# FINAL DRAINAGE REPORT FOR JICS - WAYNOKA

MAY 2023

Prepared for:

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Prepared by:



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Project #PPR239

# FINAL DRAINAGE REPORT FOR JICS – WAYNOKA

## **DRAINAGE PLAN STATEMENTS**

#### ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

#### DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY:

 TITLE:
 Jeremy Hammers

 DATE:
 05/11/23

ADDRESS: Elder Construction 4870 Centennial Boulevard, Suite 100 Colorado Springs, Colorado 80919

#### EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY:\_\_\_\_\_ Joshua Palmer, P.E. County Engineer





CONDITIONS:

## FINAL DRAINAGE REPORT FOR JICS – WAYNOKA

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## FINAL DRAINAGE REPORT FOR JICS – WAYNOKA

#### PURPOSE

This document is the Final Drainage Report for JICS - Waynoka. The purpose of this report is to identify the existing and proposed runoff patterns and recommend proposed drainage improvements for the proposed roadway improvements and to safely route runoff to downstream facilities.

#### **GENERAL LOCATION AND DESCRIPTION**

Improvements to existing Waynoka Road and Waynoka Place are required to support the surrounding developments. The roadway improvements will redevelop the roadway intersections and will extend approximately 80' east of Powers Boulevard and 750' south of Constitution Avenue. This will include the construction of an intersection and new striping on the southern half of Waynoka Place and the construction of a cul-de-sac, curb, and gutter at the west end of Waynoka Road. The striping will be installed on Waynoka Place to separate north and southbound traffic. The cul-de-sac and the proposed curb and gutter will block vehicle access from North Bound Powers Boulevard and Waynoka Road. This report will focus on the drainage solutions for the north-west quarter of Waynoka Road where the roadway improvements are to occur. Information regarding the flows along the south side of the roadway is provided, but will remain equal in the existing and proposed conditions.

Waynoka Place and Waynoka Road are located east of Powers Boulevard and south of Constitution Avenue within the El Paso County, Colorado. The segment of the roadway being improved is the western intersection of Waynoka Road and the southern half of Waynoka Place, which lie mostly in Lot 3 of the northwest half of the northwest quarter (NW <sup>1</sup>/<sub>2</sub>, NW <sup>1</sup>/<sub>4</sub>) of Section 6, Township 14 South, Range 65 west of the Sixth Principal Meridian. A portion of the improvements on the southern half of Waynoka Place lie in Lot 4 of the southwest half of the southwest quarter (NW <sup>1</sup>/<sub>2</sub>, NW <sup>1</sup>/<sub>4</sub>) of Section 31, Township 14 South, Range 65 west of the Sixth Principal Meridian. A Vicinity Map has been provided in the appendix of this report for reference.

#### WETLANDS

There are no apparent wetlands within the boundary of this project.

#### **CHANNEL IMPROVEMENTS**

The proposed project is not adjacent to Jimmy Camp Creek or any other significant drainageway. No channel improvements are necessary as a part of this project.

#### SOILS

Soils for this project, which are delineated on the map included within the appendix of this report, are classified as Blendon Sandy Loam (10) and Ellicott Loamy Coarse Sand (28) have been characterized as Hydrologic Soil Type "B" and "A", respectively. Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". The study area consists of a paved roadway, where exposed ground is present it is sparsely vegetated with native grasses. See Appendix for soils map.

#### HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals. Basins were analyzed and delineated (see Existing Conditions Map & Proposed Conditions Map in the Appendix) in order to determine areas and C coefficients. Overland flow and channelized flow paths were analyzed for each sub-basin in order to determine times of concentration and in order to analyze the hydraulic drainage system. Table 6-6 Volume 1 of DCM was used for corresponding runoff coefficients.

#### HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

#### FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) LOMR 12-08-057P, effective date February 28, 2013, Flood Insurance Rate Map (FIRM) Panel No. 08041C0751 G, effective date December 7, 2018, and Flood Insurance Rate Map (FIRM) Panel No. 08041C0752 G, effective date December 7, 2018, the site <u>DOES NOT</u> lie within a flood zone. A FIRM Panel showing the general site location is included in the Appendix with an outline of the project site shown between both adjoining panels.

