EL PASO COUNTY, COLORADO

APRIL 2023

Prepared for:

Challenger Communities, LLC Jim Byers 8605 Explorer Drive, Suite 250 Colorado Springs, Colorado, 80920



CIVIL CONSULTANTS, INC.

212 N. Wahsatch Avenue, Suite 305 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-014 PCD Project # PUDSP222

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin.



For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all the requirements specified in this drainage report and plan.

BY:

Jim Byers, VP of Community Development

TITLE: DATE: 04-28-23

ADDRESS: Challenger Communities, LLC 8605 Explorer Drive, Suite 250 Colorado Springs, CO 80920

EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

BY:

DATE:

Josh Palmer, P.E. County Engineer / ECM Administrator

TABLE OF CONTENTS

PURPOSE	4
GENERAL LOCATION AND DESCRIPTION	4
SOILS	4
HYDROLOGIC CALCULATIONS	4
HYDRAULIC CALCULATIONS	5
FLOODPLAIN STATEMENT	5
DRAINAGE CRITERIA	5
EXISTING DRAINAGE CONDITIONS	5
FOUR STEP PROCESS	6
PROPOSED DRAINAGE CHARACTERISTICS	6
EROSION CONTROL	10
CONSTRUCTION COST OPINION	10
DRAINAGE & BRIDGE FEES	11
SUMMARY	11
REFERENCES	12

APPENDIX

Vicinity Map Soils Map FIRM Panel Existing Drainage Conditions Discussion (By Others) Existing Hydrologic Calculations (By Others) Proposed Hydrologic Calculations Existing Hydraulic Calculations (By Others) Proposed Hydraulic Calculations Background Existing Drainage Maps (By Others) Proposed Drainage Map

PURPOSE

This document is the Final Drainage Report for Copper Chase at Sterling Ranch. This site was previously discussed, in the approved "Final Drainage Report for Sterling Ranch Filing No. 2" prepared by JR Engineering, approved November 2021. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual.

GENERAL LOCATION AND DESCRIPTION

Copper Chase at Sterling Ranch is located within the Southeast quarter of Section 32 and within the Southwest quarter of Section 33, Township 12 south, Range 65 West and a portion of the Northeast quarter of Section 5, Township 13, Range 65 West, all west of the 6th Principal Meridian, in unincorporated El Paso County, Colorado. Sterling Ranch Filing No. 2 infrastructure encompasses the boundary of the site. The site is bound to the north by under-construction Vollmer Road, Alzada Drive, and Bynum Drive. The site is bound to the southwest by existing Marksheffel Road and to the southeast by existing Sterling Ranch Road. Copper Chase at Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Copper Chase at Sterling Ranch consists of 19.65 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to southeast at grade rates that vary between 1.9% and 4.4%.

Copper Chase at Sterling Ranch is currently zoned RS-5000 for Residential Sub-Urban and is proposed to be PUD, or Planned Unit Development. Improvements proposed for the site include paved streets, utilities, and storm drainage improvements, as normally constructed for a planned unit development.

SOILS

Soils for this project are delineated by the map in the appendix as Blakeland Loamy Sand (8) and Columbine Gravelly Sandy Loam (19). Both are characterized as Hydrologic Soil Types "A". Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". Due to recent bulk grading activities, vegetation is sparse, consisting of native grasses and weeds.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0533 G, effective date December 7th, 2018.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current El Paso County Drainage Criteria Manual, Volumes I & II, dated October 31, 2018, City of Colorado Springs Drainage Criteria Manual, Volumes I & II, dated May 2014, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), Adopted January 2015). In addition to the ECM, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates). Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method.

EXISTING DRAINAGE CONDITIONS

The Copper Chase at Sterling Ranch site consists of 19.65 acres and is situated west of the Sand Creek Channel. This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the "Final Drainage Report for Sterling Ranch Filing No. 2" prepared by JR Engineering, LLC, approved November 2021 (henceforth referred to as "Sterling Ranch Filing No. 2 FDR"), and "Master Development Drainage Report for Sterling Ranch Filing Nos. 1 & 2", prepared by M&S Civil Consultants, dated December 2017. Copper Chase at Sterling Ranch and portions of the surrounding areas (with the exception of the existing Barbarick Subdivision), have already been bulk graded (refer to Sterling Ranch Filing No. 2: Grading, Erosion, and Stormwater Quality Control Plan, dated March 2018). Offsite flows in this condition are diverted by the exterior roadways and do not enter the site. Refer to the Final Drainage Report for Sterling Ranch Filing No 2 by JR Engineering, LLC for information on historic conditions and overlot drainage patterns and analysis. The existing condition discussion, calculations, and maps for this site come directly from the proposed condition discussion, calculations, and maps within the Sterling Ranch Filing No. 2 FDR. Supporting text, calculation, and map excerpts for the existing conditions can be found in the appendix under the following sections: "Existing Drainage Conditions Discussion", "Existing Hydrologic Calculations", "Existing Hydraulic Calculations", "Background", and "Existing Drainage Maps".

FOUR STEP PROCESS

Step 1 Employ Runoff Reduction Practices - Roof drains will be directed to side yard swales and, whenever possible, to grass lined swales to aid in minimizing direct connection of impervious surfaces. Residential lots are proposed to include open spaces and lawn areas, which helps minimize directly connected impervious areas and therefore reduces runoff volumes.

Step 2 Treat And Slowly Release the WQCV (Stabilize Drainageways) –at rates less than predevelopment conditions. With the offsite, sub-regional, full spectrum detention facility (Pond W-5) in place, the runoff from the proposed planned unit development and other areas of Sterling Ranch developments (see Pond W-5 tributary area in Appendix) will be treated and reduced to predevelopment conditions. The developed discharge from the site is not anticipated to have negative effects on downstream drainageways.

Step 3 Stabilize Stream Channels Provide Water Quality Capture Volume (WQCV) - An existing Full Spectrum Detention Facility was planned and constructed to handle tributary flows for this site (see Sterling Ranch Filing No 2 FDR with PCD Filing No. SF1820, Pond W-5) which will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours. Channel stabilization has been provided at the outlet of the aforementioned pond.

Step 4 Consider Need for Selecting Industrial and Commercial BMP's – A Stormwater Management Plan will be implemented which will include property housekeeping practices, spill containment procedures, and coverage of storage/handling areas to mitigate the potential for erosion across the site and protect downstream waters. Specialized BMP's are not required since there aren't commercial/industrial areas being implemented with this project.

PROPOSED DRAINAGE CHARACTERISTICS

General Concept Drainage Discussion

The following is a description of the onsite basins, offsite flows and the overall drainage characteristics for the development of Copper Chase at Sterling Ranch. The development of Copper Chase at Sterling Ranch consists of paved streets, parking, and lots typical of a Planned Unit Development (PUD). Surface runoff is routed via roof drains and side lot swales between the lots to either the back or front of the lots. Surface runoff from the back of the lots and open spaces is directed by swales to low points within area drainage basins. Surface runoff directed to the front of the lots is conveyed within the streets to proposed CDOT Type R at-grade inlets or to low points equipped with proposed CDOT Type R sump inlets. In the event of clogging or inlet failure at low points, emergency overflow routes have been designed to convey runoff to either a downstream inlet, existing Bynum Drive, or Sterling Ranch Road (see the Proposed Drainage Map for emergency overflow arrows and general drainage patterns). Runoff captured by area drainage inlets or CDOT Type R inlets is conveyed underground by a proposed private storm sewer system to the southern corner of the parcel. Ultimately, the proposed storm sewer system ties into an existing Type I manhole within the right of way of Sterling Ranch Road. All existing storm drainage improvements within Sterling Ranch Road are being constructed with the Sterling Ranch Filing No. 2 infrastructure. Ultimately, runoff from the proposed development is conveyed to existing Sterling ranch Pond W-5, a subregional Full spectrum Detention Facility constructed along the southern boundary of Sterling Ranch. (Refer to Pond W4 & W5 Tributary Area Exhibit by JR Engineering, included in the Background section of the Appendix). A final analysis of Pond W-5 will be included with the final plat submittal.

The following detailed drainage discussion provides an overview of the proposed development and ensures that no major modification of the proposed improvements is necessary due to the assumptions meeting that of the previously submitted Final Drainage Report for Sterling Ranch Filing No 2. Surface flow is designated as Design Points (DP). Captured flow within the storm sewer system is designated as Pipe Runs (PR). Flow bypassing the inlets is designated as flowby (FB).

Detailed Drainage Discussion (Design Points)

Design Point 1 (Q5=4.4 cfs, Q100=11.8 cfs)

Basin A consists of 3.59 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=4.4 and Q100=11.8 cfs) flows from north to south through the lots and onto Blue Feather Loop, a public roadway. The flow is conveyed to the southwest within the curb and gutter to a proposed 5' atgrade CDOT Type R inlet (IN-1, Q5=2.5 and Q100=3.8 cfs) where a portion enters PR1, a proposed private 18" RCP storm sewer. Flowby bypassing this inlet (Q5=1.9 cfs, Q100=8.0 cfs) continues to downstream infrastructure.

Design Point 2 (Q5=4.9 cfs, Q100=11.4 cfs)

Basin B consists of 3.40 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=4.9 and Q100=11.4 cfs) flows from the lots and onto Blue Feather Loop and Lost Trail Drive (two public roadways). The flow is conveyed within the streets via curb and gutter to a proposed 15' at-grade CDOT Type R inlet (IN-2, Q5=4.9 and Q100=9.7 cfs) where it enters PR2, a proposed private 18" RCP storm sewer. PR1 and PR2 join flows and are directed southeast within PR3, an 18" RCP private storm sewer. Flowby bypassing this inlet (Q5=0.0 cfs, Q100=1.7 cfs) continues to downstream infrastructure.

Design Point 3 (Q5=3.7 cfs, Q100=11.8 cfs)

Basin C consists of 1.02 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=1.8 and Q100=3.9 cfs) flows from the lots and onto Blue Feather Loop, a public roadway. The flow is conveyed southeast in the curb and gutter, combining with **FB-IN1**, to a proposed 5' at-grade CDOT Type R inlet (**IN-3**, **Q5=2.3 and Q100=3.9 cfs**). Intercepted flow enters **PR4**, a proposed private 18" RCP storm sewer. Flowby bypassing this inlet (Q5=1.4 cfs, Q100=7.9 cfs) continues to downstream infrastructure.

Design Point 4 (Q5=4.7 cfs, Q100=12.0 cfs)

Basin D consists of 2.90 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=4.8 and Q100=10.5 cfs) flows from the lots and onto Salt Fork Drive, a public roadway. The flow is conveyed southeast in the curb and gutter, combining with **FB-IN2**, to a proposed 15' at-grade CDOT Type R inlet (**IN-4**, **Q5=4.7 and Q100=10.0 cfs**). Intercepted flow enters **PR5**, a proposed private 18" RCP storm sewer. **PR3**, **PR4**, and **PR5** join flows and continue southeast in **PR12**, a proposed 24" RCP private storm sewer. Flowby bypassing this inlet (Q5=0.0 cfs, Q100= 2.0 cfs) continues to downstream infrastructure.

Design Point 5 (Q5=1.8 cfs, Q100=5.6 cfs)

Basin E consists of 0.89 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=2.1 and Q100=4.2 cfs) flows from north to south through the lots and onto Blue Feather Loop, a public roadway. The flow is conveyed southeast in the curb and gutter, combining with **FB-IN4**, to a proposed 15' sump CDOT Type R at **Design Point 9**.

Design Point 6 (Q5=4.2 cfs, Q100=10.0 cfs)

Basin F consists of 2.58 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=4.2 and Q100=10.0 cfs) flows from the lots and onto Blue Feather Loop, a public roadway. The flow is conveyed southeast in the curb and gutter to a proposed 15' at-grade CDOT Type R inlet (**IN-6**, **Q5=4.2 and Q100=8.9 cfs**) where it enters **PR6** to **PR9**, a proposed private 18" RCP storm sewer segment. Flowby bypassing this inlet (Q5=0.0 cfs, Q100=1.1 cfs) continues east to downstream infrastructure located offsite on Bynum Drive.

Design Point 7 (Q5=4.9 cfs, Q100=20.0 cfs)

Basin G consists of 1.65 acres of paved roadway and residential lots. Runoff produced within this basin (Q5=4.3 and Q100=8.7 cfs) flows to the curb and gutter of Bynum Drive, a public roadway, and combines with **FB-IN6**, **FB-INA1**, **FB-INA4**, and **FB-INA3** for peak rates of Q5=4.9 and Q100=20.0 cfs in the 5 and 100 year events, respectively. A portion of the flow is then captured by an existing 15' at-grade CDOT Type R inlet (**IN-A5**, **Q5=4.9 and Q100=13.3 cfs**) where it enters **1.3A**, an existing public 30" RCP storm sewer. A manhole redirects the flow south into **1.3**, a public 36" RCP storm sewer. Flowby bypassing this inlet (Q5=0.0 cfs, Q100=6.7 cfs) continues to downstream infrastructure located on existing Sterling Ranch Road.

Design Point 8 (Q5= 1.0 cfs, Q100=3.9 cfs)

Basin H consists of 1.22 acres of residential lots, open space, and landscaping. Runoff produced within this basin (Q5=1.0 and Q100=3.9 cfs) flows from north to south through the lots, entering a proposed triangular, earthen swale. This 2' deep swale with 3:1 side slopes directs the flow southeast, where it enters a proposed 3' CDOT Type C at grade area inlet (IN-8, Q5=1.0 and Q100=3.9 cfs) at its end. Design calculations for this swale shall be provided with the Final Drainage Report and Final Plat submittal. **PR10**, a proposed 18" RCP private storm sewer directs intercepted flows south. In the case of inlet failure or clogging, the inundated area will overflow southeast onto Blue Feather Loop and be conveyed to the sump inlet (IN-5) at DP 9. A weir-orifice analysis for this grate is provided in the Appendix.

Design Point 9 (Q5=4.0 cfs, Q100=10.5 cfs)

Basin I consists of 1.40 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=2.4 and Q100=5.2 cfs) drains from northwest to southeast to the curb and gutter of Salt Fork Drive, a public roadway, combining with surface flows from **Design Point 5** at peak rates of 4.0 and 10.5 cfs in the 5 and 100 year events, respectively. The flow is then captured by proposed 15' sump CDOT Type R inlet (**IN-5, Q5=4.0 and Q100=10.5 cfs**). Intercepted flows enter **PR11**, a proposed private 24'' RCP storm sewer. In the case of inlet failure or clogging, flows would overtop the crown of the road, enter **IN-9**, then overtop the curb and gutter to flow through Tract E.

Design Point 10 (Q5=2.2 cfs, Q100=4.3 cfs)

Basin J consists of 0.89 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=2.2 and Q100=4.3 cfs) drains to the curb and gutter of Blue Feather Loop, a public roadway. The flow is then directed south and captured by proposed 15' sump CDOT Type R inlet at **Design Point 11**.

Design Point 11 (Q5=5.4 cfs, Q100=16.7 cfs)

Basin K consists of 1.07 acres of residential lots and paved roadway. Runoff produced within this basin (Q5=1.9 and Q100=4.2 cfs) drains from west to east to the curb and gutter of Blue Feather Loop. The flow is conveyed in the curb and gutter where it combines with flows from **Design Point 10** and **FB-IN3** and is captured by proposed 15' sump CDOT Type R inlet (**IN-9**, **Q5=5.4** and **Q100=16.7** cfs). Intercepted flow enters **PR13**, a proposed private 30" RCP storm sewer where flows from **PR9** and **PR12** combine at a Type I junction manhole. Flows continue south in **PR14**, a proposed 42" RCP private storm sewer that ties into the existing 42" RCP storm sewer (private) and Type I manhole in the right of way of Sterling Ranch Road (**PR14**: Q5=26.0, Q100=60.5 cfs). Flows anticipated in the FDR for Sterling Ranch Filing No. 2 by JR Engineering at this pipe location are Q5=27.5 cfs and Q100=60.6 cfs.

Design Point 12 (Q5=1.1 cfs, Q100=3.3 cfs)

Basin L consists of 1.21 acres of residential lots and open space at the rear of the lots. Runoff produced within this basin (Q5=1.1 and Q100=3.3 cfs) drains to the curb and gutter of Bynum Drive and Sterling Ranch Road, public roadways. The flow is then directed southeast and is captured by an existing 15' CDOT Type R at grade inlet (**IN-A8**) at **Design Point 15** and enters **1.5**, a public 48" RCP storm sewer.

Design Point 13 (Q5=0.3 cfs, Q100=1.6 cfs)

Basin M consists of 0.64 acres of residential lots and open space. Runoff produced within this basin (Q5=0.3 and Q100=1.6 cfs) drains to the curb and gutter of Sterling Ranch Road, an under-construction public roadway. The flow is then directed southeast and is captured by existing 15' CDOT Type R at grade inlet (IN-A11) on Marksheffel Road.

Design Point 14 (Q5=3.0 cfs, Q100=5.4 cfs)

Basin A4 consists of 0.64 acres of public roadway (Alzada Drive). Runoff produced within this basin (Q5=3.0 and Q100=5.4 cfs) drains from northwest to southeast to an existing 10' CDOT Type R at grade inlet (**IN-A4: Q5=3.0, Q100=4.8 cfs**). Flow bypassing this inlet (Q5=0.0 cfs, Q100=0.6 cfs) continues to downstream infrastructure.

Design Point 15 (Q5=5.1 cfs, Q100=19.8 cfs)

Basin A8 consists of 0.75 acres of public roadway. Runoff produced within this basin (Q5=3.0 and Q100=5.5 cfs) drains within the curb and gutter of Sterling Ranch Road, combining with **FB-INA6**, **FB-INA15**, **DP 12**, and **FB-INA5**. **Basin A6** consists of 1.37 acres of public roadway and existing residential lots. A majority of the flow is intercepted by a 15' CDOT Type R inlet (**IN-A6**: Q5=3.3, Q100=5.4 cfs) and enter the system through a 24" RCP public storm sewer, discharging into **1.3A**. 100 yr flowby of 1.3 cfs bypasses the inlet and is intercepted by downstream infrastructure at **Design Point 15**. **Basin A6A** consists of 0.53 acres of area with a similar imperviousness to commercial areas. Runoff from this basin (Q5=2.2, Q100=4.1 cfs) drains to the curb and gutter of Sterling Ranch Road and combines with the aforementioned flows at peak rates of Q5=5.1 and Q100=19.8 cfs in the 5 and 100 year events, respectively. Runoff is collected in an existing 15' CDOT Type R at grade inlet (**IN-A8: Q5=5.1, Q100=13.6 cfs**). JR Engineering anticipated surface flows of Q5=3.0 cfs, and Q100=12.5 cfs, and intercepted and pipe flows of Q5=3.0 cfs, and Q100=10.6 cfs. Flow bypassing this inlet (Q5=0.0 cfs, Q100=6.2 cfs) continues to downstream infrastructure.

Design Point 16 (Q5=7.7 cfs, Q100=22.8 cfs)

Basin A11 consists of 2.79 acres of public roadway and landscaped right of way of Marksheffel Road. Runoff produced within this basin (Q5=7.4 and Q100=14.2 cfs) drains from northwest to southeast in the curb and gutter combining with **DP13**, **FB-INA8** and **FB-INA9** at peak rates of Q5=7.7 and Q100=20.5 cfs in the 5 and 100 year events, respectively. Runoff is collected at the existing 15' CDOT Type R at grade inlet (**IN-A11: Q5=7.6, Q100=14.7 cfs**). JR Engineering anticipated surface flows of Q5=9.5 cfs and Q100=18.1 cfs at this location, and intercepted flows of Q5=8.9 cfs and Q100=13.8 cfs. Intercepted flow enters pipe run **1.7**, and combines with flows from **1.6** in **1.8** at peak rates of Q5=60.8 cfs and Q100=124.8 cfs. Pipe flows of Q5=68.8 cfs and Q100=125.0 cfs were originally anticipated. Flows bypassing the inlet (Q5=0.1 cfs, Q100=8.1 cfs) continue to downstream infrastructure. Flows previously anticipated by this inlet prior to Copper Chase development by JR Engineering were Q5=0.6 cfs & Q100=6.1 cfs, representing a 33% increase. Downstream pipe sizes are greater than 54" past this point (up to 78" prior to discharging into Pond W-5). Based on JR's 125.0 cfs, 100 yr design flow of **1.8**, the increase in bypassed flows represents a 1.6% downstream increase. This increase has been determined to be well within the ~5% human error potentially introduced into the calculations along with other conservative factors built in to the equations. The calculated HGL by JR at the manhole tie in location is 6982.33', and is located 5.83' below finished grade. As such, the downstream facilities leading to Pond W-5 are anticipated to accommodate the additional bypass. A conveyance exhibit is provided for reference from JR's report in the Drainage Map section of the Appendix.

EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. Bulk grading was completed with approval of "Sterling Ranch Filing No. 2: Grading, Erosion, and Stormwater Quality Plan", dated March 2018. Grading and Erosion control operations are currently finished. A Grading and Erosion Control plan for the proposed development is being concurrently submitted with this report.

CONSTRUCTION COST OPINION – COPPER CHASE AT STERLING RANCH

Constructi	on Cost I	Estima	te (Non-Rein	ibursa	ble)
Item	Amount	Unit	Unit Cost		Total Cost
5' CDOT Type R Inlet	2	EA	\$ 6,500.00	\$	13,000.00
15' CDOT Type R Inlet	5	EA	\$ 13,000.00	\$	65,000.00
Type I MH	1	EA	\$ 9,800.00	\$	9,800.00
Type II MH	5	EA	\$ 6,000.00	\$	30,000.00
3' CDOT Type C Inlet	1	EA	\$ 5,000.00	\$	5,000.00
18" RCP	905	LF	\$ 45.00	\$	40,725.00
24" RCP	443	LF	\$ 81.00	\$	35,883.00
30" RCP	20	LF	\$ 100.00	\$	2,000.00
42" RCP	37	LF	\$ 166.00	\$	6,142.00
Tot	al Cost:			\$	207,550.00

Drainage Facilities:

DRAINAGE & BRIDGE FEES - COPPER CHASE AT STERLING RANCH

Use 2023 fees

This site is within the Sand Creek Drainage Basin. The 2022 Drainage and Bridge Fees per El Paso County for the Copper Chase at Sterling Ranch site are as follows:

Per Copper Chase at	Sterling Ra	nch S	Site Boundary –	Total Area	= 19.651 A	Acre	8
COPPER CHASE	AT STERL	ING	RANCH FEES	5:			
Drainage Fees:	19.651	х	58.7%	\$21,814	=	\$	251,627.48
Bridge Fees:	19.651	х	58.7%	\$8,923	=	\$	102,928.03
					Total	\$	354,555.51

It should be noted that these fees are provided in this Final Drainage Report for informational purposes only.

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2022.

SUMMARY

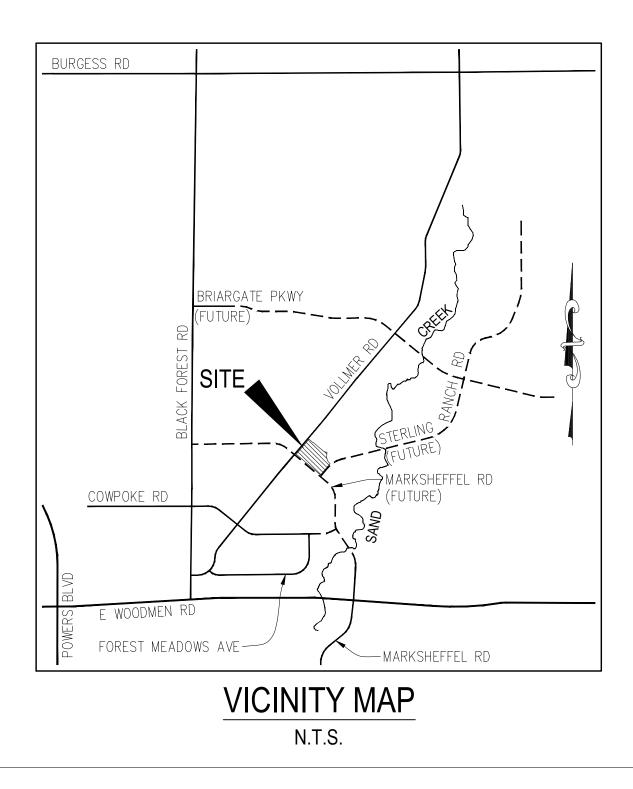
Development of this site will not adversely affect the surrounding developments per this final drainage report with no negative impacts to the neighboring developments. The proposed and existing drainage facilities will adequately convey, detain, and route runoff from tributary and onsite flows to the Sand Creek Drainage channel via proposed onsite and existing offsite drainage improvements. Full Spectrum Detention and Water Quality Ponds will be used to discharge developed flows into Sand Creek per the Urban Drainage criteria flow rates. Sterling Ranch Metropolitan District No. 1 will own and maintain the private facilities. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. The development of the Copper Chase at Sterling Ranch project shall not adversely affect adjacent or downstream property.

