

**FINAL DRAINAGE REPORT  
FOR  
STERLING RANCH RECYCLING FACILITY**

**Prepared For:**

**Colorado Concrete Crushing, LLC  
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Colorado Springs, CO 80903  
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**July 2024**

**Project No. 25188.14**

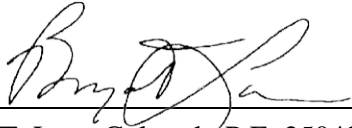
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**Prepared By:**

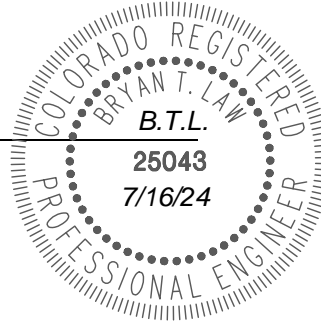
**JR Engineering, LLC  
5475 Tech Center Drive, Suite 235  
Colorado Springs, CO 80919  
719-593-2593**

**ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage letter has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.



Bryan T. Law, Colorado P.E. 25043  
For and On Behalf of JR Engineering, LLC

**DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Colorado Concrete Crushing, LLC

By:



Title:



Address:

20 Boulder Crescent, Suite 200  
Colorado Springs, CO 80903

**El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

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County Engineer/ ECM Administrator



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- Appendix A – Vicinity Map, Soil Descriptions, FEMA Floodplain Map
- Appendix B – Hydrologic Calculations
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## **PURPOSE**

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This document is the Final Drainage Report for Sterling Ranch Recycling Facility. The purpose of this report is to identify on-site and off-site drainage patterns, areas tributary to the site, and compare existing and proposed drainage conditions.

## **GENERAL SITE DESCRIPTION**

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### **GENERAL LOCATION**

Sterling Ranch Recycling Facility (hereby referred to as the “site”) is a proposed development within the Sterling Ranch master planned community with a total area of approximately 32 acres. The site is presently used as a concrete and asphalt recycling facility.

The site is located in the north half of Section 5, Township 13 South, Range 65 West of the Sixth Principal Meridian in El Paso County, State of Colorado. The site is bounded by Marksheffel Road to the east, Pioneer Sand CO land to the west and south, and unplatted land to the north. Refer to the vicinity map in Appendix A for additional information.

### **DESCRIPTION OF PROPERTY**

In the existing condition analysis, the property was analyzed at the time of the parcel sale in 2021. Before the sale of the site in 2021, the parcel had been used as a crushing facility for a nearby mining operation. The crushing business halted operations and vegetation was established on portions of the site prior to the sale. There was an asphalt access road and compacted gravel roads on the site at the time of sale. The site generally slope(s) to the south at 1 to 6% towards an existing 8’ berm on the southern edge of the property. In the proposed interim condition, the property will be used as an asphalt and concrete recycling facility with asphalt drives, a staging area and some existing grasslands. In the ultimate condition, the site and surrounding properties are assumed to be developed per their land use which includes heavy industrial, multi-family residential, and commercial.

Soils located on the project site are Blakeland Loamy Sand (8) and Columbine Gravelly Sandy Loam (19). These soils are classified as Hydrologic Soil Group A. Group A soils exhibit high infiltration rates when thoroughly wet, and consist mainly of deep, well drained to excessively drained sands or gravelly sands. Refer to the soil survey map in Appendix A for additional information.

There are no known irrigation facilities located on the project site.

### **FLOODPLAIN STATEMENT**

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the entire site lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher



than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. Refer to the FIRM Map in Appendix A for additional information.

## EXISTING DRAINAGE CONDITIONS

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### MAJOR BASIN DESCRIPTIONS

The site lies within the upper Sand Creek Drainage Basin based on the “Sand Creek Drainage Basin Planning Study” (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into 7 major sub-basins. The site is within the respective upper basin Sand Creek sub-basin as shown in Appendix D. Sand Creek ultimately enters Fountain Creek about two miles upstream of the Academy Boulevard bridge over Fountain Creek.

The site generally drains from north to southwest. Sand Creek is located to the east of the site and runs from north to south. This reach of drainage conveyance does not currently have any improvements. As of the date of this report, Kiowa is performing studies and plans to address Sand Creek stabilization adjacent to the site.

### EXISTING SUB-BASIN DRAINAGE

The existing condition analyzes the parcel at the latest time of sale in 2021. The existing condition of the site was broken into nine sub-basins including six on-site basins and three off-site basins. The basin delineation is shown in the existing drainage map in Appendix E and is described as follows:

Basin EXA ( $Q_5=1.1$  cfs,  $Q_{100}=5.4$  cfs) is 2.68 acres with an 8 percent impervious and is located on the northwestern portion of the site. This basin is comprised of part of an existing paved access road, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at design point (DP) 1. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXB ( $Q_5=0.6$  cfs,  $Q_{100}=4.3$ cfs) is 2.60 acres with a 2 percent impervious and is located on the western portion of the site. This basin is comprised of existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at DP2. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXC ( $Q_5=1.0$  cfs,  $Q_{100}=4.3$  cfs) is 2.11 acres with a 14 percent impervious and is located on the southwest portion of the site. This basin is comprised of several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest to DP3 located along the existing 8' berm. Runoff from DP3 infiltrates the ground along the berm's toe of slope.



Basin EXD ( $Q_5=7.6$  cfs,  $Q_{100}=28.1$  cfs) is 13.44 acres with a 17 percent impervious and is located on the western central portion of the site. This basin is comprised of part of an existing paved access road, several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south to DP4 located along the existing 8' berm. Runoff from DP4 flows south across the existing berm via an existing 12" PVC pipe. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin OS1 ( $Q_5=1.4$  cfs,  $Q_{100}=9.2$  cfs) is 8.74 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff from this basin sheet flows south and then east along the existing off-site berm to DP5. Runoff from DP5 flows south entering into Basin EXE. Runoff follows historical drainage patterns within Basin EXE and combines at DP7.1.

Basin OS3 ( $Q_5=0.2$  cfs,  $Q_{100}=0.9$  cfs) is 0.29 acres with a 2 percent impervious and is located to the south of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows north to DP6 entering into Basin EXE. Runoff follows historical drainage patterns within Basin EXE and combines at DP7.1.

Basin EXE ( $Q_5=2.0$  cfs,  $Q_{100}=13.4$  cfs) is 8.51 acres with a 2 percent impervious and is located on the eastern central portion of the site. This basin is comprised of part of several existing dirt access roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south and then east to DP6 located along the existing 8' berm. Runoff from DP5, DP6, and DP7 combine at DP7.1 ( $Q_5=2.8$  cfs,  $Q_{100}=18.3$  cfs). Runoff from DP7.1 continues to flow southeast through the neighboring property to the south. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.

Basin OS2 ( $Q_5=0.2$  cfs,  $Q_{100}=1.1$  cfs) is 0.53 acres with a 2 percent impervious and is located to the east of the site. Runoff from this basin sheet flows west to DP8 entering into Basin EXF. Runoff follows historical drainage patterns within Basin EXE and combines at DP9.1.

Basin EXF ( $Q_5=0.8$  cfs,  $Q_{100}=5.2$  cfs) is 3.09 acres with a 2 percent impervious and is located on the eastern portion of the site. This basin is comprised of part of an existing dirt access road and undeveloped area. Runoff from this basin sheet flows southeast to DP9 located along the eastern side of the site. Runoff from DP8 and DP9 combine at DP9.1 ( $Q_5=0.9$  cfs,  $Q_{100}=6.1$  cfs). Runoff from DP9.1 continues to flow south through the neighboring sanitary lift station property to the east. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.



## PROPOSED DRAINAGE CONDITIONS

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### PROPOSED CONVEYANCE

In general, developed flows are collected in proposed swales, which convey water to the proposed water quality and detention area. Proposed swale sections were designed to ensure they are stable and have required capacity to satisfy criteria. A swale is considered stable with a velocity of 5 ft/s or less. Where swale Froude numbers exceed 0.8, swales will be reinforced with the specified SC250 VMax TRM (turf reinforcement mat) product (or approved equivalent) shown in Appendix C. Specific locations where the TRM is required in swale sections is shown in the Grading and Erosion Control Construction Documents. To ensure capacity, swales will have a minimum of 1 ft. of freeboard over the water surface for flows anticipated in a 100-year storm event. In addition to the swales, a proposed culvert also conveys flows under the access roadway. The culvert was sized to not overtop the roadways with flows from a 100-year storm event. Detailed swale calculations, sections, and culvert calculations are located in Appendix C.

### PROPOSED SUB-BASIN DRAINAGE

The proposed condition analyzes the parcel for the interim use of a recycling facility. The Rational Method produced flows that were used to design the proposed interim swales, culverts, storm sewer, and pond forebays. The proposed site was broken into eight basins including six on-site basins and two off-site basins. The proposed basin delineation is shown on the drainage basin map within Appendix E and is described as follows:

Basin A ( $Q_5=0.3$  cfs,  $Q_{100}=1.6$  cfs) is 0.50 acres with a 2% impervious and is located on the western and a portion of the southern property line of the site. This basin is comprised of proposed area to remain undeveloped and therefore follows the historic drainage pattern flowing off-site to the west and south undetained or treated. This is in accordance with Section I.7.1.B.7 of the ECM Stormwater Quality Policy and Procedure. Runoff from this basin sheet flows southwest to DP1 and then off-site to the adjacent property to the west. Runoff then follows historical drainage patterns sheet flowing off-site and outfalls to Sand Creek.

Basin B ( $Q_5=7.4$  cfs,  $Q_{100}=25.1$  cfs) is 14.03 acres with a 19 percent impervious and is located on the western central portion of the site. This basin is comprised of part of a paved roadway, raw concrete stockpile, raw concrete with rebar stockpile, asphalt stockpile, weighing station, mobile crusher, fence, part of temporary gravel road, swales and undeveloped land. Runoff from this basin sheet flows overland south to a proposed swale that directs flows east to DP2. Runoff from DP2 is combined at the proposed 54" FES at DP4.2. Runoff from this basin is captured and treated within proposed Pond A.

Basin OS1 ( $Q_5=1.4$  cfs,  $Q_{100}=9.2$  cfs) is 8.74 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff



from this basin sheet flows south and then east along the existing off-site berm to DP3. Runoff from DP3 flows south entering into Basin C. Runoff follows the drainage patterns within Basin C and combines at the proposed 24" RCP culvert at DP4.1.

Basin C ( $Q_5=3.4$  cfs,  $Q_{100}=17.7$  cfs) is 10.70 acres with a 6 percent impervious and is located on the eastern central portion of the site. This basin is comprised of a part of proposed Sterling Ranch Road, asphalt access roads, swales and undeveloped land. Runoff from this basin flows along proposed curb and gutter as well as sheet flows overland south to proposed swales that directs flows east to DP4. Runoff from DP4 is combined with flows from DP3 at the proposed 24" RCP culvert at DP4.1 ( $Q_5=3.7$  cfs,  $Q_{100}=21.1$  cfs). Runoff from DP4.1 enters the proposed culvert into Basin B and a proposed swale directs flows to the proposed 54" FES at DP4.2 ( $Q_5=9.3$  cfs,  $Q_{100}=40.1$  cfs). DP4.2 flows are piped to the west forebay within the pond and combine at DP9.1. Runoff from this basin is captured and treated within proposed Pond A.

Basin D ( $Q_5=0.5$  cfs,  $Q_{100}=3.7$  cfs) is 2.16 acres with a 2 percent impervious and is located on the eastern boundary of the site. This basin is comprised of undeveloped land. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flows south to DP5. Runoff from DP5 is combined at the proposed Type C sump inlet at DP7.1 within Basin E. Runoff from this basin is captured and treated within proposed Pond A.

Basin E ( $Q_5=2.2$  cfs,  $Q_{100}=7.1$  cfs) is 3.10 acres with a 22 percent impervious and is located on the eastern portion of the site. This basin is comprised of a part of proposed Sterling Ranch Road, part of a temporary gravel road, asphalt access road, swale and undeveloped land. Runoff from this basin flows along proposed curb and gutter and then sheet flows overland southeast to a proposed swale that directs flows east to DP6. Runoff from DP6 is combined at the proposed Type C sump inlet at DP7.1. Runoff from this basin is captured and treated within proposed Pond A.

Basin OS2 ( $Q_5=0.1$  cfs,  $Q_{100}=0.7$  cfs) is 0.36 acres with a 2 percent impervious and is located to the east of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows west and then south along the property boundary to DP7. Runoff from DP7 is combined with DP5 and DP6 flows at the proposed Type C sump inlet at DP7.1 ( $Q_5=2.8$  cfs,  $Q_{100}=11.2$  cfs). DP7.1 flows are piped to the north forebay within the pond and combine at DP9.1.

Basin OS3 ( $Q_5=0.2$  cfs,  $Q_{100}=1.0$  cfs) is 0.30 acres with a 2 percent impervious and is located to the south of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows north to DP8. Runoff from DP8 combines with DP4.2, DP7.1, and DP6 flows at the proposed outlet structure at DP9.1.

Basin F ( $Q_5=0.6$  cfs,  $Q_{100}=4.4$  cfs) is 2.27 acres with a 2 percent impervious and is located on the southeast portion of the site. This basin is comprised of a proposed full-spectrum extended detention





basin (EDB) within Tract A and the proposed off-site detention pond easement. Runoff from this basin sheet flows overland to a proposed trickle channel that directs flows east to DP9. Runoff from DP9 is combined with flows from DP4.2, DP7.1, and DP8 at the proposed full-spectrum EDB outlet structure at DP9.1 ( $Q_5=11.4$  cfs,  $Q_{100}=49.4$  cfs). DP8.1 represents the total proposed flows that will enter the proposed full-spectrum EDB in the interim condition. Flows will be released through the outlet structure at DP9.2 ( $Q_5=0.1$  cfs,  $Q_{100}=8.3$  cfs) and connect into the existing storm infrastructure sending the flows east where they will eventually follow the historical drainage patterns into Sand Creek.

Basin G ( $Q_5=2.2$  cfs,  $Q_{100}=7.1$  cfs) is 0.06 acres with a 67 percent impervious and is located on the eastern portion of the site. This basin is comprised of a part of proposed Sterling Ranch Road. Runoff from this basin flows along proposed curb and gutter east to DP10 then flows off-site basin OS4. Flows combine at DP11.1 within Basin OS4. Due to the proposed highpoint in the Sterling Ranch Road it is not practicable to capture runoff from this basin and flows go off-site to the east undetained or treated. This is in accordance with Section I.7.1.C.1a of the ECM Stormwater Quality Policy and Procedure. The total uncaptured area for this site (Basins A and G) total 0.56 acres, which is under the 1 acre maximum threshold.

Basin OS4 ( $Q_5=6.7$  cfs,  $Q_{100}=12.8$  cfs) is 2.08 acres with an 82 percent impervious and is located to the east of the site. This basin is comprised of off-site area comprised of a portion of Marksheffel Road and an existing Type R on-grade inlet. Previously this area was analyzed in the Sterling Ranch Filing No. 2 project and the only changes are for a proposed right turn lane. The proposed basin imperviousness is consistent with the original report (82% proposed vs. 86%) and water quality treatment is accounted for within the existing Pond W-5. See EPC project number SF-20-015 (Sterling Ranch Filing No. 2), and excerpts on pages 96-97 of this report for additional information. Runoff from this basin flows southeast to DP11 and flows with DP10 combine at the existing 15' Type R on-grade inlet at DP11.1 ( $Q_5=6.9$  cfs,  $Q_{100}=13.1$  cfs). Bypass flows from this inlet follow the existing path along Marksheffel Road and are less than existing, meaning no negative impacts to existing infrastructure.

In the interim condition, there are three locations where flows leave the site.

1. Flows from Basin A leave the site uncaptured and untreated at DP1 ( $Q_5=0.3$  cfs,  $Q_{100}=1.6$  cfs). Flows from existing Basins EXA-EXD travel off-site along the western and southern boundaries at DP1-4 for a total flow of  $Q_5=10.3$  cfs,  $Q_{100}=42.1$  cfs. Compared to the existing flows, Basin A flows are less than historic and will not adversely affect downstream infrastructure.
1. Released flows from the pond outlet structure at DP9.2 ( $Q_5=0.1$  cfs,  $Q_{100}=8.3$  cfs) are released into the existing storm infrastructure located adjacent to the site. Flows from existing design points DP7.1 and 9.1 flow off-site to the south for a total flow of  $Q_5=3.7$  cfs,  $Q_{100}=24.4$  cfs. Compared to the existing flows, DP9.2 flows are less than historic and will not



adversely affect downstream infrastructure. See the ultimate section below for more information on the existing downstream infrastructure.

2. Flows from Basin G leave the site uncaptured and untreated at DP10 ( $Q_5=0.2$  cfs,  $Q_{100}=0.4$  cfs) and combine with OS4 flows at DP11 ( $Q_5=6.7$  cfs,  $Q_{100}=12.8$  cfs) at the existing 15' Type R on-grade inlet at DP11.1 ( $Q_5=6.9$  cfs,  $Q_{100}=13.1$  cfs). The existing inlet was constructed as part of Sterling Ranch Filing No. 2 (see applicable excerpts in Appendix D). The Filing 2 report Basin A10 (Basin OS4) has a total flow to the 15' Type R on-grade inlet of  $Q_5=9.2$  cfs,  $Q_{100}=17.3$  cfs. Compared to the existing flows, DP11.1 flows are less than historic and will not adversely affect downstream infrastructure.

## ULTIMATE SUB-BASIN DRAINAGE

The ultimate condition analyzes the parcel and tributary properties for the future development based on the land use in order to design the ultimate full-spectrum EDB and spillway overflow path. The ultimate site was broken into five land uses. The land uses are shown on the proposed drainage map within Appendix E and is described as follows.

- Lot 1 is 4.74 acres and is zoned as Heavy Industrial Area (90% impervious)
- Urban Non-Residential Collector Roadway (80' R.O.W.) is 1.78 acres (100% impervious for roadway, curb & gutter, and sidewalk width, 2% impervious for other areas)
- Lot 2 is 24.05 acres and is zoned as Residential-1/8 Acre or Less (65% impervious)
- Tract A is 1.85 acres and is used as detention pond area (2% impervious)
- Off-site vacant land to the north is 8.74 acres and is zoned as Commercial Area (95% impervious)
- Off-site Tract/ Lift Station land to the east is 1.87 acres and is zoned as Heavy Industrial Area (90% impervious)
- Off-site land to the east is 0.44 acres and is used as detention pond area (2% impervious)
- Off-site land to the south is 0.30 acres and flows to detention pond area (2% impervious)
- Total Area = 43.77 acres with 71.6% impervious (used 72% for design)

The ultimate condition was used overall to size the full-spectrum EDB and ensure it will operate for future developments.

In the ultimate condition, there is one location where flows leave the site.

2. Ultimate released flows from the pond outlet structure ( $Q_5=1.5$  cfs,  $Q_{100}=22.2$  cfs) are released into the existing storm infrastructure located adjacent to the site. Flows from existing design points DP7.1 and 9.1 flow off-site to the south for a total flow of  $Q_5=3.7$  cfs,  $Q_{100}=24.4$  cfs. The existing downstream 66" RCP that the outfall ties into was designed and approved as part of the Sterling Ranch Filing 2 development. The pipe shall be installed by June 2024 and for the purposes of this report, considered as existing. The existing 66" RCP was designed for Filing 2 DP4.7 flows ( $Q_5=58.4$  cfs,  $Q_{100}=248.6$  cfs) and the ultimate

condition flows ( $Q_5=32.2$  cfs,  $Q_{100}=255.6$  cfs) will result in an increase in flows in the major storm. The StormCAD analysis in Appendix C shows that the existing storm system was designed deep enough to have the capacity for the increase in flow. There are also no adverse affects from the increase in flow in the minor storm shown in the MHFD Detention spreadsheet as the existing storm system was designed to handle the peak 100-year flows which greatly surpass the 5-year flow rates. See Appendix C for the StormCAD analysis and calculations. The existing storm system the proposed site ties continues to travel east and south about 1,800 feet before ultimately releasing directly into Sand Creek.

## DRAINAGE DESIGN CRITERIA

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### DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the “*City of Colorado Springs/El Paso County Drainage Criteria Manual*” Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the “*Urban Storm Drainage Criteria Manual*” Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the “*Colorado Springs Drainage Criteria Manual*” (CSDCM), dated May 2014, as adopted by El Paso County.

### HYDROLOGIC CRITERIA

All hydrologic data was obtained from the “*El Paso Drainage Criteria Manual*” Volumes 1 and 2, and the “*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*” Volumes 1, 2, and 3. On-site drainage improvements were designed based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One-hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

**Table 1: 1-hr Point Rainfall Data**

| <b>Storm</b> | <b>Rainfall (in.)</b> |
|--------------|-----------------------|
| 5-year       | 1.50                  |
| 100-year     | 2.52                  |



## HYDRAULIC CRITERIA

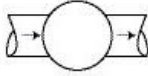
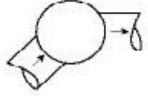
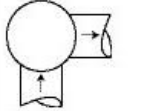
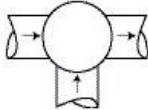
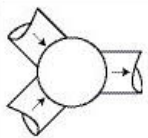
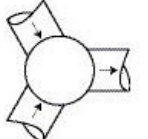
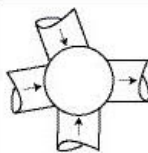
The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Autodesk Hydraflow Express was used to size the overflow channel and drainage swales per criteria. The MHFD-Detention\_v4.06 spreadsheet was utilized for evaluating proposed detention and water quality for Pond A. Bentley StormCAD v8i was used to analyze the hydraulic grade lines and energy grade lines for the storm sewer network. Manhole and pipe losses for the model were obtained from the *Modeling Hydraulic and Energy Gradients in Storm Sewers: A Comparison of Computation Methods*, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 2 (below), this method is accurate for pipes 42" and smaller for larger pipes the Standard head-loss coefficients as recommended by Bentley were used as shown in Table 3. StormCAD, Autodesk Hydraflow results, along with street and inlet capacities, are presented in Appendix C.

**Table 2: Storm Head-loss Coefficients**

| StormCAD Conversion Table |                                     |                          |            |
|---------------------------|-------------------------------------|--------------------------|------------|
| Bend Loss                 | Bend Angle                          | K coefficient Conversion |            |
|                           | 0                                   | 0.05                     |            |
|                           | 22.5                                | 0.1                      |            |
|                           | 45                                  | 0.4                      |            |
|                           | 60                                  | 0.64                     |            |
|                           | 90                                  | 1.32                     |            |
| Lateral Loss              | 1 Lateral K coefficient Conversion  |                          |            |
|                           | Bend Angle                          | Non Surcharged           | Surcharged |
|                           | 45                                  | 0.27                     | 0.47       |
|                           | 60                                  | 0.52                     | 0.9        |
|                           | 90                                  | 1.02                     | 1.77       |
|                           | 2 Laterals K coefficient Conversion |                          |            |
|                           | 45                                  | 0.96                     |            |
|                           | 60                                  | 1.16                     |            |
| 90                        | 1.52                                |                          |            |



**Table 3 - Storm Head-loss Coefficients**

| Type of Manhole  | Diagram  | Headloss Coefficient |
|--|--|----------------------|
| Trunkline only with no bend at the junction                          |    | 0.5                  |
| Trunkline only with 45° bend at the junction                         |    | 0.6                  |
| Trunkline only with 90° bend at the junction                         |    | 0.8                  |
| Trunkline with one lateral   |    | Small 0.6 Large 0.7  |
| Two roughly equivalent entrance lines with angle < 90° between lines |    | 0.8                  |
| Two roughly equivalent entrance lines with angle > 90° between lines |   | 0.9                  |
| Three or more entrance lines   |  | 1.0                  |

## DRAINAGE FACILITY DESIGN

### GENERAL CONCEPT

The project site is anticipated to be developed in phases, beginning with the development of the Sterling Ranch Recycling Facility portion of Lot 2. This is known as the “interim condition”. In the future, it is anticipated that Lot 1 will develop as a heavy industrial area, Lot 2 will develop as multi-family, proposed Sterling Ranch Road R.O.W. will develop as an urban non-residential collector roadway, unplatted land to the north of the site will develop as a commercial area, tract land to the east of the site will develop as heavy industrial, and Tract A will develop as the full-spectrum EDB. The timing and specific site details are largely unknown at this time. The fully developed site and tributary properties is referred to as the “ultimate condition”.

All on-site swales, culverts, and conveyances were designed for the interim phase. The proposed full-spectrum EDB was designed for the interim condition. To limit the amount of required modifications and re-work upon ultimate developed conditions, the outlet pipe, emergency spillway, pond volume,

6-ft trickle channel, and emergency overflow inlet structure, were all sized per the anticipated ultimate conditions. The 2-ft trickle channel, forebays and orifice plate were all designed per the interim condition to ensure the pond will function as required until the site further develops. Upon development of the remaining undeveloped lots, lot specific drainage report(s) must be submitted to ensure the proposed full-spectrum EDB and drainage system designs herein are adequate to accommodate the developed flows. The reports shall identify any proposed modification, if needed, to ensure proper functionality of the drainage system(s) and compliance with the current EPC criteria. Treated water will outfall to the existing storm infrastructure to the east of the site and will eventually outfall into Sand Creek. A proposed drainage map is provided in Appendix E.

#### **FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION**

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

**Step 1 – Reducing Runoff Volumes:** In the interim site development, the site will remain largely undeveloped. Runoff is routed by sheet flow and grass-lined swales to promote infiltration and reduce runoff. The ultimate site development partly consists of multi-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

**Step 2 – Stabilize Drainageways:** The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the future channel stabilization being designed by Kiowa adjacent to the site and on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek, therefore no downstream stabilization will be accomplished with this project.

**Step 3 – Treat the WQCV:** Water Quality treatment for this site is provided in a proposed full-spectrum extended detention basin (Pond A). It is not practicable to capture runoff from interim Basins A and G due to the grading of those basins. In accordance with Section I.7.1.C.1a of the ECM Stormwater Quality Policy and Procedure, the total uncaptured area for this site total 0.56 acres, which is under the 1 acre maximum threshold. The runoff from this site will be collected within swales to FES and inlets and conveyed to the proposed pond via storm sewer. Upon entrance to the ponds, flows will be captured in forebays designed to promote settlement of suspended solids. A concrete trickle channel is also incorporated into the pond to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. Major flows released from the ponds will be reduced to less than historic rates.



Step 4 –BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include asphalt drives, storm inlets, storm pipe, the full-spectrum EDB Pond A and permanent vegetation. Maintenance responsibilities and plans will be defined at the time of final platting.

## **WATER QUALITY**

The “Soils and Geology Study: Lot 1, Sterling Ranch Recycling Facility” prepared by Entech Engineering showed some bore test results with groundwater located within 4 to 5 feet of the surface. The test borings taken (TB-1 and TB-2) were not located in the immediate vicinity of the proposed full-spectrum EDB, which is located to the southeast portion of the site. See excerpts of the soil report in Appendix D. At the start of construction, the pond shall be excavated to the lowest final grade proposed within the pond’s footprint or observation pits shall be dug to the same elevation within the pond’s proposed footprint. If groundwater is encountered, mitigation shall be required such as clay or geomembrane liners. Any mitigation should be designed per the actual site conditions and by a qualified geotechnical engineer.

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full-spectrum water quality and detention are provided for all developed basins. The ultimate condition was used to size the full-spectrum EDB to ensure the required volume, forebay structures sized per required volumes, outlet structure, trickle channels to ensure capacity for 2% of peak 100-year inflow, and emergency spillway and overflow structure design to ensure freeboard and capacity. The concrete forebays (West and North) were sized per the ultimate tributary areas for each to ensure they had the required volumes and release rates for the ultimate condition. The outlet structure was designed to replace the interim orifice plate with the ultimate orifice plate to ensure drain times were met in both conditions.

The interim condition will utilize the same pond grading design and outlet structure, but will have a different orifice plate design to ensure the interim design meets criteria for drain times. Upon development of the surrounding properties (unplatted land to the north and tract land to the east) and the ultimate site, a lot specific drainage report shall be prepared to confirm the adequacy of Pond A to accept, treat, and detain the developed flows per EPC requirements and acceptable criteria.

Where possible, flows were routed through proposed swales to promote infiltration and reduce runoff. Flows for the interim site are routed through the proposed swales and the proposed storm sewer system to a proposed full-spectrum extended detention basin, Pond A. The proposed ultimate WQCV for the pond shall be released within 40 hours and the ultimate EURV shall be released within 72 hours. Proposed interim Basins B-F, OS1, and OS2 are tributary to the proposed Pond A. It is not practicable to capture runoff from interim Basins A and G due to the grading of those basins. In accordance with Section I.7.1.C.1a of the ECM Stormwater Quality Policy and Procedure, the



total uncaptured area for this site total 0.56 acres, which is under the 1 acre maximum threshold. The table below provides the volumes required for the proposed pond, along with the release rates for the 5-year and 100-year storm. The proposed pond will utilize forebays, trickle channels, and an outlet structure to dissipate energy and treat flows. The proposed outlet structure for this pond shall reduce the release rates for the major storm events to less than historic rates to minimize adverse impacts to downstream stormwater facilities. For some minor storm events, the release rate is higher than the existing predevelopment flows. Attempting to get the 5-year outflow ratio to 1 will severely affect the drain times for the WQCV, EURV and 100-year. Doing so would also violate the Colorado Law for the 72 hour drain time for 97% of the 5-year storm. There are no adverse affects from the increase in flow in the minor storm as the existing storm system was designed to handle the peak 100-year flows which greatly surpass the 5-year flow rates. See the proposed sub-basin section above for a comparison of flows leaving the site. The outlet structure was designed to meet drain times for the WQCV, EURV, and 100-year events.

A broad crested weir lined with Type L buried soil riprap is provided as an emergency spillway for Pond A. A concrete cutoff wall is not required as the flows are spread over the 120' wide crest and have sufficient stability with the use of Type L buried soil riprap. The emergency spillway provided will convey flows into a proposed outfall channel that will direct flows to the proposed emergency overflow structure (Double Type D sump inlet) to the south of the existing sanitary lift station. The emergency overflow structure was sized to have the capacity for the ultimate peak undetained 100-year flow for Pond A and connects to the existing storm infrastructure that crosses Marksheffel Rd. This will ensure that emergency flows are captured and are directed away from Aspen Meadows Subdivision Filing No. 2.

The released flows from Pond A discharges into the proposed emergency overflow structure and then connects to an existing 10.33'x10.33' storm junction box. Flows upstream from the north of this junction within the existing 54" RCP storm line are  $Q_5=30.7$  cfs and  $Q_{100}=233.4$  cfs. The proposed released flows ( $Q_5=1.5$  cfs,  $Q_{100}=22.2$  cfs) combine with these existing flows and then continues within an existing 66" RCP storm pipe for a total flow of  $Q_5=32.2$  cfs and  $Q_{100}=255.6$  cfs. The existing 66" RCP was designed for Filing 2 DP4.7 flows ( $Q_5=58.4$  cfs,  $Q_{100}=248.6$  cfs) and the ultimate condition flows will result in an increase in flows in the major storm. The StormCAD analysis in Appendix C shows that the existing storm system was designed deep enough to have the capacity for the increase in flow. The existing storm system the proposed site ties continues to travel east and south about 1,800 feet before ultimately releasing directly into Sand Creek.

Pond A will be private and maintained by the property owner. Access shall be granted to the owner and El Paso County for maintenance of the private full-spectrum EDB.



|                 | <b>Required Volume (ac-ft)</b> | <b>Provided Volume (ac-ft)</b> | <b>WQCV (ac-ft)</b> | <b>EURV (ac-ft)</b> | <b>5-year Release (cfs)</b> | <b>100-year Release (cfs)</b> |
|-----------------|--------------------------------|--------------------------------|---------------------|---------------------|-----------------------------|-------------------------------|
| <b>Interim</b>  | 1.054                          | 6.110                          | 0.254               | 0.349               | 0.1                         | 8.3                           |
| <b>Ultimate</b> | 5.864                          | 6.110                          | 1.039               | 4.036               | 1.5                         | 22.2                          |

**EROSION CONTROL PLAN**

We respectfully request that the Erosion Control Plan be submitted in conjunction with the Grading and Erosion Control Plan prior to obtaining a grading permit.

**OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. This includes swales, inlets, and storm sewer that is to be maintained by the property owner. Access is provided from on-site facilities and easements for proposed infrastructure located off-site. The gravel maintenance road access is off future Sterling Ranch Road and wraps around the top of the pond providing access to the 6-foot trickle channel at the bottom of the pond. The trickle channel is 6-foot wide to allow anticipated maintenance vehicles to travel towards required pond structures (forebays and outlet structure) for the proposed pond.

**DRAINAGE AND BRIDGE FEES**

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees are presented below and will be due at time of platting (depending on date of plat submittal):

| <b>Sterling Ranch Recycling Facility - Impervious Area Calculation</b> |                |              |                  |
|--|----------------|--------------|------------------|
| Breakdown  | Area (acres)   | % Impervious | Impervious Acres |
| R.O.W.   | 1.7826         | 100%         | 1.78             |
| Lot 1  | 4.7423         | 90%          | 4.27             |
| Lot 2  | 24.0565        | 65%          | 15.64            |
| Tracts A - EDB   | 1.8448         | 2%           | 0.04             |
| <b>Total</b>   | <b>32.4262</b> |              | <b>21.72</b>     |

| <b>2024 Drainage and Bridge Fees – Sterling Ranch Recycling Facility</b> |   |                            |  |  |
|--|---|----------------------------|--|--|
| Impervious Acres (ac.)   | Sand Creek Drainage Fee (Per Imp. Acre) | Bridge Fee (Per Imp. Acre) | Sterling Ranch Recycling Facility Drainage Fee | Sterling Ranch Recycling Facility Bridge Fee |
| 21.72  | \$25,632                                | \$10,484                   | \$556,837.03                                   | \$227,757.47                                 |

**CONSTRUCTION COST OPINION**

A construction cost opinion for the drainage infrastructure has been provided below. The below cost opinion is only an estimate of facility and drainage infrastructure cost and may vary.

| <b>Sterling Ranch Recycling Facility (Drainage Infrastructure)</b> |                                |          |      |                  |              |
|--|--------------------------------|----------|------|------------------|--------------|
| Item   | Description                    | Quantity | Unit | Unit Price       | Cost         |
| 1  | 18" RCP                        | 18       | L.F. | \$ 82            | \$ 1,476.00  |
| 2  | 24" RCP                        | 253      | L.F. | \$ 98            | \$ 24,794.00 |
| 3  | 36" RCP                        | 21       | L.F. | \$ 151           | \$ 3,171.00  |
| 4  | 48" RCP                        | 52       | L.F. | \$ 245           | \$ 12,740.00 |
| 5  | 54" RCP                        | 48       | L.F. | \$ 320           | \$ 15,360.00 |
| 6  | 24" FES                        | 2        | Ea.  | \$ 588           | \$ 1,176.00  |
| 7  | 54" FES                        | 1        | Ea.  | \$ 1,920         | \$ 1,920.00  |
| 8  | Type C Inlet                   | 1        | Ea.  | \$ 6,037         | \$ 6,037.00  |
| 9  | Type D Inlet                   | 2        | Ea.  | \$ 7,458         | \$ 14,916.00 |
| 10   | Storm Sewer Manhole, Box Base  | 1        | Ea.  | \$ 15,130        | \$ 15,130.00 |
| 11   | Type L Soil Riprap (18" Depth) | 8        | CY   | \$ 50            | \$ 400.00    |
|  |                                |          |      | <b>Sub-Total</b> | \$ 97,120.00 |

| <b>Sterling Ranch Recycling Facility (Pond A)</b> |   |          |      |                  |               |
|---|---|----------|------|------------------|---------------|
| Item  | Description                                     | Quantity | Unit | Unit Price       | Cost          |
| 1   | Concrete Pavement (8") Trickle Channel-6' Wide  | 652      | L.F. | \$ 60            | \$ 39,120.00  |
| 2   | Concrete Forebay-North Forebay                  | 1        | Ea.  | \$ 12,000        | \$ 12,000.00  |
| 3   | Concrete Forebay-West Forebay                   | 1        | Ea.  | \$ 18,000        | \$ 18,000.00  |
| 4   | Outlet Structure                                | 1        | Ea.  | \$ 18,000        | \$ 18,000.00  |
| 5   | Type VL Soil Riprap (12" Depth)                 | 3        | CY   | \$ 50            | \$ 150.00     |
| 6   | Type L Soil Riprap (18" Depth)                  | 748      | CY   | \$ 70            | \$ 52,360.00  |
| 7   | Aggregate Base Course (Class 6) (8" Thickness)  | 212      | CY   | \$ 133           | \$ 28,196.00  |
| 8   | Aggregate Base Course (Class 6) (12" Thickness) | 47       | CY   | \$ 133           | \$ 6,251.00   |
|   |   |          |      | <b>Sub-Total</b> | \$ 174,077.00 |

**SUMMARY**

The proposed Sterling Ranch Recycling Facility drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the off-site drainage ways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.

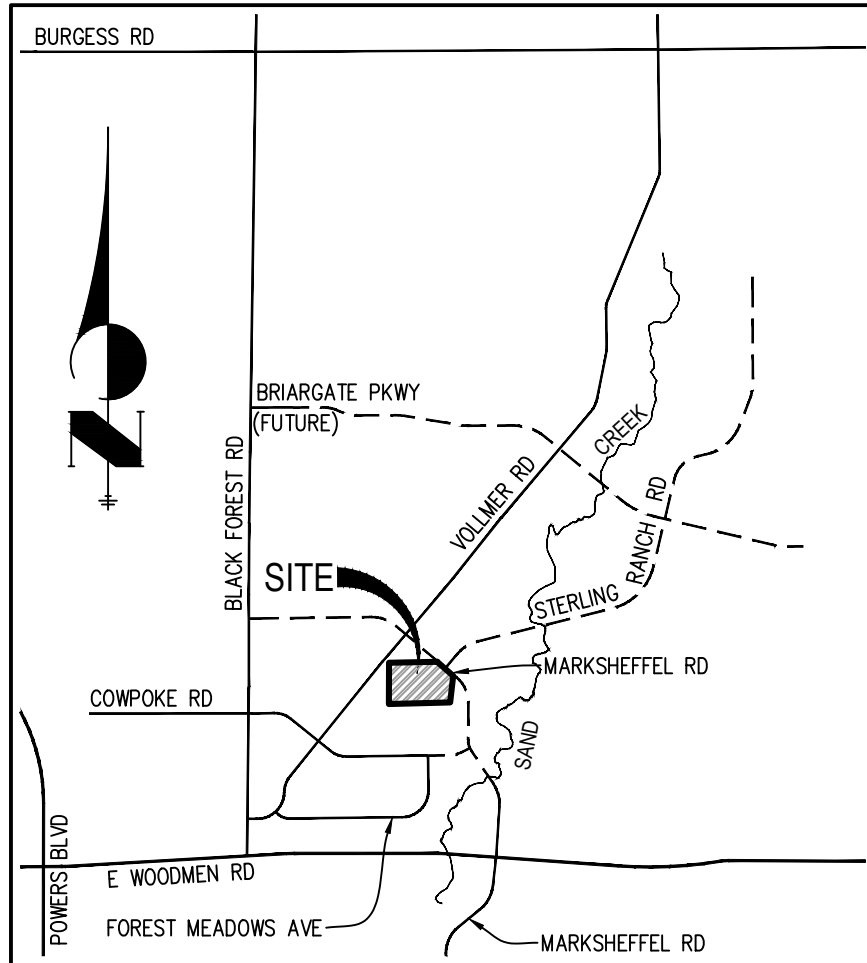
## REFERENCES

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1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
  2. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
  3. Sand Creek Drainage Basin Planning Study, prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
  4. "Final Drainage Report for Sterling Ranch Filing No. 2", prepared by JR Engineering, dated August 2021
  5. Soils and Geology Study: Lot 1, Sterling Ranch Recycling Facility, Entech Engineering, Inc., April 2023.
-

**Appendix A**  
**Vicinity Map, Soil Descriptions, FEMA Floodplain Map**





## VICINITY MAP

N.T.S.

