



INNOVATIVE DESIGN. CLASSIC RESULTS.

**PRELIMINARY/FINAL DRAINAGE REPORT
FOR
LOTS 1 – 4
SOUTH ACADEMY HIGHLANDS FILING NO. 4**

January 2022

Prepared for:
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C/O SNR DENTON
ONE METROPOLITAN SQUARE
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ST. LOUIS, MO 63102

Prepared by:
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Job no. 2186.90



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LOTS 1 - 4 SOUTH ACADEMY HIGHLANDS FILING NO. 4**

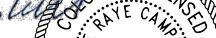
DRAINAGE REPORT STATEMENT

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City of Fountain for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Kyle R Campbell

Kyle R Campbell, Colorado P.E. #29794



5/11/22

Date

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: UTW Academy Development, LLC
By: 
Title: Jeffrey P. Otto, Authorized Signer
Address: 211 N. Broadway, Suite 3000

St. Louis, MO 63102

CITY OF FOUNTAIN:

Benjamin E. Sheets

For the City Engineer

5/12/22

Conditions:



PRELIMINARY/FINAL DRAINAGE REPORT FOR LOTS 1 - 4 SOUTH ACADEMY HIGHLANDS FILING NO. 4

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PURPOSE

This document is the Preliminary/Final Drainage Report for Lots 1-4 South Academy Highlands Filing No. 4, a re-plat of Lots 7, Lot 8, & Tract J of South Academy Highlands Filing No. 1. The purpose of this report is to identify onsite and offsite drainage patterns and general storm sewer infrastructure to support the lot development in accordance with all applicable previous reports and master drainage plans. This report accompanies a Final Plat submittal and storm sewer infrastructure plans. Site specific future Final Drainage Reports for each lot will be completed at the time of lot development.

GENERAL DESCRIPTION

Lots 1 through 4 are planned for future commercial single user developments with a portion of each lot being ‘undevelopable’ slope area draining to the west. Lot 1 is 1.341 acres, Lot 2 is 1.549 acres, Lot 3 is 1.303 acres, and Lot 4 is 1.970 acres. They are zoned PUD per the Overall Development Plan for South Academy Highlands and have been previously platted as Lot 7, Lot 8, and Tract J of South Academy Highlands Filing No. 1. A Re-Plat will be submitted in the future, along with site specific development plans for each lot. These four lots are located north of Venetucci Blvd. and S. Academy Blvd. intersection, and south-west of the signalized intersection (Wal-Mart Heights and Venetucci Blvd.) of the South Academy Highlands development. The site is located in the west half of Section 4, Township 15 South, Range 66 West of the Sixth Principal Meridian in the City of Fountain, County of El Paso, State of Colorado. The site is bounded on the north by unplatte El Paso County land, to the east by South Academy Highlands Filing No. 1 (Venetucci Blvd.) and Filing 1A (inline retail), to the south by South Academy Blvd. right-of-way, and to the west by existing Stratmoor South Subdivision Filing 3. The proposed site will contain four retail buildings; three fast food restaurants and an auto supply store. A retaining wall is required along the west edge of the developable area. The average soil condition of the proposed site reflects Hydrologic Group ‘A’ (Schamber-Razor complex) as determined by the “Web Soil Survey,” prepared by the Natural Resources Conservation Service (see map in Appendix).



EXISTING DRAINAGE CONDITIONS

The site is located within the Fishers Canyon Drainage Basin and as been overlot graded with the South Academy Highlands Filing No. 1 infrastructure construction. This site has been previously studied as part of the "Preliminary/Final Drainage Report for South Academy Highlands Filing No. 1," by Classic Consulting Engineers & Surveyors, LLC, revised August 2013. The proposed drainage patterns are in accordance with the previous approved report and the existing South Academy Highlands storm system discharges into an existing downstream full spectrum detention/water quality facility prior to releasing to the existing downstream Fishers Canyon Channel. Therefore, on-site storm water quality and detention is not required. This downstream facility is referred to as Private Detention and Storm Water Quality Facility 'T' within the Filing No. 1 report, and is a full spectrum detention, extended detention basin (EDB) storm water quality facility, including forebays, a micropool, and an outlet structure constructed to the criteria outlined within the City of Colorado Springs/El Paso County Drainage Criteria Manual and with full spectrum detention per the Urban Drainage and Flood Control District (UDFCD, now Mile High District) criteria. Maintenance of the pond components (inlets, outlet box/pipeline, forebays, etc.) and aesthetic maintenance and ownership of the pond is by the South Academy Highlands Metro District. Pond 'T' was designed and constructed to detain and treat the developed flows for all of the South Academy Highlands Phase 1 development, including future and planned commercial parcels (Filing No. 1 Basins C, D, G, I, J, & Y). The proposed site was modeled as Basin I in the previous Filing No. 1 drainage report. Per the report, "A Private 30" RCP storm pipe (Pipe 8) has been provided into the site from Venetucci Blvd. to convey these developed and interim flows. Prior to development of this basin (interim condition), the runoff from the proposed over lot grading will sheet flow north to a temporary sediment basin 'A'. The interim runoff to the sediment basin is $Q_5 = 4.1 \text{ cfs}$ and $Q_{100} = 10.8 \text{ cfs}$. The 8" pvc outfall pipe from the sediment basin is to connect to the provided 30" stub."

An Existing Conditions Map is included in the Appendix and shows two drainage basins, EX-1 and EX-2. Basin EX-1 ($Q_5 = 1.2 \text{ cfs}$ and $Q_{100} = 9.3 \text{ cfs}$) is 3.69 acres and has been graded as a flat 'pad' with the runoff sheet flowing to the north into temporary sediment basin constructed with Filing No. 1. The



undeveloped runoff collects in the sediment basin and outfalls into the existing 30" storm sewer stub provided from the adjacent Wal-Mart Heights and Venetucci Blvd. intersection. Basin EX-2 ($Q_5 = 1.1$ cfs and $Q_{100} = 8.9$ cfs) is 2.37 acres of native seed vegetated slope established with Filing No. 1 and draining to the east.

More recently than the Filing No. 1 FDR, a study was completed for the northern Venetucci Blvd. roadway extension to B Street – “Venetucci Boulevard Extension Drainage & Water Quality Improvements – Preliminary/Final Drainage Report,” by Matrix Design Group, dated May 22, 2019. This study makes reference to and correlates with the South Academy Highlands Filing No. 1 report. The roadway extension and new study area within the Matrix report are outside of the proposed South Academy Highlands Filing No. 4 development. Therefore, accordance to the Filing 1 report is all that is warranted.

PROPOSED DRAINAGE CONDITIONS

As previously mentioned, the proposed Lots 1-4 South Academy Highlands Filing No. 4 were previously platted and studied as Lot 7, Lot 8 and Tract J of South Academy Highlands Filing No. 1. The proposed condition drainage patterns do not differ from those set forth with the Filing No. 1 report and downstream infrastructure. As such, the Developed Conditions Map from that Filing No. 1 report is located in the Appendix of this report. Also in the Appendix is a site-specific Developed Conditions Map for Lots 1-4 and corresponding details below. This report is only establishing the western drive aisle and storm infrastructure including ‘stubs’ into each of the 4 Lots. Future Final Drainage Reports/Letters will be required for each individual lot development that details site specific private storm system extensions and collection locations. These details are not known at this time and therefore the ‘stubs’ are provided off the proposed Private storm main within this western drive aisle. General basin calculations are included for these developable areas to ensure pipe capacities. The proposed Private storm sewer will connect to the existing 30" RCP stub that was provided at the intersection of Wal-Mart Heights and Venetucci Blvd. The proposed Private storm sewer will be maintained by the lot owner(s). A detailed description of the developed flows is as follows:



Design Point 1 ($Q_5 = 3.3$ cfs, $Q_{100} = 6.5$ cfs) consists of runoff from Basin K, 0.83 acres of Lot 4 development. A future Final Drainage Report for Lot 4 will be completed that will detail the collection system and connection to this 18" storm stub (Pipe 1) provided with the storm sewer main and rear drive aisle construction. Pipe 1 connects to the inlet at DP-2.

Design Point 2 ($Q_5 = 0.7$ cfs, $Q_{100} = 1.3$ cfs) consists of runoff from Basin H, 0.16 acres of rear drive aisle and back of Lot 4 development. This runoff will drain over the asphalt and along the curb and gutter to a proposed 10.0' CDOT Type R curb (at-grade) inlet. Pipe 2 (Private 18" RCP, $Q_5 = 4.0$ cfs, $Q_{100} = 7.8$ cfs) conveys the intercepted runoff and that from Pipe 1 to the north within the rear drive aisle.

Design Point 3 ($Q_5 = 2.3$ cfs, $Q_{100} = 4.5$ cfs) consists of runoff from Basin J, 0.57 acres of Lot 3 development. A future Final Drainage Report for Lot 3 will be completed that will detail the collection system and connection to this 18" storm stub (Pipe 3) provided with the storm sewer main and rear drive aisle construction. Pipe 3 connects to the inlet at DP-4.

Design Point 4 ($Q_5 = 0.6$ cfs, $Q_{100} = 1.3$ cfs) consists of runoff from Basin G, 0.16 acres of rear drive aisle and back of Lot 3 development. This runoff will drain over the asphalt and along the curb and gutter to a proposed 5.0' CDOT Type R curb (at-grade) inlet. Pipe 4 (Private 24" RCP, $Q_5 = 6.9$ cfs, $Q_{100} = 13.4$ cfs) conveys the intercepted runoff and that from Pipes 2 & 3 to the north within the rear drive aisle.

Design Point 5 ($Q_5 = 2.7$ cfs, $Q_{100} = 5.3$ cfs) consists of runoff from Basin F, 0.65 acres of Lot 2 development. A future Final Drainage Report for Lot 2 will be completed that will detail the collection system and connection to this 18" storm stub (Pipe 5) provided with the storm sewer main and rear drive aisle construction. Pipe 5 connects to the inlet at DP-6.

Design Point 6 ($Q_5 = 0.9$ cfs, $Q_{100} = 1.7$ cfs) consists of runoff from Basin E, 0.20 acres of rear drive aisle and back of Lot 2 development. This runoff will drain over the asphalt and along the curb and gutter to a proposed 10.0' CDOT Type R curb (at-grade) inlet. Pipe 6 (Private 18" RCP, $Q_5 = 3.6$ cfs, $Q_{100} = 7.0$ cfs) conveys the intercepted runoff and that from Pipe 5 to the west to a junction manhole with Pipe 4.



Pipe 7 (Private 30" RCP, $Q_5 = 10.2$ cfs, $Q_{100} = 19.9$ cfs) conveys the combined runoff from this manhole to the north within the rear drive aisle.

Design Point 7 ($Q_5 = 0.5$ cfs, $Q_{100} = 1.1$ cfs) consists of runoff from Basin D, 0.15 acres of rear drive aisle and back of Lot 1 development. This runoff will drain over the asphalt and along the curb and gutter to a proposed 5.0' CDOT Type R curb (at-grade) inlet. Pipe 8 (18" RCP) conveys the intercepted runoff to the storm main in the rear drive aisle. Pipe 9 (Private 30" RCP, $Q_5 = 10.6$ cfs, $Q_{100} = 20.7$ cfs) conveys the combined runoff from this manhole (Pipes 7 & 8) to the north within the rear drive aisle.

Design Point 8 ($Q_5 = 3.9$ cfs, $Q_{100} = 7.6$ cfs) consists of runoff from Basin C, 0.94 acres of Lot 1 development. A future Final Drainage Report for Lot 1 will be completed that will detail the collection system and connection to this 24" storm stub (Pipe 10) provided with the storm sewer main and rear drive aisle construction. Pipe 10 connects to a junction manhole with Pipes 9 & 11.

Design Point 9 ($Q_5 = 0.7$ cfs, $Q_{100} = 1.4$ cfs) consists of runoff from Basin B, 0.19 acres of main entrance and rear drive aisle within Lot 1. This runoff will drain over the asphalt and along the curb and gutter to a proposed 10.0' CDOT Type R curb (at-grade) inlet. Pipe 11 (Private 18") conveys the intercepted runoff to a junction manhole with Pipes 9 & 10. This manhole connects with the existing 30" RCP stub (Pipe 12) from Venetucci Blvd. and South Academy Highlands Filing No. 1 infrastructure. Pipe 12 is the existing Private 30" RCP and contains fully developed flow rates of $Q_5 = 14.8$ cfs and $Q_{100} = 28.8$ cfs. The previously approved Filing No. 1 drainage report assumed a fully developed condition flow rate in this 30" RCP of $Q_5 = 17.5$ cfs and $Q_{100} = 32.8$ cfs, higher than the actual developed conditions of Lots 1-4 Filing No. 4. The previously approved report and infrastructure accounted for the same acreage of proposed Lots 1-4 commercial development in the downstream storm sewer main and full spectrum detention and storm water quality facility 'T' located prior to Fisher's Canyon drainage way. As previously discussed, this facility was designed and installed per all applicable criteria and no improvements are required based upon the development of Lots 1-4. As there have been no change to the tributary area, land use, drainage patterns, and a slight decrease in runoff rates, there is no need for additional analysis of the existing downstream infrastructure and the development of Lots 1-4



South Academy Highlands Filing No. 4 will not hinder adjacent properties or downstream storm sewer facilities.

Four (4) new temporary sediment basins are proposed (one for each lot) to replace the larger existing temporary sediment basin that exists within Basins B & C. Temporary sediment basin relocation design is shown on the site grading plan and construction drawings.

Design Point 10 ($Q_5 = 0.2 \text{ cfs}$, $Q_{100} = 0.5 \text{ cfs}$) consists of runoff from Basin A, 0.07 acres of existing Venetucci Blvd. and proposed entrance into the Lots 1-4 development. This runoff drains onto the existing roadway and drains to downstream facilities and ultimately to the downstream Pond 'T'. As this runoff is very minor and the proposed storm system effectively intercepts the proposed development drainage, additional downstream analysis is not warranted.

DRAINAGE CRITERIA

Hydrologic calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, Revised January 2021. The Rational Method was used to estimate stormwater runoff (5-year and 100-year recurrence intervals) to the proposed inlets, storm sewer pipes, and provided 30" storm sewer stub for the entire Lots 1 – 4 Filing No. 4 development. The UDFCD UD-Inlet workbook per Mile High Flood District (previously the Urban Drainage and Flood Control District) was used to size the proposed storm inlets. Hydraulic Grade Line (HGL) calculations for the 100-year storm event were calculated using UD-Sewer 2009 per Mile High Flood District and at no times is the 100-year line within 1.0' to the finished ground of the storm alignments. A Site-Level Low Impact Development form (IRF form) is included in the Appendix and was completed using the UD-BMP workbook from Mile High Flood District and shows a composite imperviousness of 88.1% for the 3.85 acres of developed runoff within Pipe 12.