#### **DRAINAGE CRITERIA**

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for calculations.

#### FOUR STEP PROCESS

As stated in the City of Colorado Springs DCM Volume 2, the Four Step Process is applicable to all new and re-developed projects with construction activities that disturb 1 acre or greater or that disturb less than 1 acre but are part of a larger common plan development. The roadway improvements associated with Waynoka Road and Waynoka Place disturb approximately 0.66 acres, less than an acre, and is considered a standalone project.

#### **EXISTING DRAINAGE CONDITIONS**

In the existing condition, runoff reaching the existing Waynoka Place corridor from developed grounds located to the east, west and north of the roadway are collected and conveyed to the south along Waynoka Place to the northwestern portion of the existing Waynoka Road. Runoff from undeveloped Lot 5 Block 2 Cimmaron-Northwest Industrial flows southwest onto the northwest portion of existing Waynoka Road. The combined flows along the west portion of Waynoka Road are conveyed west towards the existing north bound Powers Boulevard and are then conveyed south along the roadway. Runoff exiting the site, continues south on Powers Boulevard until entering the Sand Creek channel which is located about one thousand and two hundred feet (1200') to the south of the site. The existing pavement section located to the south of the site generally drains east to west and north to south at grades that vary from 0 to 5.5%. All analyzed lands lies within the Sand Creek Major Basin Watershed.

In accordance with the drainage criteria manual, an existing condition hydrologic analysis was prepared to determine peak runoff entering and exiting the subject site. The existing condition topography, basins boundaries, contributing design points, and peak flow summaries are depicted on the Waynoka Road at Powers Boulevard Existing Drainage Map in the appendix of this report. The following paragraphs detail the existing conditions analysis preformed on the site.

**Design Point 1** (Q5 = 5.4 cfs, Q100 = 11.6 cfs) consists of runoff produced from existing Waynoka Place and portions of surrounding lots, Lot 4 Cimmaron-Northwest Industrial Filing No. 3A, Lot 1 Schlaufman Subdivision Filing No. 1, and Lot 2 Cimmaron-Northwest Industrial Filing No. 3A to the east of Powers Boulevard. The runoff from the 2.55 acre **Basin A** (Q5 = 5.4 cfs, Q100 = 11.6 cfs) enters the northern portion of an existing Waynoka Road located along the south end of Waynoka Place at **DP1**. The runoff is then conveyed west along the northern portion of existing Waynoka Road to **Design Point 2 (DP2)**.

**Design Point 2** (Q5 = 8.9 cfs, Q100 = 20.1 cfs) consists of the runoff from **DP1**, undeveloped Lot 5, Block 2 Cimmaron-Northwest Industrial (**Basin B**), and the northern portion of existing Waynoka Road (**Basin C**). The runoff from **DP1** combines with runoff from the 0.68 acre **Basin C** (Q5 = 2.1 cfs, Q100 = 4.1 cfs) in the northern portion of existing Waynoka Road and the combined flows are conveyed west. The flows along Waynoka Road, combine with flows from 2.12 acre **Basin B** (Q5 = 2.6 cfs, Q100 = 7.2 cfs) on the southwest corner of Lot 5 Block 2 Cimmaron-Northwest Industrial at to **DP2**. The flows at **DP2** are then discharged to a swale along the east border of North Bound Powers Boulevard and the north border of Waynoka Road. These flows are then conveyed south under Waynoka Road.

**Design Point 3** (Q5 = 2.4 cfs, Q100 = 4.6 cfs) consists of runoff generated from the southern portion of existing Waynoka Road. Runoff produced within the 0.71 acre **Basin D** (Q5 = 2.4 cfs, Q100 = 4.6 cfs) generally sheet flows to west towards Powers Boulevard and collects at **DP3**, where it exists the basin and is conveyed south to a swale along the east border of North Bound Powers Boulevard and the south border of Waynoka Road. These flows continue south until they enter the Sand Creek Basin.

