



Final Drainage Report

# Meadowbrook Park El Paso County, Colorado

PCD File No.: PUDSP208  
SF-21-025

Prepared for:  
**Danny Mientka**  
**Meadowbrook Development, LLC.**  
**90 South Cascade Avenue**  
**Suite 1500**  
**Colorado Springs, Colorado 80903**

Prepared by:  
**Kimley-Horn and Associates, Inc.**  
**2 North Nevada Ave**  
**Suite 300**  
**Colorado Springs, CO 80903**  
**(719) 284-7272**  
**Contact: John Heiberger, P.E.**

Project #: 096956009

Prepared: March 18th, 2021  
Revision 1: June 2, 2021  
Revision 2: July 14, 2021  
Revision 3: September 30, 2021  
Revision 4: February 3, 2022  
Revision 5: April 21, 2022  
Revision 6: June 6, 2022

**Kimley»Horn**



## Table of Contents

<b>CERTIFICATION .....</b>	<b>3</b>
ENGINEERS STATEMENT .....	3
DEVELOPER'S STATEMENT .....	3
EL PASO COUNTY STATEMENT .....	3
<b>GENERAL LOCATION AND DESCRIPTION .....</b>	<b>4</b>
PURPOSE AND SCOPE OF STUDY .....	4
LOCATION .....	4
VICINITY MAP .....	4
DESCRIPTION OF PROPERTY .....	5
PROJECT CHARACTERISTICS .....	5
<b>DRAINAGE BASINS AND SUB-BASINS .....</b>	<b>5</b>
MAJOR BASIN DESCRIPTIONS .....	5
SUB-BASIN DESCRIPTION .....	6
<i>Historic Drainage Patterns</i> .....	6
<i>Off-Site Drainage Flow Patterns</i> .....	6
<b>DRAINAGE DESIGN CRITERIA .....</b>	<b>7</b>
DEVELOPMENT CRITERIA REFERENCE .....	7
HYDROLOGIC CRITERIA .....	7
<b>DRAINAGE FACILITY DESIGN .....</b>	<b>8</b>
GENERAL CONCEPT .....	8
COMPLIANCE WITH OFF-SITE RUNOFF .....	8
PROPOSED DRAINAGE PATTERNS .....	8
<i>Sub-Basin A</i> .....	9
<i>Sub-Basin B</i> .....	9
<i>Sub-Basin C</i> .....	9
<i>Sub-Basin D</i> .....	9
<i>Sub-Basin E</i> .....	10
<i>Sub-Basin F</i> .....	10
<i>Sub-Basin G</i> .....	10
<i>Sub-Basin H</i> .....	10
<i>Sub-Basin I</i> .....	10
<i>Sub-Basin J</i> .....	11
<i>Sub-Basin OS-A</i> .....	11
<i>Sub-Basin OS-B</i> .....	11
<i>Sub-Basin OS-C</i> .....	11
EMERGENCY OVERFLOW ROUTING .....	11
DETENTION AND WATER QUALITY .....	12
<i>Four-Step Process</i> .....	12
<i>Detention and Water Quality Design</i> .....	12
<i>Outlet Requirements</i> .....	13
<i>Channel Design and Soil Erodibility</i> .....	13
<i>Emergency Spillway Path</i> .....	13
<b>COST OF PROPOSED DRAINAGE FACILITIES .....</b>	<b>13</b>

**DRAINAGE AND BRIDGE FEES .....13**

**GRADING AND EROSION CONTROL.....14**

**MAINTENANCE AND OPERATIONS .....14**

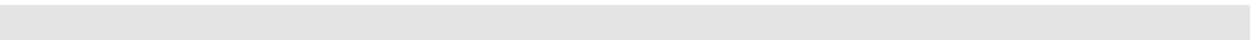
**OTHER GOVERNMENT AGENCY REQUIREMENTS .....14**

**SUMMARY .....14**

    COMPLIANCE WITH STANDARDS.....14

**REFERENCES .....15**

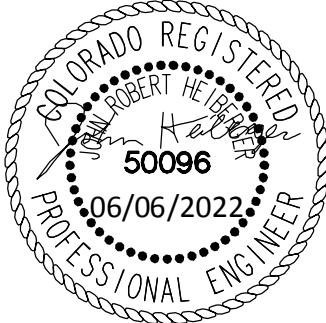
**APPENDIX .....16**



## CERTIFICATION

### ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



*John Heiberger*

06/06/2022

SIGNATURE (Affix Seal):

Colorado P.E. No. 50096

Date

### DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Meadowbrook Development LLC

Business Name

*Kelly Nelson*

By: Kelly Nelson

Development Manager

Title:

Address: 90 S. Cascade, Ste 1500  
Colorado Springs, CO 80903

### EL PASO COUNTY STATEMENT

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

APPROVED  
Engineering Department

07/18/2022 8:15:26 AM

*dsdnijkamp*

EPC Planning & Community  
Development Department

Date

County Engineer/ECM Administrator

Conditions:



## GENERAL LOCATION AND DESCRIPTION

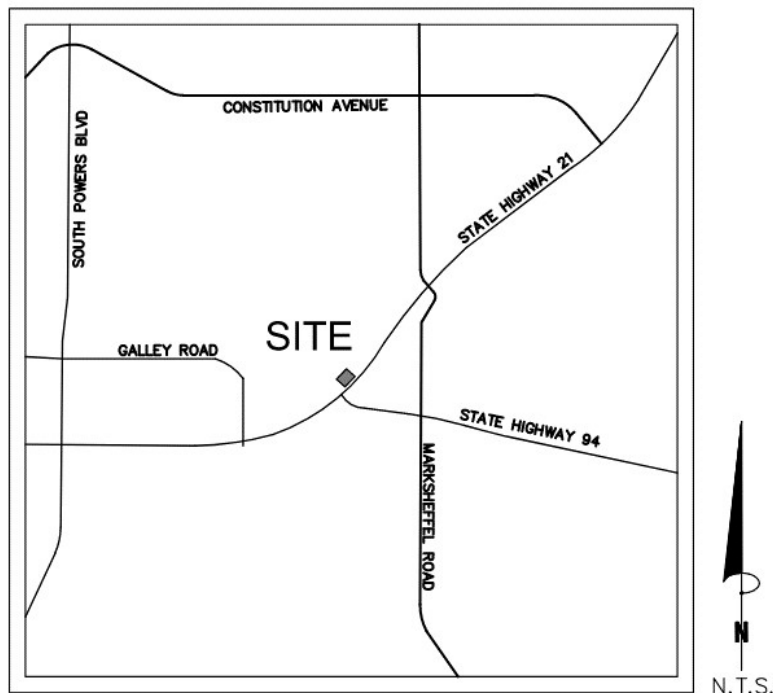
### PURPOSE AND SCOPE OF STUDY

The purpose of this Final Drainage Report (FDR) is to provide the hydrologic and hydraulic calculations and to document and finalize the drainage design methodology in support of the proposed Meadowbrook Park development (“the Project”) for Meadowbrook Development LLC. The Project is located within the jurisdictional limits of El Paso County (“the County”). Thus, the guidelines for the hydrologic and hydraulic design components were based on the criteria outlined by the County.

### LOCATION

The Project is located northwest of the Meadowbrook Parkway and US Highway 24 intersection in El Paso County, Colorado. More specifically, the Project is made up of Tract A 94/24 Business Park Filing No. 1, Tract I Meadowbrook Crossing Filing No. 1, and a Tract within the Claremont Business park Filing No. 2 (parcel number 5408000053) plat within the southeast quarter of Section 8, Township 14 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, County of El Paso, State of Colorado. The site is bounded by Meadowbrook Parkway and the Meadowbrook Crossing Filings No. 1 and No. 2 to the west, Lot 46A Claremont Business Park Filing No. 2A, a commercial storage development to the north, US Highway 24 (CDOT Right of Way) to the east, and Lot 1 24/94 Business Park Filing No. 1, a commercial gas station to the south. A vicinity map has been provided in the Appendix of this report.

### VICINITY MAP



VICINITY MAP  
N.T.S

## **DESCRIPTION OF PROPERTY**

The Project is located on approximately 8.17 acres of undeveloped land with limited vegetation and grass cover. The site currently does not provide stormwater quality or detention and there are no known major drainage ways or irrigation facilities on the site. The site generally drains from the east to west with slopes ranging from 2% to 25% with the steeper slopes along the east side of the site adjacent to US Highway 24 and Lot 46A Claremont Business Park Filing No. 2A, the commercial storage facility to the north. There is an existing 30" CMP CDOT culvert that outfalls onto the site, conveying flow from the median of Hwy 24. This runoff flows across the Site to an existing storm area inlet located in the southwest corner of the Site. The Project is not adjacent to any major drainageways and does not outfall directly to any major drainageways.

NRCS soil data is available for the Site (See Appendix) and the onsite soils are USCS Hydrologic Soil Group A. Group A soils have higher infiltration rates compared to other soil groups and are generally made up of well drained, cohesive sands or gravelly sands. A Soils and Geology Study has also been prepared for the site by Rocky Mountain Group dated August 26, 2020 and is attached in the Appendix of this report for reference.

## **PROJECT CHARACTERISTICS**

The Project is a proposed single family development that will include 67 lots. The project will include the construction of private streets, sidewalks, driveways, hardscape/landscape, and associated utility infrastructure required to serve each lot. Water quality and detention is required for the site improvements and will be accomplished with the construction of a Full Spectrum Extended Detention Basin located in the southeast corner of the site and a water quality Rain Garden located in the southwest corner of the Site. As part of the utility infrastructure improvements, a proposed storm sewer system will be constructed to collect runoff. Stormwater will be conveyed via overland flow across the lots, within the curb and gutter of the proposed streets before being captured in proposed storm inlets. Additionally, the corridors between homes shall not be graded flat. Swales proposed within the six foot corridor in-between each set of single-family homes will convey stormwater from the roof drains and from landscape areas inbetween the homes. The swales will be centered in the 6-foot corridor between the homes on the two adjacent lots and will convey stormwater to the proposed storm inlets in the proposed streets. The storm sewer system will then convey runoff into the Full Spectrum Extended Detention Basin before being discharged offsite. A small portion of the Site drains to curb chase that outfalls into the Rain Garden for water quality treatment, only. The Full Spectrum Extended Detention Basin will overdetain to include the area flowing to the Rain Garden to provide detention volume.

## **DRAINAGE BASINS AND SUB-BASINS**

### **MAJOR BASIN DESCRIPTIONS**

The site is located within the Sand Creek Drainage Basin Study (DBPS). It is not directly adjacent to East Fork Sand Creek, but East Fork Sand Creek is the ultimate receiving water for the discharge from this Site. The Sand Creek DBPS calls for bank stabilization improvements and two drop structures which were constructed with the Meadowbrook Crossing Filings No. 1

and No. 2 developments. No additional creek improvements are included with the development of this Project.

The Site is also located outside the 100-year floodplain and within Zone X (an area of minimal flood hazard) as noted on the FEMA FIRM Map No. 08041C0752G revised on December 7, 2018 (See Appendix).

There are no identified nearby irrigation facilities or other obstructions which could influence the local drainage, other than the CDOT off-site flow from the 30" CMP culvert previously mentioned.

## ***SUB-BASIN DESCRIPTION***

### **Historic Drainage Patterns**

The existing runoff onsite generally drains from east to west and is collected by an existing storm area inlet located in the southwest corner of the site. The runoff is then conveyed via storm sewer through the neighboring site to the southwest before discharging into the County storm sewer system within Meadowbrook Parkway. Runoff from offsite enters to the east of the site from US Highway 24 and drains to the same inlet as the onsite runoff in the southeast corner.

The existing drainage is divided into three sub-basins, Basin EX-A, EX-B, and EX-C. Sub-Basin EX-A is approximately 8.18 acres on consists of most of the on-site area within the property line. Runoff generated from this Sub-Basin drains overland from east to west towards the existing storm area inlet. The weighted imperviousness for Sub-Basin EX-A with existing conditions is 2% and the runoff for the 5-year and 100-year storm events are 2.49 cfs and 16.70 cfs respectively.

### **Off-Site Drainage Flow Patterns**

Sub-Basin EX-B is approximately 1.34 acres and consists of the area within the CDOT Right of Way, downstream of the existing 30" CMP culvert and area inlet within the median. It comprises of the west portion of US Highway 24 (US-24) travel lanes, shoulder and existing 4:1 slope down to Site. The flows generated from the east portion of US-24 and within the median flow south to another area inlet and culvert away from the project area. The weighted imperviousness for Sub-Basin EX-A with existing conditions is 51.1% and the runoff for the 5-year and 100-year storm events are 3.01 cfs and 6.73 cfs respectively.

Sub-Basin EX-C is approximately 3.87 acres and consists of the area within the CDOT Right of Way upstream of the existing 30" CMP culvert and area inlet within the median. It comprises of runoff generated from all four travel lanes on US-24 and runoff generated within the existing median. Runoff is either conveyed overland onto the Site or through an existing area inlet within the median and then into a 30" CMP culvert. The culvert outfalls onto the Site and flows overland to the southwest corner to the existing storm area inlet. The weighted imperviousness for Sub-Basin EX-C with existing conditions is 54.0% and the runoff for the 5-year and 100-year storm events are 7.71 cfs and 16.89 cfs respectively.

## **DRAINAGE DESIGN CRITERIA**

### ***DEVELOPMENT CRITERIA REFERENCE***

The proposed storm facilities follow the El Paso County Drainage Criteria Manual (the “CRITERIA”), El Paso Engineering Criteria Manual (the “ECM”), and the Mile High Flood District Urban Storm Drainage Criteria Manual (the “MANUAL”). Site drainage is not significantly impacted by such constraints as utilities or existing development. Further detail regarding onsite drainage patterns is provided in the Proposed Drainage Conditions Section.

There are previous drainage studies that include portions of the Project Site limits:

24/94 Business Park Final Drainage Report- This report completed by Core Engineering Group, LLC dated, July 14, 2016 details the existing 2- Type D inlets in the southwest corner of the Site. It also shows the storm alignment from the existing Type D inlet, across Meadowbrook Parkway and to the outfall in East Fork Sand Creek. This alignment will be the ultimate outfall for the discharge from this project. Proposed flows from the Site are less than the historic flows through the existing infrastructure shown in this drainage report.

Claremont Business Park Filing No. 2 Final Drainage Report- This report completed by Matrix Design Group, Inc. dated, November 2006. This report shows that the runoff from Lot 46A Claremont Business Park Filing No. 2A is maintained on the lot as does not generate runoff onto the Site that would be classified as off-site drainage for this Project.

Meadowbrook Crossing Filings No. 1 and No. 2 Preliminary and Final Drainage Report- This report completed by Kiowa Engineering Corporation dated, July 25, 2017 does not specifically include area on Site on the Drainage Map, but provides details about the improvements made to East Fork Sand Creek for stabilization and documents the extension of Meadowbrook Parkway.

### ***HYDROLOGIC CRITERIA***

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per chapter 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site basin. The detention storage requirement was calculated using Full Spectrum Detention methods as specified in the CRITERIA and MANUAL. The Full Spectrum Extended Detention Basin’s outlet structure was designed to release the Water Quality Capture Volume (WQCV) in 40 hours. The Rain Garden was designed to release the WQCV in 12 hours. Based upon this approach, we feel that the drainage design provided for the Site is conservative and in keeping with the historic drainage patterns for the Site.

The proposed drainage facilities are designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using FIRM panels by FEMA and information provided in the CRITERIA. Hydraulic calculations were computed using StormCAD for the proposed storm sewer system. Results of the hydraulic calculations are summarized in the Appendix.

## **DRAINAGE FACILITY DESIGN**

### **GENERAL CONCEPT**

#### **COMPLIANCE WITH OFF-SITE RUNOFF**

The runoff generated from US-24 currently outfalls onto the Site through an existing 30" CMP culvert. The off-site drainage basins were analyzed and found to include parts of the travel lanes, median and Right of Way. Currently, there is not a CDOT stormwater quality and detention facility that captures and treats this area. For that reason, each off-site Sub-Basin is collected in a swale parallel to US-24 roadway and within the CDOT Right of Way and conveyed to the southeast property corner of the Site. Off-site flows will be captured from the proposed swale by a proposed private CDOT Type D inlet (depressed and in series) and by-pass the property in a proposed 30" RCP storm pipe. This storm pipe runs along the southern property line within a proposed 15' private drainage easement and will connect to the existing 36" RCP storm pipe with a proposed manhole. Hydrologic and hydraulic analysis was completed to verify the capacity of the downstream facilities to handle the by-passed flows. All generated from the off-site Sub-Basins will be by-passed through the Site.

#### **PROPOSED DRAINAGE PATTERNS**

The developed runoff from the Project will generally be collected by means of a private storm sewer system with inlets located in the private streets (Nova View, Tenebris Point, Spatium View, Solum Grove and Lux Point) within each delineated sub-basin area. Side lot swales will be located within the 5' side yard setback and corresponding 1' side yard setback on the adjacent lot for a combined 6' setback corridor in-between homes. The low point of elevation/flood line will be centered in the 6-foot corridor. Side lot swales will convey stormwater to the proposed storm sewer system. The runoff collected from each Sub-Basin A, C-J will be captured by storm inlets and conveyed through storm pipes to a Full Spectrum Extended Detention Basin located in the southeast corner of the site. The controlled stormwater will be treated, detained, and released from an outlet structure which will convey stormwater through a proposed storm pipe that runs along the southern property line with a 15' private drainage easement. Eventually the outfall pipe connects to the existing private storm sewer in the southwest corner. A portion of the site Sub-Basin B, surface drains to the southwest corner, entering a proposed rain garden through a concrete chase. The WQCV in the rain garden will be treated and released through an outlet structure and conveyed through a storm pipe to a connection in the existing private 36" RCP pipe.

The existing private 36" Reinforced Concrete Pipe extends long the northern property line of Lot 1 24/94 Business Park Filing No. 1, a commercial gas station to the north east corner of the lot and stubbed into an existing public 10' Type R Inlet. The inlet is used as a junction structure and runoff is conveyed through an existing public 42" RCP storm pipe across Meadowbrook Parkway and long Newt Drive until it ultimately outfalls into the East Fork Sand Creek. This is depicted in the proposed drainage map as part of the Meadowbrook Crossing Filings No. 1 and No. 2 Preliminary and Final Drainage Report

### **SPECIFIC DETAILS**

The property has been divided into fourteen sub-basins, A through J and OS-A- OS-C. Sub-basins A through J make up the Project on-site area and Sub-Basins OS-A -OS-C are the offsite basins consisting of runoff from US Highway 24.

The weighted imperviousness of the Site area (Sub-basins A through J) with proposed conditions is 43.2%. Cumulative runoff for the 5-year and 100-year storm events are 15.54 cfs and 36.65 cfs, respectively for the site area (Sub-basins A through J). The weighted imperviousness of the entire study area: offsite area (Sub-basin OS-A-OS-C) with onsite area (Sub-Basins A through J) is 46.7%. Cumulative runoff for the 5-year and 100-year storm events for the entire study area are 26.22 cfs and 60.19 cfs, respectively.

### **Sub-Basin A**

Sub-basin A consists of approximately 2.47 acres and is the area along the eastern property line, east of Nova View and north of the Extended Detention Basin. Swales between the lots capture the roof drainage and the landscape areas between homes and direct it to the east (backside) of the lots. The runoff is then collected in swales along the backside of the lots and is conveyed directly into a grass lined swale that conveys runoff to the Extended Detention Basin down a riprap rundown/ rock chute into a forebay (Design Point 1). Additionally, this area comprises of the areas uphill of the proposed big block retaining walls. Runoff not captured from the off-site Sub-Basins is captured in a swale on top of the retaining walls and is conveyed towards the Extended Detention Basin down a riprap rundown/ rock chute into a forebay. Developed runoff during the 5-year and 100-year events are 2.08 cfs and 7.19 cfs respectively.

### **Sub-Basin B**

Sub-basin B consists of approximately 1.85 acres and is made up of a majority of the Solum Grove runoff and the lots adjacent to Solum Grove. The lots on the south side of Tenebris Point are also included within this sub-basin. This Sub-Basin is the only Sub-Basin contributing to the Rain Garden. Swales between the lots capture the roof drainage and the landscape areas between homes and is conveyed in the curb and gutter to a curb chase (Design Point 2) in the southwest corner of the Site, directly entering the proposed Rain Garden. The remaining runoff from the lots drain into the Solum Grove and is also conveyed in the curb and gutter to a curb chase in the southwest corner of the Site, directly entering the proposed Rain Garden. Developed runoff during the 5-year and 100-year events are 4.04 cfs and 8.86 cfs respectively. Portions of the 100-year flow outfalls via the overland path following Solum Grove as it curves to the northwest. During the 100-year storm, ponding will occur at the curb chase and will spill over the emergency access at the end of Solum Grove and onto Meadowbrook Parkway. These flows will not flow onto the public sidewalk.

### **Sub-Basin C**

Sub-basin C consists of approximately 0.71 acres and consists of driveway and lawn runoff from nine lots and the west portion of Nova View between Spatium View and Tenebris Point. The runoff from the lots drains into Nova View and Tenebris Point, respectively, and is conveyed in the curb and gutter before being collected a private 5-foot curb Type R inlet (Design Point 3) and conveyed through 18" RCP Storm pipe. Developed runoff during the 5-year and 100-year events are 2.42 cfs and 4.76 cfs respectively.

### **Sub-Basin D**

Sub-basin D consists of approximately 0.37 acres and consists of runoff from the tract north of the Tenebris Point lots. To prevent the runoff from the Tract from draining out towards Meadowbrook Parkway, a swale will collect runoff along the west property line and convey to an area inlet (Design Point 4). This area inlet will connect to 10" PVC Storm pipe and travel down Tenebris Point before joining the runoff from Sub-Basin C. Developed runoff during the 5-year and 100-year events are 0.21 cfs and 1.20 cfs respectively.



### **Sub-Basin E**

Sub-basin E consists of approximately 0.42 acres and consists of the eastern half of the Nova View from Tenebris Point to Lux Point and the adjacent driveway sections. The runoff flows along Nova View and is conveyed in the curb and gutter before being collected by an 8-foot Type D-10-R inlet (Design Point 5). Developed runoff during the 5-year and 100-year events are 1.38 cfs and 2.70 cfs respectively. Additionally, 0.1 cfs of by-pass flows from Sub-Basin J (Design Point 10) are captured and conveyed to the storm sewer system and detention pond.

### **Sub-Basin F**

Sub-basin F consists of approximately 0.10 acres and consists of the southern half of Spatium View. The runoff from Spatium View and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 6). Developed runoff during the 5-year and 100-year events are 0.44 cfs and 0.80 cfs respectively.

### **Sub-Basin G**

Sub-basin G consists of approximately 0.92 acres and consists of the northern half of Spatium View, the adjacent tract, and the western half of Nova View from Spatium View to Lux Point. Swales between the lots capture the roof drainage and the landscape areas between homes and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 7). The remaining runoff from the lots and driveways drain into Spatium View and Nova View and is conveyed in the curb and gutter before being collected by the 5-foot curb Type R inlet. To prevent the runoff from the Tract to drain out towards Meadowbrook Parkway, a swale will collect runoff along the west property line and convey to a small area inlet. This area inlet will connect to the 5' Type R inlet withing Spatium View (Design Point 7). Developed runoff during the 5-year and 100-year events are 1.72 cfs and 4.02 cfs respectively.

### **Sub-Basin H**

Sub-basin H consists of approximately 0.83 acres and consists of Lux Point and the adjacent driveways to the west and entire lots to the east. The runoff from the lots drains into Lux Point and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 8). Developed runoff during the 5-year and 100-year events are 1.66 cfs and 3.85 cfs respectively. Additionally, 0.2 cfs of by-pass flows from Sub-Basin I (Design Point 9) are captured and conveyed to the storm sewer system and detention pond.

### **Sub-Basin I**

Sub-basin I consists of approximately 0.28 acres and consists of the western half of Nova view north of Lux Point. It also included the driveways directly adjacent to the west. The runoff from the driveways drains into Nova View and is conveyed in the curb and gutter and collected by a 5-foot curb Type R inlet (Design Point 9). Developed runoff during the 5-year and 100-year events are 0.82 cfs and 1.73 cfs respectively. In the 100-year storm, 0.2 cfs of flow will overtop the basin and flow down Lux Point and into Sub-Basin H. These overtopping flows will be captured at Design Point 8 and are included as by-pass flows in the inlet capacity calculations in the appendix of this report.

### **Sub-Basin J**

Sub-basin J consists of approximately 0.23 acres and consists of the eastern half of Nova View north of Lux Point. It also included the driveways directly adjacent to the east. The runoff from the driveways drains into Nova View and is conveyed in the curb and gutter and is collected by a 5-foot curb Type R inlet (Design Point 10). Developed runoff during the 5-year and 100-year events are 0.77 cfs and 1.54 cfs respectively. In the 100-year storm, 0.1 cfs of flow will overtop the sub-basin and flow down Nova View into Sub-Basin E. These overtopping flows will be captured at Design Point 5 and are included as by-pass flows in the inlet capacity calculations in the appendix of this report.

### **Sub-Basin OS-A**

Sub-basin OS-A consists of approximately 1.77 acres and consists of the eastern half of US 24 (both travel lanes, shoulder and Right of Way) upstream and north of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin is conveyed in an already existing roadside ditch that converges with the outfall of the CMP culvert at Design Point 11. From Design Point 11 the flows will be routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 30" RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.76 cfs and 8.14 cfs respectively.

### **Sub-Basin OS-B**

Sub-basin OS-B consists of approximately 1.34 acres and consists of the eastern half of US 24 (both travel lanes, shoulder and Right of Way) downstream and south of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin be captured and routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 30" RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.01 cfs and 6.73 cfs respectively.

### **Sub-Basin OS-C**

Sub-basin OS-C consists of approximately 2.10 acres and consists of the western half of US 24 (both travel lanes and vegetated median) upstream and north of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin is collected in the already existing swale within the roadway median and is conveyed through the 30" CMP culvert to Design Point 11. From Design Point 11 the flows will be routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 30" RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.92 cfs and 8.67 cfs respectively.

### ***EMERGENCY OVERFLOW ROUTING***

Emergency overflow routing consists of flows following the proposed drainage pattern of northeast to southwest along the proposed roadways. Once the flows reach the southwest portion of the site, they will flow through the access driveway to Meadowbrook Parkway for Lot 1 24/94 Business Park Filing No. 1.



## **DETENTION AND WATER QUALITY**

The WQCV and 100-year detention is required for this Project. This is accomplished through the proposed private Full Spectrum Extended Detention Basin on the southeast corner of the Site and a private Rain Garden on the southwest corner of the Site. The Extended Detention Basin was sized to provide detention for the entire Site (Sub-Basins A-J) per UDFCD criteria. WQCV will be provided in the Extended Detention Basin for Sub-Basins A, C-J only. WQCV for Sub-Basin B will be provided by the Rain Garden. The water quality and detention calculations are provided in the Appendix of this report. The proposed Extended Detention Basin and Rain Garden will be maintained by the Meadowbrook Park HOA.

### **Four-Step Process**

The four-step process per the MANUAL provides guidance and requirements for the selection of siting of structural Construction Control Measures (CCMs) for new development and significant redevelopment.

#### **Step 1: Employ Runoff Reduction Practices**

Currently the site is vacant undeveloped land with surrounding development. Development of the site will increase current runoff conditions due to increased imperviousness values. However, implementation of landscaping throughout the site, the proposed storm sewer infrastructure, and the proposed Extended Detention Basin will help slow runoff and encourage infiltration.

#### **Step 2: Provide Water Quality Capture Volume (WQCV)**

The water quality capture volume will be detained using Full Spectrum Extended Detention Basin on the southeast corner of the Site and a Rain Garden on the southwest corner of the Site. The outfall pipes from the water quality outlet structures will control the release of stormwater to less than historic rates.

#### **Step 3: Stabilize Drainageways**

There are no current drainageways conveyed through this property. No improvements to stabilize drainageways are a part of this Project.

#### **Step 4: Consider need for Industrial and Commercial BMPs**

Erosion control features for the final stages of the Project will be designed to reduce contamination. Source control BMPs will include the use of, inlet protection, silt fences, concrete washout areas, stockpile management, and stabilized staging areas. The Grading and Erosion Control Plans will be submitted as a separate construction document set.

### **Detention and Water Quality Design**

The proposed private Full Spectrum Extended Detention Basin is designed with an outlet structure that is fitted with an orifice plate and restrictor plate to release the WQCV in a 40-hour time period per the MANUAL. The proposed private Rain Garden is designed with an outlet structure that is fitted with a restrictor plate to release the WQCV in a 12-hour time period per the MANUAL.

Calculations included in the Appendix provide details regarding the private water quality and detention basins design. The calculations include determination of the storage volumes required for full spectrum detention for the WQCV and 100 year detention and allowable release rates.

Overall, 0.101 acre-feet of WQCV is required for Sub-Basins A, C-J, and 0.648 acre-feet of detention volume is required for the proposed Extended Detention Basin (Sub-Basins A-J). The total area contributing to the Extended Detention Basin consists of 8.17 acres (43.2% imperviousness). The outlet structure and orifice releases approximately 0.1 cfs in the 5-year event and 5.5 cfs in the 100-year event. This is less than the historic flows of 2.49 cfs in the 5-year event and 16.70 cfs in the 100-year event.

The WQCV requirement for Sub-Basin B (1.85 acres and 54.5% imperviousness), is 1,176 cubic feet and is provided by a Rain Garden with this a 1,215 Square Foot bottom and 12" WQCV depth. See the Appendix for calculations.

### **Outlet Requirements**

The water quality standards established by the CRITERIA are met by the proposed Full Spectrum Extended Detention Basin and Rain Garden. The water quality outlet structures were designed per the specifications in the CRITERIA. The outlet structure for the Extended Detention Basin meets the micro-pool requirement that it be integrated into the design of the structure with an additional initial surcharge volume. The orifice plates of the structures were designed based on the CRITERIA. The orifice plates will allow the WQCV to be drained from the structure in 40 hours for the Extended Detention Basin and 12 hours for the Rain Garden. The calculations for the design of the outlet structures are presented in the Appendix.

### **Channel Design and Soil Erodibility**

A proposed concrete lined trickle channel within the basin was designed per the MANUAL. A forebay structure is located at both upstream entrances to the Extended Detention Base. The forebay structures were designed per the MANUAL. The surrounding protection is designed as Type L riprap. Calculations detailing the design and dimensions of the trickle channel and forebay structure are included in the Appendix. Additionally, a riprap rundown or rock chute is provided to stabilize the flows coming from swales and entering the Extended Detention Basin. Calculations for the rock chute are included in the Appendix.

### **Emergency Spillway Path**

The emergency overflow from the Extended Detention Basin and Rain Garden are both designed to spill over the sidewalk and curb and gutter into Solum Grove and run west towards the access to Lot 1 24/94 Business Park Filing No. 1. Flows in the 100-yr storm will overtop the curb in certain areas, with depth of flow remaining less than 12", consistent with Table 6-1 "Allowable Use of Roads and Streets" for a Type A Local Road. Further calculations are provided in the Appendix.

