

Drainage Letter/Report

for the

Replat of Manley Subdivision El Paso County, Colorado

April, 2022

Revised: February, 2024

Prepared for:
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El Paso County Project Number: VR2310

KCH Engineering Solutions: Job No: 2021-101

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- Exhibit 5: Drainage Basin Planning Study Exhibits
- Exhibit 6: Existing Drainage Reports/ Offsite and Onsite
- Exhibit 7: Existing Plat and Replat
- Exhibit 8: Hydrologic Summary per Existing Plat (per Berge Brewer & Assoc.)
- Exhibit 9: Hydrologic Summary per Replat (this report)
- Exhibit 10: Hydraulic Summary per Replat (this report)
- Exhibit 11: Drainage Map per Replat

Certifications and Approvals

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report had been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparation this report

Signature _____ Seal
(Kenneth C. Harrison, P.E.)

Developer/Owner Statement

I, the developer/owner, _____, have read and will comply with all of the requirements specified in this drainage report and plan.

(Business Name)

By: _____ (Date)
(Signature)

Print Name and Title _____

Address: _____

El Paso County

Filed in accordance with the requirements of the Drainage Criteria Manual, Volume 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

For El Paso County Engineer

Joshua Palmer, P.E. Date
County Engineer/ ECM Administrator (Signature)

Conditions

Flood Plain Statement

See Section V of this report

I. **REPORT PURPOSE**

Drainage from the Manley Subdivision site previously studied in 2000 with a Drainage Report entitled "Preliminary/ Final Drainage Report for Manly Subdivision, prepared by Law and Marrioti, September 2000 This report will be noted as **LM-Report 2** in this report. At that time the **LM-Report 2** was prepared the Manley subdivision consisted of seven (7) lots) (*Exhibit 6, Appendix*)

It is proposed to replat the current subdivision in order to reconfigure lot lines. In accordance with the current El Paso County Drainage Criteria, a Drainage Letter/Report is required. The drainage letter/report is entitled "Drainage Letter/Report for the Replat of Manley Subdivision El Paso County, Colorado April, 2022 Revised: February, 2024" (**KCH-3**)

The purpose of this replat is to **only** modify the existing lot lines. No surface improvements are proposed. As a result, there will be **no changes** to the existing drainage patterns as described in the **LM-Report 2**. The (**KCH-3**) report will be submitted as required by El Paso County for replats of previously platted parcels when there are to be **no** or only negligible changes to the drainage characteristics. The (**KCH-3**) will also address any change in criteria that have occurred since 2000. Included in the Appendix (*Exhibit 4*) is correspondence with El Paso County outlining the information that is to be addressed in this (**KCH-3**)

The (**KCH-3**) report will show this replat will have **no impact** on the drainage characteristics as described in Report 2.

II. **GENERAL PROPERTY DESCRIPTION AND ACREAGE**

Manley Subdivision is located in the Southwest quarter of the Southwest quarter of Section 22, Township 13 south, Range 64 West, of the 6th PM in the County of El Paso, State of Colorado. More precisely , the parcel is located in the northeast corner of the Curtis Road/ Jones Road intersection (*Exhibit 1, Appendix*). The site is located in the Solberg Ranch Drainage Basin.

Manley Subdivision presently consists of four (4) lots and an "out-parcel" labelled as Future Phase 2. Several structures have been constructed on the Lot 2, Lot 3 and Lot 4 as shown on the **LM-Report 2** (*Exhibit 6, Appendix*). The development is covered with native grasses and weeds. General site topography is characterized by a gentle slope from the northwest to the southeast at an average slope of approximately 2.5%.

Topography

The topographic map was obtained from GIS mapping obtained from El Paso County. The site is gently rolling from an elevation of 6610.0 at the northwest corner and 6566.0 at the southwest corner over 2,700 feet in length resulting in an average slope of 1.6%.

Structures

There are several single-family residential structures on the project site. They are located on Lots 2, 3, and 4 of the original plat. The approximate location is shown on *Exhibit 6 in the Appendix*. There are currently no plans to add additional structures.

III. DESIGN CRITERIA AND METHODOGY

El Paso County Drainage Criteria Manual, Volume I.

City of Colorado Springs Drainage Criteria Manual (where included with the El Paso County Drainage Criteria Manual).

Soil Survey of El Paso County Area, Colorado United States Department Detention/ Water Quality

IV. FEMA FLOODPLAIN

The project site is located in FEMA map 08041CO568G (*Exhibit 2, Appendix*). The entire site is located outside the 100-year floodplain in Zone X which is an "Area of Minimal Disturbance" for which there are no special requirements for the construction of commercial or industrial structures.

V. HYDROLOGIC SOILS INFORMATION

A Custom Soil Resource Report (*Exhibit 3, Appendix*) was obtained that shows the approximate location as well as a description of the soil associated groups. All of the soils are classified as either hydraulic group A or B. The soils are identified as follows:

- Blakeland loamy sand (SCS No. 8)
- Stapleton Sandy loam (SCS No. 83)
- Trucon Loamy Sand (SCS No. 95)

VI. OFFSITE DRAINAGE CONDITIONS

General

OS1 is the only offsite area that impacts the Manning Subdivision. It has an area of approximately 208.5 acres as determined from USGS mapping for this report. It has an average slope of 1.6%, and is vegetated with long prairie grasses and an

occasional bush. The storm water from the west sheet flows east and then is collected by a roadside swales S1 and S7 (**KCH-3**) which functions as a borrow ditch along the westerly side of Curtis Road. The storm water is then routed southerly to DP1 (**KCH-3**) where a 24" CMP carries the water under Curtis Road. The upstream end of the existing 24" CMP culvert is approximately 200 feet north of the Curtis Road/ Jones Road intersection. Any other offsite runoff is collected by S3 and S4 (**KCH-3**) and is routed north of the northerly property line. At no location does stormwater in S3 and S4 enter the **Manley Subdivision**. Analysis of S3 and S4 is beyond the scope of this project. The estimated runoff at the upstream end of the 24" culvert at DP1(**KCH-3**) is discussed in the following three (3) drainage reports. Pertinent pages of each report are included in *Exhibit 6, Appendix*.

1. **Windmill Flats Final Drainage Report, prepared by Berge Brewer, November 21, 2002, (BB-Report 1); Design Point 3 (upstream end of 24" CMP under Curtis Road)**

- Design Point: DP3 is at the same location as DP1 in both the LM-Report 2 and KCH-Report reports.
- Area draining to DP3: not available in the narrative section of the drainage report
- Runoff DP3: (Exhibit 6, Appendix)
 - Q5: 30.4 cfs
 - Q100: 79.1 cfs
 These runoff amounts were obtained from a table in the narrative section of this report.

2. **Preliminary/Final Drainage Report for Manly Subdivision, prepared by Law and Marrioti, March 29,2000 (LM-Report 2); Design Point 1 (Exhibit 6, Appendix) (upstream end of 24" CMP under Curtis Road)**

- Design Point: DP1 as shown on the **LM-Report 2** is at the same location as DP3 on the BB-Report 1 drainage plan and DP1 on the KCH-Report 3 drainage plan.
- Area draining to DP1:185 acres
- Runoff at DP1
 - The runoff at DP1 was determined with the use of the Rational Method. The current EPS design standard states that the upper limit for using the Report Rational Method is 110 acres. Runoff in the (**KCH-Report 3**) report used the TR55 method.
 - Flow Rates at DP1
 - Q5: 78.7 cfs
 - Q100: 207 cfs

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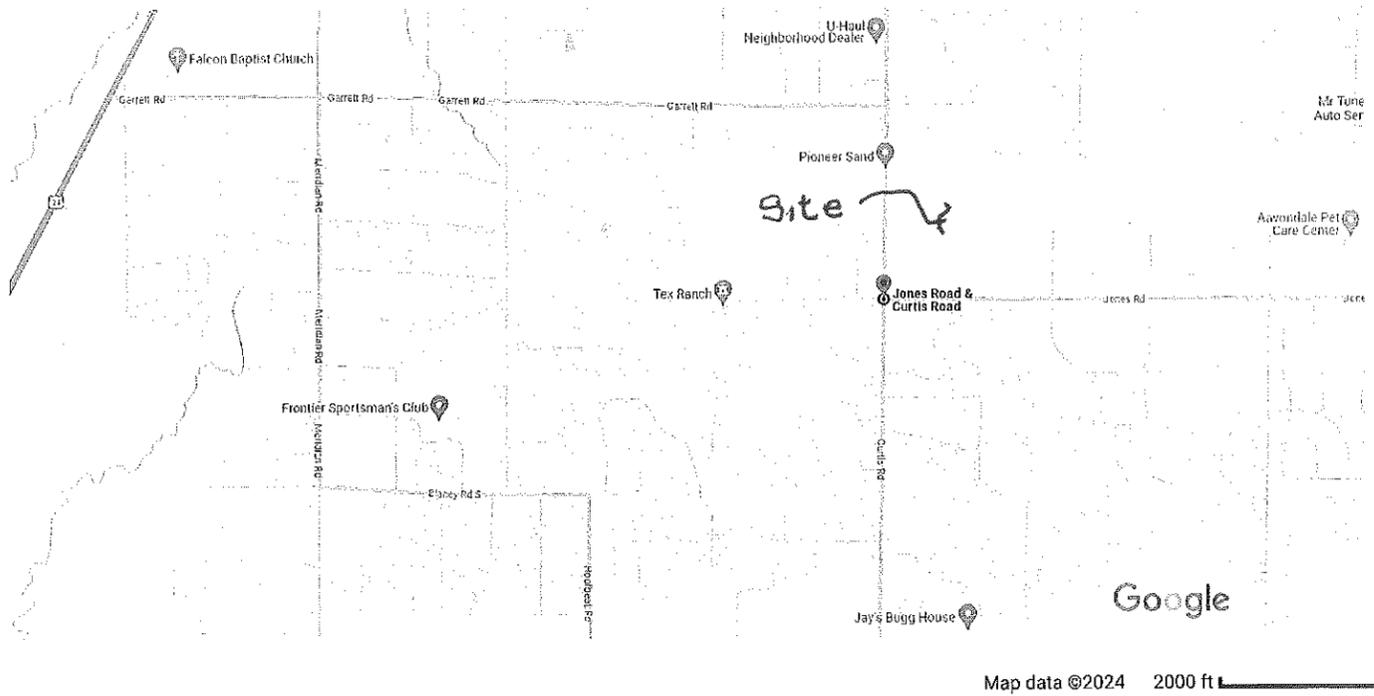
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APPENDIX

