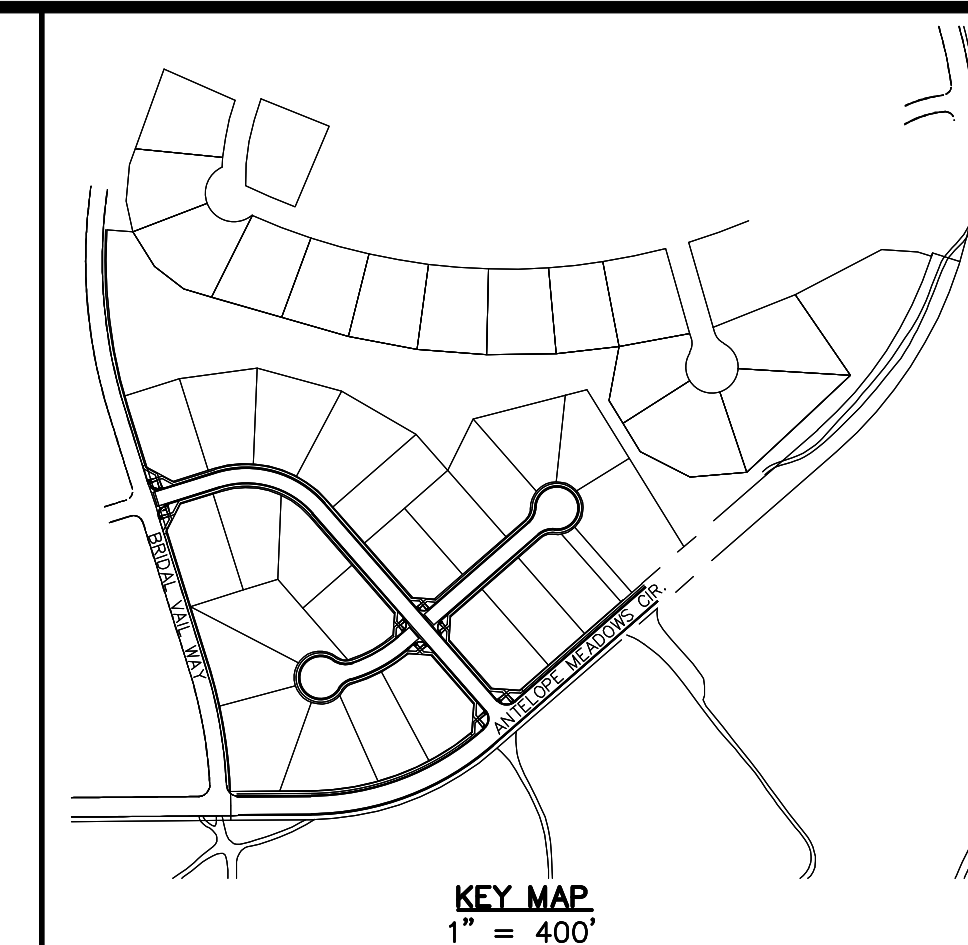
**BASIN ID**  
A-1

**5-YR RATIONAL C COEFFICIENT**  
0.50

**5-YR RATIONAL C COEFFICIENT**  
0.75

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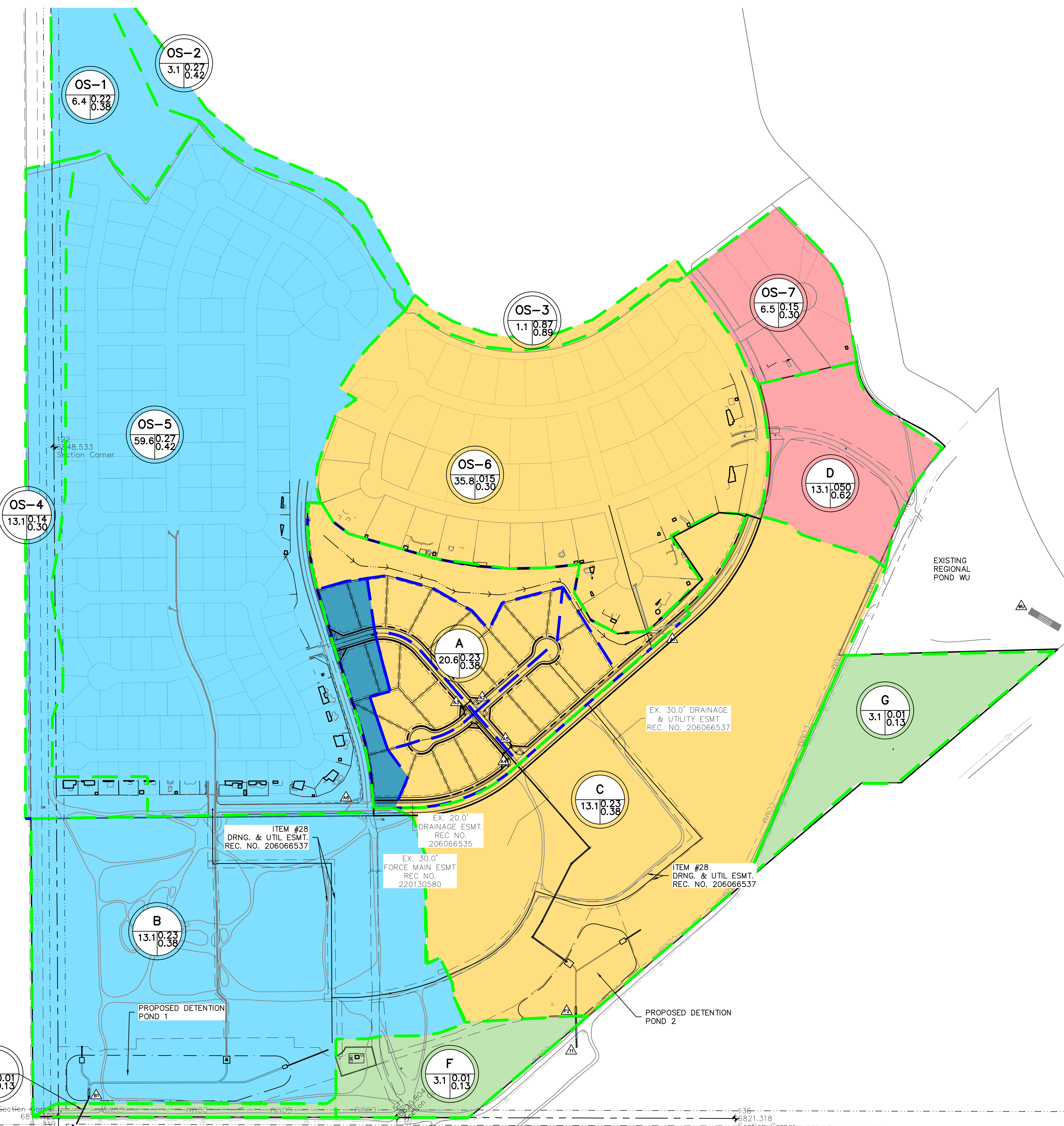


**811**  
Know what's below.  
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Basin ID	Total Area (ac)	Total Proposed Disturbed Area (ac)	Area Tributary to Pond 1 (ac)	Area Tributary to Pond 2 (ac)	Disturbed Area Treated (ac)	Un-Disturbed Area un-Treated (ac)
A-1	4.49	4.49	0	4.49	4.49	
A-2	4.83	4.83	4.83		4.83	
A-3	2.46	2.46	2.46		2.46	
A-4	2.55	2.55	2.55		2.55	
A-5	3.52	3.52	3.52		3.52	
A-6	2.75	2.75	2.75		2.75	
B	40.12	0		40.12		
C	41.08	0	41.08			
D	8.26	0	8.26			
E	1.41	0				1.41
F	5.91	0				5.91
G	8.38	0				8.38
<b>TOTAL</b>	<b>125.76</b>	<b>20.6</b>	<b>65.45</b>	<b>44.61</b>	<b>20.6</b>	<b>15.7</b>

