

PRELIMINARY/FINAL DRAINAGE REPORT

FOR

SOUTH ACADEMY BUSINESS CENTER

**Prepared For:
10230 Hall Boulevard, LLC
PO Box 38014
Colorado Springs, CO 80937**

**Prepared By:
Associated Design Professionals, Inc.
3520 Austin Bluffs Parkway, Suite 102
Colorado Springs, CO 80918
(719) 266-5212
Project No. 161103
1/25/18
PCD Project No 17-004**





ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the city/county for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Michael A. Bartusek, P.E. #23329

DEVELOPER'S STATEMENT:

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: _____
Mr Michael Turley

Title: Manager

Address: 10230 Hall Boulevard, LLC
PO Box 38014
Colorado Springs, CO 80937

EL PASO COUNTY:

Filed in accordance with the El Paso County Land Development Code; the Drainage Criteria Manual, Volumes 1 and 2; and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E., County Engineer
ECM Administrator
Conditions:

Date



PROJECT DESCRIPTION

This proposed project is contained within a new subdivision named the South Academy Business Center. This currently vacant lot consists of 7.60 acres. It is located in the Southeast Quarter of Section 3, Township 15 South, Range 66 West of the Sixth Principal Meridian, County of El Paso, State of Colorado. The site is located on a narrow strip of land which is bordered on the west by State Highway 85/87 and on the east by the Denver and Rio Grande Western Railroad. Its northern boundary is situated on the south boundary line of the South Academy Boulevard right-of-way.

FLOODPLAIN STATEMENT

This site does not lie within a designated 100-year floodplain as delineated on LOMR No. 03-08-0318P, dated April 9, 2004. It is located within the West Little Johnson drainage basin. The drainage basin map shows a split in the property between the Little Johnson and West Little Johnson Basins. However, field verification revealed that all of the property was located within the West Little Johnson Basin.

SOILS

The soils on the northern site are classified as Blakeland loamy sand by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "A". The soils on the proposed site are classified as Nunn clay loam by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "C".

METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with *City/County Drainage Criteria Manual*. The Rational Method for computation of runoff was used for determining on-site flows.

$Q = c i a$

Where

- Q = maximum rate of runoff in cubic feet per second
- c = runoff coefficient representing drainage area characteristics
- i = average rainfall intensity, in inches per hour, for the duration required for the runoff to become established
- a = drainage basin size in acres

Off-site flows were determined using the TR20 hydrologic program for project hydrology by the Soil Conservation Service.

EXISTING DRAINAGE CHARACTERISTICS

This previously unplatted site was included in the *Little Johnson/West Little Johnson Drainage Basin Planning Study* prepared by Simons, Li & Associates in 1987. Much of the land north of the proposed project lies within either the Rocky Mountain Materials property or the Stephen Schnurr Living Trust. The Rocky Mountain property encompasses approximately 42 acres of the 54.5-acre basin. The Stephen Schnurr Living Trust owns the 4.6 acres just north of the site. Flows from these properties are released at historic levels onto the site to its south. This vacant land is just north of the proposed project and is covered with rangeland grasses. The tributary area slopes generally southwest at an average slope of one percent. The existing runoff is contained within a broad drainage swale located near the existing railroad tracks.



According to the analysis performed by Simons, Li & Associates, the runoff produced by the entire drainage basin along SH 85/87 would result in no flow for the ten-year storm event and one cfs for the 100-year storm event. The low runoff amounts were due to the Type "A" soils and the long overland flow times. These flow travel toward the railroad ditch east of the parcel.

An analysis of the site using the Rational Method produced the following flow rates: Sub-Basin A, which drains toward the interior of the parcel and produces 1.6 cfs for the five-year storm and 9.2 cfs for the 100-year storm; Sub-Basin B, which drains to a ditch along SH 85/87 produces a flow of 0.4 cfs for the five-year storm and 2.1 cfs for the 100-year storm. The total flow tributary to the site is 1.9 cfs for the five-year storm and 11.1 cfs for the 100-year storm.

DEVELOPED DRAINAGE CHARACTERISTICS

The proposed development of 7.6 acres will be storage facility comprised of 8' x 40' trailers placed on the site with loose gravel placed over the site.

Runoff from Sub-Basin A will be directed in a southeasterly direction toward the south property line. Based on the proposed developed conditions, Sub-Basin A will produce flows of 4.7 cfs for the five-year storm and 14.3 cfs for the 100-year storm. The detained flows from the Water Quality/Detention Basin will be 1.0 cfs for the five-year storm and 5.0 cfs for the 100-year storm. These detained flows will be directed into an existing grass swale just east of the basin. The existing broad, grassed swale continues flowing to the east at a 0.7% slope with 10:1 side slopes. The 100 year outflow will produce a flow depth of 0.6 ft and a velocity of 1.5 fps.

Runoff from Sub-Basin B will increase slightly to 0.4 cfs for the five-year storm and 2.3 cfs for the 100-year storm. The total flow tributary to the site is 1.4 cfs for the five-year storm and 7.2 cfs for the 100-year storm.

WATER QUALITY/DETENTION REQUIREMENTS

In accordance with current NPDES, stormwater quality BMPs will be provided for this site when it is developed. Based on actual calculations, the commercial development of the site will produce an imperviousness of 48 percent. The water quality component is accomplished by a 2.42' deep 0.703 acre foot private extended detention facility located at the south end of the project. The facility will be maintained by the owner

DRAINAGE BASIN FEE

The proposed development is located within the West Little Johnson drainage basin. The 2017 drainage basin fee calculation is as follows:

Impervious Coverage	=	48%
Area Subject to Fee	=	0.48 x 7.6 acres = 3.648 acre
West Little Johnson Basin Fee	=	\$1,072/acre
Drainage Basin Fee	=	\$1,072 x 3.648 = \$3,911

There are no associated Bridge Fees for the West Little Johnson drainage basin.



PRIVATE DRAINAGE FACILITIES

Item	Unit	Quantity	Unit Cost	Total Cost
18" RCP FES	EA	1	\$500	\$ 600
18" HDPE	LF	15	\$84	\$ 1,260
Detention Outlet Structure	EA	1	\$3,000	\$ 5,000
Emergency Spillway	EA	1	\$1,000	\$ 1,500
Sub-Total				\$8,360
15% Contingency & Engineering				\$ 1,254
TOTAL				\$9,614

CONCLUSION

Storm runoff from this property will not adversely affect downstream properties or facilities. Grading will take place on the property; therefore, appropriate erosion control measures will be implemented to will include a water quality basin. An on-site detention basin will be incorporated into the parcel to reduce developed flows to historic levels.

Step 1: Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

Step 2: All drainageways, ditches and channels have been stabilized by the following methods:

- New swales within the site are broad and covered with gravel and with a slope of about 0.7% no erosion will take place
- An existing roadside ditch will be enhanced as part of the proposed development.