REFERENCES

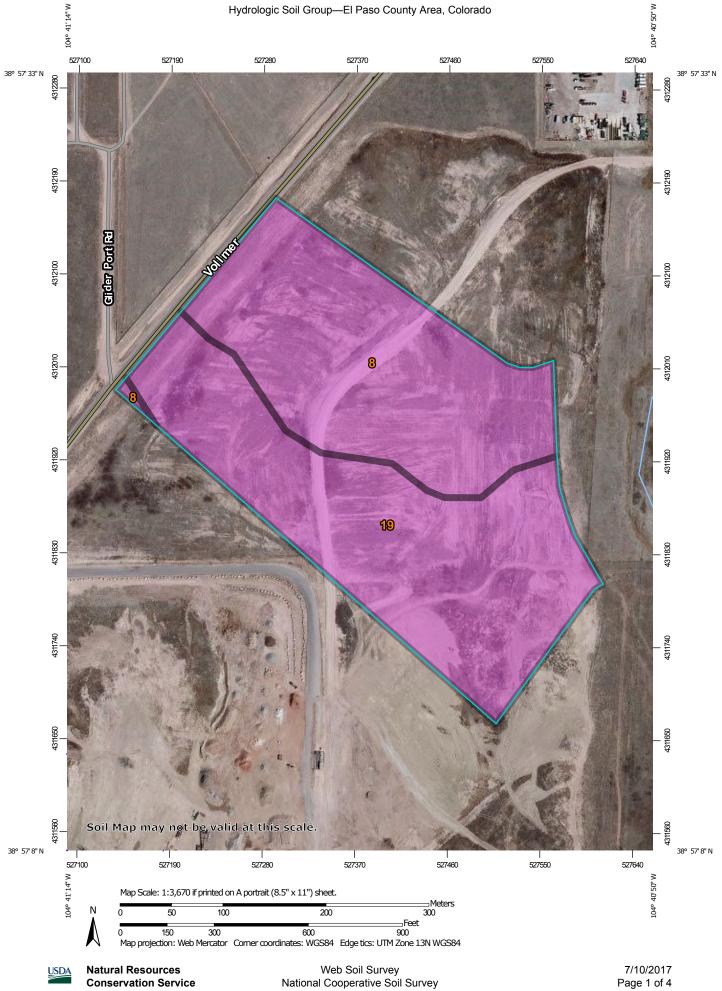
- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2.) "Urban Storm Drainage Criteria Manuals, Volumes 1-3".
- NRSC Web Soil Survey Map for El Paso County. <u>http://websoilsurvey.nrcs.usda.gov</u>. Accessed September 29th, 2020.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date December 7th, 2018. Accessed October 4th, 2021.
- 5.) "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996
- 6.) "Final Drainage Report for Sterling Ranch Filing No. 2", dated November 2021, by JR Engineering
- 7.) "Master Development Drainage Plan for Sterling Ranch", (MDDP) prepared by M&S Civil Consultants, Inc., dated December 2017.

APPENDIX

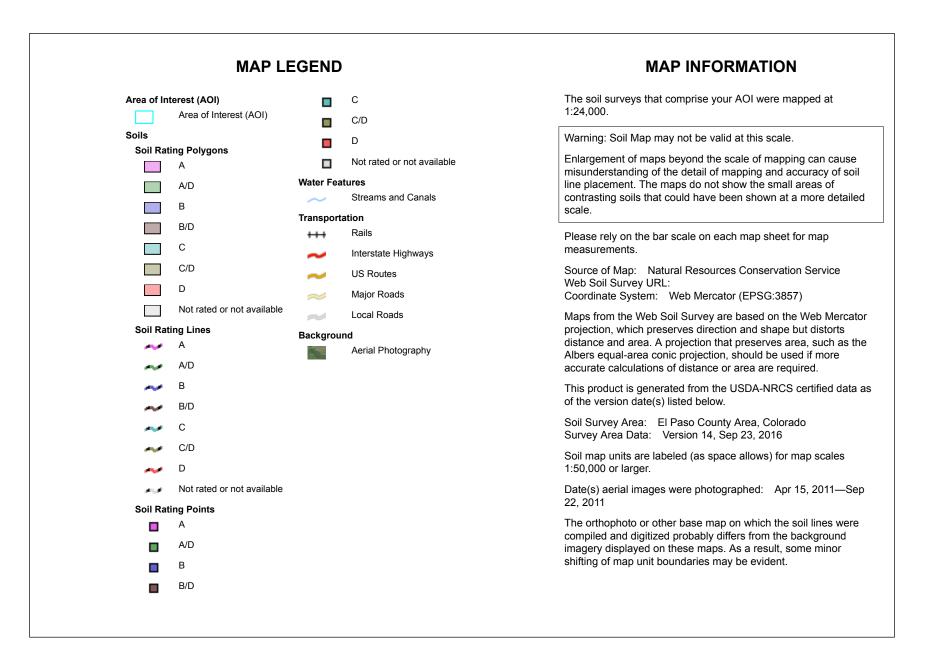
VICINITY MAP



SOILS MAP



Conservation Service



Hydrologic Soil Group

Hydrol	ogic Soil Group— Summa	ry by Map Unit — El Pas	o County Area, Colorado ((CO625)
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	13.7	46.4%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	15.8	53.6%
Totals for Area of Inter	est		29.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

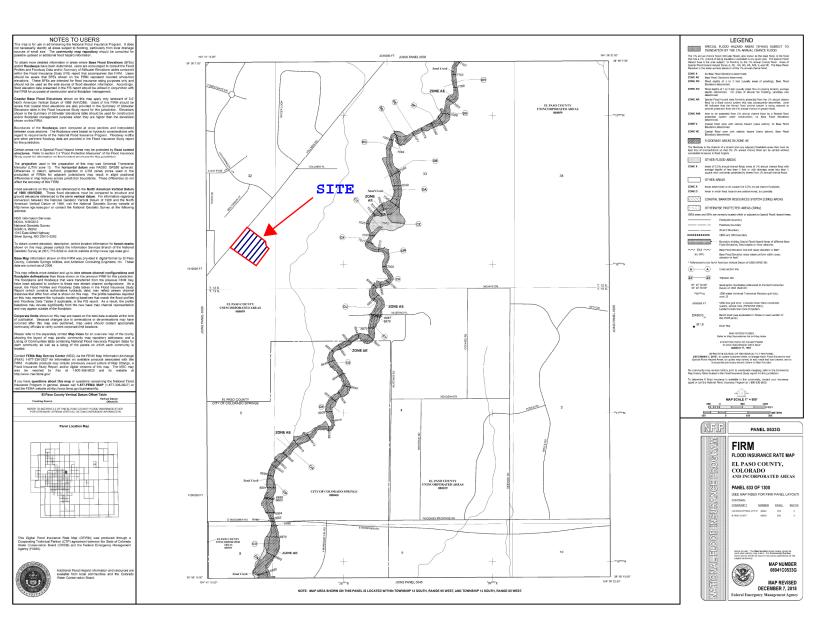
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



FIRM PANEL



EXISITNG DRAINAGE CONDITIONS DISCUSSION (BY J.R. ENGINEERING, APPROVED NOVEMBER 2021)

Final Drainage Report Sterling Ranch Filing No. 2

Basin A consists of Sub-Basins A1-A22 combining for a total of 123.19 acres. This basin represents all 49.5387 acres of the proposed Sterling Ranch Filing 2 development. This basin is primarily single-family residential, roadway and minor open space. This basin also contains future commercial sites, the future Sterling Ranch Phase 2 development, the proposed Copper Chase at Sterling Ranch Development and a proposed school site. Stormwater runoff is conveyed via public streets where it is captured via a series of on-grade and sump inlets. Runoff is then piped to a proposed onsite Full Spectrum Detention Pond W5. From the detention pond, the treated flows are then released directly into the Sand Creek Drainageway at below historic rates.

Off-Site Conveyance

The existing drainage patterns on the west side of Vollmer Road will not change due to the development of Sterling Ranch. Vollmer Road construction will address the roadside ditch flows along the west side of the road and will install drainage culverts where indicated in this report. The majority of the flows from the west side of Vollmer Road are to be routed in the historical direction to the southwest along the roadway to proposed Pond W-4. Runoff produced from the remaining offsite watershed located along the west edge of the existing development will be routed along the west side of Vollmer Road to the southwest corner of the existing development and a proposed Pond W-4. At the northwest corner of Tahiti Drive and Vollmer Road a 54" RCP will be installed to collect and convey runoff under proposed Marksheffel Road before ultimately discharging into Sand Creek. Runoff reaching the development along the south boundary line of the Barbarick Subdivision will be conveyed through and around the proposed site by proposed temporary swales and proposed storm sewer until it ultimately reaches Pond W-5. At the time of final for Sterling Ranch Filing No. 2 Phase 2, JR will coordinate with Barbarick to determine a more specific design solution for conveying the flows from their site. In general, the sand filter and double barrel 24" RCP will discharge onto the Sterling Ranch Phase 2 site where it will be picked up in a sump inlet structure and conveyed through a 48" RCP through the Sterling Ranch Storm system to Pond W5. The eastern Barbarick EDB discharge pipe will be connected into a structure and into a 36" RCP where the flows will be routed to Pond W5. Specific design details can be found within the Sterling Ranch Phase 2 drainage report. Runoff reaching the northern boundary of Phase I at proposed Briargate Parkway will be redirected around the site via a temporary swale to Sand Creek. BMP's will be installed to prevent erosion of the temporary swale. The intention of the drainage design for Sterling Ranch is to not adversely affect any adjacent property within the developed flows from Sterling Ranch.

Sub-basin A1 (Q_5 =4.4 cfs, Q_{100} =9.4 cfs) consists of approximately 2.06 acres and is the northern most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 10' on-grade inlet at DP 1. From here, the flow is piped to Pond W5.

Sub-basin A2 ($Q_5=1.9$ cfs, $Q_{100}=3.9$ cfs) consists of approximately 0.82 acres and is the north eastern most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily singlefamily residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 10' Type R on-grade inlet at DP 2. From here, the flow is piped to Pond W5.

Final Drainage Report Sterling Ranch Filing No. 2

Sub-basin A3 ($Q_5=11.1$ cfs, $Q_{100}=24.7$ cfs) consists of approximately 6.76 acres and is the north western most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type-R on-grade inlet at DP 3. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1 & A2.

Sub-basin A4 ($Q_5=3.7$ cfs, $Q_{100}=7.4$ cfs) consists of approximately 1.51 acres and is the southern portion of Alzada Drive and this basin is primarily single-family residential(Copper Chase at Sterling Ranch) and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 10' Type-R on-grade inlet at DP 4. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A3.

Sub-basin A5 (Q_5 =4.1 cfs, Q_{100} =8.3 cfs) consists of approximately 1.70 acres and is the western portion of Bynum Drive. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 5. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A4.

Sub-basin A6A ($Q_5=2.2$ cfs, $Q_{100}=4.1$ cfs) consists of approximately 0.53 acres. This basin will serve as a tract including mail kiosks, parking, landscaping and sidewalks. Runoff from this sub-basin will sheet flow to DP 6A where it flows via curb and gutter to the 15' Type R inlet at DP6. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A5.

Sub-basin A6 ($Q_5=3.3$ cfs, $Q_{100}=6.6$ cfs) consists of approximately 1.37 acres and is the eastern portion of Bynum Drive. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R inlet on-grade inlet at DP 6. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A6A.

Sub-basin A7 ($Q_5=27.5$ cfs, $Q_{100}=60.6$ cfs) represents the future Copper Chase at Sterling Ranch development and consists of approximately 19.00 acres. This basin is primarily single-family residential and open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 36" RCP storm sewer stub at DP 7 with sediment control structure. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A6. Prior to being developed, storm runoff from this sub-basin will overland flow to temporary swales, where the flows will be captured by an interim 36" FES and piped to Pond W5.

Sub-basin A8 ($Q_5=3.0$ cfs, $Q_{100}=6.3$ cfs) consists of approximately 1.48 acres and is the south western portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 8. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A7.

Sub-basin A9 ($Q_5=1.9$ cfs, $Q_{100}=3.7$ cfs) consists of approximately 0.61 acres and is the south eastern portion of Sterling Ranch Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 9. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A8.

Final Drainage Report Sterling Ranch Filing No. 2

Sub-basin A10 ($Q_5=9.2$ cfs, $Q_{100}=17.3$ cfs) consists of approximately 2.61 acres and is the south eastern portion of Marksheffel Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 10. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A9.

Sub-basin A11 ($Q_5=9.5$ cfs, $Q_{100}=18.1$ cfs) consists of approximately 2.89 acres and is the north portion of Marksheffel Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 11. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A10.

Sub-basin A12 ($Q_5=1.9$ cfs, $Q_{100}=9.5$ cfs) consists of approximately 3.87 acres and represents the open space area between the Sterling Ranch Filing No. 2 Phases 1 & 2 developments. This basin is primarily open space. This basin also contains a 50' and 30' gas easement that contain 3 major gas lines. Runoff from this sub-basin will be conveyed via sheet flow and earthen swale to an area inlet at DP 12. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A11.

Sub-basin A13 ($Q_5=15.7$ cfs, $Q_{100}=34.6$ cfs) consists of approximately 9.65 acres and is the northern portion of the future Sterling Ranch Phase 2 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be captured by a storm sewer stub at DP 13. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A12. Prior to being developed, storm runoff from this sub-basin will overland flow to temporary swales, where the flows will be captured by an interim 36" FES and piped to Pond W5.

Sub-basin A14 ($Q_5=16.0$ cfs, $Q_{100}=37.9$ cfs) consists of approximately 11.76 acres and is the proposed future school site on the northern side of Sterling Ranch Road. Runoff from this sub-basin will be routed to a 36" RCP storm sewer stub at DP 14. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A13. Prior to being developed, storm runoff from this sub-basin will overland flow to Sterling Ranch Road, where the flows will be captured by inlets and piped to Pond W5.

Sub-basin A15 ($Q_5=5.4$ cfs, $Q_{100}=11.7$ cfs) consists of approximately 2.91 acres and is the north eastern portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 15. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A14.

Sub-basin A16 (Q_5 =4.4 cfs, Q_{100} =9.6 cfs) consists of approximately 2.34 acres and is the south eastern portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 16. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A15.

Sub-basin A17 ($Q_5=1.4$ cfs, $Q_{100}=4.7$ cfs) consists of approximately 1.76 acres and is the open space located along the western portion of the sterling Ranch Phase 2 development south of Sterling Ranch Road. This basin is primarily single-family open space with a small amount of lot runoff. Runoff from this sub-basin will be captured by a future Type C inlet at DP 17 and coveyed via sheet flow

EXISTING HYDROLOGIC CALCULATIONS (BY J.R. ENGINEERING, APPROVED NOVEMBER 2021)

EXISITNG CONDITIONS COMPOSITE % IMPERVIOUS & RUNOFF COEFFICIENT SUMMARY BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

Subdivision: Location: Sterling Ranch Filing No. 2 El Paso County Project Name: Sterling Ranch Subdivision

Project No.: 25188.01 Calculated By: AAM

Checked By:

Date: 8/16/21

	Total Area (ac)	Str	reets (10	0% Impe	rvious)	Neighb	orhood	Area (70	pervious) % Impervious) 6 Impervious)	Com	mercial	•	npervious) pervious) rvious)		hool (55'	e (0% Imj % Imperv pace (12'	,	Weigl	s Total nted C ues	Basins Total Weighted %
Basin ID	Ai ca (ac)	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighte d % Imp.	C ₅	C ₁₀₀	Imp.
A1	2.06	0.90	0.96	0.48	23.3%	0.45	0.59	1.34	42.3%	0.59	0.70	0.00	0.0%	0.08	0.35	0.24	0.0%	0.51	0.65	65.6%
A2	0.82	0.90	0.96	0.20	24.4%	0.45	0.59	0.56	44.4%	0.59	0.70	0.00	0.0%	0.08	0.35	0.06	0.0%	0.53	0.66	68.8%
A3	6.76	0.90	0.96	1.32	19.5%	0.45	0.59	4.16	40.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.28	0.0%	0.47	0.62	59.5%
A4	1.51	0.90	0.96	0.51	33.8%	0.45	0.59	1.00	43.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.60	0.71	76.8%
A5	1.70	0.90	0.96	0.51	30.0%	0.45	0.59	1.19	45.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.59	0.70	75.5%
A6	1.37	0.90	0.96	0.39	28.5%	0.45	0.59	0.98	46.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.58	0.70	75.0%
A6A	0.53	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.53	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
A7	19.00	0.90	0.96	0.00	0.0%	0.45	0.59	19.00	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
A8	1.48	0.90	0.96	0.74	50.0%	0.45	0.59	0.29	12.7%	0.59	0.70	0.00	0.0%	0.08	0.35	0.45	0.0%	0.56	0.70	62.7%
A9	0.61	0.90	0.96	0.48	78.7%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.13	0.0%	0.73	0.83	78.7%
A10	2.61	0.90	0.96	2.25	86.2%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.36	0.0%	0.79	0.88	86.2%
A11	2.89	0.90	0.96	2.40	83.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.49	0.0%	0.76	0.86	83.0%
A12	3.87	0.90	0.96	0.00	0.0%	0.45	0.59	0.50	8.4%	0.59	0.70	0.00	0.0%	0.08	0.35	3.37	0.0%	0.13	0.38	8.4%
A13	9.65	0.90	0.96	0.00	0.0%	0.45	0.59	9.65	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
A14	11.76	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.00	0.0%	0.39	0.55	11.76	55.0%	0.39	0.55	55.0%
A15	2.91	0.90	0.96	1.57	54.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.34	0.0%	0.52	0.68	54.0%
A16	2.34	0.90	0.96	1.30	55.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.04	0.0%	0.54	0.69	55.6%
A17	1.76	0.90	0.96	0.00	0.0%	0.45	0.59	0.64	23.6%	0.59	0.70	0.00	0.0%	0.08	0.35	1.12	0.0%	0.21	0.44	23.6%
A18	5.27	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	1.18	21.3%	0.08	0.35	4.09	0.0%	0.24	0.47	21.3%
A19	31.85	0.90	0.96	0.00	0.0%	0.45	0.59	31.85	67.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	67.0%
A20	1.83	0.90	0.96	1.63	89.1%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.20	0.0%	0.81	0.89	89.1%
A21	1.93	0.90	0.96	1.73	89.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.20	0.0%	0.82	0.90	89.6%
A22	8.68	0.90	0.96	0.00	0.0%	0.45	0.59	0.70	5.2%	0.59	0.70	0.00	0.0%	0.08	0.35	7.98	0.0%	0.11	0.37	5.2%
B1	2.98	0.90	0.96	2.98	100.0%	0.59	0.70	0.00	0.0%	0.20	0.44	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B2	3.89	0.90	0.96	3.89	100.0%	0.59	0.70	0.00	0.0%	0.20	0.44	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B3	1.53	0.90	0.96	1.53	100.0%	0.59	0.70	0.00	0.0%	0.20	0.44	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B4	1.50	0.90	0.96	1.50	100.0%	0.59	0.70	0.00	0.0%	0.20	0.44	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B5	2.91	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.20	0.44	0.00	0.0%	0.08	0.35	2.91	0.0%	0.08	0.35	0.0%

EXISITNG CONDITIONS COMPOSITE % IMPERVIOUS & RUNOFF COEFFICIENT SUMMARY BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

	Total Area (ac)	Str	reets (10	0% Impe	rvious)	Neighb	orhood	Area (70	pervious) % Impervious) 6 Impervious)	Čom	mercial	•	npervious) pervious) vious)		hool (55	e (0% Imp % Imperv pace (129		Weigl	s Total hted C ues	Basins Total Weighted %
Basin ID	An eu (ue)	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighte d % Imp.	C ₅	C ₁₀₀	Imp.
C1	8.01	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	8.01	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
C2	5.06	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	5.06	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
D1	0.45	0.90	0.96	0.45	100.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
D2	0.43	0.90	0.96	0.43	100.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
OS20	308.00	0.90	0.96	3.36	1.1%	0.59	0.70	157.32	4.6%	0.20	0.44	2.38	0.6%	0.09	0.36	144.94	0.0%	0.13	0.40	6.3%
OS21A	20.26	0.90	0.96	1.13	5.6%	0.59	0.70	19.13	8.5%	0.20	0.44	0.00	0.0%	0.09	0.36	0.00	0.0%	0.13	0.40	14.1%
OS21B	8.71	0.90	0.96	0.00	0.0%	0.59	0.70	8.71	9.0%	0.20	0.44	0.00	0.0%	0.09	0.36	0.00	0.0%	0.13	0.40	9.0%
OS2	17.00	0.90	0.96	0.00	0.0%	0.49	0.62	17.00	70.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.49	0.62	70.0%
OS3	28.70	0.90	0.96	0.00	0.0%	0.49	0.62	28.70	70.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.49	0.62	70.0%
OS4	5.08	0.90	0.96	0.00	0.0%	0.20	0.40	5.08	15.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.20	0.40	15.0%
TOTAL (A1-A22,OS2-4)	173.97																			57.6%
TOTAL (B1-B5, OS20-21B)	349.78																			9.4%
TOTAL (C1-C2)	13.07																			95.0%
TOTAL	537.70																			27.9%

EXISTING CONDITIONS AREA RUNOFF COEFFICIENT & AREA DRAINAGE SUMMARY BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2

Location: El Paso County

Project Name: Sterling Ranch Subdivision

Project No.: 25188.01

Calculated By: AAM Checked By:

Date: 8/16/21

		SUB-E	BASIN			INITIA	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	TA				(T _i)				(T _t)			(L	JRBANIZED BA	ASINS)	FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C ₅	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	К	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
A1	2.06	А	66%	0.51	0.65	100	2.5%	7.8	388	3.0%	20.0	3.5	1.9	9.7	488.0	16.9	9.7
A2	0.82	А	69%	0.53	0.66	100	2.5%	7.6	183	1.0%	20.0	2.0	1.5	9.1	283.0	15.9	9.1
A3	6.76	А	60%	0.47	0.62	100	2.5%	8.4	1186	2.3%	20.0	3.0	6.5	15.0	1286.0	23.4	15.0
A4	1.51	А	77%	0.60	0.71	78	2.0%	6.3	795	2.9%	20.0	3.4	3.9	10.2	873.0	16.9	10.2
A5	1.70	А	76%	0.59	0.70	100	2.5%	6.9	645	3.1%	20.0	3.5	3.1	9.9	745.0	16.3	9.9
A6	1.37	А	75%	0.58	0.70	100	2.5%	7.0	632	3.1%	20.0	3.5	3.0	10.0	732.0	16.3	10.0
A6A	0.53	А	95%	0.81	0.88	100	2.0%	4.2	30	2.0%	20.0	2.8	0.2	4.3	130.0	10.0	5.0
A7	19.00	А	65%	0.45	0.59	100	2.5%	8.7	1419	1.5%	20.0	2.4	9.7	18.3	1519.0	25.6	18.3
A8	1.48	А	63%	0.56	0.70	80	2.0%	6.9	646	0.6%	20.0	1.5	7.0	13.9	726.0	23.2	13.9
A9	0.61	А	79%	0.73	0.83	15	2.0%	2.1	661	0.7%	20.0	1.7	6.6	8.7	676.0	19.2	8.7
A10	2.61	А	86%	0.79	0.88	15	2.0%	1.7	1357	3.4%	20.0	3.7	6.1	7.9	1372.0	17.2	7.9
A11	2.89	А	83%	0.76	0.86	16	2.0%	1.9	1357	2.8%	20.0	3.3	6.8	8.7	1373.0	18.4	8.7
A12	3.87	А	8%	0.13	0.38	100	5.0%	10.3	267	3.4%	15.0	2.8	1.6	11.9	367.0	26.9	11.9
A13	9.65	А	65%	0.45	0.59	100	2.5%	8.7	934	2.1%	20.0	2.9	5.4	14.0	1033.6	20.9	14.0
A14	11.76	А	55%	0.39	0.55	100	2.0%	10.2	867	2.0%	20.0	2.8	5.1	15.3	967.0	22.8	15.3
A15	2.91	А	54%	0.52	0.68	34	2.0%	4.8	1621	1.8%	20.0	2.7	10.1	14.9	1655.0	29.0	14.9
A16	2.34	А	56%	0.54	0.69	35	2.0%	4.8	1594	1.8%	20.0	2.7	9.9	14.7	1629.0	28.4	14.7
A17	1.76	А	24%	0.21	0.44	100	5.0%	9.4	403	1.1%	15.0	1.6	4.3	13.7	503.0	27.2	13.7
A18	5.27	А	21%	0.24	0.47	100	2.0%	12.3	703	2.0%	20.0	2.8	4.1	16.4	803.0	29.3	16.4
A19	31.85	А	67%	0.45	0.59	100	2.5%	8.7	2675	1.7%	20.0	2.6	17.1	25.8	2775.0	33.2	25.8
A20	1.83	А	89%	0.81	0.89	15	2.0%	1.6	936	1.5%	20.0	2.4	6.4	8.0	951.0	16.8	8.0
A21	1.93	А	90%	0.82	0.90	15	2.0%	1.6	1049	1.5%	20.0	2.4	7.1	8.7	1064.0	17.4	8.7
A22	8.68	А	5%	0.11	0.37	185	3.0%	16.9	540	0.5%	20.0	1.4	6.4	23.3	725.0	38.2	23.3
B1	2.98	А	100%	0.90	0.96	17	2.0%	1.2	2561	1.7%	20.0	2.6	16.4	17.6	2578.0	23.2	17.6
B2	3.89	А	100%	0.90	0.96	17	2.0%	1.2	2561	1.7%	20.0	2.6	16.4	17.6	2578.0	23.2	17.6
B3	1.53	А	100%	0.90	0.96	17	2.0%	1.2	1394	2.0%	20.0	2.8	8.2	9.4	1411.0	16.1	9.4
B4	1.50	А	100%	0.90	0.96	17	2.0%	1.2	1394	2.0%	20.0	2.8	8.2	9.4	1411.0	16.1	9.4

EXISTING CONDITIONS AREA RUNOFF COEFFICIENT & AREA DRAINAGE SUMMARY BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2

Location: El Paso County

Project Name: Sterling Ranch Subdivision

Project No.: 25188.01

Calculated By: AAM Checked By:

Date: 8/16/21

		SUB-I	BASIN			INITI	AL/OVERI	AND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
B5	2.91	А	0%	0.08	0.35	170	14.0%	10.1	259	0.5%	20.0	1.4	3.1	13.1	429.0	32.8	13.1
C1	8.01	А	95%	0.81	0.88	100	2.0%	4.2	965	2.0%	20.0	2.8	5.7	9.9	1065.0	14.9	9.9
C2	5.06	А	95%	0.81	0.88	100	2.0%	4.2	627	2.0%	20.0	2.8	3.7	7.9	727.0	13.2	7.9
D1	0.45	А	95%	0.81	0.88	17	2.0%	1.7	180	0.1%	20.0	0.6	5.3	7.0	197.0	14.6	7.0
D2	0.43	А	95%	0.81	0.88	17	2.0%	1.7	180	0.1%	20.0	0.6	5.3	7.0	197.0	14.6	7.0
OS20	308.00	А	6%	0.13	0.40	300	4.0%	19.2	6670	5.0%	10.0	2.2	49.7	68.9	6970.0	75.2	68.9
OS21A	20.26	А	14%	0.13	0.40	300	2.0%	24.1	2673	2.0%	10.0	1.4	31.5	55.6	2973.0	52.3	52.3
OS21B	8.71	А	9%	0.13	0.40	100	2.0%	13.9	1167	1.5%	15.0	1.8	10.6	24.5	1267.0	39.9	24.5
OS2	17.00	А	70%	0.49	0.62	300	1.0%	19.1	3020	1.5%	15.0	1.8	27.4	46.5	3320.0	36.0	36.0
OS3	28.70	А	70%	0.49	0.62	300	1.0%	19.1	4340	1.0%	15.0	1.5	48.2	67.3	4640.0	52.6	52.6
OS4	5.08	А	15%	0.20	0.40	300	1.0%	28.1	900	5.0%	10.0	2.2	6.7	34.9	1200.0	29.5	29.5

NOTES:

$t_c = t_i + t_t$	Equation 6	$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S^{0.33}}$	Equation 6-3	Table 6-2. NRCS Convey	vance factors, K
Where:		$t_i = \frac{S_0^{0.33}}{S_0^{0.33}}$	Equation 0-3	Type of Land Surface	Conveyance Factor, K
where:				Heavy meadow	2.5
t_c = computed time of concentration (minutes)		Where:		Tillage/field	5
t_i = overland (initial) flow time (minutes)		t_i = overland (initial) flow time (minutes)		Short pasture and lawns	7
		C_5 = runoff coefficient for 5-year frequency (from Table 6-4) L_i = length of overland flow (ft)		Nearly bare ground	10
t_t = channelized flow time (minutes).		$S_o =$ average slope along the overland flow path (ft/ft).		Grassed waterway	15
L. L.		L.		Paved areas and shallow paved swales	20
$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$	Equation 6-4	$t_{\rm c} = (26 - 17i) + \frac{L_{\rm r}}{60(14i + 9)\sqrt{S_{\rm r}}}$	Equation 6-5		
Where:		Where:			
t_r = channelized flow time (travel time, min) L_i = waterway length (ft) S_0 = waterway slope (ft/ft) V_r = travel time velocity (ft/sec) = K $\sqrt{S_0}$ K = NRCS conveyance factor (see Table 6-2).		t_c = minimum time of concentration for first design point when l L_t = length of channelized flow path (ft) i = imperviousness (expressed as a decimal) S_t = slope of the channelized flow path (ft/ft).	ess than t _c from Equation 6-1.		