WATER QUALITY SUMMARY

The City of Fountain has required the Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways,



and implementing long-term source controls. The Four Step Process pertains to management of smaller, frequently occurring storm events, as opposed to larger storms for which drainage and flood control infrastructure are sized. Implementation of these four steps helps to achieve stormwater permit requirements. This site adheres to this Four Step Process as follows:

1. This site is an approved PUD zoned commercial/retail site. In general, most roof drains are intended to drain across landscaping where feasible, and parking areas contain landscaping to minimize directly connected impervious areas.
2. Permanent BMPs for the overall South Academy Highlands commercial development have been implemented in initial development of the property in the form of Detention and Stormwater Quality Pond T located within Tract K Filing No. 1, later re-platted as a part of Lot 1 South Academy Highlands Filing No. 2.
3. Stormwater drainage from the subject property is being routed through a stormwater detention /stormwater quality treatment facility prior to being released to the historic drainage path as described in the previously approved reports. Developed flows will be required to adhere to release rates established within the previously approved reports and all stormwater discharge to downstream facilities will be required to employ energy dissipation measures to ensure no adverse effect to downstream facilities.
4. A site-specific stormwater quality and erosion control plan and narrative will be submitted and approved by City Engineering prior to any disturbance within the project area. Details such as site-specific source control construction BMP's will be detailed in the Grading and Erosion Control plan and in the Stormwater Management Narrative to protect receiving waters. Upon construction of the proposed development, temporary BMP's will be installed and maintained as required.

FLOODPLAIN STATEMENT

No portion of this site is located within a floodplain as determined by the Flood Insurance Rate Maps (F.I.R.M.) Map Number 08041C0743G effective date, December 7, 2018 (See Appendix).



DRAINAGE FEES

The proposed Lots 1-4 of South Academy Highlands Filing No. 4 has already been platted. A future Re-Plat will be completed along with lot specific Site Development Plans. South Academy Highlands is within the Fishers Canyon Drainage Basin, which is not a formally recognized basin with the City of Fountain's fee structure. Therefore, there are no required basin fees associated with the proposed site.

CONSTRUCTION COST OPINION

Private Drainage Facilities Non-reimbursable

ITEM	DESCRIPTION	QUANTITY	UNIT COST	COST
1.	5.0' CDOT Type R Inlet	2 EACH	\$7,440/EA	\$ 14,880.00
2.	10' CDOT Type R Inlet	3 EACH	\$8,136/EA	\$ 24,408.00
3.	Type II Manhole	4 EACH	\$6,619/EA	\$ 26,476.00
4.	18" RCP Storm Drain	282 LF	\$67/LF	\$ 18,894.00
5.	24" RCP Storm Drain	150 LF	\$81/LF	\$ 12,150.00
6.	30" RCP Storm Drain	332 LF	\$100/LF	\$ 33,200.00
SUB-TOTAL				\$ 130,008.00
10% ENGINEERING				\$ 13,000.80
5% CONTINGENCIES				\$ 6,500.40
TOTAL				<u>\$ 149,509.20</u>

Classic Consulting Engineers & Surveyors cannot and does not guarantee that the construction cost will not vary from these opinions of probable construction costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular.



SUMMARY

All drainage facilities were sized using the current City of Fountain Drainage Criteria and will safely discharge all developed runoff to the existing 30" storm stub provided from Venetucci Blvd. (Filing No. 1). An existing regional full spectrum detention and water quality facility will treat the runoff prior to releasing below historic rates into the existing Fishers Canyon Channel. The total developed runoff to the existing 30" storm stub is less than the allowable anticipated runoff calculated with the original South Academy Highlands Filing No. 1 drainage report. Therefore, the proposed development is in compliance with the master drainage study. Future Final Drainage Reports/Letters will be required for each individual lot development that details site specific private storm system extensions and collection locations. All of the proposed storm sewer is Private and will be maintained by the lot owner(s). Construction of Lots 1-4 of Filing No. 4 will not adversely affect any surrounding development or downstream facilities.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC



Matthew Larson
Project Engineer

mal/2186.90/REPORTS/PDR-SAH-FIL.4.doc



REFERENCES

1. City of Colorado Springs/El Paso County Drainage Criteria Manual Vol. 1 dated May 2014, revised January 2021.
2. Drainage Criteria Manual Vol. 2, dated May 2014, revised December 2020.
3. "Fishers Canyon Drainage Basin Planning Study," by Muller Engineering Company, dated July 16, 1991.
4. "Preliminary/Final Drainage Report for South Academy Highlands Filing No. 1," by Classic Consulting Engineers & Surveyors, LLC, revised August 2013.
5. "Final Drainage Report for Lots 1 & 2 South Academy Highlands Filing No. 1A," by Classic Consulting Engineers & Surveyors, LLC, January 2015.
6. "Final Drainage Report for Lot 1 South Academy Highlands Filing No. 2," by Classic Consulting Engineers & Surveyors, LLC, March 2015.
7. "Venetucci Boulevard Extension Drainage & Water Quality Improvements – Preliminary/Final Drainage Report," by Matrix Design Group dated May 22, 2019.

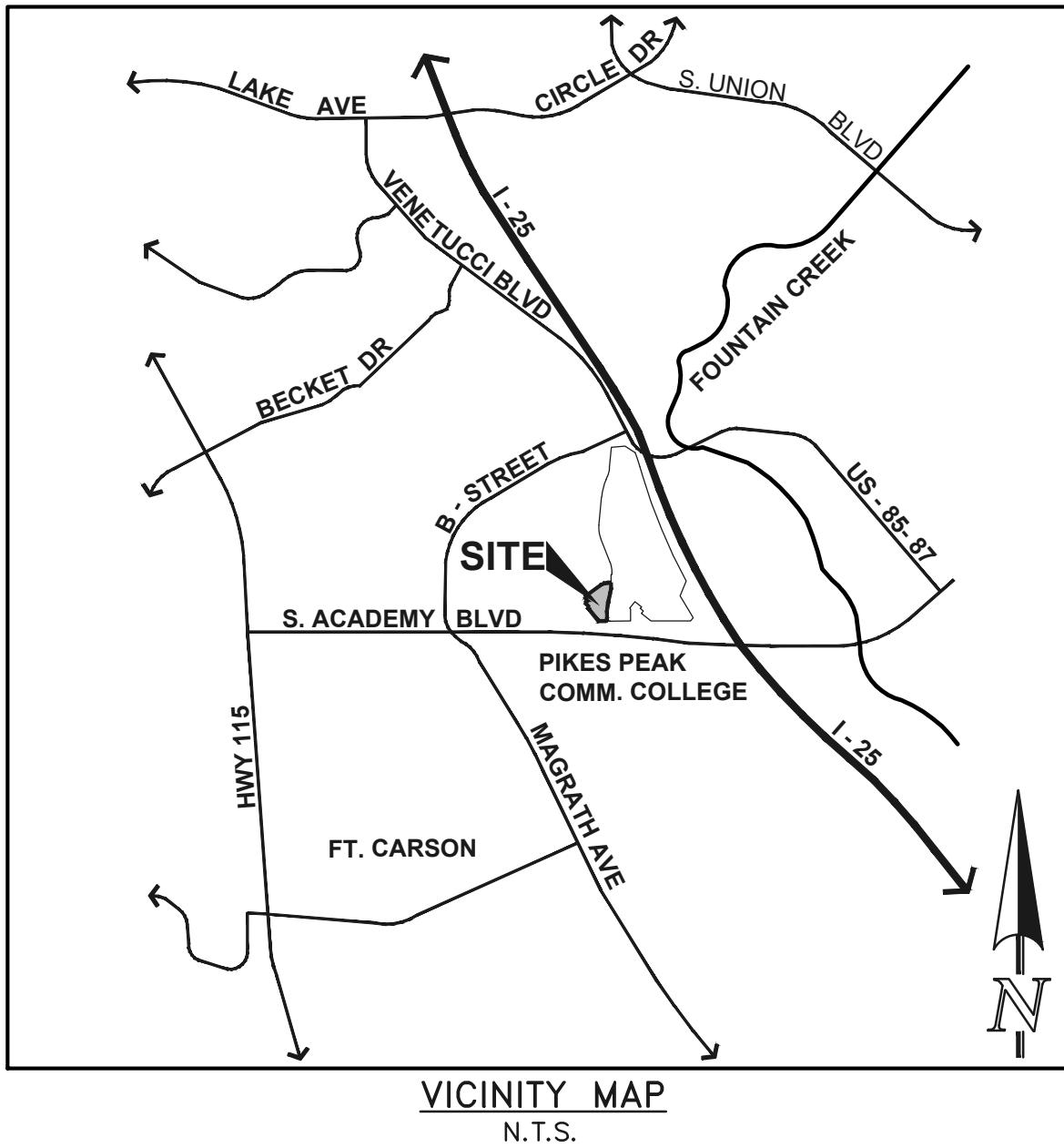


APPENDIX



VICINITY MAP

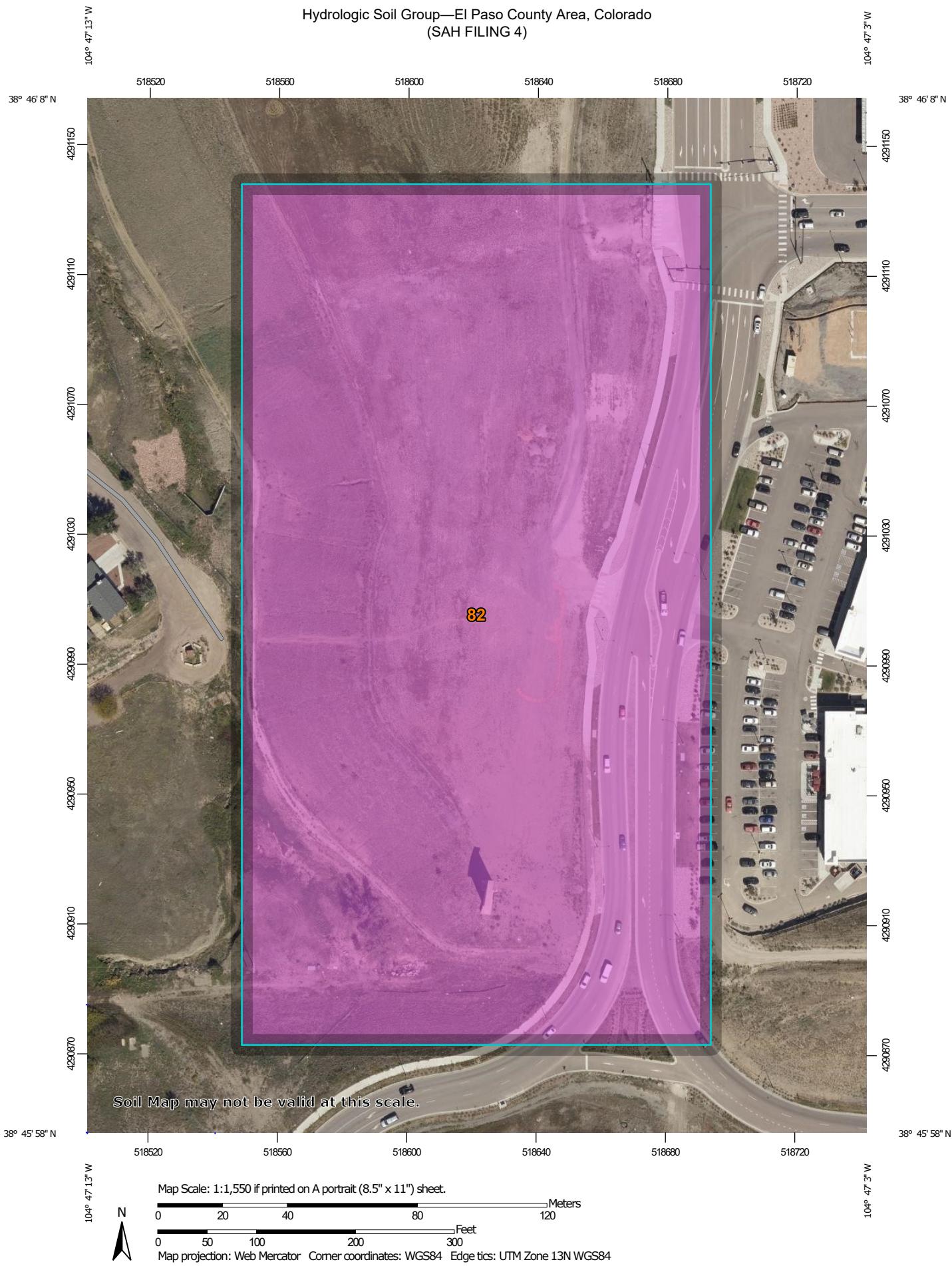




SOILS MAP (N.C.S SURVEY)

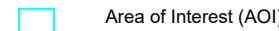


Hydrologic Soil Group—El Paso County Area, Colorado
(SAH FILING 4)



MAP LEGEND

Area of Interest (AOI)



Soils

Soil Rating Polygons

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Lines

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Points

	A
	A/D
	B
	B/D

	C
	C/D
	D
	Not rated or not available

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
82	Schamber-Razor complex, 8 to 50 percent slopes	A	9.5	100.0%
Totals for Area of Interest			9.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition



Component Percent Cutoff: None Specified

Tie-break Rule: Higher



F.E.M.A. MAP



National Flood Hazard Layer FIRMette



104°47'27"W 38°46'11"N



0 250 500

1,000

1,500

Feet

1:6,000

104°46'50"W 38°45'43"N

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS

- Without Base Flood Elevation (BFE)
Zone A, V, A99
- With BFE or Depth Zone AE, AO, AH, VE, AR
- Regulatory Floodway

- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X

- Future Conditions 1% Annual Chance Flood Hazard Zone X

- Area with Reduced Flood Risk due to Levee. See Notes. Zone X

- Area with Flood Risk due to Levee Zone D

- NO SCREEN Area of Minimal Flood Hazard Zone X

- Effective LOMRs

- Area of Undetermined Flood Hazard Zone D

- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

- Cross Sections with 1% Annual Chance

- Water Surface Elevation

- Coastal Transect

- Base Flood Elevation Line (BFE)

- Limit of Study

- Jurisdiction Boundary

- Coastal Transect Baseline

- Profile Baseline

- Hydrographic Feature

- Digital Data Available

- No Digital Data Available

- Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/2/2021 at 11:01 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