Step 3: The proposed development will disturb approximately 7.6 acres.

Step 4: The development of this project will not affect sensitive waters.

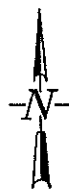
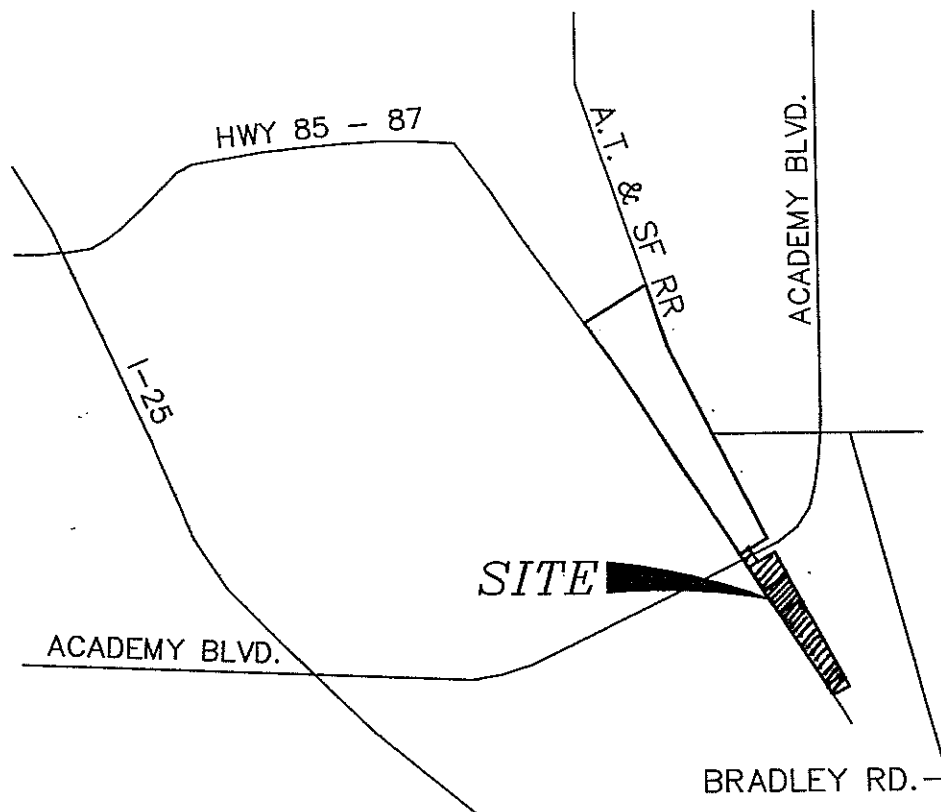
The development of this site will have little impact on downstream properties once the water quality/detention basin is constructed.

REFERENCES

1. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume 1* (DCM).
2. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume II* (DCM).
3. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
4. *El Paso County (January 2006) Engineering Criteria Manual*.
5. Urban Drainage and Flood Control District (June 2011). *Urban Storm Drainage Criteria Manual, Volume 1-3*.
6. Little Johnson/west Little Johnson Drainage Basin Planning Study prepared by Simons, Li Associates (1987)

**PRELIMINARY/FINAL DRAINAGE REPORT
SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX A
MAPS & EXHIBITS**



VICINITY MAP

N.T.S.

ADPcIVIL

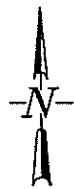
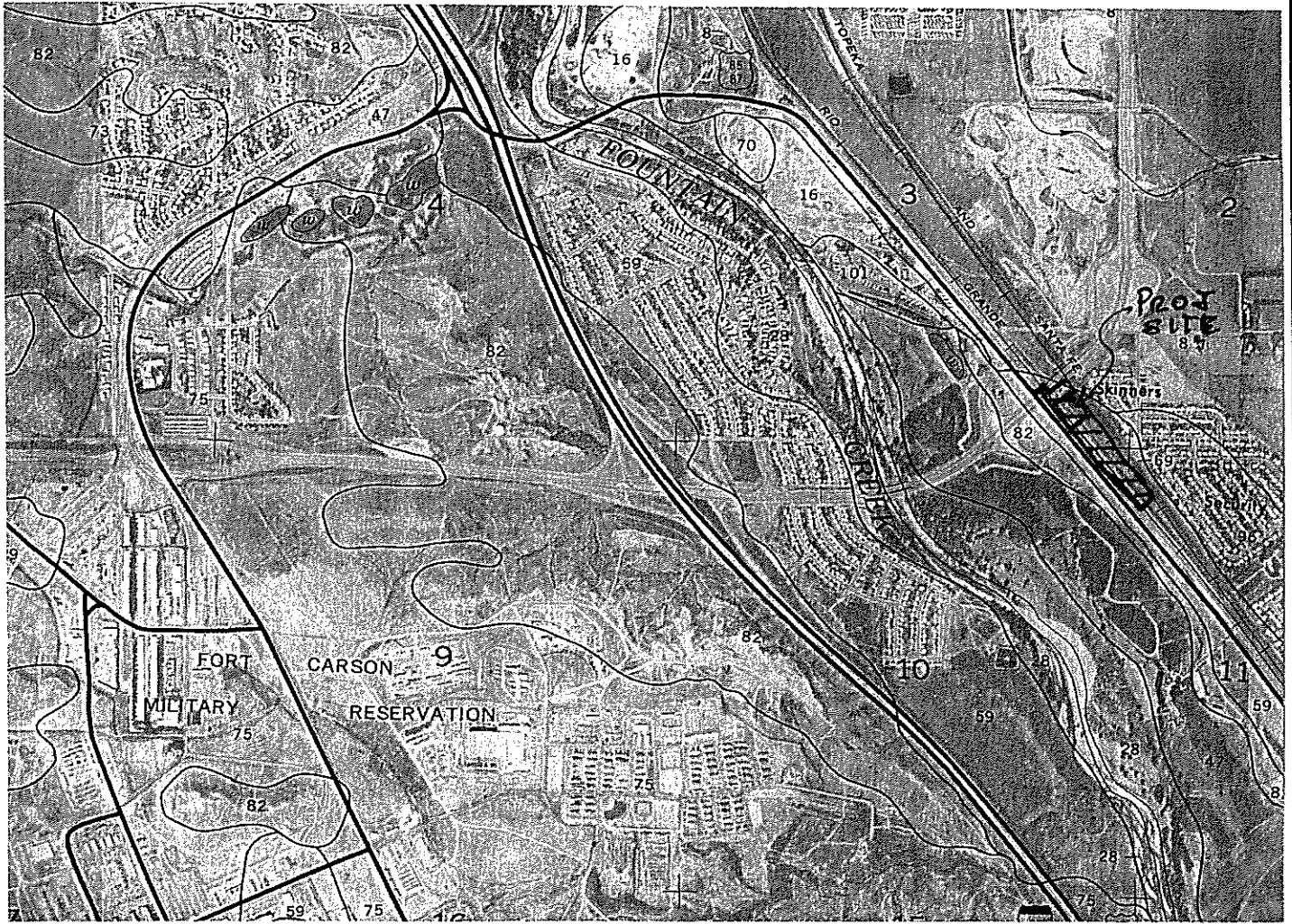
ENGINEERING FOR THE FUTURE

