STERLING RANCH MDDP AMENDMENT NO. 2 & PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH EAST PRELIMINARY PLAN NO. 1

CCES Responses in red

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Job No. 1183.22

Added

PCD Project No.
SKP-22-004/ SP-22-004

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

_____ _____

Marc A. Whorton Colorado P.E. #37155 Date

OWNER'S/DEVELOPER'S STATEMENT:

I, the owner/developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: CLASSIC SRJ LAND, LLC

By: _____

Title: _____

Address: 2138 Flying Horse Club Drive

Colorado Springs, CO 80921

EL PASO COUNTY:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

_____ _____

For County Engineer, / ECM Administrator Date

Conditions:

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VICINITY MAP

SOILS MAP (WEB SOIL SURVEY)

F.E.M.A. MAP / LOMR (08-08-0541P)

REFERENCE MATERIAL

HYDROLOGIC CALCULATIONS

STORMWATER QUALITY CALCULATIONS

DETENTION POND CALCULATIONS

DRAINAGE MAPS

PURPOSE

The purpose of this Sterling Ranch MDDP Amendment No. 2 & Preliminary Drainage Report is to address on-site and off-site drainage quantities and patterns for the proposed development, compare to approved MDDP and identify general drainage improvements and facilities required to minimize impacts to the adjacent properties. The MDDP Amendment No. 2 portion of the report only addresses adjustments proposed to help reduce the East Fork Basin transfer and the combining of ponds FSD-16A and FSD-16B into one single facility. All other overall basin hydrology and pond locations remain the same at this time.

GENERAL DESCRIPTION

Classic SRJ Land, LLC (Classic Homes) has recently purchased the remaining portion of the Sterling Ranch property east of Sand Creek from the Jim Morley. This initial development proposal east of Sand Creek in to be known as **Sterling Ranch East Preliminary Plan No. 1**. This initial Preliminary Plan consists of 3 distinct development areas east of Sand Creek separated by the proposed roadway plats, prepared by JR Engineering, for Briargate Pkwy. and Sterling Ranch Road. The area north of Briargate Pkwy. is 84.74 acres (280 lots). The area south of Briargate Pkwy. but north of Sterling Ranch Road is 161.90 acres (294 lots); and the area south of Sterling Ranch Road is 74.73 acres (187 lots). The total Preliminary Plan area is then **321.37 acres** located in portions sections 27, 28, 33 and 34, township 12 south, range 65 west of the sixth principal meridian. The site is bounded on the north by the Retreat at TimberRidge development, to the east by future Sterling Ranch East property (zoned for future urban development), to the west by Sand Creek and existing Sterling Ranch residential development and to the south by existing rural residential development zoned RR-5. The site is in the upper portion of both the Sand Creek and Sand Creek East Fork Drainage Basins. Urban single family residential development **totaling 761 lots**, along with two future District 20 school sites and several park areas are proposed within this Sterling Ranch East Preliminary Plan No. 1.

Added roadways platted with Homestead North Filing No. 1?

The average soil condition reflects Hydrologic Group "A" (Blakeland loamy sand and Columbine gravelly sandy loam) with also some presence of Hydrologic Group "B" (Pring coarse sandy loam) as determined by the "Web Soil Survey of El Paso County Area," prepared by the Natural Resources Conservation Service (see map in Appendix).

EXISTING DRAINAGE CONDITIONS

The Sterling Ranch East Preliminary Plan No. 1 property is located in the upper portion of the Sand Creek drainage basin on the south edge of Black Forest. However, some easterly portions of the site lie within the East Fork tributary of Sand Creek. (See MDDP Amendment portion of this report for further discussion) Nearly the entire site, other than the Sand Creek corridor, is mainly covered with native grasses with few or no trees. Some minor disturbance due to utility installation has also taken place within the utility esmt. corridors traversing the site for the future Briargate Pkwy. Other land disturbance including some grading operations by the previous land owner has also taken place just north of the future Briargate Pkwy. alignment and within the parcel south of Briargate Pkwy. and northwest of Sterling Ranch Road. The Sand Creek channel exists along the extreme westerly edge of the property. All required improvements to the Sand Creek channel adjacent to this property are described in a separate report prepared by JR Engineering, "Final Design Report for Sand Creek Restoration", dated October 21, 2021. Please reference this report for all adjacent creek improvement requirements and associated wetland mitigation plans and permitting within jurisdictional waters.

Update as applicable

Updated to the latest JR report and CDs

The adjacent Sand Creek portions of this site have been previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Engineering Corporation, March 1996 and more recently in the above-mentioned Sand Creek Restoration Report by JR Engineering, LLC. CORE Consultants is the wetland consultant working with JR Engineering, LLC on this stretch of Sand Creek. They are coordinating the effort with the Corps. of Eng. for the required 404 permitting for all the proposed channel improvements. Two public roadway crossings of Sand Creek are also proposed to serve as direct access for the Sterling Ranch East

Preliminary Plan No. 1 development areas. These crossings are currently covered under a 404 permit (Action No. SPA-2015-00428-SCO) with the previous land owner dated February 2016. JR Engineering, LLC is also coordinating a CLOMR/LOMR for this stretch of Sand Creek that is adjacent to the site and defined as Reach SC-8 (south of Briargate Pkwy.) and SC-9 north of Briargate Pkwy.). This entre site was also studied as a part of the "Master Development Drainage Plan for Sterling Ranch", prepared by M&S Civil Consultants, approved November 2018 which includes modeling of this property as well as the large acreage north up to the top of the Sand Creek Basin. The MDDP proposes developed flows within Sand Creek that are significantly lower than both the DBPS and FEMA currently show. These flows are as follows: At Arroya Lane crossing (North of the TimberRidge Development) Q_{10} = 430 cfs Q_{100} = 1487 cfs and Sterling Ranch south property line Q_{10} = 713 cfs Q_{100} = 1911 cfs. However, the focus of this report is not on Sand Creek, but the adjacent residential development proposed. As mentioned earlier, eastern portions of this site lie within the East descriptions represent the pre-development flow design pc the approved MDDP for Sterling Ranch, yet differentiat verses the East Fork basins. The nomenclature is similar to the MDDP for easy comparison:

Flows MDDP in app comm draina

Now included MDDP historic map in Appendix and flows updated to match.

<u>Sand Creek Main</u>

The Retreat at TimberRidge development exists at the northwest portion of the Sterling Ranch East property. Retreat at TimberRidge Filing No. 2 was recently approved by County Staff and proposes several temporary sediment basins and drainage swales adjacent to this property. These facilities will be removed upon construction from this proposed development in these areas. The following basins are off-site basins (outside the proposed Preliminary Plan area but within the overall Sterling Ranch East ownership) accounted for in the Retreat at TimberRidge development and are not tributary to the proposed development:

Now included areas for all basin descriptions

Basin TR-12 (Q_5 = 2 cfs, Q_{100} = 9 cfs) consists of future large lot residential area that currently is undeveloped and sheet flows in a southwesterly direction off-site into the future Retreat at TimberRidge development. These flows were anticipated and accounted for within that

Include area each basin discussion.

development and future downstream storm facilities. **Basin TR-20 (Q_5 = 10 cfs, Q_{100} = 32 cfs)** consists of future large lot residential area that currently is undeveloped and sheet flows in a southwesterly direction off-site directly into an existing stock pond within the future Retreat at TimberRidge development. These flows were anticipated and accounted for within that development and downstream storm facilities. **Basin TR-4 (Q_5 = 2 cfs, Q_{100} = 9 cfs)** consists of future urban residential area that currently is undeveloped and sheet flows in a southwesterly direction off-site into the future Retreat at TimberRidge development. These flows were anticipated and accounted for within that development and downstream storm facilities. **Basin TR-5 (Q_5 = 5 cfs, Q_{100} = 17 cfs)** consists of future urban residential area that currently is undeveloped and sheet flows in a southwesterly direction directly into a temporary sediment basin constructed with the Retreat at TimberRidge Filing No. 2 project. These flows were anticipated and accounted for within that development and downstream storm facilities. **Basin TR-6 (Q_5 = 1 cfs, Q_{100} = 4 cfs)** consists of a small future urban residential area that currently is undeveloped and sheet flows in a southwesterly direction off-site into the Retreat at TimberRidge development. These flows were anticipated and accounted for within that development and downstream storm facilities. **Basin TR-7 (Q_5 = 1 cfs, Q_{100} = 5 cfs)** consists of a basin that sheet flows towards the Retreat property but then captured by a temporary swale and routed to the west into another temporary sediment basin constructed by the Retreat development.

The following basins are within the proposed Preliminary Plan area and also within the Sand Creek main basin boundary:

Basin EX-4A (Q_5 = 19 cfs, Q_{100} = 50 cfs) consists of the smaller portion of the property (44.2 acres) south of the Briargate Pkwy. crossing that currently sheet flows in a southwesterly direction directly into the Sand Creek main channel. These sheet flows are then conveyed downstream as channel flow towards the south property boundary. This basin differs from the MDDP as it only represents the on-site existing flows from the east side of the channel as defined by the current ownership boundary and does not include the off-site flows from the

development along the west side of the channel or the significant existing off-site channel flow itself.

Basin EX-5 (Q_5 = 12 cfs, Q_{100} = 32 cfs) also consists of the smaller portion of the property (26.2 acres) north of the Briargate Pkwy. crossing that currently sheet flows in a southwesterly direction directly into the Sand Creek main channel. These sheet flows are then conveyed downstream as channel flow towards the proposed Briargate Pkwy. roadway crossing. This basin differs from the MDDP as it only represents the on-site existing flows from the east side of the channel as defined by the proposed platted boundary from the Homestead North at Sterling Ranch development and does not include the off-site flows from the west side of the channel or the significant existing off-site channel flow itself.

Basin EX-7 (Q_5 = 47 cfs, Q_{100} = 107 cfs) consists of approximately 155.2 acres of property that sheet flows in a southerly direction. This basin is similar to the MDDP and the east basin line defines the westerly edge of the East Fork basin. The sheet flows become more concentrated towards the south end of the basin as the topography becomes steeper and more defined south of the proposed Sterling Ranch Road crossing. The existing flows exit the property along the south boundary at **Design Point 4**. Given the difference in hydrologic modeling (SWMM 5.1 vs. HEC-HMS) these flows are fairly consistent with the flows determined by the MDDP (Q_5 = 22 cfs, Q_{100} = 107 cfs).

Sand Creek East Fork

Basin EX-9 (Q_5 = 57 cfs, Q_{100} = 124 cfs) consists of approximately 178.1 acres of property that sheet flows in a southerly direction. This basin is similar to the MDDP and the west basin line defines the westerly edge of the East Fork basin. This basin incorporates both the MDDP basins

See revised report descriptions and updated map

basin, the flows seem to remain as sheet flows as they exit

dary at **Design Point 6**. Again, these flows seem consistent

MDDP (Q_5 = 24 cfs, Q_{100} = 125 cfs).

Did not see a corresponding DP in the Calcs to compare with DP 6 or verify flows noted. See additional comments on drainage map.

Basin EX-10 (Q_5 = 105 cfs, Q_{100} = 222 cfs) consists of approximately 265.9 acres of property at the extreme top of the Sand Creek East Fork Basin. The off-site northern portion of this basin is within the Black Forest, heavily treed area. The off-site eastern portion of the basin contains existing 5 ac. lot development (Indian Wells Subd. Filing 1). The flows from this large basin sheet flow in a southerly direction across the northern portion of the Sterling Ranch property and enter Basin EX-10A.

Added additional text

Basin EX-10A (Q_5 = 52 cfs, Q_{100} = 117 cfs) consists of approximately 175.4 acres of property that sheet flows in a southerly direction through the Sterling Ranch property. The combined flows from both basins seem to remain as sheet flow traveling in a southerly direction towards **Design Point 7**. **(Q_5 = 114 cfs, Q_{100} = 259 cfs)** At this location the flows exit the property along the south boundary. Again, these flows are fairly consistent with the flows determined by the MDDP at this location (Q_5 = 57 cfs, Q_{100} = 278 cfs).

Did not see a corresponding DP in the MDDP map to compare with DP 7 or verify flows noted. See additional comments on drainage map.

Basin EX-13 (Q_5 = 36 cfs, Q_{100} = 85 cfs) consists of approximately 94.8 acres of property at the extreme eastern edge of the Sterling Ranch property. asin contains existing 5 ac. lot development (Indian Wells asin sheet flow in a southeasterly direction towards the eastern boundary of the Sterling Ranch property. To be consistent with the MDDP, the flows then seem to run along the eastern property boundary and enter Basin EX-11 near the Southeast corner of the property.

Now included MDDP historic map in Appendix and flows updated to match.

Basin EX-11 (Q_5 = 54 cfs, Q_{100} = 129 cfs) consists of approximately 214.34 acres of property that sheet flows across the southeastern corner of the Sterling Ranch property. The combined flows from both basins seem to remain as sheet flow wards **Design Point 56**. **(Q_5 = 60 cfs, Q_{100} = 160 cfs)** At th along the south boundary. Again, these flows are fairly by the MDDP at this location (Q_5 = 43 cfs, Q_{100} = 203 cfs).

Now included MDDP historic map in Appendix and flows updated to match.

Did not see a corresponding DP in the MDDP map to compare with DP 56 or verify flows noted. See additional comments on drainage map.

Include County project number that was associated with both of these reports.

Added

STERLING RANCH MDDP AMENDMENT NO. 2

PURPOSE

This portion of the report represents the second amendment to the Sterling Ranch MDDP, originally prepared by M&S Civil Consultants, Inc., approved June 2018. Amendment No. 1 was prepared by JR Engineering, LLC, dated October, 2021. All existing basin hydrology, concept routing and pond locations remain the same except for the following proposed changes:

1. As described in the Sterling Ranch MDDP Amendment No. 1, Ponds FSD-16A and FSD-16B are proposed to be combined into one full-spectrum facility located at the northeast corner of Briargate Pkwy. and Sterling Ranch Road.

Added

Indicate the new pond name

2. Rather than divert significant surface routed flows from the East Fork Sand Creek basin to the Sand Creek main basin, this report proposes to continue to release surface flows into the East Fork Sand Creek basin matching as close to pre-development conditions as possible.

3. Small portions of original MDDP basins SCE-7 and SCE-10 are now proposed to be tributary to Pond FSD-14B with the outfall in a southerly direction instead of towards Pond W3.

DETAILED DESCRIPTION

The original MDDP basins SC3-16A and SC3-16B had total acreages of 168.1 Ac. and 50.7 Ac., respectively for a total of 218.8 Ac. The following proposed basins represent this same area tributary to the single Pond FSD-16, including the tributary basins from Briargate Pkwy.:

P1-A	12.7 Ac.	P1-B	35.5 Ac.	P1-C	10.7 Ac.
P1-D	31.4 Ac.	P1-E	52.2 Ac.	P1-F	76.7 Ac.
TR-W	1.4 Ac.	TR-V	2.1 Ac.	P1-A1	5.0 Ac.

Have the areas and flows from Retreat at TimberRidge Filing No. 2 at design point 15 been accounted for?

Yes. Tributary basins TR-W, TR-V and TR-7. See revised

P1-A2 6.4 Ac.	P1-A3 1.8 Ac.	P1-A4 2.0 Ac.
P1-A5 4.3 Ac.	P1-A6 2.8 Ac.	**Total 245.0 Ac.**

This single proposed full spectrum facility is planned to be designed as a pond and useable park (play fields in the base). Based on construction phasing of the Preliminary Plan, the facility may also be built in phases with associated orifice plates to be switched out based on development. The anticipated first phase of development tributary to this facility is the Briargate Pkwy. improvements (reference "Drainage Letter for Sterling Ranch Road and Briargate Pkwy. Interim Plan", prepared by JR Engineering, LLC, dated December 2021 and "Sterling Ranch Road and Briargate Pkwy. Street Plans", prepared by JR Engineering, LLC, dated October 2021 for inlet and pipe sizes through this corridor) along with a small portion of the Sterling Ranch East Preliminary Plan No. 1 north of Briargate (42 lots) and the Sterling Ranch East Preliminary Plan/PUD No. 2 development. The outfall for this facility will continue to be the planned 48" RCP storm system as designed by JR Engineering, LLC as described in the plans mentioned above. Include where this system outfalls to. Added

Revised and added

Ster
Villa
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ones

The original MDDP as approved in 2018 proposed for a fairly significant inter-basin transfer of approximately 267 acres from East Fork Sand Creek into Sand Creek main basin. (See Excerpt below) While this transfer was still kept within the overall Sand Creek basin, there was concern of surface water rights for the immediate downstream properties just south of Sterling Ranch with this approved concept. In an effort to address this concern, this MDDP Amendment proposes to continue to release surface flows as close to pre-development condition as possible within the same historic basin location. (See Basin Exhibit below) These flows will either be treated in a formal full spectrum facility or provide WQCV runoff reduction prior to being released. Also, given the size of the historic basins and natural sheet flow characteristics at these outfall locations, this MDDP Amendment proposes a level spreader design at these locations. These facilities will help better disburse the developed flows in a historic sheet flow manner. Pre-development Design Point 6 that is currently within the East Fork basin would be the location for one of these planned facilities. Upon future Sterling Ranch East residential

(Excerpt from 2018 Sterling Ranch MDDP, M&S Civil Consultants, Inc.)

Step 2 **Implement BMPs that provide a water quality capture volume with slow release.** – Using Full Spectrum Detention Facilities which will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours. All storage facilities will be designed to meet State Statue SB15-212/ §37-92-602(8).

Step 3 **Stabilize streams.** – With the full spectrum detention facility in place, the runoff from the developments will be reduced to predevelopment conditions. The developed discharge from the sites will be less than existing and therefore is not anticipated to have negative effects on downstream drainage ways.

Step 4 **Consider need for Industrial and Commercial BMPs.** – No industrial land uses are proposed with this development. The proposed commercial development area will implement a Stormwater Management Plan (SWMP) incorporation proper housekeeping procedures. Onsite drainage will be routed through private Full Spectrum Detention (FSD) basins to minimize introduction of contaminates to the county's public drainage systems.

INTERBASIN TRANSFER EAST FORK SAND CREEK TO MAIN STEM SAND CREEK

It should be noted that the proposed development plan for the ~1444 acre of Sterling Ranch redistributes a small percentage of the historic watershed between the Sand Creek and East Fork of Sand Creek watershed.

Based upon the survey and contour mapping, prior to development approximately 682 acres of Sterling Ranch runoff was collected by the Sand Creek watershed with the remaining 762 acres was directed to the East Fork of Sand Creek.

After development approximately 267 acres will be redirected from the East Fork Sand Creek into the Sand Creek Basin, resulting in 949 acres of Sterling Ranch directed to the Sand Creek Basin with the remaining 495 acres directed to East Fork Sand Creek.

This modification is driven primarily by maximizing the area of land that can be delivered to the sanitary sewer lift station. It should be noted that the East Fork of Sand Creek is still tributary to the Main Branch of Sand Creek, and thus this transfer is between minor watersheds, not major watershed, and that the development as planned will still function to limit discharged runoff into Sand Creek and East Tributary to the historic flow rates. An exhibit was added to the appendix, which also accompanies the deviation request that shows this basin diversion.

It should be noted that the Developed Conditions Map (provided in the appendix) illustrated the diverted acreage based upon the DPBS mapped boundary(as mapped within the SCDBPS) and diversion based upon the actual field contour data.

Drainage Basin Descriptions

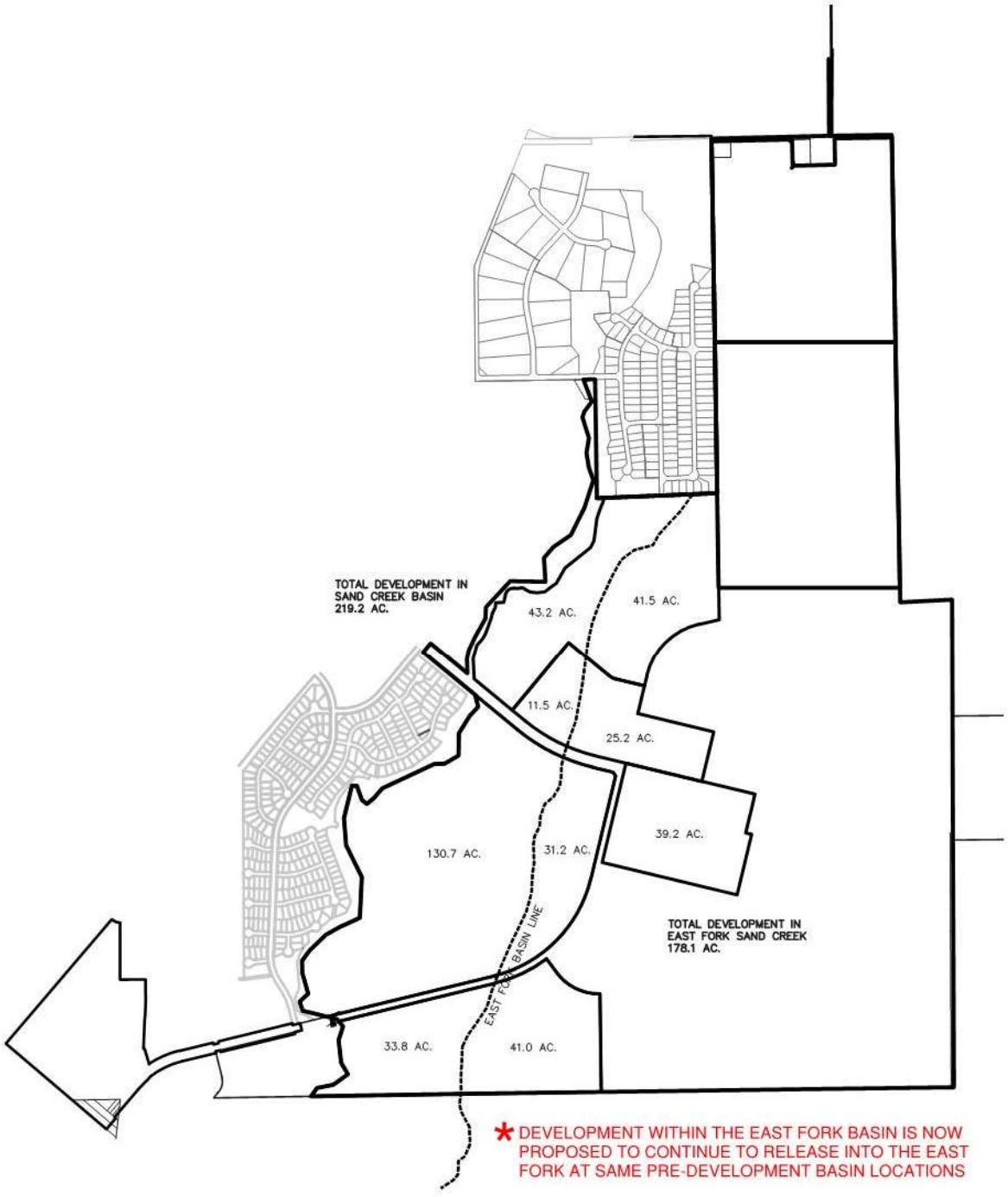
Developed Sand Creek (Main Stem) Basin Flows

Basin SC3-82 (Q5 = 33.2 cfs, Q100 = 132.3 cfs) which is located north of Sterling Ranch and Burgess Road to the east Basin SC3-81, assumes that the 117.8 is primarily undeveloped, pine forested land. In this undeveloped condition runoff from the basin continues south overland into Basin SC3-74.

Basin SC3-74 (Q5 = 36.5 cfs, Q100 = 140.7cfs) is a 119.7 acre area of 5 and 10-acre lots covered with a mixture of native prairie grasses and pine trees land located north of Sterling Ranch and south of Burgess Road to the west and north of Basins SC3-73 and SC3-75. Runoff from Basins SC3-74 and SC3-82, combine at DP-74 (Q5 = 65.3 cfs, Q100 = 262.8 cfs), which is equivalent to the anticipated existing modeled flow rates of Q5 = 65.3 cfs, Q100 = 262.8 cfs.

Basin SC3-73 (Q5 = 26.4 cfs, Q100 = 102.0 cfs) is a 90.0 acre area of 5 to 40 acres lots covered with a mixture of native prairie grasses and pine trees land located north of Sterling Ranch to the northeast of Vollmer Road. Runoff from the Basin SC3-73 will combine with runoff from DP-74 and will continue overland towards DP-75.

Basin SC3-81 (Q5 = 70.2 cfs, Q100 = 275.7 cfs) which is located north of Sterling Ranch (approx 1 mile) between Shoup and Burgess Roads, assumes that the 262.9 acre area of primarily undeveloped, pine forested, land. In this undeveloped condition runoff from the basin continues south overland into Basin SC3-75.



STERLING RANCH EAST INITIAL DEVELOPMENT PHASE
BASIN DEVELOPMENT EXHIBIT

CLASSIC CONSULTING ENGINEERS & SURVEYORS

Previously shown but now better described and shown on map

development further to the east within Basin EX10A, additional level spreader facilities will also be planned.

Indicate possible location of Future level spreader on developed drainage plan

Villages at Sterling Ranch? Include county project #.

The original MDDP as approved in 2018 proposed Basin SC3-14B to be 34.7 Ac. The proposed Sterling Ranch East Preliminary Plan/PUD No. 3 (submitted concurrently but separate submittal) development area encompasses additional property further to the east than originally depicted as Basin SC3-14B. The proposed basins that better represent the total tributary area for Pond FSD-14B are the proposed basins found in this report as P4-A (25.8 Ac.) and P4-B (37.3 Ac.). Thus, the total area is 63.1 Ac. Future basins SCE-7 and SCE-10 will be reduced by this same amount. The proposed Pond FSD-14B has been upsized accordingly to handle this additional developed flow. The outfall for this facility was originally planned to connect directly to the 48" RCP storm system within Sterling Ranch Road with an ultimate outfall location into Pond W3 and direct release into Sand Creek main channel. As mentioned in the previous paragraph, the outfall for this facility is now planned to head towards the south property line within a future pipe system. Ultimately, upon full build-out of this Preliminary Plan, a level spreader facility will be installed along the south property line as shown on the drainage map. In the interim, until full build-out, a temporary plunge pool may be installed just south of the pond to help dissipate these released treated flows. The release quantity from Pond FSD-14B will approximate the pre-developed flows for this original Basin EX-9.

Added

Include discussion on Ponds FSD-11 & FSD-14A

PROPOSED DRAINAGE CONDITIONS

As described in the General Description of the report, this proposed Preliminary Plan development contains 321+ acres that is geographically separated by two major roadways that are being final platted and constructed separately (Briargate Pkwy. and Sterling Ranch Rd.). Multiple full spectrum detention (FSD) facilities are planned with this overall Sterling Ranch East Preliminary Plan No. 1 development. They will be designed to handle these proposed lots, future adjacent development and the two other Sterling Ranch East Preliminary Plan/PUD Development Plans No. 2 and No. 3. (Submitted concurrently but under separate County file

Foursquare & Villages?

Revised

numbers) Development of these urban lots proposed will consist of overlot grading and utility installation for the planned roadways and lots. Per the El Paso County ECM, Section I.7.1.B, all urban lots are required to provide Water Quality Capture Volume (WQCV). Thus, the proposed FSD facilities within this development will provide WQCV along with an Excess Urban Runoff Volume (EURV) in the lower portion of the facility storage volume with an outlet control device. Frequent and infrequent inflows are released at rates approximating undeveloped conditions. This concept provides some mitigation of increased runoff volume by releasing a portion of the increased runoff at a low rate over an extended period of time, up to 72 hours. This means that frequent storms, smaller than the 2-year event, will be reduced to very low flows near or below the sediment carrying threshold value for downstream drainage ways. Also, by incorporating an outlet structure that limits the 100-year runoff to the undeveloped condition rate, the discharge hydrograph for storms between the 2 year and the 100-year event will approximate the hydrograph for the undeveloped conditions and will help effectively mitigate the effects of development. As reasonably possible, WQCV will be provided for all new roads and urban lots.

This report will generally describe overall anticipated developed basins tributary to each of the proposed FSD facilities. Each of these developed basins will then be detailed further in final drainage reports prepared and submitted along with Final Plats and CD's. This final design will include sizing of all inlets, storm systems and finalized FSD facilities including all required appurtenances. It is anticipated that Type-R at-grade and sump inlets ranging from 5' to 15' will be utilized in all street drainage and HGL's will be provided for all RCP storm system design.

The following developed basin descriptions will start at the north end of the project and move south and describe how this development proposes to handle both the off-site and on-site drainage conditions both from an interim standpoint based on construction phasing and the ultimate buildout scenario of the entire Sterling Ranch East ownership:

The following represent the basins and design points north of Briargate Pkwy.:

Added

As described earlier, these first several basins are all at the north end of the Sterling Ranch East overall property and are tributary to the adjacent Retreat at TimberRidge development and are consistent with what that approved report anticipated. (Reference "Final Drainage Report for Retreat at TimberRidge Filing No. 1", prepared by CCES, approved November 2020 and "Final Drainage Report for Retreat at TimberRidge Filing No. 2", prepared by CCES, dated March 2022)

List what bas
Indicate that
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The following basins are all contained within basin SC3-16A as presented in the MDDP for Sterling Ranch, prepared by M&S Civil Consultants, approved in 2018:

Include are
each basin
discussion

Added

Basin TR-V (Q_5 = 2 cfs, Q_{100} = 6 cfs) consists of rear yards of the adjacent Retreat at TimberRidge Filing No. 2 development. These flows are currently captured in a natural swale along the common property line and routed south and then west towards a temporary sediment basin at the end of Bison Valley Trail that was constructed with the TimberRidge development. With the development of this portion of the proposed Sterling Ranch East Preliminary Plan No. 1, these flows will likely remain being captured by the natural swale along the westerly property line but then be directed into **Basin P1-F** **(Q_5 = 111 cfs, Q_{100} = 215 cfs).** This basin represents the anticipated future urban residential basin tributary to a future downstream storm system within the northerly extension of Sterling Ranch Road. **Design Point 1 (Q_5 = 112 cfs, Q_{100} = 219 cfs)** represents the anticipated total developed flow at this location upon full build-out. In the interim, before development within this basin, the historic flow patterns may be captured in a temporary sediment basin located just east of Design Point 1. This facility will help mitigate the historic flows from the large upstream basin (EX-10) prior to and during the construction of the extension of Sterling Ranch Road, Pond FSD-16 and the northerly portion of this proposed Preliminary Plan area. The final drainage report(s) for this portion of t describe any temporary sediment basins and collection points for thes for safe routing further downstream.

If both basins TR-V & TR-W will continue to use the existing swale th directs both towards the temporary sedimentation pond, how does 1 end up in Basins P1-F and the other in P1-E?

See highlighted text above and below

Basin TR-W (Q_5 = 3 cfs, Q_{100} = 5 cfs) consists of rear yards and a small portion of the Bison Valley Trail roadway within the adjacent Retreat at TimberRidge Filing No. 2 development.

These flows are currently captured in a natural swale along the common property line and routed westerly towards a temporary sediment basin at the end of Bison Valley Trail that was constructed with the TimberRidge development. With the development of the proposed Sterling Ranch East – Phase 1, these temporary facilities will be removed and allowed to flow directly into Basin P1-E. **Basin P1-E (Q_5 = 83 cfs, Q_{100} = 161 cfs)** consists of the proposed urban residential at the north end of this Preliminary Plan, just east of Sand Creek and tributary to a proposed downstream storm system within the northerly extension of Sterling Ranch Road. **Design Points 2&3 (Q_5 = 42 cfs, Q_{100} = 81 cfs)** represent the anticipated split of flows from this large developed basin. The total developed flow will then combine with the upstream developed flows from Design Point 1 and be routed in a large diameter storm system further south within Sterling Ranch Road.

his flow not the P 2 & 3.

See revised text

If flows are spl DP 2 & 3 sepa

See revised text

Basin P1-C (Q_5 = 21 cfs, Q_{100} = 43 cfs) consists of the anticipated tributary area for the Sterling Ranch Road ROW extension north of Briargate Pkwy. and adjacent development. These proposed developed flows will be collected in various at-grade inlets within the roadway, combine with the upstream pipe flows described above and then routed towards the proposed Pond FSD-16. The total developed flow at this pipe outlet location into Pond FSD-16 is represented by **Design Point 4 (Q_5 = 186 cfs, Q_{100} = 374 cfs)**. The design of the required concrete forebay, impact structure and trickle channel at this outfall will be provided with the Final Drainage Report.

Foursquare project?

See revised text

Basin P1-D (Q_5 = 53 cfs, Q_{100} = 102 cfs) represents the urban residential basin that is made up of the entire Sterling Ranch East Preliminary Plan/PUD No. 2 area and a small portion of this proposed Preliminary Plan area just east of Sand Creek, north of Briargate Pkwy. This basin is tributary to **Design Point 5 (Q_5 = 53 cfs, Q_{100} = 102 cfs)** and a public storm system stub will be provided to connect to the system within Sterling Ranch Road.

Basins P1-A1 (Q_5 = 11 cfs, Q_{100} = 21 cfs), **Basin P1-A2 (Q_5 = 12 cfs, Q_{100} = 23 cfs)**, **Basin P1-A3 (Q_5 = 5 cfs, Q_{100} = 9 cfs)** and **Basin P1-A4 (Q_5 = 5 cfs, Q_{100} = 10 cfs)** all represent tributary area

within the Briargate Pkwy. roadway extension between Vollmer and Sterling Ranch Road. These basins have been studied in the "Drainage Letter for Sterling Ranch Road and Briargate Pkwy. Interim Plan", prepared by JR Engineering, LLC, dated December 2021. Reference this report as well as the "Sterling Ranch Road and Briargate Pkwy. Street Plans", prepared by JR Engineering, LLC, dated October 2021 for inlet and pipe sizes through this corridor. These final designed facilities are shown and labeled on the drainage map. However, the designed storm outfall alignment into the Pond FSD-16 will need to be adjusted as the intent of this report is to combine these flows with the previously described Design Point 5 developed flows along the proposed low point in Briargate Pkwy. just east of Sterling Ranch Road into one single outfall into Pond FSD-16 and represented by Design Point 7.

Design Point 6 (Q_5 = 17 cfs, Q_{100} = 33 cfs) is the location of the proposed low-point in Briargate Pkwy. just east of Sterling Ranch Road, with the following two basins being tributary to this sump condition. The emergency overflow release is planned to be around the corner and south down Sterling Ranch Road. **Basin P1-A5 (Q_5 = 10 cfs, Q_{100} = 19 cfs)** and **Basin P1-A6 (Q_5 = 7 cfs, Q_{100} = 14 cfs)** consist of the anticipated area within the ROW tributary to this low- point. The collected flows will then be routed via a storm system and combine with the previously described basins further west in Briargate Pkwy. and Design Point 5.

Added. See revised

Design Point 7 (Q_5 = 117 cfs, Q_{100} = 229 cfs) represents the total developed flows at this pipe outlet location into Pond FSD-16. The design of the required concrete forebay, impact structure and trickle channel at this outfall will be provided with the Final Drainage Report.

Includ for the within Sterli

The following basins are all contained within basin SC3-16B as presented in the MDDP for Sterling Ranch, prepared by M&S Civil Consultants, approved in 2018:

Basin P1-B (Q_5 = 55 cfs, Q_{100} = 108 cfs) consists of the anticipated tributary area for the future Sterling Ranch East urban residential area outside of this proposed Preliminary Plan. These anticipated future developed flows will be routed towards a downstream storm system. The total developed flow at this pipe system outlet location into Pond FSD-16 is represented by

Design Point 8 (Q_5 = 55 cfs, Q_{100} = 108 cfs). The design of the required concrete forebay, impact structure and trickle channel at this outfall will be provided with the Final Drainage Report. In the interim, before development within this basin, the historic flow patterns and quantities will continue to sheet flow in a southerly direction towards the proposed pond and Briargate Pkwy. The final drainage report(s) will describe any temporary sediment basins and collection points for these pre-development flows for safe routing around the development area and further downstream.

Basin P1-A (Q_5 = 6 cfs, Q_{100} = 19 cfs) consists of the anticipated tributary area from the adjacent future residential lots (rear yards only) along with the actual pond area itself. The developed sheet flows from this basin will sheet flow directly into the adjacent FSD-16 Pond where they will be formally treated.

As described in the MDDP Amendment portion of this report, the two FSD ponds planned in the 2018 MDDP (FSD16A and FSD16B) are now proposed to be combined into one facility (FSD-16) northeast of the intersection of Briargate Pkwy. and Sterling Ranch Road. The total anticipated developed flows entering this facility are as follows. (See Appendix for MHFD-Detention pond design sheets):

<u>Detention Pond FSD-16</u> (Full Spectrum EDB)

Total Tributary Acreage: 245.0 ac.

4.822 Ac.-ft. WQCV required

11.124 Ac.-ft. EURV required with 4:1 max. slopes

10.310 Ac.-ft. 100-yr. Storage

26.256 Ac.-ft. Total

Total Peak In-flow: Q_5 = 271 cfs, Q_{100} = 590 cfs

Pond Peak Design Release: Q_5 = 24 cfs, Q_{100} = 157 cfs

Pre-development Release: Q_5 = 52 cfs, Q_{100} = 244 cfs

(Ownership and maintenance by the Sterling Ranch East Metro District)

This facility will release into a large diameter downstream storm system within Briargate Pkwy. just east of the Sterling Ranch Road intersection. Please reference the "Drainage Letter for Sterling Ranch Road and Briargate Pkwy. Interim Plan", prepared by JR Engineering, LLC, dated December 2021 and the "Sterling Ranch Road and Briargate Pkwy. Storm Plans", prepared by JR Engineering, LLC, dated December 2021. These referenced design plans provide a 48" RCP outfall pipe at this location with an allowable release rate of (Q_5 = 9.2 cfs, Q_{100} = 156.6 cfs). The 2018 MDDP presents a combined total release rate for the originally planned two ponds (FSD16A and FSD16B) of (Q_5 = 8.8 cfs, Q_{100} = 174.9 cfs). As designed on the JR Engineering storm plans, this storm system will run in a southeasterly direction within the Sterling Ranch Roadway towards the crossing of Sand Creek. At this location, the pipe system will outfall into the planned Detention Pond W3. Reference the "Final Design Report for Sand Creek Restoration", prepared by JR Engineering, LLC, dated October 21, 2021 for these design documents.

See revised

Discuss propose 157 cfs) those as reports.

Basin SC-4 (Q_5 = 8 cfs, Q_{100} = 27 cfs) consists of the anticipated rear yards of the lots adjacent to the creek that will continue to sheet flows directly towards the Sand Creek corridor. At this time, these rear yards are not able to be captured and routed to a formal stormwater quality facility. However, given the minimal unconnected impervious area and sizeable receiving pervious are within this basin, the WQCV reduction = 100% with 0 untreated WQCV. (See Appendix)

The following represent the basins and design points south of Briargate Pkwy. and west of Sterling Ranch Road *all contained within basin SC3-14A as presented in the MDDP for Sterling Ranch, prepared by M&S Civil Consultants, approved in 2018:*

Basin P2-S1 (Q_5 = 68 cfs, Q_{100} = 133 cfs) consists of the anticipated basin for the proposed middle school site. These developed flows will be routed internally within the school site

property towards **Design Point 9** where a storm stub will be provided. This storm stub will then outfall into the proposed downstream storm system within Sterling Ranch Road. State which pond this flow ultimately releases to.

Added

Basin P2-B (Q_5 = 90 cfs, Q_{100} = 176 cfs) consists of the anticipated basin for this large urban residential area. These developed flows will be captured in multiple public storm systems on-site and routed towards the two storm stubs provided as shown at Design Points 10 and 11. **Design Points 10&11 (Q_5 = 45 cfs, Q_{100} = 88 cfs)** represent the anticipated split of flows from this basin. The total developed flow will then combine with the upstream developed flows from Design Point 9 and be routed in a large diameter storm system further south/west within Sterling Ranch Road.

are and

See revised

Basin P2-A (Q_5 = 10 cfs, Q_{100} = 33 cfs) consists of the better portion of the proposed park area. The developed sheet flows from this area are anticipated to sheet flow directly into the adjacent FSD-14A Pond where they will be formally treated.

Basin SC-3 (Q_5 = 14 cfs, Q_{100} = 32 cfs) consists of portions of the proposed linear park/open space along with the anticipated rear yards of the lots adjacent to the creek. This area will continue to sheet flow directly towards the Sand Creek corridor. At this time, these rear yards are anticipated to not be captured and routed to a formal stormwater quality facility. However, given the minimal unconnected impervious area and sizeable receiving pervious are within this basin, the WQCV reduction = 100% with 0 untreated WQCV. (See Appendix)

Basins P2-B1 (Q_5 = 7 cfs, Q_{100} = 13 cfs), **Basin P2-B2 (Q_5 = 5 cfs, Q_{100} = 10 cfs)**, **Basin P2-B3 (Q_5 = 7 cfs, Q_{100} = 13 cfs)**, **P2-B4 (Q_5 = 4 cfs, Q_{100} = 8 cfs)**, **Basin P2-B5 (Q_5 = 5 cfs, Q_{100} = 9 cfs)**, **Basin P2-B6 (Q_5 = 3 cfs, Q_{100} = 6 cfs)**, **P2-B7 (Q_5 = 6 cfs, Q_{100} = 12 cfs)**, **Basin P2-B8 (Q_5 = 3 cfs, Q_{100} = 7 cfs)**, **Basin P2-B9 (Q_5 = 5 cfs, Q_{100} = 11 cfs)**and **Basin P2-B10 (Q_5 = 5 cfs, Q_{100} = 10 cfs)** all represent tributary area within the Sterling Ranch Road roadway extension between Dines Blvd. and Briargate Pkwy. These final designed facilities (Type R curb inlets) are shown and labeled on the drainage map. These basins have been studied in the "Drainage Letter for Sterling Ranch

Road and Briargate Pkwy. Interim Plan", prepared by JR Engineering, LLC, dated December 2021. Please reference this report along with the "Sterling Ranch Road and Briargate Pkwy. Storm Plans", prepared by JR Engineering, LLC, dated December 2021 and the "Sterling Ranch Road and Briargate Pkwy. Street Plans", prepared by JR Engineering, LLC, dated October 2021. These referenced design plans provide for separate storm outfalls from each of the at-grade inlet locations within Sterling Ranch Road to daylight into a temporary graded channel on the north side of the roadway. This channel then routes the developed roadway flows towards FSD-14A Pond. The ultimate design proposed to handle these roadway flows along with the adjacent development of Basins PS-S1, P2-A and P2-B (as described above) will be a large diameter storm sewer located behind the curb within a proposed open space tract along the north side of Sterling Ranch Road. (See Drainage Map) All the designed curb inlets within this stretch of Sterling Ranch Road will then connect into this proposed storm system.

The original MDDP basin SC3-14A included the entire Sand Creek channel including both the in-line stock pond and the proposed Detention Pond W3. Thus, there is about a 30+ acre difference in area from this original basin vs. the actual development area tributary to the proposed FSD-14A Pond. The total anticipated developed flows entering this facility are as follows. (See Appendix for MHFD-Detention pond design sheets):

<u>Detention Pond FSD-14A</u> (Full Spectrum EDB)

Total Tributary Acreage: 130.8 ac.

