

MEMORANDUM

To: El Paso County - Stormwater

From: Scott Maier, PE (Ayres Associates)

Date: October 19, 2023 EPC Project No.: PPR2315

Re: Super Star Carwash – Claremont Business Park 2 – Drainage Compliance Letter

Background

Super Star Carwash is planning to construct a carwash located within the Claremont Business Park 2 located at the southwest corner of Marksheffel Road and Meadowbrook Parkway. The site is currently vacant and is 1.5+/- acres.

The proposed development will consist of a 5,000+/- square foot carwash building with access drives, parking areas with vacuum bays, patio areas, and landscaping. This lot was initially contemplated for development as part of the overall development of the Claremont Business Park 2, Filing No. 2 VR 233. The onsite runoff will be collected via onsite private storm sewers and curb and gutter. The runoff is conveyed to an onsite rain garden to provide water quality treatment. Peak runoff detention is not required for this project. The overall development will construct the storm sewer conveyance system to convey runoff from this site to the downstream outfall into the east fork of Sand Creek located southwest of this site and across Meadowbrook Parkway. The purpose of this letter is to demonstrate that the proposed development of the Super Star Carwash is in compliance with the assumptions of Claremont Business Park 2 Filing No. 2. The proposed development will discharge to an 18" RCP storm sewer system along El Jefe Heights that will be constructed as part of the overall development.

Onsite Basins

Basins A1 and A2 are primarily the parking lot for the carwash. The flows from these basins will be collected via curb and gutter to storm sewer inlets and curb cuts that run to the water quality basin. These basins are primarily impervious except for the minor landscape areas.

Basin B1 is the carwash building. The flows from this basin will run (via roof drains to storm sewer) to the water quality basin. This basin is 100% impervious.

Basins A3, A4, A5, and A6 are landscape areas. These landscape areas are collected in area drains that convey the water to the water quality pond. These basins are pervious landscape areas.

Basin OFF is primarily the El Jefe Heights road. This basin is accounted for, and is part of, Basin E1 of the Claremont Business Park 2, Filing No. 2 drainage report.

Runoff Comparison

The proposed development for the Super Star Carwash is part of Basin B within the Claremont Business Park 2 Filing No. 2 prepared by MS Civil Consultants, dated 6/11/23 as shown in the supporting documents. Below is a summary of the anticipated runoff from the overall drainage report.

Comparison Studies	Basin Area (acres)	Time of Concentration (min.)	Design Runoff Coefficient 5-yr	Design Runoff Coefficient 100-yr	Runoff (5 year) (CFS)	Runoff (100 year) (CFS)
Claremont Business Park 2 Filing No. 2 Basins A+B***	1.71	5.0	0.81	0.88	5.9	11.2
Super Star Carwash	1.8	5.0	C=0.44	C=0.67	2.95	10.09

***Runoff noted is for design point 1 within the Claremont Business Park 2 Filing No. 2 drainage study (Not including Basin E1). Basin OFF of the superstar carwash plan is included in the calculations above; however, the runoff from basin off runs into Basin E1 of the Claremont Business Park 2 Filing No. 2. The runoff from basin OFF is a small landscape area and accounts for less than 20% of the site.

The proposed development for the Super Star Carwash will have less designed runoff than those contemplated in the Claremont Business Park 2 Filing No. 2 drainage studies even after adding in the offsite areas along Marksheffel Rd and Meadowbrook Parkway.

Water Quality

Water Quality was not included as part of the improvements for the Claremont Business Park 2 Filing No. 2 overall development and is required to be constructed upon development. The Super Star Carwash proposes to construct a rain garden to serve the water quality requirements for its development. A rain garden is an acceptable method of providing water quality treatment.

	WQCV Required	WQCV Provided	Method
Super Star Carwash Parking Lot and Building	0.022 Ac-Ft	0.03 Ac-Ft	Rain Garden

The rain garden is designed to have an underdrain system and an outfall to the west. As part of the proposed improvements, the site will drain a rain garden in the southern portion of the site.

After treatment the rain garden will enter the overall development storm sewer system to the west and ultimately discharge into the east fork of Sand Creek.

Super Star Carwash will follow the “Four-Step Process” as defined below:

Step 1: Employ Runoff Reduction Practices

The proposed development utilizes reduced pavement areas with the implementation of landscaped islands in the parking lot and around the building.

Step 2: Stabilize Drainage Ways

Proposed drainage ways have been stabilized through the implementation of a concrete drainage pan for water entering the rain garden. A grass drainage swale is located along the east side of the property to capture offsite runoff that enters the property.

Step 3: Provide Water Quality Capture Volume (WQCV)

WQCV is achieved through a rain garden that treats onsite runoff. The rain garden is located at the southern portion of the property and treats building and parking lot runoff as well as offsite runoff that enters the site from the east.

Step 4: Consider Need for Industrial and Commercial BMP's

The proposed site will implement silt fence, construction entrance, concrete washout area and inlet protection to limit erosion and sediment runoff across the site.

Low Impact Development

This development will propose to construct a rain garden as part of the development. The rain garden will provide water quality benefits by providing filtration and some infiltration. The engineered media within the rain garden will provide filtration of the runoff from the site. In addition to the filtration for smaller rain events infiltration will also be a benefit of the rain garden.

Conclusion

The proposed Super Star Carwash development complies with the Claremont Business Park 2 overall drainage study. The Super Star Carwash development will install the proposed rain garden to meet the water quality requirements of the onsite development.

In summary, the Super Star Carwash is in general compliance with the original development assumptions and no additional improvements to the storm sewer system beyond those noted is necessary.

Design Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Scott Maier, P.E. #38122



10/19/23

Date

Owner/Developer Statement:

I, the Owner/Developer had read and will comply with all of the requirements specific in the is drainage report and Plan

TIM VARLEY - Director
[Name, Title]

10/19/23
Date

SSCW 22712 MEADOWBROOK LLC

Business Name SSCW 22712 MEADOWBROOK LLC
960 W BEHREND DR, SUITE 2, PHOENIX, AZ 85027

Address

EI Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volume 1 and 2, EI Paso County Engineering Criteria Manual and Land Development Code as amended.

County Engineer

Approved

By: Gilbert LaForce, P.E.
Engineering Manager

Date: 11/07/2023 5:51:40 PM

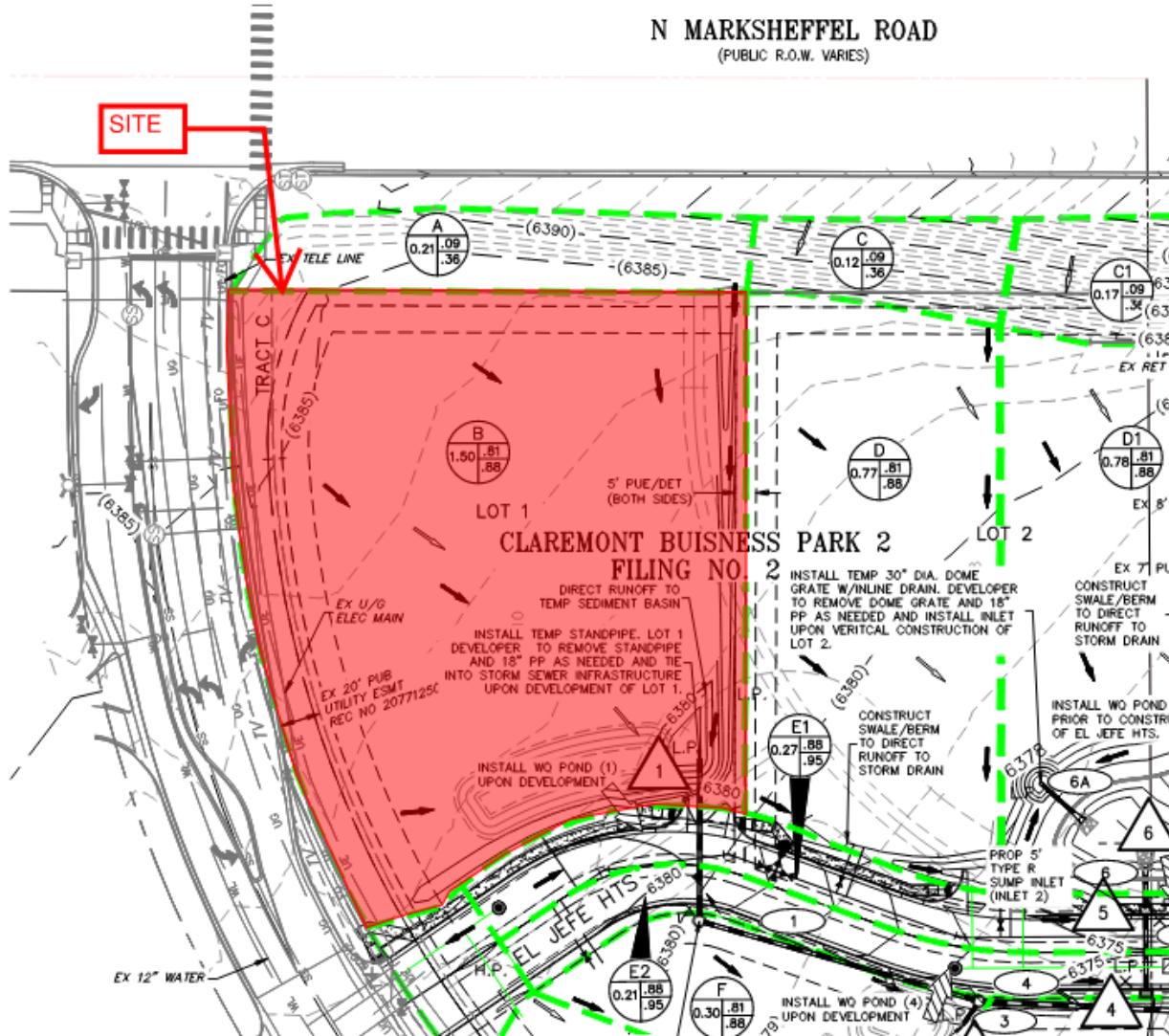
EI Paso County Department of Public Works