#### **PROPOSED DRAINAGE CONDITIONS**

Since this project will only improve the west portion of Waynoka Road and a portion of the southern half of Waynoka Place, the storm sewer collection points will be similar to those in the existing conditions. In the northern portion of the southern half of Waynoka Place, a new striping plan and a newly constructed intersection to the adjacent Lot 4 Cimmaron-Northwest Industrial Filing No. 3A is proposed. A paved cul-de-sac with a north-to-south running curb and gutter is proposed to be added on the west end of Waynoka Road. Curb openings on the north and south ends of the proposed curb and gutter will send flows along Waynoka Road to their original design points per the existing conditions. The existing roadway to the west will remain, but will be re-developed to stabilize the proposed curb. An existing channel keeps flows on the northern half of Waynoka Road until they reach an existing culvert which discharges to the south of the roadway. The increased flows from the existing to the proposed condition are added from off-site flows in the existing condition which are routed using a different path to the same existing channel. Thus, this does not increase peak flows to the channel, but reroutes the flows from the existing swale along the eastern edge of North Bound Powers Boulevard. The following paragraphs detail the proposed conditions analysis preformed on the site. All the proposed storm improvements for this project are to be publicly owned and maintained.

**Design Point 1** (Q5 = 5.7 cfs, Q100 = 12.1 cfs) runoff is generated from the southern half of Waynoka Place, an area of the eastern portion of developed Lot 4 Cimmaron-Northwest Industrial Filing No. 3A, and portions of the western halves of Lot 2 Cimmaron-Northwest Industrial Filing No. 3A and Lot 1 Schlaufman Subdivision Filing No. 1. In the developed condition, runoff produced from within 2.62-acre **Basin A** (Q5 = 5.7 cfs, Q100 = 12.1 cfs) shall be conveyed south to existing Waynoka Road at **DP1**. Runoff at **DP1** (Q5 = 5.7 cfs, Q100 = 12.1 cfs) will continue west within the northern half of Waynoka Road to **Design Point 2** (**DP2**). The addition of a proposed intersection between Lot 4 Cimmaron-Northwest Industrial Filing No. 3A and Waynoka Place, has increased the imperviousness, area and runoff produced from **Basin A** compared to the existing conditions. However, this proposed basin area and runoff increase also results in a basin area and runoff decrease from the existing adjacent property and re-routes the flows for the added portion to the proposed conditions in a different path, to the same existing channel to the south.

**Design Point 2** (Q5 = 9.1 cfs, Q100 = 20.4 cfs) runoff is generated from the southern half of Waynoka Place (DP1), the northwestern section of Waynoka Road (Basin C), and Lot 5, Block 2 Cimmaron-Northwest Industrial (**Basin B**). In the undeveloped condition, runoff produced from within 2.09-acre **Basin B** (Q5 = 2.8cfs, Q100 = 7.4 cfs) shall be conveyed southwest to **DP2.** Runoff produced from **DP1** flow-by will combine with runoff within 0.71-acre **Basin C** (Q5 = 2.3 cfs, Q100 = 4.4 cfs) and the combined runoff shall be conveyed west via the northwestern section of Waynoka Road to DP2. A cul-de-sac and new curb and gutter are proposed at the northwest end of Waynoka Road. The proposed curbs will tie into the existing curbs of the north and south ends, but will have openings on the north and south of the new curb on Waynoka Road. All combined runoff reaching opening will combine with flows from **Basin B** (Q5 = 2.8 cfs, Q100 = 7.4 cfs) and will be conveyed west and north by the existing swale at the northwest end of Waynoka Road to DP2 (Q5 = 9.1 cfs, O100 = 20.4 cfs). Flows at **DP2** will enter an existing channel at the northwest corner of Waynoka Road and will be conveyed south under the roadway. The increase in peak flow rates from **DP1**, results in an increase of peak flow rates to **DP2** from the existing to the proposed conditions. However, this proposed runoff increase does not affect the downstream drainage system, since the runoff was re-routed from an existing site, to the proposed site and both sites will lead to the same existing channel at the northwest end of Waynoka Road next to DP2.