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

EXISTING CONDITIONS SURFACE & PIPE ROUTING SUMMARY (5 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location:	Sterling Ra El Paso Col	nch Fili unty	ng No. :	2												Ca	oject N Projec Iculate	t No.: d By:	25188	3.01	nch Su	bdivisi	ion
Design Storm:	5-Year																Checke		8/16/	21			
				DIRE	CT RUI	NOFF			TC	DTAL F	RUNOF	F	STRE	ET/SW	/ALE		PI	PE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	A1	2.06	0.51	9.7	1.05	4.17	4.4					0.2	0.04	3.3	4.2	1.01		18	652 5	3.6 7.2	3.0 0.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82	0.53	9.1	0.44	4.27	1.9								1.9	0.44	2.0	18	27	5.8	0.1	On-grade inlet Piped to DP 1.0
	1.0								9.7	1.45	4.17	6.0				6.0							Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.47	15.0	3.16	3.53	11.1					1.6	0.47	2.9	9.5				426	3.4	2.1	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	4	A4	1.51					3.7					0.1	0.03	2.9	3.6				395 0	3.4	1.9	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	1.1								15.0	3.57	3.52	12.6				12.6			24	74			Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.2	5.02	3.50	17.6				17.6	5.02	3.3	24	319	12.5	0.4	Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.81	5.0	0.43	5.17	2.2															Overland Flow to DP1.3A
	6	A6	1.37	0.58	10.0	0.79	4.14	3.3								3.3	0.79	2.0	18	0	6.7	0.0	On-grade inlet Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.22	4.14	5.0				5.0	1.22	1.0	24	36	5.7	0.1	Sum of DP 6 & DP 6A, piped to DP 1.3
	5	A5	1.70	0.59	9.9	0.99	4.14	4.1	17.0	1.53	3.33	5.1				5.1	1.53	2.0	18	0	7.6	0.0	On-grade inlet Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	7.77	3.33	25.9				25.9	7.77	1.1	36	620	9.2	1.1	Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.45	18.3	8.55	3.22	27.5								27.5	8.55	1.5	42	20	10.3	0.0	Future storm infrastructure from Copper Chase Subdivision Piped to DP 1.4
	1.4								18.4	16.32	3.22	52.5				52.5	16.32	0.5	48	26	8.2	0.1	Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1.48	0.56	13.9	0.83	3.63	3.0								3.0	0.83	2.0	18	20	6.6	0.1	On-grade inlet, carryover flow to DP 11 Piped to DP 1.5
	1.5								18.4	17.15	3.21	55.1				55.1	17.15	0.5	48	91	8.3	0.2	Sum of DP 1.4 & DP 8, piped to DP 1.6
	9	A9	0.61	0.73	8.7	0.44	4.34	1.9	8.7	0.48	4.34	2.1				2.1	0.48	2.0	18	13	5.8	0.0	On-grade inlet Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								18.6	17.63	3.20	56.4	0.5	0.11	15	56.4	17.63	0.5	48	95 955	8.3 2.4		Sum of DP 1.5 & DP 9, piped to DP 1.8 On-grade inlet, carryover flow to DP 20
	10	A10	2.61	0.79	7.9	2.05	4.49	9.2								8.7	1.94	2.5	18	118 1049	2.4 9.5 2.4	0.2	Piped to DP 1.7 On-grade inlet, carryover flow to DP 21
	11	A11	2.89	0.76	8.7	2.20	4.34	9.5					0.6	0.15	1.5	8.9	2.05	2.5	18	1049		0.0	Piped to DP 1.7
	1.7								8.7	3.99	4.34	17.3				17.3	3.99	1.0	24	8	7.9	0.0	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								18.8	21.63	3.18	68.8				68.8	21.63	2.0	54	517	14.4	0.6	Sum of DP 1.6 & DP 1.7, piped to DP 2.7 Future flow released from Barbarick Subdivision
	OS2	OS2	17.00	0.49	14.0	6.25	2.20	13.8								13.8	6.25	1.0	30	787	7.5	1.7	Type C inlet
	12	A12	3.87	0.13	11.9	0.49	3.86	1.9								1.9	0.49	2.0	18	17	5.6	0.1	Piped to DP 2.0
	2.0								15.7	6.74	3.45	23.2				23.2	6.74	1.0	48	52	8.4	0.1	Sum of DP OS2 & DP 12, Piped to DP 2.1 Future storm infrastructure from Sterling Ranch Phase 2
	13	A13	9.65	0.45	14.0	4.34	3.62	15.7								15.7	4.34	1.5	30	200	9.1	0.4	Piped to DP 2.1

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EXISTING CONDITIONS SURFACE & PIPE ROUTING SUMMARY (5 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	El Paso Cou		ng No. 2												Ca	oject N Projec Iculate Checke	t No.: d By:	2518	ng Ra 8.01	nch S	Subd	livisio	on
																	Date:	8/16/	21				
			DIRE	CT RL	INOFF	1	r	T	OTAL F	RUNOF	F	STRE	et/sv	/ALE		PI	PE	_	TRA	VEL T	IME		
STREET	Design Point	Basin ID	Area (Ac) Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	forder formance	t _t (min)	REMARKS
	2.1							15.9	11.08	3.44	38.1				38.1	11.08	1.6	48	65	5 11.	.4		Sum of DP 2.0 & DP 13, piped to DP 2.5
	OS3	OS3	28.70 0.49	19.0	0 14.00	5 1.25	17.6								17.6	14.06	1.0	30	719	8	.0	1.5	Future flow released from Barbarick Subdivision Piped to DP 2.2
	14	A14	11.76 0.39	15.3	3 4.59	3.49	16.0								16.0	4.59	1.0	30	20	0 7.	.8		Future flow released from School Site Piped to DP 2.2
	2.2							20.5	18.65	3.05	56.9				56.9	18.65	1.5	48	773	3 12	.4		Sum of DP OS3 & DP 14, piped to DP 2.3
	15	A15	2.91 0.52	14.9	9 1.5	2 3.53	5.4								5.4	1.52	1.3	18	35		.5	0.1	On-grade inlet Piped to DP 2.3
	16	A16	2.34 0.54	14.	7 1.2	5 3.55	4.4					0.1	0.04	0.8	4.3	1.21	2.0	18	697 12		.8 .2	6.5 0.0	On-grade inlet, carryover flow to DP 9 Piped to DP 2.3
	2.3							15.0	2.73	3.52	9.6				9.6	2.73	1.6	48	51	1 7.	.6	0.1	Sum of DP 15 & DP 16, piped to DP 2.4
	2.4							21.5	21.38	2.98	63.7				63.7	21.38	1.6	48	19	9 13	.1	0.0	Sum of DP 2.2 & DP 2.3, piped to DP 2.5
	2.5							21.6	32.46	2.98	96.6				96.6	32.46	2.0	60	839	9 15.	.8		Sum of DP 2.1 & DP 2.4 piped to DP 2.6
	17	A17	1.76 0.21	13.	7 0.38	3 3.66	1.4								1.4	0.38	1.0	18	24	4	.1	0.1	Type C inlet Piped to DP 2.6
	2.6							21.6	32.84	2.98	97.8				97.8	32.84	2.0	60	32	2 15	.8	0.0	Sum of DP 2.5 & DP 17, piped to DP 2.7
	2.7							21.6	54.47	2.97	162.0				162.0	54.47	0.6	78	220) 11.	.5		Sum of DP1.8 & DP 2.6, piped to DP 2.8
	18	A18	5.27 0.24	16.4	4 1.28	3 3.38	4.3								4.3	1.28	1.0	18	24	1 5	.6	0.1	Area inlet Piped to DP 2.6
	19	A19	31.85 0.45	25.	3 14.3	3 2.71	38.8								38.8	14.33	1.0	18	24	1 22	.0		Area inlet Piped to DP 2.6
	2.8							25.8	70.08	2.71	189.8				189.8	70.08	0.6	78		5 12	.1	0.2	Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0.
	3.0							25.8	70.08	2.71	189.8	189.8	70.08	0.5					584	1 1	.4		Detention Pond Trickle channel conveyance to DP 3.2
	20	A20	1.83 0.81	8.0	0 1.48	3 4.47	6.6	8.0	1.59	4.47	7.1				7.1	1.59	1.0	24	105	5 6	.4	0.3	On-grade inlet Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0
	21	A21	1.93 0.82	8.	7 1.5	7 4.33	6.8	8.7	1.72	4.33	7.4	0.1	0.03	1.5	7.3	1.68	2.5	18	C) 9	.0		On-grade inlet Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9							8.7	3.27	4.33	14.2				14.2	3.27	2.0	24	58				Sum of DP 20 & DP 21,piped to DP 3.1
	3.1							8.7	3.27	4.33	14.2	14.2	3.27	0.5					568	3 1.	.4		Detention Pond Trickle channel conveyance to DP 3.2
	22	A22	8.68 0.11	23.3	3 0.9	5 2.86	2.7																Detention Pond Overland flow to DP 3.2
	OS4	OS4	5.08 0.20	29.	5 1.02	2 2.51	2.6					2.6	1.02	13.0					113	3 5	.4		Existing topography Overland flow to DP 4.1
	3.2							29.8	75.32	2.49	187.5												Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8
	Pond W5							29.8	1.45	2.49	3.6				3.6	1.45	2.0	48					Outlet structure release to DP 4.8
	23	B1	2.98 0.90	17.0	5 2.68	3 3.29	8.8					0.4	0.12	2.0	8.4	2.56	0.5	30	1399 88		.0 1	12.0	On-grade inlet Piped to DP 4.0

EXISTING CONDITIONS SURFACE & PIPE ROUTING SUMMARY (100 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: 1 Location: 1 Sign Storm:	El Paso Cou	ch Filin nty	g No. 2													C	roject N Projec alculate Checke	t No.: d By: d By:	2518 AAM	8.01	nch Su	ubdivi	sion
																		Date:	8/16				
				DIR	ECT RU	JNOFF			T	OTAL F	UNOF	F	STRE	ET/SW	ALE		PIP	E	_	TRA	/EL TIľ	ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	A1	2.06	0.65	9.7	1.34	7.01	9.4					2.8	0.40	3.3	6.6	0.94	2.0	18	652 5	3.6 8.2	3.0 0.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82		9.1	0.54	7.17	3.9					0.1	0.01	3.3	3.8	0.53	2.0	18	639 27	3.6 7.0	2.9	On-grade inlet, carryover flow to DP 6 Piped to DP 1.0
	1.0								9.7	1 47	7.00	10.3				10.3							Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.62	15.0	4.17	5.92	24.7	7.1	1.47	7.00	10.5	10.0	1.69	2.9	14.7	2.48			426	3.4	2.1	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	4	A4		0.71		1.08							1.6	0.24	2.9	5.8				395		1.9	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	1.1	74	1.51	0.71	10.2	1.00	0.00	7.4	15.0	2.22	5.91	19.7				19.7	3.33						Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.1		5.89					28.2					13.9		Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.52	0.88	5.0	0.47	8.68	4.1		4.00	5.07	20.2				20.2	4.00	5.5	24	317	13.7	0.4	Overland Flow to DP1.3A
	6	A6A		0.70		0.47	6.94			0.06	6.94	6.7	1.3	0.18	0.7	5.4	0.78	2.0	18	696 0			On-grade index, carryover flow to DP 8 Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A	AU	1.37	0.70	10.0	0.75	0.74	0.0	10.0		6.94	8.7				8.7							
		A5	1 70	0.70	9.9	1 10	6.95	0.2			5.59		6.5	1.17	0.7	13.1				664	1.7	6.6	Sum of DP 6 & DP 6A, piped to DP 1.3 On-grade inlet, carryover flow to DP 8 Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	5	AD	1.70	0.70	9.9	1.19	0.95	8.3															
	1.3		40.00	0.50	40.0		5.44		17.0	8.39	5.59	46.9				46.9					10.7		Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4 Future storm infrastructure from Copper Chase Subdivision
	7	A7	19.00	0.59	18.3	11.21	5.41	60.6								60.6					12.7		Piped to DP 1.4
	1.4								18.4				1.9	0.41	0.7	105.9			48	195	1.7	1.9	Sum of DP 1.3 & DP 7, piped to DP 1.5 On-grade inlet, carryover flow to DP 11
	8	A8	1.48	0.70	13.9	1.04	6.10	6.3	23.7	2.63	4.76	12.5				10.6	2.23	2.0	18				Sum of Sub-basin A8 & Carryover flows from DP5, DP 6 & DP 15, Piped to DP 1.5
	1.5								23.7	21.83	4.76	103.9	0.3	0.05	0.7	103.9	21.83	0.5	48	91 140			Sum of DP 1.4 & DP 8, piped to DP 1.6 On-grade inlet, carryover flow to DP 11
	9	A9	0.61	0.83	8.7	0.51	7.29	3.7	21.2	0.95	5.04	4.8				4.5	0.89	2.0	18	13	7.3	0.0	Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								23.9	22.72	4.74	107.7	4.5	0.59	15	107.7	22.72	0.5	48	95 955			Sum of DP 1.5 & DP 9, piped to DP 1.8 On-grade inlet, carryover flow to DP 20
	10	A10	2.61	0.88	7.9	2.29	7.53	17.3					6.1	0.90		12.8	1.70	2.5	18		10.3	0.2	Piped to DP 1.7 On-grade inlet, carryover flow to DP 21
	11	A11	2.89	0.86	8.7	2.48	7.28	18.1	10.6	2.94	6.77	19.9	0.1	0.70	1.5	13.8	2.04	2.5	18			0.0	Sum of Sub-basin A11 & carryover flows from DP 8 & DP 9, piped to DP 1.7
	1.7								10.6	3.74	6.77	25.3				25.3	3.74	1.0	24	8	8.1	0.0	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								24.0	26.45	4.72	125.0				125.0	26.45	2.0	54	517	17.0	0.5	Sum of DP 1.6 & DP 1.7, piped to DP 2.7
	OS2	OS2	17.00	0.62	12.0	10.54	3.71	39.1								39.1	10.54	1.0	30	787	9.5	1.4	Future flow released from Barbarick Subdivision Piped to DP 2.0
	12	A12	3.87	0.38	11.9	1.47	6.49	9.5								9.5	1.47	2.0	18	17	8.9	0.0	Type C inlet Piped to DP 2.0
	2.0								13.4	12.01	6.20	74.5				74.5	12.01	1.0	48	52	11.6	0.1	Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.59	14.0	5.69	6.08	34.6								34.6	5.69	1.5	30	200	11.0	0.3	Future storm infrastructure from Sterling Ranch Phase 2 Piped to DP 2.1

EXISTING CONDITIONS SURFACE & PIPE ROUTING SUMMARY (100 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision	vision: Sterling Ranch Filing No. 2													Project Name: Project No.:					Sterling Ranch Subdivision 25188.01				
Location:	ion: El Paso County																alculate	ed By: 🛛	AAM				
ssign Storm: 100-Year																	Checke	ed By: Date:	8/16/	21			
				DID		INCEE			Ŧ			- 1	CTD	ET (CLA)	A. F.	-		-	TRAVEL TIME				
				DIR	ECT R	UNOFF			10	DTAL R	UNOF	F	STRE	ET/SW	ALE		PIPE	E	0	IRAV	EL III	VIE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	2.1								14.3	17.70	6.02	106.6				106.6	17.70	1.6	48	65	15.1	0.1	Sum of DP 2.0 & DP 13, piped to DP 2.5
	OS3	OS3	28.70	0.62	15.0	17.79	2.75	48.9								48.9	17.79	1.0	30	719	10.0		Future flow released from Barbarick Subdivision Piped to DP 2.2
																							Future flow released from School Site
	14	A14	11.76	0.55	15.3	6.47	5.86	37.9								37.9	6.47		30	20			Piped to DP 2.2
	2.2								16.2	24.26	5.72	138.7	1.4	0.24	0.7	138.7	24.26	1.5	48	773 724			Sum of DP OS3 & DP 14, piped to DP 2.3 On-grade inlet, carryover flow to DP 8
	15	A15	2.91	0.68	14.9	1.98	5.93	11.7								10.3	1.74	1.3	18	35	7.6	0.1	Piped to DP 2.3
	16	A16	2.34	0.69	14.7	1.61	5.96	9.6					2.6	0.44	0.8	7.0	1.17	2.0	18	697 12	1.8 8.2		On-grade inlet, carryover flow to DP 9 Piped to DP 2.3
	2.3								15.0	2.91	5.91	17.2				17.2	2.91	1.6	48	15	9.0	0.0	Sum of DP 15 & DP 16, piped to DP 2.4
	2.4								17.0	27.17	5.59	151.9				151.9	27.17	1.6	48	19	16.2	0.0	Sum of DP 2.2 & DP 2.3, piped to DP 2.5
	2.5								17.1	44.87	5.59	250.7				250.7	44.87	2.0	60	839	20.1	0.7	Sum of DP 2.1 & DP 2.4 piped to DP 2.6
	17	A17	1.76	0.44	13.7	0.77	6.14	4.7								4.7	0.77	1.0	18	24	5.7		Type C inlet Piped to DP 2.6
	2.6								17.7	45.64	5.49	250.4				250.4	45.64	2.0	60	32	20.2	0.0	Sum of DP 2.5 & DP 17, piped to DP 2.7
	2.7								24.5	72.10	4.67	336.8				336.8	72.10	0.6	78	220	13.7	0.3	Sum of DP1.8 & DP 2.6, piped to DP 2.8
	18	A18	5.27	0.47	16.4	2.47	5.68	14.0								14.0	2.47	1.0	18	24	7.9	0.1	Area inlet Piped to DP 2.6
	19	A19	31.85	0.59	25.8	18.79	4.55	85.4								85.4	18.79	1.0	18	24	48.4	0.0	Area inlet Piped to DP 2.6
	2.8								25.8	93.36	4 55	424 4				424.4	93.36	0.6	78	145	13.9	0.2	Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0.
	3.0									93.36			424.4	93.36	0.5					564	1.4		Detention Pond Trickle channel conveyance to DP 3.2
													2.3	0.38	1.5								On-grade inlet
	20	A20		0.89						2.22		13.4	3.3	0.57	1.5	11.1	1.84		24	105			Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0 On-grade inlet
	21	A21	1.93	0.90	8.7	1.73	7.28	12.6	15.8	2.63	5.77	15.2				11.9	2.06		18	0	10.2		Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9								15.8	3.91	5.77	22.5	22.5	3.91	0.5	22.5	3.91	2.0	24	58 568	11.0 1.4		Sum of DP 20 & DP 21,piped to DP 3.1 Detention Pond
	3.1								15.8	3.91	5.77	22.5	22.0	0.71	0.0					000		0.7	Trickle channel conveyance to DP 3.2 Detention Pond
	22	A22	8.68	0.37	23.3	3.21	4.80	15.4															Overland flow to DP 3.2
	OS4	OS4	5.08	0.40	29.5	2.03	4.21	8.5					8.5	2.03	13.0					113	5.4	0.3	Existing topography Overland flow to DP 3.2
	3.2								29.8	102.50	4.18	428.2											Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8
	Pond W5								29.8	34.84	4.18	145.5				145.5	34.84	2.0	48	58	17.5	0.1	Outlet structure release to DP 4.8
	23	B1	2.98	0.96	17.6	2.86	5.51	15.8					3.6	0.65	2.0	12.2	2.21		30	1394 88	2.1	11.0	On-grade inlet Piped to DP 4.0
	24	B2		0.96				20.6					6.5	1.17	2.0	14.1	2.56		30	1394	2.1	11.0	On-grade inlet Piped to DP 4.0
	27	52	5.07	0.70	17.0	5.15	3.31	20.0								17.1	∠.JU	2.0	30	J	7.1	0.0	

PROPOSED HYDROLOGIC CALCULATIONS

COPPER CHASE AT STERLING RANCH PROPOSED CONDITIONS (Area Runoff Coefficient Summary)

				STREETS		D	evelopme	ENT	OPEN SP.	ACE / LAND	SCAPING		
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀
Α	156397.009	3.59	0.00	0.90	0.96	2.28	0.45	0.59	1.31	0.09	0.36	0.32	0.51
В	148304.6808	3.40	0.00	0.90	0.96	3.00	0.45	0.59	0.40	0.09	0.36	0.41	0.56
С	44335.8117	1.02	0.00	0.90	0.96	1.02	0.45	0.59	0.00	0.09	0.36	0.45	0.59
D	126236.9571	2.90	0.00	0.90	0.96	2.90	0.45	0.59	0.00	0.09	0.36	0.45	0.59
Е	38846.7466	0.89	0.21	0.90	0.96	0.68	0.45	0.59	0.00	0.09	0.36	0.56	0.68
F	112434.6262	2.58	0.00	0.90	0.96	2.18	0.45	0.59	0.40	0.09	0.36	0.39	0.55
G	71700.54	1.65	0.44	0.90	0.96	1.21	0.45	0.59	0.00	0.09	0.36	0.57	0.69
Н	53106.3075	1.22	0.00	0.90	0.96	0.39	0.45	0.83	0.83	0.12	0.39	0.23	0.53
I	60953.98	1.40	0.00	0.90	0.96	1.40	0.45	0.59	0.00	0.09	0.36	0.45	0.59
J	38881.001	0.89	0.30	0.90	0.96	0.59	0.45	0.59	0.00	0.09	0.36	0.60	0.71
K	46538.1625	1.07	0.00	0.90	0.96	1.07	0.45	0.59	0.00	0.09	0.36	0.45	0.59
L	52574.1933	1.21	0.00	0.90	0.96	0.52	0.45	0.59	0.69	0.09	0.36	0.24	0.46
М	28034.2781	0.64	0.00	0.90	0.96	0.06	0.45	0.59	0.58	0.09	0.36	0.12	0.38
A4	24837.432	0.64	0.64	0.90	0.96	0.00	0.45	0.59	0.00	0.09	0.36	0.90	0.96
A6	N/A	1.37		REFER T	O "FINAL DR.	AINAGE REPO	ORT FOR STE	ERLING RANC	H NO. 2" FOR	DETAILS		0.58	0.70
A6A	N/A	0.53		REFER T	O "FINAL DR.	AINAGE REPO	ORT FOR STE	ERLING RANC	H NO. 2" FOR	DETAILS		0.81	0.88
A8	32551.5217	0.75	0.75	0.90	0.96	0.00	0.45	0.59	0.00	0.09	0.39	0.90	0.96
A11	121476.1738	2.79	2.22	0.90	0.96	0.00	0.45	0.59	0.57	0.09	0.39	0.73	0.84

COPPER CHASE AT STERLING RANCH PROPOSED CONDITIONS (Area Drainage Summary)