STERLING RECYCLING FACILITY  
 VICINITY MAP  
 JOB NO. 25188.00  
 6/3/22  
 SHEET 1 OF 1

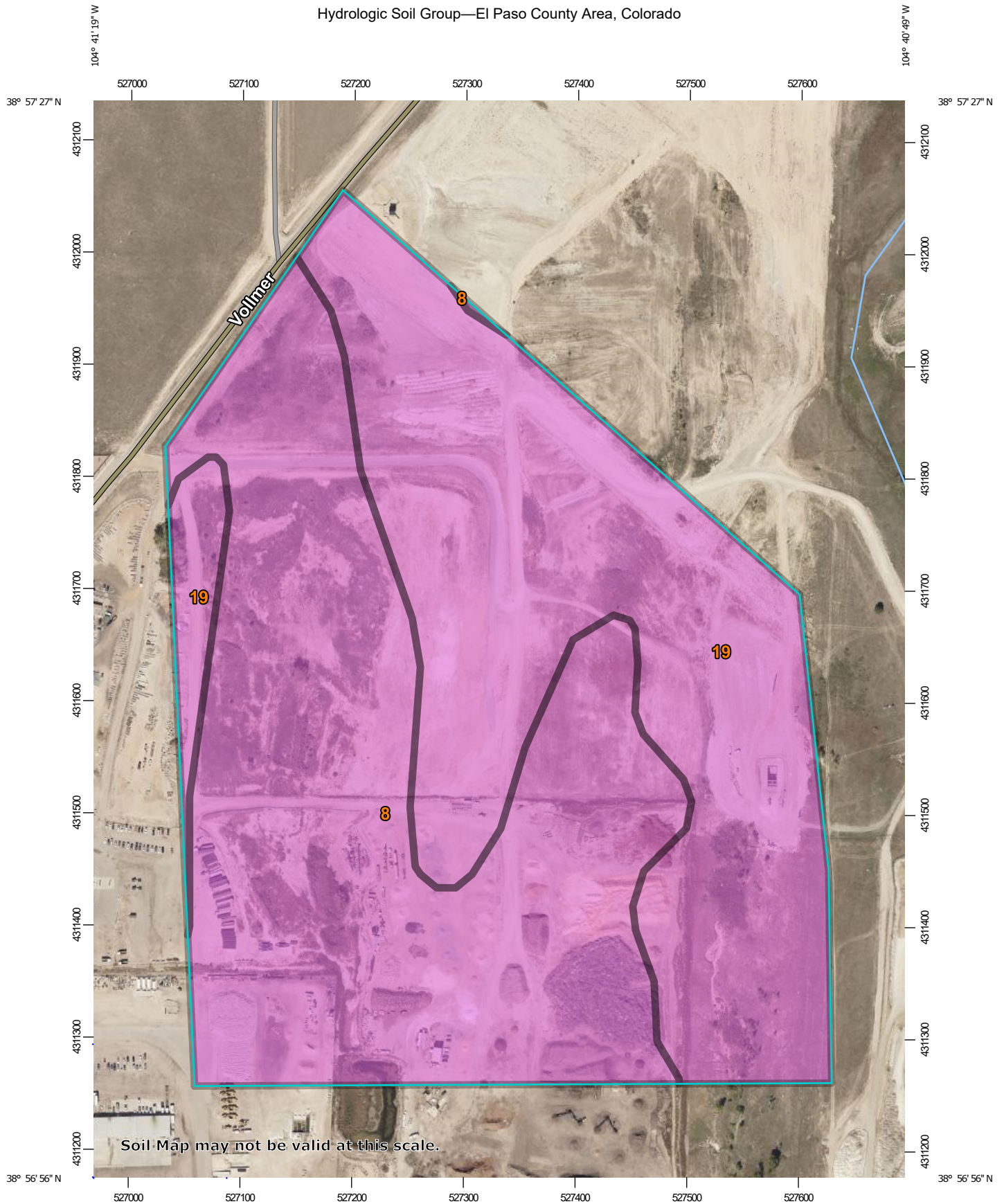


**J·R ENGINEERING**

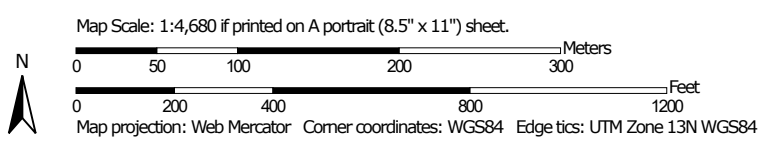
A Westrian Company

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 Fort Collins 970-491-9888 • [www.jrengineering.com](http://www.jrengineering.com)

Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**




-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

| Map unit symbol                    | Map unit name  | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| 8                                  | Blakeland loamy sand, 1 to 9 percent slopes          | A      | 46.2         | 51.5%          |
| 19                                 | Columbine gravelly sandy loam, 0 to 3 percent slopes | A      | 43.6         | 48.5%          |
| <b>Totals for Area of Interest</b> |  |        | <b>89.8</b>  | <b>100.0%</b>  |

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



## Rating Options

*Aggregation Method: Dominant Condition*

*Component Percent Cutoff: None Specified*

*Tie-break Rule: Higher*

**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community may repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones across users in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
 NOAA, NNGS12  
 National Geodetic Survey  
 SSMC-3, #9222  
 1315 East-West Highway  
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the information Services Branch of the National Geodetic Survey at (201) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

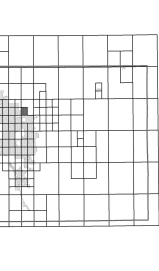
If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/inf>.

**El Paso County Vertical Datum Offset Table**

| Flooding Source | Vertical Datum Offset (ft) |
|-----------------|----------------------------|
|                 |                            |

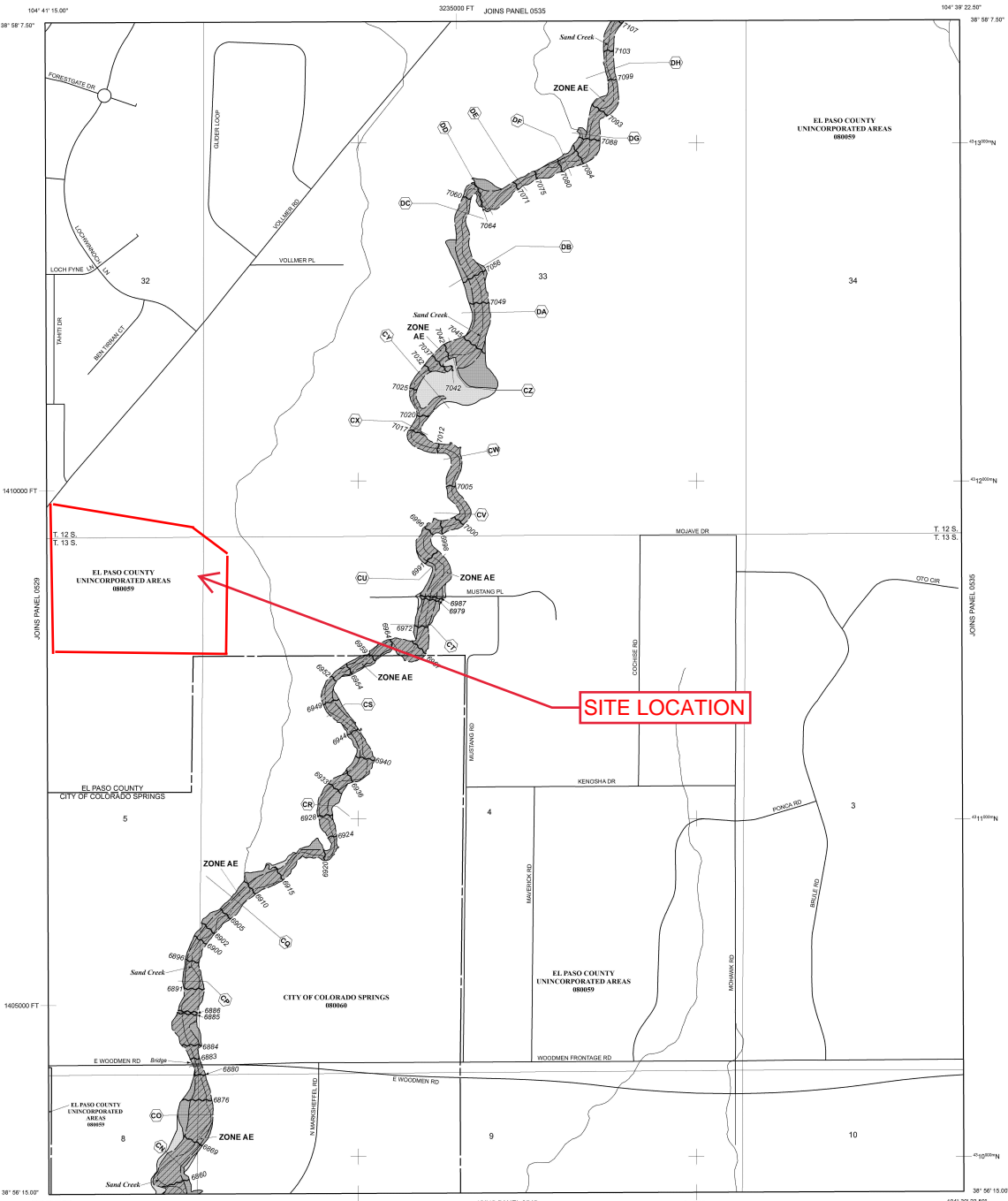
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM/STREAM VERTICAL DATUM CONVERSION INFORMATION.

**Panel Location Map**



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Plan (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

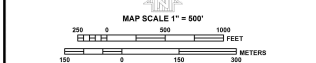
Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

**LEGEND**

- SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD
- The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AV, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.
- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was previously determined. Zone AR indicates that the former flood control system is being retained to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.
- FLOODWAY AREAS IN ZONE AE
- The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.
- OTHER FLOOD AREAS**
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with velocities less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS
- OTHERWISE PROTECTED AREAS (OPA)
- CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.
- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary of Special Flood Hazard Areas of different Base Flood Elevations, Flood Depths or Flood Velocities
- Base Flood Elevation line and value, elevation in feet\* (EL 5.87)
- Base Flood Elevation where uniform within zone; elevation in feet\*
- \* Referenced to the North American Vertical Datum of 1988 (NAVD 88)
- Cross section line
- Transect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 500-foot grid ticks, Colorado State Plane coordinate system, zone 10
- Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM report)
- River file
- M1.5** River file
- MAP REPOSITORIES**
- Refer to Map Repository list on Map Index
- EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP**
- MARCH 17, 1997**
- EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL**
- DECEMBER 7, 2018** to update cartographic information, change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.
- For community map revision history prior to cartographic mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.
- To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



**NATIONAL FLOOD INSURANCE PROGRAM**

**PANEL 0533G**

**FIRM**

**FLOOD INSURANCE RATE MAP**

**EL PASO COUNTY, COLORADO AND INCORPORATED AREAS**

**PANEL 533 OF 1300**

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

| COUNTY         | NUMBER | PANEL | SUFFIX |
|----------------|--------|-------|--------|
| COLORADO       | 0711 G | 0808  | 003 G  |
| EL PASO COUNTY | 0808   | 0038  | 003 G  |

Notes to User: The Map Number shown below should be used when ordering map copies. The Community Number shown above should be used on insurance applications for the subject community.

**MAP NUMBER**  
08041C0533G

**MAP REVISED**  
**DECEMBER 7, 2018**

Federal Emergency Management Agency

## **Appendix B**

### **Hydrologic Calculations**

# COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 1/18/24

| Basin ID | Total Area (ac) | Streets-Paved (100% Impervious) |                  |           |                 | Streets-Gravel (80% Impervious) |                  |           |                 | Historical Analysis (2% Impervious) |                  |           |                 | Basins Total Weighted C Values |                  | Basins Total Weighted % Imp. |
|----------|-----------------|---------------------------------|------------------|-----------|-----------------|---------------------------------|------------------|-----------|-----------------|-------------------------------------|------------------|-----------|-----------------|--------------------------------|------------------|------------------------------|
|          |                 | C <sub>5</sub>                  | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                  | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                      | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                 | C <sub>100</sub> |                              |
|          |                 | EXA                             | 2.68             | 0.90      | 0.96            | 0.16                            | 6.0%             | 0.59      | 0.70            | 0.00                                | 0.0%             | 0.09      | 0.36            | 2.52                           | 1.9%             |                              |
| EXB      | 2.60            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 2.60      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| EXC      | 2.11            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.33      | 12.5%           | 0.09                                | 0.36             | 1.78      | 1.7%            | 0.17                           | 0.41             | 14.2%                        |
| EXD      | 13.44           | 0.90                            | 0.96             | 0.86      | 6.4%            | 0.59                            | 0.70             | 1.48      | 8.8%            | 0.09                                | 0.36             | 11.10     | 1.7%            | 0.20                           | 0.44             | 16.9%                        |
| EXE      | 8.51            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 8.51      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| EXF      | 3.09            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 3.09      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS1      | 8.74            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 8.74      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS2      | 0.53            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.53      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS3      | 0.29            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.59                            | 0.70             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.29      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| TOTAL    | 41.99           |                                 |                  |           |                 |                                 |                  |           |                 |                                     |                  |           |                 |                                |                  | 7.7%                         |

## EXISTING STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By: \_\_\_\_\_  
Date: 1/18/24

| SUB-BASIN |           |                        |                |                |                  | INITIAL/OVERLAND  |                    |                      | TRAVEL TIME         |                    |      |             |                      | t <sub>c</sub> CHECK       |                   |                                | FINAL |
|-----------|-----------|------------------------|----------------|----------------|------------------|-------------------|--------------------|----------------------|---------------------|--------------------|------|-------------|----------------------|----------------------------|-------------------|--------------------------------|-------|
| DATA      |           |                        |                |                |                  | (T <sub>i</sub> ) |                    |                      | (T <sub>i</sub> )   |                    |      |             |                      | (URBANIZED BASINS)         |                   |                                |       |
| BASIN ID  | D.A. (ac) | Hydrologic Soils Group | Impervious (%) | C <sub>5</sub> | C <sub>100</sub> | L (ft)            | S <sub>o</sub> (%) | t <sub>i</sub> (min) | L <sub>t</sub> (ft) | S <sub>t</sub> (%) | K    | VEL. (ft/s) | t <sub>t</sub> (min) | COMP. t <sub>c</sub> (min) | TOTAL LENGTH (ft) | Urbanized t <sub>c</sub> (min) |       |
| EXA       | 2.68      | A                      | 8%             | 0.14           | 0.40             | 300               | 4.0%               | 19.0                 | 190                 | 2.3%               | 10.0 | 1.5         | 2.1                  | 21.1                       | 490.0             | 26.7                           | 21.1  |
| EXB       | 2.60      | A                      | 2%             | 0.09           | 0.36             | 300               | 2.5%               | 23.3                 | 240                 | 2.5%               | 10.0 | 1.6         | 2.5                  | 25.9                       | 540.0             | 28.4                           | 25.9  |
| EXC       | 2.11      | A                      | 14%            | 0.17           | 0.41             | 300               | 2.6%               | 21.3                 | 135                 | 1.7%               | 15.0 | 2.0         | 1.2                  | 22.4                       | 435.0             | 25.2                           | 22.4  |
| EXD       | 13.44     | A                      | 17%            | 0.20           | 0.44             | 300               | 3.6%               | 18.5                 | 810                 | 3.4%               | 15.0 | 2.8         | 4.9                  | 23.4                       | 1110.0            | 29.6                           | 23.4  |
| EXE       | 8.51      | A                      | 2%             | 0.09           | 0.36             | 300               | 4.0%               | 20.0                 | 800                 | 3.0%               | 10.0 | 1.7         | 7.7                  | 27.7                       | 1100.0            | 34.0                           | 27.7  |
| EXF       | 3.09      | A                      | 2%             | 0.09           | 0.36             | 300               | 3.5%               | 20.9                 | 400                 | 4.3%               | 10.0 | 2.1         | 3.2                  | 24.1                       | 700.0             | 29.1                           | 24.1  |
| OS1       | 8.74      | A                      | 2%             | 0.09           | 0.36             | 150               | 2.0%               | 17.8                 | 850                 | 0.2%               | 10.0 | 0.4         | 31.7                 | 49.4                       | 1000.0            | 59.8                           | 49.4  |
| OS2       | 0.53      | A                      | 2%             | 0.09           | 0.36             | 155               | 3.0%               | 15.8                 | 0                   | 0.0%               | 10.0 | 0.0         | 0.0                  | 15.8                       | 155.0             | 25.7                           | 15.8  |
| OS3       | 0.29      | A                      | 2%             | 0.09           | 0.36             | 35                | 15.0%              | 4.4                  | 0                   | 0.0%               | 10.0 | 0.0         | 0.0                  | 4.4                        | 35.0              | 25.7                           | 5.0   |

NOTES:

$$t_c = t_i + t_t$$

Equation 6-2

$$t_t = \frac{0.395(1.1 - C_5)\sqrt{L_t}}{S_o^{0.33}}$$

Equation 6-3

Where:

t<sub>c</sub> = computed time of concentration (minutes)

t<sub>i</sub> = overland (initial) flow time (minutes)

t<sub>t</sub> = channelized flow time (minutes).

Where:

t<sub>i</sub> = overland (initial) flow time (minutes)

C<sub>5</sub> = runoff coefficient for 5-year frequency (from Table 6-4)

L<sub>t</sub> = length of overland flow (ft)

S<sub>o</sub> = average slope along the overland flow path (ft/ft).

Use a minimum t<sub>c</sub> value of 5 minutes for urbanized areas and a minimum t<sub>c</sub> value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Equation 6-4  $t_t = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_o}}$

Equation 6-5

Where:

t<sub>t</sub> = channelized flow time (travel time, min)

L<sub>t</sub> = waterway length (ft)

S<sub>o</sub> = waterway slope (ft/ft)

V<sub>t</sub> = travel time velocity (ft/sec) = K√S<sub>o</sub>

K = NRCS conveyance factor (see Table 6-2).

Where:

t<sub>c</sub> = minimum time of concentration for first design point when less than t<sub>c</sub> from Equation 6-1.

L<sub>t</sub> = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S<sub>o</sub> = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

| Type of Land Surface                 | Conveyance Factor, K |
|--------------------------------------|----------------------|
| Heavy meadow                         | 2.5                  |
| Tillage/field                        | 5                    |
| Short pasture and lawns              | 7                    |
| Nearly bare ground                   | 10                   |
| Grassed waterway                     | 15                   |
| Paved areas and shallow paved swales | 20                   |

**STANDARD FORM SF-3 - EXISTING**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County  
Design Storm: 5-Year

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By:  
Date: 1/18/24

| STREET | Design Point | DIRECT RUNOFF |           |               |                      |          |           |         | TOTAL RUNOFF         |          |           |         | STREET/SWALE                    |          |           | PIPE                    |          |           |                    | TRAVEL TIME |                |                      | REMARKS   |
|--------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|---|
|        |              | Basin ID      | Area (Ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (Ac) | I (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q <sub>street/swale</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>r</sub> (min) |   |
|        | 1            | EXA           | 2.68      | 0.14          | 21.1                 | 0.37     | 3.01      | 1.1     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP1<br>Flows off-site to the west                         |
|        | 2            | EXB           | 2.60      | 0.09          | 25.9                 | 0.23     | 2.70      | 0.6     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP2<br>Flows off-site to the west                         |
|        | 3            | EXC           | 2.11      | 0.17          | 22.4                 | 0.35     | 2.92      | 1.0     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP3<br>Flows off-site to the south         |
|        | 4            | EXD           | 13.44     | 0.20          | 23.4                 | 2.65     | 2.85      | 7.6     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP4<br>Flows off-site to the south         |
|        | 5            | OS1           | 8.74      | 0.09          | 49.4                 | 0.79     | 1.73      | 1.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP5<br>Flows on-site and combines at DP7.1 |
|        | 6            | OS3           | 0.29      | 0.09          | 5.0                  | 0.03     | 5.17      | 0.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP6<br>Flows on-site and combines at DP7.1                |
|        | 7            | EXE           | 8.51      | 0.09          | 27.7                 | 0.77     | 2.60      | 2.0     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP7<br>Combines flows at DP7.1             |
|        | 7.1          |               |           |               |                      |          |           |         | 49.4                 | 1.59     | 1.73      | 2.8     |                                 |          |           |                         |          |           |                    |             |                |                      | Combines the flows from DP5, DP6, and DP7<br>Flows off-site to the south          |
|        | 8            | OS2           | 0.53      | 0.09          | 15.8                 | 0.05     | 3.44      | 0.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP8<br>Combines flows at DP9.1                            |
|        | 9            | EXF           | 3.09      | 0.09          | 24.1                 | 0.28     | 2.81      | 0.8     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP9<br>Combines flows at DP9.1                            |
|        | 9.1          |               |           |               |                      |          |           |         | 24.1                 | 0.33     | 2.81      | 0.9     |                                 |          |           |                         |          |           |                    |             |                |                      | Combines the flows from DP8 and DP9<br>Flows off-site to the east                 |

Notes:  
Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.  
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

**STANDARD FORM SF-3 - EXISTING**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County  
Design Storm: 100-Year

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By: \_\_\_\_\_  
Date: 1/18/24

| Description | Design Point | DIRECT RUNOFF |           |               |                      |          |           |         | TOTAL RUNOFF         |          |           |         | STREET/SWALE                    |          |           | PIPE                    |          |           |                    | TRAVEL TIME |                |                      | REMARKS   |
|-------------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|---|
|             |              | Basin ID      | Area (ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q <sub>street/swale</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>t</sub> (min) |   |
|             | 1            | EXA           | 2.68      | 0.40          | 21.1                 | 1.06     | 5.05      | 5.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP1<br>Flows off-site to the west                         |
|             | 2            | EXB           | 2.60      | 0.36          | 25.9                 | 0.94     | 4.54      | 4.3     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP2<br>Flows off-site to the west                         |
|             | 3            | EXC           | 2.11      | 0.41          | 22.4                 | 0.87     | 4.90      | 4.3     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP3<br>Flows off-site to the south         |
|             | 4            | EXD           | 13.44     | 0.44          | 23.4                 | 5.86     | 4.79      | 28.1    |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP4<br>Flows off-site to the south         |
|             | 5            | OS1           | 8.74      | 0.36          | 49.4                 | 3.15     | 2.90      | 9.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP5<br>Flows on-site and combines at DP7.1 |
|             | 6            | OS3           | 0.29      | 0.36          | 5.0                  | 0.10     | 8.68      | 0.9     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP6<br>Flows on-site and combines at DP7.1                |
|             | 7            | EXE           | 8.51      | 0.36          | 27.7                 | 3.06     | 4.37      | 13.4    |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP7<br>Combines flows at DP7.1             |
|             | 7.1          |               |           |               |                      |          |           |         | 49.4                 | 6.31     | 2.90      | 18.3    |                                 |          |           |                         |          |           |                    |             |                |                      | Combines the flows from DP5, DP6, and DP7<br>Flows off-site to the south          |
|             | 8            | OS2           | 0.53      | 0.36          | 15.8                 | 0.19     | 5.78      | 1.1     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP8<br>Combines flows at DP9.1                            |
|             | 9            | EXF           | 3.09      | 0.36          | 24.1                 | 1.11     | 4.72      | 5.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP9<br>Combines flows at DP9.1                            |
|             | 9.1          |               |           |               |                      |          |           |         | 24.1                 | 1.30     | 4.72      | 6.1     |                                 |          |           |                         |          |           |                    |             |                |                      | Combines the flows from DP8 and DP9<br>Flows off-site to the east                 |

Notes:  
Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.  
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

# COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 1/24/24

| Basin ID                               | Total Area (ac) | Streets-Paved<br>(100% Impervious) |                  |           |                 | Streets-Gravel<br>(80% Impervious) |                  |           |                 | Historical Analysis<br>(2% Impervious) |                  |           |                 | Basins Total Weighted C Values |                  | Basins Total Weighted % Imp. |
|--|-----------------|------------------------------------|------------------|-----------|-----------------|------------------------------------|------------------|-----------|-----------------|--|------------------|-----------|-----------------|--------------------------------|------------------|------------------------------|
|  |                 | C <sub>5</sub>                     | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                     | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                         | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                 | C <sub>100</sub> |                              |
|  |                 | A                                  | 0.50             | 0.90      | 0.96            | 0.00                               | 0.0%             | 0.59      | 0.70            | 0.00                                   | 0.0%             | 0.09      | 0.36            | 0.50                           | 2.0%             |                              |
| B                                      | 14.03           | 0.90                               | 0.96             | 2.45      | 17.5%           | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 11.58     | 1.7%            | 0.23                           | 0.46             | 19.1%                        |
| C                                      | 10.70           | 0.90                               | 0.96             | 0.47      | 4.4%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 10.23     | 1.9%            | 0.13                           | 0.39             | 6.3%                         |
| D                                      | 2.16            | 0.90                               | 0.96             | 0.00      | 0.0%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 2.16      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| E                                      | 3.10            | 0.90                               | 0.96             | 0.40      | 12.9%           | 0.59                               | 0.70             | 0.31      | 8.0%            | 0.09                                   | 0.36             | 2.39      | 1.5%            | 0.24                           | 0.47             | 22.4%                        |
| F                                      | 2.27            | 0.90                               | 0.96             | 0.00      | 0.0%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 2.27      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| G                                      | 0.06            | 0.90                               | 0.96             | 0.04      | 66.7%           | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 0.02      | 0.7%            | 0.63                           | 0.76             | 67.3%                        |
| OS1                                    | 8.74            | 0.90                               | 0.96             | 0.00      | 0.0%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 8.74      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS2                                    | 0.36            | 0.90                               | 0.96             | 0.00      | 0.0%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 0.36      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS3                                    | 0.30            | 0.90                               | 0.96             | 0.00      | 0.0%            | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 0.30      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| OS4                                    | 2.08            | 0.90                               | 0.96             | 1.70      | 81.7%           | 0.59                               | 0.70             | 0.00      | 0.0%            | 0.09                                   | 0.36             | 0.38      | 0.4%            | 0.75                           | 0.85             | 82.1%                        |
| Total W. Forebay<br>(Basins B, C, OS1) | 33.47           |                                    |                  |           |                 |                                    |                  |           |                 |  |                  |           |                 |                                |                  | 10.5%                        |
| Total N. Forebay<br>(Basins D, E, OS2) | 5.62            |                                    |                  |           |                 |                                    |                  |           |                 |  |                  |           |                 |                                |                  | 13.3%                        |
| Total Pond A<br>(Basins B-F, OS1-3)    | 41.66           |                                    |                  |           |                 |                                    |                  |           |                 |  |                  |           |                 |                                |                  | 10.4%                        |



# PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By: \_\_\_\_\_  
Date: 1/24/24

| SUB-BASIN |           |                        |                |                |                  | INITIAL/OVERLAND  |                    |                      | TRAVEL TIME         |                    |      |             |                      | t <sub>c</sub> CHECK       |                   |                                | FINAL                |
|-----------|-----------|------------------------|----------------|----------------|------------------|-------------------|--------------------|----------------------|---------------------|--------------------|------|-------------|----------------------|----------------------------|-------------------|--------------------------------|----------------------|
| DATA      |           |                        |                |                |                  | (T <sub>i</sub> ) |                    |                      | (T <sub>i</sub> )   |                    |      |             |                      | (URBANIZED BASINS)         |                   |                                |                      |
| BASIN ID  | D.A. (ac) | Hydrologic Soils Group | Impervious (%) | C <sub>5</sub> | C <sub>100</sub> | L (ft)            | S <sub>o</sub> (%) | t <sub>i</sub> (min) | L <sub>t</sub> (ft) | S <sub>t</sub> (%) | K    | VEL. (ft/s) | t <sub>t</sub> (min) | COMP. t <sub>c</sub> (min) | TOTAL LENGTH (ft) | Urbanized t <sub>c</sub> (min) | t <sub>c</sub> (min) |
| A         | 0.50      | A                      | 2%             | 0.09           | 0.36             | 20                | 33.0%              | 2.6                  | 0                   | 0.0%               | 10.0 | 0.0         | 0.0                  | 2.6                        | 20.0              | 25.7                           | 5.0                  |
| B         | 14.03     | A                      | 19%            | 0.23           | 0.46             | 300               | 2.7%               | 19.6                 | 1600                | 1.5%               | 15.0 | 1.8         | 14.5                 | 34.1                       | 1900.0            | 41.4                           | 34.1                 |
| C         | 10.70     | A                      | 6%             | 0.13           | 0.39             | 300               | 2.7%               | 22.0                 | 735                 | 1.5%               | 15.0 | 1.8         | 6.7                  | 28.6                       | 1035.0            | 35.0                           | 28.6                 |
| D         | 2.16      | A                      | 2%             | 0.09           | 0.36             | 215               | 3.0%               | 18.6                 | 400                 | 1.5%               | 10.0 | 1.2         | 5.4                  | 24.1                       | 615.0             | 31.5                           | 24.1                 |
| E         | 3.10      | A                      | 22%            | 0.24           | 0.47             | 100               | 1.2%               | 14.5                 | 910                 | 1.5%               | 15.0 | 1.8         | 8.3                  | 22.8                       | 1010.0            | 32.4                           | 22.8                 |
| F         | 2.27      | A                      | 2%             | 0.09           | 0.36             | 40                | 25.0%              | 4.0                  | 615                 | 0.5%               | 10.0 | 0.7         | 14.5                 | 18.5                       | 655.0             | 41.3                           | 18.5                 |
| G         | 0.06      | A                      | 67%            | 0.63           | 0.76             | 54                | 2.0%               | 5.0                  | 35                  | 1.0%               | 20.0 | 2.0         | 0.3                  | 5.3                        | 89.0              | 14.9                           | 5.3                  |
| OS1       | 8.74      | A                      | 2%             | 0.09           | 0.36             | 150               | 2.0%               | 17.8                 | 850                 | 0.2%               | 10.0 | 0.4         | 31.7                 | 49.4                       | 1000.0            | 59.8                           | 49.4                 |
| OS2       | 0.36      | A                      | 2%             | 0.09           | 0.36             | 115               | 3.0%               | 13.6                 | 300                 | 3.0%               | 10.0 | 1.7         | 2.9                  | 16.5                       | 415.0             | 28.8                           | 16.5                 |
| OS3       | 0.30      | A                      | 2%             | 0.09           | 0.36             | 35                | 15.0%              | 4.4                  | 0                   | 0.0%               | 10.0 | 0.0         | 0.0                  | 4.4                        | 35.0              | 25.7                           | 5.0                  |
| OS4       | 2.08      | A                      | 82%            | 0.75           | 0.85             | 15                | 2.0%               | 1.9                  | 1335                | 2.5%               | 20.0 | 3.2         | 7.0                  | 9.0                        | 1350.0            | 18.9                           | 9.0                  |

**NOTES:**

$$t_c = t_i + t_t$$

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$$

Equation 6-3

Where:

t<sub>c</sub> = computed time of concentration (minutes)

t<sub>i</sub> = overland (initial) flow time (minutes)

t<sub>t</sub> = channelized flow time (minutes).

Where:

t<sub>i</sub> = overland (initial) flow time (minutes)

C<sub>5</sub> = runoff coefficient for 5-year frequency (from Table 6-4)

L<sub>i</sub> = length of overland flow (ft)

S<sub>o</sub> = average slope along the overland flow path (ft/ft).

Use a minimum t<sub>c</sub> value of 5 minutes for urbanized areas and a minimum t<sub>c</sub> value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Equation 6-4  $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$

Equation 6-5

Where:

t<sub>t</sub> = channelized flow time (travel time, min)

L<sub>t</sub> = waterway length (ft)

S<sub>o</sub> = waterway slope (ft/ft)

V<sub>t</sub> = travel time velocity (ft/sec) = K√S<sub>o</sub>

K = NRCS conveyance factor (see Table 6-2).

Where:

t<sub>c</sub> = minimum time of concentration for first design point when less than t<sub>c</sub> from Equation 6-1.

L<sub>t</sub> = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S<sub>t</sub> = slope of the channelized flow path (ft/ft).

**Table 6-2. NRCS Conveyance factors, K**

| Type of Land Surface                 | Conveyance Factor, K |
|--------------------------------------|----------------------|
| Heavy meadow                         | 2.5                  |
| Tillage/field                        | 5                    |
| Short pasture and lawns              | 7                    |
| Nearly bare ground                   | 10                   |
| Grassed waterway                     | 15                   |
| Paved areas and shallow paved swales | 20                   |

**STANDARD FORM SF-3 - PROPOSED  
STORM DRAINAGE SYSTEM DESIGN  
(RATIONAL METHOD PROCEDURE)**

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County  
 Design Storm: 5-Year

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By:  
 Date: 1/24/24

| STREET | Design Point | DIRECT RUNOFF |           |               |                      |          |           |         | TOTAL RUNOFF         |          |           |         | STREET/SWALE                    |          |           | PIPE                    |          |           |                    | TRAVEL TIME |                |                      | REMARKS  |
|--------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|--|
|        |              | Basin ID      | Area (Ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (Ac) | I (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q <sub>street/swale</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>t</sub> (min) |  |
|        | 1            | A             | 0.50      | 0.09          | 5.0                  | 0.05     | 5.17      | 0.3     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows overland along the western site boundary to DP1<br>Flows off-site to the west  |
|        | 2            | B             | 14.03     | 0.23          | 34.1                 | 3.25     | 2.29      | 7.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP2<br>Combines flow at FES at DP4.2   |
|        | 3            | OS1           | 8.74      | 0.09          | 49.4                 | 0.79     | 1.73      | 1.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP3<br>Flows on-site and combines at culvert at DP4.1   |
|        | 4            | C             | 10.70     | 0.13          | 28.6                 | 1.34     | 2.55      | 3.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP4<br>Combines flow at culvert at DP4.1   |
|        | 4.1          |               |           |               |                      |          |           |         | 49.4                 | 2.13     | 1.73      | 3.7     |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP3 and DP4 within culvert<br>Swale to FES at DP4.2   |
|        | 4.2          |               |           |               |                      |          |           |         | 49.4                 | 5.38     | 1.73      | 9.3     |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP2 and DP4.1 at sump inlet<br>Piped to pond forebay, combines flow at DP9.1  |
|        | 5            | D             | 2.16      | 0.09          | 24.1                 | 0.19     | 2.81      | 0.5     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP5<br>Combines flow at sump inlet at DP7.1  |
|        | 6            | E             | 3.10      | 0.24          | 22.8                 | 0.76     | 2.89      | 2.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP6<br>Combines flow at sump inlet at DP7.1  |
|        | 7            | OS2           | 0.36      | 0.09          | 16.5                 | 0.03     | 3.38      | 0.1     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP7<br>Combines flow at sump inlet at DP7.1  |
|        | 7.1          |               |           |               |                      |          |           |         | 24.1                 | 0.98     | 2.81      | 2.8     |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP5, DP6, and DP7 at sump inlet<br>Piped to pond forebay, combines flow at DP9.1  |
|        | 8            | OS3           | 0.30      | 0.09          | 5.0                  | 0.03     | 5.17      | 0.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP8<br>Combines flow at DP9.1  |
|        | 9            | F             | 2.27      | 0.09          | 18.5                 | 0.20     | 3.21      | 0.6     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows along trickle channel to DP9 at outlet structure<br>Combines flow at DP9.1   |
|        | 9.1          |               |           |               |                      |          |           |         | 49.4                 | 6.59     | 1.73      | 11.4    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP4.2, DP7.1, DP8 and DP9. Total interim pond inflow.<br>Released through pond outlet structure at DP9.2                    |
|        | 9.2          |               |           |               |                      |          |           |         | -                    | -        | -         | 0.1     |                                 |          |           |                         |          |           |                    |             |                |                      | Released flow through interim outlet structure from MHFD_Detention<br>Piped to existing junction box and storm infrastructure                |
|        | 10           | G             | 0.06      | 0.63          | 5.3                  | 0.04     | 5.09      | 0.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows along prop. Sterling Ranch Rd. c&g to DP10 to Marksheffel Rd.<br>Combines at existing Marksheffel Rd. existing 15' Type R inlet.       |
|        | 11           | OS4           | 2.08      | 0.75          | 9.0                  | 1.56     | 4.29      | 6.7     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Off-site work along existing Marksheffel Rd. c&g to ex. 15' Type R inlet.<br>Combines at existing Marksheffel Rd. existing 15' Type R inlet. |
|        | 11.1         |               |           |               |                      |          |           |         | 9.0                  | 1.60     | 4.29      | 6.9     |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP 10 and DP11 within existing 15' Type R inlet.<br>Captured flow continues off-site southeast along Marksheffel Rd. storm  |

Notes:  
 Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.  
 All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

**STANDARD FORM SF-3 - PROPOSED  
STORM DRAINAGE SYSTEM DESIGN  
(RATIONAL METHOD PROCEDURE)**

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County  
 Design Storm: 100-Year