Exhibit 1

Location Map



Delays

Light traffic in this area

No known road disruptions. Traffic incidents will show up here.

Exhibit 2

FEMA FIRM Map

National Flood Hazard Layer FIRMette



Legend

104°33'21"W 38°54'4"N



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Basemap: USGS National Map: Orthoimagery; Data refreshed October, 2020

Exhibit 3

SCS Soils Map and Data



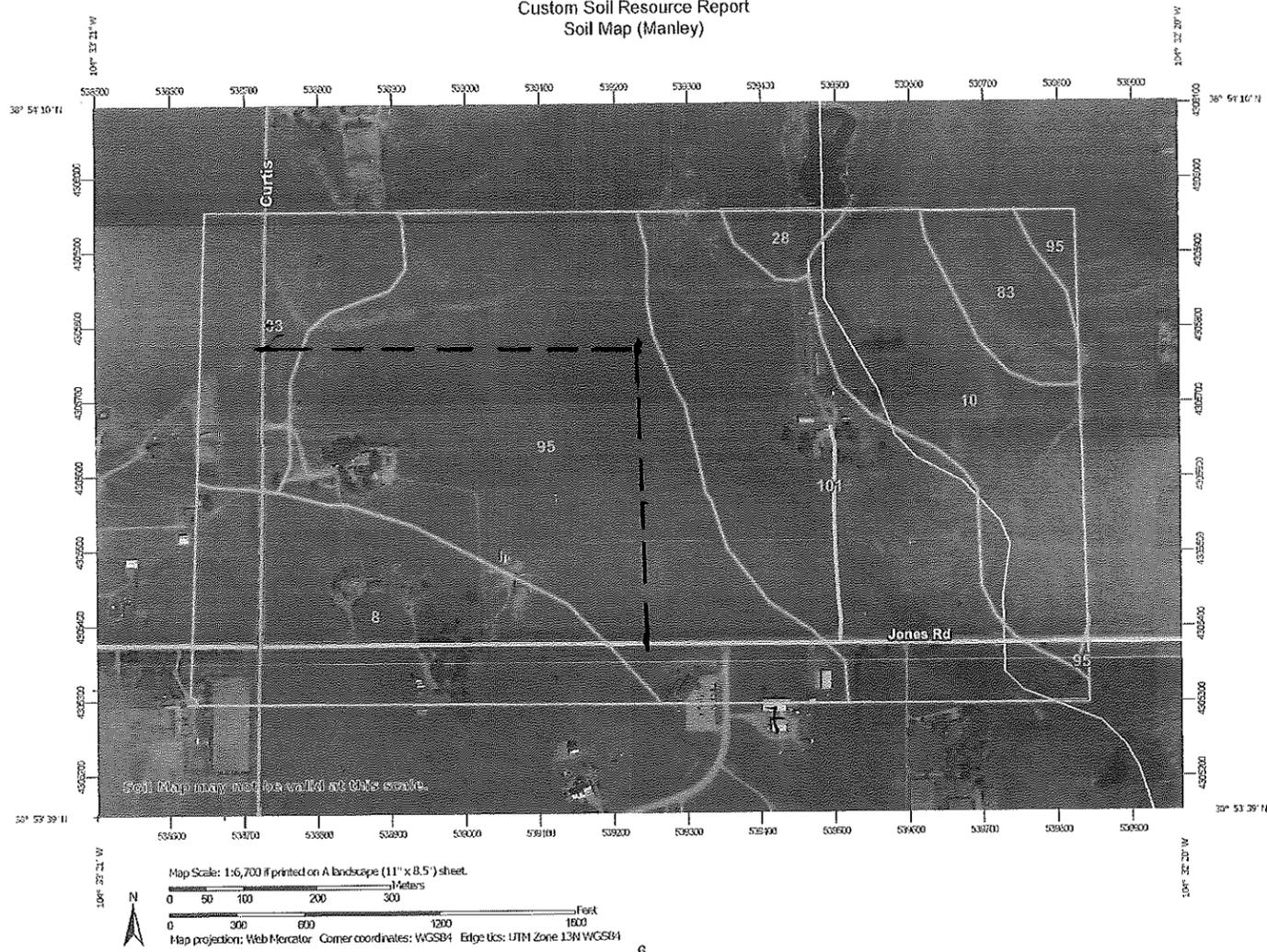
A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado

Manley Subdivision



Custom Soil Resource Report
Soil Map (Manley)



Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Map Unit Legend (Manley)

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	31.9	16.3%
18	Blendon sandy loam, 0 to 3 percent slopes	25.9	13.3%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	2.5	1.3%
83	Stapleton sandy loam, 3 to 8 percent slopes	23.8	12.2%
95	Truckton loamy sand, 1 to 9 percent slopes	67.8	34.7%
101	Ustic Torrifluvents, loamy	43.5	22.3%
Totals for Area of Interest		195.4	100.0%

Map Unit Descriptions (Manley)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

Custom Soil Resource Report

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v
Elevation: 4,600 to 5,800 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 48 degrees F
Frost-free period: 125 to 145 days
Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent
Minor components: 2 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats
Landform position (three-dimensional): Side slope, talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand
AC - 11 to 27 inches: loamy sand
C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent

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Custom Soil Resource Report

Typical profile

A - 0 to 11 inches: sandy loam
Bw - 11 to 17 inches: gravelly sandy loam
C - 17 to 60 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.7 inches)

punit.

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: B
Ecological site: R049XY214CO - Gravelly Foothill
Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: 1 percent
Landform: Swales
Hydric soil rating: Yes

Other soils

Percent of map unit: 1 percent
Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent
Landform: Depressions
Hydric soil rating: Yes

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95—Truckton loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2yvrm
Elevation: 5,800 to 7,100 feet
Mean annual precipitation: 12 to 19 inches
Mean annual air temperature: 46 to 50 degrees F
Frost-free period: 90 to 155 days
Farmland classification: Not prime farmland

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.35	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis--Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when land use is undeveloped)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_t) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

(Eq. 6-7)

n)

(Eq. 6-8)

n land uses, 100 ft maximum for

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 ublic properties of the swale, ditch,
 timated with the help of Figure 6-

(Eq. 6-9)

Table 6-7. Conveyance Coefficient, C_v

Type of Land Surface	C_v
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

*For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_o) and the travel time (t_t) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \quad (\text{Eq. 6-10})$$

Where:

t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

is & Thunderstorms for

% I	Pre-Development CN			
	HSG A	HSG B	HSG C	HSG D
---	68	79	86	89
---	49	69	79	84
---	39	61	74	80
---	98	98	98	98
---	98	98	98	98
---	83	89	92	93
---	76	85	89	91
---	72	82	87	89
---	63	77	85	88
---	96	96	96	96
85	89	92	94	95
72	81	88	91	93
65	77	85	90	92
38	61	75	83	87
30	57	72	81	86
25	54	70	80	85
20	51	68	79	84
12	46	65	77	82
% I	HSG A	HSG B	HSG C	HSG D
---	77	86	91	94
% I	HSG A	HSG B	HSG C	HSG D
---	77	86	91	94
---	76	85	90	93
---	74	83	88	90
---	72	81	88	91
---	67	78	85	89
---	71	80	87	90
---	64	75	82	85
---	70	79	84	88
---	65	75	82	86
---	69	78	83	87
---	64	74	81	85
---	66	74	80	82
---	62	71	78	81
---	65	73	79	81
---	61	70	77	80
---	65	76	84	88
---	63	75	83	87
---	64	75	83	86
---	60	72	80	84
---	63	74	82	85
---	61	73	81	84
---	62	73	81	84
---	60	72	80	83
---	61	72	79	82
---	59	70	78	81
---	60	71	78	81
---	58	69	77	80

Most Conservation Case

Table 4B-6 Values of the roughness coefficient, "n."