CALCULATIONS



JOB NAME: *South Academy Highlands Filing No. 4*
 JOB NUMBER: *2186.90*
 DATE: *01/30/22*
 CALCULATED BY: *MAL*

FINAL DRAINAGE REPORT ~ BASIN RUNOFF COEFFICIENT SUMMARY (DEVELOPED)

BASIN	TOTAL AREA (AC)	IMPERVIOUS AREA / STREETS			LANDSCAPE/UNDEVELOPED AREAS			WEIGHTED		WEIGHTED CA		USE
		AREA (AC)	C(5)	C(100)	AREA (AC)	C(5)	C(100)	C(5)	C(100)	CA(5)	CA(100)	
A	0.07	0.05	0.90	0.95	0.02	0.08	0.35	0.67	0.78	0.05	0.05	Drive Aisle
B	0.19	0.15	0.90	0.95	0.04	0.08	0.35	0.73	0.82	0.14	0.16	Drive Aisle
C	0.94	0.85	0.90	0.95	0.09	0.08	0.35	0.82	0.89	0.77	0.84	LOT 1
D	0.15	0.12	0.90	0.95	0.03	0.08	0.35	0.74	0.83	0.11	0.12	Drive Aisle
E	0.20	0.18	0.90	0.95	0.02	0.08	0.35	0.82	0.89	0.16	0.18	Drive Aisle
F	0.65	0.59	0.90	0.95	0.06	0.08	0.35	0.82	0.89	0.54	0.58	LOT 2
G	0.16	0.14	0.90	0.95	0.02	0.08	0.35	0.80	0.88	0.13	0.14	Drive Aisle
H	0.16	0.15	0.90	0.95	0.01	0.08	0.35	0.85	0.91	0.14	0.15	Drive Aisle
J	0.57	0.50	0.90	0.95	0.07	0.08	0.35	0.80	0.88	0.46	0.50	LOT 3
K	0.83	0.71	0.90	0.95	0.12	0.08	0.35	0.78	0.86	0.65	0.72	LOT 4
Q	2.06	0.00	0.90	0.95	2.06	0.08	0.35	0.08	0.35	0.16	0.72	EX. SLOPE
EX-1	3.69	0.00	0.90	0.95	3.69	0.08	0.35	0.08	0.35	0.30	1.29	EXIST
EX-2	2.37	0.00	0.90	0.95	2.37	0.08	0.35	0.08	0.35	0.19	0.83	EXIST

JOB NAME:	<i>South Academy Highlands Filing No. 4</i>		
JOB NUMBER:	2186.90		
DATE:	01/30/22		
CALC'D BY:	MAL		

FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY (DEVELOPED)

BASIN	WEIGHTED		OVERLAND			STREET / CHANNEL FLOW			Tc	INTENSITY		TOTAL FLOWS			
	CA(5)	CA(100)	C(5)	Length (ft)	Height (ft)	Tc (min)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)	TOTAL (min)	I(5) (in/hr)	I(100) (in/hr)	Q(5) (cfs)	Q(100) (cfs)
A	0.05	0.05	0.9	10	0.15	1.0	40	1.5%	4.3	0.2	5.0	5.10	9.07	0.2	0.5
B	0.14	0.16	0.9	10	0.15	1.0	190	1.5%	4.3	0.7	5.0	5.10	9.07	0.7	1.4
C	0.77	0.84	0.9	10	0.15	1.0	190	1.5%	4.3	0.7	5.0	5.10	9.07	3.9	7.6
D	0.11	0.12	0.9	10	0.15	1.0	120	1.5%	4.3	0.5	5.0	5.10	9.07	0.6	1.1
E	0.16	0.18	0.9	10	0.15	1.0	130	1.5%	4.3	0.5	5.0	5.10	9.07	0.8	1.6
F	0.54	0.58	0.9	10	0.15	1.0	220	1.5%	4.3	0.9	5.0	5.10	9.07	2.7	5.3
G	0.13	0.14	0.9	10	0.15	1.0	120	1.5%	4.3	0.5	5.0	5.10	9.07	0.7	1.3
H	0.14	0.15	0.9	10	0.15	1.0	210	1.5%	4.3	0.8	5.0	5.10	9.07	0.7	1.3
J	0.46	0.50	0.9	10	0.15	1.0	200	1.5%	4.3	0.8	5.0	5.10	9.07	2.3	4.5
K	0.65	0.72	0.9	10	0.15	1.0	230	1.5%	4.3	0.9	5.0	5.10	9.07	3.3	6.5
Q	0.16	0.72	0.08	75	26	5.1	360	4.4%	7.3	0.8	5.9	4.87	8.66	0.8	6.2

EX-1	0.30	1.29	0.08	50	2	8.5	500	2.0%	4.9	1.7	10.2	4.07	7.23	1.2	9.3
EX-2	0.19	0.83	0.08	10	3.33	1.9	90	33.0%	20.1	0.1	2.0	6.06	10.77	1.1	8.9

JOB NAME:	<i>South Academy Highlands Filing No. 4</i>
JOB NUMBER:	<u>2186.90</u>
DATE:	<u>01/30/22</u>
CALCULATED BY:	<u>MAL</u>

FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY (DEVELOPED)

Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	Intensity		Flow		Outfall
					I(5)	I(100)	Q(5)	Q(100)	
1	BASIN K	0.65	0.72	5.0	5.10	9.07	3.3	6.5	STUB
2	BASIN H	0.14	0.15	5.0	5.10	9.07	0.7	1.3	10.0' Type R At-Grade Inlet
3	BASIN J	0.46	0.50	5.0	5.10	9.07	2.3	4.5	STUB
4	BASIN G + FLOW-BY DP-2	0.13	0.14	5.0	5.10	9.07	0.6	1.3	5.0' Type R At-Grade Inlet
5	BASIN F	0.54	0.58	5.0	5.10	9.07	2.7	5.3	STUB
6	BASIN E + FLOW-BY DP-4	0.17	0.19	5.0	5.10	9.07	0.9	1.7	10.0' Type R At-Grade Inlet
7	BASIN D + FLOW-BY DP-6	0.11	0.13	5.0	5.10	9.07	0.5	1.1	5.0' Type R At-Grade Inlet
8	BASIN C	0.77	0.84	5.0	5.10	9.07	3.9	7.6	STUB
9	BASIN B + FLOW-BY DP-7	0.14	0.16	5.0	5.10	9.07	0.7	1.4	10.0' Type R St-Grade Inlet
10	BASIN A + FLOW-BY DP-9	0.05	0.05	5.0	5.10	9.07	0.2	0.5	SURFACE

JOB NAME:	<i>South Academy Highlands Filing No. 4</i>
JOB NUMBER:	<u>2186.90</u>
DATE:	<u>04/06/22</u>
CALCULATED BY:	<u>MAL</u>

* PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE.
REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY

Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	Intensity		Flow		Pipe Size*
					I(5)	I(100)	Q(5)	Q(100)	
1	DP-1	0.65	0.72	5.0	5.10	9.07	3.3	6.5	18" RCP
2	PIPE 1 + DP-2	0.78	0.86	5.0	5.10	9.07	4.0	7.8	18" RCP
3	DP-3	0.46	0.50	5.0	5.10	9.07	2.3	4.5	18" RCP
4	PIPE 2 + PIPE 3 + DP-4	1.37	1.50	5.3	5.02	8.92	6.9	13.4	24" RCP
5	DP-5	0.54	0.58	5.0	5.10	9.07	2.7	5.3	18" RCP
6	PIPE 5 + DP-6	0.71	0.77	5.0	5.10	9.07	3.6	7.0	18" RCP
7	PIPE 4 + PIPE 6	2.07	2.27	5.7	4.93	8.77	10.2	19.9	30" RCP
8	DP-7	0.11	0.13	5.0	5.10	9.07	0.5	1.1	18" RCP
9	PIPE 7 + PIPE 8	2.18	2.40	6.0	4.86	8.63	10.6	20.7	30" RCP
10	DP-8	0.77	0.84	5.0	5.10	9.07	3.9	7.6	24" RCP
11	DP-9	0.14	0.16	5.0	5.10	9.07	0.7	1.4	18" RCP
12	PIPE 9 + PIPE 10 + PIPE 11	3.10	3.40	6.4	4.77	8.48	14.8	28.8	EX. 30" RCP

JOB NAME: *South Academy Highlands Filing No. 4*
 JOB NUMBER: *2186.90*
 DATE: *01/30/22*
 CALCULATED BY: *MAL*

At-Grade Inlet - Flow Routing (DEVELOPED CONDITIONS)

Design Point	TOTAL					INTERCEPTED				FLOW-BY				
	CA5	CA100	I5	I100	Q5	Q100	Q5	Q100	CA5	CA100	Q5	Q100	CA5	CA100
2	0.14	0.15	5.10	9.07	0.7	1.3	0.7	1.3	0.14	0.14	0.0	0.0	0.00	0.00
4	0.13	0.14	5.10	9.07	0.6	1.3	0.6	1.2	0.12	0.13	0.0	0.1	0.01	0.01
6	0.17	0.19	5.10	9.07	0.9	1.7	0.9	1.7	0.18	0.19	0.0	0.0	0.00	0.00
7	0.11	0.13	5.10	9.07	0.5	1.1	0.5	1.1	0.10	0.12	0.0	0.0	0.00	0.00
9	0.14	0.16	5.10	9.07	0.7	1.4	0.7	1.4	0.14	0.15	0.0	0.0	0.00	0.00

JOB NAME:
JOB NUMBER:
DATE:
CALCULATED BY:

FINAL DRAINAGE REPORT ~ PIPE TRAVEL TIMES

PIPE RUN	STREET / CHANNEL FLOW				
	Pipe Diameter (ft)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)
2	1.5	125	1.0%	6.0	0.3
4	2.0	150	1.0%	7.2	0.3
7	2.0	140	1.0%	7.2	0.3
9	2.5	195	1.0%	8.4	0.4

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP2	DP4	DP6	DP7	DP9
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET
Hydraulic Condition	On Grade				
Inlet Type	CDOT Type R Curb Opening				

USER-DEFINED INPUT

User-Defined Design Flows					
Minor Q _{Known} (cfs)	0.7	0.6	0.9	0.5	0.7
Major Q _{Known} (cfs)	1.3	1.3	1.6	1.1	1.4
Bypass (Carry-Over) Flow from Upstream					
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	User-Defined	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.1	0.0	0.0
Watershed Characteristics					
Subcatchment Area (acres)					
Percent Impervious					
NRCS Soil Type					
Watershed Profile					
Overland Slope (ft/ft)					
Overland Length (ft)					
Channel Slope (ft/ft)					
Channel Length (ft)					
Minor Storm Rainfall Input					
Design Storm Return Period, T _r (years)					
One-Hour Precipitation, P ₁ (inches)					
Major Storm Rainfall Input					
Design Storm Return Period, T _r (years)					
One-Hour Precipitation, P ₁ (inches)					

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	0.7	0.6	0.9	0.5	0.7
Major Total Design Peak Flow, Q (cfs)	1.3	1.3	1.7	1.1	1.4
Minor Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.0	0.1	0.0	0.0	0.0
Minor Storm (Calculated) Analysis of Flow Time					
C	N/A	N/A	N/A	N/A	N/A
C ₅	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, V _i	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, V _t	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, T _i	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, T _t	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T _c	N/A	N/A	N/A	N/A	N/A
Regional T _c	N/A	N/A	N/A	N/A	N/A
Recommended T _c	N/A	N/A	N/A	N/A	N/A
T _c selected by User	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Q _p	N/A	N/A	N/A	N/A	N/A
Major Storm (Calculated) Analysis of Flow Time					
C	N/A	N/A	N/A	N/A	N/A
C ₅	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, V _i	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, V _t	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, T _i	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, T _t	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T _c	N/A	N/A	N/A	N/A	N/A
Regional T _c	N/A	N/A	N/A	N/A	N/A
Recommended T _c	N/A	N/A	N/A	N/A	N/A
T _c selected by User	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Q _p	N/A	N/A	N/A	N/A	N/A

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

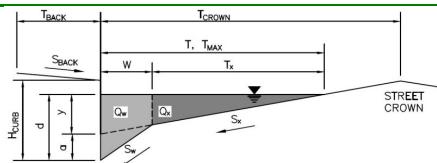
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Enter Your Project Name Here

Inlet ID:

DP2

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

T_BACK = ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

S_BACK = ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

n_BACK =

Height of Curb at Gutter Flow Line

H_CURB = inches

Distance from Curb Face to Street Crown

T_CROWN = ft

Gutter Width

W = ft

Street Transverse Slope

S_x = ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

S_w = ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

S_o = ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

n_STREET =

Max. Allowable Spread for Minor & Major Storm

Minor Storm ft

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Major Storm inches

Allow Flow Depth at Street Crown (leave blank for no)

 check = yes

MINOR STORM Allowable Capacity is based on Spread Criterion

Minor Storm cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

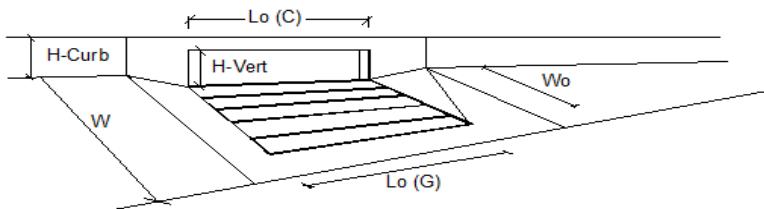
Major Storm cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type R Curb Opening		MINOR MAJOR	
Type of Inlet	CDOT Type R Curb Opening			Type =	CDOT Type R Curb Opening
Local Depression (additional to continuous gutter depression 'a')				a _{LOCAL} =	3.0 3.0
Total Number of Units in the Inlet (Grate or Curb Opening)				No =	1 1
Length of a Single Unit Inlet (Grate or Curb Opening)				L _o =	10.00 10.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)				W _o =	N/A N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)				C _r -G =	N/A N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)				C _r -C =	0.10 0.10
<small>inches ft ft cfs cfs %</small>					
Street Hydraulics: OK - Q < Allowable Street Capacity'					
Total Inlet Interception Capacity				Q =	0.7 1.3
Total Inlet Carry-Over Flow (flow bypassing inlet)				Q _b =	0.0 0.0
Capture Percentage = Q _b /Q _o =				C% =	100 100

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

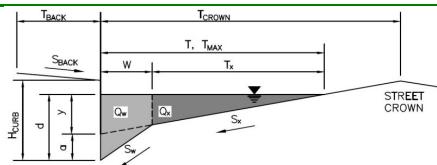
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Enter Your Project Name Here

Inlet ID:

DP4

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 6.0$ ft $S_{BACK} = 0.020$ ft/ft $n_{BACK} = 0.020$