2.770 Ac.-ft. WQCV required

6.512 Ac.-ft. EURV required with 4:1 max. slopes

5.636 Ac.-ft. 100-yr. Storage

14.918 Ac.-ft. Total

Total Peak In-flow: Q_5 = 163 cfs, Q_{100} = 345 cfs

Pond Peak Design Release: Q_5 = 19 cfs, Q_{100} = 129 cfs

Pre-development Release: Q_5 = 29 cfs, Q_{100} = 135 cfs

(Ownership and maintenance by the Sterling Ranch East Metro District)

The allowable release rate from this facility per the 2018 MDDP equals (Q_5 = 7.5 cfs, Q_{100} = 142.4 cfs). This facility is planned to release directly into the adjacent in-line Pond W3. Please reference "Final Design Report for Sand Creek Restoration", prepared by JR Engineering, LLC, dated October 21, 2021 for this pond design along with the adjacent Sand Creek improvements proposed in this area.

The following represent the basins and design points south of Briargate Pkwy. and east of Sterling Ranch Road *contained within basins SC3-14B, SCE-7 and SCE-10 as presented in the MDDP for Sterling Ranch, prepared by M&S Civil Consultants, approved in 2018:*

Basin P4-B (Q_5 = 63 cfs, Q_{100} = 123 cfs) consists of the anticipated basin for the proposed Villages at Sterling Ranch East PUD site. These developed flows will be collected via a public storm system on-site and then routed towards **Design Point 14** at the south edge of the site where a 48" RCP storm stub will be provided. This storm stub will then outfall in a southerly direction through future Sterling Ranch residential development towards Pond FSD-14B.

Basin P4-A (Q_5 = 41 cfs, Q_{100} = 80 cfs) consists of the anticipated tributary area for the future Sterling Ranch East urban residential area outside of this proposed Preliminary Plan. These anticipated future developed flows will be routed towards a downstream storm system represented by **Design Point 15.** These future developed flows then combine with the previously described developed flows from Design Point 14 and are routed into Pond FSD-14B.

Design Point 16 (Q_5 = 97 cfs, Q_{100} = 189 cfs) represents the total anticipated developed flows into Pond FSD-14B. The design of the required concrete forebay, impact structure and trickle channel at this outfall will be provided with the Final Drainage Report. In the interim, before development within this future basin P4-A, the developed flows from the Villages site may be routed via a temporary channel towards Pond FSD-14B. The final drainage report(s) will further describe any temporary conveyance facilities for these developed flows.

The original MDDP basin SC3-14B only included 34.7 acres tributary to Pond FSD-14B. The entire proposed Villages at Sterling Ranch East PUD site along with the planned future residential area due south is now proposed to be tributary to Pond FSD14-B. This total acreage equals 63.1 acres. The planned outfall for this facility as presented in the 2018 MDDP was to the west and into the previously mentioned 48" RCP outfall within Sterling Ranch Road from Pond FSD-16. However, based on this proposed MDDP Amendment, the ultimate outfall for this facility is now planned to be a 42"-48" RCP storm system routed in a southerly direction towards the south property line of the overall Sterling Ranch East ownership. At this location, a level spreader is proposed to evenly allow the developed, treated flows to exit the property within the Pre-development Basin EX-9 at DP6. The allowed release from Pond FSD-14B and the spreader facility will be equal to or less than the pre-developed flows at this location of (Q_5 = 57 cfs, Q_{100} = 124 cfs).

The total anticipated developed flows entering this facility are as follows. (See Appendix for MHFD-Detention pond design sheets):

Flows do not match pre-development flows shown developed drainage map at DP 6

See revised

In-flow rates do not match MHFD spreadsheet

See revised

<u>Detention Pond FSD-14B</u> (Full Spectrum EDB)

Total Tributary Acreage: 63.1 ac.

1.336 Ac.-ft. WQCV required

3.141 Ac.-ft. EURV required with 4:1 max. slopes

2.719 Ac.-ft. 100-yr. Storage

7.196 Ac.-ft. Total

Total Peak In-flow: Q_5 = 97 cfs, Q_{100} = 189 cfs

Pond Peak Design Release: Q_5 = 11 cfs, Q_{100} = 95 cfs

Pre-development Release: Q_5 = 57 cfs, Q_{100} = 124 cfs

(Ownership and maintenance by the Sterling Ranch East Metro District)

The following represent the basins and design points south of Sterling Ranch Road *contained within basin SC3-11B as presented in the MDDP for Sterling Ranch, prepared by M&S Civil Consultants, approved in 2018:*

Basin P3-A (Q_5 = 82 cfs, Q_{100} = 160 cfs) consists of the anticipated basin for the proposed urban residential at the south end of the overall Sterling Ranch East project. These developed flows will be collected via a public storm system on-site and then routed towards **Design Point 17** at the southwest edge of the site where a 48"-54" RCP storm stub will be provided. This storm stub will then outfall directly into the proposed Pond FSD-11B. The Sterling Ranch East Phase 1 Preliminary Plan in this area proposes RR-5 zoning adjacent to the south overall boundary. The lots presented in this area are all at least 1/2 ac. in size and typically 100' wide and 225' deep. **Basin EF-A (Q_5 = 7 cfs, Q_{100} = 20 cfs)** consists of rear portion of these proposed large lots along with a 75'+ wide buffer/utility corridor immediately adjacent to the south property line. This basin will be allowed to continue to sheet flow in a southerly direction off-site. At this time, these rear yards and buffer corridor are anticipated to not be captured and routed to a formal stormwater quality facility. However, given the minimal unconnected impervious area and sizeable receiving pervious are within this basin, the WQCV reduction = 100% with 0 untreated WQCV. (See Appendix) **Basin P3-C (Q_5 = 1 cfs, Q_{100} = 5 cfs)** consists of a small portion of the 75'+ wide buffer/utility corridor immediately adjacent to the south property line. This basin will be allowed to continue to sheet flow in a southerly direction off-site. No impervious development is anticipated within this basin and thus no formal stormwater quality feature is required for this small basin.

Basin P3-S2 (Q_5 = 25 cfs, Q_{100} = 50 cfs) consists of the anticipated basin for the proposed elementary school site. These developed flows will be routed internally within the school site property towards **Design Point 18** where a 36" RCP storm stub will be provided. This storm stub will then also outfall directly into the proposed Pond FSD-11B.

Basin SC-1 (Q_5 = 2 cfs, Q_{100} = 6 cfs) is a small basin due west of the elementary school site that consists of mainly the eastern slope of the Sand Creek channel. No impervious development is

proposed other than the required maintenance access road/trail as presented on the Sand Creek channel plans. At this time, this area is not anticipated to be captured and routed to a formal stormwater quality facility. However, given the minimal unconnected impervious area and sizeable receiving pervious are within this basin, the WQCV reduction = 100% with 0 untreated WQCV. (See Appendix)

The 2018 MDDP presented a total inflow to this facility of (Q_5 = 81.3 cfs, Q_{100} = 213.7 cfs) and an allowable release rate of (Q_5 = 4.5 cfs, Q_{100} = 69.6 cfs). The outlet pipe for this pond will outfall directly into Sand Creek just south of the Sterling Ranch Road crossing. Reference the "Final Design Report for Sand Creek Restoration", prepared by JR Engineering, LLC, dated October 21, 2021 for the Sand Creek channel design documents. The total anticipated developed flows entering this facility are as follows. (See Appendix for MHFD-Detention pond design sheets):

<u>Detention Pond FSD-11B</u> (Full Spectrum EDB)

Total Tributary Acreage: 64.5 ac.

1.387 Ac.-ft. WQCV required

3.266 Ac.-ft. EURV required with 4:1 max. slopes

2.792 Ac.-ft. 100-yr. Storage

7.445 Ac.-ft. Total

Total Peak In-flow: Q_5 = 98 cfs, Q_{100} = 201 cfs

Pond Peak Design Release: Q_5 = 8 cfs, Q_{100} = 68 cfs

Pre-development Release: Q_5 = 18 cfs, Q_{100} = 80 cfs

(Ownership and maintenance by the Sterling Ranch East Metro District)

DETENTION / STORMWATER QUALITY FACILITES

As required, storm water quality measures will be utilized in order to reduce the amount of sediment, debris and pollutants that are allowed to enter Sand Creek. These features include but are not limited to Full Spectrum Detention Basins and temporary sediment basins. Site Planning and design techniques for urban areas that require detention will provide a Water

Quality Capture Volume (WQCV) and Excess Urban Runoff Volume (EURV) in the lower portion of the facility storage volume that will release the more frequent storms at a slower rate to help minimize the effects of development of the property. The proposed detention/SWQ facilities are to be private facilities with ownership and maintenance by the Sterling Ranch Metropolitan District.

SAND CREEK CHANNEL IMPROVEMENTS

As mentioned previously, the Sand Creek channel exists along the extreme westerly edge of this property. All required improvements to the Sand Creek channel adjacent to this property are described in a separate report prepared by JR Engineering, "Final Design Report for Sand Creek Restoration", dated October 21, 2021. Please reference this report for all adjacent creek improvement requirements and associated wetland mitigation plans and permitting within jurisdictional waters. CORE Consultants is the wetland consultant working with JR Engineering, LLC on this stretch of Sand Creek. They are coordinating the effort with the Corps. of Eng. for the required 404 permitting for all the proposed channel improvements. The two public roadway crossings of Sand Creek (Briargate Pkwy. and Sterling Ranch Road) are currently covered under a 404 permit (Action No. SPA-2015-00428-SCO) with the previous land owner dated February 2016. JR Engineering, LLC is also coordinating a CLOMR/LOMR for this stretch of Sand Creek that is adjacent to the site and defined as Reach SC-8 (south of Briargate Pkwy.) and SC-9 north of Briargate Pkwy.).

DRAINAGE CRITERIA

Hydrologic calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014. General on-site and off-site basin design used for detention/SWQ basin sizing was calculated using the EPA Storm Water Management Model

method (SWMM) Ver. 5.1. Rain Gage inputs based on City of Colorado Springs 2-hr. design storm distributions. Basin imperviousness of the particular land uses in accordance with Table 6-6. The Horton infiltration method used in basin modeling. Mile High Flood District (MHFD)-Detention spreadsheet Ver. 4.05 used for Preliminary Detention/SWQ design. (See Appendix)

The City of Colorado Springs/El Paso County DCM requires the Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls. The Four Step Process pertains to management of smaller, frequently occurring storm events, as opposed to larger storms for which drainage and flood control infrastructure are sized. Implementation of these four steps helps to achieve storm water permit requirements.

At this point (MDDP level design), this site generally adheres to this **Four Step Process** as follows:

1. **Employ Runoff Reduction Practices:** Proposed urban lot impervious area (roof tops, patios, etc.) will sheet flow across landscape areas (yards) and open space areas to slow runoff and increase time of concentration prior to being conveyed to the proposed public streets or detention facilities. This will minimize directly connected impervious areas within the project site. Water quality reduction will be employed for specific areas that are anticipated not able to be captured and routed to SWQ facilities.

2. **Stabilize Drainageways:** After developed flows utilize the runoff reduction practices through the front and rear yards, developed flows will travel via curb and gutter within the public streets of the development and eventually public storm systems. These collected flows are then routed directly to multiple extended detention basins (full-spectrum facilities). Sand Creek improvements and restoration plans are being proposed for this entire reach as described in “Final Design Report for Sand Creek Restoration”, prepared by JR Engineering, LLC, dated October 21, 2021.

3. **Provide Water Quality Capture Volume (WQCV):** Runoff from this development will be treated through capture and slow release of the WQCV and excess urban runoff volume (EURV) in the proposed Full-Spectrum permanent Extended Detention Basins designed per current El Paso County drainage criteria.

4. **Consider need for Industrial and Commercial BMPs**: No industrial uses are proposed within this development. A site-specific storm water quality and erosion control plan and narrative will be submitted along with the grading and erosion control plan. Details such as site-specific sediment and erosion control construction BMP's as well as temporary and permanent BMP's were detailed in this plan and narrative to protect receiving waters. BMP's will be constructed and maintained as the development has been graded and erosion control methods employed.

Include discussion on downstream facilities, at each DP where flows exit site, and their ability to accept and handle developed flows.

Added discussion for each DP in the exist. conditions section of the report.

FLOODPLAIN STATEMENT

Portions of this site are located within a floodplain as determined by the Flood Insurance Rate Maps (F.I.R.M.) Map Numbers 08041C 0533G and 08041C 0535G with effective dates of December 7, 2018 and the previously mentioned LOMR 08-08-0541P with an effective date of July 23, 2009. (See Appendix). JR Engineering, LLC is coordinating a CLOMR/LOMR for this stretch of Sand Creek that is adjacent to the site and defined as Reach SC-8 (south of Briargate Pkwy.) and SC-9 north of Briargate Pkwy.).

DRAINAGE AND BRIDGE FEES

This site lies entirely within the Sand Creek Drainage Basin boundaries.

Fees are calculated using the following impervious acreage method approved by El Paso County. The final fee estimate will be included in the Final Drainage Report(s), however, the following represent fee estimates based on the Sterling Ranch East Preliminary Plan No. 1 submittal with a total area of 321.37 acres with the following different land uses proposed:

Development Parcel North of Briargate Blvd.

11.98 Ac.	Sand Creek Corridor
8.83 Ac.	Open Space
63.93 Ac.	0.20 Ac. avg. lot size
84.74 Ac.	**Total**

Development Parcel South of Briargate Blvd. / North of Sterling Ranch Rd.

28.99 Ac.	Sand Creek Corridor
34.40 Ac.	Open Space / Park / Pond
59.96 Ac.	0.18 Ac. avg. lot size
38.55 Ac.	School Site
161.90 Ac.	**Total**

Development Parcel South of Sterling Ranch Rd.

3.48 Ac.	Sand Creek Corridor
9.63	Open Space / Pond
39.83 Ac.	0.24 Ac. avg. lot size
9.93 AC.	1/2 AC. Lot size
11.86 Ac.	School Site
74.73 Ac.	**Total**

The percent imperviousness for this subdivision is calculated as follows:

Fees for Sand Creek Drainage Corridor

(Per El Paso County Percent Impervious Chart: 2**%**)

44.45 Ac. x 2% = **0.89 Impervious Ac.**

Fees for Detention Facilities & Park

(Per El Paso County Percent Impervious Chart: 7**%**)

52.86 Ac. x 7% = **3.70 Impervious Ac.**

Fees for 0.18 Ac. Avg. lots

(Per El Paso County Percent Impervious Chart: 46**%)**

59.96 Ac. x 46% = **27.58 Impervious Ac.**

Fees for 0.20 Ac. Avg. lots

(Per El Paso County Percent Impervious Chart: 43**%**)

63.93 Ac. x 43% = **27.49 Impervious Ac.**

Fees for 0.24 Ac. Avg. lots

(Per El Paso County Percent Impervious Chart: 41%)

39.83 Ac. x 41% = **16.33 Impervious Ac.**

Fees for 1/2 Ac. Avg. lots

(Per El Paso County Percent Impervious Chart: 25**%**)

9.93 Ac. x 25% = **2.48 Impervious Ac.**

Fees for School Site

(Per El Paso County Percent Impervious Chart: 70**%**)

50.41 Ac. x 70% = **35.29 Impervious Ac.**

Total Impervious Acreage: 111.28 Imp. Ac.

The following calculations are based on the 2022 Sand Creek drainage/bridge fees:

ESTIMATED FEE TOTALS:

Bridge Fees

$ 8,923.00 x 111.28 Impervious Ac. = **$ 992,951.44**

Drainage Fees

$ 21,814.00 x 111.28 Impervious Ac. = **$ 2,427,461.92**

SUMMARY

The proposed Sterling Ranch East Preliminary Plan No. 1 is within the Sand Creek Drainage Basin. Recommendations are made within this report concerning necessary improvements that will be required as a result of development of this property. The points of storm water release from the proposed site are required to be at or below the calculated historic flow quantities. The development of the proposed site does not significantly impact any downstream facility or property to an extent greater than that which currently exists in the pre-development conditions. All drainage facilities within this report were sized according to the Drainage Criteria Manuals and the full-spectrum storm water quality requirements.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC

Marc A. Whorton, P.E.
Project Manager

maw/118322/PDR.doc

REFERENCES

1. City of Colorado Springs/County of El Paso Drainage Criteria Manual as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

2. "Urban Storm Drainage Criteria Manual Volume 1, 2 & 3" Urban Drainage and Flood Control District, dated January 2016.

3. "Sand Creek Drainage Basin Planning Study," Kiowa Engineering Corporation, dated March 1996.

4. "2018 Sterling Ranch MDDP", M&S Civil Consultants, Inc., June 2018

5. "Final Drainage Report for Retreat at TimberRidge Filing No. 1", Classic Consulting, approved November, 2020.

6. "Final Drainage Report for Retreat at TimberRidge Filing No. 2", Classic Consulting, dated March, 2022

7. "Final Design Report for Sand Creek Restoration", JR Engineering, LLC, dated October 21, 2021

8. "Drainage Letter for Sterling Ranch Road and Briargate Pkwy. Interim Plan", prepared by JR Engineering, LLC, dated December 2021

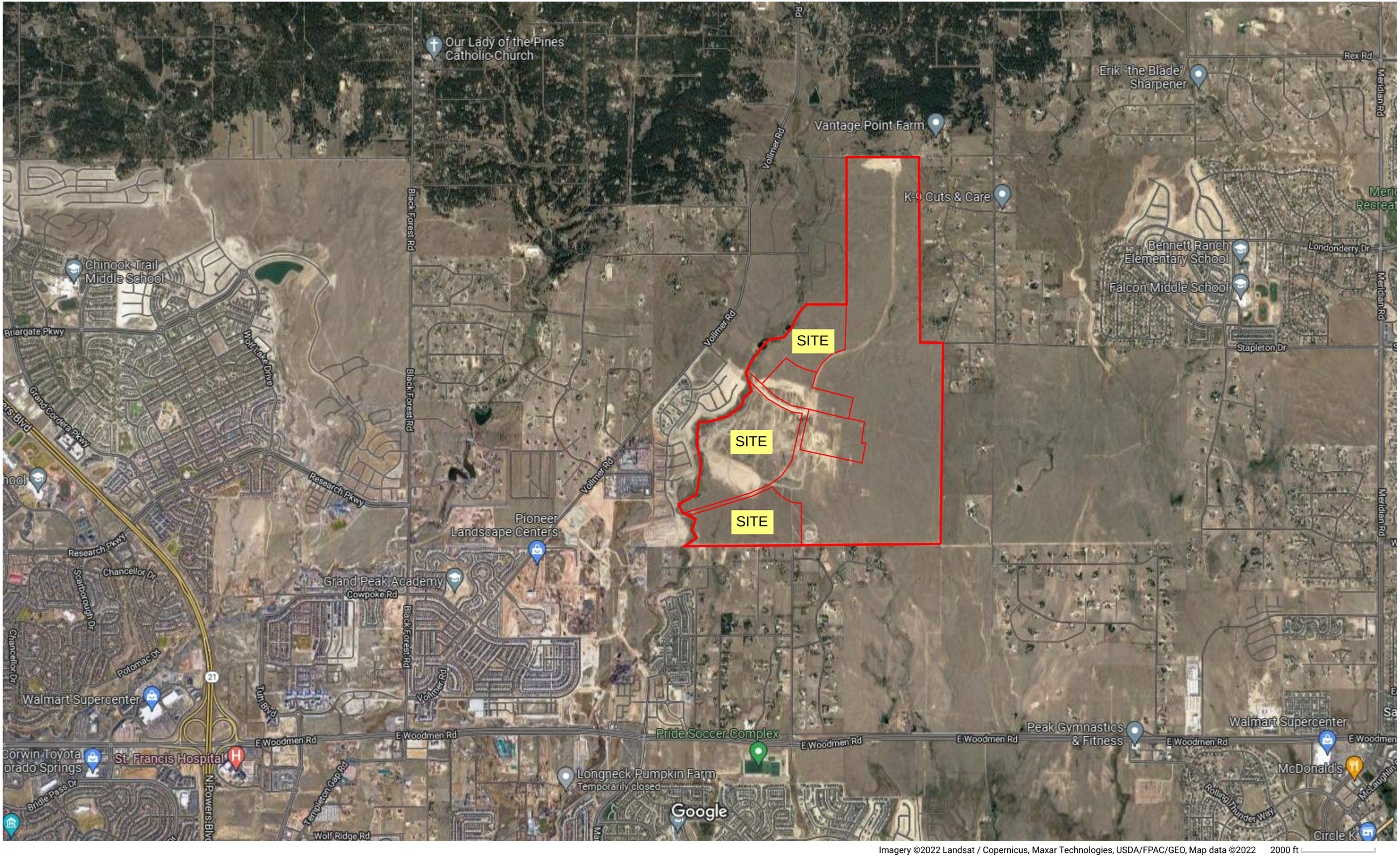
Include MDDP Amendment by JR Engineering.

Added

APPENDIX

VICINITY MAP

CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS

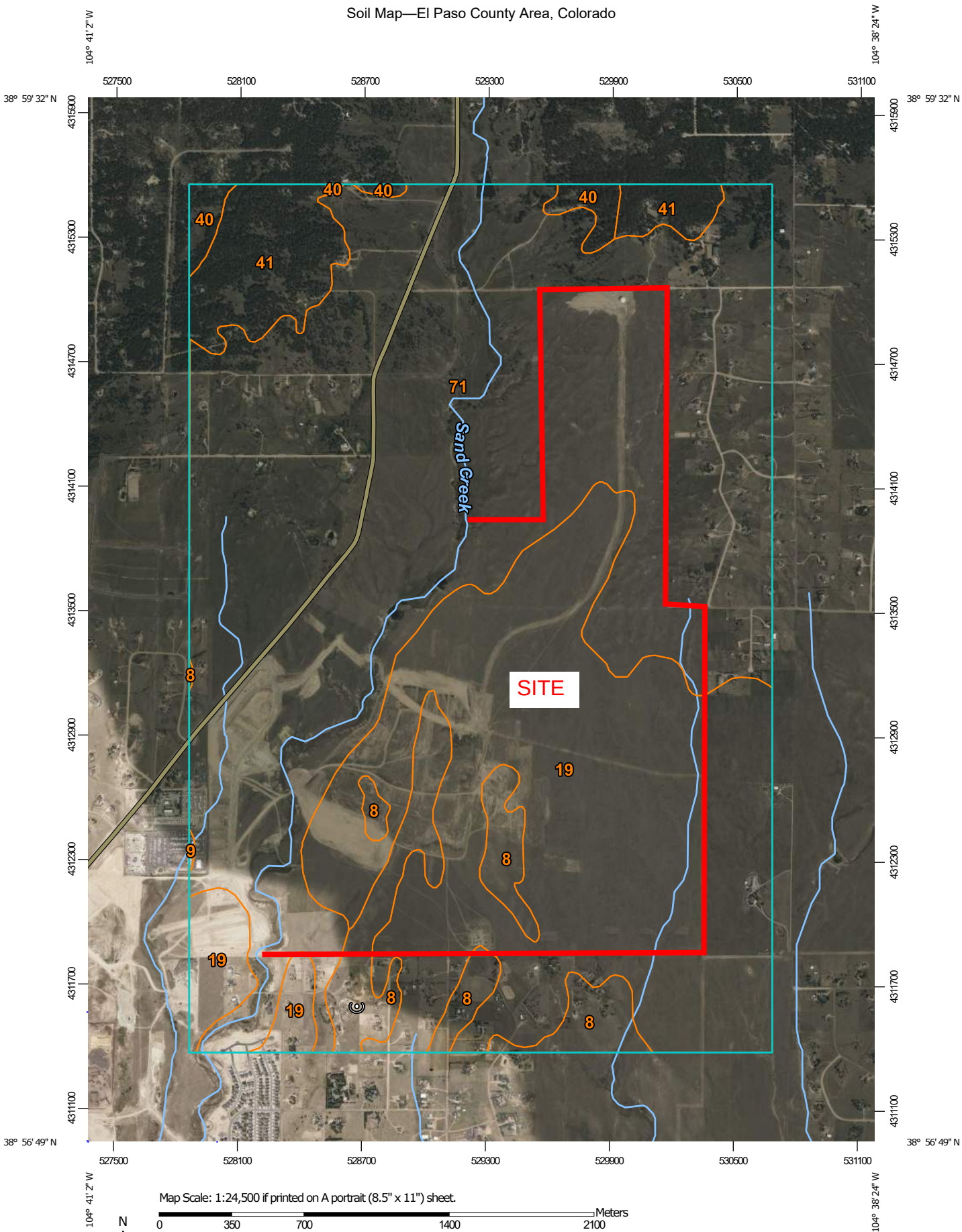


Imagery ©2022 Landsat / Copernicus, Maxar Technologies, USDA/FPAC/GEO, Map data ©2022 2000 ft

VICINITY MAP

SOILS MAP (S.C.S SURVEY)

CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS


104° 41' 2" W
104° 38' 24" W
38° 59' 32" N
38° 56' 49" N
527500
528100
528700
529300
529900
530500
531100
4315900
4315300
4314700
4314100
4313500
4312900
4312300
4311700
4311100
40
40
40
40
41
41
71
Sand Creek
8
8
8
8
9
19
19
19
SITE
Map Scale: 1:24,500 if printed on A portrait (8.5" x 11") sheet.
N
Meters
0
350
700
1400
2100
Feet
0
1000
2000
4000
6000
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

MAP LEGEND

Area of Interest (AOI)

- Area of Interest (AOI)

Soils

- Soil Map Unit Polygons
- Soil Map Unit Lines
- Soil Map Unit Points

Special Point Features

- Blowout
- Borrow Pit
- Clay Spot
- Closed Depression
- Gravel Pit
- Gravelly Spot
- Landfill
- Lava Flow
- Marsh or swamp
- Mine or Quarry
- Miscellaneous Water
- Perennial Water
- Rock Outcrop
- Saline Spot
- Sandy Spot
- Severely Eroded Spot
- Sinkhole
- Slide or Slip
- Sodic Spot
- Spoil Area
- Stony Spot
- Very Stony Spot
- Wet Spot
- Other
- Special Line Features

Water Features

- Streams and Canals

Transportation

- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

Background

- Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	171.3	5.8%
9	Blakeland-Fluvaquentic Haplaquolls	1.0	0.0%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	982.6	33.5%
40	Kettle gravelly loamy sand, 3 to 8 percent slopes	33.7	1.2%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	135.2	4.6%
71	Pring coarse sandy loam, 3 to 8 percent slopes	1,605.2	54.8%
Totals for Area of Interest		**2,929.0**	**100.0%**

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v
Elevation: 4,600 to 5,800 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 48 degrees F
Frost-free period: 125 to 145 days
Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent
Minor components: 2 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats
Landform position (three-dimensional): Side slope, talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand
AC - 11 to 27 inches: loamy sand
C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent
Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent
Landform: Depressions
Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

El Paso County Area, Colorado

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p
Elevation: 6,500 to 7,300 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F
Frost-free period: 125 to 145 days
Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 97 percent
Minor components: 3 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Columbine

Setting

Landform: Flood plains, fan terraces, fans
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam
C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: R049XY214CO - Gravelly Foothill
Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: 1 percent

Landform: Swales
Hydric soil rating: Yes

Other soils
Percent of map unit: 1 percent
Hydric soil rating: No

Pleasant
Percent of map unit: 1 percent
Landform: Depressions
Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

El Paso County Area, Colorado

71—Pring coarse sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 369k
Elevation: 6,800 to 7,600 feet
Farmland classification: Not prime farmland

Map Unit Composition

Pring and similar soils: 85 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pring

Setting

Landform: Hills
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Arkosic alluvium derived from sedimentary rock

Typical profile

A - 0 to 14 inches: coarse sandy loam
C - 14 to 60 inches: gravelly sandy loam

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 6.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: B
Ecological site: R048AY222CO - Loamy Park
Hydric soil rating: No

Minor Components

Pleasant

Percent of map unit:
Landform: Depressions
Hydric soil rating: Yes

Other soils

Percent of map unit:
Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

F.E.M.A. MAP / LOMR (08-08-0541P)

CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS

EL PASO COUNTY
UNINCORPORATED AREAS
080059

SUBLETTE RD
IC FERRAN RD
TOLTEC LN
THOMAS RD
HUNTSMAN RD
RD
ON RD
GLENSIDE DR
WILDFLOWER RD
POCO RD
PINE MEADO
PINE CONE LN
FAWN LN
TANGLEWILD LN
BUCKSKI
DERRINGTON CT
SHIPMAN LN
TAIGA LN
VOLLMER RD
BENNISON TER
MILLARD WAY
RAYGOR RD
PINE PARK TRL
ROCKI LN
SALBECK LN
RODGWICK HEIGHTS
FLAMING SUN DR
LIMIT OF STUDY
ARROYA LN
ZONE AE
7242
7235
DU
7231
DT
7225
DS
7220
7216
7210
DR
7205
7198
7192
DQ
7187
7183
DP
7177
7169
7162
DO
Sand Creek
DL
DM
DK
7128
DJ
7120
7116
DI
7111
7105
ZONE AE
DB
DA
DC
7050
ZONE AE
CY
7042
7037
7033
7025
7020
CX
7017
6998
6995
6991
CU
ZONE AE
MUSTANG PL
6987
6979
6972
6964
6957
CT
ZONE AE
6951
6944
CB
6941
6934
6930
6926
CR
6924
6920
ZONE AE
6915
6910
CQ
6906
6902
6900
6896
Sand Creek
6891
CP
6886
6885
CITY OF COLORADO SPRINGS
080060
GLIDER LOOP
VOLLMER PL
ASO COUNTY
RPORATED AREAS
080059
CORNISE RD
MUSTANG RD
KENOSHA DR
PONCA RD
MAVERICK RD
MOHAWK RD
BRULE RD
EL PASO COUNTY
UNINCORPORATED AREAS
080059
EL PASO COUNTY
UNINCORPOBATED AREAS
080059
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R. 13 E.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A — No Base Flood Elevations determined.
- ZONE AE — Base Flood Elevations determined.
- ZONE AH — Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO — Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR — Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99 — Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V — Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE — Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

- ZONE X — Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

- ZONE X — Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D — Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D Boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- 513 — Base Flood Elevation line and value; elevation in feet*
- (EL 987) — Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

- A — A — Cross section line
- 23 — 23 — Transect line
- 97° 07' 30.00" / 32° 22' 30.00" — Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 4175000mN — 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 6000000 FT — 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection
- DX5510 — Bench mark (see explanation in Notes to Users section of this FIRM panel)
- M1.5 — River Mile

MAP REPOSITORIES
Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 1000'
500 0 1000 2000 FEET
200 0 300 600 METERS

NFIP
NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0533G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO
AND INCORPORATED AREAS

PANEL 533 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0533	G
EL PASO COUNTY	080059	0533	G

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0533G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

NFIP
NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0535G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO
AND INCORPORATED AREAS

PANEL 535 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0535	G
EL PASO COUNTY	080059	0535	G

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0535G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT

COMMUNITY AND REVISION INFORMATION		PROJECT DESCRIPTION	BASIS OF REQUEST
COMMUNITY	El Paso County Colorado (Unincorporated Areas)	NO PROJECT	HYDRAULIC ANALYSIS NEW TOPOGRAPHIC DATA
	COMMUNITY NO.: 080059		
IDENTIFIER	Sand Creek Letter of Map Revision, Mustang Place to Arroya Lane	APPROXIMATE LATITUDE & LONGITUDE: 38.971, -104.668 SOURCE: USGS QUADRANGLE DATUM: NAD 27	

ANNOTATED MAPPING ENCLOSURES	ANNOTATED STUDY ENCLOSURES
TYPE: FIRM* NO.: 08041C0535 F DATE: March 17, 1997	DATE OF EFFECTIVE FLOOD INSURANCE STUDY: August 23, 1999 PROFILE(S): 204P(a), 204P(b), 204P(c) AND 204P(d) FLOODWAY DATA TABLE: 5

Enclosures reflect changes to flooding sources affected by this revision.
* FIRM - Flood Insurance Rate Map; ** FBFM - Flood Boundary and Floodway Map; *** FHBM - Flood Hazard Boundary Map

FLOODING SOURCE(S) & REVISED REACH(ES)

Sand Creek - from approximately 360 feet downstream of Mustang Place to just downstream of Arroya Lane

SUMMARY OF REVISIONS

Flooding Source	Effective Flooding	Revised Flooding	Increases	Decreases
Sand Creek	Zone A	Zone AE	YES	YES
	No BFEs*	BFEs	YES	NONE
	No Floodway	Floodway	YES	NONE

* BFEs - Base Flood Elevations

DETERMINATION

This document provides the determination from the Department of Homeland Security's Federal Emergency Management Agency (FEMA) regarding a request for a Letter of Map Revision (LOMR) for the area described above. Using the information submitted, we have determined that a revision to the flood hazards depicted in the Flood Insurance Study (FIS) report and/or National Flood Insurance Program (NFIP) map is warranted. This document revises the effective NFIP map, as indicated in the attached documentation. Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals in your community.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at http://www.fema.gov/nfip.

David N. Bascom

David N. Bascom, Program Specialist
Engineering Management Branch
Mitigation Directorate

112553 10.3.1.08080541 102-I-A-C

Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION
DETERMINATION DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

APPLICABLE NFIP REGULATIONS/COMMUNITY OBLIGATION

We have made this determination pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (P.L. 93-234) and in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, P.L. 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria, including adoption of the FIS report and FIRM, and the modifications made by this LOMR, are the minimum requirements for continued NFIP participation and do not supersede more stringent State/Commonwealth or local requirements to which the regulations apply.

We provide the floodway designation to your community as a tool to regulate floodplain development. Therefore, the floodway revision we have described in this letter, while acceptable to us, must also be acceptable to your community and adopted by appropriate community action, as specified in Paragraph 60.3(d) of the NFIP regulations.

COMMUNITY REMINDERS

We based this determination on the 1-percent-annual-chance flood discharges computed in the FIS for your community without considering subsequent changes in watershed characteristics that could increase flood discharges. Future development of projects upstream could cause increased flood discharges, which could cause increased flood hazards. A comprehensive restudy of your community's flood hazards would consider the cumulative effects of development on flood discharges subsequent to the publication of the FIS report for your community and could, therefore, establish greater flood hazards in this area.

Your community must regulate all proposed floodplain development and ensure that permits required by Federal and/or State/Commonwealth law have been obtained. State/Commonwealth or community officials, based on knowledge of local conditions and in the interest of safety, may set higher standards for construction or may limit development in floodplain areas. If your State/Commonwealth or community has adopted more restrictive or comprehensive floodplain management criteria, those criteria take precedence over the minimum NFIP requirements.

We will not print and distribute this LOMR to primary users, such as local insurance agents or mortgage lenders; instead, the community will serve as a repository for the new data. We encourage you to disseminate the information in this LOMR by preparing a news release for publication in your community's newspaper that describes the revision and explains how your community will provide the data and help interpret the NFIP maps. In that way, interested persons, such as property owners, insurance agents, and mortgage lenders, can benefit from the information.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at http://www.fema.gov/nfip.

David N. Bascom, Program Specialist
Engineering Management Branch
Mitigation Directorate

Federal Emergency Management Agency
Washington, D.C. 20472

LETTER OF MAP REVISION
DETERMINATION DOCUMENT (CONTINUED)

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Ms. Jeanine D. Petterson
Director, Mitigation Division
Federal Emergency Management Agency, Region VIII
Denver Federal Center, Building 710
P.O. Box 25267
Denver, CO 80225-0267
(303) 235-4830

STATUS OF THE COMMUNITY NFIP MAPS

We will not physically revise and republish the FIRM and FIS report for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel(s) and FIS report warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at http://www.fema.gov/nfip.

David N. Bascom, Program Specialist
Engineering Management Branch
Mitigation Directorate

Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION
DETERMINATION DOCUMENT (CONTINUED)

PUBLIC NOTIFICATION OF REVISION

PUBLIC NOTIFICATION

FLOODING SOURCE	LOCATION OF REFERENCED ELEVATION	BFE (FEET NGVD 29)		MAP PANEL NUMBER(S)
		EFFECTIVE	REVISED	
Sand Creek	Just upstream of Mustang Place	None	6,984	08041C0535 F
	Just downstream of Arroya Lane	None	7,238	08041C0535 F

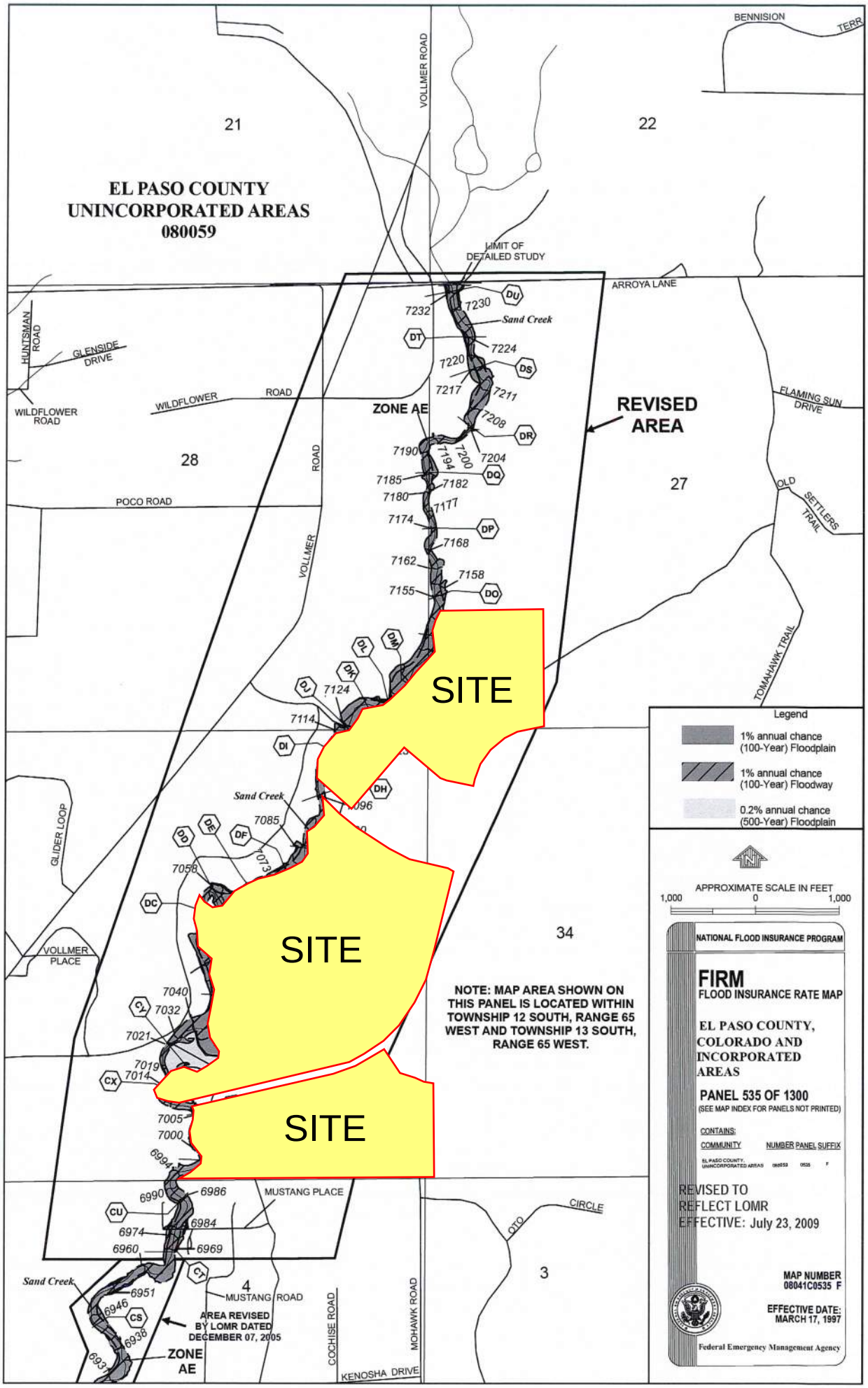
Within 90 days of the second publication in the local newspaper, a citizen may request that we reconsider this determination. Any request for reconsideration must be based on scientific or technical data. Therefore, this letter will be effective only after the 90-day appeal period has elapsed and we have resolved any appeals that we receive during this appeal period. Until this LOMR is effective, the revised BFEs presented in this LOMR may be changed.

A notice of changes will be published in the *Federal Register*. A short notice also will be published in your local newspaper on or about the dates listed below. Please refer to FEMA's website at https://www.floodmaps.fema.gov/fhm/Scripts/bfe_main.asp for a more detailed description of proposed BFE changes, which will be posted within a week of the date of this letter.

LOCAL NEWSPAPER Name: *El Paso County News*
Dates: 03/18/09 03/25/09

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at http://www.fema.gov/nfip.

David N. Bascom, Program Specialist
Engineering Management Branch
Mitigation Directorate


EL PASO COUNTY
UNINCORPORATED AREAS
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LIMIT OF DETAILED STUDY
ZONE AE
REVISED AREA
SITE
SITE
SITE
Sand Creek
VOLLMER ROAD
ARROYA LANE
BENNISION TERR
HUNTSMAN ROAD
GLENSIDE DRIVE
WILDFLOWER ROAD
WILDFLOWER ROAD
POCO ROAD
VOLLMER ROAD
VOLLMER
FLAMING SUN DRIVE
OLD SETTLERS TRAIL
TOMAHAWK TRAIL
GLIDER LOOP
VOLLMER PLACE
MUSTANG PLACE
MUSTANG ROAD
CIRCLE
OTO
COCHISE ROAD
MOHAWK ROAD
KENOSHA DRIVE
AREA REVISED BY LOMR DATED DECEMBER 07, 2005
ZONE AE
NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.
Legend
1% annual chance (100-Year) Floodplain
1% annual chance (100-Year) Floodway
0.2% annual chance (500-Year) Floodplain
APPROXIMATE SCALE IN FEET
1,000 0 1,000
NATIONAL FLOOD INSURANCE PROGRAM
FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO AND INCORPORATED AREAS
PANEL 535 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)
CONTAINS:
COMMUNITY NUMBER PANEL SUFFIX
EL PASO COUNTY, UNINCORPORATED AREAS 080059 0535 F
REVISED TO REFLECT LOMR EFFECTIVE: July 23, 2009
MAP NUMBER 08041C0535 F
EFFECTIVE DATE: MARCH 17, 1997
Federal Emergency Management Agency

REFERENCE MATERIAL

MASTER DEVELOPMENT DRAINAGE PLAN FOR STERLING RANCH

OCTOBER 2018

Prepared for:

Morley-Bentley Investments, LLC
20 Boulder Crescent, 2nd Floor
Colorado Springs, CO 80903
(719) 471-1742

Prepared by:

CIVIL CONSULTANTS, INC.