## **COST OF PROPOSED DRAINAGE FACILITIES**

An Opinion of Probable Construction Cost (OPCC) is provided in the Appendix of the report. There are no public drainage facilities. All improvements with this Project will be private.

## **DRAINAGE AND BRIDGE FEES**

The Site is located in the Sand Creek Drainage Basin. The total acreage of three parcels (5408403001, 5408000053 and 5408008002) is 8.01 acres. The site imperviousness is 46.8%. The total drainage and bridge fees due for the Site is \$107,722.50

	<b>2021 Fees (\$ / Impervious acre)</b>	<b>Impervious Area (Acre)</b>	<b>Amount Due (\$)</b>
<b>Drainage Fee</b>	\$20,387	3.75	\$76,451.25
<b>Bridge Fee</b>	\$8,339	3.75	\$31,271.25
<b>Total amount due:</b>			<b>\$107,722.50</b>

## **GRADING AND EROSION CONTROL**

The GEC plans have been submitted to El Paso County Planning and Community Development Department for review and approval prior to construction. The GEC plans are consistent with this drainage report.

## **MAINTENANCE AND OPERATIONS**

Twice per year inspections (spring and fall) of the stormwater detention and water quality structures are recommended. The owner/operator will be responsible for maintenance. A copy of this report will be provided to the owner/operator. This satisfies the EDB Operation and Maintenance (O&M) Manual.

## **OTHER GOVERNMENT AGENCY REQUIREMENTS**

Approval from other agencies such as the FEMA, the Army Corps of Engineers, Colorado State Engineer, Colorado Water Conservation Board, and others are not needed with this Project.

## **SUMMARY**

Ultimate outflow from the site occurs at the southwestern corner of the site at Manhole J3. Existing conditions releases 2.49 CFS during the 5-year storm and 16.70 CFS in the 100-year storm for the Site Area (Sub-basins A-J). Under proposed conditions, these flows would be lowered to 0.1 CFS for the 5-year storm and 5.5 CFS in the 100-year storm for the Site Area (Sub-basins A-J). Because flows being released from the site are less than historic pre-development conditions, the existing downstream 36" Reinforced Concrete Pipe and associated stormwater infrastructure will be sufficient under proposed conditions.

## **COMPLIANCE WITH STANDARDS**

The drainage design presented within this report for Meadowbrook Park, conforms to the El Paso County Drainage Criteria Manual and the Mile High Flood District Urban Storm Drainage Criteria Manual. Additionally, the Site runoff and storm drain facilities will not adversely affect the downstream and surrounding developments. The proposed developed flows entering the Extended Detention Basin and are greater than the existing ultimate outfall of the site due to the greater imperviousness of the site, however the implementation of the drainage basins will disperse the flow over an extended period of time therefore releasing at equal to or less than the historic rate.

## REFERENCES

1. City of Colorado Springs Drainage Criteria Manual, May 2014.
2. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994.
3. Mile High Flood District Drainage Criteria Manual (MHFDCM), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0459G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).

## APPENDIX

***SOILS MAP AND FEMA FIRM PANEL***



## NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only to landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NIMS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

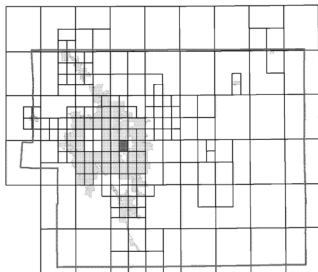
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfp>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

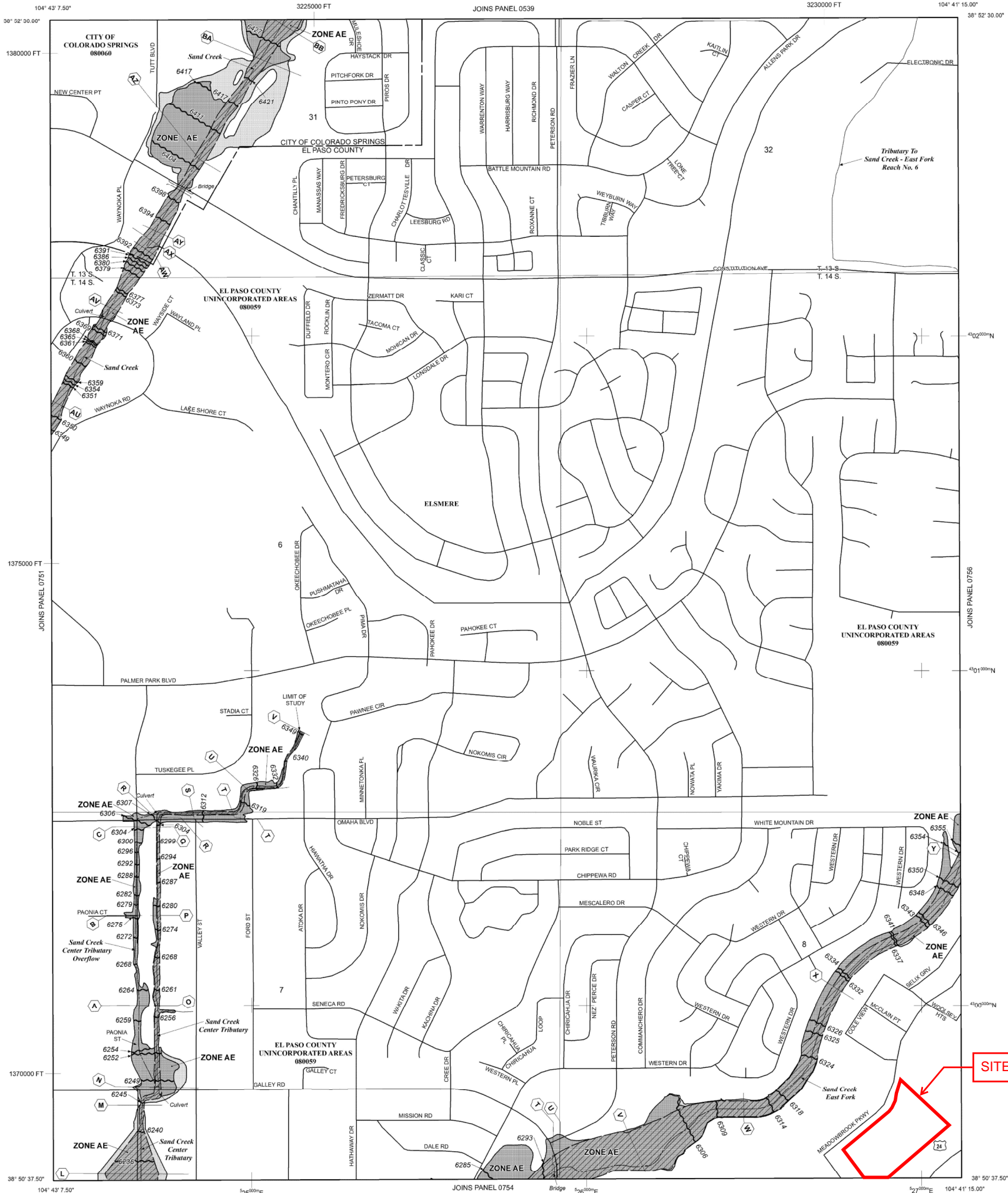
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 13 SOUTH, RANGE 65 WEST, AND TOWNSHIP 14 SOUTH, RANGE 65 WEST.

## LEGEND

**SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area primarily protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**

**ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.

**ZONE D** Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities

Base Flood Elevation line and value; elevation in feet\*

Base Flood Elevation value where uniform within zone; elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

Transect line

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, zone 13

5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPS ZONE 0502), Lambert Conformal Conic Projection

Bench mark (see explanation in Notes to Users section of this FIRM panel)

River Mile

Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'

250 0 500 1000 FEET

150 0 150 300 METERS



PANEL 0752G

**FIRM**

FLOOD INSURANCE RATE MAP

EL PASO COUNTY,

COLORADO

AND INCORPORATED AREAS

PANEL 752 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY NUMBER PANEL SUFFIX

COLORADO SPRINGS, CITY OF 080060 0752 G

EL PASO COUNTY 080059 0752 G

Notice: This map was released on 06/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details.

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

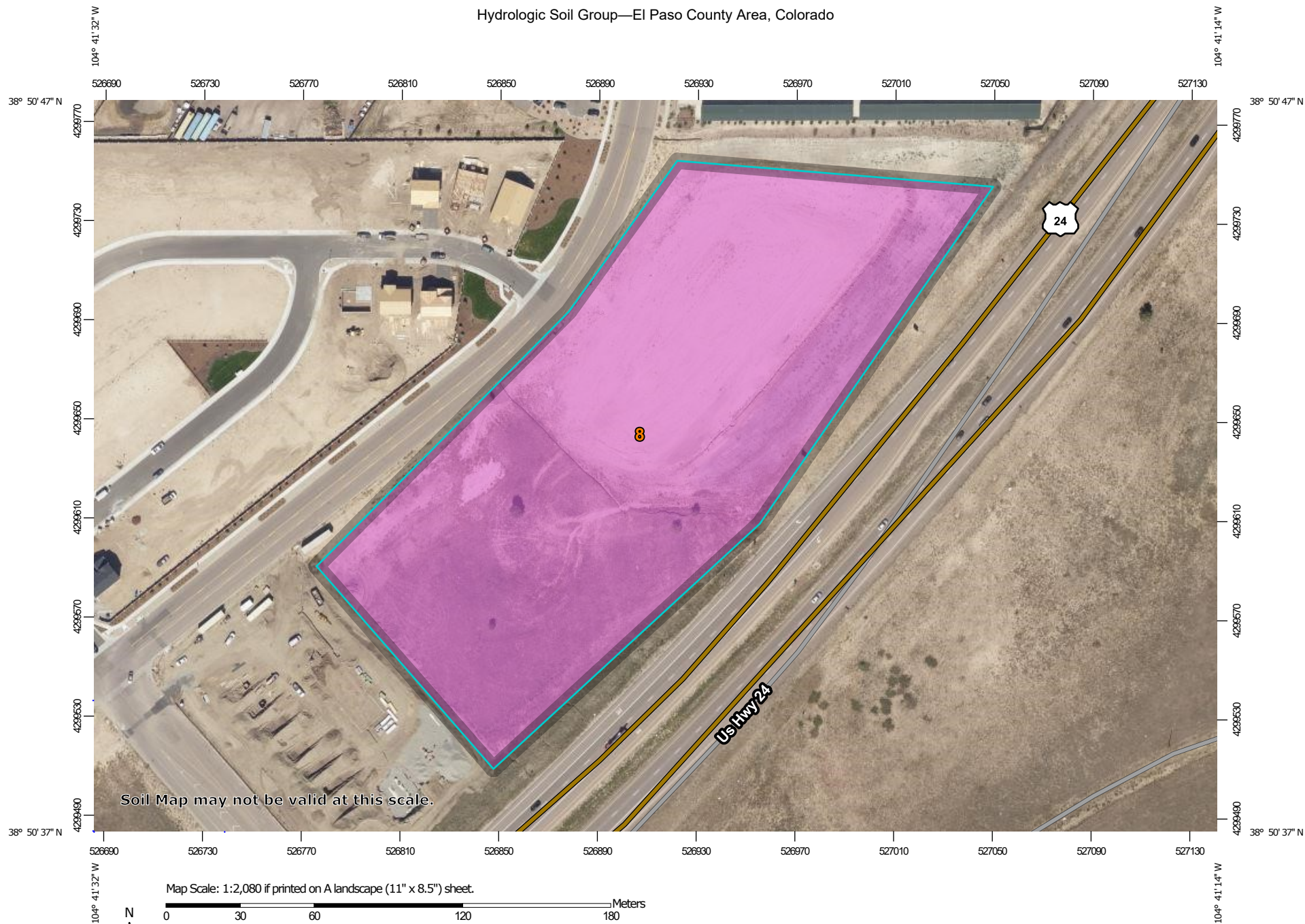
MAP NUMBER 08041C0752G

MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency



# Hydrologic Soil Group—El Paso County Area, Colorado





## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points

 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available

### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	7.4	100.0%
<b>Totals for Area of Interest</b>			<b>7.4</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

***EXISTING HYDROLOGIC CALCULATIONS***

**Meadowbrook  
Drainage Report  
El Paso County, CO**

3/21/2022  
Calculated by: GMP

IDF Equations:

$$I_{100} = -2.52\ln(D) + 12.735$$

$$I_{50} = -2.25\ln(D) + 11.375$$

$$I_{25} = -2.00\ln(D) + 10.111$$

$$I_{10} = -1.75\ln(D) + 8.847$$

$$I_5 = -1.50\ln(D) + 7.583$$

$$I_2 = -1.19\ln(D) + 6.035$$

Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

$$P_1 = \begin{matrix} & \frac{2\text{-yr}}{1.19} & \frac{5\text{-yr}}{1.5} & \frac{10\text{-yr}}{1.75} & \frac{100\text{-yr}}{2.52} \end{matrix}$$

Time Intensity Frequency Tabulation

Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

\*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Weighted Imperviousness Calculations (Existing Conditions)

SUB-BASIN	AREA (SF)	AREA (Acres)	ROOF AREA	ROOF IMPERVIOUSNESS	ROOF				LANDSCAPE AREA	LANDSCAPE IMPERVIOUSNESS	LANDSCAPE				PAVEMENT AREA	PAVEMENT IMPERVIOUSNESS	PAVEMENT				WEIGHTED IMPERVIOUSNESS	WEIGHTED COEFFICIENTS			
					C2	C5	C10	C100			C2	C5	C10	C100			C2	C5	C10	C100		C2	C5	C10	C100
EX-A	356,327	8.18	0	90%	0.71	0.73	0.75	0.81	356,327	2%	0.03	0.09	0.17	0.36	0	100%	0.89	0.90	0.92	0.96	2.0%	0.03	0.09	0.17	0.36
EX-B	58,532	1.34	0	90%	0.71	0.73	0.75	0.81	29,227	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	51.1%	0.46	0.50	0.55	0.66
EX-C	168,766	3.87	0	90%	0.71	0.73	0.75	0.81	79,173	2%	0.03	0.09	0.17	0.36	89,593	100%	0.89	0.90	0.92	0.96	54.0%	0.49	0.52	0.57	0.68
TOTAL	583,625	13.39	0	90%	0.71	0.73	0.75	0.81	385,554	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	6.3%	0.06	0.10	0.16	0.29

**Meadowbrook  
Drainage Report  
El Paso County, CO**

3/21/2022  
Calculated by: GMP

<b>Meadowbrook Park - Drainage Report</b> <b>Existing Runoff Calculations</b> <b>Time of Concentration</b>																
					Watercourse Coefficient											
					Forest & Meadow		2.50	Short Grass Pasture & Lawns		7.00	Grassed Waterway		15.00			
					Fallow or Cultivation		5.00	Nearly Bare Ground		10.00	Paved Area & Shallow Gutter		20.00			
DESIGN POINT	SUB-BASIN DATA				INITIAL / OVERLAND TIME			TRAVEL TIME T(t)				T(c) CHECK (URBANIZED BASINS)				FINAL T(c)
	DRAIN BASIN	AREA sq. ft.	AREA ac.	C(5)	Length ft.	Slope %	T(i) min	Length ft.	Slope %	Coeff.	Velocity fps	T(t) min.	COMP. T(c)	TOTAL LENGTH	L/180+10	min.
1	EX-A	356,327	8.18	0.09	300	11.5%	14.2	867	2.0%	15.00	2.1	6.8	21.0	1167	16.5	16.5
2	EX-B	58,532	1.34	0.50	65	4.5%	5.4	405	3.8%	15.00	2.9	2.3	7.7	470	12.6	7.7
3	EX-C	168,766	3.87	0.52	65	4.5%	5.2	1000	2.5%	15.00	2.4	7.0	12.2	1065	15.9	12.2

Meadowbrook Park - Drainage Report												
Existing Runoff Calculations				Design Storm 5 Year								
(Rational Method Procedure)												
Basin Information				Direct Runoff				Cumulative Runoff				Notes
Design Point	Drain Basin	Area ac.	Runoff Coeff	T(c) min	C x A	I in/hr	Q cfs	T(c) min	C x A	I in/hr	Q cfs	
1	EX-A	8.18	0.09	16.5	0.74	3.38	2.49					Existing On-Site Property (Vacant Undeveloped Land)
2	EX-B	1.34	0.50	7.7	0.67	4.52	3.01					Flows from CDOT ROW, sheet flowing onto property
3	EX-C	3.87	0.52	12.2	2.01	3.83	7.71					Flows from CDOT ROW at the culvert outlet design point



Meadowbrook Park - Drainage Report												
Existing Runoff Calculations				Design Storm 100 Year								
(Rational Method Procedure)												
BASIN INFORMATION				DIRECT RUNOFF				CUMULATIVE RUNOFF				NOTES
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	C x A	I in/hr	Q cfs	T(c) min	C x A	I in/hr	Q cfs	
1	EX-A	8.18	0.36	16.5	2.94	5.67	16.70					Existing On-Site Property (Vacant Undeveloped Land)
2	EX-B	1.34	0.66	7.7	0.89	7.59	6.73					Flows from CDOT ROW, sheet flowing onto property
3	EX-C	3.87	0.68	12.2	2.63	6.43	16.89					Flows from CDOT ROW at the culvert outlet design point

**Meadowbrook  
Drainage Report  
El Paso County, CO**

3/21/2022  
Calculated by: GMP

SUMMARY - EXISTING RUNOFF TABLE						
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100-YR RUNOFF (CFS)
1	EX-A	8.18	2.49	16.70		
2	EX-B	1.34	3.01	6.73		
3	EX-C	3.87	7.71	16.89		
TOTAL		13.39	13.21	40.32		

***PROPOSED HYDROLOGIC CALCULATIONS***

IDF Equations:

$$I_{100} = -2.52\ln(D) + 12.735$$

$$I_{50} = -2.25\ln(D) + 11.375$$

$$I_{25} = -2.00\ln(D) + 10.111$$

$$I_{10} = -1.75\ln(D) + 8.847$$

$$I_5 = -1.50\ln(D) + 7.583$$

$$I_2 = -1.19\ln(D) + 6.035$$

Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P <sub>1</sub> =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulation

Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

\*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Weighted Imperviousness Calculations

SUB-BASIN	AREA (SF)	AREA (Acres)	ROOF AREA	ROOF IMPERVIOUSNESS	ROOF				LANDSCAPE AREA	LANDSCAPE IMPERVIOUSNESS	LANDSCAPE				PAVEMENT AREA	PAVEMENT IMPERVIOUSNESS	PAVEMENT				WEIGHTED IMPERVIOUSNESS	WEIGHTED COEFFICIENTS			
					C2	C5	C10	C100			C2	C5	C10	C100			C2	C5	C10	C100		C2	C5	C10	C100
A	107,496	2.47	21,654	90%	0.71	0.73	0.75	0.81	85,842	0%	0.03	0.09	0.17	0.36	0	100%	0.89	0.90	0.92	0.96	18.1%	0.17	0.22	0.29	0.45
B	80,559	1.85	22,073	90%	0.71	0.73	0.75	0.81	34,457	0%	0.03	0.09	0.17	0.36	24,029	100%	0.89	0.90	0.92	0.96	54.5%	0.47	0.51	0.55	0.66
C	31,005	0.71	10,509	90%	0.71	0.73	0.75	0.81	6,970	0%	0.03	0.09	0.17	0.36	13,526	100%	0.89	0.90	0.92	0.96	74.1%	0.64	0.66	0.69	0.77
D	15,986	0.37	0	90%	0.71	0.73	0.75	0.81	15,554	0%	0.03	0.09	0.17	0.36	432	100%	0.89	0.90	0.92	0.96	2.7%	0.05	0.11	0.19	0.38
E	18,246	0.42	0	90%	0.71	0.73	0.75	0.81	4,546	0%	0.03	0.09	0.17	0.36	13,700	100%	0.89	0.90	0.92	0.96	75.1%	0.68	0.70	0.73	0.81
F	4,229	0.10	0	90%	0.71	0.73	0.75	0.81	79	0%	0.03	0.09	0.17	0.36	4,150	100%	0.89	0.90	0.92	0.96	98.1%	0.87	0.88	0.91	0.95
G	40,228	0.92	8,808	90%	0.71	0.73	0.75	0.81	20,973	0%	0.03	0.09	0.17	0.36	10,447	100%	0.89	0.90	0.92	0.96	45.7%	0.40	0.44	0.49	0.61
H	35,948	0.83	6,289	90%	0.71	0.73	0.75	0.81	18,616	0%	0.03	0.09	0.17	0.36	11,043	100%	0.89	0.90	0.92	0.96	46.5%	0.41	0.45	0.50	0.62
I	12,368	0.28	0	90%	0.71	0.73	0.75	0.81	5,168	0%	0.03	0.09	0.17	0.36	7,200	100%	0.89	0.90	0.92	0.96	58.2%	0.53	0.56	0.61	0.71
J	9,994	0.23	0	90%	0.71	0.73	0.75	0.81	3,127	0%	0.03	0.09	0.17	0.36	6,867	100%	0.89	0.90	0.92	0.96	68.7%	0.62	0.65	0.69	0.77
OS-A	77,099	1.77	0	90%	0.71	0.73	0.75	0.81	34,833	2%	0.03	0.09	0.17	0.36	42,266	100%	0.89	0.90	0.92	0.96	55.7%	0.50	0.53	0.58	0.69
OS-B	58,532	1.34	0	90%	0.71	0.73	0.75	0.81	29,227	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	51.1%	0.46	0.50	0.55	0.66
OS-C	91,667	2.10	0	90%	0.71	0.73	0.75	0.81	44,340	2%	0.03	0.09	0.17	0.36	47,327	100%	0.89	0.90	0.92	0.96	52.6%	0.47	0.51	0.56	0.67
TOTAL (A-J)	356,059	8.17	69,333	90%	0.71	0.73	0.75	0.81	195,332	0%	0.03	0.09	0.17	0.36	91,394	100%	0.89	0.90	0.92	0.96	43.2%	0.38	0.42	0.48	0.60
TOTAL	583,357	13.39	69333	90%	0.71	0.73	0.75	0.81	303,731	0%	0.03	0.09	0.17	0.36	210,292	100%	0.89	0.90	0.92	0.96	46.7%	0.42	0.46	0.51	0.63

**Meadowbrook Park  
Drainage Report  
El Paso County, CO**

3/21/2022  
Calculated by: GMP

Meadowbrook Park - Drainage Report																
Proposed Runoff Calculations																
Time of Concentration																
Watercourse Coefficient																
Forest & Meadow 2.50 Short Grass Pasture & Lawns 7.00 Grassed Waterway 15.00																
Fallow or Cultivation 5.00 Nearly Bare Ground 10.00 Paved Area & Shallow Gutter 20.00																
DESIGN POINT	SUB-BASIN DATA				INITIAL / OVERLAND TIME			TRAVEL TIME T(t)					T(c) CHECK (URBANIZED BASINS)			FINAL T(c) min.
	DRAIN BASIN	AREA sq. ft.	AREA ac.	C(5)	Length ft.	Slope %	T(l) min	Length ft.	Slope %	Coeff.	Velocity fps	T(t) min.	COMP. T(c)	TOTAL LENGTH	L/180+10	
1	A	107,496	2.47	0.22	100	15.0%	6.5	745	2.3%	15.00	2.3	5.5	12.0	845	14.7	12.0
2	B	80,559	1.85	0.51	90	2.9%	7.2	200	1.0%	20.00	2.0	1.7	8.9	290	11.6	8.9
3	C	31,005	0.71	0.66	30	1.3%	4.0	225	3.0%	20.00	3.5	1.1	5.1	255	11.4	5.1
4	D	15,986	0.37	0.11	0	0.0%	0.0	250	0.5%	15.00	1.1	3.9	5.0	250	11.4	5.0
5	E	18,246	0.42	0.70	70	2.8%	4.4	420	2.3%	20.00	3.0	2.3	6.7	490	12.7	6.7
6	F	4,229	0.10	0.88	6	2.0%	0.8	150	2.0%	20.00	2.8	0.9	5.0	156	10.9	5.0
7	G	40,228	0.92	0.44	100	3.0%	8.4	170	2.0%	20.00	2.8	1.0	9.4	270	11.5	9.4
8	H	35,948	0.83	0.45	100	8.5%	5.8	190	0.5%	20.00	1.4	2.2	8.0	290	11.6	8.0
9	I	12,368	0.28	0.56	100	10.0%	4.6	109	2.7%	20.00	3.3	0.6	5.2	209	11.2	5.2
10	J	9,994	0.23	0.65	70	5.5%	3.9	160	2.8%	20.00	3.3	0.8	5.0	230	11.3	5.0
11	OS-A	77,099	1.77	0.53	100	4.3%	6.4	665	2.5%	15.00	2.4	4.7	11.1	765	14.3	11.1
12	OS-B	58,532	1.34	0.50	65	4.5%	5.4	405	3.8%	15.00	2.9	2.3	7.7	470	12.6	7.7
13	OS-C	91,667	2.10	0.51	65	4.5%	5.3	1035	1.9%	15.00	2.1	8.3	13.6	1100	16.1	13.6

Meadowbrook Park - Drainage Report												
Proposed Runoff Calculations												
(Rational Method Procedure)												
BASIN INFORMATION				DIRECT RUNOFF				CUMULATIVE RUNOFF				NOTES
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	C x A	I in/hr	Q cfs	T(c) min	C x A	I in/hr	Q cfs	
1	A	2.47	0.22	12.0	0.54	3.85	2.08					
2	B	1.85	0.51	8.9	0.94	4.31	4.04					
3	C	0.71	0.66	5.1	0.47	5.14	2.42					
4	D	0.37	0.11	5.0	0.04	5.17	0.21					
5	E	0.42	0.70	6.7	0.29	4.73	1.38					
6	F	0.10	0.88	5.0	0.09	5.17	0.44					
7	G	0.92	0.44	9.4	0.41	4.22	1.72					
8	H	0.83	0.45	8.0	0.37	4.46	1.66					
9	I	0.28	0.56	5.2	0.16	5.12	0.82					
10	J	0.23	0.65	5.0	0.15	5.17	0.77					
11	OS-A	1.77	0.53	11.1	0.95	3.98	3.76					
12	OS-B	1.34	0.50	7.7	0.67	4.52	3.01					
13	OS-C	2.10	0.51	13.6	1.07	3.66	3.92					

<b>Meadowbrook Park - Drainage Report</b> <b>Proposed Runoff Calculations</b> <i>(Rational Method Procedure)</i>												
BASIN INFORMATION				DIRECT RUNOFF				CUMULATIVE RUNOFF				NOTES
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	C x A	I in/hr	Q cfs	T(c) min	C x A	I in/hr	Q cfs	
1	A	2.47	0.45	12.0	1.11	6.47	7.19					
2	B	1.85	0.66	8.9	1.22	7.24	8.86					
3	C	0.71	0.77	5.1	0.55	8.64	4.76					
4	D	0.37	0.38	5.0	0.14	8.68	1.20					
5	E	0.42	0.81	6.7	0.34	7.94	2.70					
6	F	0.10	0.95	5.0	0.09	8.68	0.80					
7	G	0.92	0.61	9.4	0.57	7.09	4.02					
8	H	0.83	0.62	8.0	0.51	7.48	3.85					
9	I	0.28	0.71	5.2	0.20	8.60	1.73					
10	J	0.23	0.77	5.0	0.18	8.68	1.54					
11	OS-A	1.77	0.69	11.1	1.22	6.68	8.14					
12	OS-B	1.34	0.66	7.7	0.89	7.59	6.73					
13	OS-C	2.10	0.67	13.6	1.41	6.15	8.67					



**Meadowbrook Park  
Drainage Report  
El Paso County, CO**

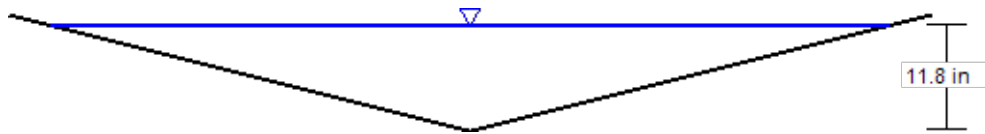
3/21/2022  
Calculated by: GMP

SUMMARY - PROPOSED RUNOFF TABLE						
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100-YR RUNOFF (CFS)
1	A	2.47	2.08	7.19		
2	B	1.85	4.04	8.86		
3	C	0.71	2.42	4.76		
4	D	0.37	0.21	1.20		
5	E	0.42	1.38	2.70		
6	F	0.10	0.44	0.80		
7	G	0.92	1.72	4.02		
8	H	0.83	1.66	3.85		
9	I	0.28	0.82	1.73		
10	J	0.23	0.77	1.54		
11	OS-A	1.77	3.76	8.14		
12	OS-B	1.34	3.01	6.73		
13	OS-C	2.10	3.92	8.67		
14	POND OUTFALL		0.10	5.50		
TOTAL		13.39	26.22	60.19		

## ***HYDRAULIC CALCULATIONS***

## Cross Section for CDOT By Pass Ditch

Project Description	
Friction Method	Manning
	Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.040 ft/ft
Normal Depth	11.8 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	23.54 cfs



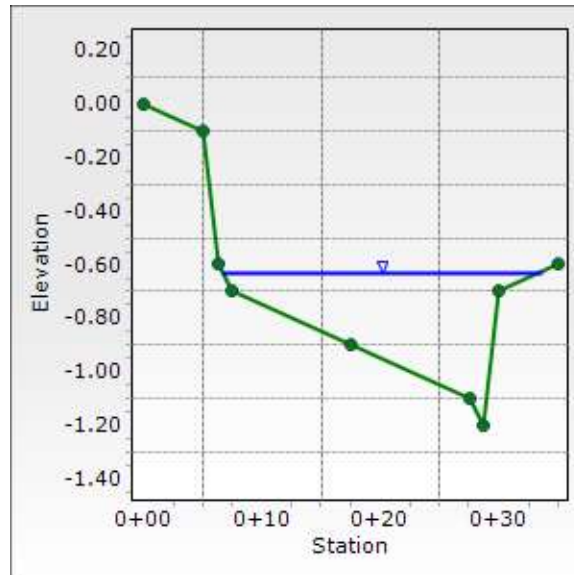
V: 1  
H: 1

## Worksheet for CDOT By Pass Ditch

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.040 ft/ft
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	23.54 cfs
Results	
Normal Depth	11.8 in
Flow Area	3.9 ft <sup>2</sup>
Wetted Perimeter	8.1 ft
Hydraulic Radius	5.7 in
Top Width	7.89 ft
Critical Depth	14.0 in
Critical Slope	0.016 ft/ft
Velocity	6.06 ft/s
Velocity Head	0.57 ft
Specific Energy	1.56 ft
Froude Number	1.521
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	11.8 in
Critical Depth	14.0 in
Channel Slope	0.040 ft/ft
Critical Slope	0.016 ft/ft

