



COTTAGES AT KETTLE CREEK

PRELIMINARY DRAINAGE REPORT

ALL TERRAIN ENGINEERING PROJECT NO: 24026

OCTOBER 2024

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I. General Purpose, Location & Description

a. Purpose

The purpose of this Preliminary Drainage Report (PDR) for COTTAGES AT KETTLE CREEK is to describe the site's onsite and offsite drainage patterns, existing and proposed storm infrastructure, and to safely route developed stormwater to adequate outfalls.

b. Location

COTTAGES AT KETTLE CREEK, referred to as 'the site' herein, is in Section 28, Township 12 South and Range 66 West of the 6th P.M., Colorado Springs, El Paso County, Colorado. The site is bound by Old Ranch Road to the south and undeveloped parcels to the east, west and north. Surrounding platted developments include Kettle Creek Estates to the south, Fairlane Technology Park No. 4A and 4B to the west and Pendleton Subdivision to the north.

c. Description of Property

The site is approximately 11.11 acres with existing vegetation consisting of native grasses and trees. The approximate disturbed area is 8.97 acres. The site is currently unplatted. The development will plat a single lot with 85 duplex units. In general, the site slopes southeasterly towards Old Ranch Road and Kettle Creek. Onsite elevations range from 6,700' – 6,726' with slopes ranging 1 – 50%. Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam and Type B Stapleton-Bernal sandy loams.

The existing site is partially developed with a single family residential buildings and associated structures. The site is zoned RR-2.5 (Rural Residential 2.5 acres). The Kettle Creek major drainageway traverses the eastern property line, however; the site is not within a Streamside Overlay Zone. The site is partially encumbered by a Preble's Jumping Mouse habitat.

There are no irrigation facilities on the site. Onsite, existing utilities include water, sewer, fiberoptic, communications, gas and overhead electric.

d. Floodplain Statement

Based on FEMA Firm map 08041C0506G dated December 7, 2018, the site is Zone X, which are areas determined to be outside the 0.2% annual chance flood.

II. Drainage Basins

a. Major Basin Description

The site is located within the Kettle Creek Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

1. "Drainage Basin Planning Study for Kettle Creek Basin" prepared by JR Engineering, May 2015.

Per the DBPS, the site is located within Basin B32 and flows from Basin B32 outfall to Kettle Creek at J24. Per the DBPS, improvements are needed to stabilize the creek adjacent to the site. Recommended channel

improvements were proposed with this DBPS; however, the City of Colorado Springs is currently studying Kettle Creek to provide updated recommendations for channel improvements.

b. Existing Subbasin Description

The existing site's drainage patterns are relatively uniform to the southeast. Existing stormwater drains towards Old Ranch Road and Kettle Creek. There is no existing storm sewer located on-site. See below for existing basin descriptions:

Basin EX1 is 15.11 acres of undeveloped land, existing residential buildings and Kettle Creek Road. Existing stormwater from this basin ($Q_5 = 3.7$ cfs $Q_{100} = 19.6$ cfs) flows to DP1. Stormwater at DP1 overtops Old Ranch Road and continues south.

Basin EX2 is 6.56 acres of undeveloped land and existing residential buildings. Existing stormwater from this basin ($Q_5 = 1.8$ cfs $Q_{100} = 9.6$ cfs) flows to an existing swale along the north side of Old Ranch Road at DP2. From here, stormwater drains east into Kettle Creek.

Basin EX3 is 10.41 acres of undeveloped land and Kettle Creek. Existing stormwater from this basin ($Q_5 = 2.2$ cfs $Q_{100} = 14.9$ cfs) drains directly into Kettle Creek at DP3. Stormwater at DP3 is conveyed under Old Ranch Road in an existing culvert. The size and material of the culvert are not known.

c. Proposed Subbasin Description

The proposed site has been divided into 10 subbasins for analysis. See below for proposed basin descriptions:

Basin A is 1.98 acres of roadway, duplex units and landscaping. Stormwater from this basin ($Q_5 = 4.7$ cfs, $Q_{100} = 9.8$ cfs) is conveyed in curb and gutter to DP1. Stormwater at DP1 is captured in a 15' Type R inlet (private, on-grade). Captured flows at DP1 are piped to DP4.1 and continue to Pond 1. A berm will be constructed along the northern property line of Basin A to direct offsite stormwater around the site to the west.

Basin B is 2.26 acres of roadway, duplex units and landscaping. Stormwater from this basin ($Q_5 = 5.4$ cfs, $Q_{100} = 11.2$ cfs) is conveyed in curb and gutter to DP2. Stormwater at DP2 is captured in a 15' Type R inlet (private, on-grade). Captured flows at DP2 are piped to DP3.1 and continue to Pond 1. A berm will be constructed along the northern property line of Basin B to direct offsite stormwater around the site to the east.

Basin C is 0.53 acres of roadway, duplex units and landscaping. Stormwater from this basin ($Q_5 = 1.4$ cfs, $Q_{100} = 2.9$ cfs) is conveyed in curb and gutter to DP4. Stormwater at DP4 is captured in a 10' Type R inlet (private, on-grade). Captured flows at DP4 are piped to DP4.1 and continue to Pond 1.

Basin D is 1.57 acres of roadway, duplex units and landscaping. Stormwater from this basin ($Q_5 = 4.8$ cfs, $Q_{100} = 9.3$ cfs) is conveyed in curb and gutter to DP3. Stormwater at DP3 is captured in a 15' Type R inlet (private, on-grade). Captured flows at DP3 are piped to DP3.1 and continue to Pond 1.

Basin E is 0.50 acres of landscaping area and Pond 1. Stormwater from this basin ($Q_5 = 0.4$ cfs, $Q_{100} = 1.8$ cfs) flows directly into Pond 1. See Water Quality and Detention section for Pond 1 details.

Basin F is 0.22 acres of roadway and landscaping. Stormwater from this basin ($Q_5 = 0.5$ cfs, $Q_{100} = 1.2$ cfs) is not captured on site. Basin F stormwater is conveyed in curb and gutter towards Old Ranch Road (DP6) and is captured in a roadside swale along the north side of Old Ranch Road. The roadside swale follows historic drainage patterns and discharges into Kettle Creek to the east of the site. The proposed flow to the roadside ditch is less than the existing condition. Pond 1 will overdetain the 5-year and 100-year storms by an amount equal to the undetained discharge from Basin F. See Water Quality and Detention section for Pond 1 details.

Basin G is 0.96 acres of offsite, undeveloped area and Old Ranch Road improvements. The City of Colorado Springs required the addition of turn lanes on Old Ranch Road. The addition of turn lanes expanded the existing pavement edge approximately 12' to the north. These improvements are downstream of the pond and can not be captured nor detained. Basin G stormwater ($Q_5 = 0.7$ cfs, $Q_{100} = 2.5$ cfs) follows historic drainage patterns along Old Ranch Road to the east in a roadside ditch. The existing roadside ditch has been shifted north per the expanded pavement, however; the total flow in the swale is reduced compared to the existing condition (Existing $Q_{100} = 9.6$ cfs, Proposed $Q_{100} = 4.1$ cfs). In the existing condition, the swale was over capacity. With the limited space between the Old Ranch Road pavement expansion and the existing right-of-way, the proposed swale has capacity for the 100-year flow but can only achieve 0.5' freeboard. A cross section is provided in Appendix C.

Basin OS1 is 1.97 acres of offsite, undeveloped area and Kettle Creek Road. Stormwater from this basin ($Q_5 = 1.1$ cfs, $Q_{100} = 4.5$ cfs) follows historic drainage patterns southerly along Kettle Creek Road to Old Ranch Road at DP8. Basin OS1 is not detained in Pond 1.

Basin OS2 is 12.06 acres of offsite, undeveloped area and Kettle Creek Road. Stormwater from this basin ($Q_5 = 2.7$ cfs, $Q_{100} = 15.3$ cfs) follows the historic drainage patterns of Basin EX1 to DP9. A berm along the site's northern boundary will ensure offsite flows from Basin OS2 do not enter the site. Basin OS2 is not detained in Pond 1.

Basin OS3 is 10.37 acres of offsite, undeveloped area and Kettle Creek. Stormwater from this basin ($Q_5 = 2.2$ cfs, $Q_{100} = 14.8$ cfs) follows the historic drainage patterns of Basin EX2 to DP10. A berm along the site's northern boundary will ensure offsite flows from Basin OS3 do not enter the site. Basin OS3 drains directly to Kettle Creek and is not detained in Pond 1.

III. Drainage Design Criteria

a. Development Criteria Reference

The drainage analysis, proposed storm sewer system, and proposed private, full spectrum water quality and detention pond follow the criteria from the "City of Colorado Springs Drainage Criteria Manual" Volumes 1 and 2" (CCSDCM, latest revision).

b. Hydrologic Criteria

Hydrologic data was obtained from the “City of Colorado Springs Drainage Criteria Manual – Chapter 6 Hydrology”. Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using 1-hr duration rainfall depths from NOAA Atlas 14. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District’s (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Full Spectrum Detention. The detention pond allowable release rate will be limited to historic rates.

d. Hydraulic Criteria

Hydraulic criteria for inlet sizing were obtained from the “City of Colorado Springs Drainage Criteria Manual – Chapter 8 Inlets”. Hydraulic criteria for storm sewer sizing were obtained from the “City of Colorado Springs Drainage Criteria Manual – Chapter 9 Storm Sewer”. Hydraulic criteria for channel sizing were obtained from the “City of Colorado Springs Drainage Criteria Manual – Chapter 12 Open Channels”.

Outfall tailwater conditions into detention facilities are based on the hydraulic grade line in the pond at the time of concentration of the tributary basin. The hydraulic grade line is adapted from the UD-Detention Drain Time v. Ponding Depth graph presented in Appendix D.

IV. Drainage Facility Design

a. General Concept

Onsite stormwater will be conveyed via curb and gutter to Type R inlets (on-grade, private). Captured stormwater will be piped to and detained in a private, full spectrum detention pond (Pond 1). Pond 1 will outfall at less than historic values to Kettle Creek. Kettle Creek is the historic outfall for the site.

b. Water Quality & Detention

Water quality and detention for Basins A – E is provided in a Pond 1, a private, full spectrum detention pond located along Old Ranch Road. Due to topography, Basin F can not be captured and routed to Pond 1. The total flow from Basin F is $Q_5 = 0.5$ cfs, $Q_{100} = 1.2$ cfs. As a result of this undetained flow leaving the site, the pond outlet structure has been designed to overdetain flow equal to the Basin F discharge. A total of 6.84 acres at 62.7% composite imperviousness will be detained in Pond 1. The WQCV is 0.140 ac-ft, the EURV is 0.387 ac-ft, and the 100-year volume is 0.265 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 72 and 79 hours, respectively. A forebay is located at the outfall into the pond and a 2.0’ trickle channel conveys flow towards the outlet structure. A 10’ access and maintenance road is provided to the bottom of the pond to facilitate future maintenance of the pond facilities. A 6’ emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0’ of freeboard towards Old Ranch Road. The spillway and downstream outfall will be lined with Type L. Pond design calculations are presented in Appendix D.

c. Operations & Maintenance

An Operations and Maintenance Manual will be submitted during the Final Drainage Report phase.

d. Grading & Erosion Control Plan

Due to the project disturbance area, a separate Grading and Erosion Control plan is required. The Grading and Erosion Control Plan will be submitted during the Final Drainage Report phase.

e. Four Step Method

Step 1 – Reducing Runoff Volumes: Cottages at Kettle Creek consists of duplex units with associated parking, sidewalks and landscape areas. The landscaped area disconnect impervious areas and reduce runoff volumes. Where possible, roof drains will route across landscape areas to promote infiltration. MHFD UD-BMP was used to calculate runoff reductions. The WQCV reduction for the site is 31%. The runoff reductions calculation and map are presented in Appendix B and F, respectively.

Step 2 – Treat and slowly release the WQCV: An onsite private, full spectrum detention pond (Pond 1) provides water quality treatment for the site. The WQCV is released over a period of 40 hours. The developed area of the site is contained within Basins A – F.

Step 3 – Stabilize stream channels: All new and re-development projects are required to construct or participate in the funding of channel stabilization measures. Drainage basin fees paid, at the time of platting, go towards channel stabilization within the drainage basin. The site lies adjacent to Kettle Creek. The City of Colorado Springs is currently completing a channel study of Kettle Creek. The channel study will determine the required improvements along the site’s frontage to Kettle Creek. Once the study is completed, the necessary improvements or fees in lieu will be detailed here.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development. However, permanent erosion control measures will be provided in the form of asphalt drives, curb and gutter, storm inlets and storm sewer. Per MHFD guidance, the following permanent source controls may be necessary for residential development: S-3 Disposal of Household Waste, S-4 Illicit Discharge Controls, S-5 Good Housekeeping, S-8 Use of Pesticides, Herbicides and Fertilizers, S-9 Landscape Maintenance, and S-10 Snow and Ice Management.

f. Drainage Basin & Bridge Fees

Kettle Creek is a closed basin and therefore no fees are due. Building permits cannot be released for the site until the channel improvements are installed or channel improvement assurances have been paid.

g. Engineer’s Opinion of Probable Cost

An engineer’s opinion of probable cost will be included during the Final Drainage Report phase.

V. Summary

COTTAGES AT KETTLE CREEK remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest City of Colorado Springs Drainage criteria and is in accordance with the Kettle Creek DBPS.



VI. References

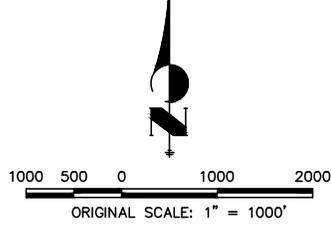
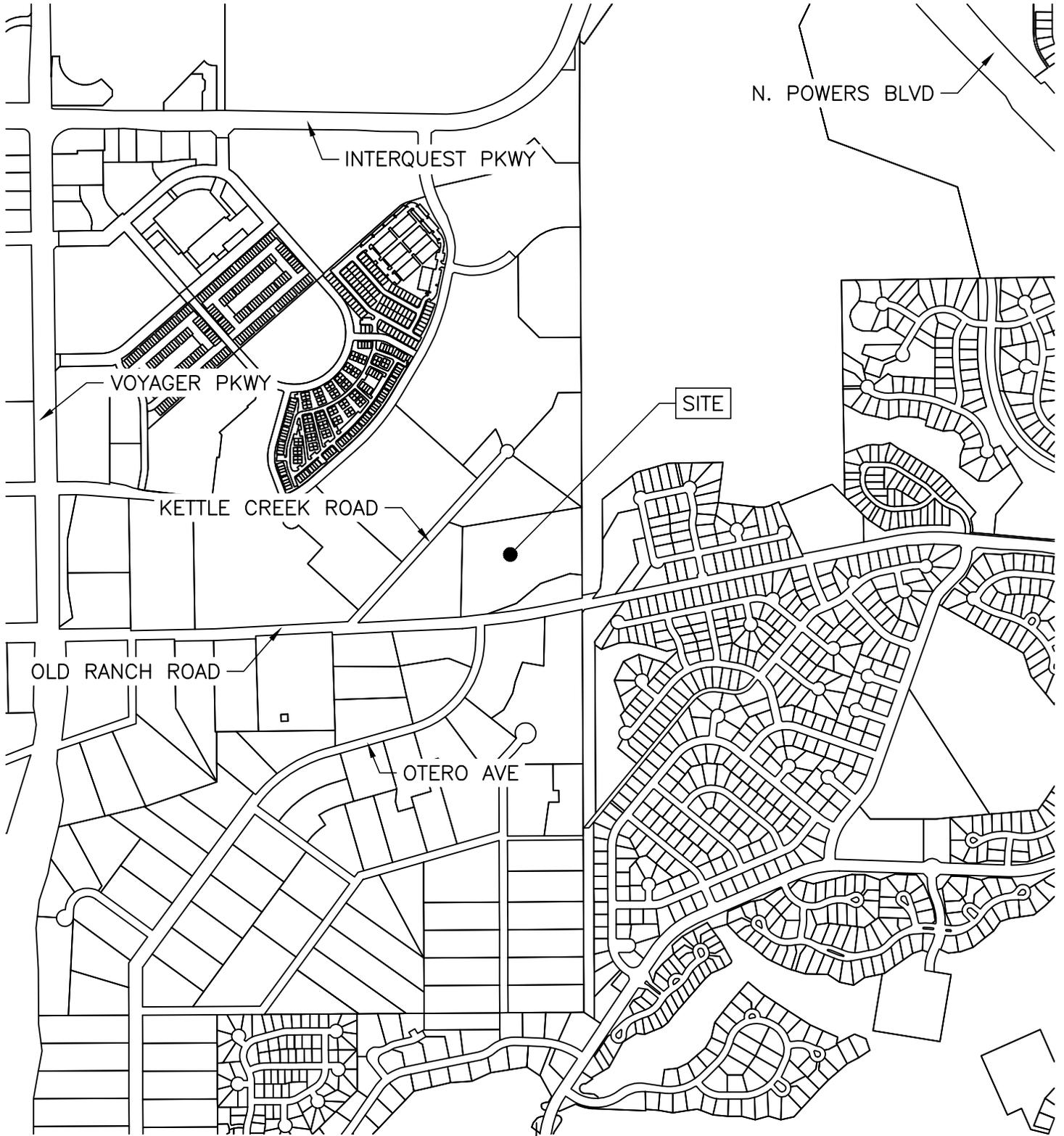
1. City of Colorado Springs – Drainage Criteria Manual, May 2014, Revised January 2021.
2. Urban Storm Drainage Criteria Manual, Mile High Flood District, January 2018.