**Design Point 3** (Q5 = 2.4 cfs, Q100 = 4.6 cfs) runoff is generated from the southwestern quarter of the existing Waynoka Road. Runoff produced within the 0.71-acre **Basin D** (Q5 = 2.4 cfs, Q100 = 4.6 cfs) generally sheet flows west and south to DP3, Lot A Replat of Lots 2, 3, Block 3 Cimmaron-Northwest Industrial, as in the existing condition. Flows discharged as sheet flow to the adjacent site will remain consistent with the existing condition (Q5 = 2.4 cfs, Q100 = 4.6 cfs).

#### **EROSION CONTROL**

It is the policy of El Paso County that a grading and erosion control plan be submitted with the drainage report. At this time, we respectfully request that the erosion control plan be submitted in conjunction with the final grading plan. Proposed rock socks, silt fence, vehicle traffic control, and reseeding are proposed as erosion control measures.

#### DRAINAGE, BRIDGE, AND POND FEES

Waynoka Place has previously been platted with additional rights-of-way dedicated for the proposed improvements as a portion of the Claremont Business Park Filing No.3 subdivision. As such, no fees for drainage, bridge and or pond are due.

#### CONSTRUCTION COST ESTIMATE

#### Storm Sewer System (Public, Non-Reimbursable)

All proposed drainage facilities will be publicly owned and maintained after the system is constructed by the developer and the improvements accepted by El Paso County.

Description	Quantity	Unit	Unit Cost	Total Cost
Curb Opening	2	EA	\$2,500.00	\$5,000.00
Subtotal:				\$5,000.00
Contingency (15%)				\$750.00
TOTAL:				\$5,750.00

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility costs in the year 2023 and is subject to change.

#### SUMMARY

Proper implementation of the concepts presented in this Final Drainage report will provide for the development of the proposed site without negative impacts to the receiving water course and surrounding developments. All drainage facilities proposed are to be publicly owned and maintained. Curb and gutter are proposed to be added north to south along the west end of existing Waynoka Road. The proposed curb openings at the north and south ends of the new cul-de-sac will allow runoff to flow through the curb lines to existing channels as per the existing conditions.

#### REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- Web Soil Survey, USDA NRCS Soils Map https://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm
- 4.) FEMA flood Map Service Center, Federal Emergency Management Agency
  <a href="https://msc.fema.gov/portal/home">https://msc.fema.gov/portal/home</a>

Flood Insurance Rate Map (FIRM) Panel No. 08041C0751 G, effective date December 7, 2018, Flood Insurance Rate Map (FIRM) Panel No. 08041C0752 G, effective date December 7, 2018

 "Sand Creek Drainage Basin Planning Study Preliminary Design Report" (DBPS), prepared by Kiowa Engineering, revised December 1998. APPENDIX

VICINITY MAP



SOILS MAP



FIRM PANELS



### HYDROLOGIC CALCULATIONS

# FINAL DRAINAGE REPORT JICS - WAYNOKA (Existing Conditions - Area Runoff Coefficient Summary)

			STRE	ETS/DEVEI	LOPED	IN	INDUSTRIAL DEV			GRAVEL/IMP LANDSCAPE			CAPED/UNDE	WEIGHTED		
BASIN	TOTAL AREA <i>(SF)</i>	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
A	111283.2	2.55	1.10	0.90	0.96	0.36	0.59	0.70	0.13	0.59	0.70	0.97	0.09	0.36	0.53	0.68
В	92447.9	2.12	0.57	0.90	0.96	0.00	0.59	0.70	0.08	0.59	0.70	1.47	0.09	0.36	0.33	0.54
С	29506.6	0.68	0.52	0.90	0.96	0.00	0.59	0.70	0.00	0.59	0.70	0.16	0.09	0.36	0.71	0.82
D	31033.8	0.71	0.53	0.90	0.96	0.00	0.59	0.70	0.09	0.59	0.70	0.09	0.09	0.36	0.76	0.85

