PRELIMINARY/FINAL DRAINAGE REPORT

FOR

SOUTH ACADEMY BUSINESS CENTER

Prepared For: 10230 Hall Boulevard, LLC PO Box 38014 Colorado Springs, CO 80937

Prepared By: Associated Design Professionals, Inc. 3520 Austin Bluffs Parkway, Suite 102 Colorado Springs, CO 80918 (719) 266-5212 Project No. 161103 1/25/18 PCD Project No 17-004





ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the city/county for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Michael A. Bartusek, P.E. #23329

DEVELOPER'S STATEMENT:

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Mr Michael Turley

Title: Manager

Address: 10230 Hall Boulevard, LLC PO Box 38014 Colorado Springs, CO 80937

EL PASO COUNTY:

Filed in accordance with the El Paso County Land Development Code; the Drainage Criteria Manual, Volumes 1 and 2; and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E., County Engineer ECM Administrator Conditions: Date



PROJECT DESCRIPTION

This proposed project is contained within a new subdivision named the South Academy Business Center. This currently vacant lot consists of 7.60 acres. It is located in the Southeast Quarter of Section 3, Township 15 South, Range 66 West of the Sixth Principal Meridian, County of El Paso, State of Colorado. The site is located on a narrow strip of land which is bordered on the west by State Highway 85/87 and on the east by the Denver and Rio Grande Western Railroad. Its northern boundary is situated on the south boundary line of the South Academy Boulevard right-of-way.

FLOODPLAIN STATEMENT

This site does not lie within a designated 100-year floodplain as delineated on LOMR No. 03-08-0318P, dated April 9, 2004. It is located within the West Little Johnson drainage basin. The drainage basin map shows a split in the property between the Little Johnson and West Little Johnson Basins. However, field verification revealed that all of the property was located within the West Little Johnson Basin.

SOILS

The soils on the northern site are classified as Blakeland loamy sand by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "A". The soils on the proposed site are classified as Nunn clay loam by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "C".

METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with *City/County Drainage Criteria Manual*. The Rational Method for computation of runoff was used for determining on-site flows.

Q = cia

Where

- Q = maximum rate of runoff in cubic feet per second
- c = runoff coefficient representing drainage area characteristics
- i = average rainfall intensity, in inches per hour, for the duration required for the runoff to become established
- a = drainage basin size in acres

Off-site flows were determined using the TR20 hydrologic program for project hydrology by the Soil Conservation Service.

EXISTING DRAINAGE CHARACTERISTICS

This previously unplatted site was included in the *Little Johnson/West Little Johnson Drainage Basin Planning Study* prepared by Simons, Li & Associates in 1987. Much of the land north of the proposed project lies within either the Rocky Mountain Materials property or the Stephen Schnurr Living Trust. The Rocky Mountain property encompasses approximately 42 acres of the 54.5-acre basin. The Stephen Schnurr Living Trust owns the 4.6 acres just north of the site. Flows from these properties are released at historic levels onto the site to its south. This vacant land is just north of the proposed project and is covered with rangeland grasses. The tributary area slopes generally southwest at an average slope of one percent. The existing runoff is contained within a broad drainage swale located near the existing railroad tracks.



According to the analysis performed by Simons, Li & Associates, the runoff produced by the entire drainage basin along SH 85/87 would result in no flow for the ten-year storm event and one cfs for the 100-year storm event. The low runoff amounts were due to the Type "A" soils and the long overland flow times. These flow travel toward the railroad ditch east of the parcel.

An analysis of the site using the Rational Method produced the following flow rates: Sub-Basin A, which drains toward the interior of the parcel and produces 1.6 cfs for the five-year storm and 9.2 cfs for the 100-year storm; Sub-Basin B, which drains to a ditch along SH 85/87 produces a flow of 0.4 cfs for the five-year storm and 2.1 cfs for the 100-year storm. The total flow tributary to the site is 1.9 cfs for the five-year storm and 11.1 cfs for the 100-year storm.

DEVELOPED DRAINAGE CHARACTERISTICS

The proposed development of 7.6 acres will be storage facility comprised of 8' x 40' trailers placed on the site with loose gravel placed over the site.

Runoff from Sub-Basin A will be directed in a southeasterly direction toward the south property line. Based on the proposed developed conditions, Sub-Basin A will produce flows of 4.7 cfs for the five-year storm and 14.3 cfs for the 100-year storm. The detained flows from the Water Quality/Detention Basin will be 1.0 cfs for the five-year storm and 5.0 cfs for the 100-year storm. These detained flows will be directed into an existing grass swale just east of the basin. The existing broad, grassed swale continues flowing to the east at a 0.7% slope with 10:1 side slopes. The 100 year outflow will produce a flow depth of 0.6 ft and a velocity of 1.5 fps.

Runoff from Sub-Basin B will increase slightly to 0.4 cfs for the five-year storm and 2.3 cfs for the 100-year storm. The total flow tributary to the site is 1.4 cfs for the five-year storm and 7.2 cfs for the 100-year storm.

WATER QUALITY/DETENTION REQUIREMENTS

In accordance with current NPDES, stormwater quality BMPs will be provided for this site when it is developed. Based on actual calculations, the commercial development of the site will produce an imperviousness of 48 percent. The water quality component is accomplished by a 2.42' deep 0.703 acre foot private extended detention facility located at the south end of the project. The facility will be maintained by the owner

DRAINAGE BASIN FEE

The proposed development is located within the West Little Johnson drainage basin. The 2017 drainage basin fee calculation is as follows:

Impervious Coverage	=	48%	
Area Subject to Fee	=	0.48 x 7.6 acres = 3.648 acre	
West Little Johnson Basin Fee	=	\$1,072/acre	
Drainage Basin Fee	=	\$1,072 x 3.648 = \$3,911	

There are no associated Bridge Fees for the West Little Johnson drainage basin.



PRIVATE DRAINAGE FACILITIES

Item	Unit	Quantity	Unit Cost	Total Cost
18" RCP FES	EA	1	\$500	\$ 600
18" HDPE	LF	15	\$84	\$ 1,260
Detention Outlet Structure	EA	1	\$3,000	\$ 5,000
Emergency Spillway	EA	1	\$1,000	<u>\$ 1,500</u>
			Sub-Total	\$8,360
		15% Conting	ency & Engineering	<u>\$ 1,254</u>
			TOTAL	\$9,614

CONCLUSION

Storm runoff from this property will not adversely affect downstream properties or facilities. Grading will take place on the property; therefore, appropriate erosion control measures will be implemented to will include a water quality basin. An on-site detention basin will be incorporated into the parcel to reduce developed flows to historic levels.