·																	
From Area Runo	ff Coefficient Sum	nary			OVERLA	4ND		ST	REET / CH	ANNEL FLO)W	Time of T	ravel (T _t)	INTEN	SITY *	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DCI	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	3.59	0.32	0.51	0.32	100	10.5	6.5	860	1.7%	2.6	5.4	11.9	15.3	3.9	6.5	4.4	11.8
В	3.40	0.41	0.56	0.41	100	1.4	11.2	735	1.6%	2.5	4.9	16.1	14.6	3.6	6.0	4.9	11.4
С	1.02	0.45	0.59	0.45	100	2.0	9.3	520	2.5%	3.2	2.7	12.1	13.4	3.8	6.5	1.8	3.9
D	2.90	0.45	0.59	0.45	100	2.2	9.0	795	1.9%	2.8	4.7	13.8	15.0	3.6	6.1	4.8	10.5
E	0.89	0.56	0.68	0.56	100	2.0	7.8	340	1.9%	2.8	2.0	9.9	12.4	4.1	7.0	2.1	4.2
F	2.58	0.39	0.55	0.39	100	13.0	5.5	855	2.7%	3.3	4.3	9.8	15.3	4.2	7.0	4.2	10.0
G	1.65	0.57	0.69	0.57	100	4.0	6.1	290	2.8%	3.4	1.4	7.5	12.2	4.6	7.7	4.3	8.7
Н	1.22	0.23	0.53	0.23	100	3.3	10.6	655	2.1%	2.2	5.0	15.6	14.2	3.6	6.0	1.0	3.9
Ι	1.40	0.45	0.59	0.45	100	2.7	8.5	760	2.1%	2.9	4.4	12.8	14.8	3.8	6.3	2.4	5.2
J	0.89	0.60	0.71	0.60	100	2.0	7.2	470	1.4%	2.4	3.3	10.5	13.2	4.1	6.8	2.2	4.3
K	1.07	0.45	0.59	0.45	100	3.0	8.2	460	2.0%	2.8	2.7	10.9	13.1	4.0	6.7	1.9	4.2
L	1.21	0.24	0.46	0.24	100	3.5	10.2	655	1.2%	2.2	4.9	15.2	14.2	3.6	6.0	1.1	3.3
М	0.64	0.12	0.38	0.12	100	4.0	11.2	195	3.2%	1.3	2.6	13.7	11.6	3.9	6.6	0.3	1.6
A4	0.64	0.90	0.96	0.90	100	1.8	3.0	350	2.3%	3.0	1.9	4.9	12.5	5.2	8.7	3.0	5.4
A6	1.37	0.58	0.70				REFER	TO "FINAL DR	AINAGE REPO	ORT FOR STE	RLING RANCI	H NO. 2" FOR	DETAILS			3.3	6.6
A6A	0.53	0.81	0.88				REFER	TO "FINAL DR	AINAGE REPO	ORT FOR STE	RLING RANCI	H NO. 2" FOR	DETAILS			2.2	4.1
A8	0.75	0.90	0.96	0.90	100	1.5	3.2	600	1.2%	2.2	4.5	7.7	13.9	4.5	7.6	3.0	5.5
A11	2.79	0.73	0.84	0.73	100	0.9	6.8	1315	2.2%	3.0	7.3	14.2	17.9	3.6	6.1	7.4	14.2

* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: <u>CVW</u> Date: <u>12/8/2021</u> Checked by: <u>VAS</u>

COPPER CHASE AT STERLING RANCH PROPOSED CONDITIONS (Surface Routing Summary)

	From Area Runoff Coefficient Summary			1	OVER	RLAND		PIPE	C / CHA	NNEL FLO)W	Time of Travel (T_t)	INTE	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	Tt	TOTAL	I ₅	I ₁₀₀	Q5	Q ₁₀₀	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	Basin A	1.14	1.82	Ba	sin A Tc wa	is used	11.9					11.9	3.9	6.5	4.4	11.8	CDOT TYPE R AT-GRADE 5' INLET
																	(IN-1)
2	Basin B	1.39	1.92	Ba	sin B Tc wa	s used	14.6					14.6	3.6	6.0	4.9	11.4	CDOT TYPE R AT-GRADE 15' INLET
																	(IN-2)
3	Basin C	0.46	0.60	Ba	sin C Tc wa	s used	12.1					12.1	3.8	6.5	3.7	11.8	CDOT TYPE R AT-GRADE 5' INLET
U U	FB-IN1	0.50	1.23		1	1										1110	(IN-3)
	Sum:	0.96	1.83														(11.5)
4	Basin D	1.30	1.71	Desig	n Point 2 Tc	was used	14.6					14.6	3.6	6.0	4.7	12.0	CDOT TYPE R AT-GRADE 15' INLET
	FB-IN2	0.0	0.29														(IN-4)
	Sum:	1.31	2.00														
5	Basin E	0.50	0.60	Desi	gn Point 4 v	vas used	14.6					14.6	3.6	6.0	1.8	5.6	CDOT TYPE R SUMP 15' INLET
	FB-IN4	0.0	0.33														(IN-5)
	Sum:	0.50	0.93														
6	Basin F	1.02	1.43	Ba	sin F Tc wa	s used	9.8					9.8	4.2	7.0	4.2	10.0	CDOT TYPE R 15' AT-GRADE INLET
																	(IN-6)
7	Basin G	0.94	1.13	We	ighted Tc w	as used	16.0					16.0	3.4	5.7	4.9	20.0	EX CDOT TYPE R 15' AT-GRADE INLET
	FB-IN6	0.00	0.16														(IN-A5)
	FB-INA1	0.05	0.40														
	FB-INA4	0.00	0.10														
	FB-INA3	0.45	1.69														
		1.44	3.48														
8	Basin H	0.27	0.65	Ba	sin H Tc wa	s used	14.2					14.2	3.6	6.0	1.0	3.9	BEEHIVE GRATE SUMP INLET
																	(IN-8)
9	Basin I	0.63	0.83	Design	n Point 5 Tc	was used	14.6					14.6	3.6	6.0	4.0	10.5	CDOT TYPE R SUMP 15' INLET
r -	DP 5	0.50	0.93														(IN-5)
	Sum:	1.13	1.76														
10	Basin J	0.54	0.64	Ba	isin J Tc wa	s used	10.5					10.5	4.1	6.8	2.2	4.3	
11	Basin K	0.48	0.63	Desi	gn Point 3 v	vas used	12.1					12.1	3.8	6.5	5.4	16.7	CDOT TYPE R SUMP 15' INLET
	FB-IN3	0.4	1.32														(IN-9)
	DP 10	0.54	0.64														
	Sum:	1.40	2.59														
12	Basin L	0.29	0.55	Ba	sin L Tc wa	s used	14.2				1	14.2	3.6	6.0	1.1	3.3	
]										
13	Basin M	0.08	0.25	Bas	sin M Tc wa	is used	11.6					11.6	3.9	6.6	0.3	1.6	
14	Basin A4	0.58	0.62	Bas	in A4 Tc wa	as used	5.0					5.0	5.2	8.7	3.0	5.4	EX CDOT TYPE R 10' AT-GRADE INLET
]										(IN-A4)
																	1

COPPER CHASE AT STERLING RANCH PROPOSED CONDITIONS (Surface Routing Summary)

	From Area Runoff Coefficient Summary				OVER	LAND		PIPE	C / CHA	NNEL FLO	W	Time of Travel (T_t)	INTEN	SITY *	TOTAL I	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q5	Q ₁₀₀	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
15	Basin A8	0.67	0.72	Basi	n A8 Tc wa	s used	13.9					13.9	3.6	6.1	5.1	19.8	EX CDOT TYPE R 15' AT-GRADE INLET
	FB-INA6	0.00	0.17														(IN-A8)
	Basin A6A	0.43	0.47														
	FB-INA15	0.00	0.24														
	DP 12	0.29	0.55														
	FB-INA5	0.01	1.10														
		1.40	3.25														
16	Basin A11	2.05	2.35	Basir	n All Tc wa	as used	14.2					14.2	3.6	6.1	7.7	22.8	EX CDOT TYPE R 15' AT-GRADE INLET
	FB-INA8	0.00	1.11														(IN-A11)
	DP 13	0.08	0.25														
	FB-INA9	0.00	0.06														
		2.13	3.77														

* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW Date: 6/16/2022 Checked by: VAS

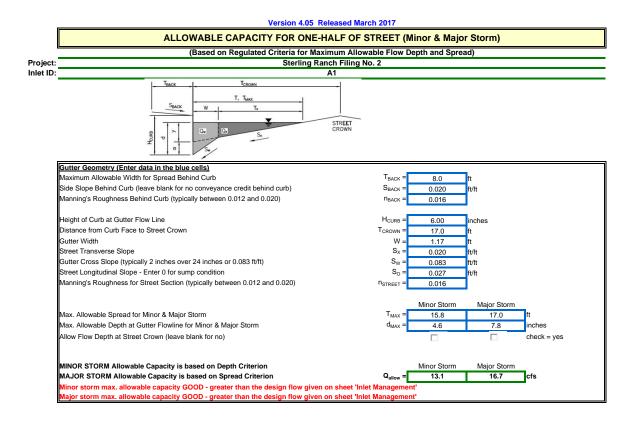
COPPER CHASE AT STERLING RANCH
PROPOSED CONDITIONS

(Storm Sewer	Routing Summary)
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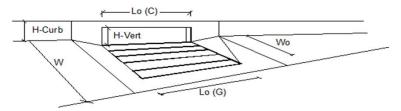
					Inter	isity*	Fl	ow
PIPE	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T _C	Ι,	I 100	Q 5	Q 100
PR1	DP1 (IN-1)	0.65	0.59	11.9	3.9	6.5	2.5	3.8
PR2	DP2 (IN-2)	1.38	1.62	14.6	3.6	6.0	4.9	9.7
PR3	PR1, PR2	2.02	2.21	14.4	3.6	6.0	7.3	13.3
PR4	DP3 (IN-3)	0.64	0.65	14.6	3.6	6.0	2.3	3.9
PR5	DP4 (IN-4)	1.31	1.67	14.6	3.6	6.0	4.7	10.0
PR6	DP6 (IN-6)	1.01	1.27	10.0	4.1	6.9	4.2	8.8
PR7	PR6	1.01	1.27	10.3	4.1	6.9	4.1	8.7
PR8	PR7	1.01	1.27	10.5	4.1	6.8	4.1	8.7
PR9	PR8	1.01	1.27	10.8	4.0	6.7	4.1	8.6
PR10	DP8 (IN-8)	0.27	0.65	14.2	3.6	6.0	1.0	3.9
PR11	PR10, DP9 (IN-5)	1.39	2.38	14.2	3.6	6.0	5.0	14.4
PR12	PR3, PR4, PR5	3.98	4.53	15.3	3.5	5.9	13.9	26.6
PR13	PR11, DP11 (IN-9)	2.79	4.97	12.1	3.8	6.5	10.7	32.1
PR14	PR9, PR12, PR13	7.78	10.78	16.9	3.3	5.6	26.0	60.5
1.0	IN-A1, IN-A2	1.45	1.47	9.7	4.2	7.0	6.1	10.3
1.1	IN-A4, IN-A3	3.27	3.10	15.5	3.5	5.8	11.4	18.1
1.2	1.0, 1.1	4.72	4.57	14.1	3.6	6.1	17.1	27.7
1.3A	1.2, IN-A5, IN-A6	6.87	7.54	15.4	3.5	5.8	23.9	44.1
1.3	1.3A	6.87	7.54	15.4	3.5	5.8	23.9	44.1
1.4	1.3, PR14	14.65	18.32	17.0	3.3	5.6	48.8	102.5
1.5	DP15 (IN-A8), 1.4	16.05	20.75	17.1	3.3	5.6	53.4	115.8
1.6	IN-A9, 1.5	16.69	21.48	17.4	3.3	5.5	55.1	119.0
1.7	DP16 (IN-A11), IN-A10	4.95	4.98	17.5	3.3	5.5	16.3	27.5
1.8	1.7, 1.6	21.65	26.46	24.1	2.8	4.7	60.8	124.8
DP - EX -	ons assume a minimum travel time of 5 minu Design Point Existing Design Point Pipe Run	tes. FB- Flow By from IN- Proposed Inlo IN-A(#)- Existing	et		(Calculated by: Date: Checked by:	6/16/2022	

Overall Im	perviousne	ss of Copper	Chase at Sterling	Ranch
Contributing Basins	Area (Acres)	<i>C</i> ₅	Impervious % (I)	(Acres)*(I)
A	3.59	0.32	44	157.39
В	3.40	0.41	58	198.10
С	1.02	0.45	65	66.16
D	2.90	0.45	65	188.37
Ε	0.89	0.56	73	65.32
F	2.58	0.39	56	144.57
G (on site portion)	0.47	0.57	260	122.39
Н	1.22	0.23	26	31.15
Ι	1.40	0.45	65	90.96
J	0.89	0.60	77	68.52
K	1.07	0.45	65	69.44
L	1.21	0.24	32	38.43
М	0.64	0.12	12	7.99
Totals	21.3			1248.79
Imperviousness of Site	58.7	%		

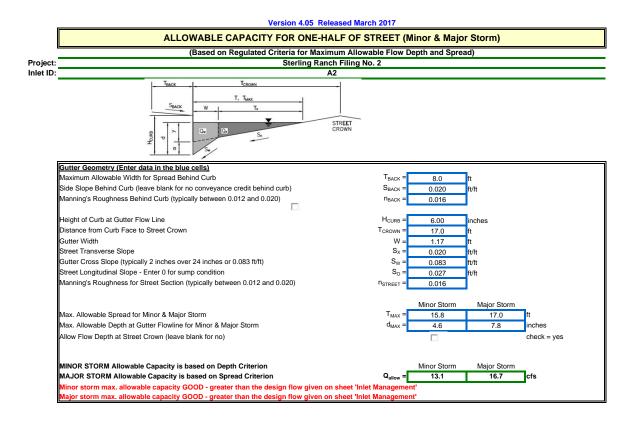
EXISTING HYDRAULIC CALCULATIONS (BY J.R. ENGINEERING, APPROVED NOVEMBER 2021)



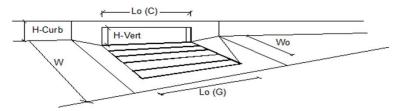
Version 4.05 Released March 2017



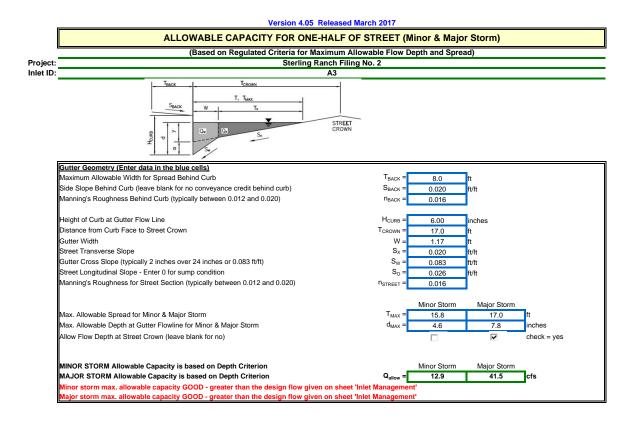
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.2	6.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.2	2.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	95	70	%



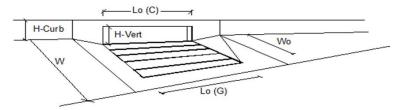
Version 4.05 Released March 2017



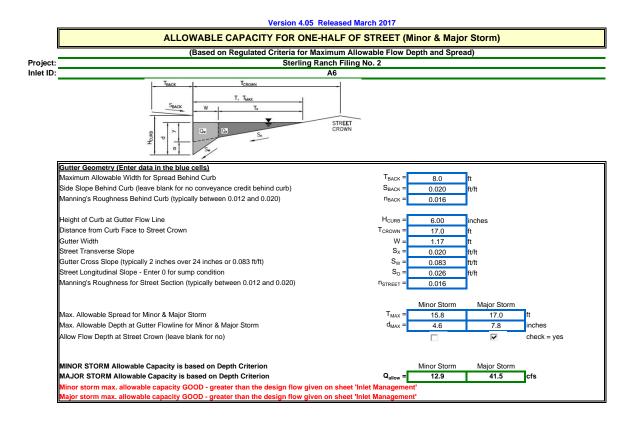
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.9	3.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	97	%



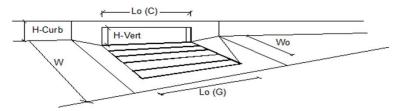
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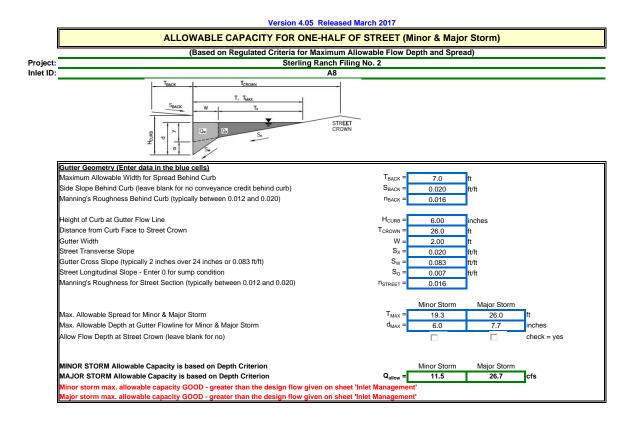
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	9.5	14.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	1.6	10.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	86	60	%



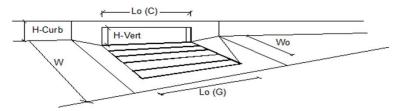
Version 4.05 Released March 2017



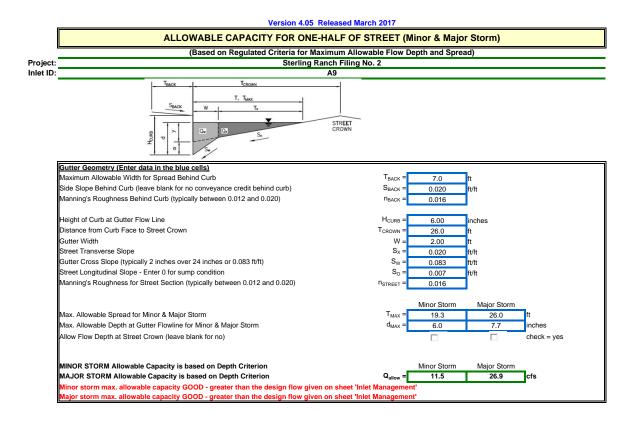
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.3	5.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	81	%



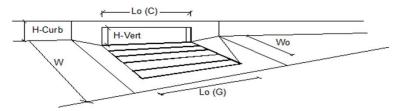
Version 4.05 Released March 2017



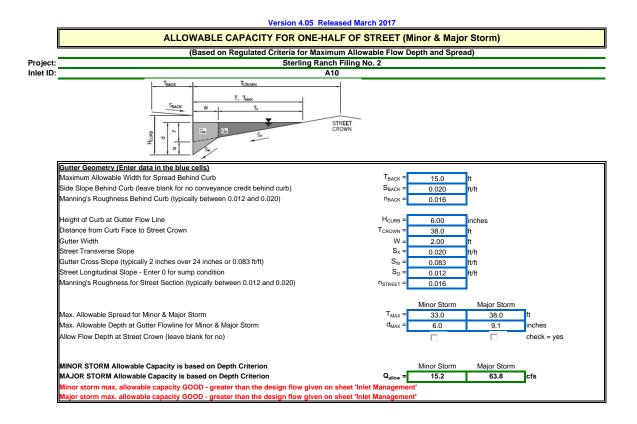
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.0	10.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	85	%



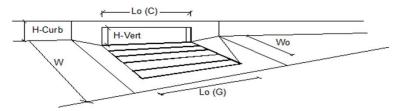
Version 4.05 Released March 2017



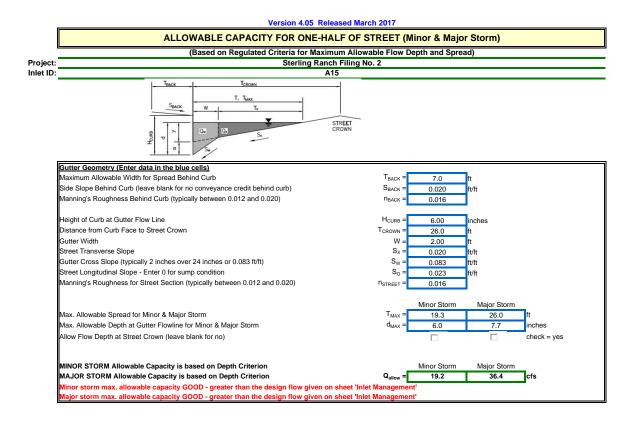
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.1	4.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	94	%



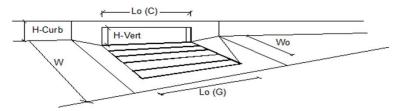
Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.7	12.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.5	4.5	cfs
Capture Percentage = Q _a /Q _o =	C% =	94	74	%



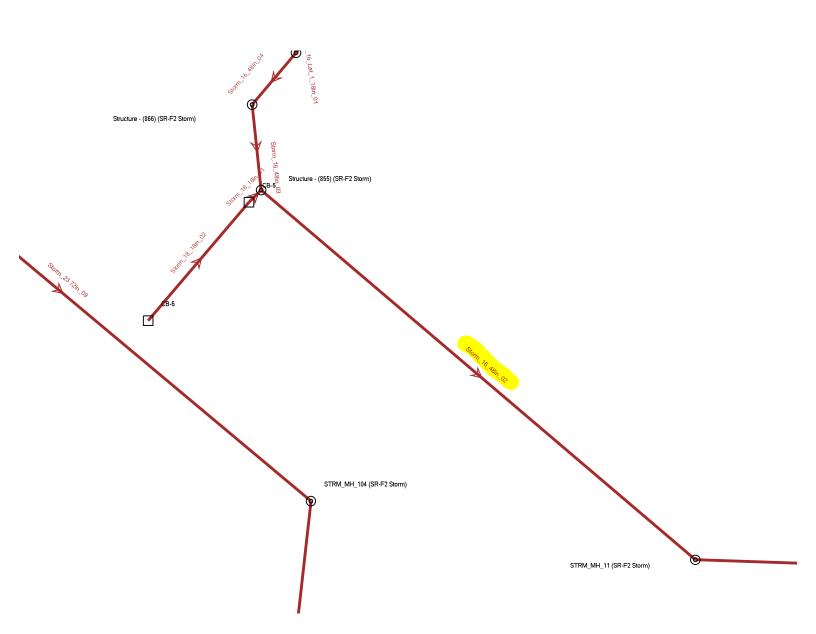
Version 4.05 Released March 2017



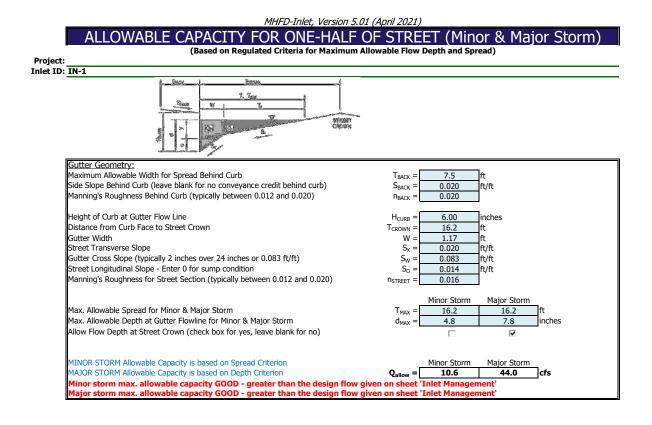
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.4	10.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	88	%