# FINAL DRAINAGE REPORT JICS - WAYNOKA

# (Existing Conditions - Area Drainage Summary)

From Area Runof	l Coefficient Sumn	nary			OVERL	AND		ST	TREET / CH	IANNEL FLO	)W	Time of T	Travel (T <sub>t</sub> )	INTENSITY *		TOTAL FLOWS	
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>
	(Acres)	From DC	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	2.55	0.53	0.68	0.53	40	0.8	5.1	820	1.3%	2.3	6.0	11.2	14.8	4.0	6.7	5.4	11.6
В	2.12	0.33	0.54	0.33	80	2.0	9.2	225	2.2%	1.0	3.6	12.8	11.7	3.8	6.3	2.6	7.2
С	0.68	0.71	0.82	0.71	40	0.8	3.6	625	1.4%	2.3	4.5	8.0	13.7	4.5	7.5	2.1	4.1
D	0.71	0.76	0.85	0.76	40	0.8	3.1	650	1.3%	2.3	4.7	7.8	13.8	4.5	7.5	2.4	4.6

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU Date: 1/26/2023 Checked by: VAS

# FINAL DRAINAGE REPORT JICS - WAYNOKA (Existing Conditions - Basin Routing Summary)

	From Area Runoff Coefficient Summary				OVE	ERLAND		PIPE	/ CHA	NNEL FLO	)W	Time of Travel $(T_t)$	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	Α	1.36	1.74				Assumes I	Basin A Tt =				11.2	4.0	6.7	5.4	11.6	North Curbline of Waynoka Road
2	DP1, B, C	2.54	3.43	Α	ssumes DP1	Tt =	11.2	625	1.6%	2.5	4.1	15.3	3.5	5.9	8.9	20.1	Existing 30" culvert
3	D	0.54	0.61			I	Assumes I	Basin D Tt =				7.8	4.5	7.5	2.4	4.6	Sheet Flow to Offsite Area
																	West of Marksheffel
	Coloulated by: TAU																

Calculated by:  $\frac{\text{TAU}}{\text{Date:}}$ 

Checked by: VAS

# FINAL DRAINAGE REPORT JICS - WAYNOKA (Proposed Conditions - Area Runoff Coefficient Summary)

			STRE	ETS/DEVE	LOPED	IN	INDUSTRIAL DEV			GRAVEL/IMP LANDSCAPE			CAPED/UNDE	WEIGHTED		
BASIN	TOTAL AREA <i>(SF)</i>	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
A	114324.9	2.62	1.17	0.90	0.96	0.36	0.59	0.70	0.13	0.59	0.70	0.97	0.09	0.36	0.54	0.69
В	91023.1	2.09	0.59	0.90	0.96	0.00	0.59	0.70	0.08	0.59	0.70	1.41	0.09	0.36	0.34	0.54
С	30931.4	0.71	0.55	0.90	0.96	0.00	0.59	0.70	0.00	0.59	0.70	0.16	0.09	0.36	0.72	0.82
D	31033.8	0.71	0.53	0.90	0.96	0.00	0.59	0.70	0.09	0.59	0.70	0.09	0.09	0.36	0.76	0.85

# FINAL DRAINAGE REPORT JICS - WAYNOKA

# (Proposed Conditions - Area Drainage Summary)

From Area Runofj	l Coefficient Sumn	nary			OVERL.	AND		ST	REET / CH	IANNEL FLO	)W	Time of T	Travel (T <sub>t</sub> )	INTENSITY *		TOTAL FLOWS	
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	Tt	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>
	(Acres)	From DC	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	2.62	0.54	0.69	0.54	40	0.8	5.1	820	1.3%	2.3	6.0	11.1	14.8	4.0	6.7	5.7	12.1
В	2.09	0.34	0.54	0.34	80	2.0	9.1	225	2.2%	1.0	3.6	12.7	11.7	3.9	6.5	2.8	7.4
С	0.71	0.72	0.82	0.72	40	0.8	3.5	625	1.4%	2.3	4.5	7.9	13.7	4.5	7.5	2.3	4.4
D	0.71	0.76	0.85	0.76	40	0.8	3.1	650	1.3%	2.3	4.7	7.8	13.8	4.5	7.5	2.4	4.6