## Cross Section for Emergency Overflow Spillway

Project Description	
Friction Method	Manning
Solve For	Formula
	Normal Depth
Input Data	
Channel Slope	0.011 ft/ft
Normal Depth	6.9 in
Discharge	26.79 cfs



## Worksheet for Emergency Overflow Spillway

Project Description	
Friction Method	Manning
Solve For	Formula
	Normal Depth
Input Data	
Channel Slope	0.011 ft/ft
Discharge	26.79 cfs

### Section Definitions

Station (ft)	Elevation (ft)
0+00	0.00
0+05	-0.09
0+06	-0.60
0+08	-0.70
0+18	-0.90
0+28	-1.10
0+29	-1.20
0+30	-0.70
0+35	-0.60

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+05, -0.09)	0.013
(0+05, -0.09)	(0+06, -0.60)	0.013
(0+06, -0.60)	(0+08, -0.70)	0.013
(0+08, -0.70)	(0+18, -0.90)	0.016
(0+18, -0.90)	(0+28, -1.10)	0.016
(0+28, -1.10)	(0+29, -1.20)	0.013
(0+29, -1.20)	(0+30, -0.70)	0.013
(0+30, -0.70)	(0+35, -0.60)	0.013

### Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

### Results

Normal Depth	6.9 in
Roughness Coefficient	0.015
Elevation	-0.63 ft
Elevation Range	-1.2 to 0.0 ft
Flow Area	6.7 ft <sup>2</sup>
Wetted Perimeter	27.2 ft

## Worksheet for Emergency Overflow Spillway

### Results

Hydraulic Radius	3.0 in
Top Width	27.08 ft
Normal Depth	6.9 in
Critical Depth	7.7 in
Critical Slope	0.005 ft/ft
Velocity	4.01 ft/s
Velocity Head	0.25 ft
Specific Energy	0.82 ft
Froude Number	1.422
Flow Type	Supercritical

### GVF Input Data

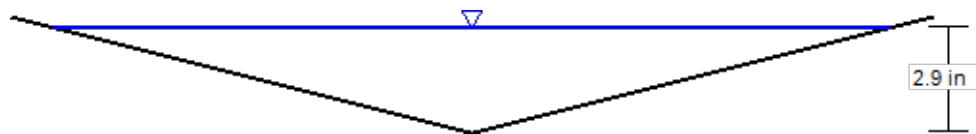
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

### GVF Output Data

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	6.9 in
Critical Depth	7.7 in
Channel Slope	0.011 ft/ft
Critical Slope	0.005 ft/ft

## Cross Section for Meadowbrook Ditch North

Project Description	
Friction Method	Manning
	Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Normal Depth	2.9 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.27 cfs



$\nabla$  V: 1  
 H: 1

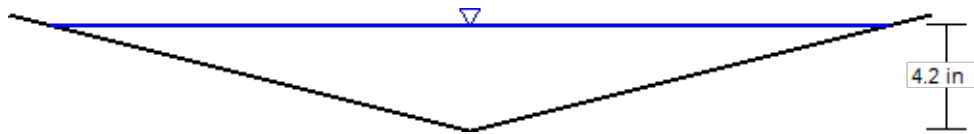


## Worksheet for Meadowbrook Ditch North

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.27 cfs
Results	
Normal Depth	2.9 in
Flow Area	0.2 ft <sup>2</sup>
Wetted Perimeter	2.0 ft
Hydraulic Radius	1.4 in
Top Width	1.91 ft
Critical Depth	2.3 in
Critical Slope	0.030 ft/ft
Velocity	1.18 ft/s
Velocity Head	0.02 ft
Specific Energy	0.26 ft
Froude Number	0.601
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	2.9 in
Critical Depth	2.3 in
Channel Slope	0.010 ft/ft
Critical Slope	0.030 ft/ft

## Cross Section for Meadowbrook Ditch-South

Project Description	
Friction Method	Manning
	Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Normal Depth	4.2 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.73 cfs



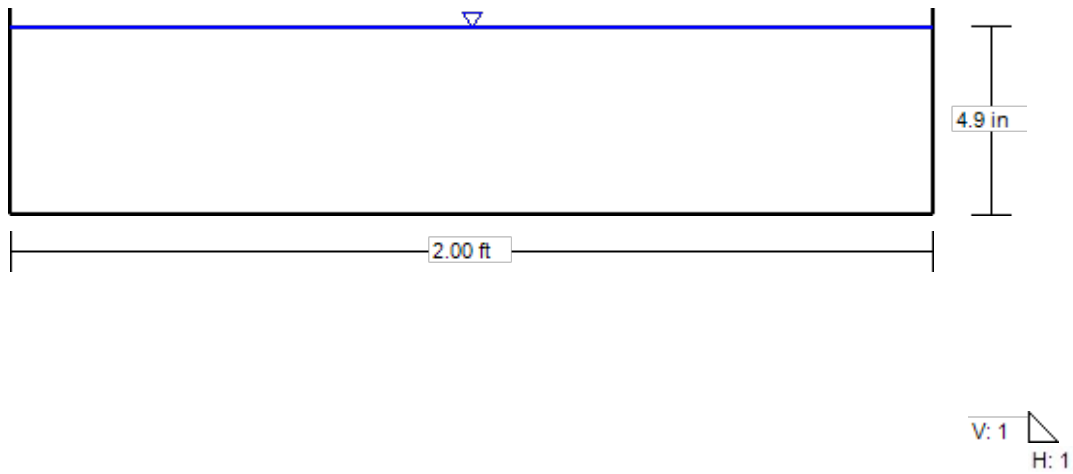
V: 1  
H: 1

## Worksheet for Meadowbrook Ditch-South

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.73 cfs
Results	
Normal Depth	4.2 in
Flow Area	0.5 ft <sup>2</sup>
Wetted Perimeter	2.9 ft
Hydraulic Radius	2.0 in
Top Width	2.78 ft
Critical Depth	3.5 in
Critical Slope	0.026 ft/ft
Velocity	1.51 ft/s
Velocity Head	0.04 ft
Specific Energy	0.38 ft
Froude Number	0.638
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	4.2 in
Critical Depth	3.5 in
Channel Slope	0.010 ft/ft
Critical Slope	0.026 ft/ft

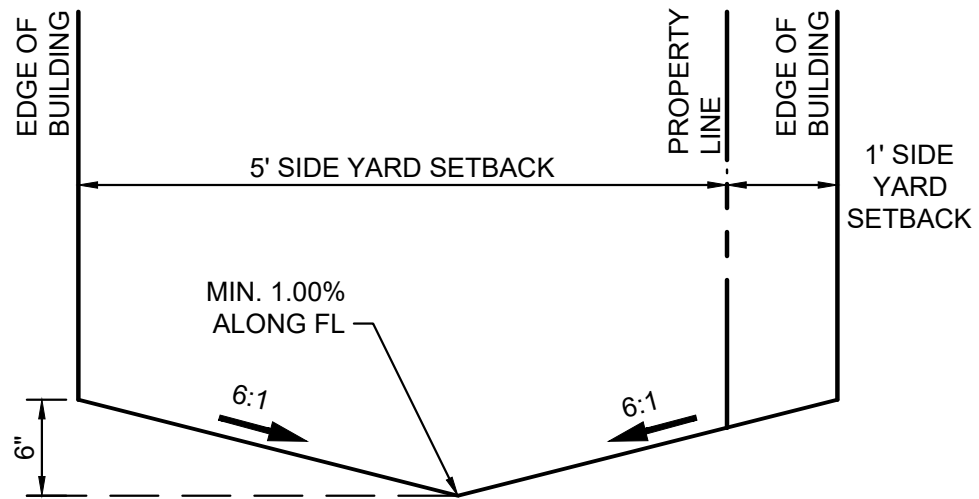
## Cross Section for Rain Garden- Curb Chase

Project Description	
Friction Method	Manning
	Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.010 ft/ft
Normal Depth	4.9 in
Bottom Width	2.00 ft
Discharge	4.04 cfs



## Worksheet for Rain Garden- Curb Chase

Project Description	
Friction Method	Manning
Solve For	Formula
	Normal Depth
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.010 ft/ft
Bottom Width	2.00 ft
Discharge	4.04 cfs
Results	
Normal Depth	4.9 in
Flow Area	0.8 ft <sup>2</sup>
Wetted Perimeter	2.8 ft
Hydraulic Radius	3.5 in
Top Width	2.00 ft
Critical Depth	6.0 in
Critical Slope	0.005 ft/ft
Velocity	4.99 ft/s
Velocity Head	0.39 ft
Specific Energy	0.79 ft
Froude Number	1.382
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	4.9 in
Critical Depth	6.0 in
Channel Slope	0.010 ft/ft
Critical Slope	0.005 ft/ft



PROPOSED SIDE LOT SWALE TYP.  
CROSS SECTION  
NTS

09/30/2021

**Kimley»Horn**

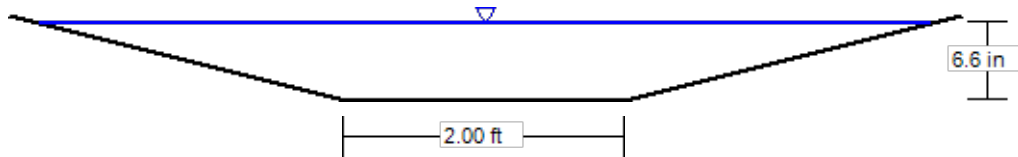
© 2021 KIMLEY-HORN AND ASSOCIATES, INC.  
2 N NEVADA AVE., SUITE 300, COLORADO SPRINGS, 80903  
PHONE: 719-453-0180

## Worksheet for Side Lot Swale - Worst Case

Project Description	
Friction Method	Manning
Solve For	Formula
	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Left Side Slope	6.000 H:V
Right Side Slope	6.000 H:V
Discharge	2.92 cfs
Results	
Normal Depth	6.0 in
Flow Area	1.5 ft <sup>2</sup>
Wetted Perimeter	6.1 ft
Hydraulic Radius	3.0 in
Top Width	6.00 ft
Critical Depth	5.2 in
Critical Slope	0.022 ft/ft
Velocity	1.95 ft/s
Velocity Head	0.06 ft
Specific Energy	0.56 ft
Froude Number	0.686
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	6.0 in
Critical Depth	5.2 in
Channel Slope	0.010 ft/ft
Critical Slope	0.022 ft/ft

## Cross Section for Trapezoidal Channel -Sub-Basin A

Project Description	
Friction Method	Manning
Solve For	Formula
	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.016 ft/ft
Normal Depth	6.6 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Bottom Width	2.00 ft
Discharge	7.19 cfs



V: 1  
H: 1



## Worksheet for Trapezoidal Channel -Sub-Basin A

Project Description	
Friction Method	Manning
	Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.016 ft/ft
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Bottom Width	2.00 ft
Discharge	7.19 cfs
Results	
Normal Depth	6.6 in
Flow Area	2.3 ft <sup>2</sup>
Wetted Perimeter	6.5 ft
Hydraulic Radius	4.2 in
Top Width	6.39 ft
Critical Depth	6.3 in
Critical Slope	0.019 ft/ft
Velocity	3.13 ft/s
Velocity Head	0.15 ft
Specific Energy	0.70 ft
Froude Number	0.919
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	6.6 in
Critical Depth	6.3 in
Channel Slope	0.016 ft/ft
Critical Slope	0.019 ft/ft

Ditches																		
Description	Drainage Area (DA)	Drainage Area (DA)	Runoff Coefficient (C)	Intensity (100-Year)	Flow (Q)	Velocity (V)	Liner	Ditch Shape	Bottom Width	Side Slope (H:V)	Total Depth	Running Slope	Depth of Flow	Manning's Number (n)	Freeboard	Channel Top Width	Ridge Width	Ridge Height
ID	sf	ac		in/hr	cfs	ft/s			ft	x:1	ft	%	ft		ft	ft	ft	ft
1) CDOT By Pass Ditch	226,948	5.21	0.69	8.67	23.54	6.09	Ch-2	Triangular	0	4:1	2.00	4.00	0.98	0.030	1.02	9.0	4	2.00
2) Meadowbrook Ditch North	4,792	0.11	0.35	6.79	0.26	1.20	N/A	Triangular	0	4:1	1.40	1.00	0.23	0.030	1.17	13.2	4	1.40
3) Meabowbrook Ditch South	13,939	0.32	0.35	6.65	0.74	2.75	N/A	Triangular	0	4:1	1.40	1.00	0.26	0.030	1.14	1.9	4	1.40
4) Trapezoidal Channel Sub-basin A	107,593	2.47	0.45	6.47	7.19	3.11	Ch-1	Trapizoidal	2	4:1	2.00	1.60	0.55	0.030	1.45	6.4	4	2.00

SITE DATA	
Location:	Colorado Springs
Frequency:	100-Year
Cover Desc.:	Graded Soil (Sandy 5-10%)
Channel Material:	Bare Soil

Blue = User Entered (Verify they reflect the current design)

Green = Calculated

Channel Lining	
Description	BMP
Bare Soil	N/A
Synthetic Mat	Ch-1
Gravel Riprap	Ch-2
Rock Riprap	Ch-2
Concrete	Ch-3
Asphalt	Ch-3

Mirafi Geosynthetic Textile Fabric, or contractor approved equivalent

Type L Gravel/Cobble Rip-Rap, per Tractive Forces Calculations included with Companion Document 580-10:  
(D50 = 7.5" Req  
Type L RipRap D50 = 9")

# Rock Chute Design - Cut/Paste Plan

(Version WI-Nov. 2017, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998)

Project: Meadowbrook Park  
 Designer: KRK  
 Date: 3/12/2021

County: El Paso County  
 Checked by: \_\_\_\_\_  
 Date: \_\_\_\_\_

## Design Values

$D_{50}$  dia. = 9.0 in.  
 Rock<sub>chute</sub> thickness = 18.0 in.  
 Inlet apron length = 10 ft.  
 Outlet apron length = 15 ft.  
 Radius = 25 ft.  
 Will bedding be used? No

## Rock Gradation Envelope

% Passing	Diameter, in. (weight, lbs.)
$D_{100}$ -----	14 - 18 (174 - 413)
$D_{85}$ -----	12 - 16 (113 - 301)
$D_{50}$ -----	9 - 14 (52 - 174)
$D_{10}$ -----	7 - 12 (26 - 113)

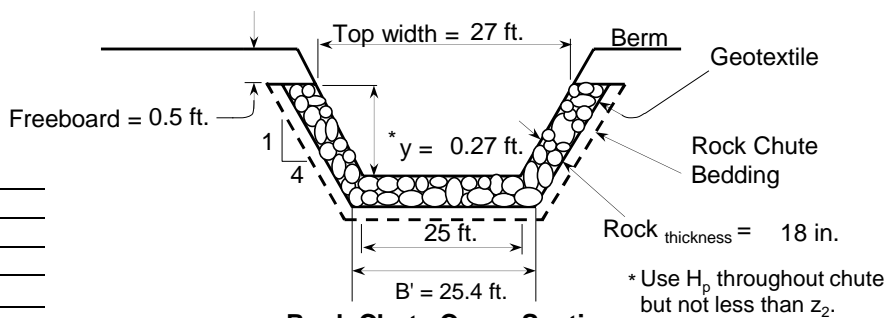
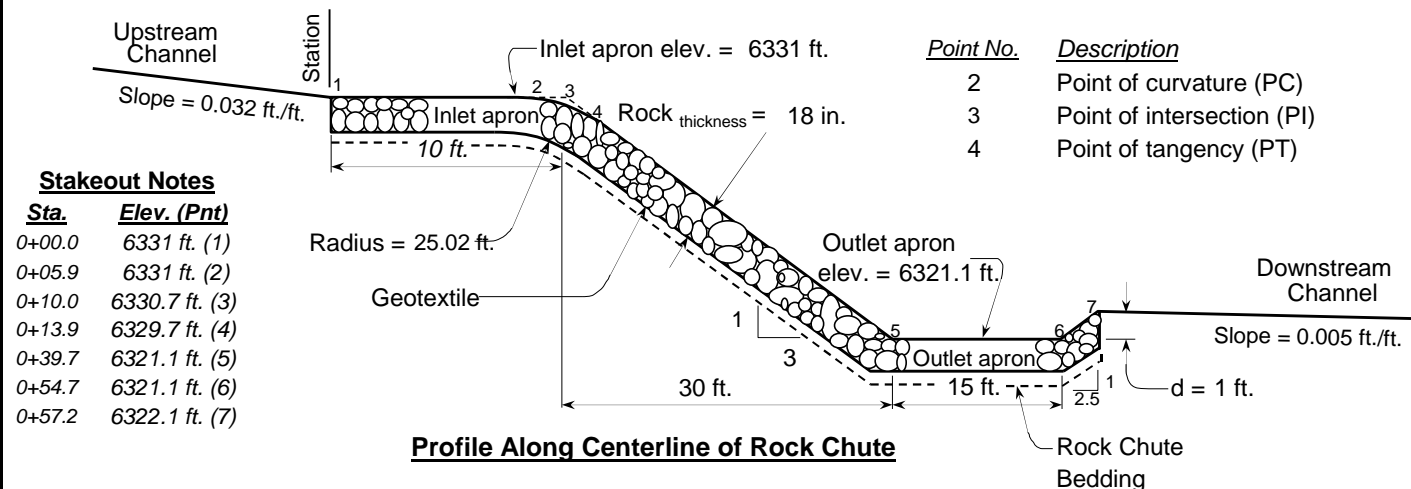
Coefficient of Uniformity,  $(D_{60})/(D_{10}) < 1.7$

## Quantities<sup>a</sup>

Rock = 111 yd<sup>3</sup>  
 Geotextile (WCS-13)<sup>b</sup> = 263 yd<sup>2</sup>  
 Bedding = 0 yd<sup>3</sup>  
 Excavation = 0 yd<sup>3</sup>  
 Earthfill = 0 yd<sup>3</sup>  
 Seeding = 0.0 acres

**Notes:** <sup>a</sup> Rock, bedding, and geotextile quantities are determined from x-section below (neglect radius).

<sup>b</sup> Geotextile Class I (Non-woven) shall be overlapped and anchored (18-in. minimum along sides and 24-in. minimum on the ends) --- quantity not included.



## Profile, Cross Sections, and Quantities



Meadowbrook Park  
 El Paso County

Designed: KRK  
 Drawn: \_\_\_\_\_  
 Checked: \_\_\_\_\_  
 Approved: \_\_\_\_\_

Date: \_\_\_\_\_  
 File Name: \_\_\_\_\_  
 Drawing Name: \_\_\_\_\_  
 Sheet \_\_\_ of \_\_\_

**ALLOWABLE VELOCITY AND MAXIMUM SHEAR STRESS  
Streambank and Shoreland Protection Code 580**

Type of Treatment	Allowable Shear lb/sq ft	Velocity ft/sec
<b>Brush Mattresses<sup>1</sup></b>		
Staked only w/ rock riprap toe (initial)	0.8 - 4.1	5
Staked only w/ rock riprap toe (grown)	4.0 - 8.0	12
<b>Coir Geotextile Roll<sup>2</sup></b>		
Roll with coir rope mesh staked only without rock riprap toe	0.2 - 0.8	< 5
Roll with Polypropylene rope mesh staked only without rock riprap toe	0.8 - 3.0	< 8
Roll with Polypropylene rope mesh staked and with rock riprap toe	3.0 - 4.0	< 12
<b>Live Fascine<sup>3</sup></b>		
LF Bundle w/ rock riprap toe	2.0 - 3.1	8
<b>Soils<sup>4</sup></b>		
Fine colloidal sand	0.02-0.03	1.5
Sandy loam (noncolloidal)	0.03-0.04	1.75
Alluvial silt (noncolloidal)	0.045-0.05	2
Silty loam (noncolloidal)	0.045-0.05	1.75-2.25
Firm loam	0.075	2.5
Fine gravels	0.075	2.5
Stiff clay	0.26	3-4.5
Alluvial silt (colloidal)	0.26	3.75
Graded loam to cobbles	0.38	3.75
Graded silts to cobbles	0.43	4
Shales and hardpan	0.67	6
<b>Gravel/Cobble<sup>4</sup></b>		
1-inch	0.33	2.5-5
2-inch	0.67	3-6
6-inch	2	4-7.5
12-inch	4	5.5-12
<b>Vegetation<sup>4</sup></b>		
Class A turf (ret class)	3.7	6-8
Class B turf (ret class)	2.1	4-7
Class C turf (ret class)	1	3.5
Retardance Class D	0.6	Design of roadside channels HEC-15
Retardance Class E	0.35	
Long native grasses	1.2-1.7	4-6
Short native and bunch grass	0.7-0.95	3-4

(=7.5" REQ.)

TYPE L RIPRAP  
D50 = 9"

Tractive Forces (psf)= 62.4 lb/cf x  
normal depth (ft) x S (ft/ft)- 62.4 x  
(11.8/12) x 0.04 = 2.5 psf

Type of Treatment	Allowable Shear lb/sq ft	Velocity ft/sec
<b>Soil Bioengineering<sup>4</sup></b>		
Wattles	0.2-1.0	3
Reed fascine	0.6-1.25	5
Coir roll	3-5	8
Vegetated coir mat	4-8	9.5
Live brush mattress (initial)	0.4-4.1	4
Live brush mattress (grown)	3.90-8.2	12
Brush layering (initial/grown)	0.4-6.25	12
Live fascine	1.25-3.10	6-8
Live willow stakes	2.10-3.10	3-10
<b>Hard Surfacing<sup>4</sup></b>		
Gabions	10	14-19
Concrete	12.5	>18
<b>Boulder Clusters<sup>5</sup></b>		
Boulder		
Very large (>80-inch diameter)	37.4	25
Large (>40-in diameter)	18.7	19
Medium (>20-inch diameter)	9.3	14
Small (>10-inch diameter)	4.7	10
Cobble		
Large (>5-inch diameter)	2.3	7
Small (>2.5-inch diameter)	1.1	5
Gravel		
Very Course (>1.25-inch diameter)	0.54	3
Course (>.63-inch diameter)	0.25	2.5

<sup>1</sup> Brush mattresses (ERDC TN EMRRP-SR-23): <http://el.erdcd.usace.army.mil/emrrp/pdf/sr23.pdf>.

<sup>2</sup> Coir Geotextile roll (ERDC TN EMRRP-SR-04): <http://el.erdcd.usace.army.mil/emrrp/pdf/sr04.pdf>.

<sup>3</sup> Live Fascine (ERDC TN EMRRP-SR-31): <http://el.erdcd.usace.army.mil/emrrp/pdf/sr31.pdf>.

<sup>4</sup> Stream Restoration Materials (ERDC TN EMRRP-SR-29): <http://el.erdcd.usace.army.mil/emrrp/pdf/sr29.pdf>.

<sup>5</sup> Boulder Clusters (ERDC TN EMRRP-SR-11): <http://el.erdcd.usace.army.mil/emrrp/pdf/sr11.pdf>.

### Additional Sources:

Wisconsin Department of Transportation, Erosion Control - Product Acceptability List (PAL):  
<http://www.dot.wisconsin.gov/library/research/docs/finalreports/tau-finalreports/erosion.pdf>

Texas Department of Transportation, Approved Products List:  
<http://www.dot.state.tx.us/mnt/erosion/contents.htm>

Figure 13-12c. Emergency Spillway Protection

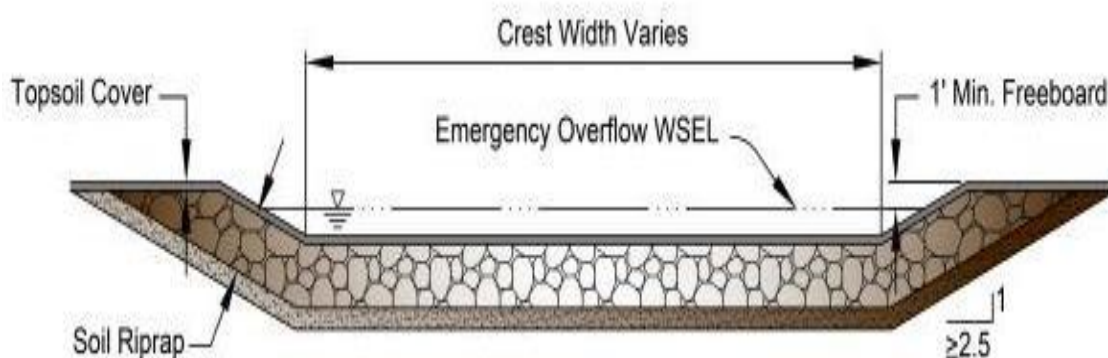
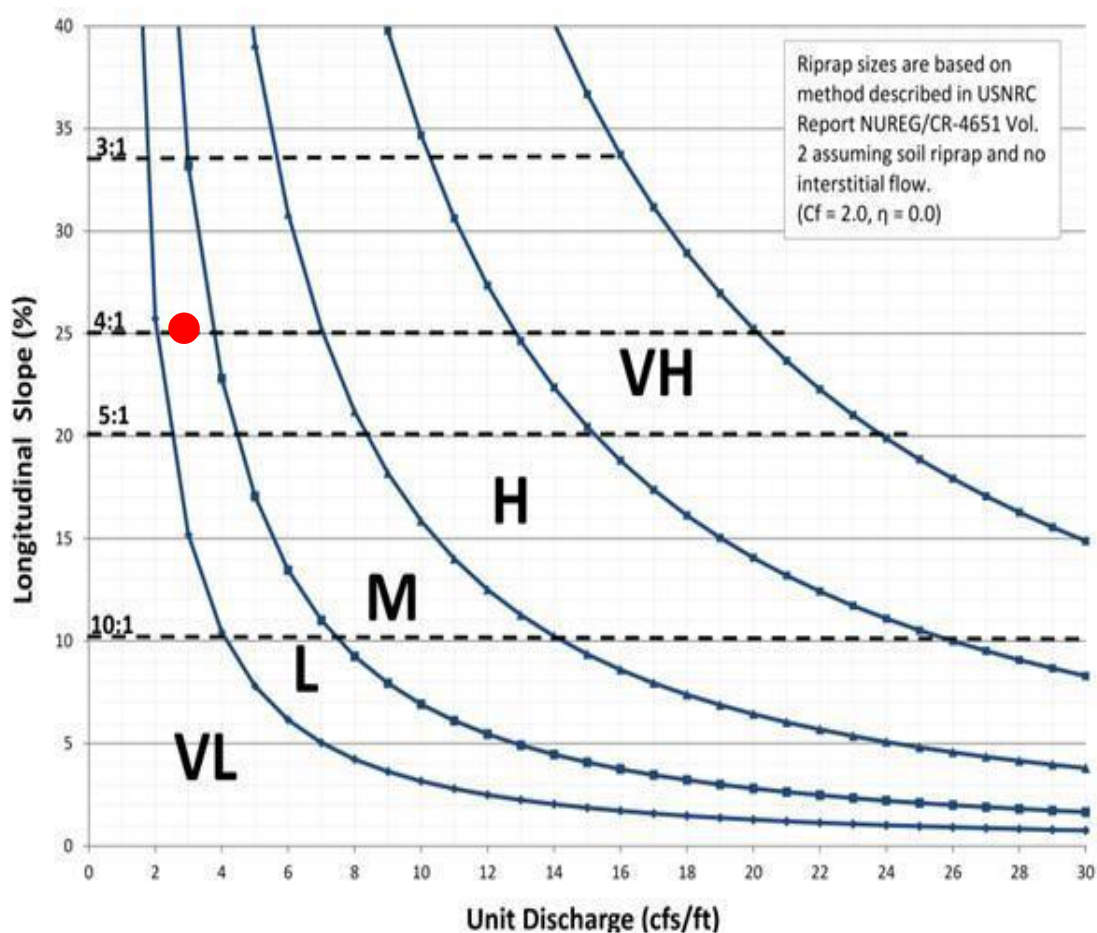
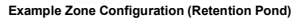


Figure 13-12d. Riprap Types for Emergency Spillway Protection



## MHFD-Detention, Version 4.04 (February 2021)

Basin ID:



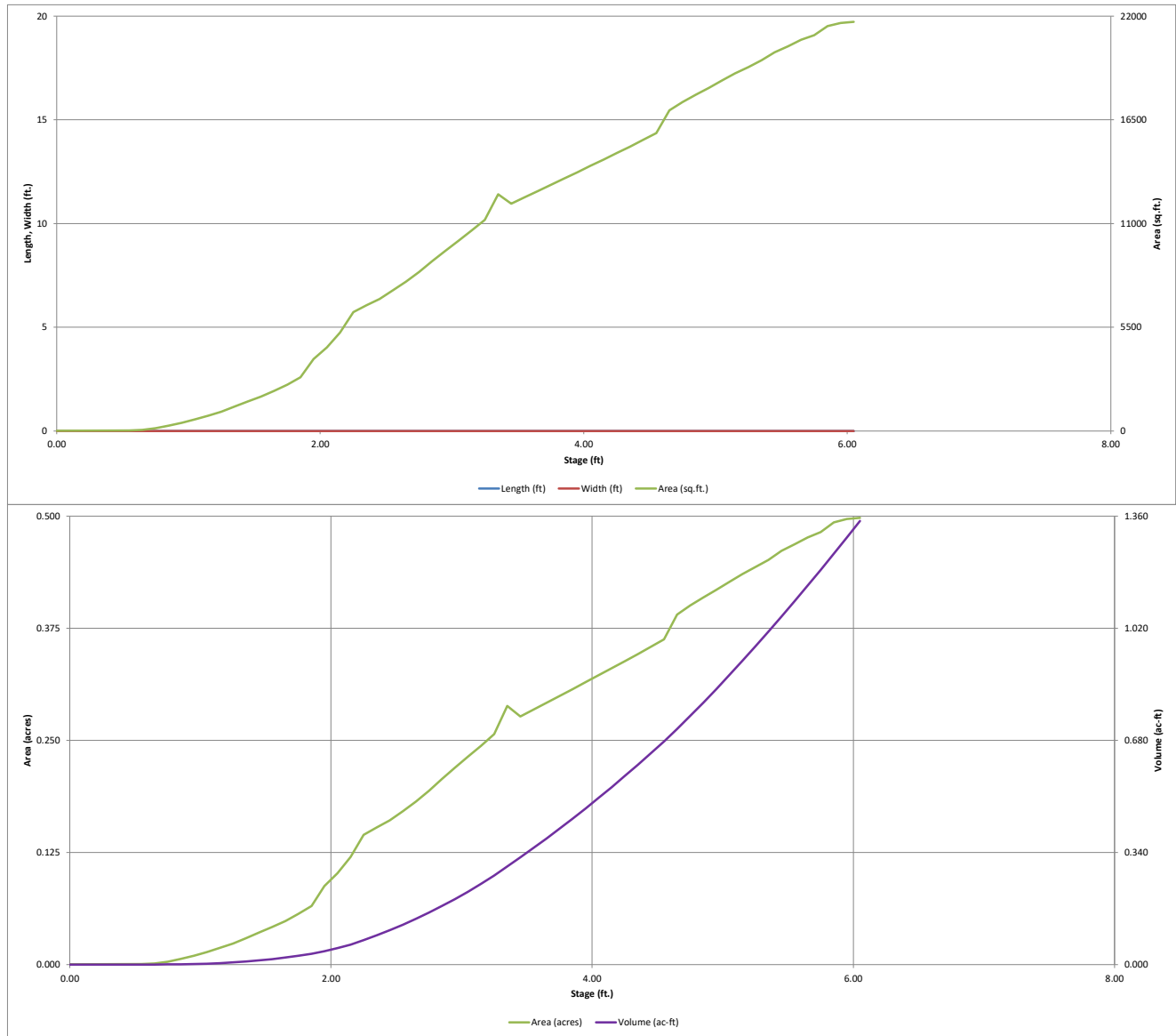
0.101	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
	inches