3520 Austin Bluffs Pkwy, Suite 102

Colorado Springs, CO 80918

(719) 266-5212

fax: (719) 266-5341



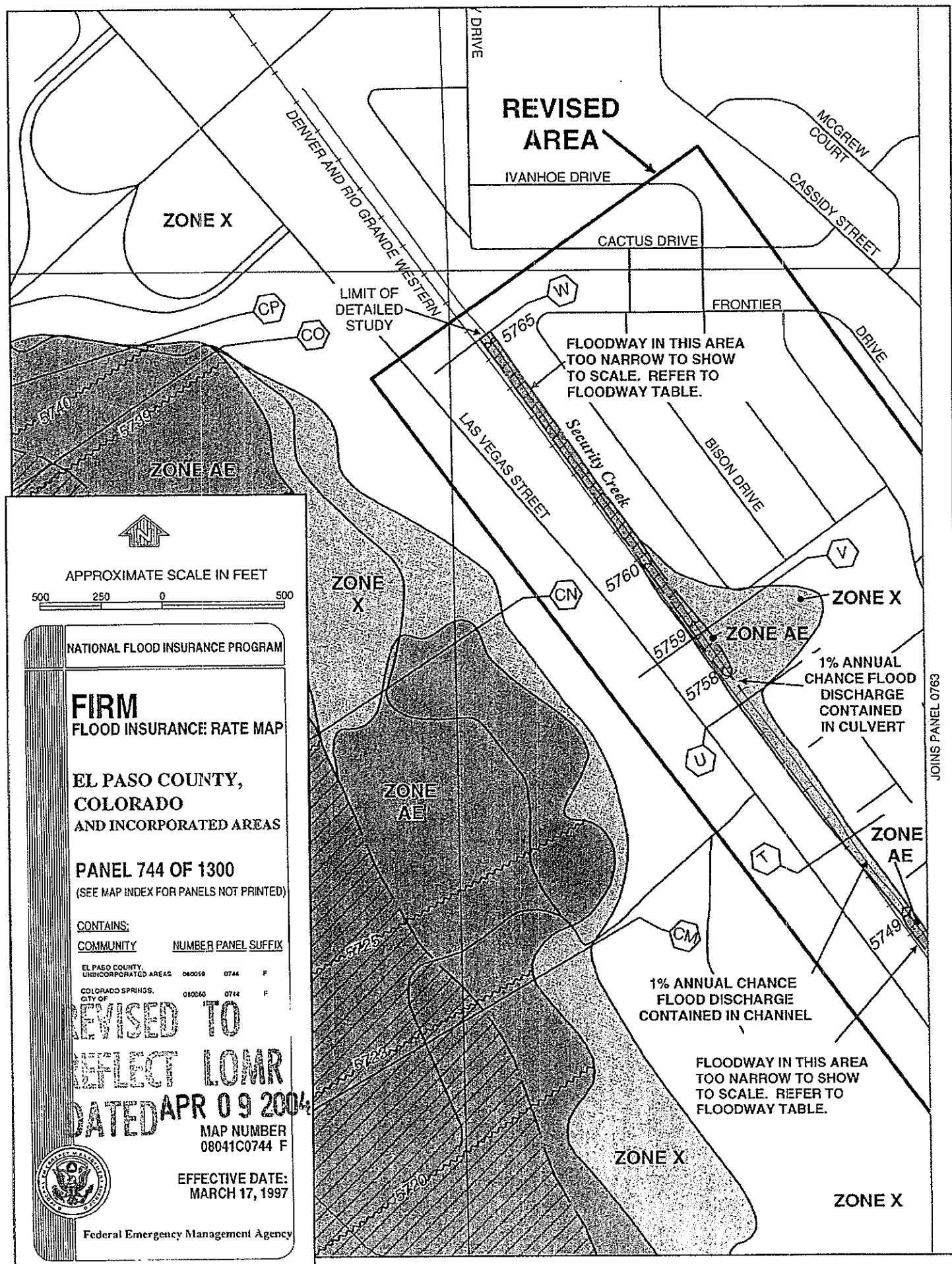
SOILS MAP

N.T.S.

ADPcIVIL

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**PRELIMINARY/FINAL DRAINAGE REPORT
SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX B
DRAINAGE CALCULATIONS**

SOUTH ACADEMY BUSINESS CENTER							
C FACTOR CALCULATION SHEET							
RUNOFF COEFFICIENT							
TYPE C SOILS							
LAND USE			5 YR	100 YR			
UNDEV & LOOSE GRAVEL			0.15	0.5			
STREETS/PARKING GRAVEL			0.63	0.74			
ROOFS/ PAVED AREAS			0.75	0.83			
Historic Conditions							
	TOTAL	SURFACE CONDITION AREAS			CALCULATED C		
AREA	AREA	UNDEV	STREETS/ PARKING	ROOFS/ PAVED	5	100	
DESIG.	(acre)		GRAVEL	AREAS	YR	YR	
Aex	6.40	6.40			0.15	0.50	
Bex	1.30	1.30			0.15	0.50	
RUNOFF COEFFICIENT							
TYPE C SOILS							
LAND USE			5 YR	100 YR			
UNDEV & LOOSE GRAVEL			0.15	0.5			
STREETS/PARKING GRAVEL			0.63	0.74			
ROOFS/ PAVED AREAS			0.75	0.83			
Developed Conditions							
	TOTAL	SURFACE CONDITION AREAS			CALCULATED C		
AREA	AREA	UNDEV	LOOSE GRAVEL	ROOFS/ PAVED	5	100	
DESIG.	(acre)			AREAS	YR	YR	
A	7.30	1.80	2.90	2.60	0.36	0.62	
B	0.30	0.30			0.15	0.50	
IMPERVIOUS							
COVERAGE	ACREAGE	% IMP					
Undev	1.80	0	0				
Loose Grav	2.90	0.4	1.16				
Trailers	2.60	0.9	2.34				
	7.30		3.50				
		TOTAL IMP	47.95%				

SOUTH ACADEMY BUSINESS CENTER

DRAINAGE CALCULATION SHEET

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06/09/17	Rev 12/18/17
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[illegible]

Include the routing calc with OS1 plus A.

Unresolved.

Review 3: Based on the contours it appears that Basin OS1 drains into the site. If runoff from Basin OS1 does not flow through the site then specifically note as such in the sub-basin summary or else update the calculations accordingly to account for the offsite runoff from Basin OS1 routing through the property.