20 Boulder Crescent, Suite 110
Colorado Springs, CO 80903
(719) 955-5485

Project #09-002
SKP-18-003
SF-17-024

at DP87 culminating in peak runoff rates within Sand Creek of Q5 = 374.6 cfs, Q100 = 1905.9 cfs.

Basin SC3-16A (Q5 = 120.4 cfs, Q100 = 351.8 cfs) consists of a 168.1 acre area located within Sterling Ranch, that is located north of Briargate Parkway and east of Sand Creek Channel. This portion of Sterling Ranch is planned to house residential development that ranges from low density rural lots 1 acres in size to medium density urban residential with lots ranging in size from 0.1 to 0.2 acres. Runoff from the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond (FSD16A), at the northwest corner of Briargate Parkway and Sterling Ranch Road. The treated detained flows from the pond will discharge to DP22 at peak flow rates of 8.8 cfs and 128.3 cfs in the 5 and 100 year events respectively.

Basin SC3-16B (Q5 = 53.7 cfs, Q100 = 143.8 cfs) consists of a 50.7 acre area located within Sterling Ranch, that is located north of Briargate Parkway and east of Sand Creek Channel. This portion of Sterling Ranch is planned for a low to medium density residential lots ranging in size from 0.1 to 0.2 acres lots and portions of roadways. Runoff from the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond (FSD16B), at the northeast corner of Briargate Parkway and Sterling Ranch Road. The treated detained flows from the pond will discharge to DP22 at peak flow rates of 0.4 cfs and 28.1 cfs in the 5 and 100 year events respectively. The combined peak flow rates from SC3-16B and FSD14A (DP22, Q5=8.8 cfs and Q100=174.9 cfs) will be conveyed south via storm sewer system to DP21.

Basin SC3-14B (Q5 = 34.3 cfs, Q100 = 94.1 cfs) consists of a 34.7 acre area located within of Sterling. Ranch, that is located between south of Briargate Parkway and east of Sterling Ranch Road, east of Sand Creek. This portion of Sterling Ranch is planned for a low to medium density residential lots ranging in size from 0.1 to 0.33 acres lots and portions of roadways. Runoff from the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond (FSD14B), at the south end of the basin. The treated detained flows from the pond will discharge to DP21 at peak flow rates of 0.3 cfs and 19.3 cfs in the 5 and 100 year events respectively. The combined peak flow rates from DP22 and FSD14B (DP21, Q5=8.8 cfs and Q100=174.9 cfs) will be conveyed to Pond W3 above the intersection of Sand Creek channel and Sterling Ranch Road.

Basin SC3-14A (Q5 = 175.4 cfs, Q100 = 466.3 cfs) consists of a 164.9 acre area located within of Sterling. Ranch, that is located between south of Briargate Parkway and east of Sterling Ranch Road, east of Sand Creek. This portion of Sterling Ranch is planned for a k-8 school site, several single family residential lots ranging in size from 0.2 to 0.33 acres lots as well as portions of park and open space. Runoff from the basin shall be collected and conveyed within street and storm sewer systems and directed to a full spectrum detention pond (FSD14A), at the southwest corner of the basin. The treated detained flows from the pond will discharge to Pond W3 at peak flow rates of 7.5 cfs and 142.2 cfs in the 5 and 100 year events respectively.

Basin SC3-13 (Q5 = 57.8 cfs, Q100 = 136.9 cfs) consists of a 41.0 acre area located within of Sterling. Ranch, that is located just the east of the Barbarick Subdivision and north of Sterling Ranch Road. This portion of Sterling Ranch is planned for residential lots ranging in size from 0.1 to 0.2 acres in size. Runoff from the basin shall be collected by storm sewer systems and conveyed to a full spectrum detention pond (FSD13) located in the south end of the basin, adjacent to sand creek. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 4.2 cfs and 47.2 cfs in the 5 and 100 year events respectively.

Runoff from DP87, DP21 and from FSD Ponds 13, and 14A will combine within the Sand Creek Channel at proposed Regional Pond Detention Facility W3. The purpose of the regional pond is to reduce the post development flow rates within the Sand Creek Channel at the Southern Sterling Ranch boundary to at or below the existing flow rates calculated by this report. The pond is also necessary due to the drainage basin diversion, as discussed in other parts of this report. The total combined discharge reaching the regional facility (Pond W-3) has been calculated at 374.5 cfs and 2204.1 cfs in the 5 and 100 year events respectively.

As conceptually designed the proposed facility will utilize a check/diversion wall located upstream of the existing stock pond and proposed detention facility that will function to divert base flows within the channel to aid in retaining a fixed water surface within the existing stock pond and in larger storm events diverted flows safely around the amenity to the west side to detention Pond W3. A small controlled outlet structure along with an improved downstream embankment will be added to the existing stock pond to stabilize it and retain a fixed maximum water surface elevation. In the larger detention pond eight (8) small 24" storm sewer pipe located within a separate embankment will allow for free flow discharge of 2 year runoff and begin to detain flows of 5 years and larger events. Flows exiting the small storm pipes or overtopping the separated embankment will enter a concrete forebay that conveys drainage to two (2) cell 8'h x10'w concrete box culvert (CBC) under Proposed Sterling Ranch Road to DP68. As the anticipated flow rate leaving the pond is planned to be less than 1,500 cfs, and the proposed culvert crossing is conceptually planned to have an open area of less than 200 ft sq of open area and thus will need to meet the headwater requirements of Table 6-5 of the DCM, which in this concept design is a ratio of about ~1.3. The total combined discharge calculated to leave the regional facility (Pond W-3) has been calculated at 200.3 cfs and 1,350.6 cfs in the 5 and 100 year events respectively, with a maximum 100 year water surface of 7017.3, a

HW/D ratio of ~1.3. The peak detained volume has been estimated at 78.2 ac-ft. A low point in Sterling Ranch Road will be designed adjacent to the facility to provide a safe overflow route. An exhibit showing the concept design and its various elements is included in the appendix of this report.

As previously discussed a Condition Letter of Map Revision and Letter of Map Revision (CLOMR/LOMR) will need to be processed through the Federal Emergency Management Agency (FEMA) to revise the hydrology to the Sand Creek Channel and allow for the remapping of the revised floodplains. It should be noted that the DBPS flow rates for Reach SC-8 (Reach 163) adjacent to this location were estimate to be 2,630 cfs and that the effective FEMA 100 year flow rate is 2,600cfs. A comparison table of the various flow rates is provided later in this text and on the accompanying drainage maps.

The final design of the culvert crossing and final determination of approved rates as well as the final pond design will be discussed within the future Sterling Ranch Channel Design Report and Sand Creek CLOMR/LOMR documents. No deviations for this pond and accompanying outlet structure are anticipated at this time.

It is important to note that the planned discharge outlet pipe for the FSD pond located to the west of the pond W3 will need to be extended to the downstream outlet side of the culvert to ensure that the 100 year water surface elevation with W3 does not affect the functionality of the adjacent FSD and its storm sewer systems.

In regards to timing, the need to construction this facility can be tied to the Sand Creek Channel improvements which is discussed within this report and also within the Subdivision Improvements Agreement. In no case should runoff from the East Fork of Sand Creek be diverted to the Main Branch of the Sand Creek Channel prior to the construction and of this facility.

Basin SC3-11A (Q5 = 7.8 cfs, Q100 = 24.3 cfs) consists of a 10.7 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, west of Sand Creek. This portion of Sterling Ranch consists of single family residential for lots ranging in size from 0.2 to 0.3 acres in size and open space associated with the Sand Creek Channel. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond FSD11A. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 0.9 cfs and 12.3 cfs in the 5 and 100 year events respectively just upstream of DP-63. It should be noted that this detention facility may not be necessary if grading can be oriented to force surface runoff to the west.

Basin SC3-11B (Q5 = 81.3 cfs, Q100 = 213.7 cfs) consists of a 76.6 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, east of Sand Creek. This portion of Sterling Ranch consists of single family residential planned for lots ranging in size from 0.2 to 0.3 acres in size and a portion of a park site and collector roadways. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems westward to a full spectrum detention pond FSD11B. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 4.5 cfs and 69.5 cfs in the 5 and 100 year events respectively. The runoff from DP68 and from FSD ponds 11A and 11B combine at DP63 at peak flow rates of Q5 = 201.0 cfs, Q100 = 1385.1, which is less than the anticipated existing modeled flow rates of Q5 = 430.7 cfs, Q100 = 1911.5 at DP63. Runoff from DP63 continues south within the Sand Creek Channel toward DP61.

Basin SC3-7 (Q5 = 69.9 cfs, Q100 = 157.2 cfs) consists of a 45.7 acre industrial zoned area, referred to as the Barbarick Subdivision, located outside of Sterling Ranch. Per the Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3and 4 the filing consists of four lots which upon which development will be constructed which will include adding a proposed Extended Detention Basin within Lot 4. This detention basin will provide water quality treatment for portions of Lots 1 & 2, and Lots 3 & 4. The EBD will structure will outfall at the south end of Lot 4 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow from the EDB pond will be Q5 = 0.3 cfs, Q100 = 45.9** cfs(**which includes pass through flows of 29.4 cfs). A second Sand Filter Basin water quality detention catchment will be provided at the southeast/downstream end of Lot 2. The SFB will outfall at the southeast corner of the Lot 2 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow the SFB pond will be Q5 = 0.1 cfs, Q100 = 3.6 cfs. At the initial writing of this report, neither EDB nor SFB structure has been fully constructed, and thus the assumption was made to utilize the full un-detained untreated runoff from the offsite development for onsite drainage planning purposes. Thus the downstream facilities planned within Sterling Ranch will account for the total un-detained runoff from the parcel of Q5 = 69.9 cfs, Q100 = 157.2 cfs and will plan to treat the total runoff onsite facilities. This provides a conservative approach for master planning. Runoff discharged from the property will be collected by proposed storm sewer within Sterling Ranch and routed to DP64. These facilities and their effects on drainage will be re-reviewed with subsequent drainage report and shall be implemented into final design and construction.

Basin SC3-6B (Q5=43.4 cfs, Q100=102.7 cfs) consists of a 30.9 acre area located within of Sterling Ranch, that is north of Sterling

Step 2 **Implement BMPs that provide a water quality capture volume with slow release.** – Using Full Spectrum Detention Facilities which will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours. All storage facilities will be designed to meet State Statue SB15-212/ §37-92-602(8).

Step 3 **Stabilize streams.** – With the full spectrum detention facility in place, the runoff from the developments will be reduced to predevelopment conditions. The developed discharge from the sites will be less than existing and therefore is not anticipated to have negative effects on downstream drainage ways.

Step 4 **Consider need for Industrial and Commercial BMPs.** – No industrial land uses are proposed with this development. The proposed commercial development area will implement a Stormwater Management Plan (SWMP) incorporation proper housekeeping procedures. Onsite drainage will be routed through private Full Spectrum Detention (FSD) basins to minimize introduction of contaminates to the county's public drainage systems.

INTERBASIN TRANSFER EAST FORK SAND CREEK TO MAIN STEM SAND CREEK

It should be noted that the proposed development plan for the ~1444 acre of Sterling Ranch redistributes a small percentage of the historic watershed between the Sand Creek and East Fork of Sand Creek watershed.

Based upon the survey and contour mapping, prior to development approximately 682 acres of Sterling Ranch runoff was collected by the Sand Creek watershed with the remaining 762 acres was directed to the East Fork of Sand Creek.

After development approximately 267 acres will be redirected from the East Fork Sand Creek into the Sand Creek Basin, resulting in 949 acres of Sterling Ranch directed to the Sand Creek Basin with the remaining 495 acres directed to East Fork Sand Creek.

This modification is driven primarily by maximizing the area of land that can be delivered to the sanitary sewer lift station. It should be noted that the East Fork of Sand Creek is still tributary to the Main Branch of Sand Creek, and thus this transfer is between minor watersheds, not major watershed, and that the development as planned will still function to limit discharged runoff into Sand Creek and East Tributary to the historic flow rates. An exhibit was added to the appendix, which also accompanies the deviation request that shows this basin diversion.

It should be noted that the Developed Conditions Map (provided in the appendix) illustrated the diverted acreage based upon the DPBS mapped boundary(as mapped within the SCDBPS) and diversion based upon the actual field contour data.

Drainage Basin Descriptions

Developed Sand Creek (Main Stem) Basin Flows

Basin SC3-82 (Q5 = 33.2 cfs, Q100 = 132.3 cfs) which is located north of Sterling Ranch and Burgess Road to the east Basin SC3-81, assumes that the 117.8 is primarily undeveloped, pine forested land. In this undeveloped condition runoff from the basin continues south overland into Basin SC3-74.

Basin SC3-74 (Q5 = 36.5 cfs, Q100 = 140.7cfs) is a 119.7 acre area of 5 and 10-acre lots covered with a mixture of native prairie grasses and pine trees land located north of Sterling Ranch and south of Burgess Road to the west and north of Basins SC3-73 and SC3-75. Runoff from Basins SC3-74 and SC3-82, combine at DP-74 (Q5 = 65.3 cfs, Q100 = 262.8 cfs), which is equivalent to the anticipated existing modeled flow rates of Q5 = 65.3 cfs, Q100 = 262.8 cfs.

Basin SC3-73 (Q5 = 26.4 cfs, Q100 = 102.0 cfs) is a 90.0 acre area of 5 to 40 acres lots covered with a mixture of native prairie grasses and pine trees land located north of Sterling Ranch to the northeast of Vollmer Road. Runoff from the Basin SC3-73 will combine with runoff from DP-74 and will continue overland towards DP-75.

Basin SC3-81 (Q5 = 70.2 cfs, Q100 = 275.7 cfs) which is located north of Sterling Ranch (approx 1 mile) between Shoup and Burgess Roads, assumes that the 262.9 acre area of primarily undeveloped, pine forested, land. In this undeveloped condition runoff from the basin continues south overland into Basin SC3-75.

LEGEND

BASIN ID — SC3-77

DESIGN POINT — 87

REACH IDENTIFIER — RT-17A

PROPERTY BNDRY

BASIN BOUNDARY

FLOW DIRECTION

STORM SEWER

FULL SPECTRUM DETENTION POND — FSD16

DETENTION POND — PNDW3

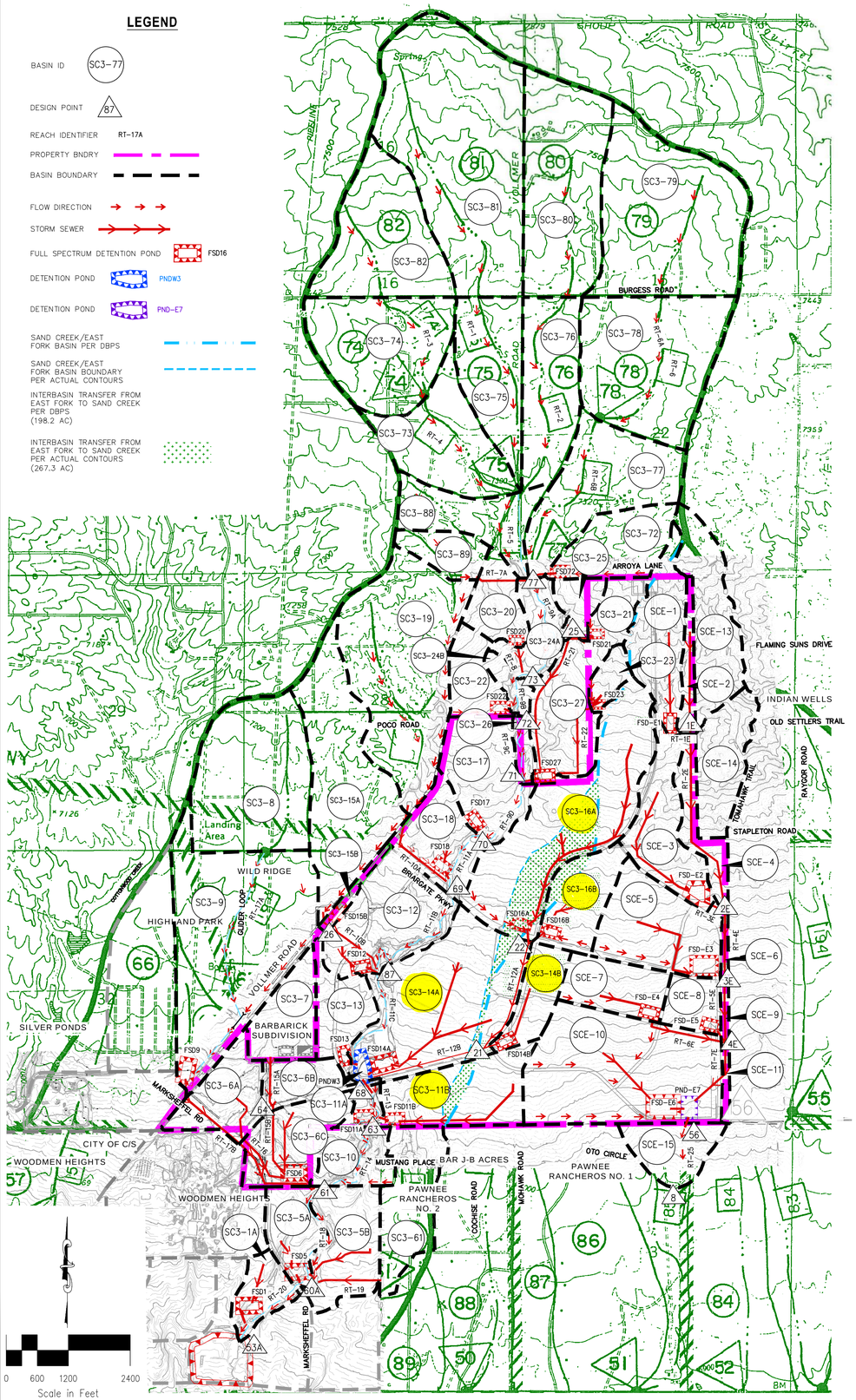
DETENTION POND — PND-E7

SAND CREEK/EAST FORK BASIN PER DBPS

SAND CREEK/EAST FORK BASIN BOUNDARY PER ACTUAL CONTOURS

INTERBASIN TRANSFER FROM EAST FORK TO SAND CREEK PER DBPS (198.2 AC)

INTERBASIN TRANSFER FROM EAST FORK TO SAND CREEK PER ACTUAL CONTOURS (267.3 AC)



BASIN SUMMARY

BASIN	CN	AREA (ACRES)	AREA (SQ MI)	Q_2 (CFS)	Q_5 (CFS)	Q_{10} (CFS)	Q_{25} (CFS)	Q_{50} (CFS)	Q_{100} (CFS)
SC3-1A	73	27.8	0.044	16.3	23.3	33.0	45.8	57.1	68.9
SC3-5A	84	39.1	0.061	40.6	53.7	71.0	92.4	110.6	129.1
SC3-5B	81	63.0	0.098	53.8	73.0	98.5	130.8	158.6	187.0
SC3-6A	88	49.3	0.077	61.4	79.3	102.2	130.1	153.6	177.1
SC3-6B	85	30.9	0.048	32.9	43.4	57.0	73.9	88.2	102.7
SC3-6C	82	58.0	0.091	53.9	72.5	97.1	128.0	154.5	181.5
SC3-7	88	45.7	0.071	54.0	69.9	90.3	115.2	136.2	157.2
SC3-8	62	143.4	0.224	25.4	42.1	66.7	100.7	132.3	166.2
SC3-9	66	217.4	0.340	45.8	71.5	108.6	158.9	204.9	254.0
SC3-10	63	36.0	0.056	7.6	12.3	19.4	29.1	38.0	47.7
SC3-11A	70	10.7	0.017	5.3	7.8	11.3	15.9	20.0	24.3
SC3-11B	80	76.6	0.120	59.4	81.3	110.8	148.1	180.5	213.7
SC3-12	81	88.2	0.138	77.8	105.6	142.5	189.1	229.1	270.0
SC3-13	85	41.0	0.064	43.9	57.8	76.0	98.5	117.6	136.9
SC3-14A	79	164.9	0.258	127.6	175.4	239.8	321.9	393.2	466.3
SC3-14B	77	34.7	0.054	24.6	34.3	47.4	64.2	79.0	94.1
SC3-15A	62	139.7	0.218	21.3	35.5	56.3	85.3	112.1	141.0
SC3-15B	87	7.9	0.012	10.8	14.0	18.2	23.3	27.6	31.9
SC3-16A	74	168.1	0.263	84.4	120.4	170.0	234.8	292.2	351.8
SC3-16B	78	50.7	0.079	39.0	53.7	73.6	99.0	121.1	143.8
SC3-17	73	70.6	0.110	41.8	59.6	85.2	119.0	149.1	180.6
SC3-18	81	53.8	0.084	49.3	67.1	91.0	121.2	147.3	174.0
SC3-19	62	184.0	0.287	28.8	47.7	75.7	114.4	150.2	188.8
SC3-20	65	34.2	0.053	9.9	15.5	23.8	35.1	45.5	56.6
SC3-21	66	23.3	0.036	7.0	10.8	16.3	23.7	30.4	37.5
SC3-22	65	33.9	0.053	9.4	14.8	22.5	32.9	42.5	52.6
SC3-23	67	14.5	0.023	5.5	8.3	12.4	18.0	23.0	28.4
SC3-24A	65	35.7	0.056	13.0	20.4	31.1	45.7	59.0	73.2
SC3-24B	65	12.2	0.019	3.4	5.3	8.1	11.8	15.2	18.9
SC3-25	66	19.0	0.030	5.8	8.9	13.4	19.5	25.1	31.0
SC3-26	63	10.0	0.016	2.5	4.0	6.2	9.2	12.1	15.1
SC3-27	71	70.0	0.109	35.1	51.2	73.8	103.7	130.3	158.3
SC3-61	63	65.5	0.102	13.7	22.2	34.4	51.6	67.6	84.8
SC3-72	64	56.2	0.088	12.8	20.2	31.4	46.7	60.9	76.0
SC3-73	63	90.0	0.141	16.4	26.4	41.3	62.1	81.3	102.0
SC3-74	63	119.7	0.187	22.3	36.5	57.3	85.9	112.3	140.7
SC3-75	63	79.3	0.124	13.1	21.5	33.7	50.5	66.1	82.8
SC3-76	63	86.4	0.135	14.2	23.1	36.4	54.6	71.4	89.6
SC3-77	62	106.9	0.167	16.6	27.6	43.8	66.2	87.0	109.4
SC3-78	63	155.6	0.243	28.1	45.3	70.6	106.2	139.1	174.5
SC3-79	63	189.0	0.295	34.9	57.0	89.5	134.3	175.6	220.1
SC3-80	63	147.7	0.231	27.3	44.3	69.6	104.5	136.8	171.4
SC3-81	62	262.9	0.411	42.6	70.2	111.0	167.4	219.6	275.7
SC3-82	62	117.8	0.184	20.0	33.2	52.8	80.0	105.1	132.1
SC3-88	62	60.2	0.094	10.5	17.4	27.6	41.8	54.9	69.0
SC3-89	62	27.5	0.043	6.1	10	15.7	23.6	30.8	38.6
SCE-1	65	64.4	0.101	23.3	35.9	53.8	79.1	102.4	127.4
SCE-2	64	15.0	0.023	4.4	7.0	10.8	15.9	20.7	25.7
SCE-3	70	67.5	0.105	30.6	45.2	65.9	93.3	118.0	143.9
SCE-4	70	29.5	0.046	13.3	19.6	28.6	40.6	257.8	62.6
SCE-5	87	85.5	0.134	100.4	130.6	169.6	217.4	257.8	298.4
SCE-6	64	3.8	0.006	1.6	2.5	3.7	5.4	7.0	8.6
SCE-7	89	44.9	0.070	58.9	75.5	96.6	122.2	143.7	165.2
SCE-8	92	25.5	0.040	38.6	48.4	60.7	75.4	87.7	99.9
SCE-9	64	4.0	0.006	1.5	2.4	3.6	5.3	6.8	8.5
SCE-10	83	174.3	0.272	7.6	189.4	19.4	29.1	398.9	467.5
SCE-11	64	5.8	0.009	2.3	3.6	5.5	8.0	10.3	12.8
SCE-13	63	78.6	0.123	19.6	31.3	48.7	73.1	95.7	120.0
SCE-14	63	52.5	0.082	13.2	21.2	33.3	49.9	65.2	81.7
SCE-15	51	39.7	0.062	2.2	5.1	10.1	17.7	25.1	33.4

DESIGN POINT SUMMARY

DESIGN POINT	AREA (SQ MI)	Q_2 (CFS)	Q_5 (CFS)	Q_{10} (CFS)	Q_{25} (CFS)	Q_{50} (CFS)	Q_{100} (CFS)	LOCATION
DP-74	0.371	39.3	65.3	104.8	158.9	209.1	262.8	
DP-75	1.413	141.2	235.1	376.6	566.6	750.9	950.5	
DP-77	2.343	209.9	351.9	580.6	886.6	1168.4	1467.7	ARROYA LANE X-ING
DP-78	0.538	59.7	98.4	154.0	232.6	306.2	385.3	
DP-73	2.471	207.5	354.3	588.5	897.1	1187.2	1506.7	
DP-72	2.543	206.2	352.5	586.7	897.2	1195.3	1518.6	POCO ROAD X-ING
DP-71	2.757	205.9	349.3	610.5	932.4	1226.9	1612.2	STERLING RANCH NORTHERN BNDRY
DP-70	2.867	205.3	349.8	614.0	940.1	1260.6	1636.7	
DP-69	3.238	212.7	366.6	653.7	1010.6	1364.1	1775.7	BRIARGATE PARKWAY X-ING
DP-87	3.594	216.9	374.6	681.9	1072.1	1471.5	1905.9	
DP-68	4.312	214.6	374.5	714.9	1187.6	1674.9	2204.1	UPSTREAM OF POND W3
DP-64	0.119	85.9	112.1	145.9	187.5	222.6	258.0	
DP-63	4.449	154.4	201.0	375.7	815.9	1112.1	1385.1	STERLING RANCH SOUTHERN BNDRY
DP-61	5.356	156.6	223.9	428.0	928.2	1287.3	1620.1	COLORADO SPRINGS/EL PASO BNDRY
DP-60A	5.617	161.6	224.8	439.1	950.4	1320.5	1661.8	MARKSHEFFEL X-ING
DP-53A	5.661	161.6	225.7	441.8	951.1	1326.0	1668.9	SAND CREEK AND POND 3
DP-1E	0.247	23.9	38.3	70.1	132.8	173.0	220.9	
DP-2E	0.486	48.9	76.8	123.0	228.7	319.7	419.4	
DP-3E	0.626	48.5	75.7	122.2	271.1	387.1	500.1	
DP-4E	0.745	48.1	76.2	122.4	286.9	407.3	534.8	
DP-56	1.017	23.1	35.3	71.5	108.3	152.1	196.4	NEAR SE PROP CORNER
DP-8	1.079	24.1	37.2	73.5	111.3	155.4	200.7	BELOW SE PROP CORNER
DP-21	0.396	0.6	8.8	17.8	57.1	116.8	174.9	
DP-22	0.342	0.6	8.8	17.6	56.8	105.1	156.4	
DP-25	0.066	5.9	9.1	16.3	35.1	46.4	58.2	
DP-26	0.012	0.1	1.1	3.2	7.3	9.5	12.0	

DESIGN POINT SUMMARY (VOLUME)

DESIGN POINT	AREA (SQ MI)	V_2 (AC-FT)	V_5 (AC-FT)	V_{10} (AC-FT)	V_{25} (AC-FT)	V_{50} (AC-FT)	V_{100} (AC-FT)	LOCATION
DP-74	0.371	5.9	9.0	13.6	19.8	25.5	31.6	
DP-75	1.413	22.7	34.5	51.7	75.4	97.1	120.5	
DP-77	2.343	37.7	57.4	85.9	125.1	161.1	199.9	ARROYA LANE X-ING
DP-78	0.538	8.9	13.5	20.1	29.3	37.7	46.7	
DP-73	2.471	40.0	60.8	91.0	132.5	170.7	211.7	
DP-72	2.543	41.3	62.9	94.0	136.8	176.2	218.5	POCO ROAD X-ING
DP-71	2.757	46.3	70.0	104.3	151.3	194.5	240.8	STERLING RANCH NORTHERN BNDRY
DP-70	2.867	49.5	74.5	110.6	160.1	205.4	254.0	
DP-69	3.238	57.5	86.1	127.4	183.8	235.3	290.6	BRIARGATE PARKWAY X-ING
DP-87	3.594	66.5	98.9	145.6	209.1	267.1	329.1	
DP-68	4.312	81.8	123.7	183.9	264.9	338.0	415.8	UPSTREAM OF POND W3
DP-64	0.119	7.0	9.1	11.8	15.2	18.1	21.1	
DP-63	4.449	85.6	129.5	192.3	276.7	352.8	433.5	STERLING RANCH SOUTHERN BNDRY
DP-61	5.356	103.7	157.8	235.1	338.4	431.3	529.8	COLORADO SPRINGS/EL PASO BNDRY
DP-60A	5.617	111.0	168.6	250.4	359.5	457.7	561.5	MARKSHEFFEL X-ING
DP-53A	5.661	112.0	170.0	252.6	362.6	461.7	566.5	SAND CREEK AND POND 3
DP-1E	0.247	3.1	5.2	8.4	12.7	16.6	20.9	
DP-2E	0.480	6.1	10.4	16.9	25.7	33.7	42.2	
DP-3E	0.620	7.0	13.7	23.4	36.1	47.4	59.3	
DP-4E	0.736	7.6	15.6	27.2	43.0	57.2	72.0	
DP-56	1.017	7.7	16.1	28.6	51.3	71.7	92.9	NEAR SE PROP CORNER
DP-8	1.079	8.0	16.7	26.6	53.0	74.0	95.9	BELOW SE PROP CORNER
DP-21	0.396	6.3	11.3	18.3	27.5	35.6	44.0	
DP-22	0.736	6.3	10.7	16.7	24.6	31.5	38.7	
DP-25	1.017	1.3	1.9	2.8	4.1	5.2	6.4	
DP-26	1.079	0.7	0.9	1.2	1.5	1.8	2.1	

WATER QUALITY & DETENTION POND SUMMARY

FSD1						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	16.3	23.3	33.0	45.8	57.1	68.9
ALLOWABLE RELEASE (CFS)	0.1	1.7	3.3	10.9	17.5	25.5
MODELED RELEASE (CFS)	0.1	1.6	3.2	10.9	17.4	25.4
STORED VOLUME (AC-FT)	2.4	2.6	3.0	3.6	1.9	2.2

FSD5						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	40.6	53.7	71.0	92.4	110.6	129.1
ALLOWABLE RELEASE (CFS)	0.1	1.4	2.6	11.3	19.8	30.2
MODELED RELEASE (CFS)	0.1	1.4	2.6	11.2	19.7	30.1
STORED VOLUME (AC-FT)	3.0	3.2	3.8	4.1	4.7	5.2

FSD6						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	196.5	258.5	339.1	438.7	523.3	608.6
ALLOWABLE RELEASE (CFS)	0.5	7.6	14.6	58.4	99.6	149.7
MODELED RELEASE (CFS)	0.5	7.5	14.5	58.2	99.6	149.6
STORED VOLUME (AC-FT)	15.5	16.4	18.7	20.8	23.3	26.0

FSD9						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	64.6	105.6	169.5	252.3	327.1	410.1
ALLOWABLE RELEASE (CFS)	1.7	24.9	49.8	141.1	207.2	290.0
MODELED RELEASE (CFS)	1.7	24.9	49.8	141.1	207.0	289.9
STORED VOLUME (AC-FT)	8.7	8.7	9.6	10.8	12.3	13.8

FSD11A						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	5.3	7.8	11.3	15.9	20.0	24.3
ALLOWABLE RELEASE (CFS)	0.1	1.6	3.2	7.5	9.7	12.4
MODELED RELEASE (CFS)	0.2	0.9	3.0	7.5	9.7	12.3
STORED VOLUME (AC-FT)	0.3	0.3	0.4	0.4	0.5	0.6

FSD11B						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	59.4	81.3	110.8	148.1	180.5	213.7
ALLOWABLE RELEASE (CFS)	0.3	4.5	8.7	29.6	47.7	69.6
MODELED RELEASE (CFS)	0.3	4.5	8.6	29.5	47.7	69.5
STORED VOLUME (AC-FT)	4.8	4.9	5.5	6.4	7.3	8.2

FSD12						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	77.8	105.6	142.5	189.1	229.1	270.0
ALLOWABLE RELEASE (CFS)	0.9	13.2	26.7	62.0	80.2	103.2
MODELED RELEASE (CFS)	0.9	9.0	26.7	61.9	80.1	103.1
STORED VOLUME (AC-FT)	5.2	5.5	5.8	6.7	7.8	8.9

FSD13						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	43.9	57.8	76.0	98.5	117.6	136.9
ALLOWABLE RELEASE (CFS)	0.4	6.1	12.3	28.6	37.0	47.6
MODELED RELEASE (CFS)	0.4	4.2	12.3	28.6	36.9	47.2
STORED VOLUME (AC-FT)	3.1	3.1	3.3	3.8	4.4	5.0

FSD14A						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	127.6	175.4	239.8	321.9	393.2	466.3
ALLOWABLE RELEASE (CFS)	0.5	7.5	14.4	56.2	95.2	142.4
MODELED RELEASE (CFS)	0.5	7.5	14.4	56.2	95.1	142.2
STORED VOLUME (AC-FT)	9.9	10.6	11.9	13.5	15.3	17.3

FSD14B						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	24.6	34.3	47.4	64.2	79.0	94.1
ALLOWABLE RELEASE (CFS)	0.0	0.3	0.5	5.7	11.8	19.3
MODELED RELEASE (CFS)	0.0	0.3	0.5	4.5	11.8	19.3
STORED VOLUME (AC-FT)	1.9	2.5	3.3	3.5	3.5	3.8

FSD15B						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	10.8	14.0	18.2	23.3	27.6	31.9
ALLOWABLE RELEASE (CFS)	0.1	1.6	3.2	7.3	9.5	12.0
MODELED RELEASE (CFS)	0.1	1.1	3.2	7.3	9.5	12.0
STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0

FSD16A						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	84.4	120.4	170.0	234.8	292.2	351.8
ALLOWABLE RELEASE (CFS)	0.6	8.8	17.3	56.2	88.4	128.3
MODELED RELEASE (CFS)	0.6	8.8	17.3	56.2	88.3	128.3
STORED VOLUME (AC-FT)	7.6	7.7	8.9	10.4	12.1	13.8

SAND CREEK FLOW COMPARISON CHART

DESIGN POINT	AREA (SQ MI)	Q_{100} (CFS)	DESCRIPTION
DP-77	2.343	1468	PROPOSED CONDITION
	2.91	2262	SAND CREEK DBPS
		2600	FEMA
DP-71	2.757	1612	PROPOSED CONDITION
		2260	SAND CREEK DBPS
DP-63	4.449	1385	PROPOSED CONDITION
	4.33	2630	SAND CREEK DBPS
		2600	FEMA
DP-60A	5.661	1662	PROPOSED CONDITION
	5.38	3295	SAND CREEK DBPS

EFSC DBPS DESIGN POINT SUMMARY (PEAK FLOW)

DBPS DESIGN POINT	AREA (SQ MI)	Q_{10} (CFS) (EXIST)	Q_{100} (CFS) (EXIST)	AREA (SQ MI)	Q_{10} (CFS) (PROP)	Q_{100} (CFS) (PROP)
DP-50	0.32	47.0	195.7	0.32	146.7	370.3
DP-51 (BASIN 86)	0.33	17.7	74.1	0.33	110.0	233.5
DP-52	1.67	80.5	456.5	1.67	1207.9	2123.0
DP-56	0.79	63.6	265.0	0.79	513.0	908.2

Values reported from SCDBPS, (DP 50, 51, 52 Not analyzed as a part of this study)
DBPS Reach: 85(Basin91)=Q10=28.8cfs Q100=115.2cfs / Q10=345.7cfs Q100=588.9cfs
(EXISTING) (PROPOSED)

WATER QUALITY & DETENTION POND SUMMARY

FSD16B						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	39.0	53.7	73.6	99.0	121.1	143.8
ALLOWABLE RELEASE (CFS)	0.0	0.4	0.7	8.3	17.2	28.2
MODELED RELEASE (CFS)	0.0	0.4	0.7	7.9	17.2	28.1
STORED VOLUME (AC-FT)	3.0	3.9	5.1	5.1	5.3	5.8

FSD17						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	41.8	59.6	85.2	119.0	149.1	180.6
ALLOWABLE RELEASE (CFS)	0.7	11.1	22.5	52.0	67.2	86.3
MODELED RELEASE (CFS)	0.7	8.4	22.4	52.0	67.2	86.1
STORED VOLUME (AC-FT)	2.6	2.6	2.8	3.4	4.0	4.7

FSD18						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	49.3	67.1	91.0	121.2	147.3	174.0
ALLOWABLE RELEASE (CFS)	0.6	9.2	18.4	42.2	54.6	69.9
MODELED RELEASE (CFS)	0.6	6.3	18.4	42.2	54.6	69.6
STORED VOLUME (AC-FT)	3.2	3.2	3.4	4.0	4.7	5.3

FSD20						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	9.9	15.5	23.8	35.1	45.5	56.6
ALLOWABLE RELEASE (CFS)	0.4	5.5	11.1	25.7	33.2	42.5
MODELED RELEASE (CFS)	0.4	2.8	10.9	25.7	33.0	42.4
STORED VOLUME (AC-FT)	0.7	0.8	0.8	0.9	1.0	1.2

FSD21						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	7.0	10.8	16.3	23.7	30.4	37.5
ALLOWABLE RELEASE (CFS)	0.3	4.0	8.0	18.3	23.7	30.3
MODELED RELEASE (CFS)	0.3	3.3	8.0	18.3	23.7	30.1
STORED VOLUME (AC-FT)	0.5	0.5	0.5	0.6	0.7	0.8

FSD22						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	9.4	14.8	22.5	32.9	42.5	52.6
ALLOWABLE RELEASE (CFS)	0.4	5.8	11.5	26.5	34.3	43.9
MODELED RELEASE (CFS)	0.4	5.8	11.4	26.5	34.3	43.8
STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0

FSD23						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	5.5	8.3	12.4	18.0	23.0	28.4
ALLOWABLE RELEASE (CFS)	0.2	2.4	4.9	11.2	14.5	18.6
MODELED RELEASE (CFS)	0.2	2.0	4.9	11.2	14.5	18.6
STORED VOLUME (AC-FT)	0.3	0.3	0.4	0.4	0.5	0.6

FSD27						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	38.8	57.6	84.1	119.7	159.2	206.3
ALLOWABLE RELEASE (CFS)	1.4	21.1	42.4	97.8	126.4	161.9
MODELED RELEASE (CFS)	1.4	18.4	42.3	97.7	126.2	161.9
STORED VOLUME (AC-FT)	2.7	2.8	2.9	3.2	3.7	4.2

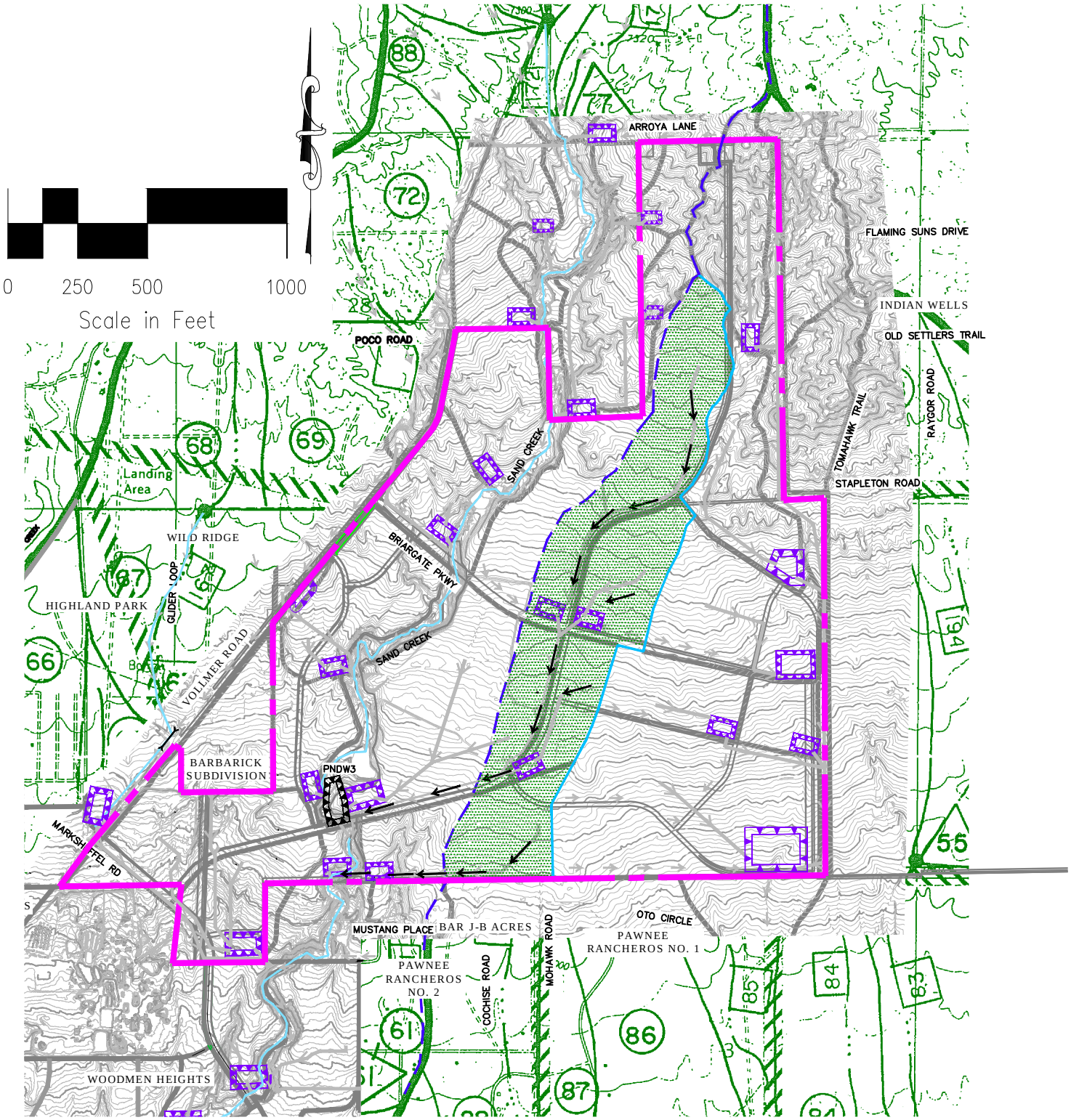
FSD72						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	12.8	20.2	31.4	46.7	60.9	76.0
ALLOWABLE RELEASE (CFS)	0.6	9.6	19.3	44.4	57.4	73.4
MODELED RELEASE (CFS)	0.6	9.3	19.2	44.4	57.4	73.4
STORED VOLUME (AC-FT)	1.0	1.0	1.1	1.1	1.2	1.3

PNDW3						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	214.6	374.5	714.9	1187.6	1674.9	2204.1
MODELED RELEASE (CFS)	154.3	200.3	366.8	799.9	1085.6	1350.6
STORED VOLUME (AC-FT)	2.8	9.5	26.3	41.2	57.2	78.2

FSD-E1						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	23.3	35.9	53.8	79.1	102.4	127.4
ALLOWABLE RELEASE (CFS)	0.7	11.0	22.1	50.9	65.7	84.1
MODELED RELEASE (CFS)	0.7	5.4	19.9	48.9	62.8	84.0
STORED VOLUME (AC-FT)	1.3	1.3	1.5	1.8	2.1	2.5

FSD-E2						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	30.6	45.2	65.9	93.3	118.0	143.9
ALLOWABLE RELEASE (CFS)	0.6	9.5	19.2	45.5	59.8	77.6
MODELED RELEASE (CFS)	0.6	3.2	18.5	41.3	58.5	74.7
STORED VOLUME (AC-FT)	2.1	2.3	2.4	2.8

STERLING RANCH DRAINAGE DIVERSION EXHIBIT



PROPERTY BNDRY

HISTORIC SC/EFSC BNDRY LINE

PROPOSED SC/EFSC BNDRY LINE

BASIN DIVERSION AREA (EAST FORK SAND CREEK TO SAND CREEK) * ~267.3 AC

PNDW3 POND W3 WILL BE UTILIZED TO AID IN REDUCING CHANNELIZED RUNOFF TO HISTORIC LEVELS.