Step 1: Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

- Step 2: All drainageways, ditches and channels have been stabilized by the following methods:
 - New swales within the site are broad and covered with gravel and with a slope of about 0.7% no erosion will take place
 - An existing roadside ditch will be enhanced as part of the proposed development.

Step 3: The proposed development will disturb approximately 7.6 acres.

Step 4: The development of this project will not affect sensitive waters.

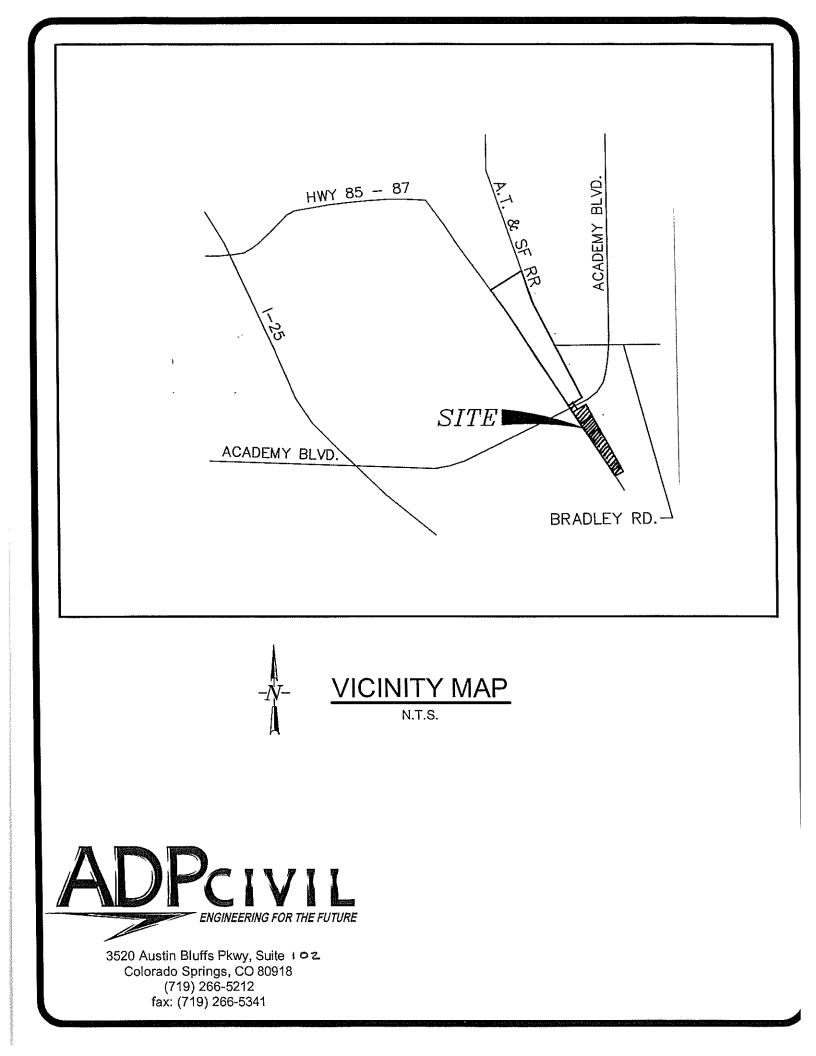
The development of this site will have little impact on downstream properties once the water quality/detention basin is constructed.

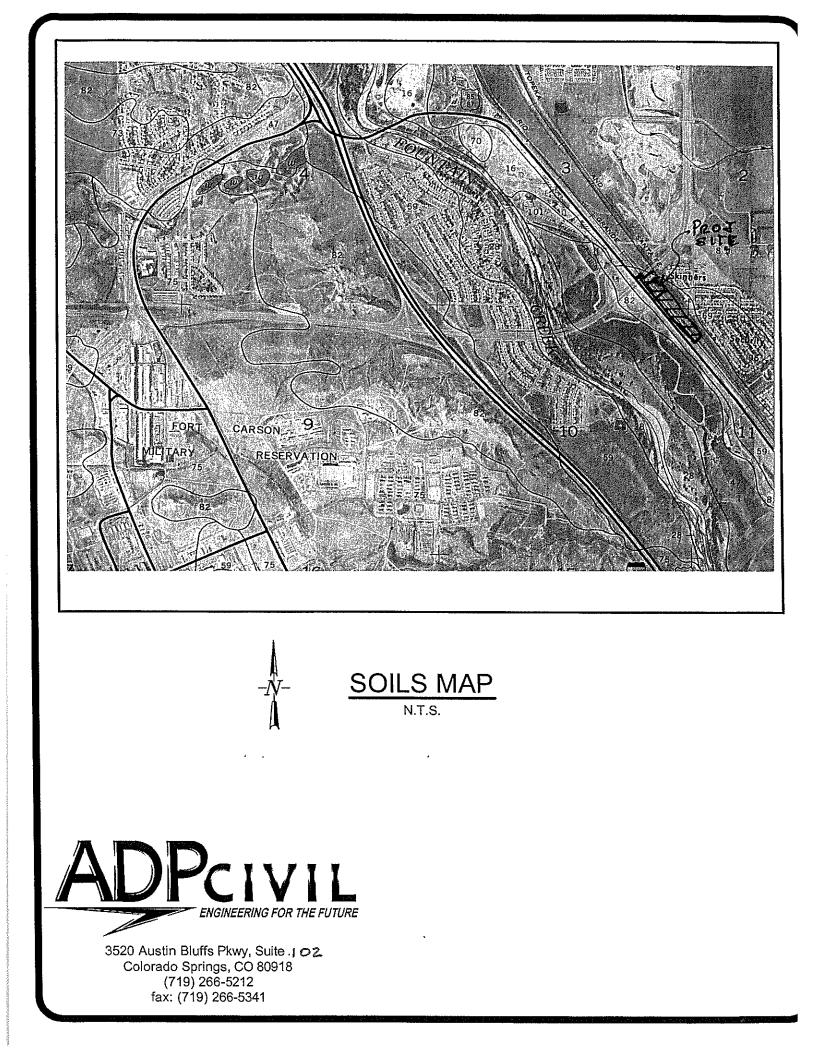
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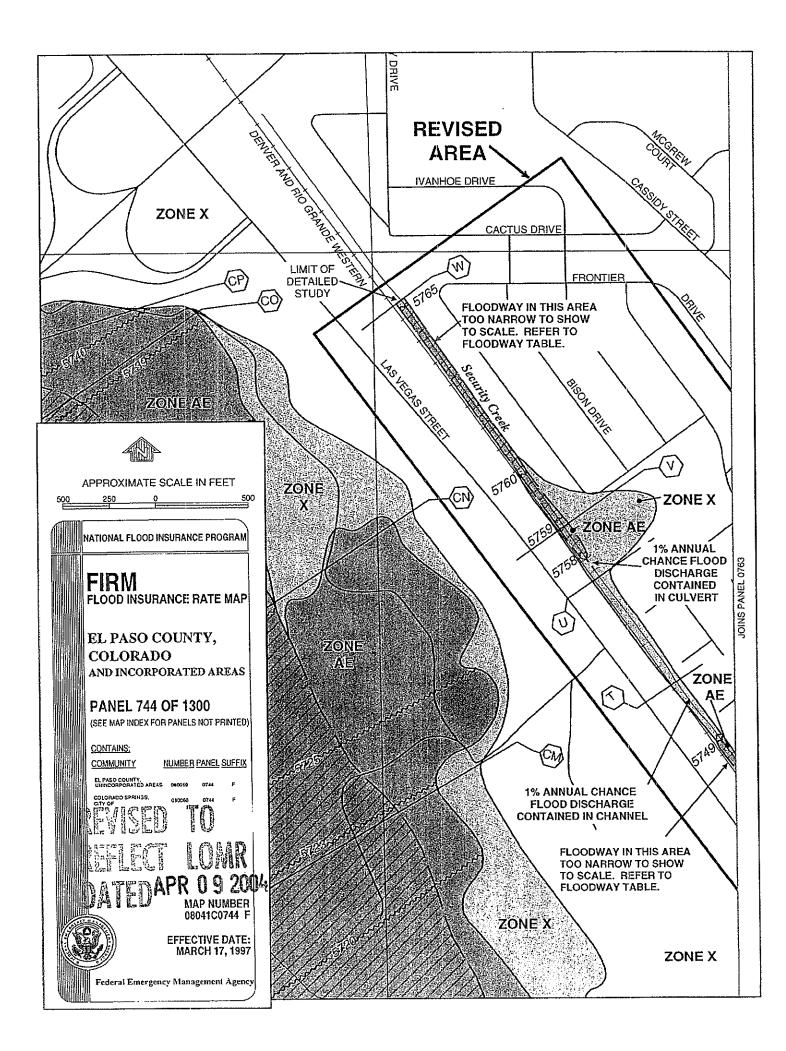
- City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume* 1 (DCM).
- 2. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume II* (DCM).
- 3. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
- 4. El Paso County (January 2006) Engineering Criteria Manual.
- 5. Urban Drainage and Flood Control District (June 2011). *Urban Storm Drainage Criteria Manual, Volume 1-3*.
- 6. Little Johnson/west Little Johnson Drainage Basin Planning Study prepared by Simons, Li Associates (1987)