Date

Conditions:

Claremont Business Park 2– Supporting Documents



(EXHIBIT ABOVE IS PORTION OF Claremont Business Park 2 Filing No. 2 DRAINAGE PLAN)

FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2
PROPOSED DRAINAGE CALCULATIONS
(Area Runoff Coefficient Summary)

BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	ROOFS 0.73-0.81		COMMERCIAL AREAS 0.81-0.88		LANDSCAPED AREAS 0.16-0.41		GRAVEL STORAGE YARD 0.38-0.59		LIGHT INDUST AREAS 0.53-0.70		PARKS 0.12-0.39		GREENBELTS/AGR. 0.09-0.36		WEIGHTED				
			C ₁	C ₂	C ₃	C ₄	AREA (Acres)	C ₁	C ₂	C ₃	C ₄	AREA (Acres)	C ₁	C ₂	C ₃	C ₄	AREA (Acres)	C ₁	C ₂	C ₃	C ₄
A	9,908.8	0.21	0.10	0.29	0.90	0.96	0.00	0.07	0.16	0.41	0.41	0.21	0.03	0.09	0.36	0.03	0.03	0.09	0.36	0.03	0.09
B	65,204.4	1.50	1.20	0.79	0.83	0.88	0.00	0.23	0.50	0.20	0.00	0.00	0.03	0.12	0.39	0.03	0.03	0.12	0.39	0.03	0.09
C	5,172.3	0.12	0.10	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.41	0.12	0.03	0.09	0.36	0.03	0.03	0.12	0.36	0.03	0.09
D	7457.3	0.17	0.10	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.41	0.17	0.03	0.09	0.36	0.03	0.03	0.17	0.36	0.03	0.09
E	3,220.4	0.07	0.07	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.41	0.17	0.03	0.09	0.36	0.03	0.03	0.17	0.36	0.03	0.09

(EXHIBIT ABOVE IS PORTION OF Claremont Business Park 2 Filing No. 2 Proposed Drainage Calculations-Area Runoff Coefficient Summary)

FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2
PROPOSED DRAINAGE CALCULATIONS

(Area Drainage Summary)

BASIN	STREET / CHANNEL FLOW										TOTAL FLOWS							
	OVERLAND			CHANNEL			TOTAL			CHECK			TOTAL			Q _s		
	AREA ft ²	C ₁	C ₂	C ₃	Height ft	Length ft	T _c (min)	Slope %	Velocity ft/sec	T _i (min)	T _f (min)	Q _{in} ft ³ /sec	Q _{out} ft ³ /sec	Q _{loss} (ft ³ /sec)	Q _s ft ³ /sec	Q _s ft ³ /sec		
A	0.21	0.53	0.59	0.36	0.09	40	5.0	0	0.075	0.0	0.0	5.0	10.2	4.1	0.6	0.6		
B	1.50	0.70	0.81	0.26	0.09	30	1.0	-4.4	240	1.5	5.9	1.8	3.0	4.9	6.0	6.0	6.0	
C	0.12	0.63	0.69	0.36	0.09	40	16.0	3.4	0	0.075	0.0	5.0	10.2	4.1	0.7	0.7		
C1	0.17	0.65	0.69	0.36	0.09	40	27.0	-4.1	0	0.075	0.0	5.0	10.5	4.1	0.7	0.7		
D	0.77	0.79	0.84	0.88	0.81	60	1.2	3.2	250	1.6	5.0	1.7	4.1	5.2	6.7	6.7		
D1	0.78	0.79	0.81	0.88	0.81	60	1.2	3.2	250	1.6	5.0	1.7	4.1	5.2	6.7	6.7		
E1	0.27	0.67	0.88	0.95	0.88	30	0.6	1.7	280	2.8	5.0	1.7	4.1	5.2	8.7	8.7		
E2	0.21	0.67	0.88	0.95	0.88	30	0.6	1.7	280	2.8	5.0	1.7	4.1	5.2	8.7	8.7		
F	0.30	0.79	0.81	0.86	0.81	60	1.2	3.2	150	1.7	5.0	1.7	4.1	5.2	6.7	6.7		
G1	0.27	0.26	0.30	0.52	0.30	30	1.0	5.3	0	0.075	0.0	5.3	10.2	4.1	0.4	0.4		
G2	1.15	0.79	0.81	0.86	0.81	60	0.6	4.1	400	1.6	3.3	7.4	12.6	3.7	3.3	3.3		
H1	0.16	0.63	0.69	0.36	0.09	76	21.0	5.4	0	0.075	0.0	5.4	10.4	4.0	5.1	5.1		
H2	0.40	0.63	0.69	0.36	0.09	100	17.0	7.2	0	0.075	0.0	7.2	10.6	3.7	4.6	4.6		
H3	0.24	0.63	0.69	0.36	0.09	100	17.0	7.2	0	0.075	1.4	0.6	7.2	10.6	3.7	4.6		
H4	0.10	0.63	0.69	0.36	0.09	100	17.0	7.2	0	0.075	0.0	7.2	10.6	3.7	4.6	4.6		
I1	0.55	0.62	0.83	0.90	0.83	100	3.0	3.4	216	2.5%	5.2	1.1	4.1	5.2	8.7	8.7		
I2	0.40	0.77	0.79	0.87	0.72	50	7.0	3.4	364	1.6%	7.0	3.3	5.0	11.7	4.1	4.1		

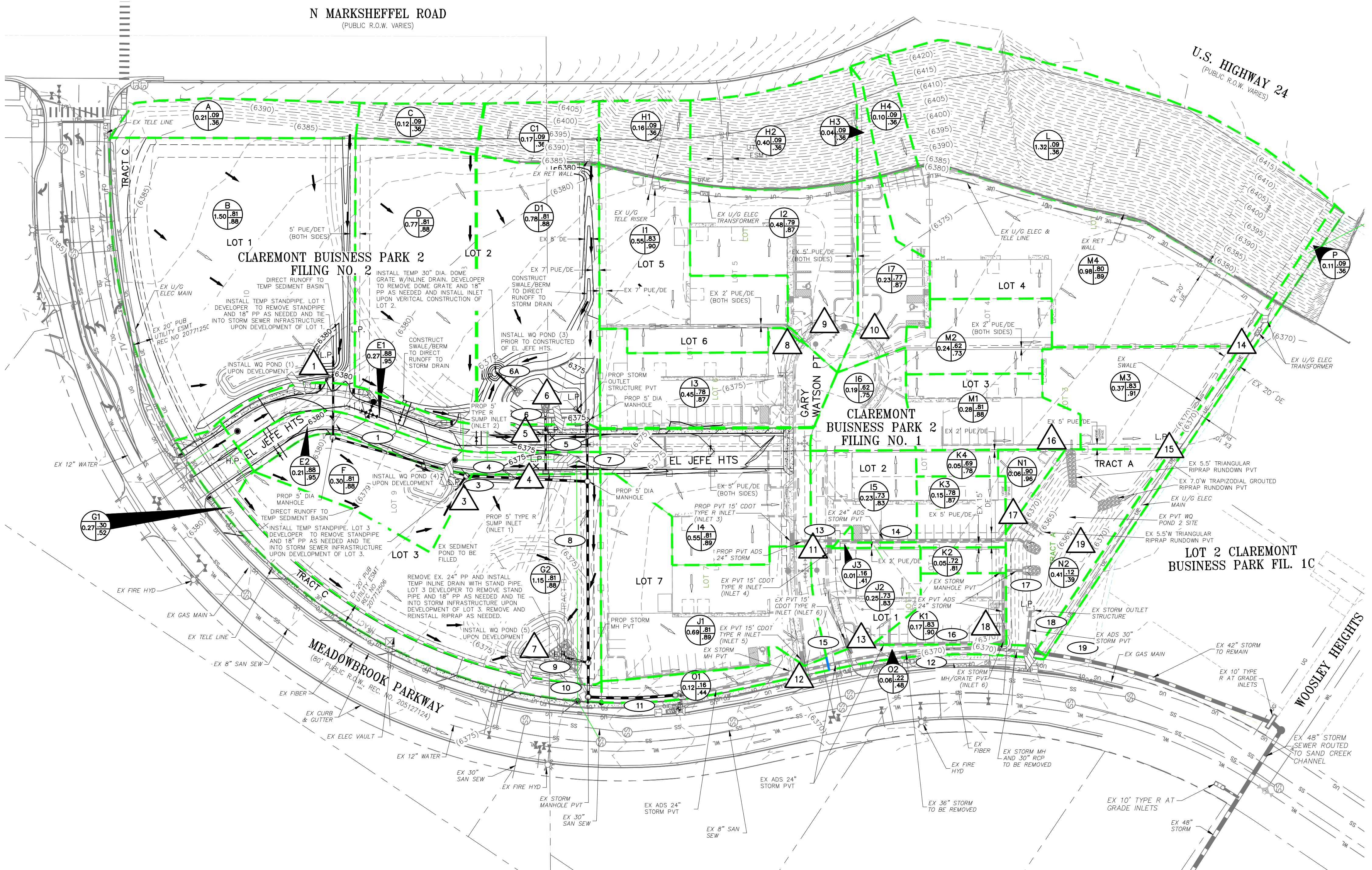
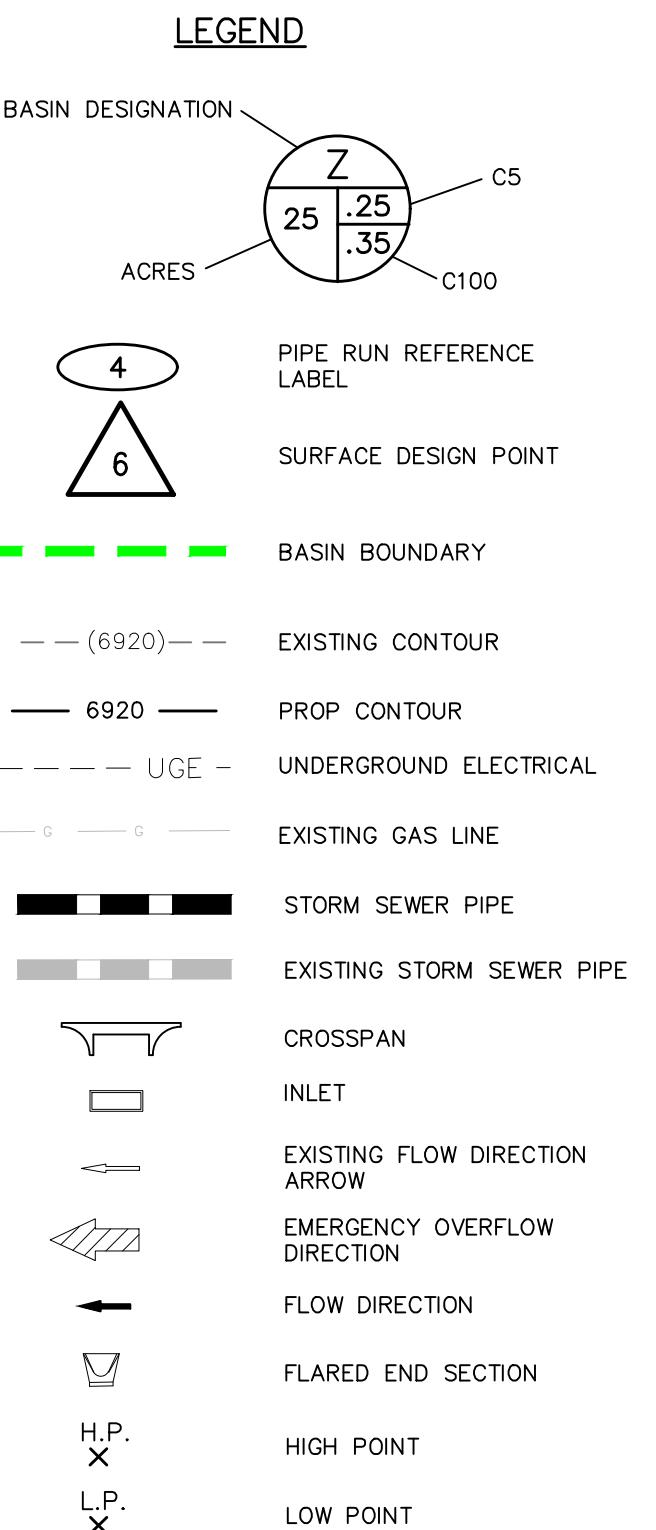
(EXHIBIT ABOVE IS PORTION OF Claremont Business Park 2 Filing No. 2 Proposed Drainage Calculations-Area Drainage Summary)

FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.1

COUNTY OF EL PASO, STATE OF COLORADO

PROPOSED CONDITIONS DRAINAGE MAP

MAY 2023



BASIN SUMMARY			
BASIN	AREA (ACRES)	Q ₅	Q ₁₀₀
A	0.21	0.1	0.7
B	1.50	6.0	10.9
C	0.12	0.1	0.4
C1	0.17	0.1	0.5
D	0.77	3.2	5.9
D1	0.78	3.3	6.0
E1	0.27	1.2	2.2
E2	0.21	1.0	1.7
F	0.30	1.2	2.3
G1	0.27	0.4	1.2
G2	1.15	4.3	7.8
H1	0.16	0.1	0.5
H2	0.40	0.2	1.1
H3	0.04	0.0	0.36
H4	0.10	0.0	0.36
I1	0.55	2.3	4.3
I2	0.48	2.0	3.6
I3	0.45	1.8	3.3
I4	0.55	2.3	4.2
I5	0.23	0.9	1.7
I6	0.19	0.6	1.2
I7	0.23	0.9	1.6
J1	0.69	2.7	5.1
J2	0.25	1.0	1.8
J3	0.01	0.0	0.1
K1	0.17	0.7	1.3
K2	0.05	0.2	0.4
K3	0.15	0.6	1.1
K4	0.05	0.2	0.4
L	1.32	0.5	3.7
M1	0.28	1.2	2.2
M2	0.24	0.8	1.5
M3	0.37	1.6	2.9
M4	0.98	3.5	6.6
N1	0.06	0.3	0.5
N2	0.41	0.2	1.1
O1	0.12	0.1	0.4
O2	0.06	0.1	0.3
P	0.11	0.0	0.3

DESIGN POINT SUMMARY			
DESIGN POINT	Q ₅	Q ₁₀₀	BASIN
1	5.9	11.2	A, B
2			OMITTED
3	1.2	2.3	F
4	1.0	1.7	E2
5	1.2	2.2	E1
6	7.8	14.6	C, D, C1, D1, PR6
7	4.7	8.7	G2
8	2.2	4.3	H1, H2
9	1.8	4.1	H2, I2
10	0.8	1.6	H3, I3
11	8.4	16.7	DP3-5, I3-16
12	2.8	8.1	FB INLET3, J1
13	1.0	5.0	FB INLET4, J2, J3
14	3.8	9.7	H4, L, M4
15	5.3	12.3	DP2, M2, M3
16	1.4	2.5	M1, K4
17	1.1	2.0	K2, K3, N1
18	0.7	1.3	K1
19	19.3	43.7	DP15-17, N2, PR14, PR17

SF WQCV FUTURE PONDS SUMMARY			
PIPE RUN	Q ₅	Q ₁₀₀	PIPE SIZE
1	2.4	5.7	18"
2			NOT USED
3	0.4	1.0	18"
4	3.9	6.7	24"
5	1.0	1.7	18"
6	2.2	3.9	18"
6A	6.0	11.6	18"
7	3.3	4.0	18"
8	6.1	10.7	24"
9	1.3	3.0	18"
10	7.4	13.8	24"/EX24"
11	7.4	13.8	EX 24"
12	7.4	13.8	EX 24"
13	4.2	8.0	EX 15"
14	8.4	16.0	EX 24"
15	2.8	7.8	EX 18"
16	3.7	12.6	EX 24"
17	4.4	13.8	EX 24"
18	13.7	23.8	EX 30"
19	21.1	37.6	EX 42"

STORM SEWER SUMMARY			
PIPE RUN	Q ₅	Q ₁₀₀	PIPE SIZE
1	2.4	5.7	18"
2			FUT POND 1 OUTFALL
3	0.4	1.0	18"
4	3.9	6.7	24"
5	1.0	1.7	18"
6	2.2	3.9	18"
6A	6.0	11.6	18"
7	3.3	4.0	18"
8	6.1	10.7	24"
9	1.3	3.0	18"
10	7.4	13.8	24"/EX24"
11	7.4	13.8	EX 24"
12	7.4	13.8	EX 24"
13	4.2	8.0	EX 15"
14	8.4	16.0	EX 24"
15	2.8	7.8	EX 18"
16	3.7	12.6	EX 24"
17	4.4	13.8	PR15, INLET 6
18	13.7	23.8	PR16, DP18
19	21.1	37.6	DP18, PR12

POND 3 SAND FILTER DETENTION BASIN DATA			
WQ WATER SURFACE EL =	6371.78		
WQ VOLUME =	0.051 AC-FT		
100-YR WATER SURFACE EL=	6373.36		
100-YR VOLUME =	0.153 AC-FT		
SPILLWAY CREST EL =	6375.30		
TOP OF EMBANKMENT EL =	6376.55		
RATIONAL 100-YR INFLOW =	14.8 CFS		
MHFD 100-YR INFLOW =	9.0 CFS		
MHFD 100-YR RELEASE =	4.0 CFS		

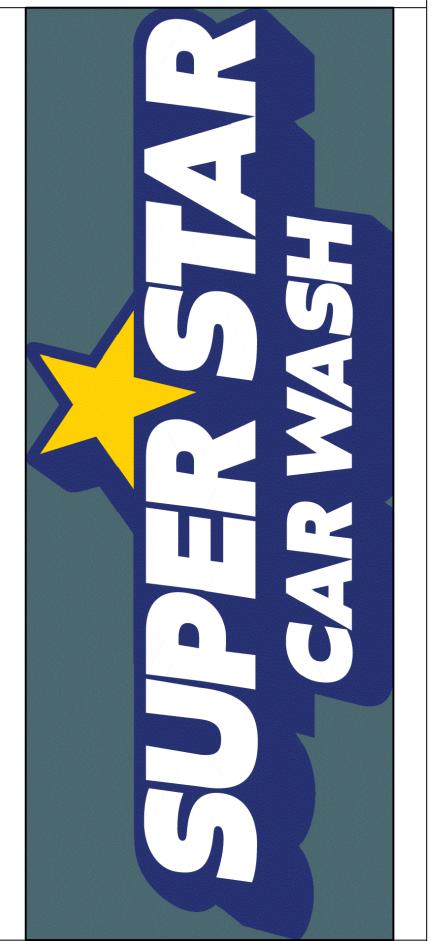
1" = 60'
 0 30 60 120
 Scale in Feet



102 E. PIKES PEAK AVE., 5TH FLOOR
COLORADO SPRINGS, CO 80903
PHONE: 719.955.5485

CLAREMONT BUSINESS PARK 2 FIL. NO.2			
PROP. CONDITIONS DRAINAGE MAP			
PROJECT NO. 10-022A	FILE: \dwg\Eng Exhibits\10020 PDM.dwg		
DESIGNED BY: DLM	DRAWN BY: DLM	SCALE: 1"=60'	DATE: 05-17-2023
DRAWN BY: VAS	CHECKED BY: N/A	VERT: N/A	SHEET 1 OF 1
			PDM01