POTENTIAL LOCATION FOR FULL SPECTRUM DETENTION POND

*ALL DIVERTED RUNOFF SHALL BE DIRECTED TO FULL SPECTRUM DETENTION PONDS PRIOR TO DISCHARGE INTO SAND CREEK CHANNEL. WHENEVER POSSIBLE ADDITIONAL LID BMP'S WILL BE UTILIZED TO REDUCE INCREASES IN RUNOFF VOLUMES.

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SHEET 1 OF 1

HYDROLOGIC CALCULATIONS

CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS

EPA- 600/R-14/413b
Revisied September 2015

Storm Water Management Model User's Manual Version 5.1

by

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September 2015

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RAIN GAGE

City of Colorado Springs DCM

2-hr Storm Cumulative Distribution

Table 6-5. 2-Hour Design Storm Distributions by Drainage Basin Area
(DARF-adjusted fraction of 1-Hour Depth)

Time Min.	Drainage Basin Area (square miles)						
	0-1	>1-5	>5-10	>10-15	>15-20	>20-40	>40-60
0	0	0	0	0	0	0	0
5	0.014	0.014	0.014	0.014	0.015	0.015	0.017
10	0.046	0.044	0.041	0.041	0.042	0.042	0.040
15	0.079	0.076	0.074	0.074	0.073	0.070	0.068
20	0.120	0.116	0.109	0.109	0.106	0.102	0.095
25	0.179	0.176	0.169	0.168	0.163	0.157	0.147
30	0.258	0.249	0.239	0.236	0.227	0.216	0.198
35	0.421	0.396	0.354	0.327	0.307	0.276	0.242
40	0.712	0.655	0.559	0.495	0.448	0.381	0.315
45	0.824	0.756	0.637	0.560	0.506	0.422	0.345
50	0.892	0.824	0.700	0.619	0.566	0.479	0.396
55	0.935	0.866	0.740	0.658	0.601	0.512	0.428
60	0.972	0.901	0.774	0.690	0.634	0.543	0.456
65	1.004	0.934	0.806	0.717	0.661	0.570	0.482
70	1.018	0.948	0.821	0.732	0.678	0.589	0.501
75	1.030	0.962	0.835	0.746	0.692	0.603	0.515
80	1.041	0.973	0.849	0.760	0.706	0.617	0.529
85	1.052	0.984	0.863	0.774	0.720	0.631	0.543
90	1.063	0.995	0.875	0.788	0.734	0.645	0.557
95	1.072	1.006	0.886	0.802	0.748	0.659	0.571
100	1.082	1.017	0.896	0.813	0.762	0.673	0.585
105	1.091	1.026	0.907	0.824	0.773	0.687	0.599
110	1.100	1.036	0.918	0.835	0.783	0.698	0.611
115	1.109	1.045	0.929	0.846	0.794	0.709	0.622
120	1.119	1.054	0.938	0.857	0.805	0.720	0.633

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City of Colorado Springs DCM

5-year, 2-hour Storm (Cumulative)

Time Min.	Drainage Basin Area (square miles)						
	0-1	>1-5	>5-10	>10-15	>15-20	>20-40	>40-60
0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.021	0.021	0.021	0.021	0.023	0.023	0.026
10	0.069	0.066	0.062	0.062	0.063	0.063	0.060
15	0.119	0.114	0.111	0.111	0.110	0.105	0.102
20	0.180	0.174	0.164	0.164	0.159	0.153	0.143
25	0.269	0.264	0.254	0.252	0.245	0.236	0.221
30	0.387	0.374	0.359	0.354	0.341	0.324	0.297
35	0.632	0.594	0.531	0.491	0.461	0.414	0.363
40	1.068	0.983	0.839	0.743	0.672	0.572	0.473
45	1.236	1.134	0.956	0.840	0.759	0.633	0.518
50	1.338	1.236	1.050	0.929	0.849	0.719	0.594
55	1.403	1.299	1.110	0.987	0.902	0.768	0.642
60	1.458	1.352	1.161	1.035	0.951	0.815	0.684
65	1.506	1.401	1.209	1.076	0.992	0.855	0.723
70	1.527	1.422	1.232	1.098	1.017	0.884	0.752
75	1.545	1.443	1.253	1.119	1.038	0.905	0.773
80	1.562	1.460	1.274	1.140	1.059	0.926	0.794
85	1.578	1.476	1.295	1.161	1.080	0.947	0.815
90	1.595	1.493	1.313	1.182	1.101	0.968	0.836
95	1.608	1.509	1.329	1.203	1.122	0.989	0.857
100	1.623	1.526	1.344	1.220	1.143	1.010	0.878
105	1.637	1.539	1.361	1.236	1.160	1.031	0.899
110	1.650	1.554	1.377	1.253	1.175	1.047	0.917
115	1.664	1.568	1.394	1.269	1.191	1.064	0.933
120	1.679	1.581	1.407	1.286	1.208	1.080	0.950

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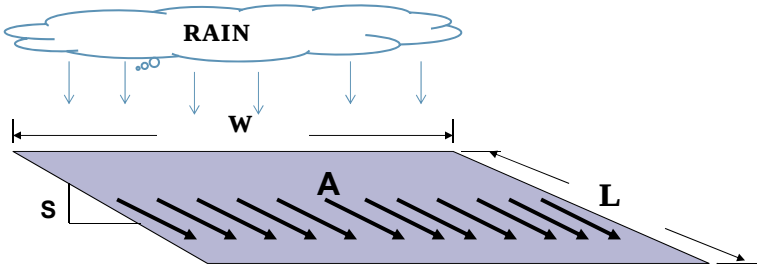
City of Colorado Springs DCM

100-year, 2-hour Storm (Cumulative)

Time Min.	Drainage Basin Area (square miles)						
	0-1	>1-5	>5-10	>10-15	>15-20	>20-40	>40-60
0	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.035	0.035	0.035	0.035	0.038	0.038	0.043
10	0.116	0.111	0.103	0.103	0.106	0.106	0.101
15	0.199	0.192	0.186	0.186	0.184	0.176	0.171
20	0.302	0.292	0.275	0.275	0.267	0.257	0.239
25	0.451	0.444	0.426	0.423	0.411	0.396	0.370
30	0.650	0.627	0.602	0.595	0.572	0.544	0.499
35	1.061	0.998	0.892	0.824	0.774	0.696	0.610
40	1.794	1.651	1.409	1.247	1.129	0.960	0.794
45	2.076	1.905	1.605	1.411	1.275	1.063	0.869
50	2.248	2.076	1.764	1.560	1.426	1.207	0.998
55	2.356	2.182	1.865	1.658	1.515	1.290	1.079
60	2.449	2.271	1.950	1.739	1.598	1.368	1.149
65	2.530	2.354	2.031	1.807	1.666	1.436	1.215
70	2.565	2.389	2.069	1.845	1.709	1.484	1.263
75	2.596	2.424	2.104	1.880	1.744	1.520	1.298
80	2.623	2.452	2.139	1.915	1.779	1.555	1.333
85	2.651	2.480	2.175	1.950	1.814	1.590	1.368
90	2.679	2.507	2.205	1.986	1.850	1.625	1.404
95	2.701	2.535	2.233	2.021	1.885	1.661	1.439
100	2.727	2.563	2.258	2.049	1.920	1.696	1.474
105	2.749	2.586	2.286	2.076	1.948	1.731	1.509
110	2.772	2.611	2.313	2.104	1.973	1.759	1.540
115	2.795	2.633	2.341	2.132	2.001	1.787	1.567
120	2.820	2.656	2.364	2.160	2.029	1.814	1.595

7

Subcatchment Conceptual Model



Subcatchment represented as a sloped, rectangular plane

W = width
L = length
S = slope
A = area

8

Percent Impervious

Estimating/Measuring Percent Impervious:

- **If site-specific information is not available, use land use classification**
- **Sometimes, site-specific impervious GIS layers are available**

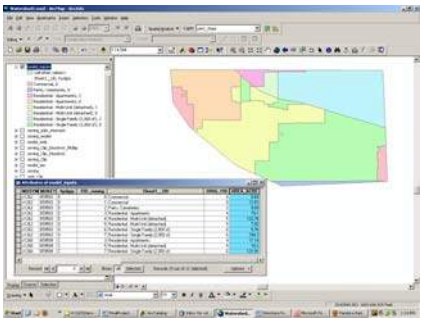


Table RO-3—Recommended Percentage Imperviousness Values

Land Use or Surface Characteristics	Percentage Imperviousness
Business:	
Commercial areas	95
Neighborhood areas	85
Residential:	
Single-family	*
Multi-unit (detached)	60
Multi-unit (attached)	75
Half-acre lot or larger	*
Apartments	80
Industrial:	
Light areas	80
Heavy areas	90
Parks, cemeteries	5
Playgrounds	10
Schools	50
Railroad yard areas	15
Undeveloped Areas:	
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
Streets:	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	0
Lawns, clayey soil	0

* See Figures RO-3 through RO-5 for percentage imperviousness.

Source: UDFCD Storm Drainage Criteria Manual

15

City of Colorado Springs DCM - Manning's n

Table 6-11. Roughness Coefficients (Manning's n) for NRCS Overland Flow

Surface description	n[1]
Smooth surfaces (concrete, asphalt, gravel, bare soil, etc.)	0.011
Fallow (no residue)	0.05
Cultivated Soils:	
Residue cover ≤20%	0.06
Residue cover >20%	0.17
Grass:	
Short grass prairie	0.15
Dense grasses[2]	0.24
Bermuda grass	0.41
Range (natural)	0.13
Woods[3]	
Light underbrush	0.40
Dense underbrush	0.80

16

Table 3-1 Impervious area as a percentage of land use.

Land Use	Percent Impervious Area
Commercial	56
Industrial	76
High density residential	51
Medium density residential	38
Low density residential	19
Institutional	34
Agricultural	2
Forest	1.9
Open Urban Land	11

As mentioned earlier, impervious areas in SWMM are hydraulically (directly) connected to the drainage system – called directly connected impervious areas (DCIA). For instance, if rooftops drain onto adjacent pervious lawn areas, they should not be treated as a hydraulically effective impervious area. Such areas are non-effective impervious areas (Doyle and Miller, 1980). On the other hand, if a driveway drains to a street and then to a stormwater inlet, the driveway would be considered hydraulically connected. Rooftops with downspouts connected directly to a sewer are clearly hydraulically connected. An example of careful measurements and statistics on imperviousness may be found in Field et al. (2000), Lee (2003), and Roy and Shuster (2007). Lee and Heaney (2003) provide detailed comparisons of imperviousness computations and their implications for modeling.

Should rooftops be treated as "pervious," the real surrounding pervious area is subject to more incoming water than rainfall alone and thus might produce runoff sooner than if rainfall alone were considered. In the possible event that this effect is important (a judgment based on infiltration parameters) it can be modeled using the overland flow re-routing option discussed earlier in Section 3.7. For example, if disconnected rooftops comprised 25 percent of the total impervious area of a subcatchment (as opposed to the total DCIA) then one could tell SWMM that this percentage of impervious area should be internally routed onto the pervious sub-area of the subcatchment.

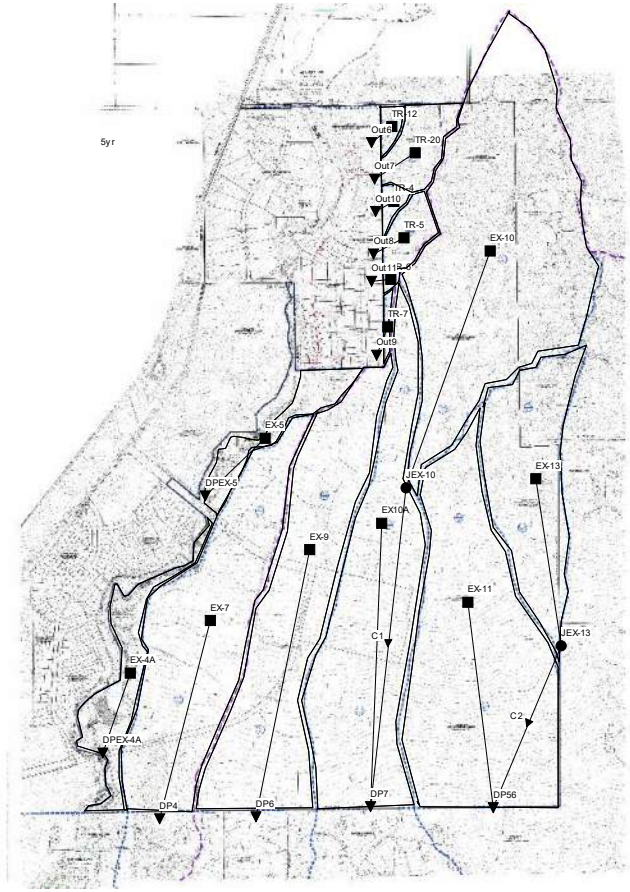
Another method of estimating the effective impervious area given measured data is to plot the runoff (in. or mm) vs. rainfall (in. or mm) for small storms. The slope of the regression line is a good estimate of the effective impervious area (Doyle and Miller, 1980).

Table 3-5 Estimates of Manning's roughness coefficient for overland flow

Source	Ground Cover	n	Range
Crawford and Linsley (1966)[a]	Smooth asphalt	0.01	
	Asphalt of concrete paving	0.014	
	Packed clay	0.03	
	Light turf	0.20	
	Dense turf	0.35	
	Dense shrubbery and forest litter	0.4	
Engman (1986)[b]	Concrete or asphalt	0.011	0.010-0.013
	Bare sand	0.010	0.01-0.016
	Graveled surface	0.02	0.012-0.03
	Bare clay-loam (eroded)	0.02	0.012-0.033
	Range (natural)	0.13	0.01-0.32
	Bluegrass sod	0.45	0.39-0.63
	Short grass prairie	0.15	0.10-0.20
	Bermuda grass	0.41	0.30-0.48
Yen (2001)[c]	Smooth asphalt pavement	0.012	0.010-0.015
	Smooth impervious surface	0.013	0.011-0.015
	Tar and sand pavement	0.014	0.012-0.016
	Concrete pavement	0.017	0.014-0.020
	Rough impervious surface	0.019	0.015-0.023
	Smooth bare packed soil	0.021	0.017-0.025
	Moderate bare packed soil	0.030	0.025-0.035
	Rough bare packed soil	0.038	0.032-0.045
	Gravel soil	0.032	0.025-0.045
	Mowed poor grass	0.038	0.030-0.045
	Average grass, closely clipped sod	0.050	0.040-0.060
	Pasture	0.055	0.040-0.070
	Timberland	0.090	0.060-0.120
	Dense grass	0.090	0.060-0.120
	Shrubs and bushes	0.120	0.080-0.180
	Business land use	0.022	0.014-0.035
	Semi-business land use	0.035	0.022-0.050
	Industrial land use	0.035	0.020-0.050
	Dense residential land use	0.040	0.025-0.060
	Suburban residential land use	0.055	0.030-0.080
	Parks and lawns	0.075	0.040-0.120

[a]Obtained by calibration of Stanford Watershed Model.
[b]Computed by Engman (1986) by kinematic wave and storage analysis of measured rainfall-runoff data.
[c]Computed on basis of kinematic wave analysis.

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS



include larger scale map

See revised larger SWMM Map

Need to provide SWMM Input information. Include calculations for % impervious, C-values & time of cocentration.

SWMM input info. now provided along with area and % imp. for each basin

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (5yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	1.68	0.00	0.00	1.50	0.18	1.28	105.15	0.106
EX10A	1.68	0.00	0.00	1.53	0.15	0.70	52.19	0.087
EX-11	1.68	0.00	0.00	1.54	0.14	0.80	53.86	0.082
EX-13	1.68	0.00	0.00	1.48	0.20	0.50	35.71	0.117
EX-4A	1.68	0.00	0.00	1.52	0.15	0.18	19.26	0.091
EX-5	1.68	0.00	0.00	1.52	0.16	0.11	11.51	0.093
EX-7	1.68	0.00	0.00	1.52	0.15	0.64	46.80	0.090
EX-9	1.68	0.00	0.00	1.52	0.15	0.73	56.96	0.090
TR-12	1.68	0.00	0.00	1.43	0.25	0.03	1.88	0.148
TR-20	1.68	0.00	0.00	1.45	0.22	0.14	10.01	0.131
TR-4	1.68	0.00	0.00	1.42	0.25	0.03	1.78	0.150
TR-5	1.68	0.00	0.00	1.48	0.20	0.07	4.56	0.116
TR-6	1.68	0.00	0.00	1.38	0.30	0.01	0.83	0.177
TR-7	1.68	0.00	0.00	1.43	0.24	0.02	1.01	0.144

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (5yr. Event)

Outfall Loading Summary

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DP4	91.92	4.30	46.80	0.639
DP56	98.59	8.23	59.57	1.311
DP6	98.59	4.60	56.96	0.733
DP7	98.59	12.48	114.01	1.989
DPEX-4A	61.64	1.84	19.26	0.183
DPEX-5	53.38	1.29	11.51	0.111
Out10	36.27	0.51	1.78	0.030
Out11	34.38	0.22	0.83	0.012
Out6	36.44	0.54	1.88	0.032
Out7	48.80	1.75	10.01	0.138
Out8	41.34	1.09	4.56	0.073
Out9	35.63	0.30	1.01	0.017

Include EX-10 & EX-13

Now included

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS
PRELIMINARY DRAINAGE REPORT
PRE-DEVELOPMENT DRAINAGE (5 yr.)

****
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
****

****
Analysis Options
****
Flow Units ..... CFS
Process Models:
  Rainfall/Runoff ..... YES
  RDII ..... NO
  Snowmelt ..... NO
  Groundwater ..... NO
  Flow Routing ..... YES
  Ponding Allowed ..... NO
  Water Quality ..... NO
Infiltration Method ..... HORTON
Flow Routing Method ..... KINWAVE
Starting Date 04/15/2022 00:00:00
Ending Date 04/15/2022 06:00:00
Antecedent Dry Days 0.0
Report Time Step 00:05:00
Wet Time Step 00:01:00
Dry Time Step 01:00:00
Routing Time Step ..... 5.00 sec

********** Volume Depth
Runoff Quantity Continuity acre-feet inches
********** --------- -------
Total Precipitation 168.488 1.679
Evaporation Loss 0.000 0.000
Infiltration Loss 151.953 1.514
Surface Runoff 16.119 0.161
Final Storage 0.426 0.004
Continuity Error (%) ..... -0.006

********** Volume Volume

Flow Routing Continuity	acre-feet	10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	16.119	5.253
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	16.166	5.268
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.005	0.002
Continuity Error (%)	-0.324	

****
Highest Flow Instability Indexes
****
All links are stable.

****
Routing Time Step Summary
****

Minimum Time Step	:	5.00 sec
Average Time Step	:	5.00 sec
Maximum Time Step	:	5.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	1.00
Percent Not Converging	:	0.00

****
Subcatchment Runoff Summary
****

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-7	1.68	0.00	0.00	1.52	0.15			

```
0.64    46.80   0.090
  EX-9                      1.68       0.00       0.00       1.52       0.15
0.73    56.96   0.090
  EX10A                     1.68       0.00       0.00       1.53       0.15
0.70    52.19   0.087
  EX-11                     1.68       0.00       0.00       1.54       0.14
0.80    53.86   0.082
  EX-13                     1.68       0.00       0.00       1.48       0.20
0.50    35.71   0.117
  EX-10                     1.68       0.00       0.00       1.50       0.18
1.28   105.15   0.106
  TR-7                      1.68       0.00       0.00       1.43       0.24
0.02     1.01   0.144
  TR-6                      1.68       0.00       0.00       1.38       0.30
0.01     0.83   0.177
  TR-5                      1.68       0.00       0.00       1.48       0.20
0.07     4.56   0.116
  TR-4                      1.68       0.00       0.00       1.42       0.25
0.03     1.78   0.150
  TR-12                     1.68       0.00       0.00       1.43       0.25
0.03     1.88   0.148
  TR-20                     1.68       0.00       0.00       1.45       0.22
0.14    10.01   0.131
  EX-4A                     1.68       0.00       0.00       1.52       0.15
0.18    19.26   0.091
  EX-5                      1.68       0.00       0.00       1.52       0.16
0.11    11.51   0.093


  ******************
  Node Depth Summary
  ******************

  --------------------------------------------------------------------------------
                                Average  Maximum  Maximum  Time of Max    Reported
                                  Depth    Depth      HGL   Occurrence   Max Depth
  Node                 Type        Feet     Feet     Feet  days hr:min        Feet
  --------------------------------------------------------------------------------
  JEX-10               JUNCTION    0.18     1.14  7149.14     0  00:45        1.14
  JEX-13               JUNCTION    0.14     0.84  7070.84     0  00:45        0.84
  DP4                  OUTFALL     0.00     0.00  6998.00     0  00:00        0.00
  DP6                  OUTFALL     0.00     0.00  7026.00     0  00:00        0.00
  DP7                  OUTFALL     0.19     1.01  7017.01     0  00:47        0.98
  DP56                 OUTFALL     0.15     0.64  7008.64     0  00:52        0.63
  Out6                 OUTFALL     0.00     0.00  7270.00     0  00:00        0.00
  Out7                 OUTFALL     0.00     0.00  7246.00     0  00:00        0.00
  Out8                 OUTFALL     0.00     0.00  7230.00     0  00:00        0.00
  Out9                 OUTFALL     0.00     0.00  7190.00     0  00:00        0.00
  Out10                OUTFALL     0.00     0.00  7250.00     0  00:00        0.00
  Out11                OUTFALL     0.00     0.00  7228.00     0  00:00        0.00
```

DPEX-4A	OUTFALL	0.00	0.00	7001.00	0	00:00	0.00
DPEX-5	OUTFALL	0.00	0.00	7144.00	0	00:00	0.00

****
Node Inflow Summary
****

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
JEX-10	JUNCTION	105.15	105.15	0 00:45	1.28	1.28	0.000
JEX-13	JUNCTION	35.71	35.71	0 00:45	0.505	0.505	0.000
DP4	OUTFALL	46.80	46.80	0 00:45	0.639	0.639	0.000
DP6	OUTFALL	56.96	56.96	0 00:45	0.733	0.733	0.000
DP7	OUTFALL	52.19	114.01	0 00:47	0.699	1.99	0.000
DP56	OUTFALL	53.86	59.57	0 00:45	0.797	1.31	0.000
Out6	OUTFALL	1.88	1.88	0 00:45	0.0317	0.0317	0.000
Out7	OUTFALL	10.01	10.01	0 00:45	0.138	0.138	0.000
Out8	OUTFALL	4.56	4.56	0 00:45	0.0727	0.0727	0.000
Out9	OUTFALL	1.01	1.01	0 00:45	0.0171	0.0171	0.000
Out10	OUTFALL	1.78	1.78	0 00:45	0.0301	0.0301	0.000
Out11	OUTFALL	0.83	0.83	0 00:50	0.0121	0.0121	0.000
DPEX-4A	OUTFALL	19.26	19.26	0 00:45	0.183	0.183	0.000
DPEX-5	OUTFALL	11.51	11.51	0 00:45	0.111	0.111	0.000

****
Node Flooding Summary
****

No nodes were flooded.

****
Outfall Loading Summary
****

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
DP4	91.92	4.30	46.80	0.639
DP6	98.59	4.60	56.96	0.733
DP7	98.59	12.48	114.01	1.989
DP56	98.59	8.23	59.57	1.311
Out6	36.44	0.54	1.88	0.032
Out7	48.80	1.75	10.01	0.138
Out8	41.34	1.09	4.56	0.073
Out9	35.63	0.30	1.01	0.017
Out10	36.27	0.51	1.78	0.030
Out11	34.38	0.22	0.83	0.012
DPEX-4A	61.64	1.84	19.26	0.183
DPEX-5	53.38	1.29	11.51	0.111
System	61.30	37.15	317.58	5.268

****
Link Flow Summary
****

Link	Type	Maximum |Flow| CFS	Time of Max Occurrence days hr:min	Maximum |Veloc| ft/sec	Max/ Full Flow	Max/ Full Depth
C2	CHANNEL	20.17	0 00:52	2.85	0.01	0.16
C1	CHANNEL	81.10	0 00:47	5.50	0.04	0.25

****
Conduit Surcharge Summary
****

No conduits were surcharged.

Analysis begun on: Wed May 25 09:45:57 2022
Analysis ended on: Wed May 25 09:45:57 2022
Total elapsed time: < 1 sec

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (100 yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	2.82	0.00	0.00	2.12	0.70	5.04	221.82	0.248
EX10A	2.82	0.00	0.00	2.16	0.65	3.10	116.83	0.231
EX-11	2.82	0.00	0.00	2.16	0.66	3.84	129.43	0.234
EX-13	2.82	0.00	0.00	1.98	0.83	2.15	85.43	0.296
EX-4A	2.82	0.00	0.00	2.01	0.80	0.96	49.54	0.285
EX-5	2.82	0.00	0.00	1.97	0.85	0.60	31.56	0.300
EX-7	2.82	0.00	0.00	2.14	0.68	2.86	106.53	0.240
EX-9	2.82	0.00	0.00	2.17	0.65	3.13	124.02	0.230
TR-12	2.82	0.00	0.00	1.66	1.16	0.15	9.32	0.411
TR-20	2.82	0.00	0.00	1.79	1.03	0.65	31.58	0.365
TR-4	2.82	0.00	0.00	1.65	1.16	0.14	8.91	0.413
TR-5	2.82	0.00	0.00	1.81	1.01	0.38	17.25	0.359
TR-6	2.82	0.00	0.00	1.57	1.25	0.05	4.42	0.443
TR-7	2.82	0.00	0.00	1.67	1.14	0.08	4.90	0.405

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (100 yr. Event)

Outfall Loading Summary

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DP4	92.55	19.10	106.53	2.856
DP56	98.59	37.64	160.10	5.996
DP6	98.59	19.66	124.02	3.131
DP7	98.59	51.21	258.75	8.157
DPEX-4A	62.08	9.61	49.54	0.964
DPEX-5	53.80	6.93	31.56	0.603
Out10	36.62	2.35	8.91	0.139
Out11	34.56	0.91	4.42	0.051
Out6	36.90	2.48	9.32	0.148
Out7	49.14	8.16	31.58	0.648
Out8	42.15	5.53	17.25	0.376
Out9	37.27	1.34	4.90	0.081

Include EX-10 & EX-13

Now included

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS
PRELIMINARY DRAINAGE REPORT
PRE-DEVELOPMENT DRAINAGE (100 yr.)

****
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
****

****
Analysis Options
****
Flow Units ..... CFS
Process Models:
  Rainfall/Runoff ..... YES
  RDII ..... NO
  Snowmelt ..... NO
  Groundwater ..... NO
  Flow Routing ..... YES
  Ponding Allowed ..... NO
  Water Quality ..... NO
Infiltration Method ..... HORTON
Flow Routing Method ..... KINWAVE
Starting Date 04/15/2022 00:00:00
Ending Date 04/15/2022 06:00:00
Antecedent Dry Days 0.0
Report Time Step 00:05:00
Wet Time Step 00:01:00
Dry Time Step 01:00:00
Routing Time Step ..... 5.00 sec

**********	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
**********	---	---
Total Precipitation	282.987	2.820
Evaporation Loss	0.000	0.000
Infiltration Loss	211.612	2.109
Surface Runoff	70.972	0.707
Final Storage	0.426	0.004
Continuity Error (%)	-0.008	

**********	Volume	Volume

Flow Routing Continuity	acre-feet	10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	70.972	23.127
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	71.044	23.151
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.006	0.002
Continuity Error (%)	-0.110	

****
Highest Flow Instability Indexes
****
All links are stable.

****
Routing Time Step Summary
****

Minimum Time Step	:	5.00 sec
Average Time Step	:	5.00 sec
Maximum Time Step	:	5.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	1.01
Percent Not Converging	:	0.00

****
Subcatchment Runoff Summary
****

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-7	2.82	0.00	0.00	2.14	0.68			

2.86 106.53 0.240
  EX-9   2.82   0.00   0.00   2.17   0.65
3.13 124.02 0.230
  EX10A   2.82   0.00   0.00   2.16   0.65
3.10 116.83 0.231
  EX-11   2.82   0.00   0.00   2.16   0.66
3.84 129.43 0.234
  EX-13   2.82   0.00   0.00   1.98   0.83
2.15   85.43 0.296
  EX-10   2.82   0.00   0.00   2.12   0.70
5.04 221.82 0.248
  TR-7   2.82   0.00   0.00   1.67   1.14
0.08   4.90 0.405
  TR-6   2.82   0.00   0.00   1.57   1.25
0.05   4.42 0.443
  TR-5   2.82   0.00   0.00   1.81   1.01
0.38   17.25 0.359
  TR-4   2.82   0.00   0.00   1.65   1.16
0.14   8.91 0.413
  TR-12   2.82   0.00   0.00   1.66   1.16
0.15   9.32 0.411
  TR-20   2.82   0.00   0.00   1.79   1.03
0.65   31.58 0.365
  EX-4A   2.82   0.00   0.00   2.01   0.80
0.96   49.54 0.285
  EX-5   2.82   0.00   0.00   1.97   0.85
0.60   31.56 0.300

  ****
  Node Depth Summary
  ****

                              Average Maximum Maximum Time of Max   Reported
                                Depth   Depth   HGL   Occurrence   Max Depth
  Node   Type   Feet   Feet   Feet days hr:min   Feet

  JEX-10   JUNCTION 0.42   1.58 7149.58   0 00:45   1.58
  JEX-13   JUNCTION 0.33   1.25 7071.25   0 00:45   1.24
  DP4   OUTFALL   0.00   0.00 6998.00   0 00:00   0.00
  DP6   OUTFALL   0.00   0.00 7026.00   0 00:00   0.00
  DP7   OUTFALL   0.43   1.42 7017.42   0 00:47   1.38
  DP56   OUTFALL   0.34   1.08 7009.08   0 01:11   1.08
  Out6   OUTFALL   0.00   0.00 7270.00   0 00:00   0.00
  Out7   OUTFALL   0.00   0.00 7246.00   0 00:00   0.00
  Out8   OUTFALL   0.00   0.00 7230.00   0 00:00   0.00
  Out9   OUTFALL   0.00   0.00 7190.00   0 00:00   0.00
  Out10   OUTFALL   0.00   0.00 7250.00   0 00:00   0.00
  Out11   OUTFALL   0.00   0.00 7228.00   0 00:00   0.00

DPEX-4A	OUTFALL	0.00	0.00	7001.00	0	00:00	0.00
DPEX-5	OUTFALL	0.00	0.00	7144.00	0	00:00	0.00

****
Node Inflow Summary
****

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
JEX-10	JUNCTION	221.82	221.82	0 00:45	5.04	5.04	0.000
JEX-13	JUNCTION	85.43	85.43	0 00:45	2.15	2.15	0.000
DP4	OUTFALL	106.53	106.53	0 00:45	2.86	2.86	0.000
DP6	OUTFALL	124.02	124.02	0 00:45	3.13	3.13	0.000
DP7	OUTFALL	116.83	258.75	0 00:47	3.1	8.16	0.000
DP56	OUTFALL	129.43	160.10	0 01:05	3.84	6	0.000
Out6	OUTFALL	9.32	9.32	0 00:50	0.148	0.148	0.000
Out7	OUTFALL	31.58	31.58	0 00:45	0.648	0.648	0.000
Out8	OUTFALL	17.25	17.25	0 00:45	0.376	0.376	0.000
Out9	OUTFALL	4.90	4.90	0 00:50	0.0807	0.0807	0.000
Out10	OUTFALL	8.91	8.91	0 00:50	0.139	0.139	0.000
Out11	OUTFALL	4.42	4.42	0 00:45	0.0509	0.0509	0.000
DPEX-4A	OUTFALL	49.54	49.54	0 00:45	0.964	0.964	0.000
DPEX-5	OUTFALL	31.56	31.56	0 00:45	0.603	0.603	0.000

****
Node Flooding Summary
****

No nodes were flooded.

****
Outfall Loading Summary
****

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
DP4	92.55	19.10	106.53	2.856
DP6	98.59	19.66	124.02	3.131
DP7	98.59	51.21	258.75	8.157
DP56	98.59	37.64	160.10	5.996
Out6	36.90	2.48	9.32	0.148
Out7	49.14	8.16	31.58	0.648
Out8	42.15	5.53	17.25	0.376
Out9	37.27	1.34	4.90	0.081
Out10	36.62	2.35	8.91	0.139
Out11	34.56	0.91	4.42	0.051
DPEX-4A	62.08	9.61	49.54	0.964
DPEX-5	53.80	6.93	31.56	0.603
System	61.74	164.92	765.76	23.149

****
Link Flow Summary
****

Link	Type	Maximum |Flow| CFS	Time of Max Occurrence days hr:min	Maximum |Veloc| ft/sec	Max/ Full Flow	Max/ Full Depth
C2	CHANNEL	61.82	0 01:11	3.58	0.04	0.27
C1	CHANNEL	173.59	0 00:47	6.32	0.08	0.35

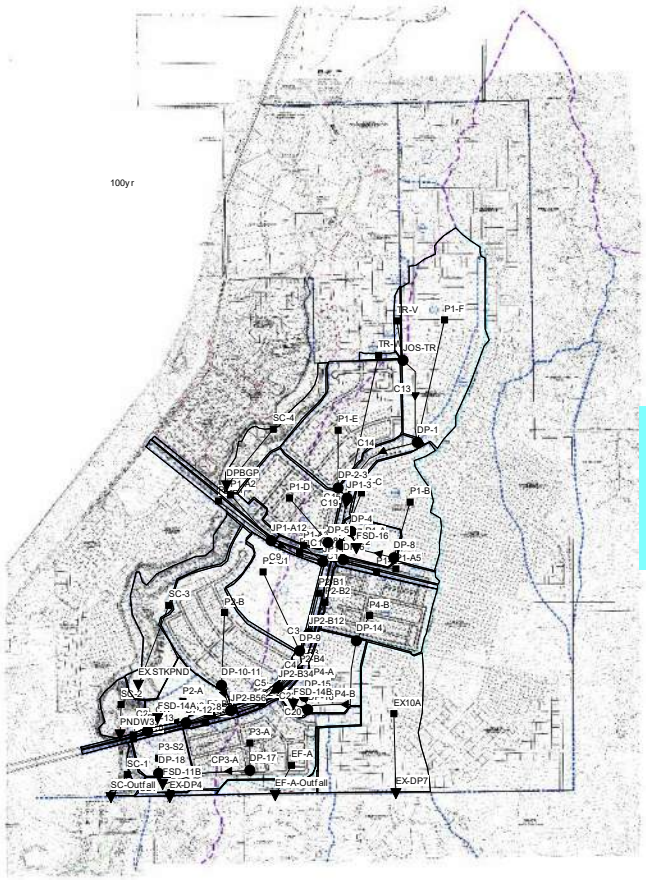
****
Conduit Surcharge Summary
****

No conduits were surcharged.

Analysis begun on: Wed May 25 09:42:25 2022
Analysis ended on: Wed May 25 09:42:25 2022
Total elapsed time: < 1 sec

STERLING RANCH EAST PRELIMINARY PLAN NO. 1

04/18/2022 00:15:00



Include map at larger scale & Clean up labels so they are all readable on map

See revised larger SWMM Map

Need to provide SWMM Input information. Include calculations for % impervious, C-values & time of cocentration.

SWMM input info. now provided along with area and % imp. for each basin

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Can Ac-ft be used?

Unfortunately not as this is the std. format for SWMM.

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EF-A	1.68	0.00	0.00	1.30	0.38	0.08	7.24	0.224
EX10A	1.68	0.00	0.00	1.53	0.15	0.24	17.80	0.088
P1-A	1.68	0.00	0.00	1.43	0.24	0.08	6.19	0.144
P1-A1	1.68	0.00	0.00	0.86	0.79	0.11	10.79	0.473
P1-A2	1.68	0.00	0.00	0.88	0.77	0.13	11.96	0.457
P1-A3	1.68	0.00	0.00	0.75	0.90	0.04	4.61	0.534
P1-A4	1.68	0.00	0.00	0.76	0.89	0.05	5.08	0.532
P1-A5	1.68	0.00	0.00	0.85	0.80	0.09	9.64	0.479
P1-A6	1.68	0.00	0.00	0.76	0.89	0.07	7.00	0.529
P1-B	1.68	0.00	0.00	1.00	0.65	0.63	55.37	0.387
P1-C	1.68	0.00	0.00	0.95	0.71	0.21	21.19	0.420
P1-D	1.68	0.00	0.00	1.00	0.66	0.56	52.52	0.392
P1-E	1.68	0.00	0.00	1.04	0.61	0.87	83.14	0.365
P1-F	1.68	0.00	0.00	1.12	0.54	1.12	110.51	0.321
P2-A	1.68	0.00	0.00	1.38	0.30	0.13	10.28	0.178
P2-B	1.68	0.00	0.00	1.01	0.65	1.04	90.08	0.385

Include all basins in summary table, as shown on drainage map

SEE REVISED

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
P2-B1	1.68	0.00	0.00	0.74	0.91	0.06	6.56	0.540
P2-B10	1.68	0.00	0.00	0.73	0.92	0.04	4.59	0.549
P2-B2	1.68	0.00	0.00	0.74	0.91	0.05	4.98	0.540
P2-B3	1.68	0.00	0.00	0.83	0.82	0.06	6.59	0.491
P2-B4	1.68	0.00	0.00	0.75	0.90	0.04	4.16	0.538
P2-B5	1.68	0.00	0.00	0.82	0.84	0.04	4.58	0.498
P2-B6	1.68	0.00	0.00	0.73	0.92	0.03	2.96	0.547
P2-B7	1.68	0.00	0.00	0.82	0.83	0.06	5.96	0.494
P2-B8	1.68	0.00	0.00	0.74	0.92	0.03	3.21	0.545
P2-B9	1.68	0.00	0.00	0.73	0.92	0.05	5.40	0.549
P2-S1	1.68	0.00	0.00	0.95	0.71	0.69	68.31	0.423
P3-A	1.68	0.00	0.00	1.00	0.65	0.93	82.07	0.387
P3-C	1.68	0.00	0.00	1.31	0.36	0.02	1.27	0.216
P3-S2	1.68	0.00	0.00	0.92	0.74	0.24	24.68	0.439
P4-A	1.68	0.00	0.00	1.04	0.61	0.43	41.04	0.365
P4-B	1.68	0.00	0.00	1.03	0.63	0.64	63.26	0.373
SC-1	1.68	0.00	0.00	1.43	0.25	0.02	1.78	0.148

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
SC-2	1.68	0.00	0.00	1.40	0.27	0.08	5.63	0.163
SC-3	1.68	0.00	0.00	1.49	0.19	0.16	13.85	0.112
SC-4	1.68	0.00	0.00	1.42	0.26	0.11	8.25	0.153
TR-V	1.68	0.00	0.00	1.23	0.44	0.02	2.29	0.259
TR-W	1.68	0.00	0.00	0.97	0.69	0.03	2.66	0.410

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Outfall Loading Summary

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DPBGP	46.25	1.54	8.25	0.115
EF-A-Outfall	50.14	1.03	7.24	0.084
EX.STKPND	66.53	1.48	13.85	0.159
EX-DP4	37.22	0.28	1.27	0.017
EX-DP7	58.33	2.57	17.80	0.242
FSD-11B	98.19	7.33	102.33	1.163
FSD-14A	98.47	14.51	200.17	2.309
FSD-14B	97.64	6.72	96.95	1.060
FSD-16	98.47	25.12	362.95	3.997
PNDW3	42.78	1.16	5.63	0.080
SC-Outfall	40.00	0.38	1.78	0.024

All DP's/Outfalls need to be shown and labeled on drainage map

SEE REVISED

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DP-1	JUNCTION	110.51	111.99	0	00:45	1.12	1.15	0.000
DP-10-11	JUNCTION	90.08	90.08	0	00:45	1.04	1.04	0.000
DP-12	JUNCTION	9.16	185.88	0	00:47	0.0862	2.09	0.000
DP-13	JUNCTION	9.99	9.99	0	00:45	0.0926	0.0926	0.000
DP-14	JUNCTION	63.26	63.26	0	00:45	0.635	0.635	0.000
DP-15	JUNCTION	41.04	41.04	0	00:45	0.429	0.429	0.000
DP-16	JUNCTION	0.00	96.75	0	00:46	0	1.06	0.000
DP-17	JUNCTION	82.07	82.07	0	00:45	0.927	0.927	0.000
DP-18	JUNCTION	24.68	24.68	0	00:45	0.238	0.238	0.000
DP-2-3	JUNCTION	83.14	83.14	0	00:45	0.869	0.869	0.000
DP-4	JUNCTION	0.00	187.03	0	00:47	0	2.03	0.000
DP-5	JUNCTION	52.52	52.52	0	00:45	0.561	0.561	0.000
DP-6	JUNCTION	16.64	16.64	0	00:45	0.161	0.161	0.000
DP-7	JUNCTION	21.19	117.48	0	00:46	0.205	1.26	0.000
DP-8	JUNCTION	55.37	55.37	0	00:45	0.626	0.626	0.000
DP-9	JUNCTION	68.31	79.41	0	00:45	0.686	0.794	-0.000

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SEE REVISED

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DPBGP	OUTFALL	8.25	8.25	0	00:45	0.115	0.115	0.000
EF-A-Outfall	OUTFALL	7.24	7.24	0	00:45	0.0838	0.0838	0.000
EX.STKPND	OUTFALL	13.85	13.85	0	00:45	0.159	0.159	0.000
EX-DP4	OUTFALL	1.27	1.27	0	00:45	0.0168	0.0168	0.000
EX-DP7	OUTFALL	17.80	17.80	0	00:45	0.242	0.242	0.000
FSD-11B	OUTFALL	0.00	102.33	0	00:46	0	1.16	0.000
FSD-14A	OUTFALL	10.28	200.17	0	00:48	0.135	2.31	0.000
FSD-14B	OUTFALL	0.00	96.95	0	00:46	0	1.06	0.000
FSD-16	OUTFALL	6.19	362.95	0	00:46	0.0832	4	0.000
JOS-TR	JUNCTION	2.29	2.29	0	00:45	0.0248	0.0248	0.000
JP1-3	JUNCTION	2.66	190.10	0	00:46	0.0261	2.04	0.000
JP1-A12	JUNCTION	22.75	22.75	0	00:45	0.241	0.241	0.000
JP1-A34	JUNCTION	9.69	30.20	0	00:46	0.0924	0.333	0.000
JP2-B12	JUNCTION	11.54	11.54	0	00:45	0.108	0.108	0.000
JP2-B34	JUNCTION	10.76	87.69	0	00:46	0.102	0.894	0.000
JP2-B56	JUNCTION	7.54	179.56	0	00:46	0.0706	2	0.000
PNDW3	OUTFALL	5.63	5.63	0	00:45	0.0804	0.0804	0.000

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (5yr. Event)

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
SC-Outfall	OUTFALL	1.78	1.78	0	00:45	0.0243	0.0243	0.000

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

STERLING RANCH EAST PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
DEVELOPED DRAINAGE (5 yr.)

