March 28, 2018



ENTECH ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

Hammers Construction 1411 Woolsey Heights Colorado Springs, CO 80915

Attn: Zack Crabtree

Re: Soil, Geology and Geologic Hazard Evaluation

Big O Tires

6985 Meridian Road Falcon, Colorado Add "PCD File No. SF-18-003" Unresolved

Provide evaluation/recommendation for the foundation preparation and

Unresolved. See DCM Chapter 11 Section 11.3.3.

embankment construction for the permanent detention facility.

Dear Mr. Butler:

As requested, personnel of Entech Engineering, Inc. have investigated the above referenced site to evaluate the conditions with respect to geology and geologic hazards affecting development of the site. The subsurface soil conditions were previously investigated by Entech Engineering, Inc. in a Subsurface Soil Investigation, October 20, 2017 (Reference 1). This investigation is not intended to be a complete Soil and Geology Study that satisfies the El Paso County Land Development Code.

The project consists of commercial development on a 1.2-acre site. The site lies in El Paso County, Colorado, in the southern portion of Falcon, Colorado. The approximate location of the site is shown on the Vicinity Location Map, Figure 1.

The topography of the site is generally flat. No major drainages exist on the site. The site lies in portions of Sections 7 and 12, Township 13 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado. Currently several commercial buildings exist on the site with a gravel parking area. It is our understanding the existing structures are to be removed and a new 4,710 square-foot auto service building with a 1,120 square-foot retail/sales building will be constructed. The Site Plan is presented in Figure 2.

Two test borings were drilled on the site to evaluate the subsurface soil conditions. The Test Boring logs are included in Appendix A. Laboratory Test Results are summarized in Table 1 and included in Appendix B. Information from this report was used evaluating the site.

The scope of this report will include a geologic analysis evaluation of the site utilizing published geologic data, available subsurface soils information and site-specific mapping of major geologic features, and identification of geologic hazards with respect to the development with recommended mitigation techniques. The Natural Resource Conservation Service (NRCS), previously the Soil Conservation Service (SCS) Survey was also reviewed to evaluate the site.

SOIL AND GEOLOGIC CONDITIONS

Soil Survey

The Natural Resource Conservation Service (NRCS) (Reference 2, Figure 3), previously the Soil Conservation Service (Reference 3) has mapped one soil type on the site. Complete

description of the soils is presented in Appendix C. In general, the soils consist of gravelly sandy, loam. The soils are described as follows:

Type Description
Columbine gravelly sand loam, 0-3% slopes

Soils

The soils encountered in the test borings from Subsurface Soil Investigation (Reference 1) consisted of three feet of silty sand fill and slightly to silty native sand overlying silty sandstone. The upper soils were encountered as very loose to loose states and moist conditions. The soils are considered to have low expansion potential.

Groundwater

Groundwater was encountered at 10 to 10.5 feet the test borings drilled on this site (Reference 1). It is anticipated groundwater will not affect shallow foundations on site with no basement construction. Fluctuations in groundwater conditions may occur due to variations in rainfall or other factors not readily apparent at this time. Isolated sand layers within the soil profile can carry water in the subsurface. Contractors should be cognizant of the potential for the occurrence of subsurface water features during construction.

Geology

Approximately 16 miles west of the site is a major structural feature known as the Rampart Range Fault. This fault marks the boundary between the Great Plains Physiographic Province and the Southern Rocky Mountain Province. The site exists within a large structural feature known as the Denver Basin. Bedrock in the area is typically gently dipping in a northwesterly direction. The bedrock underlying the site consists of the Black Squirrel Formation of Cretaceous Age. The Black Squirrel Formation typically consists of coarse-grained arkosic sandstone with interbedded layers of fine-grained sandstone, siltstone or claystone.

The geology of the site was evaluated using the *Geologic Map of the Falcon Quadrangle*, by Morgan and White in 2012, (Reference 4, Figure 4). The Geology for the site is indicated in Figure 2. One mappable unit was identified on this site which, is as follows:

Tbs Black Squirrel Formation of Tertiary Age: The Black Squirrel Formation typically consists of arkosic sandstone with interbedded fine-grained sandstone, siltstone and claystone. Overlying this formation is a variable layer of residual soil. The residual soils were derived from the in-situ weathering of the bedrock

materials on-site. These soils consisted of silty sands and may contain layers of sandy clays.

ENGINEERING GEOLOGIC HAZARDS

Mapping has been performed on this site to identify areas where various geologic conditions exist of which developers should be cognizant during the planning, design and construction stages should new construction be proposed. The engineering geologic hazards identified on this site include artificial fill and loose soils. These hazards and recommended mitigation techniques are discussed as follows:

Artificial Fill

Up to three feet of fill was encountered in one of the borings test drilled on site. Fill likely exists associated with the existing buildings, as well.

<u>Mitigation</u>: It is anticipated the fill will be removed during site grading. The old fill and debris from the existing buildings should be completely removed. All old formation remnants and utilities should be completely removed. Any uncontrolled fill encountered beneath new foundations should be removed and recompacted at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557.

Loose Soils

Loose to very loose soils were encountered in borings drilled on site (Reference 1). Loose soils encountered beneath the foundation or floor slabs will require mitigation.