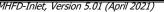
			I a marth				Consolity	L lu calmanullia	L hardward in
	Flow	Diameter	Length (User	Slope	Manning's	Velocity	Capacity (Full	Hydraulic Grade	Hydraulic Grade
Label	(cfs)	(in)	Defined)	(Calculated)	n	(ft/s)	Flow)	Line (In)	Line
	. ,	× ,	(ft) ´	(ft/ft)		. ,	(cfs)	(ft) ´	(Out) (ft)
Storm_17_48in_01	151.90	48.0	15.6	-0.020	0.013	17.70	202.74	6,990.38	6,989.68
Storm_14_66in_05	250.70	66.0	354.4	-0.014	0.013	17.68	397.24	6,985.83	6,982.04
Storm_20_48in_01	139.30	48.0	57.9	-0.020	0.013	17.42	203.30	6,964.17	6,962.31
Storm_17_48in_05	138.70	48.0	292.3	-0.020	0.013	17.39	203.11	7,001.66	6,996.18
Storm_23 54in_11 Storm 23 54in 12	233.40 233.40	54.0 54.0	333.6 412.3	-0.014 -0.014	0.013 0.013	16.67 16.67	232.65 232.63	6,996.60 7,004.71	6,991.45 6,998.44
Storm_17Lat2_36in_01	233.40	36.0	110.1	-0.014	0.013	16.24	133.20	7,004.71	7,003.91
Storm 14 48in 06	106.60	48.0	59.3	-0.017	0.013	15.42	187.87	6,990.60	6,988.91
Storm_17_48in_04	138.70	48.0	82.9	-0.014	0.013	15.23	172.06	6,995.63	6,994.99
Storm_17_48in_03	138.70	48.0	150.3	-0.014	0.013	15.21	171.79	6,994.44	6,992.83
CO-6	74.50	48.0	9.5	-0.021	0.013	15.20	208.41	6,991.39	6,991.40
Storm_17_48in_02	138.70 19.70	48.0 18.0	102.0 76.7	-0.014 -0.049	0.013 0.013	15.09 14.72	170.08 23.16	6,992.28 7.006.74	6,991.01 7,003.66
Storm_19_Lat 2_18in_01 Storm 23 54in 10	233.40	54.0	298.5	-0.049	0.013	14.72	232.69	6,986.54	6,982.33
Storm 23 54in 09	233.40	54.0	402.5	-0.015	0.013	14.68	240.88	6,981.49	6,975.82
Storm 23 54in 08	233.40	54.0	567.0	-0.015	0.013	14.68	240.76	6,974.99	6,967.00
Storm_23 54in_05	233.40	54.0	120.0	-0.015	0.013	14.68	240.88	6,962.34	6,960.65
Storm_23 54in_13	233.40	54.0	265.9	-0.005	0.013	14.68	138.03	7,015.89	7,011.98
Storm_23 54in_06	233.40	54.0	93.0	-0.015	0.013	14.68	240.46	6,965.32	6,964.01
Storm_18_18in_01 Storm 23 54in 14	25.30 221.60	18.0 54.0	22.4 43.7	-0.059 -0.005	0.013 0.013	14.32 13.93	25.59 136.36	6,984.40 7,019.46	6,983.10 7.018.90
Storm_19_24in_05	30.00	24.0	43.7	-0.005	0.013	13.93	39.18	7,019.46	6,997.04
Storm_19_24in_04	30.00	24.0	144.7	-0.030	0.013	13.74	39.18	6,997.59	6,994.14
Storm_14_36in_07	34.60	36.0	76.3	-0.020	0.013	12.31	94.31	6,991.91	6,991.40
Storm_14_72in_03	336.80	72.0	74.5	-0.005	0.013	11.91	306.40	6,977.10	6,976.63
Storm_14_72in_02	336.80	72.0	127.9	-0.005	0.013	11.91	299.58	6,976.08	6,975.27
Storm_19_18in_06	10.30	18.0	339.5	-0.040	0.013	11.81	20.95	7,016.29	7,003.66
Storm_17_48in_06 Storm 14 84in 01	138.70 424.40	48.0 84.0	22.6 107.3	-0.020 -0.005	0.013 0.013	11.04 11.03	202.28 453.09	7,002.97 6,974.79	7,002.76 6,974.32
Storm_14_66in_04	250.70	66.0	512.4	-0.003	0.013	10.55	366.67	6,981.61	6,978.75
Storm 23 66in 02	243.40	66.0	549.0	-0.002	0.013	10.24	138.58	6,957.00	6,954.11
Storm_23_66in_03	243.40	66.0	167.7	-0.002	0.013	10.24	139.63	6,958.28	6,957.40
Storm 19 Lat 1 18in_01	8.70	18.0	36.4	-0.030	0.013	10.18	18.18	6,994.36	6,994.14
Storm_16_48in_02	<mark>125.00</mark> 382.70	48.0	348.6	<mark>-0.024</mark> -0.003	0.013	<mark>9.95</mark> 9.94	220.31	6,982.33	6,979.69
Storm_23_84in_02 Storm 23 84in 01	382.70	84.0 84.0	27.0 200.4	-0.003	0.013 0.013	9.94 9.94	347.91 325.38	6,951.54 6,953.31	6,951.16 6,952.64
Storm 19 30in 03	46.90	30.0	165.0	-0.024	0.013	9.55	64.17	6,993.43	6,991.28
Storm_15_42in_01-E	85.40	42.0	63.9	-0.004	0.013	8.88	65.41	6,975.73	6,975.27
Storm_16_48in_03	107.70	48.0	50.4	-0.020	0.013	8.57	203.42	6,983.38	6,983.10
Storm_16_48in_04	107.70	48.0	42.5	-0.020	0.013	8.57	203.12	6,984.19	6,983.95
Storm 23 three 42in_04	243.40	42.0	258.8	-0.008	0.013	8.43	264.00	6,960.38	6,958.69
Storm_21_48in_02 Storm 19 Lat 2 18in 02	105.90 14.70	48.0 18.0	25.8 35.3	-0.030 -0.015	0.013 0.013	8.43 8.32	248.66 12.86	6,986.94 7,008.40	6,986.80 7,007.71
Storm 21 48in 01	103.90	48.0	57.3	-0.015	0.013	8.27	248.76	6,986.27	6,985.97
Storm_16_48in_05	103.90	48.0	26.8	-0.020	0.013	8.27	203.11	6,984.90	6,984.76
Storm_15_18in_02-W	14.00	18.0	25.5	-0.049	0.013	7.92	23.36	6,975.72	6,975.27
Storm_18_18in_02	12.80	18.0	82.7	-0.050	0.013	7.24	23.47	6,987.22	6,985.99
Storm_19_Lat 3_18in_02	3.80	18.0	29.3	-0.020	0.013	7.05	14.90	7,016.96	7,016.97
Storm_17_36in_07 STRM 29 01	48.90 11.80	36.0 18.0	9.8 66.2	-0.020 -0.008	0.013 0.013	6.92 6.68	94.31 9.40	7,003.97 7,019.74	7,003.91 7,018.90
Storm_19_36in_02	46.90	36.0	144.5	-0.008	0.013	6.63	51.15	6,990.59	6,989.88
Storm 19 36in 01	46.90	36.0	302.2	-0.006	0.013	6.63	51.04	6,989.53	6,988.04
Storm_16_42in_01	125.00	42.0	158.3	-0.002	0.013	6.50	90.47	6,979.36	6,978.75
Storm_28 30in_01	12.20	30.0	90.0	-0.007	0.013	6.44	34.60	7,044.41	7,044.53
Storm_21_42in_03	60.60	42.0	101.2	-0.005	0.013	6.30	71.15	6,988.41	6,988.04
Storm_21_Lat_1_18in_01 Storm 28 30in 01	10.60 26.10	18.0 30.0	19.4 35.4	-0.005 -0.004	0.013 0.013	6.00 5.99	7.16 25.78	6,986.99 7,044.53	6,986.80 7,044.20
Storm_28 30in_01 Storm 22 30in 01	26.10 29.10	30.0	35.4 113.0	-0.004	0.013	5.99	25.78	7,044.53	7,044.20
Storm 17 Lat 1 24in 01	17.20	24.0	8.8	-0.006	0.013	5.47	17.03	6,991.06	6,991.01
Storm_26 24in_01	14.50	24.0	80.7	-0.010	0.013	4.62	22.68	7,022.43	7,022.10
Storm_19_Lat 3_18in_01	6.60	18.0	6.0	-0.020	0.013	3.73	14.84	7,016.99	7,016.97
Storm_22_30in_02	13.70	30.0	79.4	-0.009	0.013	2.79	38.24	7,022.22	7,022.13
Storm_16_Lat_1_18in_01	4.50	18.0	13.2	-0.020	0.013	2.55	15.01	6,984.79	6,984.76
STRM_29_02 Storm_17_Lat_1_24in_02	4.10 7.00	18.0 24.0	79.6 53.4	-0.027 -0.007	0.013 0.013	2.32 2.23	17.27 18.29	7,020.00 6,991.23	7,019.88 6,991.18
Storm 25 30in 01	10.00	30.0	28.2	0.007	0.013	2.23	29.93	6,960.67	6,960.65
		. 00.0		. 0.000				-,-,-,-,-,	

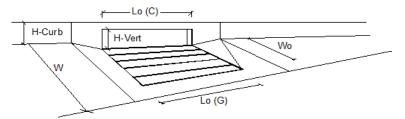
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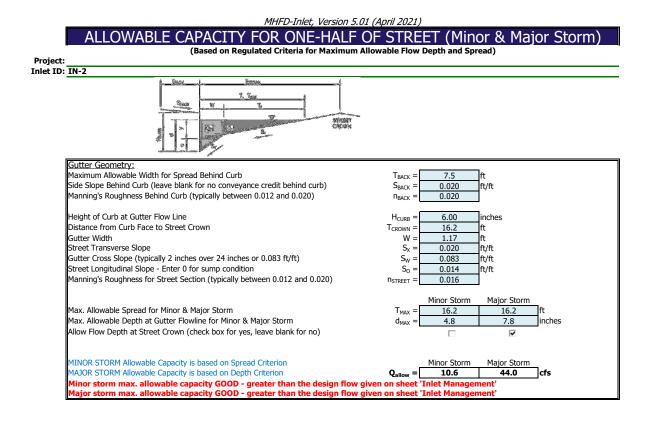
PROPOSED HYDRAULIC CALCULATIONS

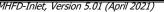


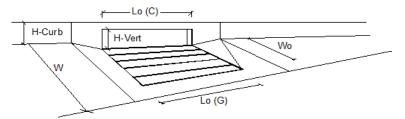




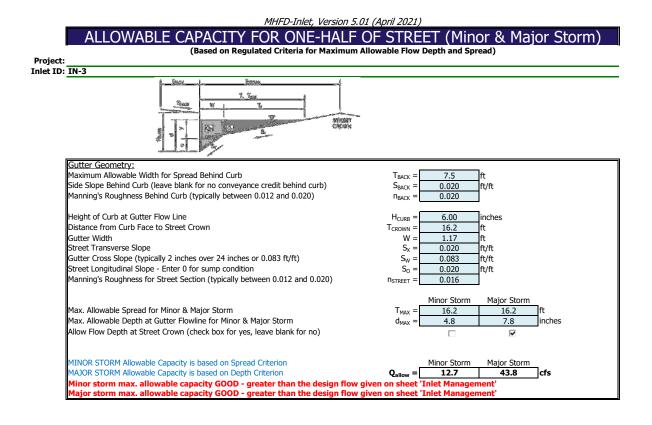
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.5	3.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	1.9	8.0	cfs
Capture Percentage = Q_a/Q_o =	C% =	57	33	%

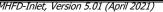


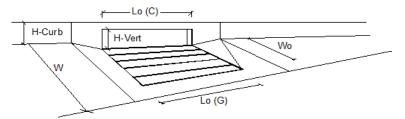




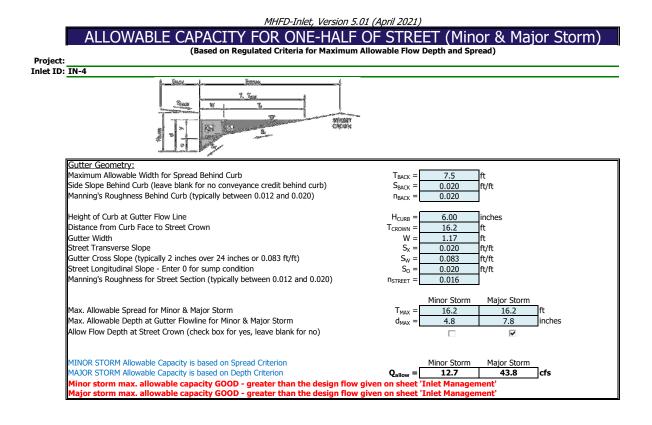
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	-
Total Inlet Interception Capacity	Q =	4.9	9.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	1.7	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	85	%

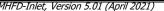


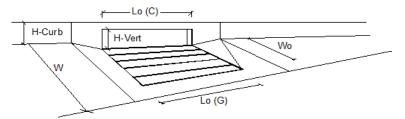




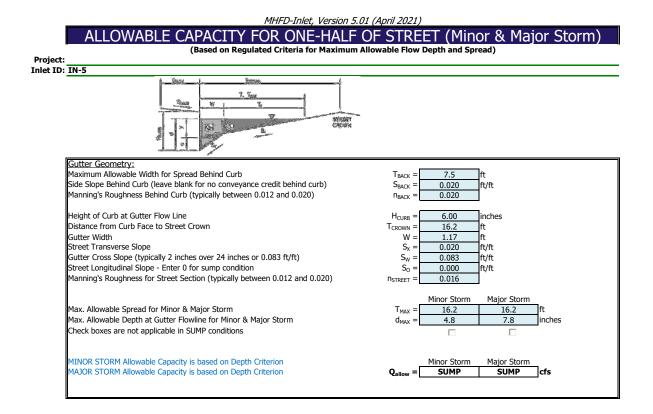
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.3	3.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	1.4	7.9	cfs
Capture Percentage = Q_a/Q_o =	C% =	63	33	%



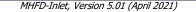


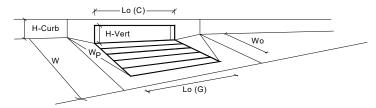


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	-
Total Inlet Interception Capacity	Q =	4.7	10.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.0	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	83	%

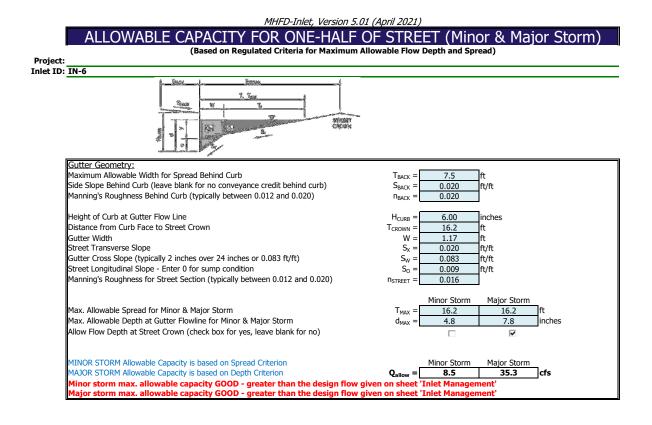


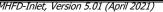
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

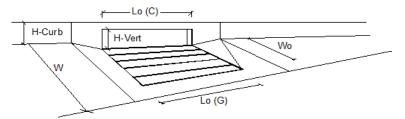




Design Information (Input)	- 5	MINOR	MAJOR	-
Type of Inlet	Type =	CDOT Type R		
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	7.8	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{0}(C) =$	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.55	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.45	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.70	0.88	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
· · · · · · · · · · · · · · · · · · ·	Grate			-
	_	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.8	21.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.0	10.5	cfs

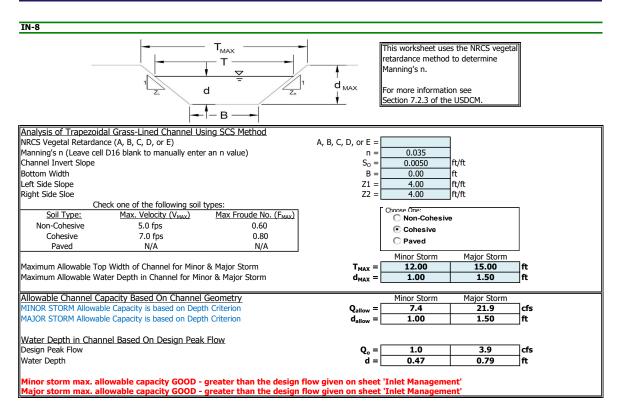




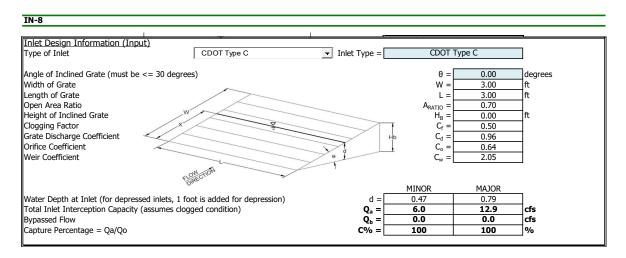


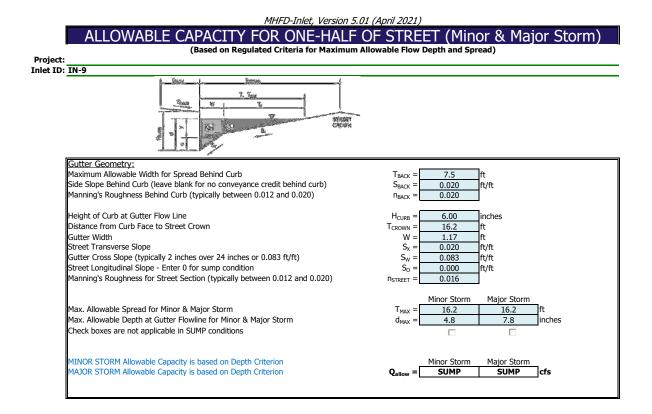
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.2	8.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.1	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	89	%

MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE

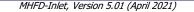


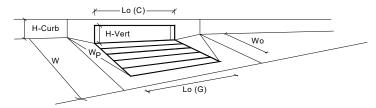
MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE



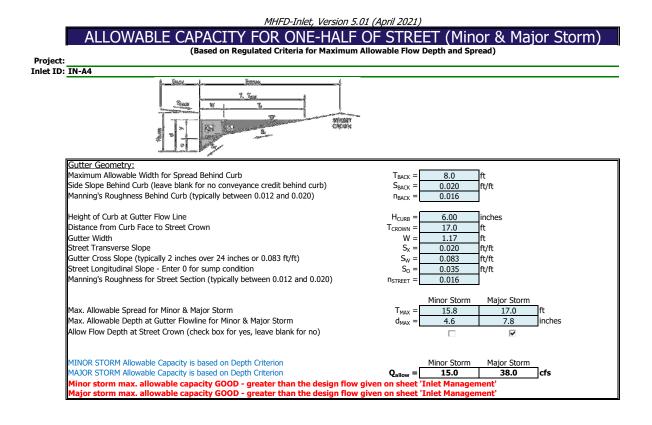


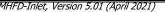
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

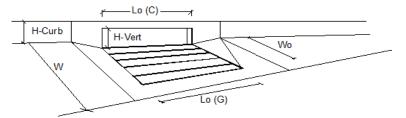




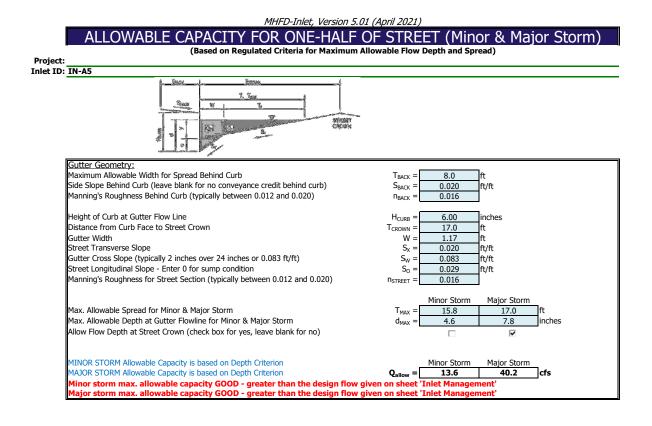
Desire Information (Insut)		MINOD	111100	
Design Information (Input)	- 5	MINOR	MAJOR	-
Type of Inlet	Type =	CDOT Type R		
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	7.8	inches
Grate Information	=	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_{w} (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Law Llond Devfermence Deduction (Calculated)		MINOR	MA100	
Low Head Performance Reduction (Calculated)	. F	-	MAJOR	٦
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.55	ft
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{Combination} =$	0.45	0.74	_
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} =$	0.70	0.88	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.8	21.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	5.4	16.7	cfs

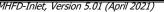


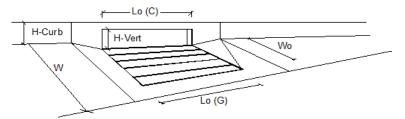




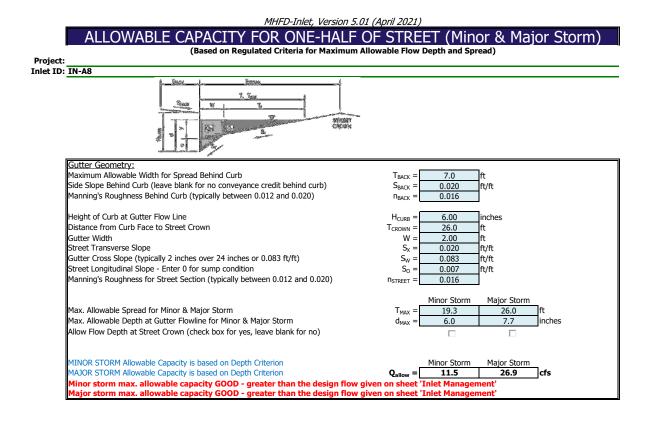
Design Information (Input)	1	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.0	4.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.6	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	89	%

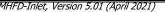


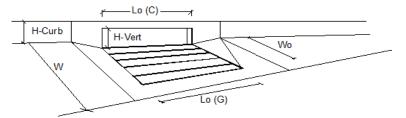




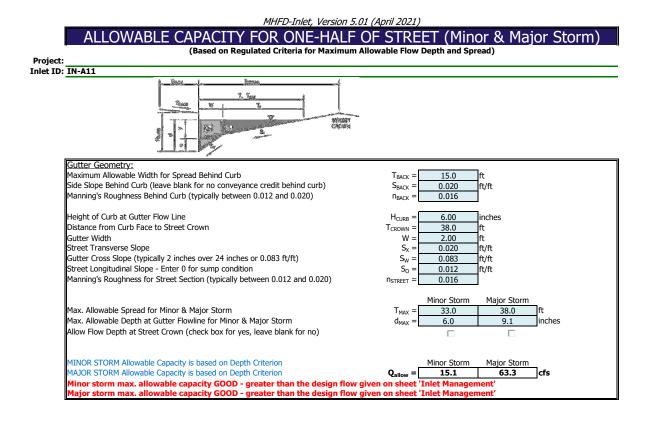
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	-
Total Inlet Interception Capacity	Q =	4.9	13.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	6.5	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	67	%

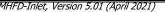


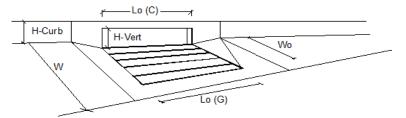




Design Information (Input)	1	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.1	13.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	6.2	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	69	%