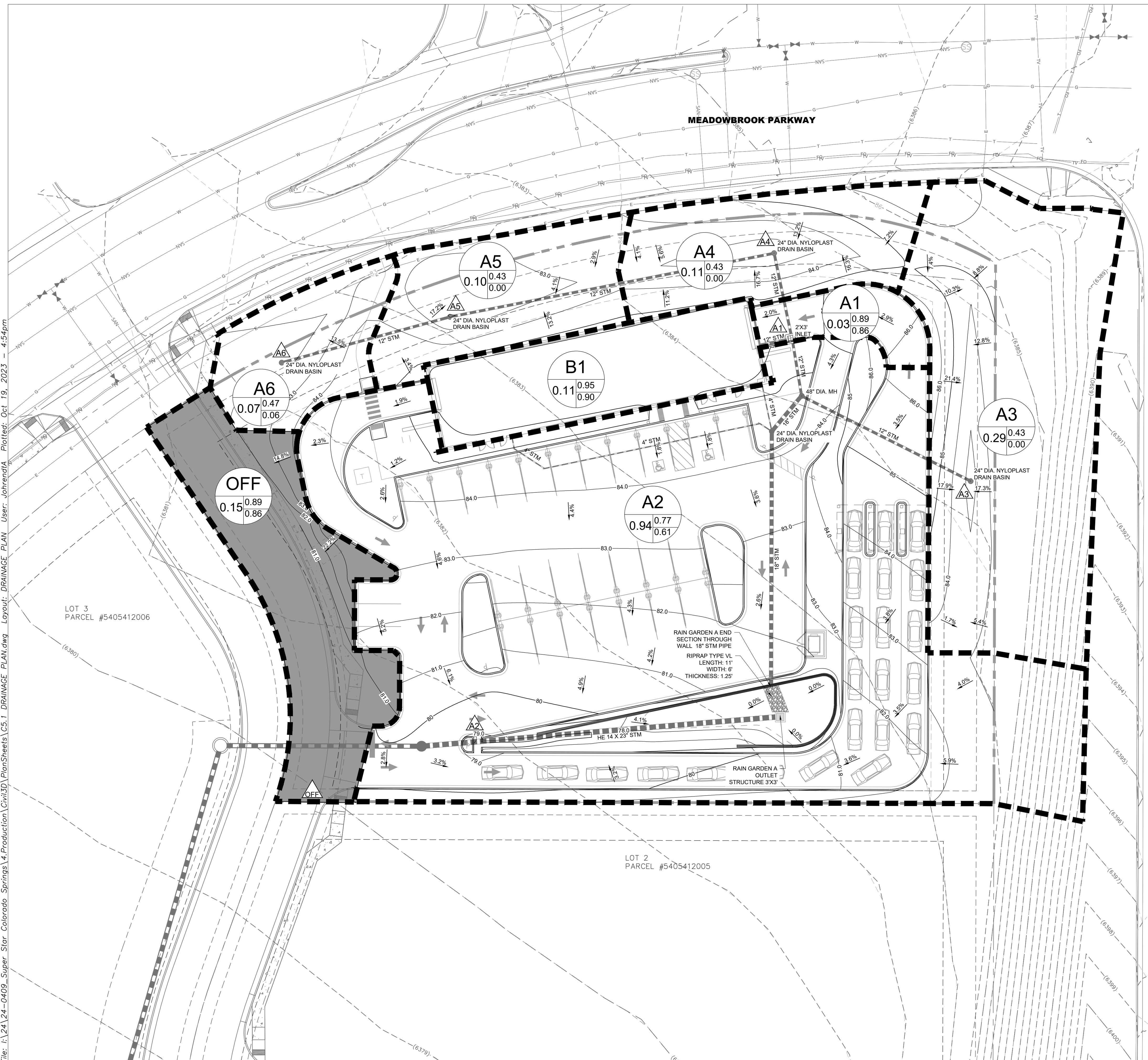
Super Star Carwash Onsite Drainage Calculations



REVISION	DATE
RESUBMITTAL #1	7/25/2023
RESUBMITTAL #2	9/18/2023
RESUBMITTAL #3	10/20/2023

SUPERSTAR CARWASH MEADOWBROOK PKWY COLORADO SPRINGS, CO 80915

DRAINAGE PLAN



Area-Weighted Runoff Coefficient Calculations

Version 2.00 released May 2017

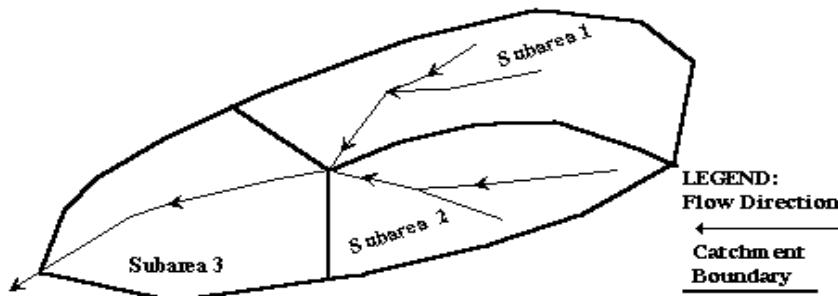
Designer: Scott Maier

Company: Ayres Associates

Date: 9/11/2023

Project: SUPER STAR CAR WASH

Location: MEADOWBROOK, Mesa County



Subcatchment Name

Cells of this color are for required user-input

Cells of this color are for optional override values

Cells of this color are for calculated results based on overrides

See sheet "Design Info" for imperviousness-based runoff coefficient values.

Sub-Area ID	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	Runoff Coefficient, C						
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr
Basin A1	0.03	B	100.0	0.84	0.86	0.86	0.88	0.89	0.89	0.90
Basin A2	0.94	B	73.0	0.58	0.61	0.65	0.71	0.74	0.77	0.80
Basin A3	0.29	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54
Basin A4	0.11	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54
Basin A5	0.10	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54
Basin A6	0.07	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54
Basin B1	0.11	B	100.0	0.84	0.86	0.86	0.88	0.89	0.89	0.90
OFF	0.15	B	74.0	0.59	0.62	0.65	0.71	0.74	0.77	0.81
Total Area (ac)	1.80		Area-Weighted C	0.42	0.44	0.48	0.58	0.62	0.67	0.73
			Area-Weighted Override C	0.42	0.44	0.48	0.58	0.62	0.67	0.73

Calculation of Peak Runoff using Rational Method																																																							
Designer: Scott Maier Company: Ayres Associates Date: 10/19/2023 Project: SUPER STAR CAR WASH Location: MEADOWBROOK, Mesa County				Version 2.00 released May 2017 Cells of this color are for required user-input Cells of this color are for optional override values Cells of this color are for calculated results based on overrides						$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_i^{0.33}}$			Computed $t_c = t_i + t_t$			$t_{\text{minimum}} = 5 \text{ (urban)}$ $t_{\text{minimum}} = 10 \text{ (non-urban)}$			Select UDFCD location for NOAA Atlas 14 Rainfall Depths from the pulldown list OR enter your own depths obtained from the NOAA website (click this link)																																				
										$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$			Regional $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$			Selected $t_c = \max[t_{\text{minimum}}, \min(\text{Computed } t_c, \text{Regional } t_c)]$			1-hour rainfall depth, P1 (in) = <table border="1"><tr><td>2-yr</td><td>5-yr</td><td>10-yr</td><td>25-yr</td><td>50-yr</td><td>100-yr</td><td>500-yr</td></tr><tr><td>0.83</td><td>1.11</td><td>1.38</td><td>1.69</td><td>2.17</td><td>2.58</td><td>3.14</td></tr></table>					2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	0.83	1.11	1.38	1.69	2.17	2.58	3.14	Rainfall Intensity Equation Coefficients = <table border="1"><tr><td>a</td><td>b</td><td>c</td><td>$I(in/hr) = \frac{a * P_i}{(b + t_c)^c}$</td></tr><tr><td>28.50</td><td>10.00</td><td>0.786</td><td></td></tr></table>					a	b	c	$I(in/hr) = \frac{a * P_i}{(b + t_c)^c}$	28.50	10.00	0.786		Q(cfs) = CIA				
2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr																																																	
0.83	1.11	1.38	1.69	2.17	2.58	3.14																																																	
a	b	c	$I(in/hr) = \frac{a * P_i}{(b + t_c)^c}$																																																				
28.50	10.00	0.786																																																					
Subcatchment Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousness	Runoff Coefficient, C					Overland (Initial) Flow Time					Channelized (Travel) Flow Time					Time of Concentration			Rainfall Intensity, I (in/hr)					Peak Flow, Q (cfs)																												
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	Overland Flow Length L_i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S_i (ft/ft)	Overland Flow Time t_i (min)	Channelized Flow Length L_t (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	NRCS Conveyance Factor K	Channelized Flow Slope S_t (ft/ft)	Channelized Flow Velocity V_t (ft/sec)	Channelized Flow Time t_t (min)	Computed t_c (min)	Regional t_c (min)	Selected t_c (min)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr																
Basin A1	0.03	B	100.0	0.84	0.86	0.86	0.88	0.89	0.89	0.90	10.00			0.250	0.48	20.00			0.010	20	2.00	0.17	0.65	9.14	5.00	2.80	3.76	4.68	5.73	7.36	8.75	10.65	0.07	0.10	0.12	0.15	0.20	0.23	0.29																
Basin A2	0.94	B	73.0	0.58	0.61	0.65	0.71	0.74	0.77	0.80	20.00			0.050	2.33	200.00			0.015	20	2.45	1.36	3.69	15.01	5.00	2.80	3.76	4.68	5.73	7.36	8.75	10.65	1.52	2.15	2.84	3.81	5.09	6.30	8.04																
Basin A3	0.29	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54	20.00			0.020	7.07	100.00			0.010	15	1.50	1.11	8.18	27.85	10.00	2.23	3.00	3.73	4.57	5.87	6.98	8.50	0.00	0.00	0.06	0.33	0.56	0.86	1.32																
Basin A4	0.11	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54	20.00			0.020	7.07	30.00			0.020	15	2.12	0.24	7.30	26.39	10.00	2.23	3.00	3.73	4.57	5.87	6.98	8.50	0.00	0.00	0.02	0.13	0.21	0.33	0.50																
Basin A5	0.10	B	0.0	0.00	0.00	0.06	0.25	0.33	0.43	0.54	20.00			0.250	3.07	30.00			0.030	15	2.60	0.19	3.26	26.32	10.00	2.23	3.00	3.73	4.57	5.87	6.98	8.50	0.00	0.00	0.02	0.12	0.20	0.31	0.47																
Basin A6	0.07	B	9.0	0.05	0.06	0.13	0.31	0.38	0.47	0.57	20.00			0.050	4.93	10.00			0.043	15	3.11	0.05	4.98	24.55	10.00	2.23	3.00	3.73	4.57	5.87	6.98	8.50	0.01	0.01	0.03	0.10	0.16	0.23	0.34																
Basin B1	0.11	B	100.0	0.84	0.86	0.86	0.88	0.89	0.89	0.90	20.00			0.020	1.56	50.00			0.020	20	2.83	0.29	1.86	9.26	5.00	2.80	3.76	4.68	5.73	7.36	8.75	10.65	0.25	0.34	0.42	0.53	0.68	0.82	1.01																
OFF	0.15	B	74.0	0.59	0.62	0.65	0.71	0.74	0.77	0.81	10.00				150.00			0.020	20	2.83	0.88		14.33	5.00	2.80	3.76	4.68	5.73	7.36	8.75	10.65	0.25	0.35	0.46	0.61	0.82	1.01	1.29																	