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 1/24/24

| Description | Design Point | DIRECT RUNOFF |           |               |                      |          |           |         | TOTAL RUNOFF         |          |           |         | STREET/SWALE                    |          |           | PIPE                    |          |           |                    | TRAVEL TIME |                |                      | REMARKS  |
|-------------|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|--|
|             |              | Basin ID      | Area (ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac) | I (in/hr) | Q (cfs) | Q <sub>street/swale</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>t</sub> (min) |  |
|             | 1            | A             | 0.50      | 0.36          | 5.0                  | 0.18     | 8.68      | 1.6     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows overland along the western site boundary to DP1<br>Flows off-site to the west  |
|             | 2            | B             | 14.03     | 0.46          | 34.1                 | 6.52     | 3.84      | 25.1    |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP2<br>Combines flow at FES at DP4.2   |
|             | 3            | OS1           | 8.74      | 0.36          | 49.4                 | 3.15     | 2.90      | 9.2     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland and along berm to DP3<br>Flows on-site and combines at culvert at DP4.1   |
|             | 4            | C             | 10.70     | 0.39          | 28.6                 | 4.13     | 4.28      | 17.7    |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP4<br>Combines flow at culvert at DP4.1   |
|             | 4.1          |               |           |               |                      |          |           |         | 49.4                 | 7.28     | 2.90      | 21.1    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP3 and DP4 within culvert<br>Swale to FES at DP4.2   |
|             | 4.2          |               |           |               |                      |          |           |         | 49.4                 | 13.80    | 2.90      | 40.1    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP2 and DP4.1 at sump inlet<br>Piped to pond forebay, combines flow at DP9.1  |
|             | 5            | D             | 2.16      | 0.36          | 24.1                 | 0.78     | 4.72      | 3.7     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP5<br>Combines flow at sump inlet at DP7.1  |
|             | 6            | E             | 3.10      | 0.47          | 22.8                 | 1.46     | 4.86      | 7.1     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to swale and then to DP6<br>Combines flow at sump inlet at DP7.1  |
|             | 7            | OS2           | 0.36      | 0.36          | 16.5                 | 0.13     | 5.67      | 0.7     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP7<br>Combines flow at sump inlet at DP7.1  |
|             | 7.1          |               |           |               |                      |          |           |         | 24.1                 | 2.37     | 4.72      | 11.2    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP5, DP6, and DP7 at sump inlet<br>Piped to pond forebay, combines flow at DP9.1  |
|             | 8            | OS3           | 0.30      | 0.36          | 5.0                  | 0.11     | 8.68      | 1.0     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Sheet flows overland to DP8<br>Combines flow at DP9.1  |
|             | 9            | F             | 2.27      | 0.36          | 18.5                 | 0.82     | 5.38      | 4.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows along trickle channel to DP9 at outlet structure<br>Combines flow at DP9.1   |
|             | 9.1          |               |           |               |                      |          |           |         | 49.4                 | 16.99    | 2.90      | 49.4    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP4.2, DP7.1, DP8 and DP9. Total interim pond inflow.<br>Released through pond outlet structure at DP9.2                    |
|             | 9.2          |               |           |               |                      |          |           |         | -                    | -        | -         | 8.3     |                                 |          |           |                         |          |           |                    |             |                |                      | Released flow through interim outlet structure from MHFD_Detention<br>Piped to existing junction box and storm infrastructure                |
|             | 10           | G             | 0.06      | 0.76          | 5.3                  | 0.05     | 8.56      | 0.4     |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Flows along prop. Sterling Ranch Rd. c&g to DP10 to Marksheffel Rd.<br>Combines at existing Marksheffel Rd. existing 15' Type R inlet.       |
|             | 11           | OS4           | 2.08      | 0.85          | 9.0                  | 1.77     | 7.21      | 12.8    |                      |          |           |         |                                 |          |           |                         |          |           |                    |             |                |                      | Off-site work along existing Marksheffel Rd. c&g to ex. 15' Type R inlet.<br>Combines at existing Marksheffel Rd. existing 15' Type R inlet. |
|             | 11.1         |               |           |               |                      |          |           |         | 9.0                  | 1.82     | 7.21      | 13.1    |                                 |          |           |                         |          |           |                    |             |                |                      | Combined flow of DP 10 and DP11 within existing 15' Type R inlet.<br>Captured flow continues off-site southeast along Marksheffel Rd. storm  |

Notes:  
 Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.  
 All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

## COMPOSITE % IMPERVIOUS & COMPOSITE ULTIMATE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 2/8/24

| Basin ID  | Total Area (ac) | Industrial-Heavy Areas (90% Impervious) |                  |           |                 | Business-Commercial Areas (95% Impervious) |                  |           |                 | Residential-1/8 Acre or Less (65% Impervious) |                  |           |                 | Streets-Paved (100% Impervious) |                  |           |                 | Historical Analysis (2% Impervious) |                  |           |                 | Basins Total Weighted C Values |                  | Basins Total Weighted % Imp. |
|---|-----------------|---|------------------|-----------|-----------------|--|------------------|-----------|-----------------|---|------------------|-----------|-----------------|---------------------------------|------------------|-----------|-----------------|-------------------------------------|------------------|-----------|-----------------|--------------------------------|------------------|------------------------------|
|   |                 | C <sub>5</sub>                          | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                             | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                                | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                  | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                      | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                 | C <sub>100</sub> |                              |
|   |                 | Lot 1 Heavy Industrial                  | 4.74             | 0.73      | 0.81            | 4.74                                       | 90.0%            | 0.81      | 0.88            | 0.00  | 0.0%             | 0.45      | 0.59            | 0.00                            | 0.0%             | 0.90      | 0.96            | 0.00                                | 0.0%             | 0.09      | 0.36            | 0.00                           | 0.0%             |                              |
| Urban Non-Residential Collector Roadway (R.O.W.)          | 1.78            | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 1.40      | 78.7%           | 0.09                                | 0.36             | 0.38      | 0.4%            | 0.73                           | 0.83             | 79.1%                        |
| Lot 2 Residential-1/8 Acre or Less                        | 24.05           | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 24.05     | 65.0%           | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.00      | 0.0%            | 0.45                           | 0.59             | 65.0%                        |
| Tract A Detention Pond                                    | 1.85            | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 1.85      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| Future Commercial (Off-site to north)                     | 8.74            | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 8.74      | 95.0%           | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.00      | 0.0%            | 0.81                           | 0.88             | 95.0%                        |
| Future Heavy Industrial (Off-site to east)                | 1.87            | 0.73                                    | 0.81             | 1.87      | 90.0%           | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.00      | 0.0%            | 0.73                           | 0.81             | 90.0%                        |
| Detention Pond (Off-site to east)                         | 0.44            | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.44      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| Detention Pond (Off-site to south)                        | 0.30            | 0.73                                    | 0.81             | 0.00      | 0.0%            | 0.81                                       | 0.88             | 0.00      | 0.0%            | 0.45  | 0.59             | 0.00      | 0.0%            | 0.90                            | 0.96             | 0.00      | 0.0%            | 0.09                                | 0.36             | 0.30      | 2.0%            | 0.09                           | 0.36             | 2.0%                         |
| <b>Total Pond A</b>                                       | <b>43.77</b>    |   |                  |           |                 |  |                  |           |                 |   |                  |           |                 |                                 |                  |           |                 |                                     |                  |           |                 |                                |                  | <b>71.6%</b>                 |
| <b>Total W. Forebay (North Commercial, Lot 2, R.O.W.)</b> | <b>34.57</b>    |   |                  |           |                 |  |                  |           |                 |   |                  |           |                 |                                 |                  |           |                 |                                     |                  |           |                 | <b>0.56</b>                    | <b>0.68</b>      | <b>73.3%</b>                 |
| <b>Total N. Forebay (Lot 1, East Heavy Industrial)</b>    | <b>6.61</b>     |   |                  |           |                 |  |                  |           |                 |   |                  |           |                 |                                 |                  |           |                 |                                     |                  |           |                 | <b>0.73</b>                    | <b>0.81</b>      | <b>90.0%</b>                 |

## **Appendix C**

### **Hydraulic Calculations**

# Channel Report

## Swale DP2

### Triangular

Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.60

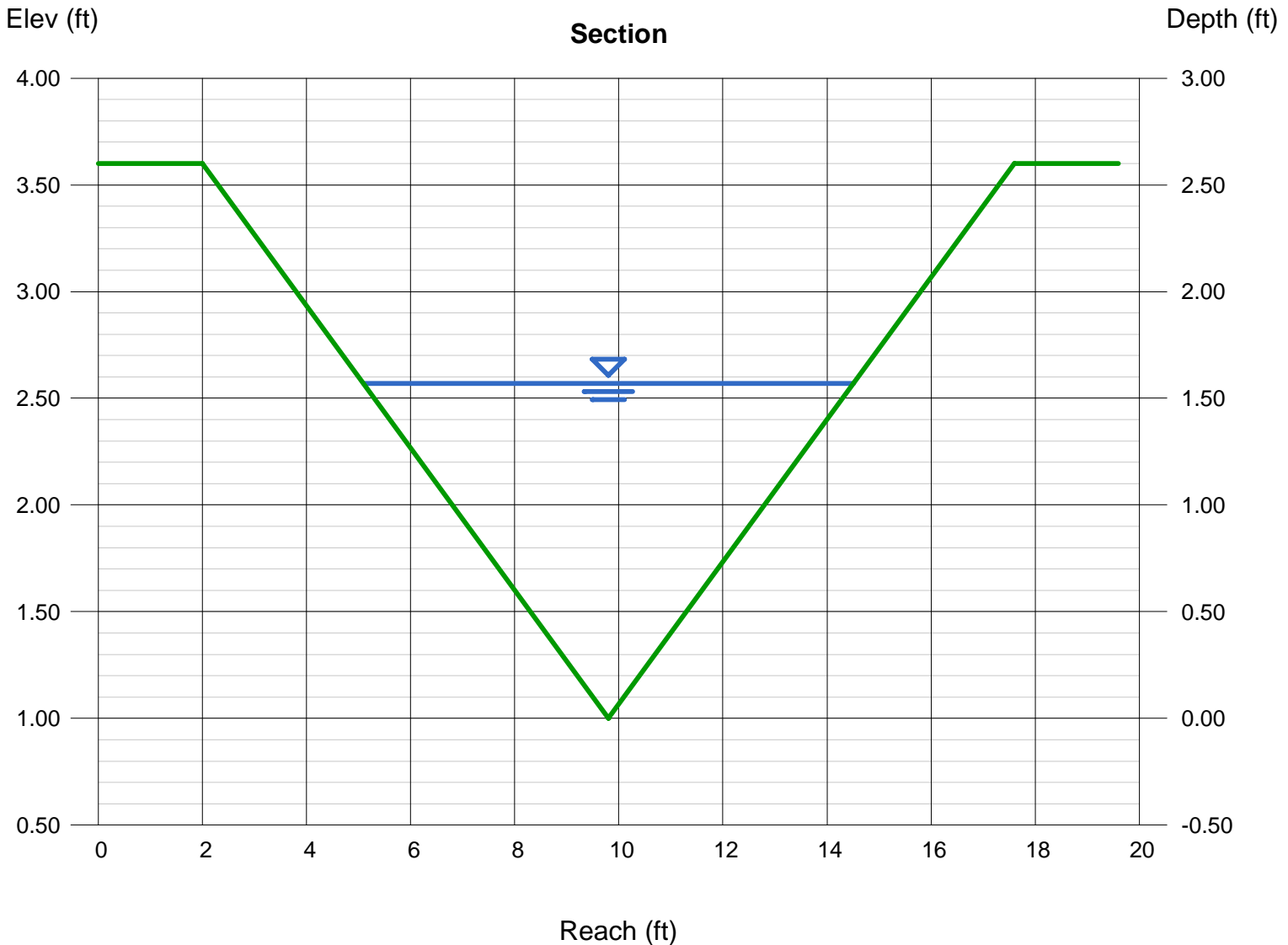
Invert Elev (ft) = 1.00  
Slope (%) = 1.00  
N-Value = 0.035

### Calculations

Compute by: Known Q  
Known Q (cfs) = 25.50

### Highlighted

Depth (ft) = 1.57  
Q (cfs) = 25.50  
Area (sqft) = 7.39  
Velocity (ft/s) = 3.45  
Wetted Perim (ft) = 9.93  
Crit Depth, Yc (ft) = 1.36  
Top Width (ft) = 9.42  
EGL (ft) = 1.75



# Channel Report

## Swale DP4

### Triangular

Side Slopes (z:1) = 4.00, 3.00  
Total Depth (ft) = 2.50

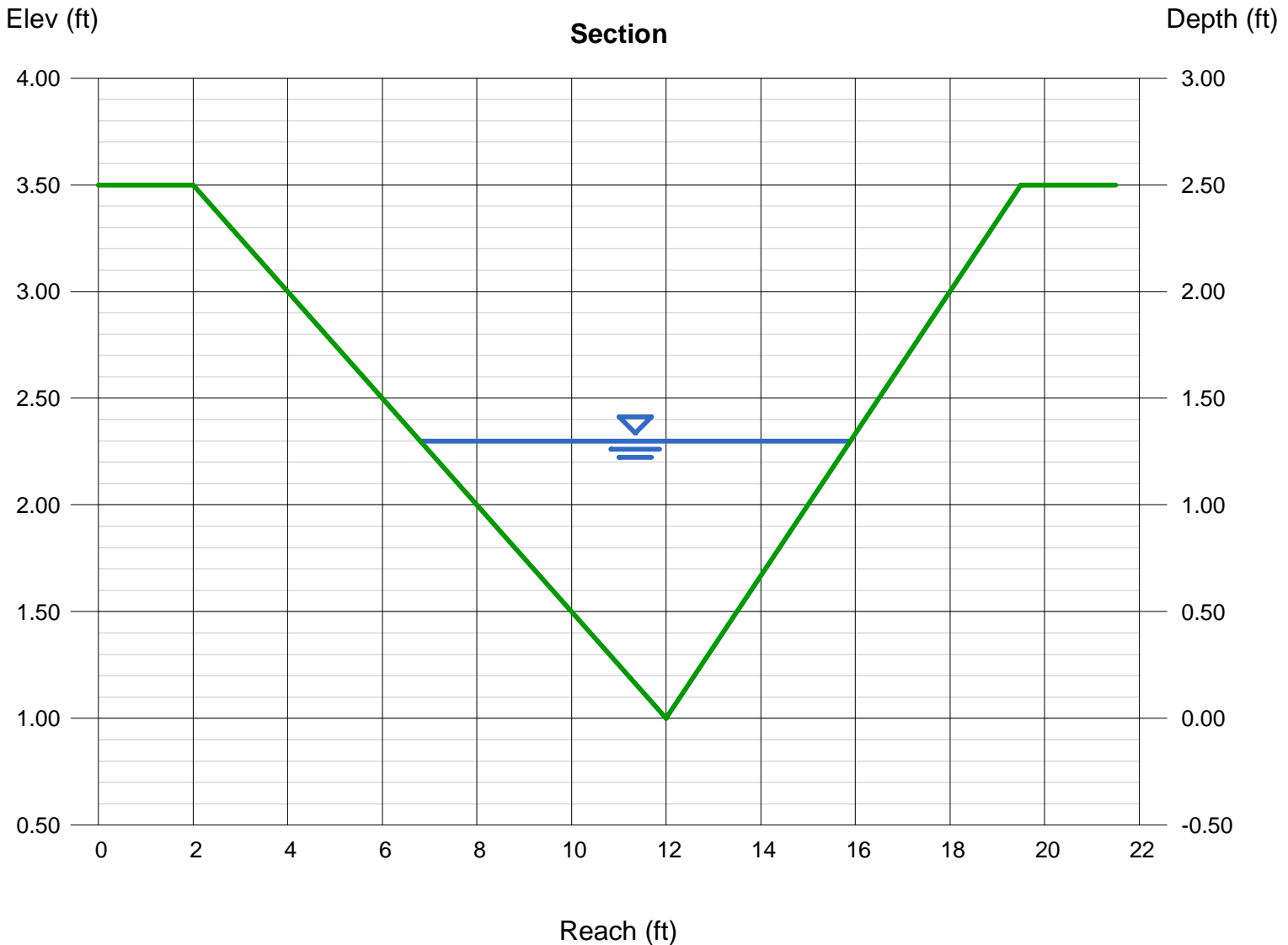
Invert Elev (ft) = 1.00  
Slope (%) = 1.00  
N-Value = 0.035

### Calculations

Compute by: Known Q  
Known Q (cfs) = 18.00

### Highlighted

Depth (ft) = 1.30  
Q (cfs) = 18.00  
Area (sqft) = 5.91  
Velocity (ft/s) = 3.04  
Wetted Perim (ft) = 9.47  
Crit Depth, Yc (ft) = 1.11  
Top Width (ft) = 9.10  
EGL (ft) = 1.44



# Channel Report

## Swale DP4.1

### Triangular

Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.50

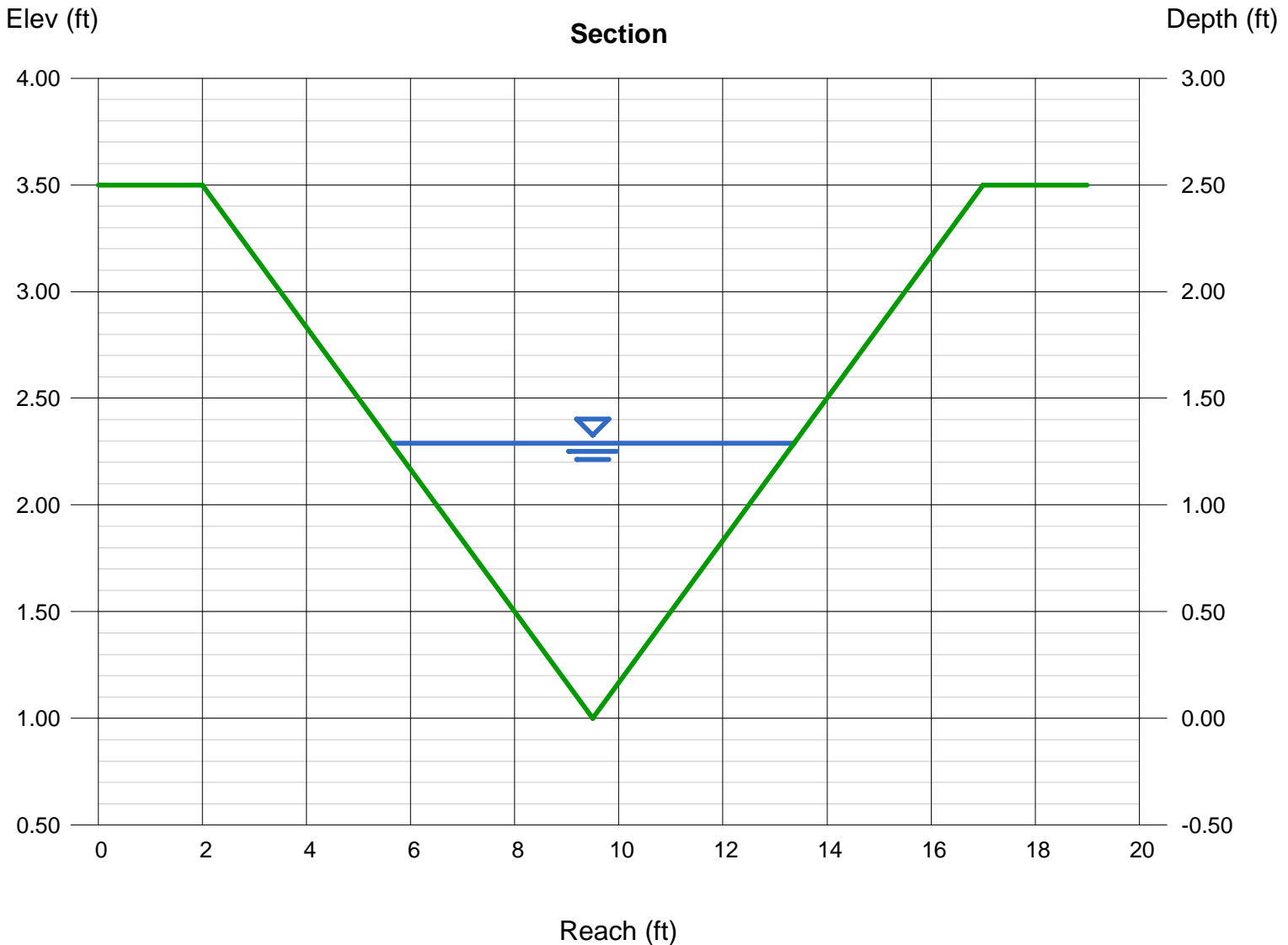
Invert Elev (ft) = 1.00  
Slope (%) = 2.00  
N-Value = 0.035

### Calculations

Compute by: Known Q  
Known Q (cfs) = 21.50

### Highlighted

Depth (ft) = 1.29  
Q (cfs) = 21.50  
Area (sqft) = 4.99  
Velocity (ft/s) = 4.31  
Wetted Perim (ft) = 8.16  
Crit Depth, Yc (ft) = 1.27  
Top Width (ft) = 7.74  
EGL (ft) = 1.58





# Culvert Report

## DP4.1-5 year

|                     |                                |
|---------------------|--------------------------------|
| Invert Elev Dn (ft) | = 6978.36                      |
| Pipe Length (ft)    | = 69.60                        |
| Slope (%)           | = 0.99                         |
| Invert Elev Up (ft) | = 6979.05                      |
| Rise (in)           | = 24.0                         |
| Shape               | = Circular                     |
| Span (in)           | = 24.0                         |
| No. Barrels         | = 1                            |
| n-Value             | = 0.013                        |
| Culvert Type        | = Circular Concrete            |
| Culvert Entrance    | = Groove end projecting (C)    |
| Coeff. K,M,c,Y,k    | = 0.0045, 2, 0.0317, 0.69, 0.2 |

### Embankment

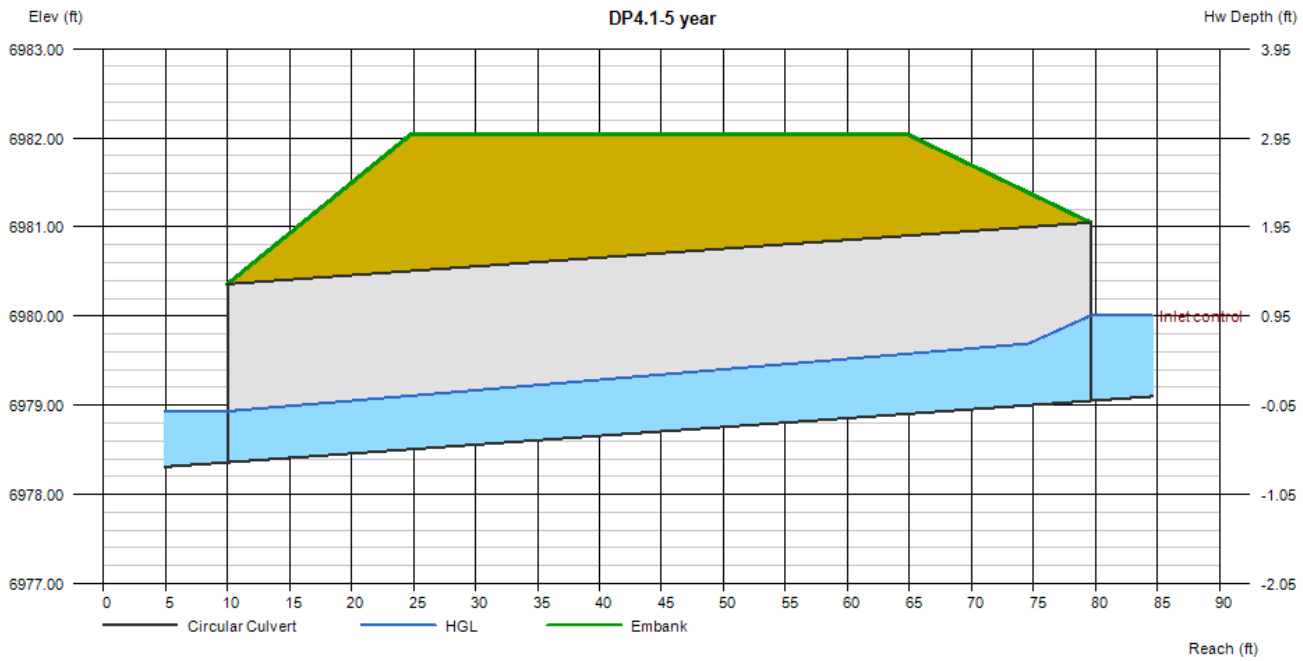
|                    |           |
|--------------------|-----------|
| Top Elevation (ft) | = 6982.04 |
| Top Width (ft)     | = 40.00   |
| Crest Width (ft)   | = 125.00  |

### Calculations

|                     |        |
|---------------------|--------|
| Qmin (cfs)          | = 4.00 |
| Qmax (cfs)          | = 4.00 |
| Tailwater Elev (ft) | = 0.00 |

### Highlighted

|                 |                 |
|-----------------|-----------------|
| Qtotal (cfs)    | = 4.00          |
| Qpipe (cfs)     | = 4.00          |
| Qovertop (cfs)  | = 0.00          |
| Veloc Dn (ft/s) | = 5.38          |
| Veloc Up (ft/s) | = 4.08          |
| HGL Dn (ft)     | = 6978.93       |
| HGL Up (ft)     | = 6979.75       |
| Hw Elev (ft)    | = 6980.01       |
| Hw/D (ft)       | = 0.48          |
| Flow Regime     | = Inlet Control |



# Culvert Report

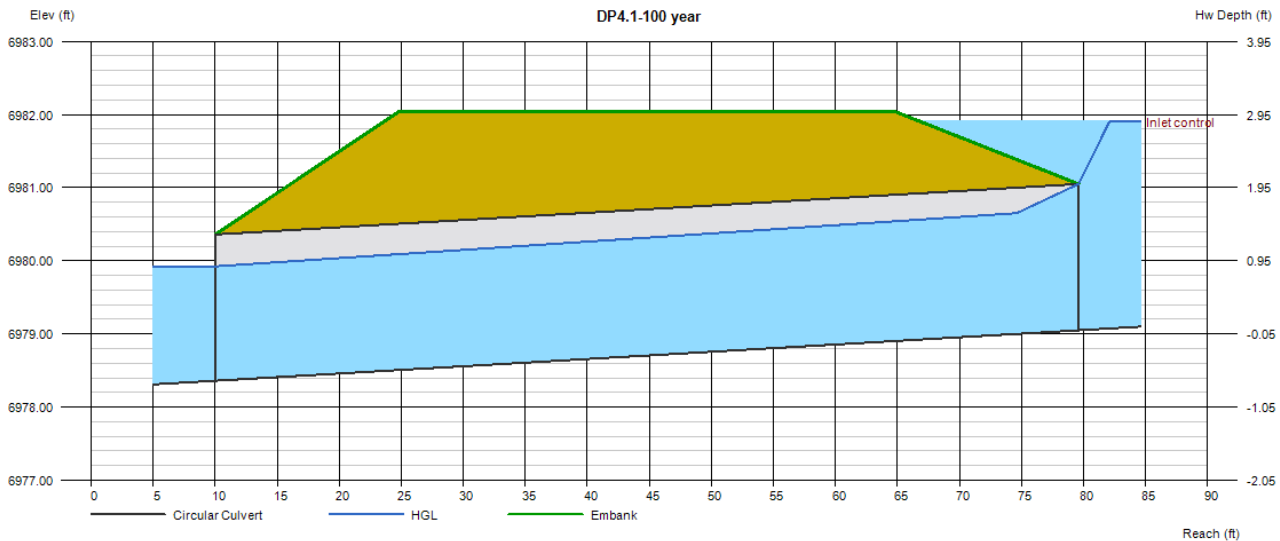
## DP4.1-100 year

|                     |                                |
|---------------------|--------------------------------|
| Invert Elev Dn (ft) | = 6978.36                      |
| Pipe Length (ft)    | = 69.60                        |
| Slope (%)           | = 0.99                         |
| Invert Elev Up (ft) | = 6979.05                      |
| Rise (in)           | = 24.0                         |
| Shape               | = Circular                     |
| Span (in)           | = 24.0                         |
| No. Barrels         | = 1                            |
| n-Value             | = 0.013                        |
| Culvert Type        | = Circular Concrete            |
| Culvert Entrance    | = Groove end projecting (C)    |
| Coeff. K,M,c,Y,k    | = 0.0045, 2, 0.0317, 0.69, 0.2 |

|                    |           |
|--------------------|-----------|
| <b>Embankment</b>  |           |
| Top Elevation (ft) | = 6982.04 |
| Top Width (ft)     | = 40.00   |
| Crest Width (ft)   | = 125.00  |

|                     |         |
|---------------------|---------|
| <b>Calculations</b> |         |
| Qmin (cfs)          | = 21.50 |
| Qmax (cfs)          | = 21.50 |
| Tailwater Elev (ft) | = 0.00  |

|                    |                 |
|--------------------|-----------------|
| <b>Highlighted</b> |                 |
| Qtotal (cfs)       | = 21.50         |
| Qpipe (cfs)        | = 21.50         |
| Qovertop (cfs)     | = 0.00          |
| Veloc Dn (ft/s)    | = 8.16          |
| Veloc Up (ft/s)    | = 7.72          |
| HGL Dn (ft)        | = 6979.92       |
| HGL Up (ft)        | = 6980.71       |
| Hw Elev (ft)       | = 6981.91       |
| Hw/D (ft)          | = 1.43          |
| Flow Regime        | = Inlet Control |



# Culvert Report

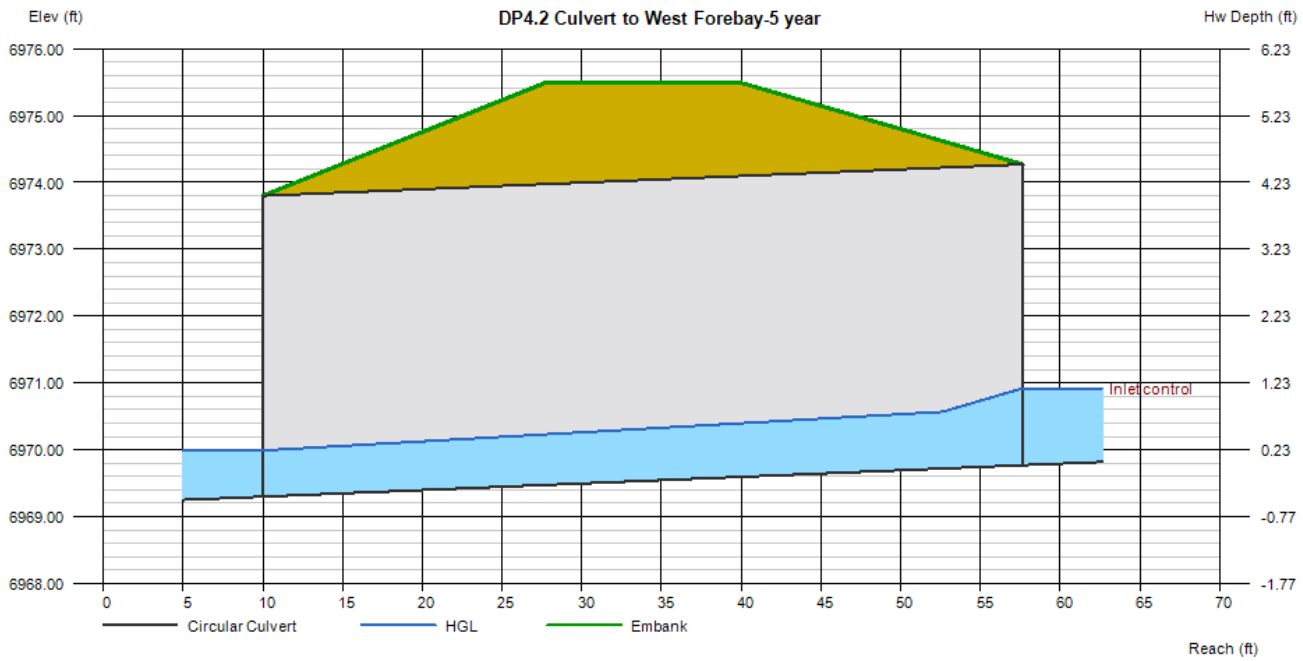
## DP4.2 Culvert to West Forebay-5 year

|                     |                                |
|---------------------|--------------------------------|
| Invert Elev Dn (ft) | = 6969.30                      |
| Pipe Length (ft)    | = 47.65                        |
| Slope (%)           | = 0.99                         |
| Invert Elev Up (ft) | = 6969.77                      |
| Rise (in)           | = 54.0                         |
| Shape               | = Circular                     |
| Span (in)           | = 54.0                         |
| No. Barrels         | = 1                            |
| n-Value             | = 0.013                        |
| Culvert Type        | = Circular Concrete            |
| Culvert Entrance    | = Groove end projecting (C)    |
| Coeff. K,M,c,Y,k    | = 0.0045, 2, 0.0317, 0.69, 0.2 |

|                    |           |
|--------------------|-----------|
| <b>Embankment</b>  |           |
| Top Elevation (ft) | = 6975.50 |
| Top Width (ft)     | = 12.00   |
| Crest Width (ft)   | = 78.00   |

|                     |           |
|---------------------|-----------|
| <b>Calculations</b> |           |
| Qmin (cfs)          | = 9.50    |
| Qmax (cfs)          | = 9.50    |
| Tailwater Elev (ft) | = 6967.62 |

|                    |                 |
|--------------------|-----------------|
| <b>Highlighted</b> |                 |
| Qtotal (cfs)       | = 9.50          |
| Qpipe (cfs)        | = 9.50          |
| Qovertop (cfs)     | = 0.00          |
| Veloc Dn (ft/s)    | = 6.14          |
| Veloc Up (ft/s)    | = 4.42          |
| HGL Dn (ft)        | = 6969.99       |
| HGL Up (ft)        | = 6970.64       |
| Hw Elev (ft)       | = 6970.92       |
| Hw/D (ft)          | = 0.26          |
| Flow Regime        | = Inlet Control |



# Culvert Report

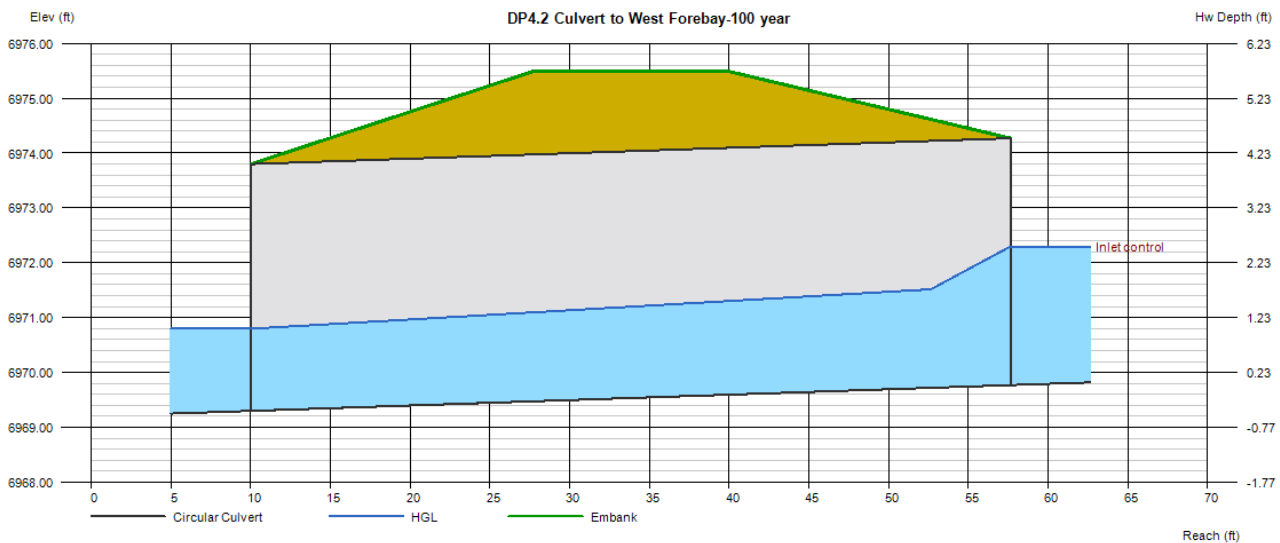
## DP4.2 Culvert to West Forebay-100 year

|                     |                                |
|---------------------|--------------------------------|
| Invert Elev Dn (ft) | = 6969.30                      |
| Pipe Length (ft)    | = 47.65                        |
| Slope (%)           | = 0.99                         |
| Invert Elev Up (ft) | = 6969.77                      |
| Rise (in)           | = 54.0                         |
| Shape               | = Circular                     |
| Span (in)           | = 54.0                         |
| No. Barrels         | = 1                            |
| n-Value             | = 0.013                        |
| Culvert Type        | = Circular Concrete            |
| Culvert Entrance    | = Groove end projecting (C)    |
| Coeff. K,M,c,Y,k    | = 0.0045, 2, 0.0317, 0.69, 0.2 |

|                    |           |
|--------------------|-----------|
| <b>Embankment</b>  |           |
| Top Elevation (ft) | = 6975.50 |
| Top Width (ft)     | = 12.00   |
| Crest Width (ft)   | = 78.00   |

|                     |           |
|---------------------|-----------|
| <b>Calculations</b> |           |
| Qmin (cfs)          | = 40.50   |
| Qmax (cfs)          | = 40.50   |
| Tailwater Elev (ft) | = 6969.67 |

|                    |                 |
|--------------------|-----------------|
| <b>Highlighted</b> |                 |
| Qtotal (cfs)       | = 40.50         |
| Qpipe (cfs)        | = 40.50         |
| Qovertop (cfs)     | = 0.00          |
| Veloc Dn (ft/s)    | = 8.74          |
| Veloc Up (ft/s)    | = 6.66          |
| HGL Dn (ft)        | = 6970.80       |
| HGL Up (ft)        | = 6971.60       |
| Hw Elev (ft)       | = 6972.30       |
| Hw/D (ft)          | = 0.56          |
| Flow Regime        | = Inlet Control |



# Channel Report

## Swale DP5

### Triangular

Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.00

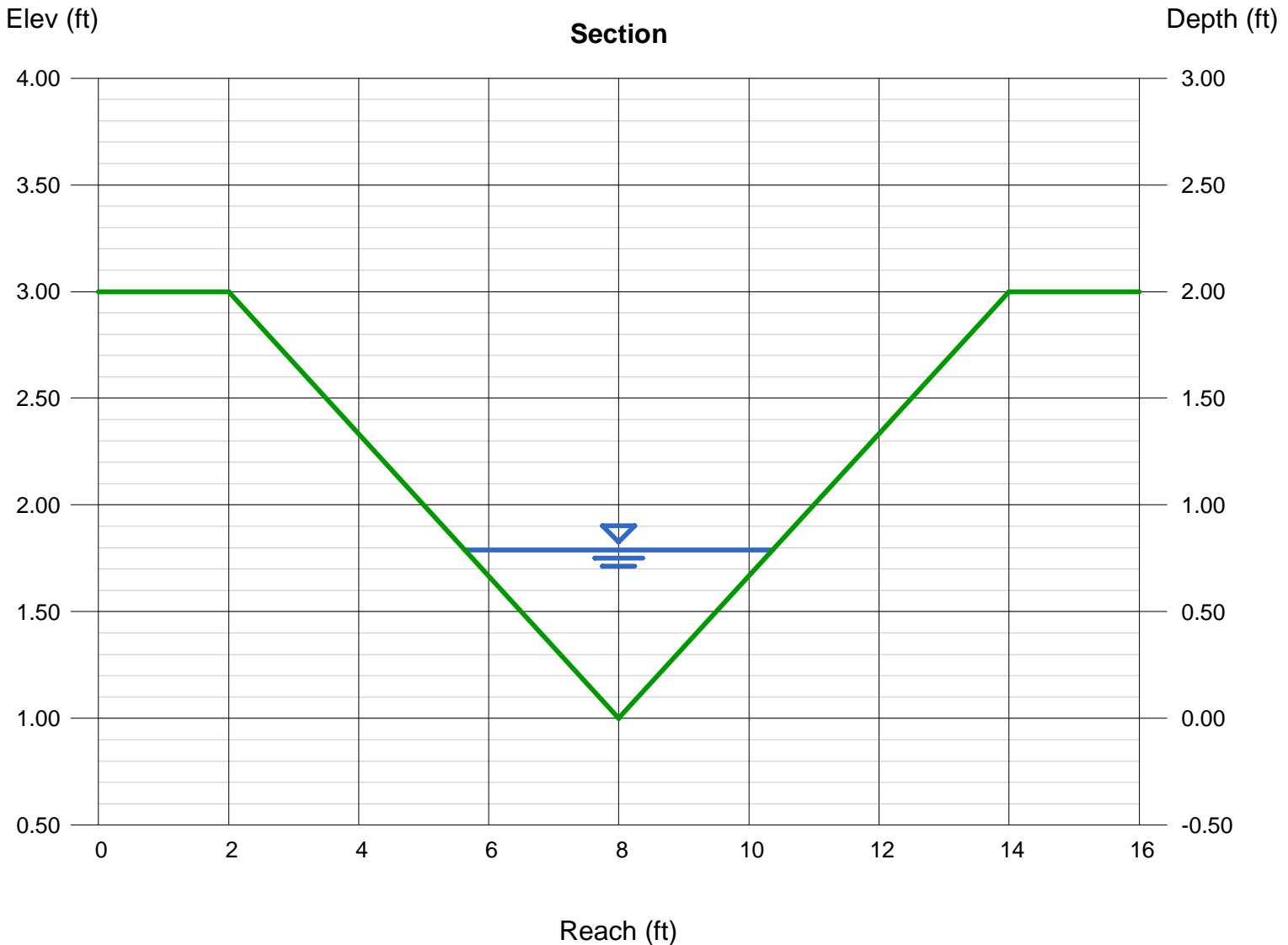
Invert Elev (ft) = 1.00  
Slope (%) = 1.00  
N-Value = 0.035