**APPENDIX A – VICINITY MAP, FEMA MAP, NRCS WEB SOIL SURVEY & NOAA
ATLAS 14**

COTTAGES AT KETTLE CREEK

VICINITY MAP

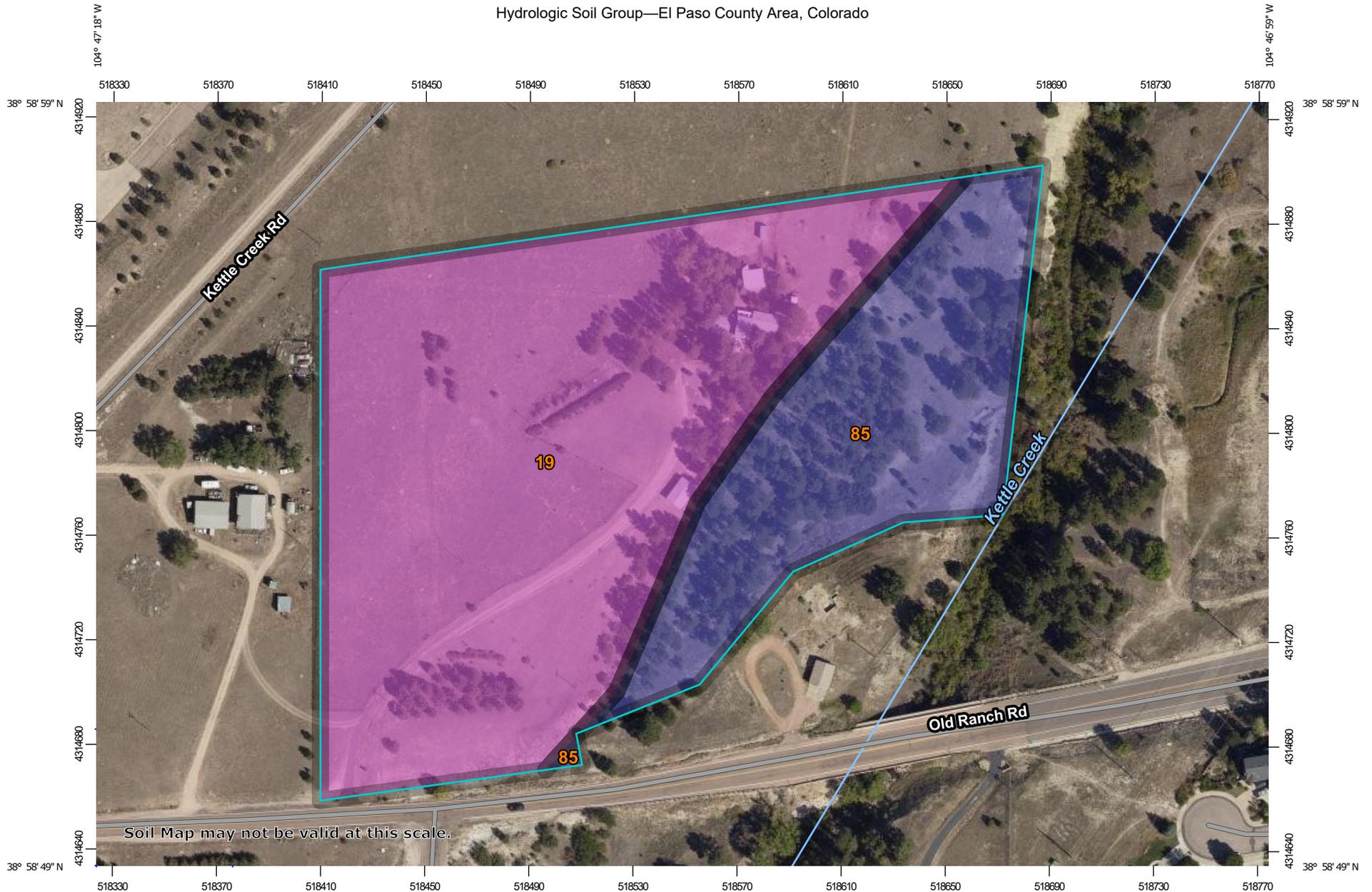


| | |
|--------------------------|-------|
| VICINITY MAP | |
| COTTAGES AT KETTLE CREEK | |
| JOB NO. 24026 | |
| LOCATION: CS | SHEET |
| 10/03/2024 | |
| SHEET: 1 | |

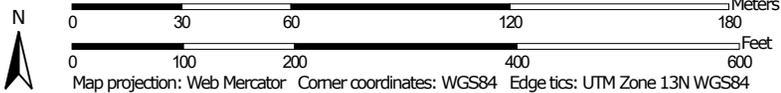
TALL
ENGINEERING

1004 WEST VAN BUREN STREET
COLORADO SPRINGS, CO 80907

Hydrologic Soil Group—El Paso County Area, Colorado



Map Scale: 1:2,060 if printed on A landscape (11" x 8.5") sheet.



MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

Soil Rating Polygons

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points

-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 21, Aug 24, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| 19 | Columbine gravelly sandy loam, 0 to 3 percent slopes | A | 8.1 | 70.5% |
| 85 | Stapleton-Bernal sandy loams, 3 to 20 percent slopes | B | 3.4 | 29.5% |
| Totals for Area of Interest | | | 11.5 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



NOAA Atlas 14, Volume 8, Version 2
Location name: Colorado Springs, Colorado, USA*
Latitude: 38.9824°, Longitude: -104.7856°
Elevation: 6728 ft**
 * source: ESRI Maps
 ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

PF tabular

| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹ | | | | | | | | | | |
|--|-------------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------|------------------------------|-----------------------------|-----------------------------|
| Duration | Average recurrence interval (years) | | | | | | | | | |
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.231 (0.190-0.281) | 0.286 (0.235-0.349) | 0.381 (0.312-0.466) | 0.464 (0.378-0.570) | 0.584 (0.462-0.750) | 0.682 (0.525-0.886) | 0.785 (0.582-1.04) | 0.893 (0.633-1.22) | 1.04 (0.709-1.46) | 1.16 (0.767-1.65) |
| 10-min | 0.338 (0.278-0.412) | 0.419 (0.345-0.511) | 0.558 (0.457-0.683) | 0.679 (0.554-0.835) | 0.856 (0.676-1.10) | 0.999 (0.768-1.30) | 1.15 (0.852-1.53) | 1.31 (0.927-1.78) | 1.53 (1.04-2.14) | 1.70 (1.12-2.41) |
| 15-min | 0.412 (0.339-0.502) | 0.511 (0.420-0.623) | 0.680 (0.558-0.833) | 0.828 (0.675-1.02) | 1.04 (0.824-1.34) | 1.22 (0.937-1.58) | 1.40 (1.04-1.86) | 1.59 (1.13-2.18) | 1.86 (1.27-2.61) | 2.07 (1.37-2.94) |
| 30-min | 0.583 (0.481-0.712) | 0.722 (0.594-0.882) | 0.960 (0.788-1.18) | 1.17 (0.953-1.44) | 1.47 (1.16-1.89) | 1.72 (1.32-2.23) | 1.98 (1.47-2.63) | 2.25 (1.60-3.07) | 2.63 (1.79-3.69) | 2.93 (1.93-4.16) |
| 60-min | 0.755 (0.622-0.921) | 0.911 (0.750-1.11) | 1.19 (0.977-1.46) | 1.45 (1.18-1.78) | 1.84 (1.46-2.38) | 2.17 (1.67-2.83) | 2.52 (1.87-3.37) | 2.90 (2.06-3.98) | 3.45 (2.35-4.86) | 3.89 (2.57-5.52) |
| 2-hr | 0.926 (0.768-1.12) | 1.10 (0.910-1.33) | 1.42 (1.17-1.73) | 1.73 (1.42-2.11) | 2.20 (1.77-2.84) | 2.61 (2.04-3.40) | 3.06 (2.30-4.08) | 3.56 (2.55-4.86) | 4.27 (2.94-5.99) | 4.86 (3.23-6.84) |
| 3-hr | 1.03 (0.857-1.24) | 1.20 (0.997-1.45) | 1.53 (1.27-1.85) | 1.86 (1.53-2.26) | 2.38 (1.93-3.09) | 2.85 (2.23-3.71) | 3.36 (2.54-4.49) | 3.94 (2.85-5.39) | 4.79 (3.31-6.71) | 5.49 (3.67-7.71) |
| 6-hr | 1.22 (1.02-1.46) | 1.40 (1.17-1.68) | 1.77 (1.47-2.12) | 2.14 (1.77-2.58) | 2.75 (2.25-3.56) | 3.30 (2.61-4.29) | 3.93 (2.99-5.21) | 4.63 (3.37-6.30) | 5.66 (3.95-7.90) | 6.53 (4.39-9.11) |
| 12-hr | 1.43 (1.20-1.70) | 1.66 (1.39-1.97) | 2.10 (1.76-2.51) | 2.54 (2.11-3.04) | 3.24 (2.66-4.14) | 3.87 (3.07-4.97) | 4.56 (3.49-6.00) | 5.34 (3.91-7.21) | 6.48 (4.55-8.97) | 7.43 (5.03-10.3) |
| 24-hr | 1.67 (1.41-1.97) | 1.96 (1.65-2.31) | 2.50 (2.10-2.96) | 3.00 (2.52-3.58) | 3.79 (3.11-4.77) | 4.47 (3.56-5.68) | 5.21 (4.00-6.78) | 6.03 (4.43-8.04) | 7.20 (5.07-9.86) | 8.16 (5.56-11.2) |
| 2-day | 1.94 (1.65-2.27) | 2.29 (1.95-2.69) | 2.91 (2.47-3.43) | 3.48 (2.94-4.12) | 4.34 (3.57-5.39) | 5.06 (4.04-6.35) | 5.83 (4.50-7.50) | 6.67 (4.92-8.80) | 7.85 (5.56-10.6) | 8.81 (6.04-12.0) |
| 3-day | 2.12 (1.82-2.48) | 2.50 (2.14-2.92) | 3.17 (2.70-3.72) | 3.77 (3.19-4.44) | 4.68 (3.85-5.77) | 5.43 (4.35-6.77) | 6.23 (4.82-7.97) | 7.09 (5.25-9.32) | 8.31 (5.91-11.2) | 9.30 (6.41-12.7) |
| 4-day | 2.28 (1.95-2.66) | 2.67 (2.29-3.12) | 3.37 (2.87-3.94) | 3.99 (3.38-4.69) | 4.92 (4.07-6.06) | 5.70 (4.58-7.09) | 6.53 (5.06-8.32) | 7.42 (5.51-9.72) | 8.68 (6.19-11.7) | 9.69 (6.70-13.2) |
| 7-day | 2.68 (2.31-3.11) | 3.10 (2.67-3.60) | 3.84 (3.30-4.47) | 4.51 (3.84-5.27) | 5.51 (4.57-6.73) | 6.34 (5.12-7.83) | 7.22 (5.63-9.14) | 8.17 (6.10-10.6) | 9.51 (6.82-12.7) | 10.6 (7.36-14.3) |
| 10-day | 3.04 (2.63-3.51) | 3.49 (3.02-4.03) | 4.29 (3.69-4.96) | 5.00 (4.27-5.81) | 6.05 (5.03-7.35) | 6.92 (5.61-8.51) | 7.85 (6.14-9.89) | 8.84 (6.62-11.5) | 10.2 (7.36-13.6) | 11.3 (7.92-15.3) |
| 20-day | 4.05 (3.52-4.64) | 4.64 (4.03-5.32) | 5.65 (4.89-6.49) | 6.51 (5.60-7.52) | 7.75 (6.46-9.29) | 8.75 (7.12-10.6) | 9.78 (7.68-12.2) | 10.9 (8.17-13.9) | 12.3 (8.92-16.3) | 13.5 (9.49-18.0) |
| 30-day | 4.88 (4.26-5.57) | 5.60 (4.88-6.40) | 6.79 (5.90-7.77) | 7.79 (6.73-8.96) | 9.18 (7.66-10.9) | 10.3 (8.37-12.4) | 11.4 (8.94-14.1) | 12.5 (9.42-15.9) | 14.0 (10.2-18.3) | 15.2 (10.7-20.2) |
| 45-day | 5.93 (5.19-6.73) | 6.81 (5.95-7.74) | 8.23 (7.17-9.38) | 9.39 (8.13-10.7) | 11.0 (9.14-12.9) | 12.1 (9.91-14.5) | 13.3 (10.5-16.3) | 14.5 (10.9-18.3) | 16.0 (11.6-20.8) | 17.1 (12.1-22.7) |
| 60-day | 6.81 (5.98-7.71) | 7.82 (6.86-8.86) | 9.43 (8.24-10.7) | 10.7 (9.31-12.2) | 12.4 (10.4-14.5) | 13.7 (11.2-16.3) | 14.9 (11.8-18.2) | 16.1 (12.2-20.2) | 17.6 (12.8-22.7) | 18.6 (13.3-24.7) |