APPENDIX A MAPS & EXHIBITS

Prepared by Associated Design Professionals, Inc.







APPENDIX B DRAINAGE CALCULATIONS

Prepared by Associated Design Professionals, Inc.

SOUTH ACAI		ESS CENTE	R			
C FACTOR C	ALCULATION	SHEET				
RUNOFF CO						
TYPE C SO	ILS					
LAND USE			5 YR	100 YR		
UNDEV & L	OOSE GRAVI	EL	0.15	0.5		
STREETS/P.	ARKING GRA	AVEL	0.63	0.74		
ROOFS/ PA	VED AREAS		0.75	0.83		
Historic Con				1		
HISTORIC CON						
			ONDITION	:	CALCULATE	
AREA	AREA	UNDEV			5	100
	(PARKING			
DESIG.	(acre)		GRAVEL	AREAS	YR	YR
Aex	6.40	6.40			0.15	0.50
Bex	1.30				0.15	0.50
	1.50	1.00		·····	0.15	0.50
RUNOFF CO	DEFICIENT			· · · · · · · · · · · · · · · · · · ·		
TYPE C SO	ILS					
LAND USE			5 YR	100 YR		
	OOSE GRAV	FT.	0.15	0.5		
	ARKING GR		0.63			
	VED AREAS		0.75			
Developed C	onditions					
	TOTAL		CONDITION		CALCULATE	DC
AREA	AREA	UNDEV	LOOSE	ROOFS/	5	100
			GRAVEL	PAVED		
DESIG.	(acre)			AREAS	YR	YR
A	7.30	1.80	2.90	2.60	0.36	0.62
В	0.30				0.15	0.50
IMPERVIOU	JŚ		-	-		
COVERAGE	E ACREAGE	. % IMP				
Undev	1.80	C	C C)		
Loose Grav	2.90	0.4	1.16)		
Trailers	2.60	0.9	2.34	ŀ		
	7.30		3.50)		
		TOTAL IMP	47.95%	b		

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Corrent Method Correlation OPENING VOLUME FOREBAY DEPTH Q = C x D^3/2 2% WQCV D = 6" 28 cfs 0.02 X 0.122 ac ft = 0.002 ac ft D = 6" Q = 0.28 cfs 0.002 ac ft x 43560 = 87.1 cf D	(Per Table EDB-4)			n 	s h iı s	'n												
ОРЕВИТИС VOLUME FOREBAY DEPTH Q = C x D^3/2 2% WQCV D = 6" .28 cfs @W = 0.26" 0.02 X 0.122 ac ft = 0.002 ac ft Q = 0.28 cfs 0.002 ac ft x 43560 = 87.1 cf D					n													
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@W = 0.26' 0.02 X 0.122 ac ft = 0.002 ac ft Q = 0.28 cfs 0.002 ac ft x 43560 = 87.1 cf	2% 100 yr stm	$Q = C \times D^{3}$	12	2% WQC	<u>></u>		D = 6"			Q = 0.28 C	tis							
0.002 ac ft x 43560 = 87.1 cf	0.02 X 14.3 = 0.28 cfs	@W = 0.26		0.02 X 0.1	122 ac ft = 0.(002 ac ft			@d = 4".t	0= 1', s =0.	.5%							
		Q = 0.28 cfs		0.002 ac 1	ft x 43560 = 8	17.1 cf			MAX Q = I	0.79 cfs								

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Project: <u>S Academy Business Ctr</u> Basin (D: <u>A</u> Control (Control (