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.00

### Highlighted

Depth (ft) = 0.79  
Q (cfs) = 4.000  
Area (sqft) = 1.87  
Velocity (ft/s) = 2.14  
Wetted Perim (ft) = 5.00  
Crit Depth, Yc (ft) = 0.65  
Top Width (ft) = 4.74  
EGL (ft) = 0.86



# Channel Report

## Swale DP6

### Triangular

Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.00

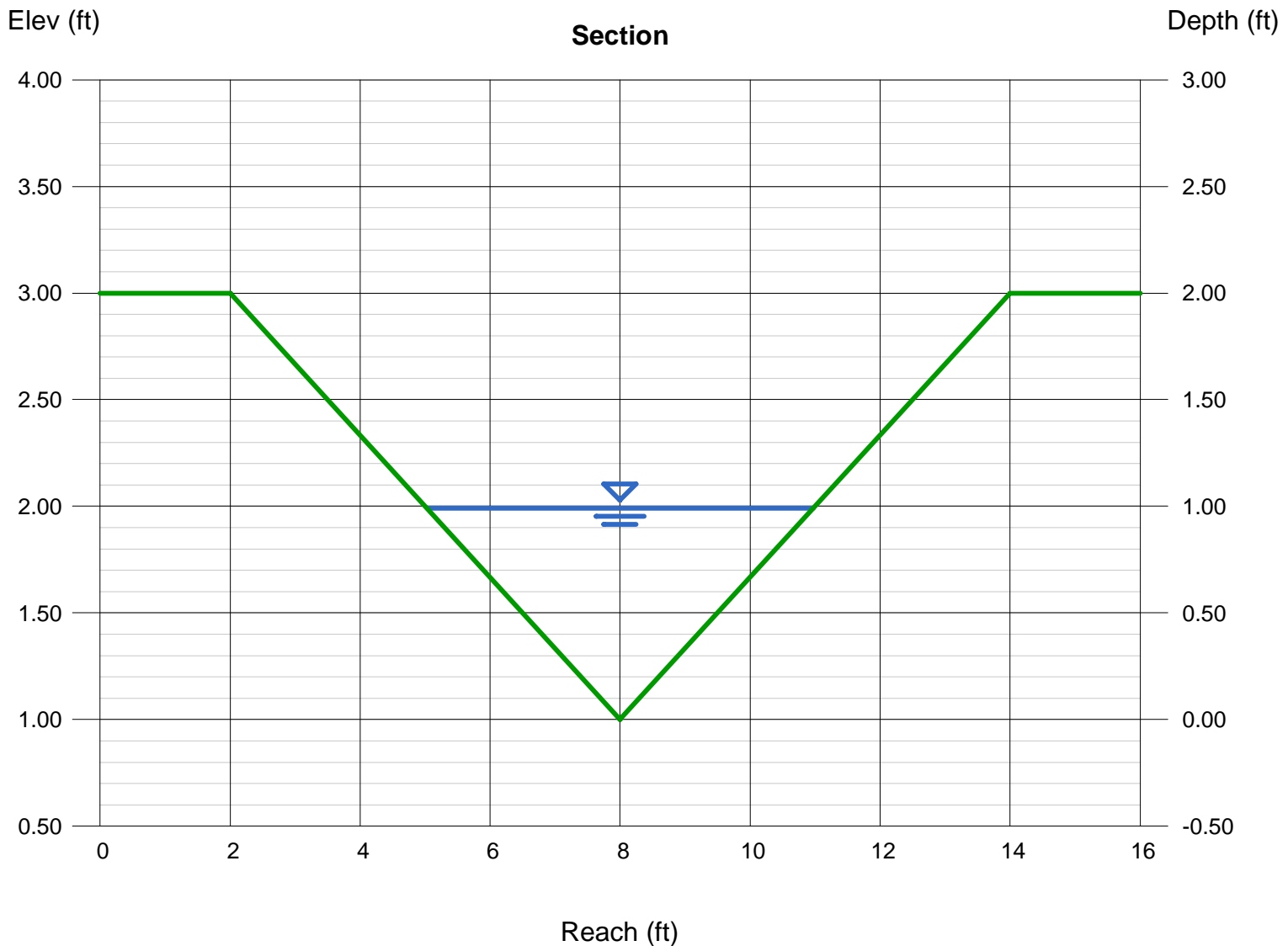
Invert Elev (ft) = 1.00  
Slope (%) = 1.00  
N-Value = 0.035

### Calculations

Compute by: Known Q  
Known Q (cfs) = 7.50

### Highlighted

Depth (ft) = 0.99  
Q (cfs) = 7.500  
Area (sqft) = 2.94  
Velocity (ft/s) = 2.55  
Wetted Perim (ft) = 6.26  
Crit Depth, Yc (ft) = 0.83  
Top Width (ft) = 5.94  
EGL (ft) = 1.09



# Froude Number Calculations

## Sterling Ranch Recycling Facility

### Froude Number Equation:

$$Fr = \frac{v}{(gh_m)^{1/2}}$$

Where:

v= velocity (ft/s)

g= acceleration of gravity (32.2ft/s<sup>2</sup>)

h<sub>m</sub>=hydraulic mean depth (ft)

### Hydraulic Mean Depth Equation:

$$h_m = \frac{A}{T}$$

Where:

A= cross sectional area of filled flow in channel (ft<sup>2</sup>)

T= width of channel open to surface (ft)

### Swale DP2 Calculations:

Parameters: S= 1.0%, A= 7.39 ft<sup>2</sup>, T= 9.42 ft, v= 3.45 ft/s

Therefore:

$$h_m = \frac{7.39}{9.42} = 0.78 \text{ ft}$$

$$Fr = \frac{3.45}{(32.2 * 0.78)^{1/2}} = 0.69$$

For cohesive soils, maximum Froude Number is 0.80.

### Swale DP4 Calculations:

Parameters: S= 1.0%, A= 5.91 ft<sup>2</sup>, T= 9.10 ft, v= 3.04 ft/s

Therefore:

$$h_m = \frac{5.91}{9.10} = 0.65 \text{ ft}$$

$$Fr = \frac{3.04}{(32.2 * 0.65)^{1/2}} = 0.66$$

For cohesive soils, maximum Froude Number is 0.80.

**Swale DP4.1 Calculations:**

Parameters: S= 2.0%, A= 4.99 ft<sup>2</sup>, T= 7.74 ft, v= 4.31 ft/s

Therefore: 
$$h_m = \frac{4.99}{7.74} = 0.64 \text{ ft}$$

$$Fr = \frac{4.31}{(32.2 * 0.64)^{1/2}} = 0.95$$

For cohesive soils, maximum Froude Number is 0.80.

Turf Reinforcement Mat (TRM) used for this swale.

**Swale DP5 Calculations:**

Parameters: S= 1.0%, A= 1.87 ft<sup>2</sup>, T= 4.74 ft, v= 2.14 ft/s

Therefore: 
$$h_m = \frac{1.87}{4.74} = 0.39 \text{ ft}$$

$$Fr = \frac{2.14}{(32.2 * 0.39)^{1/2}} = 0.60$$

For cohesive soils, maximum Froude Number is 0.80.

**Swale DP6 Calculations:**

Parameters: S= 1.0%, A= 2.94 ft<sup>2</sup>, T= 5.94 ft, v= 2.55 ft/s

Therefore: 
$$h_m = \frac{2.94}{5.94} = 0.49 \text{ ft}$$

$$Fr = \frac{2.55}{(32.2 * 0.49)^{1/2}} = 0.64$$

For cohesive soils, maximum Froude Number is 0.80.



# VMax<sup>®</sup> TRMs



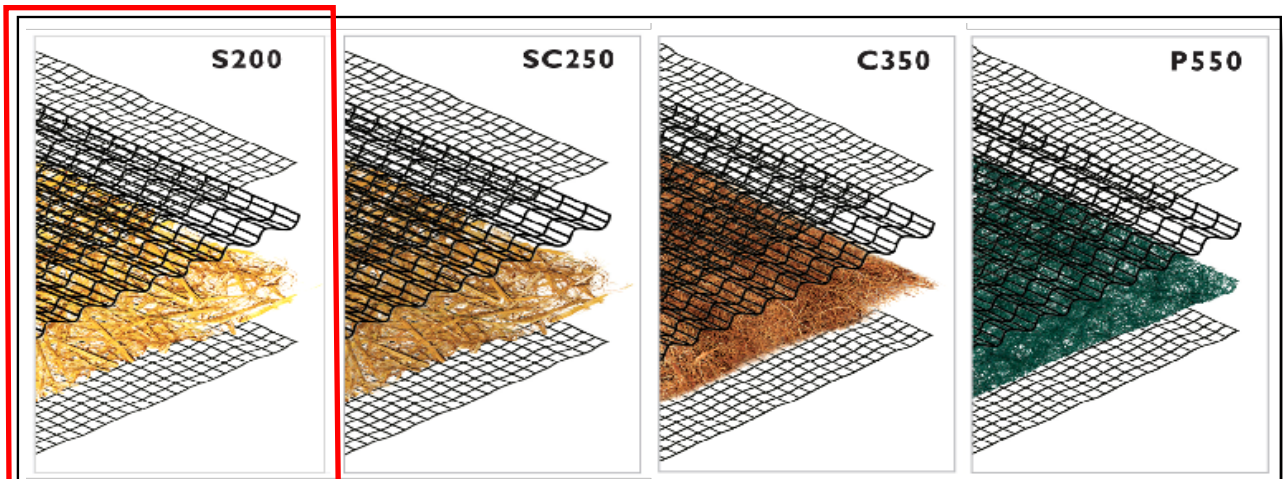
## A Permanent Turf Reinforcement Mat Solution for Every Design

The VMax system of permanent TRMs are ideal for high-flow channels, streambanks, shorelines, and other areas needing permanent vegetation reinforcement and protection from water and wind. Our VMax TRMs combine a three-dimensional matting and a fiber matrix material for all-out erosion protection, vegetation establishment and reinforcement. The VMax TRMs are available with various performance capabilities and support reinforced vegetative lining development from germination to maturity.

## VMax<sup>®</sup> Unique Three-Dimensional Design

North American Green VMax TRMs are each designed to maximize performance through all development phases of a reinforced vegetative lining. The corrugated matting structure lends a true reinforcement zone for vegetation entanglement, especially compared to flat net mats. The unique design of the corrugated matting also helps to create a shear plane that deflects flowing water away from the soil surface. And the incorporation of a fiber matrix supplements the 3-D structure by creating a ground cover that blocks soil movement and aids in vegetation establishment.

### Four VMax Turf Reinforcement Mats Designed for Every Level of Performance



|   |   |  |   |   |
|---|---|--|---|---|
| <b>Matrix Fiber</b>                     | 100% Straw  | 70% Straw / 30% Coconut                                | 100% Coconut  | 100% Polypropylene  |
| <b>Netting Types</b>                    | Top and Bottom light-weight UV-stabilized PP, Crimped PP center net | Top and Bottom UV-stabilized PP, Crimped PP center net | Top and Bottom heavy-weight UV-stabilized PP, Crimped PP center net | Top and Bottom ultra heavy-weight UV-stabilized PP, Crimped PP center net |
| <b>Typical Slope Applications (H:V)</b> | 1:1 and greater   | 1:1 and greater  | 1:1 and greater   | 1:1 and greater   |
| <b>Channel Shear Stress Threshold</b>   | Unvegetated: 2.3 psf<br>Vegetated: 10.0 psf                         | Unvegetated: 3.0 psf<br>Vegetated: 10.0 psf            | Unvegetated: 3.2 psf<br>Vegetated: 12.0 psf                         | Unvegetated: 4.0 psf<br>Vegetated: 14.0 psf                               |
| <b>Channel Velocity Threshold</b>       | Unvegetated: 8.5 fps<br>Vegetated: 18 fps                           | Unvegetated: 9.5 fps<br>Vegetated: 15 fps              | Unvegetated: 10.5 fps<br>Vegetated: 20 fps                          | Unvegetated: 12.5 fps<br>Vegetated: 25 fps                                |

Selected product that will work for all swales above 5 ft/s. Has maximum channel velocity of 18 ft/s.

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North American Green, LLC.  
4609 E. Boonville-New Harmony Rd., Evansville, IN  
(800) 772-2040 | [www.nagreen.com](http://www.nagreen.com)



# VMax<sup>®</sup> TRMs cont.

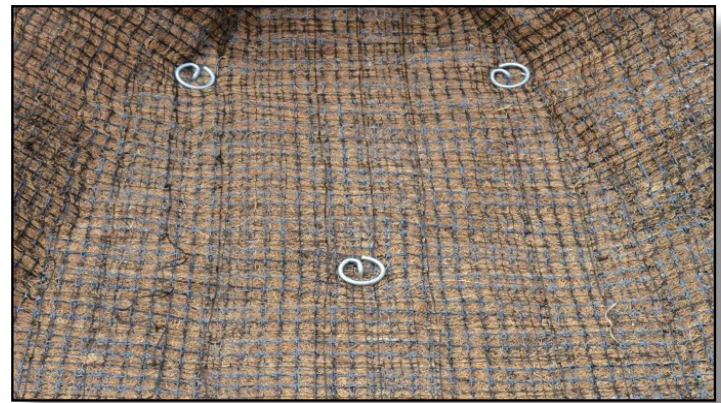
## Selecting the Right VMax TRM

Choosing the right VMax TRM can be made easy by utilizing our Erosion Control Materials Design Software ([www.ecmds.com](http://www.ecmds.com)), which allows users to input project specific parameters for channels, slopes, spillways, and more and ensures proper evaluation, design, and product selection in return. Our four VMax TRMs offer varying performance values, fiber matrix longevities, and price points, to help you meet your project specific goals.

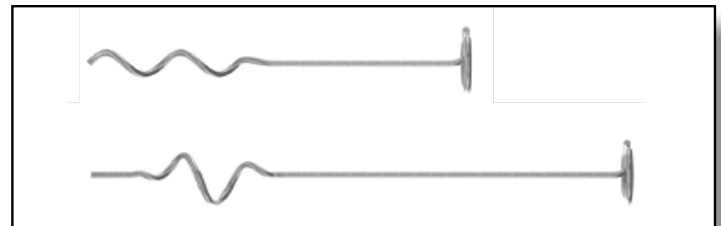


## Twist Pin + VMax TRM - an Ideal Installation

Utilizing the VMax TRMs in conjunction with Twist Pin fastener technology can result in an installed system that pushes TRM performance with increased factors of safety. The combined system has been shown to have superior pullout strength performance up to 200 lbs when compared to installation with traditional wire staples and pins. This is up to 10x the pullout resistance of wire staples and pins. Additionally, the use of the twist pins provides intimate contact between the TRM and the soil, and have been shown to be effective in a wide range of soil types. With a quick and easy installation using an electric drill and custom chuck, the TRM+Twist Pin system can eliminate time and labor costs from day 1 through project release.



*VMax turf reinforcement mat being installed on a channel application (top right), twist pins installed with TRMs can have increased system performance and pullout resistance (middle right), twist pins are available in 8" and 12" lengths and two coil configurations designed for hard or soft soil types (lower right).*



*Comparison of common TRM fasteners based on pullout performance and typical application (below).*

| Fastener            | Pullout Resistance (lb) | Comment   |
|---------------------|-------------------------|---|
| 6" Round Top Pin    | 14                      | Best for hardened soils where other fasteners are damaged during installation.  |
| 6" Regular U-staple | 42                      | Standard fastener that develops additional pullout as legs may deflect and add friction during installation.  |
| 12" Pin with Washer | 35                      | Standard fastener good for soils where staples can be bent frequently and are too difficult to install.   |
| 18" Pin with Washer | 27                      | Standard fastener good for soils where staples are frequently bent and 12" straight pins fail to provide sufficient pullout because surface soil is wet or loose. |
| Twist Pin           | 170                     | Upgraded fastener that provides high pullout and ideal for loose or soft soils.   |



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4609 E. Boonville-New Harmony Rd., Evansville, IN  
(800) 772-2040 | [www.nagreen.com](http://www.nagreen.com)

## PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 1/24/24

|   | STORM DRAIN SYSTEM |              |              | Notes   |
|---|--------------------|--------------|--------------|---|
|   | DP4.1              | DESIGN POINT | DESIGN POINT |   |
| Q <sub>100</sub> (cfs):                               | 21.5               |              |              | Flows are the greater of proposed vs. future              |
| Conduit   | Pipe               |              |              |   |
| D <sub>c</sub> , Pipe Diameter (in):                  | 24                 |              |              |   |
| W, Box Width (ft):                                    | N/A                |              |              |   |
| H, Box Height (ft):                                   | N/A                |              |              |   |
| Y <sub>t</sub> , Tailwater Depth (ft):                | 1.60               |              |              | If unknown, use Y <sub>t</sub> /D <sub>c</sub> (or H)=0.4 |
| Y <sub>t</sub> /D <sub>c</sub> or Y <sub>t</sub> /H   | 0.80               |              |              |   |
| Q/D <sup>2.5</sup> or Q/(WH <sup>3/2</sup> )          | 3.80               |              |              |   |
| Supercritical?  | No                 |              |              |   |
| Y <sub>n</sub> , Normal Depth (ft) [Supercritical]:   |                    |              |              |   |
| D <sub>a</sub> , H <sub>a</sub> (in) [Supercritical]: | N/A                |              |              | D <sub>a</sub> =(D <sub>c</sub> +Y <sub>n</sub> )/2       |
| Riprap d <sub>50</sub> (in) [Supercritical]:          | N/A                |              |              |   |
| Riprap d <sub>50</sub> (in) [Subcritical]:            | 2.74               |              |              |   |
| Required Riprap Size:                                 | L                  |              |              | Fig. 9-38 or Fig. 9-36                                    |
| d <sub>50</sub> (in):                                 | 9                  |              |              |   |
| Expansion Factor, 1/(2 tan θ):                        | 6.80               |              |              | Read from Fig. 9-35 or 9-36                               |
| θ:  | 0.07               |              |              |   |
| Erosive Soils?  | No                 |              |              |   |
| Area of Flow, A <sub>t</sub> (ft <sup>2</sup> ):      | 3.07               |              |              | A <sub>t</sub> =Q/V                                       |
| Length of Protection, L <sub>p</sub> (ft):            | -0.5               |              |              | L=(1/(2 tan θ))(A <sub>t</sub> /Y <sub>t</sub> - D)       |
| Min Length (ft)                                       | 6.0                |              |              | Min L=3D or 3H  |
| Max Length (ft)                                       | 20.0               |              |              | Max L=10D or 10H  |
| Min Bottom Width, T (ft):                             | 1.9                |              |              | T=2*(L <sub>p</sub> *tanθ)+W                              |
| Design Length (ft)                                    | 6.0                |              |              |   |
| Design Width (ft)                                     | 1.9                |              |              |   |
| Riprap Depth (in)                                     | 18                 |              |              | Depth=2(d <sub>50</sub> )                                 |
| Type II Bedding Depth (in)*                           | 6                  |              |              | *Not used if Soil Riprap                                  |
| Cutoff Wall   | No                 |              |              |   |
| Cutoff Wall Depth (ft)                                |                    |              |              | Depth of Riprap and Base                                  |
| Cutoff Wall Width (ft)                                |                    |              |              |   |

Note: No Type II Base to be used if Soil Riprap is specified within the plans  
 \* For use when the flow in the culvert is supercritical (and less than full).

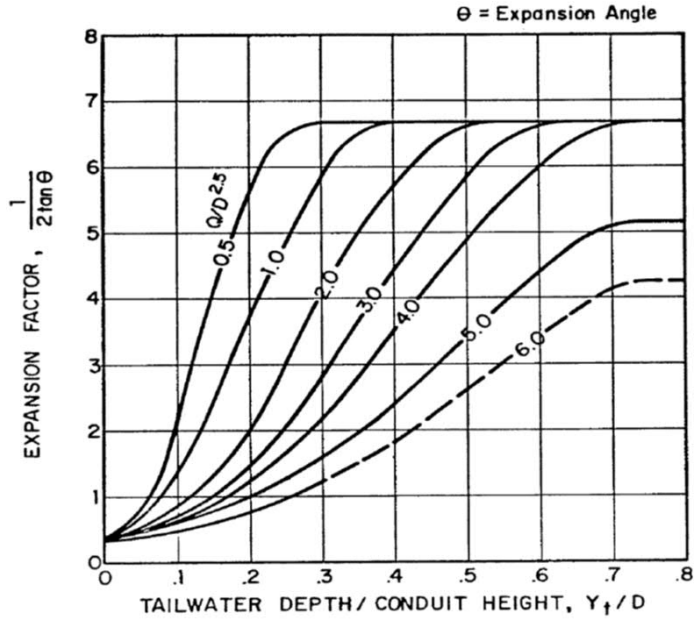


Figure 9-35. Expansion factor for circular conduits

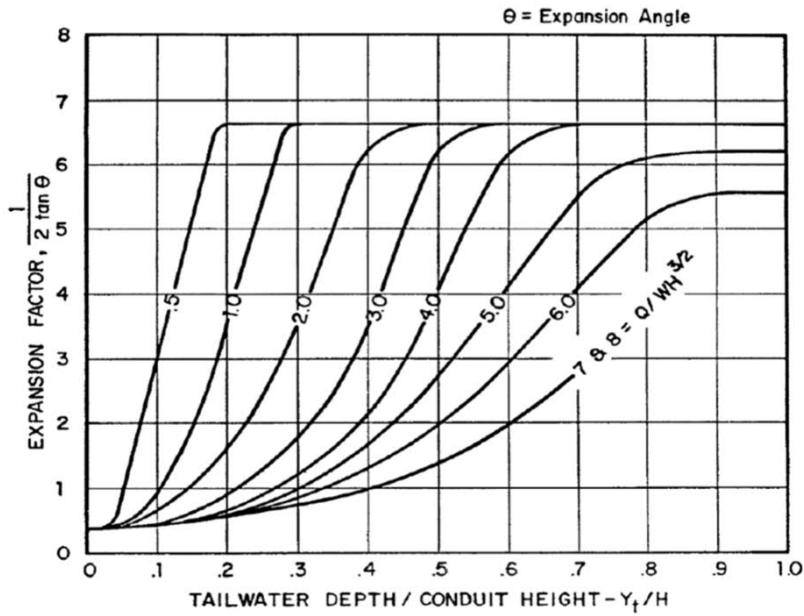


Figure 9-36. Expansion factor for rectangular conduits

# INLET MANAGEMENT

Worksheet Protected

|                                    |             |
|------------------------------------|-------------|
| INLET NAME                         | DP7.1       |
| Site Type (Urban or Rural)         | URBAN       |
| Inlet Application (Street or Area) | AREA        |
| Hydraulic Condition                | Swale       |
| Inlet Type                         | CDOT Type C |

## USER-DEFINED INPUT

|  |                         |
|--|-------------------------|
| User-Defined Design Flows  |                         |
| Minor $Q_{\text{Known}}$ (cfs)   | 2.8                     |
| Major $Q_{\text{Known}}$ (cfs)   | 11.2                    |
| Bypass (Carry-Over) Flow from Upstream <span style="color: blue;">Inlets must be organized from upstream (let</span> |                         |
| Receive Bypass Flow from:  | No Bypass Flow Received |
| Minor Bypass Flow Received, $Q_b$ (cfs)  | 0.0                     |
| Major Bypass Flow Received, $Q_b$ (cfs)  | 0.0                     |
| Watershed Characteristics  |                         |
| Subcatchment Area (acres)  |                         |
| Percent Impervious   |                         |
| NRCS Soil Type   |                         |
| Watershed Profile  |                         |
| Overland Slope (ft/ft)   |                         |
| Overland Length (ft)   |                         |
| Channel Slope (ft/ft)  |                         |
| Channel Length (ft)  |                         |
| Minor Storm Rainfall Input   |                         |
| Design Storm Return Period, $T_r$ (years)  |                         |
| One-Hour Precipitation, $P_1$ (inches)   |                         |
| Major Storm Rainfall Input   |                         |
| Design Storm Return Period, $T_r$ (years)  |                         |
| One-Hour Precipitation, $P_1$ (inches)   |                         |

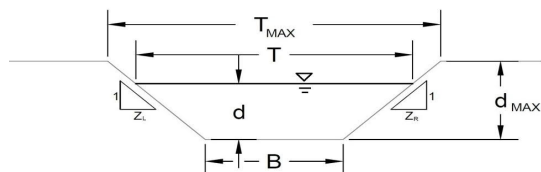
## CALCULATED OUTPUT

|   |      |
|---|------|
| Minor Total Design Peak Flow, $Q$ (cfs)     | 2.8  |
| Major Total Design Peak Flow, $Q$ (cfs)     | 11.2 |
| Minor Flow Bypassed Downstream, $Q_b$ (cfs) | 0.0  |
| Major Flow Bypassed Downstream, $Q_b$ (cfs) | 0.0  |

## AREA INLET IN A SWALE

Sterling Ranch Recycling Facility

DP7.1



This worksheet uses the NRCS vegeta-  
retardance method to determine  
Manning's n for grass-lined channels.

An override Manning's n can be  
entered for other channel materials.

**Analysis of Trapezoidal Channel (Grass-Lined uses SCS Method)**

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

| Soil Type:   | Max. Velocity (V <sub>MAX</sub> ) | Max. Froude No. (F <sub>MAX</sub> ) |
|--------------|-----------------------------------|-------------------------------------|
| Non-Cohesive | 5.0 fps                           | 0.60                                |
| Cohesive     | 7.0 fps                           | 0.80                                |
| Paved        | N/A                               | N/A                                 |

A, B, C, D, or E =

|                  |              |
|------------------|--------------|
| n =              | 0.030        |
| S <sub>0</sub> = | 0.0100 ft/ft |
| B =              | 0.00 ft      |
| Z1 =             | 3.00 ft/ft   |
| Z2 =             | 3.00 ft/ft   |

Choose One:

- Non-Cohesive  
 Cohesive  
 Paved

Maximum Allowable Top Width of Channel for Minor & Major Storm

Maximum Allowable Water Depth in Channel for Minor & Major Storm

|                    | Minor Storm | Major Storm |    |
|--------------------|-------------|-------------|----|
| T <sub>MAX</sub> = | 9.00        | 12.00       | ft |
| d <sub>MAX</sub> = | 1.50        | 2.00        | ft |

**Allowable Channel Capacity Based On Channel Geometry**

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

|                      | Minor Storm | Major Storm |     |
|----------------------|-------------|-------------|-----|
| Q <sub>allow</sub> = | 26.7        | 57.5        | cfs |
| d <sub>allow</sub> = | 1.50        | 2.00        | ft  |

**Water Depth in Channel Based On Design Peak Flow**

Design Peak Flow

Water Depth

|                  |      |      |     |
|------------------|------|------|-----|
| Q <sub>o</sub> = | 2.8  | 11.2 | cfs |
| d =              | 0.64 | 1.08 | ft  |

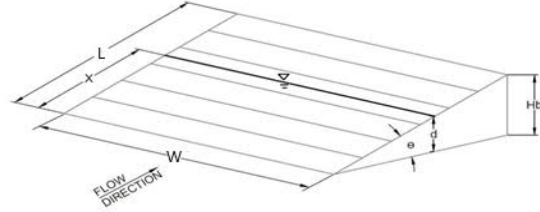
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

MHFD-Inlet, Version 5.03 (August 2023)  
**AREA INLET IN A SWALE**

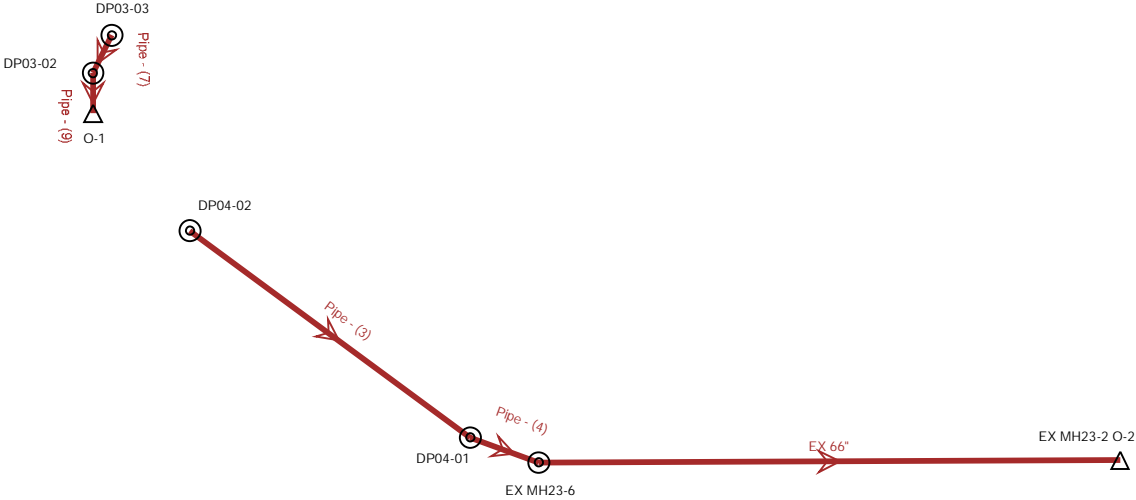
Sterling Ranch Recycling Facility  
 DP7.1

| Inlet Design Information (Input)  |  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
|---|--|-------|-------|-------|--|-------|------|------|--|---------|-----|------|-----|---------|-----|-----|-----|---------|-----|-----|---|
| Type of Inlet   | CDOT Type C  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Inlet Type =  | CDOT Type C  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Angle of Inclined Grate (must be $\leq 30$ degrees)                         | $\theta = 0.00$ degrees  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Width of Grate  | $W = 3.00$ ft  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Length of Grate   | $L = 3.00$ ft  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Open Area Ratio   | $A_{RATIO} = 0.70$   |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Height of Inclined Grate  | $H_B = 0.00$ ft  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Clogging Factor   | $C_f = 0.50$   |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Grate Discharge Coefficient   | $C_d = 0.96$   |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Orifice Coefficient   | $C_o = 0.64$   |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Weir Coefficient  | $C_w = 2.05$   |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
|   | <table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> <th></th> </tr> </thead> <tbody> <tr> <td><math>d =</math></td> <td>0.64</td> <td>1.08</td> <td></td> </tr> <tr> <td><math>Q_a =</math></td> <td>9.5</td> <td>16.8</td> <td>cfs</td> </tr> <tr> <td><math>Q_b =</math></td> <td>0.0</td> <td>0.0</td> <td>cfs</td> </tr> <tr> <td><math>C\% =</math></td> <td>100</td> <td>100</td> <td>%</td> </tr> </tbody> </table> |       | MINOR | MAJOR |  | $d =$ | 0.64 | 1.08 |  | $Q_a =$ | 9.5 | 16.8 | cfs | $Q_b =$ | 0.0 | 0.0 | cfs | $C\% =$ | 100 | 100 | % |
|   | MINOR  | MAJOR |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| $d =$   | 0.64   | 1.08  |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| $Q_a =$   | 9.5  | 16.8  | cfs   |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| $Q_b =$   | 0.0  | 0.0   | cfs   |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| $C\% =$   | 100  | 100   | %     |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) |  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Total Inlet Interception Capacity (assumes clogged condition)               |  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Bypassed Flow   |  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |
| Capture Percentage = $Q_a/Q_o$  |  |       |       |       |  |       |      |      |  |         |     |      |     |         |     |     |     |         |     |     |   |



Warning 03: Velocity exceeds USDCM Volume I recommendation.  
 Warning 04: Froude No. exceeds USDCM Volume I recommendation.

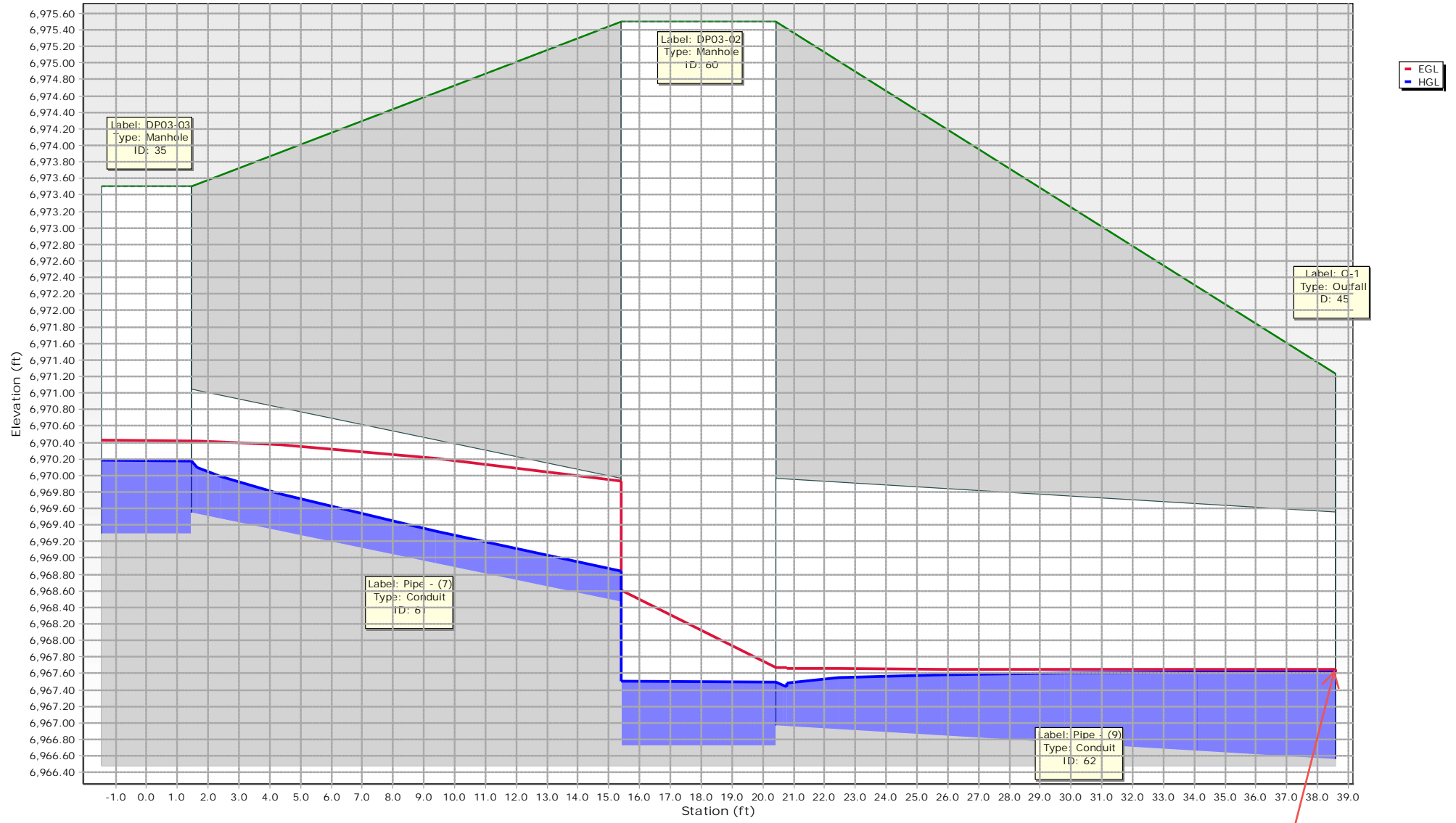
Scenario: 100-YEAR





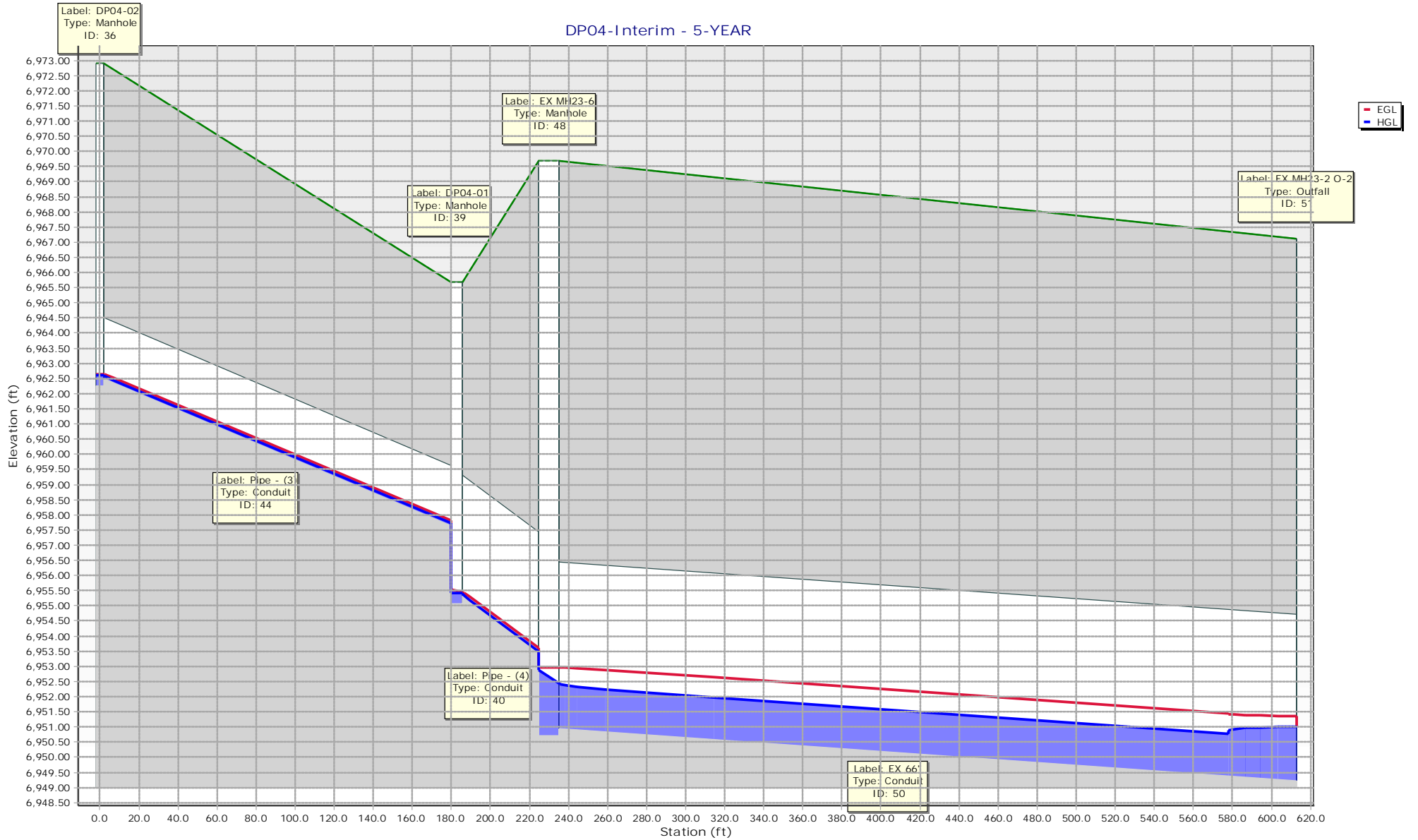
| 5-year Interim Report   |            |            |                            |               |             |                            |                            |                     |                    |                               |                              |               |                |                             |                              |                 |   |
|-------------------------|------------|------------|----------------------------|---------------|-------------|----------------------------|----------------------------|---------------------|--------------------|-------------------------------|------------------------------|---------------|----------------|-----------------------------|------------------------------|-----------------|---|
| Upstream Structure      | Label      | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Manning's n | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | HGL (In) (ft) | HGL (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Velocity (ft/s) | Upstream Structure Headloss Coefficient |
| EX MH23-6               | EX 66"     | 30.8       | 224.37                     | 66            | 0.013       | 383                        | 0.004                      | 6,950.94            | 6,949.23           | 6,969.69                      | 6,967.11                     | 6,952.44      | 6,951.02       | 6,952.98                    | 6,951.35                     | 6.62            | 0.8                                     |
| DP04-02                 | Pipe - (3) | 0.1        | 36.88                      | 24            | 0.013       | 182.8                      | 0.027                      | 6,962.50            | 6,957.64           | 6,972.90                      | 6,965.69                     | 6,962.61      | 6,957.72       | 6,962.64                    | 6,957.82                     | 2.53            | 0.05                                    |
| DP04-01                 | Pipe - (4) | 0.1        | 286.97                     | 48            | 0.013       | 47.1                       | 0.04                       | 6,955.32            | 6,953.44           | 6,965.69                      | 6,969.69                     | 6,955.41      | 6,953.50       | 6,955.44                    | 6,953.61                     | 2.64            | 0.6                                     |
| DP03-03                 | Pipe - (7) | 2.8        | 25.67                      | 18            | 0.013       | 17.9                       | 0.06                       | 6,969.54            | 6,968.47           | 6,973.50                      | 6,975.50                     | 6,970.18      | 6,968.84       | 6,970.42                    | 6,969.93                     | 9.53            | 0.05                                    |
| DP03-02                 | Pipe - (9) | 2.8        | 93.93                      | 36            | 0.013       | 20.7                       | 0.02                       | 6,966.97            | 6,966.56           | 6,975.50                      | 6,971.23                     | 6,967.49      | 6,967.62       | 6,967.67                    | 6,967.64                     | 5.93            | 0.1                                     |
| 100-year Interim Report |            |            |                            |               |             |                            |                            |                     |                    |                               |                              |               |                |                             |                              |                 |   |
| Upstream Structure      | Label      | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Manning's n | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | HGL (In) (ft) | HGL (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Velocity (ft/s) | Upstream Structure Headloss Coefficient |
| EX MH23-6               | EX 66"     | 241.7      | 224.37                     | 66            | 0.013       | 383                        | 0.004                      | 6,950.94            | 6,949.23           | 6,969.69                      | 6,967.11                     | 6,959.37      | 6,957.39       | 6,960.98                    | 6,959.00                     | 10.17           | 0.8                                     |
| DP04-02                 | Pipe - (3) | 8.3        | 36.88                      | 24            | 0.013       | 182.8                      | 0.027                      | 6,962.50            | 6,957.64           | 6,972.90                      | 6,965.69                     | 6,963.53      | 6,960.67       | 6,963.93                    | 6,960.77                     | 9.48            | 0.05                                    |
| DP04-01                 | Pipe - (4) | 8.3        | 286.97                     | 48            | 0.013       | 47.1                       | 0.04                       | 6,955.32            | 6,953.44           | 6,965.69                      | 6,969.69                     | 6,960.66      | 6,960.66       | 6,960.67                    | 6,960.67                     | 0.66            | 0.6                                     |
| DP03-03                 | Pipe - (7) | 11.2       | 25.67                      | 18            | 0.013       | 17.9                       | 0.06                       | 6,969.54            | 6,968.47           | 6,973.50                      | 6,975.50                     | 6,970.82      | 6,969.31       | 6,971.58                    | 6,971.17                     | 14.04           | 0.05                                    |
| DP03-02                 | Pipe - (9) | 11.2       | 93.93                      | 36            | 0.013       | 20.7                       | 0.02                       | 6,966.97            | 6,966.56           | 6,975.50                      | 6,971.23                     | 6,969.67      | 6,969.67       | 6,969.71                    | 6,969.71                     | 8.94            | 0.1                                     |