****
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
****

****
Analysis Options
****
Flow Units ..... CFS
Process Models:
  Rainfall/Runoff ..... YES
  RDII ..... NO
  Snowmelt ..... NO
  Groundwater ..... NO
  Flow Routing ..... YES
  Ponding Allowed ..... NO
  Water Quality ..... NO
Infiltration Method ..... HORTON
Flow Routing Method ..... KINWAVE
Starting Date 04/18/2022 00:00:00
Ending Date 04/18/2022 06:00:00
Antecedent Dry Days 0.0
Report Time Step 00:15:00
Wet Time Step 00:05:00
Dry Time Step 01:00:00
Routing Time Step ..... 30.00 sec

**********	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
**********	---	---
Total Precipitation	88.931	1.679
Evaporation Loss	0.000	0.000
Infiltration Loss	59.490	1.123
Surface Runoff	28.497	0.538
Final Storage	1.207	0.023
Continuity Error (%)	-0.296	

**********	Volume	Volume

Flow Routing Continuity	acre-feet	10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	28.496	9.286
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	28.384	9.249
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.005	0.002
Continuity Error (%)	0.376	

****
Highest Flow Instability Indexes
****
Link C4 (1)
Link C7 (1)
Link C13 (1)
Link C16 (1)

****
Routing Time Step Summary
****
Minimum Time Step : 30.00 sec
Average Time Step : 30.00 sec
Maximum Time Step : 30.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.71
Percent Not Converging : 0.00

****
Subcatchment Runoff Summary
****

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff

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--------------------------------------------------------------------------------
--------------------
  P2-B10                    1.68       0.00       0.00       0.73       0.92
0.04     4.59   0.549
  P2-B9                     1.68       0.00       0.00       0.73       0.92
0.05     5.40   0.549
  P3-S2                     1.68       0.00       0.00       0.92       0.74
0.24    24.68   0.439
  P3-A                      1.68       0.00       0.00       1.00       0.65
0.93    82.07   0.387
  P3-C                      1.68       0.00       0.00       1.31       0.36
0.02     1.27   0.216
  EF-A                      1.68       0.00       0.00       1.30       0.38
0.08     7.24   0.224
  P2-B8                     1.68       0.00       0.00       0.74       0.92
0.03     3.21   0.545
  P2-B7                     1.68       0.00       0.00       0.82       0.83
0.06     5.96   0.494
  P2-B5                     1.68       0.00       0.00       0.82       0.84
0.04     4.58   0.498
  P2-B6                     1.68       0.00       0.00       0.73       0.92
0.03     2.96   0.547
  P2-A                      1.68       0.00       0.00       1.38       0.30
0.13    10.28   0.178
  P2-B3                     1.68       0.00       0.00       0.83       0.82
0.06     6.59   0.491
  P2-B4                     1.68       0.00       0.00       0.75       0.90
0.04     4.16   0.538
  P4-A                      1.68       0.00       0.00       1.04       0.61
0.43    41.04   0.365
  P2-B                      1.68       0.00       0.00       1.01       0.65
1.04    90.08   0.385
  P2-S1                     1.68       0.00       0.00       0.95       0.71
0.69    68.31   0.423
  P2-B1                     1.68       0.00       0.00       0.74       0.91
0.06     6.56   0.540
  P2-B2                     1.68       0.00       0.00       0.74       0.91
0.05     4.98   0.540
  P4-B                      1.68       0.00       0.00       1.03       0.63
0.64    63.26   0.373
  P1-A6                     1.68       0.00       0.00       0.76       0.89
0.07     7.00   0.529
  P1-A5                     1.68       0.00       0.00       0.85       0.80
0.09     9.64   0.479
  P1-A4                     1.68       0.00       0.00       0.76       0.89
0.05     5.08   0.532
  P1-A                      1.68       0.00       0.00       1.43       0.24
0.08     6.19   0.144
  P1-A1                     1.68       0.00       0.00       0.86       0.79
0.11    10.79   0.473
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  P1-A2                    1.68       0.00       0.00       0.88       0.77
0.13    11.96   0.457
  P1-A3                    1.68       0.00       0.00       0.75       0.90
0.04     4.61   0.534
  P1-C                     1.68       0.00       0.00       0.95       0.71
0.21    21.19   0.420
  P1-B                     1.68       0.00       0.00       1.00       0.65
0.63    55.37   0.387
  P1-D                     1.68       0.00       0.00       1.00       0.66
0.56    52.52   0.392
  P1-E                     1.68       0.00       0.00       1.04       0.61
0.87    83.14   0.365
  TR-W                     1.68       0.00       0.00       0.97       0.69
0.03     2.66   0.410
  TR-V                     1.68       0.00       0.00       1.23       0.44
0.02     2.29   0.259
  P1-F                     1.68       0.00       0.00       1.12       0.54
1.12   110.51   0.321
  SC-2                     1.68       0.00       0.00       1.40       0.27
0.08     5.63   0.163
  SC-3                     1.68       0.00       0.00       1.49       0.19
0.16    13.85   0.112
  SC-4                     1.68       0.00       0.00       1.42       0.26
0.11     8.25   0.153
  SC-1                     1.68       0.00       0.00       1.43       0.25
0.02     1.78   0.148
  EX10A                    1.68       0.00       0.00       1.53       0.15
0.24    17.80   0.088


  ******************
  Node Depth Summary
  ******************

  ------------------------------------------------------------------------------
                                Average  Maximum  Maximum  Time of Max    Reported
                                  Depth    Depth      HGL   Occurrence   Max Depth
  Node                 Type        Feet     Feet     Feet  days hr:min        Feet
  ------------------------------------------------------------------------------
  DP-14                JUNCTION    0.26     1.80  7081.80     0  00:45        1.75
  DP-10-11             JUNCTION    0.39     2.59  7048.59     0  00:45        2.48
  DP-12                JUNCTION    1.93     4.28  7036.28     0  00:47        4.04
  DP-13                JUNCTION    0.11     0.81  7011.81     0  00:45        0.79
  JP2-B12              JUNCTION    0.12     0.88  7072.88     0  00:45        0.86
  DP-9                 JUNCTION    0.63     1.90  7068.90     0  00:45        1.84
  JP2-B34              JUNCTION    1.27     2.87  7057.87     0  00:46        2.76
  JP2-B56              JUNCTION    1.79     3.56  7047.56     0  00:45        3.45
  JP1-A12              JUNCTION    0.21     1.35  7105.35     0  00:45        1.31
  JP1-A34              JUNCTION    0.22     1.42  7099.42     0  00:46        1.34
  DP-7                 JUNCTION   10.24    14.00  7110.00     0  00:46       11.41
```

DP-8	JUNCTION	0.31	1.93	7097.93	0	00:45	1.88
DP-4	JUNCTION	22.42	24.84	7120.84	0	00:47	24.56
JP1-3	JUNCTION	10.32	12.10	7140.10	0	00:46	11.93
DP-1	JUNCTION	10.06	10.35	7165.35	0	00:48	10.29
JOS-TR	JUNCTION	0.05	0.38	7190.38	0	00:45	0.37
DP-17	JUNCTION	0.32	1.98	7031.98	0	00:45	1.91
DP-6	JUNCTION	0.18	1.36	7099.36	0	00:45	1.32
DP-5	JUNCTION	0.23	1.47	7111.47	0	00:45	1.43
DP-2-3	JUNCTION	0.32	2.18	7134.18	0	00:45	2.12
DP-15	JUNCTION	0.22	1.44	7061.44	0	00:45	1.40
DP-18	JUNCTION	0.16	1.17	7013.17	0	00:45	1.14
DP-16	JUNCTION	2.26	3.73	7061.73	0	00:47	3.53
EF-A-Outfall	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
EX-DP4	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
FSD-11B	OUTFALL	5.32	6.94	7016.94	0	00:46	6.78
FSD-14A	OUTFALL	10.44	12.90	7018.90	0	00:48	12.45
FSD-14B	OUTFALL	0.31	2.05	7058.05	0	00:46	1.90
FSD-16	OUTFALL	0.44	3.38	7098.38	0	00:46	3.00
PNDW3	OUTFALL	0.00	0.00	7001.00	0	00:00	0.00
EX.STKPND	OUTFALL	0.00	0.00	7030.00	0	00:00	0.00
DPBGP	OUTFALL	0.00	0.00	7100.00	0	00:00	0.00
EX-DP7	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
SC-Outfall	OUTFALL	0.00	0.00	0.00	0	00:00	0.00

****
Node Inflow Summary
****

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DP-14	JUNCTION	63.26	63.26	0 00:45	0.635	0.635	0.000
DP-10-11	JUNCTION	90.08	90.08	0 00:45	1.04	1.04	0.000
DP-12	JUNCTION	9.16	185.88	0 00:47	0.0862	2.09	0.000
DP-13	JUNCTION	9.99	9.99	0 00:45	0.0926		

0.0926	0.000							
JP2-B12		JUNCTION	11.54	11.54	0	00:45	0.108	
0.108	0.000							
DP-9		JUNCTION	68.31	79.41	0	00:45	0.686	
0.794	-0.000							
JP2-B34		JUNCTION	10.76	87.69	0	00:46	0.102	
0.894	0.000							
JP2-B56		JUNCTION	7.54	179.56	0	00:46	0.0706	
2	0.000							
JP1-A12		JUNCTION	22.75	22.75	0	00:45	0.241	
0.241	0.000							
JP1-A34		JUNCTION	9.69	30.20	0	00:46	0.0924	
0.333	0.000							
DP-7		JUNCTION	21.19	117.48	0	00:46	0.205	
1.26	0.000							
DP-8		JUNCTION	55.37	55.37	0	00:45	0.626	
0.626	0.000							
DP-4		JUNCTION	0.00	187.03	0	00:47	0	
2.03	0.000							
JP1-3		JUNCTION	2.66	190.10	0	00:46	0.0261	
2.04	0.000							
DP-1		JUNCTION	110.51	111.99	0	00:45	1.12	
1.15	0.000							
JOS-TR		JUNCTION	2.29	2.29	0	00:45	0.0248	
0.0248	0.000							
DP-17		JUNCTION	82.07	82.07	0	00:45	0.927	
0.927	0.000							
DP-6		JUNCTION	16.64	16.64	0	00:45	0.161	
0.161	0.000							
DP-5		JUNCTION	52.52	52.52	0	00:45	0.561	
0.561	0.000							
DP-2-3		JUNCTION	83.14	83.14	0	00:45	0.869	
0.869	0.000							
DP-15		JUNCTION	41.04	41.04	0	00:45	0.429	
0.429	0.000							
DP-18		JUNCTION	24.68	24.68	0	00:45	0.238	
0.238	0.000							
DP-16		JUNCTION	0.00	96.75	0	00:46	0	
1.06	0.000							
EF-A-Outfall		OUTFALL	7.24	7.24	0	00:45	0.0838	
0.0838	0.000							
EX-DP4		OUTFALL	1.27	1.27	0	00:45	0.0168	
0.0168	0.000							
FSD-11B		OUTFALL	0.00	102.33	0	00:46	0	
1.16	0.000							
FSD-14A		OUTFALL	10.28	200.17	0	00:48	0.135	
2.31	0.000							
FSD-14B		OUTFALL	0.00	96.95	0	00:46	0	
1.06	0.000							
FSD-16		OUTFALL	6.19	362.95	0	00:46	0.0832	

```
 4       0.000
  PNDW3                OUTFALL       5.63     5.63     0  00:45      0.0804
0.0804       0.000
  EX.STKPND            OUTFALL      13.85    13.85     0  00:45       0.159
0.159       0.000
  DPBGP                OUTFALL       8.25     8.25     0  00:45       0.115
0.115       0.000
  EX-DP7               OUTFALL      17.80    17.80     0  00:45       0.242
0.242       0.000
  SC-Outfall           OUTFALL       1.78     1.78     0  00:45      0.0243
0.0243       0.000


  *********************
  Node Flooding Summary
  *********************

  Flooding refers to all water that overflows a node, whether it ponds or not.
  ------------------------------------------------------------------------
                                                              Total   Maximum
                                  Maximum   Time of Max       Flood    Ponded
                    Hours         Rate    Occurrence      Volume    Volume
  Node              Flooded        CFS   days hr:min    10^6 gal  1000 ft3
  ------------------------------------------------------------------------
  DP-7                 0.02      0.10      0  00:46       0.000     0.000


  ***********************
  Outfall Loading Summary
  ***********************

  ---------------------------------------------------------
                      Flow       Avg       Max       Total
                      Freq      Flow      Flow      Volume
  Outfall Node         Pcnt       CFS       CFS    10^6 gal
  ---------------------------------------------------------
  EF-A-Outfall        50.14      1.03      7.24       0.084
  EX-DP4              37.22      0.28      1.27       0.017
  FSD-11B             98.19      7.33    102.33       1.163
  FSD-14A             98.47     14.51    200.17       2.309
  FSD-14B             97.64      6.72     96.95       1.060
  FSD-16              98.47     25.12    362.95       3.997
  PNDW3               42.78      1.16      5.63       0.080
  EX.STKPND           66.53      1.48     13.85       0.159
  DPBGP               46.25      1.54      8.25       0.115
  EX-DP7              58.33      2.57     17.80       0.242
  SC-Outfall          40.00      0.38      1.78       0.024
  ---------------------------------------------------------
  System              66.73     62.11    802.87       9.249
```

****
Link Flow Summary
****

Link	Type	Maximum |Flow| CFS	Time of Max Occurrence days	hr:min	Maximum |Veloc| ft/sec	Max/ Full Flow	Max/ Full Depth
CP4-B	CONDUIT	59.07	0	00:47	11.86	0.39	0.43
C2	CONDUIT	9.81	0	00:46	7.28	0.22	0.32
C3	CONDUIT	11.36	0	00:46	8.71	0.40	0.44
C4	CONDUIT	77.45	0	00:46	13.62	0.45	0.47
C5	CONDUIT	86.38	0	00:46	13.95	0.50	0.50
C6	CONDUIT	178.08	0	00:47	16.02	0.60	0.56
C7	CONDUIT	183.66	0	00:48	15.88	0.64	0.58
C8	CONDUIT	88.93	0	00:45	11.87	0.88	0.74
C9	CONDUIT	21.50	0	00:47	7.45	0.39	0.44
C10	CONDUIT	30.13	0	00:46	8.24	0.35	0.41
C11	CONDUIT	120.22	0	00:46	10.86	1.03	0.90
C12	CONDUIT	54.72	0	00:46	9.24	0.47	0.48
C13	CONDUIT	1.96	0	00:48	5.85	0.07	0.17
C14	CONDUIT	107.12	0	00:46	14.03	0.37	0.42
C15	CONDUIT	187.03	0	00:47	15.28	0.53	0.52
C16	CONDUIT	187.29	0	00:47	15.11	0.53	0.52
CP3-A	CONDUIT	79.26	0	00:46	13.37	0.47	0.48
C17	CONDUIT	51.83	0	00:46	12.57	0.29	0.37
C18	CONDUIT	16.16	0	00:46	6.18	0.56	0.53
C19	CONDUIT	81.88	0	00:46	11.90	0.57	0.54
C20	CONDUIT	40.35	0	00:45	11.06	0.35	0.41
C21	CONDUIT	24.23	0	00:45	9.73	0.31	0.39
C22	CONDUIT	96.95	0	00:46	13.72	0.43	0.46

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EF-A	2.82	0.00	0.00	1.53	1.29	0.29	19.75	0.458
EX10A	2.82	0.00	0.00	2.02	0.80	1.32	50.17	0.285
P1-A	2.82	0.00	0.00	1.75	1.07	0.37	18.97	0.380
P1-A1	2.82	0.00	0.00	1.05	1.75	0.24	20.94	0.621
P1-A2	2.82	0.00	0.00	1.15	1.65	0.29	23.30	0.584
P1-A3	2.82	0.00	0.00	0.88	1.92	0.09	9.12	0.682
P1-A4	2.82	0.00	0.00	0.88	1.91	0.10	10.01	0.679
P1-A5	2.82	0.00	0.00	1.02	1.79	0.21	18.89	0.633
P1-A6	2.82	0.00	0.00	0.90	1.90	0.14	13.69	0.674
P1-B	2.82	0.00	0.00	1.36	1.44	1.39	108.03	0.512
P1-C	2.82	0.00	0.00	1.13	1.67	0.49	42.78	0.593
P1-D	2.82	0.00	0.00	1.31	1.49	1.27	101.80	0.529
P1-E	2.82	0.00	0.00	1.37	1.43	2.03	161.09	0.509
P1-F	2.82	0.00	0.00	1.46	1.34	2.80	215.28	0.476
P2-A	2.82	0.00	0.00	1.63	1.19	0.54	32.61	0.423
P2-B	2.82	0.00	0.00	1.37	1.43	2.30	176.39	0.505

Include all basins in summary table, as shown on drainage map

SEE REVISED

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
P2-B1	2.82	0.00	0.00	0.86	1.94	0.13	13.20	0.689
P2-B10	2.82	0.00	0.00	0.83	1.97	0.09	9.53	0.698
P2-B2	2.82	0.00	0.00	0.86	1.94	0.10	10.02	0.689
P2-B3	2.82	0.00	0.00	0.97	1.84	0.14	13.28	0.651
P2-B4	2.82	0.00	0.00	0.86	1.94	0.08	8.32	0.687
P2-B5	2.82	0.00	0.00	0.94	1.86	0.10	9.46	0.660
P2-B6	2.82	0.00	0.00	0.84	1.97	0.06	6.11	0.697
P2-B7	2.82	0.00	0.00	0.95	1.85	0.13	12.14	0.656
P2-B8	2.82	0.00	0.00	0.84	1.96	0.06	6.57	0.695
P2-B9	2.82	0.00	0.00	0.83	1.97	0.11	11.22	0.698
P2-S1	2.82	0.00	0.00	1.18	1.62	1.57	132.76	0.576
P3-A	2.82	0.00	0.00	1.36	1.44	2.06	160.11	0.512
P3-C	2.82	0.00	0.00	1.51	1.32	0.06	4.80	0.469
P3-S2	2.82	0.00	0.00	1.09	1.71	0.55	49.53	0.607
P4-A	2.82	0.00	0.00	1.37	1.43	1.00	79.51	0.508
P4-B	2.82	0.00	0.00	1.30	1.50	1.52	123.34	0.532
SC-1	2.82	0.00	0.00	1.73	1.10	0.11	5.65	0.389

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
SC-2	2.82	0.00	0.00	1.66	1.17	0.34	20.21	0.415
SC-3	2.82	0.00	0.00	1.99	0.83	0.70	32.41	0.295
SC-4	2.82	0.00	0.00	1.70	1.12	0.50	27.41	0.399
TR-V	2.82	0.00	0.00	1.45	1.36	0.08	5.72	0.483
TR-W	2.82	0.00	0.00	1.19	1.62	0.06	5.23	0.573

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Outfall Loading Summary

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DPBGP	46.53	6.66	27.41	0.501
EF-A-Outfall	50.56	3.52	19.75	0.288
EX.STKPND	67.22	6.46	32.41	0.702
EX-DP4	37.36	1.01	4.80	0.061
EX-DP7	58.75	13.86	50.17	1.316
FSD-11B	98.33	16.43	201.40	2.611
FSD-14A	98.47	32.64	352.16	5.193
FSD-14B	97.92	15.90	189.49	2.516
FSD-16	98.47	57.84	587.24	9.202
PNDW3	42.92	4.95	20.21	0.343
SC-Outfall	41.53	1.60	5.65	0.107

All DP's/Outfalls need to be shown and labeled on drainage map

SEE REVISED

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DP-1	JUNCTION	215.28	219.02	0	00:45	2.8	2.87	0.000
DP-10-11	JUNCTION	176.39	176.39	0	00:45	2.3	2.3	-0.000
DP-12	JUNCTION	18.71	298.18	0	00:47	0.189	4.47	0.000
DP-13	JUNCTION	20.75	20.75	0	00:45	0.198	0.198	0.000
DP-14	JUNCTION	123.34	123.34	0	00:45	1.52	1.52	0.000
DP-15	JUNCTION	79.51	79.51	0	00:45	1	1	0.000
DP-16	JUNCTION	0.00	188.99	0	00:46	0	2.52	0.000
DP-17	JUNCTION	160.11	160.11	0	00:45	2.06	2.06	0.000
DP-18	JUNCTION	49.53	49.53	0	00:45	0.553	0.553	0.000
DP-2-3	JUNCTION	161.09	161.09	0	00:45	2.03	2.03	0.000
DP-4	JUNCTION	0.00	372.38	0	00:47	0	4.94	0.000
DP-5	JUNCTION	101.80	101.80	0	00:45	1.27	1.27	0.000
DP-6	JUNCTION	32.58	32.58	0	00:45	0.353	0.353	-0.000
DP-7	JUNCTION	42.78	229.27	0	00:46	0.486	2.83	0.000
DP-8	JUNCTION	108.03	108.03	0	00:45	1.39	1.39	0.000
DP-9	JUNCTION	132.76	155.04	0	00:45	1.57	1.8	0.000

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DPBGP	OUTFALL	27.41	27.41	0	00:45	0.501	0.501	0.000
EF-A-Outfall	OUTFALL	19.75	19.75	0	00:45	0.288	0.288	0.000
EX.STKPND	OUTFALL	32.41	32.41	0	00:45	0.702	0.702	0.000
EX-DP4	OUTFALL	4.80	4.80	0	00:45	0.0611	0.0611	0.000
EX-DP7	OUTFALL	50.17	50.17	0	00:45	1.32	1.32	0.000
FSD-11B	OUTFALL	0.00	201.40	0	00:46	0	2.61	0.000
FSD-14A	OUTFALL	32.61	352.16	0	00:48	0.537	5.19	0.000
FSD-14B	OUTFALL	0.00	189.49	0	00:46	0	2.52	0.000
FSD-16	OUTFALL	18.97	587.24	0	00:48	0.37	9.2	0.000
JOS-TR	JUNCTION	5.72	5.72	0	00:45	0.0777	0.0777	0.000
JP1-3	JUNCTION	5.23	364.91	0	00:46	0.0615	4.95	0.000
JP1-A12	JUNCTION	44.24	44.24	0	00:45	0.524	0.524	0.000
JP1-A34	JUNCTION	19.13	59.50	0	00:46	0.198	0.72	0.000
JP2-B12	JUNCTION	23.22	23.22	0	00:45	0.232	0.232	0.000
JP2-B34	JUNCTION	21.61	172.30	0	00:46	0.224	2.02	0.000
JP2-B56	JUNCTION	15.57	284.55	0	00:46	0.155	4.28	-0.000
PNDW3	OUTFALL	20.21	20.21	0	00:45	0.343	0.343	0.000

STERLING RANCH EAST PRELIMINARY PLAN NO. 1 (100yr. Event)

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
SC-Outfall	OUTFALL	5.65	5.65	0	00:45	0.107	0.107	0.000

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

STERLING RANCH EAST PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
DEVELOPED DRAINAGE (100 yr.)

****
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
****

****
Analysis Options
****
Flow Units ..... CFS
Process Models:
  Rainfall/Runoff ..... YES
  RDII ..... NO
  Snowmelt ..... NO
  Groundwater ..... NO
  Flow Routing ..... YES
  Ponding Allowed ..... NO
  Water Quality ..... NO
Infiltration Method ..... HORTON
Flow Routing Method ..... KINWAVE
Starting Date 04/18/2022 00:00:00
Ending Date 04/18/2022 06:00:00
Antecedent Dry Days 0.0
Report Time Step 00:15:00
Wet Time Step 00:05:00
Dry Time Step 01:00:00
Routing Time Step ..... 30.00 sec

**********	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
**********	---	---
Total Precipitation	149.366	2.820
Evaporation Loss	0.000	0.000
Infiltration Loss	76.803	1.450
Surface Runoff	71.885	1.357
Final Storage	1.209	0.023
Continuity Error (%)	-0.355	

**********	Volume	Volume

Flow Routing Continuity	acre-feet	10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	71.884	23.425
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	70.091	22.840
Flooding Loss	1.666	0.543
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.005	0.002
Continuity Error (%)	0.170	

****
Highest Flow Instability Indexes
****
Link C8 (3)
Link C16 (3)
Link C18 (2)
Link C13 (1)
Link CP3-A (1)

****
Routing Time Step Summary
****
Minimum Time Step	:	30.00 sec
Average Time Step	:	30.00 sec
Maximum Time Step	:	30.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	2.08
Percent Not Converging	:	0.00

****
Subcatchment Runoff Summary
****

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff

```
-------------------------------------------------------------------------------
--------------------
  P2-B10                    2.82       0.00       0.00       0.83       1.97
0.09     9.53   0.698
  P2-B9                     2.82       0.00       0.00       0.83       1.97
0.11    11.22   0.698
  P3-S2                     2.82       0.00       0.00       1.09       1.71
0.55    49.53   0.607
  P3-A                      2.82       0.00       0.00       1.36       1.44
2.06   160.11   0.512
  P3-C                      2.82       0.00       0.00       1.51       1.32
0.06     4.80   0.469
  EF-A                      2.82       0.00       0.00       1.53       1.29
0.29    19.75   0.458
  P2-B8                     2.82       0.00       0.00       0.84       1.96
0.06     6.57   0.695
  P2-B7                     2.82       0.00       0.00       0.95       1.85
0.13    12.14   0.656
  P2-B5                     2.82       0.00       0.00       0.94       1.86
0.10     9.46   0.660
  P2-B6                     2.82       0.00       0.00       0.84       1.97
0.06     6.11   0.697
  P2-A                      2.82       0.00       0.00       1.63       1.19
0.54    32.61   0.423
  P2-B3                     2.82       0.00       0.00       0.97       1.84
0.14    13.28   0.651
  P2-B4                     2.82       0.00       0.00       0.86       1.94
0.08     8.32   0.687
  P4-A                      2.82       0.00       0.00       1.37       1.43
1.00    79.51   0.508
  P2-B                      2.82       0.00       0.00       1.37       1.43
2.30   176.39   0.505
  P2-S1                     2.82       0.00       0.00       1.18       1.62
1.57   132.76   0.576
  P2-B1                     2.82       0.00       0.00       0.86       1.94
0.13    13.20   0.689
  P2-B2                     2.82       0.00       0.00       0.86       1.94
0.10    10.02   0.689
  P4-B                      2.82       0.00       0.00       1.30       1.50
1.52   123.34   0.532
  P1-A6                     2.82       0.00       0.00       0.90       1.90
0.14    13.69   0.674
  P1-A5                     2.82       0.00       0.00       1.02       1.79
0.21    18.89   0.633
  P1-A4                     2.82       0.00       0.00       0.88       1.91
0.10    10.01   0.679
  P1-A                      2.82       0.00       0.00       1.75       1.07
0.37    18.97   0.380
  P1-A1                     2.82       0.00       0.00       1.05       1.75
```

0.24 20.94 0.621
  P1-A2 2.82 0.00 0.00 1.15 1.65
0.29 23.30 0.584
  P1-A3 2.82 0.00 0.00 0.88 1.92
0.09 9.12 0.682
  P1-C 2.82 0.00 0.00 1.13 1.67
0.49 42.78 0.593
  P1-B 2.82 0.00 0.00 1.36 1.44
1.39 108.03 0.512
  P1-D 2.82 0.00 0.00 1.31 1.49
1.27 101.80 0.529
  P1-E 2.82 0.00 0.00 1.37 1.43
2.03 161.09 0.509
  TR-W 2.82 0.00 0.00 1.19 1.62
0.06 5.23 0.573
  TR-V 2.82 0.00 0.00 1.45 1.36
0.08 5.72 0.483
  P1-F 2.82 0.00 0.00 1.46 1.34
2.80 215.28 0.476
  SC-2 2.82 0.00 0.00 1.66 1.17
0.34 20.21 0.415
  SC-3 2.82 0.00 0.00 1.99 0.83
0.70 32.41 0.295
  SC-4 2.82 0.00 0.00 1.70 1.12
0.50 27.41 0.399
  SC-1 2.82 0.00 0.00 1.73 1.10
0.11 5.65 0.389
  EX10A 2.82 0.00 0.00 2.02 0.80
1.32 50.17 0.285

****
Node Depth Summary
****

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
DP-14	JUNCTION	0.41	2.73	7082.73	0 00:45	2.62
DP-10-11	JUNCTION	0.61	3.50	7049.50	0 00:41	3.50
DP-12	JUNCTION	2.16	6.50	7038.50	0 00:46	4.98
DP-13	JUNCTION	0.15	1.21	7012.21	0 00:45	1.17
JP2-B12	JUNCTION	0.17	1.37	7073.37	0 00:45	1.31
DP-9	JUNCTION	0.73	2.94	7069.94	0 00:45	2.82
JP2-B34	JUNCTION	1.41	3.89	7058.89	0 00:46	3.66
JP2-B56	JUNCTION	1.96	4.70	7048.70	0 00:46	4.50
JP1-A12	JUNCTION	0.31	2.05	7106.05	0 00:45	1.97
JP1-A34	JUNCTION	0.33	2.12	7100.12	0 00:46	1.98

DP-7	JUNCTION	10.44	14.00	7110.00	0	00:41	14.00
DP-8	JUNCTION	0.48	3.03	7099.03	0	00:45	2.89
DP-4	JUNCTION	22.70	27.50	7123.50	0	00:47	25.90
JP1-3	JUNCTION	10.53	15.00	7143.00	0	00:46	12.85
DP-1	JUNCTION	10.10	10.57	7165.57	0	00:48	10.46
JOS-TR	JUNCTION	0.10	0.60	7190.60	0	00:45	0.58
DP-17	JUNCTION	0.49	3.13	7033.13	0	00:45	2.98
DP-6	JUNCTION	0.28	2.50	7100.50	0	00:44	2.50
DP-5	JUNCTION	0.36	2.14	7112.14	0	00:45	2.07
DP-2-3	JUNCTION	0.52	4.00	7136.00	0	00:44	4.00
DP-15	JUNCTION	0.34	2.13	7062.13	0	00:45	2.05
DP-18	JUNCTION	0.25	1.75	7013.75	0	00:45	1.69
DP-16	JUNCTION	2.41	4.61	7062.61	0	00:47	4.27
EF-A-Outfall	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
EX-DP4	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
FSD-11B	OUTFALL	5.49	8.03	7018.03	0	00:46	7.71
FSD-14A	OUTFALL	10.68	14.43	7020.43	0	00:48	13.49
FSD-14B	OUTFALL	0.50	3.14	7059.14	0	00:46	2.85
FSD-16	OUTFALL	0.73	5.47	7100.47	0	00:47	4.00
PNDW3	OUTFALL	0.00	0.00	7001.00	0	00:00	0.00
EX.STKPND	OUTFALL	0.00	0.00	7030.00	0	00:00	0.00
DPBGP	OUTFALL	0.00	0.00	7100.00	0	00:00	0.00
EX-DP7	OUTFALL	0.00	0.00	0.00	0	00:00	0.00
SC-Outfall	OUTFALL	0.00	0.00	0.00	0	00:00	0.00

****
Node Inflow Summary
****

Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
DP-14	JUNCTION	123.34	123.34	0 00:45	1.52	1.52	0.000
DP-10-11	JUNCTION	176.39	176.39	0 00:45	2.3	2.3	-0.000
DP-12	JUNCTION	18.71	298.18	0 00:47	0.189	4.47	0.000

DP-13	JUNCTION	20.75	20.75	0	00:45	0.198	0.198	0.000
JP2-B12	JUNCTION	23.22	23.22	0	00:45	0.232	0.232	0.000
DP-9	JUNCTION	132.76	155.04	0	00:45	1.57	1.8	0.000
JP2-B34	JUNCTION	21.61	172.30	0	00:46	0.224	2.02	0.000
JP2-B56	JUNCTION	15.57	284.55	0	00:46	0.155	4.28	-0.000
JP1-A12	JUNCTION	44.24	44.24	0	00:45	0.524	0.524	0.000
JP1-A34	JUNCTION	19.13	59.50	0	00:46	0.198	0.72	0.000
DP-7	JUNCTION	42.78	229.27	0	00:46	0.486	2.83	0.000
DP-8	JUNCTION	108.03	108.03	0	00:45	1.39	1.39	0.000
DP-4	JUNCTION	0.00	372.38	0	00:47	0	4.94	0.000
JP1-3	JUNCTION	5.23	364.91	0	00:46	0.0615	4.95	0.000
DP-1	JUNCTION	215.28	219.02	0	00:45	2.8	2.87	0.000
JOS-TR	JUNCTION	5.72	5.72	0	00:45	0.0777	0.0777	0.000
DP-17	JUNCTION	160.11	160.11	0	00:45	2.06	2.06	0.000
DP-6	JUNCTION	32.58	32.58	0	00:45	0.353	0.353	-0.000
DP-5	JUNCTION	101.80	101.80	0	00:45	1.27	1.27	0.000
DP-2-3	JUNCTION	161.09	161.09	0	00:45	2.03	2.03	0.000
DP-15	JUNCTION	79.51	79.51	0	00:45	1	1	0.000
DP-18	JUNCTION	49.53	49.53	0	00:45	0.553	0.553	0.000
DP-16	JUNCTION	0.00	188.99	0	00:46	0	2.52	0.000
EF-A-Outfall	OUTFALL	19.75	19.75	0	00:45	0.288	0.288	0.000
EX-DP4	OUTFALL	4.80	4.80	0	00:45	0.0611	0.0611	0.000
FSD-11B	OUTFALL	0.00	201.40	0	00:46	0	2.61	0.000
FSD-14A	OUTFALL	32.61	352.16	0	00:48	0.537	5.19	0.000
FSD-14B	OUTFALL	0.00	189.49	0	00:46	0	2.52	0.000

```
  FSD-16               OUTFALL      18.97   587.24     0  00:48        0.37
9.2       0.000
  PNDW3                OUTFALL      20.21    20.21     0  00:45       0.343
0.343       0.000
  EX.STKPND            OUTFALL      32.41    32.41     0  00:45       0.702
0.702       0.000
  DPBGP                OUTFALL      27.41    27.41     0  00:45       0.501
0.501       0.000
  EX-DP7               OUTFALL      50.17    50.17     0  00:45        1.32
1.32       0.000
  SC-Outfall           OUTFALL       5.65     5.65     0  00:45       0.107
0.107       0.000


  **********************
  Node Flooding Summary
  **********************

  Flooding refers to all water that overflows a node, whether it ponds or not.
  ----------------------------------------------------------------------------
                                                                  Total   Maximum
                                 Maximum   Time of Max           Flood    Ponded
                   Hours          Rate    Occurrence          Volume    Volume
  Node           Flooded           CFS   days hr:min       10^6 gal  1000 ft3
  ----------------------------------------------------------------------------
  DP-10-11          0.21         72.94      0  00:46          0.188     0.000
  DP-12             0.04          9.15      0  00:47          0.006     0.000
  DP-7              0.23        110.83      0  00:46          0.327     0.000
  DP-4              0.03         13.28      0  00:48          0.006     0.000
  JP1-3             0.03          7.39      0  00:47          0.004     0.000
  DP-6              0.05          2.89      0  00:46          0.002     0.000
  DP-2-3            0.05         14.39      0  00:46          0.010     0.000