Type of Channel and Description	Manning's "n" (Normal)	Type of Channel and Description	Manning's "n" (Normal)
A. Constructed Channels		6. Sluggish reaches, weedy deep pools	0.070
a. <i>Earth, straight and uniform</i>		7. Very weedy reaches, deep pools, or floodways with heavy stand of timber and underbrush	0.100
1. Clean, recently completed	0.018	b. <i>Mountain streams, no vegetation in channel, banks usually steep, trees and brush along banks submerged at high stages</i>	
2. Gravel, uniform selection, clean	0.025	1. Bottom: gravel, cobbles, and few boulders	0.040
3. With short grass, few weeds	0.027	2. Bottom: cobbles with large boulders	0.050
b. <i>Earth, winding and sluggish</i>		B-2 Flood plains	
1. No vegetation	0.025	a. <i>Pasture, no brush</i>	
2. Grass, some weeds	0.030	1. Short grass	0.030
3. Dense weeds or aquatic plants in deep channels	0.035	2. High grass	0.035
4. Earth bottom and rubble sides	0.030	b. <i>Cultivated areas</i>	
5. Stony bottom and weedy banks	0.035	1. No crop	0.030
6. Cobble bottom and clean sides	0.040	2. Mature row crops	0.035
c. <i>Rock-lined</i>		3. Mature field crops	0.040
1. Smooth and uniform	0.035	c. <i>Brush</i>	
2. Jagged and irregular	0.040	1. Scattered brush, heavy weeds	0.050
d. <i>Channels not maintained, weeds and brush uncut</i>		2. Light brush and trees	0.060
1. Dense weeds, high as flow depth	0.080	3. Medium to dense brush	0.070
2. Clean bottom, brush on sides	0.050	4. Heavy, dense brush	0.100
3. Same, highest stage of flow	0.070	d. <i>Trees</i>	
4. Dense brush, high stage	0.100	1. Dense willows, straight	0.150
B. Natural Streams		2. Cleared land with tree stumps, no sprouts	0.040
B-1 Minor streams (top width at flood stage < 100 ft.)		3. Same as above, but with heavy growth of sprouts	0.060
a. <i>Streams on plain</i>		4. Heavy stand of timber, a few downed trees, little undergrowth, flood stage below branches	0.100
1. Clean, straight, full stage, no rifts or deep pools	0.030	5. Same as above, but with flood stage reaching branches	0.120
2. Same as above, but more stones and weeds	0.035		
3. Clean, winding, some pools and shoals	0.040		
4. Same as above, but some weeds	0.040		
5. Same as 4, but more stones	0.050		

*Note: These "n" values are "normal" values for use in analysis of channels. For conservative design for channel capacity, the maximum values listed in other references should be considered. For channel bank stability, the minimum values should be considered.

From: Daniel Torres
Sent: Thursday, March 18, 2021 8:22 AM
To: 'KEN HARRISON'
Subject: RE: Rural Road Construction Document examples

Hi Ken,

I have provided answers to your questions below in blue:

Does the Drainage Letter need to address the updated criteria? Yes. The drainage letter should be done per the current criteria. **There are also several mistakes in the report. It uses the Rational Method for 185 acres which is currently limited to less than 100 acres. Does this need to be addressed in the Drainage Letter?** Any previous errors should be noted/addressed in the report. **Nothing was stated in the report about a FSD pond either. Will this have to be addressed even though the Drainage Report was approved?** Yes. Detention should be addressed for the site in question. Whether detention is needed depends on your analysis of the site and development proposed. **Also does El Paso County have similar requirements for Drainage Letters since they have adopted the majority of the C/CS Drainage Criteria Manuals?** Our drainage criteria manual can be found on the County website ([Engineering - El Paso County Planning Development](#)). DCM vol. 1 Chapter 4 has the requirements for drainage letters and reports.

If this is for a specific project that you have submitted for review in the County, I can get you in touch with the review engineer that has been assigned the project to better answer any of your questions. Additionally, the review engineer would know the specifics of the project and can tell you what you will need to provide. My answers above are for most projects in general.

Respectfully,

Daniel Torres, P.E.
Engineer II
El Paso County
Planning and Community Development
[2880 International Circle, Suite 110](#)
[Colorado Springs, CO 80910](#)
[\(719\) 520-6300 \(Main\)](#)
[\(719\) 520-6305 \(Direct\)](#)
[www.elpasoco.com](#)

PERSONAL WORK SCHEDULE

Monday - Thursday, 7:00 am to 5:30 pm

DEPARTMENT HOURS

Monday - Friday, 7:30 am to 4:30 pm

I have provided a few projects that have a rural local roadways within their construction documents. They can be found on EDARP by searching the following file numbers or clicking on the link provided.

SF207: [Project Details - EDARP \(epcdevplanreview.com\)](#)

SF1911: [Project Details - EDARP \(epcdevplanreview.com\)](#)

SF1824: [Project Details - EDARP \(epcdevplanreview.com\)](#)

Respectfully,

Daniel Torres, P.E.

Engineer II

El Paso County

Planning and Community Development

[2880 International Circle, Suite 110](#)

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PERSONAL WORK SCHEDULE

Monday - Thursday, 7:00 am to 5:30 pm

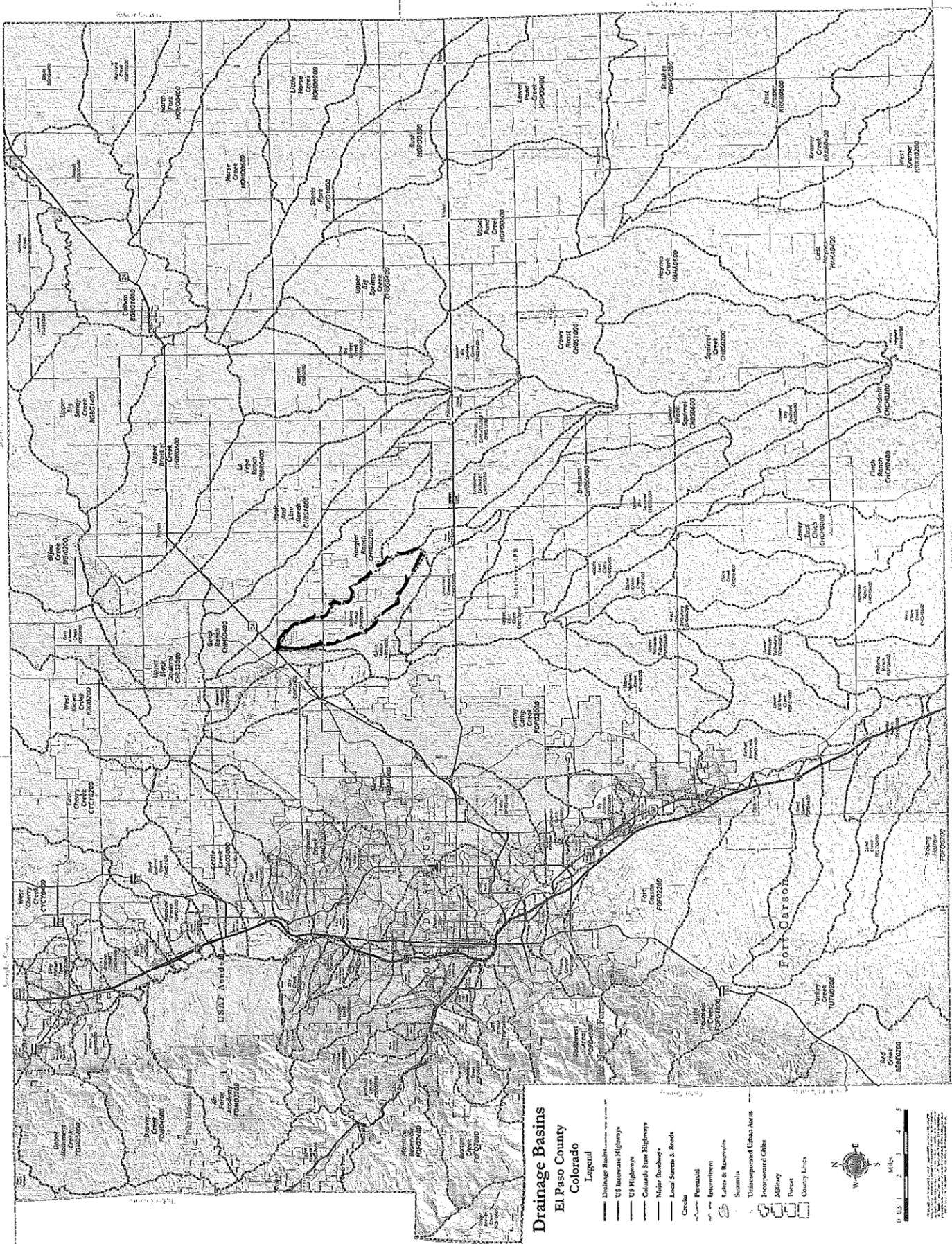
DEPARTMENT HOURS

Monday - Friday, 7:30 am to 4:30 pm

NOTE: In an effort to be respectful of the health of our employees, family, and all citizens in El Paso County, we are limiting our face-to-face public interactions. During this timeframe we will be making every effort to operate "business as usual". All phone calls and emails will be returned, projects reviewed, and necessary meetings held via conference call. Thank you for your patience. Be safe!