DPO3 - 5-YEAR

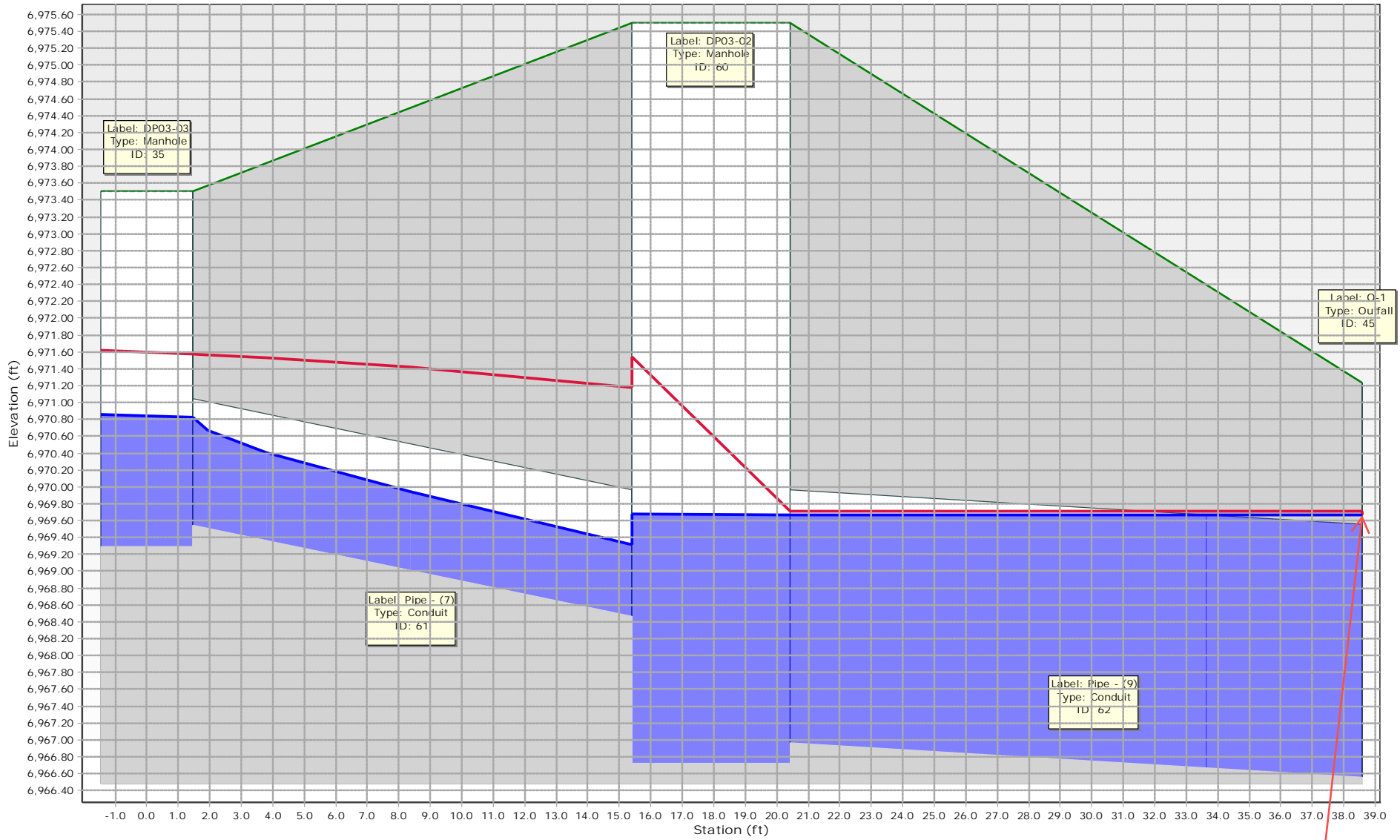


Interim Pond 5-year  
Tailwater: 6967.62

DPO4-Interim - 5-YEAR



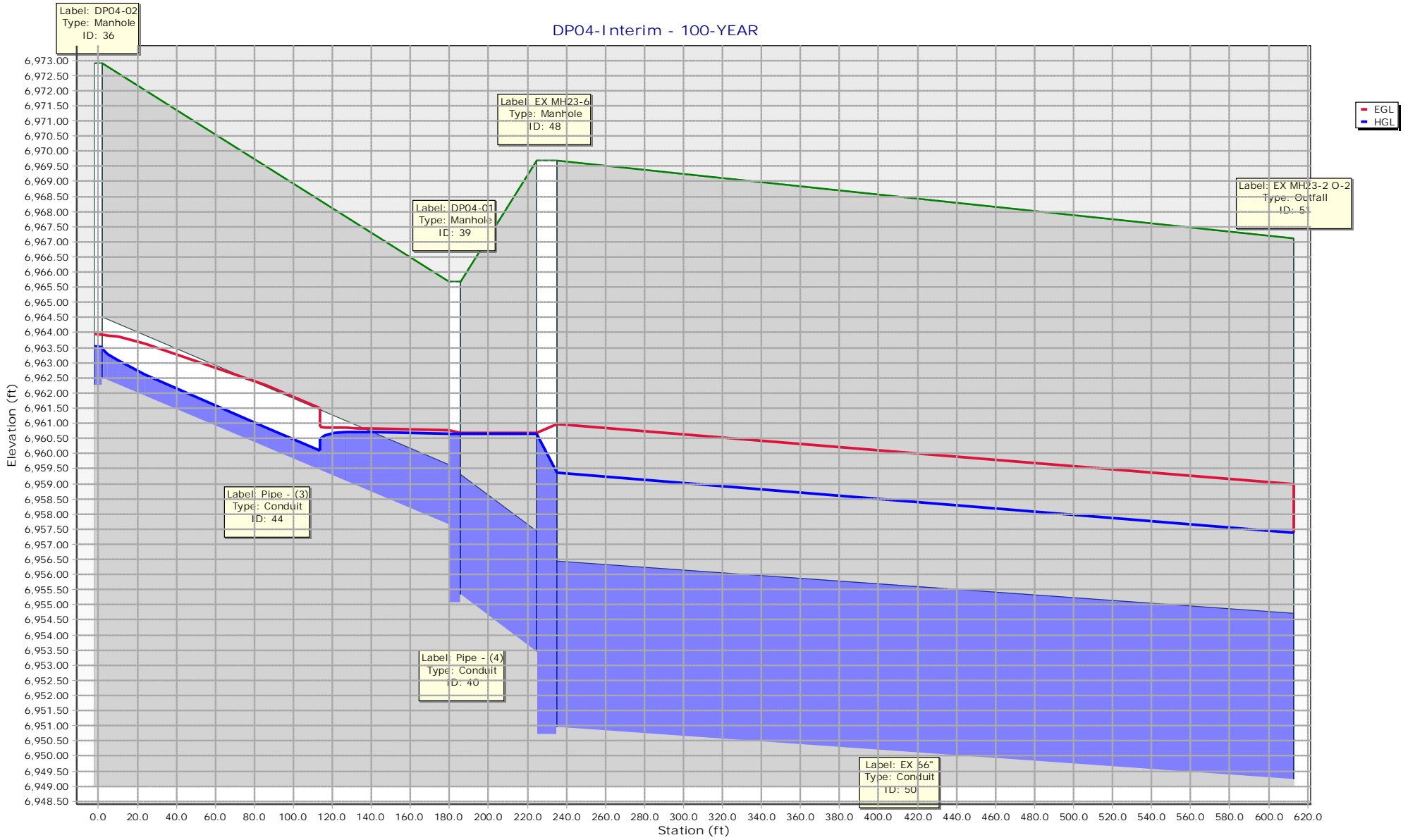
DPO3 - 100-YEAR



EGL  
HGL

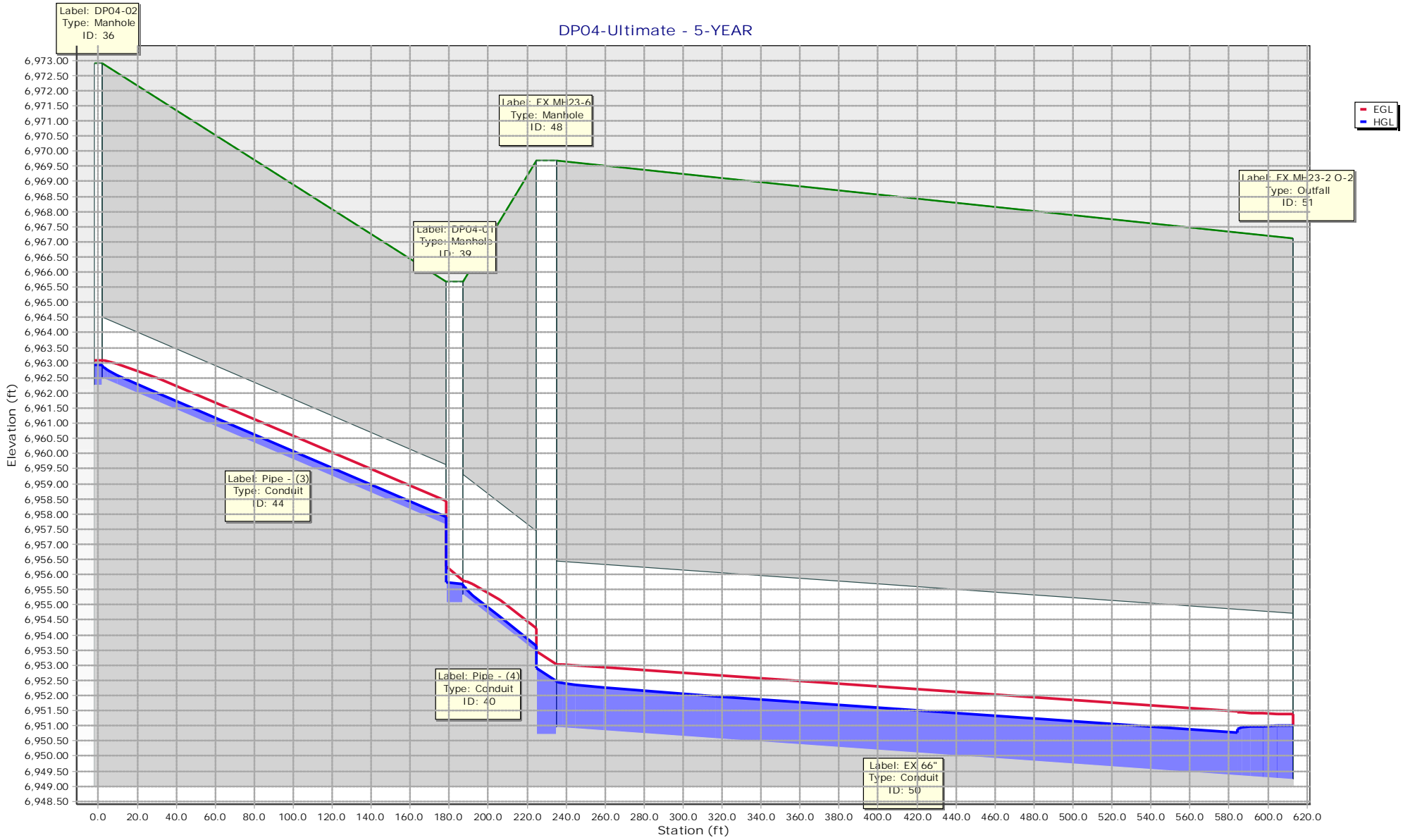
Interim Pond 100-year  
Tailwater: 6969.67

DPO4-Interim - 100-YEAR

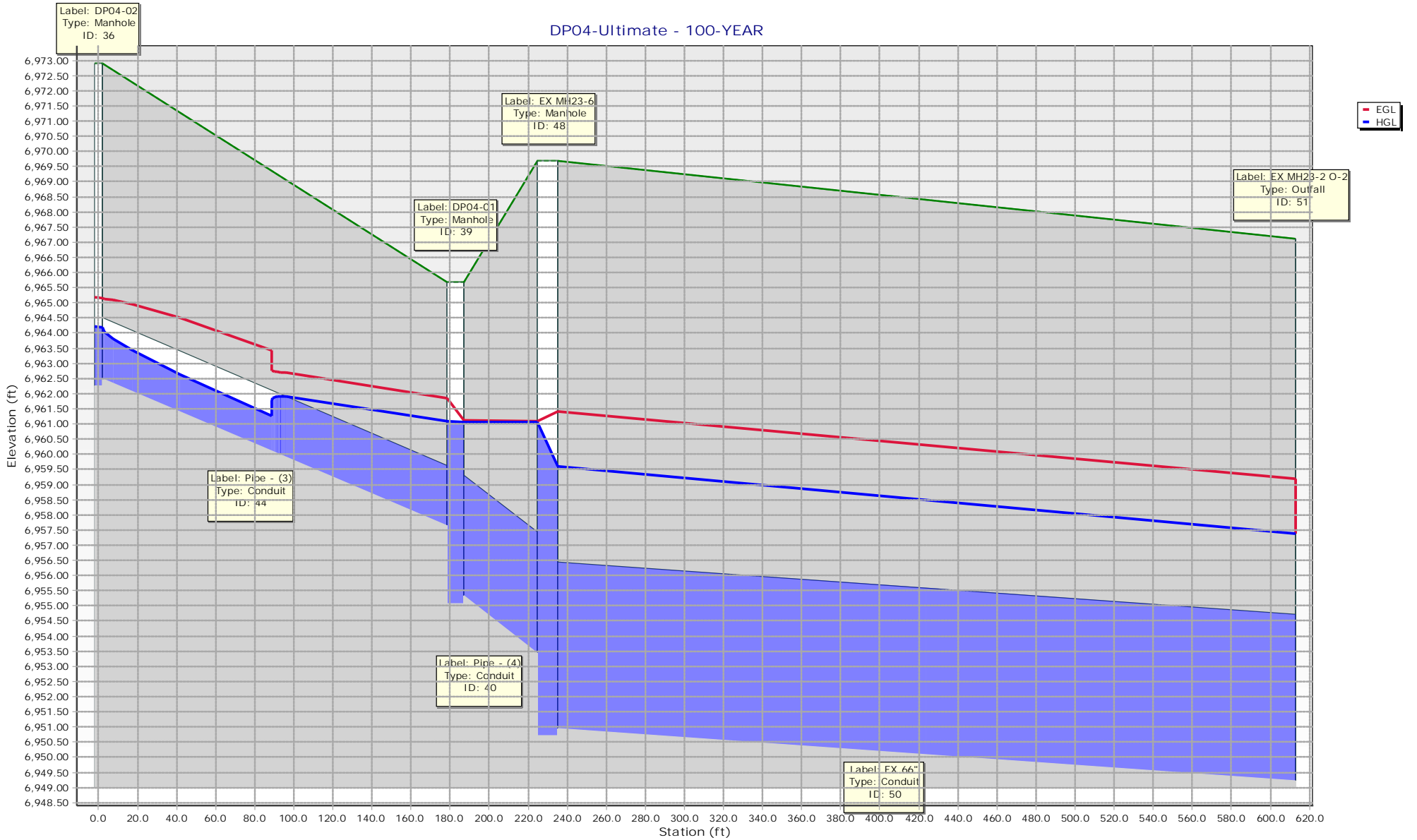


| 5-year Ultimate Report                       |            |            |                            |               |             |                            |                            |                     |                    |                               |                              |               |                |                             |                              |                 |   |
|--|------------|------------|----------------------------|---------------|-------------|----------------------------|----------------------------|---------------------|--------------------|-------------------------------|------------------------------|---------------|----------------|-----------------------------|------------------------------|-----------------|---|
| Upstream Structure                           | Label      | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Manning's n | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | HGL (In) (ft) | HGL (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Velocity (ft/s) | Upstream Structure Headloss Coefficient |
| EX MH23-6                                    | EX 66"     | 32.2       | 224.37                     | 66            | 0.013       | 383                        | 0.004                      | 6,950.94            | 6,949.23           | 6,969.69                      | 6,967.11                     | 6,952.47      | 6,951.02       | 6,953.02                    | 6,951.38                     | 6.71            | 0.8                                     |
| DP04-02                                      | Pipe - (3) | 1.5        | 36.88                      | 24            | 0.013       | 182.8                      | 0.027                      | 6,962.50            | 6,957.64           | 6,972.90                      | 6,965.69                     | 6,962.92      | 6,957.92       | 6,963.07                    | 6,958.43                     | 5.75            | 0.05                                    |
| DP04-01                                      | Pipe - (4) | 1.5        | 286.97                     | 48            | 0.013       | 47.1                       | 0.04                       | 6,955.32            | 6,953.44           | 6,965.69                      | 6,969.69                     | 6,955.67      | 6,953.65       | 6,955.79                    | 6,954.21                     | 6.01            | 0.6                                     |
| 100-year Ultimate Report                     |            |            |                            |               |             |                            |                            |                     |                    |                               |                              |               |                |                             |                              |                 |   |
| Upstream Structure                           | Label      | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Manning's n | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | HGL (In) (ft) | HGL (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Velocity (ft/s) | Upstream Structure Headloss Coefficient |
| EX MH23-6                                    | EX 66"     | 255.6      | 224.37                     | 66            | 0.013       | 383                        | 0.004                      | 6,950.94            | 6,949.23           | 6,969.69                      | 6,967.11                     | 6,959.61      | 6,957.39       | 6,961.41                    | 6,959.19                     | 10.76           | 0.8                                     |
| DP04-02                                      | Pipe - (3) | 22.2       | 36.88                      | 24            | 0.013       | 182.8                      | 0.027                      | 6,962.50            | 6,957.64           | 6,972.90                      | 6,965.69                     | 6,964.18      | 6,961.09       | 6,965.15                    | 6,961.86                     | 12.28           | 0.05                                    |
| DP04-01                                      | Pipe - (4) | 22.2       | 286.97                     | 48            | 0.013       | 47.1                       | 0.04                       | 6,955.32            | 6,953.44           | 6,965.69                      | 6,969.69                     | 6,961.06      | 6,961.05       | 6,961.11                    | 6,961.10                     | 1.77            | 0.6                                     |
| 100-year Ultimate Report- Emergency Overflow |            |            |                            |               |             |                            |                            |                     |                    |                               |                              |               |                |                             |                              |                 |   |
| Upstream Structure                           | Label      | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Manning's n | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | HGL (In) (ft) | HGL (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Velocity (ft/s) | Upstream Structure Headloss Coefficient |
| EX MH23-6                                    | EX 66"     | 358.4      | 224.37                     | 66            | 0.013       | 383                        | 0.004                      | 6,950.94            | 6,949.23           | 6,969.69                      | 6,967.11                     | 6,961.75      | 6,957.39       | 6,965.29                    | 6,960.93                     | 15.09           | 0.8                                     |
| DP04-02                                      | Pipe - (3) | 22.2       | 36.88                      | 24            | 0.013       | 182.8                      | 0.027                      | 6,962.50            | 6,957.64           | 6,972.90                      | 6,965.69                     | 6,967.45      | 6,965.69       | 6,968.23                    | 6,966.47                     | 7.07            | 0.05                                    |
| DP04-01                                      | Pipe - (4) | 125        | 286.97                     | 48            | 0.013       | 47.1                       | 0.04                       | 6,955.32            | 6,953.44           | 6,965.69                      | 6,969.69                     | 6,964.94      | 6,964.58       | 6,966.48                    | 6,966.12                     | 9.95            | 0.6                                     |

DP04-Ultimate - 5-YEAR

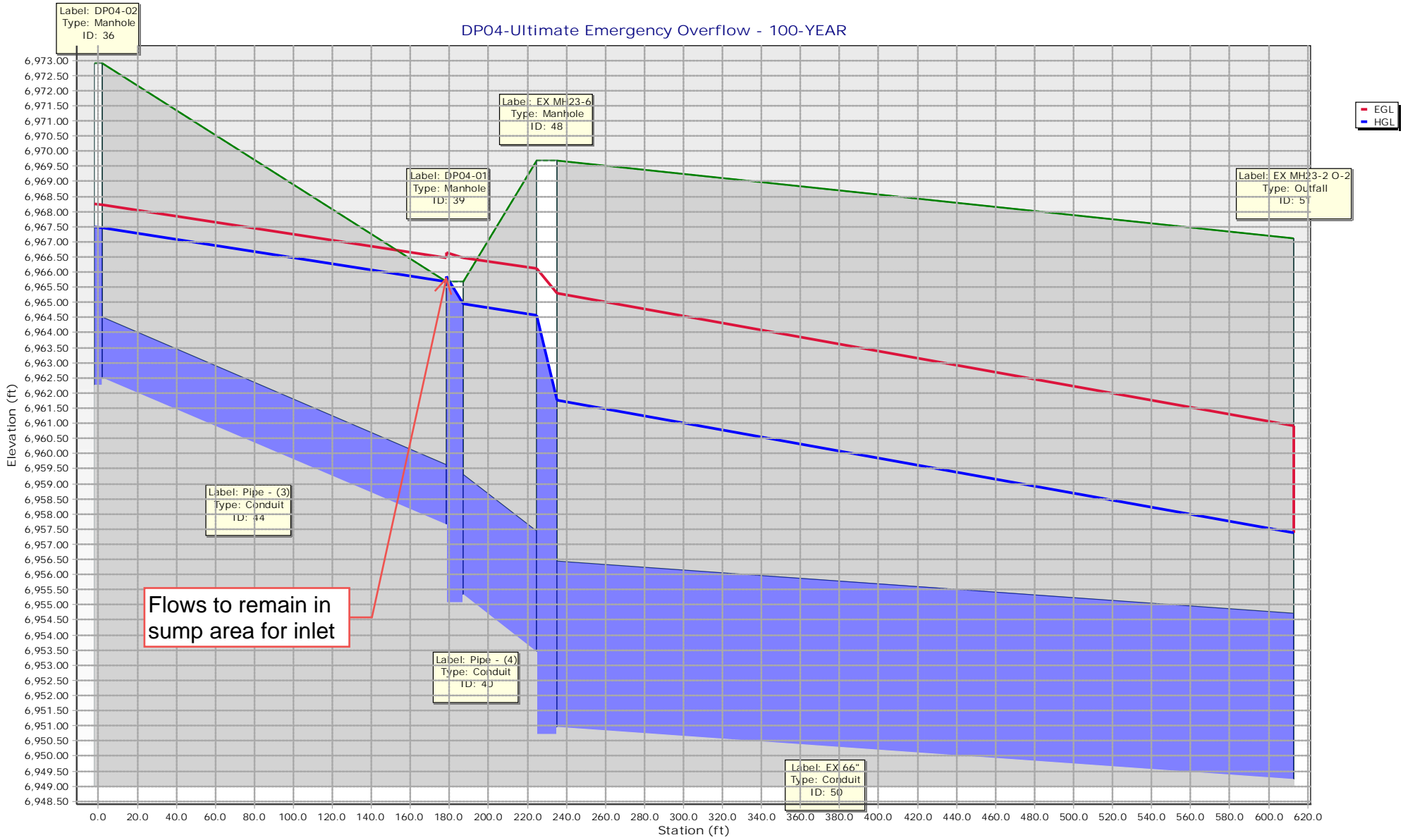


# DP04-Ultimate - 100-YEAR





DP04-Ultimate Emergency Overflow - 100-YEAR



**Design Procedure Form: Extended Detention Basin (EDB)**

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

**Designer:** Gabe Gonzales  
**Company:** JR Engineering  
**Date:** February 12, 2024  
**Project:** Sterling Ranch Recycling Facility  
**Location:** West Forebay

**1. Basin Storage Volume**

- A) Effective Imperviousness of Tributary Area,  $I_a$
- B) Tributary Area's Imperviousness Ratio ( $i = I_a / 100$ )
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept  
(Select EURV when also designing for flood control)
- F) Design Volume (WQCV) Based on 40-hour Drain Time  
( $V_{DESIGN} = (1.0 * (0.91 * i^2 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$ )
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume  
( $V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$ )
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
(Only if a different WQCV Design Volume is desired)
- I) NRCS Hydrologic Soil Groups of Tributary Watershed
  - i) Percentage of Watershed consisting of Type A Soils
  - ii) Percentage of Watershed consisting of Type B Soils
  - iii) Percentage of Watershed consisting of Type C/D Soils
- J) Excess Urban Runoff Volume (EURV) Design Volume  
 For HSG A:  $EURV_A = 1.68 * i^{1.28}$   
 For HSG B:  $EURV_B = 1.36 * i^{1.08}$   
 For HSG C/D:  $EURV_{C/D} = 1.20 * i^{1.08}$
- K) User Input of Excess Urban Runoff Volume (EURV) Design Volume  
(Only if a different EURV Design Volume is desired)

$I_a =$   %  
 $i =$    
 Area =  ac  
 $d_6 =$    
 Choose One  
 Water Quality Capture Volume (WQCV)  
 Excess Urban Runoff Volume (EURV)

$V_{DESIGN} =$   ac-ft  
 $V_{DESIGN\ OTHER} =$   ac-ft  
 $V_{DESIGN\ USER} =$   ac-ft

$HSG_A =$   %  
 $HSG_B =$   %  
 $HSG_{C/D} =$   %

$EURV_{DESIGN} =$   ac-ft  
 $EURV_{DESIGN\ USER} =$   ac-ft

- 2. Basin Shape: Length to Width Ratio  
(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

$L : W =$   : 1

**3. Basin Side Slopes**

- A) Basin Maximum Side Slopes  
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

$Z =$   ft / ft

**4. Inlet**

- A) Describe means of providing energy dissipation at concentrated inflow locations:

**5. Forebay**

- A) Minimum Forebay Volume  
( $V_{FMN} =$   of the WQCV)
- B) Actual Forebay Volume
- C) Forebay Depth  
( $D_F =$   inch maximum)
- D) Forebay Discharge
  - i) Undetained 100-year Peak Discharge
  - ii) Forebay Discharge Design Flow  
( $Q_F = 0.02 * Q_{100}$ )
- E) Forebay Discharge Design
- F) Discharge Pipe Size (minimum 8-inches)
- G) Rectangular Notch Width

$V_{FMN} =$   ac-ft  
 $V_F =$   ac-ft  
 $D_F =$   in  
 $Q_{100} =$   cfs  
 $Q_F =$   cfs

Choose One  
 Berm With Pipe  
 Wall with Rect. Notch  
 Wall with V-Notch Weir

Calculated  $D_P =$   in  
 Calculated  $W_N =$   in

**Design Procedure Form: Extended Detention Basin (EDB)**

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

**Designer:** Gabe Gonzales  
**Company:** JR Engineering  
**Date:** February 8, 2024  
**Project:** Sterling Ranch Recycling Facility  
**Location:** North Forebay

**1. Basin Storage Volume**

- A) Effective Imperviousness of Tributary Area,  $I_a$
- B) Tributary Area's Imperviousness Ratio ( $i = I_a / 100$ )
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept  
(Select EURV when also designing for flood control)
- F) Design Volume (WQCV) Based on 40-hour Drain Time  
( $V_{DESIGN} = (1.0 * (0.91 * i^2 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$ )
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume  
( $V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$ )
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
(Only if a different WQCV Design Volume is desired)
- I) NRCS Hydrologic Soil Groups of Tributary Watershed
  - i) Percentage of Watershed consisting of Type A Soils
  - ii) Percentage of Watershed consisting of Type B Soils
  - iii) Percentage of Watershed consisting of Type C/D Soils
- J) Excess Urban Runoff Volume (EURV) Design Volume  
 For HSG A:  $EURV_A = 1.68 * i^{1.28}$   
 For HSG B:  $EURV_B = 1.36 * i^{1.08}$   
 For HSG C/D:  $EURV_{C/D} = 1.20 * i^{1.08}$
- K) User Input of Excess Urban Runoff Volume (EURV) Design Volume  
(Only if a different EURV Design Volume is desired)

$I_a =$   %  
 $i =$    
 Area =  ac  
 $d_6 =$    
 Choose One  
 Water Quality Capture Volume (WQCV)  
 Excess Urban Runoff Volume (EURV)

$V_{DESIGN} =$   ac-ft  
 $V_{DESIGN\ OTHER} =$    
 $V_{DESIGN\ USER} =$    
 $HSG_A =$   %  
 $HSG_B =$   %  
 $HSG_{C/D} =$   %  
 $EURV_{DESIGN} =$   ac-ft  
 $EURV_{DESIGN\ USER} =$   ac-ft

- 2. Basin Shape: Length to Width Ratio  
(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

L : W =  : 1

**3. Basin Side Slopes**

- A) Basin Maximum Side Slopes  
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Z =  ft / ft

**4. Inlet**

- A) Describe means of providing energy dissipation at concentrated inflow locations:

**5. Forebay**

- A) Minimum Forebay Volume  
( $V_{FMIN} =$   of the WQCV)
- B) Actual Forebay Volume
- C) Forebay Depth  
( $D_F =$   inch maximum)
- D) Forebay Discharge
  - i) Undetained 100-year Peak Discharge
  - ii) Forebay Discharge Design Flow  
( $Q_F = 0.02 * Q_{100}$ )
- E) Forebay Discharge Design
- F) Discharge Pipe Size (minimum 8-inches)
- G) Rectangular Notch Width

$V_{FMIN} =$   ac-ft  
 $V_F =$   ac-ft  
 $D_F =$   in  
 $Q_{100} =$   cfs  
 $Q_F =$   cfs

Choose One  
 Berm With Pipe  
 Wall with Rect. Notch  
 Wall with V-Notch Weir

Calculated  $D_P =$   in  
 Calculated  $W_N =$   in

Flow too small for berm w/ pipe

# Weir Report

## West Forebay Interim Release Rate

### Compound Weir

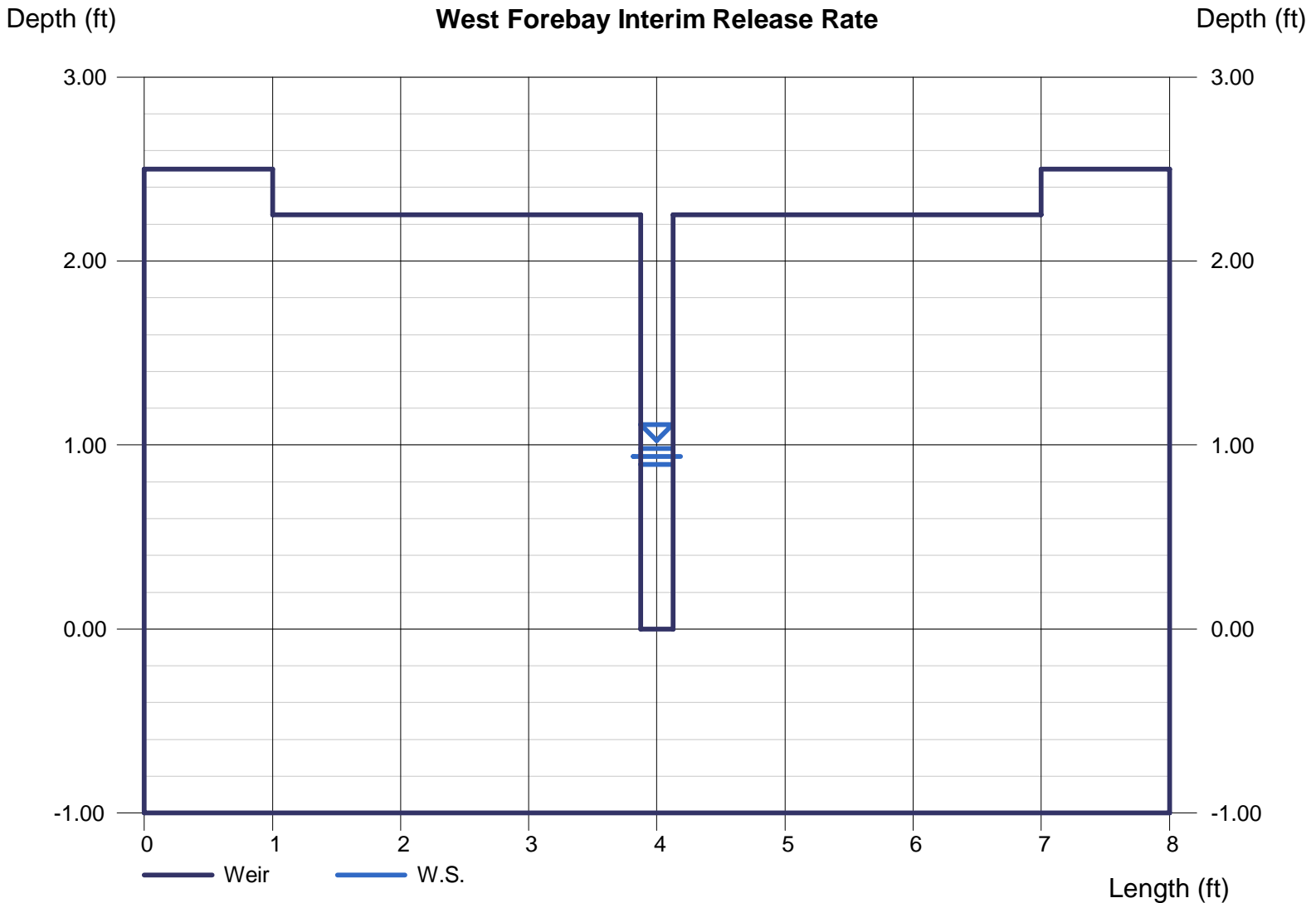
|                    |         |
|--------------------|---------|
| Crest              | = Sharp |
| Bottom Length (ft) | = 6.00  |
| Total Depth (ft)   | = 2.50  |
| Length, x (ft)     | = 0.25  |
| Depth, a (ft)      | = 2.25  |

### Highlighted

|                 |         |
|-----------------|---------|
| Depth (ft)      | = 0.98  |
| Q (cfs)         | = 0.810 |
| Area (sqft)     | = 0.25  |
| Velocity (ft/s) | = 3.30  |
| Top Width (ft)  | = 0.25  |

### Calculations

|                |         |
|----------------|---------|
| Weir Coeff. Cw | = 3.33  |
| Compute by:    | Known Q |
| Known Q (cfs)  | = 0.81  |