<u>Mitigation</u>: Should loose soils be encountered beneath any new foundations or floor slabs, mitigation will be necessary. Overexcavation and recompaction at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 is a suitable mitigation, which is common in the area. An overexcavation depth of 2 to 3 feet is anticipated.

RELEVANCE OF GEOLOGIC CONDITIONS TO LAND USE PLANNING

As mentioned, the proposed development will be commercial. The existing buildings on the site are to be removed. The existing geologic and engineering geologic conditions will impose minor constraints on development and construction. The geologic conditions on the site include artificial fill and the loose soils, which can be satisfactorily mitigated through proper engineering design and construction practices. The site Subsurface Soil Investigation (Reference 1), was reviewed by the Colorado Geological Survey (CGS) February 19, 2018 (Reference 5). The CGS review letter is presented in Appendix D.

The upper granular soils encountered in the borings drilled on the site were encountered at loose to very loose states. Loose or collapsible soils, if encountered beneath foundation or floor

slabs, will require recompaction. Expansive layers may also be encountered in the soil on this site. Expansive soils, if encountered, will require special foundation design. These soils will not prohibit development.

Fill exists on this site that is likely associated with the existing buildings. All fill, debris, foundation remnants and utilities should be completely removed and prior to construction. Any uncontrolled fill encountered beneath new foundations and floor slabs will require removal and recompaction at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557.

Groundwater was encountered at 10 to 10.5 feet in the test borings. It is anticipated groundwater will not affect a shallow foundation with slab-on-grade construction and no basement construction. According to the Drainage Report by JPS Engineering, January 18, 2018, (Reference 6) the site should not be affected by any delineated 100-year FEMA floodplains.

In summary, the recompacted granular soils will likely provide suitable support for shallow foundations. The geologic conditions encountered on site can be mitigated with proper engineering and construction practices. Specific recommendations have been made in the Subsurface Soil Investigation (Reference 1).

CLOSURE

It should be pointed out that because of the nature of data obtained by random sampling of such variable nonhomogeneous materials as soil and rock, it is important that we be informed of any differences observed between surface and subsurface conditions encountered in construction and those assumed in the body of this report. Any new construction considered on this site will require additional investigation. Construction and design personnel should be made familiar with the contents of this report. Specific construction and foundation recommendations will be provided when investigations are completed for any new construction.

This report has been prepared for Hammers Construction for application to the proposed development in accordance with generally accepted geologic, soil and engineering practices. No other warranty expresses or implied is made.

We trust that this report has provided you with all the information that you required. Should you have any questions or require additional information, please do not hesitate to contact us.

Respectfully Submitted,

the la-Culm

ENTECH ENGINEERING, INC.

Reviewed by:

Kristen A. Andrew-Hoeser, P. G. Engineering Geologist

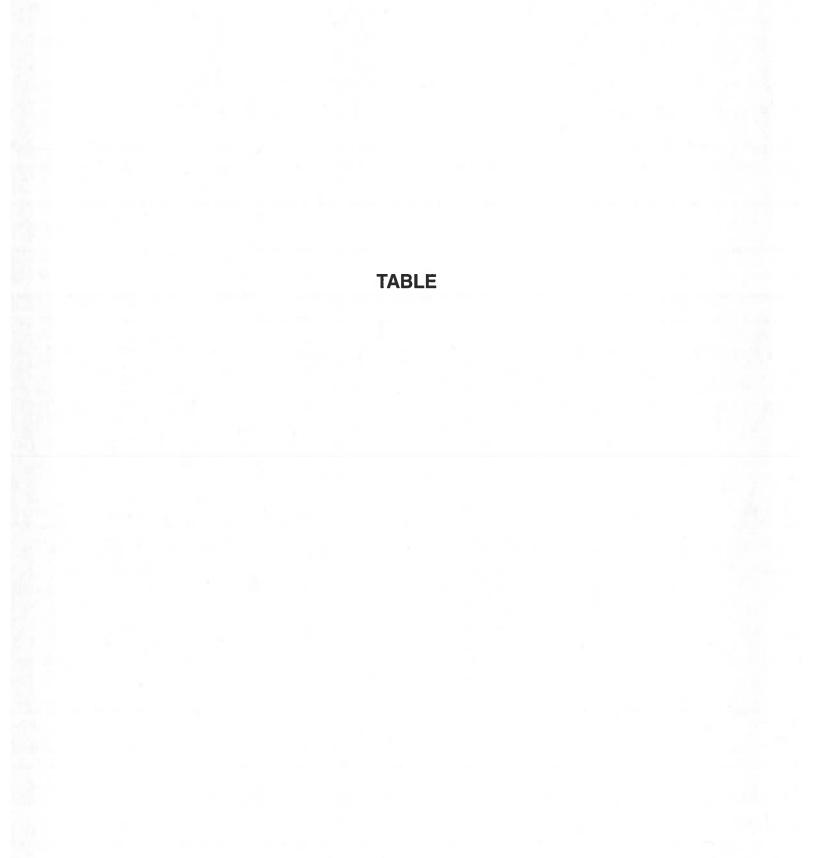
KAH/kc

Encl.