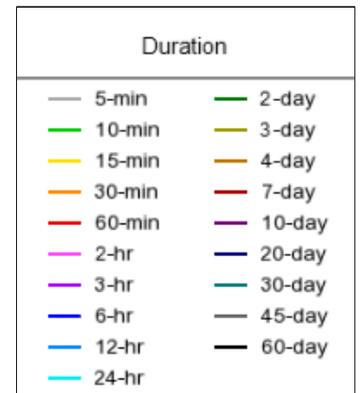
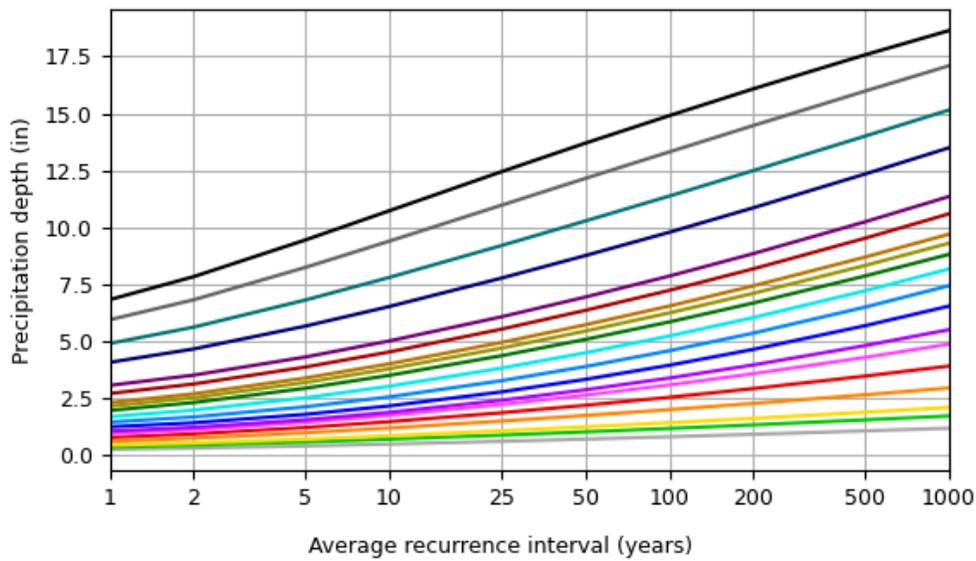
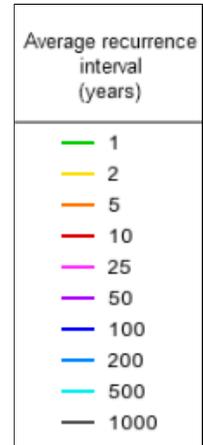
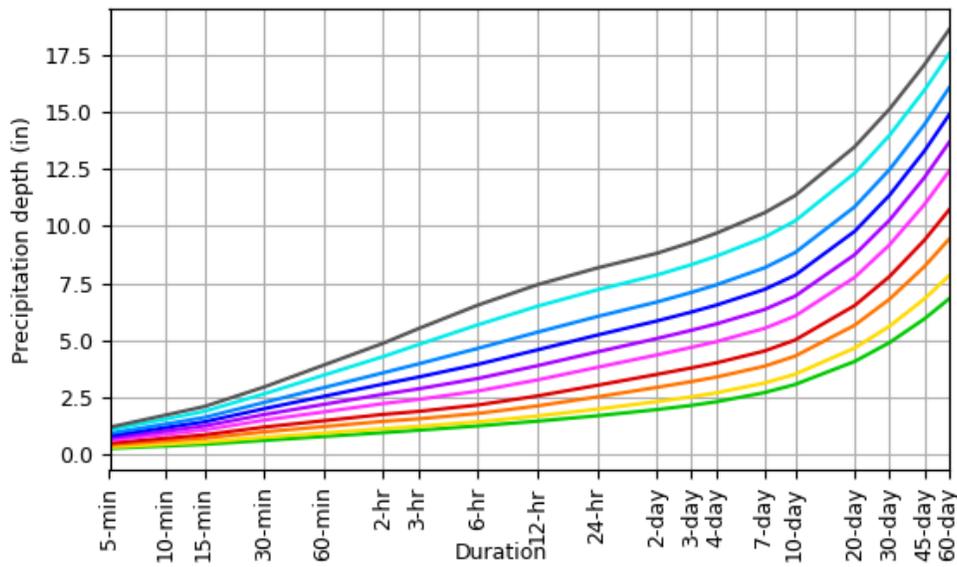
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves

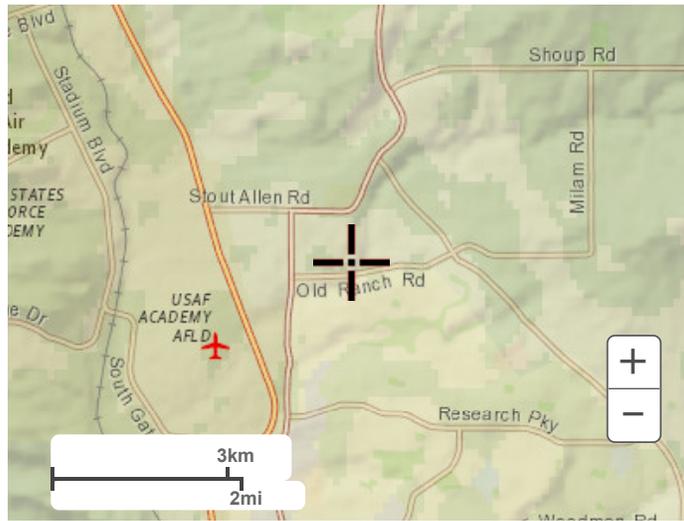
Latitude: 38.9824°, Longitude: -104.7856°



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Maps & aerials

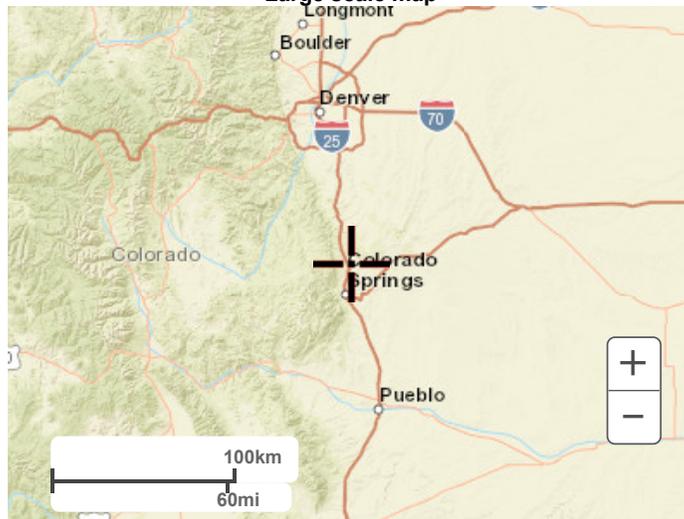
Small scale terrain



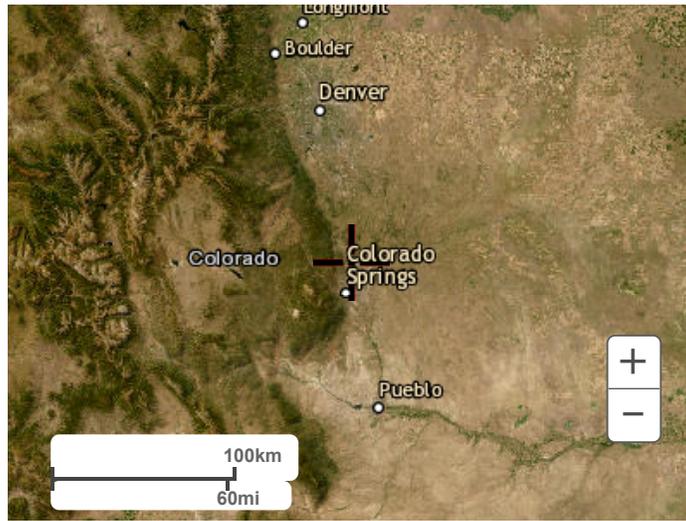
Large scale terrain



Large scale map



Large scale aerial



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Silver Spring, MD 20910
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APPENDIX B – HYDROLOGIC CALCULATIONS

Subdivision: Cottages at Kettle Creek
Location: Colorado Springs
Project Name: Cottages at Kettle Creek
Project Number: 24026
Calculated By: NQJ
Checked By:
Date: 9/30/2024

| EX DRAINAGE CALCS - BASIN SUMMARY TABLE | | | | | | | |
|---|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| Tributary Sub-basin | Area (acres) | Percent Impervious | C ₅ | C ₁₀₀ | t _c (min) | Q ₅ (cfs) | Q ₁₀₀ (cfs) |
| EX1 | 15.11 | 7% | 0.09 | 0.36 | 40.5 | 3.7 | 19.6 |
| EX2 | 6.56 | 6% | 0.09 | 0.36 | 34.3 | 1.8 | 9.6 |
| EX3 | 10.41 | 2% | 0.09 | 0.36 | 32.3 | 2.2 | 14.9 |

| DESIGN POINT SUMMARY TABLE | | |
|----------------------------|-------------------|---------------------|
| DP# | Q _{5-YR} | Q _{100-YR} |
| 1 | 3.7 | 19.6 |
| 2 | 1.8 | 9.6 |
| 3 | 3.9 | 23.9 |

COMPOSITE % IMPERVIOUS CALCULATIONS - EXISTING CONDITIONS

Subdivision: Cottages at Kettle Creek
 Location: Colorado Springs

Project Name: Cottages at Kettle Creek
 Project No.: 24026.00
 Calculated By: NQJ
 Checked By: _____
 Date: 9/30/24

| Basin ID | Total Area (ac) | Gravel Drives | | | | Paved | | | | Roofs | | | | Historic/Agriculture | | | | Weighted C ₅ & C ₁₀₀ | | Basins Total Weighted % Imp. |
|--------------|-----------------|----------------|------------------|-----------|--------|----------------|------------------|-----------|--------|----------------|------------------|-----------|--------|----------------------|------------------|-----------|--------|--|------------------|------------------------------|
| | | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | |
| | | | | | | | | | | | | | | | | | | | | |
| EX1 | 15.11 | 0.59 | 0.70 | 0.83 | 80.0% | 0.90 | 0.96 | 0.00 | 100.0% | 0.73 | 0.81 | 0.06 | 90.0% | 0.09 | 0.36 | 14.22 | 2.0% | 0.12 | 0.38 | 6.6% |
| EX2 | 6.56 | 0.59 | 0.70 | 0.22 | 80.0% | 0.90 | 0.96 | 0.05 | 100.0% | 0.73 | 0.81 | 0.08 | 90.0% | 0.09 | 0.36 | 6.21 | 2.0% | 0.12 | 0.38 | 6.4% |
| EX3 | 10.41 | 0.59 | 0.70 | 0.00 | 80.0% | 0.90 | 0.96 | 0.00 | 100.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 10.41 | 2.0% | 0.09 | 0.36 | 2.0% |
| Total | 32.08 | | | | | | | | | | | | | | | | | | | 3.8% |

STANDARD FORM SF-2 - EXISTING CONDITIONS TIME OF CONCENTRATION

Subdivision: Cottages at Kettle Creek
 Location: El Paso County

Project Name: Cottages at Kettle Creek
 Project No.: 24019.00
 Calculated By: NQJ
 Checked By: _____
 Date: 9/30/24

| SUB-BASIN DATA | | | | | INITIAL/OVERLAND (T _i) | | | TRAVEL TIME (T _t) | | | | | t _c CHECK (URBANIZED BASINS) | | | FINAL |
|----------------|-----------|------------------------|-------------------------|----------------|------------------------------------|--------------------|----------------------|-------------------------------|--------------------|-----|-------------|----------------------|---|-------------------|--------------------------------|----------------------|
| BASIN ID | D.A. (ac) | Hydrologic Soils Group | Weighted C _s | Impervious (%) | L (ft) | S _o (%) | t _i (min) | L _t (ft) | S _t (%) | K | VEL. (ft/s) | t _t (min) | COMP. t _c (min) | TOTAL LENGTH (ft) | Urbanized t _c (min) | t _c (min) |
| EX1 | 15.11 | B | 0.12 | 6.6% | 300 | 2.7% | 22.1 | 1280 | 1.9% | 7.0 | 1.0 | 22.1 | 44.2 | 1580.0 | 40.5 | 40.5 |
| EX2 | 6.56 | B | 0.12 | 6.4% | 300 | 1.8% | 25.2 | 920 | 2.7% | 7.0 | 1.2 | 13.3 | 38.6 | 1220.0 | 34.3 | 34.3 |
| EX3 | 10.41 | B | 0.09 | 2.0% | 300 | 1.6% | 27.0 | 1006 | 7.3% | 7.0 | 1.9 | 8.9 | 35.9 | 1306.0 | 32.3 | 32.3 |
| | | | | | | | | | | | | | | | | |

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)

L_t = waterway length (ft)

S_o = waterway slope (ft/ft)

V_t = travel time velocity (ft/sec) = K√S_o

K = NRCS conveyance factor (see Table 6-2).

Eq
$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$$

Where:

t_i = overland (initial) flow time (minutes)

C_s = runoff coefficient for 5-year frequency (from Table 6-4)

L_i = length of overland flow (ft)

S_o = average slope along the overland flow path (ft/ft).

Equation 6-4
$$t_t = \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

∴

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S_t = slope of the channelized flow path (ft/ft).

Equation 6-3

Equation 6-5

Table 6-2. NRCS Conveyance factors, K

| Type of Land Surface | Conveyance Factor, K |
|--------------------------------------|----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3 - EXISTING CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Cottages at Kettle Creek
 Location: Colorado Springs
 Design Storm: 5-Year

Project Name: Cottages at Kettle Creek
 Project No.: 24026.00
 Calculated By: NQJ
 Checked By:
 Date: 9/30/24

| STREET | Design Point | DIRECT RUNOFF | | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | TRAVEL TIME | | | REMARKS | |
|--------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|---------|--|
| | | Basin ID | Area (Ac) | Runoff Coeff. | t _c (min) | C*A (Ac) | I (in/hr) | Q (cfs) | t _c (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q _{street} (cfs) | C*A (ac) | Slope (%) | Q _{pipe} (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | | t _t (min) |
| | 1 | EX1 | 15.11 | 0.12 | 40.5 | 1.81 | 2.03 | 3.7 | | | | | | | | | | | | | | | BASIN EX1 HISTORIC FLOW @ DP1, DRAINS WEST ALONG OLD RANCH ROAD |
| | 2 | EX2 | 6.56 | 0.12 | 34.3 | 0.79 | 2.28 | 1.8 | | | | | | | | | | | | | | | BASIN EX2 HISTORIC FLOW @ DP2, DRAINS EAST ALONG OLD RANCH ROAD TO DP3 |
| | 3 | EX3 | 10.41 | 0.09 | 32.3 | 0.94 | 2.37 | 2.2 | 34.3 | 1.73 | 2.28 | 3.9 | | | | | | | | | | | BASIN EX3 HISTORIC FLOW & DP2 FLOW @ DP3, FLOWS SOUTH UNDER OLD RANCH ROAD IN EX CULVERT |

Notes:
 Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - EXISTING CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Cottages at Kettle Creek
Location: Colorado Springs
Design Storm: 100-Year

Project Name: Cottages at Kettle Creek
Project No.: 24026.00
Calculated By: NQJ
Checked By:
Date: 9/30/24

| STREET | Design Point | DIRECT RUNOFF | | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | TRAVEL TIME | | | REMARKS | |
|--------|--------------|---------------|-----------|---------------|-------------|----------|-----------|---------|--------------|----------|-----------|---------|--------------------|----------|-----------|------------------|----------|-----------|--------------------|-------------|----------------|---------|--|
| | | Basin ID | Area (ac) | Runoff Coeff. | t_c (min) | C*A (ac) | I (in/hr) | Q (cfs) | t_c (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q_{street} (cfs) | C*A (ac) | Slope (%) | Q_{pipe} (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | | t_t (min) |
| | 1 | EX1 | 15.11 | 0.38 | 40.5 | 5.75 | 3.41 | 19.6 | | | | | | | | | | | | | | | BASIN EX1 HISTORIC FLOW @ DP1, DRAINS WEST ALONG OLD RANCH ROAD |
| | 2 | EX2 | 6.56 | 0.38 | 34.3 | 2.50 | 3.82 | 9.6 | | | | | | | | | | | | | | | BASIN EX2 HISTORIC FLOW @ DP2, DRAINS EAST ALONG OLD RANCH ROAD TO DP3 |
| | 3 | EX3 | 10.41 | 0.36 | 32.3 | 3.75 | 3.97 | 14.9 | 34.3 | 6.25 | 3.82 | 23.9 | | | | | | | | | | | BASIN EX3 HISTORIC FLOW & DP2 FLOW @ DP3, FLOWS SOUTH UNDER OLD RANCH ROAD IN EX CULVERT |
| | | | | | | | | | | | | | | | | | | | | | | | |

