Drainage Letter

for:

Lot 1, Meadow Lake Airport, Filing No. 10 (a.k.a. 8136 Cessna Drive, Peyton, CO 80831)

August 1, 2019

Prepared By:

CCP, LLC 14255 Judge Orr Road Peyton, CO 80831

For

Tom Shaffer

PH: (719) 651-9082

Add PCD File No. PPR-19-044

CERTIFICATION STATEMENTS

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the established criteria for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Jessie J. Shaffer Registered Professional Engineer State of Colorado No. 36636	Date
Developer's Statement:	
I, the developer have read and will comply with a report and plan.	ll of the requirements specified in this drainage
Tom C. Shaffer	
Ву:	_
Title: Owner	
Mailing Address: 14255 Judge Orr Road Peyton, CO 80915	
EL PASO COUNTY: Filed in accordance with Section 51.1 of the El Pa amended.	so County Land Development Code, as
Director of Public Works	Date
Conditions:	
Replace El Paso County signature block: Filed in accordance with the requirements of t County Engineering Criteria Manual and Land	he Drainage Criteria Manual, Volumes 1 and 2, El Paso I Development Code as amended.
Jennifer Irvine, P.E. County Engineer / ECM Administrator	 Date
Conditions:	

August 30, 2019

Attn: Jennifer Irvine, P.E. El Paso County Engineer 2880 International Circle Colorado Springs, Colorado 80910

RE: Final Drainage Letter for Lot 1, Meadow Lake Airport, Filing 10, in El Paso County, Colorado.

Dear Ms. Irvine,

The purpose of this letter is to identify existing and proposed conditions for conveyance of storm water flows from the above referenced site to accommodate the planned construction of improvements consisting of a 37.5'x68' pre-engineered metal airplane storage hangar, a 58.65'x15' concrete apron, A 38"x24" elliptical concrete culvert and one 12'x20' concrete driveway together with the associated drainage and grading appurtenances. This report follows the "letter type" report format.

Current El Paso County drainage criteria are incorporated in the grading and drainage plan to mitigate storm water runoff that results from the increase of impervious area attributable to the construction of planned improvements.

General Site Description:

The site is generally located 0.5 miles south east of the intersection of Judge Orr Road and Colorado State Highway 24 in the Falcon area of El Paso County, Colorado (El Paso County Assessor Parcel ID 4304002102). More particularly the site is contained within the NW1/4 of SW1/4 of the NW1/4 of Section 4, Township 13 south, Range 65 west of the 6th Principal Meridian (see Exhibit 1 in the attachments to this letter). The site is bound by an existing dirt road to the north, existing hangar structures to the south, an existing paved taxiway to the west and undeveloped parcels of land to the east. The property is zoned R-4 with a General Aviation Overlay and is 0.208 acres in area.

Hydraulic Methods Used:

Pursuant to the governing drainage criteria, the rational method for prediction of peak storm water runoff was utilized for calculating existing and developed flows from the site in conjunction with the rational stored rate method of detention for detaining storm water flows attributable to the 5-year and 100-year storm events for the developed condition. The Principals of storm water capture for quality related purposes are also addressed.

Revise. Current criteria requires detention pond design for full spectrum detention.

Existing Site/Soils/Drainage Conditions:

Existing ground cover consists of the paved taxiway located on the west side of the site and native prairie/pasture grasses covering the remainder of the site. Existing topology and drainage is depicted in Exhibit 2 (see attachments) which shows existing drainage patterns and site discharge points originating from existing sub-drainage basins from within the site. Sub-basin E-1 depicts the western portion of the site where storm water flows generally drain via sheet flow toward the east traversing the existing native grass and taxiway landscapes and accumulating in a low lying swale east of the existing taxiway. Flows are then conveyed southerly in the swale where they discharge from the site at discharge point DP-1. Sub-basin E-2 shows the north and eastern portion of the site which drains to the existing roadside drainage ditch located along the northern end of the site. This roadside ditch conveys flows easterly where they exit the site at discharge point DP-2. This roadside ditch also conveys flows from the existing developed area to the northwest of the site which is approximately 5 acres in size. Flows from the southeast portion of the site originate in sub-basin E-3 where they travel overland via sheet flow toward the southeast corner of the site and discharge onto adjacent developed and undeveloped property. Flow patterns from sub-basin E-3 do not accumulate at any discernable point(s) of concentration (i.e. pan, gutter, ditch, etc.) prior to leaving the site, however for analytic purposes; flows are shown to exit the site at discharge point DP-3. Existing flows exiting the site at discharge points DP-1, DP-2 and DP-3 all converge in the roadside drainage ditch located along the west side of Cessna Drive at a point approximately 400 feet southeast of the site where they continue along their historic flow path through the greater Solberg Ranch Drainage Basin. Table 1 below summarizes existing flows at their respective discharge locations for both the 5-year and 100year storm events.

Table 1 - Existing Site Discharge

	Pre-D	eveloped
	Dis	charge
Point		(cfs)
	5-Yr	100-Yr
DP-1	0.20	0.48
DP-2	0.02	0.14
DP-3	0.02	0.18

Total Site 0.24 0.80

Data obtained from the Natural Resources Conservation Service (NRCS) soil survey of El Paso County, Colorado shows site soils are comprised of sands and gravels with 100% of the site contained within map unit classification 19 (Columbine gravelly sandy loam). This soils classification is comprised of deep, well drained soils with a hydrologic soils classification of "A" and a depth to groundwater or any restrictive features expected to be greater than 80 inches. Rates of infiltration for this soil type are high to very high with expected rates of saturated transmission (Ksat) ranging from 5.95 to 19.98 in/hr. For detailed soil information refer to Soil Map and Soil Unit Descriptions contained in the attachment to this report.

According to the flood insurance rate map, the site is located in zone "X" (area of minimal flood hazard) and outside of any flood hazard areas. Please reference National Flood Hazard Layer FirMette contained in the attachment to this report.