Exhibit 5

Drainage Basin Planning Study Exhibits



Drainage Basins
El Paso County
Colorado

- Legend**
- Drainage Basins
 - US Interstate Highways
 - US Highways
 - Colorado State Highways
 - Major Roadways
 - Local Streets & Roads
 - Creeks
 - Poretable
 - Irrigation
 - Lakes & Reservoirs
 - Swamps
 - Unincorporated Urban Areas
 - Incorporated Cities
 - Military
 - County Lines

0 0.5 1 2 3 4 5 Miles

USDA, National Center for Earth and Environmental Assessment
 National Hydrography Dataset
 Version 1.0
 Date: 08/20/2001
 Scale: 1:250,000
 Projection: NAD83
 Contour Interval: 20 Feet
 Contour Type: Spot
 Contour Method: Triangulation
 Contour Accuracy: 10 Feet
 Contour Source: 1:250,000
 Contour Date: 08/20/2001

El Paso County Drainage Basin Fees

Resolution No. 22-442

Basin Number	Receiving Waters	Year Studied	Drainage Basin Name	2023 Drainage Fee (per Impervious Acre)	2023 Bridge Fee (per Impervious Acre)
--------------	------------------	--------------	---------------------	---	---------------------------------------

Drainage Basins with DBPS's:

CHMS0200	Chico Creek	2013	Haegler Ranch	\$12,985	\$1,916
CHWS1200	Chico Creek	2001	Bennett Ranch	\$14,536	\$5,576
CHWS1400	Chico Creek	2013	Falcon	\$37,256	\$5,118
FOFO2000	Fountain Creek	2001	West Fork Jimmy Camp Creek	\$15,802	\$4,675
FOFO2600	Fountain Creek	1991*	Big Johnson / Crews Gulch	\$23,078	\$2,980
FOFO2800	Fountain Creek	1988*	Widefield	\$23,078	\$0
FOFO2900	Fountain Creek	1988*	Security	\$23,078	\$0
FOFO3000	Fountain Creek	1991*	Windmill Gulch	\$23,078	\$346
FOFO3100 / FOFO3200	Fountain Creek	1988*	Carson Street / Little Johnson	\$14,077	\$0
FOFO3400	Fountain Creek	1984*	Peterson Field	\$16,646	\$1,262
FOFO3600	Fountain Creek	1991*	Fisher's Canyon	\$23,078	\$0
FOFO4000	Fountain Creek	1996	Sand Creek	\$23,821	\$9,743
FOFO4200	Fountain Creek	1977	Spring Creek	\$11,969	\$0
FOFO4600	Fountain Creek	1984*	Southwest Area	\$23,078	\$0
FOFO4800	Fountain Creek	1991	Bear Creek	\$23,078	\$1,262
FOFO5800	Fountain Creek	1964	Camp Creek	\$2,557	\$0
FOMO1000	Monument Creek	1981	Douglas Creek	\$14,514	\$321
FOMO1200	Monument Creek	1977	Templeton Gap	\$14,900	\$346
FOMO2000	Monument Creek	1971	Pulpit Rock	\$7,653	\$0
FOMO2200	Monument Creek	1994	Cottonwood Creek / S. Pine	\$23,078	\$1,262
FOMO2400	Monument Creek	1966	Dry Creek	\$18,219	\$660
FOMO3600	Monument Creek	1989*	Black Squirrel Creek	\$10,478	\$660
FOMO3700	Monument Creek	1987*	Middle Tributary	\$19,259	\$0
FOMO3800	Monument Creek	1987*	Monument Branch	\$23,078	\$0
FOMO4000	Monument Creek	1996	Smith Creek	\$9,409	\$1,262
FOMO4200	Monument Creek	1989*	Black Forest	\$23,078	\$628
FOMO5200	Monument Creek	1993*	Dirty Woman Creek	\$23,078	\$1,262
FOMO5300	Fountain Creek	1993*	Crystal Creek	\$23,078	\$1,262

Miscellaneous Drainage Basins: 1

CHBS0800	Chico Creek		Book Ranch	\$21,654	\$3,135
CHEC0400	Chico Creek		Upper East Chico	\$11,797	\$342
CHWS0200	Chico Creek		Telephone Exchange	\$12,962	\$304
CHWS0400	Chico Creek		Livestock Company	\$21,351	\$254
CHWS0600	Chico Creek		West Squirrel	\$11,129	\$4,619
CHWS0800	Chico Creek		Solberg Ranch	\$23,078	\$0
FOFO1200	Fountain Creek		Crooked Canyon	\$6,968	\$0
FOFO1400	Fountain Creek		Calhan Reservoir	\$5,817	\$339
FOFO1600	Fountain Creek		Sand Canyon	\$4,203	\$0
FOFO2000	Fountain Creek		Jimmy Camp Creek ³	\$23,078	\$1,079
FOFO2200	Fountain Creek		Fort Carson	\$18,219	\$660
FOFO2700	Fountain Creek		West Little Johnson	\$1,521	\$0
FOFO3800	Fountain Creek		Stratton	\$11,070	\$495
FOFO5000	Fountain Creek		Midland	\$18,219	\$660
FOFO6000	Fountain Creek		Palmer Trail	\$18,219	\$660
FOFO6800	Fountain Creek		Black Canyon	\$18,219	\$660
FOMO4600	Monument Creek		Beaver Creek	\$13,797	\$0
FOMO3000	Monument Creek		Kettle Creek	\$12,463	\$0
FOMO3400	Monument Creek		Elkhorn	\$2,094	\$0
FOMO5000	Monument Creek		Monument Rock	\$10,003	\$0
FOMO5400	Monument Creek		Palmer Lake	\$15,995	\$0
FOMO5600	Monument Creek		Raspberry Mountain	\$5,380	\$0
PLPL0200	Monument Creek		Bald Mountain	\$11,465	\$0

Interim Drainage Basins: 2

FOFO1800	Fountain Creek		Little Fountain Creek	\$2,950	\$0
FOMO4400	Monument Creek		Jackson Creek	\$9,135	\$0
FOMO4800	Monument Creek		Teachout Creek	\$6,343	\$953

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies performed within the last 14 years.

2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available information suitable for setting a fee.)

3. This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shall be provided to secure payment of additional fees in the event that the DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Resolution 16-320 (9/07/16).

Exhibit 6

Existing Drainage Reports

Exh 6.2

Berge-Brewer & Associates, Inc.



phone (719) 227-7181 - fax (719) 227-7186 - 711 north cascade avenue - colorado springs, co 80903

ENGINEERS
PLANNERS
SURVEYORS

FINAL DRAINAGE REPORT

WINDMILL FLATS

PREPARED FOR:

JOB LARRANAGA

4290 LOS RANCHITOS DRIVE

PEYTON, CO 80831

PREPARED BY:

BERGE-BREWER AND ASSOCIATES, INC.

711 N. CASCADE AVENUE

COLORADO SPRINGS, CO 80903

Prepared by: Anna C. Sparks, EIT
Reviewed by: Roger G. Berge, PE & PLS
May 15, 2002
Revised: June 27, 2002
Revised: August 15, 2002
Revised: September 25, 2002
Revised: November 21, 2002



CERTIFICATION:

Engineers Statement:

This attached drainage plan and report for "Windmill Flats" were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City of Colorado Springs\El Paso County for drainage reports and said report is in conformity with the master plan of the Solberg Ranch Drainage Basin. I accept responsibility for any liability caused by any acts, errors of omissions on my part in preparing this report.

Roger G. Berge 11/25/12
Professional Engineer No. 9646
For and on behalf of Berge, Brewer & Associates, Inc.

Developers Statement:

The developer has read and will comply with all of the requirements specified in this report and plan.

Windmill Flats
Business Name:

By: John Sarranaga

Title: Owner

Address: 4290 Las Ranchitos Dr.
Falcon, Co. 80831

El Paso County:

Filed in accordance with Section 51.1 of the El Paso Land Development Code, as amended.

BY: John A. McCarty

1-13-03
DATE

CONDITIONS:

Exh 6.1

Coyote Estates

Flowrate Summary Table

Description	Q₅ (cfs)	Q₁₀₀ (cfs)
Off-site Basin	5.47	14.88
Basin A Developed Conditions	24.92	64.18
Basin A Current Conditions	21.60	57.76
Basin B	2.34	5.66
Design Point 1	7.55	19.33
Design Point 2	1.50	2.99
Design Point 3 Developed Conditions	30.39	79.06
Design Point 3 Current Conditions	27.07	72.64

Ex 1 &
Ex 17.6.2

**PRELIMINARY/FINAL DRAINAGE REPORT
FOR
MANLEY SUBDIVISION**

March 29, 2000

Prepared for:

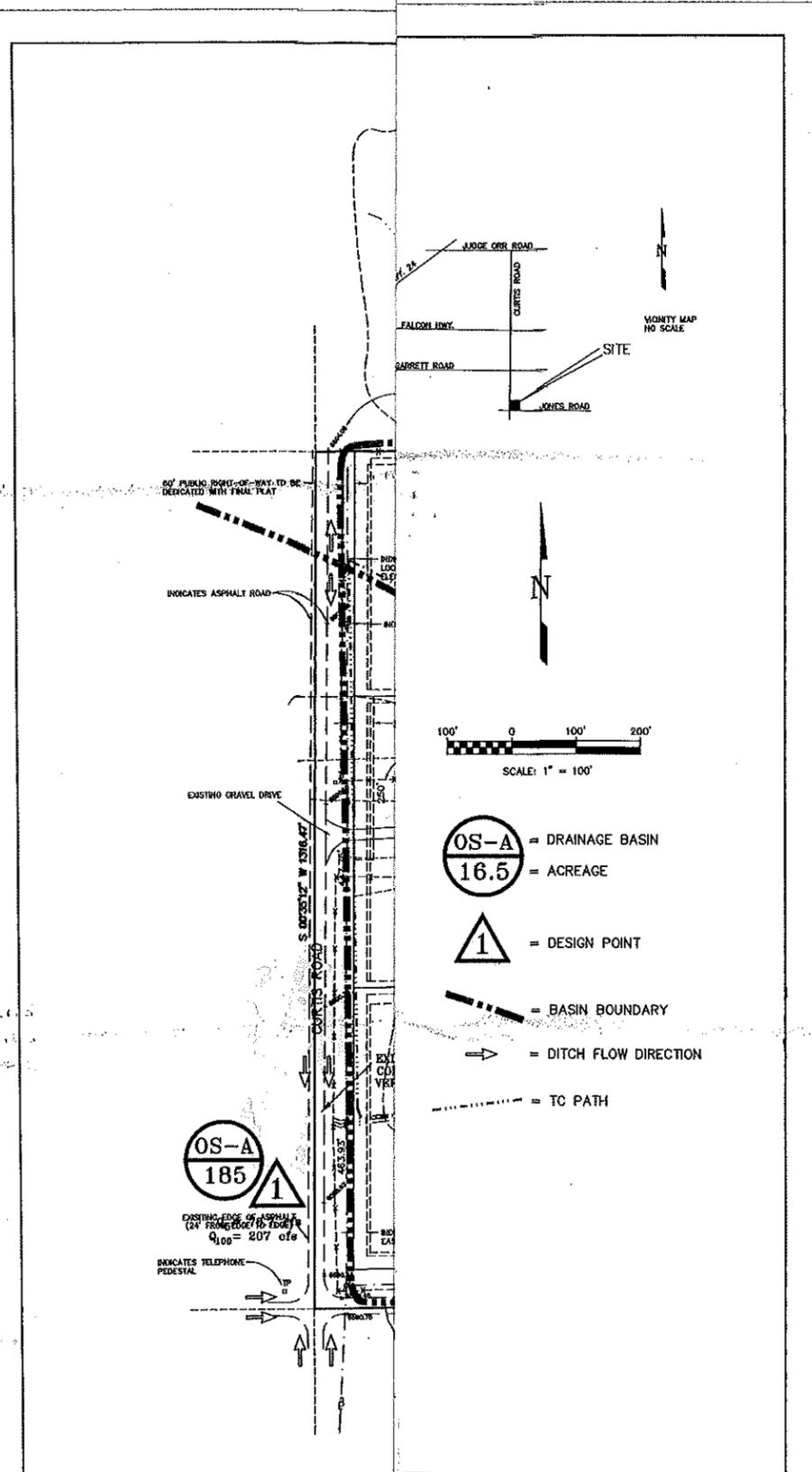
Jerry L. & Nancy Manley
4645 N. Curtis Road
Falcon, CO 80831

Prepared by:

Law & Mariotti Consultants, Inc.
619 North Cascade Avenue, Suite 206
Colorado Springs, CO 80903
(719) 442-1541

LMCI PN 00-021

Exp #6.2



LAW & MARIOTTI CONSULTANTS, INC.
 CIVIL ENGINEERING - LAND SURVEYING
 413 W. Chester Ave., Suite 208, Colorado Springs, CO 80905
 719.442.1511 • FAX: 719.442.1542

DRAINAGE PLAN	DATE	AUG 30, 2000	NO. SHEETS	00-021	SHEET NO.	1
	SCALE	H: AS SHOWN	PROJECT NO.	00-021	SHEET	1

Exhibit 7

Existing Plat and Proposed Replat

Exhibit 8

Hydrologic Summary for Existing Plat (per Law and Marrioti)

(see Exhibit 6)

Exhibit 9

Hydrologic Summary for Proposed Replat

EXHIBIT 9
Hydrology
STORM WATER RUNOFF
Manley Proposed Replat

Hydrology is the same for existing and developed conditions since construction is not proposed for the replat

AVG

BASIN	Gravel Road				Buildings				NATURAL				RUNOFF COEFFICIENT		
	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀
A	14.30	0.13	0.59	0.70	0.09	0.73	0.81	14.08	0.08	0.35	0.09	0.08	0.36	0.08	0.35
B	13.82	0.00	0.59	0.70	0.00	0.73	0.81	13.82	0.08	0.35	0.08	0.08	0.35	0.08	0.35
C	2.19	0.00	0.59	0.70	0.00	0.73	0.81	2.19	0.08	0.35	0.08	0.08	0.35	0.08	0.35
D	6.63	0.05	0.59	0.70	0.07	0.73	0.81	6.51	0.08	0.35	0.09	0.08	0.36	0.09	0.36
E	2.23	0.00	0.59	0.70	0.00	0.73	0.81	2.23	0.08	0.35	0.08	0.08	0.35	0.08	0.35
OSI	208.53	0.00	0.59	0.70	0.00	0.73	0.81	208.53	0.08	0.35	0.08	0.08	0.35	0.08	0.35

Exhibit 9 - Design Point Summary
Existing and Proposed Conditions
Manley Subdivision Proposed Replat

21-Feb-2024

Design Point	Sub Basins	Total Acres (acres)	Existing/ proposed Runoff (see note)		Hydrologic Method
			Q5	Q100	
			cfs	cfs	
1	OS1	208.56	19.2	88	TR55Rational and Method
2	OS1,A, D, E	231.6	20.4	92.5	TR55Rational and Method
3	B	13.82	3.7	27.3	Rational Method
4	OS1, A, D	229.4	23.4	116.1	TR55 and Rational Method

Notes

1 The quantity of runoff for both the existing and proposed runoff is the same since no development is or construction is to occur.

Exhibit 9 Hydrologic Summary

Existing and Proposed Conditions

Manley Subdivision Proposed Replat

21-Feb-2024

ID	Area	Runoff Coef		Runoff	
		5yr	100 Year	5yr	100 Year
OS1	208.5	0.08	0.35	19.20	88.00
A	14.3	0.08	0.35	2.90	19.30
B	13.8	0.08	0.35	3.70	27.30
C	2.19	0.08	0.35	0.50	3.50
D	6.6	0.08	0.35	1.30	8.80
E	2.2	0.08	0.35	0.40	3.00

EXHIBIT 9
Hydrology
STORM WATER RUNOFF
Manley Proposed Replat

Hydrology is the same for existing and developed conditions since construction is not proposed for the replat

BASIN	From Area Runoff Coefficients Summary		OVERLAND				SHALLOW CHANNEL FLOW				Time of Travel (T _t)				INTENSITY *			TOTAL FLOWS	
	AREA TOTAL (Acres)	C _s	C ₁₀₀	C _s	Length (ft)	Height (ft)	T _c (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I _s (in/hr)	I ₁₀₀ (in/hr)	I ₅ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)		
A	14.30	0.09	0.36	0.09	100	3	12.7	1050	2.5%	0.8	22.1	34.8	2.3	3.8	2.9	27.3	19.3		
B	13.82	0.08	0.35	0.08	100	2	14.7	126	4.5%	1.1	2.0	16.6	3.4	5.6	3.7	27.3	27.3		
C	2.19	0.08	0.35	0.08	100	14	7.7	903	2.7%	0.8	18.3	26.0	2.7	4.5	0.5	3.5	3.5		
D	6.63	0.09	0.36	0.09	200	20	12.1	1100	2.4%	0.8	23.7	35.7	2.2	3.7	1.3	8.8	8.8		
E	2.23	0.08	0.35	0.08	200	2	26.0	400	3.0%	0.9	7.7	33.7	2.3	3.9	0.4	3.0	3.0		
OSI	208.53	0.08	0.35	0.08	100	10	8.6	5800	2.6%	0.8	119.9	128.5	0.3	0.5	5.0	36.3	36.3		

* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: Ken H

Date: 1/20/2022

Checked by: _____

Exhibit 9
 Manley

Manley

Harrison

El Paso County, Colorado

Hydrograph Peak/Peak Time Table

Sub-Area or Reach Identifier	Peak Flow and Peak Time (hr) by Rainfall Return Period	
	5-Yr (cfs) (hr)	100-Yr (cfs) (hr)

SUBAREAS		
OS	19.18 13.46	87.99 13.36
A	3.23 12.31	15.78 12.24
D	1.45 12.34	7.11 12.27
E	0.51 12.30	2.48 12.25
REACHES		
OUTLET	20.44 24.2	92.50 113.36

Include of net rods
 in Exhibits
 Check Tables

Design Flows

Areas

Area	Area	Value
OS-A	Area	0.336
A	208.5	0.326 0.33284 0.02334
B	13.8	
C	2.2	
D	6.6	0.61386 0.01036
E	2.2	0.603

~~1 mile Area~~
 1 mile²
 640 A

640 Acres
 1 mile²

WinTR-20 Printed Page File Beginning of Input Data List
 TR20.inp

WinTR-20: Version 1.10 0 0 0.05
 Manley
 no project subtitle provided

SUB-AREA:
 OS A Outlet .32583 66. 2.1
 A Outlet .02234 66. .57
 D Outlet .01036 66. .595
 E Outlet .00348 66. .56