	PERMANE		ZONE	LI AND 2	ORFICE
	POOL	Example	Zone	Configuration	(Retention Pond)
uired Vo	olume Cak	culation Selected BMP		EDB	

Selected BMP Type =	EDB			
Watershed Area =	7.30	acres	Note: L / WI	Ratio > 8
Watershed Length =	1,900	ft	L / W Ratio	11.4
Watershed Slope =	0.007	ft/ft		
Watershed Imperviousness =	48.00%	percent		
Percentage Hydrologic Soil Group A =	0.0%	percent		
Percentage Hydrologic Soil Group B =	0.0%	percent		
Percentage Hydrologic Soil Groups C/D =	100.0%	percent		
Desired WQCV Drain Time =	40.0	hours		
Location for 1-hr Rainfall Depths = D	Denver - Cap	atol Building		
Water Quality Capture Volume (WQCV) =	0.122	acre-feet	Optional Use	e Override
Excess Urban Runoff Volume (EURV) =	0.330	acre-feet	1-hr Precipits	noite
2-yr Runoff Volume (P1 = 1.19 in.) =	0.310	acre-feet	1.19	inches
5-yr Runoff Volume (P1 = 1.5 in.) =	0.464	acre-feet	1.50	inches
10-yr Runoff Volume (P1 = 1.75 in.) =	0.601	acre-feet	1.75	inches
25-yr Runoff Volume (P1 = 2 in.) =	0.830	acre-feet	2.00	inches
50-yr Runoff Volume (P1 = 2.25 in.) =	1.003	acre-feet	2.25	inches
100-yr Runoff Volume (P1 = 2.52 in.) =	1.218	acre-feet	2.52	inches
500-yr Runoff Volume (P1 = 3.01 in.) =	1.579	acre-feet	3.01	inches
Approximate 2-yr Detention Volume =	0.291	acre-feet		-
Approximate 5-yr Detention Volume =	0.437	acre-feet		
Approximate 10-yr Detention Volume =	0.499	acre-feet		
Approximate 25-yr Detention Volume =	0.541	acre-feet		
Approximate 50-yr Detention Volume =	0.561	acre-feet		
Approximate 100-yr Detention Volume =	0.642	acre-feet		

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Stage-Storage Calculation

VOLUME ELWY

Zone 1 Volume (WQCV) =	0.122	acre-fee
Zone 2 Volume (EURV - Zone 1) =	0.208	acre-fee
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	0.373	acre-fee
Total Detention Basin Volume =	0.703	acre-fee
Initial Surcharge Volume (ISV) =	user	ft*3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (Htotal) =	user	ft
Depth of Trickle Channel (H _{TC}) =	User	ft
Slope of Trickle Channel (S ₁₇) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (RLW) =	user	

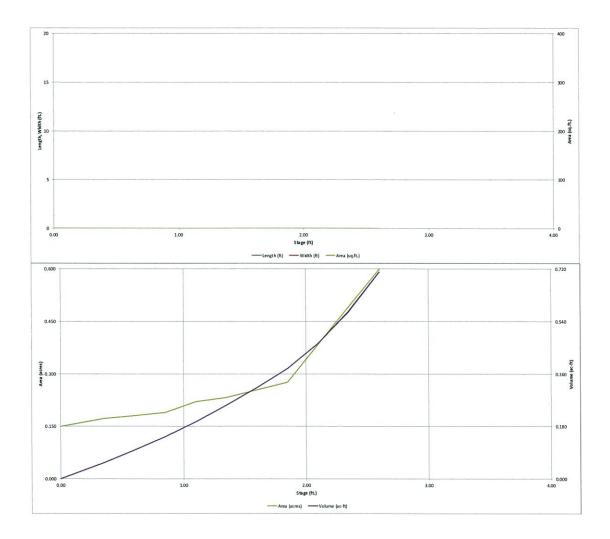
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Depth Increment =	0.25	ft							
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft*2)	Area (ft*2)	(acre)	(ft'3)	(ac-ft)
Top of Micropool	-	0.00	-	-	-	6,500	0.149	2Sada	Carling Co
CARGE SERVICES		0.35	-	-	-	7,500	0.172	2,375	0.055
Children (1996)	-	0.60	-	-	-	7,875	0.181	4,293	0.000
		0.85	-	-	-	8,250	0.189	6,305	0.145
State States	-			-					
	-	1.10	-	-	-	9,590	0.220	8,522	0.196
	-	1.35	-	-	-	10,130	0.233	10,981	0.252
SALST TRADED	-	1.60		-	-	11,070	0.254	13,622	0.313
	-	1.85	-	-	-	12,010	0.276	16,498	0.379
Service Contraction of the	-	2.10	-	-	-	16,700	0.383	20,206	0.464
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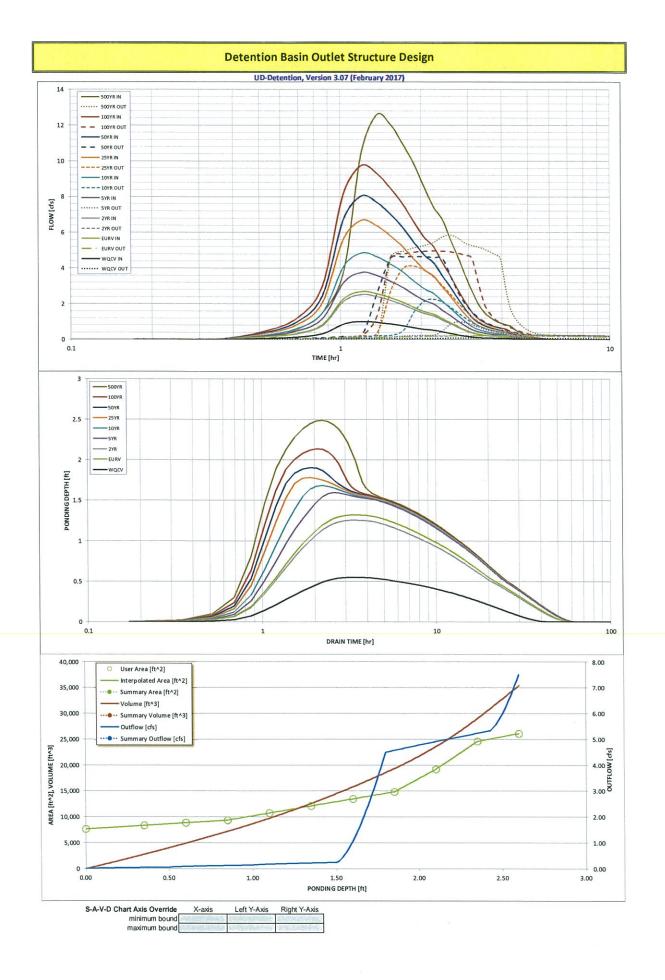
S Acad Bus Ctr Copy of UD-Detention_v3.07.xlsm, Basin