Proposed Site/Soils/Drainage Conditions:

Proposed topology is depicted in Exhibit 2 which shows proposed drainage patterns and site discharge points originating from sub-drainage basins from within the developed site. Four (4) post development sub-basins were created to accommodate the planned improvements and to mitigate storm water runoff from the developed site. Primary focus of the design was placed on developed flows (in total) exiting the site at or below the pre-developed flow condition such that planned development does not create adverse downstream impacts in the larger Solberg Ranch Drainage basin and, to the extent practical, the design strived to balance developed storm water flows to levels at or below pre-developed conditions at each discharge point from the site in order to minimize the potential for any adverse localized impacts. Table 2 below summarizes developed flows at their respective discharge locations for both the 5-year and 100- year storm events:

Table 2-Developed Site Discharge

	Develo	oed Discharge
Point		(cfs)
	5-Yr	100-Yr
DP-1	0.20	0.39
DP-2	0.03	0.10
DP-3	0.01	0.08
I-Basin	0.32	0.63

Total Exiting Site
(I-Basin not Included) 0.24 0.58

In the developed condition, direct site discharge from sub-basins D-1, D-2 and D-3 exit the site at points DP-1, DP-2 and DP-3 which correspond to the same discharge locations as that of the pre-developed condition. Based on the classification of soils at the site and their ability to infiltrate storm water, a new sub-basin (D-4) was created which encompasses most of the planned improvements, impervious areas and site real estate. Developed discharge from subbasin D-4 is proposed to be conveyed by a combination of trench drains, roof drains and surface flow to an infiltration basin (I-Basin) located at the northwestern corner of the site where full subsurface infiltration of detained flows stemming from the 100 year storm event will occur. The I-Basin is required to be a minimum of 490 cubic feet in volume (see table 3, below), however, as designed and shown on the site drainage and grading plan (see attached), actual volume (exclusive of freeboard) is approximately 607 cubic feet. Due to the sites flat topography, small footprint, and safety concerns associated with above grade structures along an aeronautical taxiway, freeboard for the I-Basin is proposed to be 9.6 inches, however, the 10 foot wide emergency spillway is capable of passing 100-year developed flows at a flow depth of only 2". Discharge from the planned I-Basin is unlikely; however developed flows stemming from a storm event in excess of the 100-year event will exit the site; a) by back pressuring the trench

drain piping and flowing out of the trench drain to the south, and b) by passing over the I-Basin's emergency spillway and discharging into the roadside drainage ditch located along the north end of the site.

A 38"x24" elliptical culvert is proposed to be installed under the northern driveway entrance to convey developed flows in the roadside ditch stemming from the offsite development. Current offsite flows from the existing developed area were calculated to be 21.80 cfs for the 100-year storm event. These flows will continue to be conveyed in the existing roadside drainage ditch and routed through the proposed development where they will continue along their historic path. To mitigate the potential for erosion, the roadside drainage ditch is proposed to be lined with armament (i.e. rip rap) to slow velocities and convey the 100 year storm event in a controlled fashion.

Analysis & Conclusions:

In comparing tables 1 and 2 above, a slight in 5-year event at discharge point DP-2. This is discharge for the 100-year storm event is recompacted downstream. Developed discharges below the pre-developed flow conditions for true for aggregated developed flows leaving

Infiltration test must be provided, not assumed. Update to note an infiltration test of the subgrade must be provided to the design engineer and County prior to installation of the pond.

Redesign may be required if the test shows infiltration rate does not meet the required drain time.

true for aggregated developed flows leaving the entire site.

For developed sub-basin D-4, the rational stored rate method of detention was utilized for determining the minimum detention volume of the I-Basin. Outflow from the proposed I-Basin is in the form of soil infiltration whereby developed flows reporting to the I-Basin percolate into the substrate without leaving the site. Since developed flows leaving the site are at or below historic values, only the 100-year storm event was analyzed for storm water detention requirements as the 5-year storm volume, with respect to the I-basin, becomes irrelevant. A conservative value of 5.95 in/hr was assumed for the infiltration rate based on the lowest expected saturated transmission rate per the NRCS soils information. Utilizing the fundamental rational equation of Q=CIA along with the calculated time of concentration for sub-basin D-4, a family of hydrograph curves, based on the 100-year storm event, were developed with durations equal to or greater than the calculated time of concentration (i.e. 100-year rainfall intensities with durations ranging from 10 to 60 minutes). Multiplying developed peak runoff rates less infiltration by the duration of each curve in the family yields a maximum storage volume that must be detained in order to reduce developed flows to that of the existing conditions. Tables 3a and 3b (below) summarize the results of the volume analysis and indicate that a minimum storage volume of 490 cubic feet must be reserved within the I-basin and a minimum infiltration area (i.e. I-Basin floor area) of 327 square feet must be supplied for a storage depth of 1.5 feet. Per the proposed grading and drainage plan, the I-Basin will capture and hold 607 cubic feet of storm water with 340 square feet of floor area.

Table 3a - Infiltration Basin Volume Required

Den	th of Pond	1.5	Ft			
Infiltration f			in/hr	Minimum Pa	guired Volume	e & Floor Area
C=	, ,		111/1111	iviiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii	quirea voluin	e di Flooi Alea
II -	•					
Area =	0.097	Acres		i ·		
					ĺ	
Storm	Storm	Peak Runoff	Soil Infiltration	I-Basin	Volume of	Minimum Basin
Duration	Intensity	Q = I-Basin Inflow	Rate	Outflow	storage	Floor Area
(min.)	(in/hr.)	(cfs)	(ft/sec)	(cfs)	(CF)	(ft ²)
10	6.93	0.50	0.000138	0.026	286	191
15	5.91	0.43	0.000138	0.033	356	238
20	5.19	0.38	0.000138	0.037	406	271
25	4.62	0.34	0.000138	0.041	442	295
30	4.16	0.30	0.000138	0.043	466	311
35	3.78	0.27	0.000138	0.044	482	321
40	3.44	0.25	0.000138	0.045	490	327
45	3.14	0.23	0.000138	0.045	493	329
50	2.88	0.21	0.000138	0.045	491	327
55	2.64	0.19	0.000138	0.044	484	323
60	2.42	0.18	0.000138	0.044	474	316

Time to empty (hrs):

3.03

Table 3b - Infiltration Basin Volume Proposed

Р	roposed V	olume & Floor Are	a (calculated from	drainage plan)	•
Contour Elevation (ft - MSL)	AREA (ft²)	Average AREA	Elevation Difference (ft)	Incrimental Volume (ft ³)	Cumulative Volume (ft ³)
6839.0	340.6	(1.7)	(1.7)	(,	romine (it)
		340.6	1.0	340.6	340.6
6840.0	340.6				
		369.4	0.5	184.7	525.3
6840.5	398.2				
		409.6	0.2	81.9	607.3
6840.7	421.0				

Total Volume Proposed:

607.3

Mitigation of increased runoff due to site development is not the only criteria that must be considered. Storm water quality must also be addressed. In evaluating the site, full spectrum detention methods were considered for addressing both water quantity and water quality concerns, but due to the sites limited size and lack of ample elevational relief, the site was not considered to be conducive for implementation of full spectrum detention methods. However, water quality concerns are mitigated through the use of the proposed I-Basin which is analogous to that of a sand filter. Detained storm water flows are trapped within the I-Basin and are filtered as the basin drains into the subterranean soil. The upper I-Basin strata which, like a sand filter, acts as a membrane in the capture of contaminants/particulates. Periodic removal and

The design is a retention pond, not detention. Verify water rights.

replacement of the upper strata within the I-Basin will be required to prevent plugging and maintain design infiltration rates as well as to remove accumulated particulates/waste and dispose of it. Operation and maintenance requirements are presented in "I-Basin Operation and Maintenance Manual" attached hereto.