Initial Surcharge Area ( $A_{ISV}$ )	=	user	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ )	=	user	ft
Surcharge Volume Width ( $W_{ISV}$ )	=	user	ft
Depth of Basin Floor ( $H_{FLOOR}$ )	=	user	ft
Length of Basin Floor ( $L_{FLOOR}$ )	=	user	ft
Width of Basin Floor ( $W_{FLOOR}$ )	=	user	ft
Area of Basin Floor ( $A_{FLOOR}$ )	=	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ )	=	user	ft <sup>3</sup>
Depth of Main Basin ( $H_{MAIN}$ )	=	user	ft
Length of Main Basin ( $L_{MAIN}$ )	=	user	ft
Width of Main Basin ( $W_{MAIN}$ )	=	user	ft
Area of Main Basin ( $A_{MAIN}$ )	=	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ )	=	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{TOTAL}$ )	=	user	acre-feet

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft <sup>2</sup> )	Optional Override Area (ft <sup>2</sup> )	Area (acre)	Volume (ft <sup>3</sup> )	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	16	0.000		
Top of ISV	--	0.55	--	--	--	22	0.001	10	0.000
	--	0.65	--	--	--	57	0.001	14	0.000
	--	0.75	--	--	--	147	0.003	25	0.001
	--	0.85	--	--	--	278	0.006	46	0.001
	--	0.95	--	--	--	434	0.010	81	0.002
	--	1.05	--	--	--	615	0.014	134	0.003
	--	1.15	--	--	--	814	0.019	205	0.005
	--	1.25	--	--	--	1,026	0.024	297	0.007
	--	1.35	--	--	--	1,287	0.030	413	0.009
	--	1.45	--	--	--	1,556	0.036	555	0.013
	--	1.55	--	--	--	1,823	0.042	724	0.017
	--	1.65	--	--	--	2,124	0.049	921	0.021
	--	1.75	--	--	--	2,458	0.056	1,151	0.026
	--	1.85	--	--	--	2,846	0.065	1,416	0.033
	--	1.95	--	--	--	3,816	0.088	1,749	0.040
	--	2.05	--	--	--	4,437	0.102	2,161	0.050
	--	2.15	--	--	--	5,224	0.120	2,644	0.061
	--	2.25	--	--	--	6,307	0.145	3,221	0.074
	--	2.35	--	--	--	6,666	0.153	3,870	0.089
	--	2.45	--	--	--	7,002	0.161	4,553	0.105
	--	2.55	--	--	--	7,449	0.171	5,276	0.121
	--	2.65	--	--	--	7,916	0.182	6,044	0.139
	--	2.75	--	--	--	8,441	0.194	6,862	0.158
	--	2.85	--	--	--	9,005	0.207	7,734	0.178
	--	2.95	--	--	--	9,556	0.219	8,662	0.199
	--	3.05	--	--	--	10,096	0.232	9,645	0.221
	--	3.15	--	--	--	10,634	0.244	10,681	0.245
	--	3.25	--	--	--	11,191	0.257	11,772	0.270
	--	3.35	--	--	--	12,559	0.288	12,960	0.298
	--	3.45	--	--	--	12,056	0.277	14,191	0.326
	--	3.55	--	--	--	12,386	0.284	15,413	0.354
	--	3.65	--	--	--	12,718	0.292	16,668	0.383
	--	3.75	--	--	--	13,050	0.300	17,956	0.412
	--	3.85	--	--	--	13,384	0.307	19,278	0.443
	--	3.95	--	--	--	13,720	0.315	20,633	0.474
	--	4.05	--	--	--	14,057	0.323	22,022	0.506
	--	4.15	--	--	--	14,395	0.330	23,445	0.538
	--	4.25	--	--	--	14,734	0.338	24,901	0.572
	--	4.35	--	--	--	15,080	0.346	26,392	0.606
	--	4.45	--	--	--	15,434	0.354	27,918	0.641
	--	4.55	--	--	--	15,793	0.363	29,479	0.677
	--	4.65	--	--	--	17,002	0.390	31,119	0.714
	--	4.75	--	--	--	17,444	0.400	32,841	0.754
	--	4.85	--	--	--	17,833	0.409	34,605	0.794
	--	4.95	--	--	--	18,199	0.418	36,406	0.836
	--	5.05	--	--	--	18,586	0.427	38,246	0.878
	--	5.15	--	--	--	18,965	0.435	40,123	0.921
	--	5.25	--	--	--	19,308	0.443	42,037	0.965
	--	5.35	--	--	--	19,656	0.451	43,985	1.010
	--	5.45	--	--	--	20,089	0.461	45,972	1.055
	--	5.55	--	--	--	20,410	0.469		

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



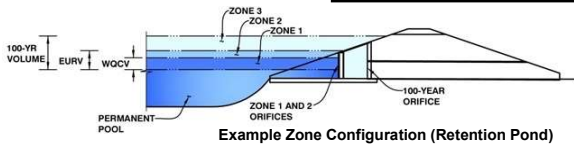


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Meadowbrook Park

Basin ID:



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.43	0.101	Orifice Plate
Zone 2 (EURV)	3.69	0.291	Rectangular Orifice
Zone 3 (100-year)	4.48	0.256	Weir&Pipe (Restrict)
Total (all zones)		0.648	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	N/A ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	3.69	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	0.47	sq. inches (diameter = 3/4 inch)

Calculated Parameters for Plate	
WQ Orifice Area per Row =	3.264E-03 ft <sup>2</sup>
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50						
Orifice Area (sq. inches)	0.47	0.47						

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.43	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.85	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	1.00	N/A	inches
Vertical Orifice Width =	2.00		inches

	Zone 2 Rectangular	Not Selected	
Calculated Parameters for Vertical Orifice			
Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.04	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	3.85	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	2.92	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	2.92	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	50%	N/A	%

	Zone 3 Weir	Not Selected	
Calculated Parameters for Overflow Weir			
Height of Grate Upper Edge, H <sub>u</sub> =	3.85	N/A	feet
Overflow Weir Slope Length =	2.92	N/A	feet
Grate Open Area / 100-yr Orifice Area =	11.04	N/A	
Overflow Grate Open Area w/o Debris =	5.93	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	2.97	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	5.00		inches

	Zone 3 Restrictor	Not Selected	
Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate			
Outlet Orifice Area =	0.54	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.25	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	0.84	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	4.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	15.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway		
Spillway Design Flow Depth=	0.47	feet
Stage at Top of Freeboard =	5.97	feet
Basin Area at Top of Freeboard =	0.50	acres
Basin Volume at Top of Freeboard =	1.31	acre-ft

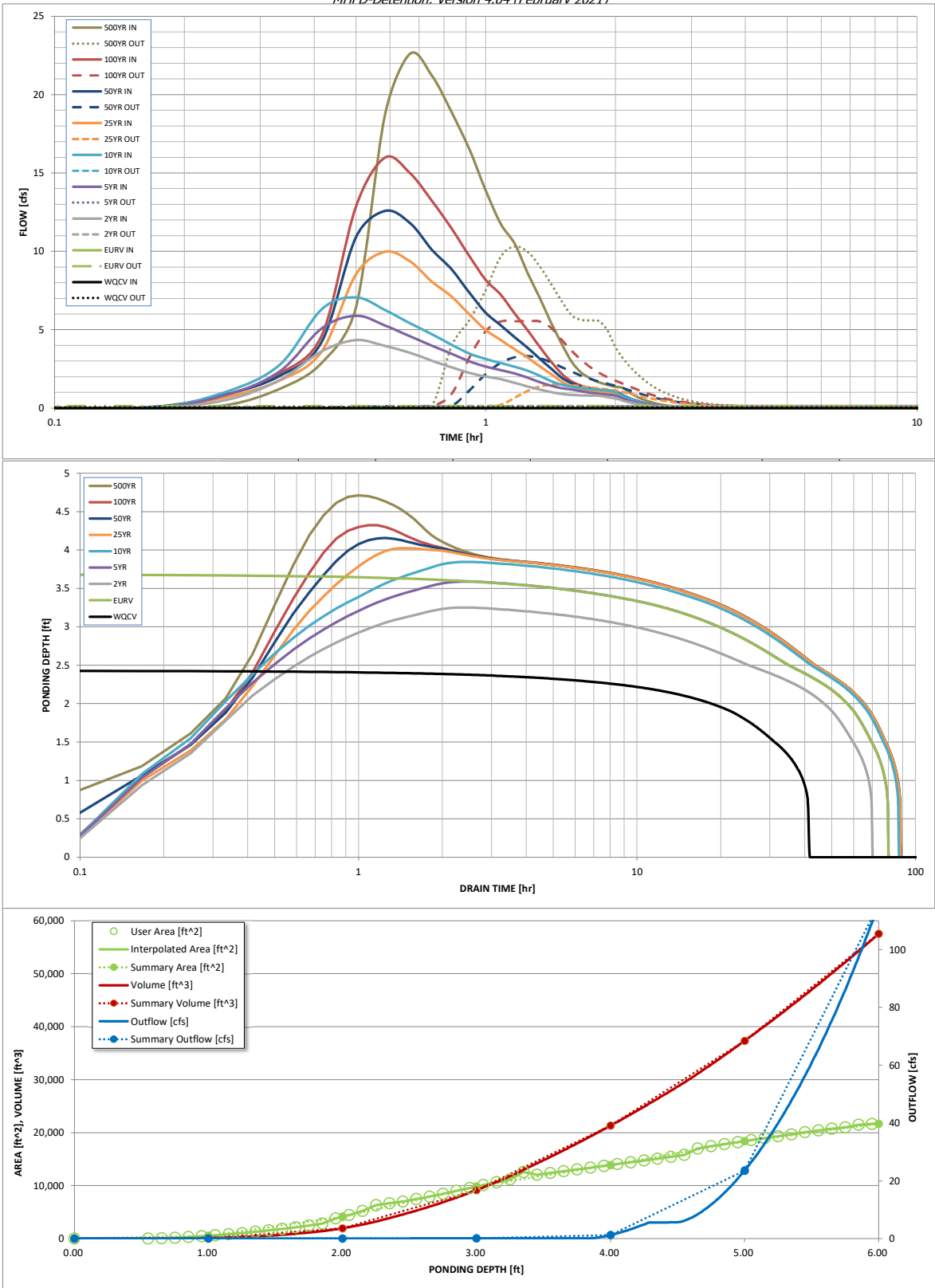
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
One-Hour Rainfall Depth (in) =	N/A	N/A	0.288	0.386	0.463	0.600	0.734	0.908	1.282
CUHP Runoff Volume (acre-ft) =	0.101	0.392	0.288	0.386	0.463	0.600	0.734	0.908	1.282
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.288	0.386	0.463	0.600	0.734	0.908	1.282
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.1	0.2	1.7	3.4	5.6	9.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.02	0.21	0.42	0.68	1.22
Peak Inflow Q (cfs) =	N/A	N/A	4.3	5.9	7.1	10.0	12.6	16.0	22.6
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.1	1.5	3.3	5.5	10.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.9	0.7	0.9	1.0	1.0	1.0
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.2	0.5	0.9	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	71	64	72	77	76	74	72	68
Time to Drain 99% of Inflow Volume (hours) =	41	77	68	77	83	84	83	82	79
Maximum Ponding Depth (ft) =	2.43	3.69	3.25	3.59	3.84	4.02	4.15	4.32	4.71
Area at Maximum Ponding Depth (acres) =	0.16	0.30	0.26	0.29	0.31	0.32	0.33	0.34	0.40
Maximum Volume Stored (acre-ft) =	0.101	0.394	0.270	0.362	0.439	0.496	0.538	0.596	0.738

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.19
	0:15:00	0.00	0.00	0.51	0.83	1.04	0.70	0.88	0.86	1.23
	0:20:00	0.00	0.00	1.81	2.36	2.78	1.76	2.05	2.21	2.88
	0:25:00	0.00	0.00	3.63	5.09	6.31	3.63	4.24	4.65	6.44
	0:30:00	0.00	0.00	4.33	5.88	7.06	8.53	10.91	12.87	18.68
	0:35:00	0.00	0.00	3.97	5.27	6.26	9.98	12.58	15.98	22.60
	0:40:00	0.00	0.00	3.53	4.58	5.41	9.37	11.81	15.00	21.21
	0:45:00	0.00	0.00	3.02	3.98	4.71	8.06	10.11	13.23	18.88
	0:50:00	0.00	0.00	2.59	3.47	4.04	7.11	8.85	11.45	16.50
	0:55:00	0.00	0.00	2.24	2.98	3.47	5.97	7.35	9.69	13.89
	1:00:00	0.00	0.00	2.01	2.65	3.13	4.98	6.08	8.19	11.76
	1:05:00	0.00	0.00	1.84	2.42	2.88	4.34	5.28	7.24	10.49
	1:10:00	0.00	0.00	1.61	2.21	2.63	3.75	4.52	6.03	8.64
	1:15:00	0.00	0.00	1.39	1.94	2.39	3.23	3.86	4.98	7.04
	1:20:00	0.00	0.00	1.18	1.66	2.06	2.66	3.15	3.91	5.47
	1:25:00	0.00	0.00	1.01	1.42	1.71	2.17	2.53	2.98	4.10
	1:30:00	0.00	0.00	0.90	1.27	1.48	1.69	1.94	2.19	2.94
	1:35:00	0.00	0.00	0.84	1.19	1.36	1.38	1.57	1.69	2.26
	1:40:00	0.00	0.00	0.81	1.07	1.27	1.21	1.37	1.43	1.89
	1:45:00	0.00	0.00	0.80	0.98	1.21	1.10	1.25	1.26	1.64
	1:50:00	0.00	0.00	0.79	0.91	1.17	1.03	1.16	1.16	1.47
	1:55:00	0.00	0.00	0.69	0.86	1.12	0.99	1.11	1.08	1.36
	2:00:00	0.00	0.00	0.61	0.80	1.02	0.95	1.07	1.02	1.28
	2:05:00	0.00	0.00	0.47	0.61	0.77	0.73	0.81	0.76	0.95
	2:10:00	0.00	0.00	0.35	0.45	0.57	0.54	0.60	0.56	0.70
	2:15:00	0.00	0.00	0.26	0.34	0.42	0.40	0.44	0.42	0.52
	2:20:00	0.00	0.00	0.19	0.25	0.31	0.29	0.33	0.31	0.38
	2:25:00	0.00	0.00	0.14	0.18	0.23	0.21	0.23	0.22	0.27
	2:30:00	0.00	0.00	0.10	0.13	0.16	0.15	0.17	0.16	0.19
	2:35:00	0.00	0.00	0.07	0.09	0.12	0.11	0.12	0.11	0.14
	2:40:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.08	0.09
	2:45:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	2:50:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.02	0.03
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

[illegible]

Forebay Release and Configuration	Required	Flow: $Q_{100}$ = (cfs)	Forebay A Release Rate
	Release 2% of the undetained 100-year peak discharge by way of a wall/notch or berm/pipe configuration	19.60	0.39

Minimum Forebay Volume Required	Required (CF)	Provided (CF)
2% of the WQCV	70.07	84.00
40hr drain time $a = 1$ $I = 0.641$ $A = 3.85$ AC		

Maximum Forebay Depth	Required	Provided	Concrete Forebay Structure
	18" Max	18"	

Forebay Notch Calculations			
$Q = C_o A_o (2gH_o)^{0.5}$			
$Q_a$	0.39 cfs		2% of Peak 100 YR Discharge for contributing Sub-Basins
$C_o$	0.6		
$H_o$	0.5 ft		
$g$	32.2 ft/s <sup>2</sup>		
$A_a$	0.12 ft <sup>2</sup>		
$L_a$	0.08 ft		
	0.92 in		3" Minimum per Criteria

$$WQCV = a(0.91I^3 - 1.19I^2 + 0.78I) \quad \text{Equation 3-1}$$

Where:

- WQCV = Water Quality Capture Volume (watershed inches)  
 $a$  = Coefficient corresponding to WQCV drain time (Table 3-2)  
 $I$  = Imperviousness (%/100) (see Figures 3-3 through 3-5 [single family land use] and /or the *Runoff* chapter of Volume 1[other typical land uses])

**Table 3-2. Drain Time Coefficients for WQCV Calculations**

Drain Time (hrs)	Coefficient, $a$
12 hours	0.8
24 hours	0.9
40 hours	1.0

Forebay Release and Configuration	Required	Flow: $Q_{100}$ = (cfs)	Forebay B Release Rate
	Release 2% of the undetained 100-year peak discharge by way of a wall/notch or berm/pipe configuration	7.19	0.14

Minimum Forebay Volume Required	Required (CF)	Provided (CF)
2% of the WQCV	20.52	154.00
40hr drain time $a = 1$ $I = 0.197$ $A = 2.47$ AC		

Maximum Forebay Depth	Required	Provided	Concrete Berm
	12" Max	12"	

Forebay Notch Calculations		
$Q = C_o A_o (2gH_o)^{0.5}$		
$Q_a$	0.14 cfs	2% of Peak 100 YR Discharge for contributing Sub-Basins
$C_o$	0.6	
$H_o$	0.5 ft	
$g$	32.2 ft/s <sup>2</sup>	
$A_a$	0.04 ft <sup>2</sup>	
$L_a$	0.03 ft	
	0.34 in	3" Minimum per Criteria

$$WQCV = a(0.91I^3 - 1.19I^2 + 0.78I) \quad \text{Equation 3-1}$$

Where:

- WQCV = Water Quality Capture Volume (watershed inches)  
 $a$  = Coefficient corresponding to WQCV drain time (Table 3-2)  
 $I$  = Imperviousness (%/100) (see Figures 3-3 through 3-5 [single family land use] and /or the *Runoff* chapter of Volume 1[other typical land uses])

**Table 3-2. Drain Time Coefficients for WQCV Calculations**

Drain Time (hrs)	Coefficient, $a$
12 hours	0.8
24 hours	0.9
40 hours	1.0

**INLET MANAGEMENT**

Worksheet Protected

INLET NAME	Design Point 3	Design Point 4	Design Point 5	Design Point 6	Design Point 7
Site Type (Urban or Rural)					
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	On Grade	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type C Grate	Colorado Springs D-10-R	CDOT Type R Curb Opening	CDOT Type R Curb Opening

**USER-DEFINED INPUT**

<b>User-Defined Design Flows</b>					
Minor $Q_{known}$ (cfs)	2.4	0.2	1.4	0.4	1.7
Major $Q_{known}$ (cfs)	4.8	1.2	2.7	0.8	4.0

**Bypass (Carry-Over) Flow from Upstream**

Receive Bypass Flow from:	No Bypass Flow Received	User-Defined	User-Defined	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.1	0.1	0.0	0.0

**Watershed Characteristics**

Subcatchment Area (acres)					
Percent Impervious					
NRCS Soil Type					

**Watershed Profile**

Overland Slope (ft/ft)					
Overland Length (ft)					
Channel Slope (ft/ft)					
Channel Length (ft)					

**Minor Storm Rainfall Input**

Design Storm Return Period, $T_r$ (years)					
One-Hour Precipitation, $P_1$ (inches)					

**Major Storm Rainfall Input**

Design Storm Return Period, $T_r$ (years)					
One-Hour Precipitation, $P_1$ (inches)					

**CALCULATED OUTPUT**

Minor Total Design Peak Flow, $Q$ (cfs)	2.4	0.2	1.4	0.4	1.7
Major Total Design Peak Flow, $Q$ (cfs)	4.8	1.3	2.8	0.8	4.0
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	0.0	N/A	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	0.0	N/A	N/A

**Minor Storm (Calculated) Analysis of Flow Time**

C	N/A	N/A	N/A	N/A	N/A
$C_s$	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, $V_i$	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, $V_t$	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, $T_i$	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, $T_t$	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, $T_c$	N/A	N/A	N/A	N/A	N/A
Regional $T_c$	N/A	N/A	N/A	N/A	N/A
Recommended $T_c$	N/A	N/A	N/A	N/A	N/A
$T_c$ selected by User	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, $I$	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, $Q_p$	N/A	N/A	N/A	N/A	N/A

**Major Storm (Calculated) Analysis of Flow Time**

C	N/A	N/A	N/A	N/A	N/A
$C_s$	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, $V_i$	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, $V_t$	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, $T_i$	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, $T_t$	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, $T_c$	N/A	N/A	N/A	N/A	N/A
Regional $T_c$	N/A	N/A	N/A	N/A	N/A
Recommended $T_c$	N/A	N/A	N/A	N/A	N/A
$T_c$ selected by User	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, $I$	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, $Q_p$	N/A	N/A	N/A	N/A	N/A

**INLET MANAGEMENT**

Worksheet Protected

INLET NAME	Design Point 8	Design Point 9	Design Point 10	Design Point 12
Site Type (Urban or Rural)				RURAL
Inlet Application (Street or Area)	STREET	STREET	STREET	AREA
Hydraulic Condition	In Sump	On Grade	On Grade	Swale
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type D (In Series & Depressed)

**USER-DEFINED INPUT****User-Defined Design Flows**

Minor $Q_{Known}$ (cfs)	1.7	0.8	0.8	10.7
Major $Q_{Known}$ (cfs)	3.9	1.7	1.5	23.5

**Bypass (Carry-Over) Flow from Upstream**

Receive Bypass Flow from:	User-Defined	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.2	0.0	0.0	0.0

**Watershed Characteristics**

Subcatchment Area (acres)				
Percent Impervious				
NRCS Soil Type				

**Watershed Profile**

Overland Slope (ft/ft)				
Overland Length (ft)				
Channel Slope (ft/ft)				
Channel Length (ft)				

**Minor Storm Rainfall Input**

Design Storm Return Period, $T_r$ (years)				
One-Hour Precipitation, $P_1$ (inches)				

**Major Storm Rainfall Input**

Design Storm Return Period, $T_r$ (years)				
One-Hour Precipitation, $P_1$ (inches)				

**CALCULATED OUTPUT**

Minor Total Design Peak Flow, $Q$ (cfs)	1.7	0.8	0.8	10.7
Major Total Design Peak Flow, $Q$ (cfs)	4.1	1.7	1.5	23.5
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	0.0	0.0	0.0
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	0.2	0.1	0.0

**Minor Storm (Calculated) Analysis of Flow T1**

C	N/A	N/A	N/A	N/A
$C_s$	N/A	N/A	N/A	N/A
Overland Flow Velocity, $V_i$	N/A	N/A	N/A	N/A
Channel Flow Velocity, $V_t$	N/A	N/A	N/A	N/A
Overland Flow Time, $T_i$	N/A	N/A	N/A	N/A
Channel Travel Time, $T_t$	N/A	N/A	N/A	N/A
Calculated Time of Concentration, $T_c$	N/A	N/A	N/A	N/A
Regional $T_c$	N/A	N/A	N/A	N/A
Recommended $T_c$	N/A	N/A	N/A	N/A
$T_c$ selected by User	N/A	N/A	N/A	N/A
Design Rainfall Intensity, $I$	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, $Q_p$	N/A	N/A	N/A	N/A

**Major Storm (Calculated) Analysis of Flow T1**

C	N/A	N/A	N/A	N/A
$C_s$	N/A	N/A	N/A	N/A
Overland Flow Velocity, $V_i$	N/A	N/A	N/A	N/A
Channel Flow Velocity, $V_t$	N/A	N/A	N/A	N/A
Overland Flow Time, $T_i$	N/A	N/A	N/A	N/A
Channel Travel Time, $T_t$	N/A	N/A	N/A	N/A
Calculated Time of Concentration, $T_c$	N/A	N/A	N/A	N/A
Regional $T_c$	N/A	N/A	N/A	N/A
Recommended $T_c$	N/A	N/A	N/A	N/A
$T_c$ selected by User	N/A	N/A	N/A	N/A
Design Rainfall Intensity, $I$	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, $Q_p$	N/A	N/A	N/A	N/A



**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

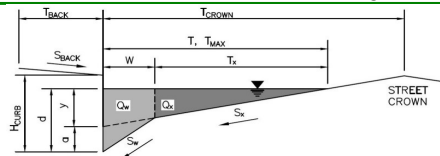
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 3

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

**MINOR STORM** Allowable Capacity is based on Depth Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$T_{BACK} = 8.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 22.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

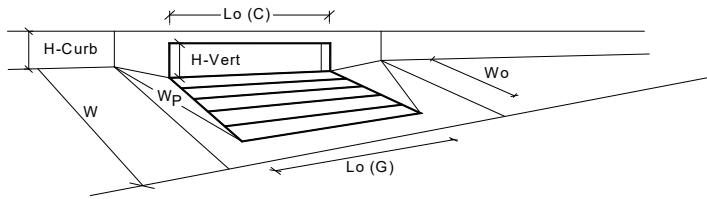
	Minor Storm	Major Storm	
$I_{MAX} =$	12.0	20.0	ft
$d_{MAX} =$	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

$Q_{allow} =$

	Minor Storm	Major Storm	
	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



## Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from above)

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

## Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

## Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

## Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

## Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
$a_{local}$ =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	4.4	6.0	inches
	MINOR	MAJOR	<input type="checkbox"/> Override Defaults
$L_o (G)$ =	N/A	N/A	feet
$W_o$ =	N/A	N/A	feet
$A_{ratio}$ =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	5.00	5.00	feet
$H_{vert}$ =	6.00	6.00	inches
$H_{throat}$ =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
$W_p$ =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
$d_{Grate}$ =	N/A	N/A	ft
$d_{Curb}$ =	0.20	0.33	ft
$RF_{Combination}$ =	0.56	0.77	
$RF_{Curb}$ =	1.00	1.00	
$RF_{Grate}$ =	N/A	N/A	
	MINOR	MAJOR	
$Q_a$ =	2.5	5.4	cfs
$Q_{PEAK REQUIRED}$ =	2.4	4.8	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

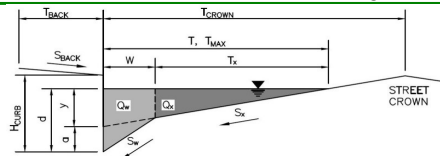
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 4

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

**MINOR STORM** Allowable Capacity is based on Depth Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$T_{BACK} = 8.0$  ft  
 $S_{BACK} = 0.050$  ft/ft  
 $n_{BACK} = 0.018$

$H_{CURB} = 12.00$  inches  
 $T_{CROWN} = 22.0$  ft  
 $W = 0.85$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.018$

	Minor Storm	Major Storm	
$I_{MAX} =$	12.0	20.0	ft
$d_{MAX} =$	6.0	6.0	inches

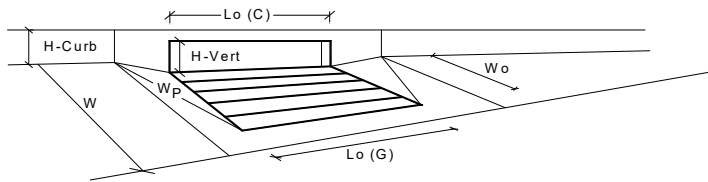
☐ ☐

$Q_{allow} =$

	Minor Storm	Major Storm	
	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



## Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from above)

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

### Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

### Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

### Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

## Total Inlet Interception Capacity (assumes clogged condition)

**Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)**

	MINOR	MAJOR	
Type =	CDOT Type C Grate		
$Q_{local}$ =	12.00	12.00	inches
No =	1	1	
Ponding Depth =	3.5	5.4	inches
	MINOR	MAJOR	<input type="checkbox"/> Override Depths
$L_o$ (G) =	2.92	2.92	
$W_o$ =	0.85	0.85	feet
$A_{ratio}$ =	0.70	0.70	
$C_r$ (G) =	0.50	0.50	
$C_w$ (G) =	2.41	2.41	
$C_o$ (G) =	0.67	0.67	
	MINOR	MAJOR	
$L_o$ (C) =	N/A	N/A	feet
$H_{vert}$ =	N/A	N/A	inches
$H_{throat}$ =	N/A	N/A	inches
Theta =	N/A	N/A	degrees
$W_p$ =	N/A	N/A	feet
$C_r$ (C) =	N/A	N/A	
$C_w$ (C) =	N/A	N/A	
$C_o$ (C) =	N/A	N/A	
	MINOR	MAJOR	
$d_{Grate}$ =	0.758	0.918	ft
$d_{Curb}$ =	N/A	N/A	ft
$RF_{Combination}$ =	N/A	N/A	
$RF_{Curb}$ =	N/A	N/A	
$RF_{Grate}$ =	0.56	0.86	
	MINOR	MAJOR	
$Q_a$ =	1.7	3.5	cfs
$Q_{PEAK REQUIRED}$ =	0.2	1.3	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

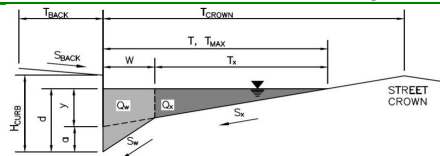
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 5

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 6.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 22.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.030$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor &amp; Major Storm

	Minor Storm	Major Storm	
$I_{MAX} =$	11.0	22.0	ft
$d_{MAX} =$	6.0	6.0	inches

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
**MINOR STORM** Allowable Capacity is based on Spread Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

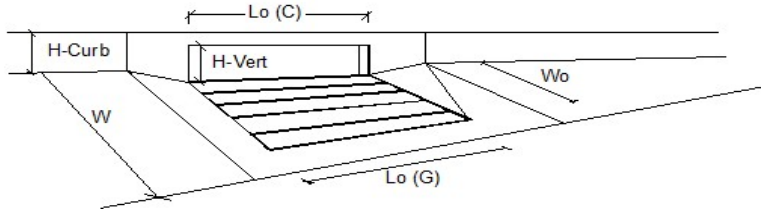
	Minor Storm	Major Storm	
$Q_{allow} =$	6.7	17.8	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Springs D-10-R		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL}$ =	4.0	4.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o$ =	8.00	8.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o$ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_{r-G}$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_{r-C}$ =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	1.4	2.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b$ =	0.0	0.0	cfs
Capture Percentage = $Q_i/Q_o$ =		C% =	100	100	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

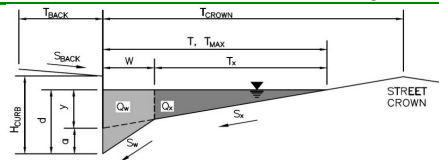
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 6

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

**MINOR STORM** Allowable Capacity is based on Depth Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$T_{BACK} = 6.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