[illegible][illegible]

ti = (0 395*(1 1.C5)*1 A0 5)/S^0 33/(EQ 6-8)		
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$U = (0.250 \pm 1.1) \times 10^{-3}$	V from Fig 6.25
--------------------------------------	-------------------

<p> $T_4 = 1.7150$ </p>	<p> $V_{1000} = 1.1000$ </p>
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DITCH CAPACITY CALCULATION SHEET

Swale Location	Q5 cfs	Q100 cfs	S %
Outlet Swale	1.00	5.00	0.70
Spillway	4.70	14.30	1.00

FOREBAY CALCULATION SHEET

(Per Table EDB-4)

RELEASE RATE	OPENING	VOLUME	FOREBAY DEPTH	TRICKLE CHAN CAP
2% 100 yr sim	$Q = C \times D^{3/2}$	2% WQCV	$D = 6"$	OUTLET $Q = 0.28$ cfs
0.02 X 14.3 = 0.28 cfs	@ $W = 0.26'$	0.002 X 0.122 ac ft = 0.002 ac ft		@ $d = 4"$, $b = 1'$, $s = 0.5\%$
	$Q = 0.28$ cfs	0.002 ac ft x 43560 = 87.1 cf		MAX $Q = 0.79$ cfs

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Project: S Academy Business Ctr

Basin ID: A



Required Volume Calculation

Selected BMP Type = **EDB**

Watershed Area =	7.30	acres	Note: L / W Ratio = 8 L / W Ratio = 11.4
Watershed Length =	1,900	ft	
Watershed Slope =	0.007	ft/ft	
Watershed Imperviousness =	48.00%	percent	
Percentage Hydrologic Soil Group A =	0.0%	percent	
Percentage Hydrologic Soil Group B =	0.0%	percent	
Percentage Hydrologic Soil Group C/D =	100.0%	percent	
Desired WQCV Drain Time =	40.0	hours	
Location for 1-yr Rainfall Depth =	Denver - Capital Building		
Water Quality Capture Volume (WQCV) =	0.122	acm-feet	
Excess Urban Runoff Volume (EURV) =	0.330	acm-feet	Optional User Overrides 1-yr Precipitation 1.00 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches 3.01 inches
2-yr Runoff Volume (P1 = 1.19 in.) =	0.310	acm-feet	
5-yr Runoff Volume (P1 = 1.51 in.) =	0.464	acm-feet	
10-yr Runoff Volume (P1 = 1.75 in.) =	0.601	acm-feet	
25-yr Runoff Volume (P1 = 2.1 in.) =	0.830	acm-feet	
50-yr Runoff Volume (P1 = 2.25 in.) =	1.003	acm-feet	
100-yr Runoff Volume (P1 = 2.52 in.) =	1.218	acm-feet	
500-yr Runoff Volume (P1 = 3.01 in.) =	1.579	acm-feet	
Approximate 2-yr Detention Volume =	0.291	acm-feet	
Approximate 5-yr Detention Volume =	0.437	acm-feet	
Approximate 10-yr Detention Volume =	0.499	acm-feet	
Approximate 25-yr Detention Volume =	0.541	acm-feet	
Approximate 50-yr Detention Volume =	0.561	acm-feet	
Approximate 100-yr Detention Volume =	0.642	acm-feet	