Super Star Carwash Soil Information

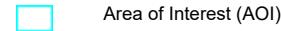
Hydrologic Soil Group—El Paso County Area, Colorado



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

10/25/2022
Page 1 of 4

MAP LEGEND**Area of Interest (AOI)****Soils****Soil Rating Polygons**

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Lines

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Points

	A
	A/D
	B
	B/D

C**C/D****D****Not rated or not available****Water Features**

Streams and Canals

Transportation

Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 20, Sep 2, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	0.0	0.5%
10	Blendon sandy loam, 0 to 3 percent slopes	B	1.4	58.1%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	A	1.0	41.3%
Totals for Area of Interest			2.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Super Star Carwash Onsite Water Quality Basin Calculations

Design Procedure Form: Rain Garden (RG)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

Designer: Scott Maier
Company: Ayres Associates
Date: October 19, 2023
Project: Super Star Carwash
Location: Meadowbrook

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, I_a (100% if all paved and roofed areas upstream of rain garden)</p> <p>B) Tributary Area's Imperviousness Ratio ($i = I_a/100$)</p> <p>C) Water Quality Capture Volume (WQCV) for a 12-hour Drain Time ($WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$)</p> <p>D) Contributing Watershed Area (including rain garden area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume $Vol = (WQCV / 12) * Area$</p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{50.0} \%$ $i = \boxed{0.500}$ $WQCV = \boxed{0.17}$ watershed inches $Area = \boxed{71.874}$ sq ft $V_{WQCV} = \boxed{\quad}$ cu ft $d_6 = \boxed{0.42}$ in $V_{WQCV\ OTHER} = \boxed{965}$ cu ft $V_{WQCV\ USER} = \boxed{\quad}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth (12-inch maximum)</p> <p>B) Rain Garden Side Slopes ($Z = 4$ min., horiz. dist per unit vertical) (Use "0" if rain garden has vertical walls)</p> <p>C) Minimum Flat Surface Area</p> <p>D) Actual Flat Surface Area</p> <p>E) Area at Design Depth (Top Surface Area)</p> <p>F) Rain Garden Total Volume ($V_T = ((A_{Top} + A_{Actual}) / 2) * Depth$)</p>	$D_{WQCV} = \boxed{12}$ in $Z = \boxed{0.00}$ ft / ft $A_{Min} = \boxed{719}$ sq ft $A_{Actual} = \boxed{1080}$ sq ft $A_{Top} = \boxed{1680}$ sq ft $V_T = \boxed{1,380}$ cu ft
<p>3. Growing Media</p>	<p>Choose One</p> <input checked="" type="radio"/> 18" Rain Garden Growing Media <input type="radio"/> Other (Explain): <hr/> <hr/>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One</p> <input checked="" type="radio"/> YES <input type="radio"/> NO $y = \boxed{2.1}$ ft $Vol_{12} = \boxed{965}$ cu ft $D_o = \boxed{11/16}$ in

Design Procedure Form: Rain Garden (RG)

Sheet 2 of 2

Designer: Scott Maier
Company: Ayres Associates
Date: October 19, 2023
Project: Super Star Carwash
Location: Meadowbrook

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?	Choose One <input type="radio"/> YES <input checked="" type="radio"/> NO
6. Inlet / Outlet Control A) Inlet Control	Choose One <input type="radio"/> Sheet Flow- No Energy Dissipation Required <input checked="" type="radio"/> Concentrated Flow- Energy Dissipation Provided
7. Vegetation	Choose One <input checked="" type="radio"/> Seed (Plan for frequent weed control) <input type="radio"/> Plantings <input type="radio"/> Sand Grown or Other High Infiltration Sod
8. Irrigation A) Will the rain garden be irrigated?	Choose One <input type="radio"/> YES <input type="radio"/> NO
Notes: _____ _____ _____	

Super Star Carwash Onsite Inlet Calculations

INLET MANAGEMENT

Worksheet Protected

INLET NAME	Basin A1	Rain Garden Outlet Structure	Basin A4
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	AREA	AREA
Hydraulic Condition	On Grade	Swale	Swale
Inlet Type	CDOT Type C Grate	CDOT Type C (Depressed)	User-Defined

USER-DEFINED INPUT

User-Defined Design Flows

Minor Q _{Known} (cfs)	0.10	2.59	0.00
Major Q _{Known} (cfs)	0.23	9.08	0.33

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	User-Defined	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P ₁ (inches)			

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P ₁ (inches)			

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	0.12	2.59	0.00
Major Total Design Peak Flow, Q (cfs)	0.23	9.08	0.33
Minor Flow Bypassed Downstream, Q _b (cfs)	0.1	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.1	0.0	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>Basin A5</u>	<u>Basin A3</u>	<u>Basin A6</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	AREA	AREA	AREA
Hydraulic Condition	Swale	Swale	Swale
Inlet Type	User-Defined	User-Defined	User-Defined

USER-DEFINED INPUT

User-Defined Design Flows

Minor Q _{Known} (cfs)	0.00	0.00	0.00
Major Q _{Known} (cfs)	0.31	0.86	0.23

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P ₁ (inches)			

Major Storm Rainfall Input

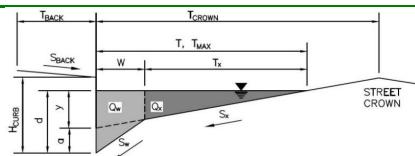
Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P ₁ (inches)			

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	0.00	0.00	0.00
Major Total Design Peak Flow, Q (cfs)	0.31	0.86	0.23
Minor Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Super Star Car Wash - Meadowbrook
Inlet ID: Basin A1**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T_{BACK} =	10.0	ft
S_{BACK} =		ft/ft
n_{BACK} =	0.013	

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H_{CURB} =	6.00	inches
T_{CROWN} =	10.0	ft
W =	1.00	ft
S_x =	0.048	ft/ft
S_w =	0.083	ft/ft
S_o =	0.007	ft/ft
n_{STREET} =	0.013	

Max. Allowable Spread for Minor & Major Storm
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
T_{MAX} =	10.0	10.0
d_{MAX} =	6.0	6.0

Maximum Capacity for 1/2 Street based On Allowable Spread
Water Depth without Gutter Depression (Eq. ST-2)
Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")
Gutter Depression ($d_c = (W * S_x * 12)$)
Water Depth at Gutter Flowline
Allowable Spread for Discharge outside the Gutter Section W ($T - W$)
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
Discharge outside the Gutter Section W, carried in Section T_x
Discharge within the Gutter Section W ($Q_T - Q_x$)
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
Maximum Flow Based On Allowable Spread
Flow Velocity within the Gutter Section
V*d Product: Flow Velocity times Gutter Flowline Depth

	Minor Storm	Major Storm
y =	5.76	5.76
d_c =	1.0	1.0
a =	0.42	0.42
d =	6.18	6.18
T_x =	9.0	9.0
E_o =	0.257	0.257
Q_x =	8.0	8.0
Q_w =	2.8	2.8
Q_{BACK} =	0.0	0.0
Q_T =	10.8	10.8
V =	1.5	1.5
$V*d$ =	0.8	0.8