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 17.0$ ft

Gutter Width

 $W = 1.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.063$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.015$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm

Minor Storm Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

 $T_{MAX} = 17.0$ ft $T_{MAX} = 17.0$ ft

Allow Flow Depth at Street Crown (leave blank for no)

 $d_{MAX} = 6.0$ inches $d_{MAX} = 9.1$ inches

check = yes

MINOR STORM Allowable Capacity is based on Spread Criterion

Minor Storm Major Storm

MAJOR STORM Allowable Capacity is based on Depth Criterion

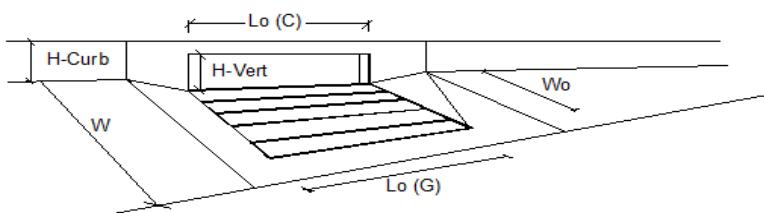
 $Q_{allow} = 12.3$ cfs $Q_{allow} = 76.2$ cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type R Curb Opening		MINOR MAJOR	
Type of Inlet	Type = CDOT Type R Curb Opening			inches	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} = 3.0		3.0		
Total Number of Units in the Inlet (Grate or Curb Opening)	No = 1		1		
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o = 5.00		5.00		ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o = N/A		N/A		ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _r -G = N/A		N/A		
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _r -C = 0.10		0.10		
<u>Street Hydraulics: OK - Q < Allowable Street Capacity'</u>					
Total Inlet Interception Capacity	Q = 0.6		1.2		cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b = 0.0		0.1		cfs
Capture Percentage = Q _b /Q _o =	C% = 100		94		%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

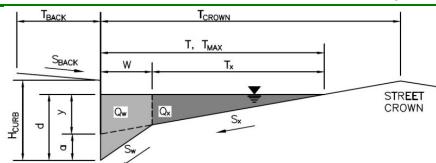
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Enter Your Project Name Here

Inlet ID:

DP6

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 6.0$ ft $S_{BACK} = 0.020$ ft/ft $n_{BACK} = 0.020$

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 17.0$ ft

Gutter Width

 $W = 1.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.063$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.015$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm

Minor Storm Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

 $T_{MAX} = 17.0$ ft $T_{MAX} = 17.0$ ft

Allow Flow Depth at Street Crown (leave blank for no)

 $d_{MAX} = 6.0$ inches $d_{MAX} = 9.1$ inches

check = yes

MINOR STORM Allowable Capacity is based on Spread Criterion

Minor Storm Major Storm

MAJOR STORM Allowable Capacity is based on Depth Criterion

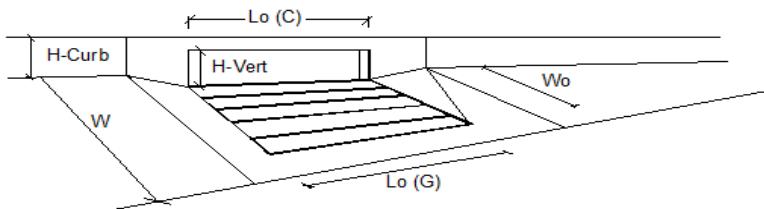
 $Q_{allow} = 12.3$ cfs $Q_{allow} = 76.2$ cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type R Curb Opening		MINOR MAJOR	
Type of Inlet	CDOT Type R Curb Opening			Type =	CDOT Type R Curb Opening
Local Depression (additional to continuous gutter depression 'a')				a _{LOCAL} =	3.0 3.0 inches
Total Number of Units in the Inlet (Grate or Curb Opening)				No =	1 1
Length of a Single Unit Inlet (Grate or Curb Opening)				L _o =	10.00 10.00 ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)				W _o =	N/A N/A ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)				C _r -G =	N/A N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)				C _r -C =	0.10 0.10
<u>Street Hydraulics: OK - Q < Allowable Street Capacity'</u>					
Total Inlet Interception Capacity				Q =	0.9 1.7 cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)				Q _b =	0.0 0.0 cfs
Capture Percentage = Q _b /Q _o =				C% =	100 100 %

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

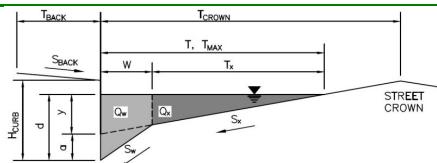
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Enter Your Project Name Here

Inlet ID:

DP7

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

T_BACK = ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

S_BACK = ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

n_BACK =

Height of Curb at Gutter Flow Line

H_CURB = inches

Distance from Curb Face to Street Crown

T_CROWN = ft

Gutter Width

W = ft

Street Transverse Slope

S_x = ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

S_w = ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

S_o = ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

n_STREET =

Max. Allowable Spread for Minor & Major Storm

Minor Storm ft

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Major Storm inches

Allow Flow Depth at Street Crown (leave blank for no)

 check = yes

MINOR STORM Allowable Capacity is based on Spread Criterion

Minor Storm cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

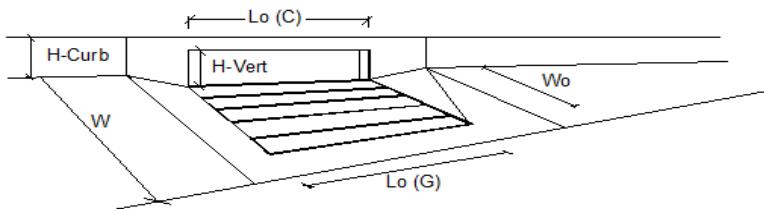
Major Storm cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type R Curb Opening		MINOR MAJOR	
Type of Inlet	Type = CDOT Type R Curb Opening			inches	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} = 3.0		3.0		
Total Number of Units in the Inlet (Grate or Curb Opening)	No = 1		1		
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o = 5.00		5.00		ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o = N/A		N/A		ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _r -G = N/A		N/A		
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _r -C = 0.10		0.10		
<u>Street Hydraulics: OK - Q < Allowable Street Capacity'</u>					
Total Inlet Interception Capacity	Q = 0.5		1.1		cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b = 0.0		0.0		cfs
Capture Percentage = Q _b /Q _o =	C% = 100		98		%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

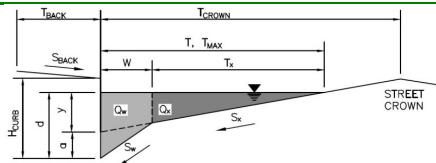
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Enter Your Project Name Here

Inlet ID:

DP9

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 13.0$ ft $S_{BACK} = 0.020$ ft/ft $n_{BACK} = 0.020$

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 43.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.063$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.012$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm

Minor Storm Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

 $T_{MAX} = 43.0$ ft $d_{MAX} = 6.0$ inches

Allow Flow Depth at Street Crown (leave blank for no)



check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

Minor Storm Major Storm

MAJOR STORM Allowable Capacity is based on Depth Criterion

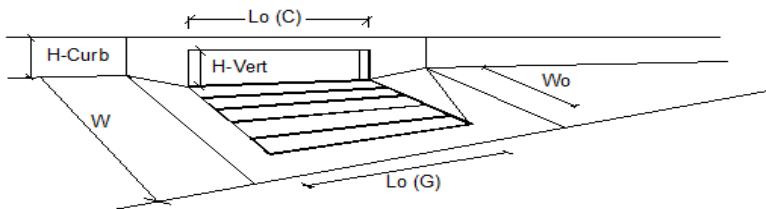
 $Q_{allow} = 19.2$ cfs 72.1 cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

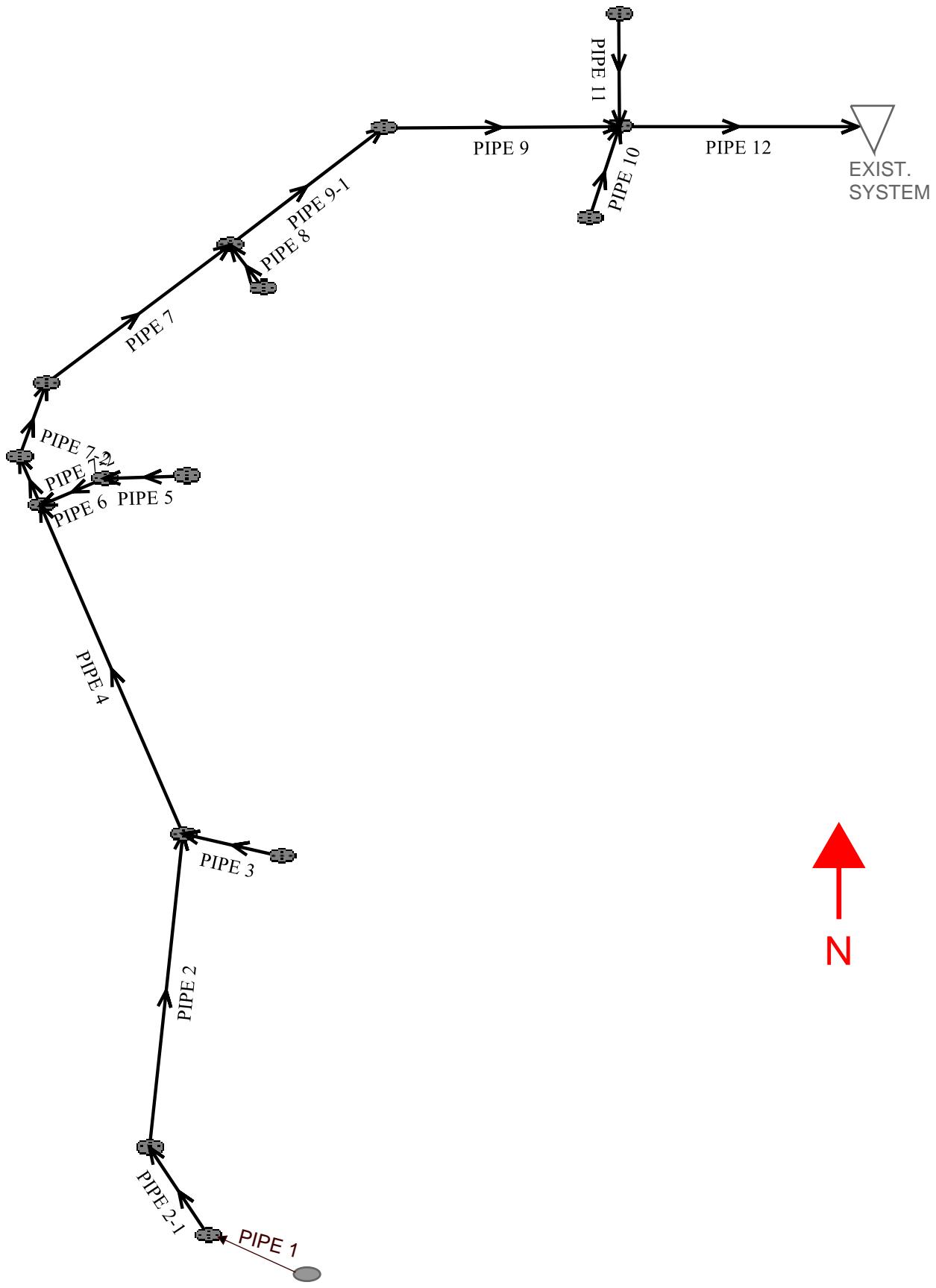
INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')			
Total Number of Units in the Inlet (Grate or Curb Opening)	Type = MINOR MAJOR		
Length of a Single Unit Inlet (Grate or Curb Opening)	a _{LOCAL} = 3.0	3.0	inches
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	L _o = 15.00	15.00	ft
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	W _o = N/A	N/A	ft
	C _r -G = N/A	N/A	
	C _r -C = 0.10	0.10	
<u>Street Hydraulics: OK - Q < Allowable Street Capacity'</u>			
Total Inlet Interception Capacity	MINOR MAJOR		
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q = 0.7	1.4	cfs
Capture Percentage = Q _b /Q _o =	Q _b = 0.0	0.0	cfs
	C% = 100	100	%

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator																																																																																																																																																																																																																																																											
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System Input Summary - FILING 4 HGL – 100 YR

Rainfall Parameters

Rainfall Return Period: 100

Rainfall Calculation Method: Formula

One Hour Depth (in):

Rainfall Constant "A": 28.5

Rainfall Constant "B": 10

Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20

Maximum Rural Overland Len. (ft): 500

Maximum Urban Overland Len. (ft): 300

Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00

Maximum Depth to Rise Ratio: 0.90

Maximum Flow Velocity (fps): 18.0

Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 0.00

Manhole Input Summary:

Manhole Output Summary:

	Local Contribution					Total Design Flow					
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment	
OUTFALL 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
PIPE 12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	28.80	Surface Water Present (Downstream)	
PIPE 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	20.70		
PIPE 9-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	20.70		
PIPE 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	19.90		
PIPE 7-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	19.90		
PIPE 7-2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	19.90		
PIPE 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	7.00		
PIPE 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5.30		
PIPE 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	13.40		
PIPE 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.50		
PIPE 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	7.80		
PIPE 2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	7.80		
PIPE 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.50		
PIPE 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.10		
PIPE 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	7.60		
PIPE 11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.40		