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

Subdivision: Cottages at Kettle Creek
Location: Colorado Springs
Project Name: Cottages at Kettle Creek
Project Number: 24026
Calculated By: NQJ
Checked By:
Date: 9/24/2024

| PROPOSED CALCS - BASIN SUMMARY TABLE | | | | | | | |
|--------------------------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| Tributary Sub-basin | Area (acres) | Percent Impervious | C ₅ | C ₁₀₀ | t _c (min) | Q ₅ (cfs) | Q ₁₀₀ (cfs) |
| A | 1.98 | 62% | 0.57 | 0.71 | 17.9 | 4.7 | 9.8 |
| B | 2.26 | 64% | 0.58 | 0.72 | 18.1 | 5.4 | 11.2 |
| C | 0.53 | 65% | 0.60 | 0.73 | 15.9 | 1.4 | 2.9 |
| D | 1.57 | 76% | 0.69 | 0.80 | 15.4 | 4.8 | 9.3 |
| E | 0.50 | 12% | 0.17 | 0.42 | 25.9 | 0.4 | 1.8 |
| F | 0.22 | 47% | 0.46 | 0.63 | 19.7 | 0.5 | 1.2 |
| G | 0.96 | 17% | 0.22 | 0.45 | 27.8 | 0.7 | 2.5 |
| OS1 | 1.97 | 14% | 0.17 | 0.41 | 35.4 | 1.1 | 4.5 |
| OS2 | 12.06 | 5% | 0.11 | 0.38 | 40.9 | 2.7 | 15.3 |
| OS3 | 10.37 | 2% | 0.09 | 0.36 | 17.9 | 2.2 | 14.8 |

| DESIGN POINT SUMMARY TABLE | | |
|----------------------------|-------------------|---------------------|
| DP# | Q _{5-YR} | Q _{100-YR} |
| 1 | 4.7 | 9.8 |
| 2 | 5.4 | 11.2 |
| 3 | 4.8 | 9.4 |
| 3.1 | 9.6 | 18.4 |
| 4 | 1.4 | 3.5 |
| 4.1 | 10.8 | 20.7 |
| 5 | 11.1 | 22.0 |
| 6 | 0.5 | 1.7 |
| 7 | 1.1 | 4.1 |
| 8 | 1.1 | 4.5 |
| 9 | 2.7 | 15.3 |
| 10 | 2.2 | 14.8 |

COMPOSITE % IMPERVIOUS CALCULATIONS - PROPOSED CONDITIONS

Subdivision: Cottages at Kettle Creek
 Location: Colorado Springs

Project Name: Cottages at Kettle Creek
 Project No.: 24026.00
 Calculated By: NQJ
 Checked By:
 Date: 9/24/24

| Basin ID | Total Area (ac) | Paved | | | | Gravel | | | | Roofs | | | | Landscaping/Undeveloped | | | | Weighted C ₅ & C ₁₀₀ | | Basins Total Weighted % Imp. |
|-------------------|-----------------|----------------|------------------|-----------|--------|----------------|------------------|-----------|--------|----------------|------------------|-----------|--------|-------------------------|------------------|-----------|--------|--|------------------|------------------------------|
| | | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | Area (ac) | % Imp. | C ₅ | C ₁₀₀ | |
| | | | | | | | | | | | | | | | | | | | | |
| A | 1.98 | 0.90 | 0.96 | 0.82 | 100.0% | 0.59 | 0.70 | 0.06 | 80.0% | 0.73 | 0.81 | 0.39 | 90.0% | 0.09 | 0.36 | 0.71 | 2.0% | 0.57 | 0.71 | 62.3% |
| B | 2.26 | 0.90 | 0.96 | 0.97 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.52 | 90.0% | 0.09 | 0.36 | 0.77 | 2.0% | 0.58 | 0.72 | 64.3% |
| C | 0.53 | 0.90 | 0.96 | 0.27 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.08 | 90.0% | 0.09 | 0.36 | 0.18 | 2.0% | 0.60 | 0.73 | 65.2% |
| D | 1.57 | 0.90 | 0.96 | 0.93 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.29 | 90.0% | 0.09 | 0.36 | 0.35 | 2.0% | 0.69 | 0.80 | 76.3% |
| E | 0.50 | 0.90 | 0.96 | 0.05 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 0.45 | 2.0% | 0.17 | 0.42 | 11.8% |
| F | 0.22 | 0.90 | 0.96 | 0.10 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 0.12 | 2.0% | 0.46 | 0.63 | 46.5% |
| G | 0.96 | 0.90 | 0.96 | 0.15 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 0.81 | 2.0% | 0.22 | 0.45 | 17.3% |
| OS1 | 1.97 | 0.90 | 0.96 | 0.00 | 100.0% | 0.59 | 0.70 | 0.30 | 80.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 1.67 | 2.0% | 0.17 | 0.41 | 13.9% |
| OS2 | 12.06 | 0.90 | 0.96 | 0.00 | 100.0% | 0.59 | 0.70 | 0.46 | 80.0% | 0.73 | 0.81 | 0.06 | 90.0% | 0.09 | 0.36 | 11.54 | 2.0% | 0.11 | 0.38 | 5.4% |
| OS3 | 10.37 | 0.90 | 0.96 | 0.00 | 100.0% | 0.59 | 0.70 | 0.00 | 80.0% | 0.73 | 0.81 | 0.00 | 90.0% | 0.09 | 0.36 | 10.37 | 2.0% | 0.09 | 0.36 | 2.0% |
| Total | 32.42 | | | | | | | | | | | | | | | | | | | 17.6% |
| Pond (A-E) | 6.84 | | | | | | | | | | | | | | | | | | | 62.7% |

STANDARD FORM SF-2 - PROPOSED CONDITIONS TIME OF CONCENTRATION

Subdivision: Cottages at Kettle Creek
 Location: El Paso County

Project Name: Cottages at Kettle Creek
 Project No.: 24019.00
 Calculated By: NQJ
 Checked By: _____
 Date: 9/24/24

| SUB-BASIN DATA | | | | | INITIAL/OVERLAND (T _i) | | | TRAVEL TIME (T _t) | | | | | t _c CHECK (URBANIZED BASINS) | | | FINAL |
|----------------|-----------|------------------------|-------------------------|----------------|------------------------------------|--------------------|----------------------|-------------------------------|--------------------|------|-------------|----------------------|---|-------------------|--------------------------------|----------------------|
| BASIN ID | D.A. (ac) | Hydrologic Soils Group | Weighted C _s | Impervious (%) | L (ft) | S _o (%) | t _i (min) | L _t (ft) | S _t (%) | K | VEL. (ft/s) | t _t (min) | COMP. t _c (min) | TOTAL LENGTH (ft) | Urbanized t _c (min) | t _c (min) |
| A | 1.98 | A | 0.57 | 62.3% | 100 | 2.0% | 7.7 | 340 | 1.7% | 20.0 | 2.6 | 2.2 | 9.8 | 440.0 | 17.9 | 9.8 |
| B | 2.26 | A | 0.58 | 64.3% | 100 | 2.0% | 7.4 | 420 | 1.6% | 20.0 | 2.5 | 2.8 | 10.2 | 520.0 | 18.1 | 10.2 |
| C | 0.53 | A | 0.60 | 65.2% | 100 | 2.0% | 7.2 | 270 | 6.0% | 20.0 | 4.9 | 0.9 | 8.1 | 370.0 | 15.9 | 8.1 |
| D | 1.57 | A | 0.69 | 76.3% | 100 | 2.0% | 5.9 | 400 | 2.0% | 20.0 | 2.8 | 2.4 | 8.3 | 500.0 | 15.4 | 8.3 |
| E | 0.50 | A | 0.17 | 11.8% | 65 | 33.0% | 4.3 | 123 | 1.0% | 20.0 | 2.0 | 1.0 | 5.3 | 188.0 | 25.9 | 5.3 |
| F | 0.22 | A | 0.46 | 46.5% | 24 | 2.0% | 4.5 | 310 | 4.4% | 20.0 | 4.2 | 1.2 | 5.7 | 334.0 | 19.7 | 5.7 |
| G | 0.96 | A | 0.22 | 17.3% | 140 | 2.8% | 13.4 | 630 | 3.8% | 20.0 | 3.9 | 2.7 | 16.1 | 770.0 | 27.8 | 16.1 |
| OS1 | 1.97 | A | 0.17 | 13.9% | 10 | 2.0% | 4.2 | 980 | 1.6% | 10.0 | 1.3 | 12.9 | 17.2 | 990.0 | 35.4 | 17.2 |
| OS2 | 12.06 | A | 0.11 | 5.4% | 300 | 2.7% | 22.3 | 1280 | 1.9% | 7.0 | 1.0 | 22.1 | 44.4 | 1580.0 | 40.9 | 40.9 |
| OS3 | 10.37 | A | 0.09 | 2.0% | 300 | 1.6% | 27.0 | 1006 | 7.3% | 7.0 | 1.9 | 8.9 | 35.9 | 1306.0 | 32.3 | 32.3 |

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)

L_t = waterway length (ft)

S_o = waterway slope (ft/ft)

V_t = travel time velocity (ft/sec) = K√S_o

K = NRCS conveyance factor (see Table 6-2).

Eq
$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$$

Where:

t_i = overland (initial) flow time (minutes)

C_s = runoff coefficient for 5-year frequency (from Table 6-4)

L_i = length of overland flow (ft)

S_o = average slope along the overland flow path (ft/ft).

Equation 6-4
$$t_c = 1.48L^{0.76}S_o^{-0.38} + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

∴

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S_t = slope of the channelized flow path (ft/ft).

Equation 6-3

Equation 6-5

Table 6-2. NRCS Conveyance factors, K

| Type of Land Surface | Conveyance Factor, K |
|--------------------------------------|----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3 - PROPOSED CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Cottages at Kettle Creek
Location: Colorado Springs
Design Storm: 5-Year

Project Name: Cottages at Kettle Creek
Project No.: 24026.00
Calculated By: NQJ
Checked By:
Date: 9/24/24

| STREET | Design Point | DIRECT RUNOFF | | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | | TRAVEL TIME | | | REMARKS |
|--------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|--|---------|
| | | Basin ID | Area (Ac) | Runoff Coeff. | t _c (min) | C*A (Ac) | I (in/hr) | Q (cfs) | t _c (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q _{street} (cfs) | C*A (ac) | Slope (%) | Q _{pipe} (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t _t (min) | |
| | 1 | A | 1.98 | 0.57 | 9.8 | 1.12 | 4.15 | 4.7 | | | | | | | 4.7 | 1.12 | 2.0 | 18 | 196 | 7.4 | 0.4 | BASIN A FLOW @ DP1, CAPTURED IN 15' TYPE R, PIPE TO DP4.1 | |
| | 2 | B | 2.26 | 0.58 | 10.2 | 1.32 | 4.10 | 5.4 | | | | | | | 5.4 | 1.32 | 2.0 | 18 | 360 | 7.7 | 0.8 | BASIN B FLOW @ DP2, CAPTURED IN 15' TYPE R, PIPE TO DP4.1 | |
| | | C | 0.53 | 0.60 | 8.1 | 0.32 | 4.44 | 1.4 | | | | | | | | | | | | | | BASIN C FLOW @ DP4 | |
| | 3 | D | 1.57 | 0.69 | 8.3 | 1.08 | 4.41 | 4.8 | | | | | | | 4.8 | 1.08 | 2.0 | 18 | 360 | 7.4 | 0.8 | BASIN D FLOW @ DP3, CAPTURED IN 15' TYPE R INLET, PIPE TO DP4.1 | |
| | 3.1 | | | | | | | | 10.9 | 2.40 | 3.99 | 9.6 | | | 9.6 | 2.40 | 2.0 | 18 | 45 | 8.9 | 0.1 | COMBINED DP2 & DP3 FLOW @ DP3.1, PIPE TO DP4.1 | |
| | 4 | | | | | | | | 8.1 | 0.32 | 4.44 | 1.4 | | | 1.4 | 0.32 | 2.0 | 18 | 360 | 5.1 | 1.2 | BASIN C FLOW @ DP4, CAPTURED IN 10' TYPE R, PIPE TO DP4.1 | |
| | 4.1 | | | | | | | | 11.0 | 2.72 | 3.98 | 10.8 | | | 10.8 | 2.72 | 2.0 | 24 | 50 | 9.1 | 0.1 | COMBINED DP1-DP4 FLOW, PIPE TO DP5 | |
| | 5 | E | 0.50 | 0.17 | 5.3 | 0.09 | 5.08 | 0.4 | 11.1 | 2.81 | 3.97 | 11.1 | | | | | | | | | | COMBINED DP4.1 & BASIN E FLOW, TOTAL FLOW ENTERING WQ POND | |
| | 6 | F | 0.22 | 0.46 | 5.7 | 0.10 | 4.96 | 0.5 | 5.7 | 0.10 | 4.96 | 0.5 | | | | | | | | | | COMBINED DP3 FLOWBY & BASIN F FLOW, TOTAL FLOW LEAVING SITE UNDETAINED | |
| | 7 | G | 0.96 | 0.22 | 16.1 | 0.21 | 3.41 | 0.7 | 16.1 | 0.31 | 3.41 | 1.1 | | | | | | | | | | COMBINED DP6 & BASIN G FLOW @ DP7 | |
| | 8 | OS1 | 1.97 | 0.17 | 17.2 | 0.33 | 3.32 | 1.1 | | | | | | | | | | | | | | BASIN OS1 FLOW @ DP7, FOLLOW HISTORIC DRAINAGE PATTERNS WEST ALONG OLD RANCH ROAD | |
| | 9 | OS2 | 12.06 | 0.11 | 40.9 | 1.35 | 2.01 | 2.7 | | | | | | | | | | | | | | BASIN OS2 FLOW @ DP8, FOLLOWS HISTORIC DRAINAGE PATTERNS SOUTH ACROSS OLD RANCH ROAD | |
| | 10 | OS3 | 10.37 | 0.09 | 32.3 | 0.93 | 2.37 | 2.2 | | | | | | | | | | | | | | BASIN OS3 FLOW @ DP9, FOLLOWS HISTORIC DRAINAGE PATTERNS UNDER OLD RANCH ROAD | |

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - PROPOSED CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Cottages at Kettle Creek
Location: Colorado Springs
Design Storm: 100-Year

Project Name: Cottages at Kettle Creek
Project No.: 24026.00
Calculated By: NJJ
Checked By:
Date: 9/24/24

| STREET | Design Point | DIRECT RUNOFF | | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | TRAVEL TIME | | | REMARKS | |
|--------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|---------|--|
| | | Basin ID | Area (ac) | Runoff Coeff. | t _c (min) | C*A (ac) | I (in/hr) | Q (cfs) | t _c (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q _{street} (cfs) | C*A (ac) | Slope (%) | Q _{pipe} (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | | t _t (min) |
| | 1 | A | 1.98 | 0.71 | 9.8 | 1.40 | 6.97 | 9.8 | | | | | 1.1 | 0.15 | 4.80 | | | | | 280 | 2.2 | 2.1 | DP1 BYPASS, C&G FLOW TO DP4 |
| | | | | | | | | | | | | | | | | | | | | 196 | 8.7 | 0.4 | BASIN A FLOW @ DP1, CAPTURED IN 15' TYPE R, PIPE TO DP4.1 |
| | 2 | B | 2.26 | 0.72 | 10.2 | 1.63 | 6.89 | 11.2 | | | | | 1.7 | 0.25 | 4.00 | | | | | 360 | 2.0 | 3.0 | DP2 BYPASS, C&G FLOW TO DP3 |
| | | | | | | | | | | | | | | | | | | | | 360 | 8.8 | 0.7 | BASIN B FLOW @ DP2, CAPTURED IN 15' TYPE R, PIPE TO DP4.1 |
| | | C | 0.53 | 0.73 | 8.1 | 0.39 | 7.46 | 2.9 | | | | | | | | | | | | | | | BASIN C FLOW @ DP4 |
| | 3 | D | 1.57 | 0.80 | 8.3 | 1.25 | 7.41 | 9.3 | 13.2 | 1.50 | 6.24 | 9.4 | 0.9 | 0.14 | 4.00 | | | | | 60 | 2.0 | 0.5 | DP3 BYPASS FLOW, C&G FLOW TO DP6 |
| | | | | | | | | | | | | | | | | | | | | 360 | 8.6 | 0.7 | |
| | 3.1 | | | | | | | | 10.8 | 2.74 | 6.73 | 18.4 | | | | 18.4 | 2.74 | 2.0 | 18 | 45 | 10.4 | 0.1 | COMBINED DP2 & DP3 FLOW @ DP3.1, PIPE TO DP4.1 |
| | 4 | | | | | | | | 12.0 | 0.54 | 6.48 | 3.5 | | | | 3.5 | 0.54 | 2.0 | 18 | 360 | 6.8 | 0.9 | BASIN C & DP1 BYPASS FLOW @ DP4, CAPTURED IN 10' TYPE R INLET, PIPE TO DP4.1 |
| | 4.1 | | | | | | | | 12.8 | 3.28 | 6.30 | 20.7 | | | | 20.7 | 3.28 | 2.0 | 24 | 50 | 10.8 | 0.1 | COMBINED DP1-DP4 FLOW, PIPE TO DP5 |
| | 5 | E | 0.50 | 0.42 | 5.3 | 0.21 | 8.54 | 1.8 | 12.9 | 3.49 | 6.29 | 22.0 | | | | | | | | | | | COMBINED DP4.1 & BASIN E FLOW, TOTAL FLOW ENTERING WQ POND |
| | 6 | F | 0.22 | 0.63 | 5.7 | 0.14 | 8.33 | 1.2 | 13.7 | 0.28 | 6.15 | 1.7 | | | | | | | | | | | COMBINED DP3 FLOWBY & BASIN F FLOW, TOTAL FLOW LEAVING SITE UNDETAINED |
| | 7 | G | 0.96 | 0.45 | 16.1 | 0.44 | 5.73 | 2.5 | 16.1 | 0.72 | 5.73 | 4.1 | | | | | | | | | | | COMBINED DP6 & BASIN G FLOW @ DP7 |
| | 8 | OS1 | 1.97 | 0.41 | 17.2 | 0.81 | 5.57 | 4.5 | | | | | | | | | | | | | | | BASIN OS1 FLOW @ DP7, FOLLOW HISTORIC DRAINAGE PATTERNS WEST ALONG OLD RANCH ROAD |
| | 9 | OS2 | 12.06 | 0.38 | 40.9 | 4.53 | 3.38 | 15.3 | | | | | | | | | | | | | | | BASIN OS2 FLOW @ DP8, FOLLOWS HISTORIC DRAINAGE PATTERNS SOUTH ACROSS OLD RANCH ROAD |
| | 10 | OS3 | 10.37 | 0.36 | 32.3 | 3.73 | 3.97 | 14.8 | | | | | | | | | | | | | | | BASIN OS3 FLOW @ DP9, FOLLOWS HISTORIC DRAINAGE PATTERNS UNDER OLD RANCH ROAD |