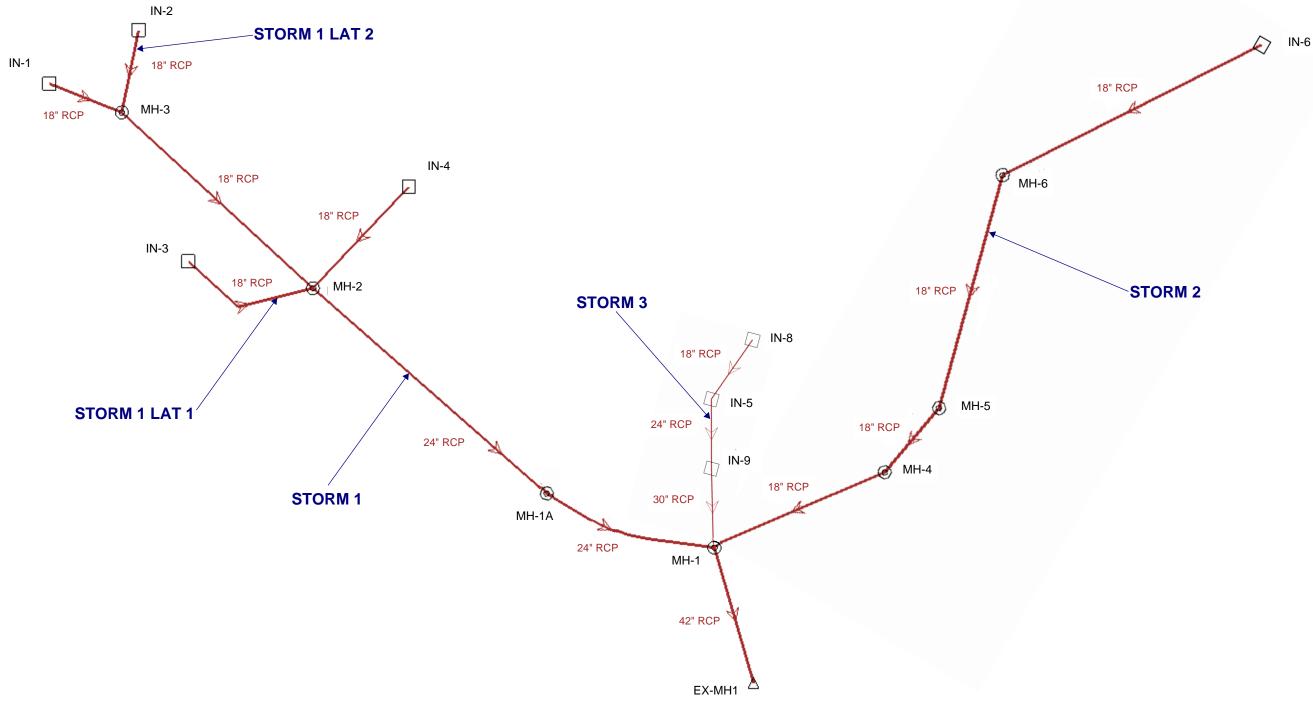


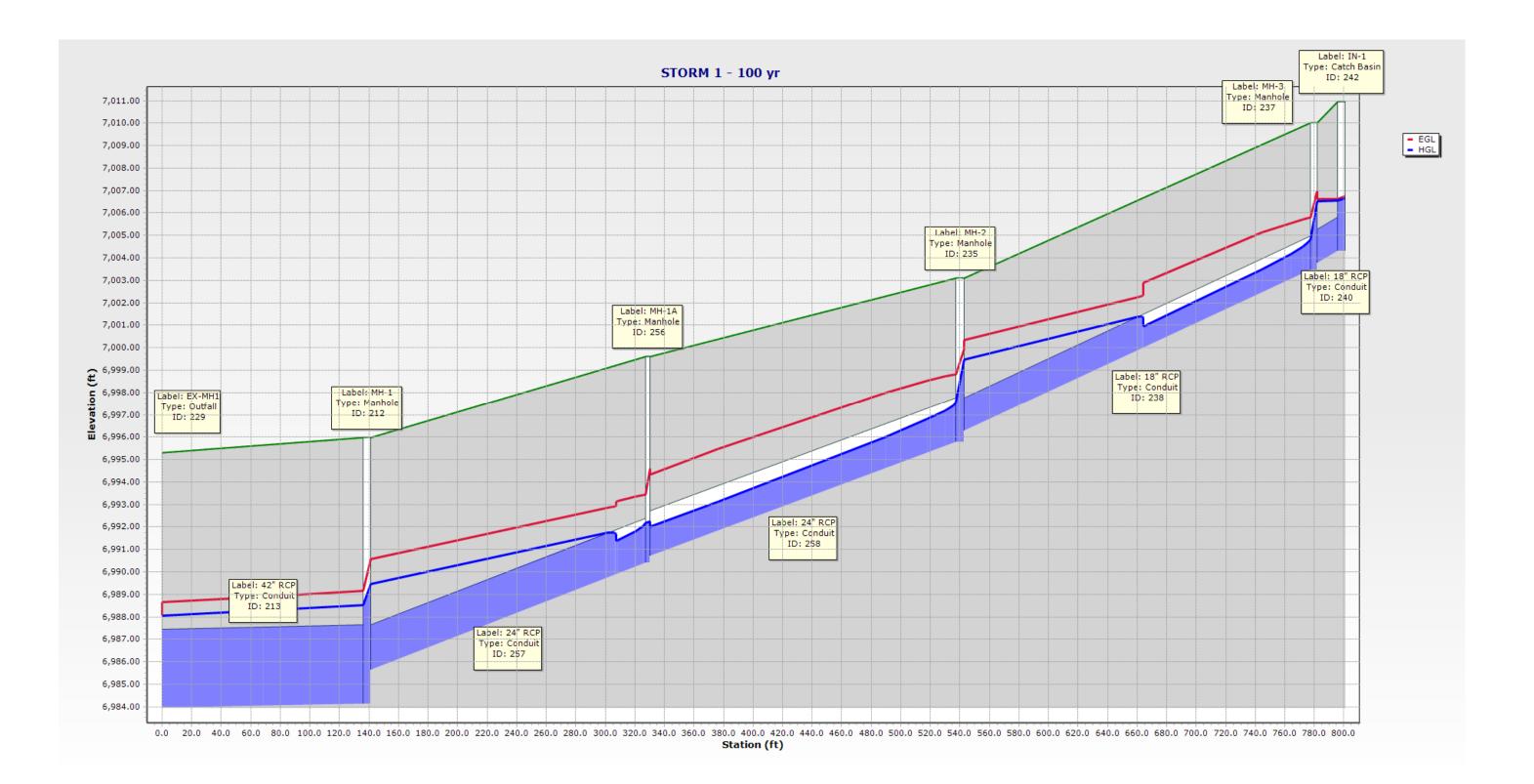


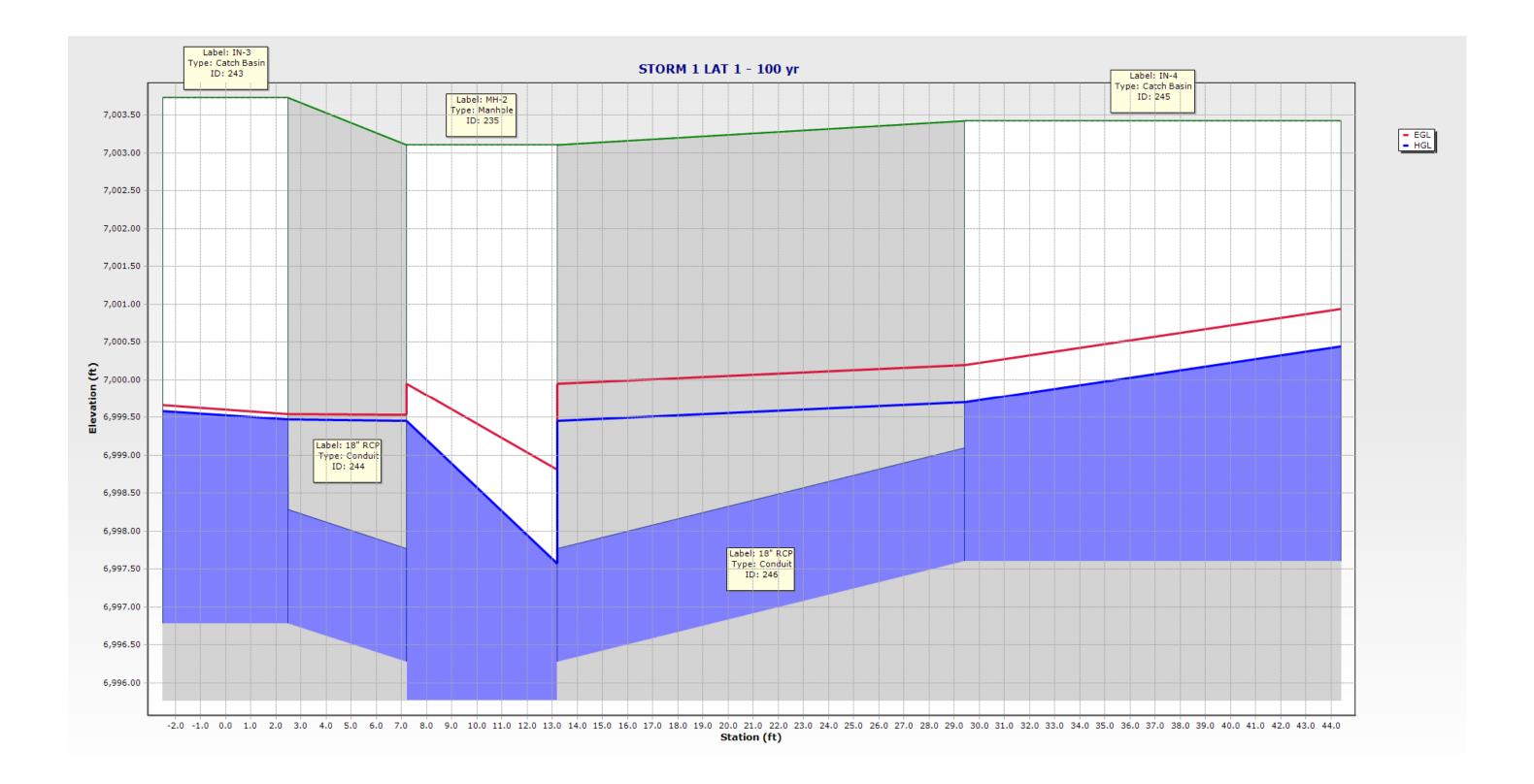


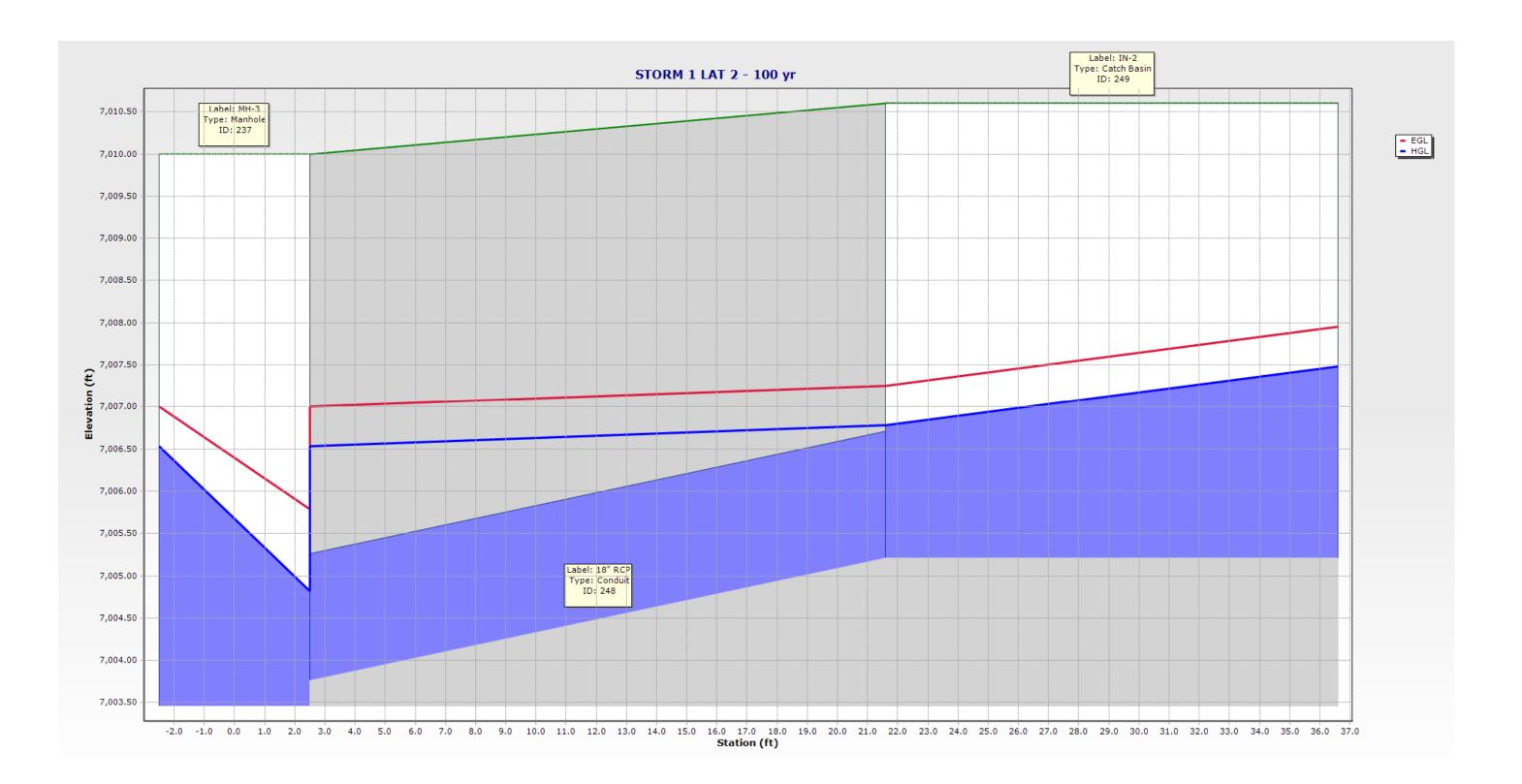
Design Information (Input)	1	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.6	14.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.1	8.1	cfs
Capture Percentage = Q_a/Q_o =	C% =	98	65	%

STORM NETWORK LAYOUT







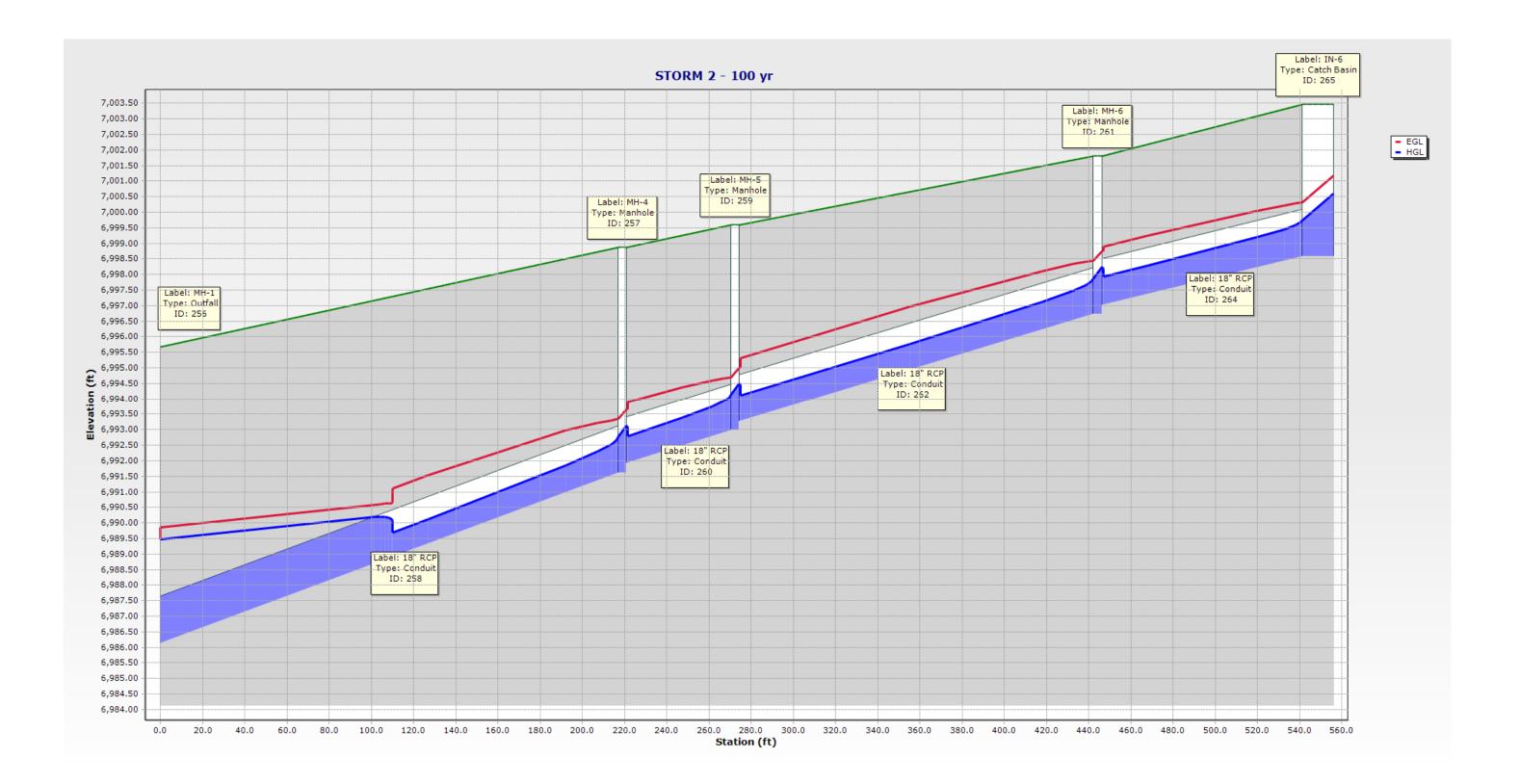


STORM 1: 100 YR FLEX TABLE

Conduit FlexTable: STRM 1,2,3 - 100YR

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
18" RCP	238	MH-3	13.30	73.1	239.5	11.25	(N/A)	0.95	1.36	7,005.79	7,000.33	7,004.82	6,999.45	5.37
18" RCP	240	IN-1	3.80	21.1	18.7	2.15	(N/A)	0.47	0.75	7,006.63	7,006.61	7,006.56	7,006.53	0.02
18" RCP	244	IN-3	3.90	16.6	10.2	2.21	(N/A)	0.41	0.76	6,999.54	6,999.53	6,999.47	6,999.45	0.01
18" RCP	246	IN-4	10.00	42.7	26.7	5.66	(N/A)	0.68	1.22	7,000.19	6,999.95	6,999.70	6,999.45	0.24
18" RCP	248	IN-2	9.70	41.4	29.1	5.49	(N/A)	0.67	1.20	7,007.25	7,007.00	7,006.78	7,006.53	0.25
24" RCP	257	MH-1A	26.60	74.3	190.2	12.48	(N/A)	1.28	1.80	6,993.44	6,990.59	6,992.20	6,989.48	2.72
24" RCP	258	MH-2	26.60	76.0	211.3	12.26	(N/A)	1.30	1.80	6,998.81	6,994.35	6,997.57	6,992.01	5.56
42" RCP	213	MH-1	60.50	166.9	138.6	6.29	(N/A)	(N/A)	2.44	6,989.16	6,988.65	6,988.54	6,988.04	0.50
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	(Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description						
7,006.53	5.49	1.770	1.71	7,003.11	7,010.00	6,996.27		Circle - 18.0 in						
7,006.67	2.15	1.500	0.11	7,010.00	7,010.95	7,003.76		Circle - 18.0 in						
6,999.58	2.21	1.500	0.11	7,003.11	7,003.73	6,996.27		Circle - 18.0 in						
7,000.44	5.66	1.500	0.75	7,003.11	7,003.42	6,996.27		Circle - 18.0 in						
7,007.49	5.49	1.500	0.70	7,010.00	7,010.60	7,003.76		Circle - 18.0 in						
6,992.26	12.26	0.050	0.06	6,995.98		6,985.64		Circle - 24.0 in						
6,999.45	5.66	1.520	1.88	6,999.59	7,003.11	6,990.71	-	Circle - 24.0 in						
6,989.48	8.47	1.520	0.93	6,995.29	6,995.98	6,983.96	6,984.14	Circle - 42.0 in						

StormCAD [10.03.04.53] Page 1 of 1

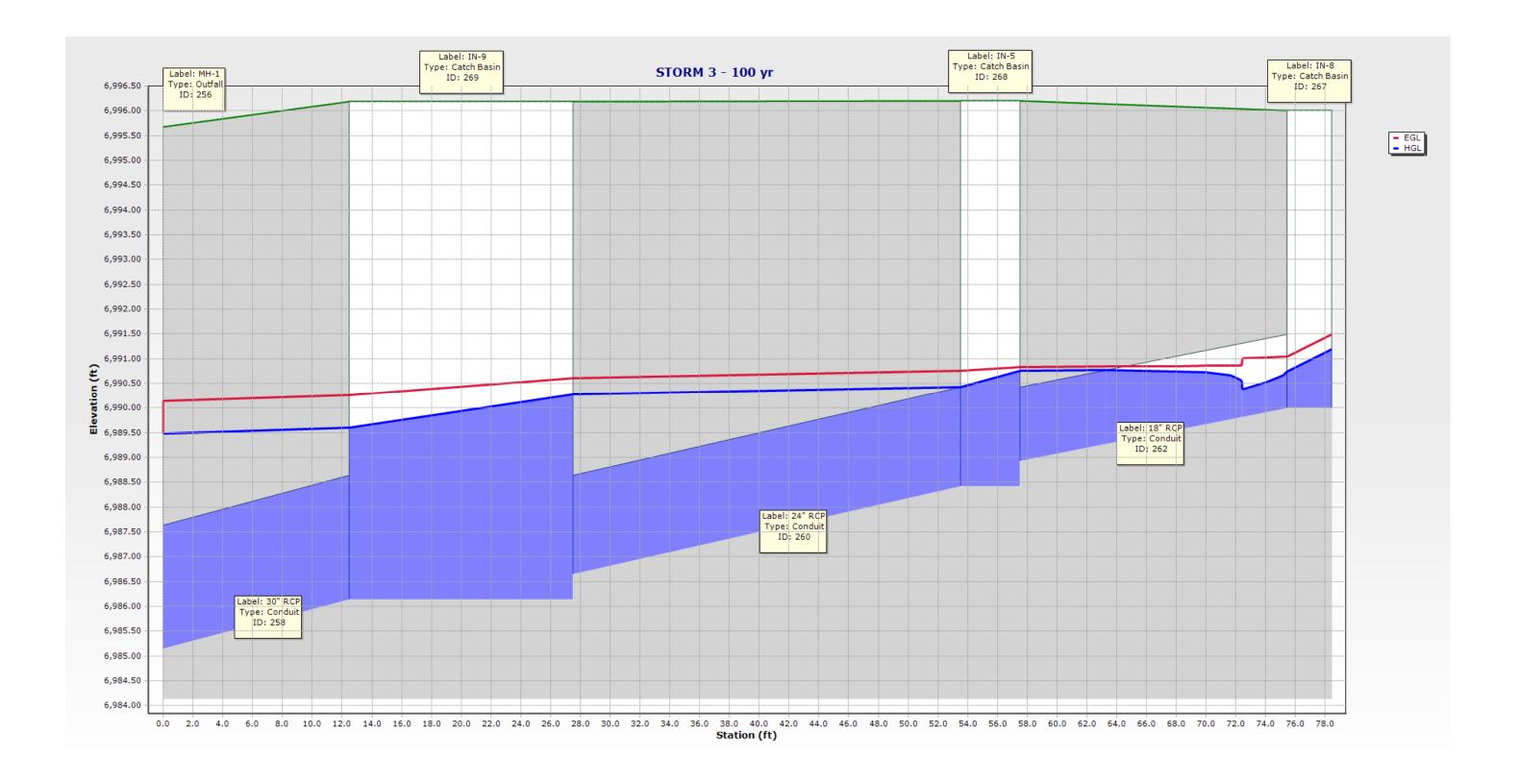


STORM 2: 100 YR FLEX TABLE

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
				(70)						(10)	(it)			
18" RCP	258	MH-4	8.80	53.0	219.0	9.54	(N/A)	0.78	1.15	6,993.34	6,989.87	6,992.77	6,989.48	3.29
18" RCP	260	MH-5	8.80	59.5	53.4	8.74	(N/A)	0.83	1.15	6,994.70	6,993.65	6,994.13	6,993.13	0.99
18" RCP	262	MH-6	8.80	59.2	171.8	8.76	(N/A)	0.83	1.15	6,998.44	6,995.01	6,997.87	6,994.49	3.38
18" RCP	264	IN-6	8.80	68.3	104.4	7.85	(N/A)	0.91	1.15	7,000.31	6,998.75	6,999.74	6,998.23	1.50
Upstream	Upstream	Upstream	Upstream	Elevation Ground	Elevation Ground	Invert (Start)	Invert (Stop)	Conduit						
Structure	Structure	Structure	Structure	(Start)	(Stop)	(ft)	(ft)	Description						
Hydraulic Grade	Velocity (In-	Headloss	Headloss	(ft)	(ft)									
Line (In)	Governing)	Coefficient	(ft)											
(ft)	(ft/s)													
6,993.13	5.74	0.640	0.37	6,995.68	6,998.87	6,986.14	6,991.62	Circle - 18.0 in						
6,994.49	5.74	0.640	0.37	6,998.87	6,999.60	6,991.92	6,992.98	Circle - 18.0 in						
6,998.23	5.74	0.640	0.37	6,999.60	7,001.80	6,993.28	6,996.72	Circle - 18.0 in						
7,000.59	6.06	1.500	0.86	7,001.80	7,003.46	6,997.02	6,998.59	Circle - 18.0 in						

Conduit FlexTable: STRM 1,2,3 - 100YR

StormCAD [10.03.04.53] Page 1 of 1



STORM 3: 100 YR FLEX TABLE

Conduit FlexTable: STRM 1,2,3 - 100YR

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
18" RCP	262	IN-8	3.90	16.6	21.4	9.84	(N/A)	0.41	0.76	6,991.04	6,990.83	6,990.75	6,990.76	-0.01
24" RCP	260	IN-5	14.40	28.4	35.5	4.58	(N/A)	0.73	1.37	6,990.75	6,990.61	6,990.42	6,990.28	0.14
30" RCP	258	IN-9	32.10	35.0	20.0	6.54	(N/A)	1.02	1.93	6,990.27	6,990.14	6,989.60	6,989.48	0.12
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description						
6,991.19	4.37	1.500	0.45	6,996.20	6,996.00	6,988.92	6,989.99	Circle - 18.0 in						
6,990.76	2.21	1.020	0.33	6,996.19	6,996.20	6,986.64	6,988.42	Circle - 24.0 in						
6,990.28	4.58	1.020	0.68	6,995.68	6,996.19	6,985.14	6,986.14	Circle - 30.0 in						

StormCAD [10.03.04.53] Page 1 of 1 BACKGROUND

Subdivision: Location: Design Storm:	El Paso Co	anch Fil ounty	ing No.	2												Ca	oject Na Project Iculate Checke [t No.: d By: d By:	25188	3.01	nch Sul	odivis	sion
	r —	1		DIRF	CT RU	NOFF			T	OTAL F	RUNOF	F	STRF	ET/SW	/ALF		PIF				/EL TIN	1F	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	A1	2.06	0.51	9.7	1.05	4.17	4.4					0.2	0.04	3.3	4.2	1.01	2.0	18	652 5	3.6 7.2	3.0 0.0	O On-grade inlet, carryover flow to DP 5 0 Piped to DP 1.0
	2	A2	0.82	0.53	9.1	0.44	4.27	1.9								1.9	0.44	2.0	18	27	5.8		On-grade inlet 1 Piped to DP 1.0
	1.0								9.7	1.45	4.17	6.0				6.0	1.45	3.0	18	335	9.1	0.6	6 Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.47	15.0	3.16	3.53	11.1					1.6	0.47	2.9	9.5	2.69		18	426 36	3.4	2.1 0.0	1 On-grade inlet, carryover flow to DP 5 0 Piped to DP 1.1
	4	A4		0.60			4.10	3.7					0.1	0.03	2.9	3.6	0.88	4.7	18	395 0	3.4	1.9	9 On-grade inlet, carryover flow to DP 5 0 Piped to DP 1.1
	1.1								15.0	3.57	3.52	12.6				12.6		1.0	24	74	7.4	0.2	2 Sum of DP 3 & DP 4, piped to DP 1.2
	1.2									5.02						17.6	5.02	3.3	24	319	12.5		4 Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.81	5.0	0.43	5.17	2.2															Overland Flow to DP1.3A
	6	A6	1.37	0.58	10.0	0.79	4.14	3.3								3.3	0.79	2.0	18	0	6.7	0.0	On-grade inlet 0 Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.22	4.14	5.0				5.0	1.22	1.0	24	36	5.7	0.1	1 Sum of DP 6 & DP 6A, piped to DP 1.3
	5	A5	1.70	0.59	9.9	0.99	4.14	4.1	17.0	1.53	3.33	5.1				5.1	1.53	2.0	18	0	7.6	0.0	On-grade inlet 0 Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	7.77	3.33	25.9				25.9	7.77	1.1	36	620	9.2	1.1	1 Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.45	18.3	8.55	3.22	27.5								27.5	8.55	1.5	42	20	10.3	0.0	Future storm infrastructure from Copper Chase Subdivision D Piped to DP 1.4
	1.4								18.4	16.32	3.22	52.5				52.5	16.32	0.5	48	26	8.2	0.1	1 Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1.48	0.56	13.9	0.83	3.63	3.0								3.0	0.83	2.0	18	20	6.6	0.1	On-grade inlet, carryover flow to DP 11 1 Piped to DP 1.5
	1.5								18.4	17.15	3.21	55.1				55.1	17.15	0.5	48	91	8.3	0.2	2 Sum of DP 1.4 & DP 8, piped to DP 1.6
	9	A9	0.61	0.73	8.7	0.44	4.34	1.9	8.7	0.48	4.34	2.1				2.1	0.48	2.0	18	13	5.8	0.0	On-grade inlet D Sum of Sub-basin A9 & carryover flows fro <mark>m DP 16, piped to DP 1.6</mark>
	1.6								18.6	17.63	3.20	56.4	0.5	0.11	4.5	56.4	17.63	0.5	48			0.2	2 Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.79	7.9	2.05	4.49	9.2						0.11		8.7	1.94	2.5	18	955 118		6.5 0.2	5 On-grade inter, carry over flow to DP 20 2 Piped to DP 1.7 2 On-grade inter, carry over flow to DP 20
	11	A11	2.89	0.76	8.7	2.20	4.34	9.5					0.6	0.15	1.5	8.9	2.05	2.5	18	1049 0		0.0	1 On-grade inlet, carryover flow to DP 21 D Piped to DP 1.7
	1.7								8.7	3.99	4.34	17.3				17.3	3.99	1.0	24	8	7.9	0.0	0 Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								18.8	21.63	3.18	68.8				68.8	21.63	2.0	54	517	14.4	0.6	6 Sum of DP 1.6 & DP 1.7, piped to DP 2.7 Future flow released from Barbarick Subdivision
	OS2	OS2	17.00	0.49	14.0	6.25	2.20	13.8								13.8	6.25	1.0	30	787	7.5	1.7	Pluce now release from Barbarck Subdivision 7 Piped to DP 2.0 Type C inlet
	12	A12	3.87	0.13	11.9	0.49	3.86	1.9								1.9	0.49	2.0	18	17	5.6	0.1	Piped to DP 2.0
	2.0	 							15.7	6.74	3.45	23.2				23.2	6.74	1.0	48	52	8.4	0.1	1 Sum of DP OS2 & DP 12, Piped to DP 2.1 Future storm infrastructure from Sterling Ranch Phase 2
	13	A13	9.65	0.45	14.0	4.34	3.62	15.7								15.7	4.34	1.5	30	200	9.1	0.4	4 Piped to DP 2.1