For comparative purposes, the minimum required water quality capture volume (WQCV) for the entire site was calculated using the UDFCD-Detention spreadsheet tool (sand filter) and a developed site composite imperviousness of 54.44% (Refer to Tables 4 and 5 in the attachment). Results show a minimum WQCV of .003 AF (130.79 ft³) and a minimum infiltration area of 88 ft² for a drain time of 12 hrs. The proposed I-Basin volume is well in excess of these minimums. Based on the infiltration rate selected, the proposed I-Basin will empty in approximately 3.03 hrs after the 100-year storm event concludes, however for a basin of this character; drain time is not of critical concern since detained storm water flows are not being conveyed to the surface drainage system after filtration, therefore no consideration for drain time has been specifically evaluated.

Based on the analysis performed, no negative drainage effects will be associated with the construction of the planned improvements. Removal of contaminants through water quality enhancements have been addressed with the implementation of the proposed I-Basin and, as previously discussed above, small additional flows generated from the construction improvements contemplated herein are negligible and are within the margin of error of this report.

This letter has been prepared according to the El Paso County drainage criteria and is being submitted for approval. If you have any question about this submittal, please feel free to call me at 719-661-7924 or email me at jishaffer@elpasotel.net

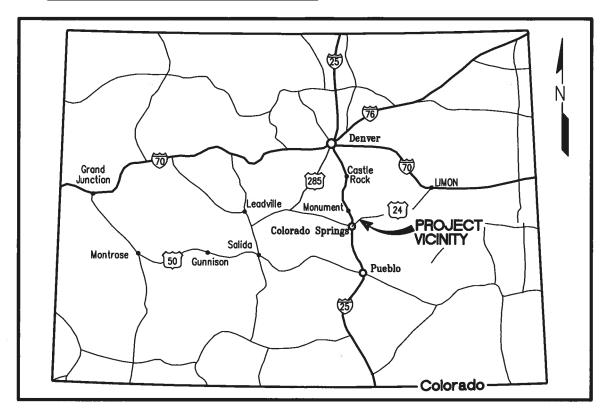
Sincerely,

Jessie J. Shaffer, P.E.

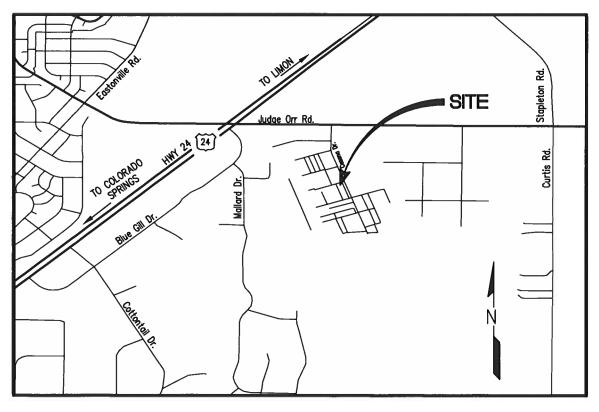
Add a section for the 4-step process (ECM Appendix I Section I.7.2) List each step as a subheading. Under each step provide a narrative on how the specific step was considered/implemented.

ATTACHMENTS

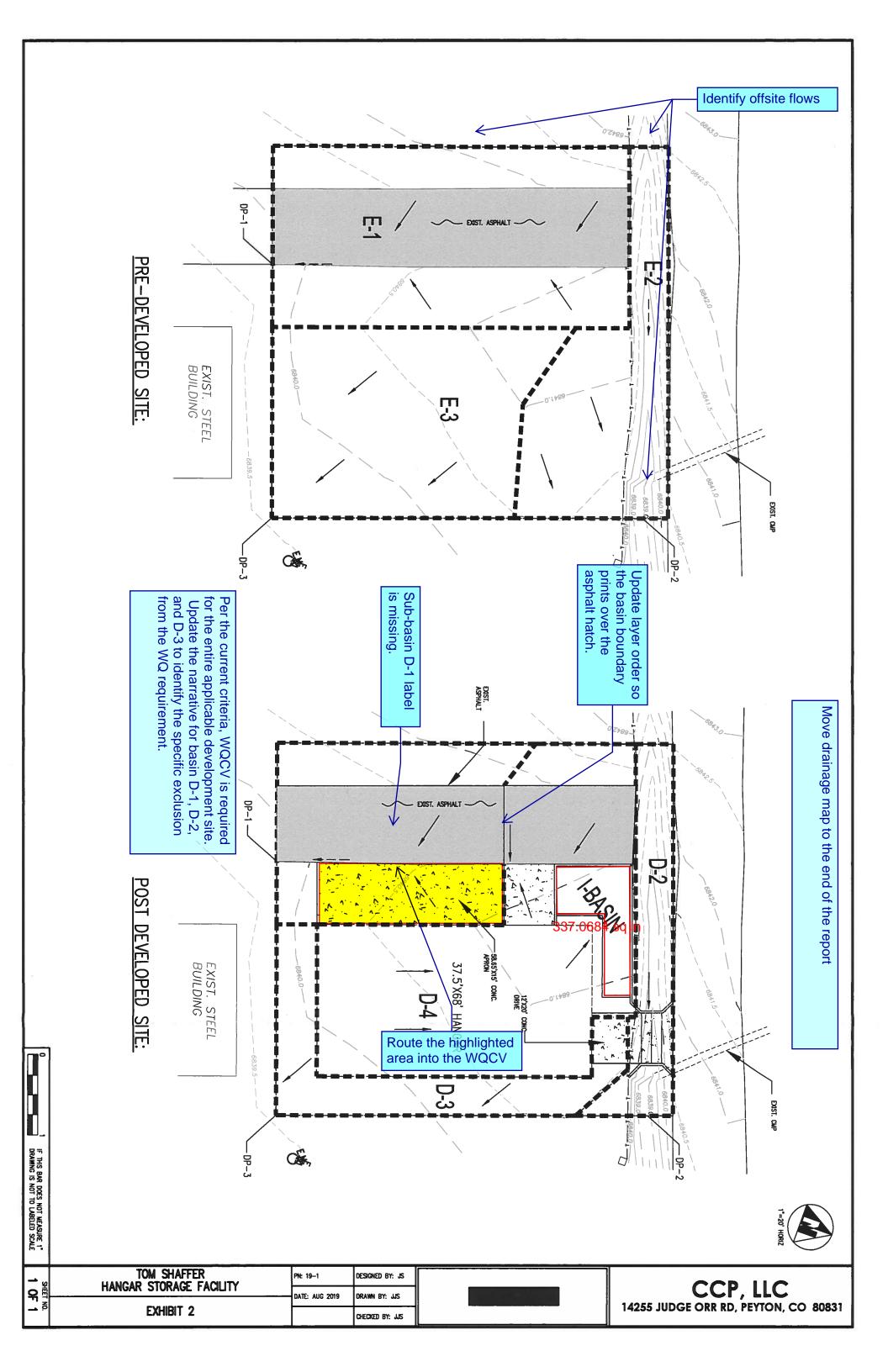
EXHIBIT 1 - SITE LOCATION



VICINITY MAP



LOCATION MAP



38° 56' 7" N

104a 35, 54. M

Meters 2100

<u>\$</u>

Map Scale: 1:24,000 if printed on A landscape (11" $\times 8.5$ ") sheet.