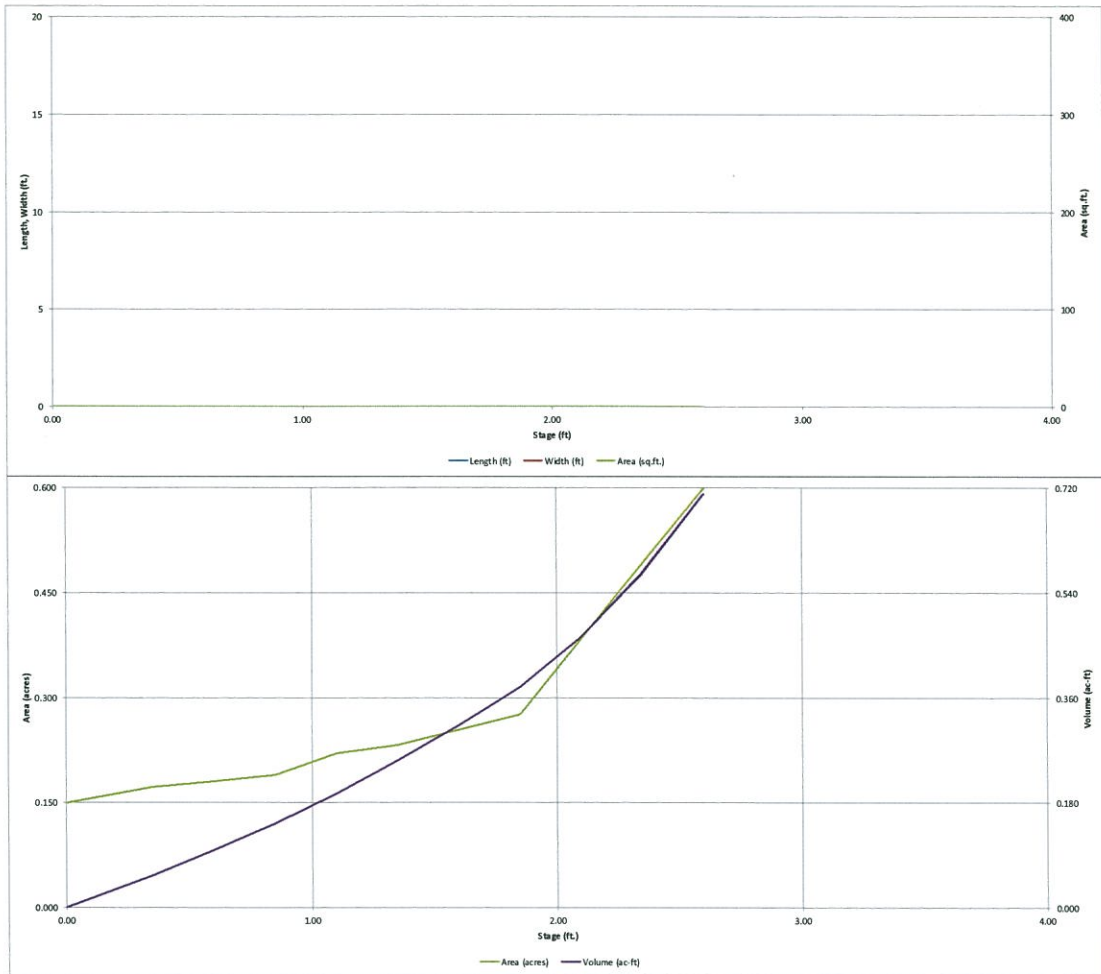
Zone 1 Volume (WQCV) = 0.122 acre-feet

Zone 2 Volume (ELURV - Zone 1) =	0.208	acre-foot
Zone 3 (100yr + 1/2 WQCV - Zones 1 & 2) =	0.373	acre-foot
Total Detention Basin Volume =	0.703	acre-foot
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{AD}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{MB}) =	user	ft/V
Basin Length-to-Width Ratio (R _{MB}) =	user	
Initial Surcharge Area (A _{IS}) =	user	ft ²
Surcharge Volume Length (L _{IS}) =	user	ft
Surcharge Volume Width (W _{IS}) =	user	ft
Depth of Basin Floor (H _{100yr}) =	user	ft
Length of Basin Floor (L _{100yr}) =	user	ft
Width of Basin Floor (W _{100yr}) =	user	ft
Area of Basin Floor (A _{100yr}) =	user	ft ²
Volume of Basin Floor (V _{100yr}) =	user	ft ³
Depth of Main Basin (H _{MB}) =	user	ft
Length of Main Basin (L _{MB}) =	user	ft
Width of Main Basin (W _{MB}) =	user	ft
Area of Main Basin (A _{MB}) =	user	ft ²
Volume of Main Basin (V _{MB}) =	user	ft ³
Calculated Total Basin Volume (V _{MB}) =	user	acre-foot

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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

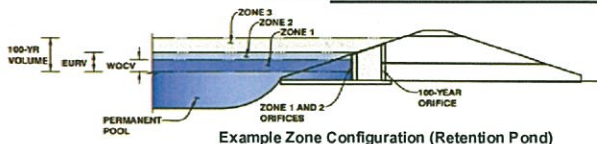


Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: s Academy Business Ctr

Basin ID: A



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.65	0.122	Orifice Plate
Zone 2 (EURV)	1.50	0.208	Orifice Plate
100+1/2WQCV	2.42	0.373	Weir&Pipe (Rect.)
		0.703	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-3/4 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.50	1.00					
Orifice Area (sq. inches)	2.45	2.45	2.45					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Zone 3 Weir Not Selected
Overflow Weir Front Edge Height, Ho = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Slope = H:V (enter zero for flat grate)
Horiz. Length of Weir Sides = feet
Overflow Grate Open Area % = %
Debris Clogging % = %

Calculated Parameters for Overflow Weir

Zone 3 Weir Not Selected
Height of Grate Upper Edge, H_u = feet
Over Flow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area = should be ≥ 4
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Rectangular Not Selected
Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Rectangular Orifice Width = inches
Rectangular Orifice Height = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Zone 3 Rectangular Not Selected
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

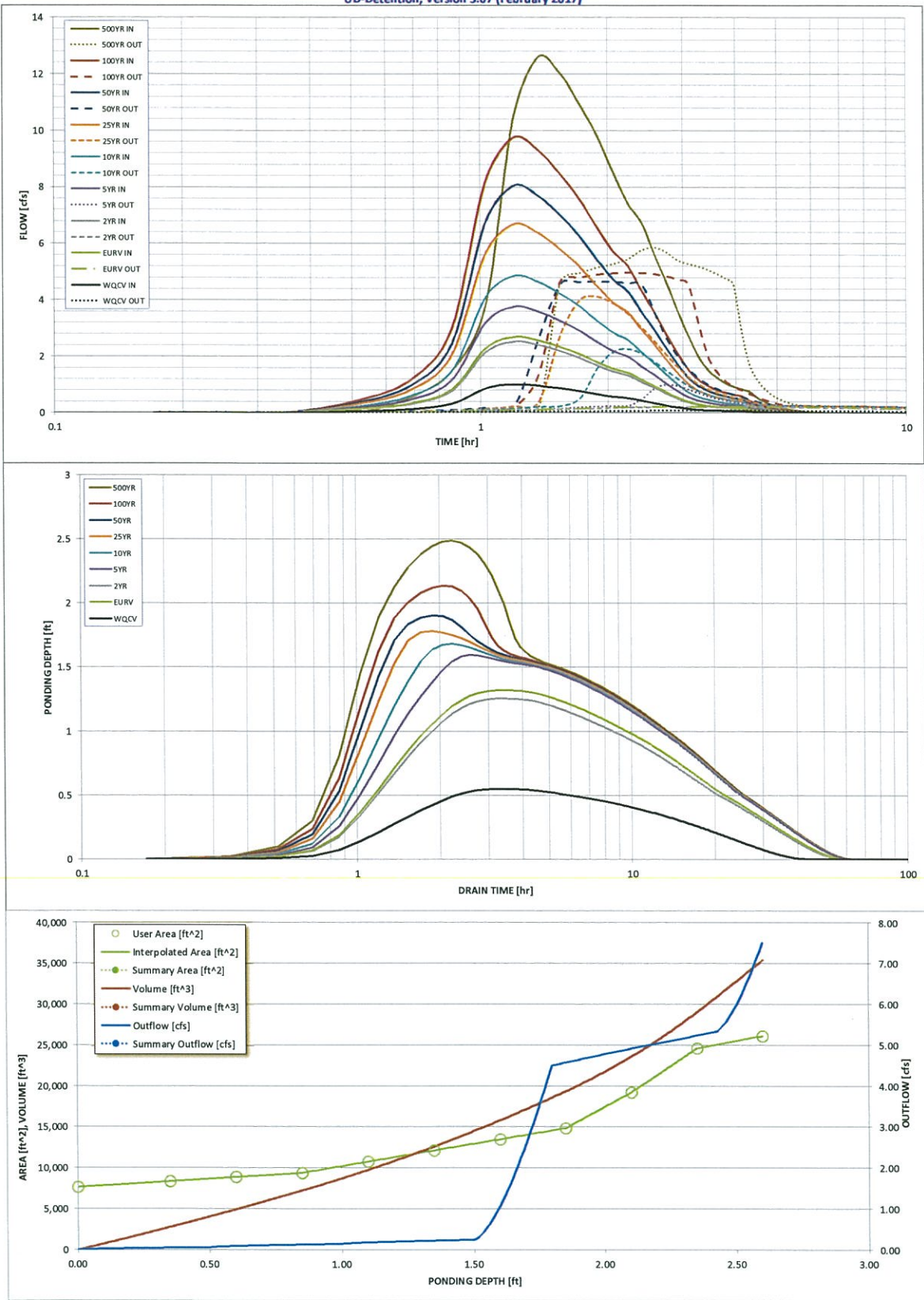
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in)	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.01
Calculated Runoff Volume (acre-ft)	0.122	0.330	0.310	0.464	0.601	0.830	1.003	1.218	1.579
OPTIONAL Override Runoff Volume (acre-ft)									
Inflow Hydrograph Volume (acre-ft)	0.121	0.330	0.310	0.463	0.600	0.830	1.002	1.217	1.578
Predevelopment Unit Peak Flow, q (cfs/acre)	0.00	0.00	0.01	0.07	0.19	0.47	0.62	0.82	1.15
Predevelopment Peak Q (cfs)	0.0	0.0	0.1	0.5	1.4	3.4	4.5	6.0	8.4
Peak Inflow Q (cfs)	1.0	2.7	2.5	3.7	4.8	6.7	8.0	9.7	12.6
Peak Outflow Q (cfs)	0.1	0.2	0.2	1.0	2.3	4.1	4.6	5.0	5.9
Ratio Peak Outflow to Predevelopment Q	N/A	N/A	N/A	2.0	1.6	1.2	1.0	0.8	0.7
Structure Controlling Flow	Plate	Plate	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps)	N/A	N/A	N/A	0.1	0.3	0.6	0.7	0.7	0.8
Max Velocity through Grate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours)	37	48	47	49	47	44	42	40	37
Time to Drain 99% of Inflow Volume (hours)	40	53	52	55	54	52	51	50	49
Maximum Ponding Depth (ft)	0.55	1.32	1.25	1.59	1.68	1.78	1.90	2.13	2.49
Area at Maximum Ponding Depth (acres)	0.20	0.27	0.27	0.31	0.32	0.33	0.36	0.46	0.58
Maximum Volume Stored (acre-ft)	0.102	0.278	0.262	0.359	0.388	0.417	0.461	0.555	0.742