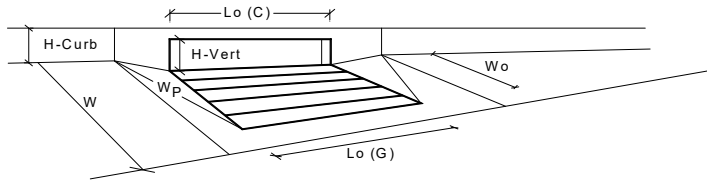
	Minor Storm	Major Storm	
$I_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	6.0	inches

☐ ☐

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



## Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from above)

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

## Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

## Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

## Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

## Total Inlet Interception Capacity (assumes clogged condition)

**Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)**

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
$q_{local}$ =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	5.6	5.6	inches
	MINOR	MAJOR	<input type="checkbox"/> Override Depths
$L_o (G)$ =	N/A	N/A	feet
$W_o$ =	N/A	N/A	feet
$A_{ratio}$ =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	5.00	5.00	feet
$H_{vert}$ =	6.00	6.00	inches
$H_{throat}$ =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
$W_p$ =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
$d_{Grate}$ =	N/A	N/A	ft
$d_{Curb}$ =	0.30	0.30	ft
$RF_{Combination}$ =	0.72	0.72	
$RF_{Curb}$ =	1.00	1.00	
$RF_{Grate}$ =	N/A	N/A	
	MINOR	MAJOR	
$Q_a$ =	4.6	4.6	cfs
$Q_{PEAK REQUIRED}$ =	0.4	0.8	cfs



**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

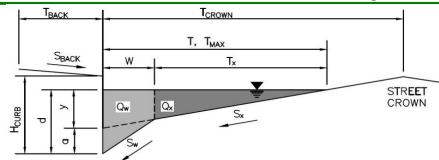
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 7

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

**MINOR STORM** Allowable Capacity is based on Depth Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$T_{BACK} = 6.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

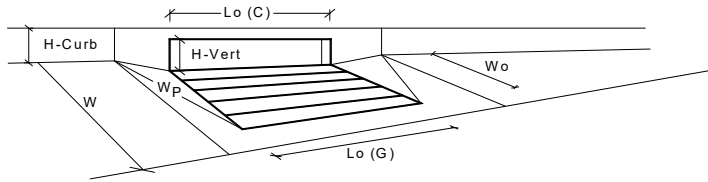
	Minor Storm	Major Storm	
$I_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	6.0	inches

☐ ☐

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



## Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from above)

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

## Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

## Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

## Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

## Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
$a_{local}$ =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	5.6	5.6	inches
	MINOR	MAJOR	
$L_o$ (G) =	N/A	N/A	feet
$W_o$ =	N/A	N/A	feet
$A_{ratio}$ =	N/A	N/A	
$C_r$ (G) =	N/A	N/A	
$C_w$ (G) =	N/A	N/A	
$C_o$ (G) =	N/A	N/A	
	MINOR	MAJOR	
$L_o$ (C) =	5.00	5.00	feet
$H_{vert}$ =	6.00	6.00	inches
$H_{throat}$ =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
$W_p$ =	2.00	2.00	feet
$C_r$ (C) =	0.10	0.10	
$C_w$ (C) =	3.60	3.60	
$C_o$ (C) =	0.67	0.67	
	MINOR	MAJOR	
$d_{Grate}$ =	N/A	N/A	ft
$d_{Curb}$ =	0.30	0.30	ft
$RF_{Combination}$ =	0.72	0.72	
$RF_{Curb}$ =	1.00	1.00	
$RF_{Grate}$ =	N/A	N/A	
	MINOR	MAJOR	
$Q_a$ =	4.6	4.6	cfs
$Q_{PEAK REQUIRED}$ =	1.7	4.0	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

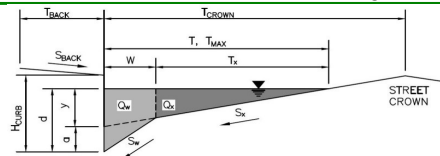
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 8

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

**MINOR STORM** Allowable Capacity is based on Depth Criterion**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$T_{BACK} = 8.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

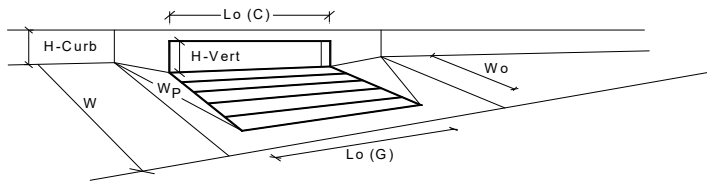
$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 20.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

	Minor Storm	Major Storm	
$I_{MAX} =$	12.0	20.0	ft
$d_{MAX} =$	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



## Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from above)

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

## Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

## Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

## Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

## Total Inlet Interception Capacity (assumes clogged condition)

**Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)**

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
$\theta_{local}$ =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	4.4	6.0	inches
	MINOR	MAJOR	<input type="checkbox"/> Override Depths
$L_o (G)$ =	N/A	N/A	feet
$W_o$ =	N/A	N/A	feet
$A_{ratio}$ =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	5.00	5.00	feet
$H_{vert}$ =	6.00	6.00	inches
$H_{throat}$ =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
$W_p$ =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
$d_{Grate}$ =	N/A	N/A	ft
$d_{Curb}$ =	0.20	0.33	ft
$RF_{Combination}$ =	0.56	0.77	
$RF_{Curb}$ =	1.00	1.00	
$RF_{Grate}$ =	N/A	N/A	
	MINOR	MAJOR	
$Q_a$ =	2.5	5.4	cfs
$Q_{PEAK REQUIRED}$ =	1.7	4.1	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

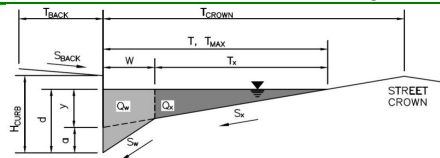
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Design Point 9

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 6.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 12.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.010$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$I_{MAX} =$	11.0	12.0	ft
$d_{MAX} =$	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	check = yes

**MINOR STORM** Allowable Capacity is based on Spread Criterion**MAJOR STORM** Allowable Capacity is based on Spread Criterion

$Q_{allow} =$ 

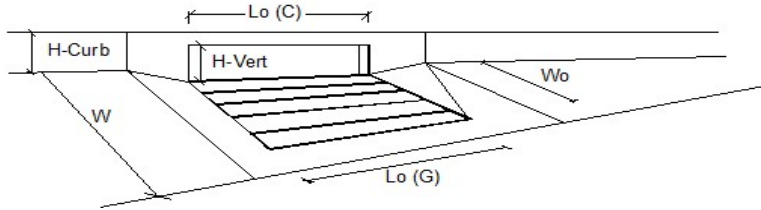
Minor Storm	Major Storm	
3.9	4.7	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL}$ =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o$ =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o$ =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o$ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_{r-G}$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_{r-C}$ =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	0.8	1.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_o$ =	0.0	0.2	cfs
Capture Percentage = $Q_i/Q_o$ =		C% =	100	91	%

9% Carry-Over Flows = 0.2 cfs  
(Accepted by Design Point 8)

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

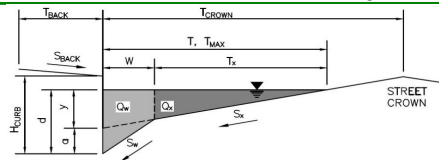
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Meadowbrook Park

Inlet ID:

Deisgn Point 10

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 6.0$  ft  
 $S_{BACK} = 0.018$  ft/ft  
 $n_{BACK} = 0.013$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 11.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.027$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$I_{MAX} =$	11.0	11.0	ft
$d_{MAX} =$	6.0	6.0	inches
<input type="checkbox"/> check = yes			

**MINOR STORM** Allowable Capacity is based on Spread Criterion**MAJOR STORM** Allowable Capacity is based on Spread Criterion

$Q_{allow} =$ 

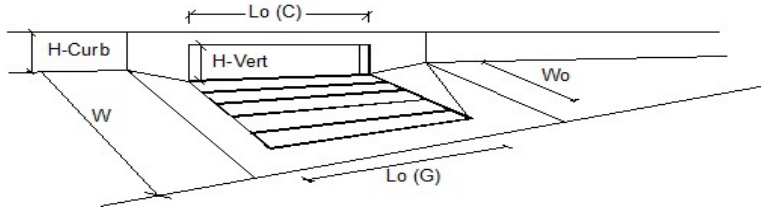
Minor Storm	Major Storm	cfs
6.3	6.3	

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



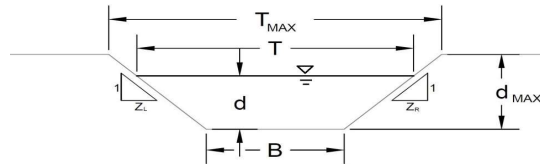
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL}$ =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o$ =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o$ =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o$ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_{r-G}$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_{r-C}$ =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	0.7	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b$ =	0.0	0.1	cfs
Capture Percentage = $Q_i/Q_o$ =		C% =	100	95	%

5% Carry-Over Flow = 0.1 cfs  
(Accepted by Design Point 5)



# AREA INLET IN A SWALE

Meadowbrook Park  
Design Point 12



This worksheet uses the NRCS  
vegetal retardance method to  
determine Manning's n.

For more information see  
Section 7.2.3 of the USDCM.

## Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

Soil Type:	Max. Velocity ( $V_{MAX}$ )	Max Froude No. ( $F_{MAX}$ )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Max. Allowable Top Width of Channel for Minor & Major Storm

Max. Allowable Water Depth in Channel for Minor & Major Storm

A, B, C, D or E

n = 0.030

$S_0$  = 0.0340 ft/ft

B = 0.00 ft

Z1 = 4.00 ft/ft

Z2 = 4.00 ft/ft

Choose One:

☐ Non-Cohesive

☒ Cohesive

☐ Paved

	Minor Storm	Major Storm	
$T_{MAX}$ =	20.00	20.00	feet
$d_{MAX}$ =	1.00	1.25	feet

## Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow}$ =	22.6	41.0	cfs
$d_{allow}$ =	1.00	1.25	ft

## Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

	Minor Storm	Major Storm	
$Q_o$ =	10.7	23.5	cfs
d =	0.76	1.02	feet

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

## AREA INLET IN A SWALE

Meadowbrook Park  
Design Point 12

## Inlet Design Information (Input)

Type of Inlet

CDOT Type D (In Series &amp; Depressed)

Inlet Type =

CDOT Type D (In Series &amp; Depressed)

Angle of Inclined Grate (must be  $\leq 30$  degrees)

Width of Grate

Length of Grate

Open Area Ratio

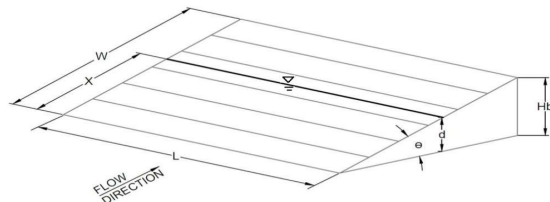
Height of Inclined Grate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



$\theta$ =	0.00	degrees
W =	3.00	feet
L =	6.00	feet
$A_{RATIO}$ =	0.70	
$H_B$ =	0.00	feet
$C_d$ =	0.38	
$C_d$ =	0.72	
$C_o$ =	0.48	
$C_w$ =	1.53	

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

Total Inlet Interception Capacity (assumes clogged condition)

	MINOR	MAJOR	
d =	1.76	2.02	
$Q_a$ =	39.9	42.8	cfs
Bypassed Flow, $Q_b$ =	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o = C\%$	100	100	%

Warning 04: Froude No. exceeds USDCM Volume I recommendation.

# Design Procedure Form: Rain Garden (RG)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

Designer: KRK  
 Company: Kimley-Horn and Associates  
 Date: March 12, 2021  
 Project: Meadowbrook Park  
 Location: RG SWC of Site

## 1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area,  $I_a$   
 (100% if all paved and roofed areas upstream of rain garden)
- B) Tributary Area's Imperviousness Ratio ( $i = I_a/100$ )
- C) Water Quality Capture Volume (WQCV) for a 12-hour Drain Time  
 (WQCV =  $0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$ )
- D) Contributing Watershed Area (including rain garden area)
- E) Water Quality Capture Volume (WQCV) Design Volume  
 Vol = (WQCV / 12) \* Area
- F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
 (Only if a different WQCV Design Volume is desired)

$I_a =$  54.5 %

$i =$  0.545

WQCV = 0.18 watershed inches

Area = 80,559 sq ft

$V_{WQCV} =$             cu ft

$d_e =$  0.43 in

$V_{WQCV \text{ OTHER}} =$  1,176 cu ft

$V_{WQCV \text{ USER}} =$             cu ft

## 2. Basin Geometry

- A) WQCV Depth (12-inch maximum)
- B) Rain Garden Side Slopes ( $Z = 4$  min., horiz. dist per unit vertical)  
 (Use "0" if rain garden has vertical walls)
- C) Minimum Flat Surface Area
- D) Actual Flat Surface Area
- E) Area at Design Depth (Top Surface Area)
- F) Rain Garden Total Volume  
 ( $V_T = ((A_{Top} + A_{Actual}) / 2) * \text{Depth}$ )

$D_{WQCV} =$  12 in

$Z =$  0.00 ft / ft

$A_{Min} =$  878 sq ft

$A_{Actual} =$  1215 sq ft

$A_{Top} =$  1215 sq ft

$V_T =$  1,215 cu ft

## 3. Growing Media

Choose One             
☒ 18" Rain Garden Growing Media  
☐ Other (Explain):  
            
          

## 4. Underdrain System

- A) Are underdrains provided?
- B) Underdrain system orifice diameter for 12 hour drain time
- i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice
- ii) Volume to Drain in 12 Hours
- iii) Orifice Diameter, 3/8" Minimum

Choose One             
☒ YES  
☐ NO

$y =$  0.3 ft

$Vol_{12} =$  1,176 cu ft

$D_o =$  1 3/16 in

# Design Procedure Form: Rain Garden (RG)

Sheet 2 of 2

Designer: KRK  
 Company: Kimley-Horn and Associates  
 Date: March 12, 2021  
 Project: Meadowbrook Park  
 Location: RG SWC of Site

## 5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

- ☒ YES  
☐ NO

PROVIDE A 30 MIL (MIN) PVC LINER WITH CDOT CLASS B GEOTEXTILE ABOVE IT. USE THE SAME GEOTEXTILE BELOW THE LINER IF THE SUBGRADE IS ANGULAR

## 6. Inlet / Outlet Control

- A) Inlet Control

Choose One

- ☐ Sheet Flow- No Energy Dissipation Required  
☒ Concentrated Flow- Energy Dissipation Provided

## 7. Vegetation

Choose One

- ☒ Seed (Plan for frequent weed control)  
☐ Plantings  
☐ Sand Grown or Other High Infiltration Sod

## 8. Irrigation

- A) Will the rain garden be irrigated?

Choose One

- ☐ YES  
☐ NO

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

## Meadowbrook StormCAD.stsw

**Active Scenario: 5 YR**

### FlexTable: Catch Basin Table

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow (Total Out) (cfs)	Headloss Coefficient (Standard)
INLET A8	6,334.79	6,330.42	6,330.91	6,330.90	1.66	0.050
INLET B2	6,324.87	6,320.57	6,321.48	6,321.47	1.38	0.050
INLET C1	6,323.00	6,321.90	6,322.10	6,322.10	0.21	0.050
INLET D1	6,324.49	6,320.58	6,321.57	6,321.57	2.42	0.050
INLET F1	6,329.50	6,325.45	6,325.77	6,325.77	0.44	0.050
INLET F2	6,329.50	6,325.37	6,325.87	6,325.86	1.72	0.050
INLET G1	6,336.34	6,327.28	6,327.94	6,327.94	0.77	0.050
INLET H1	6,336.24	6,328.60	6,329.13	6,329.12	0.82	0.050
INLET I1	6,318.35	6,315.40	6,316.92	6,316.92	0.03	0.050
INLET J4	6,323.01	6,318.31	6,319.42	6,319.40	10.69	0.050
INLET K1	6,320.04	6,317.25	6,318.69	6,318.69	0.10	0.050

## Meadowbrook StormCAD.stsw

**Active Scenario: 5 YR**

**FlexTable: Conduit Table**

Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)
MH A7	MH A6	6,328.31	6,327.71	0.011	18.0	0.013	2.48	5.00	10.93
MH A6	MH A5	6,327.51	6,327.19	0.011	18.0	0.013	2.48	4.98	10.87
INLET G1	MH A5	6,327.28	6,327.19	0.020	18.0	0.013	0.77	4.43	14.85
INLET H1	MH A7	6,328.60	6,328.51	0.019	18.0	0.013	0.82	4.45	14.59
MH A5	MH A4	6,326.99	6,324.07	0.015	18.0	0.013	3.25	6.11	12.98
INLET A8	MH A7	6,330.42	6,328.51	0.011	18.0	0.013	1.66	4.45	10.89
MH E1	MH A4	6,324.90	6,323.77	0.006	18.0	0.013	2.16	3.83	7.97
MH A4	MH A3	6,323.57	6,322.46	0.007	24.0	0.013	5.41	5.32	19.57
INLET F1	MH E1	6,325.45	6,325.32	0.005	18.0	0.013	0.44	2.31	7.46
INLET F2	MH E1	6,325.37	6,325.32	0.005	18.0	0.013	1.72	3.50	7.68
MH A3	MH A2	6,322.26	6,320.99	0.012	24.0	0.013	5.41	6.29	24.68
MH A2	Outfall A1	6,319.99	6,319.85	0.003	36.0	0.013	9.42	4.36	36.79
MH C1	MH A2	6,320.47	6,320.19	0.005	18.0	0.013	2.63	3.84	7.42
INLET B2	MH A2	6,320.57	6,320.39	0.006	18.0	0.013	1.38	3.41	8.05
MH C1	INLET D1	6,320.58	6,320.56	0.005	18.0	0.013	2.42	1.37	7.45
INLET C1	MH C1	6,321.90	6,321.14	0.006	10.0	0.010	0.21	2.48	2.13
MH J3	INLET K1	6,317.25	6,317.16	0.005	30.0	0.013	0.10	0.02	29.00
MH J3	MH J2	6,317.16	6,315.21	0.007	30.0	0.013	10.79	6.26	34.82
INLET J4	MH J3	6,318.31	6,317.36	0.022	30.0	0.013	10.69	9.33	60.85
MH J2	MH J1	6,315.01	6,314.62	0.009	30.0	0.013	10.79	6.79	38.96
MH J1	O-2	6,314.44	6,313.87	0.011	36.0	0.013	10.82	7.09	68.65
INLET I1	MH J1	6,315.40	6,314.62	0.005	18.0	0.013	0.03	0.02	7.28

## Meadowbrook StormCAD.stsw

**Active Scenario: 5 YR**

### FlexTable: Conduit Table

Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow / Capacity (Design) (%)
6,328.91	6,328.40	22.7
6,328.11	6,327.95	22.8
6,327.94	6,327.95	5.2
6,329.12	6,329.13	5.6
6,327.68	6,324.58	25.0
6,330.90	6,329.13	15.2
6,325.46	6,324.71	27.1
6,324.39	6,323.18	27.6
6,325.77	6,325.77	5.9
6,325.86	6,325.80	22.4
6,323.08	6,321.63	21.9
6,321.02	6,320.82	25.6
6,321.49	6,321.47	35.4
6,321.47	6,321.47	17.1
6,321.57	6,321.56	32.5
6,322.10	6,321.56	9.9
6,318.69	6,318.69	0.3
6,318.26	6,316.92	31.0
6,319.40	6,318.69	17.6
6,316.92	6,316.92	27.7
6,316.87	6,316.87	15.8
6,316.92	6,316.92	0.4

## Meadowbrook StormCAD.stsw

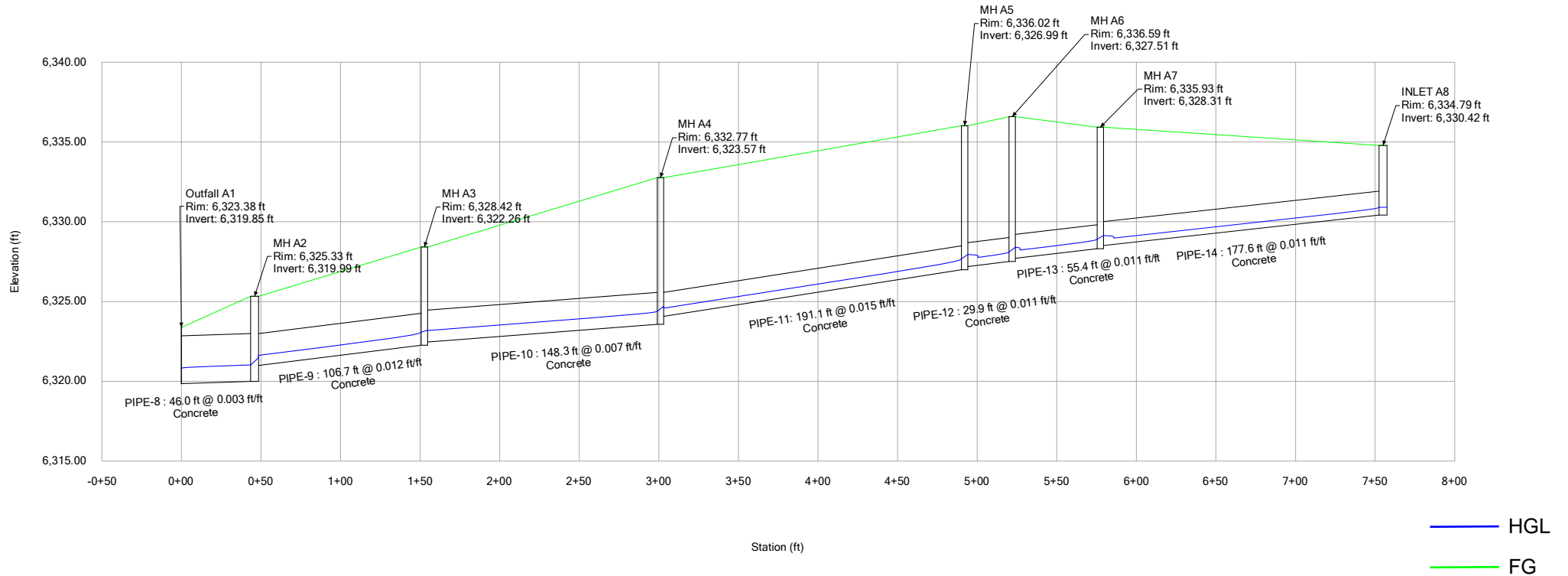
**Active Scenario: 5 YR**

**FlexTable: Manhole Table**

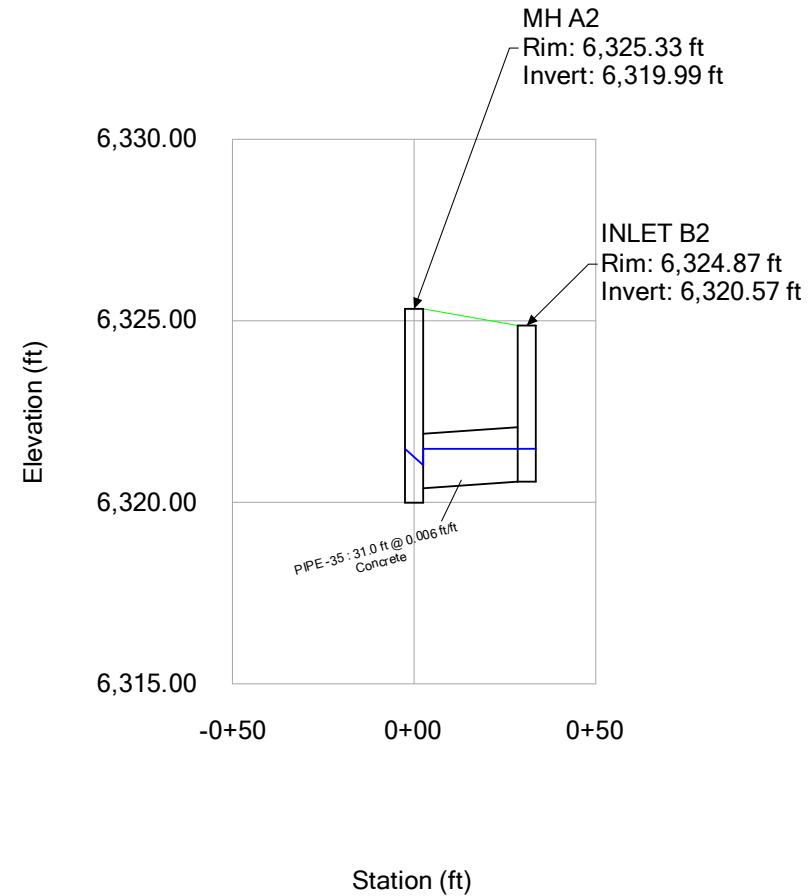
Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Elevation (Invert Out) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Headloss Method	Headloss Coefficient (Standard)
6,336.59	6,336.59	6,327.51	6,327.51	2.48	6,328.11	6,328.40	Standard	1.320
6,336.02	6,336.02	6,326.99	6,326.99	3.25	6,327.68	6,327.95	Standard	1.020
6,335.93	6,335.93	6,328.31	6,328.31	2.48	6,328.91	6,329.13	Standard	1.020
6,332.77	6,332.77	6,323.57	6,323.57	5.41	6,324.39	6,324.71	Standard	1.020
6,329.46	6,329.46	6,324.90	6,324.90	2.16	6,325.46	6,325.77	Standard	1.520
6,328.42	6,328.42	6,322.26	6,322.26	5.41	6,323.08	6,323.20	Standard	0.400
6,325.33	6,325.33	6,319.99	6,319.99	9.42	6,321.02	6,321.47	Standard	1.520
6,324.21	6,324.21	6,320.47	6,320.47	2.63	6,321.49	6,321.56	Standard	1.020
6,323.40	6,323.40	6,317.16	6,317.16	10.79	6,318.26	6,318.69	Standard	1.020
6,321.76	6,321.76	6,315.01	6,315.01	10.79	6,316.92	6,316.92	Standard	0.040
6,320.86	6,320.86	6,314.44	6,314.44	10.82	6,316.87	6,316.92	Standard	1.020



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE A (Meadowbrook StormCAD.stsw)**



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE B (Meadowbrook StormCAD.stsw)**



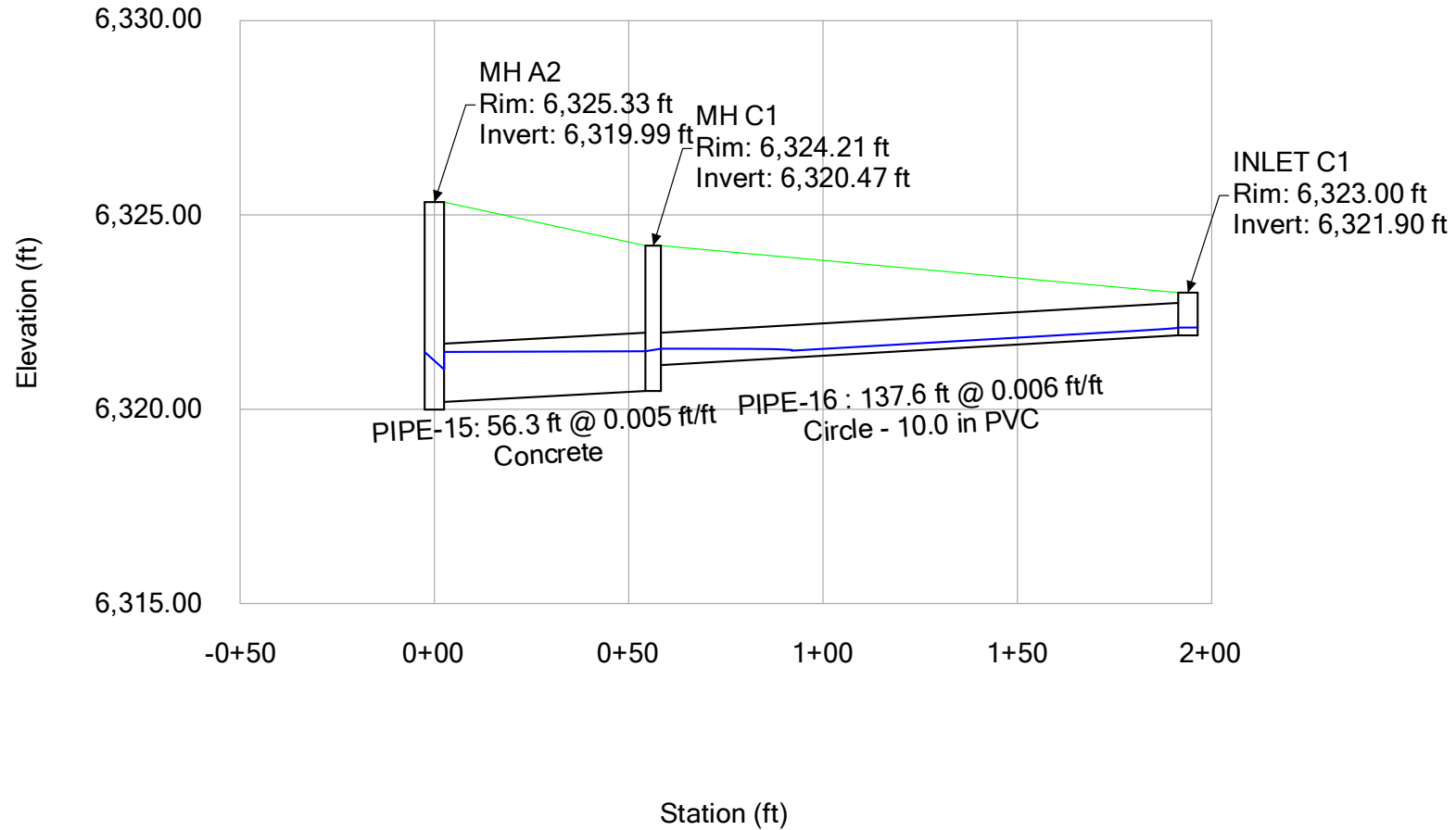
— HGL  
— FG

# Meadowbrook StormCAD.stsw

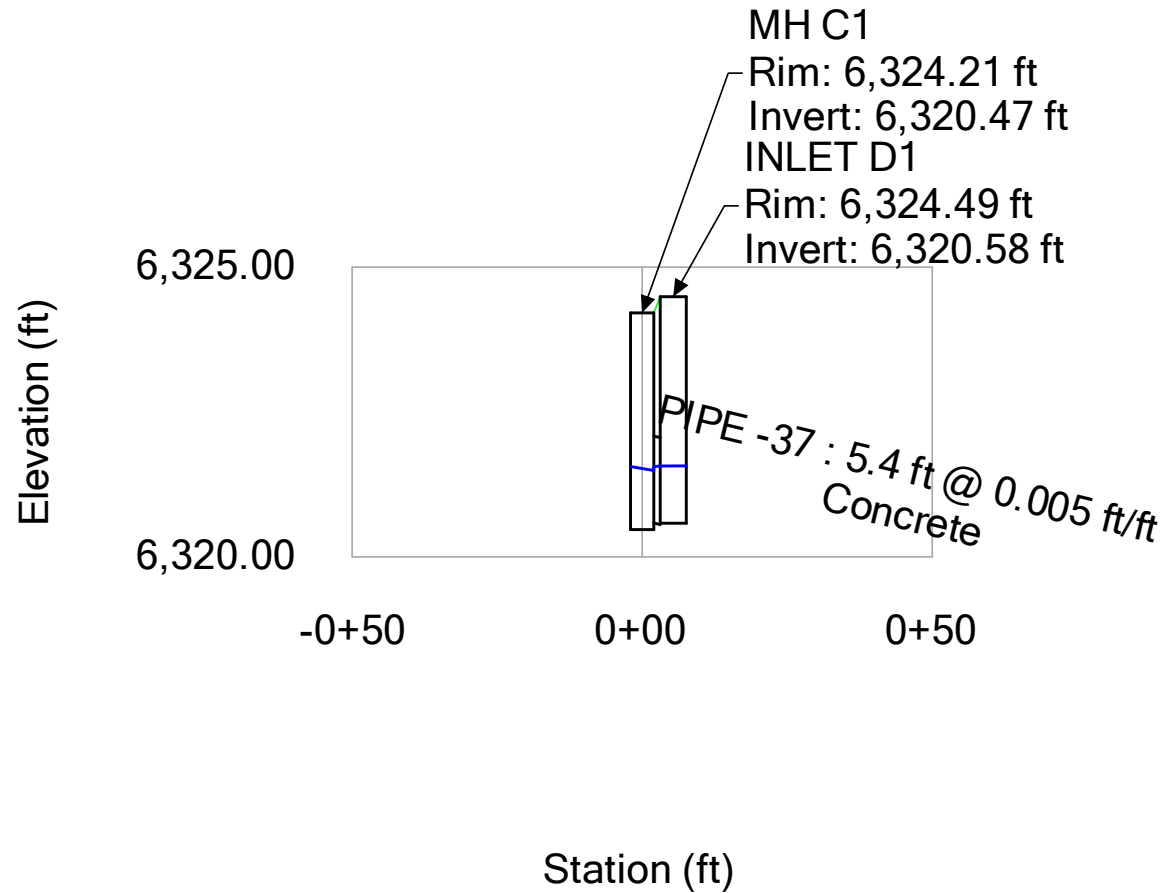
Active Scenario: 5 YR

## Profile Report

### Engineering Profile - STRM LINE C (Meadowbrook StormCAD.stsw)



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE D (Meadowbrook StormCAD.stsw)**