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU Date: 1/10/2023 Checked by: VAS

# FINAL DRAINAGE REPORT JICS - WAYNOKA (Proposed Conditions - Basin Routing Summary)

	From Area Runoff Coefficient Summary	v			OVERLAND			PIPE / CHANNEL FLOW			Time of Travel $(T_t)$ INTENSITY *		TOTAL	FLOWS			
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q100	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	Α	1.43	1.81		Assumes Br							11.1	4.0	6.7	5.7	12.1	North Curbline of Waynoka Road
2	DP1, B, C	2.65	3.53		Assumes B	Tt =	11.7	625	1.6%	2.5	4.1	15.8	3.4	5.8	9.1	20.4	Existing 30" culvert
3	D	0.54	0.61		Assumes I							7.8	4.5	7.5	2.4	4.6	Sheet Flow to Offsite Area
																West of Marksheffel	

Calculated by: TAU

Date: 12/21/2022 Checked by: VAS

## HYDRAULIC CALCULATIONS



Project Description				_
Friction Method	Manning			
	Formula			
Solve For	Normal Depth			_
Input Data				
Channel Slope	0.018 ft/ft			
Discharge	20.10 cfs			_
	See	ction Definitions		
Statio	on		Elevation	
(ft)		0 + 00	(ft)	70.15
		0+00		72.15
		0+18		71.02
		0+20		/1.30
		0+20		72.03
		0125		72.50
	Roughnes	ss Segment Definitions		
Start Station		Ending Station	Roughness Coefficient	t
(0+00, 72.15)		(0+20, 72.03)		0.015
(0+20, 72.03)		(0+25, 72.50)		0.030
				_
Options				
Current Roughness Weighted Method	Pavlovskii's Method			
Open Channel Weighting	Pavlovskii's			
Method	Method			
Closed Channel Weighting Method	Pavlovskii's Method			
	Fielded			_
Results				
Normal Depth	8.0 in			
Roughness Coefficient	0.015			
Elevation	72.03 ft			
Elevation Range	/1.4 to /2.5			
Flow Aron	10 <del>11</del> 2			
Notted Parimeter	4.0 IL-			
Hydraulic Radius	10.0 It			
	2.9 III 15 00 <del>0</del>			
Normal Dopth	15.90 IL			
Critical Depth	8.0 In			
	9.0 III			
	5.U8 TC/S			
	0.40 π			
Specific Energy	1.0/ ft			
Froude Number	1./94			
	Bentley Syste	ms, Inc. Haestad Methods Solution		FlowMaster
cui-de-sac.tm8 4/4/2023	27 Siemo	Center on Company Drive Suite 200 W		[10.03.00.03] Page 1 of 2
	Watertown,	CT 06795 USA +1-203-755-1666		-

## 1) Worksheet for Existing North Street Section - 20.1cfs

Results		
Flow Type	Supercritical	
CV/E Input Data		
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	8.0 in	
Critical Depth	9.6 in	
Channel Slope	0.018 ft/ft	
Critical Slope	0.005 ft/ft	