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
PIPE 12	98.50	5880.19	1.0	5881.17	0.013	0.03	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 9	113.45	5881.47	0.5	5882.04	0.013	0.05	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 9-1	76.79	5882.34	0.5	5882.72	0.013	0.25	0.53	CIRCULAR	30.00 in	30.00 in
PIPE 7	110.00	5883.02	0.5	5883.57	0.013	0.05	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 7-1	21.99	5883.57	0.5	5883.68	0.013	0.20	0.58	CIRCULAR	30.00 in	30.00 in
PIPE 7-2	10.00	5883.68	0.5	5883.73	0.013	0.20	0.58	CIRCULAR	30.00 in	30.00 in
PIPE 6	10.00	5884.73	0.5	5884.78	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 5	16.00	5885.08	0.5	5885.16	0.013	0.05	0.84	CIRCULAR	18.00 in	18.00 in
PIPE 4	150.32	5884.23	0.5	5884.98	0.013	0.05	1.00	CIRCULAR	24.00 in	24.00 in
PIPE 3	25.00	5885.49	0.5	5885.61	0.013	0.31	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 2	133.22	5885.48	0.6	5886.28	0.013	0.13	0.68	CIRCULAR	18.00 in	18.00 in
PIPE 2-1	27.37	5886.29	0.6	5886.45	0.013	0.38	0.44	CIRCULAR	18.00 in	18.00 in
PIPE 1	20.00	5886.75	0.6	5886.87	0.013	0.05	0.84	CIRCULAR	18.00 in	18.00 in
PIPE 8	5.36	5883.72	10.1	5884.26	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 10	24.00	5881.67	0.5	5881.79	0.013	1.19	0.00	CIRCULAR	24.00 in	24.00 in
PIPE 11	20.99	5882.17	0.5	5882.27	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity		Critical Flow		Normal Flow						
Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
PIPE 12	41.13	8.38	21.96	7.48	18.50	9.07	1.40	Supercritical	28.80	0.00	
PIPE 9	29.08	5.92	18.54	6.50	18.70	6.43	0.98	Subcritical	20.70	0.00	
PIPE 9-1	29.08	5.92	18.54	6.50	18.70	6.43	0.98	Subcritical	20.70	0.00	
PIPE 7	29.08	5.92	18.17	6.40	18.22	6.38	0.99	Subcritical	19.90	0.00	
PIPE 7-1	29.08	5.92	18.17	6.40	18.22	6.38	0.99	Subcritical	19.90	0.00	
PIPE 7-2	29.08	5.92	18.17	6.40	18.22	6.38	0.99	Subcritical	19.90	0.00	
PIPE 6	7.45	4.21	12.29	5.45	13.87	4.79	0.78	Subcritical	7.00	0.00	
PIPE 5	7.45	4.21	10.64	4.87	11.22	4.58	0.90	Subcritical	5.30	0.00	
PIPE 4	16.04	5.11	15.81	6.10	16.77	5.72	0.89	Subcritical	13.40	0.00	
PIPE 3	7.45	4.21	9.77	4.59	10.09	4.41	0.94	Subcritical	4.50	0.00	
PIPE 2	8.16	4.62	12.98	5.72	14.09	5.26	0.85	Subcritical	7.80	0.00	
PIPE 2-1	8.16	4.62	12.98	5.72	14.09	5.26	0.85	Pressurized	7.80	27.37	
PIPE 1	8.16	4.62	11.83	5.28	12.14	5.13	0.95	Subcritical Surcharged	6.50	9.39	
PIPE 8	33.47	18.94	4.70	3.00	2.24	8.71	4.30	Supercritical	1.10	0.00	
PIPE 10	16.05	5.11	11.76	4.96	11.63	5.04	1.02	Pressurized	7.60	24.00	
PIPE 11	7.45	4.21	5.32	3.21	5.29	3.23	1.01	Pressurized	1.40	20.99	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft^2)	Comment
PIPE 12	28.80	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 9	20.70	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 9-1	20.70	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 7	19.90	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 7-1	19.90	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 7-2	19.90	CIRCULAR	30.00 in	30.00 in	27.00 in	27.00 in	30.00 in	30.00 in	4.91	
PIPE 6	7.00	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 5	5.30	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 4	13.40	CIRCULAR	24.00 in	24.00 in	24.00 in	24.00 in	24.00 in	24.00 in	3.14	
PIPE 3	4.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 2	7.80	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 2-1	7.80	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 1	6.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 8	1.10	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 10	7.60	CIRCULAR	24.00 in	24.00 in	21.00 in	21.00 in	24.00 in	24.00 in	3.14	
PIPE 11	1.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.

- All hydraulics were calculated using the 'Used' parameters.
-

Grade Line Summary:

Tailwater Elevation (ft): 0.00

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
PIPE 12	5880.19	5881.17	0.00	0.00	5881.73	5883.00	5883.00	0.87	5883.87
PIPE 9	5881.47	5882.04	0.01	0.26	5883.86	5884.04	5884.14	0.27	5884.42
PIPE 9-1	5882.34	5882.72	0.07	0.13	5884.24	5884.36	5884.65	0.28	5884.93
PIPE 7	5883.02	5883.57	0.01	0.02	5884.53	5885.09	5885.17	0.55	5885.72
PIPE 7-1	5883.57	5883.68	0.05	0.11	5885.51	5885.54	5885.88	0.06	5885.94
PIPE 7-2	5883.68	5883.73	0.05	0.11	5885.78	5885.79	5886.10	0.02	5886.12
PIPE 6	5884.73	5884.78	0.32	0.00	5886.19	5886.23	5886.44	0.04	5886.48
PIPE 5	5885.08	5885.16	0.01	0.13	5886.46	5886.49	5886.61	0.04	5886.65
PIPE 4	5884.23	5884.98	0.01	0.00	5885.81	5886.35	5886.20	0.68	5886.88
PIPE 3	5885.49	5885.61	0.03	0.00	5886.79	5886.82	5886.91	0.04	5886.96
PIPE 2	5885.48	5886.28	0.04	0.08	5886.56	5887.53	5887.07	0.84	5887.91
PIPE 2-1	5886.29	5886.45	0.11	0.17	5887.89	5888.04	5888.19	0.15	5888.34
PIPE 1	5886.75	5886.87	0.01	0.13	5888.27	5888.34	5888.48	0.07	5888.55
PIPE 8	5883.72	5884.26	0.01	0.00	5884.37	5885.06	5885.08	0.00	5885.08

PIPE 10	5881.67	5881.79	0.11	0.00	5883.89	5883.91	5883.98	0.03	5884.00
PIPE 11	5882.17	5882.27	0.01	0.00	5883.87	5883.88	5883.88	0.00	5883.89

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
 - Bend loss = Bend K * $V_{fi}^2 / (2*g)$
 - Lateral loss = $V_{fo}^2 / (2*g)$ - Junction Loss K * $V_{fi}^2 / (2*g)$.
 - Friction loss is always Upstream EGL - Downstream EGL.
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Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
PIPE 12	98.50	3.50	6.00	6.08	0.00	0.79	0.00	20.00	11.54	7.96	225.12	Sewer Too Shallow
PIPE 9	113.45	3.50	6.00	6.08	19.39	11.24	7.66	20.88	11.98	8.40	504.83	
PIPE 9-1	76.79	3.50	6.00	6.08	20.29	11.69	8.10	21.88	12.48	8.90	369.51	
PIPE 7	110.00	3.50	6.00	6.08	21.28	12.18	8.60	23.36	13.22	9.64	584.41	
PIPE 7-1	21.99	3.50	6.00	6.08	23.36	13.22	9.64	23.14	13.11	9.53	125.24	
PIPE 7-2	10.00	3.50	6.00	6.08	23.14	13.11	9.53	24.40	13.74	10.16	59.25	
PIPE 6	10.00	2.50	4.00	4.92	23.40	12.49	10.24	23.62	12.60	10.35	54.86	
PIPE 5	16.00	2.50	4.00	4.92	23.02	12.30	10.05	24.18	12.88	10.63	88.45	

PIPE 4	150.32	3.00	4.00	5.50	23.90	13.03	10.20	27.42	14.79	11.96	996.14	
PIPE 3	25.00	2.50	4.00	4.92	26.91	14.25	12.00	28.28	14.93	12.68	185.58	
PIPE 2	133.22	2.50	4.00	4.92	26.92	14.25	12.00	28.94	15.26	13.01	1012.49	
PIPE 2-1	27.37	2.50	4.00	4.92	28.93	15.26	13.01	29.86	15.72	13.47	229.09	
PIPE 1	20.00	2.50	4.00	4.92	29.26	15.42	13.17	29.76	15.67	13.42	168.64	
PIPE 8	5.36	2.50	4.00	4.92	20.88	11.23	8.98	20.58	11.08	8.83	23.30	
PIPE 10	24.00	3.00	4.00	5.50	19.50	10.83	8.00	23.42	12.79	9.96	115.21	
PIPE 11	20.99	2.50	4.00	4.92	19.01	10.30	8.05	18.54	10.06	7.81	76.24	

Total earth volume for sewer trenches = 4818 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

System Input Summary

5 – YEAR HGL CALCS

Rainfall Parameters

Rainfall Return Period: 5

Rainfall Calculation Method: Formula

One Hour Depth (in):

Rainfall Constant "A": 28.5

Rainfall Constant "B": 10

Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20

Maximum Rural Overland Len. (ft): 500

Maximum Urban Overland Len. (ft): 300

Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00

Maximum Depth to Rise Ratio: 0.90

Maximum Flow Velocity (fps): 18.0

Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 0.00

Manhole Input Summary:

Manhole Output Summary:

	Local Contribution					Total Design Flow					
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment	
OUTFALL 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
PIPE 12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	16.00	Surface Water Present (Downstream)	
PIPE 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	10.60		
PIPE 9-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	10.60		
PIPE 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	10.20		
PIPE 7-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	10.20		
PIPE 7-2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	10.20		
PIPE 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.60		
PIPE 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.70		
PIPE 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.90		
PIPE 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.30		
PIPE 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.00		
PIPE 2-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.00		
PIPE 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.30		
PIPE 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.50		
PIPE 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.90		
PIPE 11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.70		

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
PIPE 12	98.50	5880.19	1.0	5881.17	0.013	0.03	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 9	113.45	5881.47	0.5	5882.04	0.013	0.05	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 9-1	76.79	5882.34	0.5	5882.72	0.013	0.25	0.53	CIRCULAR	30.00 in	30.00 in
PIPE 7	110.00	5883.02	0.5	5883.57	0.013	0.05	1.00	CIRCULAR	30.00 in	30.00 in
PIPE 7-1	21.99	5883.57	0.5	5883.68	0.013	0.20	0.58	CIRCULAR	30.00 in	30.00 in
PIPE 7-2	10.00	5883.68	0.5	5883.73	0.013	0.20	0.58	CIRCULAR	30.00 in	30.00 in
PIPE 6	10.00	5884.73	0.5	5884.78	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 5	16.00	5885.08	0.5	5885.16	0.013	0.05	0.84	CIRCULAR	18.00 in	18.00 in
PIPE 4	150.32	5884.23	0.5	5884.98	0.013	0.05	1.00	CIRCULAR	24.00 in	24.00 in
PIPE 3	25.00	5885.49	0.5	5885.61	0.013	0.31	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 2	133.22	5885.48	0.6	5886.28	0.013	0.13	0.68	CIRCULAR	18.00 in	18.00 in
PIPE 2-1	27.37	5886.29	0.6	5886.45	0.013	0.38	0.44	CIRCULAR	18.00 in	18.00 in
PIPE 1	20.00	5886.75	0.6	5886.87	0.013	0.05	0.84	CIRCULAR	18.00 in	18.00 in
PIPE 8	5.36	5883.72	10.1	5884.26	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in
PIPE 10	24.00	5881.67	0.5	5881.79	0.013	1.19	0.00	CIRCULAR	24.00 in	24.00 in
PIPE 11	20.99	5882.17	0.5	5882.27	0.013	1.32	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity		Critical Flow		Normal Flow						
Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
PIPE 12	41.13	8.38	16.21	5.91	12.99	7.85	1.53	Supercritical	16.00	0.00	
PIPE 9	29.08	5.92	13.07	5.16	12.53	5.46	1.08	Supercritical	10.60	0.00	
PIPE 9-1	29.08	5.92	13.07	5.16	12.53	5.46	1.08	Supercritical	10.60	0.00	
PIPE 7	29.08	5.92	12.81	5.10	12.27	5.40	1.09	Supercritical	10.20	0.00	
PIPE 7-1	29.08	5.92	12.81	5.10	12.27	5.40	1.09	Supercritical	10.20	0.00	
PIPE 7-2	29.08	5.92	12.81	5.10	12.27	5.40	1.09	Supercritical	10.20	0.00	
PIPE 6	7.45	4.21	8.69	4.26	8.82	4.18	0.97	Subcritical	3.60	0.00	
PIPE 5	7.45	4.21	7.48	3.89	7.50	3.88	1.00	Subcritical	2.70	0.00	
PIPE 4	16.04	5.11	11.18	4.81	11.00	4.91	1.03	Supercritical	6.90	0.00	
PIPE 3	7.45	4.21	6.88	3.70	6.87	3.71	1.00	Supercritical	2.30	0.00	
PIPE 2	8.16	4.62	9.18	4.41	8.90	4.59	1.06	Supercritical	4.00	0.00	
PIPE 2-1	8.16	4.62	9.18	4.41	8.90	4.59	1.06	Supercritical	4.00	0.00	
PIPE 1	8.16	4.62	8.30	4.14	7.97	4.37	1.08	Supercritical	3.30	0.00	
PIPE 8	33.47	18.94	3.14	2.42	1.54	6.87	4.11	Supercritical	0.50	0.00	
PIPE 10	16.05	5.11	8.31	4.04	8.06	4.21	1.06	Supercritical	3.90	0.00	
PIPE 11	7.45	4.21	3.73	2.65	3.73	2.65	1.00	Subcritical	0.70	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft^2)	Comment
PIPE 12	16.00	CIRCULAR	30.00 in	30.00 in	24.00 in	24.00 in	30.00 in	30.00 in	4.91	
PIPE 9	10.60	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
PIPE 9-1	10.60	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
PIPE 7	10.20	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
PIPE 7-1	10.20	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
PIPE 7-2	10.20	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
PIPE 6	3.60	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 5	2.70	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 4	6.90	CIRCULAR	24.00 in	24.00 in	18.00 in	18.00 in	24.00 in	24.00 in	3.14	
PIPE 3	2.30	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 2	4.00	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 2-1	4.00	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 1	3.30	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 8	0.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
PIPE 10	3.90	CIRCULAR	24.00 in	24.00 in	18.00 in	18.00 in	24.00 in	24.00 in	3.14	
PIPE 11	0.70	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.