104e 36.5.M

38° 56' 7" N

88

900 Ef

0 1000 2000 4000 Map projection: Web Mercator Comer coordinates: WGS84

ADS

Soil Map—El Paso County Area, Colorado (8136 Cessna Drive)

1040 35.54.M

38° 57 58" N

Judge Orr Rd Curtis Curtis Rd AC TEMPORY ST

38° 57 58" N

1040 36'2" W

Slide or Slip

Sinkhole

Sodic Spot

This product is generated from the USDA-NRCS certified data as distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator Date(s) aerial images were photographed: Sep 8, 2018—May The orthophoto or other base map on which the soil lines were projection, which preserves direction and shape but distorts compiled and digitized probably differs from the background Soil map units are labeled (as space allows) for map scales Source of Map: Natural Resources Conservation Service imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. Albers equal-area conic projection, should be used if more The soil surveys that comprise your AOI were mapped at Please rely on the bar scale on each map sheet for map accurate calculations of distance or area are required. Soil Survey Area: El Paso County Area, Colorado Coordinate System: Web Mercator (EPSG:3857) MAP INFORMATION Version 16, Sep 10, 2018 of the version date(s) listed below. Web Soil Survey URL: Survey Area Data: 1:50,000 or larger. measurements. Special Line Features Streams and Canals Interstate Highways Aerial Photography Very Stony Spot Major Roads Local Roads Stony Spot **US Routes** Spoil Area Wet Spot Other Rails Water Features Transportation Background **MAP LEGEND** W 8 4 Ī Soil Map Unit Polygons Severely Eroded Spot Area of Interest (AOI) Soil Map Unit Points Miscellaneous Water Soil Map Unit Lines Closed Depression Marsh or swamp Perennial Water Mine or Quarry Special Point Features Rock Outcrop **Gravelly Spot** Saline Spot Sandy Spot **Borrow Pit** Lava Flow **Gravel Pit** Area of Interest (AOI) Clay Spot Blowout Landfill 9 0 K 0

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	43.1	14.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	242.3	82.1%
29	Fluvaquentic Haplaquolls, nearly level	9.9	3.4%
Totals for Area of Interest		295.3	100.0%

El Paso County Area, Colorado

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Columbine

Setting

Landform: Flood plains, fan terraces, fans

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to

very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Gravelly Foothill (R049BY214CO)

Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: Landform: Swales

Hydric soil rating: Yes

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 16, Sep 10, 2018

National Flood Hazard Layer FIRMette



104°33'53.20"W 38°56'45.86"N USGS The Nettonal Map: Orthoimagen; Defa refreshed April, 2019. T13S R64W S004 1:6,000 AREA OF MINIMAL PROOD HAZARD eff. 12/7/201 $08041 \cos 5$ T13S R64W S00 EL PASO COUNTY

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

With BFE or Depth Zone AE, AO, AH, VE, AR Without Base Flood Elevation (BFE) SPECIAL FLOOD HAZARD AREAS

of 1% annual chance flood with average depth less than one foot or with drainage 0.2% Annual Chance Flood Hazard, Area Regulatory Floodway

areas of less than one square mile Zone Future Conditions 1% Annual

Area with Flood Risk due to Levee Zone D Area with Reduced Flood Risk due to Chance Flood Hazard Zone X Levee. See Notes. Zone X

OTHER AREAS OF FLOOD HAZARD

NO SCREEN Area of Minimal Flood Hazard Zone X

Area of Undetermined Flood Hazard Zone **Effective LOMRs**

OTHER AREAS

Channel, Culvert, or Storm Sewer

STRUCTURES | 1111111 Levee, Dike, or Floodwall

Cross Sections with 1% Annual Chance Water Surface Elevation

Base Flood Elevation Line (BFE) Coastal Transect

Jurisdiction Boundary Limit of Study

Coastal Transect Baseline Hydrographic Feature **Profile Baseline**

OTHER FEATURES

Digital Data Available

No Digital Data Available

The pin displayed on the map is an approximate point selected by the user and does not represer an authoritative property location.

MAP PANELS

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

authoritative NFHL web services provided by FEMA. This map reflect changes or amendments subsequent to this date and was exported on 7/25/2019 at 1:38:12 PM and does not time. The NFHL and effective information may change or The flood hazard information is derived directly from the become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, FIRM panel number, and FIRM effective date. Map images for legend, scale bar, map creation date, community identifiers, unmapped and unmodernized areas cannot be used for



Identify the design storm

Table 3a - Infiltration Basin Volume Required

Dep	th of Pond	1.5	Ft			
Infiltration	Rate (Ksat)	5.95	in/hr	Minimum Reg	uired Volume 8	k Floor Area
C=	0.744					
Area =	0.097	Acres				
Storm Duration (min.)	Storm Intensity (in/hr.)	Peak Runoff Q = I-Basin Inflow (cfs)	Soil Infiltration Rate (ft/sec)	I-Basin Outflow (cfs)	Volume of storage (CF)	Minimum Basin Floor Area (ft²)
	6.93	0.50		0.026		
10			0.000138		286	191
15	5.91	0.43	0.000138	0.033	356	238
20	5.19	0.38	0.000138	0.037	406	271
25	4.62	0.34	0.000138	0.041	442	295
30	4.16	0.30	0.000138	0.043	466	311
35	3.78	0.27	0.000138	0.044	482	321
40	3.44	0.25	0.000138	0.045	490	327
45	3.14	0.23	0.000138	0.045	493	329
50	2.88	0.21	0.000138	0.045	491	327
55	2.64	0.19	0.000138	0.044	484	323
60	2.42	0.18	0.000138	0.044	474	316

Time to empty (hrs):

3.03

Table 3b - Infiltration Basin Volume Proposed

	Proposed \	Volume & Floor Are	a (calculated from d	rainage plan)	
Contour Elevation (ft - MSL)	AREA (ft²)	Average AREA (ft²)	Elevation Difference (ft)	Incrimental Volume (ft³)	Cumulative Volume (ft ³)
6839.0	340.6	· · · · · · · · · · · · · · · · · · ·			
		340.6	1.0	340.6	340.6
6840.0	340.6				
		369.4	0.5	184.7	525.3
6840.5	398.2				
		409.6	0.2	81.9	607.3
6840.7	421.0				

Total Volume Proposed:

607.3

Current design is full infiltration. There should be no outflow other than the infiltration. Update the worksheet to include a footnote identifying the equations used to obtain the values for the columns in Table 3a and 3b

Soil infiltration rate over time should decay over time.