Maximum Capacity for 1/2 Street based on Allowable Depth
Theoretical Water Spread
Theoretical Spread for Discharge outside the Gutter Section W ($T - W$)
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
Theoretical Discharge outside the Gutter Section W, carried in Section $T_{x,TH}$
Actual Discharge outside the Gutter Section W, (limited by distance T_{CROWN})
Discharge within the Gutter Section W ($Q_d - Q_x$)
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
Total Discharge for Major & Minor Storm (Pre-Safety Factor)
Average Flow Velocity Within the Gutter Section
V*d Product: Flow Velocity Times Gutter Flowline Depth
Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \geq 6"$) Storm
Max Flow Based on Allowable Depth (Safety Factor Applied)
Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)
Resultant Flow Depth at Street Crown (Safety Factor Applied)

	Minor Storm	Major Storm
T_{TH} =	9.7	9.7
$T_{x,TH}$ =	8.7	8.7
E_o =	0.265	0.265
$Q_{x,TH}$ =	7.3	7.3
Q_x =	7.3	7.3
Q_w =	2.6	2.6
Q_{BACK} =	0.0	0.0
Q =	9.9	9.9
V =	1.4	1.4
$V*d$ =	0.7	0.7
R =	1.00	1.00
Q_d =	9.9	9.9
d =	6.00	6.00
d_{CROWN} =	0.00	0.00

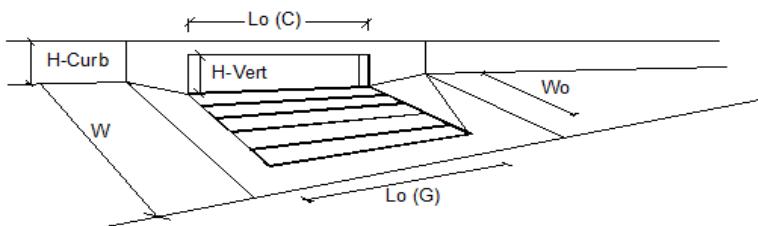
MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm
Q_{allow} =	9.9	9.9

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

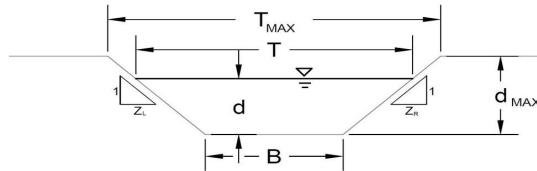
MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		CDOT Type C Grate		
Type of Inlet		MINOR	MAJOR	
Local Depression (additional to continuous gutter depression 'a')		a _{LOCAL} =	CDOT Type C Grate	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	0.0	0.0	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	1	1	
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	2.92	2.92	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _{r-G} =	2.92	2.92	ft
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _{r-C} =	0.50	0.50	
N/A	N/A	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity*		MINOR	MAJOR	
Design Discharge for Half of Street (from Inlet Management)	Q _o =	0.1	0.2	cfs
Water Spread Width	T =	1.6	2.1	ft
Water Depth at Flowline (outside of local depression)	d =	1.3	1.7	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E _o =	0.968	0.867	
Discharge outside the Gutter Section W, carried in Section T _x	Q _x =	0.0	0.0	cfs
Discharge within the Gutter Section W	Q _w =	0.1	0.2	cfs
Discharge Behind the Curb Face	Q _{BACK} =	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _w =	0.07	0.10	sq ft
Velocity within the Gutter Section W	V _w =	1.7	2.1	fps
Water Depth for Design Condition	d _{LOCAL} =	1.3	1.7	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	2.92	2.92	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	-0.487	0.422	
Under No-Clogging Condition		MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V _o =	9.94	9.94	fps
Interception Rate of Frontal Flow	R _f =	1.00	1.00	
Interception Rate of Side Flow	R _x =	0.61	0.56	
Interception Capacity	Q _i =	0.1	0.2	cfs
Under Clogging Condition		MINOR	MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoef =	1.00	1.00	
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	0.50	0.50	
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	1.46	1.46	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	6.91	6.91	fps
Interception Rate of Frontal Flow	R _f =	1.00	1.00	
Interception Rate of Side Flow	R _x =	0.24	0.20	
Actual Interception Capacity	Q _a =	0.0	0.1	cfs
Carry-Over Flow = Q _o ·Q _a (to be applied to curb opening or next d/s inlet)	Q _b =	0.1	0.1	cfs
Curb or Slotted Inlet Opening Analysis (Calculated)		MINOR	MAJOR	
Equivalent Slope S _e (based on grate carry-over)	S _e =	N/A	N/A	ft/ft
Required Length L _T to Have 100% Interception	L _T =	N/A	N/A	ft
Under No-Clogging Condition		MINOR	MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L _T)	L =	N/A	N/A	ft
Interception Capacity	Q _i =	N/A	N/A	cfs
Under Clogging Condition		MINOR	MAJOR	
Clogging Coefficient	CurbCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	N/A	N/A	
Effective (unclogged) Length	L _e =	N/A	N/A	ft
Actual Interception Capacity	Q _a =	N/A	N/A	cfs
Carry-Over Flow = Q _o ·E _{o-GRATE} ·Q _a	Q _b =	N/A	N/A	cfs
Summary		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.0	0.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	0.1	cfs
Capture Percentage = Q _b /Q _o =	C% =	-12	54	%

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Rain Garden Outlet Structure



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

A, B, C, D, or E =	
n =	0.013
S ₀ =	0.0050 ft/ft
B =	75.00 ft
Z ₁ =	100.00 ft/ft
Z ₂ =	100.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:
 Non-Cohesive
 Cohesive
 Paved

	Minor Storm	Major Storm
T _{MAX} =	100.00	100.00
d _{MAX} =	0.20	0.70

Maximum Channel Capacity Based On Allowable Top Width

Maximum Allowable Top Width

Water Depth

Flow Area

Wetted Perimeter

Hydraulic Radius

Manning's n

Flow Velocity

Velocity-Depth Product

Hydraulic Depth

Froude Number

Maximum Flow Based on Allowable Water Depth

	Minor Storm	Major Storm
T _{MAX} =	100.00	100.00
d =	0.13	0.13
A =	10.94	10.94
P =	100.00	100.00
R =	0.11	0.11
n =	0.013	0.013
V =	1.85	1.85
VR =	0.20	0.20
D =	0.11	0.11
Fr =	0.99	0.99
Q _T =	20.3	20.3

Maximum Channel Capacity Based On Allowable Water Depth

Maximum Allowable Water Depth

Top Width

Flow Area

Wetted Perimeter

Hydraulic Radius

Manning's n

Flow Velocity

Velocity-Depth Product

Hydraulic Depth

Froude Number

Maximum Flow Based On Allowable Water Depth

	Minor Storm	Major Storm
d _{MAX} =	0.20	0.70
T =	115.00	215.00
A =	19.00	101.50
P =	115.00	215.01
R =	0.17	0.47
n =	0.013	0.013
V =	2.44	4.91
VR =	0.40	2.32
D =	0.17	0.47
Fr =	1.06	1.26
Q _d =	46.4	498.7

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Top Width Criterion

MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm
Q _{allow} =	20.3	20.3
d _{allow} =	0.13	0.13

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

Top Width

Flow Area

Wetted Perimeter

Hydraulic Radius

Manning's n

Flow Velocity

Velocity-Depth Product

Hydraulic Depth

Froude Number

Q _o =	2.6	9.1
d =	0.04	0.08
T =	82.48	90.68
A =	2.95	6.50
P =	82.48	90.68
R =	0.04	0.07
n =	0.013	0.013
V =	0.88	1.40
VR =	0.03	0.10
D =	0.04	0.07
Fr =	0.82	0.92

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

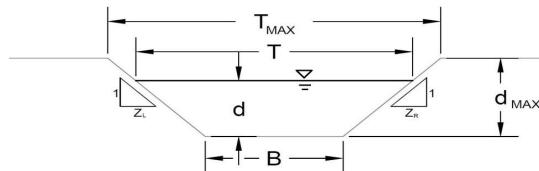
MHFD-Inlet, Version 5.01 (April 2021)
AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Rain Garden Outlet Structure

Inlet Design Information (Input)		Inlet Type =
Type of Inlet	CDOT Type C (Depressed)	
Angle of Inclined Grate (must be <= 30 degrees)		
Width of Grate	W = 3.00 ft	
Length of Grate	L = 3.00 ft	
Open Area Ratio	A _{RATIO} = 0.70	
Height of Inclined Grate	H _B = 0.00 ft	
Clogging Factor	C _f = 0.50	
Grate Discharge Coefficient	C _d = 0.84	
Orifice Coefficient	C _o = 0.56	
Weir Coefficient	C _w = 1.81	
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	MINOR	MAJOR
	d = 1.04	1.08
Grate Capacity as a Weir		
Submerged Side Weir Length	X = 3.00 ft	3.00 ft
Inclined Side Weir Flow	Q _{ws} = 10.0 cfs	10.6 cfs
Base Weir Flow	Q _{wb} = 14.3 cfs	15.2 cfs
Interception Without Clogging	Q _{wi} = 34.4 cfs	36.4 cfs
Interception With Clogging	Q _{wa} = 17.2 cfs	18.2 cfs
Grate Capacity as an Orifice		
Interception Without Clogging	Q _{oi} = 29.0 cfs	29.5 cfs
Interception With Clogging	Q _{oa} = 14.5 cfs	14.8 cfs
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = 14.5 cfs	14.8 cfs
Bypassed Flow	Q _b = 0.0 cfs	0.0 cfs
Capture Percentage = Q _a /Q _o	C% = 100 %	100 %

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A4



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

A, B, C, D, or E =	B
n =	see details below
S _o =	0.0200 ft/ft
B =	4.00 ft
Z _l =	10.00 ft/ft
Z ₂ =	20.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:
 Non-Cohesive
 Cohesive
 Paved