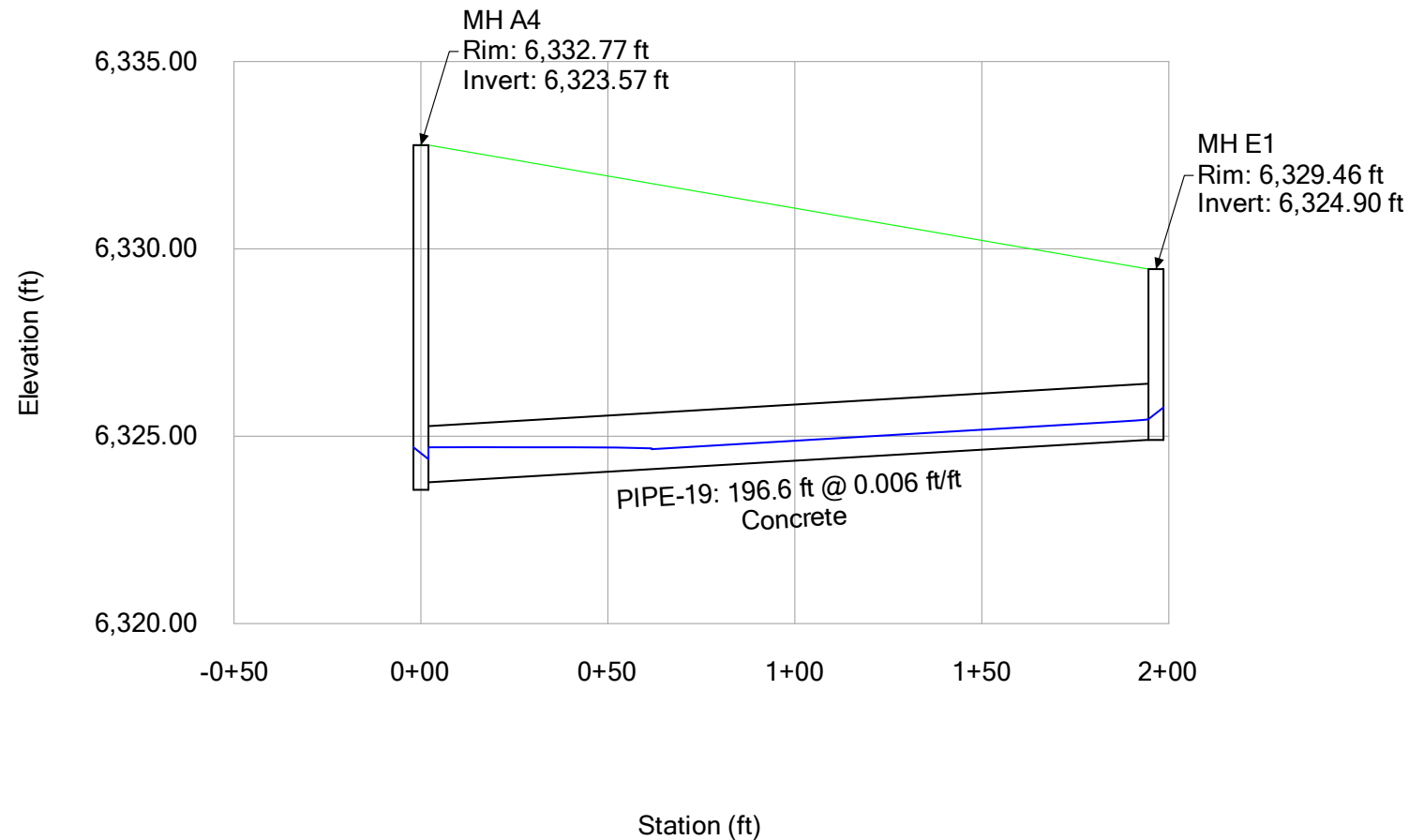
— HGL  
— FG

# Meadowbrook StormCAD.stsw

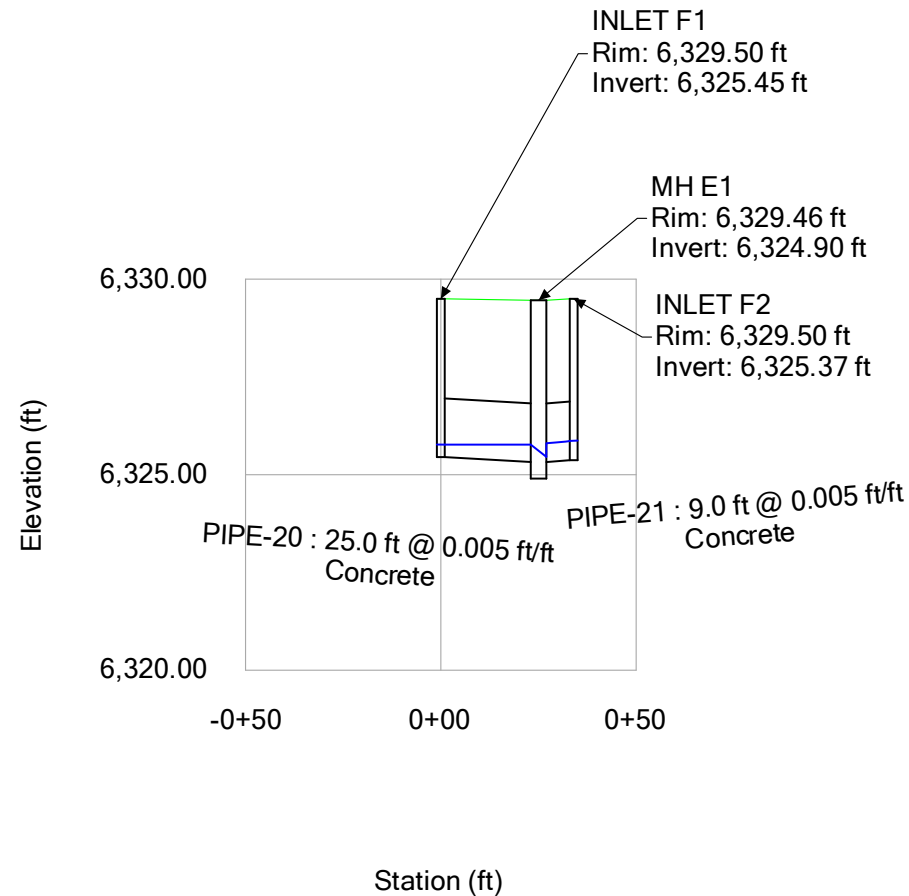
Active Scenario: 5 YR

## Profile Report

### Engineering Profile - STRM LINE E (Meadowbrook StormCAD.stsw)

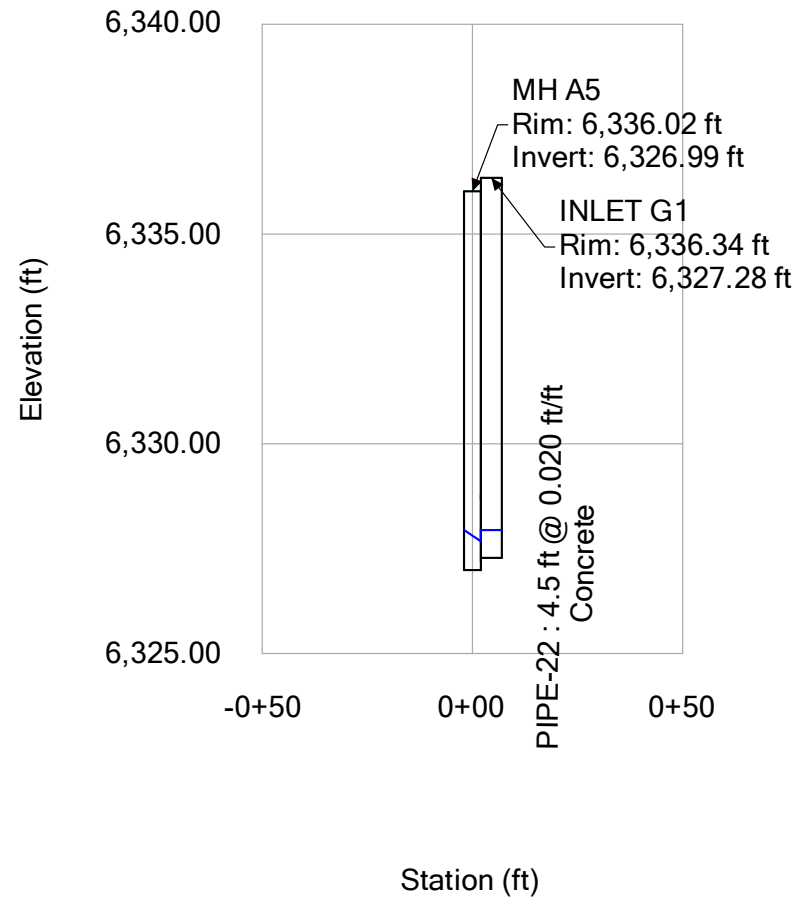


**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE F (Meadowbrook StormCAD.stsw)**



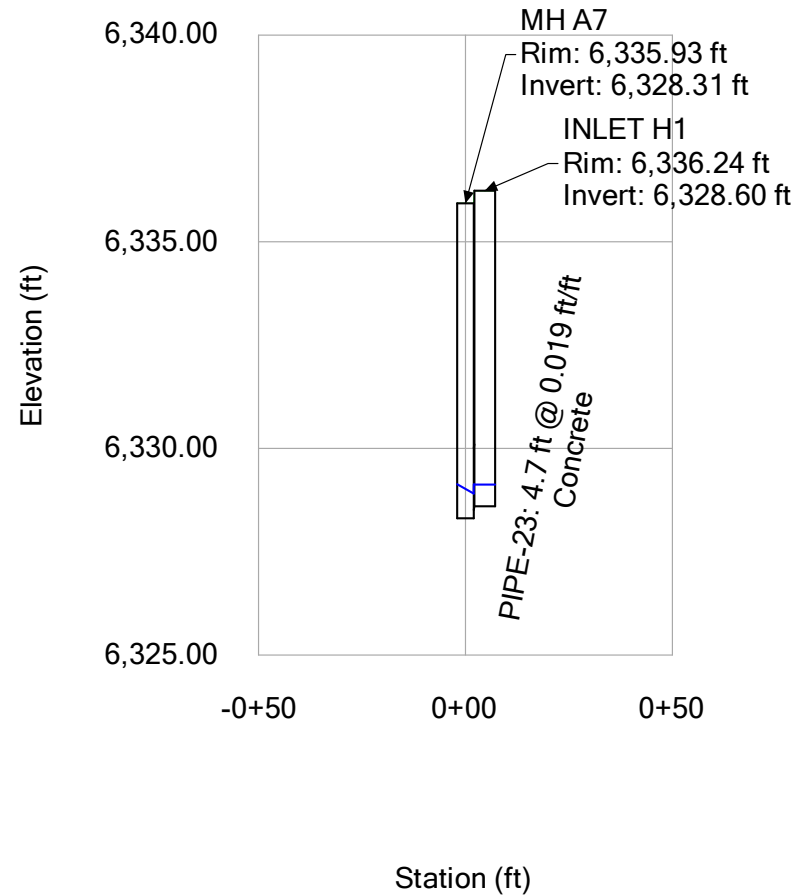
— HGL  
— FG

**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE G (Meadowbrook StormCAD.stsw)**



— HGL  
— FG

**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE H (Meadowbrook StormCAD.stsw)**



— HGL  
 — FG

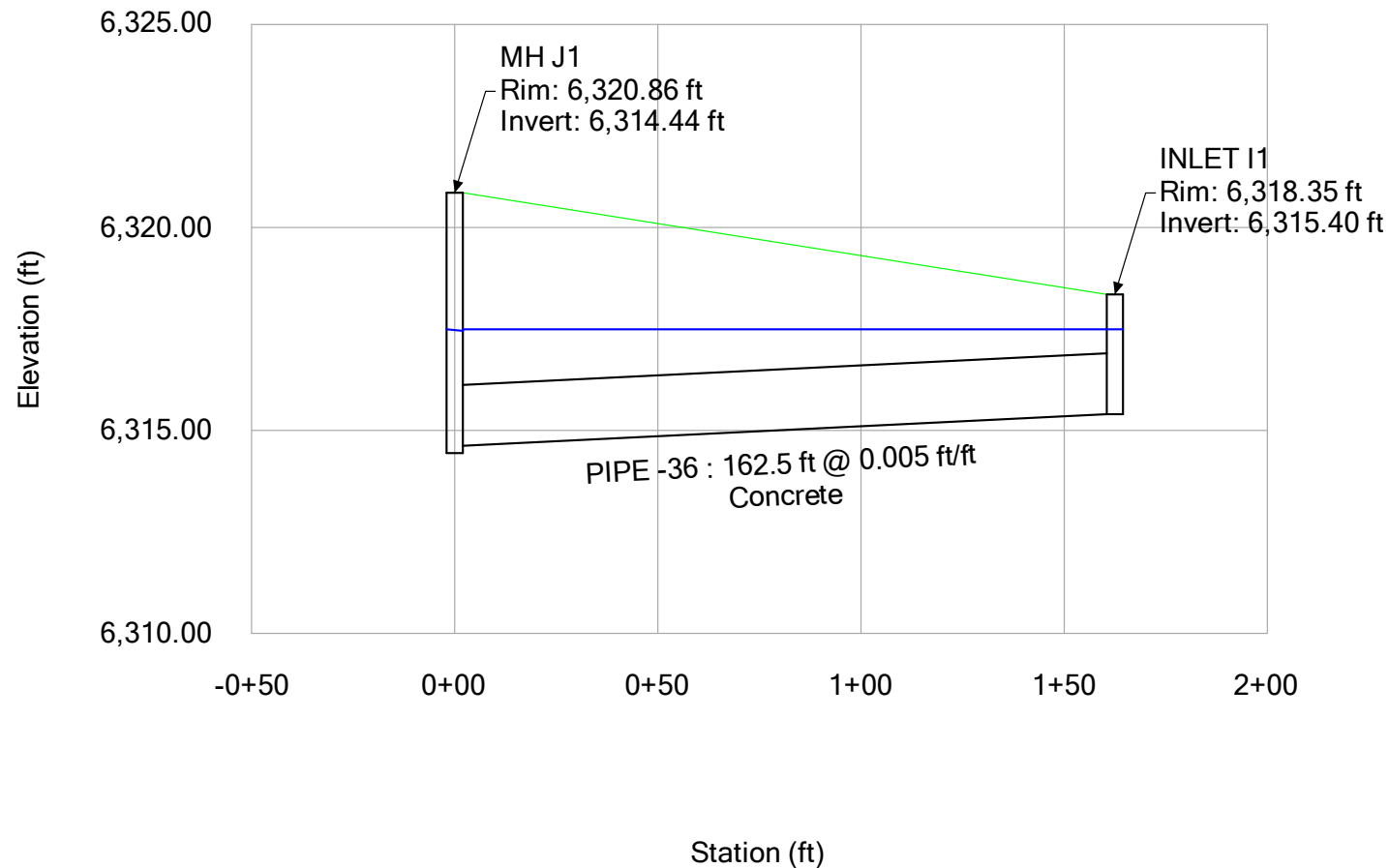


# Meadowbrook StormCAD.stsw

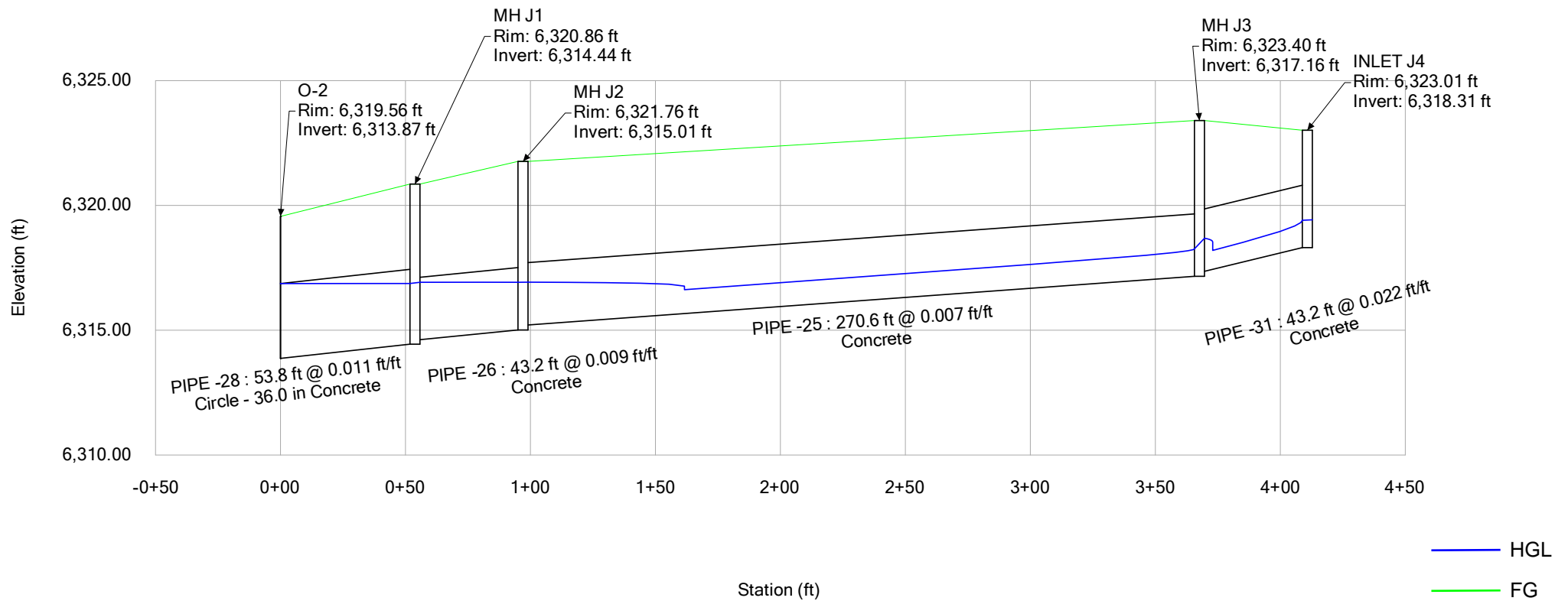
Active Scenario: 5 YR

## Profile Report

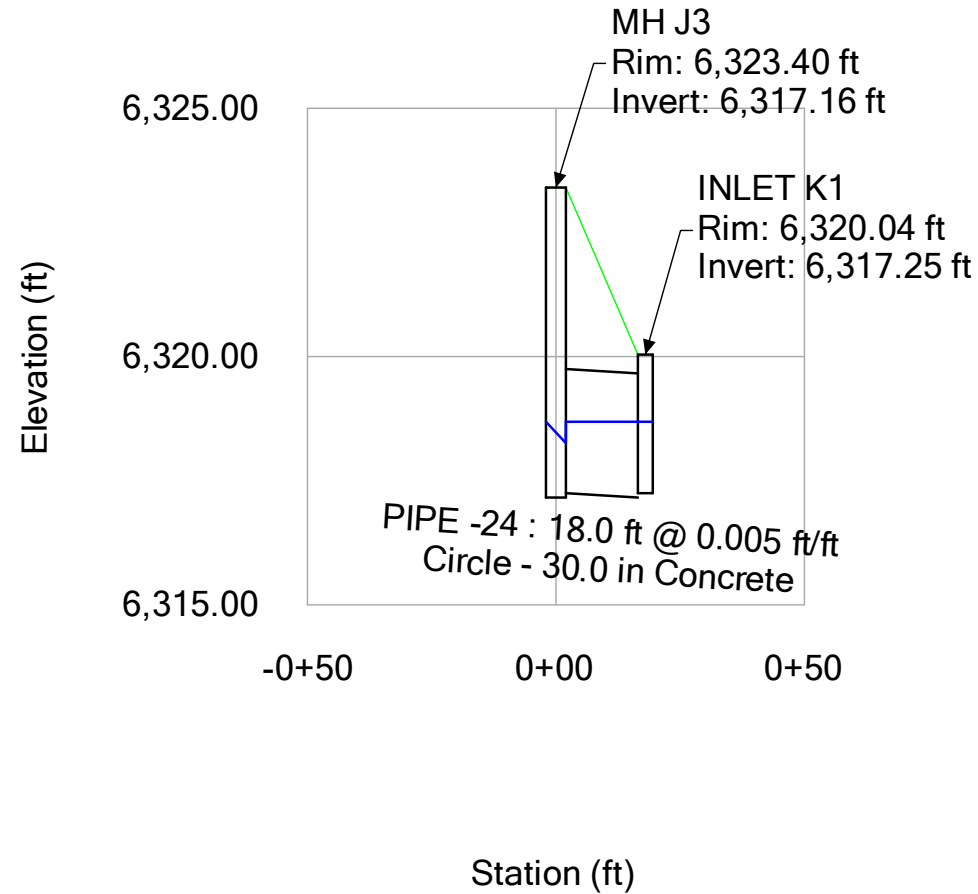
### Engineering Profile - STRM LINE I (Meadowbrook StormCAD.stsw)



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE J (Meadowbrook StormCAD.stsw)**



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 5 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE K (Meadowbrook StormCAD.stsw)**



## Meadowbrook StormCAD.stsw

**Active Scenario: 100 YR**

### FlexTable: Catch Basin Table

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow (Total Out) (cfs)	Headloss Coefficient (Standard)
INLET A8	6,334.79	6,330.42	6,331.21	6,331.20	4.10	0.050
INLET B2	6,324.87	6,320.57	6,322.31	6,322.31	2.80	0.050
INLET C1	6,323.00	6,321.90	6,322.90	6,322.89	1.20	0.050
INLET D1	6,324.49	6,320.58	6,322.67	6,322.66	4.76	0.050
INLET F1	6,329.50	6,325.45	6,326.27	6,326.27	0.80	0.050
INLET F2	6,329.50	6,325.37	6,326.29	6,326.28	4.02	0.050
INLET G1	6,336.34	6,327.28	6,328.51	6,328.51	1.53	0.050
INLET H1	6,336.24	6,328.60	6,329.63	6,329.63	1.60	0.050
INLET I1	6,318.35	6,315.40	6,317.23	6,317.23	0.03	0.050
INLET J4	6,323.01	6,318.31	6,320.00	6,319.96	23.54	0.050
INLET K1	6,320.04	6,317.25	6,319.87	6,319.87	5.10	0.050

## Meadowbrook StormCAD.stsw

**Active Scenario: 100 YR**

### FlexTable: Conduit Table

Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)
MH A7	MH A6	6,328.31	6,327.71	0.011	18.0	0.013	5.70	6.25	10.93
MH A6	MH A5	6,327.51	6,327.19	0.011	18.0	0.013	5.70	6.23	10.87
INLET G1	MH A5	6,327.28	6,327.19	0.020	18.0	0.013	1.53	5.42	14.85
INLET H1	MH A7	6,328.60	6,328.51	0.019	18.0	0.013	1.60	5.42	14.59
MH A5	MH A4	6,326.99	6,324.07	0.015	18.0	0.013	7.23	7.55	12.98
INLET A8	MH A7	6,330.42	6,328.51	0.011	18.0	0.013	4.10	5.73	10.89
MH E1	MH A4	6,324.90	6,323.77	0.006	18.0	0.013	4.82	4.72	7.97
MH A4	MH A3	6,323.57	6,322.46	0.007	24.0	0.013	12.05	6.55	19.57
INLET F1	MH E1	6,325.45	6,325.32	0.005	18.0	0.013	0.80	2.75	7.46
INLET F2	MH E1	6,325.37	6,325.32	0.005	18.0	0.013	4.02	4.39	7.68
MH A3	MH A2	6,322.26	6,320.99	0.012	24.0	0.013	12.05	7.81	24.68
MH A2	Outfall A1	6,319.99	6,319.85	0.003	36.0	0.013	20.81	5.37	36.79
MH C1	MH A2	6,320.47	6,320.19	0.005	18.0	0.013	5.96	3.37	7.42
INLET B2	MH A2	6,320.57	6,320.39	0.006	18.0	0.013	2.80	1.58	8.05
MH C1	INLET D1	6,320.58	6,320.56	0.005	18.0	0.013	4.76	2.69	7.45
INLET C1	MH C1	6,321.90	6,321.14	0.006	10.0	0.010	1.20	2.20	2.13
MH J3	INLET K1	6,317.25	6,317.16	0.005	30.0	0.013	5.10	1.04	29.00
MH J3	MH J2	6,317.16	6,315.21	0.007	30.0	0.013	28.64	7.92	34.82
INLET J4	MH J3	6,318.31	6,317.36	0.022	30.0	0.013	23.54	11.60	60.85
MH J2	MH J1	6,315.01	6,314.62	0.009	30.0	0.013	28.64	8.68	38.96
MH J1	O-2	6,314.44	6,313.87	0.011	36.0	0.013	28.67	9.28	68.65
INLET I1	MH J1	6,315.40	6,314.62	0.005	18.0	0.013	0.03	0.02	7.28

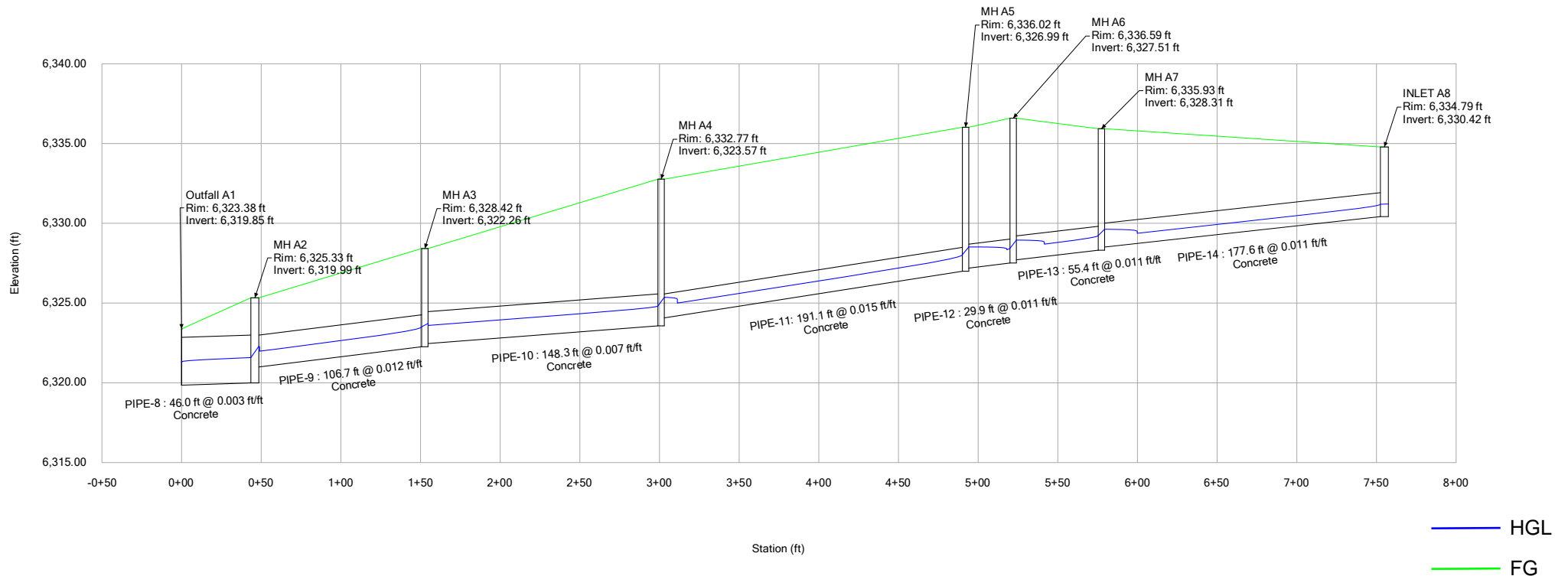
**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**FlexTable: Conduit Table**

Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow / Capacity (Design) (%)
6,329.23	6,328.95	52.1
6,328.43	6,328.51	52.4
6,328.51	6,328.51	10.3
6,329.63	6,329.63	11.0
6,328.03	6,325.36	55.7
6,331.20	6,329.63	37.6
6,325.75	6,325.36	60.5
6,324.82	6,323.72	61.6
6,326.27	6,326.27	10.7
6,326.28	6,326.27	52.4
6,323.51	6,322.29	48.8
6,321.58	6,321.32	56.6
6,322.47	6,322.29	80.3
6,322.31	6,322.29	34.8
6,322.66	6,322.65	63.9
6,322.89	6,322.65	56.4
6,319.87	6,319.87	17.6
6,318.98	6,317.44	82.3
6,319.96	6,319.87	38.7
6,317.42	6,317.23	73.5
6,316.88	6,316.87	41.8
6,317.23	6,317.23	0.4