  ************************
  Outfall Loading Summary
  ************************

  -----------------------------------------------------------
                       Flow       Avg       Max       Total
                       Freq      Flow      Flow      Volume
  Outfall Node         Pcnt       CFS       CFS    10^6 gal
  -----------------------------------------------------------
  EF-A-Outfall        50.56      3.52     19.75       0.288
  EX-DP4              37.36      1.01      4.80       0.061
  FSD-11B             98.33     16.43    201.40       2.611
  FSD-14A             98.47     32.64    352.16       5.193
  FSD-14B             97.92     15.90    189.49       2.516
  FSD-16              98.47     57.84    587.24       9.202
  PNDW3               42.92      4.95     20.21       0.343
```

EX.STKPND	67.22	6.46	32.41	0.702
DPBGP	46.53	6.66	27.41	0.501
EX-DP7	58.75	13.86	50.17	1.316
SC-Outfall	41.53	1.60	5.65	0.107
System	67.10	160.88	1447.90	22.839

****
Link Flow Summary
****

Link	Type	Maximum |Flow| CFS	Time of Max Occurrence days	hr:min	Maximum |Veloc| ft/sec	Max/ Full Flow	Max/ Full Depth
CP4-B	CONDUIT	115.72	0	00:47	13.93	0.76	0.65
C2	CONDUIT	20.40	0	00:46	8.87	0.47	0.48
C3	CONDUIT	22.88	0	00:46	10.26	0.80	0.67
C4	CONDUIT	151.63	0	00:46	15.85	0.87	0.72
C5	CONDUIT	169.73	0	00:46	16.06	0.98	0.80
C6	CONDUIT	282.73	0	00:47	17.50	0.95	0.78
C7	CONDUIT	305.99	0	00:48	17.38	1.06	0.91
C8	CONDUIT	106.79	0	00:52	12.03	1.06	1.00
C9	CONDUIT	42.03	0	00:46	8.77	0.77	0.66
C10	CONDUIT	59.38	0	00:46	9.76	0.68	0.61
C11	CONDUIT	124.40	0	00:54	10.81	1.06	1.00
C12	CONDUIT	106.61	0	00:46	10.66	0.91	0.75
C13	CONDUIT	5.11	0	00:48	7.23	0.18	0.28
C14	CONDUIT	210.70	0	00:46	16.56	0.72	0.63
C15	CONDUIT	372.38	0	00:47	17.66	1.05	0.91
C16	CONDUIT	360.70	0	00:48	17.23	1.02	1.00
CP3-A	CONDUIT	154.58	0	00:46	15.51	0.92	0.75
C17	CONDUIT	100.31	0	00:46	14.94	0.55	0.53
C18	CONDUIT	30.99	0	00:47	7.03	1.07	0.93
C19	CONDUIT	149.42	0	00:46	13.42	1.04	1.00
C20	CONDUIT	78.26	0	00:45	13.03	0.67	0.60
C21	CONDUIT	48.63	0	00:45	11.61	0.63	0.58
C22	CONDUIT	189.49	0	00:46	15.99	0.83	0.70

STORMWATER QUALITY CALCULATIONS

For each pond, include a summary table listing all contributing basins with area and percent impervious and determine overall area & imperviousness.

Now provided on maps

CLASSIC SM
CONSULTING ENGINEERS & SURVEYORS

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-11B

Will review forebay calculations with Final Drainage Report

1. Basin Storage Volume

A) Effective Imperviousness of Tributary Area, I_a — I_a = 66.0 %

B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$) — i = 0.660

C) Contributing Watershed Area — Area = 64.500 ac

D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm — d_6 = 0.42 in

E) Design Concept (Select EURV when also designing for flood control)
- ○ Water Quality Capture Volume (WQCV)
- ◉ Excess Urban Runoff Volume (EURV)

F) Design Volume (WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$) — V_{DESIGN} = ac-ft

G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN}/0.43))$) — $V_{DESIGN\ OTHER}$ = 1.355 ac-ft

H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired) — $V_{DESIGN\ USER}$ = ac-ft

I) NRCS Hydrologic Soil Groups of Tributary Watershed
- i) Percentage of Watershed consisting of Type A Soils — HSG_A = 0 %
- ii) Percentage of Watershed consisting of Type B Soils — HSG_B = 100 %
- iii) Percentage of Watershed consisting of Type C/D Soils — $HSG_{C/D}$ = 0 %

J) Excess Urban Runoff Volume (EURV) Design Volume
For HSG A: $EURV_A = 1.68 * i^{1.28}$
For HSG B: $EURV_B = 1.36 * i^{1.08}$
For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$
— $EURV_{DESIGN}$ = 4.667 ac-f t

K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired) — $EURV_{DESIGN\ USER}$ = ac-f t

2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.) — L : W = 2.0 : 1

3. Basin Side Slopes

A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred) — Z = 4.00 ft / ft

4. Inlet

A) Describe means of providing energy dissipation at concentrated inflow locations:

5. Forebay

A) Minimum Forebay Volume (V_{FMIN} = 3% of the WQCV) — V_{FMIN} = 0.041 ac-ft

B) Actual Forebay Volume — V_F = 0.041 ac-ft

C) Forebay Depth (D_F = 30 inch maximum) — D_F = 30.0 in

D) Forebay Discharge

i) Undetained 100-year Peak Discharge — Q_{100} = 201.00 cfs

ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$) — Q_F = 4.02 cfs

E) Forebay Discharge Design
- ○ Berm With Pipe
- ◉ Wall with Rect. Notch
- ○ Wall with V-Notch Weir

F) Discharge Pipe Size (minimum 8-inches) — Calculated D_P = in

G) Rectangular Notch Width — Calculated W_N = 9.7 in

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-11B

6. Trickle Channel	
A) Type of Trickle Channel	Choose One: (•) Concrete ( ) Soft Bottom
F) Slope of Trickle Channel	S = 0.0060 ft / ft
7. Micropool and Outlet Structure	
A) Depth of Micropool (2.5-feet minimum)	D_M = 2.5 ft
B) Surface Area of Micropool (10 ft^2 minimum)	A_M = 132 sq ft
C) Outlet Type	Choose One: (•) Orifice Plate ( ) Other (Describe):
D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)	$D_{orifice}$ = 2.99 inches
E) Total Outlet Area	A_{ot} = 30.50 square inches
8. Initial Surcharge Volume	
A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)	D_{IS} = 6 in
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)	V_{IS} = 177 cu ft
C) Initial Surcharge Provided Above Micropool	V_s = 66.0 cu ft
9. Trash Rack	
A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5*(e^{-0.095D})$	A_t = 884 square inches
B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)	*Aluminum Amico-Klemp SR Series with Cross Rods 2" O.C.*
Other (Y/N): N	
C) Ratio of Total Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water Quality Screen Area (based on screen type)	A_{total} = 1245 sq. in.
E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)	H= 5 feet
F) Height of Water Quality Screen (H_{TR})	H_{TR}= 88 inches
G) Width of Water Quality Screen Opening ($W_{opening}$) (Minimum of 12 inches is recommended)	$W_{opening}$ = 14.1 inches

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-11B

10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

B) Slope of Overflow Embankment
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Ze = 4.00 ft / ft

11. Vegetation

Choose One
- ○ Irrigated
- ◉ Not Irrigated

12. Access

A) Describe Sediment Removal Procedures

Notes:

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14A

1. Basin Storage Volume		
A) Effective Imperviousness of Tributary Area, I_a	I_a = 65.0	%
B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$)	i = 0.650	
C) Contributing Watershed Area	Area = 130.800	ac
D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm	d_6 = 0.42	in
E) Design Concept (Select EURV when also designing for flood control)	Choose One: ○ Water Quality Capture Volume (WQCV) ◉ Excess Urban Runoff Volume (EURV)	
F) Design Volume (WQCV) Based on 40-hour Drain Time ($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$)	V_{DESIGN}=	ac-ft
G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume ($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN}/0.43))$)	$V_{DESIGN\ OTHER}$= 2.706	ac-ft
H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)	$V_{DESIGN\ USER}$=	ac-ft
I) NRCS Hydrologic Soil Groups of Tributary Watershed		
i) Percentage of Watershed consisting of Type A Soils	HSG_A = 0	%
ii) Percentage of Watershed consisting of Type B Soils	HSG_B = 100	%
iii) Percentage of Watershed consisting of Type C/D Soils	$HSG_{C/D}$ = 0	%
J) Excess Urban Runoff Volume (EURV) Design Volume For HSG A: $EURV_A = 1.68 * i^{1.28}$ For HSG B: $EURV_B = 1.36 * i^{1.08}$ For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$	$EURV_{DESIGN}$ = 9.309	ac-f t
K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired)	$EURV_{DESIGN\ USER}$=	ac-f t
2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)	L : W = 2.0	: 1
3. Basin Side Slopes		
A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)	Z = 4.00	ft / ft
4. Inlet		
A) Describe means of providing energy dissipation at concentrated inflow locations:		
5. Forebay		
A) Minimum Forebay Volume (V_{FMIN} = 3% of the WQCV)	V_{FMIN} = 0.081	ac-ft
B) Actual Forebay Volume	V_F = 0.081	ac-ft
C) Forebay Depth (D_F = 30 inch maximum)	D_F = 30.0	in
D) Forebay Discharge		
i) Undetained 100-year Peak Discharge	Q_{100} = 345.00	cfs
ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$)	Q_F = 6.90	cfs
E) Forebay Discharge Design	Choose One: ○ Berm With Pipe ◉ Wall with Rect. Notch ○ Wall with V-Notch Weir	
F) Discharge Pipe Size (minimum 8-inches)	Calculated D_P =	in
G) Rectangular Notch Width	Calculated W_N = 12.3	in

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14A

6. Trickle Channel	
A) Type of Trickle Channel	Choose One: (●) Concrete ( ) Soft Bottom
F) Slope of Trickle Channel	S = 0.0060 ft / ft
7. Micropool and Outlet Structure	
A) Depth of Micropool (2.5-feet minimum)	D_M = 2.5 ft
B) Surface Area of Micropool (10 ft^2 minimum)	A_M = 132 sq ft
C) Outlet Type	Choose One: (●) Orifice Plate ( ) Other (Describe):
D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)	$D_{orifice}$ = 4.54 inches
E) Total Outlet Area	A_{ot} = 48.66 square inches
8. Initial Surcharge Volume	
A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)	D_{IS} = 6 in
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)	V_{IS} = 354 cu ft
C) Initial Surcharge Provided Above Micropool	V_s = 66.0 cu ft
9. Trash Rack	
A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5*(e^{-0.095D})$	A_t = 1,217 square inches
B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)	*Aluminum Amico-Klemp SR Series with Cross Rods 4" O.C.*
Other (Y/N): N	
C) Ratio of Total Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water Quality Screen Area (based on screen type)	A_{total} = 1581 sq. in.
E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)	H= 6.5 feet
F) Height of Water Quality Screen (H_{TR})	H_{TR}= 106 inches
G) Width of Water Quality Screen Opening ($W_{opening}$) (Minimum of 12 inches is recommended)	$W_{opening}$ = 14.9 inches

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14A

10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

B) Slope of Overflow Embankment
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Ze = 4.00 ft / ft

11. Vegetation

Choose One
- ○ Irrigated
- ◉ Not Irrigated

12. Access

A) Describe Sediment Removal Procedures

Notes:

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14B

1. Basin Storage Volume		
A) Effective Imperviousness of Tributary Area, I_a	I_a = 65.0	%
B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$)	i = 0.650	
C) Contributing Watershed Area	Area = 63.100	ac
D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm	d_6 = 0.42	in
E) Design Concept (Select EURV when also designing for flood control)	Choose One: ○ Water Quality Capture Volume (WQCV) ◉ Excess Urban Runoff Volume (EURV)	
F) Design Volume (WQCV) Based on 40-hour Drain Time ($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$)	V_{DESIGN}=	ac-ft
G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume ($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN}/0.43))$)	$V_{DESIGN\ OTHER}$= 1.305	ac-ft
H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)	$V_{DESIGN\ USER}$=	ac-ft
I) NRCS Hydrologic Soil Groups of Tributary Watershed		
i) Percentage of Watershed consisting of Type A Soils	HSG_A = 0	%
ii) Percentage of Watershed consisting of Type B Soils	HSG_B = 100	%
iii) Percentage of Watershed consisting of Type C/D Soils	$HSG_{C/D}$ = 0	%
J) Excess Urban Runoff Volume (EURV) Design Volume For HSG A: $EURV_A = 1.68 * i^{1.28}$ For HSG B: $EURV_B = 1.36 * i^{1.08}$ For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$	$EURV_{DESIGN}$ = 4.491	ac-f t
K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired)	$EURV_{DESIGN\ USER}$=	ac-f t
2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)	L : W = 2.0	: 1
3. Basin Side Slopes		
A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)	Z = 4.00	ft / ft
4. Inlet		
A) Describe means of providing energy dissipation at concentrated inflow locations:		
5. Forebay		
A) Minimum Forebay Volume (V_{FMIN} = 3% of the WQCV)	V_{FMIN} = 0.039	ac-ft
B) Actual Forebay Volume	V_F = 0.039	ac-ft
C) Forebay Depth (D_F = 30 inch maximum)	D_F = 18.0	in
D) Forebay Discharge		
i) Undetained 100-year Peak Discharge	Q_{100} = 189.00	cfs
ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$)	Q_F = 3.78	cfs
E) Forebay Discharge Design	Choose One: ○ Berm With Pipe ◉ Wall with Rect. Notch ○ Wall with V-Notch Weir	
F) Discharge Pipe Size (minimum 8-inches)	Calculated D_P =	in
G) Rectangular Notch Width	Calculated W_N = 11.0	in

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14B

6. Trickle Channel	
A) Type of Trickle Channel	Choose One: (●) Concrete ( ) Soft Bottom
F) Slope of Trickle Channel	S = 0.0060 ft / ft
7. Micropool and Outlet Structure	
A) Depth of Micropool (2.5-feet minimum)	D_M = 2.5 ft
B) Surface Area of Micropool (10 ft^2 minimum)	A_M = 132 sq ft
C) Outlet Type	Choose One: (●) Orifice Plate ( ) Other (Describe):
D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)	$D_{orifice}$ = 3.06 inches
E) Total Outlet Area	A_{ot} = 26.76 square inches
8. Initial Surcharge Volume	
A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)	D_{IS} = 6 in
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)	V_{IS} = 171 cu ft
C) Initial Surcharge Provided Above Micropool	V_s = 66.0 cu ft
9. Trash Rack	
A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5*(e^{-0.095D})$	A_t = 770 square inches
B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)	*Aluminum Amico-Klemp SR Series with Cross Rods 2" O.C.*
Other (Y/N): N	
C) Ratio of Total Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water Quality Screen Area (based on screen type)	A_{total} = 1085 sq. in.
E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)	H= 5.25 feet
F) Height of Water Quality Screen (H_{TR})	H_{TR}= 91 inches
G) Width of Water Quality Screen Opening ($W_{opening}$) (Minimum of 12 inches is recommended)	$W_{opening}$ = 12.0 inches **VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.**

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-14B

10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

B) Slope of Overflow Embankment
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Ze = 4.00 ft / ft

11. Vegetation

Choose One
- ○ Irrigated
- ◉ Not Irrigated

12. Access

A) Describe Sediment Removal Procedures

Notes:

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-16

1. Basin Storage Volume

A) Effective Imperviousness of Tributary Area, I_a — I_a = 60.0 %

B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$) — i = 0.600

C) Contributing Watershed Area — Area = 245.000 ac

D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm — d_6 = 0.42 in

E) Design Concept (Select EURV when also designing for flood control)
Choose One
- ○ Water Quality Capture Volume (WQCV)
- ◉ Excess Urban Runoff Volume (EURV)

F) Design Volume (WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$) — V_{DESIGN} = ac-ft

G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN}/0.43))$) — $V_{DESIGN\ OTHER}$ = 4.709 ac-ft

H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired) — $V_{DESIGN\ USER}$ = ac-ft

I) NRCS Hydrologic Soil Groups of Tributary Watershed
- i) Percentage of Watershed consisting of Type A Soils — HSG_A = 0 %
- ii) Percentage of Watershed consisting of Type B Soils — HSG_B = 100 %
- iii) Percentage of Watershed consisting of Type C/D Soils — $HSG_{C/D}$ = 0 %

J) Excess Urban Runoff Volume (EURV) Design Volume
For HSG A: $EURV_A = 1.68 * i^{1.28}$
For HSG B: $EURV_B = 1.36 * i^{1.08}$
For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$
— $EURV_{DESIGN}$ = 15.993 ac-f t

K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired) — $EURV_{DESIGN\ USER}$ = ac-f t

2. Basin Shape: Length to Width Ratio
(A basin length to width ratio of at least 2:1 will improve TSS reduction.) — L : W = 2.0 : 1

3. Basin Side Slopes

A) Basin Maximum Side Slopes
(Horizontal distance per unit vertical, 4:1 or flatter preferred) — Z = 4.00 ft / ft

4. Inlet

A) Describe means of providing energy dissipation at concentrated inflow locations:

5. Forebay

A) Minimum Forebay Volume
(V_{FMIN} = 3% of the WQCV) — V_{FMIN} = 0.141 ac-ft

B) Actual Forebay Volume — V_F = 0.141 ac-ft

C) Forebay Depth
(D_F = 30 inch maximum) — D_F = 30.0 in

D) Forebay Discharge

i) Undetained 100-year Peak Discharge — Q_{100} = 589.00 cfs

ii) Forebay Discharge Design Flow
($Q_F = 0.02 * Q_{100}$) — Q_F = 11.78 cfs

E) Forebay Discharge Design
Choose One
- ○ Berm With Pipe
- ◉ Wall with Rect. Notch
- ○ Wall with V-Notch Weir

F) Discharge Pipe Size (minimum 8-inches) — Calculated D_P = in

G) Rectangular Notch Width — Calculated W_N = 16.7 in

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-16

6. Trickle Channel	
A) Type of Trickle Channel	Choose One: (●) Concrete ( ) Soft Bottom
F) Slope of Trickle Channel	S = 0.0060 ft / ft
7. Micropool and Outlet Structure	
A) Depth of Micropool (2.5-feet minimum)	D_M = 2.5 ft
B) Surface Area of Micropool (10 ft^2 minimum)	A_M = 132 sq ft
C) Outlet Type	Choose One: (●) Orifice Plate ( ) Other (Describe):
D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)	$D_{orifice}$ = 4.51 inches
E) Total Outlet Area	A_{ot} = 116.00 square inches
8. Initial Surcharge Volume	
A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)	D_{IS} = 6 in
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)	V_{IS} = 615 cu ft
C) Initial Surcharge Provided Above Micropool	V_s = 66.0 cu ft
9. Trash Rack	
A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5*(e^{-0.095D})$	A_t = 2,910 square inches
B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)	*Aluminum Amico-Klemp SR Series with Cross Rods 4" O.C.*
Other (Y/N): N	
C) Ratio of Total Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water Quality Screen Area (based on screen type)	A_{total} = 3779 sq. in.
E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)	H= 6.5 feet
F) Height of Water Quality Screen (H_{TR})	H_{TR}= 106 inches
G) Width of Water Quality Screen Opening ($W_{opening}$) (Minimum of 12 inches is recommended)	$W_{opening}$ = 35.6 inches

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 30, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: FSD-16

10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

B) Slope of Overflow Embankment
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Ze = 4.00 ft / ft

11. Vegetation

Choose One
- ○ Irrigated
- ◉ Not Irrigated

12. Access

A) Describe Sediment Removal Procedures

Notes:

WATER QUALITY TREATMENT PLAN MAP

	STERLING RANCH EAST PHASE 1 DEVELOPMENT AREA
61.1 AC.	AREA QUALIFIES FOR EXCLUSION H – STREAM STABILIZATION (PBMP FORM)
64.5 AC.	AREA TREATED IN PROPOSED PERMANENT POND FSD–11B
130.8 AC.	AREA TREATED IN PROPOSED PERMANENT POND FSD–14A
63.1 AC.	AREA TREATED IN PROPOSED PERMANENT POND FSD–14B
245.0 AC.	AREA TREATED IN PROPOSED PERMANENT POND FSD–16
10.3 AC.	AREAS OF RUNOFF REDUCTION WATER QUALITY TREATMENT

ARROYA LANE
EXIST. 48" CMP CULVERT
EXIST. 60" CMP CULVERT
EXIST. 18" CMP CULVERT
OVERALL TIMBERRIDGE PROPERTY BOUNDARY
OVERALL STERLING RANCH PROPERTY BOUNDARY
UNPLATTED (5 AC. ÷ RESIDENTIAL)
UNPLATTED (FUTURE TIMBERRIDGE DEVELOPMENT RESIDENTIAL USE)
UNPLATTED (FUTURE STERLING RANCH RESIDENTIAL USE)
VOLLMER ROAD
ASPEN VALLEY RD.
SAND CREEK REACH SC-9
EXIST. 30" RCP STORM OUTFALL
EXIST. DUAL 30" RCP CULVERTS
EXIST. 24" RCP STOCK POND OUTFALL
EXIST. STOCK POND
RETREAT AT TIMBERRIDGE FILING NO. 2
RETREAT AT TIMBERRIDGE FILING NO. 2 POND 1
RETREAT AT TIMBERRIDGE FILING NO. 1
EXIST. TEMP. SEDIMENT BASIN
ELK ANTLER LANE
EXIST. DUAL 24" RCP CULVERTS
POCO ROAD
EXIST. DUAL ARCH CULVERTS
EXIST. RAIN GARDEN
OWL PERCH LOOP
BISON VALLEY TRAIL
SAND CREEK EAST FORK
UNPLATTED (FUTURE HOMESTEAD NORTH AT STERLING RANCH FILING NO. 3 RESIDENTIAL USE)
PROPOSED HOMESTEAD NORTH AT STERLING RANCH FILING NO. 2
PROPOSED HOMESTEAD NORTH AT STERLING RANCH FILING NO. 1
REFERENCE SAND CREEK CHANNEL IMPROVEMENTS PROPOSED WITH HOMESTEAD NORTH AT STERLING RANCH FIL.NO. 1 PREPARED BY JR ENG.
PROP. OPEN SPACE
PROP. STERLING RANCH EAST PRELIMINARY PLAN NO. 1
PROP. STERLING RANCH EAST PRELIMINARY PLAN/PUD NO. 2
PROP. STERLING RANCH EAST PRELIMINARY PLAN/PUD NO. 3
BASIN SC–4–2 UIA AREA
BASIN SC–4–2 RPA AREA (25' REAR SETBACK)
BASIN SC–4–1 UIA AREA
BASIN SC–4–1 RPA AREA (25' REAR SETBACK)
BASIN SC–3–2 UIA AREA
BASIN SC–3–2 RPA AREA (25' REAR SETBACK)
BASIN SC–3–1 UIA AREA
BASIN SC–3–1 RPA AREA (25' REAR SETBACK)
BASIN EF–A UIA AREA
BASIN EF–A RPA AREA (25' REAR SETBACK)
BRIARGATE BLVD. (130' ROW)
FUTURE BRIARGATE BLVD. (130' ROW)
STERLING RANCH RD. (120' ROW)
STERLING RANCH RD. (100' ROW)
PROP. POND FSD–16
PROP. POND FSD–14B
PROP. POND FSD–14A
PROP. POND FSD–11B
PROP. SCHOOL SITE
PROP. PARK/OPEN SPACE
EX. STOCK POND
PNDW3
PROP. 1/2 AC. LOTS
HOMESTEAD AT STERLING RANCH FILING NO. 2
HOMESTEAD AT STERLING RANCH FILING NO. 1
BRANDING IRON AT STERLING RANCH FILING NO. 1
BRANDING IRON AT STERLING RANCH FILING NO. 2
STERLING RANCH FILING NO. 2
PAWNEE RANCHEROS FILING NO. 2
PAWNEE RANCHEROS FILING NO. 1
MUSTANG PLACE
MUSTANG ROAD
COCHISE ROAD
MOHAWK ROAD
BRULE ROAD
OTO CIRCLE
BAR J-S ACRES FILING NO. 2
UNPLATTED BLH NO. 1 LLC (BANNING LEWIS RA
TR–12 4.7
TR–20 23.2
TR–4 4.4
TR–5 13.7
TR–6 1.5

Design Procedure Form: Runoff Reduction

UD-BMP (Version 3.07, March 2018) **Sheet 1 of 1**

Designer: Marc A. Whorton, P.E.
Company: Classic Consulting
Date: May 31, 2022
Project: Sterling Ranch East Preliminary Plan No. 1
Location: BASINS NOT TRIBUTARY TO PERMANENT SWQ FACILITY

SITE INFORMATION (User Input in Blue Cells)

WQCV Rainfall Depth: 0.53 inches
Depth of Average Runoff Producing Storm, d_6 = 0.42 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)

Area Type	UIA:RPA	UIA:RPA	UIA:RPA	UIA:RPA	UIA:RPA							