Table 4-Developed Condition Imperviousness

	Δr	ea of Surface Ch	aracteristics (ft²)	
Sub-Basin	Drives Walks Pavement	Roof	Pasture or Meadow	Total	Composite Imperviousness (%)
D-1	1778	0	787	2565	
D-2	256	0	718	974	1 54 441
D-3	0	0	1279	1279	54.441
D-4	818	2550	879	4247	
Totals	2852	2550	3663	9065	

From Table 6-3 (UDFCD):

Surface Characteristic	% Impervious
Pasture/meadow	2
Paved Street	100
Gravel Street	40
Drives & Walks	90
Roofs	90

Project: Lot 1, Meadow Lake Airport, Filing 10, in El Paso County, Colorado (a.k.a. 8136 Cessna Drive)

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Basin ID: Solberg Ranch Drainage Basin VOLUME EURY WOCY Depth Increment Stage - Storage Width **Example Zone Configuration (Retention Pond)** Stage Length Description (ft) (ft) (ft^2) (acre) (ft^3) (ac-ft) **Required Volume Calculation** Media Surface 0.00 13.3 6.6 88 0.002 Selected BMP Type 0.50 13.3 6.6 RR 0.002 43 0.001 0.21 1.00 13.3 6.6 88 0.002 87 Watershed Area acres 0.002 Watershed Length 98 1.50 13.3 6.6 88 0.002 131 0.003 Watershed Slope 0.005 ft/ft Zone 1 (WQCV) 1.50 13.3 6.6 88 0.002 132 0.003 54.44% Watershed Imperviousness 2.00 13.3 6.6 88 0.002 175 0.004 Percentage Hydrologic Soil Group A 100.0% 2.50 13.3 6.6 88 0.002 0.005 220 Percentage Hydrologic Soil Group B 0.0% 3.00 13.3 6.6 88 0.002 264 0.006 percent Percentage Hydrologic Soil Groups C/D 3.50 13.3 6.6 88 0.002 308 0.007 Desired WQCV Drain Time = 12.0 13.3 6.6 88 0.002 352 hours 4.00 0.008 Location for 1-hr Rainfall Depths = Denver - Capitol Building 4.50 13.3 88 0.002 396 0.009 6.6 Water Quality Capture Volume (WQCV) = 0.003 13.3 88 0.002 440 0.010 acre-feet Ontional User Override 5.00 6.6 Excess Urban Runoff Volume (EURV) 0.013 acre-feet 1-hr Precipitation 5.50 13.3 6.6 88 0.002 485 0.011 2-yr Runoff Volume (P1 = 0.94 in.) = 0.007 0.94 88 0.002 acre-feet inches 6.00 13.3 6.6 529 0.012 5-yr Runoff Volume (P1 = 1.22 in.) = 0.010 1.22 6.50 13.3 88 0.002 573 0.013 acre-feet nches 6.6 10-yr Runoff Volume (P1 = 1.48 in.) = 617 0.012 1,48 7.00 13.3 6.6 88 0.002 acre-feet inches 0.014 25-yr Runoff Volume (P1 = 1.86 in.) 0.017 acre-feet nches 7.50 13.3 6.6 88 0.002 0.015 1.86 661 50-yr Runoff Volume (P1 = 2.18 in.) = 0.022 6.6 88 acre-feet 2.18 8.00 13.3 0.002 705 0.016 inches nches 100-yr Runoff Volume (P1 = 2.52 in.) = 0.027 acre-feet 2.52 8.50 13.3 6.6 88 0.002 749 0.017 500-yr Runoff Volume (P1 = 3.42 in.) = 0.042 13.3 6.6 88 793 acre-feet 3.42 inches 9.00 0.002 0.018 Approximate 2-yr Detention Volume : 0.007 acre-feet 9.50 13.3 6.6 88 0.002 837 0.019 Approximate 5-vr Detention Volume : 10.00 0.009 13.3 6.6 88 0.002 881 0.020 acre-feet Approximate 10-yr Detention Volume 0.012 acre-feet 10.50 13.3 6.6 88 0.002 925 0.021 Approximate 25-yr Detention Volume : 0.016 0.022 acre-feet Approximate 50-yr Detention Volume acre-feet 0.018 Based on the narrative, the BMP is also providing retention for th Approximate 100-vr Detention Volume = 0.021 acre-feet 100yr design storm. Stage-Storage Calculation 0.003 acre-feet Select Zone 2 Storage Volume (Optional) Provide calculation for the 100yr. Tota Select Zone 3 Storage Volume (Optional) is le Total Detention Basin Volume 0.003 Per the UDFCD memo regarding senate bill 15-212, retention pond Initial Surcharge Volume (ISV) ft^3 Initial Surcharge Depth (ISD) N/A is subject to water rights. Contact the state engineer's office for Total Available Detention Depth (Htotal) 1.50 requirements for a full infiltration retention pond or revise the BMP Depth of Trickle Channel (H_{TC}) N/A Slope of Trickle Channel (Stc) N/A ft/ft design to release the flood control runoff instead of infiltration. Slopes of Main Basin Sides (S......) 0 H:V Basin Length-to-Width Ratio (RLW) Initial Surcharge Area (A_{ISV}) Surcharge Volume Length (Lrsv) 0.0 Surcharge Volume Width (WISV) Depth of Basin Floor (H_{FLOOR}) 0.00 Length of Basin Floor (LFLOOR) Width of Basin Floor (W_{FLOOR}) 6.6 Area of Basin Floor (A_{FLOOR}) Volume of Basin Floor (V_{FLOOR}) 0 Depth of Main Basin (H_{MAIN}) Length of Main Basin (LMAIN) 13.3 Width of Main Basin (WMAIN) 6.6 Area of Main Basin (A_{MAIN}) 88 Volume of Main Basin (VMAIN) 132 Calculated Total Basin Volume (V. 1) =

SITE DISCHARGE CALCULATIONS

Existing Conditions:

I5 = -1.5ln(D)+7.583 I100 = -2.52ln(D)+12.735

Total	E-3	E-2	E-1	Sub-Basin					
1692	0	0	1692	Pavement	Walks	Drives	Area of Surface Characteristics (ft ²		
0			0	Roof			ce Character		
7465	3145	2036	2284	Meadow	Pasture or		istics (ft²)		
9065	3053	2036	3976	Total					
	0.082	0.080	0.429	ς			Coef	Compos	
	0.361	0.350	0.610	C ₁₀₀			Coefficient	Composite Runoff	
	83	5	30	(ft)	Length "L"	Overland		Init	
	0.018	0.5	0.024	(ft/ft)	Slope		(min.)	tial/Overla	
	13.79	1.13	4.97	Event			2	Initial/Overland Time (t)	
	10.02	0.83	3.63	Event	100-Year			_	
	N/A	10	20	(Table 6-7)	Coefficient	Conveyance			
	N/A	1.47	3.10	(ft/sec.)	Velocity			Travel Ti	
	N/A	92.5	85	(ft)	Length "L,"	Waterway	(min.)	Travel Time in Waterway (t,)	
	N/A	0.0216	0.024	(ft/ft)	Slope	Waterway		è	
	N/A	1.05	0.46	(min.)		Travel			
	13.79	2.18	5.43	Event	5-Year	i	ŝ	~	
	10.02	1.88	4.09	Event	100-Year		(min.)	;;+t,	
	N/A	N/A	N/A	Event	S-Year		(m	$t_r = (L_{Tot}/180)+10$	1.3 (II)
	N/A	N/A	N/A	Event			(min.)	/180)+10	⁽¹⁾ t, Check
	13.79	5.00	5.43	Event	5-Year		(n	(2) Fi	
	10.02	5.00	5.00	Event	100-Year		iin.)	(2)Final t,	
	0.02	0.02	0.20	(cfs)	ç		S		
	0.18	0.14	0.48	(cfs)	Ω ₁₀₀		Site Discharge		
	ω	2	1	Point	Discharge		rge		

- (1) Applicable to post developed urbanized catchments
 (2) To values of 5 minutes (min.) are used if calculated values yield smaller results

0.81	0.73	Roofs
0.96	0.9	Drives & Walks
0.7	0.59	Gravel Street
0.96	0.9	Paved Street
0.35	0.08	Pasture/meadow
100-year	5-Year	Surface Characteristic
(HSG - Type A)	(HSG-	From Table 6-6:
Runoff Coefficients	Runoff Co	

Developed Conditions:

Site Discharge

	Pre-Developed	eloped	
Point	(cfs)	3	
	5-Yr	100-Yr	
Outfall-1	0.20	0.48	
Outfall-2	20.0	0.14	

Outfall-3 0.02 0.18 Total Site 0.24 0.80

IS = -1.5ln(D)+7.583 I100 = -2.52ln(D)+12.735

Here of Surface Characteristics (ft²) Area of Surface Characteristics (ft²) Composite Runoff Compo	Total	7	D-3	D-2	P	Sub			Τ		
Composite Runoff Initial/Overland Time (t)			L	L		Ë	1		,		
Composite Runoff Initial/Overland Time (t)	2852	818	٥	256	1778	Pavement	Walks	Drives	rea of Surfac		
Composite Runoff Initial/Overland Time (t)	0,550	2550	0	0	0	Roof			e Characteris		
Composite Runoff Initial/Overland Time (t)	2662	879	1279	718	787	Meadow	Pasture or		tics (ft ²)		
Site Runoff Initial/Overland Time (t) Travel Time in Waterway (t) Travel	2506	4247	1279	974	2565	Total			L		
		0.628	0.080	0.296	0.648	Ç			Coeff	Composit	
Travel		0.744	0.350	0.510	0.773	C ₁₀₀			icient	te Runoff	
Travel Time in Waterway (t) t, = t,+t t, Check (Injnal t, min.) t, = (Injnal t, min.) t,		30	5	5	30	(ft)	Length "L,"	Overland		Ini	
Travel Time in Waterway (t) t, = t,+t t, Check (Injnal t, min.) t, = (Injnal t, min.) t,		0.03	0.01	0.5	0.012	(ft/ft)	Slope		(mi	tial/Overla	
Travel Time in Waterway (t) t, = t,+t t, Check (Injnal t, min.) t, = (Injnal t, min.) t,		3.25	4.12	0.89	4.21	Event	5-Year		2	ind Time (t	
Travel Time in Waterway (τ) τ, = τ, τ, Check τ, Check τ, Check τ τ, Check τ τ, Check τ τ τ, ε τ		2.45	3.03	0.65	3.05	Event	100-Year			_	
Travel City Travel City Ci		20	7	10	20	(Table 6-7)		Conveyance			
Travel City Travel City Ci		2.19	0.61	1.47	3.32	(ft/sec.)	Velocity			Travel Ti	
(t) t, = t,+t, (min.) t, Check (min.) (i)Final t, (min.) (i)Final t, (min.) Flow (min.) Waterway Travel Slope 100-Year 5-Year 100-Year 5-Year 100-Year 5-Year 100-Year 5-Year 100-Year 60,9 100-Year 60,0	1	30	138	92.5	35	(ft)		Waterway	(min.)	me in Waterwa	
t _c = t _r +t _q t _c Check (min.) (ni) Final t _q (min.) (min.) Flow (min.) 5-Year 100-Year 5-Year 100-Year 5-Year 100-Year 69.0 Event Event Event Event Event Event Cfs 4.38 3.22 10.36 10.36 5.00 5.00 0.20 1.94 1.70 10.54 10.54 5.00 5.00 0.03 7.91 6.82 10.79 10.79 7.91 6.82 0.01 3.48 2.68 10.33 10.33 5.00 5.00 0.32		0.012	0.0075	0.0216	0.0276	(ft/ft)	Slope	Waterway		ý (t)	
1,4+t		0.23	3.79	1.05	0.18	(min.)	Time	Travel			
t, Check t,= (L _{na/} 180)+10 (min.) Flow t_= (L _{na/} 180)+10 t_= (L _{na/} 180)+10		3.48	7.91	1.94	4.38	Event	5-Year		(T	, t	
ck (min.) Flow (Mi		2.68	6.82	1.70	3.22	Event	100-Year		in.)	4+4	
ck (min.) Flow (Mi		10.33	10.79	10.54	10.36	Event	5-Year		$t_c = \{L_{Tot}$	5′،	
11 t, 10 Flow 100-Year (da) Event cfs 5.00 0.23 0.01 5.00 0.32		10.33	10.79	10.54	10.36	Event	LOO-Year		/180)+10	heck	
11 t, 10 Flow 100-Year (da) Event cfs 5.00 0.23 0.01 5.00 0.32		5.00	7.91	5.00	5.00	Event	5-Year		(a)	H ₍₁₎	
Flow (Q _s) cfs cfs 0.20		5.00	6.82	5.00	5.00	Event	100-Year		in.)	nal t	
- - - ≥ ≥		0.32	0.01	0.03	0.20	슜	ô	Flow			1100 = -2
e Discha Flow (Q ₁₀₀) cfs 0.39 0.10 0.08		0.63	0.08	0.10	0.39		(0,100)	Flow	Site Discharge		$100 = -2.52\ln(D) + 12.735$
Discharge Point 1 2 2 3 1-Basin		I-Basin	3	2	1	Point	Discharge		ige		2.735