# Weir Report

## North Forebay Interim Release Rate

### Compound Weir

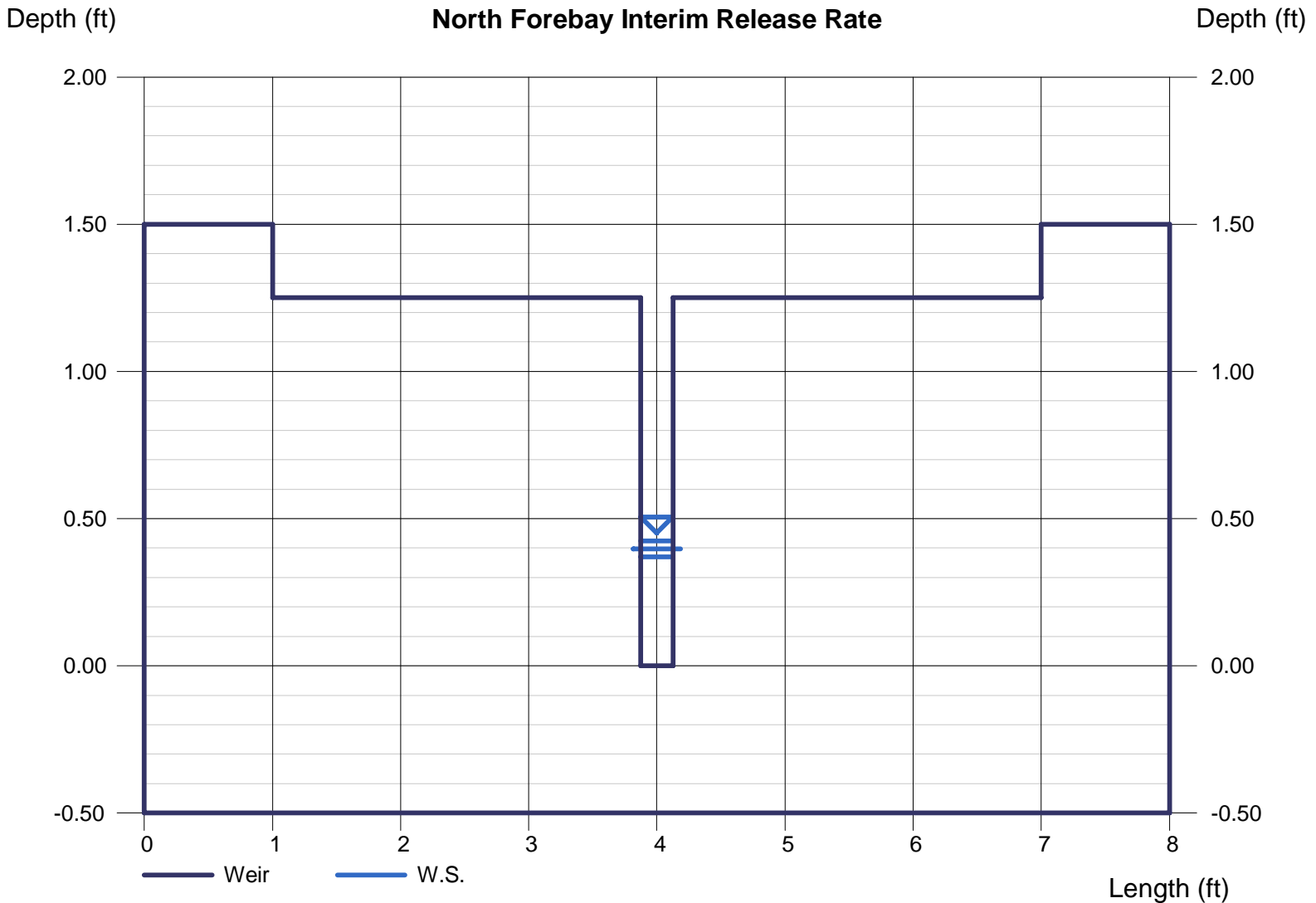
|                    |         |
|--------------------|---------|
| Crest              | = Sharp |
| Bottom Length (ft) | = 6.00  |
| Total Depth (ft)   | = 1.50  |
| Length, x (ft)     | = 0.25  |
| Depth, a (ft)      | = 1.25  |

### Highlighted

|                 |         |
|-----------------|---------|
| Depth (ft)      | = 0.42  |
| Q (cfs)         | = 0.230 |
| Area (sqft)     | = 0.11  |
| Velocity (ft/s) | = 2.17  |
| Top Width (ft)  | = 0.25  |

### Calculations

|                |         |
|----------------|---------|
| Weir Coeff. Cw | = 3.33  |
| Compute by:    | Known Q |
| Known Q (cfs)  | = 0.23  |



# Channel Report

## Trickle Channel Capacity-Interim 6 ft

### Rectangular

Bottom Width (ft) = 6.00  
Total Depth (ft) = 0.50

Invert Elev (ft) = 100.00  
Slope (%) = 0.50  
N-Value = 0.013

### Calculations

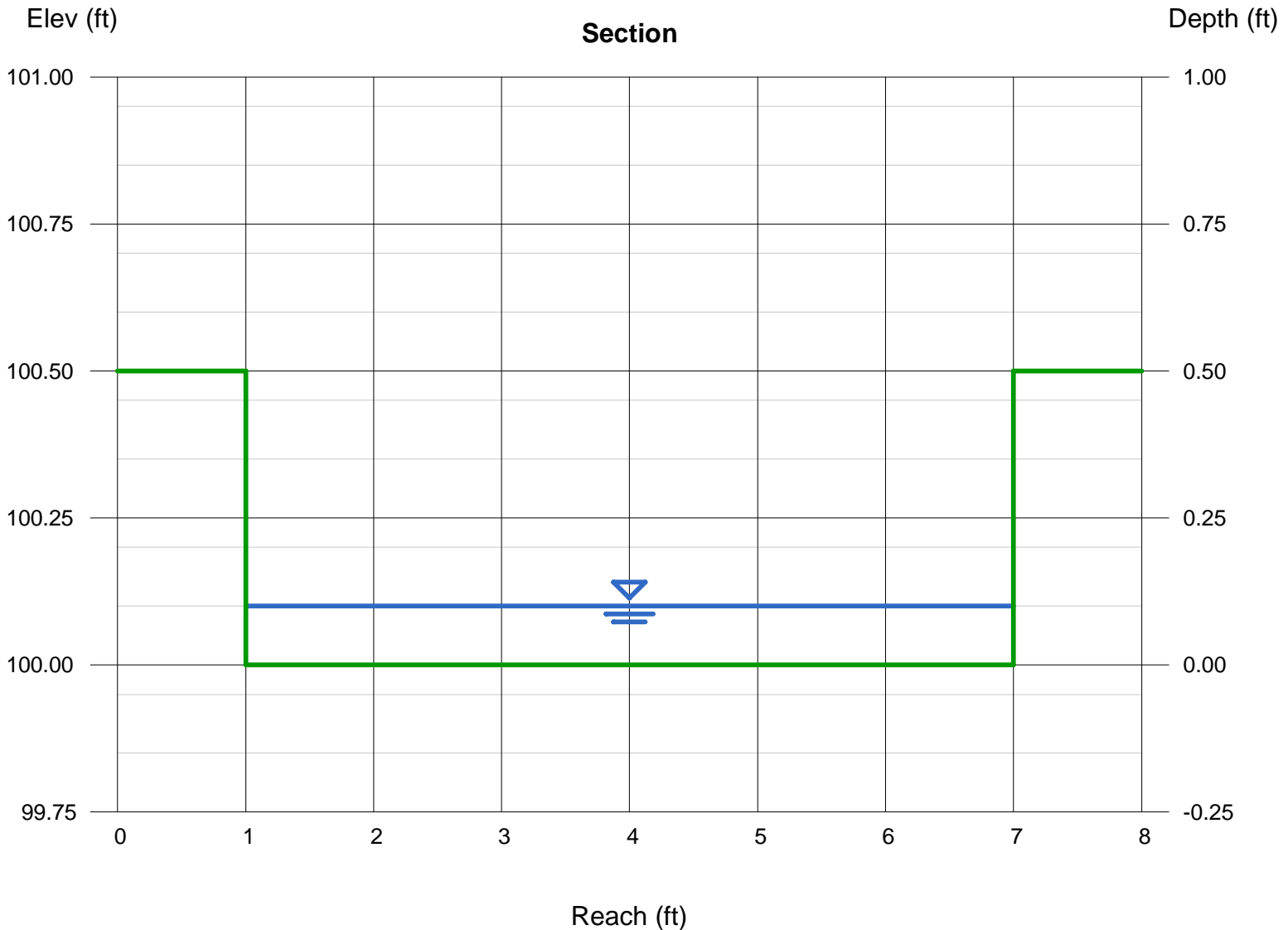
Compute by: Known Q  
Known Q (cfs) = 1.00

### Highlighted

Depth (ft) = 0.10  
Q (cfs) = 1.000  
Area (sqft) = 0.60  
Velocity (ft/s) = 1.67  
Wetted Perim (ft) = 6.20  
Crit Depth, Yc (ft) = 0.10  
Top Width (ft) = 6.00  
EGL (ft) = 0.14

Interim Peak Inflow= 49.5 cfs

2% of  $Q_{100} = 49.5 * 0.02 = 1.0 \text{ cfs}$



# Channel Report

## Trickle Channel Capacity-Ultimate

### Rectangular

Bottom Width (ft) = 6.00  
Total Depth (ft) = 0.50

Invert Elev (ft) = 100.00  
Slope (%) = 0.50  
N-Value = 0.013

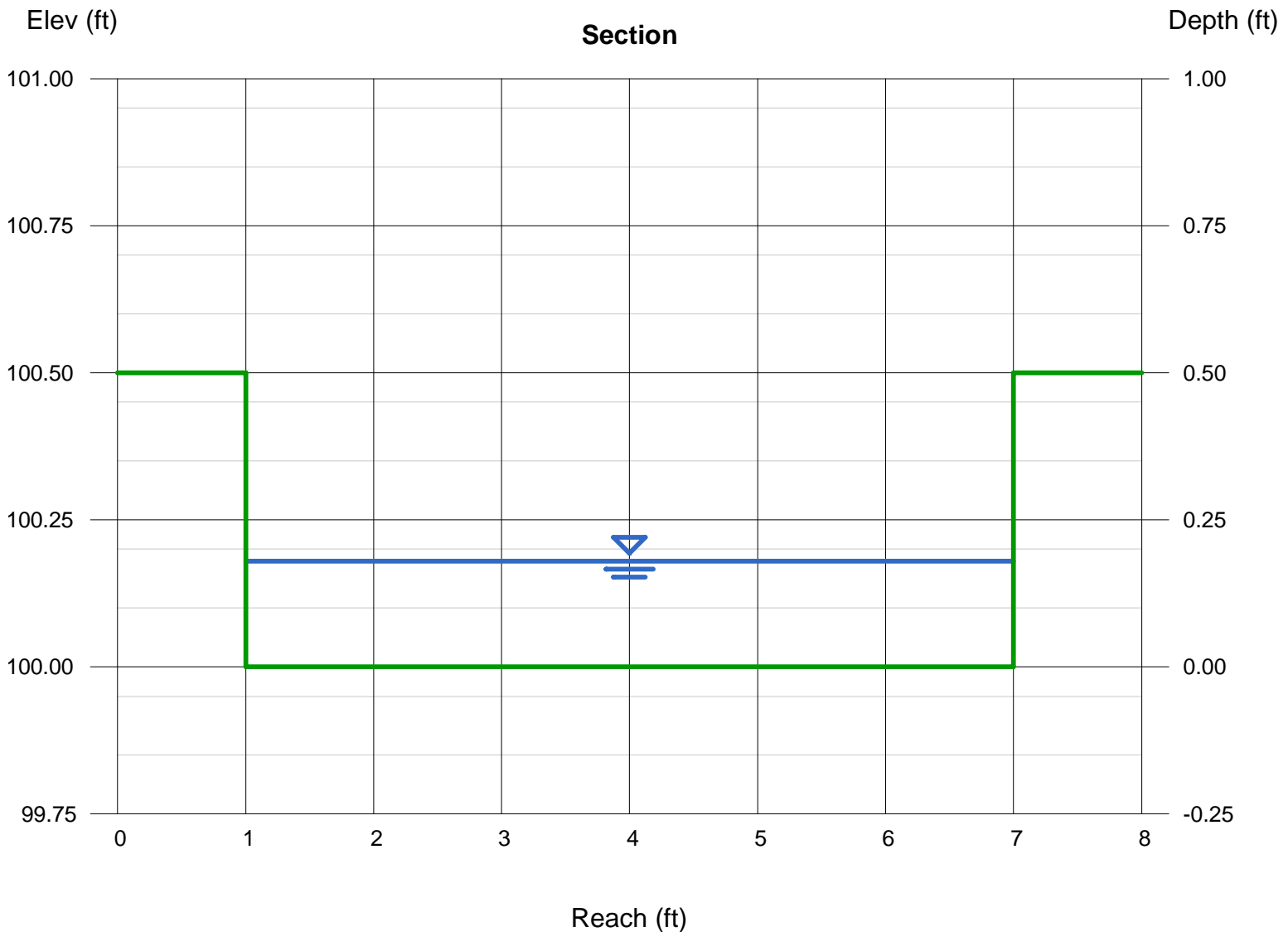
### Calculations

Compute by: Known Q  
Known Q (cfs) = 2.50

### Highlighted

Depth (ft) = 0.18  
Q (cfs) = 2.500  
Area (sqft) = 1.08  
Velocity (ft/s) = 2.31  
Wetted Perim (ft) = 6.36  
Crit Depth, Yc (ft) = 0.18  
Top Width (ft) = 6.00  
EGL (ft) = 0.26

Ultimate Peak Inflow= 123.1 cfs  
2% of  $Q_{100} = 125 * 0.02 = 2.5 \text{ cfs}$

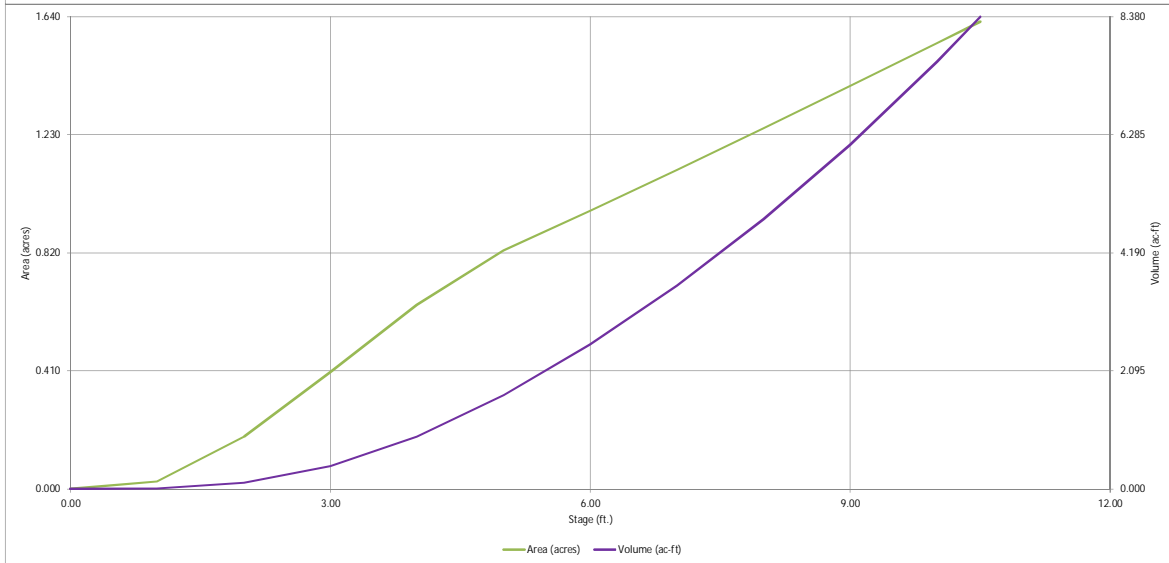
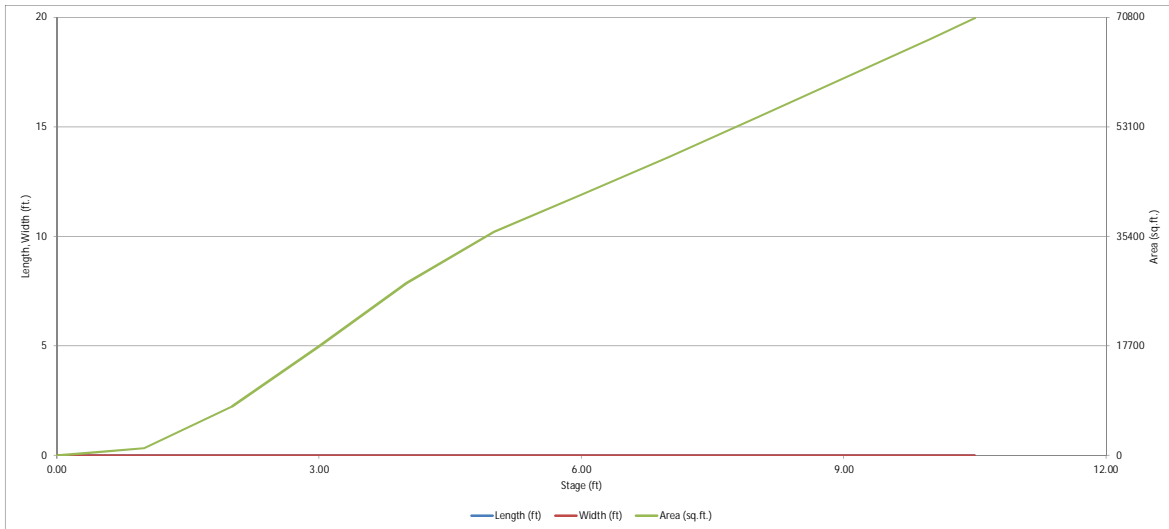






# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

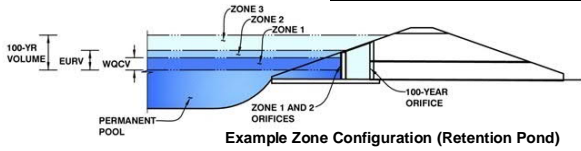
*MHFD-Defention, Version 4.06 (July 2022)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*

Project: Sterling Ranch Recycling Facility  
Basin ID: Pond A-Interim



|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)     | 2.56                 | 0.254                    | Orifice Plate        |
| Zone 2 (EURV)     | 2.84                 | 0.094                    | Rectangular Orifice  |
| Zone 3 (100-year) | 4.19                 | 0.706                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 1.054                    |                      |

**Example Zone Configuration (Retention Pond)**

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

|                                   |     |  |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter =     | N/A | inches   |

Calculated Parameters for Underdrain

|                               |     |                 |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area =     | N/A | ft <sup>2</sup> |
| Underdrain Orifice Centroid = | N/A | feet            |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

|  |      |   |
|--|------|---|
| Centroid of Lowest Orifice =               | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 2.75 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing =  | N/A  | inches  |
| Orifice Plate: Orifice Area per Row =      | N/A  | sq. inches                                    |

Calculated Parameters for Plate

|                            |     |                 |
|----------------------------|-----|-----------------|
| WO Orifice Area per Row =  | N/A | ft <sup>2</sup> |
| Elliptical Half-Width =    | N/A | feet            |
| Elliptical Slot Centroid = | N/A | feet            |
| Elliptical Slot Area =     | N/A | ft <sup>2</sup> |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.00             |                  |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.00             | 1.10             |                  |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Zone 2 Rectangular | Not Selected |   |
|---|--------------------|--------------|---|
| Invert of Vertical Orifice =                  | 2.85               | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | 4.55               | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Height =                     | 21.00              | N/A          | inches  |
| Vertical Orifice Width =                      | 12.00              |              | inches  |

Calculated Parameters for Vertical Orifice

|                             | Zone 2 Rectangular | Not Selected |                 |
|-----------------------------|--------------------|--------------|-----------------|
| Vertical Orifice Area =     | 1.75               | N/A          | ft <sup>2</sup> |
| Vertical Orifice Centroid = | 0.88               | N/A          | feet            |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

|                                       | Zone 3 Weir     | Not Selected |   |
|---------------------------------------|-----------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 7.90            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length =     | 4.00            | N/A          | feet  |
| Overflow Weir Gate Slope =            | 0.00            | N/A          | H:V   |
| Horiz. Length of Weir Sides =         | 4.00            | N/A          | feet  |
| Overflow Gate Type =                  | Close Mesh Gate | N/A          |   |
| Debris Clogging % =                   | 50%             | N/A          | %   |

Calculated Parameters for Overflow Weir

|   | Zone 3 Weir | Not Selected |                 |
|---|-------------|--------------|-----------------|
| Height of Gate Upper Edge, H <sub>1</sub> = | 7.90        | N/A          | feet            |
| Overflow Weir Slope Length =                | 4.00        | N/A          | feet            |
| Gate Open Area / 100-yr Orifice Area =      | 4.03        | N/A          |                 |
| Overflow Gate Open Area w/o Debris =        | 12.66       | N/A          | ft <sup>2</sup> |
| Overflow Gate Open Area w/ Debris =         | 6.33        | N/A          | ft <sup>2</sup> |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|   | Zone 3 Restrictor | Not Selected |  |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe =            | 2.50              | N/A          | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter =                      | 24.00             | N/A          | inches   |
| Restrictor Plate Height Above Pipe Invert = | 24.00             |              | inches   |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

|  | Zone 3 Restrictor | Not Selected |                 |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area =                            | 3.14              | N/A          | ft <sup>2</sup> |
| Outlet Orifice Centroid =                        | 1.00              | N/A          | feet            |
| Half-Central Angle of Restrictor Plate on Pipe = | 3.14              | N/A          | radians         |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

|                                     |        |   |
|-------------------------------------|--------|---|
| Spillway Invert Stage =             | 9.00   | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length =             | 120.00 | feet  |
| Spillway End Slopes =               | 4.00   | H:V   |
| Freeboard above Max Water Surface = | 1.00   | feet  |

Calculated Parameters for Spillway

|                                    |       |         |
|------------------------------------|-------|---------|
| Spillway Design Flow Depth =       | 0.48  | feet    |
| Stage at Top of Freeboard =        | 10.48 | feet    |
| Basin Area at Top of Freeboard =   | 1.62  | acres   |
| Basin Volume at Top of Freeboard = | 8.34  | acre-ft |

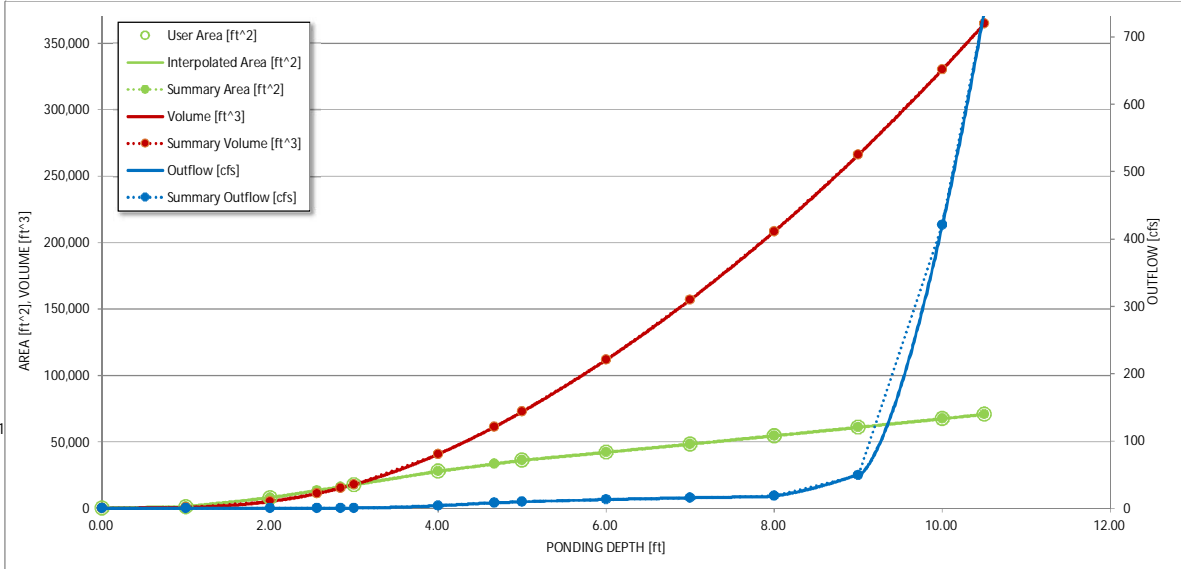
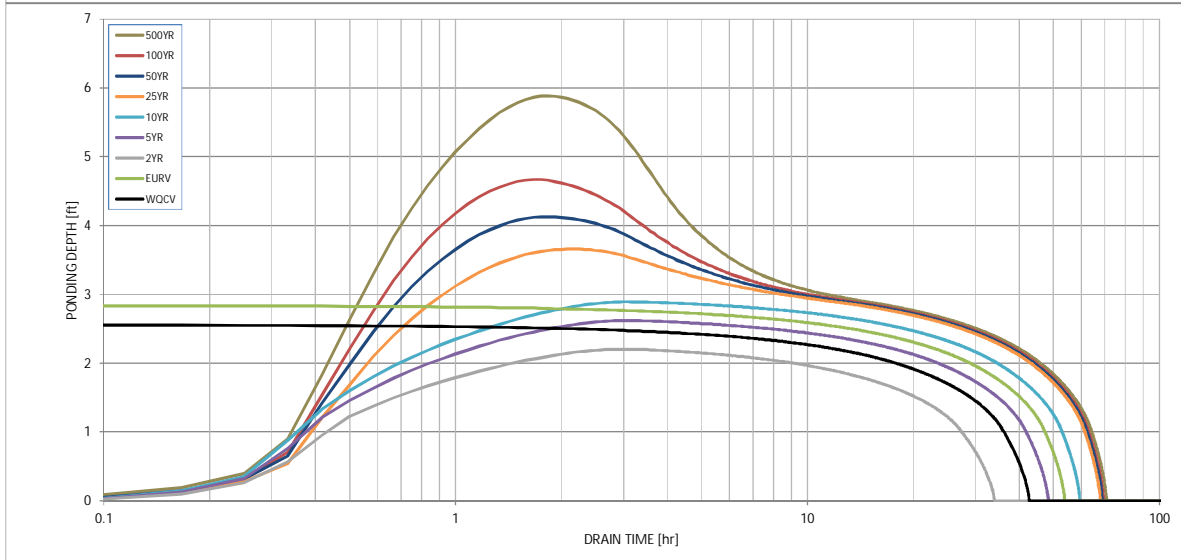
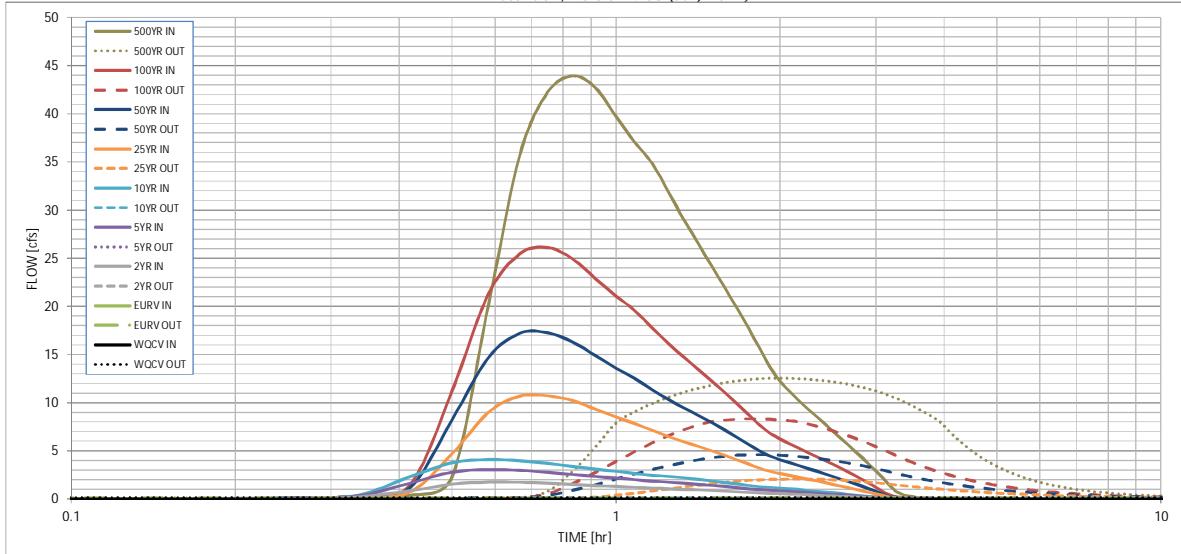
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|   | WOCV  | EURV  | 2 Year | 5 Year | 10 Year            | 25 Year            | 50 Year            | 100 Year           | 500 Year         |
|---|-------|-------|--------|--------|--------------------|--------------------|--------------------|--------------------|------------------|
| Design Storm Return Period =                    |       |       |        |        |                    |                    |                    |                    |                  |
| One-Hour Rainfall Depth (in) =                  | N/A   | N/A   | 1.19   | 1.50   | 1.75               | 2.00               | 2.25               | 2.52               | 3.14             |
| CUHP Runoff Volume (acre-ft) =                  | 0.254 | 0.349 | 0.180  | 0.296  | 0.395              | 0.972              | 1.547              | 2.354              | 4.129            |
| Inflow Hydrograph Volume (acre-ft) =            | N/A   | N/A   | 0.180  | 0.296  | 0.395              | 0.972              | 1.547              | 2.354              | 4.129            |
| CUHP Predevelopment Peak Q (cfs) =              | N/A   | N/A   | 0.3    | 0.5    | 0.7                | 6.3                | 12.7               | 21.2               | 38.6             |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A   | N/A   |        |        |                    |                    |                    |                    |                  |
| Predevelopment Unit Peak Flow, q (cfs/acre) =   | N/A   | N/A   | 0.01   | 0.01   | 0.02               | 0.15               | 0.30               | 0.50               | 0.92             |
| Peak Inflow Q (cfs) =                           | N/A   | N/A   | 1.7    | 3.0    | 4.1                | 10.7               | 17.2               | 26.1               | 43.9             |
| Peak Outflow Q (cfs) =                          | 0.1   | 0.1   | 0.1    | 0.1    | 0.1                | 2.1                | 4.6                | 8.3                | 12.5             |
| Ratio Peak Outflow to Predevelopment Q =        | N/A   | N/A   | N/A    | 0.2    | 0.2                | 0.3                | 0.4                | 0.4                | 0.3              |
| Structure Controlling Flow =                    | Plate | Plate | Plate  | Plate  | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice |
| Max Velocity through Gate 1 (fps) =             | N/A   | N/A   | N/A    | N/A    | N/A                | N/A                | N/A                | N/A                | N/A              |
| Max Velocity through Gate 2 (fps) =             | N/A   | N/A   | N/A    | N/A    | N/A                | N/A                | N/A                | N/A                | N/A              |
| Time to Drain 97% of Inflow Volume (hours) =    | 39    | 49    | 31     | 44     | 54                 | 58                 | 55                 | 52                 | 45               |
| Time to Drain 99% of Inflow Volume (hours) =    | 41    | 52    | 33     | 46     | 57                 | 63                 | 62                 | 61                 | 58               |
| Maximum Ponding Depth (ft) =                    | 2.56  | 2.84  | 2.20   | 2.62   | 2.89               | 3.66               | 4.13               | 4.67               | 5.88             |
| Area at Maximum Ponding Depth (acres) =         | 0.31  | 0.37  | 0.23   | 0.32   | 0.38               | 0.56               | 0.66               | 0.76               | 0.95             |
| Maximum Volume Stored (acre-ft) =               | 0.254 | 0.349 | 0.158  | 0.270  | 0.368              | 0.724              | 1.012              | 1.398              | 2.451            |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

**Inflow Hydrographs**

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

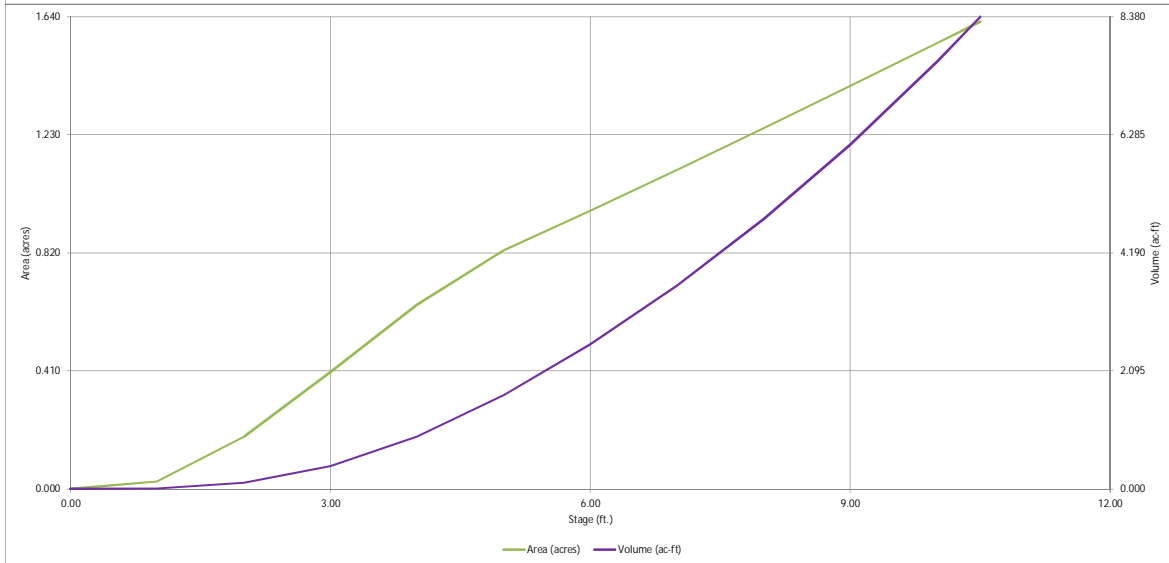
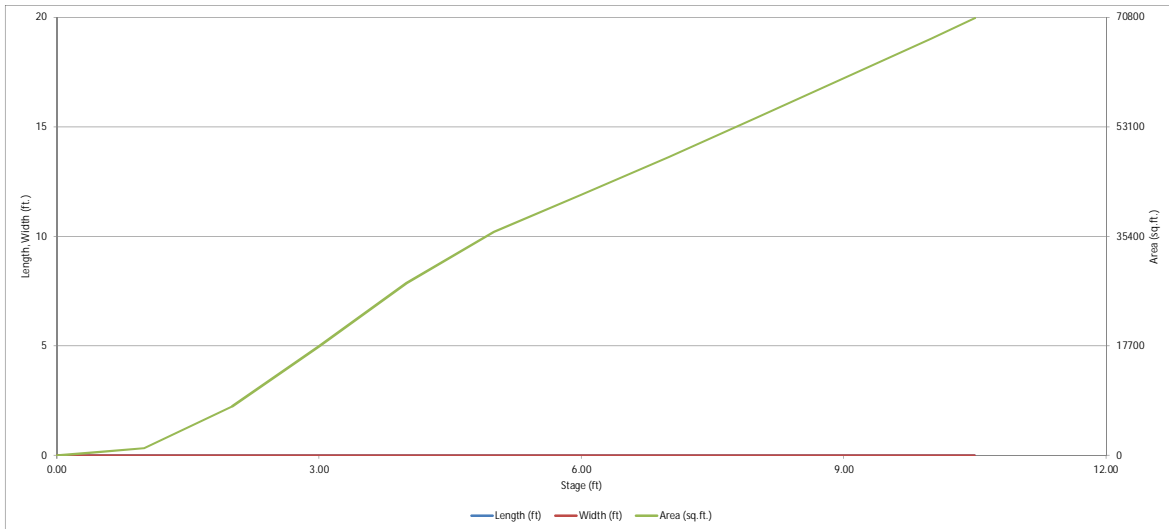
| Time Interval | SOURCE  | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.01          | 0.00           | 0.02           |
|               | 0:15:00 | 0.00       | 0.00       | 0.05         | 0.09         | 0.11          | 0.07          | 0.09          | 0.09           | 0.14           |
|               | 0:20:00 | 0.00       | 0.00       | 0.21         | 0.29         | 0.34          | 0.22          | 0.26          | 0.27           | 0.37           |
|               | 0:25:00 | 0.00       | 0.00       | 0.82         | 1.61         | 2.26          | 0.67          | 1.07          | 1.32           | 2.28           |
|               | 0:30:00 | 0.00       | 0.00       | 1.53         | 2.77         | 3.75          | 4.67          | 8.24          | 11.20          | 20.13          |
|               | 0:35:00 | 0.00       | 0.00       | 1.75         | 3.04         | 4.08          | 9.00          | 14.67         | 21.30          | 35.82          |
|               | 0:40:00 | 0.00       | 0.00       | 1.73         | 2.96         | 3.97          | 10.68         | 17.22         | 25.45          | 42.28          |
|               | 0:45:00 | 0.00       | 0.00       | 1.63         | 2.77         | 3.69          | 10.70         | 17.24         | 26.10          | 43.93          |
|               | 0:50:00 | 0.00       | 0.00       | 1.50         | 2.53         | 3.36          | 10.20         | 16.30         | 24.90          | 42.71          |
|               | 0:55:00 | 0.00       | 0.00       | 1.39         | 2.33         | 3.10          | 9.33          | 14.88         | 22.89          | 39.70          |
|               | 1:00:00 | 0.00       | 0.00       | 1.30         | 2.17         | 2.86          | 8.50          | 13.59         | 21.09          | 37.02          |
|               | 1:05:00 | 0.00       | 0.00       | 1.21         | 2.00         | 2.64          | 7.81          | 12.48         | 19.53          | 34.79          |
|               | 1:10:00 | 0.00       | 0.00       | 1.13         | 1.86         | 2.46          | 7.10          | 11.32         | 17.76          | 31.84          |
|               | 1:15:00 | 0.00       | 0.00       | 1.05         | 1.74         | 2.33          | 6.46          | 10.29         | 16.10          | 28.98          |
|               | 1:20:00 | 0.00       | 0.00       | 0.99         | 1.63         | 2.19          | 5.93          | 9.43          | 14.70          | 26.48          |
|               | 1:25:00 | 0.00       | 0.00       | 0.93         | 1.52         | 2.04          | 5.45          | 8.65          | 13.43          | 24.14          |
|               | 1:30:00 | 0.00       | 0.00       | 0.86         | 1.41         | 1.88          | 4.99          | 7.90          | 12.23          | 21.93          |
|               | 1:35:00 | 0.00       | 0.00       | 0.80         | 1.29         | 1.71          | 4.53          | 7.15          | 11.07          | 19.82          |
|               | 1:40:00 | 0.00       | 0.00       | 0.74         | 1.18         | 1.55          | 4.08          | 6.42          | 9.92           | 17.75          |
|               | 1:45:00 | 0.00       | 0.00       | 0.68         | 1.06         | 1.39          | 3.63          | 5.69          | 8.78           | 15.70          |
|               | 1:50:00 | 0.00       | 0.00       | 0.63         | 0.97         | 1.28          | 3.20          | 4.98          | 7.68           | 13.74          |
|               | 1:55:00 | 0.00       | 0.00       | 0.59         | 0.91         | 1.21          | 2.85          | 4.44          | 6.82           | 12.24          |
|               | 2:00:00 | 0.00       | 0.00       | 0.56         | 0.86         | 1.14          | 2.62          | 4.08          | 6.22           | 11.14          |
|               | 2:05:00 | 0.00       | 0.00       | 0.51         | 0.79         | 1.05          | 2.42          | 3.76          | 5.72           | 10.20          |
|               | 2:10:00 | 0.00       | 0.00       | 0.47         | 0.73         | 0.96          | 2.23          | 3.46          | 5.26           | 9.35           |
|               | 2:15:00 | 0.00       | 0.00       | 0.43         | 0.66         | 0.88          | 2.04          | 3.18          | 4.82           | 8.55           |
|               | 2:20:00 | 0.00       | 0.00       | 0.39         | 0.60         | 0.79          | 1.86          | 2.89          | 4.39           | 7.78           |
|               | 2:25:00 | 0.00       | 0.00       | 0.35         | 0.53         | 0.71          | 1.69          | 2.62          | 3.97           | 7.03           |
|               | 2:30:00 | 0.00       | 0.00       | 0.31         | 0.48         | 0.63          | 1.52          | 2.35          | 3.57           | 6.33           |
|               | 2:35:00 | 0.00       | 0.00       | 0.27         | 0.42         | 0.55          | 1.35          | 2.08          | 3.18           | 5.63           |
|               | 2:40:00 | 0.00       | 0.00       | 0.24         | 0.36         | 0.48          | 1.18          | 1.82          | 2.78           | 4.94           |
|               | 2:45:00 | 0.00       | 0.00       | 0.20         | 0.31         | 0.41          | 1.01          | 1.56          | 2.39           | 4.25           |
|               | 2:50:00 | 0.00       | 0.00       | 0.17         | 0.26         | 0.34          | 0.85          | 1.30          | 2.00           | 3.56           |
|               | 2:55:00 | 0.00       | 0.00       | 0.14         | 0.20         | 0.27          | 0.69          | 1.04          | 1.61           | 2.88           |
|               | 3:00:00 | 0.00       | 0.00       | 0.11         | 0.15         | 0.20          | 0.52          | 0.79          | 1.22           | 2.20           |
|               | 3:05:00 | 0.00       | 0.00       | 0.08         | 0.11         | 0.14          | 0.36          | 0.53          | 0.83           | 1.52           |
|               | 3:10:00 | 0.00       | 0.00       | 0.06         | 0.08         | 0.10          | 0.21          | 0.29          | 0.46           | 0.87           |
|               | 3:15:00 | 0.00       | 0.00       | 0.05         | 0.06         | 0.08          | 0.12          | 0.16          | 0.25           | 0.52           |
|               | 3:20:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.07          | 0.08          | 0.11          | 0.16           | 0.34           |
|               | 3:25:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.06          | 0.06          | 0.08          | 0.11           | 0.22           |
|               | 3:30:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.05          | 0.05          | 0.06          | 0.08           | 0.15           |
|               | 3:35:00 | 0.00       | 0.00       | 0.03         | 0.03         | 0.04          | 0.04          | 0.05          | 0.06           | 0.10           |
|               | 3:40:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.04          | 0.03          | 0.04          | 0.04           | 0.06           |
|               | 3:45:00 | 0.00       | 0.00       | 0.02         | 0.02         | 0.03          | 0.03          | 0.03          | 0.03           | 0.04           |
|               | 3:50:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.02          | 0.02          | 0.02          | 0.02           | 0.03           |
|               | 3:55:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.02          | 0.02          | 0.02          | 0.02           | 0.02           |
|               | 4:00:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.02          | 0.01          | 0.02          | 0.01           | 0.02           |
|               | 4:05:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 4:10:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.01           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