STREAM REACH:

STORM ANALYSIS:
 5-Yr 2.7 Type II 2
 100-Yr 4.6 Type II 2

STRUCTURE RATING:

GLOBAL OUTPUT:
 2 0.05 YYYYN YYYYNN

WinTR-20 Printed Page File End of Input Data List

 Manley
 no project subtitle provided

 Name of printed page file:
 TR20.out

 STORM 5-Yr

Area or Reach Identifier	Drainage Area (sq mi)	Rain Gage ID or Location	Runoff Amount (in)	Elevation (ft)	Peak Flow Time (hr)	Rate (cfs)	Rate (csm)
OS A	0.326		0.409		13.46	19.18	58.87

Line Start Time (hr)	Flow (cfs)	Values @ time (cfs)	increment (cfs)	of 0.133 hr (cfs)	Flow (cfs)	Flow (cfs)	Flow (cfs)
11.868	0.10	0.57	1.51	2.84	4.70	7.18	10.06
12.797	12.79	15.12	16.91	18.17	18.97	19.18	19.08
13.725	18.64	17.80	16.66	15.59	14.67	13.79	13.00
14.654	12.30	11.63	11.00	10.42	9.91	9.44	9.02
15.582	8.63	8.28	7.95	7.65	7.38	7.13	6.89
16.510	6.66	6.45	6.25	6.06	5.88	5.72	5.57
17.439	5.44	5.31	5.20	5.09	4.98	4.89	4.79
18.367	4.70	4.61	4.54	4.47	4.39	4.32	4.26
19.296	4.19	4.12	4.06	3.99	3.93	3.86	3.79
20.224	3.73	3.66	3.60	3.53	3.47	3.41	3.36
21.152	3.31	3.26	3.22	3.18	3.14	3.11	3.08
22.081	3.06	3.04	3.01	3.00	2.98	2.96	2.94
23.009	2.93	2.92	2.90	2.89	2.87	2.86	2.85
23.938	2.84	2.82	2.80	2.75	2.69	2.60	2.47
24.866	2.31	2.13	1.93	1.72	1.51	1.31	1.13
25.795	0.96	0.81	0.68	0.58	0.49	0.42	0.35
26.723	0.30	0.26	0.22	0.18	0.16	0.13	0.11
27.651	0.09	0.08	0.07	0.06			

Time of Concentration

Calc scale of each map

A. Main Top map

Distance along northerly P.L. $650.07 + 669.19 = 1319.2$

Distance (ruler) $6 \frac{3}{16} \text{ in} = 6.1875$

Scale $1'' = 213.3$ use $1'' = 200'$

11x17 map

Distance along northerly P.L. - 1320

Distance = $6 \frac{5}{16} \text{ in} = 6.3125$

Scale = 209 - use 210" $1'' = 210'$

B. OS-A

- 300' @ 10' Fall (Overland)

- shallow channeled to culvert under Curbie

Distance along Northerly P.L. = 1320'

Length in inches "1"

Scale 2.9'

Scale $1320 / 2.9 = 455.2'$ $\therefore 1'' = 455'$

C OS-A

1. Overland

$$L = \frac{1''}{455 \text{ ft}} \times 200' = 200' / 455 = 0.43 \text{ in.}$$

Fall = 6

2. Shallow Swale (to culvert and Curbie)

Actual on Paper = 10.2

Scaled distance $455 \text{ ft} \times 10.2 = 4614$

Vert. Fall: $6700 - 6590 = 110'$

Scale $110 / 4614 = 2.6$

3. Shallow to Easterly P.L.

L = another 1200 ft = Total

$4614 + 1200 = 5800$, Drop = $6700 - 6554 = 146'$, $S = 146 / 5800 = 2.52$

Chris

KCH Engineering Solutions

5228 Cracker Barrel Circle
Colorado Springs, CO 80917
(719) 246-4471

JOB Exhibit 9
SHEET NO. _____ OF _____
CALCULATED BY K. Harrison DATE 1/18/22
CHECKED BY _____ DATE _____
SCALE _____

Tc (cont)

D. Subbasin A

- Sheet Flow - 100 ft

Fall = 3' slope = 3%

- shallow swale to Eastern PL

Length = 1050

Vert Drop = 6580 - 6554 =

Slope = 26 / 1050 = 26' / 1050 = 2.5% 9009

E. Subbasin B

- shallow sheet flow = 100 ft V = 6" S = 6/100 = 6%

- shallow channel flow

Distance to East PL = 850'

V = (6592 - 6554) = 38'

S = 38' / 850' = 4.47%

F. Subbasin C

- Shallow Sheet = (0.6") x 210' / inch = 126'

- Shallow Swale

6592 - 6568 = 24'; S = 24'

Distance: 4.3" (paper) x 210' / inch = 903'

Slope = 24 / 903 = 2.7%

G. Subbasin D (SG)

- Shallow Sheet = 6200, Vert Drop = 20' S = 20 / 200 = 10%

- Shallow channel flow

Distance to East PL = 1100'

Drop = 6588 - 6562 = 26'

Slope = 2.4%

WinTR-20 Printed Page File
TR20.inp

Beginning of Input Data List

WinTR-20: Version 1.10
y
no project subtitle provided

0 0 0.05

(continued)

STORM 100-Yr

SUB-AREA:

OS A Outlet
A Outlet
D Outlet

.32583 66. 2.1
.02234 66. .57
.01036 66. .595

Exhibit 10

Hydraulic Summary for Swales and Culverts for Proposed Replat

Exhibit 10 - Hydraulic Summary

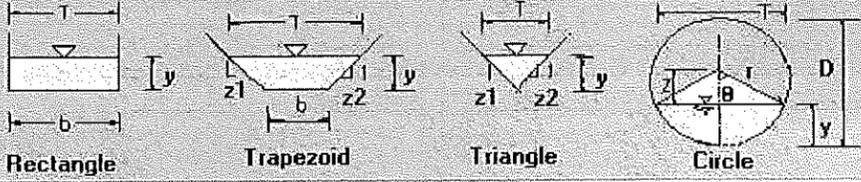
Existing and Proposed Conditions
 Manley Subdivision Proposed Replat

22-Feb-2024

Swale #	Contributing Subbasins	Location	Slope		Side Slopes	Design Flow		Depth of Flow		Velocity		Froude #	
			%			Q5 cfs	Q100 cfs	Q5 ft	Q100 ft	Q5 fps	Q100 fps	5 year	100 year
1						Outside scope of this study							
2	OS 1, A, D	see map	3.0			23.4	116.1	0.6	1.2	4.9	7.3	1.38	1.52
3						Outside scope of this study							
4						Outside scope of this study							
5	B	inside SB	3.5			3.7	27.3	0.3	0.7	3.2	5.6	1.29	1.49
6						Outside scope of this study							
7						Outside scope of this study							
8	OS1,A,D,E	DP4 to DP2	3.5			23.8	119.1	0.6	1.3	5.2	7.7	1.47	1.63

Swale #2 - 5yr

The open channel flow calculator

Select Channel Type: Trapezoid ▾		
Depth from Q ▾	Select unit system: Feet(ft) ▾	
Channel slope: 0.03 ft/ft	Water depth(y): 0.66 ft	Bottom width(b): 3 ft
Flow velocity: 5.076 ft/s	LeftSlope (z1): 6 to 1 (H:V)	RightSlope (z2): 6 to 1 (H:V)
Flow discharge: 23.4 ft ³ /s	Input n value: 0.028 or select n	
Calculate!	Status: Calculation finished	Reset
Wetted perimeter: 11.05 ft	Flow area: 4.61 ft ²	Top width(T): 10.94 ft
Specific energy: 1.06 ft	Froude number: 1.38	Flow status: Supercritical flow
Critical depth: 0.78 ft	Critical slope: 0.0145 ft/ft	Velocity head: 0.4 ft

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Swale #2 - 100yr

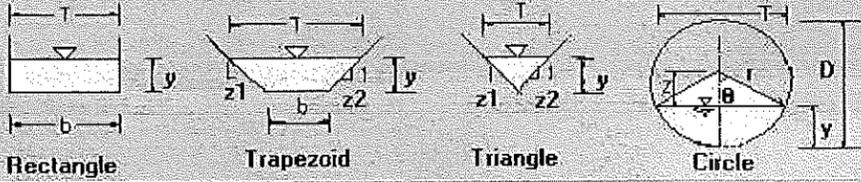
The open channel flow calculator

Select Channel Type: Trapezoid ▾			
Depth from Q ▾	Select unit system: Feet(ft) ▾		
Channel slope: 0.03 ft/ft	Water depth(y): 1.35 ft	Bottom width(b): 3 ft	
Flow velocity: 7.724 ft/s	Left Slope (z1): 6 to 1 (H:V)	Right Slope (z2): 6 to 1 (H:V)	
Flow discharge: 116.1 ft ³ /s	Input n value: 0.028 or select n		
Calculate!	Status: Calculation finished	Reset	
Wetted perimeter: 19.45 ft	Flow area: 15.03 ft ²	Top width(T): 19.23 ft	
Specific energy: 2.28 ft	Froude number: 1.54	Flow status: Supercritical flow	
Critical depth: 1.65 ft	Critical slope: 0.0119 ft/ft	Velocity head: 0.93 ft	