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

Design Procedure Form: Runoff Reduction

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

Designer: NQJ
Company: ALL TERRAIN ENGINEERING
Date: October 4, 2024
Project: COTTAGES AT KETTLE CREEK
Location: COLORADO SPRINGS

SITE INFORMATION (User Input in Blue Cells)

WQCV Rainfall Depth 0.60 inches
 Depth of Average Runoff Producing Storm, d_e = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)

| Area Type | UIA:RPA | DCIA | SPA | UIA:RPA | DCIA | | | | | | | | |
|------------------------------|-----------|--------|--------|-----------|--------|--|--|--|--|--|--|--|--|
| Area ID | A:UIA-RPA | A:DCIA | A:SPA | B:UIA-RPA | B:DCIA | | | | | | | | |
| Downstream Design Point ID | 1 | 1 | 1 | 1 | 1 | | | | | | | | |
| Downstream BMP Type | EDB | EDB | EDB | EDB | EDB | | | | | | | | |
| DCIA (ft ²) | -- | 37,836 | -- | -- | 56,702 | | | | | | | | |
| UIA (ft ²) | 9,025 | -- | -- | 4,535 | -- | | | | | | | | |
| RPA (ft ²) | 9,300 | -- | -- | 6,783 | -- | | | | | | | | |
| SPA (ft ²) | -- | -- | 25,942 | -- | -- | | | | | | | | |
| HSG A (%) | 100% | -- | 100% | 100% | -- | | | | | | | | |
| HSG B (%) | 0% | -- | 0% | 0% | -- | | | | | | | | |
| HSG C/D (%) | 0% | -- | 0% | 0% | -- | | | | | | | | |
| Average Slope of RPA (ft/ft) | 0.020 | -- | -- | 0.020 | -- | | | | | | | | |
| UIA:RPA Interface Width (ft) | 35.00 | -- | -- | 35.00 | -- | | | | | | | | |

CALCULATED RUNOFF RESULTS

| Area ID | A:UIA-RPA | A:DCIA | A:SPA | B:UIA-RPA | B:DCIA | | | | | | | | |
|-------------------------------------|-----------|--------|-------|-----------|--------|--|--|--|--|--|--|--|--|
| UIA:RPA Area (ft ²) | 18,325 | -- | -- | 11,318 | -- | | | | | | | | |
| L / W Ratio | 14.96 | -- | -- | 9.24 | -- | | | | | | | | |
| UIA / Area | 0.4925 | -- | -- | 0.4007 | -- | | | | | | | | |
| Runoff (in) | 0.00 | 0.50 | 0.00 | 0.00 | 0.50 | | | | | | | | |
| Runoff (ft ³) | 0 | 1577 | 0 | 0 | 2363 | | | | | | | | |
| Runoff Reduction (ft ³) | 376 | 0 | 1297 | 189 | 0 | | | | | | | | |

CALCULATED WQCV RESULTS

| Area ID | A:UIA-RPA | A:DCIA | A:SPA | B:UIA-RPA | B:DCIA | | | | | | | | |
|-----------------------------------|-----------|--------|-------|-----------|--------|--|--|--|--|--|--|--|--|
| WQCV (ft ³) | 376 | 1577 | 0 | 189 | 2363 | | | | | | | | |
| WQCV Reduction (ft ³) | 376 | 0 | 0 | 189 | 0 | | | | | | | | |
| WQCV Reduction (%) | 100% | 0% | 0% | 100% | 0% | | | | | | | | |
| Untreated WQCV (ft ³) | 0 | 1577 | 0 | 0 | 2363 | | | | | | | | |

CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID)

| Downstream Design Point ID | 1 | 1 | 1 | 1 | 1 | | | | | | | | |
|--|---------|---------|---------|---------|---------|--|--|--|--|--|--|--|--|
| DCIA (ft ²) | 94,538 | 94,538 | 94,538 | 94,538 | 94,538 | | | | | | | | |
| UIA (ft ²) | 13,560 | 13,560 | 13,560 | 13,560 | 13,560 | | | | | | | | |
| RPA (ft ²) | 16,083 | 16,083 | 16,083 | 16,083 | 16,083 | | | | | | | | |
| SPA (ft ²) | 25,942 | 25,942 | 25,942 | 25,942 | 25,942 | | | | | | | | |
| Total Area (ft ²) | 150,123 | 150,123 | 150,123 | 150,123 | 150,123 | | | | | | | | |
| Total Impervious Area (ft ²) | 108,098 | 108,098 | 108,098 | 108,098 | 108,098 | | | | | | | | |
| WQCV (ft ³) | 4,504 | 4,504 | 4,504 | 4,504 | 4,504 | | | | | | | | |
| WQCV Reduction (ft ³) | 565 | 565 | 565 | 565 | 565 | | | | | | | | |
| WQCV Reduction (%) | 13% | 13% | 13% | 13% | 13% | | | | | | | | |
| Untreated WQCV (ft ³) | 3,939 | 3,939 | 3,939 | 3,939 | 3,939 | | | | | | | | |

CALCULATED SITE RESULTS (sums results from all columns in worksheet)

| | |
|--|---------|
| Total Area (ft ²) | 750,615 |
| Total Impervious Area (ft ²) | 540,490 |
| WQCV (ft ³) | 4,504 |
| WQCV Reduction (ft ³) | 565 |
| WQCV Reduction (%) | 13% |
| Untreated WQCV (ft ³) | 3,939 |



APPENDIX C – HYDRAULIC CALCULATIONS

INLET MANAGEMENT

Worksheet Protected

| INLET NAME | DP1 | DP2 | DP3 | DP4 |
|------------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Site Type (Urban or Rural) | URBAN | URBAN | URBAN | URBAN |
| Inlet Application (Street or Area) | STREET | STREET | STREET | STREET |
| Hydraulic Condition | On Grade | On Grade | On Grade | On Grade |
| Inlet Type | CDOT Type R Curb Opening |

USER-DEFINED INPUT

| User-Defined Design Flows | | | | |
|--|-------------------------|-------------------------|-------------------------|-------------------------|
| Minor Q_{known} (cfs) | 4.7 | 5.4 | 4.8 | 1.4 |
| Major Q_{known} (cfs) | 9.8 | 11.2 | 9.4 | 3.5 |
| Bypass (Carry-Over) Flow from Upstream <small>Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.</small> | | | | |
| Receive Bypass Flow from: | No Bypass Flow Received |
| Minor Bypass Flow Received, Q_b (cfs) | 0.0 | 0.0 | 0.0 | 0.0 |
| Major Bypass Flow Received, Q_b (cfs) | 0.0 | 0.0 | 0.0 | 0.0 |
| Watershed Characteristics | | | | |
| Subcatchment Area (acres) | | | | |
| Percent Impervious | | | | |
| NRCS Soil Type | | | | |
| Watershed Profile | | | | |
| Overland Slope (ft/ft) | | | | |
| Overland Length (ft) | | | | |
| Channel Slope (ft/ft) | | | | |
| Channel Length (ft) | | | | |
| Minor Storm Rainfall Input | | | | |
| Design Storm Return Period, T_r (years) | | | | |
| One-Hour Precipitation, P_1 (inches) | | | | |
| Major Storm Rainfall Input | | | | |
| Design Storm Return Period, T_r (years) | | | | |
| One-Hour Precipitation, P_1 (inches) | | | | |

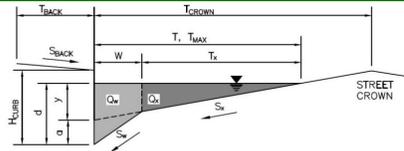
CALCULATED OUTPUT

| | | | | |
|--|------------|-------------|------------|------------|
| Minor Total Design Peak Flow, Q (cfs) | 4.7 | 5.4 | 4.8 | 1.4 |
| Major Total Design Peak Flow, Q (cfs) | 9.8 | 11.2 | 9.4 | 3.5 |
| Minor Flow Bypassed Downstream, Q_b (cfs) | 0.0 | 0.0 | 0.0 | 0.0 |
| Major Flow Bypassed Downstream, Q_b (cfs) | 1.1 | 1.7 | 0.9 | 0.0 |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: **COTTAGES AT KETTLE CREEK**
 Inlet ID: **DP1**



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)
 Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

| | | |
|-----------------------|-------|--------|
| T _{BACK} = | 0.0 | ft |
| S _{BACK} = | 0.020 | ft/ft |
| n _{BACK} = | 0.016 | |
| H _{CURB} = | 6.00 | inches |
| T _{CROWN} = | 24.0 | ft |
| W = | 1.00 | ft |
| S _X = | 0.020 | ft/ft |
| S _W = | 0.083 | ft/ft |
| S _O = | 0.048 | ft/ft |
| n _{STREET} = | 0.016 | |

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

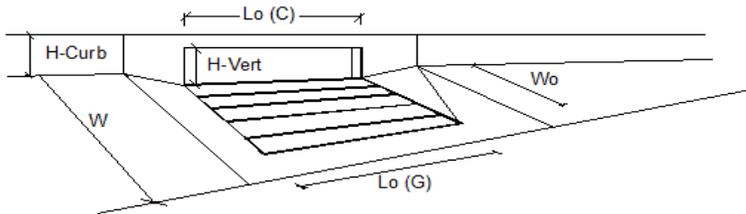
| | | | |
|--------------------|--------------------------|--------------------------|--------|
| | Minor Storm | Major Storm | |
| T _{MAX} = | 24.0 | 24.0 | ft |
| d _{MAX} = | 6.0 | 6.0 | inches |
| | <input type="checkbox"/> | <input type="checkbox"/> | |

MINOR STORM Allowable Capacity is based on Depth Criterion
 MAJOR STORM Allowable Capacity is based on Depth Criterion

| | | | |
|----------------------|-------------|-------------|-----|
| | Minor Storm | Major Storm | |
| Q _{allow} = | 21.9 | 21.9 | cfs |

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.70 cfs on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design peak flow of 9.80 cfs on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE



Design Information (Input)

Type of Inlet: CDOT Type R Curb Opening
 Local Depression (additional to continuous gutter depression 'a')
 Total Number of Units in the Inlet (Grate or Curb Opening)
 Length of a Single Unit Inlet (Grate or Curb Opening)
 Width of a Unit Grate (cannot be greater than W, Gutter Width)
 Clogging Factor for a Single Unit Grate (typical min. value = 0.5)
 Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)

| | MINOR | MAJOR | |
|----------------------|--------------------------|-------|--------|
| Type = | CDOT Type R Curb Opening | | |
| a _{LOCAL} = | 3.0 | 3.0 | inches |
| No = | 3 | 3 | |
| L _u = | 5.00 | 5.00 | ft |
| W _u = | N/A | N/A | ft |
| C _f (G) = | N/A | N/A | |
| C _f (C) = | 0.10 | 0.10 | |

Street Hydraulics: OK - Q < Allowable Street Capacity

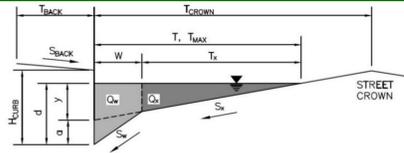
Total Inlet Interception Capacity
 Total Inlet Carry-Over Flow (flow bypassing inlet)
 Capture Percentage = Q_i/Q_s

| | MINOR | MAJOR | |
|------------------|-------|-------|-----|
| Q = | 4.7 | 8.7 | cfs |
| Q _s = | 0.0 | 1.1 | cfs |
| C% = | 100 | 89 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: **COTTAGES AT KETTLE CREEK**
 Inlet ID: **DP2**



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)
 Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

| | | |
|---------------------|-------|-------|
| T _{BACK} = | 0.0 | ft |
| S _{BACK} = | 0.020 | ft/ft |
| n _{BACK} = | 0.016 | |

| | | |
|-----------------------|-------|--------|
| H _{CURB} = | 6.00 | inches |
| T _{CROWN} = | 24.0 | ft |
| W = | 1.00 | ft |
| S _X = | 0.020 | ft/ft |
| S _W = | 0.083 | ft/ft |
| S _O = | 0.041 | ft/ft |
| n _{STREET} = | 0.016 | |

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

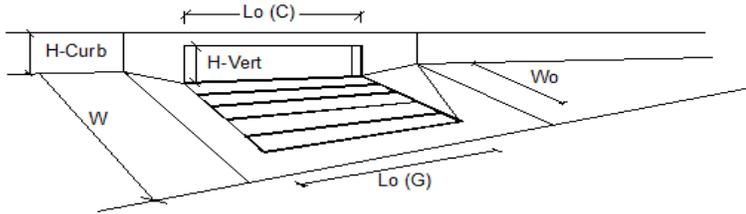
| | | | |
|--------------------|--------------------------|--------------------------|--------|
| | Minor Storm | Major Storm | |
| T _{MAX} = | 24.0 | 24.0 | ft |
| d _{MAX} = | 6.0 | 6.0 | inches |
| | <input type="checkbox"/> | <input type="checkbox"/> | |

MINOR STORM Allowable Capacity is based on Depth Criterion
 MAJOR STORM Allowable Capacity is based on Depth Criterion

| | | | |
|----------------------|-------------|-------------|-----|
| | Minor Storm | Major Storm | |
| Q _{allow} = | 22.9 | 22.9 | cfs |

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 5.40 cfs on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design peak flow of 11.20 cfs on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE



Design Information (Input)

Type of Inlet: CDOT Type R Curb Opening
 Local Depression (additional to continuous gutter depression 'a')
 Total Number of Units in the Inlet (Grate or Curb Opening)
 Length of a Single Unit Inlet (Grate or Curb Opening)
 Width of a Unit Grate (cannot be greater than W, Gutter Width)
 Clogging Factor for a Single Unit Grate (typical min. value = 0.5)
 Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)

| | MINOR | MAJOR | |
|----------------------|--------------------------|-------|--------|
| Type = | CDOT Type R Curb Opening | | |
| a _{LOCAL} = | 3.0 | 3.0 | inches |
| No = | 3 | 3 | |
| L _u = | 5.00 | 5.00 | ft |
| W _u = | N/A | N/A | ft |
| C _f (G) = | N/A | N/A | |
| C _f (C) = | 0.10 | 0.10 | |