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

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SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX C
DESIGN CHARTS**

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis-- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Figure 6-25. Estimate of Average Concentrated Shallow Flow

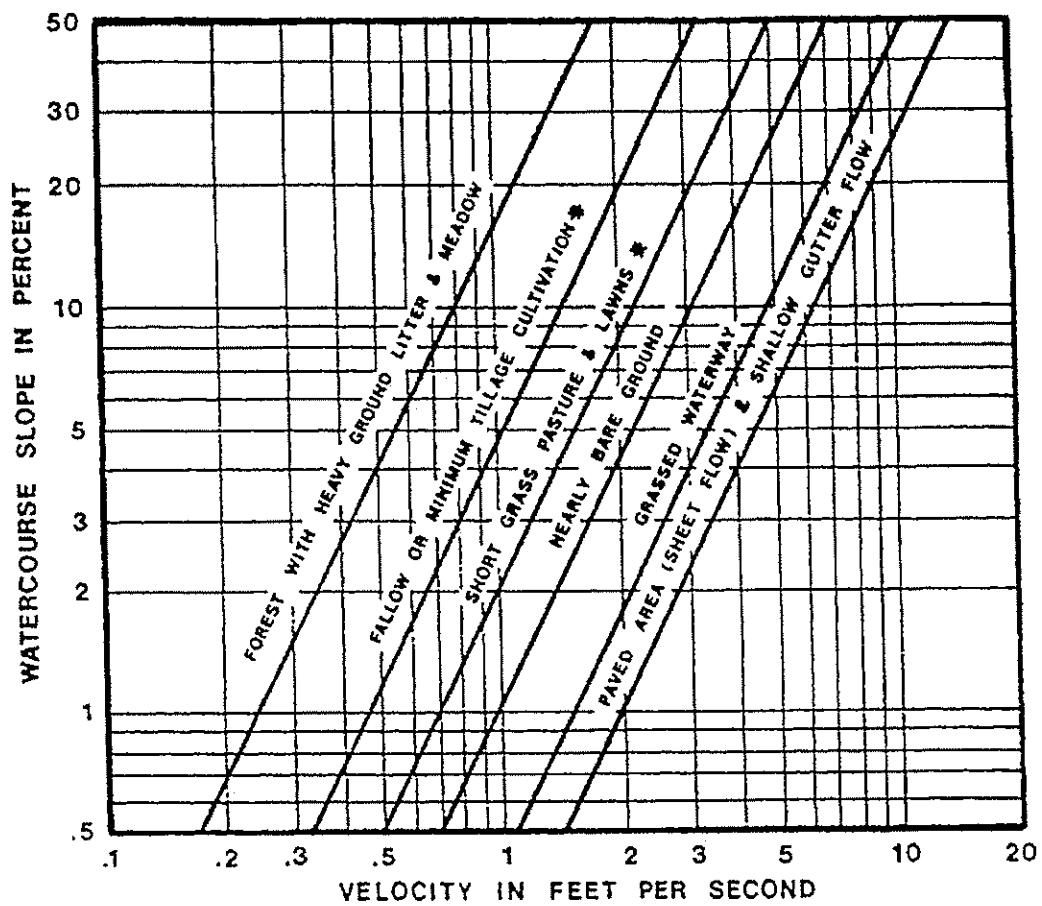
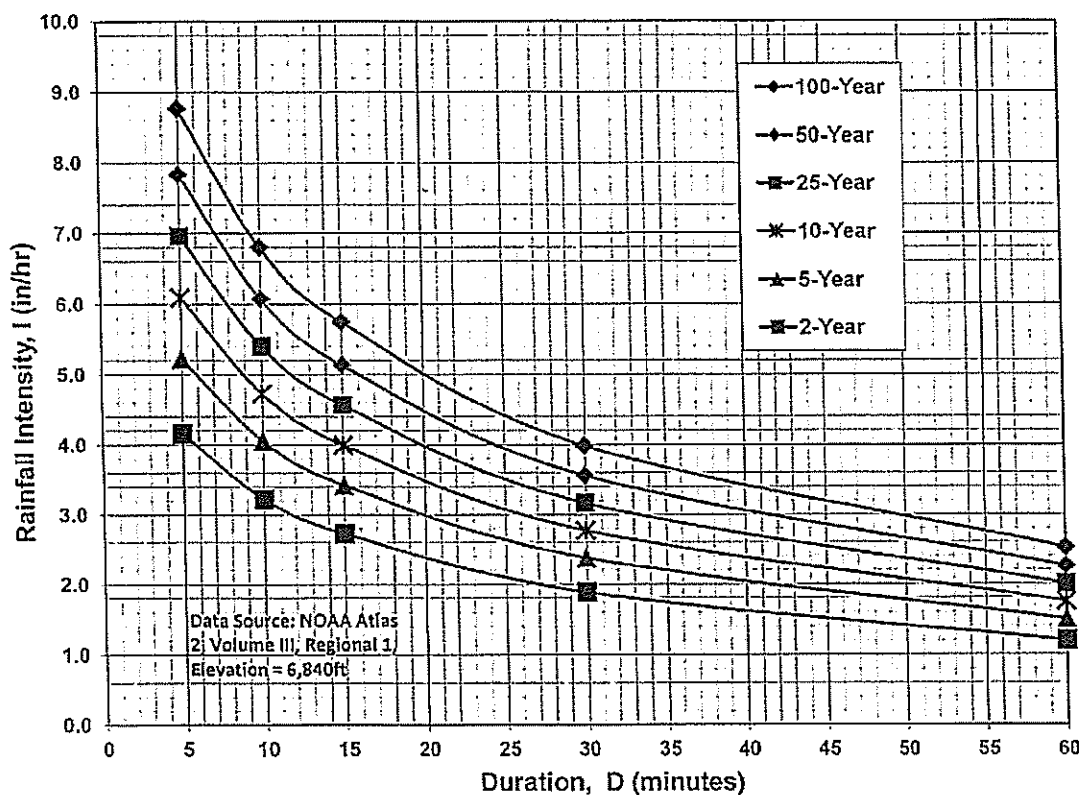