**Meadowbrook StormCAD.stsw****Active Scenario: 100 YR****FlexTable: Manhole Table**

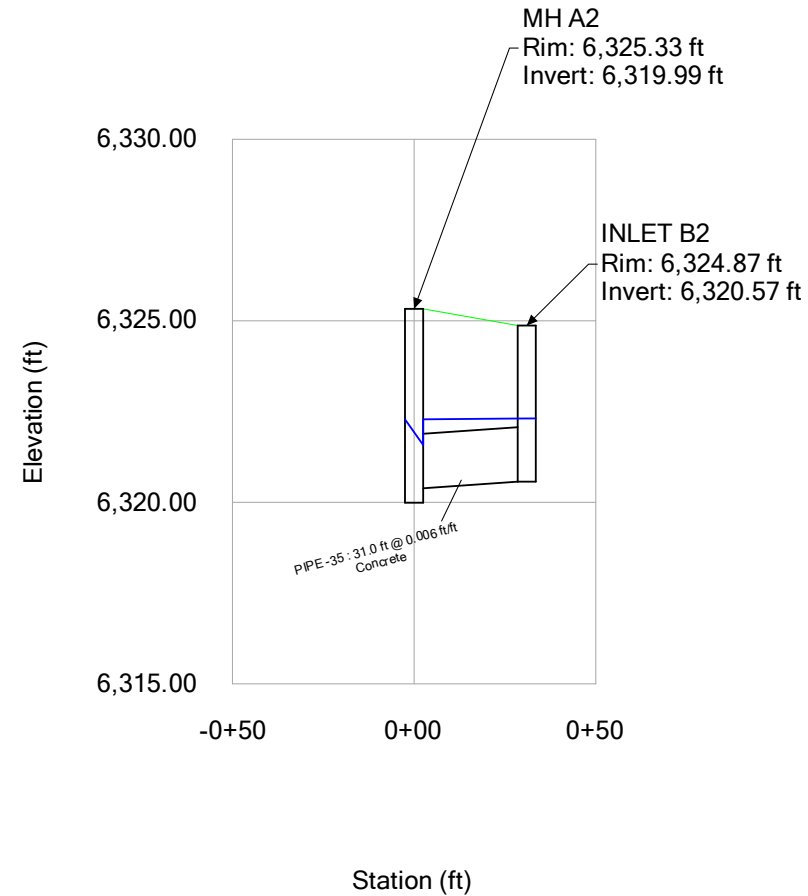
Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Elevation (Invert Out) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Headloss Method	Headloss Coefficient (Standard)
6,336.59	6,336.59	6,327.51	6,327.51	5.70	6,328.43	6,328.95	Standard	1.320
6,336.02	6,336.02	6,326.99	6,326.99	7.23	6,328.03	6,328.51	Standard	1.020
6,335.93	6,335.93	6,328.31	6,328.31	5.70	6,329.23	6,329.63	Standard	1.020
6,332.77	6,332.77	6,323.57	6,323.57	12.05	6,324.82	6,325.36	Standard	1.020
6,329.46	6,329.46	6,324.90	6,324.90	4.82	6,325.75	6,326.27	Standard	1.520
6,328.42	6,328.42	6,322.26	6,322.26	12.05	6,323.51	6,323.72	Standard	0.400
6,325.33	6,325.33	6,319.99	6,319.99	20.81	6,321.58	6,322.29	Standard	1.520
6,324.21	6,324.21	6,320.47	6,320.47	5.96	6,322.47	6,322.65	Standard	1.020
6,323.40	6,323.40	6,317.16	6,317.16	28.64	6,318.98	6,319.87	Standard	1.020
6,321.76	6,321.76	6,315.01	6,315.01	28.64	6,317.42	6,317.44	Standard	0.040
6,320.86	6,320.86	6,314.44	6,314.44	28.67	6,316.88	6,317.23	Standard	1.020

**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE A (Meadowbrook StormCAD.stsw)**





**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE B (Meadowbrook StormCAD.stsw)**



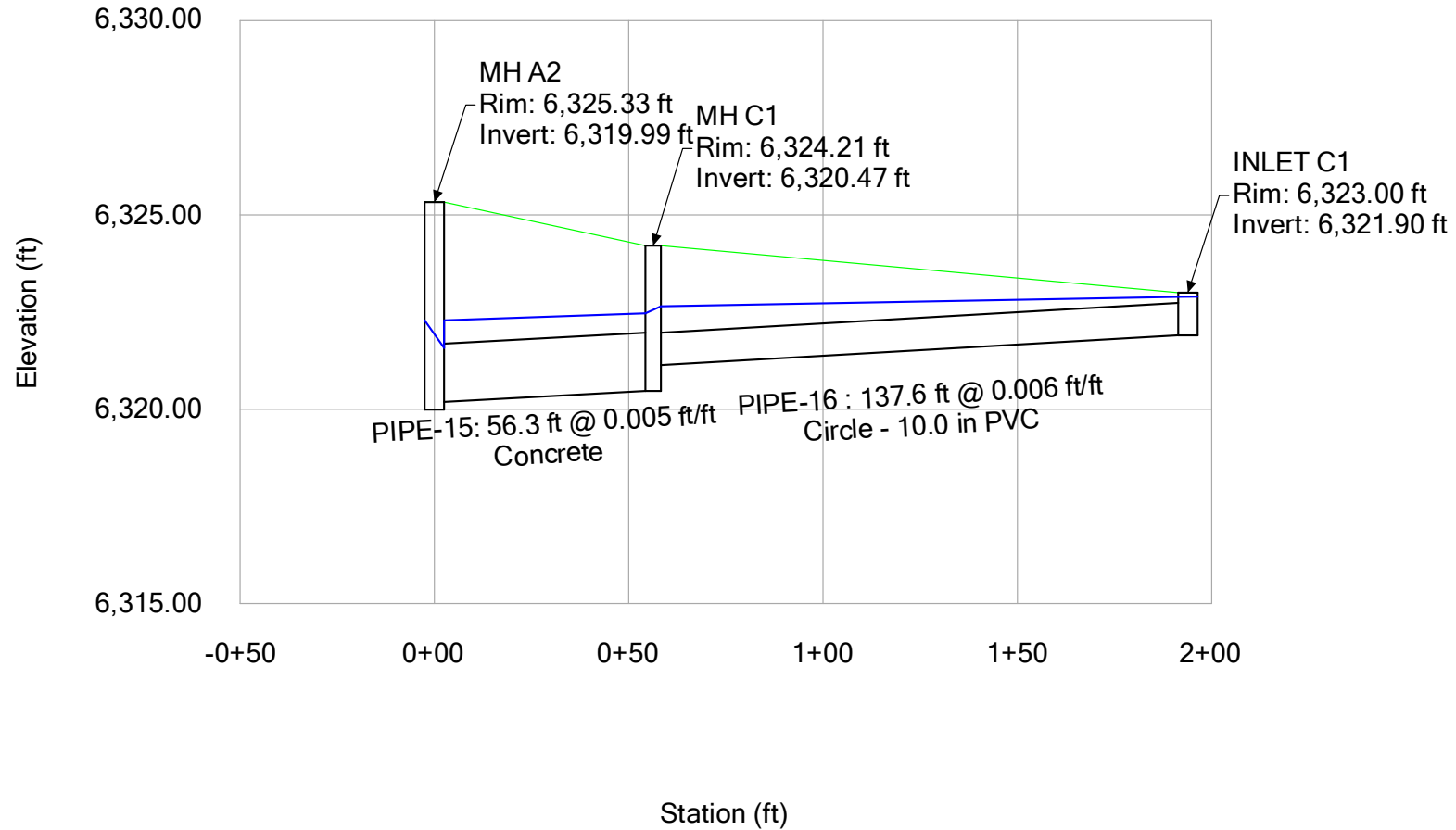
— HGL  
— FG

# Meadowbrook StormCAD.stsw

Active Scenario: 100 YR

## Profile Report

### Engineering Profile - STRM LINE C (Meadowbrook StormCAD.stsw)

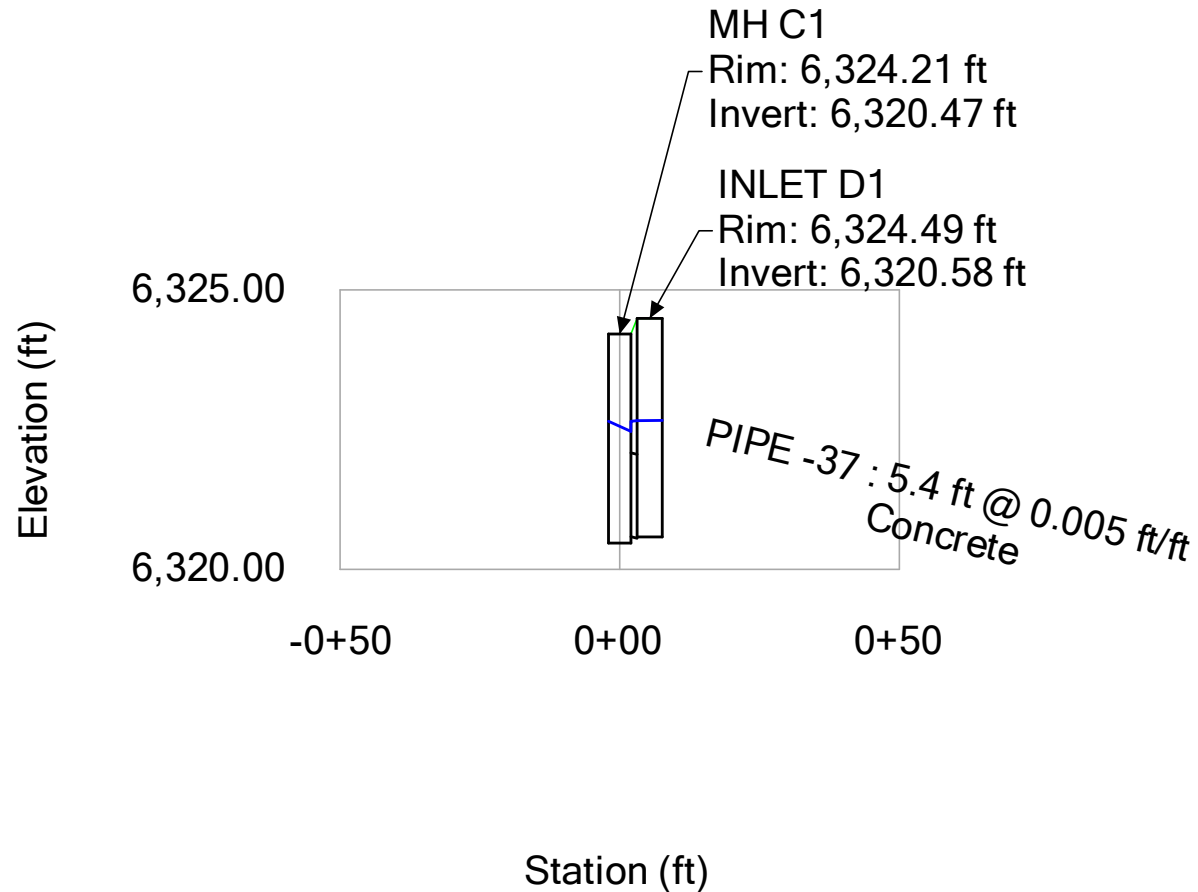


**Meadowbrook StormCAD.stsw**

**Active Scenario: 100 YR**

**Profile Report**

**Engineering Profile - STRM LINE D (Meadowbrook StormCAD.stsw)**

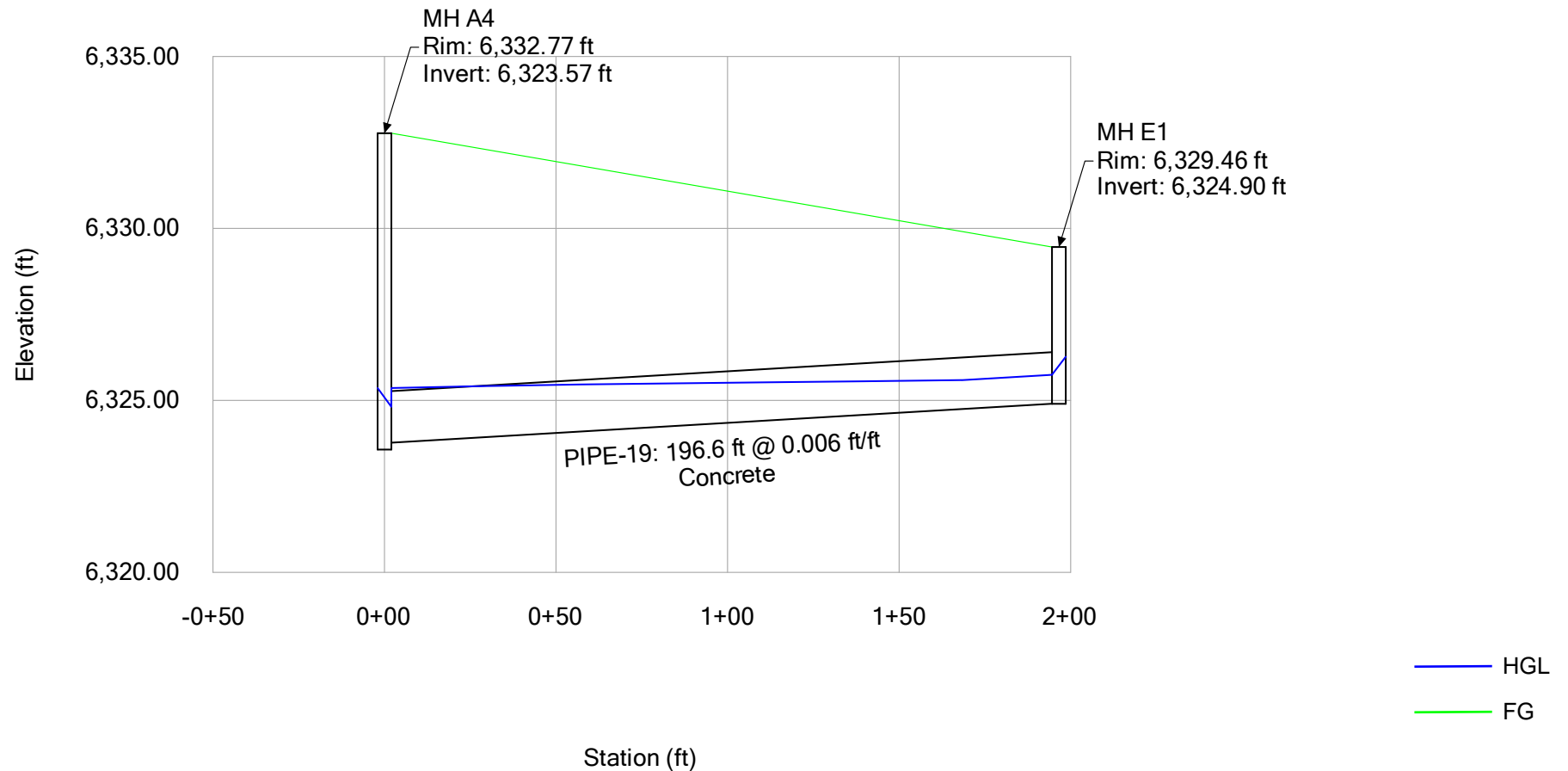


# Meadowbrook StormCAD.stsw

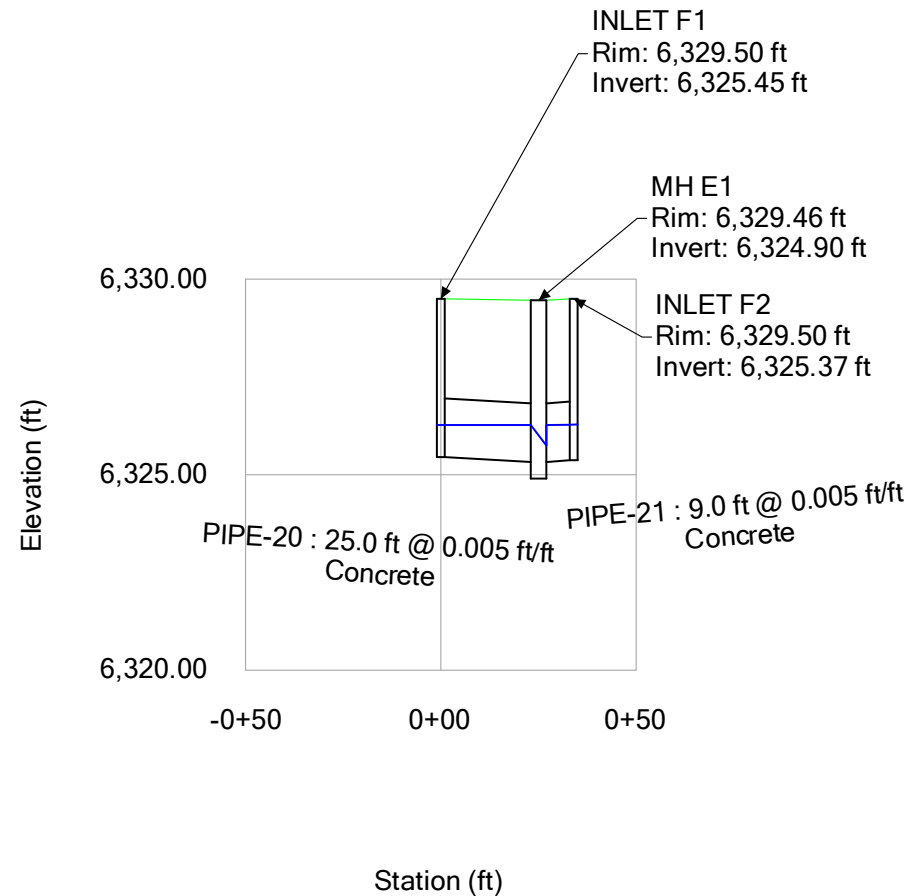
Active Scenario: 100 YR

## Profile Report

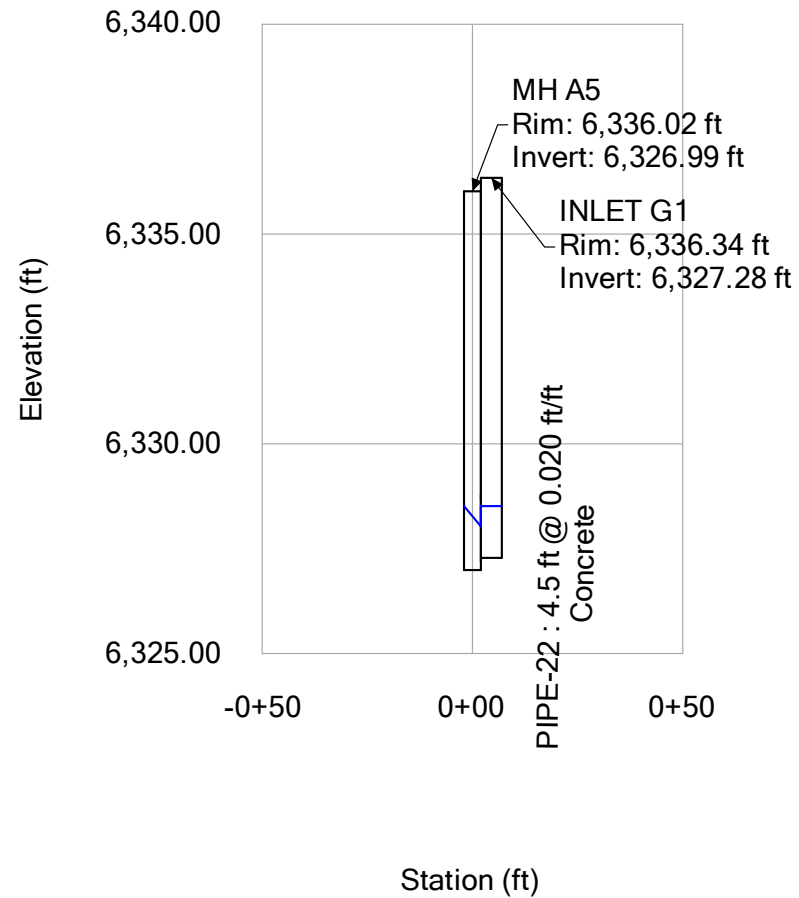
### Engineering Profile - STRM LINE E (Meadowbrook StormCAD.stsw)



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE F (Meadowbrook StormCAD.stsw)**

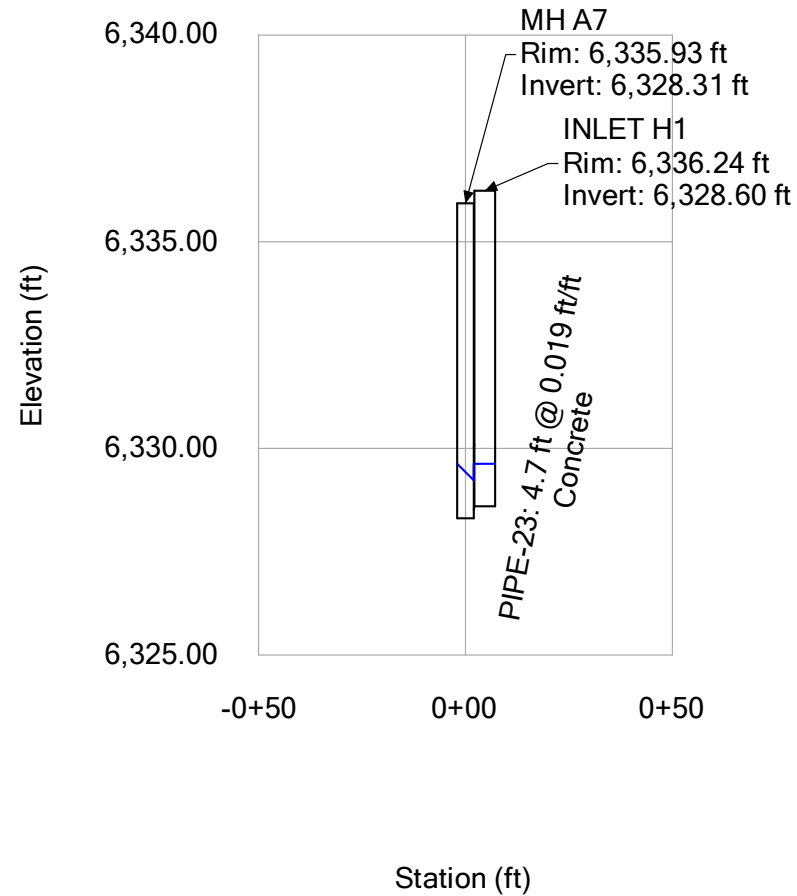


**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE G (Meadowbrook StormCAD.stsw)**



— HGL  
— FG

**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE H (Meadowbrook StormCAD.stsw)**



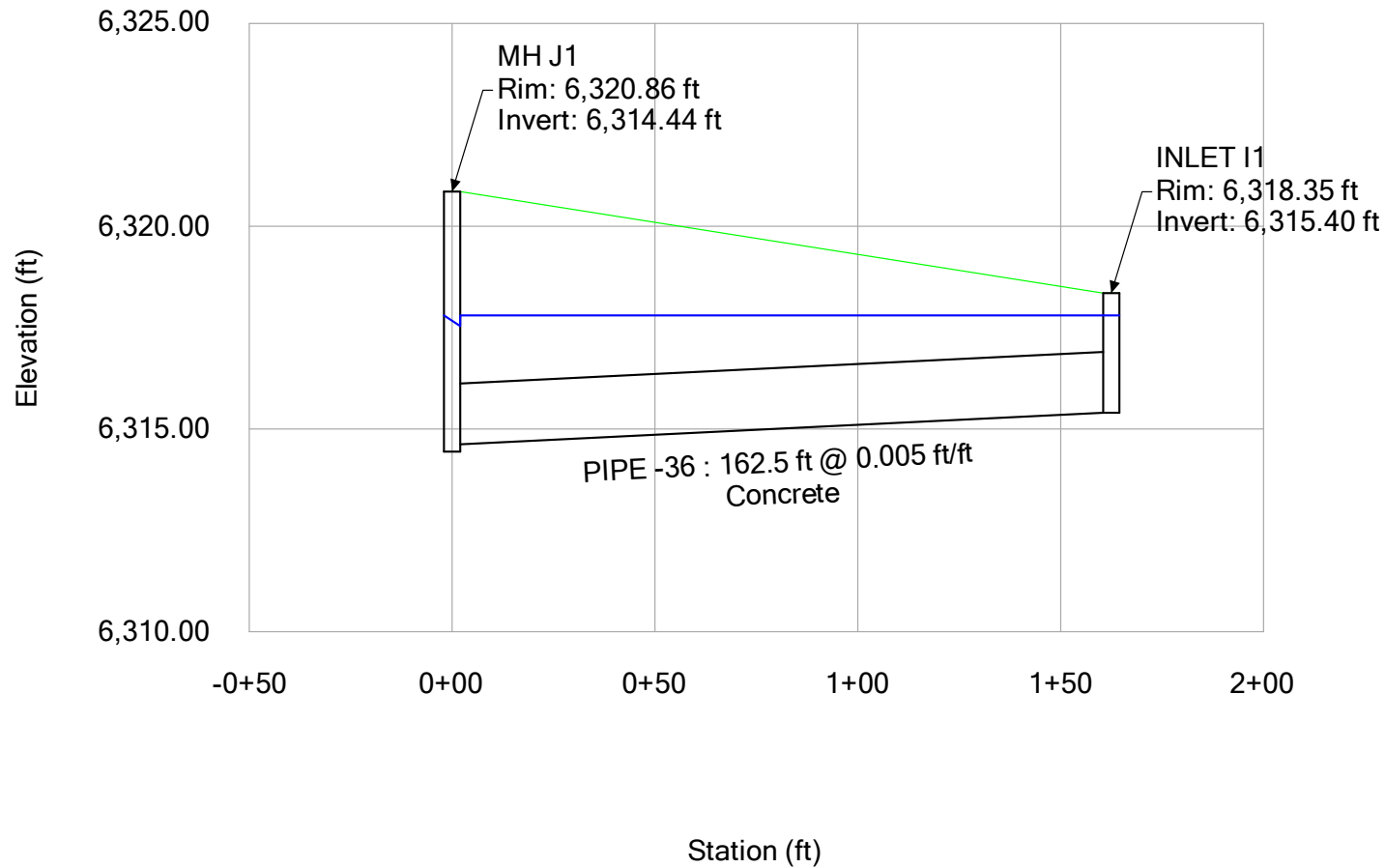
— HGL  
— FG

# Meadowbrook StormCAD.stsw

Active Scenario: 100 YR

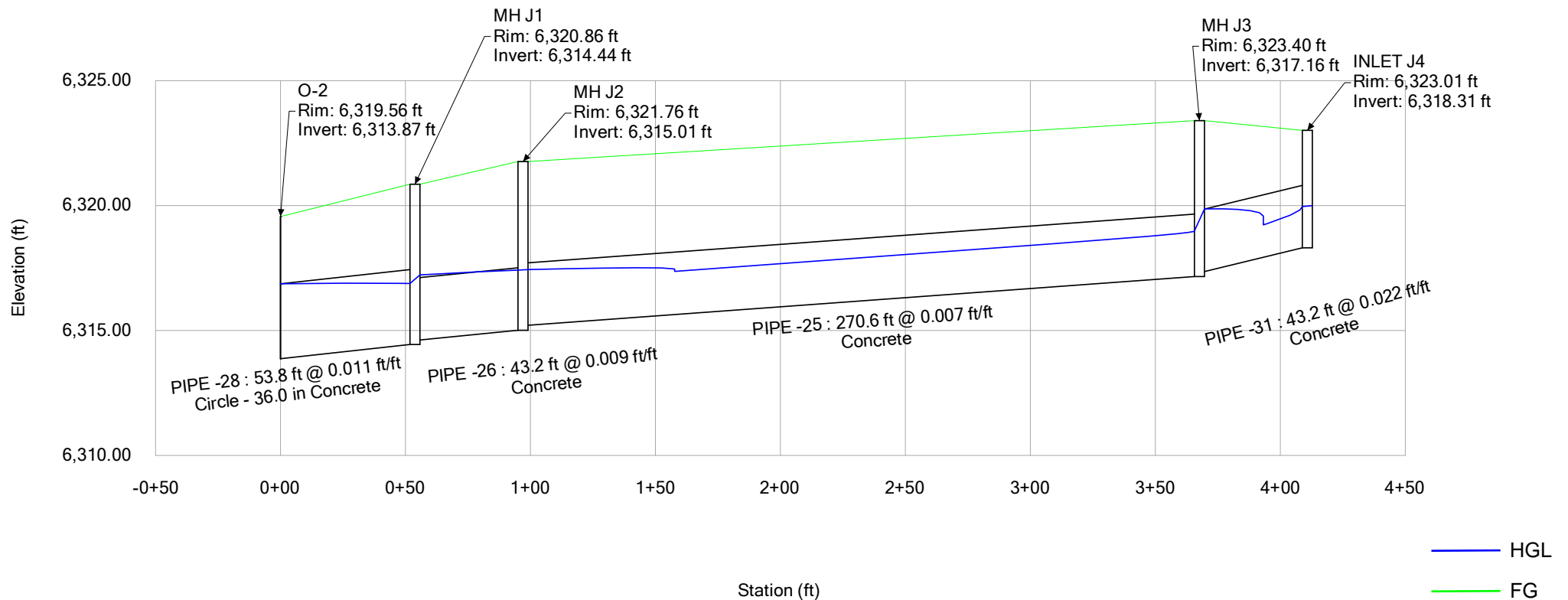
## Profile Report

### Engineering Profile - STRM LINE I (Meadowbrook StormCAD.stsw)

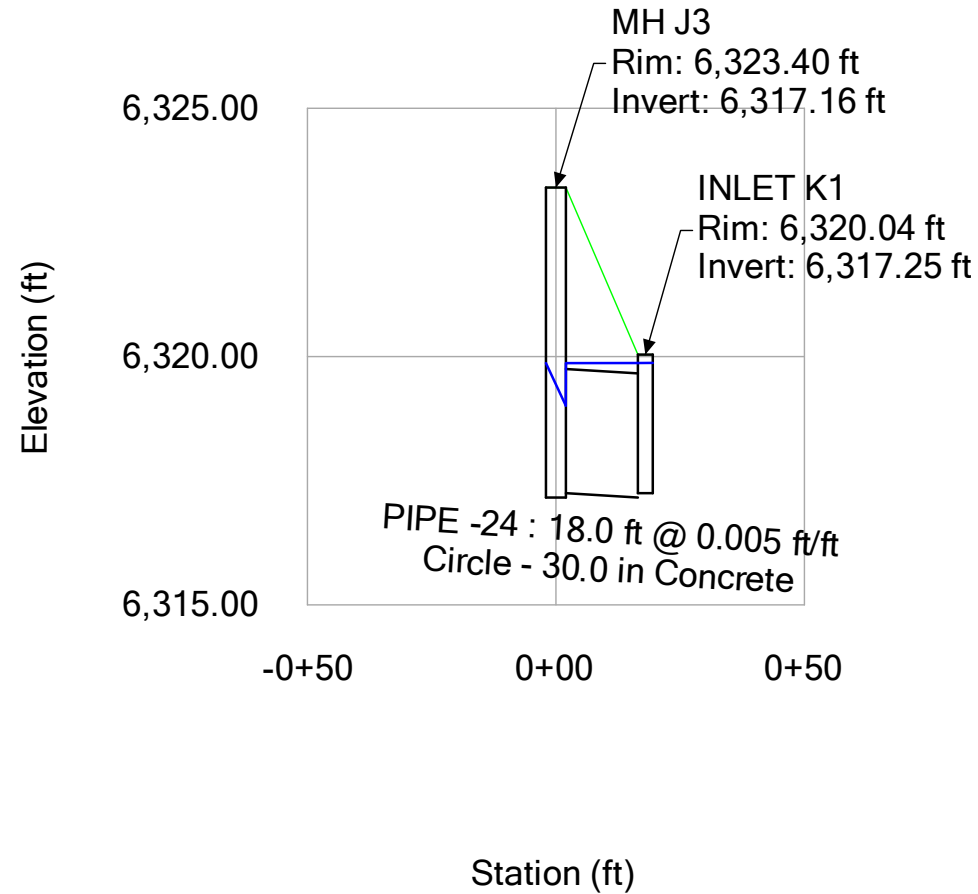




**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE J (Meadowbrook StormCAD.stsw)**



**Meadowbrook StormCAD.stsw**  
**Active Scenario: 100 YR**  
**Profile Report**  
**Engineering Profile - STRM LINE K (Meadowbrook StormCAD.stsw)**



— HGL  
— FG

***OPINION OF PROBABLE CONSTRUCTION COST***



Kimley-Horn &amp; Associates, Inc.