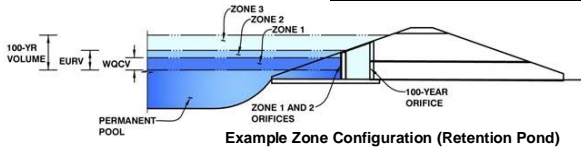
*MHFD-Defention, Version 4.06 (July 2022)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*

Project: Sterling Ranch Recycling Facility  
Basin ID: Pond A-Ultimate



**Example Zone Configuration (Retention Pond)**

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)     | 4.16                 | 1.037                    | Orifice Plate        |
| Zone 2 (EURV)     | 7.38                 | 2.987                    | Circular Orifice     |
| Zone 3 (100-year) | 8.83                 | 1.839                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 5.864                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

|                                   |     |  |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter =     | N/A | inches   |

Calculated Parameters for Underdrain

|                               |     |                 |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area =     | N/A | ft <sup>2</sup> |
| Underdrain Orifice Centroid = | N/A | feet            |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

|  |      |   |
|--|------|---|
| Centroid of Lowest Orifice =               | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 4.16 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing =  | N/A  | inches  |
| Orifice Plate: Orifice Area per Row =      | N/A  | sq. inches                                    |

Calculated Parameters for Plate

|                            |     |                 |
|----------------------------|-----|-----------------|
| WO Orifice Area per Row =  | N/A | ft <sup>2</sup> |
| Elliptical Half-Width =    | N/A | feet            |
| Elliptical Slot Centroid = | N/A | feet            |
| Elliptical Slot Area =     | N/A | ft <sup>2</sup> |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.35             | 2.77             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 2.80             | 2.80             | 2.80             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Zone 2 Circular | Not Selected |   |
|---|-----------------|--------------|---|
| Invert of Vertical Orifice =                  | 4.16            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | 7.38            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter =                   | 4.30            | N/A          | inches  |

Calculated Parameters for Vertical Orifice

|                             | Zone 2 Circular | Not Selected |                 |
|-----------------------------|-----------------|--------------|-----------------|
| Vertical Orifice Area =     | 0.10            | N/A          | ft <sup>2</sup> |
| Vertical Orifice Centroid = | 0.18            | N/A          | feet            |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

|                                       | Zone 3 Weir     | Not Selected |   |
|---------------------------------------|-----------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 7.90            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length =     | 4.00            | N/A          | feet  |
| Overflow Weir Gate Slope =            | 0.00            | N/A          | H:V   |
| Horiz. Length of Weir Sides =         | 4.00            | N/A          | feet  |
| Overflow Gate Type =                  | Close Mesh Gate | N/A          |   |
| Debris Clogging % =                   | 50%             | N/A          | %   |

Calculated Parameters for Overflow Weir

|   | Zone 3 Weir | Not Selected |                 |
|---|-------------|--------------|-----------------|
| Height of Gate Upper Edge, H <sub>1</sub> = | 7.90        | N/A          | feet            |
| Overflow Weir Slope Length =                | 4.00        | N/A          | feet            |
| Gate Open Area / 100-yr Orifice Area =      | 9.01        | N/A          |                 |
| Overflow Gate Open Area w/o Debris =        | 12.66       | N/A          | ft <sup>2</sup> |
| Overflow Gate Open Area w/ Debris =         | 6.33        | N/A          | ft <sup>2</sup> |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|   | Zone 3 Restrictor | Not Selected |  |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe =            | 2.50              | N/A          | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter =                      | 24.00             | N/A          | inches   |
| Restrictor Plate Height Above Pipe Invert = | 11.00             | N/A          | inches   |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

|  | Zone 3 Restrictor | Not Selected |                 |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area =                            | 1.40              | N/A          | ft <sup>2</sup> |
| Outlet Orifice Centroid =                        | 0.53              | N/A          | feet            |
| Half-Central Angle of Restrictor Plate on Pipe = | 1.49              | N/A          | radians         |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

|                                     |        |   |
|-------------------------------------|--------|---|
| Spillway Invert Stage =             | 9.00   | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length =             | 120.00 | feet  |
| Spillway End Slopes =               | 4.00   | H:V   |
| Freeboard above Max Water Surface = | 1.00   | feet  |

Calculated Parameters for Spillway

|                                    |       |         |
|------------------------------------|-------|---------|
| Spillway Design Flow Depth =       | 0.48  | feet    |
| Stage at Top of Freeboard =        | 10.48 | feet    |
| Basin Area at Top of Freeboard =   | 1.62  | acres   |
| Basin Volume at Top of Freeboard = | 8.34  | acre-ft |

## Routed Hydrograph Results

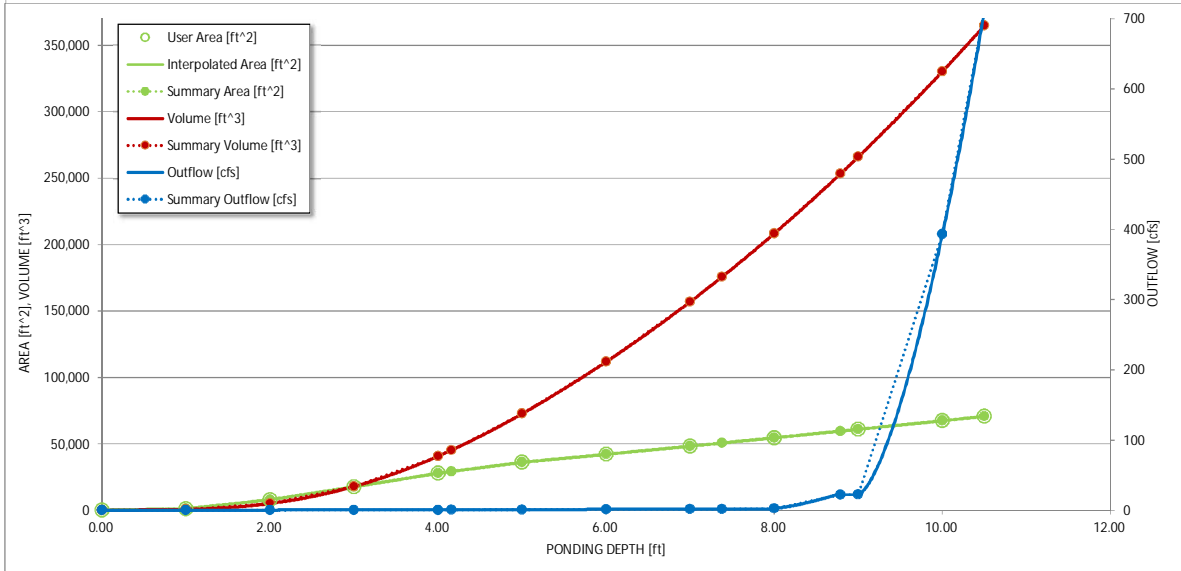
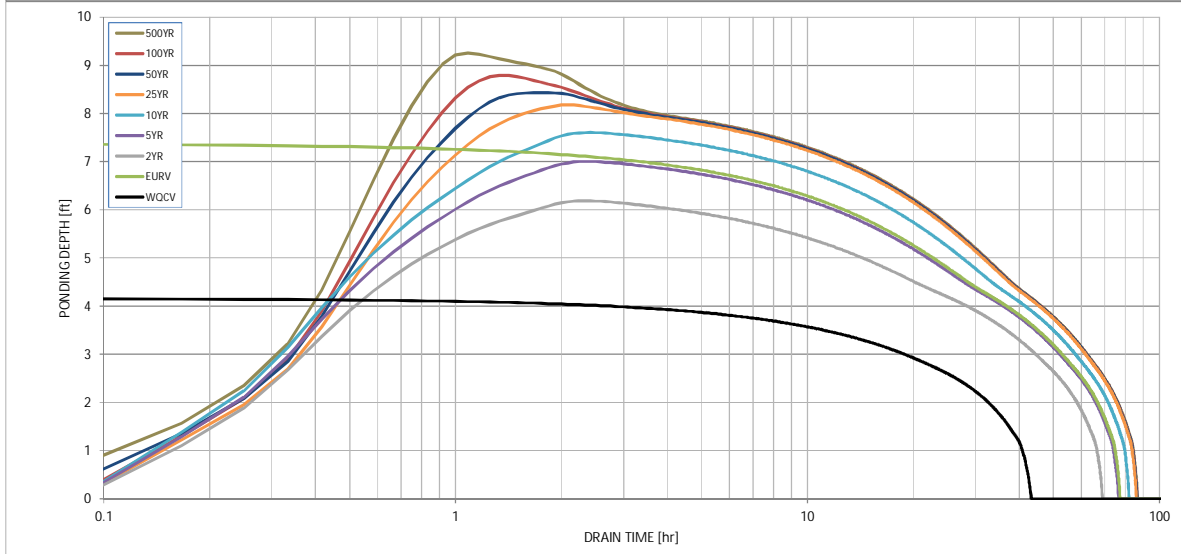
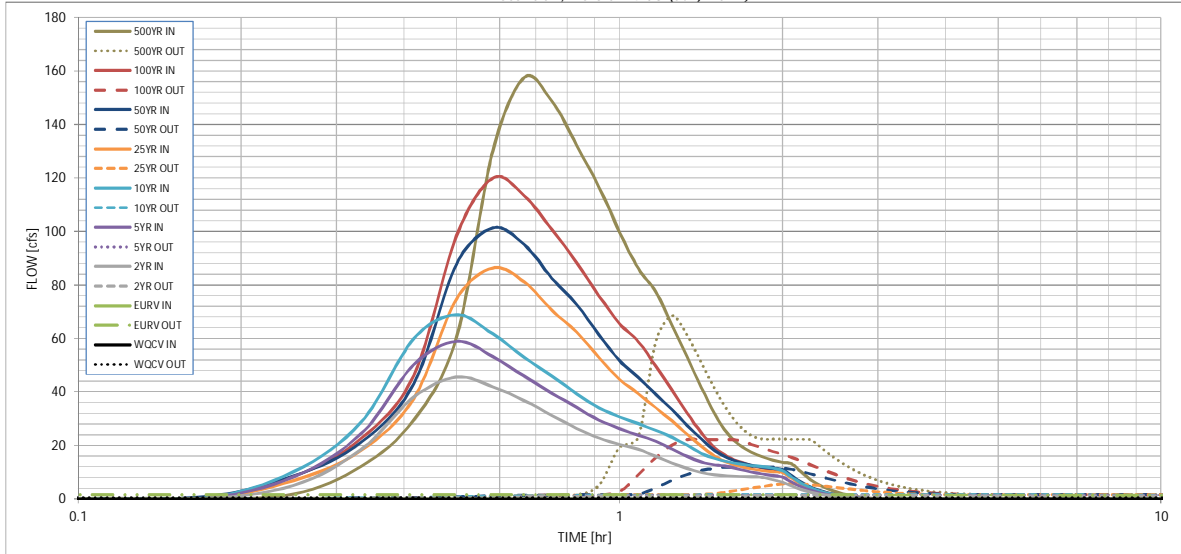
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|   | WOCV               | EURV               | 2 Year             | 5 Year             | 10 Year            | 25 Year         | 50 Year         | 100 Year       | 500 Year |
|---|--------------------|--------------------|--------------------|--------------------|--------------------|-----------------|-----------------|----------------|----------|
| Design Storm Return Period =                    |                    |                    |                    |                    |                    |                 |                 |                |          |
| One-Hour Rainfall Depth (in) =                  | N/A                | N/A                | 1.19               | 1.50               | 1.75               | 2.00            | 2.25            | 2.52           | 3.14     |
| CUHP Runoff Volume (acre-ft) =                  | 1.037              | 4.024              | 2.942              | 3.836              | 4.555              | 5.444           | 6.314           | 7.348          | 9.622    |
| Inflow Hydrograph Volume (acre-ft) =            | N/A                | N/A                | 2.942              | 3.836              | 4.555              | 5.444           | 6.314           | 7.348          | 9.622    |
| CUHP Predevelopment Peak Q (cfs) =              | N/A                | N/A                | 0.3                | 0.5                | 0.7                | 6.7             | 13.4            | 22.5           | 40.9     |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A                | N/A                |                    |                    |                    |                 |                 |                |          |
| Predevelopment Unit Peak Flow, q (cfs/acre) =   | N/A                | N/A                | 0.01               | 0.01               | 0.02               | 0.15            | 0.31            | 0.51           | 0.93     |
| Peak Inflow Q (cfs) =                           | N/A                | N/A                | 45.5               | 58.9               | 68.8               | 86.3            | 101.3           | 120.0          | 157.6    |
| Peak Outflow Q (cfs) =                          | 0.5                | 1.5                | 1.3                | 1.5                | 1.6                | 5.6             | 12.1            | 22.2           | 68.5     |
| Ratio Peak Outflow to Predevelopment Q =        | N/A                | N/A                | N/A                | 2.7                | 2.1                | 0.8             | 0.9             | 1.0            | 1.7      |
| Structure Controlling Flow =                    | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Gate 1 (fps) =             | N/A                | N/A                | N/A                | N/A                | N/A                | 0.3             | 0.8             | 1.6            | 1.6      |
| Max Velocity through Gate 2 (fps) =             | N/A                | N/A                | N/A                | N/A                | N/A                | N/A             | N/A             | N/A            | N/A      |
| Time to Drain 97% of Inflow Volume (hrs) =      | 39                 | 67                 | 60                 | 66                 | 71                 | 73              | 72              | 71             | 68       |
| Time to Drain 99% of Inflow Volume (hours) =    | 41                 | 72                 | 65                 | 71                 | 76                 | 80              | 79              | 79             | 78       |
| Maximum Ponding Depth (ft) =                    | 4.16               | 7.38               | 6.19               | 7.00               | 7.61               | 8.18            | 8.43            | 8.79           | 9.25     |
| Area at Maximum Ponding Depth (acres) =         | 0.67               | 1.16               | 0.99               | 1.11               | 1.19               | 1.28            | 1.32            | 1.37           | 1.44     |
| Maximum Volume Stored (acre-ft) =               | 1.039              | 4.036              | 2.743              | 3.604              | 4.295              | 5.012           | 5.336           | 5.819          | 6.464    |



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

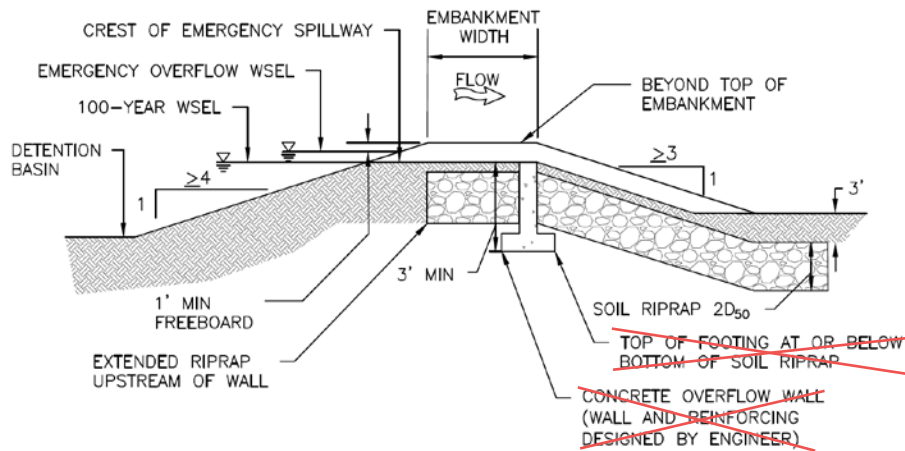
**Inflow Hydrographs**

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

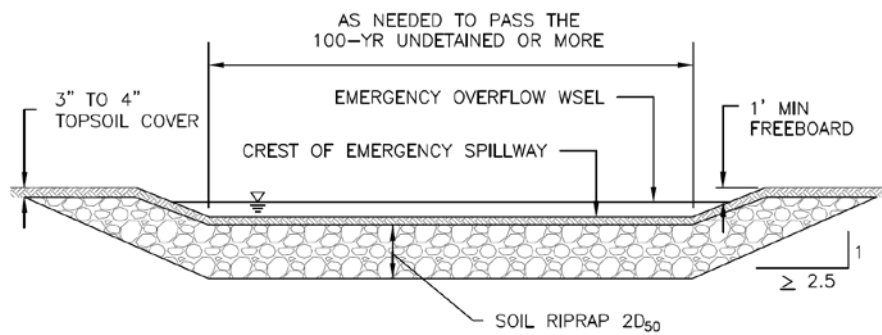
| Time Interval | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
|               | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.57          | 0.06           | 1.83           |
|               | 0:15:00 | 0.00       | 0.00       | 5.05         | 8.22         | 10.18         | 6.84          | 8.59          | 8.34           | 12.16          |
|               | 0:20:00 | 0.00       | 0.00       | 18.49        | 24.39        | 28.72         | 18.15         | 21.18         | 22.63          | 29.51          |
|               | 0:25:00 | 0.00       | 0.00       | 38.05        | 50.12        | 59.86         | 37.51         | 43.02         | 46.17          | 60.49          |
|               | 0:30:00 | 0.00       | 0.00       | 45.54        | 58.87        | 68.83         | 74.78         | 87.92         | 98.38          | 130.15         |
|               | 0:35:00 | 0.00       | 0.00       | 41.90        | 53.26        | 61.67         | 86.30         | 101.33        | 119.99         | 157.58         |
|               | 0:40:00 | 0.00       | 0.00       | 36.74        | 45.86        | 52.97         | 81.13         | 95.11         | 113.39         | 148.64         |
|               | 0:45:00 | 0.00       | 0.00       | 31.21        | 39.50        | 45.91         | 70.58         | 82.55         | 100.68         | 132.31         |
|               | 0:50:00 | 0.00       | 0.00       | 26.39        | 34.22        | 39.33         | 62.32         | 72.70         | 88.45          | 116.56         |
|               | 0:55:00 | 0.00       | 0.00       | 22.70        | 29.43        | 33.99         | 52.82         | 61.36         | 75.91          | 99.84          |
|               | 1:00:00 | 0.00       | 0.00       | 20.32        | 26.23        | 30.69         | 44.70         | 51.70         | 65.52          | 86.12          |
|               | 1:05:00 | 0.00       | 0.00       | 18.51        | 23.80        | 28.11         | 39.37         | 45.45         | 58.85          | 77.48          |
|               | 1:10:00 | 0.00       | 0.00       | 15.95        | 21.50        | 25.59         | 34.05         | 39.18         | 49.59          | 64.99          |
|               | 1:15:00 | 0.00       | 0.00       | 13.45        | 18.71        | 23.09         | 29.16         | 33.43         | 40.80          | 53.16          |
|               | 1:20:00 | 0.00       | 0.00       | 11.32        | 15.89        | 20.06         | 24.06         | 27.48         | 32.11          | 41.61          |
|               | 1:25:00 | 0.00       | 0.00       | 9.80         | 13.80        | 16.95         | 19.69         | 22.38         | 24.67          | 31.79          |
|               | 1:30:00 | 0.00       | 0.00       | 8.99         | 12.73        | 15.05         | 15.90         | 17.99         | 19.07          | 24.43          |
|               | 1:35:00 | 0.00       | 0.00       | 8.58         | 12.15        | 13.89         | 13.59         | 15.33         | 15.79          | 20.11          |
|               | 1:40:00 | 0.00       | 0.00       | 8.35         | 11.01        | 13.06         | 12.15         | 13.69         | 13.82          | 17.52          |
|               | 1:45:00 | 0.00       | 0.00       | 8.20         | 10.02        | 12.46         | 11.21         | 12.62         | 12.47          | 15.72          |
|               | 1:50:00 | 0.00       | 0.00       | 8.08         | 9.31         | 12.04         | 10.55         | 11.88         | 11.56          | 14.50          |
|               | 1:55:00 | 0.00       | 0.00       | 7.16         | 8.78         | 11.48         | 10.11         | 11.38         | 10.90          | 13.63          |
|               | 2:00:00 | 0.00       | 0.00       | 6.26         | 8.16         | 10.49         | 9.80          | 11.03         | 10.45          | 13.03          |
|               | 2:05:00 | 0.00       | 0.00       | 4.79         | 6.27         | 8.01          | 7.59          | 8.53          | 8.03           | 10.00          |
|               | 2:10:00 | 0.00       | 0.00       | 3.51         | 4.55         | 5.79          | 5.49          | 6.17          | 5.81           | 7.23           |
|               | 2:15:00 | 0.00       | 0.00       | 2.55         | 3.31         | 4.20          | 3.98          | 4.47          | 4.23           | 5.27           |
|               | 2:20:00 | 0.00       | 0.00       | 1.84         | 2.38         | 3.04          | 2.89          | 3.25          | 3.10           | 3.85           |
|               | 2:25:00 | 0.00       | 0.00       | 1.31         | 1.66         | 2.15          | 2.04          | 2.29          | 2.19           | 2.72           |
|               | 2:30:00 | 0.00       | 0.00       | 0.90         | 1.13         | 1.50          | 1.43          | 1.60          | 1.53           | 1.90           |
|               | 2:35:00 | 0.00       | 0.00       | 0.60         | 0.78         | 1.04          | 1.01          | 1.13          | 1.08           | 1.34           |
|               | 2:40:00 | 0.00       | 0.00       | 0.37         | 0.51         | 0.66          | 0.66          | 0.74          | 0.70           | 0.87           |
|               | 2:45:00 | 0.00       | 0.00       | 0.19         | 0.30         | 0.37          | 0.39          | 0.43          | 0.41           | 0.50           |
|               | 2:50:00 | 0.00       | 0.00       | 0.08         | 0.14         | 0.17          | 0.18          | 0.20          | 0.19           | 0.24           |
|               | 2:55:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.05          | 0.06          | 0.06          | 0.06           | 0.07           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |



**SPILLWAY RIPRAP CALCULATION**



**EMERGENCY SPILLWAY PROFILE**



**EMERGENCY SPILLWAY SECTION AND SPILLWAY CHANNEL**

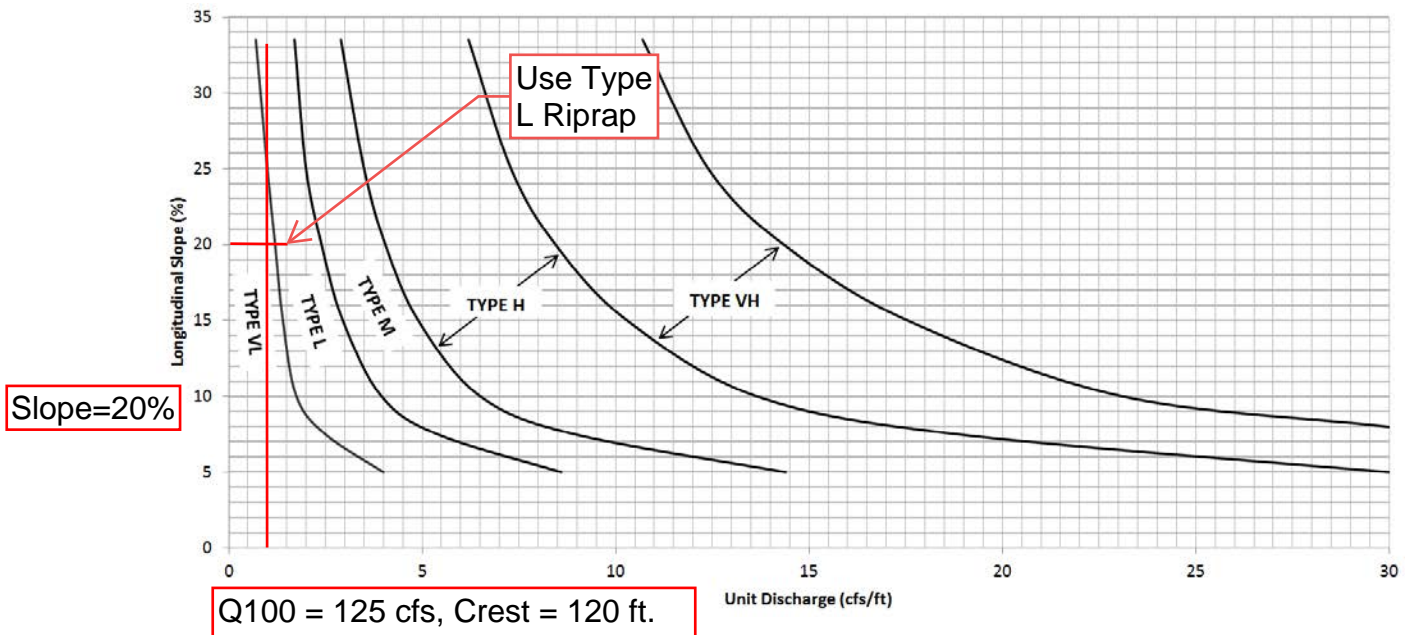


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

# Channel Report

## Spillway Overflow Channel (Wide)

### Trapezoidal

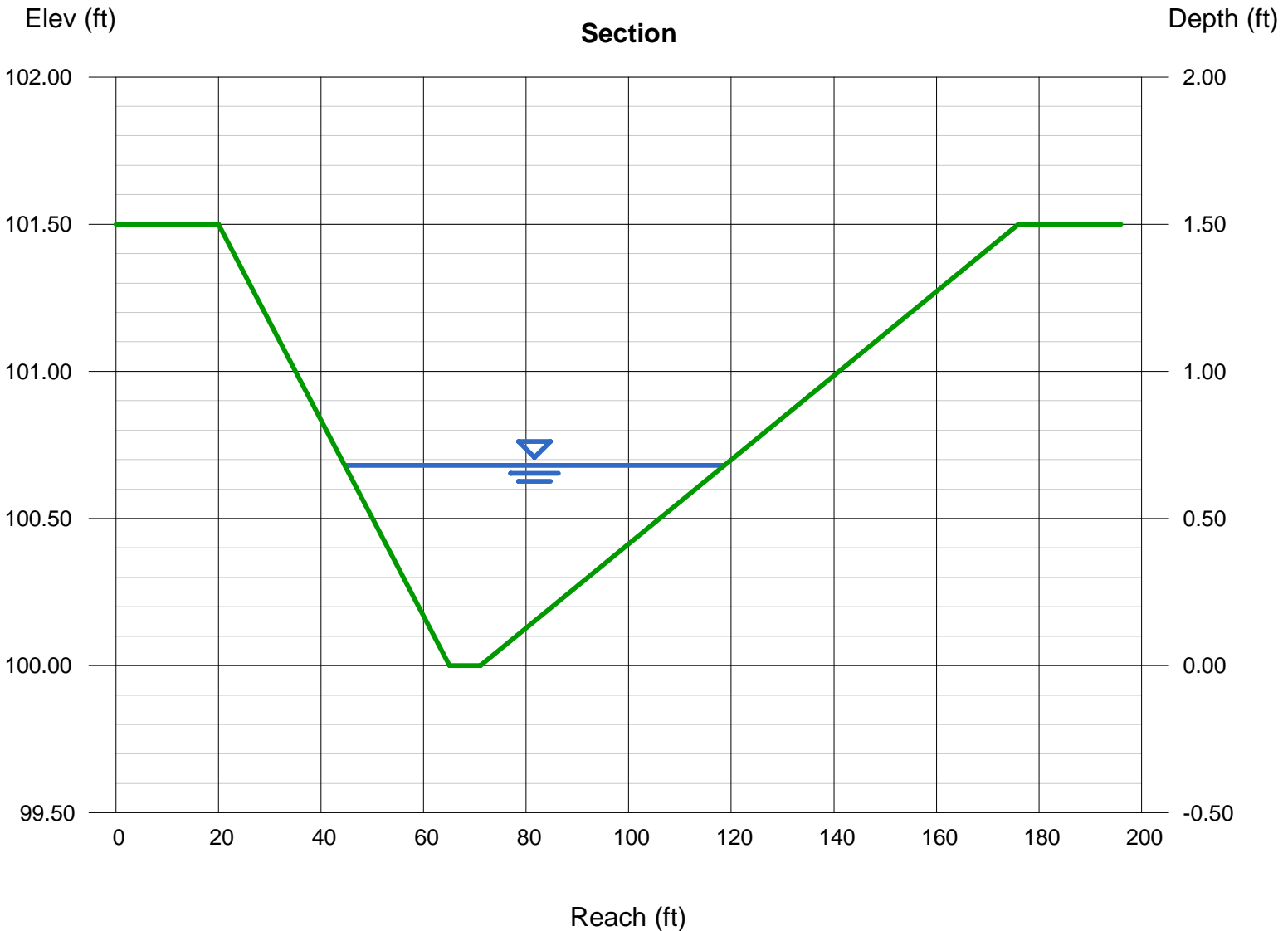
Bottom Width (ft) = 6.00  
Side Slopes (z:1) = 30.00, 70.00  
Total Depth (ft) = 1.50  
Invert Elev (ft) = 100.00  
Slope (%) = 4.50  
N-Value = 0.035

### Highlighted

Depth (ft) = 0.68  
Q (cfs) = 125.00  
Area (sqft) = 27.20  
Velocity (ft/s) = 4.60  
Wetted Perim (ft) = 74.02  
Crit Depth, Yc (ft) = 0.78  
Top Width (ft) = 74.00  
EGL (ft) = 1.01

### Calculations

Compute by: Known Q  
Known Q (cfs) = 125.00



# Channel Report

## Spillway Overflow Channel (Narrow)

### Trapezoidal

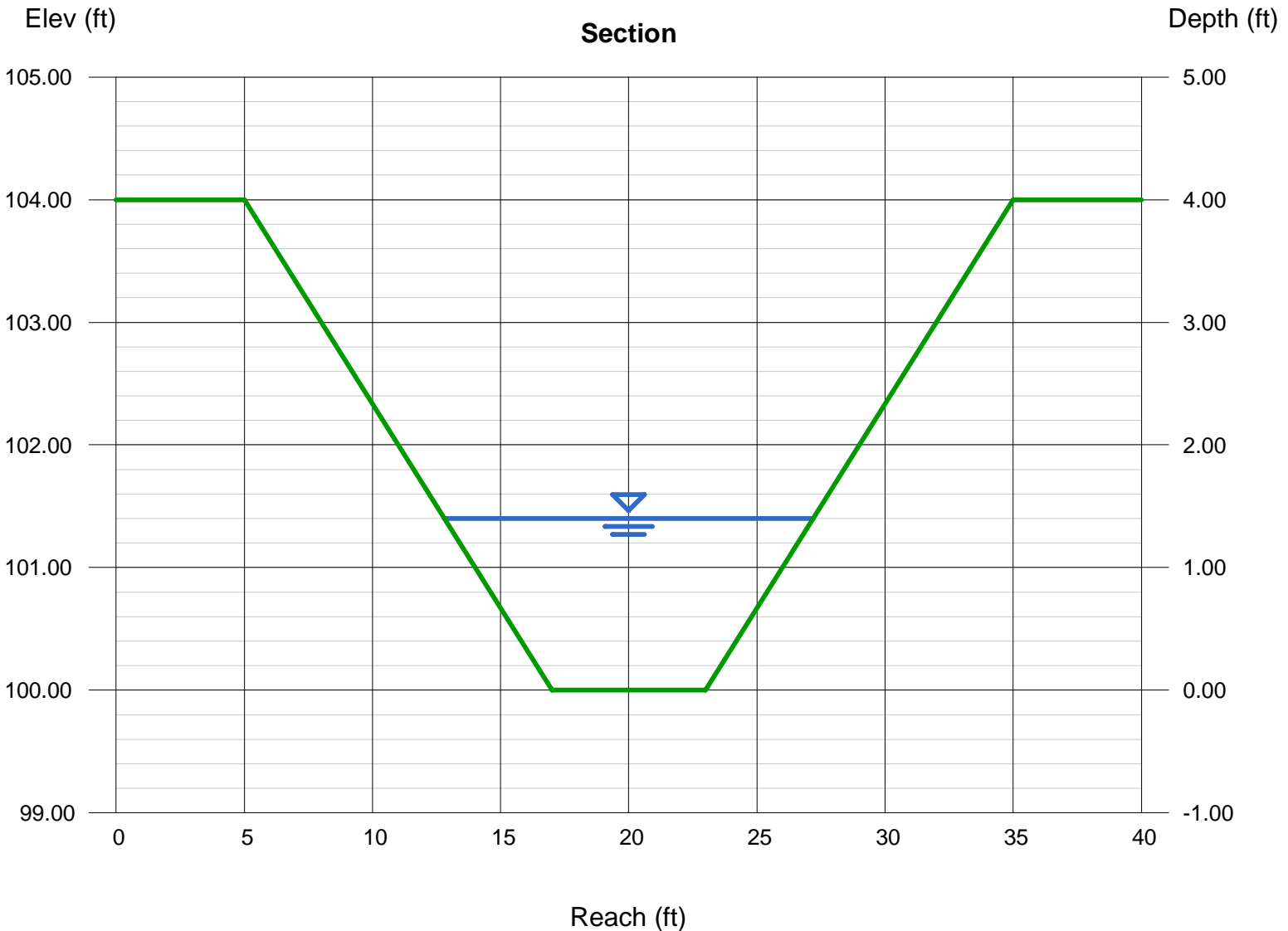
Bottom Width (ft) = 6.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 4.00  
Invert Elev (ft) = 100.00  
Slope (%) = 4.50  
N-Value = 0.035

### Highlighted

Depth (ft) = 1.40  
Q (cfs) = 125.00  
Area (sqft) = 14.28  
Velocity (ft/s) = 8.75  
Wetted Perim (ft) = 14.85  
Crit Depth,  $Y_c$  (ft) = 1.78  
Top Width (ft) = 14.40  
EGL (ft) = 2.59

### Calculations

Compute by: Known Q  
Known Q (cfs) = 125.00



# INLET MANAGEMENT

Worksheet Protected

|                                    |   |
|------------------------------------|---|
| INLET NAME                         | <a href="#">Pond Emergency Overflow</a> |
| Site Type (Urban or Rural)         | URBAN                                   |
| Inlet Application (Street or Area) | AREA                                    |
| Hydraulic Condition                | Swale                                   |
| Inlet Type                         | User-Defined                            |

## USER-DEFINED INPUT

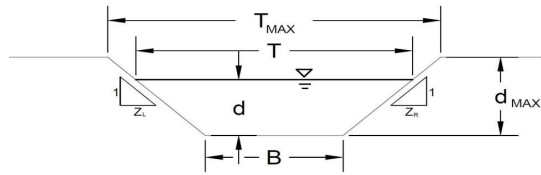
|  |                         |
|--|-------------------------|
| User-Defined Design Flows  |                         |
| Minor $Q_{\text{Known}}$ (cfs)   | 0.0                     |
| Major $Q_{\text{Known}}$ (cfs)   | 125.0                   |
| Bypass (Carry-Over) Flow from Upstream <a href="#">Inlets must be organized from upstream (let</a> |                         |
| Receive Bypass Flow from:  | No Bypass Flow Received |
| Minor Bypass Flow Received, $Q_b$ (cfs)  | 0.0                     |
| Major Bypass Flow Received, $Q_b$ (cfs)  | 0.0                     |
| Watershed Characteristics  |                         |
| Subcatchment Area (acres)  |                         |
| Percent Impervious   |                         |
| NRCS Soil Type   |                         |
| Watershed Profile  |                         |
| Overland Slope (ft/ft)   |                         |
| Overland Length (ft)   |                         |
| Channel Slope (ft/ft)  |                         |
| Channel Length (ft)  |                         |
| Minor Storm Rainfall Input   |                         |
| Design Storm Return Period, $T_r$ (years)  |                         |
| One-Hour Precipitation, $P_1$ (inches)   |                         |
| Major Storm Rainfall Input   |                         |
| Design Storm Return Period, $T_r$ (years)  |                         |
| One-Hour Precipitation, $P_1$ (inches)   |                         |

## CALCULATED OUTPUT

|   |       |
|---|-------|
| Minor Total Design Peak Flow, $Q$ (cfs)     | 0.0   |
| Major Total Design Peak Flow, $Q$ (cfs)     | 125.0 |
| Minor Flow Bypassed Downstream, $Q_b$ (cfs) | 0.0   |
| Major Flow Bypassed Downstream, $Q_b$ (cfs) | 0.0   |

## AREA INLET IN A SWALE

Sterling Ranch Recycling Facility  
Pond Emergency Overflow



This worksheet uses the NRCS vegetal retardance method to determine Manning's n for grass-lined channels.  
An override Manning's n can be entered for other channel materials.