- All hydraulics were calculated using the 'Used' parameters.
-

Grade Line Summary:

Tailwater Elevation (ft): 0.00

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
PIPE 12	5880.19	5881.17	0.00	0.00	5881.27	5882.52	5882.23	0.84	5883.06
PIPE 9	5881.47	5882.04	0.00	0.09	5882.98	5883.13	5883.16	0.38	5883.54
PIPE 9-1	5882.34	5882.72	0.02	0.03	5883.38	5883.81	5883.84	0.38	5884.22
PIPE 7	5883.02	5883.57	0.00	0.01	5884.04	5884.64	5884.50	0.55	5885.04
PIPE 7-1	5883.57	5883.68	0.01	0.03	5884.81	5884.81	5885.08	0.07	5885.16
PIPE 7-2	5883.68	5883.73	0.01	0.03	5884.93	5884.93	5885.20	0.03	5885.23
PIPE 6	5884.73	5884.78	0.09	0.00	5885.45	5885.52	5885.74	0.05	5885.79
PIPE 5	5885.08	5885.16	0.00	0.03	5885.70	5885.79	5885.94	0.08	5886.02
PIPE 4	5884.23	5884.98	0.00	0.00	5885.15	5885.91	5885.52	0.75	5886.27
PIPE 3	5885.49	5885.61	0.01	0.00	5886.01	5886.18	5886.28	0.12	5886.40
PIPE 2	5885.48	5886.28	0.01	0.02	5886.22	5887.05	5886.55	0.80	5887.35
PIPE 2-1	5886.29	5886.45	0.03	0.04	5887.25	5887.25	5887.42	0.10	5887.52
PIPE 1	5886.75	5886.87	0.00	0.03	5887.41	5887.56	5887.71	0.12	5887.83
PIPE 8	5883.72	5884.26	0.00	0.00	5883.85	5884.52	5884.58	0.03	5884.61

PIPE 10	5881.67	5881.79	0.03	0.00	5883.05	5883.05	5883.09	0.01	5883.10
PIPE 11	5882.17	5882.27	0.00	0.00	5883.06	5883.06	5883.07	0.00	5883.07

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
 - Bend loss = Bend K * $V_{fi}^2 / (2*g)$
 - Lateral loss = $V_{fo}^2 / (2*g)$ - Junction Loss K * $V_{fi}^2 / (2*g)$.
 - Friction loss is always Upstream EGL - Downstream EGL.
-

Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

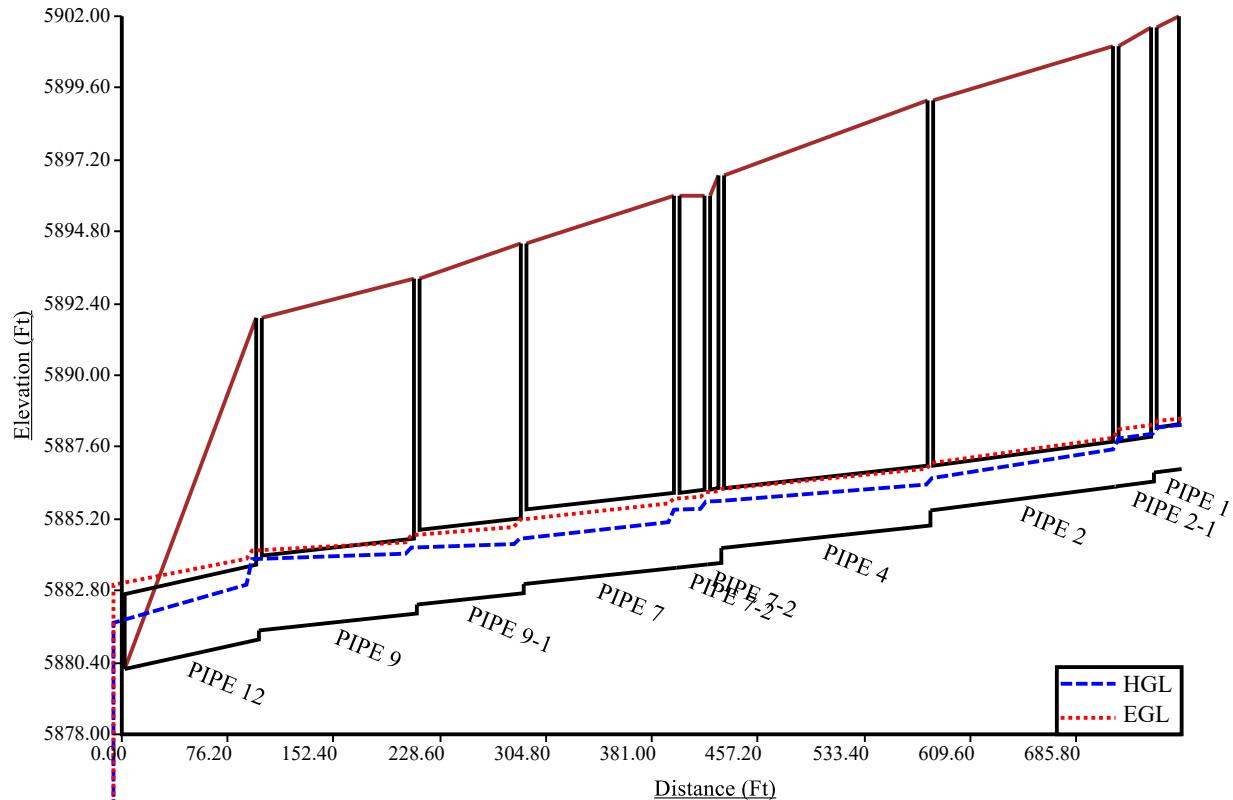
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
PIPE 12	98.50	3.50	6.00	6.08	0.00	0.79	0.00	20.00	11.54	7.96	225.12	Sewer Too Shallow
PIPE 9	113.45	3.50	6.00	6.08	19.39	11.24	7.66	20.88	11.98	8.40	504.83	
PIPE 9-1	76.79	3.50	6.00	6.08	20.29	11.69	8.10	21.88	12.48	8.90	369.51	
PIPE 7	110.00	3.50	6.00	6.08	21.28	12.18	8.60	23.36	13.22	9.64	584.41	
PIPE 7-1	21.99	3.50	6.00	6.08	23.36	13.22	9.64	23.14	13.11	9.53	125.24	
PIPE 7-2	10.00	3.50	6.00	6.08	23.14	13.11	9.53	24.40	13.74	10.16	59.25	
PIPE 6	10.00	2.50	4.00	4.92	23.40	12.49	10.24	23.62	12.60	10.35	54.86	
PIPE 5	16.00	2.50	4.00	4.92	23.02	12.30	10.05	24.18	12.88	10.63	88.45	

PIPE 4	150.32	3.00	4.00	5.50	23.90	13.03	10.20	27.42	14.79	11.96	996.14	
PIPE 3	25.00	2.50	4.00	4.92	26.91	14.25	12.00	28.28	14.93	12.68	185.58	
PIPE 2	133.22	2.50	4.00	4.92	26.92	14.25	12.00	28.94	15.26	13.01	1012.49	
PIPE 2-1	27.37	2.50	4.00	4.92	28.93	15.26	13.01	29.86	15.72	13.47	229.09	
PIPE 1	20.00	2.50	4.00	4.92	29.26	15.42	13.17	29.76	15.67	13.42	168.64	
PIPE 8	5.36	2.50	4.00	4.92	20.88	11.23	8.98	20.58	11.08	8.83	23.30	
PIPE 10	24.00	3.00	4.00	5.50	19.50	10.83	8.00	23.42	12.79	9.96	115.21	
PIPE 11	20.99	2.50	4.00	4.92	19.01	10.30	8.05	18.54	10.06	7.81	76.24	

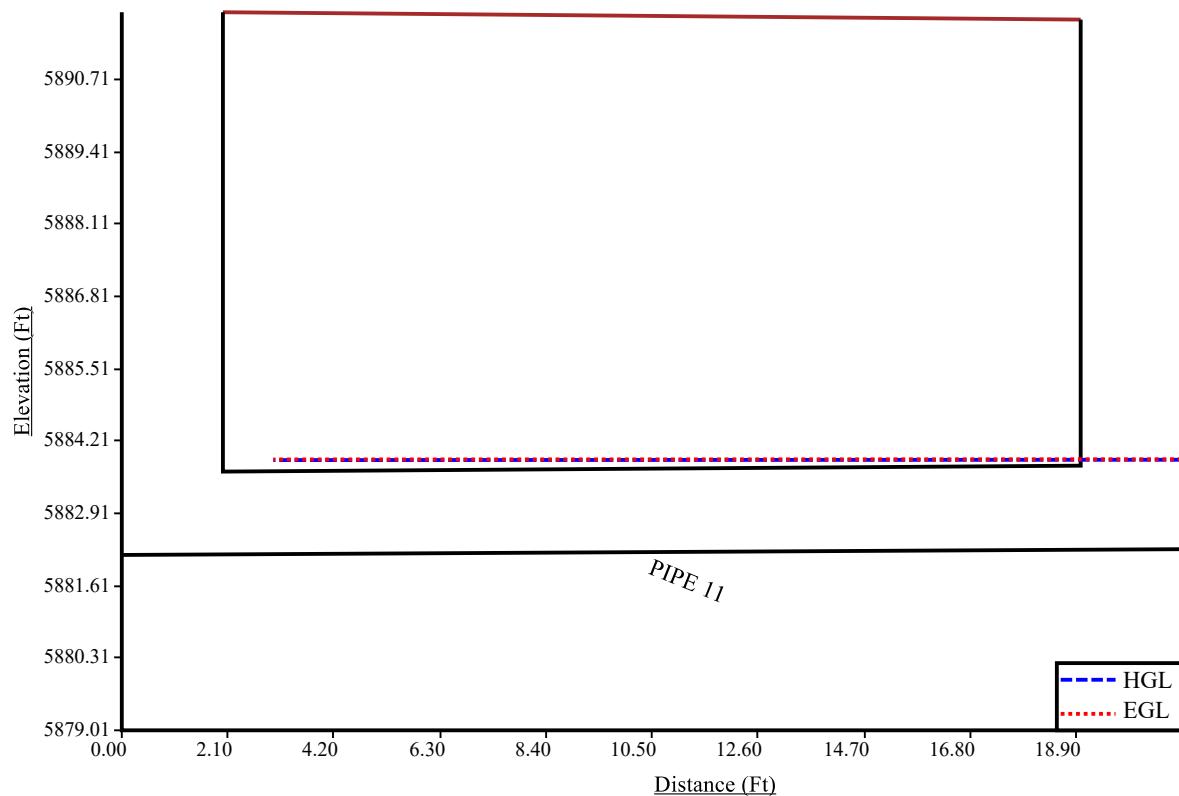
Total earth volume for sewer trenches = 4818 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