Area ID	EF-A	SC-3-1	SC-3-2	SC-4-1	SC-4-2							
Downstream Design Point ID	SC	SC	SC	SC	SC							
Downstream BMP Type	None	None	None	None	None							
DCIA (ft^2)	--	--	--	--	--							
UIA (ft^2)	40,000	26,790	19,924	30,053	48,697							
RPA (ft^2)	37,188	17,918	12,924	21,985	28,692							
SPA (ft^2)	--	--	--	--	--							
HSG A (%)	0%	0%	0%	0%	0%							
HSG B (%)	100%	100%	100%	100%	100%							
HSG C/D (%)	0%	0%	0%	0%	0%							
Average Slope of RPA (ft/ft)	0.020	0.040	0.030	0.040	0.040							
UIA:RPA Interface Width (ft)	800.00	700.00	400.00	800.00	1000.00							

CALCULATED RUNOFF RESULTS

Area ID	EF-A	SC-3-1	SC-3-2	SC-4-1	SC-4-2							
UIA:RPA Area (ft^2)	77,188	44,708	32,848	52,038	77,389							
L / W Ratio	0.12	0.09	0.21	0.08	0.08							
UIA / Area	0.5182	0.5992	0.6066	0.5775	0.6292							
Runoff (in)	0.00	0.00	0.00	0.00	0.00							
Runoff (ft^3)	0	0	0	0	0							
Runoff Reduction (ft^3)	1433	960	714	1077	1745							

CALCULATED WQCV RESULTS

Area ID	EF-A	SC-3-1	SC-3-2	SC-4-1	SC-4-2							
WQCV (ft^3)	1628	1090	811	1223	1982							
WQCV Reduction (ft^3)	1628	1090	811	1223	1982							
WQCV Reduction (%)	100%	100%	100%	100%	100%							
Untreated WQCV (ft^3)	0	0	0	0	0							

CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID)

Downstream Design Point ID	SC											
DCIA (ft^2)	0											
UIA (ft^2)	165,464											
RPA (ft^2)	118,707											
SPA (ft^2)	0											
Total Area (ft^2)	284,171											
Total Impervious Area (ft^2)	165,464											
WQCV (ft^3)	6,734											
WQCV Reduction (ft^3)	6,734											
WQCV Reduction (%)	100%											
Untreated WQCV (ft^3)	0											

CALCULATED SITE RESULTS (sums results from all columns in worksheet)

Total Area (ft^2)	284,171
Total Impervious Area (ft^2)	165,464
WQCV (ft^3)	6,734
WQCV Reduction (ft^3)	6,734
WQCV Reduction (%)	100%
Untreated WQCV (ft^3)	0

DETENTION POND CALCULATIONS

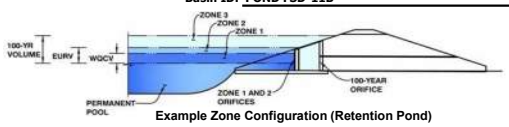
CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: STERLING RANCH EAST PRELIMINARY PLAN NO. 1

Basin ID: POND FSD-11B



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	64.50	acres
Watershed Length =	2,500	ft
Watershed Length to Centroid =	1,250	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	66.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

All soils type in project are Group A. Please move 100% to Group A

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides
Water Quality Capture Volume (WQCV) =	1.387	acre-feet	acre-feet
Excess Urban Runoff Volume (EURV) =	4.653	acre-feet	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	4.293	acre-feet	1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	5.841	acre-feet	1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	7.157	acre-feet	1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	8.754	acre-feet	2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	10.141	acre-feet	2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	11.816	acre-feet	2.52 inches
500-yr Runoff Volume (P1 = 3.48 in.) =	17.305	acre-feet	3.48 inches
Approximate 2-yr Detention Volume =	3.614	acre-feet	
Approximate 5-yr Detention Volume =	4.839	acre-feet	
Approximate 10-yr Detention Volume =	6.156	acre-feet	
Approximate 25-yr Detention Volume =	6.628	acre-feet	
Approximate 50-yr Detention Volume =	6.900	acre-feet	
Approximate 100-yr Detention Volume =	7.445	acre-feet	

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.387	acre-feet
Zone 2 Volume (EURV - Zone 1) =	3.266	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.792	acre-feet
Total Detention Basin Volume =	7.445	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	**user**	acre-feet

Depth Increment = ft

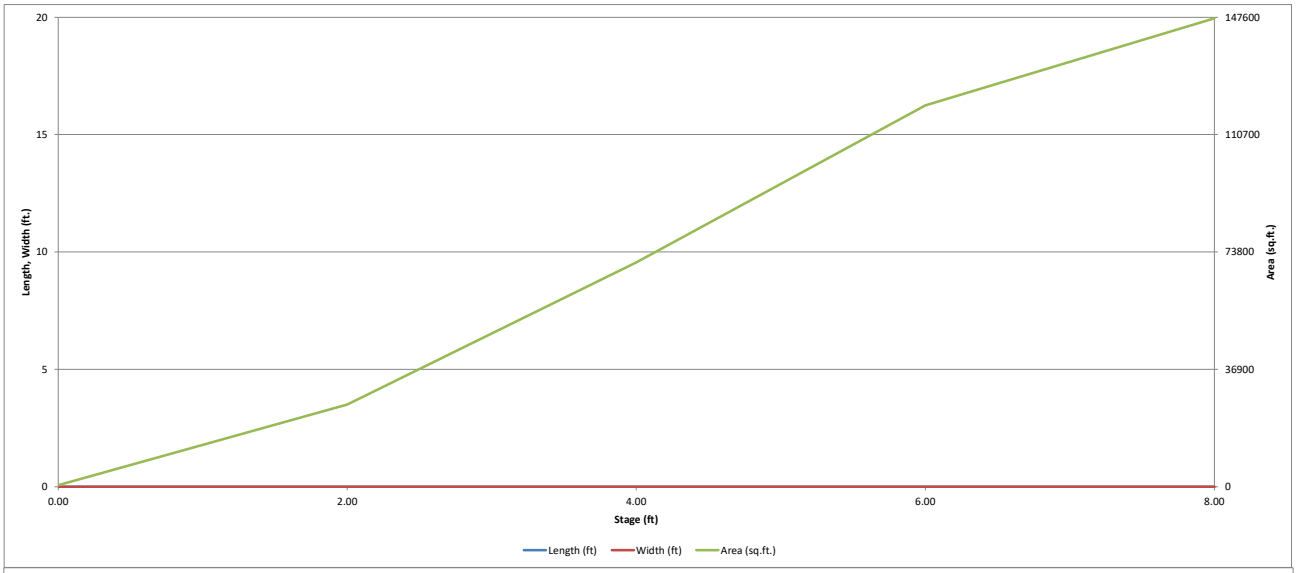
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	525	0.012		
7004	--	2.00	--	--	--	25,865	0.594	26,390	0.606
7006	--	4.00	--	--	--	70,579	1.620	122,834	2.820
7008	--	6.00	--	--	--	119,914	2.753	313,327	7.193
7010	--	8.00	--	--	--	147,297	3.381	580,538	13.327

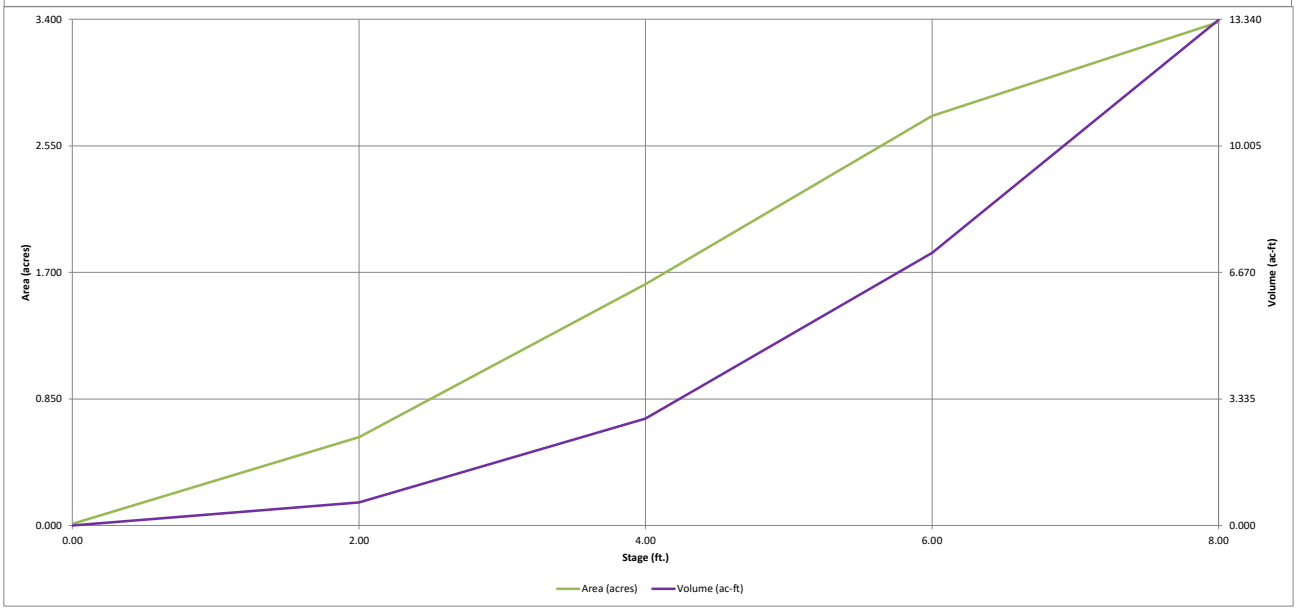
UNDERTAND, HOWEVER, GIVEN THAT OVERLOT GRADING WILL BE TAKING PLACE WITH IMPORT BEING NEEDED PLEASE REFERENCE DCM 5.3.4 WHERE IT SAYS TO NOT USE TYPE "A" SOILS WHEN OVERLOT GRADING OR FILL OPERATIONS HAVE OCCURED.

USING TYPE "B" SOILS IS MORE CONSERVATIVE AS WELL.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



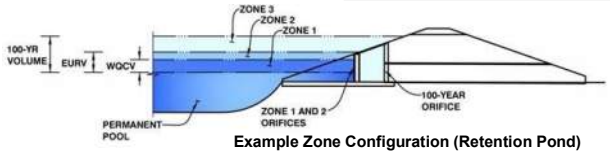


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: **STERLING RANCH EAST PRELIMINARY PLAN NO. 1**

Basin ID: **POND FSD-11B**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.94	1.387	Orifice Plate
Zone 2 (EURV)	4.97	3.266	Orifice Plate
Zone 3 (100-year)	6.10	2.792	Weir&Pipe (Restrict)
Total (all zones)		7.445	

Outlet design will be reviewed with Final Drainage Reports

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	N/A	ft^2
Depth at top of Zone using Orifice Plate =	5.00	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	20.00	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.70	3.40					
Orifice Area (sq. inches)	7.00	7.50	16.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected			Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.00	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	5.00	N/A	feet
Overflow Weir Front Edge Length =	10.00	N/A	feet	Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	4.48	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Grate Open Area w/o Debris =	31.64	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	15.82	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	7.07	N/A	ft^2
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.50	N/A	feet
Restrictor Plate Height Above Pipe Invert =	36.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	6.50	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.95	feet
Spillway Crest Length =	70.00	feet	Stage at Top of Freeboard =	8.45	feet
Spillway End Slopes =	3.00	H:V	Basin Area at Top of Freeboard =	3.38	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	13.33	acre-ft

Calculated Parameters for Spillway

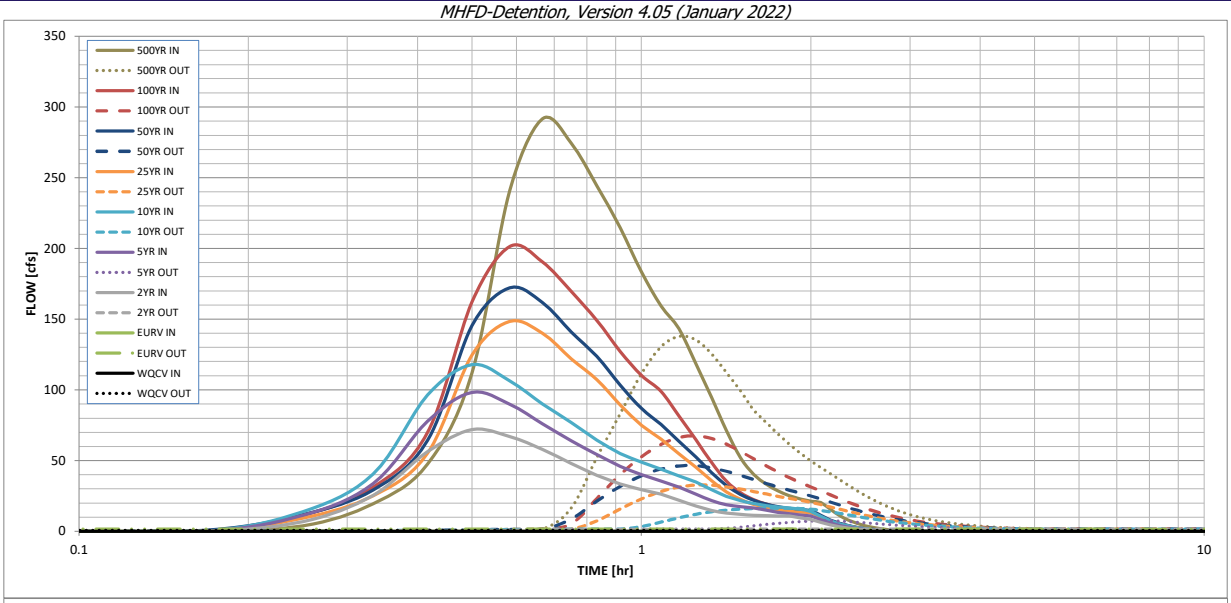
Routed Hydrograph Results

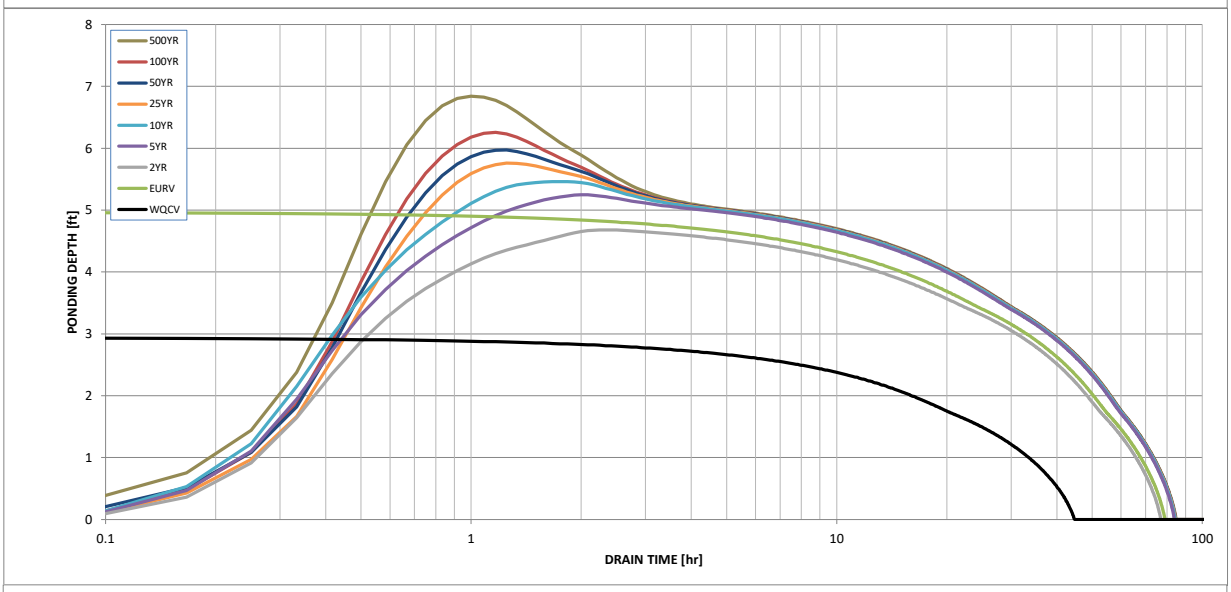
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

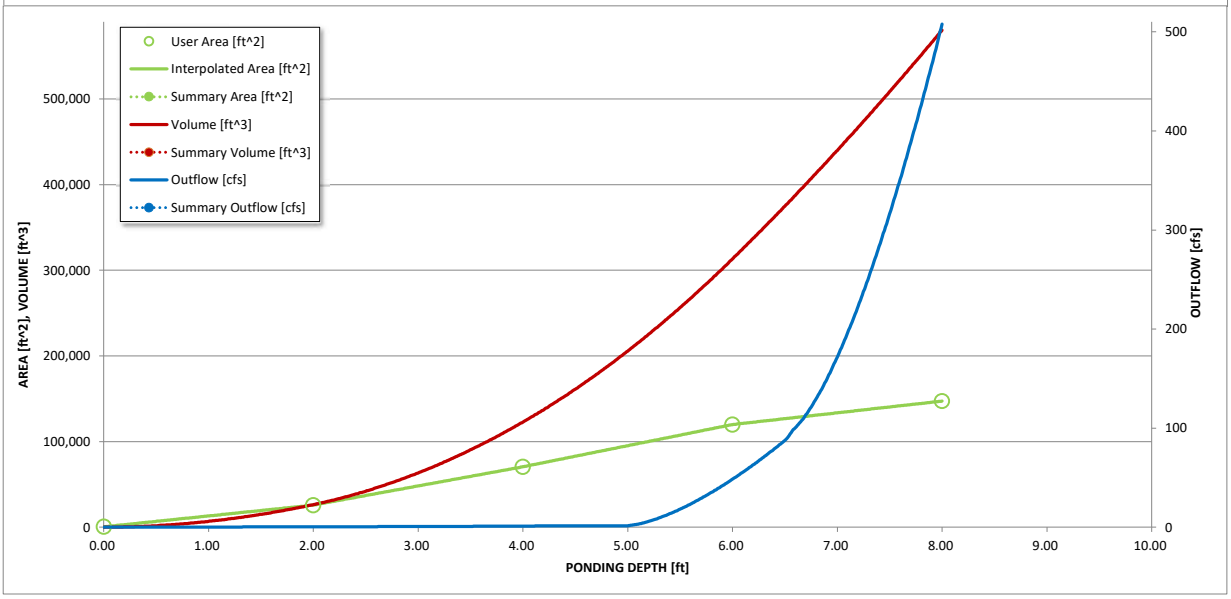
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.48
CUHP Runoff Volume (acre-ft) =	1.387	4.653	4.293	5.841	7.157	8.754	10.141	11.816	17.305
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.293	5.841	7.157	8.754	10.141	11.816	17.305
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	6.6	18.4	28.0	50.1	63.0	80.0	130.0
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.29	0.43	0.78	0.98	1.24	2.02
Peak Inflow Q (cfs) =	N/A	N/A	71.9	98.3	117.8	148.3	172.1	201.3	291.7
Peak Outflow Q (cfs) =	0.7	1.6	1.5	7.5	16.4	32.7	46.4	67.5	137.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.7	0.8	1.1
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.5	1.0	1.4	2.1	2.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	41	69	67	72	70	68	67	64	59
Time to Drain 99% of Inflow Volume (hours) =	**43**	74	73	79	78	77	77	76	73
Maximum Ponding Depth (ft) =	2.94	4.97	4.68	5.25	5.46	5.76	5.97	6.26	6.84
Area at Maximum Ponding Depth (acres) =	1.08	2.17	2.01	2.32	2.45	2.61	2.74	2.83	3.02
Maximum Volume Stored (acre-ft) =	1.391	4.658	4.053	5.264	5.789	6.522	7.111	7.891	9.616

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.78	0.08	3.82
	0:15:00	0.00	0.00	6.87	11.21	13.87	9.31	11.72	11.35	19.51
	0:20:00	0.00	0.00	25.39	33.68	40.41	25.06	29.22	31.19	47.45
	0:25:00	0.00	0.00	56.34	77.94	96.43	55.11	64.21	69.80	112.10
	0:30:00	0.00	0.00	71.88	98.26	117.80	124.61	145.55	162.31	240.92
	0:35:00	0.00	0.00	66.99	89.81	106.30	148.33	172.14	201.33	291.73
	0:40:00	0.00	0.00	57.88	76.05	90.13	140.06	161.83	190.39	274.50
	0:45:00	0.00	0.00	48.02	64.06	76.98	121.99	140.88	169.62	244.42
	0:50:00	0.00	0.00	39.64	54.32	64.57	107.14	123.71	149.12	214.64
	0:55:00	0.00	0.00	33.54	46.00	55.09	89.45	103.35	127.24	183.36
	1:00:00	0.00	0.00	29.45	40.14	48.97	74.98	86.79	110.24	159.34
	1:05:00	0.00	0.00	26.22	35.53	44.00	65.21	75.61	98.94	143.14
	1:10:00	0.00	0.00	21.95	31.20	39.15	54.80	63.62	81.42	118.39
	1:15:00	0.00	0.00	17.87	26.33	34.74	45.24	52.60	64.61	94.62
	1:20:00	0.00	0.00	14.68	21.62	29.41	35.74	41.51	48.63	71.17
	1:25:00	0.00	0.00	12.82	18.84	24.77	27.89	32.34	35.43	52.02
	1:30:00	0.00	0.00	11.88	17.41	21.70	22.52	26.06	27.35	40.34
	1:35:00	0.00	0.00	11.38	16.51	19.66	18.96	21.85	22.46	33.19
	1:40:00	0.00	0.00	11.11	14.88	18.21	16.71	19.16	19.23	28.41
	1:45:00	0.00	0.00	10.91	13.42	17.19	15.17	17.31	17.01	25.12
	1:50:00	0.00	0.00	10.75	12.40	16.47	14.18	16.12	15.50	22.87
	1:55:00	0.00	0.00	9.50	11.65	15.55	13.48	15.27	14.42	21.24
	2:00:00	0.00	0.00	8.27	10.79	14.06	13.01	14.70	13.77	20.26
	2:05:00	0.00	0.00	6.29	8.22	10.59	10.02	11.30	10.61	15.58
	2:10:00	0.00	0.00	4.50	5.83	7.46	7.07	7.96	7.50	10.99
	2:15:00	0.00	0.00	3.20	4.15	5.30	5.04	5.66	5.39	7.88
	2:20:00	0.00	0.00	2.26	2.90	3.75	3.57	4.01	3.84	5.61
	2:25:00	0.00	0.00	1.55	1.96	2.58	2.46	2.76	2.65	3.86
	2:30:00	0.00	0.00	1.03	1.31	1.75	1.68	1.89	1.81	2.64
	2:35:00	0.00	0.00	0.65	0.87	1.14	1.13	1.27	1.21	1.76
	2:40:00	0.00	0.00	0.36	0.52	0.67	0.69	0.77	0.73	1.06
	2:45:00	0.00	0.00	0.16	0.26	0.32	0.35	0.39	0.37	0.53
	2:50:00	0.00	0.00	0.06	0.09	0.11	0.12	0.14	0.13	0.18
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

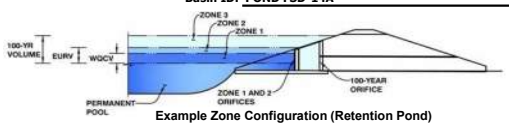
Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: STERLING RANCH EAST PRELIMINARY PLAN NO. 1

Basin ID: POND FSD-14A



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	130.80	acres
Watershed Length =	4,500	ft
Watershed Length to Centroid =	2,250	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	65.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

All soils type in project are Group A. Please move 100% to Group A

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides
Water Quality Capture Volume (WQCV) =	2.770	acre-feet	acre-feet
Excess Urban Runoff Volume (EURV) =	9.282	acre-feet	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	8.609	acre-feet	1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	11.740	acre-feet	1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	14.406	acre-feet	1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	17.668	acre-feet	2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	20.486	acre-feet	2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	23.901	acre-feet	2.52 inches
500-yr Runoff Volume (P1 = 3.48 in.) =	35.063	acre-feet	3.48 inches
Approximate 2-yr Detention Volume =	7.197	acre-feet	
Approximate 5-yr Detention Volume =	9.650	acre-feet	
Approximate 10-yr Detention Volume =	12.301	acre-feet	
Approximate 25-yr Detention Volume =	13.252	acre-feet	
Approximate 50-yr Detention Volume =	13.799	acre-feet	
Approximate 100-yr Detention Volume =	14.917	acre-feet	

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	2.770	acre-feet
Zone 2 Volume (EURV - Zone 1) =	6.512	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	5.636	acre-feet
Total Detention Basin Volume =	14.917	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	**user**	acre-feet

Depth Increment = ft

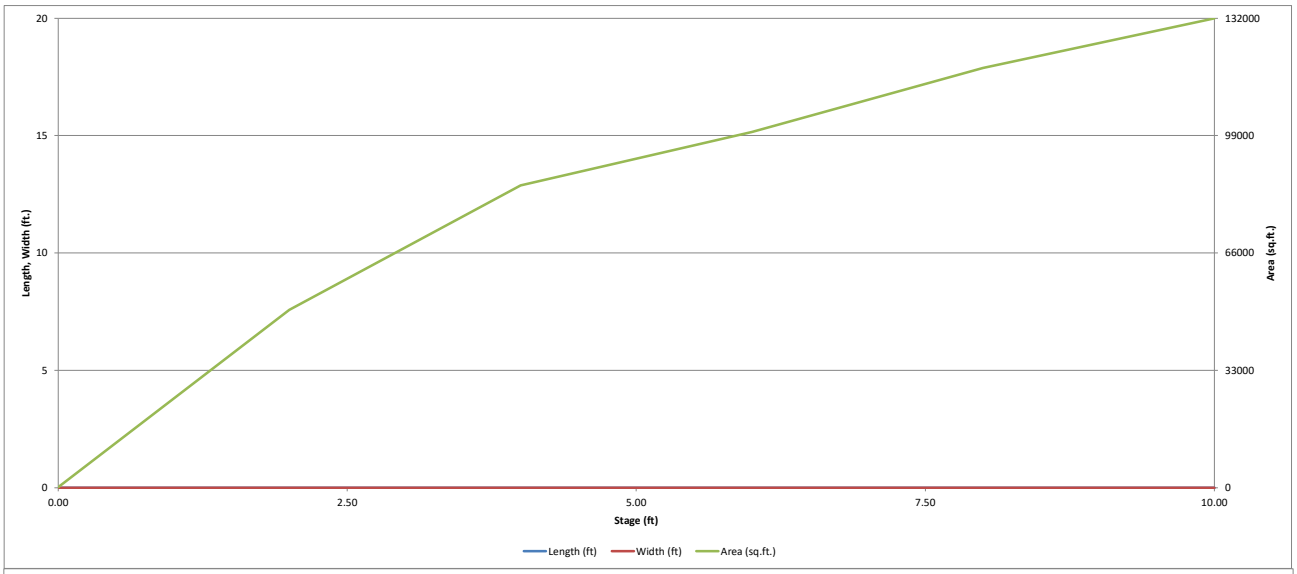
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	200	0.005		
7014	--	2.00	--	--	--	50,000	1.148	50,199	1.152
7016	--	4.00	--	--	--	85,000	1.951	185,199	4.252
			--	--	--	100,000	2.296	370,199	8.499
			--	--	--	118,000	2.709	588,199	13.503
			--	--	--	132,000	3.030	838,199	19.242
			--	--	--				
			--	--	--				
			--	--	--				
	--		--	--	--				
	--		--	--	--				

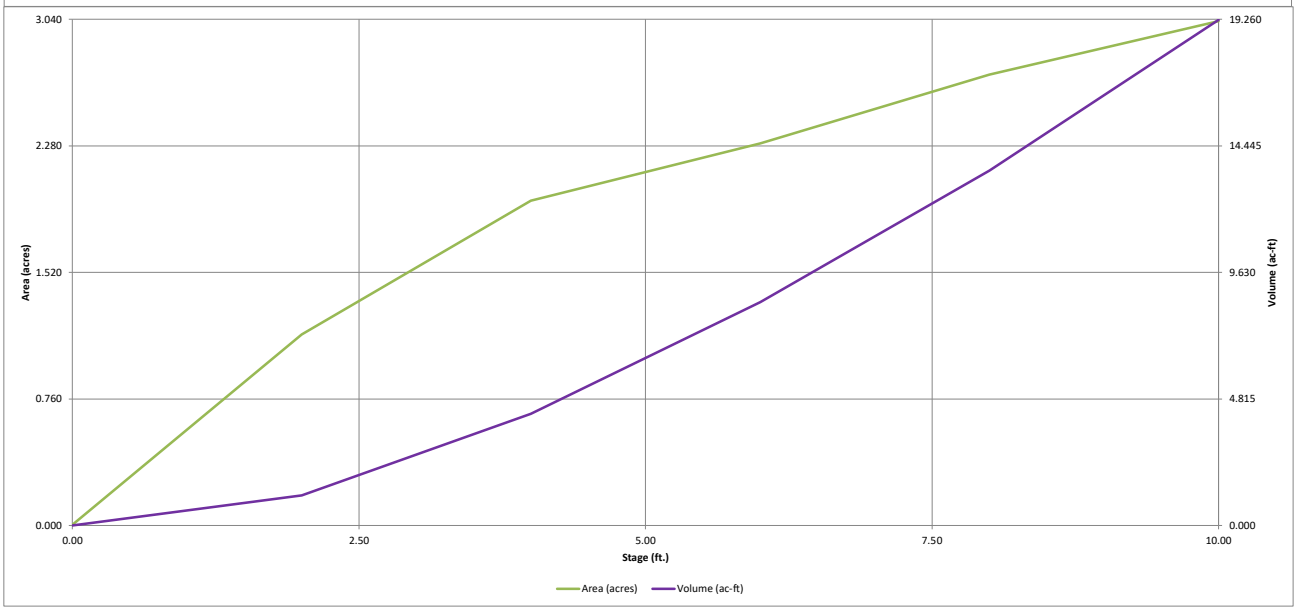
UNDERTAND, HOWEVER, GIVEN THAT OVERLOT GRADING WILL BE TAKING PLACE WITH IMPORT BEING NEEDED PLEASE REFERENCE DCM 5.3.4 WHERE IT SAYS TO NOT USE TYPE "A" SOILS WHEN OVERLOT GRADING OR FILL OPERATIONS HAVE OCCURED.

USING TYPE "B" SOILS IS MORE CONSERVATIVE AS WELL.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



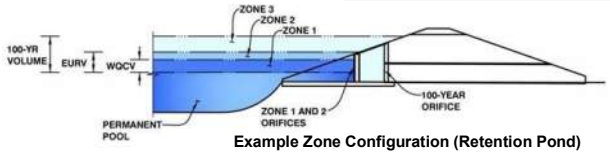


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: **STERLING RANCH EAST PRELIMINARY PLAN NO. 1**

Basin ID: **POND FSD-14A**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.17	2.770	Orifice Plate
Zone 2 (EURV)	6.34	6.512	Orifice Plate
Zone 3 (100-year)	8.52	5.636	Weir&Pipe (Restrict)
Total (all zones)		14.917	

Outlet design will be reviewed with Final Drainage Reports

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	1.126E-01	ft^2
Depth at top of Zone using Orifice Plate =	6.50	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	26.00	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	16.22	sq. inches (use rectangular openings)	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.20	4.40					
Orifice Area (sq. inches)	16.22	16.22	16.22					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected			Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.50	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	6.50	N/A	feet
Overflow Weir Front Edge Length =	20.00	N/A	feet	Overflow Weir Slope Length =	5.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	9.01	N/A	
Horiz. Length of Weir Sides =	5.00	N/A	feet	Overflow Grate Open Area w/o Debris =	79.10	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	39.55	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	8.78	N/A	ft^2
Outlet Pipe Diameter =	42.00	N/A	inches	Outlet Orifice Centroid =	1.61	N/A	feet
Restrictor Plate Height Above Pipe Invert =	36.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	2.37	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	8.50	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	1.07	feet
Spillway Crest Length =	100.00	feet	Stage at Top of Freeboard =	10.57	feet
Spillway End Slopes =	3.00	H:V	Basin Area at Top of Freeboard =	3.03	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	19.24	acre-ft

Calculated Parameters for Spillway

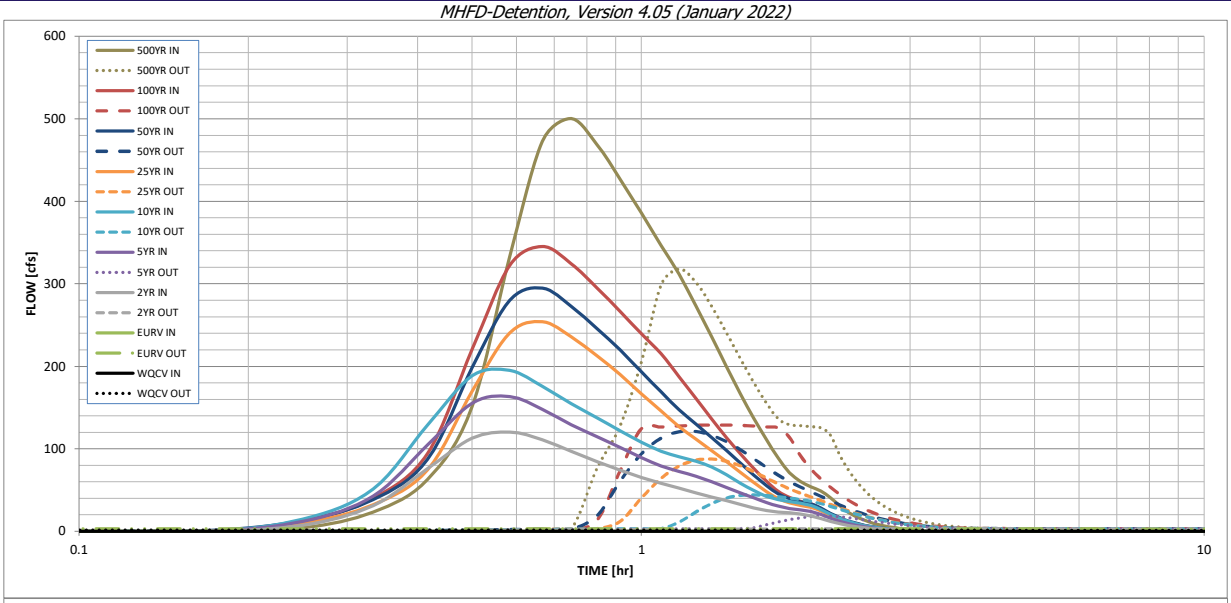
Routed Hydrograph Results

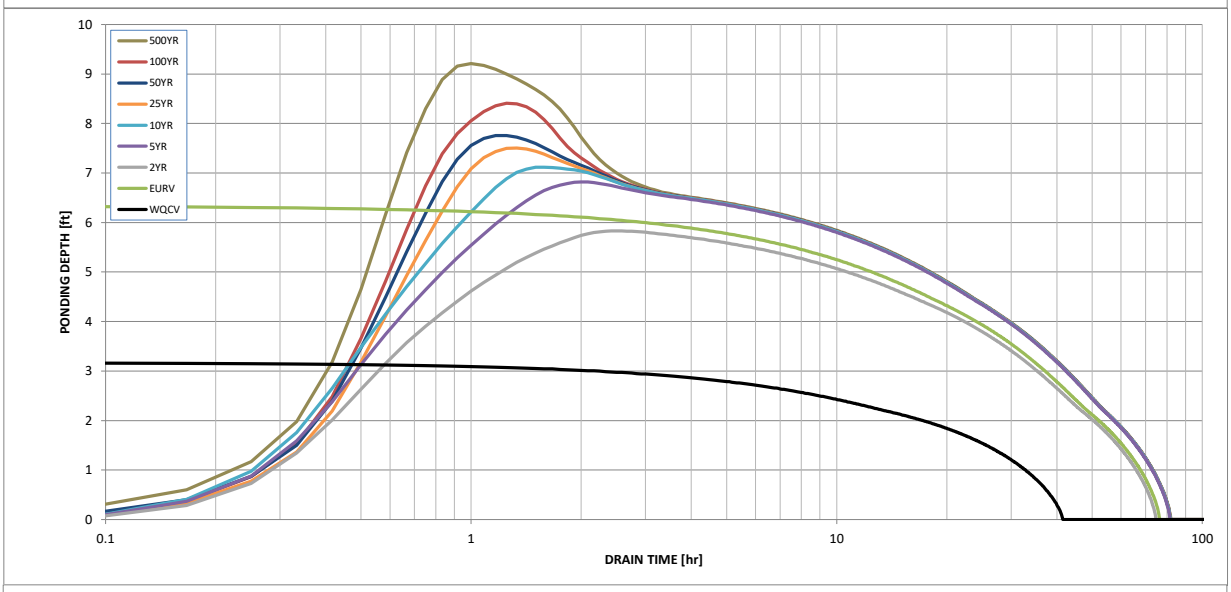
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

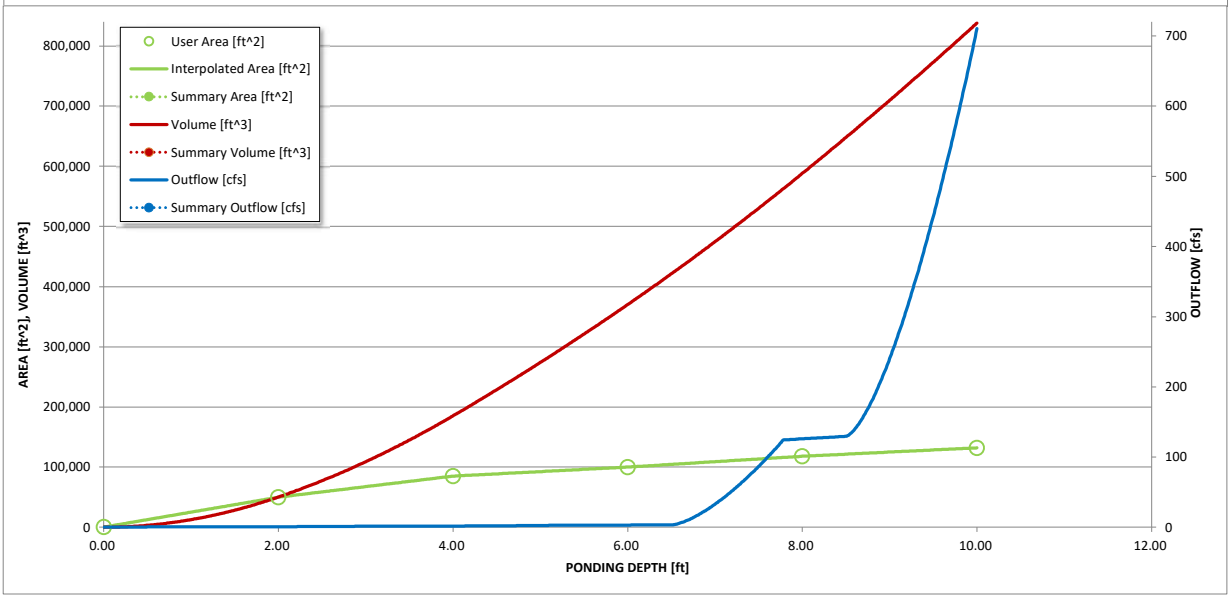
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.48
CUHP Runoff Volume (acre-ft) =	2.770	9.282	8.609	11.740	14.406	17.668	20.486	23.901	35.063
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	8.609	11.740	14.406	17.668	20.486	23.901	35.063
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	10.4	29.4	45.4	83.2	104.6	134.7	219.3
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.08	0.22	0.35	0.64	0.80	1.03	1.68
Peak Inflow Q (cfs) =	N/A	N/A	120.4	163.4	195.0	254.2	294.7	345.0	500.4
Peak Outflow Q (cfs) =	1.5	3.2	3.0	18.6	44.1	87.6	121.1	128.9	317.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	1.0	1.1	1.2	1.0	1.4
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.5	1.1	1.5	1.6	1.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	67	72	70	68	67	65	59
Time to Drain 99% of Inflow Volume (hours) =	**40**	73	71	77	77	76	75	74	72
Maximum Ponding Depth (ft) =	3.17	6.34	5.83	6.82	7.12	7.51	7.76	8.41	9.21
Area at Maximum Ponding Depth (acres) =	1.62	2.37	2.27	2.47	2.53	2.61	2.66	2.77	2.90
Maximum Volume Stored (acre-ft) =	2.770	9.291	8.111	10.451	11.199	12.175	12.832	14.600	16.899

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.83	0.08	4.10
	0:15:00	0.00	0.00	7.34	11.99	14.85	9.97	13.01	12.20	23.15
	0:20:00	0.00	0.00	31.15	42.58	51.34	32.27	38.23	40.05	62.65
	0:25:00	0.00	0.00	75.83	104.57	128.91	74.63	87.15	94.34	150.88
	0:30:00	0.00	0.00	112.78	155.26	188.30	169.61	198.29	220.11	332.99
	0:35:00	0.00	0.00	120.41	163.39	195.05	240.34	279.90	322.30	472.85
	0:40:00	0.00	0.00	110.81	147.76	175.58	254.22	294.73	345.04	500.39
	0:45:00	0.00	0.00	96.96	129.27	154.76	235.64	272.59	324.43	469.02
	0:50:00	0.00	0.00	84.57	114.87	137.59	212.75	245.96	295.05	426.65
	0:55:00	0.00	0.00	74.18	101.73	121.89	189.94	219.80	266.52	385.70
	1:00:00	0.00	0.00	65.29	89.30	107.94	166.57	192.99	239.37	346.52
	1:05:00	0.00	0.00	58.31	79.25	97.09	145.75	169.04	215.23	311.87
	1:10:00	0.00	0.00	52.29	72.69	90.30	126.81	147.28	187.41	272.92
	1:15:00	0.00	0.00	46.70	66.78	85.00	111.80	130.02	161.00	235.79
	1:20:00	0.00	0.00	41.63	59.97	78.00	97.70	113.61	136.21	199.86
	1:25:00	0.00	0.00	37.05	53.03	68.47	84.42	98.06	113.63	166.42
	1:30:00	0.00	0.00	32.62	46.42	58.33	71.38	82.74	93.80	137.12
	1:35:00	0.00	0.00	28.50	40.63	49.46	59.17	68.36	76.23	111.23
	1:40:00	0.00	0.00	25.19	34.79	42.45	48.27	55.56	60.80	88.67
	1:45:00	0.00	0.00	23.36	30.49	38.49	39.50	45.33	48.41	71.06
	1:50:00	0.00	0.00	22.53	27.72	36.08	34.54	39.54	41.15	60.59
	1:55:00	0.00	0.00	20.81	25.79	33.99	31.34	35.77	36.47	53.77
	2:00:00	0.00	0.00	18.59	24.05	31.45	29.25	33.27	33.18	48.96
	2:05:00	0.00	0.00	15.45	20.39	26.52	24.82	28.19	27.65	40.81
	2:10:00	0.00	0.00	12.08	15.90	20.65	19.29	21.87	21.01	30.99
	2:15:00	0.00	0.00	9.28	12.13	15.73	14.55	16.48	15.51	22.86
	2:20:00	0.00	0.00	7.13	9.29	11.97	11.04	12.47	11.57	17.04
	2:25:00	0.00	0.00	5.48	7.09	9.05	8.43	9.50	8.85	12.99
	2:30:00	0.00	0.00	4.16	5.32	6.74	6.32	7.11	6.67	9.76
	2:35:00	0.00	0.00	3.13	3.92	5.02	4.69	5.27	5.00	7.32
	2:40:00	0.00	0.00	2.31	2.86	3.74	3.48	3.91	3.74	5.47
	2:45:00	0.00	0.00	1.67	2.08	2.76	2.61	2.92	2.80	4.09
	2:50:00	0.00	0.00	1.14	1.44	1.93	1.86	2.08	1.99	2.90
	2:55:00	0.00	0.00	0.71	0.95	1.25	1.23	1.38	1.32	1.92
	3:00:00	0.00	0.00	0.39	0.56	0.71	0.74	0.82	0.79	1.14
	3:05:00	0.00	0.00	0.17	0.28	0.33	0.37	0.41	0.39	0.56
	3:10:00	0.00	0.00	0.06	0.09	0.10	0.12	0.13	0.13	0.18
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

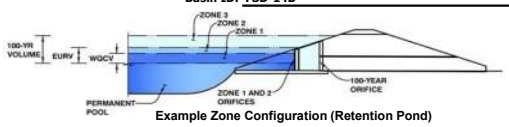
Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: STERLING RANCH EAST PRELIMINARY PLAN/PUD NO. 3

Basin ID: FSD-14B



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	63.10	acres
Watershed Length =	2,500	ft
Watershed Length to Centroid =	1,250	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	65.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

All soils type in project are Group A. Please move 100% to Group A

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides	
Water Quality Capture Volume (WQCV) =	1.336	acre-feet		acre-feet
Excess Urban Runoff Volume (EURV) =	4.478	acre-feet		acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	4.138	acre-feet	1.19	inches
5-yr Runoff Volume (P1 = 1.5 in.) =	5.644	acre-feet	1.50	inches
10-yr Runoff Volume (P1 = 1.75 in.) =	6.926	acre-feet	1.75	inches
25-yr Runoff Volume (P1 = 2 in.) =	8.495	acre-feet	2.00	inches
50-yr Runoff Volume (P1 = 2.25 in.) =	9.849	acre-feet	2.25	inches
100-yr Runoff Volume (P1 = 2.52 in.) =	11.491	acre-feet	2.52	inches
500-yr Runoff Volume (P1 = 3.48 in.) =	16.858	acre-feet	3.48	inches
Approximate 2-yr Detention Volume =	3.472	acre-feet		
Approximate 5-yr Detention Volume =	4.655	acre-feet		
Approximate 10-yr Detention Volume =	5.934	acre-feet		
Approximate 25-yr Detention Volume =	6.393	acre-feet		
Approximate 50-yr Detention Volume =	6.657	acre-feet		
Approximate 100-yr Detention Volume =	7.196	acre-feet		

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.336	acre-feet
Zone 2 Volume (EURV - Zone 1) =	3.141	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.719	acre-feet
Total Detention Basin Volume =	7.196	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

Depth Increment = 1.00 ft

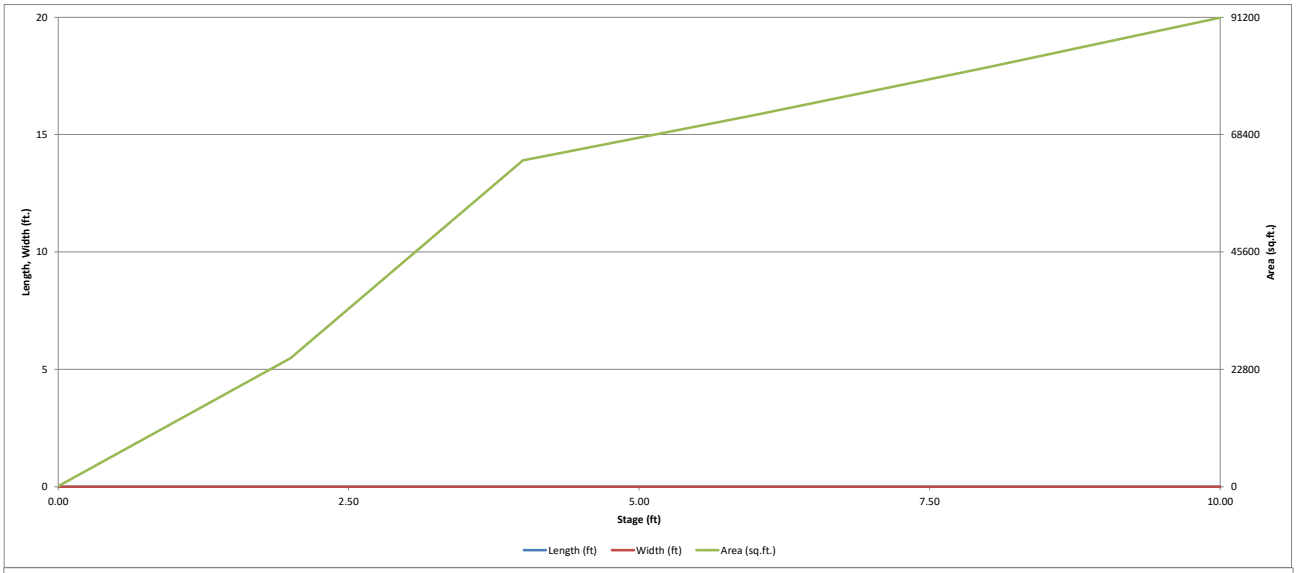
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	100	0.002		
7052	--	2.00	--	--	--	25,000	0.574	25,100	0.576
7054	--	4.00	--	--	--	63,400	1.455	113,500	2.606
7056	--	6.00	--	--	--	72,250	1.659	249,150	5.720
				--	--	81,500	1.871	402,900	9.249
				--	--	91,150	2.093	575,550	13.213
				--	--				
				--	--				
				--	--				
				--	--				
				--	--				
	--		--	--	--				
	--		--	--	--				

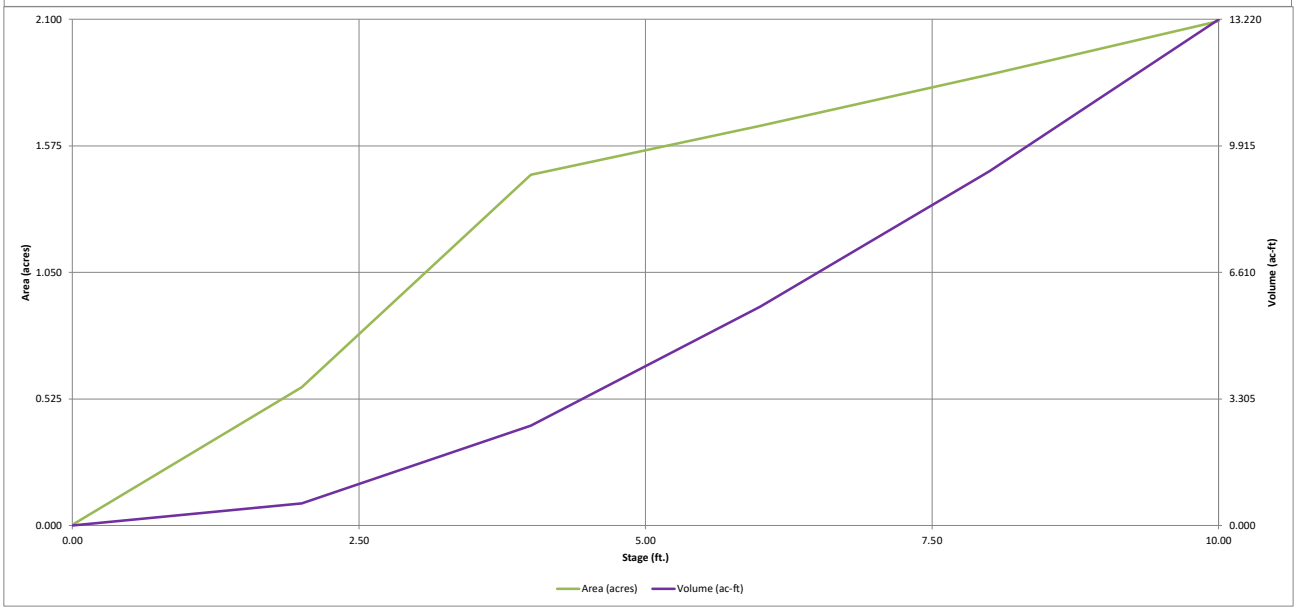
UNDERTAND, HOWEVER, GIVEN THAT OVERLOT GRADING WILL BE TAKING PLACE WITH IMPORT BEING NEEDED PLEASE REFERENCE DCM 5.3.4 WHERE IT SAYS TO NOT USE TYPE "A" SOILS WHEN OVERLOT GRADING OR FILL OPERATIONS HAVE OCCURED.

USING TYPE "B" SOILS IS MORE CONSERVATIVE AS WELL.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



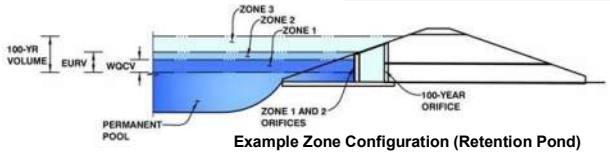


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: **STERLING RANCH EAST PRELIMINARY PLAN/PUD NO. 3**

Basin ID: **FSD-14B**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.97	1.336	Orifice Plate
Zone 2 (EURV)	5.24	3.141	Orifice Plate
Zone 3 (100-year)	6.87	2.719	Weir&Pipe (Restrict)
Total (all zones)		7.196	

Outlet design will be reviewed with Final Drainage Reports

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	N/A	ft^2
Depth at top of Zone using Orifice Plate =	5.24	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	21.00	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.75	3.49					
Orifice Area (sq. inches)	7.29	7.29	10.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected			Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.24	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	5.24	N/A	feet
Overflow Weir Front Edge Length =	16.00	N/A	feet	Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	5.26	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Grate Open Area w/o Debris =	50.62	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	25.31	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	9.62	N/A	ft^2
Outlet Pipe Diameter =	42.00	N/A	inches	Outlet Orifice Centroid =	1.75	N/A	feet
Restrictor Plate Height Above Pipe Invert =	42.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	7.00	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	1.02	feet
Spillway Crest Length =	60.00	feet	Stage at Top of Freeboard =	9.02	feet
Spillway End Slopes =	3.00	H:V	Basin Area at Top of Freeboard =	1.98	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	11.22	acre-ft

Calculated Parameters for Spillway

Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

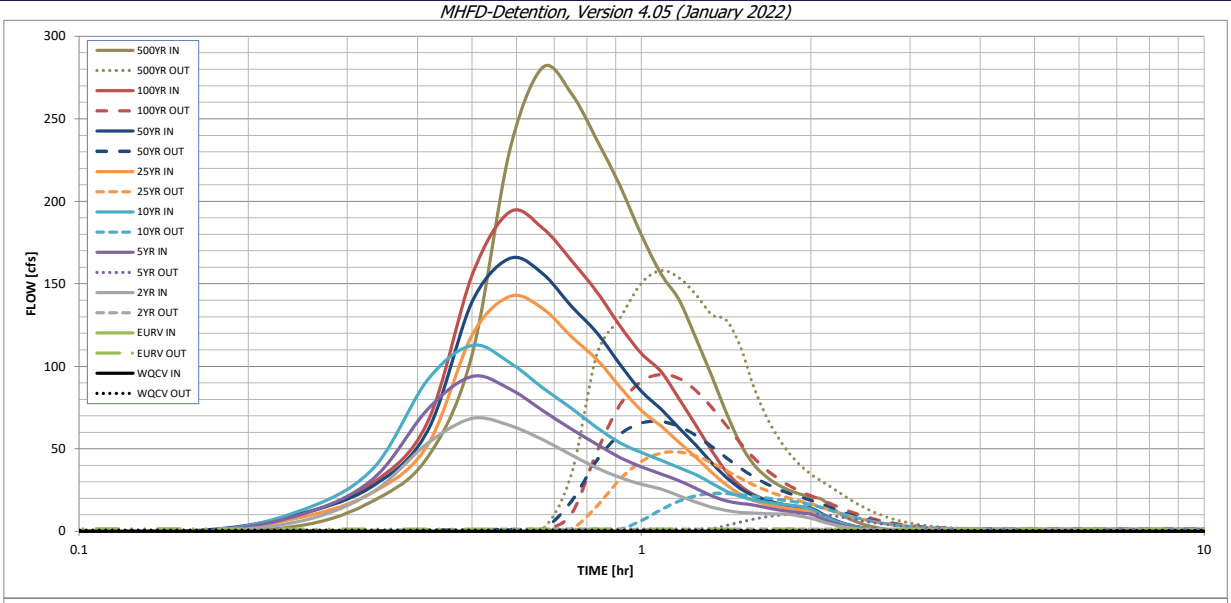
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.48