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

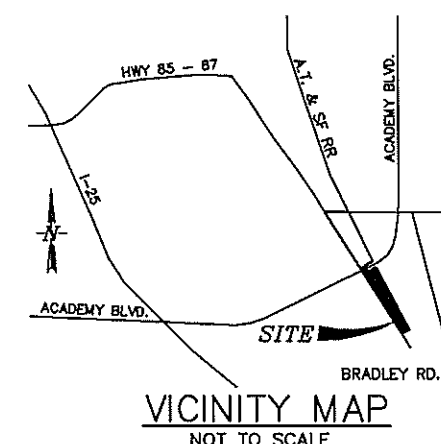
$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

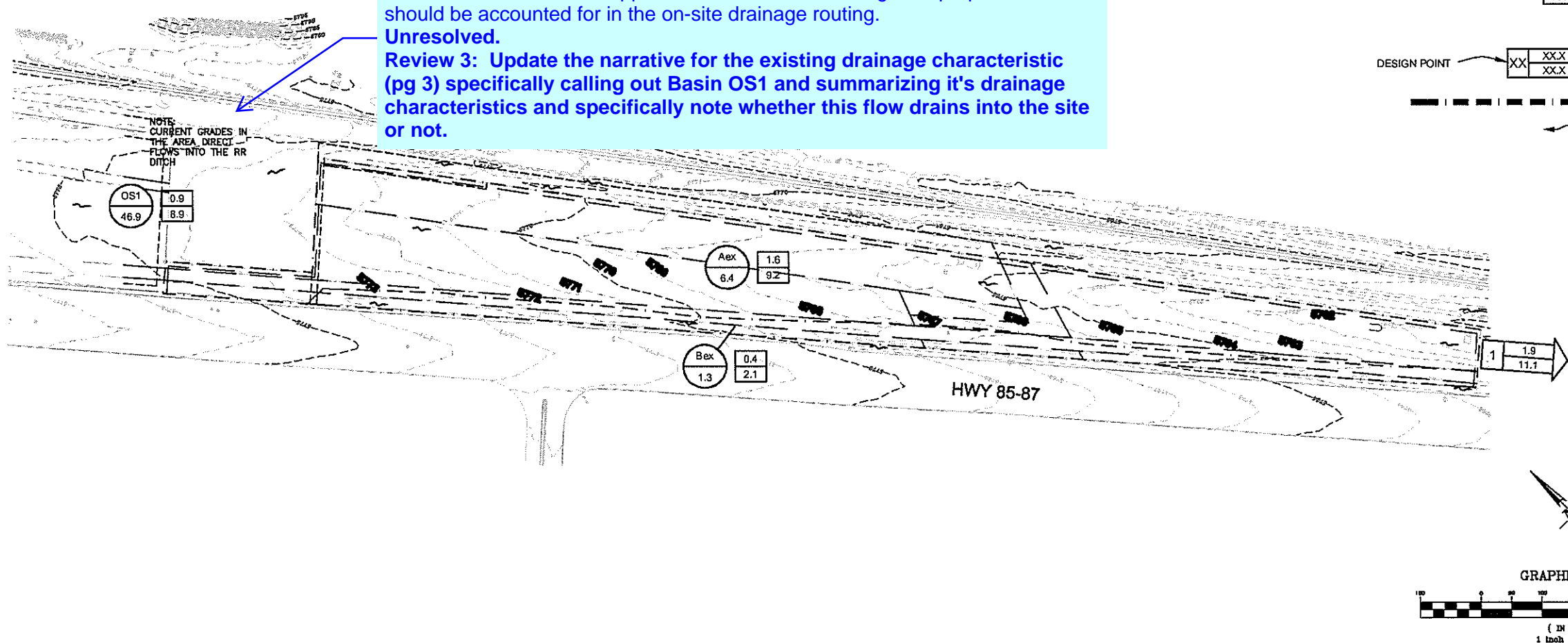
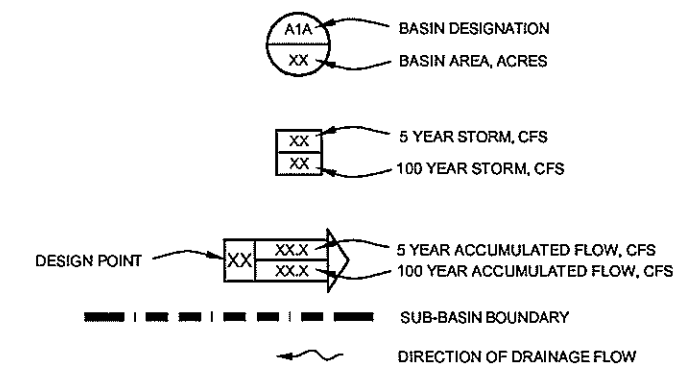
$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.



LEGEND



Include in the rational method calculation in Appendix B and describe/summarize in the narrative section of the report. Based on the contours it appears that this drains through the proposed site and should be accounted for in the on-site drainage routing.

Unresolved.

Review 3: Update the narrative for the existing drainage characteristic (pg 3) specifically calling out Basin OS1 and summarizing it's drainage characteristics and specifically note whether this flow drains into the site or not.