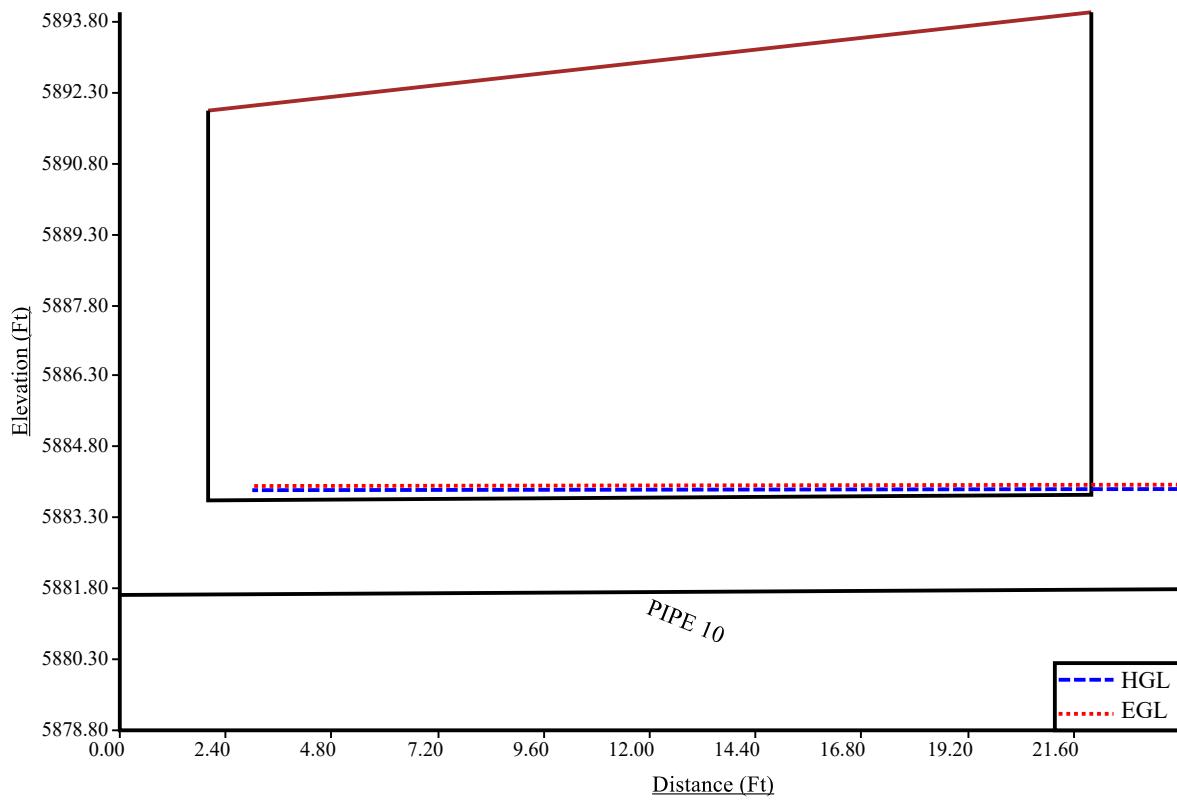
MAIN



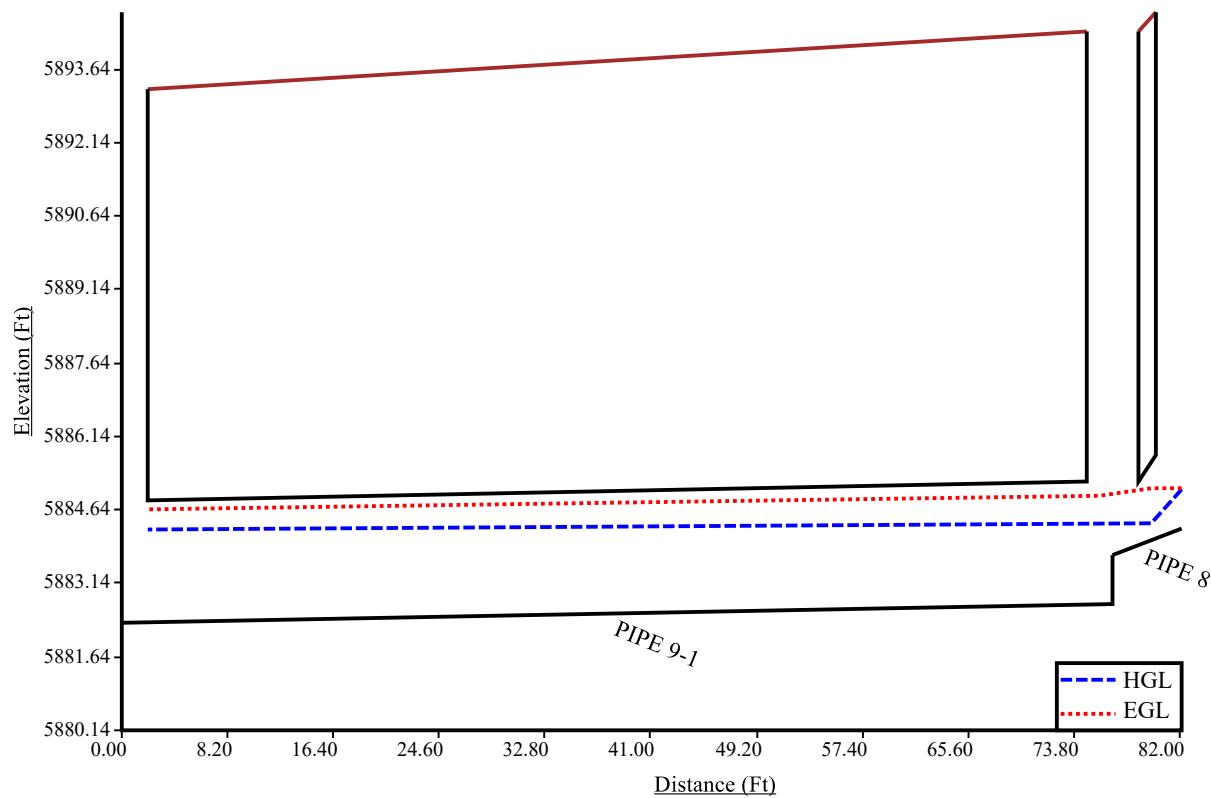
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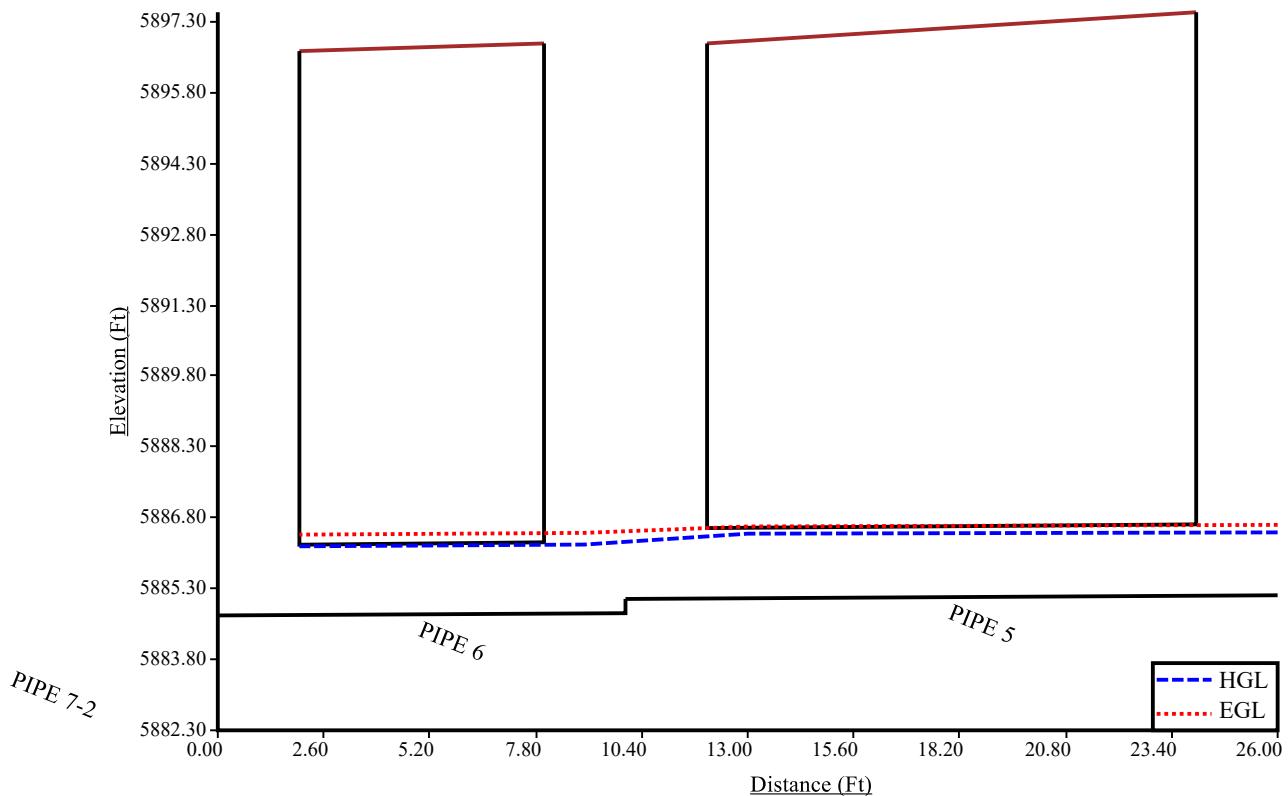
LATB-2-100YR