**LEGEND**

- PROPERTY BOUNDARY
- EXISTING RIGHT-OF-WAY
- PROPOSED RIGHT-OF-WAY
- EXISTING LOT LINE
- PROPOSED LOT LINE
- EXISTING SECTION LINE
- EXISTING EASEMENT
- EXISTING CONTOURS
- PROPOSED CONTOURS

**BASIN SIZE IN ACRES**

**DESIGN POINT ID**

**MAJOR BASIN BOUNDARY**

**FLOW ARROW**

- AREA TRIBUTARY TO POND 1
- AREA TRIBUTARY TO POND 2
- FULLY UNDEVELOPED PERVIOUS AREA RUNNING OFFSITE
- AREA TRIBUTARY TO REGIONAL POND WU

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**CHALLENGER HOMES**  
FALCON HIGHLANDS SOUTH - FILING 1  
EL PASO COUNTY, COLORADO  
DRAINAGE MAPS  
GREEN INFRASTRUCTURE MAP

CLIENT: CHALLENGER HOMES  
DATE: --  
SUBMITTAL TO JURISDICTION: 07/08/2024 - KME  
REVISIONS:  
COUNTY FILE NO.:  
DR: TN CH: KB  
P.M. DM  
JOB: 24004308  
SHEET NO.: 5