## 1)Worksheet for Existing North Street Section - 20.1cfs

Project Description				
Friction Method	Manning			
Solve For	Normal Depth			
Input Data				
Channel Slope	0.011 ft/ft			
Discharge	4.60 cfs			
	Se	ction Definitions		
Static	n		Elevation	
(17)		0+00		72.27
		0+18		71.79
		0+21		71.53
		0+21		72.20
	Roughne	ss Segment Definitio	ons	
Start Station		Ending Station	Roughness Coefficient	
(0+00, 72.23)		(0+21, 72.2)	0)	0.015
Options				
Current Roughness Weighted Method	Pavlovskii's Method			
Open Channel Weighting Method	Pavlovskii's Method			
Closed Channel Weighting	Pavlovskii's			
Method	Method			
Results				
Normal Depth	5.3 in			
Roughness Coefficient	0.015			
Elevation	71.97 ft			
Elevation Range	/1.5 to /2.2			
Flow Area	1.6 ft <sup>2</sup>			
Wetted Perimeter	10.8 ft			
Hydraulic Radius	1.8 in			
Top Width	10.38 ft			
Normal Depth	5.3 in			
Critical Depth	5.7 in			
Critical Slope	0.006 ft/ft			
Velocity	2.87 ft/s			
Velocity Head	0.13 ft			
Specific Energy	0.57 ft			
Froude Number	1.285			
Flow Type	Supercritical			

## 2)Worksheet for Existing South Street Section - 4.6cfs

cul-de-sac.fm8 4/4/2023 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 FlowMaster [10.03.00.03] Page 1 of 2

GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.3 in	
Critical Depth	5.7 in	
Channel Slope	0.011 ft/ft	
Critical Slope	0.006 ft/ft	

## 2)Worksheet for Existing South Street Section - 4.6cfs



Project Description		
Solve For	Headwater Elevation	
Input Data		
Discharge	20.40 cfs	
Crest Elevation	0.00 ft	
Tailwater Elevation	0.00 ft	
Weir Coefficient	3.10 ft^(1/2)/s	
Crest Length	13.9 ft	
Number Of Contractions	0	
Results		
Headwater Elevation	0.61 ft	
Headwater Height Above Crest	0.61 ft	
Tailwater Height Above Crest	0.00 ft	
Flow Area	8.4 ft <sup>2</sup>	
Velocity	2.42 ft/s	
Wetted Perimeter	15.1 ft	
Top Width	13.90 ft	

## 1) Worksheet for North Weir-20.4cfs

Project Description		
Friction Method	Manning	
Solve For	Normal Depth	
	F -	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.012 ft/ft	
Bottom Width	5.00 ft	
Discharge	20.40 cfs	
Results		
Normal Depth	6.6 in	
Flow Area	2.8 ft <sup>2</sup>	
Wetted Perimeter	6.1 ft	
Hydraulic Radius	5.4 in	
Top Width	5.00 ft	
Critical Depth	9.6 in	
Critical Slope	0.004 ft/ft	
Velocity	7.38 ft/s	
Velocity Head	0.85 ft	
Specific Energy	1.40 ft	
Froude Number	1.751	
Flow Type	Supercritical	
GVF Input Data		
Downstream Denth	0.0 in	
l enath	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	6.6 in	
Critical Depth	9.6 in	
Channel Slope	0.012 ft/ft	
Critical Slope	0.004 ft/ft	

## 2)Worksheet for North Retangular Curb Chase-20.4cfs

Project Description				—
Friction Method	Manning			
Solve For	Normal Depth			
				=
	0.040.0.0			_
Channel Slope Discharge	0.018 ft/ft 20.40 cfs			
	Se	ction Definitions		_
Static	n		Elevation	
(11)		0+00	(11)	72.15
		0+18		71.62
		0+20		71.36
		0+20		72.03
		0+25		72.50
	Roughne	ss Segment Definitions		
Start Station		Ending Station	Roughness Coefficien	t
(0+00, 72.15)		(0+20, 72.03)	5	0.015
(0+20, 72.03)		(0+25, 72.50)		0.030
Options				
Current Roughness Weighted	Pavlovskii's			
Method	Method			
Open Channel Weighting	Pavlovskii's			
Method Closed Channel Weighting	Pavlovskii's			
Method	Method			_
Results				_
Normal Denth	8 1 in			_
Roughness Coefficient	0.015			
Elevation	72.03 ft			
Elevation Pango	71.4 to 72.5			
Lievation Range	ft			
Flow Area	4.0 ft <sup>2</sup>			
Wetted Perimeter	16.7 ft			
Hydraulic Radius	2.9 in			
Top Width	16.01 ft			
Normal Depth	8.1 in			
	9.7 in			
Unitical Slope	0.005 ft/ft			
Velocity Hood	5.09 IL/S			
Specific Energy	0.40 IL 1 00 A			
Froude Number	1.00 IL 1 706			
	1.730			
cul-de-sac.fm8 4/4/2023	Bentley Syste 27 Sieme Watertown.	ems, Inc. Haestad Methods Solution Center on Company Drive Suite 200 W CT 06795 USA +1-203-755-1666		FlowMaster [10.03.00.03] Page 1 of 2