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



		Dete	ntion Basin C	Outlet Structu	ure Design				
Project	s Academy Busines	e Ctr	UD-Detention, Ver	sion 3.07 (February	(2017)				
Basin ID:		scu							
(20NE 3 (20NE 2 (20NE 1									
			r		Zone Volume (ac-ft)	Outlet Type			
COUNCEL EDAN WOCK			Zone 1 (WQCV)	0.65	0.122	Orifice Plate			
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	1.50	0.208	Orifice Plate			
PERMANENT ORIFICES	configuration (Ret	antion Rond)	; (100+1/2WQCV)	2.42	0.373	Weir&Pipe (Rect.)			
				l	0.703	Total			
er Input: Orifice at Underdrain Outlet (typically us Underdrain Orifice Invert Depth =	1	t a Filtration BMP) ft (distance below th	· filenetice modie au	(r.c.)	Under	Calculate drain Orifice Area =	d Parameters for Un		
Underdrain Orifice Diameter =		inches	e intration media sui	iace)		n Orifice Centroid =		ft ² feet	
er Input: Orifice Plate with one or more orifices o	r Elliptical Slot Weir	(typically used to dra	ain WQCV and/or EU	RV in a sedimentatio	on BMP)	Calcul	ated Parameters for	Plate	
Invert of Lowest Orifice =			oottom at Stage = 0 ft			ifice Area per Row =	1.701E-02	ft²	
Depth at top of Zone using Orifice Plate =	1.50	and the second	oottom at Stage = 0 ft)		iptical Half-Width =		feet	
Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	6.00 2.45	inches sq. inches (diameter	- 1 2/4 inches)			tical Slot Centroid = Elliptical Slot Area =		feet ft ²	
Office Plate. Office Alea per Now -	2.43	sq. menes (utameter	- 1-3/4 menes/			Linplical Slot Alea - [N/A	π	
er Input: Stage and Total Area of Each Orifice R									is.
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.50	1.00						
Orifice Area (sq. inches)	2.40	2,40	2.45						L
1	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	l
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
Heer Insult Vertical Orifica (Cira	uler or Restancyler)					Coloulated	Desemations for Mart		
User Input: Vertical Orifice (Circ	Not Selected	Not Selected	1			Calculated	Parameters for Vert Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin b	oottom at Stage = 0 ft	.) V	ertical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A		pottom at Stage = 0 ft		al Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						50
User Input: Overflow Weir (Dropbox) and G	rate (Flat as flaned)					Calaulatad	Parameters for Ove	-fl	
User input: Overnow weir (Dropbox) and G		1	1			Calculated		The second second second	1
Overflow Weir Front Edge Height, Ho =	1.50	N/A	ft (relative to basin bo	ottom at Stage = 0 ft)	Height of Gr	ate Upper Edge, H _t =	1.50	N/A	feet
Overflow Weir Front Edge Length = 3.00 N/A feet Over Flow Weir Slope Length = 3.00 N/A feet Overflow Weir Slope = 0.00 N/A H:V (enter zero for flat grate) Grate Open Area / 100-yr Orifice Area = 8.40 N/A should								feet	
Overflow Weir Front Edge Length = 3.00 N/A feet Over Flow Weir Slope Length = 3.00 N/A feet Overflow Weir Slope = 0.00 N/A H:V (enter zero for flat grate) Grate Open Area / 100-yr Orifice Area = 8.40 N/A should Horiz. Length of Weir Sides = 3.00 N/A feet Overflow Grate Open Area w/o Debris = 6.30 N/A ft ²								should be ≥ 4	
Overflow Weir Slope = 0.00 N/A H:V (enter zero for flat grate) Grate Open Area / 100-yr Orifice Area = 8.40 N/A should									
Overflow Grate Open Area % = Debris Clogging % =	50%	N/A N/A	%, grate open area/ %	total area	Overflow Grate Op	oen Area w/ Debris =	3.15	N/A]ft²
Debris clogging /a -	50%	1 174							
ser Input: Outlet Pipe w/ Flow Restriction Plate (C	ircular Orifice, Restr	ictor Plate, or Rectar	ngular Orifice)		c	alculated Parameter	rs for Outlet Pipe w/	Flow Restriction Pla	te
	Zone 3 Rectangular	Not Selected]				Zone 3 Rectangular	Not Selected]
Depth to Invert of Outlet Pipe =	0.00	N/A	-	sin bottom at Stage = 0	1.2	Outlet Orifice Area =	0.75	N/A	ft ²
Rectangular Orifice Width =	18.00	N/A	inches			et Orifice Centroid =	0.25	N/A	feet
	6.00		inches	Halt-	Central Angle of Rest	rictor Plate on Pipe =	N/A	N/A	radians
Rectangular Orifice Height =									
Rectangular Orifice Height = User Input: Emergency Spillway (Rectang)				Calcula	ted Parameters for	Spillway	
	gular or Trapezoidal)		bottom at Stage = 0 f	t)	Spillway	Calcula Design Flow Depth=	0.48	feet	
User Input: Emergency Spillway (Rectang	gular or Trapezoidal) 2.42		bottom at Stage = 0 f	t)				1	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	zular or Trapezoidal) 2.42 8.00 4.00	ft (relative to basin feet H:V	bottom at Stage = 0 f	t)	Stage a	Design Flow Depth=	0.48	feet	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length =	gular or Trapezoidal) 2.42 8.00	ft (relative to basin feet	bottom at Stage = 0 f	t)	Stage a	Design Flow Depth= t Top of Freeboard =	0.48	feet feet	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	gular or Trapezoidal) 2.42 8.00 4.00 1.00	ft (relative to basin feet H:V	bottom at Stage = 0 f	t)	Stage a	Design Flow Depth= t Top of Freeboard =	0.48	feet feet	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	zular or Trapezoidal) 2.42 8.00 4.00 1.00 WQCV	ft (relative to basin feet H:V feet EURV	2 Year	5 Year	Stage a Basin Area a 10 Year	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year	0.48 3.90 0.60 50 Year	feet feet acres 100 Year	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) =	zular or Trapezoidal) 2.42 8.00 4.00 1.00 WQCV 0.53	ft (relative to basin feet H:V feet <u>EURV</u> 1.07	2 Year 1.19	5 Year 1.50	Stage a Basin Area a 10 Year 1.75	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = <u>25 Year</u> 2.00	0.48 3.90 0.60 50 Year 2.25	feet feet acres 100 Year 2.52	3.01
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	zular or Trapezoidal) 2.42 8.00 4.00 1.00 WQCV 0.53 0.122	ft (relative to basin feet H:V feet EURV	2 Year	5 Year	Stage a Basin Area a 10 Year	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year	0.48 3.90 0.60 50 Year	feet feet acres 100 Year	
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	2.42 8.00 4.00 1.00 WQCV 0.53 0.122 0.121	ft (relative to basin feet H:V feet <u>EURV</u> 1.07 0.330 0.330	2 Year 1.19 0.310	5 Year 1.50 0.464 0.463	Stage a Basin Area a 1.75 0.601 0.600	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.830	0.48 3.90 0.60 50 Year 2.25 1.003 1.002	feet feet acres 2.52 1.218 1.217	3.01 1.579 1.578