Entech Job No. 171206 2MSW/ltr/2017/171206sg&ghs Joseph C. Geode, Jr., P.E. President

BIBLIOGRAPHY

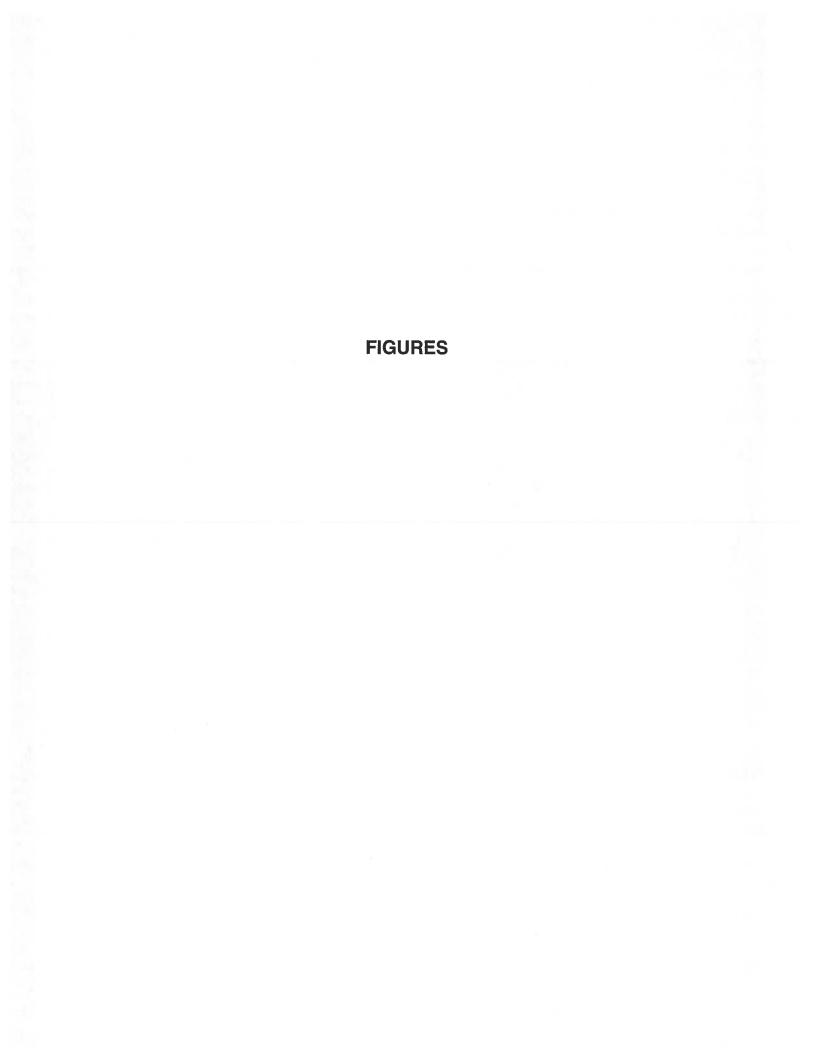
- 1. Entech Engineering, Inc. October 20, 2017. Subsurface Soil Investigation, Big O Tires, 6985 Meridian Road, Falcon, Colorado. Entech Job No. C5.12.019.
- 2. Natural Resources Conservation Service. September 23, 2016. *Web Soil Survey*. United States Department of Agriculture. http://websoilsurvey.sc.egov..usda.gov.
- 3. United States Department of Agriculture Soil Conservation Service. June, 1981. Soil Survey of El Paso County Area, Colorado.
- 4. Morgan, Matthew L. and White, Jonathan L. 2012. Falcon Quadranagle Geologic Map, El Paso County, Colorado. Colorado Geological Survey. Open-File Report 12-05.
- 5. Colorado Geological Survey. February 19, 2018. Largent Subdivision, File Number SF 183: El Paso County, CO: CGS Unique No. EP-18-0043.
- 6. JPS Engineering. January 18, 2018. *Final Drainage Report, Largent Subdivision, 6895 meridian Road.* JPS Project No. 091701.