(1) Tc values of 5 minutes (min.) are used if calculated values yield smaller results

From Table 6-6:	Runoff Co (HSG -	Runoff Coefficients (HSG - Type A)
Surface Characteristic	5-Year	100-year
Pasture/meadow	0.08	0.35
Paved Street	0.9	0.96
Gravel Street	0.59	0.7
Drives & Walks	0.9	0.96
Roofs	0.73	0.81

	-		
	Developed	ped	
Point	(cfs)	_	
	5-Yr	100-Yr	
1	0.20	0.39	
2	0.03	0.10	
3	0.01	0.08	
I-Basin	0.32	0.63	

Total Site 0.24 0.58

OFFSITE DISCHARGE CALCULATIONS

Existing Offsite Conditions:

Area of Surface Characteristics (Acres)

Composite Runoff
Coefficient

Initial/Overland Time (t,)
(min.)

Travel Time in Waterway to ditch (t,)
(min.)

Travel Time in Roadside Ditch (t_c)
(min.)

 $t_c = t_i + t_i$ (min.)

(1)_{t_c} Check t_c = {L_{Tot}/180}+10 (min.)

⁽²⁾Final t_c (min.)

Flow

Roofs	Drives & Walks	Gravel Street	Paved Street	Pasture/meadow	Surface Characteristic	From Table 6-6:		
0.73	0.9	0.59	0.9	0.08	5-Year	(HSG.	Runoff C	
0.81	0.96	0.7	0.96	0.35	100-year	(HSG - Type A)	Runoff Coefficients	

Notes:

(1) Applicable to post developed urbanized catchments
(2) To values of 5 minutes (min.) are used if calculated values yield smaller results

| Pasture or | Pas

Conveyance Coefficient (Table 6-7)
20
20
20

 Waterway
 Waterway
 Travel
 Conveyance

 Velocity
 Length "L,"
 Slope
 Time
 Coefficient

 (ft/sec.)
 (ft)
 (ft/ft)
 (min.)
 (Table 6-7)

 2.83
 496
 0.02
 2.92
 10

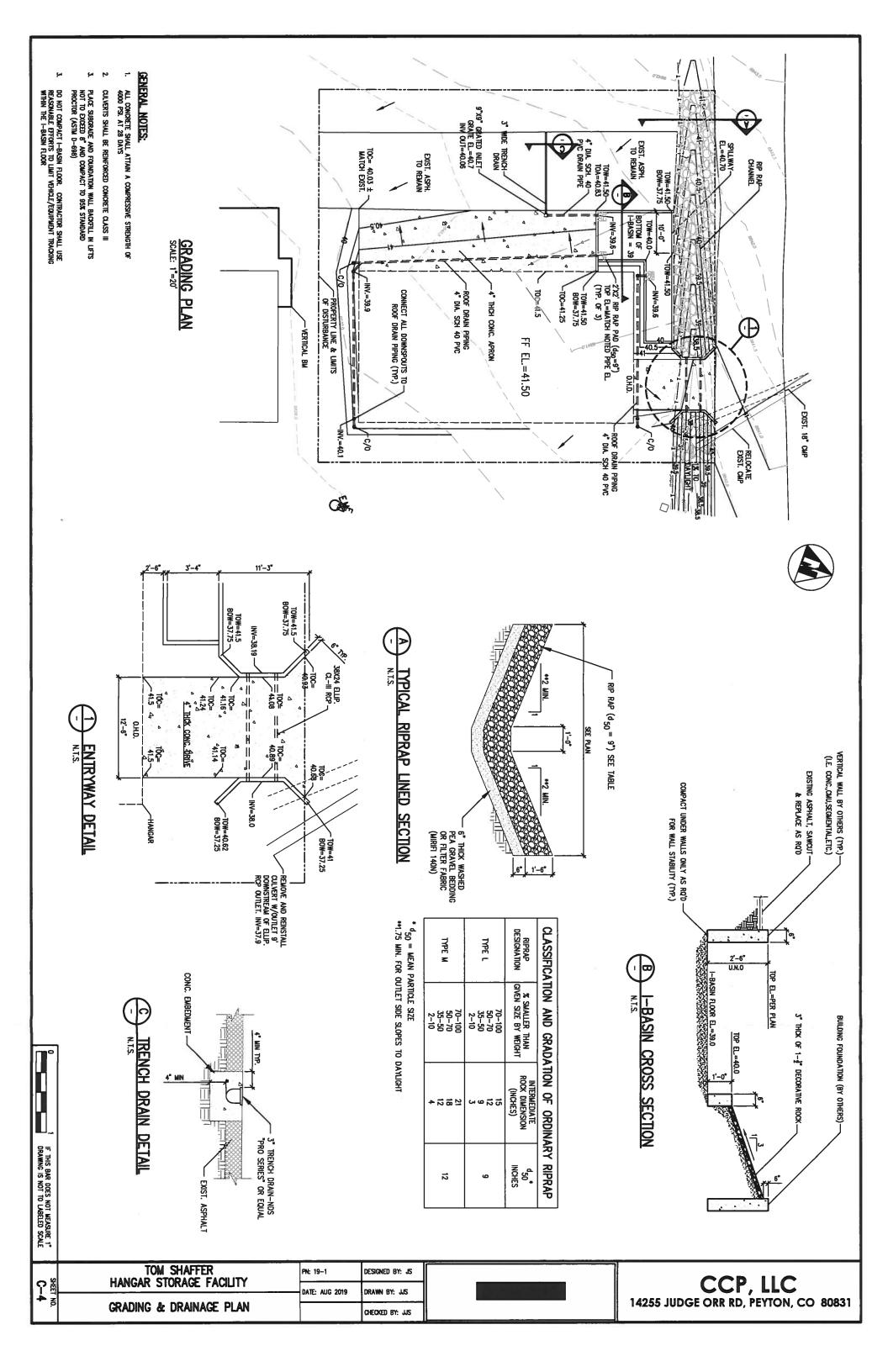
 2.83
 496
 0.02
 2.92
 10

 2.83
 496
 0.02
 2.92
 10

 Velocity (ff)**
 Waterway (ff)**
 Travel (ff)**
 5-Year (100-Year)
 6-Year (100-Year)
 6-Year (100-Year)
 5-Year (100-Year)
 5-Year (100-Year)
 6-Year (100-Year)
 5-Year (100-Year)
 5-Year (100-Year)
 6-Year (100-Year)
 6-Year (100-Year)
 5-Year (100-Year)
 5-Year (100-Year)
 6-Year (100-Year)
 6-Year (100-Year)
 5-Year (100-Year)
 6-Year (100-Year)
 7-Year (100-Year)
 7

| Existing Offsite | Inflow |

t₅ = -1.5ln(D)+7.583 t₁₀₀ = -2.52ln(D)+12.735



I-BASIN OPERATION AND MAINTENANCE MANUAL

August 30, 2019

Remove the O&M and upload as a separate document.