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rairfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) =	2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00	ft (relative to basin feet H:V feet 1.07 0.330 0.330 0.00	2 Year 1.19 0.310 0.310 0.01	5 Year 1.50 0.464 0.463 0.07	Stage a Basin Area a 1.75 0.601 0.600 0.19	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.830 0.47	0.48 3.90 0.60 2.25 1.003 1.002 0.62	feet feet acres 2.52 1.218 1.217 0.82	3.01 1.579 1.578 1.15
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	2.42 8.00 4.00 1.00 WQCV 0.53 0.122 0.121 0.00 0.0	ft (relative to basin feet H:V feet <u>EURV</u> 1.07 0.330 0.330	2 Year 1.19 0.310 0.01 0.1	5 Year 1.50 0.464 0.463	Stage a Basin Area a 1.75 0.601 0.600	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.830	0.48 3.90 0.60 50 Year 2.25 1.003 1.002	feet feet acres 2.52 1.218 1.217	3.01 1.579 1.578
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Coexisting Storm Return Period = One-Hour Rainfall Depth (inj = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Volume (acre-ft) = Predevelopment Peak Q(cfs) = Peak Inflow Q(cfs) = Peak Unflow Q(cfs) =	xular or Trapezoidal) 2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00 0.0 1.0 0.1	ft (relative to basin feet H:V feet 0.330 0.00 0.00 2.7 0.2	2Year 1.19 0.310 0.01 0.1 2.5 0.2	5 Year 1.50 0.464 0.463 0.07 0.5 3.7 1.0	Stage a Basin Area a 1.75 0.601 0.600 0.19 1.4 4.8 2.3	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.830 0.47 3.4 6.7 4.1	0.48 3.90 0.60 50 Year 2.25 1.003 1.002 0.62 4.5 8.0 4.6	feet feet acres 2.52 1.218 1.217 0.82 6.0 9.7 5.0	3.01 1.579 1.578 1.15 8.4 12.6 5.9
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	xular or Trapezoidal) 2.42 8.00 4.00 1.00 0.53 0.122 0.00 0.0 1.0 0.0 1.0 0.1 N/A	ft (relative to basin feet H:V feet 0.330 0.00 0.0 2.7 0.2 N/A	2 Year 1.19 0.310 0.01 0.1 2.5 0.2 N/A	5 Year 1.50 0.464 0.07 0.5 3.7 1.0 2.0	Stage a Basin Area a 1.75 0.601 0.19 1.4 4.8 2.3 1.6	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 2.00 0.830 0.830 0.47 3.4 6.7 4.1 1.2	0.48 3.90 0.60 50 Year 2.25 1.003 0.62 4.5 8.0 4.6 1.0	feet feet acres <u>100 Year</u> 2.52 1.218 <u>1.217</u> 0.82 6.0 9.7 5.0 0.8	3.01 1.579 1.578 1.15 8.4 12.6 5.9 0.7
User Input: Emergency Spillway (Rectang Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Coexisting Storm Return Period = One-Hour Rairfall Depth (inj = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Volume (acre-ft) = Predevelopment Peak Q(cfs) = Peak Inflow Q(cfs) = Peak Unflow Q(cfs) =	2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00 0.0 1.0 0.0 1.0 N/A Plate	ft (relative to basin feet H:V feet 0.330 0.00 0.00 2.7 0.2	2Year 1.19 0.310 0.01 0.1 2.5 0.2	5 Year 1.50 0.464 0.463 0.07 0.5 3.7 1.0	Stage a Basin Area a 1.75 0.601 0.19 1.4 4.8 2.3 1.6	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.830 0.47 3.4 6.7 4.1	0.48 3.90 0.60 50 Year 2.25 1.003 1.002 0.62 4.5 8.0 4.6	feet feet acres 2.52 1.218 1.217 0.82 6.0 9.7 5.0	3.01 1.579 1.578 1.15 8.4 12.6 5.9 0.7
User Input: Emergency Spillway (Rectand Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Volume (acre-ft) = Predevelopment Peak R(cfs) = Predevelopment Peak Q(cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00 1.0 1.0 0.1 N/A Plate N/A N/A	ft (relative to basin feet H:V feet 0.330 0.00 0.00 0.0 2.7 0.2 N/A Plate N/A N/A	2 Year 1.19 0.310 0.01 0.1 2.5 0.2 N/A Plate N/A N/A	5 Year 1.50 0.464 0.463 0.07 0.5 3.7 1.0 2.0 Overflow Grate 1 0.1 N/A	Stage a Basin Area a 1.75 0.601 0.601 0.19 1.4 4.8 2.3 1.6 Overflow Grate 1 0.3 N/A	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 2.00 0.830 0.830 0.47 3.4 6.7 4.1 1.2 Overflow Grate 1 0.6 N/A	0.48 3.90 0.60 50 Year 2.25 1.003 0.62 4.5 8.0 4.6 1.00 Outlet Plate 1 0.7 N/A	feet feet acres 100 Year 2.52 1.218 2.217 0.82 6.0 9.7 5.0 0.82 0.041et Plate 1 0.7 N/A	3.01 1.579 1.578 1.15 8.4 12.6 5.9 0.7 Spillwa 0.8 N/A
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User Input: Emergency Spillway (Rectan Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Raiffall Depth (n) = Calculated Runoff Volume (acre-ft) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 3% of Inflow Volume (hours) =	xular or Trapezoidal) 2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00 0.0 1.0 0.1 N/A Plate N/A 37 40	ft (relative to basin feet H:V feet 0.330 0.330 0.00 0.0 2.7 0.2 N/A Plate N/A N/A N/A 48 53	2 Year 1.19 0.310 0.310 0.01 2.5 0.2 N/A Plate N/A N/A A 47 52	S Year 1.50 0.464 0.07 0.5 3.7 1.0 2.0 Overflow Grate 1 0.1 N/A 49 55	Stage a Basin Area a 1.75 0.601 0.19 1.4 4.8 2.3 1.6 Overflow Grate 1 0.3 N/A 47 54	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 0.830 0.47 3.4 6.7 4.1 1.2 0.verflow Grate 1 0.6 N/A 44 52	0.48 3.90 0.60 50 Year 2.25 1.003 1.002 0.62 4.5 8.0 4.6 1.0 Outlet Plate 1 0.7 N/A 42 51	feet feet acres 2.52 1.218 2.52 1.217 0.82 6.0 9.7 5.0 0.8 Outlet Plate 1 0.7 N/A 40 50	3.01 1.579 1.578 1.15 8.4 12.6 5.9 0.7 Spillway 0.8 N/A 37 49
User Input: Emergency Spillway (Rectan Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Volume (acre-ft) = Predevelopment Peak Q (cfs) = Predevelopment Deak Q (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	2.42 8.00 4.00 1.00 0.53 0.122 0.121 0.00 0.0 1.0 0.0 1.0 0.0 1.0 N/A Plate N/A 37 40 0.55 0.20	ft (relative to basin feet H-V feet 0.330 0.00 0.0 0.0 2.7 0.2 N/A Plate N/A N/A 48	2 Year 1.19 0.310 0.01 0.1 2.5 0.2 N/A Plate N/A N/A 47	5 Year 1.50 0.464 0.463 0.07 0.5 3.7 1.0 2.0 Overflow Grate 1 0.1 N/A 49	Stage a Basin Area a 1.75 0.601 0.600 0.19 1.4 4.8 2.3 1.6 Overflow Grate 1 0.3 N/A 47	Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 2.00 0.830 0.830 0.47 3.4 6.7 4.1 1.2 Overflow Grate 1 0.6 N/A 44	0.48 3.90 0.60 50 Year 2.25 1.003 0.62 4.5 8.0 4.6 1.0 Outlet Plate 1 0.7 N/A 42	feet feet acres 100 Year 2.52 1.217 0.82 6.0 9.7 5.0 0.8 Outlet Plate 1 0.7 N/A 40	1.579 1.578 1.15 8.4 12.6 5.9 0.7 Spillway 0.8 N/A 37



Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename:

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK																	
Fime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs																	
10.31 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00																	
	0:10:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00																	
Hydrograph	0:20:37	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00																	
Constant	0:30:56	0.05	0.12	0.11	0.17	0.21	0.29	0.35	0.42	0.54																	
0.485	0:41:14	0.12	0.32	0.30	0.45	0.58	0.79	0.95	1.15	1.48																	
ŀ	0:51:33	0.31	0.83	0.78	1.15 3.17	1.48	2.04	2.45 6.72	2.96 8.12	3.81 10.45																	
ŀ	1:12:10	1.00	2.68	2.52	3.74	4.84	6.66	8.03	9.72	12.58																	
t t	1:22:29	0.95	2.55	2.40	3.57	4.62	6.36	7.67	9.30	12.04																	
	1:32:47	0.86	2.32	2.18	3.25	4.20	5.79	6.98	8.46	10.96																	
-	1:43:06	0.76	2.07	1.94	2.90	3.75	5.18	6.25	7.58	9.83																	
-	1:53:25	0.65	1.78	1.67	2.49	3.24	4.48	5.41	6.57	8.53																	
-	2:03:43 2:14:02	0.57	1.55	1.46	2.18	2.82	3.90	4.71	5.72	7.41																	
-	2:24:20	0.51	1.40	1.32	1.97	2.56	3.54	4.27 3.54	5.18 4.30	6.72 5.59																	
t	2:34:39	0.33	0.93	0.88	1.32	1.72	2.32	2.90	3.53	4.60																	
Ì	2:44:58	0.25	0.71	0.67	1.01	1.32	1.85	2.25	2.75	3.60																	
	2:55:16	0.18	0.52	0.49	0.75	0.98	1.38	1.69	2.07	2.73																	
[3:05:35	0.13	0.38	0.36	0.54	0.71	1.00	1.22	1.51	2.00																	
-	3:15:53	0.11	0.30	0.28	0.42	0.55	0.77	0.94	1.16	1.52																	
-	3:26:12	0.09	0.25	0.23	0.35	0.46	0.64	0.77	0.95	1.24																	
ł	3:36:31	0.07	0.21 0.18	0.20	0.30	0.39	0.54	0.65	0.80	1.05																	
-	3:57:08	0.07	0.18	0.17	0.26	0.34	0.47	0.57	0.70	0.92																	
	4:07:26	0.06	0.15	0.14	0.22	0.28	0.43	0.48	0.58	0.76																	
	4:17:45	0.04	0.11	0.11	0.16	0.21	0.29	0.35	0.43	0.56																	
	4:28:04	0.03	0.08	0.08	0.12	0.15	0.21	0.26	0.31	0.41																	
	4:38:22	0.02	0.06	0.06	0.09	0.11	0.15	0.19	0.23	0.30																	
	4:48:41	0.02	0.04	0.04	0.06	0.08	0.11	0.14	0.17	0.22																	
	4:58:59	0.01	0.03	0.03	0.04	0.06	0.08	0.10	0.17 0.12 0.09 0.06 0.04 0.03 0.01	0.16																	
	5:09:18 5:19:37	0.01	0.02	0.02	0.03	0.04	0.06	0.07		0.11																	
	5:29:55	0.01	0.02	0.01	0.02	0.03	0.04	0.05		0.08																	
	5:40:14	0.00	0.01	0.01	0.01	0.02	And the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	And and the Artes and a second		0.08																	
	5:50:32	0.00	0.00	0.00	0.00	0.01	The second statement of the second statement of the second	Charles and the second states	And a state of the set of the local sectors of the	0.02																	
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APPENDIX C DESIGN CHARTS

Prepared by Associated Design Professionals, Inc.