### 3)Worksheet for North Street Section - 20.4cfs

Results		
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	8.1 in	
Critical Depth	9.7 in	
Channel Slope	0.018 ft/ft	
Critical Slope	0.005 ft/ft	

## 3)Worksheet for North Street Section - 20.4cfs

Project Description		
Solve For	Headwater Elevation	
Input Data		
Discharge Crest Elevation Tailwater Elevation Weir Coefficient Crest Length Number Of Contractions	4.60 cfs 0.00 ft 0.00 ft 3.10 ft^(1/2)/s 12.7 ft 0	
Results		
Headwater Elevation Headwater Height Above	0.24 ft 0.24 ft	
Tailwater Height Above Crest Flow Area	0.00 ft 3.0 ft <sup>2</sup>	
Velocity Wetted Perimeter Top Width	1.52 ft/s 13.2 ft 12.70 ft	

## 4)Worksheet for South Weir-4.6cfs

Project Description		
Friction Method	Manning	
Solve For	Normal Depth	
	······ - •P •··	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.012 ft/ft	
Bottom Width	2.00 ft	
Discharge	4.60 cfs	
Results		
Normal Depth	5.0 in	
Flow Area	0.8 ft <sup>2</sup>	
Wetted Perimeter	2.8 ft	
Hydraulic Radius	3.5 in	
Top Width	2.00 ft	
Critical Depth	6.6 in	
Critical Slope	0.005 ft/ft	
Velocity	5.54 ft/s	
Velocity Head	0.48 ft	
Specific Energy	0.89 ft	
Froude Number	1.514	
Flow Type	Supercritical	
GVE Input Data		
Downstroom Donth	0.0 in	
Longth	0.0 11	
Length Number Of Stops	0.0 10	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.0 in	
Critical Depth	6.6 in	
Channel Slope	0.012 ft/ft	
Critical Slope	0.005 ft/ft	

## 5)Worksheet for South Rectangular Curb Chase 4.6cfs

Project Description		
Friction Method	Manning	
Solve For	Normal Depth	
	······ - •P •··	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.012 ft/ft	
Bottom Width	2.00 ft	
Discharge	4.60 cfs	
Results		
Normal Depth	5.0 in	
Flow Area	0.8 ft <sup>2</sup>	
Wetted Perimeter	2.8 ft	
Hydraulic Radius	3.5 in	
Top Width	2.00 ft	
Critical Depth	6.6 in	
Critical Slope	0.005 ft/ft	
Velocity	5.54 ft/s	
Velocity Head	0.48 ft	
Specific Energy	0.89 ft	
Froude Number	1.514	
Flow Type	Supercritical	
GVE Input Data		
Downstroom Donth	0.0 in	
Longth	0.0 11	
Length Number Of Stops	0.0 10	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.0 in	
Critical Depth	6.6 in	
Channel Slope	0.012 ft/ft	
Critical Slope	0.005 ft/ft	

## 6) Worksheet for South Rectangular Curb Chase 4.6cfs

### **DRAINAGE MAPS**



955.5485	EXIST	ING	CONDITIO	NS D	RAINAGE	MAP
PROJECT NO. 10-02		-022	SCALE:	DATE: 1-17-2023		
D D C	DESIGNED BY: DRAWN BY: CHECKED BY:	dlm Dlm Vas	N/A	SHEE	ET 1 OF 1	DM

LEGEND