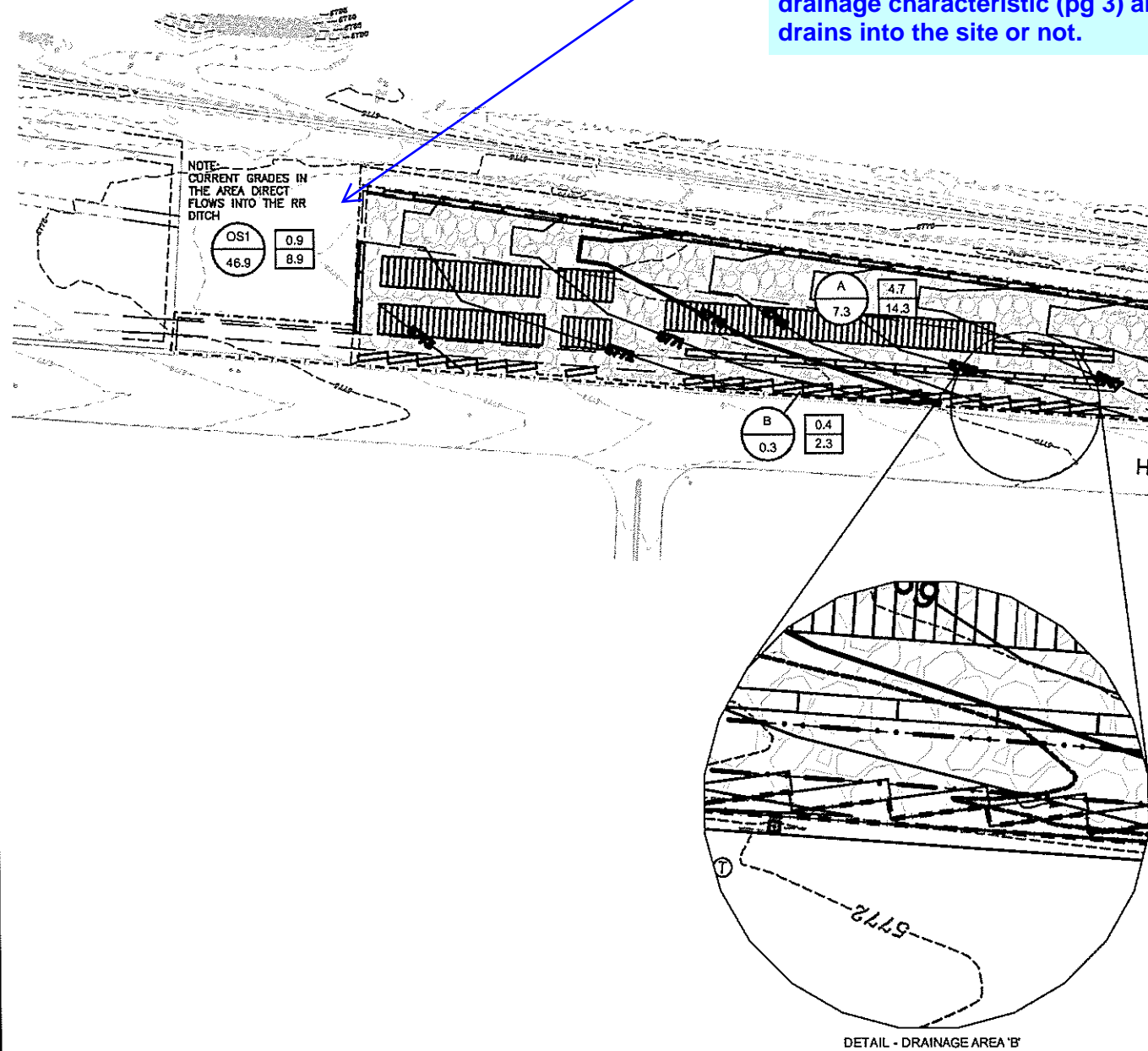
ASSOCIATED DESIGN PROFESSIONALS

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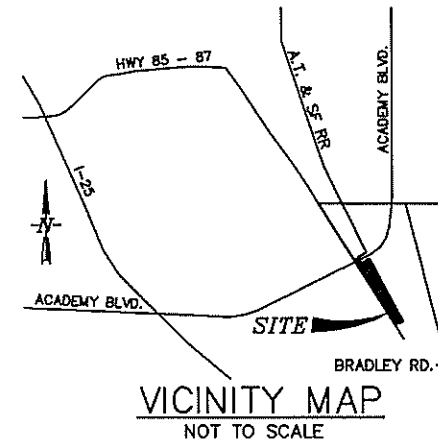
MICHAEL BARTUSEK, COLORADO P.E. #2332

DATE _____

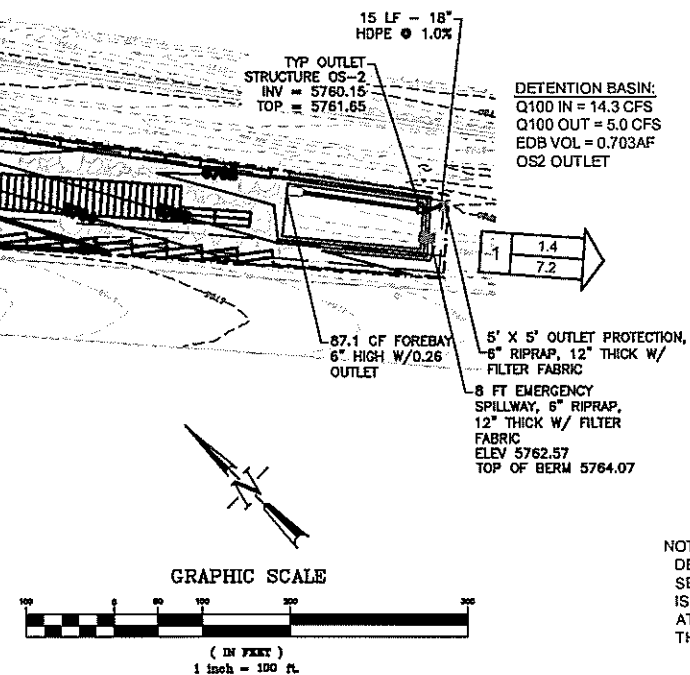
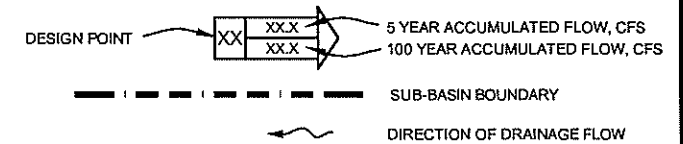
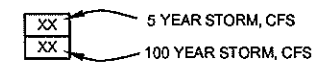
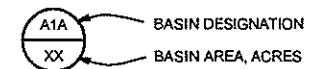
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Include in the rational method calculation in Appendix B and describe/summarize in the narrative section of the report. Based on the contours it appears that this drains through the proposed site and should be accounted for in the on-site drainage routing.
Unresolved.
Review 3: Provide a subbasin summary for Basin OS1 in the existing drainage characteristic (pg 3) and specifically note whether this flow drains into the site or not.



LEGEND



NOTE:
DETENTION POND AREA TO BE UTILIZED AS A SEDIMENTATION BASIN UNTIL EARTH MOVING IS COMPLETED AND THE GROUND STABILIZED, AT WHICH TIME IT WILL BE CLEANED OUT AND THE DETENTION POND STRUCTURES ADDED.

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MICHAEL BARTUSEK, COLORADO P.E. #23329

DATE

PREPARED BY:

ADPCIVIL
ENGINEERING FOR THE FUTURE

3520 Austin Bluffs Parkway
Suite 102
Colorado Springs, CO 80915
(719) 266-5212
Fax: (719) 266-0341

BY	REVISION	DATE	NO.

SOUTH ACADEMY BUSINESS CENTER
4425 HWY 85-87

EL PASO COUNTY, COLORADO

DRAINAGE PLAN - PROPOSED CONDITIONS

SHEET

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