Opinion of Probable Construction Cost

<b>Client:</b> Meadowbrook Development, LLC	<b>Date:</b> 4/21/2022
<b>Project:</b> Meadowbrook Park	<b>Prepared By:</b> KRK
<b>KHA No.:</b> 096956009	<b>Checked By:</b> JRH

Sheet: 1 of 1

This OPC is not intended for basing financial decisions, or securing funding. Review all notes and assumptions. Since Kimley-Horn & Associates, Inc. has no control over the cost of labor, materials, equipment, or services furnished by others, or over methods of determining price, or over competitive bidding or market conditions, any and all opinions as to the cost herein, including but not limited to opinions as to the costs of construction materials, shall be made on the basis of experience and best available data. Kimley-Horn & Associates, Inc. cannot and does not guarantee that proposals, bids, or actual costs will not vary from the opinions on costs shown herein. The total costs and other numbers in this Opinion of Probable Cost have been rounded.

Item No.	Item Description	Quantity	Unit	Unit Price	Item Cost
<b>Private Storm Sewer - Non-Reimbursable</b>					
1	10" PVC	175	LF	\$32.50	\$5,688
2	10" Culvert	8	LF	\$32.50	\$260
3	18" RCP	955	LF	\$70.00	\$66,850
4	24" RCP	255	LF	\$83.00	\$21,165
5	30" RCP	377	LF	\$104.00	\$39,208
6	36" RCP	46	LF	\$128.00	\$5,888
7	5' Type R Inlet (Depth < 5')	5	EA	\$6,138.00	\$30,690
8	5' Type R Inlet (5' < Depth < 10')	2	EA	\$7,981.00	\$15,962
9	8' Type D-10-R Inlet (Depth < 5')	1	EA	\$16,000.00	\$16,000
10	CDOT Type D Inlet	2	EA	\$6,347.00	\$12,694
11	CDOT Type C Inlet	1	EA	\$5,138.00	\$5,138
12	Modified Type C Inlet	1	EA	\$10,750.00	\$10,750
13	8" Area Drain	2	EA	\$540.00	\$1,080
14	4' Type II Manhole (Eccentric, Flat)	2	EA	\$7,082.00	\$14,164
15	4' Type II Manhole (Eccentric, Cone)	3	EA	\$7,082.00	\$21,246
16	5' Type II Manhole (Eccentric, Flat)	4	EA	\$12,876.00	\$51,504
17	5' Type II Manhole (Eccentric, Cone)	2	EA	\$12,876.00	\$25,752
18	Concrete Forebay	2	EA	\$7,750.00	\$15,500
19	Concrete Trickle Channel	330	LF	\$12.00	\$3,960
20	Maintenance Road Material (CDOT Class 6 Base)	36	CY	\$95.00	\$3,420
21	Emergency Overflow (Type L Riprap)	20	CY	\$89.00	\$1,780
22	Rock Chute (Type L Riprap)	110	CY	\$89.00	\$9,790
Subtotal:					\$378,489
Contingency (%,+/-) 10%					\$37,849
<b>Project Total:</b>					<b>\$416,337</b>

## Basis for Cost Projection:

- ☐ No Design Completed  
☐ Preliminary Design  
☒ Final Design



Design Engineer:

John Heiberger  
Registered Professional Engineer, State of Colorado No. 50096

***EXISTING AND PROPOSED DRAINAGE MAP***


22/2022 10:59 AM  
MATCHLINE- SEE EXDR-2



LOT 46A CLAREMONT  
BUSINESS PARK FIL NO 2A

SUMMARY - EXISTING RUNOFF TABLE						
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100-YR RUNOFF (CFS)
1	EX-A	8.18	2.49	16.70		
2	EX-B	1.34	3.01	6.73		
3	EX-C	3.87	7.71	16.89		
TOTAL		13.39	13.21	40.32		

A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)



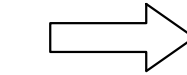
# = DESIGN POINT



FLOW DIRECTION

.....

■ DRAINAGE BASIN BOUNDARY



EMERGENCY OVERFLOW PATH

— XXXX —

— PROPOSED MAJOR CONTOUR

— XXXX —

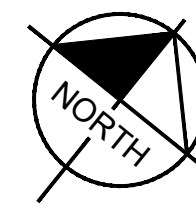
— PROPOSED MINOR CONTOUR

— EXISTING MAJOR CONTOUR

— EXISTING MINOR CONTOUR

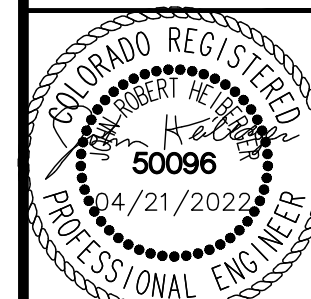
\_\_\_\_\_

— PROPERTY LINE



GRAPHIC SCALE IN FEET

0 20 40 80

A horizontal line with vertical tick marks at 0, 20, 40, and 80 feet. The segment between 0 and 20 is divided into four equal parts by three vertical lines. The segment between 20 and 40 is divided into two equal parts by one vertical line. The segment between 40 and 80 is divided into four equal parts by three vertical lines. The segments from 0 to 20 and 40 to 80 are white, while the segments from 20 to 40 and the four sub-segments within 0-20 and 40-80 are black.

**MEADOWBROOK PARK  
EL PASO COUNTY, COLORADO  
CONSTRUCTION DOCUMENTS  
EXISTING DRAINAGE MAP**

PROJECT NO.  
096956009

SHEET

EXDR-1

**Kimley»»Horn**

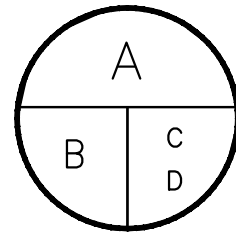
2021 KIMLEY-HORN AND ASSOCIATES, INC.  
2 North Nevada Avenue Suite 300  
Colorado Springs, Colorado 80903 (719) 451-1100

DESIGNED BY: KK  
DRAWN BY: KK  
CHECKED BY: JH  
DATE: 03/21/2022

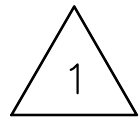


K:\COS\_Civil\096956009\_Meadowbrook\CADD\PlanSheets\096956009-EXIST DRMP.dwg Petik, Grant 4/22/2022 10:59 AM

LEGEND



A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)



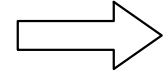
# = DESIGN POINT



FLOW DIRECTION



DRAINAGE BASIN BOUNDARY



EMERGENCY OVERFLOW PATH



PROPOSED MAJOR CONTOUR



PROPOSED MINOR CONTOUR



EXISTING MAJOR CONTOUR

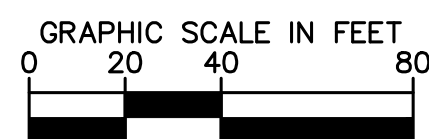
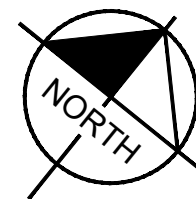
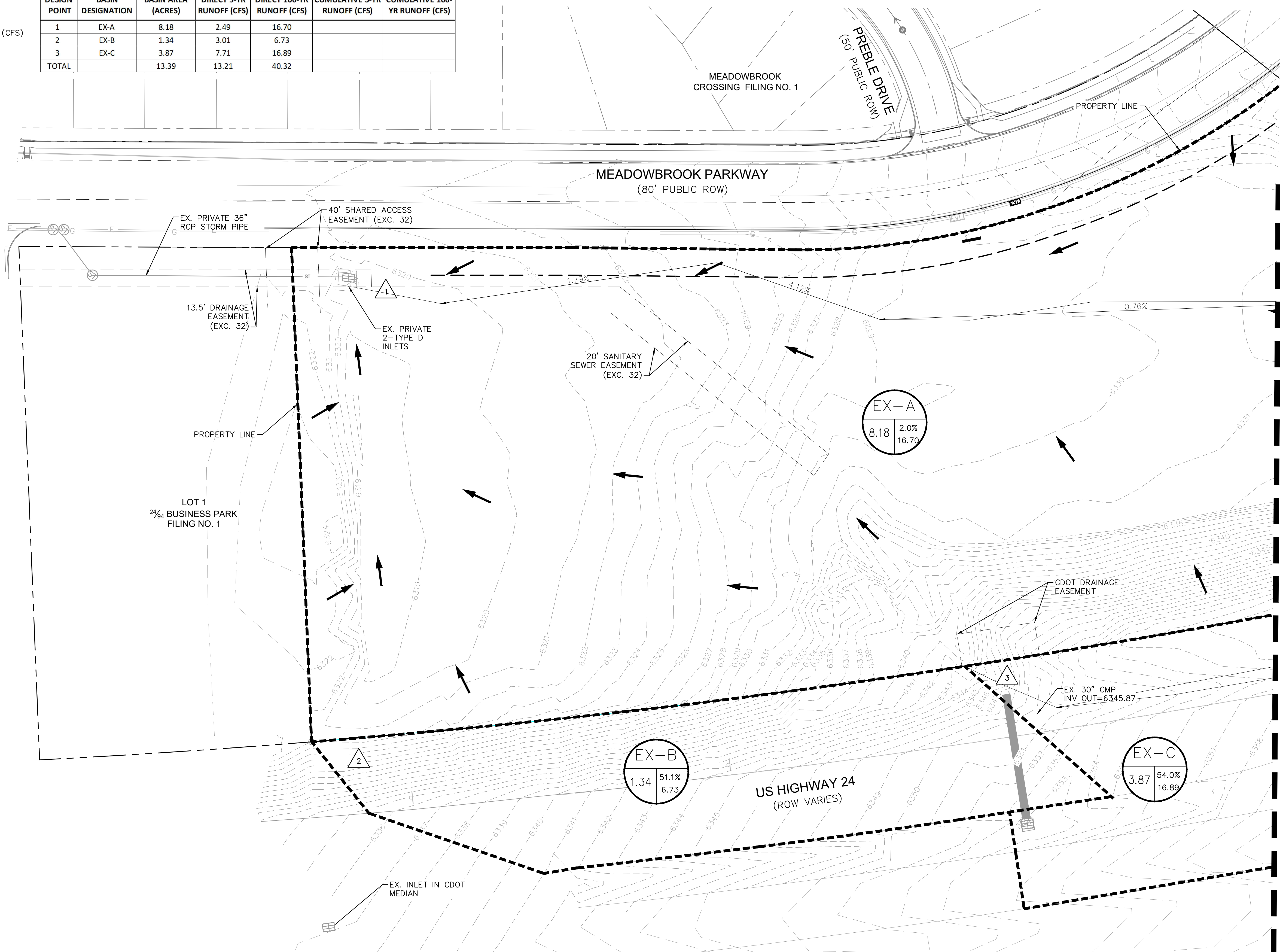


EXISTING MINOR CONTOUR



PROPERTY LINE

SUMMARY - EXISTING RUNOFF TABLE					
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)
1	EX-A	8.18	2.49	16.70	
2	EX-B	1.34	3.01	6.73	
3	EX-C	3.87	7.71	16.89	
TOTAL		13.39	13.21	40.32	



**Kimley»Horn**

2021 KIMLEY-HORN AND ASSOCIATES, INC.  
2 North Nevada Avenue Suite 300  
Colorado Springs, Colorado 80903 (719) 453-0180

DESIGNED BY: KK  
DRAWN BY: KK  
CHECKED BY: JH  
DATE: 03/21/2022

**MEADOWBROOK PARK**  
EL PASO COUNTY, COLORADO  
CONSTRUCTION DOCUMENTS  
EXISTING DRAINAGE MAP



PROJECT NO.  
096956009

SHEET

EXDR-2

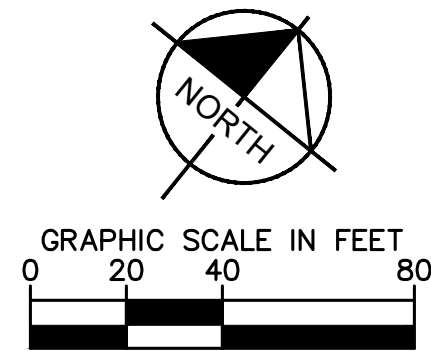
NO. BY DATE APPR.

REVISION



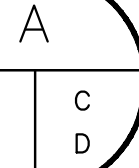
11:18 AM

MATCHLINE- SEE DR-2

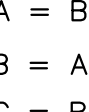


SUMMARY - PROPOSED RUNOFF TABLE						
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100-YR RUNOFF (CFS)
1	A	2.47	2.08	7.19		
2	B	1.85	4.04	8.86		
3	C	0.71	2.42	4.76		
4	D	0.37	0.21	1.20		
5	E	0.42	1.38	2.70		
6	F	0.10	0.44	0.80		
7	G	0.92	1.72	4.02		
8	H	0.83	1.66	3.85		
9	I	0.28	0.82	1.73		
10	J	0.23	0.77	1.54		
11	OS-A	1.77	3.76	8.14		
12	OS-B	1.34	3.01	6.73		
13	OS-C	2.10	3.92	8.67		
14	POND OUTFALL		0.10	5.50		
TOTAL		13.39	26.22	60.19		


## LEGEND




A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)




# = DESIGN POINT




FLOW DIRECTION




DRAINAGE BASIN BOUNDARY




EMERGENCY OVERTFLOW PATH




PROPOSED MAJOR CONTOUR




PROPOSED MINOR CONTOUR



EXISTING MAJOR CONTOUR



EXISTING MINOR CONTOUR

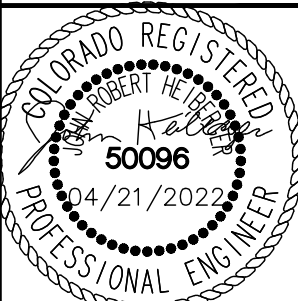


PROPERTY LINE

**Kimley»»Horn**  
2021 KIMLEY-HORN AND ASSOCIATES, INC.  
2 North Nevada Avenue Suite 300  
Colorado Springs, Colorado 80903 (719) 453-0180

DESIGNED BY: KK  
DRAWN BY: KK  
CHECKED BY: JH  
DATE: 03/21/2022

**MEADOWBROOK PARK  
EL PASO COUNTY, COLORADO  
CONSTRUCTION DOCUMENTS  
PROPOSED DRAINAGE MAP**

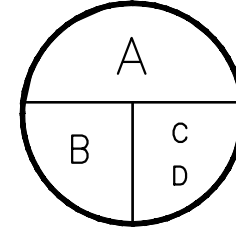


PROJECT NO. 096956009
SHEET  DR-1

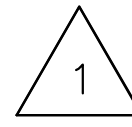


K:\COS\_Civil\096956009\_Meadowbrook\CADD\PlanSheets\096956009-PROP DRMP.dwg Petik, Grant 4/22/2022 1:50 PM

## LEGEND



A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)

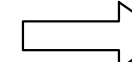


# = DESIGN POINT



FLOW DIRECTION

--- DRAINAGE BASIN BOUNDARY



EMERGENCY OVERFLOW PATH

----- PROPOSED MAJOR CONTOUR

----- PROPOSED MINOR CONTOUR

----- EXISTING MAJOR CONTOUR

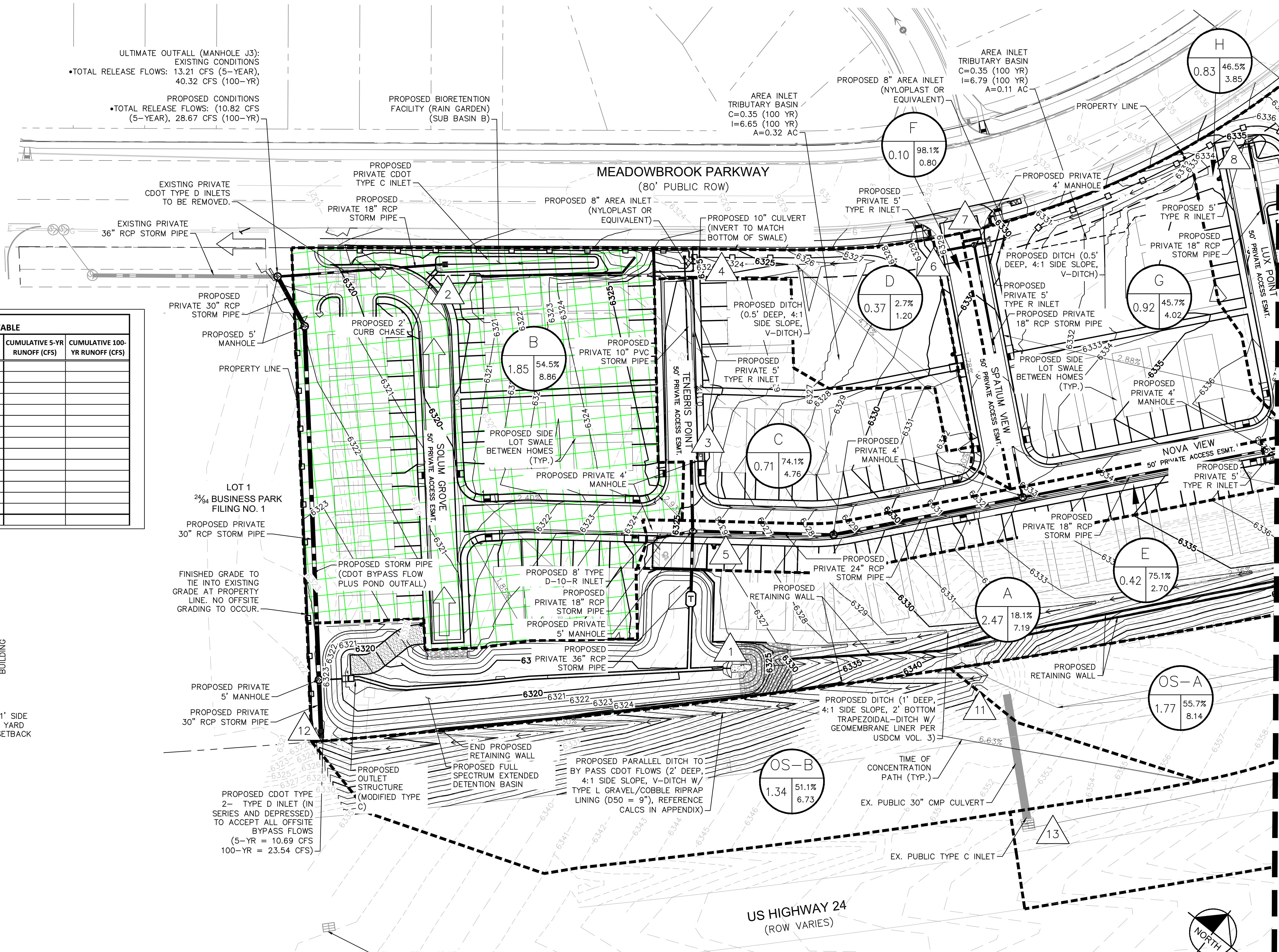
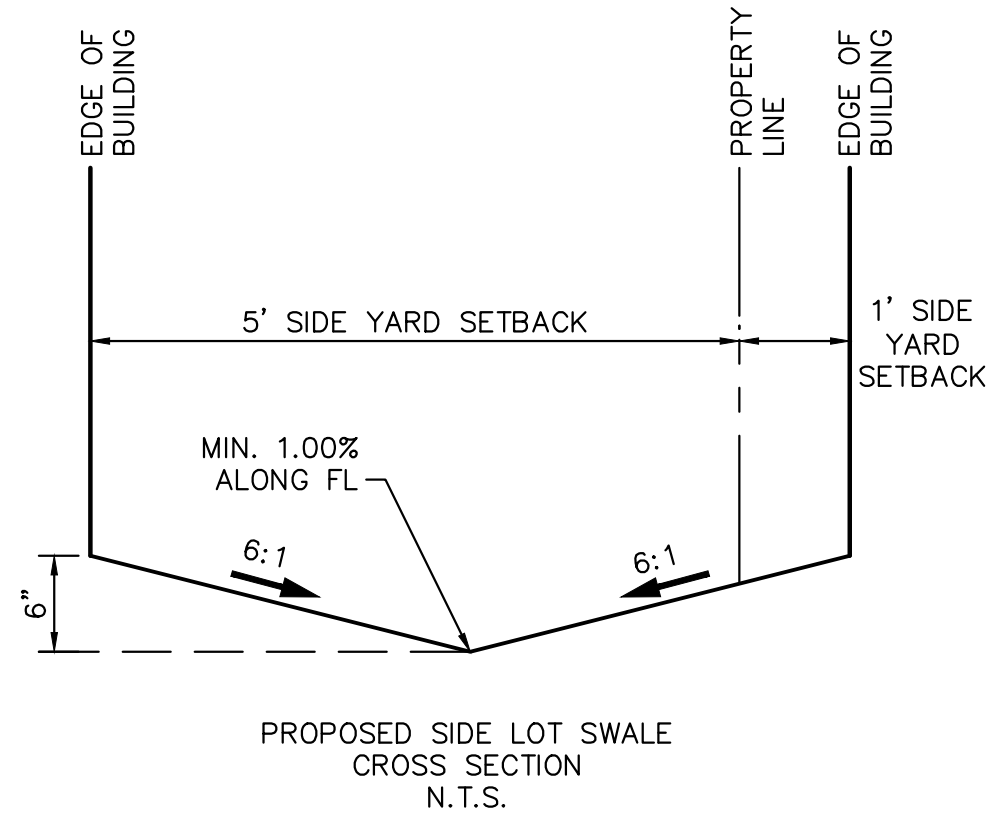
----- EXISTING MINOR CONTOUR

----- PROPERTY LINE

XXXXX RAIN GARDEN TRIBUTARY BASIN AREA

SUMMARY - PROPOSED RUNOFF TABLE

DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100-YR RUNOFF (CFS)
1	A	2.47	2.08	7.19		
2	B	1.85	4.04	8.86		
3	C	0.71	2.42	4.76		
4	D	0.37	0.21	1.20		
5	E	0.42	1.38	2.70		
6	F	0.10	0.44	0.80		
7	G	0.92	1.72	4.02		
8	H	0.83	1.66	3.85		
9	I	0.28	0.82	1.73		
10	J	0.23	0.77	1.54		
11	OS-A	1.77	3.76	8.14		
12	OS-B	1.34	3.01	6.73		
13	OS-C	2.10	3.92	8.67		
14	POND OUTFALL		0.10	5.50		
TOTAL		13.39	26.22	60.19		



**Kimley»Horn**

2021 KIMLEY-HORN AND ASSOCIATES, INC.  
2 North Nevada Avenue Suite 300  
Colorado Springs, Colorado 80903 (719) 453-0180

DESIGNED BY: KK  
DRAWN BY: KK  
CHECKED BY: JH  
DATE: 03/21/2022

MEADOWBROOK PARK  
EL PASO COUNTY, COLORADO  
CONSTRUCTION DOCUMENTS  
PROPOSED DRAINAGE MAP



PROJECT NO.  
096956009

SHEET

DR-2

BY DATE APPR  
REVISION  
NO.



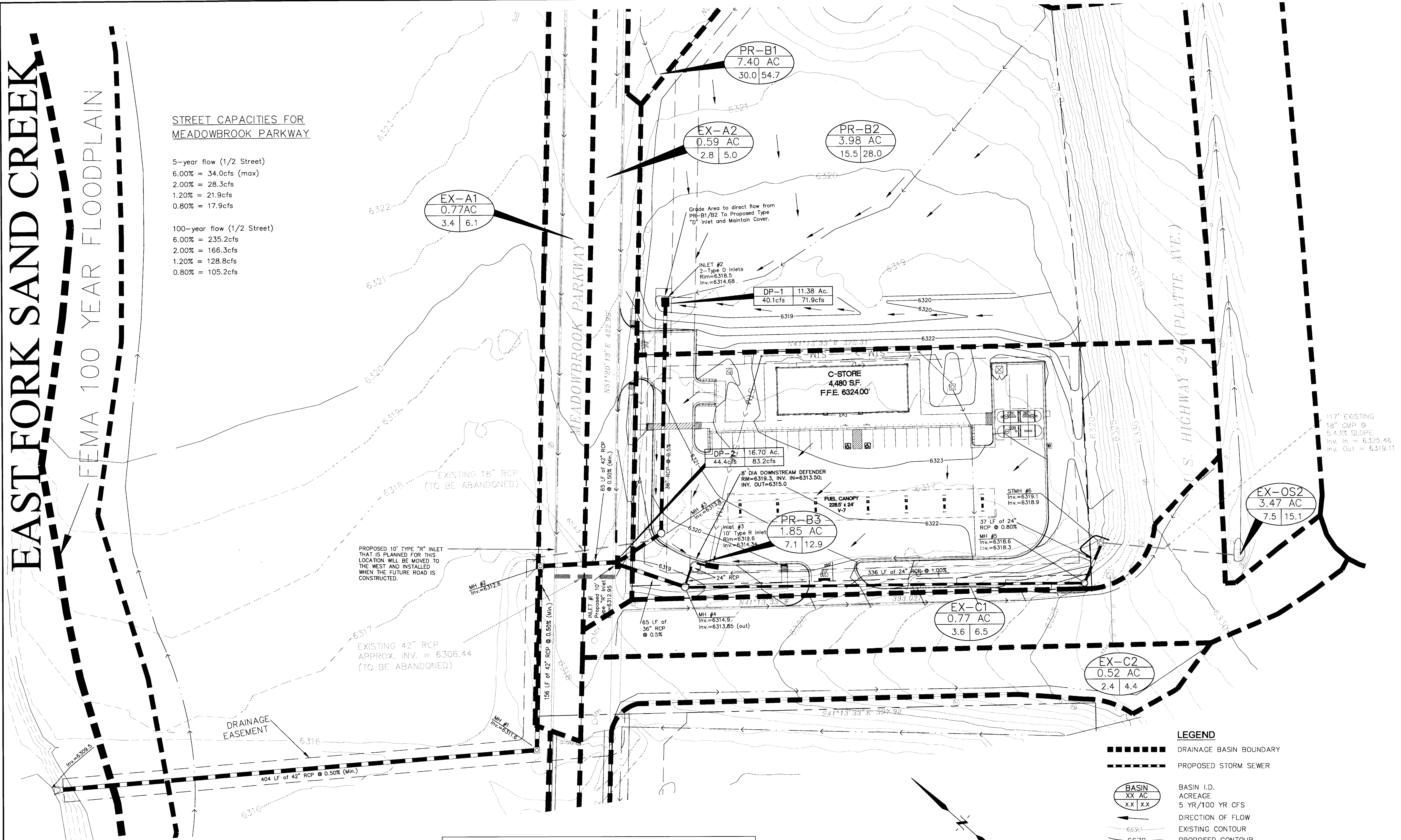
# EASTFORK SAND CREEK

## FEMA 100 YEAR FLOODPLAIN

### STREET CAPACITIES FOR MEADOWBROOK PARKWAY

5-year flow (1/2 Street)  
6.00% = 34.0cfs (max)  
2.00% = 28.3cfs  
1.20% = 21.9cfs  
0.80% = 17.9cfs

100-year flow (1/2 Street)  
6.00% = 235.2cfs  
2.00% = 166.3cfs  
1.20% = 128.8cfs  
0.80% = 105.2cfs



DESIGN POINT SUMMARY TABLE			
DESIGN POINT	RUNOFF 5 YR (cfs)	RUNOFF 100 YR (cfs)	COMMENTS
DP-1	40.1	71.9	FLOW IN PIPE
DP-2	44.4	83.2	FLOW IN PIPE
INLET #3	7.1	12.9	ON-SITE INLET, 24" RCP TO WQ VAULT
STMH #6	7.5	15.1	FROM BASIN EX-OS2

- LEGEND**
- DRAINAGE BASIN BOUNDARY
  - PROPOSED STORM SEWER
  - BASIN I.D. ACREAGE 5 YR/100 YR CFS
  - DIRECTION OF FLOW
  - EXISTING CONTOUR
  - PROPOSED CONTOUR
  - HIGH POINT
  - LOW POINT
  - GRADE BREAK
  - TOP BACK OF CURB
  - FLOWLINE
  - TIME OF CONCENTRATION

**CORE ENGINEERING GROUP**  
15004 1ST AVENUE S.  
BURKSVILLE, MN 55306  
PH: 763-255-1000  
FAX: 763-255-1001  
CONTACT: RICHARD L. SCHINDLER, P.E.  
EMAIL: Rich@cegi.com

DATE: \_\_\_\_\_

DESCRIPTION: \_\_\_\_\_

NO. \_\_\_\_\_

PREPARED FOR: Circle K Stores, Inc.  
1199 S. BANKERS BUILDING  
COPPELL, TEXAS 75019  
(940) 453-0015  
CONTACT: Tim Peters

PROJECT: 24/94 BUSINESS PARK  
Meadowbrook Parkway & Platte Avenue  
COLORADO SPRINGS, COLORADO

DRAWN: LAB, 9/9/15  
DESIGNED: LAB, 9/9/15  
CHECKED: RLS, 9/10/15

DATE: JULY, 2016

PROJECT NO. 319.001

SHEET NUMBER 1

TOTAL SHEETS: 2