For:

Cor.

1.0 OPERATION AND MAINTENANCE REQUIREMENTS

1.1 Sand Filters – General

1.1.1 Sand filters, like the I-Basin referenced herein have relatively low routine maintenance requirements. Maintenance frequency depends on pollutant loads in runoff, the amount of construction activity within the tributary watershed, the erosion control measures implemented, the size of the watershed, and the design of the facility.

1.2 Inspection

1.2.1 Inspect the detention area once or twice annually following precipitation events to determine if the native filter material is providing acceptable infiltration. Also check for erosion and repair as necessary.

1.3 Debris and Litter Removal

1.3.1 Remove debris and litter from detention area to minimize clogging of the media. Remove debris and litter from the overflow structure.

1.4 Surface Maintenance

1.4.1 Scarify the top 2 inches of the surface of the I-Basin. This may be required once every two to five years depending on observed drain times. After this has been done two or three times, remove and replace the top few inches of the surface of the basin with clean coarse sand (AASHTO C-33) to the original elevation, do not compact with vibratory or heavy equipment. It may also be necessary to remove and reinstall any landscaping rock that may be overlying the permeable surfaces of the I-Basin. Maintain a minimum loose surface depth of 12 inches.

1.5 Erosion and Structural Repairs

1.5.1 Repair basin inlets, outlets, and all other structural components required for the BMP to operate as intended. Repair and vegetate any eroded side slopes as needed following inspection.

Elaborate to define the condition that triggers the need to repair each specific component.

Provide the following:

- Inspections log

Drainage_V1.pdf Markup Summary

dsdlaforce (21)



Subject: Callout Page Label: 1 Author: dsdlaforce

Date: 10/21/2019 11:06:45 AM

Status: Color: Layer: Space: Add PCD File No. PPR-19-044



Subject: Callout Page Label: 2 Author: dsdlaforce

Date: 10/21/2019 11:11:35 AM

Status: Color: Layer: Space: Replace El Paso County signature block: Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E.

Date

County Engineer / ECM Administrator

Conditions:



Subject: Callout Page Label: 3 Author: dsdlaforce

Date: 10/21/2019 11:15:04 AM

Status: Color: Layer: Space: Revise. Current criteria requires detention pond

design for full spectrum detention.



Subject: Callout Page Label: 24 Author: dsdlaforce

Date: 10/21/2019 11:16:05 AM

Status: Color: Layer: Space: Remove the O&M and upload as a separate

document.



Subject: Text Box Page Label: 11 Author: dsdlaforce

Date: 10/21/2019 11:40:23 AM

Status: Color: Layer: Space: Move drainage map to the end of the report



Subject: Callout

Page Label: 11
Author: dsdlaforce

Date: 10/21/2019 11:44:21 AM

Status: Color: Layer: Space: Update layer order so the basin boundary prints over the asphalt hatch.

Statement of the statem

Subject: Callout Page Label: 11 Author: dsdlaforce

Date: 10/21/2019 11:45:12 AM

Status: Color: Layer: Space: Sub-basin D-1 label is missing.



Subject: Callout Page Label: 6 Author: dsdlaforce

Date: 10/21/2019 12:58:14 PM

Status: Color: Layer: Space: Infiltration test must be provided, not assumed. Update to note an infiltration test of the subgrade must be provided to the design engineer and County prior to installation of the pond.

Redesign may be required if the test shows infiltration rate does not meet the required drain ...

time.



Subject: Text Box Page Label: 8 Author: dsdlaforce

Date: 10/21/2019 2:50:44 PM

Status: Color: Layer: Space: Add a section for the 4-step process (ECM

Appendix I Section I.7.2)

List each step as a subheading. Under each step provide a narrative on how the specific step was

considered/implemented.



Subject: Area Measurement

Page Label: 11
Author: dsdlaforce

Date: 10/21/2019 3:04:34 PM

Status: Color: Layer: Space: 337.0684 sq in



Subject: Callout Page Label: 18 Author: dsdlaforce

Date: 10/21/2019 3:21:17 PM

Status: Color: Layer: Space: Identify the design storm



Subject: Callout Page Label: 20 Author: dsdlaforce

Date: 10/21/2019 4:20:07 PM

Status: Color: Layer: Space:

Based on the narrative, the BMP is also providing retention for th 100yr design storm.

Provide calculation for the 100yr.

Per the UDFCD memo regarding senate bill 15-212, retention pond is subject to water rights. Contact the state engineer's office for requirements for a full infiltration retention pond or revise the BMP design to release the flood control runoff

instead of infiltration.



Subject: Callout Page Label: 7 Author: dsdlaforce

Date: 10/21/2019 4:34:02 PM

Status: Color: Layer: Space:

The design is a retention pond, not detention. Verify water rights.



Subject: Callout Page Label: 11

Author: dsdlaforce

Date: 10/21/2019 4:34:48 PM

Status: Color: Layer: Space:

Identify offsite flows



Subject: Callout Page Label: 22 Author: dsdlaforce

Date: 10/21/2019 4:39:28 PM

Status: Color: Layer: Space:

Provide a sub-basin ID and show on the drainage

map



Subject: Text Box Page Label: 25 Author: dsdlaforce

Date: 10/21/2019 4:40:20 PM

Status: Color: Layer: Space:

Provide the following: - Inspections log

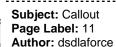


Subject: Callout Page Label: 25 Author: dsdlaforce

Date: 10/21/2019 4:42:01 PM

Status: Color: Layer: Space:

Elaborate to define the condition that triggers the need to repair each specific component.



Date: 10/21/2019 4:57:03 PM

Status: Color: Layer: Space: Route the highlighted area into the WQCV



Subject: Rectangle Page Label: 11 Author: dsdlaforce

Date: 10/21/2019 4:57:29 PM

Status: Color: Layer: Space:



Subject: Text Box Page Label: 11 Author: dsdlaforce

Date: 10/21/2019 5:01:00 PM

Status: Color: Layer: Space: Per the current criteria, WQCV is required for the entire applicable development site. Update the narrative for basin D-1, D-2, and D-3 to identify the specific exclusion from the WQ requirement.



Subject: Text Box Page Label: 18 Author: dsdlaforce

Date: 10/21/2019 5:03:51 PM

Status: Color: Layer: Space: Current design is full infiltration. There should be no outflow other than the infiltration. Update the worksheet to include a footnote identifying the equations used to obtain the values for the columns in Table 3a and 3b

Soil infiltration rate over time should decay over

time.