	Minor Storm	Major Storm
T _{MAX} =	15.00	15.00
d _{MAX} =	0.50	0.50

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Top Width Criterion

MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm
Q _{allow} =	0.9	0.9
d _{allow} =	0.37	0.37

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

	Minor Storm	Major Storm
Q _o =	0.0	0.3
d =	0.00	0.23

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

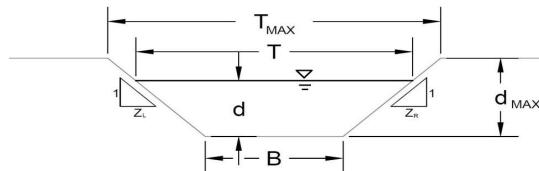
AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A4

Inlet Design Information (Input)																
Type of Inlet	User-Defined															
Inlet Type	User-Defined															
Angle of Inclined Grate (must be <= 30 degrees)																
Width of Grate	$\theta = 0.00$ degrees															
Length of Grate	$W = 2.00$ ft															
Open Area Ratio	$L = 2.00$ ft															
Height of Inclined Grate	$A_{RATIO} = 0.70$															
Clogging Factor	$H_B = 0.00$ ft															
Grate Discharge Coefficient	$C_f = 0.50$															
Orifice Coefficient	$C_d = N/A$															
Weir Coefficient	$C_o = 0.64$															
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	$C_w = 2.05$															
Total Inlet Interception Capacity (assumes clogged condition)																
Bypassed Flow																
Capture Percentage = Q_a/Q_o																
<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>$d =$</td> <td>0.00</td> <td>0.23</td> </tr> <tr> <td>$Q_a =$</td> <td>0.0</td> <td>1.4 cfs</td> </tr> <tr> <td>$Q_b =$</td> <td>0.0</td> <td>0.0 cfs</td> </tr> <tr> <td>$C\% =$</td> <td>100</td> <td>100 %</td> </tr> </tbody> </table>			MINOR	MAJOR	$d =$	0.00	0.23	$Q_a =$	0.0	1.4 cfs	$Q_b =$	0.0	0.0 cfs	$C\% =$	100	100 %
	MINOR	MAJOR														
$d =$	0.00	0.23														
$Q_a =$	0.0	1.4 cfs														
$Q_b =$	0.0	0.0 cfs														
$C\% =$	100	100 %														

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A5



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

A, B, C, D, or E =	B
n =	see details below
S _o =	0.0200 ft/ft
B =	4.00 ft
Z _l =	10.00 ft/ft
Z _r =	10.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:
 Non-Cohesive
 Cohesive
 Paved

	Minor Storm	Major Storm
T _{MAX} =	10.00	10.00
d _{MAX} =	0.50	0.50

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Top Width Criterion

MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm
Q _{allow} =	0.5	0.5
d _{allow} =	0.30	0.30

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

	Minor Storm	Major Storm
Q _o =	0.0	0.3
d =	0.00	0.24

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

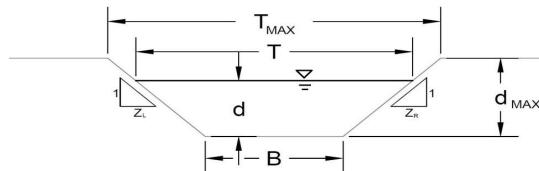
AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A5

Inlet Design Information (Input)																
Type of Inlet	User-Defined															
Inlet Type	User-Defined															
Angle of Inclined Grate (must be <= 30 degrees)																
Width of Grate	$\theta = 0.00$ degrees															
Length of Grate	$W = 2.00$ ft															
Open Area Ratio	$L = 2.00$ ft															
Height of Inclined Grate	$A_{RATIO} = 0.70$															
Clogging Factor	$H_B = 0.00$ ft															
Grate Discharge Coefficient	$C_f = 0.50$															
Orifice Coefficient	$C_d = N/A$															
Weir Coefficient	$C_o = 0.64$															
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	$C_w = 2.05$															
Total Inlet Interception Capacity (assumes clogged condition)																
Bypassed Flow																
Capture Percentage = Q_a/Q_o																
<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>$d =$</td> <td>0.00</td> <td>0.24</td> </tr> <tr> <td>$Q_a =$</td> <td>0.0</td> <td>1.4 cfs</td> </tr> <tr> <td>$Q_b =$</td> <td>0.0</td> <td>0.0 cfs</td> </tr> <tr> <td>$C\% =$</td> <td>100</td> <td>100 %</td> </tr> </tbody> </table>			MINOR	MAJOR	$d =$	0.00	0.24	$Q_a =$	0.0	1.4 cfs	$Q_b =$	0.0	0.0 cfs	$C\% =$	100	100 %
	MINOR	MAJOR														
$d =$	0.00	0.24														
$Q_a =$	0.0	1.4 cfs														
$Q_b =$	0.0	0.0 cfs														
$C\% =$	100	100 %														

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A3



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

A, B, C, D, or E =	B
n =	see details below
S ₀ =	0.0200 ft/ft
B =	4.00 ft
Z ₁ =	5.00 ft/ft
Z ₂ =	5.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:
 Non-Cohesive
 Cohesive
 Paved

	Minor Storm	Major Storm
T _{MAX} =	10.00	10.00
d _{MAX} =	0.50	0.50

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm
Q _{allow} =	1.1	1.1
d _{allow} =	0.50	0.50

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

	Minor Storm	Major Storm
Q ₀ =	0.0	0.9
d =	0.00	0.44

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

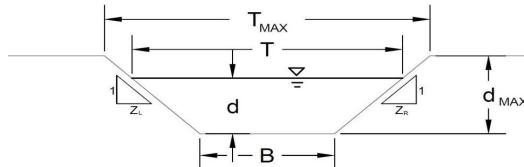
AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A3

Inlet Design Information (Input)																
Type of Inlet	User-Defined															
Inlet Type	User-Defined															
Angle of Inclined Grate (must be <= 30 degrees)																
Width of Grate	$\theta = 0.00$ degrees															
Length of Grate	$W = 2.00$ ft															
Open Area Ratio	$L = 2.00$ ft															
Height of Inclined Grate	$A_{RATIO} = 0.70$															
Clogging Factor	$H_B = 0.00$ ft															
Grate Discharge Coefficient	$C_f = 0.50$															
Orifice Coefficient	$C_d = N/A$															
Weir Coefficient	$C_o = 0.64$															
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	$C_w = 2.05$															
Total Inlet Interception Capacity (assumes clogged condition)																
Bypassed Flow																
Capture Percentage = Q_a/Q_o																
<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>$d =$</td> <td>0.00</td> <td>0.44</td> </tr> <tr> <td>$Q_a =$</td> <td>0.0</td> <td>3.6 cfs</td> </tr> <tr> <td>$Q_b =$</td> <td>0.0</td> <td>0.0 cfs</td> </tr> <tr> <td>$C\% =$</td> <td>100</td> <td>100 %</td> </tr> </tbody> </table>			MINOR	MAJOR	$d =$	0.00	0.44	$Q_a =$	0.0	3.6 cfs	$Q_b =$	0.0	0.0 cfs	$C\% =$	100	100 %
	MINOR	MAJOR														
$d =$	0.00	0.44														
$Q_a =$	0.0	3.6 cfs														
$Q_b =$	0.0	0.0 cfs														
$C\% =$	100	100 %														

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A6



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

A, B, C, D, or E =	B
n =	see details below
S _o =	0.0200 ft/ft
B =	4.00 ft
Z ₁ =	5.00 ft/ft
Z ₂ =	5.00 ft/ft

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

Soil Type:	Max. Velocity (V _{MAX})	Max Froude No. (F _{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:
 Non-Cohesive
 Cohesive
 Paved

	Minor Storm	Major Storm
T _{MAX} =	10.00	10.00
d _{MAX} =	0.50	0.50

Maximum Allowable Top Width of Channel for Minor & Major Storm

Maximum Allowable Water Depth in Channel for Minor & Major Storm

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm
Q _{allow} =	1.1	1.1
d _{allow} =	0.50	0.50

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

O _o =	0.0	cfs
d =	0.00	ft

Water Depth

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

AREA INLET IN A SWALE

Super Star Car Wash - Meadowbrook
Basin A6

Inlet Design Information (Input)		Inlet Type =	User-Defined
Type of Inlet	User-Defined	Inlet Type =	User-Defined
Angle of Inclined Grate (must be <= 30 degrees)			
Width of Grate	θ = 0.00	degrees	
Length of Grate	W = 2.00	ft	
Open Area Ratio	L = 2.00	ft	
Height of Inclined Grate	A _{RATIO} = 0.70		
Clogging Factor	H _B = 0.00	ft	
Grate Discharge Coefficient	C _f = 0.50		
Orifice Coefficient	C _d = N/A		
Weir Coefficient	C _o = 0.64		
	C _w = 2.05		
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)			
Total Inlet Interception Capacity (assumes clogged condition)			
Bypassed Flow			
Capture Percentage = Q _a /Q _o			
	MINOR		MAJOR
	d = 0.00	cfs	
	Q _a = 0.0	1.2	
	Q _b = 0.0	0.0	
	C% = 100	100	
	%		