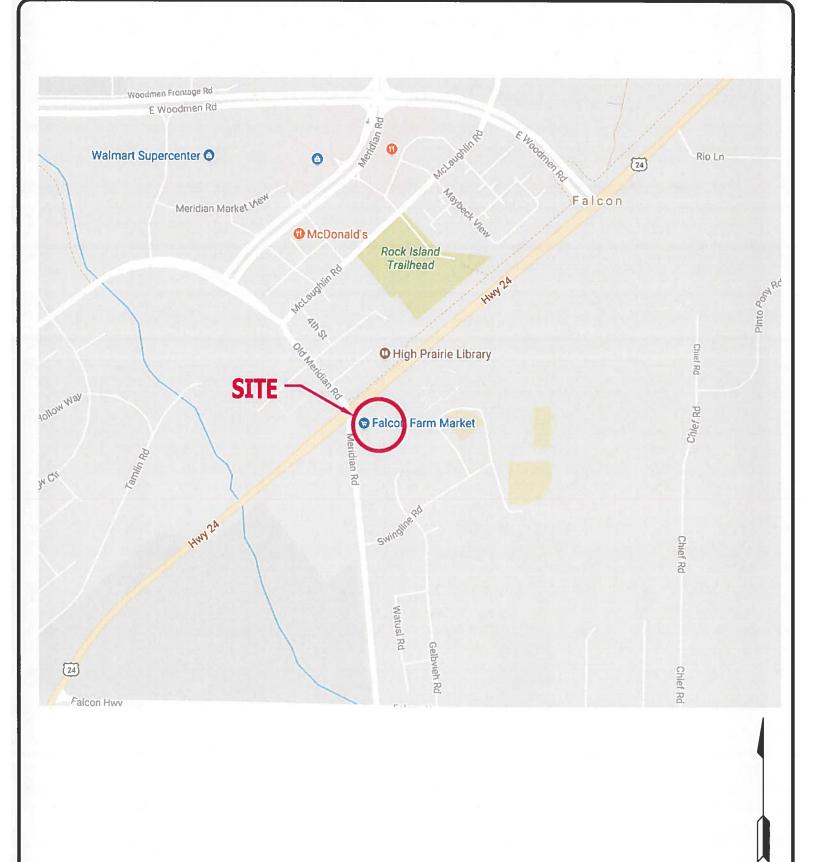


SUMMARY OF LABORATORY TEST RESULTS TABLE 1

HAMMERS CONSTRUCTION 6985 MERIDIAN ROAD 171206 CLIENT PROJECT JOB NO.

		_		_	_	
	SOIL DESCRIPTION	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SANDSTONE, SILTY	SAND, SILTY
	ONSOL UNIFIED (%) CLASSIFICATION	SM	WS-MS	SM	SM	SM
SWELL	CONSOL (%)		18		1 37 7 8	
FHA	SWELL (PSF)					
	SULFATE (WT %)	<0.01				<0.01
PLASTIC	INDEX (%)	NP				2
LIQUID	LIMIT (%)	NV				24
PASSING	NO. 200 SIEVE (%)	12.3	6.2	12.8	18.7	18.2
DRY	DENSITY (PCF)					
	DEPTH WATER (FT) (%)					0.00
	DEPTH (FT)	5	2	15	20	50
TEST	BORING NO.	1	2	2	1	2
	SOIL	1	1	1	2	1







VICINITY LOCATION MAP 6985 MERIDIAN ROAD FALCON, CO FOR: HAMMERS CONSTRUCTION

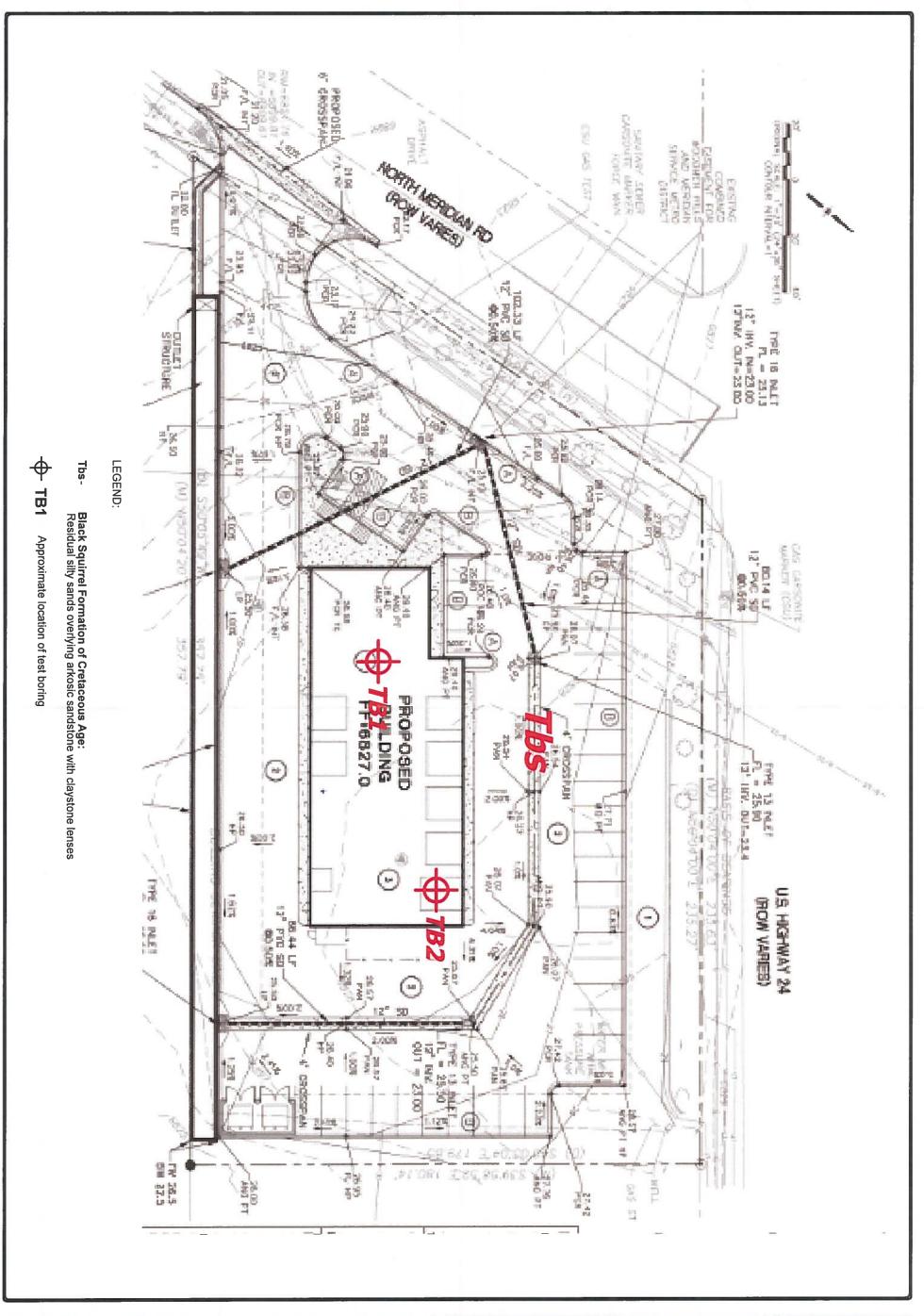
DRAWN BY:

DATE DRAWN: 09/29/17 DESIGNED BY: DS CHECKED:

JOB NO.: 171206 FIG. NO.:

N

1

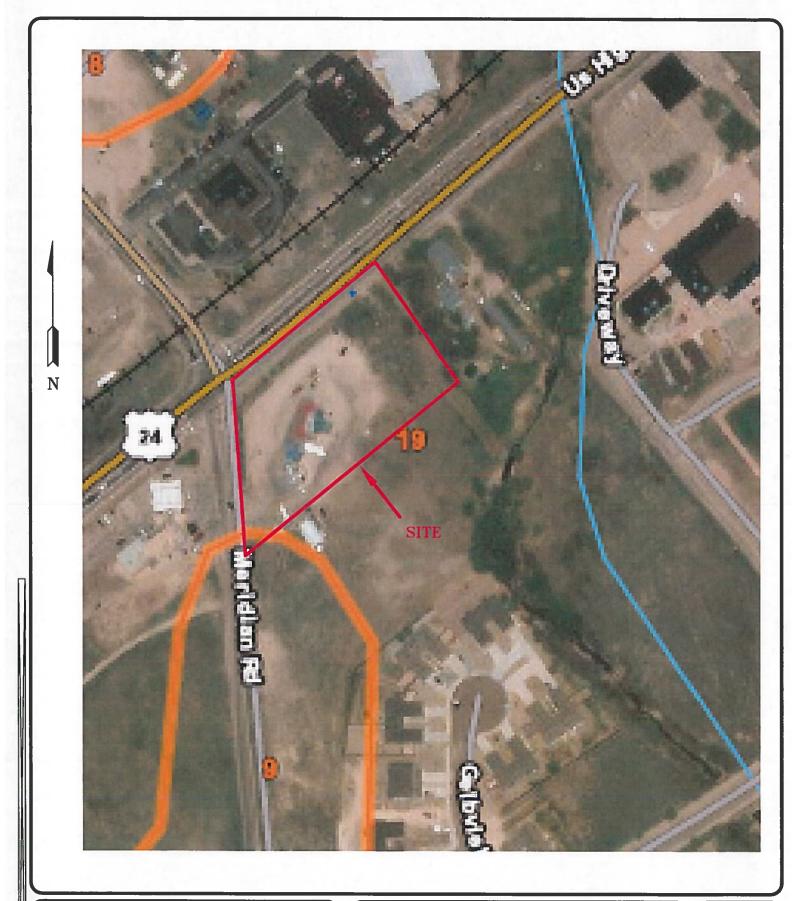




Site/Test Boring Location Map 6985 Meridian Road Colorado Springs, CO. For: Hammers Construction







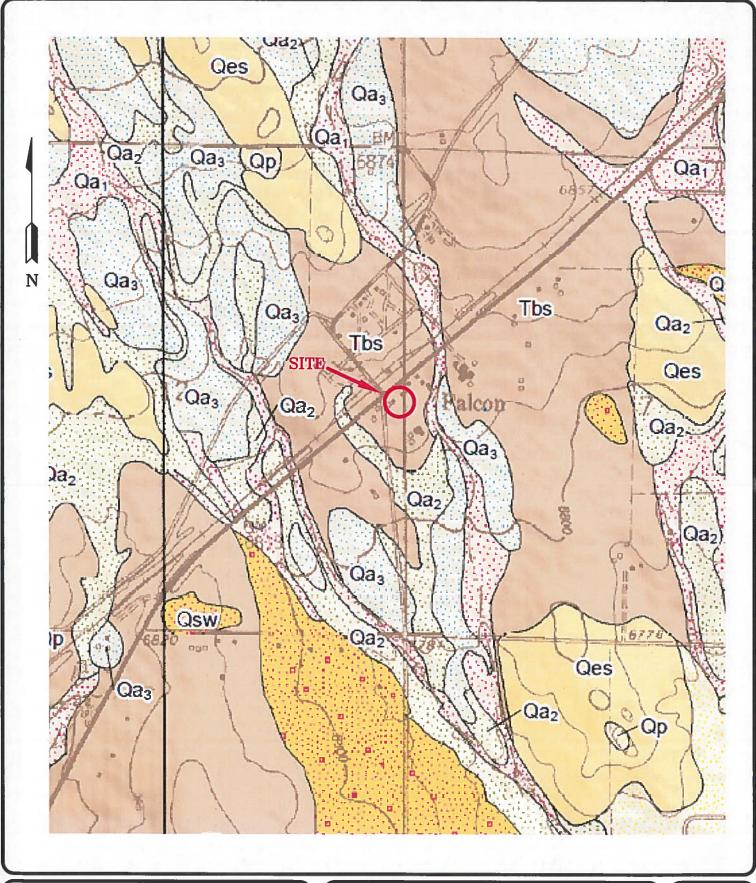


Soil Survey Map 6985 Meridian Road Falcon, CO. For: Hammers Construction

JOB NO.: 171206

FIG NO.:

3





Falcon Quadrangle Geology Map 6985 Meridian Road Falcon, CO. For: Hammers Construction

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JOB NO.: 171206

FIG NO.:

APPENDIX A: Test Boring Logs

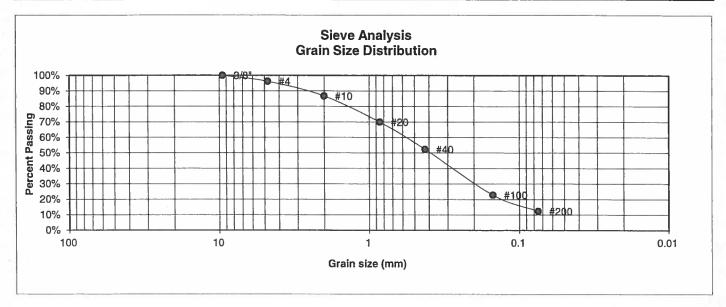
TEST BORING NO. TEST BORING NO. DATE DRILLED 9/14/2017 DATE DRILLED 9/14/2017 Job # 171206 CLIENT HAMMERS CONSTRUCTION LOCATION 6985 MERIDIAN ROAD REMARKS REMARKS % % Blows per foot Blows per foot Watercontent Watercontent WATER @ 10', Soil Type Depth (ft) Samples Samples 9/14/17 Symbol Symbol CAVED TO 6', 9/26/17, DRY WATER @ 10.5', 9/26/17 FILL O-3', SAND, SILTY, FINE SAND, SLIGHTLY SILTY, FINE TO COARSE GRAINED, BROWN, GRAINED, TAN, LOOSE 8.1 1A MOIST LOOSE, MOIST 6 8 2.2 1 SAND, SILTY, FINE TO 8.0 1 COARSE GRAINED, BROWN, 6 2.4 1 VERY LOOSE, MOIST SAND, SILTY, FINE TO COARSE GRAINED, TAN, MEDIUM DENSE, SAND, SILTY, FINE TO COARSE VERY MOIST TO WET 10 21 7.6 12 5.0 GRAINED, TAN TO GRAY, 10 MEDIUM DENSE TO DENSE, VERY MOIST TO WET 15 9.6 1 18 15 30 9.9 SANDSTONE, SILTY, FINE TO COARSE GRAINED, GRAY BROWN, VERY DENSE, MOIST <u>50</u> 9.8 2 25 14.8



	TEST BORING LOG				
DRAWN:	DATE:	CHECKED;	DATE: /0/17/17		

JOB NO.: 171206 FIG NO.: A- 1 **APPENDIX B: Laboratory Testing Results**

UNIFIED CLASSIFICATION	SM	CLIENT	HAMMERS CONSTRUCTION
SOIL TYPE #	1	PROJECT	6985 MERIDIAN ROAD
TEST BORING #	1	JOB NO.	171206
DEPTH (FT)	5	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
1/2" 3/8"	100.0%	
4	96.2%	<u>Swell</u>
10	86.7%	Moisture at start
20	69.9%	Moisture at finish
40	52.3%	Moisture increase
100	22.8%	Initial dry density (pcf)
200	12.3%	Swell (psf)

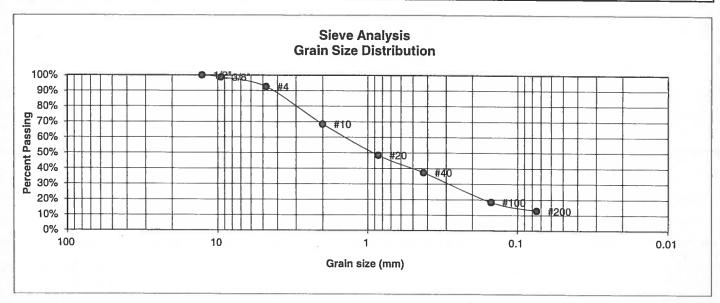


_	LABOI RESU		
DRAWN:	DATE:	CHECKED:	DATE: 9/29/17

JOB NO.: 171206

FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	HAMMERS CONSTRUCTION
SOIL TYPE #	1	PROJECT	6985 MERIDIAN ROAD
TEST BORING #	2	JOB NO.	171206
DEPTH (FT)	15	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2"	100.0%	
3/8"	98.7%	
4	92.5%	<u>Swell</u>
10	68.5%	Moisture at start
20	48.4%	Moisture at finish
40	37.3%	Moisture increase
100	18.4%	Initial dry density (pcf)
200	12.8%	Swell (psf)