CUHP Runoff Volume (acre-ft) =	1.336	4.478	4.138	5.644	6.926	8.495	9.849	11.491	16.858
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.138	5.644	6.926	8.495	9.849	11.491	16.858
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	6.4	17.9	27.2	48.6	61.1	77.6	126.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A		57.0				124.0	
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.90	0.43	0.77	0.97	1.97	2.00
Peak Inflow Q (cfs) =	N/A	N/A	68.4	93.9	112.8	142.4	165.4	193.6	281.0
Peak Outflow Q (cfs) =	0.7	1.5	1.4	10.6	22.9	48.0	66.5	95.0	158.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.8	1.0	1.1	0.8	1.3
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.4	0.9	1.3	1.8	2.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	67	70	69	67	65	63	57
Time to Drain 99% of Inflow Volume (hours) =	**40**	74	72	77	76	75	74	73	71
Maximum Ponding Depth (ft) =	2.97	5.24	4.88	5.51	5.71	6.03	6.22	6.49	7.28
Area at Maximum Ponding Depth (acres) =	1.00	1.58	1.54	1.61	1.63	1.66	1.68	1.71	1.79
Maximum Volume Stored (acre-ft) =	1.340	4.488	3.910	4.903	5.227	5.753	6.087	6.545	7.912

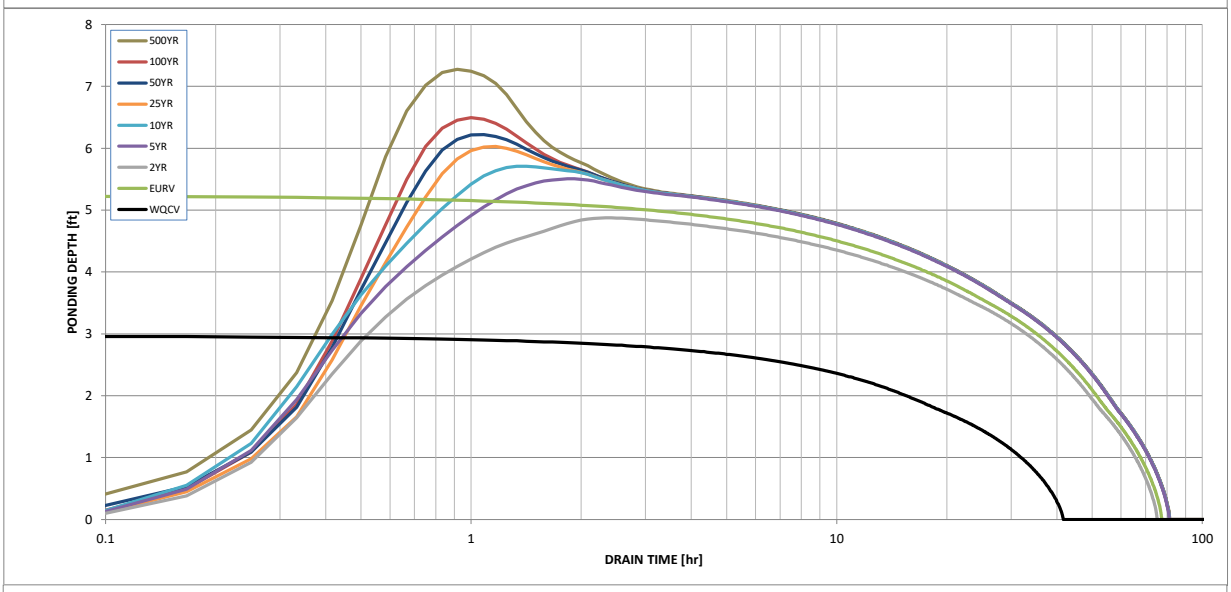
NOW CORRECT SEE REVISED

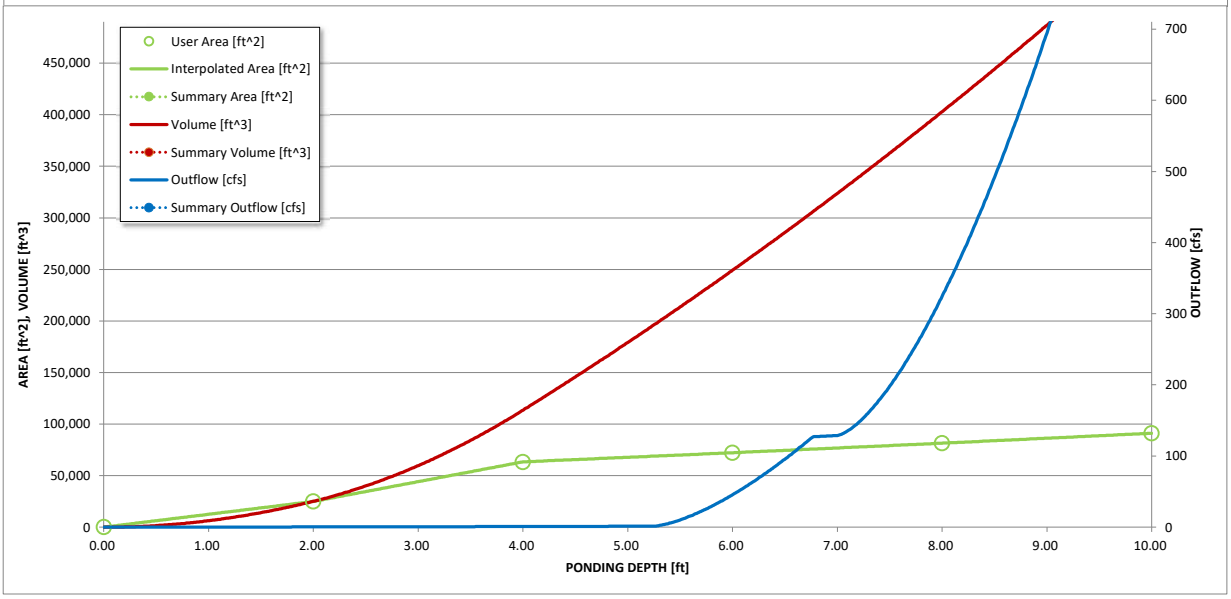
Flows shown do not match those shown on developed drainage map. Confirm which flows are correct and update as needed.

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.73	0.07	3.60
	0:15:00	0.00	0.00	6.46	10.54	13.05	8.76	11.03	10.68	18.39
	0:20:00	0.00	0.00	23.94	31.77	38.11	23.64	27.59	29.43	44.82
	0:25:00	0.00	0.00	53.28	73.95	91.70	52.12	60.79	66.14	106.78
	0:30:00	0.00	0.00	68.40	93.86	112.76	118.88	139.02	155.14	230.89
	0:35:00	0.00	0.00	64.09	86.25	102.28	142.40	165.44	193.57	281.00
	0:40:00	0.00	0.00	55.59	73.32	87.06	135.11	156.25	183.92	265.56
	0:45:00	0.00	0.00	46.35	62.02	74.67	118.05	136.45	164.34	237.21
	0:50:00	0.00	0.00	38.42	52.81	62.91	104.13	120.35	145.11	209.22
	0:55:00	0.00	0.00	32.49	44.67	53.58	87.34	101.01	124.37	179.48
	1:00:00	0.00	0.00	28.56	39.02	47.69	73.16	84.77	107.68	155.92
	1:05:00	0.00	0.00	25.54	34.71	43.04	63.78	74.04	96.82	140.34
	1:10:00	0.00	0.00	21.57	30.69	38.56	53.92	62.67	80.21	116.85
	1:15:00	0.00	0.00	17.73	26.07	34.36	44.84	52.19	64.17	94.16
	1:20:00	0.00	0.00	14.61	21.49	29.17	35.74	41.56	48.87	71.66
	1:25:00	0.00	0.00	12.59	18.46	24.27	28.08	32.59	36.03	52.90
	1:30:00	0.00	0.00	11.54	16.89	21.11	22.34	25.88	27.45	40.53
	1:35:00	0.00	0.00	11.00	15.97	19.09	18.67	21.53	22.30	33.02
	1:40:00	0.00	0.00	10.71	14.40	17.65	16.36	18.78	19.02	28.14
	1:45:00	0.00	0.00	10.52	12.99	16.63	14.80	16.91	16.73	24.75
	1:50:00	0.00	0.00	10.36	12.00	15.92	13.78	15.68	15.18	22.44
	1:55:00	0.00	0.00	9.18	11.27	15.04	13.07	14.82	14.07	20.78
	2:00:00	0.00	0.00	8.00	10.44	13.62	12.59	14.23	13.37	19.71
	2:05:00	0.00	0.00	6.11	7.99	10.32	9.74	10.99	10.31	15.16
	2:10:00	0.00	0.00	4.41	5.72	7.32	6.92	7.80	7.33	10.76
	2:15:00	0.00	0.00	3.16	4.09	5.23	4.96	5.58	5.29	7.75
	2:20:00	0.00	0.00	2.25	2.90	3.73	3.55	3.98	3.81	5.57
	2:25:00	0.00	0.00	1.57	1.98	2.60	2.47	2.77	2.65	3.88
	2:30:00	0.00	0.00	1.05	1.33	1.78	1.70	1.91	1.83	2.67
	2:35:00	0.00	0.00	0.68	0.90	1.19	1.17	1.31	1.25	1.82
	2:40:00	0.00	0.00	0.40	0.56	0.72	0.73	0.82	0.78	1.13
	2:45:00	0.00	0.00	0.19	0.30	0.37	0.40	0.44	0.42	0.61
	2:50:00	0.00	0.00	0.08	0.12	0.14	0.16	0.18	0.17	0.24
	2:55:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

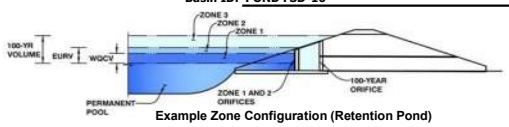
Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: STERLING RANCH EAST PRELIMINARY PLAN NO. 1

Basin ID: POND FSD-16



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	245.00	acres
Watershed Length =	5,800	ft
Watershed Length to Centroid =	2,900	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	60.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

All soils type in project are Group A. Please move 100% to Group A

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides
Water Quality Capture Volume (WQCV) =	4.822	acre-feet	acre-feet
Excess Urban Runoff Volume (EURV) =	15.946	acre-feet	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	14.895	acre-feet	1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	20.580	acre-feet	1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	25.471	acre-feet	1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	31.662	acre-feet	2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	36.887	acre-feet	2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	43.326	acre-feet	2.52 inches
500-yr Runoff Volume (P1 = 3.48 in.) =	64.093	acre-feet	3.48 inches
Approximate 2-yr Detention Volume =	12.261	acre-feet	
Approximate 5-yr Detention Volume =	16.552	acre-feet	
Approximate 10-yr Detention Volume =	21.333	acre-feet	
Approximate 25-yr Detention Volume =	23.070	acre-feet	
Approximate 50-yr Detention Volume =	24.049	acre-feet	
Approximate 100-yr Detention Volume =	26.256	acre-feet	

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	4.822	acre-feet
Zone 2 Volume (EURV - Zone 1) =	11.124	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	10.310	acre-feet
Total Detention Basin Volume =	26.256	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	**user**	acre-feet

UNDERTAND, HOWEVER, GIVEN THAT OVERLOT GRADING WILL BE TAKING PLACE WITH IMPORT BEING NEEDED PLEASE REFERENCE DCM 5.3.4 WHERE IT SAYS TO NOT USE TYPE "A" SOILS WHEN OVERLOT GRADING OR FILL OPERATIONS HAVE OCCURED.

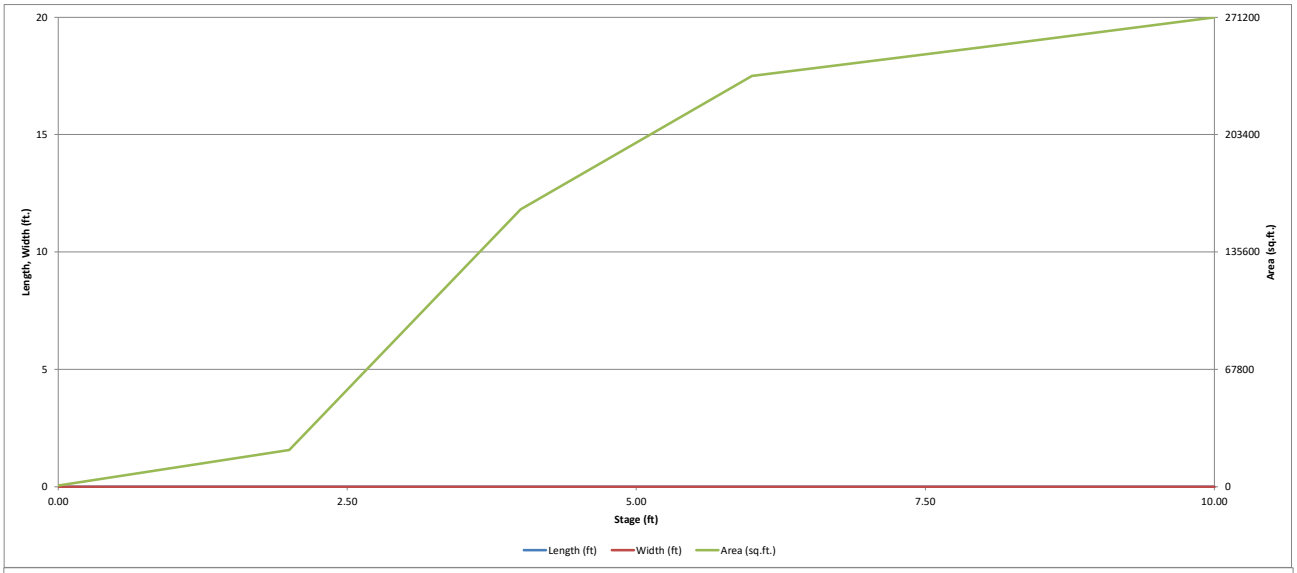
USING TYPE "B" SOILS IS MORE CONSERVATIVE AS WELL.

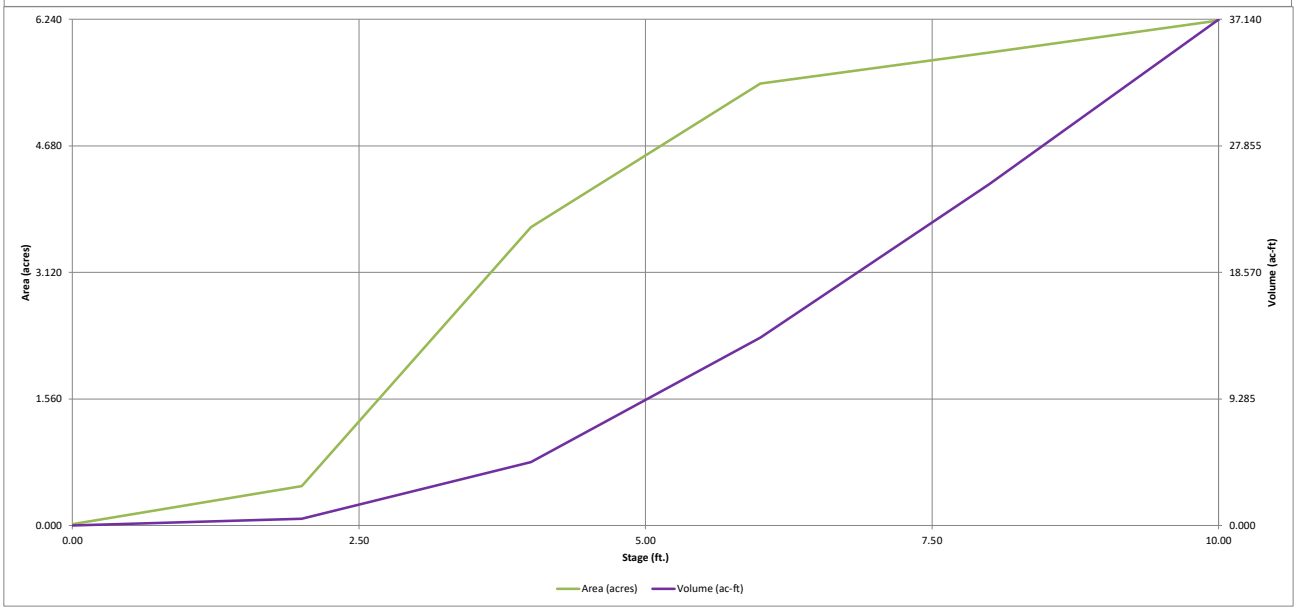
Depth Increment = ft

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	683	0.016		
7094	--	2.00	--	--	--	21,230	0.487	21,913	0.503
7096	--	4.00	--	--	--	160,188	3.677	203,330	4.668
7098	--	6.00	--	--	--	237,278	5.447	600,796	13.792
7100	--	8.00	--	--	--	253,964	5.830	1,092,038	25.070
7102	--	10.00	--	--	--	271,164	6.225	1,617,166	37.125

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



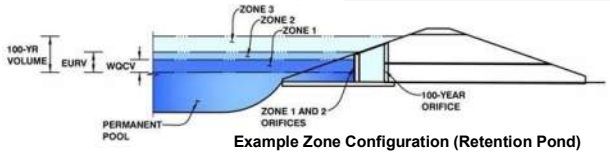


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: **STERLING RANCH EAST PRELIMINARY PLAN NO. 1**

Basin ID: **POND FSD-16**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.05	4.822	Orifice Plate
Zone 2 (EURV)	6.40	11.124	Orifice Plate
Zone 3 (100-year)	8.21	10.310	Weir&Pipe (Restrict)
Total (all zones)		26.256	

Outlet design will be reviewed with Final Drainage Reports

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	N/A	ft^2
Depth at top of Zone using Orifice Plate =	6.50	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	26.00	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.20	4.40					
Orifice Area (sq. inches)	16.00	20.00	80.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected			Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.50	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	6.50	N/A	feet
Overflow Weir Front Edge Length =	20.00	N/A	feet	Overflow Weir Slope Length =	5.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	6.56	N/A	
Horiz. Length of Weir Sides =	5.00	N/A	feet	Overflow Grate Open Area w/o Debris =	79.10	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	39.55	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	12.07	N/A	ft^2
Outlet Pipe Diameter =	48.00	N/A	inches	Outlet Orifice Centroid =	1.93	N/A	feet
Restrictor Plate Height Above Pipe Invert =	44.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	2.56	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	9.00	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	1.18	feet
Spillway Crest Length =	150.00	feet	Stage at Top of Freeboard =	11.18	feet
Spillway End Slopes =	3.00	H:V	Basin Area at Top of Freeboard =	6.23	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	37.13	acre-ft

Calculated Parameters for Spillway

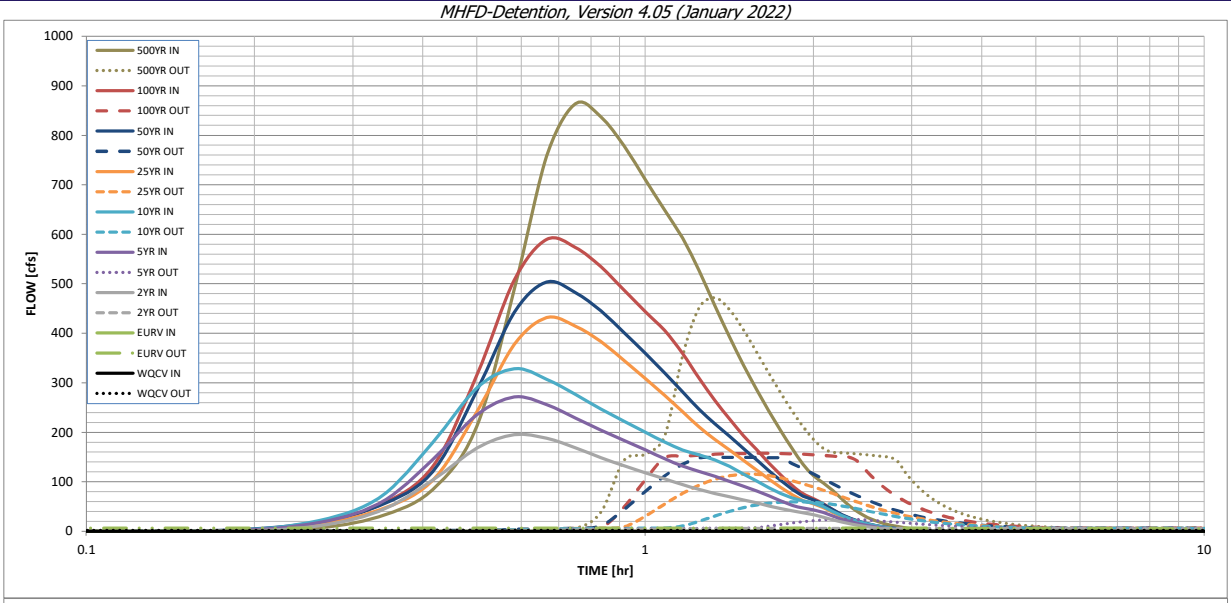
Routed Hydrograph Results

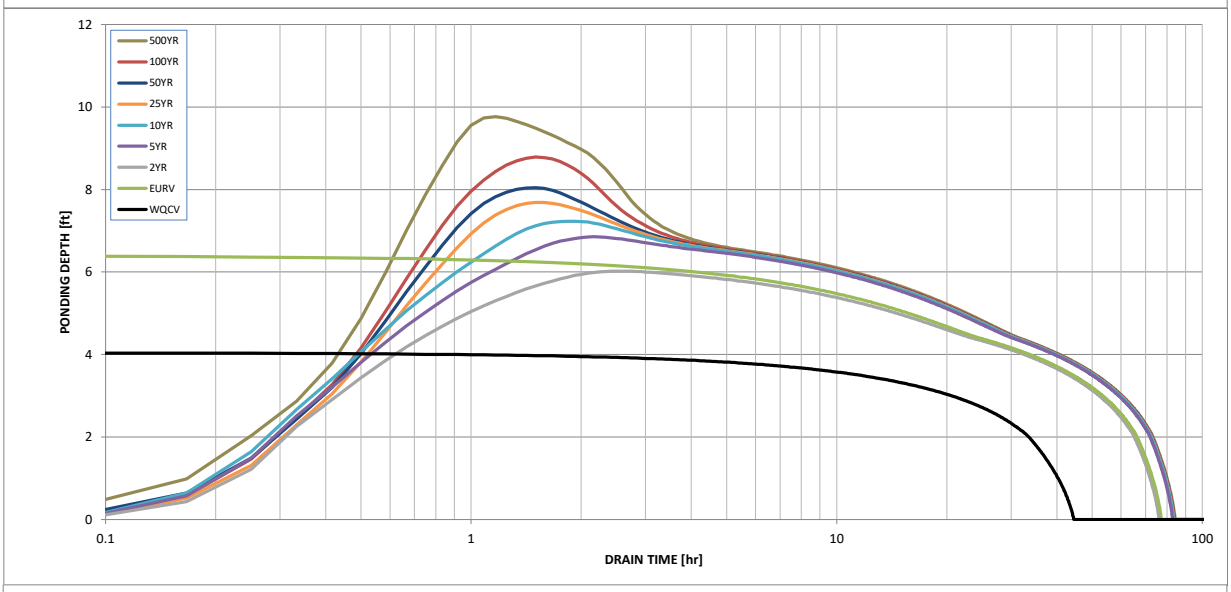
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

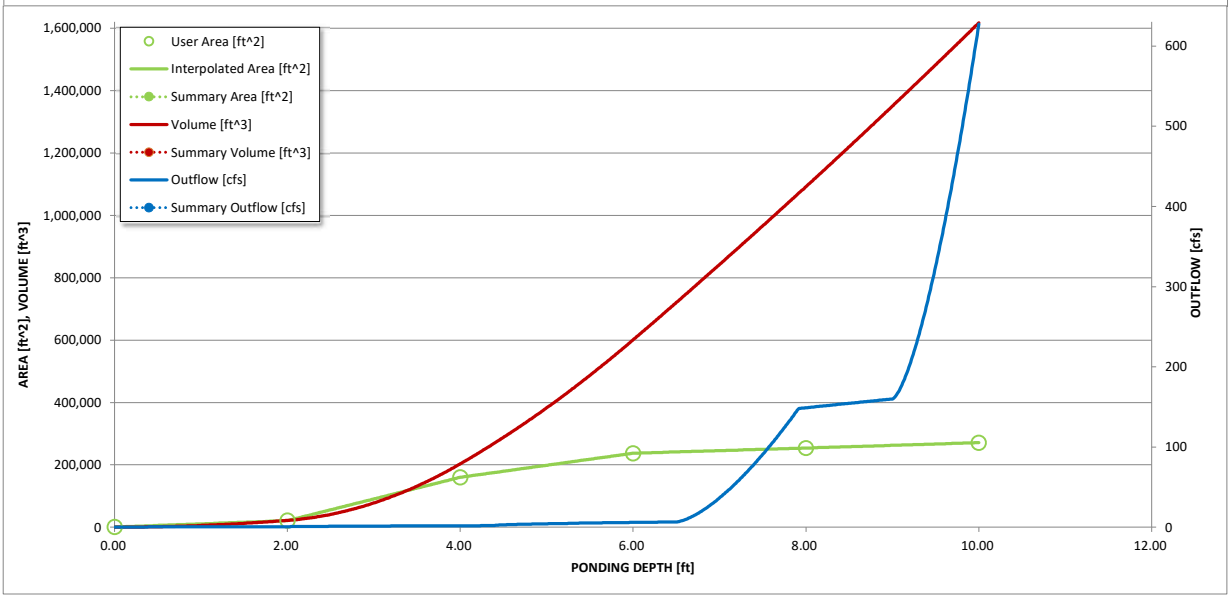
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.48
CUHP Runoff Volume (acre-ft) =	4.822	15.946	14.895	20.580	25.471	31.662	36.887	43.326	64.093
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	14.895	20.580	25.471	31.662	36.887	43.326	64.093
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	18.5	52.4	81.6	150.3	189.1	243.5	396.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.08	0.21	0.33	0.61	0.77	0.99	1.62
Peak Inflow Q (cfs) =	N/A	N/A	195.2	271.3	328.6	431.7	503.6	589.5	863.9
Peak Outflow Q (cfs) =	2.0	6.5	6.0	24.4	59.3	115.4	149.5	157.6	471.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.7	0.8	0.8	0.6	1.2
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.7	1.4	1.8	1.9	2.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	67	66	70	69	67	66	64	59
Time to Drain 99% of Inflow Volume (hours) =	**43**	73	72	77	77	76	75	74	71
Maximum Ponding Depth (ft) =	4.05	6.40	6.02	6.85	7.23	7.69	8.04	8.78	9.76
Area at Maximum Ponding Depth (acres) =	3.72	5.52	5.45	5.61	5.68	5.77	5.84	5.98	6.18
Maximum Volume Stored (acre-ft) =	4.853	15.987	13.901	18.492	20.637	23.214	25.303	29.677	35.637

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.99	0.10	4.86
	0:15:00	0.00	0.00	8.69	14.20	17.60	11.82	15.77	14.51	29.18
	0:20:00	0.00	0.00	39.89	55.39	66.84	42.38	50.75	52.57	84.21
	0:25:00	0.00	0.00	103.42	144.47	179.21	102.69	120.50	130.45	212.27
	0:30:00	0.00	0.00	168.01	235.50	289.50	241.38	283.75	315.50	488.55
	0:35:00	0.00	0.00	195.18	271.34	328.62	377.22	442.14	507.75	757.70
	0:40:00	0.00	0.00	187.80	256.08	307.18	431.68	503.60	589.49	863.89
	0:45:00	0.00	0.00	168.48	228.93	276.42	414.47	481.99	573.59	837.24
	0:50:00	0.00	0.00	148.80	204.51	247.24	383.29	445.38	534.38	778.69
	0:55:00	0.00	0.00	132.19	183.80	222.54	345.40	401.50	487.50	711.22
	1:00:00	0.00	0.00	118.44	164.51	200.27	309.18	359.91	444.29	648.86
	1:05:00	0.00	0.00	105.97	146.47	180.40	274.73	320.27	405.65	592.59
	1:10:00	0.00	0.00	94.32	131.79	164.21	241.61	281.95	359.41	526.37
	1:15:00	0.00	0.00	84.51	120.99	154.30	210.51	246.07	308.77	455.64
	1:20:00	0.00	0.00	76.57	110.96	144.41	185.79	217.36	264.64	392.21
	1:25:00	0.00	0.00	69.78	100.67	130.97	163.98	191.74	226.94	336.19
	1:30:00	0.00	0.00	63.52	90.95	115.79	143.33	167.25	193.51	285.93
	1:35:00	0.00	0.00	57.41	81.74	101.40	123.73	143.95	164.56	242.53
	1:40:00	0.00	0.00	51.33	71.63	88.16	105.39	122.19	137.93	202.88
	1:45:00	0.00	0.00	45.72	61.18	76.56	88.73	102.49	113.75	166.96
	1:50:00	0.00	0.00	41.31	52.27	67.34	73.89	84.98	92.48	135.68
	1:55:00	0.00	0.00	37.51	46.96	61.68	62.23	71.36	75.94	112.15
	2:00:00	0.00	0.00	33.64	43.42	56.89	55.51	63.50	65.90	97.69
	2:05:00	0.00	0.00	28.70	38.02	49.47	47.78	54.55	55.66	82.64
	2:10:00	0.00	0.00	23.34	30.89	40.17	38.31	43.68	43.79	65.06
	2:15:00	0.00	0.00	18.40	24.20	31.58	29.53	33.63	33.09	49.17
	2:20:00	0.00	0.00	14.56	19.06	24.82	23.01	26.15	25.09	37.26
	2:25:00	0.00	0.00	11.42	14.95	19.32	17.78	20.16	18.89	28.02
	2:30:00	0.00	0.00	8.93	11.64	14.91	13.73	15.52	14.35	21.24
	2:35:00	0.00	0.00	6.95	8.91	11.32	10.50	11.84	11.00	16.21
	2:40:00	0.00	0.00	5.38	6.74	8.55	7.95	8.94	8.38	12.31
	2:45:00	0.00	0.00	4.10	5.09	6.52	6.05	6.79	6.45	9.47
	2:50:00	0.00	0.00	3.09	3.83	4.99	4.65	5.21	4.98	7.31
	2:55:00	0.00	0.00	2.23	2.77	3.66	3.46	3.88	3.71	5.42
	3:00:00	0.00	0.00	1.50	1.91	2.54	2.45	2.74	2.62	3.82
	3:05:00	0.00	0.00	0.93	1.25	1.62	1.61	1.80	1.72	2.49
	3:10:00	0.00	0.00	0.50	0.73	0.92	0.95	1.06	1.01	1.45
	3:15:00	0.00	0.00	0.21	0.35	0.42	0.46	0.51	0.48	0.69
	3:20:00	0.00	0.00	0.07	0.11	0.12	0.14	0.16	0.15	0.20
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]

DRAINAGE MAPS

CLASSIC SM
CONSULTING
ENGINEERS & SURVEYORS

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (5yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	1.68	0.00	0.00	1.50	0.18	1.28	105.15	0.106
EX10A	1.68	0.00	0.00	1.53	0.15	0.70	52.19	0.087
EX-11	1.68	0.00	0.00	1.54	0.14	0.80	53.86	0.082
EX-13	1.68	0.00	0.00	1.48	0.20	0.50	35.71	0.117
EX-4A	1.68	0.00	0.00	1.52	0.15	0.18	19.26	0.091
EX-5	1.68	0.00	0.00	1.52	0.16	0.11	11.51	0.093
EX-7	1.68	0.00	0.00	1.52	0.15	0.64	46.80	0.090
EX-9	1.68	0.00	0.00	1.52	0.15	0.73	56.96	0.090
TR-12	1.68	0.00	0.00	1.43	0.25	0.03	1.88	0.148
TR-20	1.68	0.00	0.00	1.45	0.22	0.14	10.01	0.131
TR-4	1.68	0.00	0.00	1.42	0.25	0.03	1.78	0.150
TR-5	1.68	0.00	0.00	1.48	0.20	0.07	4.56	0.116
TR-6	1.68	0.00	0.00	1.38	0.30	0.01	0.83	0.177
TR-7	1.68	0.00	0.00	1.43	0.24	0.02	1.01	0.144

SWMM 5.1 Page 1

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (100 yr. Event)

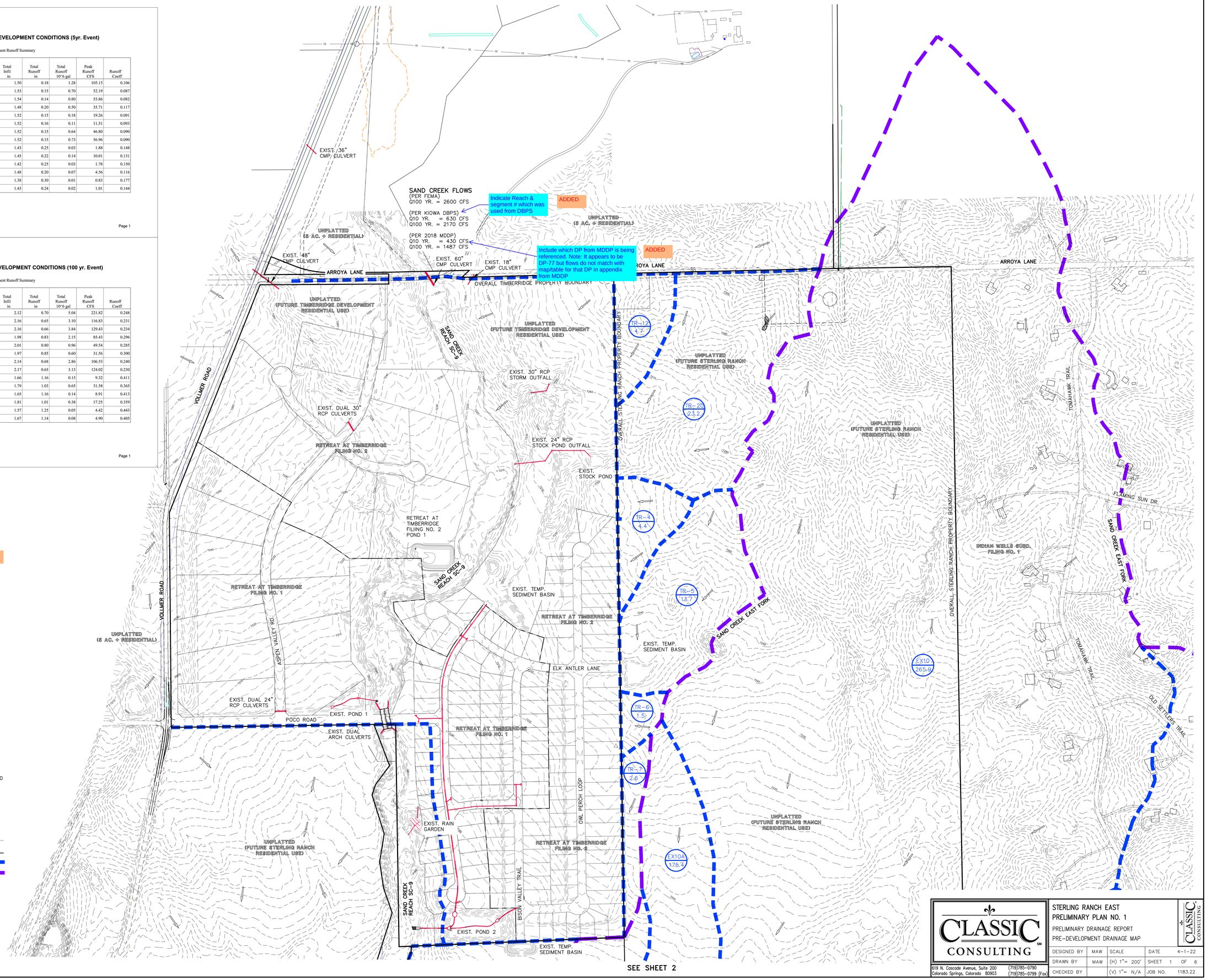
Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	2.82	0.00	0.00	2.12	0.70	5.04	221.82	0.248
EX10A	2.82	0.00	0.00	2.16	0.65	3.10	116.83	0.231
EX-11	2.82	0.00	0.00	2.16	0.66	3.84	129.43	0.234
EX-13	2.82	0.00	0.00	1.98	0.83	2.15	85.43	0.296
EX-4A	2.82	0.00	0.00	2.01	0.80	0.96	49.54	0.285
EX-5	2.82	0.00	0.00	1.97	0.85	0.60	31.56	0.300
EX-7	2.82	0.00	0.00	2.14	0.68	2.86	106.53	0.240
EX-9	2.82	0.00	0.00	2.17	0.65	3.13	124.02	0.230
TR-12	2.82	0.00	0.00	1.66	1.16	0.15	9.32	0.411
TR-20	2.82	0.00	0.00	1.79	1.03	0.65	31.58	0.365
TR-4	2.82	0.00	0.00	1.65	1.16	0.14	8.91	0.413
TR-5	2.82	0.00	0.00	1.81	1.01	0.38	17.25	0.359
TR-6	2.82	0.00	0.00	1.57	1.25	0.05	4.42	0.443
TR-7	2.82	0.00	0.00	1.67	1.14	0.08	4.90	0.405

SWMM 5.1 Page 1

Show all design points/outfalls from hydrology tables on maps. (all sheets) ADDED

Include design point summary table (all sheets) ADDED



200 100 0 200 400

SCALE: 1" = 200'

LEGEND

DESCRIPTION	SYMBOL
EXISTING GROUND CONTOUR	6910
PROPOSED FINISHED CONTOUR	6910
SUB-BASIN BOUNDARY	
SAND CREEK EAST FORK BASIN LINE	
DESIGN POINT	4
BASIN IDENTIFIER / AREA IN ACRES	BB 10.0
EXISTING DIRECTION OF FLOW	
EXISTING STORM SEWER	

CLASSIC CONSULTING
619 N. Cascade Avenue, Suite 200 (719)785-0790
Colorado Springs, Colorado 80903 (719)785-0799 (Fax)

STERLING RANCH EAST
PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
PRE-DEVELOPMENT DRAINAGE MAP

DESIGNED BY	MAW	SCALE		DATE	4-1-22
DRAWN BY	MAW	(H) 1"= 200'		SHEET	1 OF 6
CHECKED BY		(V) 1"= N/A		JOB NO.	1183.22

N:\1183\2\REPORTS\PRELIM DRAINAGE REPORT\1183DP00 HOM2.dwg, 5/25/2022 10:18:29 AM, 1:1

SEE SHEET 1

LEGEND

DESCRIPTION	SYMBOL
EXISTING GROUND CONTOUR	6910
PROPOSED FINISHED CONTOUR	6910
SUB-BASIN BOUNDARY	
SAND CREEK EAST FORK BASIN LINE	
DESIGN POINT	4
BASIN IDENTIFIER / AREA IN ACRES	BB / 10.0
EXISTING DIRECTION OF FLOW	
EXISTING STORM SEWER	

N

200 100 0 200 400

SCALE: 1" = 200'

Road Name

ADDED

SAND CREEK REACH SC-10

BISON VALLEY

EXIST. POND 2

EXIST. TEMP. SEDIMENT BASIN

HOMESTEAD NORTH PLATTED BOUNDARY

(HOMESTEAD NORTH AT STERLING RANCH RESIDENTIAL USE)

CLASSIC OWNERSHIP BOUNDARY

SAND CREEK REACH SC-9

EX-6 26.8

BRIARGATE BLVD. (130' ROW)

REFERENCE SAND CREEK CHANNEL IMPROVEMENTS PROPOSED WITH HOMESTEAD NORTH AT STERLING RANCH FIL.NO. 1 PREPARED BY JR ENG.

UNPLATTED (FUTURE STERLING RANCH RESIDENTIAL USE)

SAND CREEK EAST FORK

EX-7 155.2

EX-9 178.1

EX10A 175.4

EX-11 214.3

EX10 265.9

EX-13 94.8

INDIAN WELLS SUBD. FILING NO. 1

TOMAHAWK TRAIL

STAPLETON ROAD

BOW VALLEY SUBD.

OVERALL STERLING RANCH PROPERTY BOUNDARY

HOMESTEAD AT STERLING RANCH FILING NO. 2

EX-8A 44.6

HOMESTEAD AT STERLING RANCH FILING NO. 1

SAND CREEK REACH SC-8

REFERENCE SAND CREEK CHANNEL IMPROVEMENTS PROPOSED WITH HOMESTEAD NORTH AT STERLING RANCH FIL.NO. 1 PREPARED BY JR ENG.

CLASSIC OWNERSHIP BOUNDARY

BRANDING IRON AT STERLING RANCH FILING NO. 2

STERLING RANCH RD. (80' ROW)

Owner Information

ADDED

Owner Information

ADDED

SEE SHEET 3

N:\1183.22\REPORTS\PRELIM DRAINAGE REPORT\1183.22PDR PDM2.dwg, 5/25/2022 10:17:01 AM, kit

CLASSIC CONSULTING

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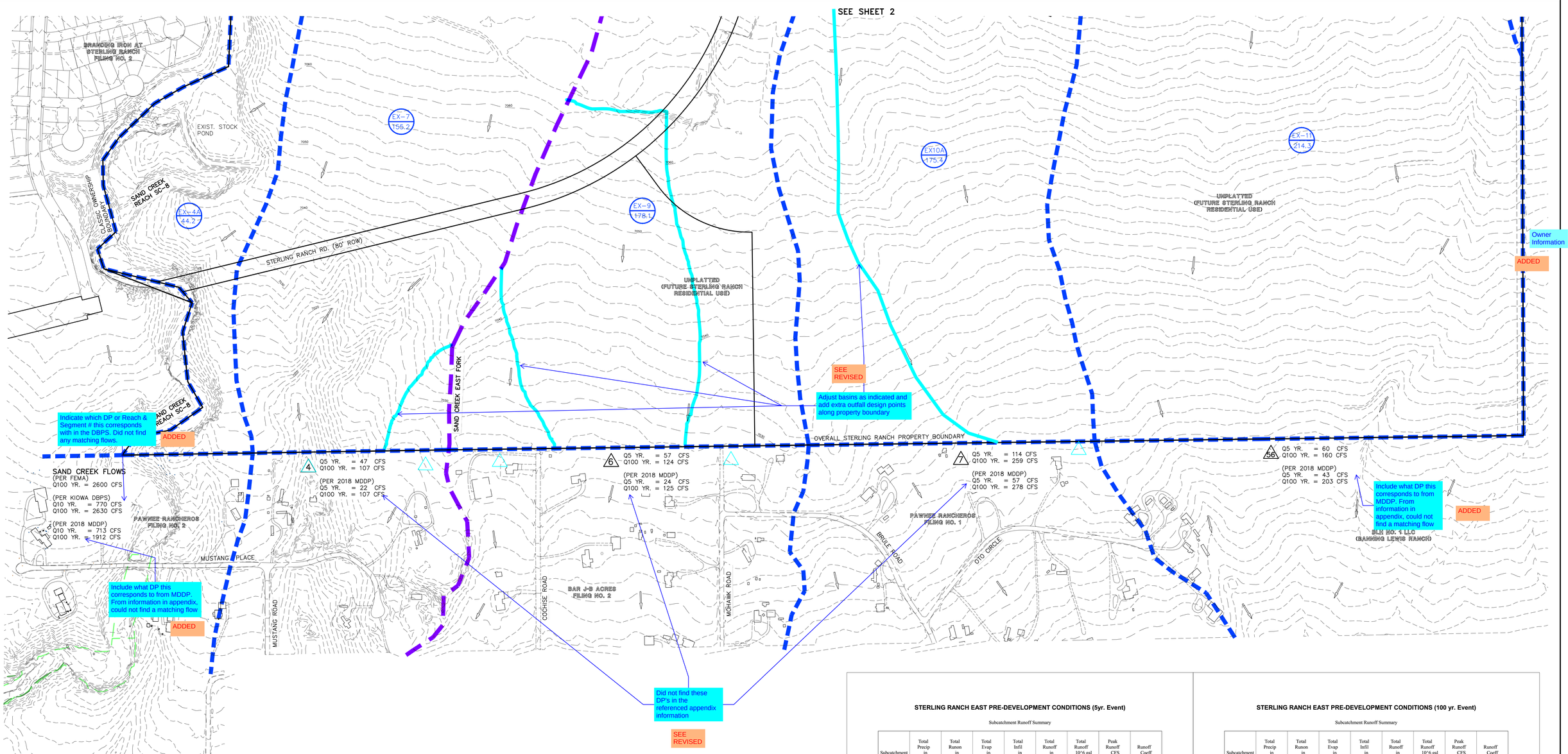
Colorado Springs, Colorado 80903 (719)785-0799 (Fax)

STERLING RANCH EAST
PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
PRE-DEVELOPMENT DRAINAGE MAP

DESIGNED BY	MAW	SCALE	DATE 4-1-22
DRAWN BY	MAW	(H) 1"= 200'	SHEET 2 OF 6
CHECKED BY		(V) 1"= N/A	JOB NO. 1183.22



STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (5yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	1.68	0.00	0.00	1.50	0.18	1.28	105.15	0.106
EX10A	1.68	0.00	0.00	1.53	0.15	0.70	52.19	0.087
EX-11	1.68	0.00	0.00	1.54	0.14	0.80	53.86	0.082
EX-13	1.68	0.00	0.00	1.48	0.20	0.50	35.71	0.117
EX-4A	1.68	0.00	0.00	1.52	0.15	0.18	19.26	0.091
EX-5	1.68	0.00	0.00	1.52	0.16	0.11	11.51	0.093
EX-7	1.68	0.00	0.00	1.52	0.15	0.64	46.80	0.090
EX-9	1.68	0.00	0.00	1.52	0.15	0.73	56.96	0.090
TR-12	1.68	0.00	0.00	1.43	0.25	0.03	1.88	0.148
TR-20	1.68	0.00	0.00	1.45	0.22	0.14	10.01	0.131
TR-4	1.68	0.00	0.00	1.42	0.25	0.03	1.78	0.150
TR-5	1.68	0.00	0.00	1.48	0.20	0.07	4.56	0.116
TR-6	1.68	0.00	0.00	1.38	0.30	0.01	0.83	0.177
TR-7	1.68	0.00	0.00	1.43	0.24	0.02	1.01	0.144

Please provide area in acres also on all tables

ADDED

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (100 yr. Event)

Subcatchment Runoff Summary

Subcatchment	Total Precip in	Total Runon in	Total Evap in	Total Infil in	Total Runoff in	Total Runoff 10^6 gal	Peak Runoff CFS	Runoff Coeff
EX-10	2.82	0.00	0.00	2.12	0.70	5.04	221.82	0.248
EX10A	2.82	0.00	0.00	2.16	0.65	3.10	116.83	0.231
EX-11	2.82	0.00	0.00	2.16	0.66	3.84	129.43	0.234
EX-13	2.82	0.00	0.00	1.98	0.83	2.15	85.43	0.296
EX-4A	2.82	0.00	0.00	2.01	0.80	0.96	49.54	0.285
EX-5	2.82	0.00	0.00	1.97	0.85	0.60	31.56	0.300
EX-7	2.82	0.00	0.00	2.14	0.68	2.86	106.53	0.240
EX-9	2.82	0.00	0.00	2.17	0.65	3.13	124.02	0.230
TR-12	2.82	0.00	0.00	1.66	1.16	0.15	9.32	0.411
TR-20	2.82	0.00	0.00	1.79	1.03	0.65	31.58	0.365
TR-4	2.82	0.00	0.00	1.65	1.16	0.14	8.91	0.413
TR-5	2.82	0.00	0.00	1.81	1.01	0.38	17.25	0.359
TR-6	2.82	0.00	0.00	1.57	1.25	0.05	4.42	0.443
TR-7	2.82	0.00	0.00	1.67	1.14	0.08	4.90	0.405

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (5yr. Event)

Outfall Loading Summary

use Ac-ft unit?

REMOVED

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DP4	91.92	4.30	46.80	0.639
DP56	98.59	8.23	59.57	1.311
DP6	98.59	4.60	56.96	0.733
DP7	98.59	12.48	114.01	1.989
DPEX-4A	61.64	1.84	19.26	0.183
DPEX-5	53.38	1.29	11.51	0.111
Out10	36.27	0.51	1.78	0.030
Out11	34.38	0.22	0.83	0.012
Out6	36.44	0.54	1.88	0.032
Out7	48.80	1.75	10.01	0.138
Out8	41.34	1.09	4.56	0.073
Out9	35.63	0.30	1.01	0.017

STERLING RANCH EAST PRE-DEVELOPMENT CONDITIONS (100 yr. Event)

Outfall Loading Summary

Outfall Node	Flow Freq. Pcnt.	Avg. Flow CFS	Max. Flow CFS	Total Volume 10^6 gal
DP4	92.55	19.10	106.53	2.856
DP56	98.59	37.64	160.10	5.996
DP6	98.59	19.66	124.02	3.131
DP7	98.59	51.21	258.75	8.157
DPEX-4A	62.08	9.61	49.54	0.964
DPEX-5	53.80	6.93	31.56	0.603
Out10	36.62	2.35	8.91	0.139
Out11	34.56	0.91	4.42	0.051
Out6	36.90	2.48	9.32	0.148
Out7	49.14	8.16	31.58	0.648
Out8	42.15	5.53	17.25	0.376
Out9	37.27	1.34	4.90	0.081

LEGEND

DESCRIPTION	SYMBOL
EXISTING GROUND CONTOUR	6910
PROPOSED FINISHED CONTOUR	6910
SUB-BASIN BOUNDARY	
SAND CREEK EAST FORK BASIN LINE	
DESIGN POINT	4
BASIN IDENTIFIER / AREA IN ACRES	BB 10.0
EXISTING DIRECTION OF FLOW	
EXISTING STORM SEWER	

N

200 100 0 200 400

SCALE: 1" = 200'

CLASSIC CONSULTING
619 N. Cascade Avenue, Suite 200 (719)785-0790
Colorado Springs, Colorado 80903 (719)785-0799 (Fax)

STERLING RANCH EAST
PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
PRE-DEVELOPMENT DRAINAGE MAP

DESIGNED BY	MAW	SCALE		DATE	4-1-22
DRAWN BY	MAW	(H) 1"= 200'		SHEET	3 OF 6
CHECKED BY		(V) 1"= N/A		JOB NO.	1183.22

N:\1183.22\REPORTS\PRELIM DRAINAGE REPORT\1183.22PRE HDM2.dwg, 5/25/2022 10:15:42 AM, 1:1

BASIN ID	PEAK FLOWS (CFS) 5YR.	100YR.
(EXISTING BASINS)		
TR-12	2	9
TR-20	10	32
TR-4	2	9
TR-5	5	17
TR-6	1	4
TR-7	1	5
(PROPOSED BASINS)		
TR-V	2	6
TR-W	3	5
P1-F	111	215

Basin label missing from map

TR-7 INCLUDED IN BASIN P1-F SEE REVISED

Show all design points/outfalls from hydrology tables on maps. (all sheets)

ADDED

N

200 100 0 200 400

SCALE: 1" = 200'

LEGEND

DESCRIPTION	SYMBOL
EXISTING GROUND CONTOUR	6910
PROPOSED FINISHED CONTOUR	6910
BASIN BOUNDARY	
EAST FORK BASIN BOUNDARY	
DESIGN POINT	15
BASIN IDENTIFIER / AREA IN ACRES	BB 10.0
EXISTING DIRECTION OF FLOW	
PROPOSED DIRECTION OF FLOW	
PROPOSED STORM SEWER	
PROPOSED STORM SEWER PER JR ENG. PLANS	
PROPOSED POND OUTFALL PER JR ENG. PLANS	

EXIST. 36" CMP CULVERT

SAND CREEK FLOWS
(PER FEMA)
Q100 YR. = 2600 CFS

(PER KIOWA DBPS)
Q10 YR. = 630 CFS
Q100 YR. = 2170 CFS

(PER STERLING MDDP)
Q10 YR. = 430 CFS
Q100 YR. = 1487 CFS

UNPLATTED (5 AC. ± RESIDENTIAL)

EXIST. 48" CMP CULVERT

EXIST. 60" CMP CULVERT

EXIST. 18" CMP CULVERT

ARROYA LANE

OVERALL TIMBERRIDGE PROPERTY BOUNDARY

UNPLATTED (FUTURE TIMBERRIDGE DEVELOPMENT RESIDENTIAL USE)

SAND CREEK REACH SC-9

VOLLMER ROAD

EXIST. DUAL 30" RCP CULVERTS

RETREAT AT TIMBERRIDGE FILING NO. 2

EXIST. 30" RCP STORM OUTFALL

EXIST. 24" RCP STOCK POND OUTFALL

EXIST. STOCK POND

RETREAT AT TIMBERRIDGE FILING NO. 2 POND 1

OVERALL STERLING RANCH PROPERTY BOUNDARY

TR-12 4.2

UNPLATTED (FUTURE STERLING RANCH RESIDENTIAL USE)

TR-20 23.2

Basin label

ADDED

TOMAHAWK TRAIL

FLEMING SUN DR.

TR-4 4.4

TR-4 13.7

UNPLATTED (FUTURE STERLING RANCH RESIDENTIAL USE)

INDIAN WELLS SUBD. FILING NO. 1

RETREAT AT TIMBERRIDGE FILING NO. 1

EXIST. TEMP. SEDIMENT BASIN

RETREAT AT TIMBERRIDGE FILING NO. 2

UNPLATTED (5 AC. ± RESIDENTIAL)

ELK ANTLER LANE

TR-6 1.5

EXIST. DUAL 24" RCP CULVERTS

POCO ROAD

EXIST. DUAL ARCH CULVERTS

RETREAT AT TIMBERRIDGE FILING NO. 1

OWL PERCH LOOP

P1-F 76.7

Basin label

ADDED

EXIST. RAIN GARDEN

UNPLATTED (FUTURE HORSEHEAD NORTH BY STERLING RANCH PLAN/PDL-1 RESIDENTIAL USE)

RETREAT AT TIMBERRIDGE FILING NO. 2

TR-V 2.1

TR-W 1.4

BISON VALLEY TRAIL

SAND CREEK EAST FORK

SAND CREEK REACH SC-9

See Sheet

ADDED

CLASSIC CONSULTING ENGINEERS & SURVEYORS
619 N. Cascade Avenue, Suite 200 (719)785-0790
Colorado Springs, Colorado 80903 (719)785-0799 (Fax)

STERLING RANCH EAST
PRELIMINARY PLAN NO. 1
PRELIMINARY DRAINAGE REPORT
DEVELOPED DRAINAGE MAP

DESIGNED BY	MAW	SCALE		DATE	4-1-22
DRAWN BY	MAW	(H) 1"= 200'		SHEET	4 OF 6
CHECKED BY		(V) 1"= N/A		JOB NO.	1183.22