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and Use or Surface	Percent						Runoff Co	efficients					
Tharacteristics	Impervious	2.y	ear	5-y	ear	10-y	(ear	25-j	/e3/	50-1	/eər	100-	year
		HSG A&B	HSG C&D	HSG A&B	KSG CLD	HSG A&B	HSG C&D	HSG A&B	HSG CED	HSGALB	HSGC&D	HSG A&B	HSG CLO
Jusiness						·				<u> </u>	L	l	
Commercial Areas	<u>95</u>	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0,57	0.58	0.52	0.60	0.65	0.62	D,68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4Acre	40	0.23	0.28	0.30	0,35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0,25	0.30	0,32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0,20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial		+	<u> </u>				1						
Ught Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.65	0.70	0.6B	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0,75	0.75	0.77	0.78	03.0	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0,23	0.28	0.30	0.35	0.36	0,42	0,42	0.50	D.46	0.54	0.50	0.58
Undeveloped Areas					1					+	. 	-	
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.65	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0,45	0.36	0,51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0,25	0.25	0,37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.95
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0,38	0.44	0.44	0.51	0,48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Grave)	80	0.57	0.60	0,59	0.63	0.63	0.65	0.66	0.70	0.68	0,72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.83	0.03	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82		0.83
Lawns		0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44		0.50

Table 6-6. Runoff Coefficients for Rational Method(Source: UDFCD 2001)

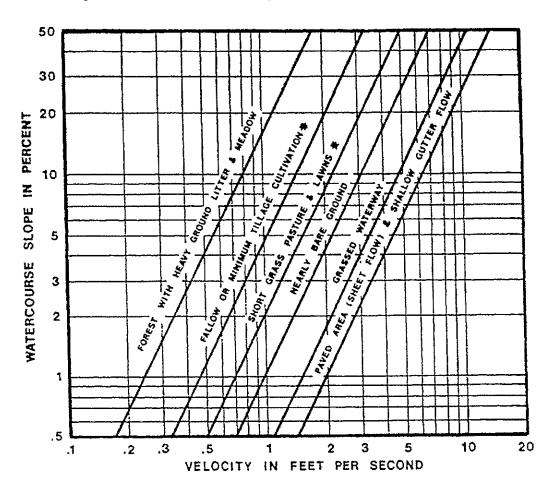


Figure 6-25. Estimate of Average Concentrated Shallow Flow

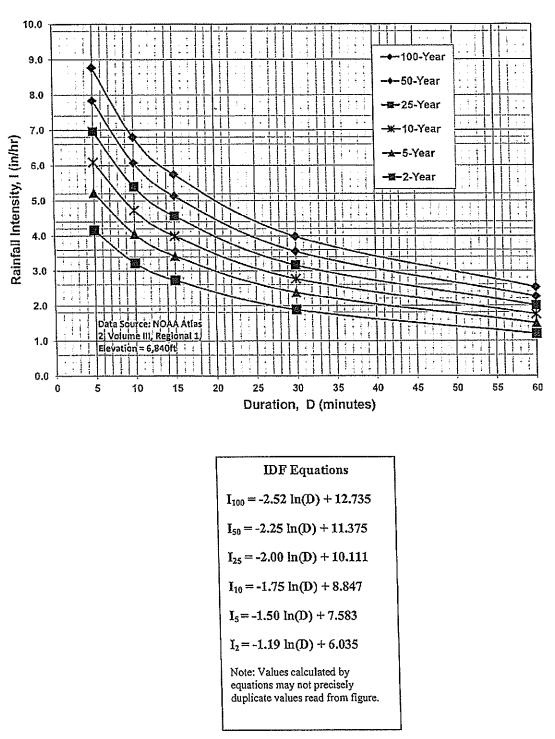
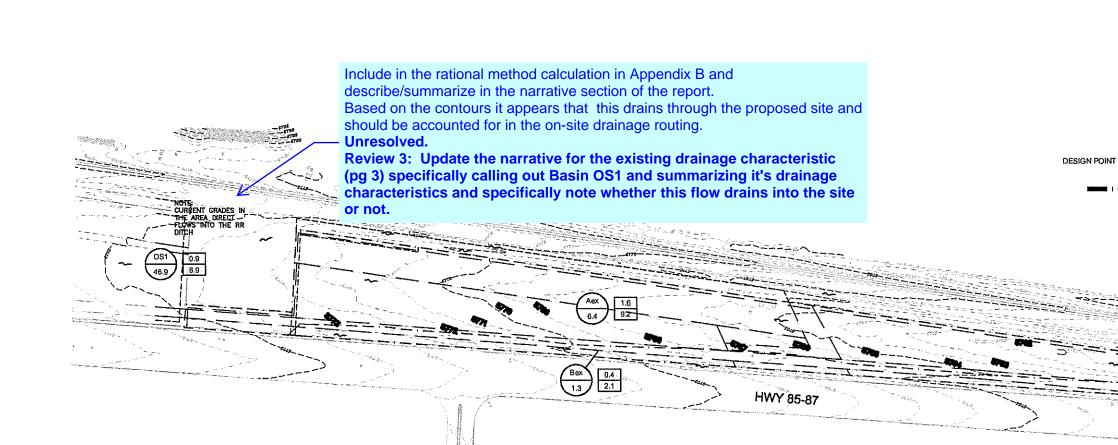
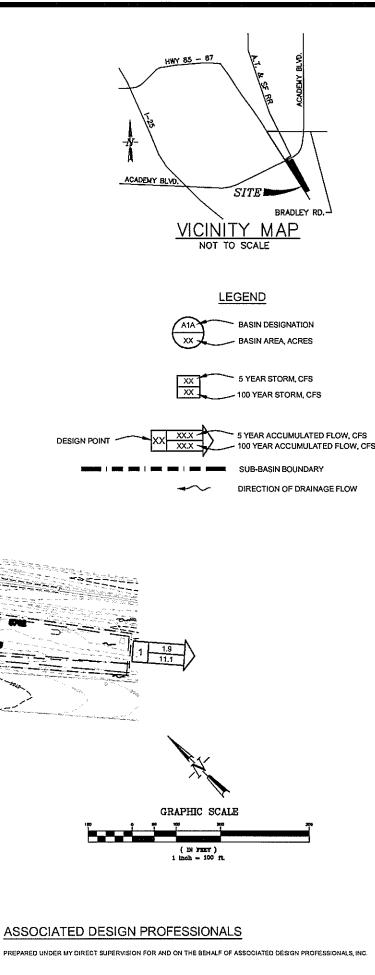


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



MICHAEL BARTUSEK, COLORADO P.E. #23329



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