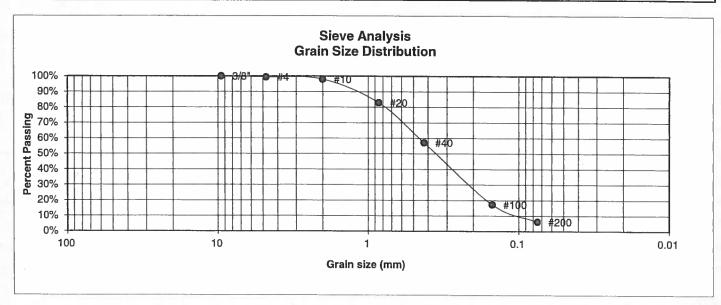


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JOB NO.: 171206

FIG NO .:

UNIFIED CLASSIFICATION	SM-SW	CLIENT	HAMMERS CONSTRUCTION
SOIL TYPE #	1	PROJECT	6985 MERIDIAN ROAD
TEST BORING #	2	JOB NO.	171206
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8" 4 10	100.0% 99.4% 98.1%	<u>Swell</u> Moisture at start
20 40	82.9% 57.1%	Moisture at finish Moisture increase
100 200	17.3% 6.2%	Initial dry density (pcf) Swell (psf)

DRAWN:

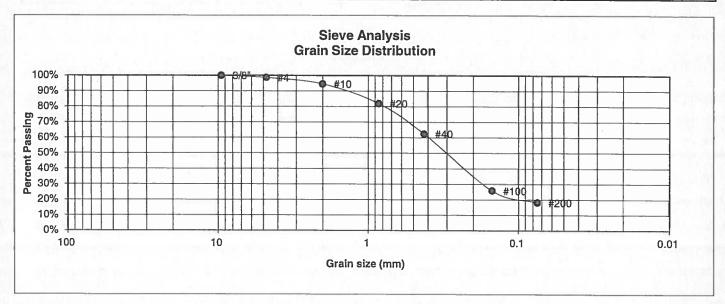


LABOR RESUI	RATORY TEST LTS	
DATE:	CHECKED:	DATE: 9/29/17

JOB NO.: 171206

FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	HAMMERS CONSTRUCTION
SOIL TYPE #	1	PROJECT	6985 MERIDIAN ROAD
TEST BORING #	2	JOB NO.	171206
DEPTH (FT)	20	TEST BY	BL



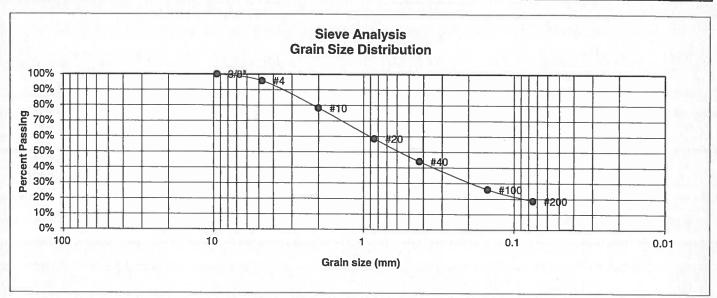
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	98.6%	Swell
10	94.6%	Moisture at start
20	81.9%	Moisture at finish
40	62.5%	Moisture increase
100	25.8%	Initial dry density (pcf)
200	18.2%	Swell (psf)



	LABOI RESU	RATORY TEST	
DRAWN:	DATE:	CHECKED:	DATE: 10/17/17

> JOB NO.: FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	HAMMERS CONSTRUCTION
SOIL TYPE #	2	PROJECT	6985 MERIDIAN ROAD
TEST BORING #	1	JOB NO.	171206
DEPTH (FT)	20	TEST BY	BL



U.S. Sieve # 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2" 3/8" 4 10	100.0% 95.8% 78.3%	<u>Swell</u> Moisture at start
20	58.6%	Moisture at finish
40	44.0%	Moisture increase
100	26.1%	Initial dry density (pcf)
200	18.7%	Swell (psf)



	LABOI RESU	RATORY TEST LTS	
DRAWN:	DATE:	CHECKED:	DATE: 10/17/17

JOB NO.: 171206

FIG NO.:

13-5

CLIENT	HAMMERS CONSTRUCTION	JOB NO.	171206
PROJECT	6985 MERIDIAN ROAD	DATE	9/25/2017
LOCATION	6985 MERIDIAN ROAD	TEST BY	BL

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-1	5	1 1	SM	<0.01
TB-2	20	1	SM	<0.01
<u> </u>				

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LABORATORY TEST SULFATE RESULTS			
DRAWN:	DATE:	CHECKED:	DATE:

JOB NO.: 171206

FIGNO.:
B-6

APPENDIX C: Soil Survey Description

19—Columbine gravelly sandy loam, 0 to 3 percent slopes. This deep, well drained to excessively drained soil formed in coarse textured material on alluvial terraces and fans and on flood plains. Elevation ranges from 6,500 to 7,300 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown gravelly sandy loam about 14 inches thick. The underlying material is light yellowish brown very gravelly loamy sand.

Included with this soil in mapping are small areas of Stapleton sandy loam, 3 to 8 percent slopes; Blendon sandy loam, 0 to 3 percent slopes; Louviers silty clay loam, 3 to 18 percent slopes; and Fluvaquentic Haplaquolls, nearly level. In places the parent arkose beds of sandstone or shale are at a depth of 0 to 40 inches.