Subdivision:	Storling Do	noh Fili	ng No. 1	- -												Pro	oject Na Project	ame:	Sterli	ng Ran	ich Sul	odivisi	on
Location:	El Paso Cou		ng no. 2	2												Cal	culáteo	d By:		5.01			
Design Storm:	5-Year															C	heckeo E	d By: Date:	8/16/	21			
				DIRE	CT RUI	NOFF			TC	OTAL R	UNOF	F	STREE	ET/SW	ALE		PIP	ΡĒ		TRAV	EL TIN	1E	
											_								les)				
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	(min)	C*A (Ac)	(in/hr)	(cfs)	(min)	C*A (ac)	(in/hr)	Q (cfs)	reet/swale (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	ipe Size (inches)	-ength (ft)	/elocity (fps)	(min)	REMARKS
	De	Ba	Are	Ru	t.	Š	 	Ö	tc	ڭ	I (i	ŏ	Qstr	Š	Slo	Q	ť	Slo	Pip	Ler	Vel	t _t (
	2.1								15.9	11.08	3.44	38.1				38.1	11.08	1.6	48	65	11.4	0.1	Sum of DP 2.0 & DP 13, piped to DP 2.5
	OS3	OS3	28.70	0.49	19.0	14.06	1.25	17.6								17.6	14.06	1.0	30	719	8.0		Future flow released from Barbarick Subdivision Piped to DP 2.2
	14	A14	11.76	0.39	15.3	4.59	3.49	16.0								16.0	4.59	1.0	30	20	7.8		Future flow released from School Site Piped to DP 2.2
	2.2								20.5	18.65	3.05	56.9				56.9	18.65	1.5	48	773	12.4	1.0	 Sum of DP OS3 & DP 14, piped to DP 2.3
	15	A15	2.91	0.52	14.9	1.52	3.53	5.4								5.4		1.3		35	6.5	0.1	On-grade inlet
	16	A16	2.34	0.54				4.4					0.1	0.04	0.8	4.3				697	1.8	6.5	On-grade inlet, carryover flow to DP 9 Piped to DP 2.3
	2.3	71.0	210.	0.0 .	1	Ties	0.00		15.0	2.73	3 5 2	9.6				9.6					7.6		Sum of DP 15 & DP 16, piped to DP 2.4
	2.3									21.38							21.38						Sum of DP 2.2 & DP 2.3, piped to DP 2.5
	2.5									32.46		96.6					32.46				15.8		Sum of DP 2.1 & DP 2.4 piped to DP 2.6
	17	A17	1.76	0.21	13.7	0.38	3.66	1.4	21.0	32.70	2.70	70.0				1.4		1.0	18	24			Type C inlet Piped to DP 2.4 piped to DP 2.0 Piped to DP 2.6
	2.6	A17	1.70	0.2 1	10.7	0.50	3.00	1.5	21.6	32.84	2.08	07.8					32.84						Sum of DP 2.5 & DP 17, piped to DP 2.7
	2.7	410	5.07	0.04	1/ 4	1.00	2.20	- 12	21.0	54.47	2.91	102.0					54.47	0.6		220			Sum of DP1.8 & DP 2.6, piped to DP 2.8 Area inlet
	18	A18	5.27			1.28			┟──┤	\vdash						4.3				24			Piped to DP 2.6 Area inlet
	19	A19	31.85	0.45	25.8	14.33	2.71	38.8		$\left \right $							14.33				22.0		Piped to DP 2.6
	2.8						\vdash]		70.08			189.8	70.08	0.5	189.8	70.08	0.6	78	145 584	12.1 1.4		Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0. Detention Pond
	3.0						\vdash			70.08													Trickle channel conveyance to DP 3.2 On-grade inlet
	20	A20	1.83	0.81	8.0	1.48	4.47	6.6	8.0	1.59	4.47	7.1	0.1	0.03	1.5	7.1	1.59	1.0	24	105	6.4		Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0 On-grade inlet
ļ	21	A21	1.93	0.82	8.7	1.57	4.33	6.8	8.7	1.72	4.33	7.4				7.3	1.68	2.5	18	0	9.0	0.0	Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9						\square		8.7	3.27	4.33	14.2	14.2	3.27	0.5	14.2	3.27	2.0	24	58 568			Sum of DP 20 & DP 21,piped to DP 3.1 Detention Pond
	3.1								8.7	3.27	4.33	14.2	14.2	3.21	0.5					200	1.4	0.7	Trickle channel conveyance to DP 3.2
	22	A22	8.68	0.11	23.3	0.95	2.86	2.7															Detention Pond Overland flow to DP 3.2
	OS4	OS4	5.08	0.20	29.5	1.02	2.51	2.6					2.6	1.02	13.0					113	5.4		Existing topography Overland flow to DP 4.1
	3.2								29.8	75.32	2.49	187.5											Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8
	Pond W5								29.8	1.45	2.49	3.6				3.6	1.45	2.0	48	58	6.2	0.2	Outlet structure release to DP 4.8
	23	B1	2.98	0.90	17.6	2.68	3.29	8.8					0.4	0.12	2.0		2.56			1399	2.0	12.0	On-grade inlet Piped to DP 4.0

Subdivision: Location: sign Storm:	El Paso Cour		g No. 2													Ca	oject N Projec alculate Checke	t No.: d By: d By:	2518 AAM	8.01	nch Su	ubdivi	sion
																		Date:	1/5/2				
				DIF	RECT R	JNOFF			T	OTAL F	RUNOF	F	STRE	ET/SWA	LE		PIPE	E	-	TRAV	'EL TII	ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	A1	2.06	0.65	9.7	1.34	7.01	9.4		Ĭ			2.8	0.40	3.3	6.6	0.94	2.0	18	-652 5	3.6 8.2	3.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82			0.54	7.17	3.9					0.1	0.01	3.3	3.8	0.53	2.0	18	639 27	3.6 7.0	2.9	On-grade inlet, carryover flow to DP 6 Piped to DP 1.0
	1.0	R2	0.02	0.00	7.1	0.54	7.17	3.7	9.7	1 47	7.00	10.2			-	10.3	1.47						
			(7(0.40	15.0	4 17	5.00	04.7	9.1	1.47	7.00	10.3	10.0	1.69	2.9					426 36	10.8 3.4 13.6	2.1	Sum of DP 1 & DP 2, piped to DP 1.2 On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	3	A3	<u>6.76</u>			4.17	5.92	24.7					1.6	0.24	2.9	14.7	2.48		18	395	3.4	1.9	On-grade inlet, carryover flow to DP 5
	4	A4	1.51	0.71	10.2	1.08	6.88	7.4							\rightarrow	5.8							Piped to DP 1.1
	1.1								15.0		5.91				\dashv	19.7	3.33						Sum of DP 3 & DP 4, piped to DP 1.2
	1.2		-						15.1	4.80	5.89	28.2			\rightarrow	28.2	4.80	3.3	24	319	13.9	0.4	Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.88	5.0	0.47	8.68	4.1					1.3	0.18	0.7					696	1.7	7.0	Overland Flow to DP1.3A On-grade inlet, carryover flow to DP 8
	6	A6	1.37	0.70	10.0	0.95	6.94	6.6	10.0	0.96	6.94	6.7			<u> </u>	5.4	0.78	2.0	18	0	7.7	0.0	Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.25	6.94	8.7	6.5	1.17	0.7	8.7	1.25	1.0	24	36 664	6.7 1.7		Sum of DP 6 & DP 6A, piped to DP 1.3 On-grade inlet, carryover flow to DP 8
	5	A5	1.70	0.70	9.9	1.19	6.95	8.3	17.0	3.51	5.59	19.6	0.0			13.1	2.34	2.0	18	0			Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	8.39	5.59	46.9			\rightarrow	46.9	8.39	1.1	36	620	10.7	1.0	Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4 Future storm infrastructure from Copper Chase Subdivision
	7	A7	19.00	0.59	18.3	11.21	5.41	60.6							$ \rightarrow $	60.6	11.21	1.5	42	20	12.7	0.0	Piped to DP 1.4
	1.4								18.4	19.60	5.40	105.9	1.0			105.9	19.60	0.5	48	26			Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1.48	0.70	13.9	1.04	6.10	6.3	23.7	2.63	4.76	12.5	1.9	0.41	0.7	10.6	2.23	2.0	18	195 20	1.7 9.1		On-grade inlet, carryover flow to DP 11 Sum of Sub-basin A8 & Carryover flows from DP5, DP 6 & DP 15, Piped to DP 1.5
	1.5								23.7	21.83	4.76	103.9				103.9	21.83	0.5	48			0.2	Sum of DP 1.4 & DP 8, piped to DP 1.6
	9	A9	0.61	0.83	8.7	0.51	7.29	3.7	21.2	0.95	5.04	4.8	0.3	0.05	0.7	4.5	0.89	2.0	18	140 13	1.7 7.3	1.4 0.0	On-grade inlet, carryover flow to DP 11 Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								23.9	22.72	4.74	107.7				107.7	22.72	0.5	48		9.1	0.2	Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.88	7.9	2.29	7.53	17.3					4.5	0.59	1.5	12.8	1.70	2.5	18	955 118	2.4 10.3	6.5	On-grade inlet, carryover flow to DP 20 Pined to DP 1.7
	11	A11	2.89	0.86	8.7	2.48	7.28	18.1	10.6	2.94	6.77	19.9	6.1	0.90	1.5	13.8	2.04	2.5	18	1049	2.4	7.1	On-grade inlet, carryover flow to DP 21 Sum of Sub-basin A11 & carryover flows from DP 8 & DP 9, piped to DP 1.7
	1.7								10.6		6.77				1	25.3	3.74					1	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8									26.45					\neg	125.0	26.45				17.0		Sum of DP 1.6 & DP 1.7, piped to DP 2.7
	OS2	OS2	17.00	0.62	12.0	10.54	3.71	39.1	2 1.0	20.40		.20.0			\dashv	39.1	10.54						Piped to DP 2.0
															\dashv							1	Type C inlet
	12	A12	3.87	0.38	11.9	1.47	6.49	9.5	10.4	10.01	(00	74.5			\dashv	9.5	1.47						Piped to DP 2.0
	2.0								13.4	12.01	6.20	/4.5			\dashv	74.5	12.01				11.6		Sum of DP OS2 & DP 12, Piped to DP 2.1 Future storm infrastructure from Sterling Ranch Phase 2
	13	A13	9.65	0.59	14.0	5.69	6.08	34.6								34.6	5.69	1.5	30	200	11.0	0.3	Piped to DP 2.1

Subdivision: Location: sign Storm:	El Paso Cour	ch Filin Ity	g No. 2									-					roject N Projec alculate Checke	t No.: d By:	2518 AAM	8.01	inch Si	ubdivi	sion
				DIR	ECT RI	UNOFF			<u> </u>	TOTAL	RUNO	FF	STR	ET/SW	ALE	1	PIPE				/EL TI	MF	
					LOTIN								(cfs)						ches)				
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (G	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	2.1								14.3	17.70	0 6.02	106.6				106.6	17.70	1.6	48	65	15.1	0.1	Sum of DP 2.0 & DP 13, piped to DP 2.5
	OS3	OS3	28.70	0.62	15.0	17.79	2.75	48.9)							48.9					10.0		Future flow released from Barbarick Subdivision Piped to DP 2.2
	14	A14	11.76						,							37.9							Future flow released from School Site Piped to DP 2.2
	2.2								16.2	24.26	5 5.72	138.7				138.7	24.26	1.5	48	773	15.5	0.8	Sum of DP OS3 & DP 14, piped to DP 2.3
	15	A15	2.91	0.68	14.9	1.98	5.93	11.7	,				1.4	0.24	0.7	10.3	1.74		18	724 35	1.7	7.2	On-grade inlet, carryover flow to DP 8 Piped to DP 2.3
	16	A16	2.34	0.69	14.7	1.61	5.96	9.6	ò				2.6	0.44	0.8	7.0	1.17	2.0	18	697 12	1.8 8.2	6.5 0.0	On-grade inlet, carryover flow to DP 9 Piped to DP 2.3
	2.3								15.0	2.91	1 5.91	17.2				17.2	2.91	1.6	48	15	9.0	0.0	Sum of DP 15 & DP 16, piped to DP 2.4
	2.4								17.0	27.17	7 5.59	151.9				151.9	27.17	1.6	48	19	16.2	0.0	Sum of DP 2.2 & DP 2.3, piped to DP 2.5
	2.5								17.1	44.8	7 5.59	250.7				250.7	44.87	2.0	60	839	20.1	0.7	Sum of DP 2.1 & DP 2.4 piped to DP 2.6
	17	A17	1.76	0.44	13.7	0.77	6.14	4.7	,							4.7	0.77	1.0	18	24	5.7	0.1	Type C inlet Piped to DP 2.6
	2.6								17.7	45.64	1 5.49	250.4				250.4	45.64	2.0	60	32	20.2	0.0	Sum of DP 2.5 & DP 17, piped to DP 2.7
	2.7								24.5	72.10	4.67	336.8				336.8	72.10	0.6	78	220	13.7	0.3	Sum of DP1.8 & DP 2.6, piped to DP 2.8
	18	A18	5.27	0.47	16.4	2.47	5.68	14.0)							14.0	2.47	1.0	18	24	7.9	0.1	Area inlet Piped to DP 2.6
	19	A19	31.85	0.59	25.8	18.79	4.55	85.4	ı							85.4	18.79	1.0	18	24	48.4	0.0	Area inlet Piped to DP 2.6
	2.8								25.8	93.36	5 4.55	424.4				424.4	93.36	0.6	78				Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0.
	3.0								25.8	93.36	5 4.55	424.4		93.36						564	1.4	6.6	Detention Pond Trickle channel conveyance to DP 3.2
	20	A20	1.83	0.89	8.0	1.63	7.50	12.2	2 14.4	2.22	2 6.02	13.4	2.3	0.38	1.5	11.1	1.84	1.0	24	105	7.2	0.2	On-grade inlet Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0
	21	A21	1.93	0.90	8.7	1.73	7.28	12.6	5 15.8	2.63	3 5.77	15.2	3.3	0.57	1.5	11.9	2.06	2.5	18	0	10.2	0.0	On-grade inlet Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9								15.8	3.91	1 5.77	22.5				22.5	3.91	2.0	24		11.0	0.1	Sum of DP 20 & DP 21,piped to DP 3.1
	3.1								15.8	3.91	1 5.77	22.5	22.5	3.91	0.5					568	1.4	6.7	Detention Pond Trickle channel conveyance to DP 3.2
	22	A22	8.68	0.37	23.3	3.21	4.80	15.4	ļ														Detention Pond Overland flow to DP 3.2
	OS4	OS4	5.08	0.40	29.5	2.03	4.21	8.5	5				8.5	2.03	13.0					113	5.4	0.3	Existing topography Overland flow to DP 3.2
	3.2								29.8	102.50	4.18	428.2											Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8
	Pond W5								29.8	34.84	4.18	145.5				145.5	34.84	2.0	48	58	17.5	0.1	Outlet structure release to DP 4.8
	23	B1	2.98	0.96	17.6	2.86	5.51	15.8					3.6	0.65	2.0	12.2				1394	2.1	11.0	On-grade inlet Piped to DP 4.0
	24	B2	3.89				5.51						6.5	1.17	2.0	14.1			30	1394 0	2.1	11.0	On-grade inlet Piped to DP 4.0

EXISTING CONDITIONS PIPE ROUTING FOR COMPARISON (5 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision:	Storling Ra	nch Fili	na No	2												Pro	oject Na Project	ame:	Sterlii 25189	ng Rai	nch Su	ubdivis	ion
Location:	El Paso Co		ing No	2												Ca	culated	d By:	AAM	5.01			
Design Storm:	5-Year															(hecked Г		1/5/2	1			
	DIRECT RUNOFF TOTAL RUNOFF																						
				DIRE	CT RUI	NOFF			10) I AL K	UNOFI		STREE	1/SW	ALE		PIP	ΥĽ	0	IRAV	/EL TII	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	(min)	C*A (Ac)	(in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	ipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	De	Bas	Are	Rui	ر د	š.	i)) O	tc	C*/	I (i	0				Q	C*/	Slo	Pip				
	1	A1	2.06	0.51	9.7	1.05	4.17	4.4					0.2	0.04	3.3	4.2	1.01	2.0	18	652 5	3.6	3.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82	0.53	9.1	0.44	4.27	1.9								1.9	0.44	2.0	18	27	5.8	01	On-grade inlet Piped to DP 1.0
		7.2	0.02	0.00	7.1	0.11	1.27	,															
	1.0								9.7	1.45	4.17	6.0	1.6	0.47	2.9	6.0				426	3.4	2.1	Sum of DP 1 & DP 2, piped to DP 1.2 On-grade inlet, carryover flow to DP 5
	3	A3	6.76	0.47	15.0	3.16	3.53	11.1					0.1	0.03	2.0	9.5	2.69	4.7	18	36 395	12.2		Piped to DP 1.1 On-grade inlet, carryover flow to DP 5
	4	A4	1.51	0.60	10.2	0.91	4.10	3.7					0.1	0.03	2.7	3.6	0.88	4.7	18	0		0.0	Piped to DP 1.1
	1.1								15.0	3.57	3.52	12.6				12.6	3.57	1.0	24	74	7.4	0.2	Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.2	5.02	3.50	17.6				17.6	5.02	3.3	24	319	12.5	0.4	Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.81	E O	0.42	5.17	2.2	10.2	0.02	0.00	1710				11.0	0.02	0.0	2.	017	12.10	0.1	Overland Flow to DP1.3A
																							On-grade inlet
	6	A6	1.37	0.58	10.0	0.79	4.14	3.3								3.3	0.79	2.0	18	0	6.7	0.0	Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.22	4.14	5.0				5.0	1.22	1.0	24	36	5.7	0.1	Sum of DP 6 & DP 6A, piped to DP 1.3 On-orade inlet
	5	A5	1.70	0.59	9.9	0.99	4.14	4.1	17.0	1.53	3.33	5.1				5.1	1.53	2.0	18	0	7.6	0.0	Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	7.77	3.33	25.9				25.9	7.77	1.1	36	620	9.2	1.1	Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.45	18.3	8.55	3.22	27.5								27.5	8.55	1.5	42	20	10.3	0.0	Future storm infrastructure from Copper Chase Subdivision Piped to DP 1.4
	1.4								18 /	16.32	3 22	52.5				52.5	16.32	0.5	48	26			Sum of DP 1.3 & DP 7, piped to DP 1.5
									10.4	10.52	J.22	52.5											On-grade inlet, carryover flow to DP 11
	8	A8	1.48	0.56	13.9	0.83	3.63	3.0								3.0	0.83	2.0	18	20	6.6	0.1	Piped to DP 1.5
	1.5								18.4	17.15	3.21	55.1				55.1	17.15	0.5	48	91	8.3	0.2	Sum of DP 1.4 & DP 8, piped to DP 1.6 On-grade inlet
	9	A9	0.61	0.73	8.7	0.44	4.34	1.9	8.7	0.48	4.34	2.1				2.1	0.48	2.0	18	13	5.8	0.0	Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								18.6	17.63	3.20	56.4				56.4	17.63	0.5	48	95	8.3	0.2	Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.79	7.9	2.05	4.49	9.2					0.5	0.11	1.5	8.7	1.94	2.5	18	955 118	2.4	0.2	On-grade inlet, carryover flow to DP 20 Piped to DP 1.7
	11	A11	2.89	0.76		2.20		9.5					0.6	0.15	1.5	8.9			18	1049	2.4	7.1	On-grade inlet, carryover flow to DP 21 Piped to DP 1.7
		ATT	2.09	0.70	0.7	2.20	4.34	7.0	0.7	2.00	4.24	17 0											
	1.7										4.34	17.3				17.3							Sum of DP 10 & DP 11, piped to DP 1.8
	1.8					<u> </u>			18.8	21.63	3.18	68.8				68.8	21.63	2.0	54	517	14.4	0.6	Sum of DP 1.6 & DP 1.7, piped to DP 2.7 Future flow released from Barbarick Subdivision
	OS2	OS2	17.00	0.49	14.0	6.25	2.20	13.8								13.8	6.25	1.0	30	787	7.5	1.7	Piped to DP 2.0 Type C inlet
	12	A12	3.87	0.13	11.9	0.49	3.86	1.9								1.9	0.49	2.0	18	17	5.6	0.1	Piped to DP 2.0
	2.0								15.7	6.7 <u>4</u>	3.45	23.2				23.2	6.74	1.0	48	52	8.4	0.1	Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.45	14.0	4.34	3.62	15.7								15.7	4.34	1.5	30	200	9.1		Future storm infrastructure from Sterling Ranch Phase 2 Piped to DP 2.1

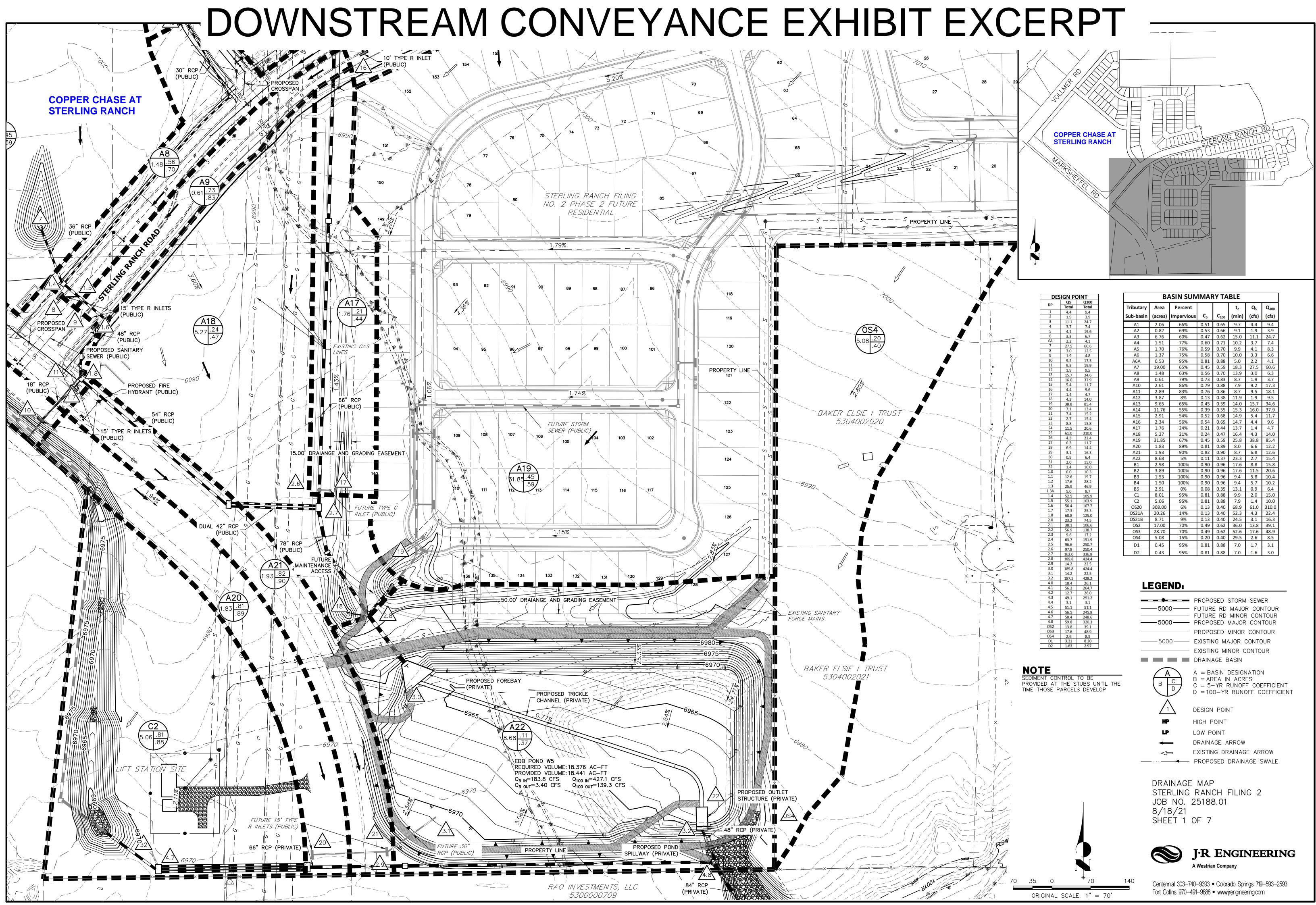
EXISTING CONDITIONS PIPE ROUTING FOR COMPARISON (100 YEAR) BY J.R. ENGINEERING (APPROVED NOVEMBER 2021)