Street Hydraulics: OK - Q < Allowable Street Capacity

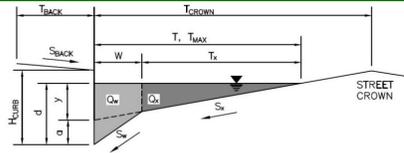
Total Inlet Interception Capacity
 Total Inlet Carry-Over Flow (flow bypassing inlet)
 Capture Percentage = Q_i/Q_s

| | MINOR | MAJOR | |
|------------------|-------|-------|-----|
| Q = | 5.4 | 9.5 | cfs |
| Q _s = | 0.0 | 1.7 | cfs |
| C% = | 100 | 84 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: **COTTAGES AT KETTLE CREEK**
 Inlet ID: **DP3**



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)
 Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

| | | |
|---------------------|-------|-------|
| T _{BACK} = | 0.0 | ft |
| S _{BACK} = | 0.020 | ft/ft |
| n _{BACK} = | 0.016 | |

| | | |
|-----------------------|-------|--------|
| H _{CURB} = | 6.00 | inches |
| T _{CROWN} = | 24.0 | ft |
| W = | 1.00 | ft |
| S _X = | 0.020 | ft/ft |
| S _W = | 0.083 | ft/ft |
| S _O = | 0.040 | ft/ft |
| n _{STREET} = | 0.016 | |

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

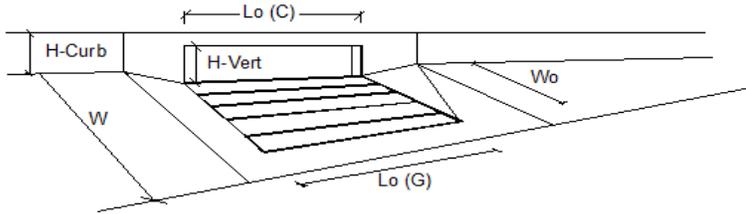
| | | | |
|--------------------|--------------------------|--------------------------|--------|
| | Minor Storm | Major Storm | |
| T _{MAX} = | 24.0 | 24.0 | ft |
| d _{MAX} = | 6.0 | 6.0 | inches |
| | <input type="checkbox"/> | <input type="checkbox"/> | |

MINOR STORM Allowable Capacity is based on Depth Criterion
 MAJOR STORM Allowable Capacity is based on Depth Criterion

| | | | |
|----------------------|-------------|-------------|-----|
| | Minor Storm | Major Storm | |
| Q _{allow} = | 23.1 | 23.1 | cfs |

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.80 cfs on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design peak flow of 9.40 cfs on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE



Design Information (Input)

Type of Inlet: CDOT Type R Curb Opening
 Local Depression (additional to continuous gutter depression 'a')
 Total Number of Units in the Inlet (Grate or Curb Opening)
 Length of a Single Unit Inlet (Grate or Curb Opening)
 Width of a Unit Grate (cannot be greater than W, Gutter Width)
 Clogging Factor for a Single Unit Grate (typical min. value = 0.5)
 Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)

| | MINOR | MAJOR | |
|----------------------|--------------------------|-------|--------|
| Type = | CDOT Type R Curb Opening | | |
| a _{LOCAL} = | 3.0 | 3.0 | inches |
| No = | 3 | 3 | |
| L _u = | 5.00 | 5.00 | ft |
| W _u = | N/A | N/A | ft |
| C _f (G) = | N/A | N/A | |
| C _f (C) = | 0.10 | 0.10 | |

Street Hydraulics: OK - Q < Allowable Street Capacity

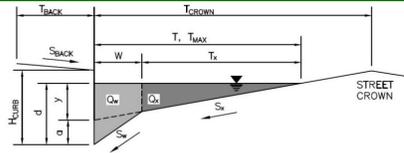
Total Inlet Interception Capacity
 Total Inlet Carry-Over Flow (flow bypassing inlet)
 Capture Percentage = Q_i/Q_s

| | MINOR | MAJOR | |
|------------------|-------|-------|-----|
| Q = | 4.8 | 8.5 | cfs |
| Q _o = | 0.0 | 0.9 | cfs |
| C% = | 100 | 90 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

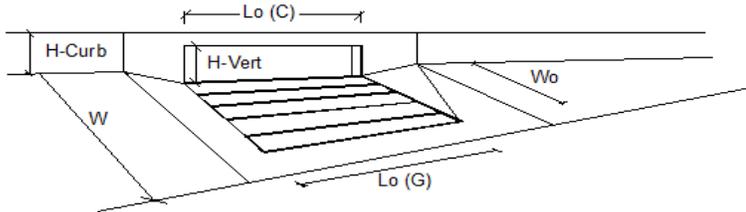
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: COTTAGES AT KETTLE CREEK
Inlet ID: DP4



| Gutter Geometry: | | | | | |
|---|--|--------------------------|--------------------------|------|------|
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 0.0$ ft | | | | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft | | | | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.016$ | | | | |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches | | | | |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 24.0$ ft | | | | |
| Gutter Width | $W = 1.00$ ft | | | | |
| Street Transverse Slope | $S_X = 0.020$ ft/ft | | | | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_W = 0.083$ ft/ft | | | | |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_G = 0.040$ ft/ft | | | | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.016$ | | | | |
| Max. Allowable Spread for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <th style="padding: 2px;">Minor Storm</th> <th style="padding: 2px;">Major Storm</th> </tr> <tr> <td style="padding: 2px; text-align: center;">24.0</td> <td style="padding: 2px; text-align: center;">24.0</td> </tr> </table> ft | Minor Storm | Major Storm | 24.0 | 24.0 |
| Minor Storm | Major Storm | | | | |
| 24.0 | 24.0 | | | | |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <th style="padding: 2px;">Minor Storm</th> <th style="padding: 2px;">Major Storm</th> </tr> <tr> <td style="padding: 2px; text-align: center;">6.0</td> <td style="padding: 2px; text-align: center;">6.0</td> </tr> </table> inches | Minor Storm | Major Storm | 6.0 | 6.0 |
| Minor Storm | Major Storm | | | | |
| 6.0 | 6.0 | | | | |
| Allow Flow Depth at Street Crown (check box for yes, leave blank for no) | <table style="display: inline-table; border-collapse: collapse;"> <tr> <td style="padding: 2px; text-align: center;"><input type="checkbox"/></td> <td style="padding: 2px; text-align: center;"><input type="checkbox"/></td> </tr> </table> | <input type="checkbox"/> | <input type="checkbox"/> | | |
| <input type="checkbox"/> | <input type="checkbox"/> | | | | |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | | | | |
| MAJOR STORM Allowable Capacity is based on Depth Criterion | | | | | |
| Minor storm max. allowable capacity GOOD - greater than the design peak flow of 1.40 cfs on sheet 'Inlet Management' | | | | | |
| Major storm max. allowable capacity GOOD - greater than the design peak flow of 3.50 cfs on sheet 'Inlet Management' | | | | | |
| $Q_{allow} =$ | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <th style="padding: 2px;">Minor Storm</th> <th style="padding: 2px;">Major Storm</th> </tr> <tr> <td style="padding: 2px; text-align: center;">23.1</td> <td style="padding: 2px; text-align: center;">23.1</td> </tr> </table> cfs | Minor Storm | Major Storm | 23.1 | 23.1 |
| Minor Storm | Major Storm | | | | |
| 23.1 | 23.1 | | | | |

INLET ON A CONTINUOUS GRADE



| Design Information (Input) | |
|--|--------------------------|
| Type of Inlet | CDOT Type R Curb Opening |
| Local Depression (additional to continuous gutter depression 'a') | $a_{LOCAL} = 3.0$ inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) | $N_u = 2$ |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $L_u = 5.00$ ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $W_u = N/A$ ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | $C_f(G) = N/A$ |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | $C_f(C) = 0.10$ |
| Street Hydraulics: OK - $Q < Q_{allow}$ Allowable Street Capacity | |
| Total Inlet Interception Capacity | $Q = 1.4$ cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $Q_o = 0.0$ cfs |
| Capture Percentage = Q_i/Q_o | $C\% = 100$ % |

Channel Report

Old Ranch Road - Roadside Ditch (Q = DP7 = 4.1 cfs)

Triangular

Side Slopes (z:1) = 3.00, 3.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 1.00

Slope (%) = 4.00

N-Value = 0.025

Calculations

Compute by: Known Q

Known Q (cfs) = 4.10

Highlighted

Depth (ft) = 0.54

Q (cfs) = 4.100

Area (sqft) = 0.87

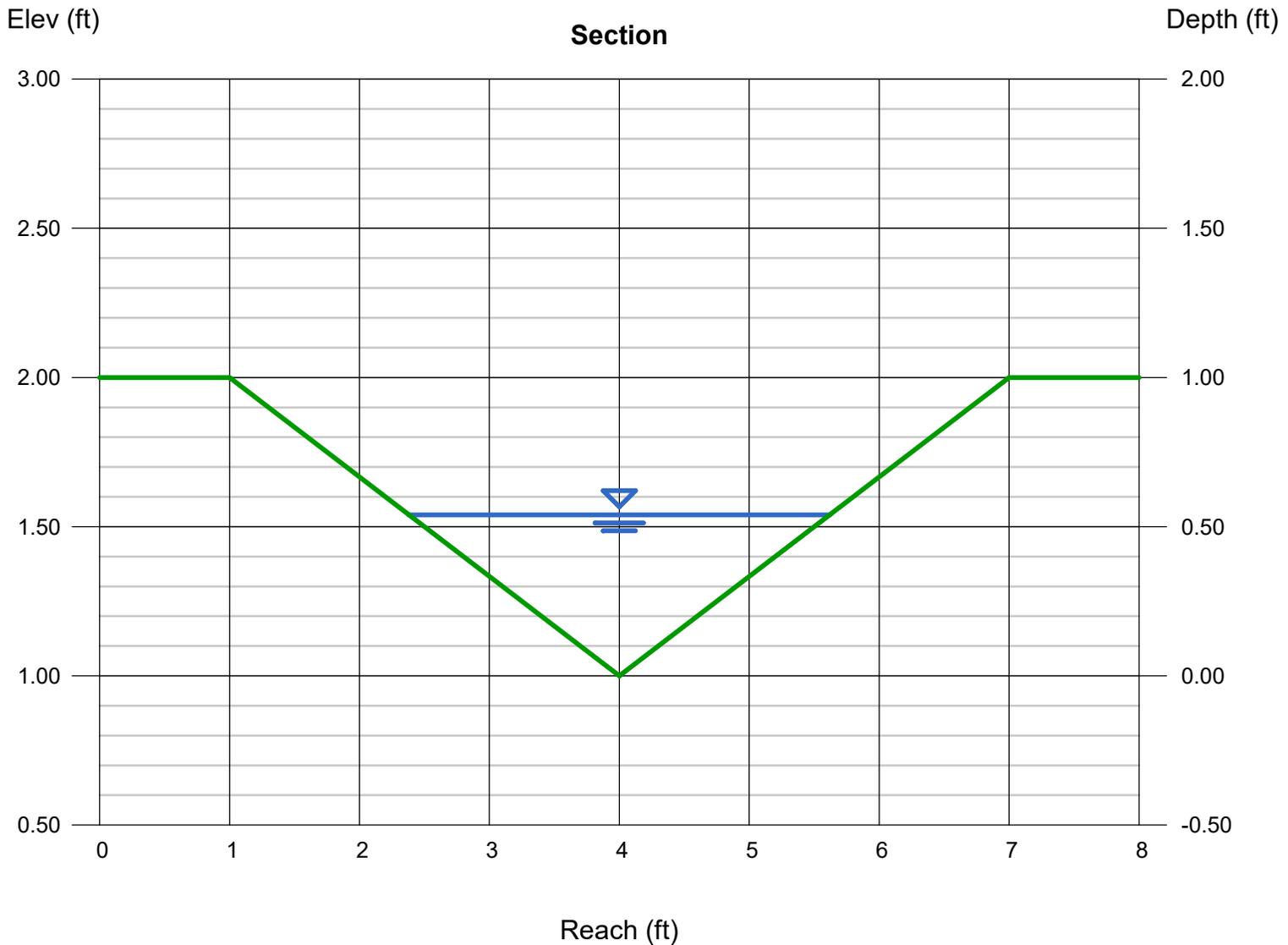
Velocity (ft/s) = 4.69

Wetted Perim (ft) = 3.42

Crit Depth, Yc (ft) = 0.66

Top Width (ft) = 3.24

EGL (ft) = 0.88



Channel Report

TRICKLE CHANNEL SIZING (1% OF 100-YR = 2.2 cfs)

Rectangular

Bottom Width (ft) = 2.00
Total Depth (ft) = 0.50

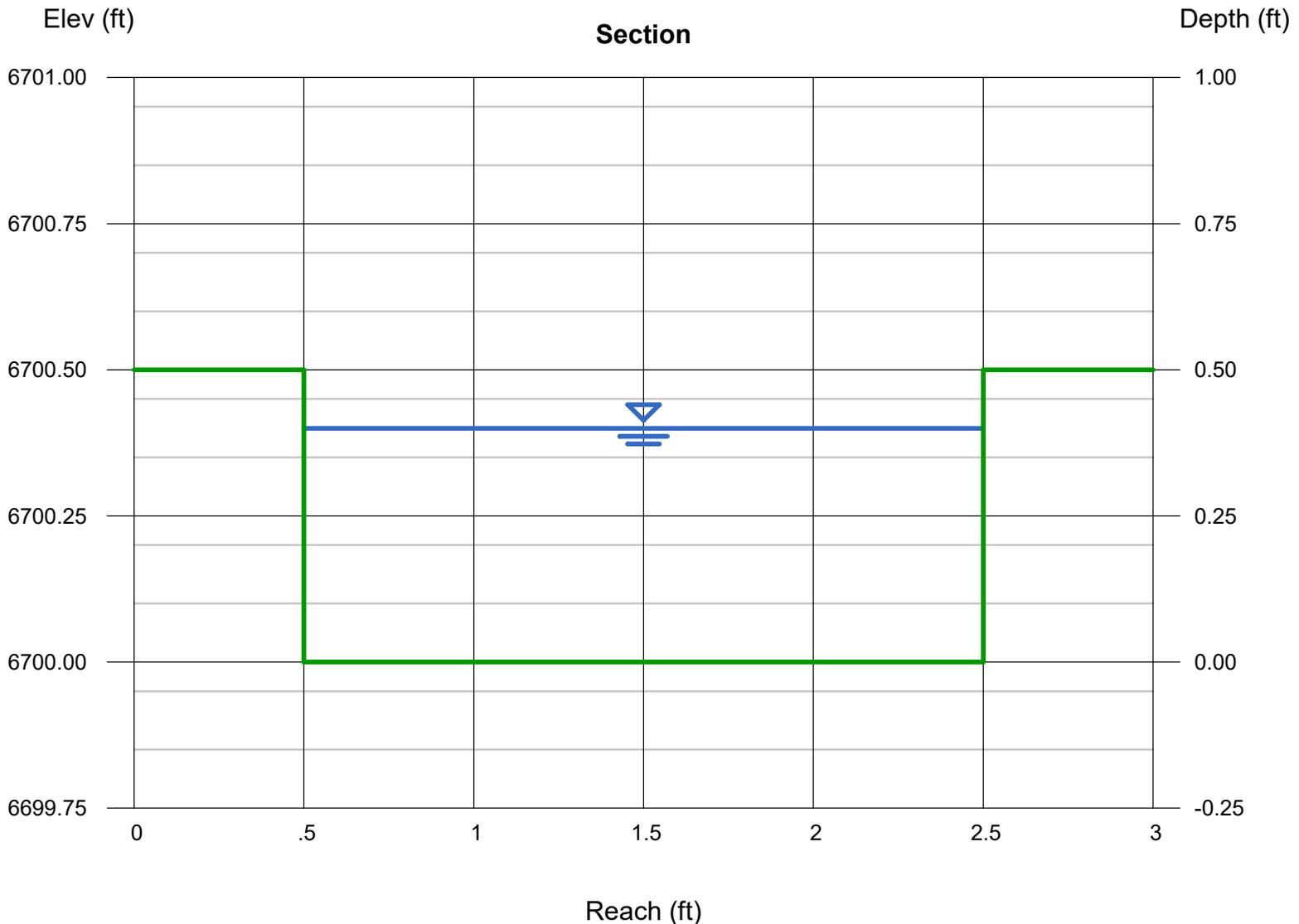
Invert Elev (ft) = 6700.00
Slope (%) = 0.50
N-Value = 0.016