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Swate 8-5 yr

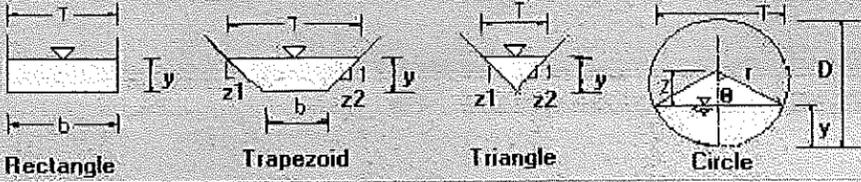
The open channel flow calculator

Select Channel Type: Trapezoid ▾		
Depth from Q ▾	Select unit system: Feet(ft) ▾	
Channel slope: 0.035 ft/ft	Water depth(y): 0.25 ft	Bottom width(b): 3 ft
Flow velocity: 3.206411 ft/s	Left Slope (z1): 6 to 1 (H:V)	Right Slope (z2): 6 to 1 (H:V)
Flow discharge: 3.7 ft ³ /s	Input n value: 0.028 or select n	
Calculate!	Status: Calculation finished	Reset
Wetted perimeter: 6.1 ft	Flow area: 1.15 ft ²	Top width(T): 6.06 ft
Specific energy: 0.41 ft	Froude number: 1.29	Flow status: Supercritical flow
Critical depth: 0.3 ft	Critical slope: 0.0183 ft/ft	Velocity head: 0.16 ft

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Slide 5 100 year

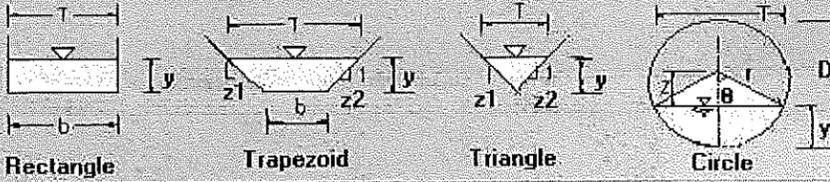
The open channel flow calculator

Select Channel Type: Trapezoid ▾					
Depth from Q ▾		Select unit system: Feet(ft) ▾			
Channel slope: 0.035 ft/ft	Water depth(y): 0.69 ft	Bottom width(b): 3 ft			
Flow velocity: 5.592 ft/s	LeftSlope (z1): 6 to 1 (H:V)	RightSlope (z2): 6 to 1 (H:V)			
Flow discharge: 27.3 ft^3/s	Input n value: 0.028 or select n				
Calculate!	Status: Calculation finished	Reset			
Wetted perimeter: 11.35 ft	Flow area: 4.88 ft^2	Top width(T): 11.23 ft			
Specific energy: 1.17 ft	Froude number: 1.49	Flow status: Supercritical flow			
Critical depth: 0.84 ft	Critical slope: 0.0144 ft/ft	Velocity head: 0.49 ft			

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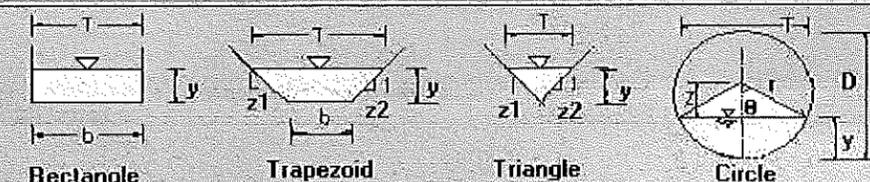
Swale 8 - 5 year

The open channel flow calculator

Select Channel Type: Trapezoid ▾		
Depth from Q ▾	Select unit system: Feet(ft) ▾	
Channel slope: 0.035 ft/ft	Water depth(y): 0.64 ft	Bottom width(b): 3 ft
Flow velocity: 5.412 ft/s	LeftSlope (z1): 6 to 1 (H:V)	RightSlope (z2): 6 to 1 (H:V)
Flow discharge: 23.8 ft ³ /s	Input n value: 0.028 or select n	
Calculate!	Status: Calculation finished	Reset
Wetted perimeter: 10.81 ft	Flow area: 4.4 ft ²	Top width(T): 10.7 ft
Specific energy: 1.1 ft	Froude number: 1.49	Flow status: Supercritical flow
Critical depth: 0.78 ft	Critical slope: 0.0146 ft/ft	Velocity head: 0.45 ft

Swale 8 - 100 year

The open channel flow calculator

Select Channel Type: Trapezoid ▾					
Depth from Q ▾		Select unit system: Feet(ft) ▾			
Channel slope: 0.035 ft/ft	Water depth(y): 1.32 ft	Bottom width(b): 3 ft			
Flow velocity: 8.23 ft/s	LeftSlope (z1): 6 to 1 (H:V)	RightSlope (z2): 6 to 1 (H:V)			
Flow discharge: 119.1 ft ³ /s	Input n value: 0.028 or select n				
Calculate!		Status: Calculation finished		Reset	
Wetted perimeter: 19.09 ft	Flow area: 14.47 ft ²	Top width(T): 18.88 ft			
Specific energy: 2.37 ft	Froude number: 1.66		Flow status: Supercritical flow		
Critical depth: 1.67 ft	Critical slope: 0.0118 ft/ft		Velocity head: 1.05 ft		

DP #1 = Culvert #1 - 24" CMD (Existing)
 $Q_5 = 19.2$ $Q_{10} = 88$

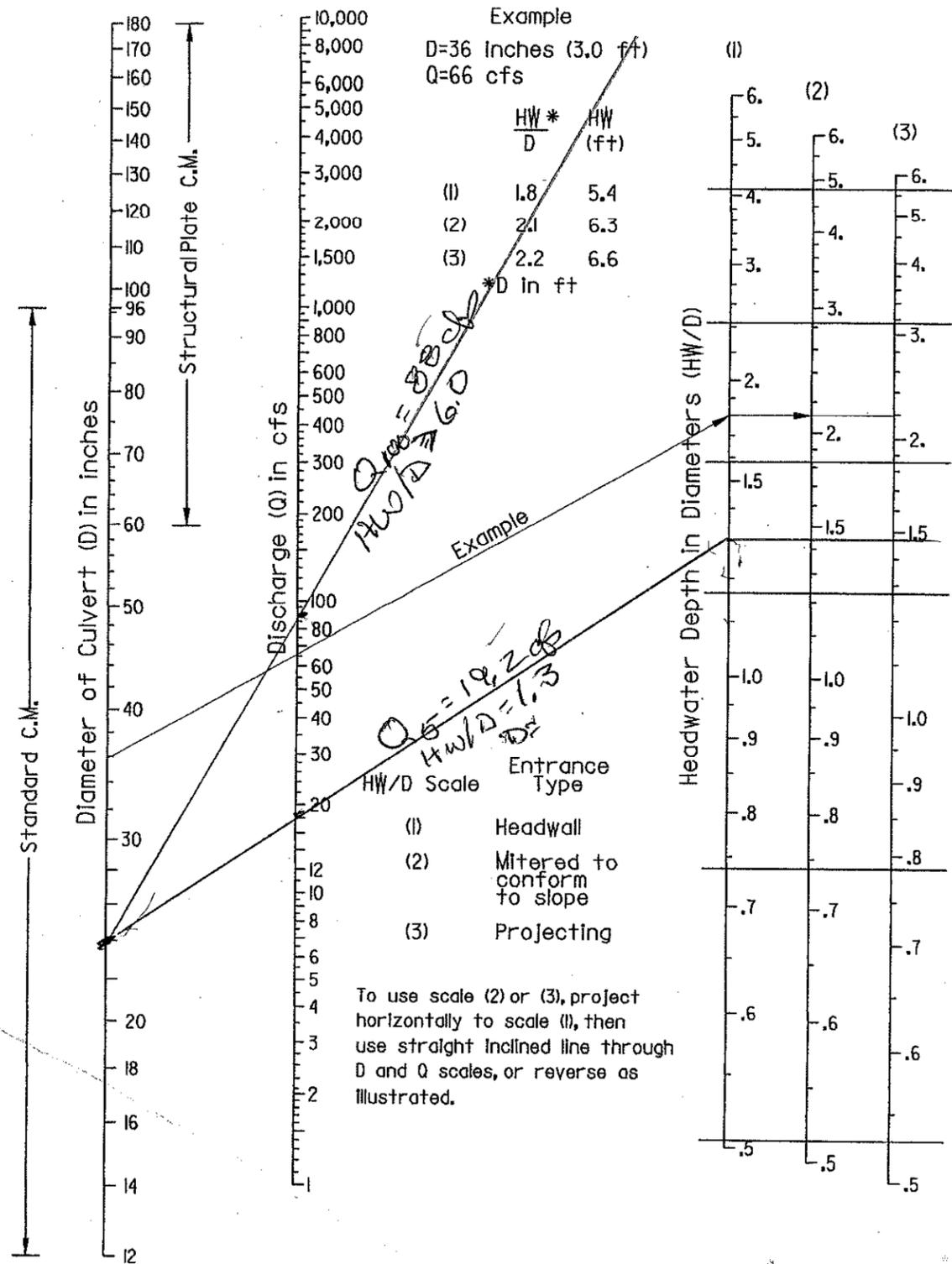


Exhibit F.2 Headwater Depth for CMP Culverts with Inlet Control
 (Source: Reference F.1)

Exhibit 11

Drainage Map for Proposed Replat

MANLEY SUBDIVISION FILING NO. 2

A PORTION OF THE SOUTHWEST QUARTER OF THE SOUTHWEST QUARTER OF SECTION 22, TOWNSHIP 13 SOUTH, RANGE 64 WEST, OF THE 6th P.M., COUNTY OF EL PASO, STATE OF COLORADO

DESIGN POINT SUMMARY

DESIGN POINT	CONTRIB SUB BASINS	TOTAL AREA (acres)	EXISTING/PROP. RUNOFF		HYDROLOGIC METHOD
			Q5 (cfs)	Q100 (cfs)	
1	OS 1	208.56	19.2	88.0	TR55 and Rational Method
2	OS 1, A, D, E	231.60	20.4	92.5	TR55 and Rational Method
3	B	13.82	3.7	27.3	Rational Method
4	OS 1, A, D	229.40	23.4	116.1	TR55 and Rational Method

NOTES: The quantity of runoff for both the existing and proposed runoff is the same since no development is, or construction is, to occur.