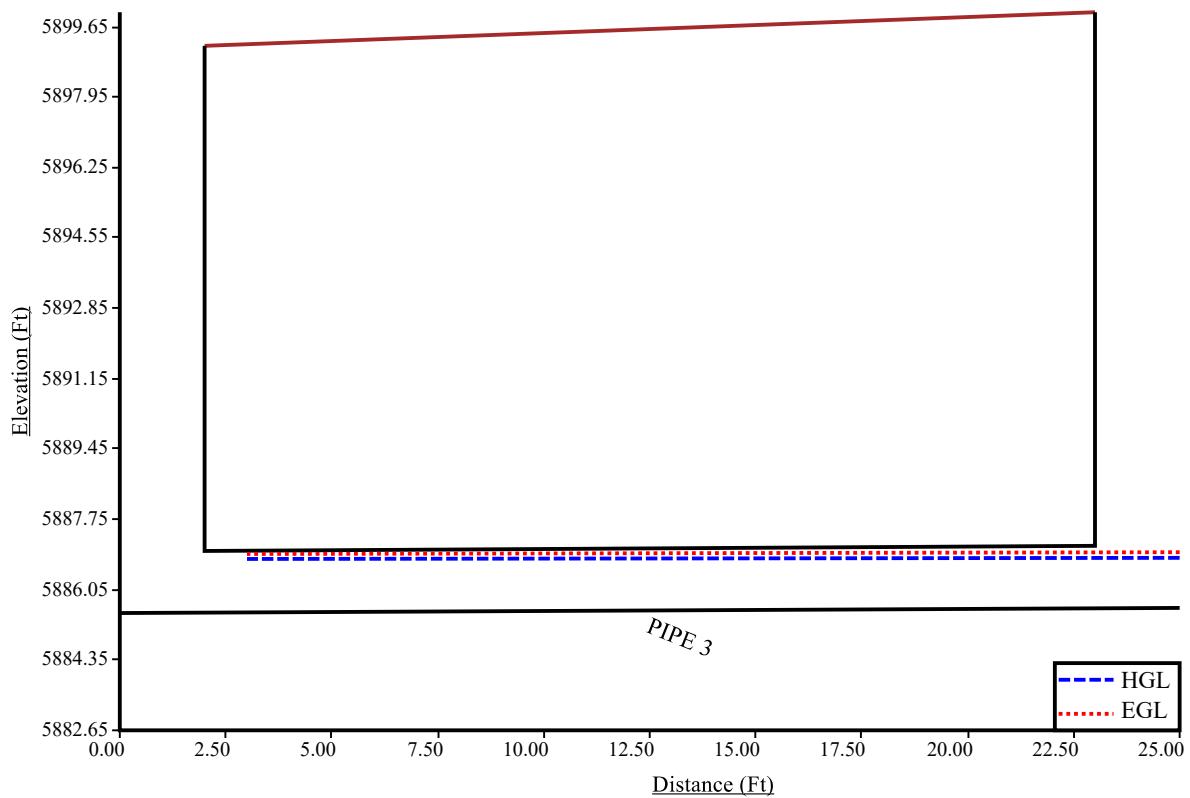
LAT C



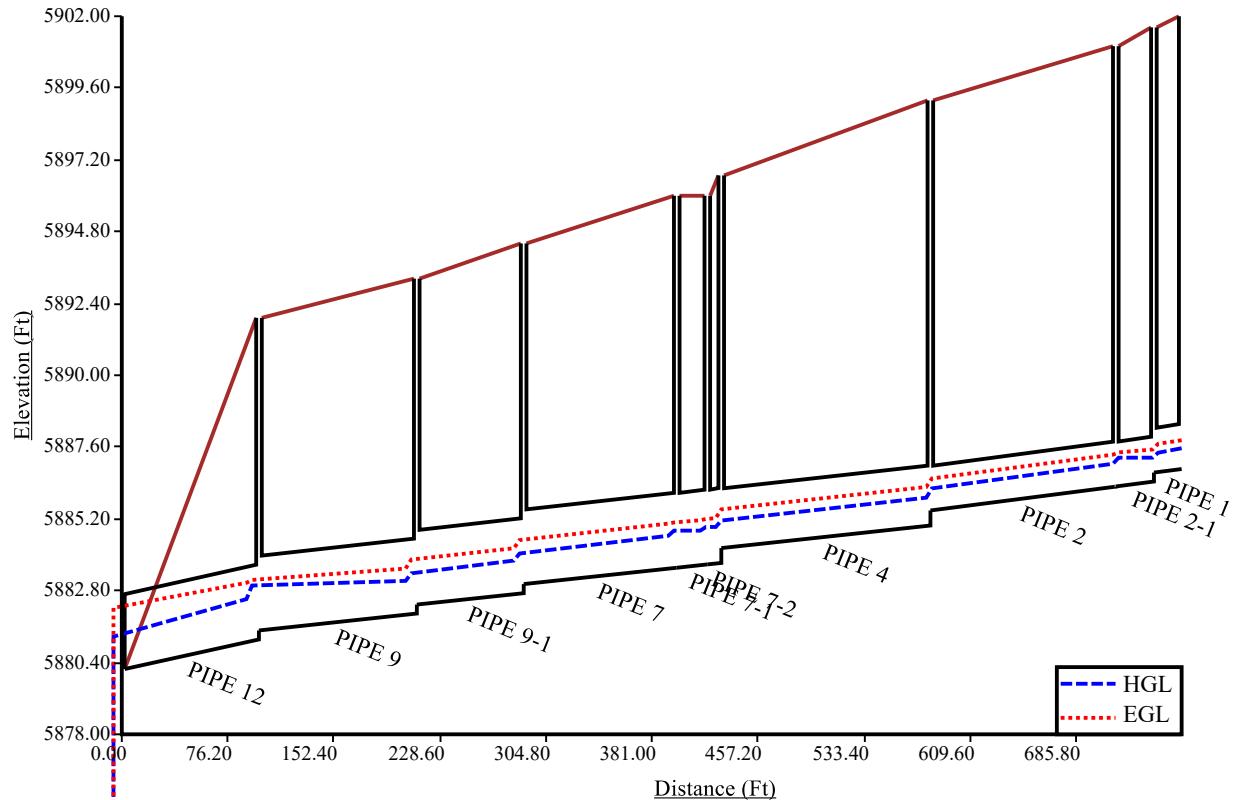
LAT D



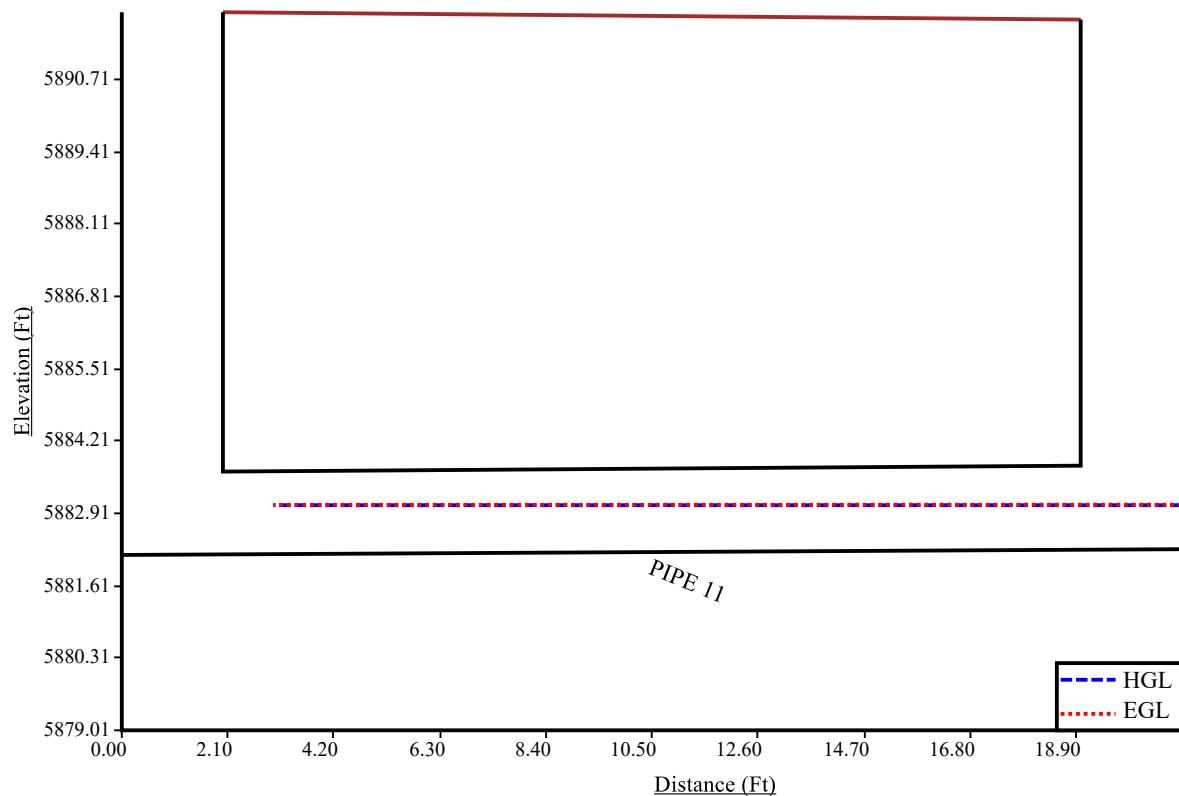
LAT E



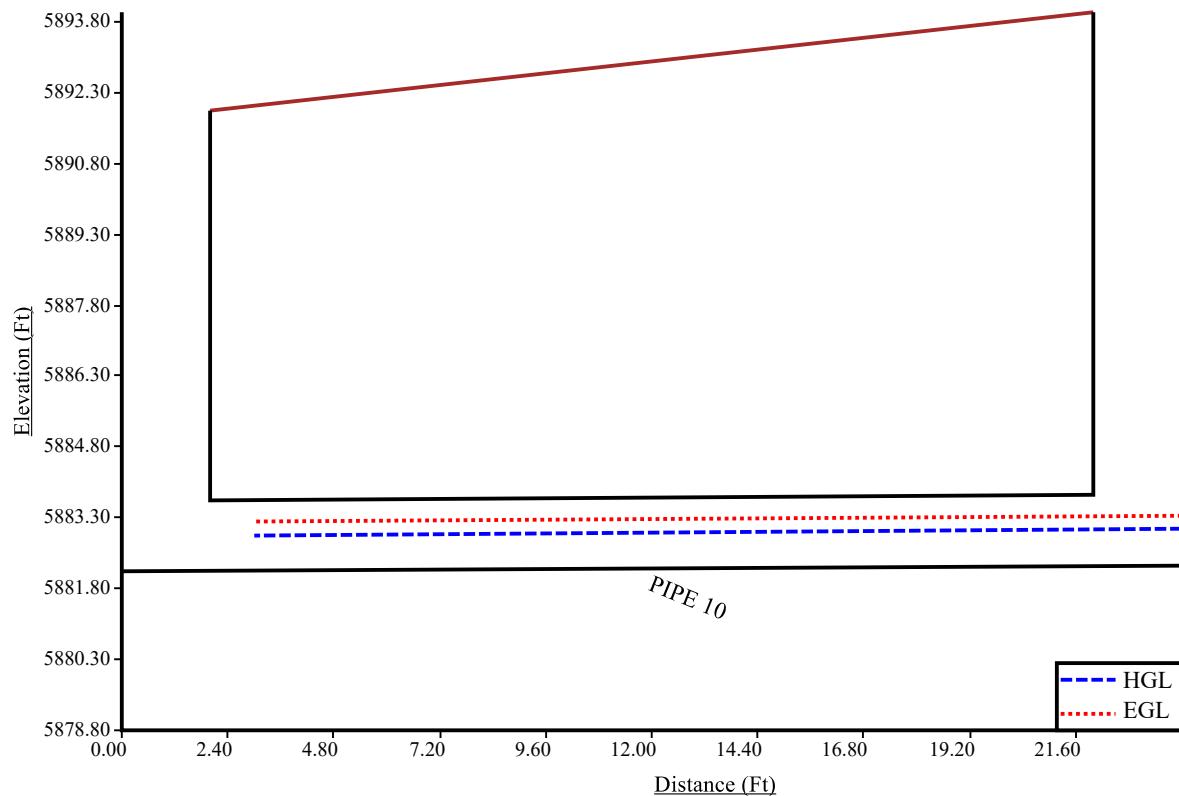
MAIN-5YR



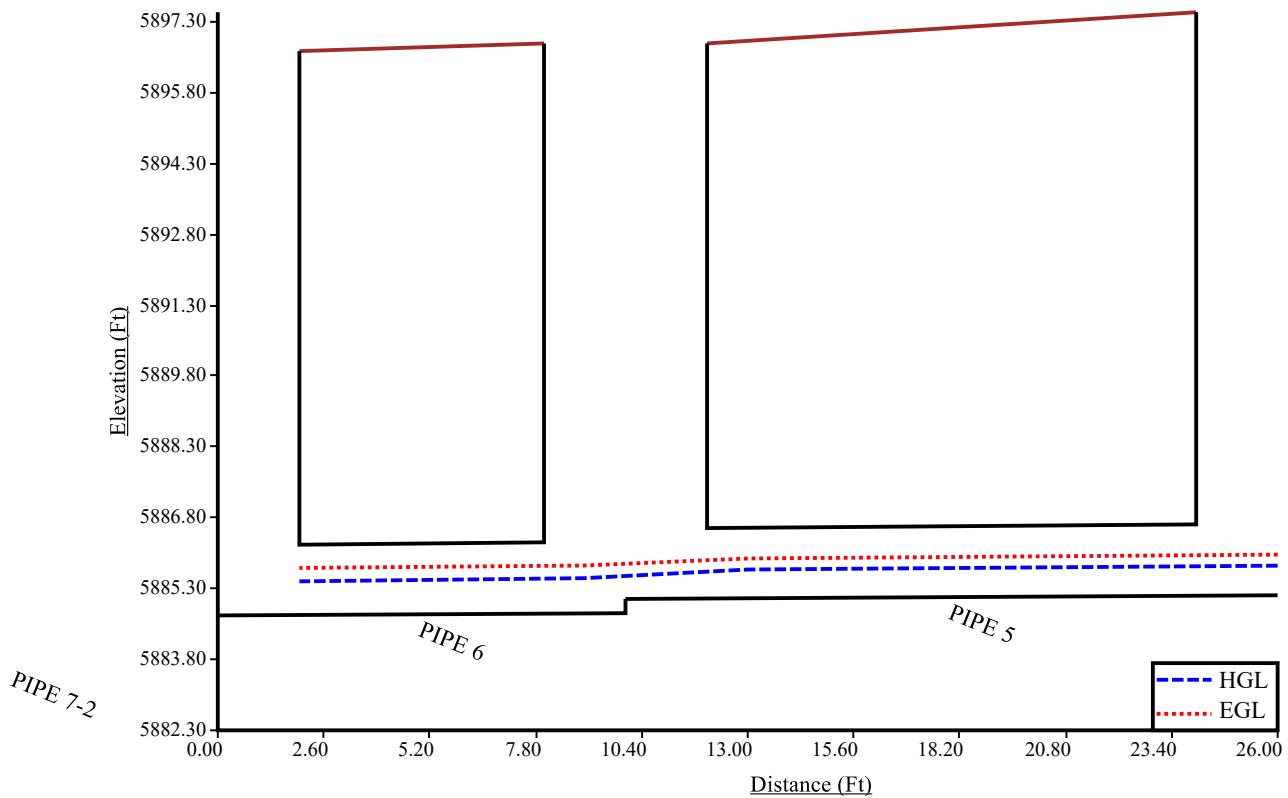
B-1-5YR



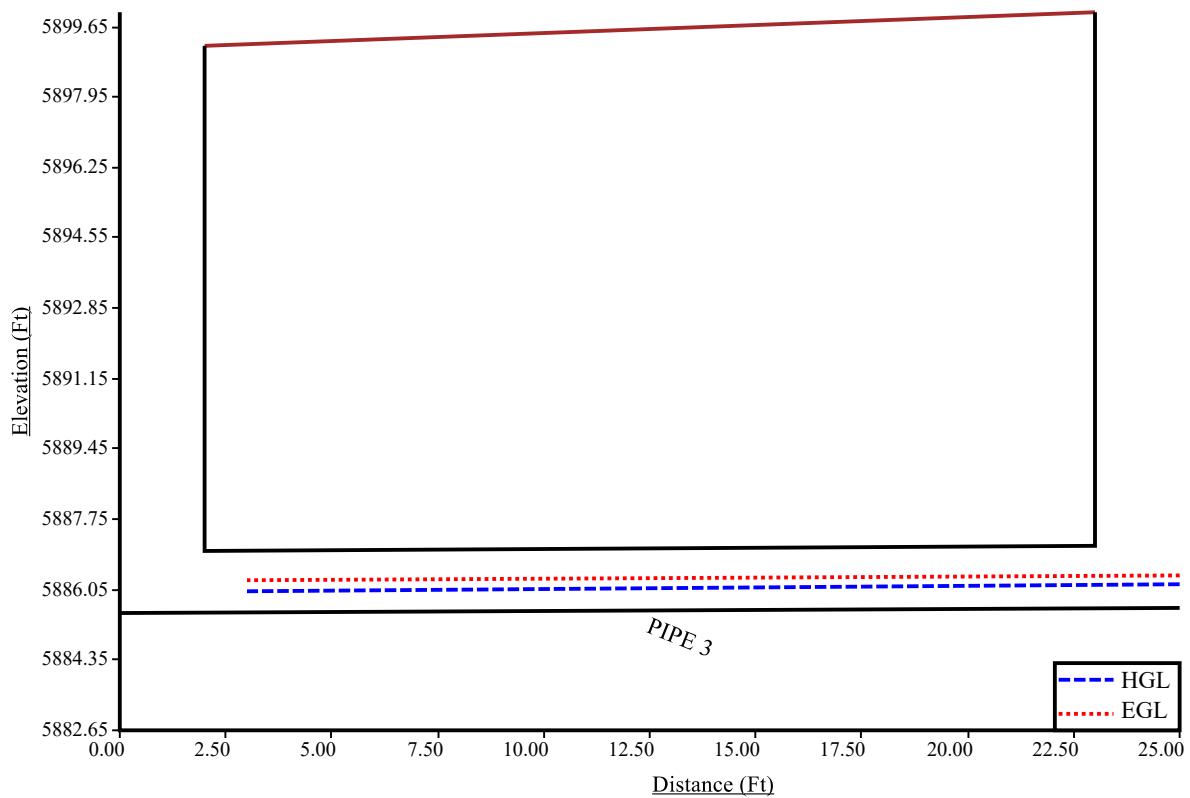
B-2-5YR



D-5YR




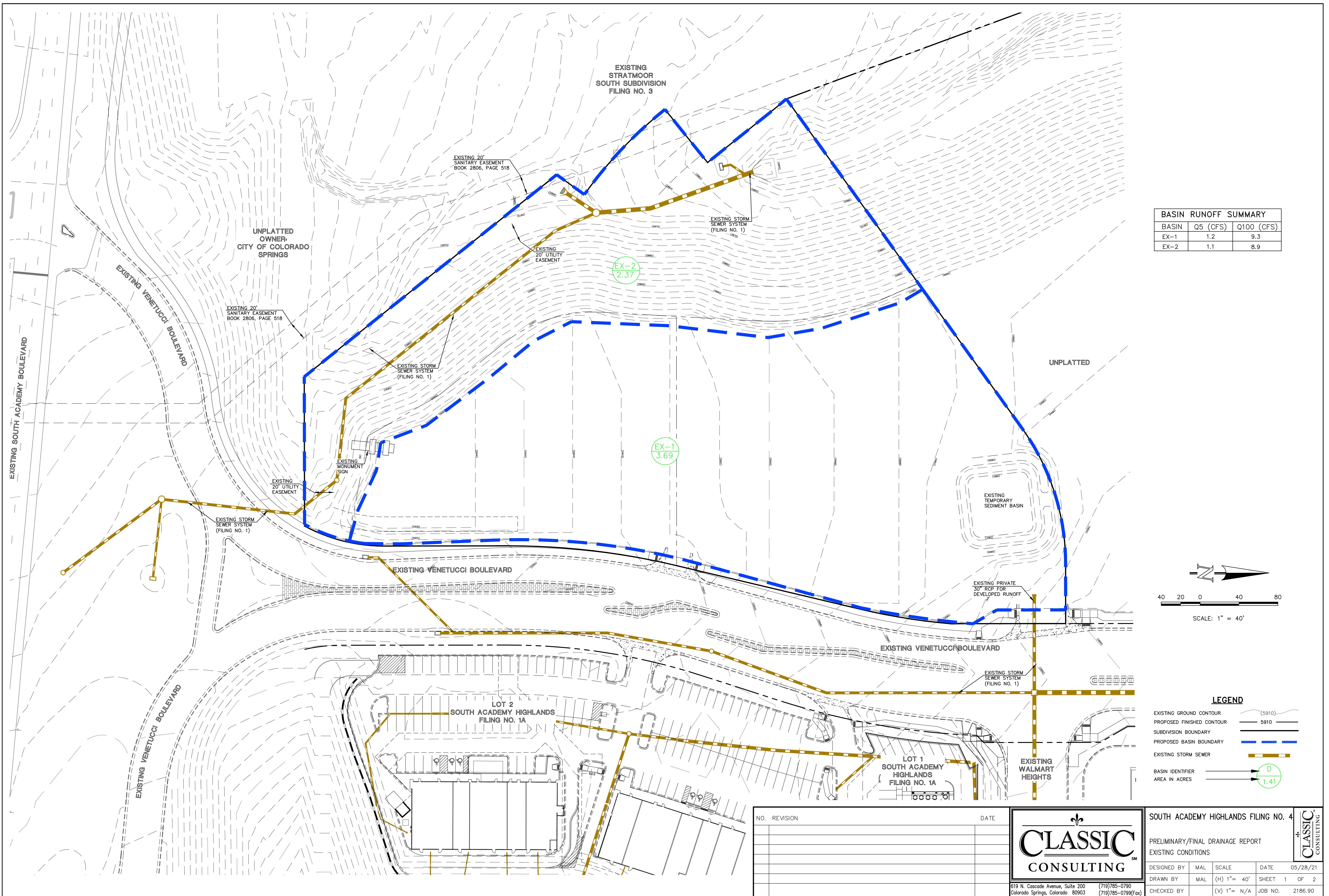
E-5YR



DRAINAGE MAPS







STORM SYSTEM NOTES:

ALL PROPOSED STORM SEWER IS REINFORCED CONCRETE PIPE (RCP) AND PRIVATE WITH A CONNECTION TO THE PRIVATE STORM MAIN IN VENETUCCI BLVD

FULL SPECTRUM DETENTION AND STORM WATER QUALITY FOR THE PROPOSED SITE IS PROVIDED AT THE DOWNSTREAM PRIVATE FACILITY REFERRED TO AS SOUTH ACADEMY HIGHLANDS FILING NO. 1 FACILITY 'T'.

ALL INLETS ARE PRIVATE CDOT TYPE R CURB INLETS.

BASIN RUNOFF SUMMARY		
BASIN	Q5 (CFS)	Q100 (CFS)
A	0.2	0.5
B	0.7	1.4
C	3.9	7.6
D	0.6	1.1
E	0.8	1.6
F	2.7	5.3
G	0.7	1.3
H	0.7	1.3
J	2.3	4.5
K	3.3	6.5
Q	0.8	6.2

DESIGN POINT SUMMARY			
DESIGN POINT	Q5 (CFS)	Q100 (CFS)	OUTFALL
1	3.3	6.5	18" STUB
2	0.7	1.3	10' TYPE R (A-G)
3	2.3	4.5	18" STUB
4	0.6	1.3	5' TYPE R (A-G)
5	2.7	5.3	18" STUB
6	0.9	1.7	10' TYPE R (A-G)
7	0.5	1.1	5' TYPE R (A-G)
8	3.9	7.6	18" STUB
9	0.7	1.4	10' TYPE R (A-G)
10	0.2	0.5	SURFACE

PIPE RUN SUMMARY			
PIPE	Q5 (CFS)	Q100 (CFS)	SIZE
1	3.3	6.5	18"
2	4.0	7.8	18"
3	2.3	4.5	18"
4	6.9	13.4	24"
5	2.7	5.3	18"
6	3.6	7.0	18"
7	10.2	19.9	30"
8	0.5	1.1	18"
9	10.6	20.7	30"
10	3.9	7.6	24"
11	0.7	1.4	18"
12	14.8	28.8	30"

SCALE: 1" = 40'