Calculations

Compute by: Known Q
Known Q (cfs) = 2.20

Highlighted

Depth (ft) = 0.40
Q (cfs) = 2.200
Area (sqft) = 0.80
Velocity (ft/s) = 2.75
Wetted Perim (ft) = 2.80
Crit Depth, Yc (ft) = 0.34
Top Width (ft) = 2.00
EGL (ft) = 0.52





Project: Cottages at Kettle Creek

Project No: 24026

10/2/2024

Forebay Sizing (Per USDCM Volume 3, Table 4-12)

| WQCV (ac-ft) | 1% WQCV (ft ³) | Forebay Area (ft ²) | Forebay Depth (ft) | Forebay Volume (ft ³) |
|--------------|----------------------------|---------------------------------|--------------------|-----------------------------------|
| 0.142 | 62 | 46 | 1.5 | 69 |

**Forebay Notch Sizing
(Per USDCM Volume 3 Equation 4-1)**

$$w = 9.23(A_{FB}/t)(1/\sqrt{h_{max}})$$

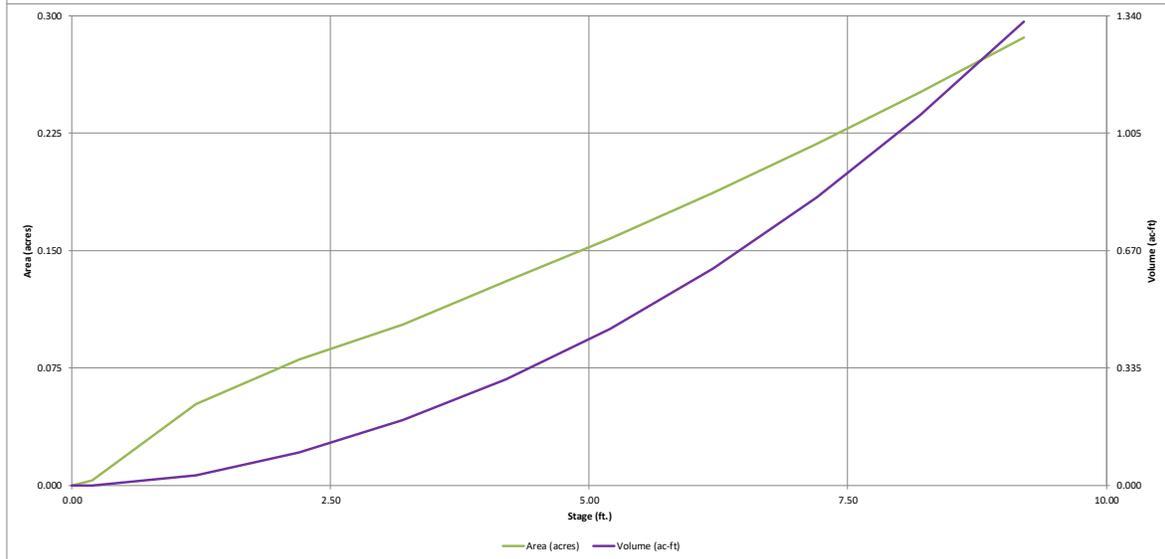
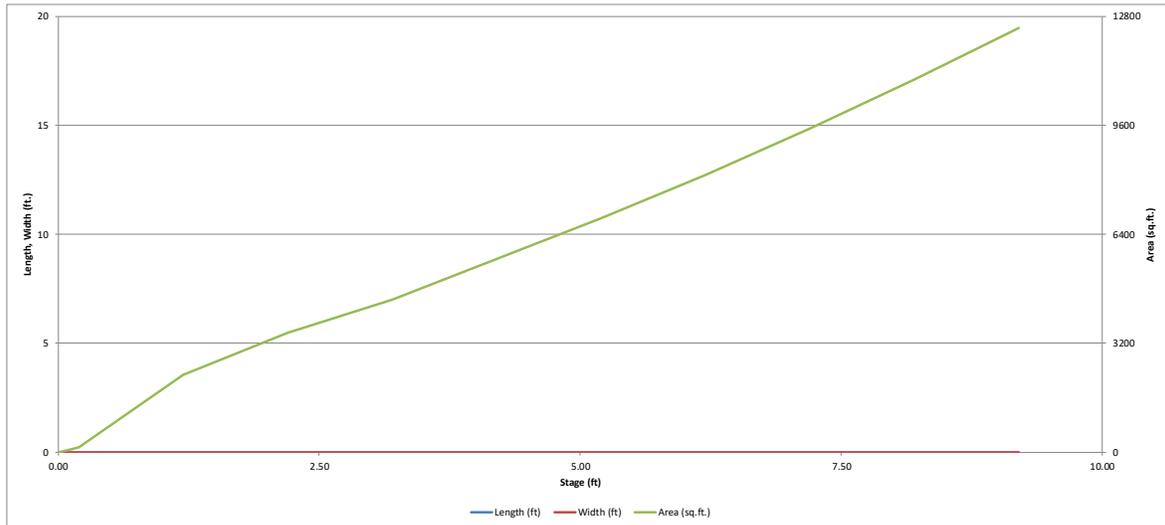
| A _{FB} (ft ²) | t (s) | h _{max} (ft) | w (in) |
|------------------------------------|-------|-----------------------|--------|
| 46 | 240 | 1.5 | 1.44 |



APPENDIX D – WATER QUALITY & DETENTION

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

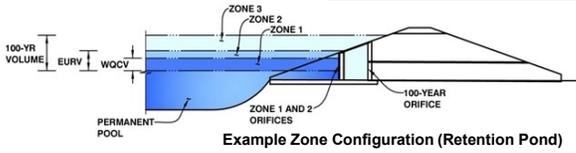
MHFD-Detention, Version 4.06 (July 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention, Version 4.06 (July 2022)*

Project: COTTAGES AT KETTLE CREEK
Basin ID: PRELIM POND SIZING



Example Zone Configuration (Retention Pond)

| | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV) | 2.73 | 0.140 | Orifice Plate |
| Zone 2 (EURV) | 5.69 | 0.387 | Circular Orifice |
| Zone 3 (100-year) | 7.07 | 0.265 | Weir&Pipe (Restrict) |
| Total (all zones) | | 0.792 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

| | | |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter = | N/A | inches |

Calculated Parameters for Underdrain

| | | |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| | | |
|--|-------|---|
| Centroid of Lowest Orifice = | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 2.73 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing = | 10.90 | inches |
| Orifice Plate: Orifice Area per Row = | 0.61 | sq. inches (diameter = 7/8 inch) |

Calculated Parameters for Plate

| | | |
|----------------------------|-----------|-----------------|
| WQ Orifice Area per Row = | 4.236E-03 | ft ² |
| Elliptical Half-Width = | N/A | feet |
| Elliptical Slot Centroid = | N/A | feet |
| Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 0.91 | 1.82 | | | | | |
| Orifice Area (sq. inches) | 0.61 | 0.61 | 0.61 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Zone 2 Circular | Not Selected | |
|---|-----------------|--------------|---|
| Invert of Vertical Orifice = | 2.75 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | 5.69 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter = | 0.90 | N/A | inches |

Calculated Parameters for Vertical Orifice

| | Zone 2 Circular | Not Selected | |
|-----------------------------|-----------------|--------------|-----------------|
| Vertical Orifice Area = | 0.00 | N/A | ft ² |
| Vertical Orifice Centroid = | 0.04 | N/A | feet |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

| | Zone 3 Weir | Not Selected | |
|---------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 6.25 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length = | 2.00 | N/A | feet |
| Overflow Weir Gate Slope = | 0.00 | N/A | H:V |
| Horiz. Length of Weir Sides = | 2.00 | N/A | feet |
| Overflow Gate Type = | Type C Gate | N/A | |
| Debris Clogging % = | 50% | N/A | % |

Calculated Parameters for Overflow Weir

| | Zone 3 Weir | Not Selected | |
|---|-------------|--------------|-----------------|
| Height of Gate Upper Edge, H ₁ = | 6.25 | N/A | feet |
| Overflow Weir Slope Length = | 2.00 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 16.31 | N/A | |
| Overflow Gate Open Area w/o Debris = | 2.78 | N/A | ft ² |
| Overflow Gate Open Area w/ Debris = | 1.39 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | Zone 3 Restrictor | Not Selected | |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe = | 2.50 | N/A | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter = | 18.00 | N/A | inches |
| Restrictor Plate Height Above Pipe Invert = | 2.75 | | inches |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

| | Zone 3 Restrictor | Not Selected | |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area = | 0.17 | N/A | ft ² |
| Outlet Orifice Centroid = | 0.14 | N/A | feet |
| Half-Central Angle of Restrictor Plate on Pipe = | 0.80 | N/A | radians |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

| | | |
|-------------------------------------|------|---|
| Spillway Invert Stage = | 7.15 | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length = | 6.00 | feet |
| Spillway End Slopes = | 4.00 | H:V |
| Freeboard above Max Water Surface = | 1.00 | feet |

Calculated Parameters for Spillway

| | | |
|------------------------------------|------|---------|
| Spillway Design Flow Depth = | 0.77 | feet |
| Stage at Top of Freeboard = | 8.92 | feet |
| Basin Area at Top of Freeboard = | 0.28 | acres |
| Basin Volume at Top of Freeboard = | 1.25 | acre-ft |