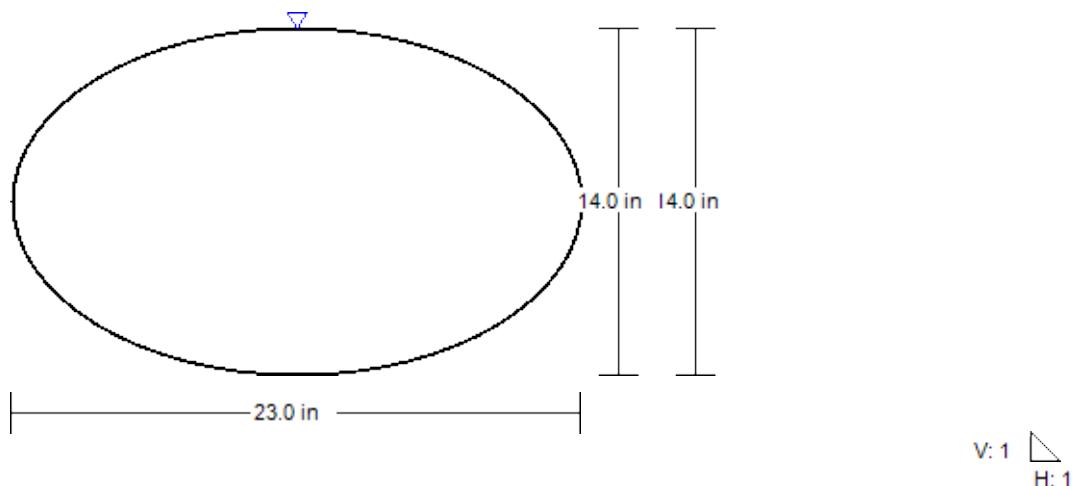
Cross Section for RG Discharge

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.013
Channel Slope	0.005 ft/ft
Normal Depth	14.0 in
Rise	14.0 in
Span	23.0 in
Discharge	7.15 cfs



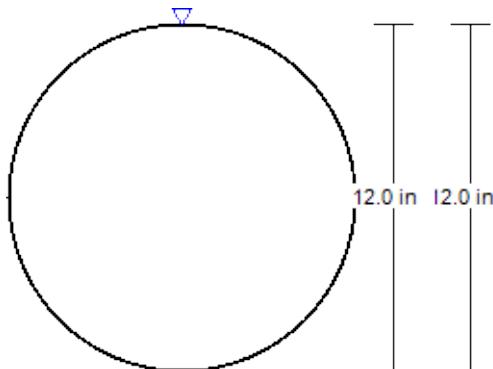
Cross Section for A3-MANHOLE

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.010
Channel Slope	0.020 ft/ft
Normal Depth	12.0 in
Diameter	12.0 in
Discharge	6.55 cfs



V: 1 
H: 1

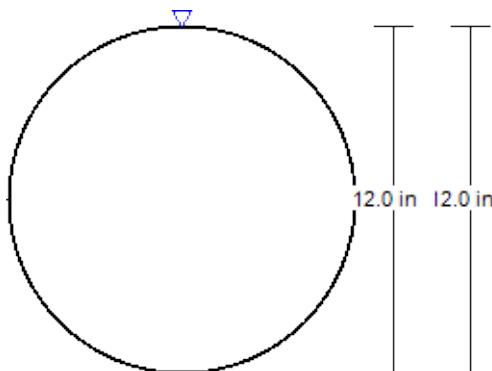
Cross Section for A6-A5

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.010
Channel Slope	0.005 ft/ft
Normal Depth	12.0 in
Diameter	12.0 in
Discharge	3.27 cfs



V: 1 H: 1

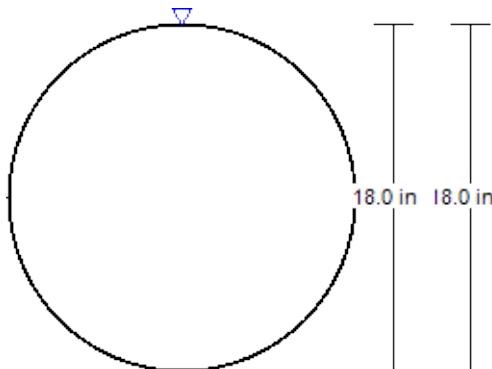
Cross Section for MANHOLE-RG

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.010
Channel Slope	0.005 ft/ft
Normal Depth	18.0 in
Diameter	18.0 in
Discharge	9.66 cfs



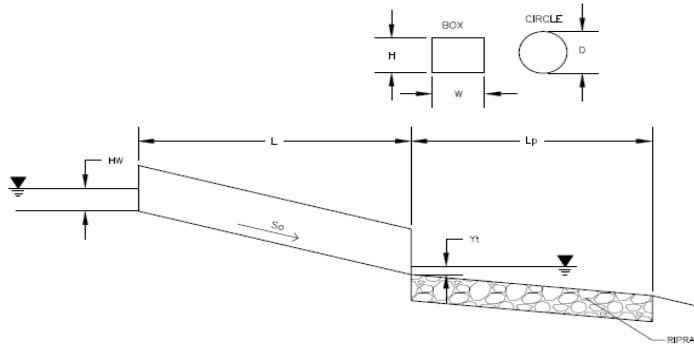
V: 1 H: 1

DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.00 (May 2020)

Project: Super Star Carwash Riprap

ID:



Soil Type:

- Choose One:
 Sandy
 Non-Sandy

Design Information:

Design Discharge

$Q = \boxed{6}$ cfs

Circular Culvert:

Barrel Diameter in Inches

$D = \boxed{18}$ inches

Inlet Edge Type (Choose from pull-down list)

Grooved Edge in Headwall

OR:

Box Culvert:

Barrel Height (Rise) in Feet

OR
 $H \text{ (Rise)} = \boxed{\text{ }}$ ft

Barrel Width (Span) in Feet

$W \text{ (Span)} = \boxed{\text{ }}$ ft

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

$\# \text{ Barrels} = \boxed{1}$

Inlet Elevation

$\text{Elev IN} = \boxed{6378.16}$ ft

Outlet Elevation **OR** Slope

$\text{Elev OUT} = \boxed{6377.7}$ ft

Culvert Length

$L = \boxed{101.4}$ ft

Manning's Roughness

$n = \boxed{0.012}$

Bend Loss Coefficient

$k_b = \boxed{0}$

Exit Loss Coefficient

$k_e = \boxed{1}$

Tailwater Surface Elevation

$Y_t, \text{Elevation} = \boxed{\text{ }}$ ft

Max Allowable Channel Velocity

$V = \boxed{5}$ ft/s

Calculated Results:

Culvert Cross Sectional Area Available

$A = \boxed{1.77}$ ft²

Culvert Normal Depth

$Y_n = \boxed{1.00}$ ft

Culvert Critical Depth

$Y_c = \boxed{0.95}$ ft

Froude Number

$Fr = \boxed{0.90}$

Entrance Loss Coefficient

$k_e = \boxed{0.20}$

Friction Loss Coefficient

$k_f = \boxed{1.57}$

Sum of All Loss Coefficients

$k_s = \boxed{2.77}$ ft

Headwater:

Inlet Control Headwater

$HW_1 = \boxed{1.38}$ ft

Outlet Control Headwater

$HW_0 = \boxed{1.26}$ ft

Design Headwater Elevation

$HW = \boxed{6379.54}$ ft

Headwater/Diameter OR Headwater/Rise Ratio

$HW/D = \boxed{0.92}$

Outlet Protection:

Flow/(Diameter^{2.5})

$Q/D^{2.5} = \boxed{2.18}$ ft^{0.5}/s

Tailwater Surface Height

$Y_t = \boxed{0.60}$ ft

Tailwater/Diameter

$Yt/D = \boxed{0.40}$

Expansion Factor

$1/(2\tan(\Theta)) = \boxed{5.50}$

Flow Area at Max Channel Velocity

$A_t = \boxed{1.20}$ ft²

Width of Equivalent Conduit for Multiple Barrels

$W_{eq} = \boxed{-}$ ft

Length of Riprap Protection

$L_p = \boxed{5}$ ft

Width of Riprap Protection at Downstream End

$T = \boxed{3}$ ft

Adjusted Diameter for Supercritical Flow

$Da = \boxed{-}$ ft

Minimum Theoretical Riprap Size

$d_{50, \text{min}} = \boxed{3}$ in

Nominal Riprap Size

$d_{50, \text{nominal}} = \boxed{6}$ in

MHFD Riprap Type

Type = VL

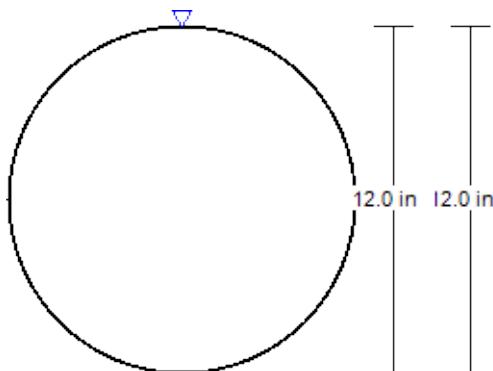
Cross Section for A4-A1

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.010
Channel Slope	0.005 ft/ft
Normal Depth	12.0 in
Diameter	12.0 in
Discharge	3.27 cfs



V: 1 H: 1

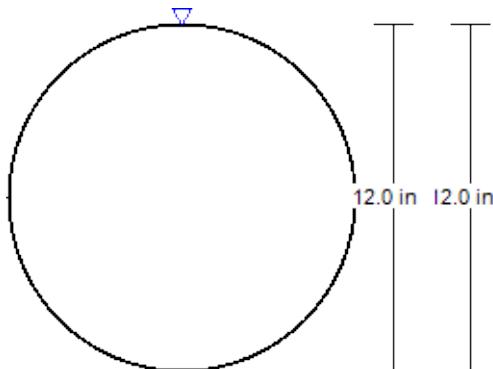
Cross Section for A5-A4

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.010
Channel Slope	0.005 ft/ft
Normal Depth	12.0 in
Diameter	12.0 in
Discharge	3.27 cfs



V: 1 H: 1