SWALE HYDRAULIC SUMMARY

SWALE #	CONTRIBUTING SUBBASINS	LOCATION	SLOPE %	DESIGN FLOW		DEPTH OF FLOW		VELOCITY		FROUDE #	
				Q5 cfs	Q100 cfs	Q5 ft	Q100 ft	Q5 fps	Q100 fps	5 year	100 year
1	OUTSIDE SCOPE OF THIS STUDY										
2	OS 1, A, D	SEE MAP	3.0	23.4	116.1	0.6	1.2	4.9	7.3	1.38	1.52
3	OUTSIDE SCOPE OF THIS STUDY										
4	OUTSIDE SCOPE OF THIS STUDY										
5	B	INSIDE SB	3.5	3.7	27.3	0.3	0.7	3.2	5.6	1.29	1.49
6	OUTSIDE SCOPE OF THIS STUDY										
7	OUTSIDE SCOPE OF THIS STUDY										
8	OS 1, A, D, E	DP4 TO DP2	3.5	23.8	119.1	0.6	1.3	5.2	7.7	1.47	1.63

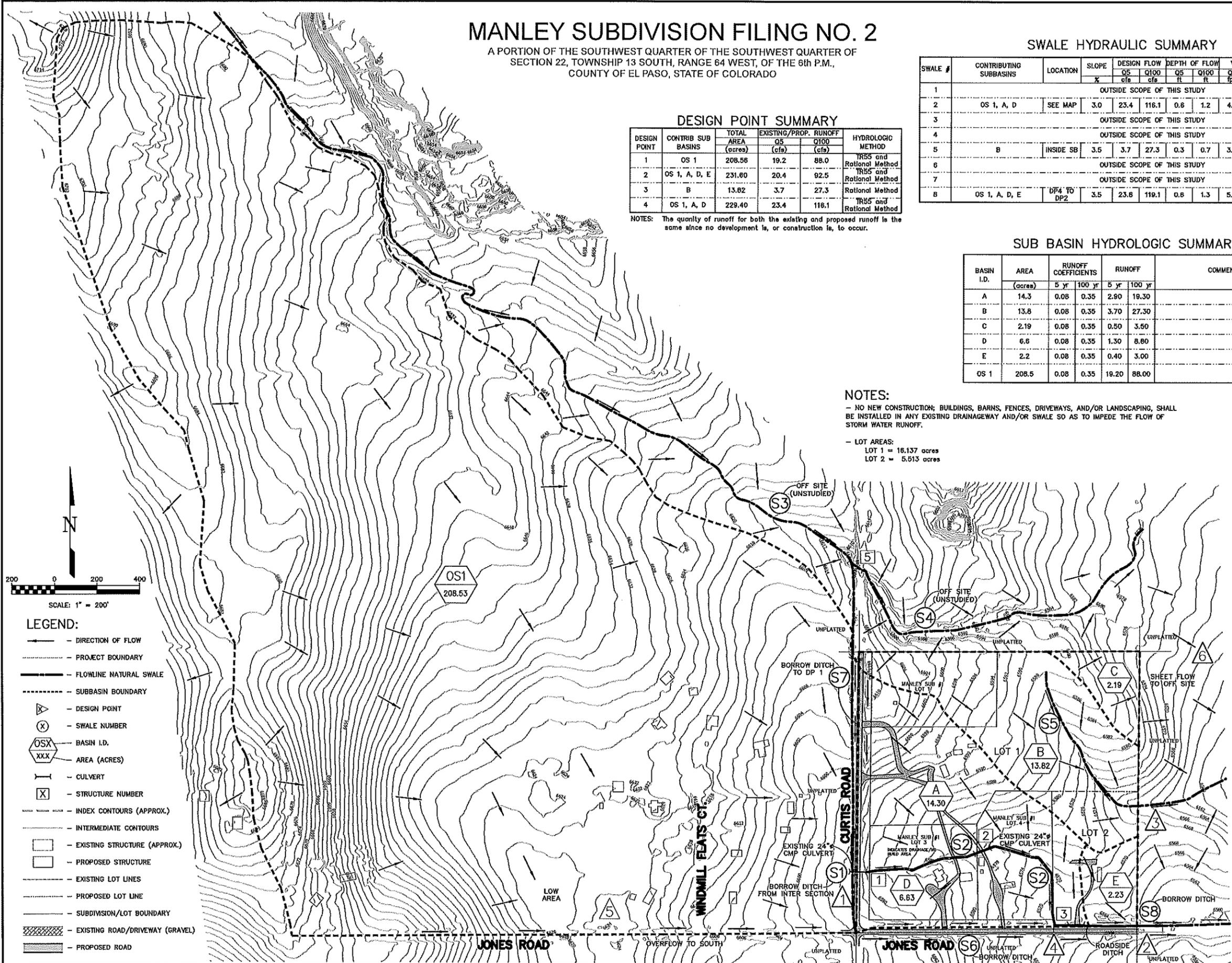
SUB BASIN HYDROLOGIC SUMMARY

BASIN I.D.	AREA (acres)	RUNOFF COEFFICIENTS		RUNOFF		COMMENTS
		5 yr	100 yr	5 yr	100 yr	
A	14.3	0.08	0.35	2.90	19.30	
B	13.8	0.08	0.35	3.70	27.30	
C	2.19	0.08	0.35	0.50	3.50	
D	6.6	0.08	0.35	1.30	8.60	
E	2.2	0.08	0.35	0.40	3.00	
OS 1	208.5	0.08	0.35	19.20	88.00	

NOTES:

- NO NEW CONSTRUCTION; BUILDINGS, BARN, FENCES, DRIVEWAYS, AND/OR LANDSCAPING, SHALL BE INSTALLED IN ANY EXISTING DRAINAGEWAY AND/OR SWALE SO AS TO IMPEDE THE FLOW OF STORM WATER RUNOFF.

- LOT AREAS:
LOT 1 = 16.137 acres
LOT 2 = 5.613 acres



- LEGEND:**
- DIRECTION OF FLOW
 - - - PROJECT BOUNDARY
 - FLOWLINE NATURAL SWALE
 - - - SUBBASIN BOUNDARY
 - △ DESIGN POINT
 - ⊗ SWALE NUMBER
 - OSX BASIN I.D.
 - XXX AREA (ACRES)
 - I I I CULVERT
 - ⊠ STRUCTURE NUMBER
 - - - INDEX CONTOURS (APPROX.)
 - - - INTERMEDIATE CONTOURS
 - EXISTING STRUCTURE (APPROX.)
 - PROPOSED STRUCTURE
 - - - EXISTING LOT LINES
 - - - PROPOSED LOT LINE
 - - - SUBDIVISION/LOT BOUNDARY
 - ▨ EXISTING ROAD/DRIVEWAY (GRAVEL)
 - ▨ PROPOSED ROAD

According to Colorado law, the engineer shall be held liable for any error or omission in this plan. In no event, may any action be taken against the engineer for any error or omission in this plan unless the same is shown to have resulted from negligence on the part of the engineer.

CALL BEFORE YOU DIG ...

811 DIAL 811

4 HOURS BEFORE WORKING CALL UTILITY LOCATIONS FOR LOCATIONS AND MARKING GAS, ELECTRIC, WATER AND TELEPHONE LINES.

REVISIONS

No.	Description	By	Date
1	UPDATED SUMMARY TABLES	DAS	02/14/2023

H Scale: 1" = 200'

V Scale: N/A

Designed By: KGH

Drawn By: DAS

Checked By: KGH

Date: 02/14/2023

Land Development Consultants, Inc.

PLANNING • SURVEYING

www.ldc-inc.com • TEL: (719) 526-8155 • FAX: (719) 526-6646

3698 MAZELAND ROAD • COLORADO SPRINGS, CO 80909

MANLEY SUBDIVISION FILING NO. 2

DRAINAGE PLAN OF EXISTING CONDITIONS

Project No.: 99158

Sheet: 1 of 1

N:\S\1220\08\REDOUBT\08 MANLEY SUB\MANLEY SUB NO 2\DRP\DRP-ILLDRNAGE REV 0224.dwg