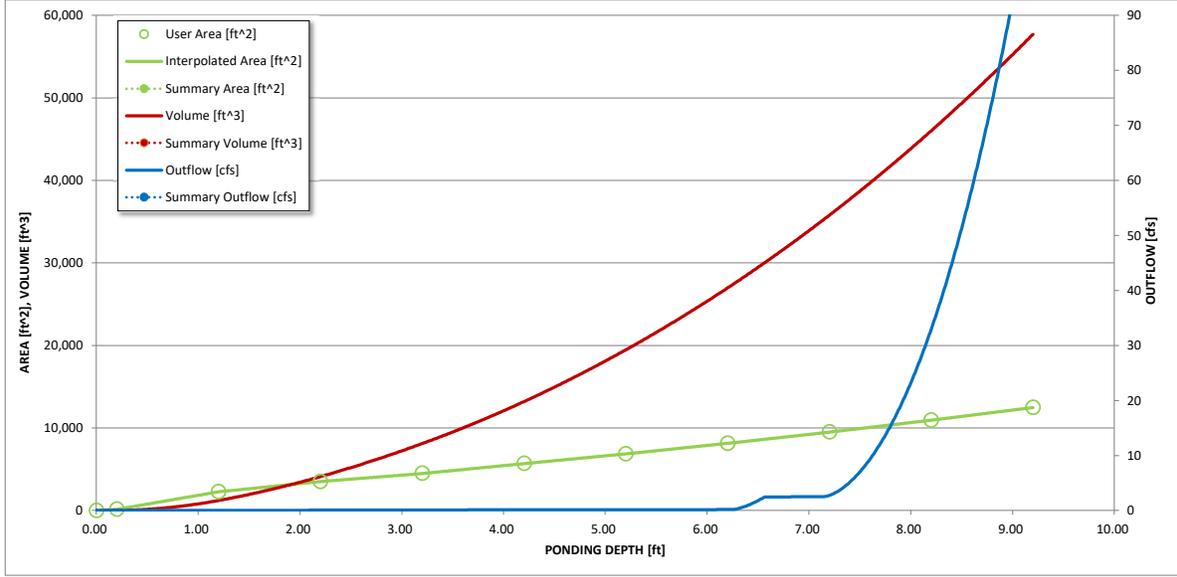
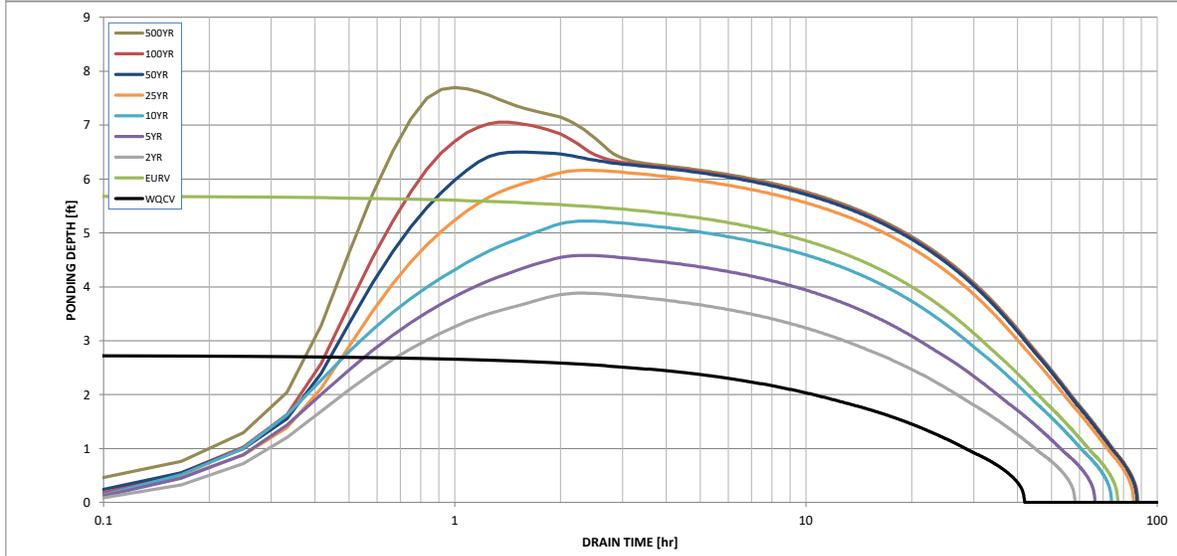
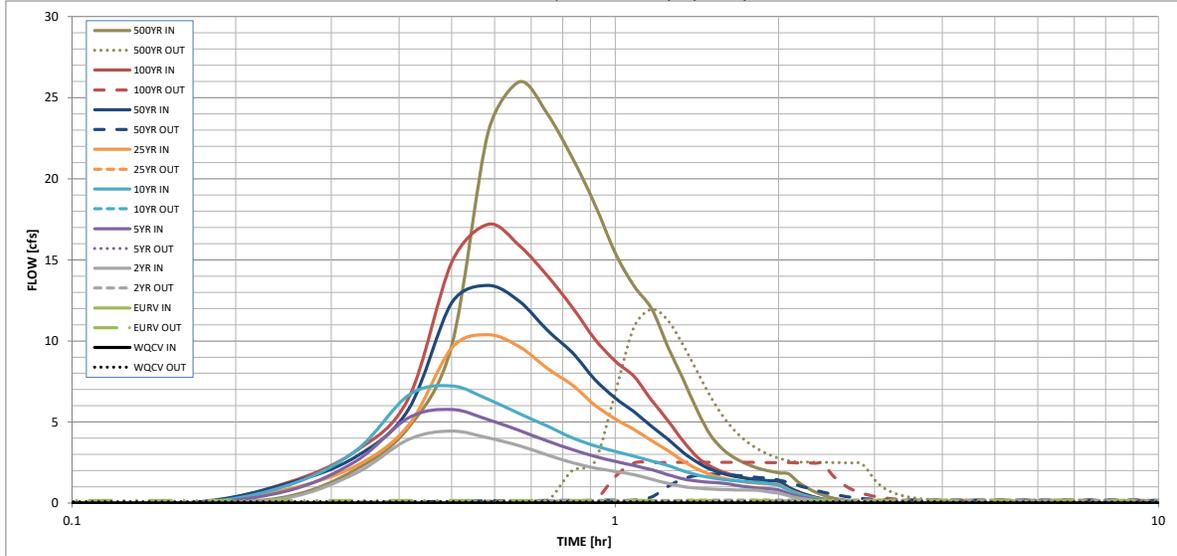
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|-------|--------------------|--------------------|--------------------|--------------------|--------------------|-----------------|----------------|----------|
| Design Storm Return Period = | N/A | N/A | 0.91 | 1.19 | 1.45 | 1.84 | 2.17 | 2.52 | 3.45 |
| One-Hour Rainfall Depth (in) = | N/A | N/A | 0.282 | 0.377 | 0.475 | 0.640 | 0.803 | 0.995 | 1.501 |
| CUHP Runoff Volume (acre-ft) = | N/A | N/A | 0.282 | 0.377 | 0.475 | 0.640 | 0.803 | 0.995 | 1.501 |
| Inflow Hydrograph Volume (acre-ft) = | N/A | N/A | 0.0 | 0.0 | 0.1 | 0.5 | 2.0 | 4.0 | 8.9 |
| CUHP Predevelopment Peak Q (cfs) = | N/A | N/A | | | | | | | |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A | N/A | | | | | | | |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | N/A | N/A | 0.00 | 0.01 | 0.01 | 0.07 | 0.30 | 0.58 | 1.30 |
| Peak Inflow Q (cfs) = | N/A | N/A | 4.4 | 5.8 | 7.2 | 10.4 | 13.4 | 17.2 | 26.0 |
| Peak Outflow Q (cfs) = | 0.1 | 0.2 | 0.1 | 0.1 | 0.2 | 0.2 | 1.8 | 2.5 | 12.0 |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 3.4 | 2.0 | 0.4 | 0.9 | 0.6 | 1.3 |
| Structure Controlling Flow = | Plate | Vertical Orifice 1 | Overflow Weir 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Gate 1 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | 0.6 | 0.8 | 0.9 |
| Max Velocity through Gate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 38 | 65 | 51 | 57 | 63 | 72 | 72 | 70 | 65 |
| Time to Drain 99% of Inflow Volume (hours) = | 40 | 72 | 55 | 63 | 70 | 80 | 81 | 79 | 77 |
| Maximum Ponding Depth (ft) = | 2.73 | 5.69 | 3.88 | 4.58 | 5.22 | 6.16 | 6.50 | 7.05 | 7.69 |
| Area at Maximum Ponding Depth (acres) = | 0.09 | 0.17 | 0.12 | 0.14 | 0.16 | 0.19 | 0.20 | 0.21 | 0.23 |
| Maximum Volume Stored (acre-ft) = | 0.140 | 0.527 | 0.261 | 0.353 | 0.448 | 0.610 | 0.674 | 0.787 | 0.932 |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.01 | 0.42 |
| | 0:15:00 | 0.00 | 0.00 | 0.34 | 0.78 | 1.10 | 0.88 | 1.22 | 1.28 | 2.08 |
| | 0:20:00 | 0.00 | 0.00 | 1.85 | 2.59 | 3.24 | 2.30 | 2.87 | 3.22 | 4.67 |
| | 0:25:00 | 0.00 | 0.00 | 3.93 | 5.26 | 6.65 | 4.80 | 5.79 | 6.48 | 9.70 |
| | 0:30:00 | 0.00 | 0.00 | 4.44 | 5.77 | 7.23 | 9.55 | 12.35 | 14.85 | 22.88 |
| | 0:35:00 | 0.00 | 0.00 | 4.02 | 5.15 | 6.40 | 10.38 | 13.42 | 17.19 | 25.98 |
| | 0:40:00 | 0.00 | 0.00 | 3.54 | 4.47 | 5.51 | 9.65 | 12.43 | 15.88 | 24.00 |
| | 0:45:00 | 0.00 | 0.00 | 2.96 | 3.83 | 4.75 | 8.31 | 10.65 | 14.02 | 21.29 |
| | 0:50:00 | 0.00 | 0.00 | 2.49 | 3.31 | 4.03 | 7.28 | 9.28 | 12.08 | 18.45 |
| | 0:55:00 | 0.00 | 0.00 | 2.17 | 2.88 | 3.53 | 6.06 | 7.63 | 10.12 | 15.42 |
| | 1:00:00 | 0.00 | 0.00 | 1.95 | 2.58 | 3.19 | 5.18 | 6.47 | 8.75 | 13.38 |
| | 1:05:00 | 0.00 | 0.00 | 1.76 | 2.31 | 2.89 | 4.54 | 5.63 | 7.80 | 11.98 |
| | 1:10:00 | 0.00 | 0.00 | 1.47 | 2.06 | 2.59 | 3.85 | 4.73 | 6.34 | 9.64 |
| | 1:15:00 | 0.00 | 0.00 | 1.21 | 1.76 | 2.31 | 3.23 | 3.94 | 5.09 | 7.66 |
| | 1:20:00 | 0.00 | 0.00 | 1.02 | 1.49 | 2.00 | 2.59 | 3.13 | 3.83 | 5.69 |
| | 1:25:00 | 0.00 | 0.00 | 0.92 | 1.35 | 1.73 | 2.10 | 2.51 | 2.84 | 4.17 |
| | 1:30:00 | 0.00 | 0.00 | 0.86 | 1.28 | 1.57 | 1.75 | 2.07 | 2.25 | 3.27 |
| | 1:35:00 | 0.00 | 0.00 | 0.83 | 1.22 | 1.46 | 1.53 | 1.81 | 1.91 | 2.75 |
| | 1:40:00 | 0.00 | 0.00 | 0.82 | 1.10 | 1.37 | 1.39 | 1.64 | 1.69 | 2.39 |
| | 1:45:00 | 0.00 | 0.00 | 0.80 | 1.00 | 1.31 | 1.29 | 1.52 | 1.54 | 2.15 |
| | 1:50:00 | 0.00 | 0.00 | 0.79 | 0.93 | 1.27 | 1.22 | 1.44 | 1.44 | 1.99 |
| | 1:55:00 | 0.00 | 0.00 | 0.69 | 0.88 | 1.21 | 1.18 | 1.39 | 1.36 | 1.87 |
| | 2:00:00 | 0.00 | 0.00 | 0.60 | 0.82 | 1.09 | 1.14 | 1.35 | 1.32 | 1.80 |
| | 2:05:00 | 0.00 | 0.00 | 0.45 | 0.60 | 0.80 | 0.84 | 0.99 | 0.97 | 1.33 |
| | 2:10:00 | 0.00 | 0.00 | 0.32 | 0.43 | 0.58 | 0.61 | 0.72 | 0.70 | 0.96 |
| | 2:15:00 | 0.00 | 0.00 | 0.23 | 0.31 | 0.41 | 0.44 | 0.51 | 0.51 | 0.69 |
| | 2:20:00 | 0.00 | 0.00 | 0.16 | 0.22 | 0.29 | 0.31 | 0.36 | 0.36 | 0.49 |
| | 2:25:00 | 0.00 | 0.00 | 0.11 | 0.15 | 0.20 | 0.21 | 0.25 | 0.25 | 0.34 |
| | 2:30:00 | 0.00 | 0.00 | 0.07 | 0.10 | 0.14 | 0.15 | 0.17 | 0.17 | 0.23 |
| | 2:35:00 | 0.00 | 0.00 | 0.05 | 0.07 | 0.09 | 0.10 | 0.11 | 0.11 | 0.15 |
| | 2:40:00 | 0.00 | 0.00 | 0.02 | 0.04 | 0.05 | 0.06 | 0.07 | 0.07 | 0.09 |
| | 2:45:00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.02 | 0.03 | 0.03 | 0.03 | 0.04 |
| | 2:50:00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 2:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |



APPENDIX E – REFERENCE MATERIAL



APPENDIX F – DRAINAGE MAPS

COTTAGES AT KETTLE CREEK

PROPOSED DRAINAGE MAP



LEGEND

| | EXISTING | PROPOSED |
|-------------------------|----------|----------|
| SECTION LINE | --- | --- |
| BOUNDARY LINE | --- | --- |
| PROPERTY LINE | --- | --- |
| EASEMENT LINE | --- | --- |
| RIGHT OF WAY | --- | --- |
| CENTERLINE | --- | --- |
| STORM SEWER | --- | --- |
| SWALE/WATERWAY FLOWLINE | --- | --- |
| INDEX CONTOUR | --- | --- |
| INTERMEDIATE CONTOUR | --- | --- |
| FLOW DIRECTION | --- | --- |
| BASIN ID | | |
| SUB-BASIN DRAINAGE AREA | --- | --- |

NOTES

- ALL PROPOSED STORM SEWER IS PRIVATE.
- THE FULL SPECTRUM (F.S.) WATER QUALITY AND DETENTION POND AND ITS APPURTENANCES ARE ALL PRIVATE.
- NON-STORMWATER, EXISTING UTILITIES ARE NOT SHOWN, SEE EXISTING DRAINAGE MAP FOR REFERENCE.
- SEE EXISTING DRAINAGE MAP FOR NORTHERN LIMITS OF BASIN OS1 AND OS2. THERE ARE NO IMPROVEMENTS OR CHANGES TO DRAINAGE BEYOND THE LIMITS OF THIS DRAINAGE MAP.

PROPOSED CALCS - BASIN SUMMARY TABLE

| Tributary Sub-basin | Area (acres) | Percent Impervious | C _s | C ₁₀₀ | t _c (min) | Q _s (cfs) | Q ₁₀₀ (cfs) |
|---------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| A | 1.98 | 62% | 0.57 | 0.71 | 17.9 | 4.7 | 9.8 |
| B | 2.26 | 64% | 0.58 | 0.72 | 18.1 | 5.4 | 11.2 |
| C | 0.53 | 65% | 0.60 | 0.73 | 15.9 | 1.4 | 2.9 |
| D | 1.57 | 76% | 0.69 | 0.80 | 15.4 | 4.8 | 9.3 |
| E | 0.50 | 12% | 0.17 | 0.42 | 25.9 | 0.4 | 1.8 |
| F | 0.22 | 47% | 0.46 | 0.63 | 19.7 | 0.5 | 1.2 |
| G | 0.96 | 17% | 0.22 | 0.45 | 27.8 | 0.7 | 2.5 |
| OS1 | 1.97 | 14% | 0.17 | 0.41 | 35.4 | 1.1 | 4.5 |
| OS2 | 12.06 | 5% | 0.11 | 0.38 | 40.9 | 2.7 | 15.3 |
| OS3 | 10.37 | 2% | 0.09 | 0.36 | 17.9 | 2.2 | 14.8 |

DESIGN POINT SUMMARY TABLE

| DP# | Q _s YR | Q ₁₀₀ YR |
|-----|-------------------|---------------------|
| 1 | 4.7 | 9.8 |
| 2 | 5.4 | 11.2 |
| 3 | 4.8 | 9.4 |
| 3.1 | 9.6 | 18.4 |
| 4 | 1.4 | 3.5 |
| 4.1 | 10.8 | 20.7 |
| 5 | 11.1 | 22.0 |
| 6 | 0.5 | 1.7 |
| 7 | 1.1 | 4.1 |
| 8 | 1.1 | 4.5 |
| 9 | 2.7 | 15.3 |
| 10 | 2.2 | 14.8 |

50 25 0 50 100
ORIGINAL SCALE: 1" = 50'

PROPOSED DRAINAGE MAP

COTTAGES AT KETTLE CREEK

| | |
|---------------|-------|
| JOB NO. 24026 | SHEET |
| LOCATION: CS | 1 |
| 09/30/2024 | |

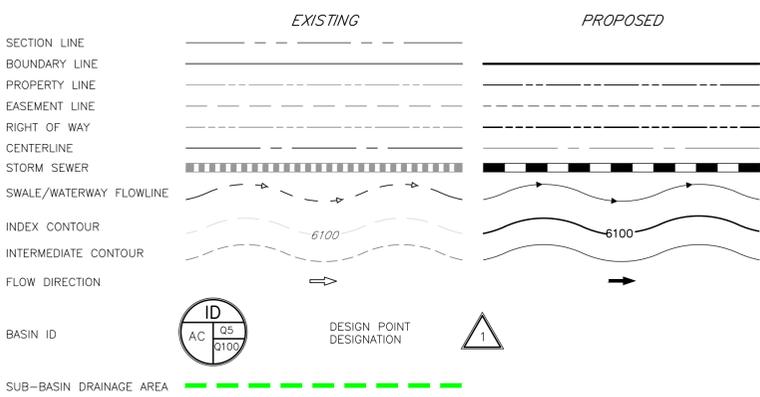
ALL TERRAIN
ENGINEERING

COTTAGES AT KETTLE CREEK

PROPOSED DRAINAGE MAP



LEGEND



PROPOSED CALCS - BASIN SUMMARY TABLE

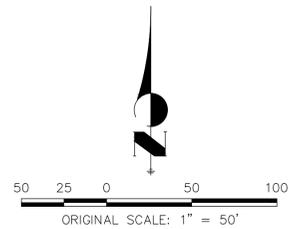
| Tributary Sub-basin | Area (acres) | Percent Impervious | C _s | C ₁₀₀ | t _c (min) | Q _s (cfs) | Q ₁₀₀ (cfs) |
|---------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| A | 1.98 | 62% | 0.57 | 0.71 | 17.9 | 4.7 | 9.8 |
| B | 2.26 | 64% | 0.58 | 0.72 | 18.1 | 5.4 | 11.2 |
| C | 0.53 | 65% | 0.60 | 0.73 | 15.9 | 1.4 | 2.9 |
| D | 1.57 | 76% | 0.69 | 0.80 | 15.4 | 4.8 | 9.3 |
| E | 0.50 | 12% | 0.17 | 0.42 | 25.9 | 0.4 | 1.8 |
| F | 0.22 | 47% | 0.46 | 0.63 | 19.7 | 0.5 | 1.2 |
| G | 0.96 | 17% | 0.22 | 0.45 | 27.8 | 0.7 | 2.5 |
| OS1 | 1.97 | 14% | 0.17 | 0.41 | 35.4 | 1.1 | 4.5 |
| OS2 | 12.06 | 5% | 0.11 | 0.38 | 40.9 | 2.7 | 15.3 |
| OS3 | 10.37 | 2% | 0.09 | 0.36 | 17.9 | 2.2 | 14.8 |

DESIGN POINT SUMMARY TABLE

| DP# | Q _p -YR | Q ₁₀₀ -YR |
|-----|--------------------|----------------------|
| 1 | 4.7 | 9.8 |
| 2 | 5.4 | 11.2 |
| 3 | 4.8 | 9.4 |
| 3.1 | 9.6 | 18.4 |
| 4 | 1.4 | 3.5 |
| 4.1 | 10.8 | 20.7 |
| 5 | 11.1 | 22.0 |
| 6 | 0.5 | 1.7 |
| 7 | 1.1 | 4.1 |
| 8 | 1.1 | 4.5 |
| 9 | 2.7 | 15.3 |
| 10 | 2.2 | 14.8 |

NOTES

- ALL PROPOSED STORM SEWER IS PRIVATE.
- THE FULL SPECTRUM (F.S.) WATER QUALITY AND DETENTION POND AND ITS APPURTENANCES ARE ALL PRIVATE.
- NON-STORMWATER, EXISTING UTILITIES ARE NOT SHOWN, SEE EXISTING DRAINAGE MAP FOR REFERENCE.
- SEE EXISTING DRAINAGE MAP FOR NORTHERN LIMITS OF BASIN OS1 AND OS2. THERE ARE NO IMPROVEMENTS OR CHANGES TO DRAINAGE BEYOND THE LIMITS OF THIS DRAINAGE MAP.



PROPOSED DRAINAGE MAP

COTTAGES AT KETTLE CREEK

JOB NO. 24026 SHEET 2

LOCATION: CS

DATE: 09/30/2024

COTTAGES AT KETTLE CREEK

RUNOFF REDUCTION MAP

LEGEND:

- DCIA
- UIA
- RPA
- SPA



| | |
|--------------------------|-------|
| RUNOFF REDUCTION MAP | |
| COTTAGES AT KETTLE CREEK | |
| JOB NO. 24026 | SHEET |
| LOCATION: CS | 1 |
| 10/01/2024 | |
| | |