Permeability of this Columbine soil is very rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate.

This soil is used mainly for grazing livestock and for wildlife habitat. It is also used for homesites.

Native vegetation is mainly western wheatgrass, sideoats grama, needleandthread, and little bluestem. The main shrub is true mountainmahogany.

Proper location of livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are fairly well suited to this soil. Blowing sand and low available water capacity are the principal limitations to the establishment of trees and shrubs. The soil is so loose that trees need to be planted in the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

Rangeland wildlife, such as pronghorn antelope, cottontail, coyote, and scaled quail, is best adapted to life on this droughty soil. Forage production is typically loam, and proper livestock grazing management is necessary if wildlife and livestock share the range. Livestock watering developments are also important and are used by various wildlife species.

The main limitation of this soil for urban development is a hazard of flooding in some areas. Care must be taken when locating septic tank absorption fields because of possible pollution as a result of the very rapid permeability of this soil. Capability subclass VIe.



222	COIL	DESRIPTION
SU.S.	SOII	DESKIPTION

Drawn Date Checked Date 3/24//6

Job No. 171206 Fig. No. C-1 APPENDIX D: Colorado Geological Survey Review Letter

COLORADO GEOLOGICAL SURVEY

1801 19th Street Golden, Colorado 80401 303.384.2655



Karen Berry State Geologist

February 19, 2018

Kari Parsons El Paso County Development Services Dept. 2880 International Circle, Suite 110 Colorado Springs, CO 80910 Portions of Lot 2 and 3 of Sec 7 and SE NE and NE SE of Sec 12 T13S, R64W of the 6th PM 38.933°, -104.608°

Subject:

Largent Subdivision

File Number SF183; El Paso County, CO; CGS Unique No. EP-18-0043

Dear Kari:

Colorado Geological Survey has reviewed the subject referral. For this review we received: Application (1.23.18), Letter of Intent (Hammers Construction, Undated), Plat (Ridgeline Land Surveying, 10.25.17), Final Drainage Report (JPS Engineering, 1.18.18), Erosion Control Plan and Map (JPS Engineering, 1.18.18), Subsurface Soil Investigation (Entech, 10.20.17), and various other documents.

Geologic Hazards: The subsurface soils investigation submitted, while providing useful information for the project, is not a geology hazard report. There are several geologic hazards that CGS identifies within this site. However, our review is not a substitute for a lot-specific geologic hazard report with mapping of site geology and areas of identified geologic hazards. The hazards identified by CGS review include collapsible and/or loose soils, erosion, undocumented fill, and the potential for shallow groundwater and expansive clays. All of these identified geologic hazards can be mitigated with specific engineering as outlined in the soils and erosion reports.

Per El Paso County Land Development Code 8.4.2 (B) "Lots or tracts subject to natural hazards which may be eliminated through specialized engineering shall be identified on the plat." The plat should include the listing of these identified geologic hazards. The soils report includes engineering mitigation for loose soils, undocumented fill, and potential expansive clay and provides surface and subsurface drain recommendations for shallow groundwater. The erosion control plan and map includes design to control erosion.

Shallow groundwater: Entech reports groundwater levels in their borings of 10 and 10.5 feet below the ground surface. One of the borings caved at 6 feet below ground surface between times of measurements. Caving is typical at groundwater level. The groundwater levels reported were measured in September, a typically dry time of year. This location is in an area generally known for shallow groundwater issues. Groundwater levels typically fluctuate throughout the year and are generally highest in the spring and summer months. Without specific groundwater monitoring throughout the year it cannot be determined what groundwater levels may be over the engineered life of the planned structures. However, groundwater should be expected to be shallower than 6 to 10 feet below existing ground level on a seasonal basis. Entech's recommendations on perimeter drains must be strictly adhered to.

Geotechnical observation: As stated on page 5 of Entech's report, observation by the geotechnical engineer of overall foundation excavation and any overexcavated subgrade is critical to determine specific engineering requirements that may be necessary for the long-term performance of the foundation system.

Kari Parsons February 19, 2018 Page 2 of 2

Provided the recommendations of this letter and those of the geotechnical engineer are followed, CGS has no objections to this plat request.

Thank you for the opportunity to review and comment on this project. If you have questions or need additional review, please call at (303) 384-2643, or e-mail jlovekin@mines.edu.

Sincerely,

Jonathan R. Lovekin, P.G.

Senior Engineering Geologist

Markup Summary

5/7/2018 4:24:26 PM (1)

n Add "PCD File No. SF-18-003" Unresolved Subject: Text Box Page Label: 1 Lock: Unlocked

Status:

Checkmark: Unchecked Author: dsdlaforce Date: 5/7/2018 4:24:26 PM

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Add "PCD File No. SF-18-003"

Unresolved

5/7/2018 4:29:12 PM (1)



Subject: Text Box Page Label: 1 Lock: Unlocked

Status:

Checkmark: Unchecked Author: dsdlaforce Date: 5/7/2018 4:29:12 PM

Color:

Provide evaluation/recommendation for the foundation preparation and embankment construction for the permanent detention facility. Unresolved. See DCM Chapter 11 Section 11.3.3.