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

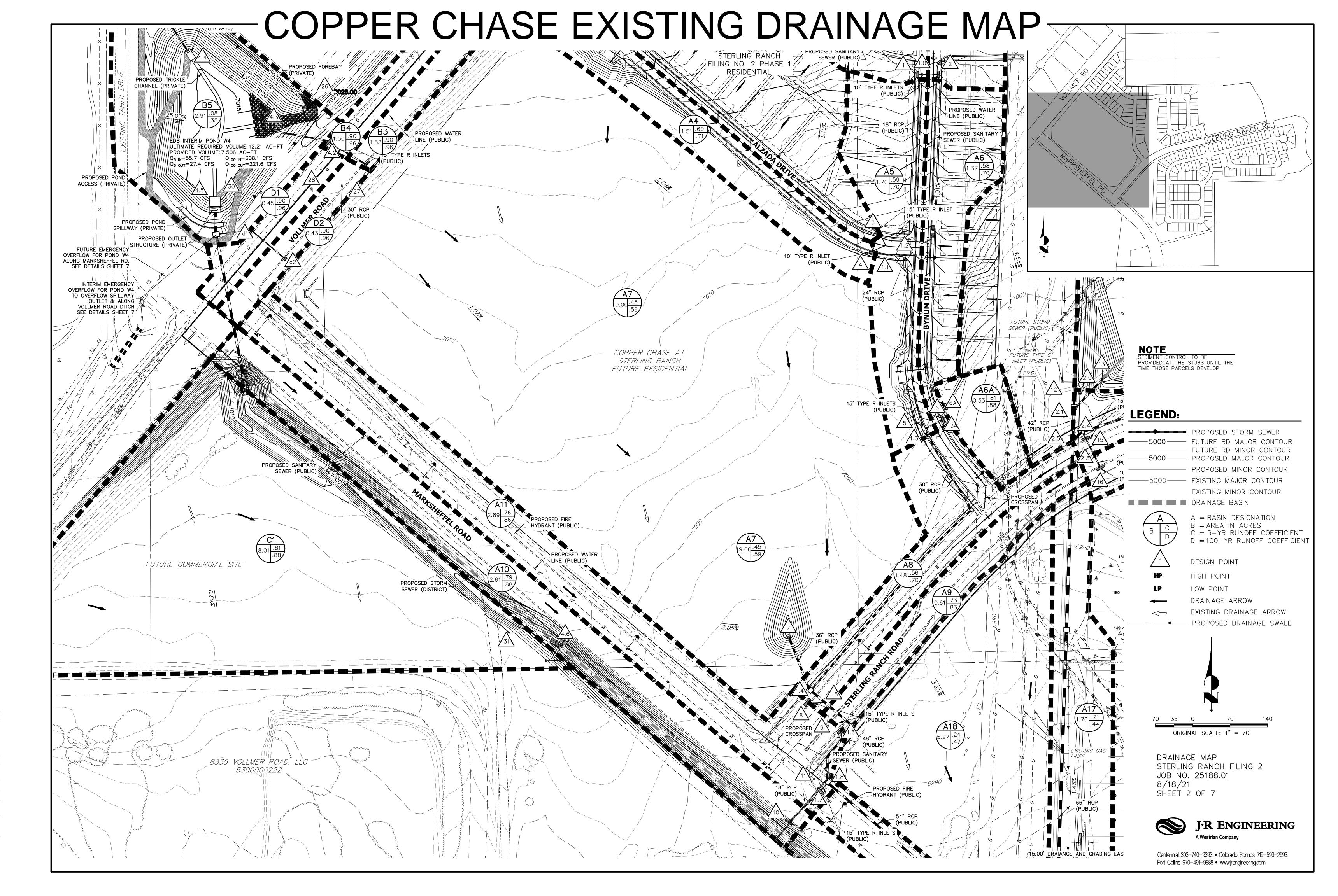
Subdivision:	Storling Dan	h Filin	No 2													Р	roject N Projec					Subdiv	vision	
Location:	El Paso Cour		J NO. 2													С	alculate	d By:	AAN	<u>л 1</u>	1			
sign Storm:	100-Year																Checke		1/5/	/21				
_	Date: 1/5/21																							
				DIR	ECT R	UNOFF			T	OTAL F	RUNOF	F	STRE	ET/SW/	ALE		PIP	E		TR.	AVEL T	IME		
Description	Jesign Point	Basin ID	Area (ac)	Runoff Coeff.	c (min)	C*A (ac)	(in/hr)	Q (cfs)	c (min)	C*A (ac)	(in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	oipe Size (inches)	andth (ft)	Velocity (fps)	(min)		REMARKS
				-	+				Ŧ	0		0	2.8	0.40	3.3					6	52 3.0	6 3.	0 On-gr	rade inlet, carryover flow to DP 5
	1	A1	2.06	0.65	9.7		7.01	9.4					0.1	0.01	3.3	6.6		1		6	5 8.3 39 3.0	6 2.	.9 On-gr	d to DP 1.0 rade inlet, carryover flow to DP 6
	2	A2	0.82	0.66	9.1	0.54	7.17	3.9								3.8	0.53	2.0	18	8 3	27 7.0	0 0.	1 Piped	d to DP 1.0
	1.0								9.7	1.47	7.00	10.3	10.0	1 (0	2.0	10.3	1.47	3.0	18		35 10.			of DP 1 & DP 2, piped to DP 1.2 rade inlet, carryover flow to DP 5
	3	A3	6.76	0.62	15.0	4.17	5.92	24.7					10.0	1.69		14.7	2.48	4.7	18	B		6 0.	0 Piped	d to DP 1.1
	4	A4	1.51	0.71	10.2	1.08	6.88	7.4					1.6	0.24	2.9	5.8	0.84	4.7	18		95 3.4 0 10.	4 1. 7 0.	.9 On-gr 0 Piped	rade inlet, carryover flow to DP 5 d to DP 1.1
	1.1								15.0	2 22	5.91	19.7				19.7	3.33	1.0	24	4	74 8.	1 0	2 Sum c	of DP 3 & DP 4, piped to DP 1.2
	1.2								15.1		5.89					28.2								of DP 1.0 & DP 1.1, piped to DP 1.3
			0.50			0.17			10.1	4.00	0.09	20.2				20.2	4.00	3.3	24	4 3	19 13.	9 0.		
	6A	A6A	0.53	0.88	5.0	0.47	8.68	4.1					1.3	0.18	0.7					6	96 1.	7 7.	.0 On-gr	land Flow to DP1.3A rade inlet, carryover flow to DP 8
	6	A6	1.37	0.70	10.0	0.95	6.94	6.6	10.0	0.96	6.94	6.7				5.4	0.78	2.0	18	8	0 7.	7 0.	.0 Sum c	of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.25	6.94	8.7		4 4 7	0.7	8.7	1.25	1.0	24		36 6.	7 0.	1 Sum c	of DP 6 & DP 6A, piped to DP 1.3 rade inlet, carryover flow to DP 8
	5	A5	1.70	0.70	9.9	1.19	6.95	8.3	17.0	3.51	5.59	19.6	6.5	1.17	0.7	13.1	2.34	2.0	18		64 1. 0 9.	7 6. 4 0.	.6 On-gr .0 Sum c	of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	8.39	5.59	46.9				46.9	8.39	1.1	36	6 6	20 10.	7 1.	.0 Sum c	of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.59	18.3	11.21	5.41	60.6								60.6	11.21	15	42	2	20 12	7 0		re storm infrastructure from Copper Chase Subdivision d to DP 1.4
	1.4								18.4	10.60	5.40	105.0				105.9	19.60				26 9.1			of DP 1.3 & DP 7, piped to DP 1.5
													1.9	0.41	0.7					1	95 1.	7 1.	.9 On-gr	rade inlet, carryover flow to DP 11
	8	A8	1.48	0.70	13.9	1.04	6.10	6.3			4.76					10.6					20 9.			of Sub-basin A8 & Carryover flows from DP5, DP 6 & DP 15, Piped to DP 1.5
	1.5								23.7	21.83	4.76	103.9	0.3	0.05	0.7	103.9	21.83	0.5	48		91 9.1 40 1.1			of DP 1.4 & DP 8, piped to DP 1.6 rade inlet, carryover flow to DP 11
	9	A9	0.61	0.83	8.7	0.51	7.29	3.7	21.2	0.95	5.04	4.8	0.5	0.05	0.7	4.5	0.89	2.0	18		13 7.3			of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								23.9	22.72	4.74	107.7				107.7	22.72	0.5	48	8	95 9.	1 0.	.2 Sum c	of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.88	7.9	2.29	7.53	17.3					4.5	0.59	1.5	12.8	1.70	2.5	18		55 2.4 18 10.3	4 6. 3 0.	.5 On-gr 2 Piped	a de inter carryover flow to DP 20 d to DP 1.7
	11	A11	2.89	0.86					10.6	2.04	6.77	10.0	6.1	0.90	1.5	13.8				10	49 2.4	4 7.	1 On-gr	rade inlet, carryover flow to DP 21 of Sub-basin A11 & carryover flows from DP 8 & DP 9, piped to DP 1.7
	1.7		2.07	0.00	0.7	2.40	7.20	10.1	10.6		6.77					25.3	3.74							of DP 10 & DP 11, piped to DP 1.8
	<mark>1.8</mark>								24.0	26.45	4.72	125.0				125.0		2.0					Future	of DP 1.6 & DP 1.7, piped to DP 2.7 re flow released from Barbarick Subdivision
	OS2	OS2	17.00	0.62	12.0	10.54	3.71	39.1								39.1	10.54	1.0	30	0 7	87 9.	5 1.		d to DP 2.0 .C inlet
	12	A12	3.87	0.38	11.9	1.47	6.49	9.5							<u> </u>	9.5	1.47	2.0	18	8	17 8.	9 0.		d to DP 2.0
	2.0								13.4	12.01	6.20	74.5				74.5	12.01	1.0	48	8	52 11.	6 0.		of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.59	14.0	5.69	6.08	34.6								34.6	5.69	1.5	30	0 2	00 11.0	0 0.		re storm infrastructure from Sterling Ranch Phase 2 d to DP 2.1

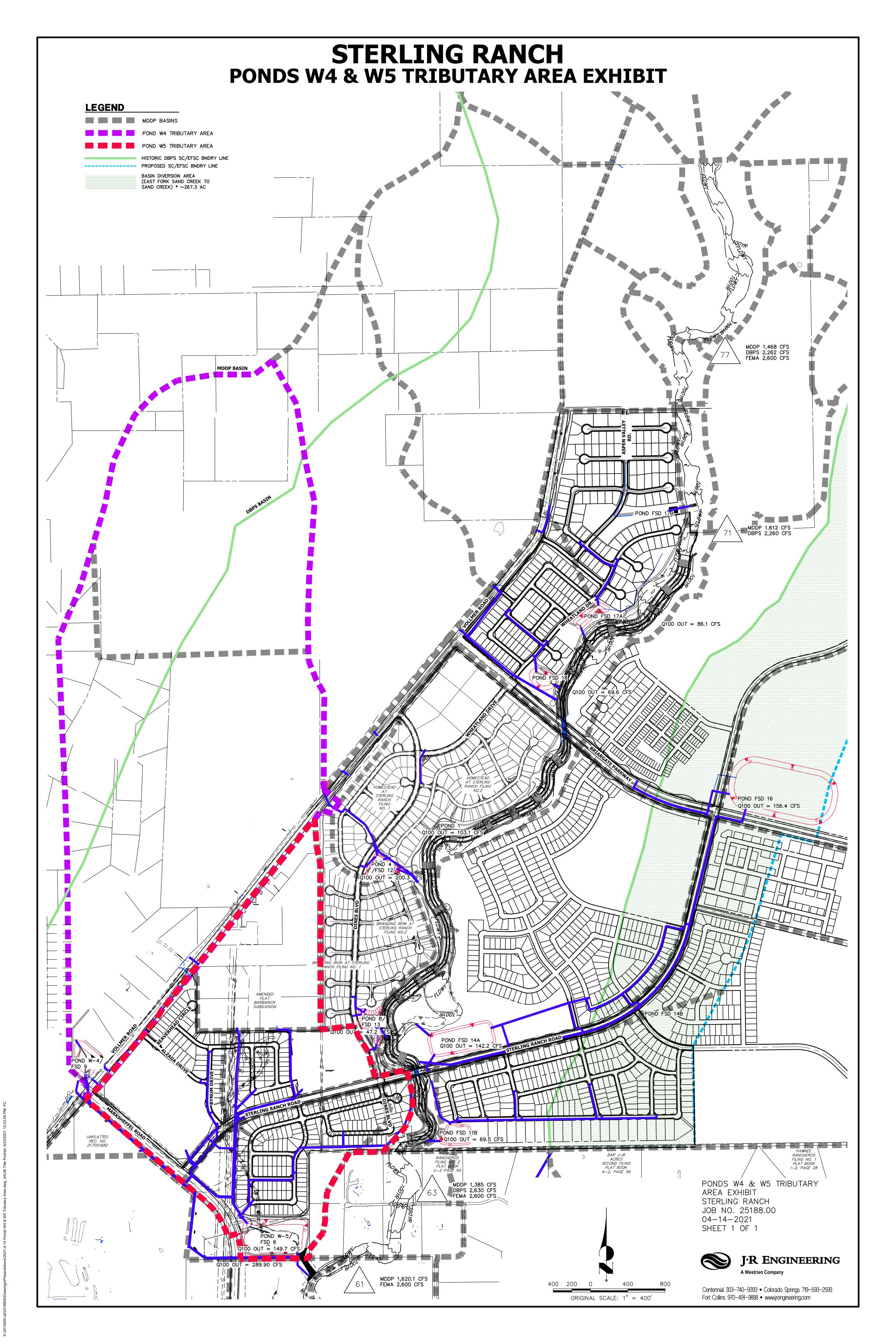
EXISTING DRAINAGE MAP (BY J.R. ENGINEERING, APPROVED NOVEMBER 2021)



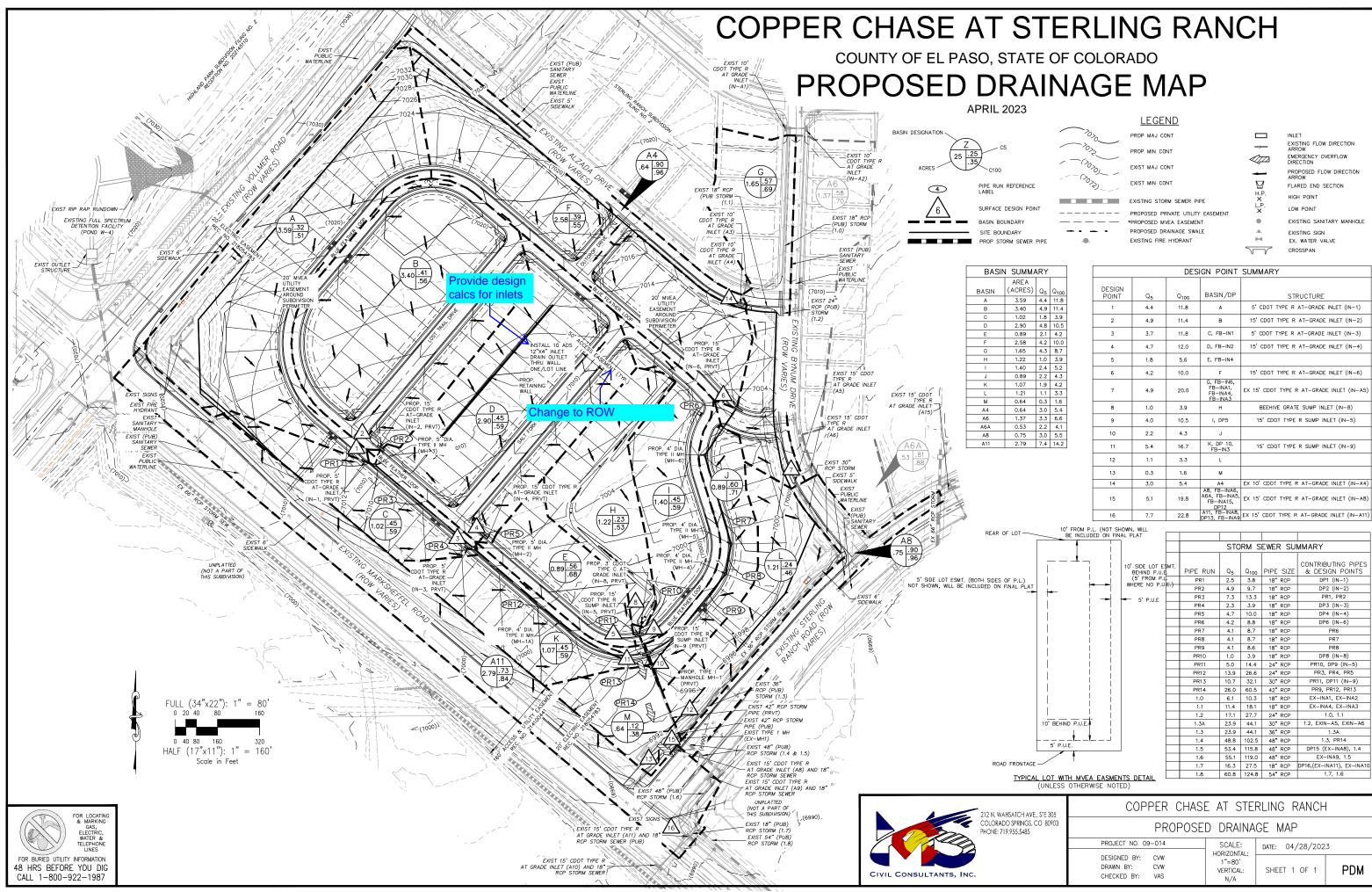
3	11.1	24.7
4	3.7	7.4
5	4.1	19.6
6	3.3	6.7
6A	2.2	4.1
7	27.5	60.6
8	3.0	12.5
9	1.9	4.8
10	9.2	17.3
10	9.5	
11		19.9
	1.9	9.5
13	15.7	34.6
14	16.0	37.9
15	5.4	11.7
16	4.4	9.6
17	1.4	4.7
18	4.3	14.0
19	38.8	85.4
20	1000 2000	
	7.1	13.4
21	7.4	15.2
22	2.7	15.4
23	8.8	15.8
24	11.5	20.6
25	61.0	310.0
26	4.3	22.4
27	6.3	11.7
28	6.9	14.4
29		
	3.1	16.3
30	0.9	6.4
31	2.0	15.0
32	1.4	10.0
1.0	6.0	10.3
1.1	12.6	19.7
1.2	17.6	28.2
1.3	25.9	46.9
1.3A	5.0	8.7
1.4		
	52.5	105.9
1.5	55.1	103.9
1.6	56.4	107.7
1.7	17.3	25.3
1.8	68.8	125.0
2.0	23.2	74.5
2.1	38.1	106.6
2.2	56.9	138.7
2.3	9.6	17.2
2.4	63.7	151.9
2.5	96.6	250.7
2.6	97.8	250.4
2.0		
111111	162.0	336.8
2.8	189.8	424.4
2.9	14.2	22.5
3.0	189.8	424.4
3.1	14.2	22.5
3.2	187.5	428.2
4.0	18.4	26.1
4.1	56.2	264.7
4.2	12.7	26.0
4.3	49.1	291.2
4.4	3.1	3.1
4.5		
	51.1	51.1
4.6	56.5	245.8
4.7	58.4	248.6
4.8	59.8	320.3
OS2	13.8	39.1
OS3	17.6	48.9
OS4	2.6	8.5
	2.0	0.5
D1	3.31	8.20

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Tributary	Area	Percent			t _c	Q₅	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
A1	2.06	66%	0.51	0.65	9.7	4.4	9.4
A2	0.82	69%	0.53	0.66	9.1	1.9	3.9
A3	6.76	60%	0.47	0.62	15.0	11.1	24.7
A4	1.51	77%	0.60	0.71	10.2	3.7	7.4
A5	1.70	76%	0.59	0.70	9.9	4.1	8.3
A6	1.37	75%	0.58	0.70	10.0	3.3	6.6
A6A	0.53	95%	0.81	0.88	5.0	2.2	4.1
A7	19.00	65%	0.45	0.59	18.3	27.5	60.6
A8	1.48	63%	0.56	0.70	13.9	3.0	6.3
A9	0.61	79%	0.73	0.83	8.7	1.9	3.7
A10	2.61	86%	0.79	0.88	7.9	9.2	17.3
A11	2.89	83%	0.76	0.86	8.7	9.5	18.1
A12	3.87	8%	0.13	0.38	11.9	1.9	9.5
A13	9.65	65%	0.45	0.59	14.0	15.7	34.6
A14	11.76	55%	0.39	0.55	15.3	16.0	37.9
A15	2.91	54%	0.52	0.68	14.9	5.4	11.7
A16	2.34	56%	0.54	0.69	14.7	4.4	9.6
A17	1.76	24%	0.21	0.44	13.7	1.4	4.7
A18	5.27	21%	0.24	0.47	16.4	4.3	14.0
A19	31.85	67%	0.45	0.59	25.8	38.8	85.4
A20	1.83	89%	0.81	0.89	8.0	6.6	12.2
A21	1.93	90%	0.82	0.90	8.7	6.8	12.6
A22	8.68	5%	0.11	0.37	23.3	2.7	15.4
B1	2.98	100%	0.90	0.96	17.6	8.8	15.8
B2	3.89	100%	0.90	0.96	17.6	11.5	20.6
B3	1.53	100%	0.90	0.96	9.4	5.8	10.4
B4	1.50	100%	0.90	0.96	9.4	5.7	10.2
B5	2.91	0%	0.08	0.35	13.1	0.9	6.4
C1	8.01	95%	0.81	0.88	9.9	2.0	15.0
C2	5.06	95%	0.81	0.88	7.9	1.4	10.0
OS20	308.00	6%	0.13	0.40	68.9	61.0	310.0
OS21A	20.26	14%	0.13	0.40	52.3	4.3	22.4
OS21B	8.71	9%	0.13	0.40	24.5	3.1	16.3
OS2	17.00	70%	0.49	0.62	36.0	13.8	<u>39.1</u>
OS3	28.70	70%	0.49	0.62	52.6	17.6	48.9
OS4	5.08	15%	0.20	0.40	29.5	2.6	<mark>8.5</mark>
D1	0.45	95%	0.81	0.88	7.0	1.7	3.1
D2	0.43	95%	0.81	0.88	7.0	1.6	3.0





PROPOSED DRAINAGE MAP



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PROP MAJ CONT
PROP MIN CONT
EXIST MAJ CONT
EXIST MIN CONT
EXISTING STORM SEWER PIPE
PROPOSED PRIVATE UTILITY EA
*PROPOSED MVEA EASEMENT
PROPOSED DRAINAGE SWALE
EXISTING FIRE HYDRANT



1				DES	IGN POINT	SUMMARY
5	Q ₁₀₀ 11.8	DESIGN POINT	Q ₅	Q ₁₀₀	BASIN/DP	STRUCTURE
,	11.4	1	4.4	11.8	A	5' CDOT TYPE R AT-GRADE INLET (IN-1)
3	3.9 10.5	2	4.9	11.4	в	15' CDOT TYPE R AT-GRADE INLET (IN-2)
, I	4.2	3	3.7	11.8	C, FB-IN1	5' CDOT TYPE R AT-GRADE INLET (IN-3)
	10.0 8.7	4	4.7	12.0	D, FB-IN2	15' CDOT TYPE R AT-GRADE INLET (IN-4)
,	8.7 3.9	5	1.8	5.6	E, FB-IN4	
	5.2 4.3	6	4.2	10.0	F	15' CDOT TYPE R AT-GRADE INLET (IN-6)
•	4.2 3.3	7	4.9	20.0	G, FB-IN6, FB-INA1, FB-INA4, FB-INA3	EX 15' CDOT TYPE R AT-GRADE INLET (IN-A5)
)	1.6 5.4	8	1.0	3.9	н	BEEHIVE GRATE SUMP INLET (IN-8)
;	6.6	9	4.0	10.5	I, DP5	15' CDOT TYPE R SUMP INLET (IN-5)
,	4.1 5.5	10	2.2	4.3	J	
	14.2	11	5.4	16.7	K, DP 10, FB-IN3	15' CDOT TYPE R SUMP INLET (IN-9)
		12	1.1	3.3	L	
		13	0.3	1.6	м	
		14	3.0	5.4	A4	EX 10' CDOT TYPE R AT-GRADE INLET (IN-A4)
		15	5.1	19.8	A8, FB-INA6, A6A, FB-INA5, FB-INA15, DP12	EX 15' CDOT TYPE R AT-GRADE INLET (IN-A8)
		16	7.7	22.8	A11, FB-INA8, DP13, FB-INA9	EX 15' CDOT TYPE R AT-GRADE INLET (IN-A11)

CH AVE., STE 305				1
RINGS, CO 80903 .5485	PROPOSE	d draina	GE MAP	
	PROJECT NO. 09-014	SCALE:	DATE: 04/28/202	3
	DESIGNED BY: CVW DRAWN BY: CVW CHECKED BY: VAS	HORIZONTAL: 1"=80' VERTICAL: N/A	SHEET 1 OF 1	PDM

### V_1 Drainage.pdf Markup Summary