**Analysis of Trapezoidal Channel (Grass-Lined uses SCS Method)**

NRCS Vegetal Retardance (A, B, C, D, or E) A, B, C, D, or E =

Manning's n (Leave cell D16 blank to manually enter an n value) n = 0.030

Channel Invert Slope S<sub>0</sub> = 0.0005 ft/ft

Bottom Width B = 6.00 ft

Left Side Slope Z1 = 3.00 ft/ft

Right Side Slope Z2 = 3.00 ft/ft

Check one of the following soil types:

| Soil Type:   | Max. Velocity (V <sub>max</sub> ) | Max. Froude No. (F <sub>max</sub> ) |
|--------------|-----------------------------------|-------------------------------------|
| Non-Cohesive | 5.0 fps                           | 0.60                                |
| Cohesive     | 7.0 fps                           | 0.80                                |
| Paved        | N/A                               | N/A                                 |

Choose One:

Non-Cohesive

Cohesive

Paved

|  | Minor Storm | Major Storm |    |
|--|-------------|-------------|----|
| Maximum Allowable Top Width of Channel for Minor & Major Storm   | 18.00       | 30.00       | ft |
| Maximum Allowable Water Depth in Channel for Minor & Major Storm | 3.00        | 4.00        | ft |

---

**Allowable Channel Capacity Based On Channel Geometry**

MINOR STORM Allowable Capacity is based on Top Width Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

|                    | Minor Storm | Major Storm |     |
|--------------------|-------------|-------------|-----|
| Q <sub>allow</sub> | 29.9        | 132.2       | cfs |
| d <sub>allow</sub> | 2.00        | 4.00        | ft  |

---

**Water Depth in Channel Based On Design Peak Flow**

Design Peak Flow

Water Depth

|                | 0.0  | 125.0 |     |
|----------------|------|-------|-----|
| Q <sub>o</sub> | 0.0  | 125.0 | cfs |
| d              | 0.00 | 3.90  | ft  |

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'



MHFD-Inlet, Version 5.03 (August 2023)  
**AREA INLET IN A SWALE**

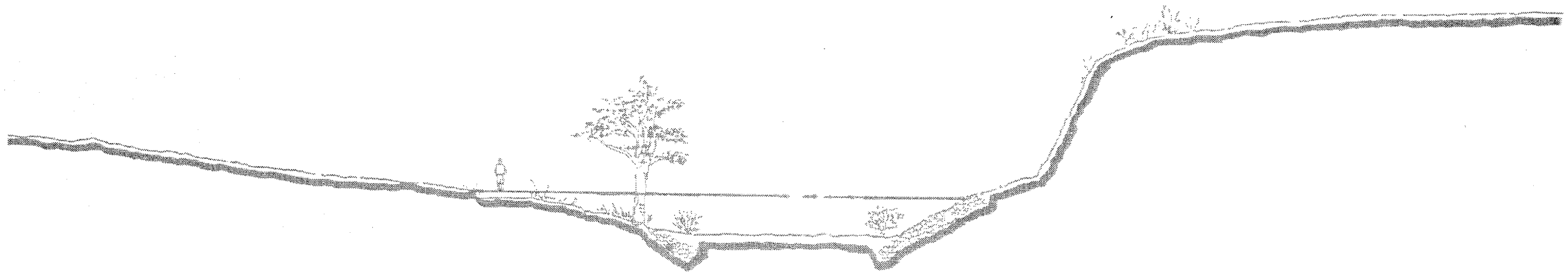
Sterling Ranch Recycling Facility  
 Pond Emergency Overflow

| Inlet Design Information (Input)  |                           |
|---|---------------------------|
| Type of Inlet   | User-Defined              |
| Inlet Type =  | User-Defined              |
| Angle of Inclined Grate (must be $\leq 30$ degrees)                         | $\theta = 0.00$ degrees   |
| Width of Grate  | $W = 6.00$ ft             |
| Length of Grate   | $L = 6.00$ ft             |
| Open Area Ratio   | $A_{RATIO} = 0.70$        |
| Height of Inclined Grate  | $H_B = 0.00$ ft           |
| Clogging Factor   | $C_f = 0.50$              |
| Grate Discharge Coefficient   | $C_d = N/A$               |
| Orifice Coefficient   | $C_o = 0.64$              |
| Weir Coefficient  | $C_w = 2.05$              |
|   |                           |
| Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) | $d = 0.00$ MINOR MAJOR    |
| Total Inlet Interception Capacity (assumes clogged condition)               | $Q_a = 0.0$ 0.0 127.8 cfs |
| Bypassed Flow   | $Q_b = 0.0$ 0.0 cfs       |
| Capture Percentage = $Q_a/Q_o$  | $C\% = 100$ 100 %         |

## **Appendix D**

### **Reference Materials**

**SAND CREEK DRAINAGE BASIN PLANNING STUDY**  
**PRELIMINARY DESIGN REPORT**  
**CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO**



**PREPARED FOR:**

City of Colorado Springs  
Department of Comprehensive Planning, Development and Finance  
Engineering Division  
30 S. Nevada  
Colorado Springs, Colorado 80903

**PREPARED BY:**

Kiowa Engineering Corporation  
1011 North Weber  
Colorado Springs, CO 80903

## II. STUDY AREA DESCRIPTION

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The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

### Basin Description

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence is most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

### Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about 30°F in the winter

to 75° in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

### Soils and Geology

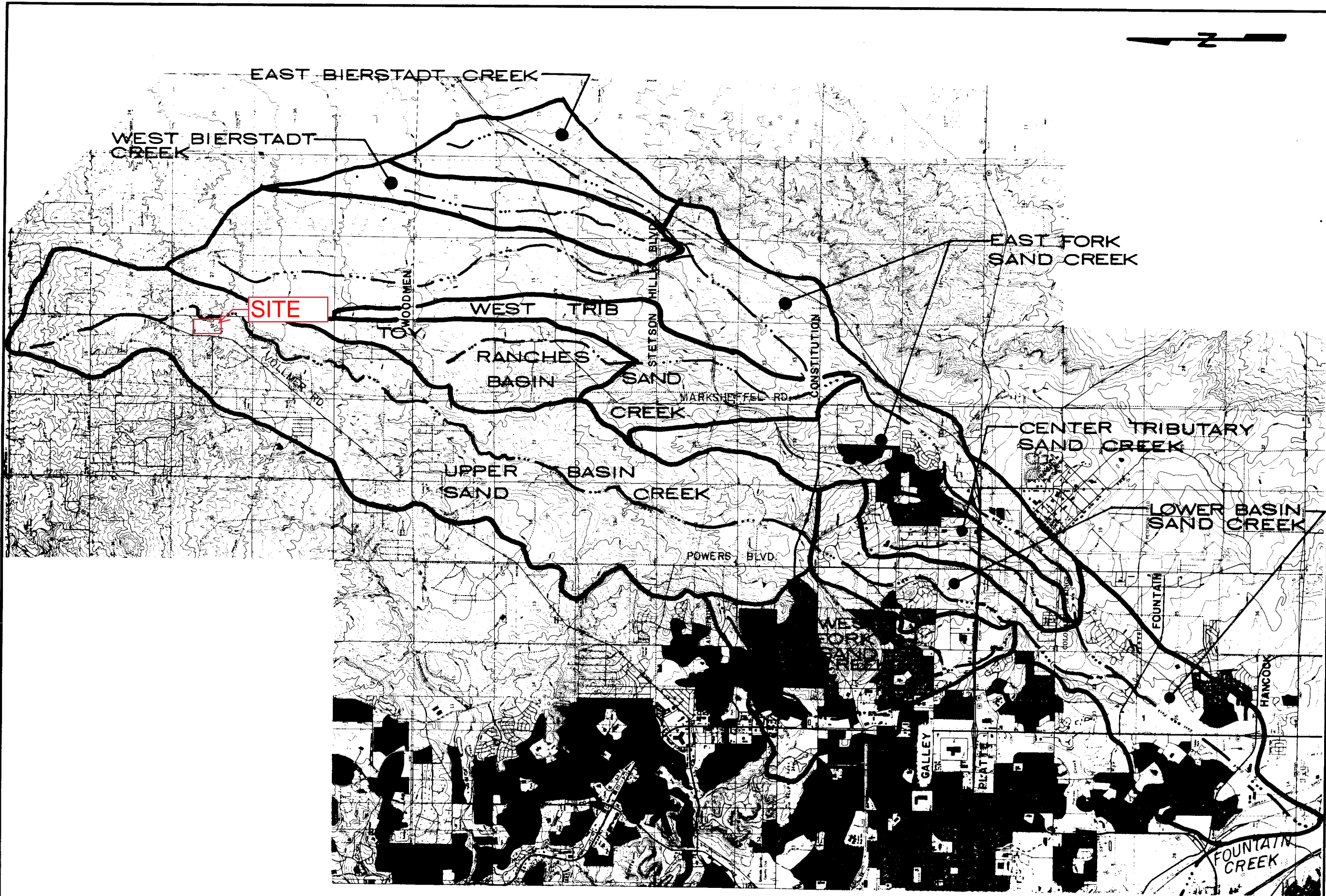
Soils within the Sand Creek basin vary between soil types A through D, as identified by the U. S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residuum, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

### Property Ownership and Impervious Land Densities

Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within



Kiowa Engineering Corporation  
 419 W. Bijou Street  
 Colorado Springs, Colorado  
 80905-1308

SAND CREEK DRAINAGE  
 BASIN PLANNING STUDY  
 REGIONAL SUB-BASINS

|            |          |
|------------|----------|
| Project No | 90-04-09 |
| Date:      | 11/90    |
| Design:    |          |
| Drawn:     | EAK      |
| Check:     |          |
| Revisions: |          |

**FINAL DRAINAGE REPORT  
FOR  
STERLING RANCH FILING NO. 2**

**Prepared For:  
SR Land, LLC  
20 Boulder Crescent, Suite 210  
Colorado Springs, CO 80903**

**August 2021  
Project No. 25188.01**

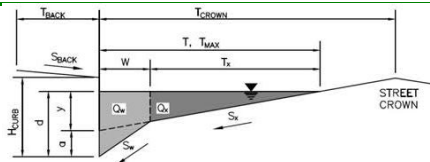
**Prepared By:  
JR Engineering, LLC  
5475 Tech Center Drive  
Colorado Springs, CO 80919  
719-593-2593**

**PCD File No. SF-20-015**

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

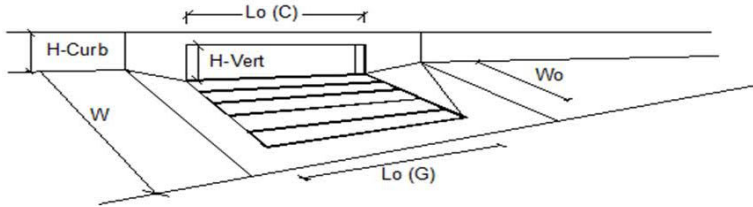
Project: **Sterling Ranch Filing No. 2**  
 Inlet ID: **A10**



| Gutter Geometry (Enter data in the blue cells)  |  |             |             |             |  |             |      |      |     |             |     |     |        |
|---|--|-------------|-------------|-------------|--|-------------|------|------|-----|-------------|-----|-----|--------|
| Maximum Allowable Width for Spread Behind Curb  | $T_{BACK} = 15.0$ ft   |             |             |             |  |             |      |      |     |             |     |     |        |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb)                                 | $S_{BACK} = 0.020$ ft/ft   |             |             |             |  |             |      |      |     |             |     |     |        |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020)                                       | $n_{BACK} = 0.016$   |             |             |             |  |             |      |      |     |             |     |     |        |
| Height of Curb at Gutter Flow Line  | $H_{CURB} = 6.00$ inches   |             |             |             |  |             |      |      |     |             |     |     |        |
| Distance from Curb Face to Street Crown   | $T_{CROWN} = 38.0$ ft  |             |             |             |  |             |      |      |     |             |     |     |        |
| Gutter Width  | $W = 2.00$ ft  |             |             |             |  |             |      |      |     |             |     |     |        |
| Street Transverse Slope   | $S_x = 0.020$ ft/ft  |             |             |             |  |             |      |      |     |             |     |     |        |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)                                     | $S_w = 0.083$ ft/ft  |             |             |             |  |             |      |      |     |             |     |     |        |
| Street Longitudinal Slope - Enter 0 for sump condition  | $S_o = 0.012$ ft/ft  |             |             |             |  |             |      |      |     |             |     |     |        |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020)                                | $n_{STREET} = 0.016$   |             |             |             |  |             |      |      |     |             |     |     |        |
| Max. Allowable Spread for Minor & Major Storm   | <table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td><math>T_{MAX} =</math></td> <td>33.0</td> <td>38.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX} =</math></td> <td>6.0</td> <td>9.1</td> <td>inches</td> </tr> </tbody> </table> |             | Minor Storm | Major Storm |  | $T_{MAX} =$ | 33.0 | 38.0 | ft  | $d_{MAX} =$ | 6.0 | 9.1 | inches |
|   | Minor Storm  | Major Storm |             |             |  |             |      |      |     |             |     |     |        |
| $T_{MAX} =$   | 33.0   | 38.0        | ft          |             |  |             |      |      |     |             |     |     |        |
| $d_{MAX} =$   | 6.0  | 9.1         | inches      |             |  |             |      |      |     |             |     |     |        |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm   |  |             |             |             |  |             |      |      |     |             |     |     |        |
| Allow Flow Depth at Street Crown (leave blank for no)   | <input type="checkbox"/> <input type="checkbox"/> check = yes  |             |             |             |  |             |      |      |     |             |     |     |        |
| <b>MINOR STORM</b> Allowable Capacity is based on Depth Criterion   |  |             |             |             |  |             |      |      |     |             |     |     |        |
| <b>MAJOR STORM</b> Allowable Capacity is based on Depth Criterion   |  |             |             |             |  |             |      |      |     |             |     |     |        |
| Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' |  |             |             |             |  |             |      |      |     |             |     |     |        |
| Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' |  |             |             |             |  |             |      |      |     |             |     |     |        |
| $Q_{allow} =$   | <table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td></td> <td>15.2</td> <td>63.8</td> <td>cfs</td> </tr> </tbody> </table>   |             | Minor Storm | Major Storm |  |             | 15.2 | 63.8 | cfs |             |     |     |        |
|   | Minor Storm  | Major Storm |             |             |  |             |      |      |     |             |     |     |        |
|   | 15.2   | 63.8        | cfs         |             |  |             |      |      |     |             |     |     |        |

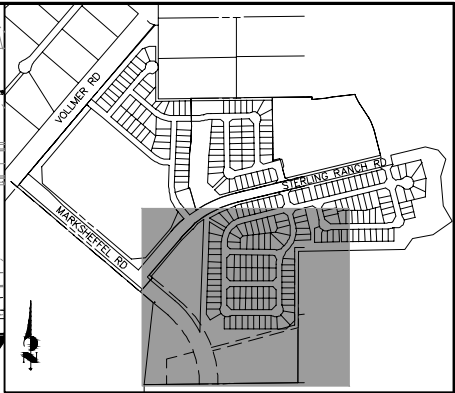
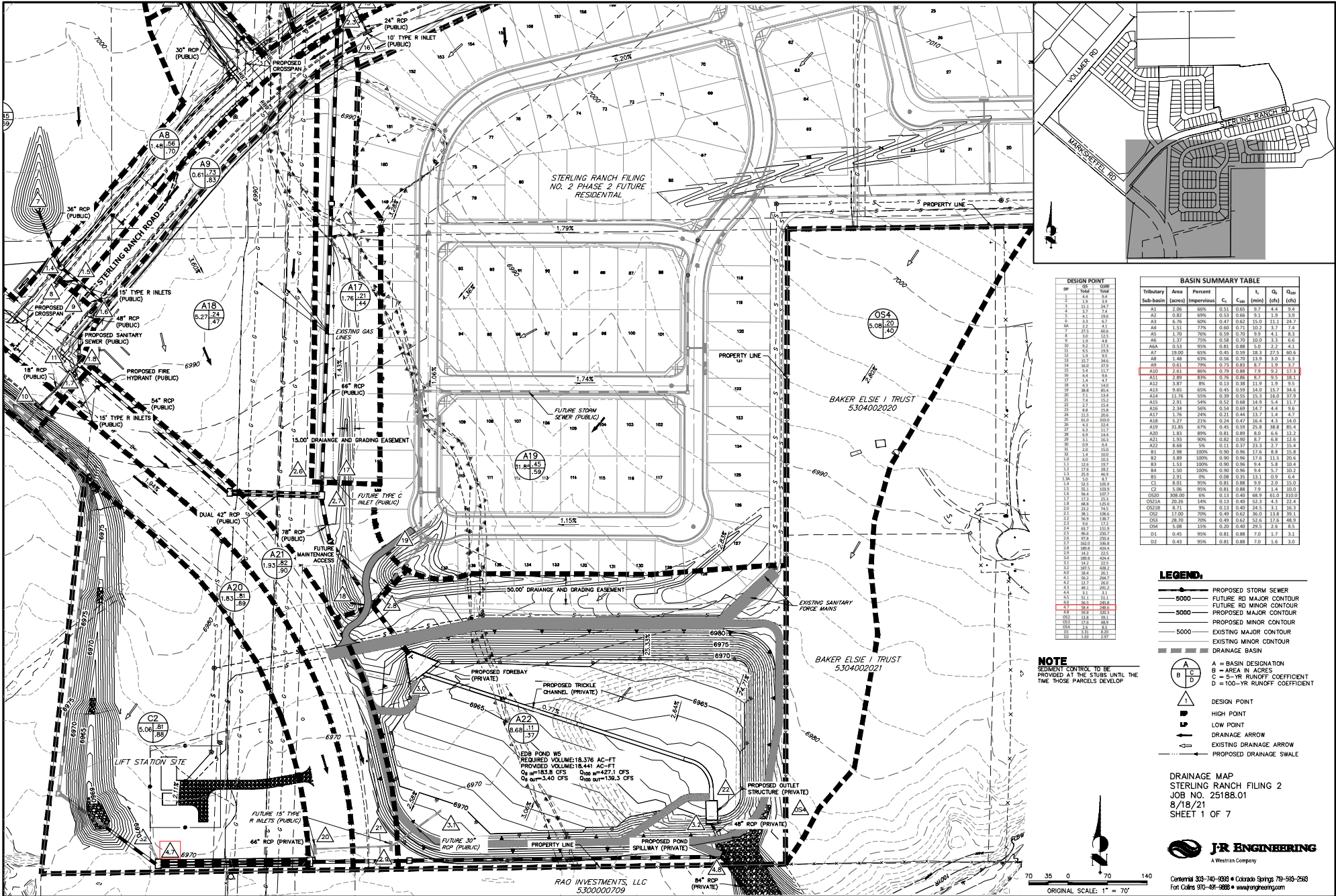
## INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



| Design Information (Input)  | CDOT Type R Curb Opening | MINOR         | MAJOR                    |       |
|---|--------------------------|---------------|--------------------------|-------|
| Type of Inlet   | CDOT Type R Curb Opening | Type =        | CDOT Type R Curb Opening |       |
| Local Depression (additional to continuous gutter depression 'a')                 |                          | $R_{LOCAL} =$ | 3.0                      | 3.0   |
| Total Number of Units in the Inlet (Grate or Curb Opening)                        |                          | No =          | 1                        | 1     |
| Length of a Single Unit Inlet (Grate or Curb Opening)                             |                          | $L_o =$       | 15.00                    | 15.00 |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)                    |                          | $W_o =$       | N/A                      | N/A   |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)                |                          | $C_{T-G} =$   | N/A                      | N/A   |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)         |                          | $C_{T-C} =$   | 0.10                     | 0.10  |
| <b>Street Hydraulics: OK - <math>Q &lt; Q_{allowable}</math> Street Capacity.</b> |                          |               |                          |       |
| Total Inlet Interception Capacity   |                          | $Q =$         | 8.7                      | 12.8  |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                                |                          | $Q_b =$       | 0.5                      | 4.5   |
| Capture Percentage = $Q_s/Q_o =$  |                          | C% =          | 94                       | 74    |
|   |                          |               |                          | %     |





| DESIGN POINT | C     |       | C50  |      | t <sub>c</sub> (hrs) | Q <sub>10</sub> (cfs) | Q <sub>50</sub> (cfs) |
|--------------|-------|-------|------|------|----------------------|-----------------------|-----------------------|
|              | Year  | Year  | Year | Year |                      |                       |                       |
| A6           | 1.48  | 1.56  | 1.70 |      |                      |                       |                       |
| A9           | 0.61  | 0.23  | 0.53 |      |                      |                       |                       |
| A17          | 1.70  | 2.1   | 2.4  |      |                      |                       |                       |
| A18          | 5.27  | 2.4   | 1.47 |      |                      |                       |                       |
| A19          | 11.85 | 4.5   | 1.59 |      |                      |                       |                       |
| A20          | 1.83  | 1.82  | 1.89 |      |                      |                       |                       |
| A21          | 1.83  | 1.82  | 1.89 |      |                      |                       |                       |
| A22          | 6.68  | 11.37 |      |      |                      |                       |                       |
| C2           | 5.06  | 1.81  | 1.85 |      |                      |                       |                       |

| BASIN SUMMARY TABLE |              |                    |                |                       |                      |                       |                       |
|---------------------|--------------|--------------------|----------------|-----------------------|----------------------|-----------------------|-----------------------|
| Tributary           | Area (acres) | Percent Impervious | C <sub>s</sub> | C <sub>50</sub> (min) | t <sub>c</sub> (hrs) | Q <sub>10</sub> (cfs) | Q <sub>50</sub> (cfs) |
| A1                  | 0.44         | 95%                | 0.51           | 0.52                  | 9.7                  | 0.2                   | 0.5                   |
| A2                  | 0.82         | 69%                | 0.53           | 0.66                  | 9.1                  | 1.9                   | 3.9                   |
| A3                  | 6.76         | 60%                | 0.47           | 0.62                  | 13.0                 | 11.1                  | 24.7                  |
| A4                  | 4.51         | 67%                | 0.46           | 1.31                  | 8.1                  | 7.4                   | 16.5                  |
| A5                  | 1.70         | 70%                | 0.59           | 0.70                  | 9.9                  | 4.1                   | 8.3                   |
| A6                  | 1.87         | 70%                | 0.58           | 0.68                  | 10.3                 | 3.1                   | 6.4                   |
| A6A                 | 0.33         | 95%                | 0.81           | 0.88                  | 5.0                  | 2.2                   | 4.1                   |
| A7                  | 19.00        | 60%                | 0.49           | 0.64                  | 13.7                 | 11.9                  | 27.0                  |
| A8                  | 1.48         | 63%                | 0.56           | 0.70                  | 13.9                 | 1.0                   | 6.3                   |
| A9                  | 0.61         | 79%                | 0.73           | 0.83                  | 8.7                  | 1.9                   | 3.7                   |
| A10                 | 2.63         | 60%                | 0.79           | 0.88                  | 7.9                  | 2.2                   | 3.9                   |
| A11                 | 2.89         | 87%                | 0.76           | 0.89                  | 8.7                  | 0.5                   | 1.8                   |
| A12                 | 3.97         | 8%                 | 0.33           | 0.41                  | 11.9                 | 1.9                   | 9.9                   |
| A13                 | 9.85         | 65%                | 0.45           | 0.59                  | 14.0                 | 15.7                  | 34.6                  |
| A14                 | 11.76        | 60%                | 0.48           | 0.61                  | 16.0                 | 16.0                  | 37.9                  |
| A15                 | 13.76        | 54%                | 0.52           | 0.68                  | 14.9                 | 16.0                  | 37.9                  |
| A16                 | 2.34         | 50%                | 0.54           | 0.69                  | 14.7                 | 4.4                   | 9.6                   |
| A17                 | 1.76         | 24%                | 0.71           | 0.84                  | 13.7                 | 2.4                   | 4.7                   |
| A18                 | 5.27         | 21%                | 0.24           | 0.27                  | 16.4                 | 4.3                   | 14.0                  |
| A19                 | 31.85        | 61%                | 0.45           | 0.59                  | 18.8                 | 22.3                  | 60.4                  |
| A20                 | 1.83         | 89%                | 0.81           | 0.89                  | 8.0                  | 6.6                   | 12.2                  |
| A21                 | 1.83         | 95%                | 0.82           | 0.90                  | 8.7                  | 6.8                   | 12.4                  |
| A22                 | 6.68         | 6%                 | 0.33           | 0.37                  | 13.3                 | 2.7                   | 15.4                  |
| B1                  | 2.96         | 100%               | 0.90           | 0.96                  | 17.6                 | 8.8                   | 15.8                  |
| B2                  | 3.89         | 100%               | 0.90           | 0.96                  | 17.6                 | 11.5                  | 20.6                  |
| B3                  | 1.53         | 100%               | 0.90           | 0.96                  | 9.4                  | 5.8                   | 10.4                  |
| B4                  | 1.50         | 100%               | 0.90           | 0.96                  | 9.4                  | 5.7                   | 10.2                  |
| B5                  | 2.31         | 10%                | 0.08           | 0.35                  | 13.1                 | 0.9                   | 6.4                   |
| C1                  | 8.01         | 95%                | 0.81           | 0.88                  | 9.9                  | 2.0                   | 15.0                  |
| C2                  | 5.06         | 95%                | 0.81           | 0.88                  | 7.9                  | 1.4                   | 10.0                  |
| CS20                | 308.00       | 9%                 | 0.13           | 0.40                  | 18.9                 | 61.0                  | 103.0                 |
| CS21A               | 79.26        | 4%                 | 0.13           | 0.40                  | 23.4                 | 4.1                   | 22.4                  |
| CS21B               | 8.71         | 9%                 | 0.13           | 0.40                  | 24.5                 | 1.1                   | 16.3                  |
| CS2                 | 37.00        | 9%                 | 0.13           | 0.40                  | 23.4                 | 4.1                   | 22.4                  |
| CS3                 | 28.70        | 70%                | 0.49           | 0.62                  | 15.6                 | 17.6                  | 48.3                  |
| CS4                 | 5.98         | 15%                | 0.20           | 0.25                  | 2.9                  | 2.8                   | 8.5                   |
| D1                  | 6.95         | 95%                | 0.81           | 0.88                  | 7.9                  | 1.4                   | 10.0                  |
| D2                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D3                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D4                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D5                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D6                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D7                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D8                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D9                  | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |
| D10                 | 0.43         | 95%                | 0.81           | 0.88                  | 7.0                  | 1.6                   | 3.0                   |

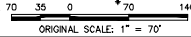
- LEGEND:**
- 5000 — PROPOSED STORM SEWER
  - 5000 — FUTURE RD MAJOR CONTOUR
  - 5000 — FUTURE RD MINOR CONTOUR
  - 5000 — PROPOSED MAJOR CONTOUR
  - 5000 — PROPOSED MINOR CONTOUR
  - 5000 — EXISTING MAJOR CONTOUR
  - 5000 — EXISTING MINOR CONTOUR
  - DRAINAGE BASIN
- NOTE:**  
 SEDIMENT CONTROL TO BE PROVIDED AT THE STUBS UNTIL THE TIME THOSE PARCELS DEVELOP
- DESIGN POINT**  
 A = BASIN DESIGNATION  
 B = AREA IN ACRES  
 C = 5-YR RUNOFF COEFFICIENT  
 D = 100-YR RUNOFF COEFFICIENT
- DESIGN POINT**  
 ▲ HIGH POINT  
 ▼ LOW POINT  
 → DRAINAGE ARROW  
 ← EXISTING DRAINAGE ARROW  
 → PROPOSED DRAINAGE SWALE

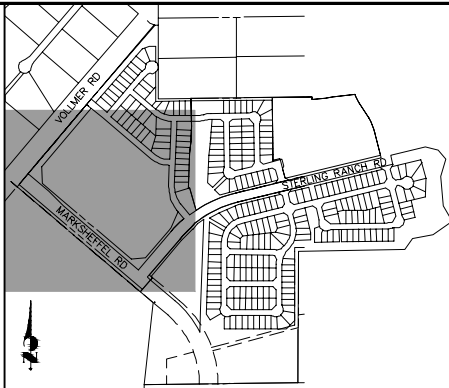
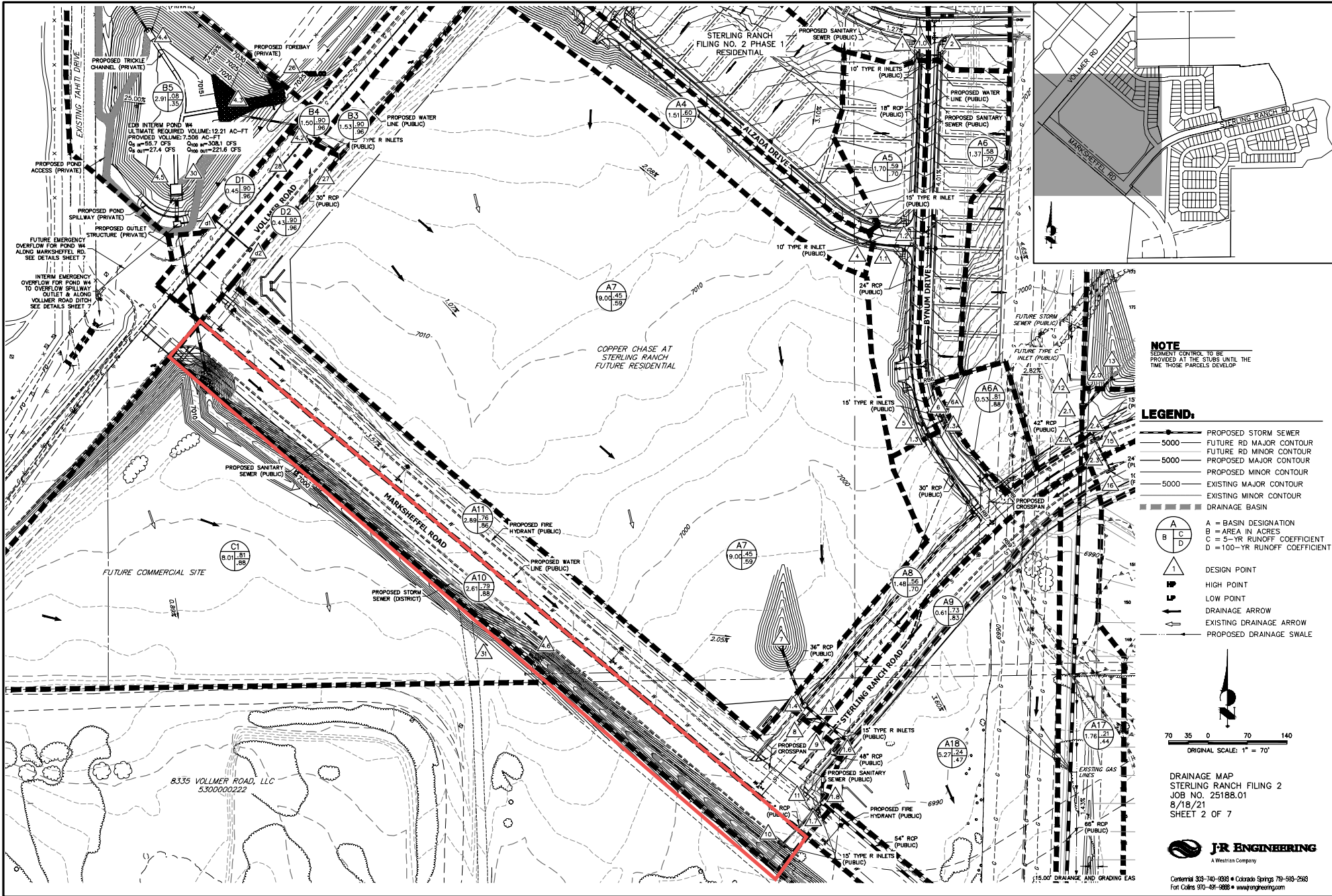
**DRAINAGE MAP**  
**STERLING RANCH FILING 2**  
**JOB NO. 25188.01**  
**8/18/21**  
**SHEET 1 OF 7**



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 Fort Collins 970-498-9888 • www.jrengineering.com

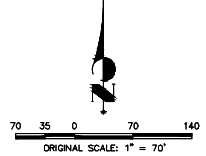
RAO INVESTMENTS, LLC  
 5300000709





**NOTE**  
 SEDIMENT CONTROL TO BE PROVIDED AT THE STUBS UNTIL THE TIME THOSE PARCELS DEVELOP

- LEGEND:**
- PROPOSED STORM SEWER
  - FUTURE RD MAJOR CONTOUR
  - FUTURE RD MINOR CONTOUR
  - PROPOSED MAJOR CONTOUR
  - PROPOSED MINOR CONTOUR
  - EXISTING MAJOR CONTOUR
  - EXISTING MINOR CONTOUR
  - DRAINAGE BASIN
- |   |   |   |   |
|---|---|---|---|
| A | B | C | D |
| 1 |   |   |   |
- A = BASIN DESIGNATION
  - B = AREA IN ACRES
  - C = 5-YR RUNOFF COEFFICIENT
  - D = 100-YR RUNOFF COEFFICIENT
- △ DESIGN POINT
  - ▽ HIGH POINT
  - ▽ LOW POINT
  - DRAINAGE ARROW
  - EXISTING DRAINAGE ARROW
  - PROPOSED DRAINAGE SWALE



DRAINAGE MAP  
 STERLING RANCH FILING 2  
 JOB NO. 25188.01  
 8/18/21  
 SHEET 2 OF 7



Callendar 333-740-9295 • Colorado Springs 719-589-2569  
 Fort Collins 970-591-9888 • www.jrengineering.com

EDB INTERIM POND W4  
 ULTIMATE REQUIRED VOLUME: 12.21 AC-FT  
 PROVIDED VOLUME: 7.509 AC-FT  
 C<sub>5</sub> = 59.7 CFS  
 C<sub>100</sub> = 27.4 CFS  
 Q<sub>100</sub> = 308.1 CFS  
 Q<sub>100</sub> = 221.6 CFS

8335 VOLLMER ROAD, LLC  
 5300000222

COPPER CHASE AT  
 STERLING RANCH  
 FUTURE RESIDENTIAL

FUTURE STORM  
 SEWER (PUBLIC)  
 FUTURE TYPE C  
 INLET (PUBLIC)

15.00' DRAINAGE AND GRADING EAS



**ENTECH**  
ENGINEERING, INC.

505 ELKTON DRIVE  
COLORADO SPRINGS, CO 80907  
PHONE (719) 531-5599

**SOILS AND GEOLOGY STUDY  
LOT 1, STERLING RECYCLING FACILITY  
PARCEL NO. 53000-00-743  
COLORADO SPRINGS, COLORADO**

Prepared for:  
**Rhetoric LLC  
20 Boulder Crescent  
Colorado Springs, CO 80903**

Attn: Chaz Collins

August 17, 2023

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Logan L. Langford, P.G.  
Geologist

LLL

Reviewed by:



Joseph C. Goode Jr., P.E.  
President

## 5.5 Groundwater

Groundwater was encountered in TB-1 and TB-2 at depths of 4 to 5 feet. TB-3 which was drilled to 20 feet was dry. Fluctuation in groundwater conditions may occur due to variations in rainfall and other factors not readily apparent at this time. It should be noted that in the sandy materials on-site, some groundwater conditions might be encountered due to the variability in the soil profile. Isolated sand and gravel layers within the soils, sometimes only a few feet in thickness and width, can carry water in the subsurface. Groundwater may also flow on top of the underlying bedrock. Builders and planners should be cognizant of the potential for the occurrence of such subsurface water features during construction on-site and deal with each individual problem as necessary at the time of construction.

## 6 ENGINEERING GEOLOGY – IDENTIFICATION AND MITIGATION OF GEOLOGIC HAZARDS

Geologic mapping has been performed on this site to produce an Engineering Geology Map Figure 7. This map shows the location of various geologic conditions of which the developers should be cognizant during the planning, design and construction stages of the project. These hazards and the recommended mitigation techniques are as follows:

### Artificial Fill – Constraint

These are areas of man-made fill associated with past quarry operations and fill dumped across the site, in addition to the asphalt, concrete, and soil piles associated with the Sterling Recycling Facility. Fill was encountered in the test borings at depths of 3 to 5 feet. Fill depths are variable across the site and test pits and or additional test borings in the building areas are recommended once development plans are finalized.

Mitigation: The fill on this site is considered uncontrolled for construction purposes. Any uncontrolled fill encountered beneath foundations will require removal and recompaction at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557.

### Collapsible Soils – Constraint

The majority of the soils encountered on-site do not exhibit collapsible characteristics, however, areas of loose soils were encountered in the test borings drilled on site. Additionally, areas mapped as Qes (eolian sand) have the potential for hydrocompaction (Reference 7, Figure 5).

Mitigation: Should loose or collapsible soils be encountered beneath foundations, recompaction and moisture conditioning of the upper 2 feet of soil at 95% of its maximum Modified Proctor Dry

Density ASTM D-1557 will be required. Exterior flatwork and parking areas may also experience movement. Proofrolling and recompaction of soft areas should be performed during site work.

#### Expansive Soils – Constraint

Expansive soils were encountered in the test borings at depths of 11 to 15 feet. These occurrences are typically sporadic; therefore, none have been indicated on the maps. The clays and claystone, if encountered at foundation grade, can cause differential movement in structures. These occurrences should be identified and dealt with on an individual basis.

Mitigation Should expansive soils be encountered beneath foundations; mitigation will be necessary. Mitigation of expansive soils will require special foundation design. Overexcavation 3 to 5 feet and replacement with non-expansive soils at a minimum of 95% of its maximum Modified Proctor Dry Density, ASTM D-1557 is a suitable mitigation, which is common in the area. Floor slabs on expansive soils should be expected to experience movement. Overexcavation and replacement has been successful in minimizing slab movements. The use of structural floors should be considered for basement construction on highly expansive clays. Final recommendations should be determined after additional investigation of each building site.

#### Shallow Bedrock – Constraint

Areas of shallow bedrock were encountered (TB-3 previously completed on the site encountered bedrock at a depth of 1 foot, Reference 4, Appendix D). A Summary of the Depth to Bedrock is included in Table B-1. Shallow bedrock will be encountered in some areas of this site. Where claystone or sandstone are encountered, excavation/grading may be difficult requiring track-mounted excavators. Bedrock will likely be encountered cuts for utility excavations.

#### Groundwater and Floodplain Areas – Constraint

The site is not mapped within floodplain zones according to the FEMA Map No. 08041CO533G, Figure 8 (Reference 7). No drainages were observed on the site, however, an area of ponded water was observed in the northeastern portion of the site. These areas are discussed as follows:

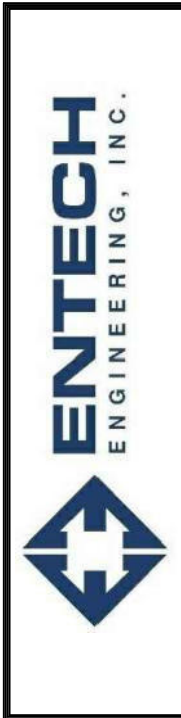
#### Potential Seasonally Shallow Groundwater Area – Constraint

In these areas, we would anticipate the potential for periodically high subsurface moisture conditions, frost heave potential and highly organic soils. These areas are primarily located in the eastern half of the site where groundwater was encountered at depths of 4 to 5 feet in the test borings. Preliminary grading plans available at the time of this investigation, indicate that this area is to be filled during site grading. A minimum separation of 3 feet between foundation components and groundwater levels are recommended.

# LOT 1, STERLING RECYCLING FACILITY

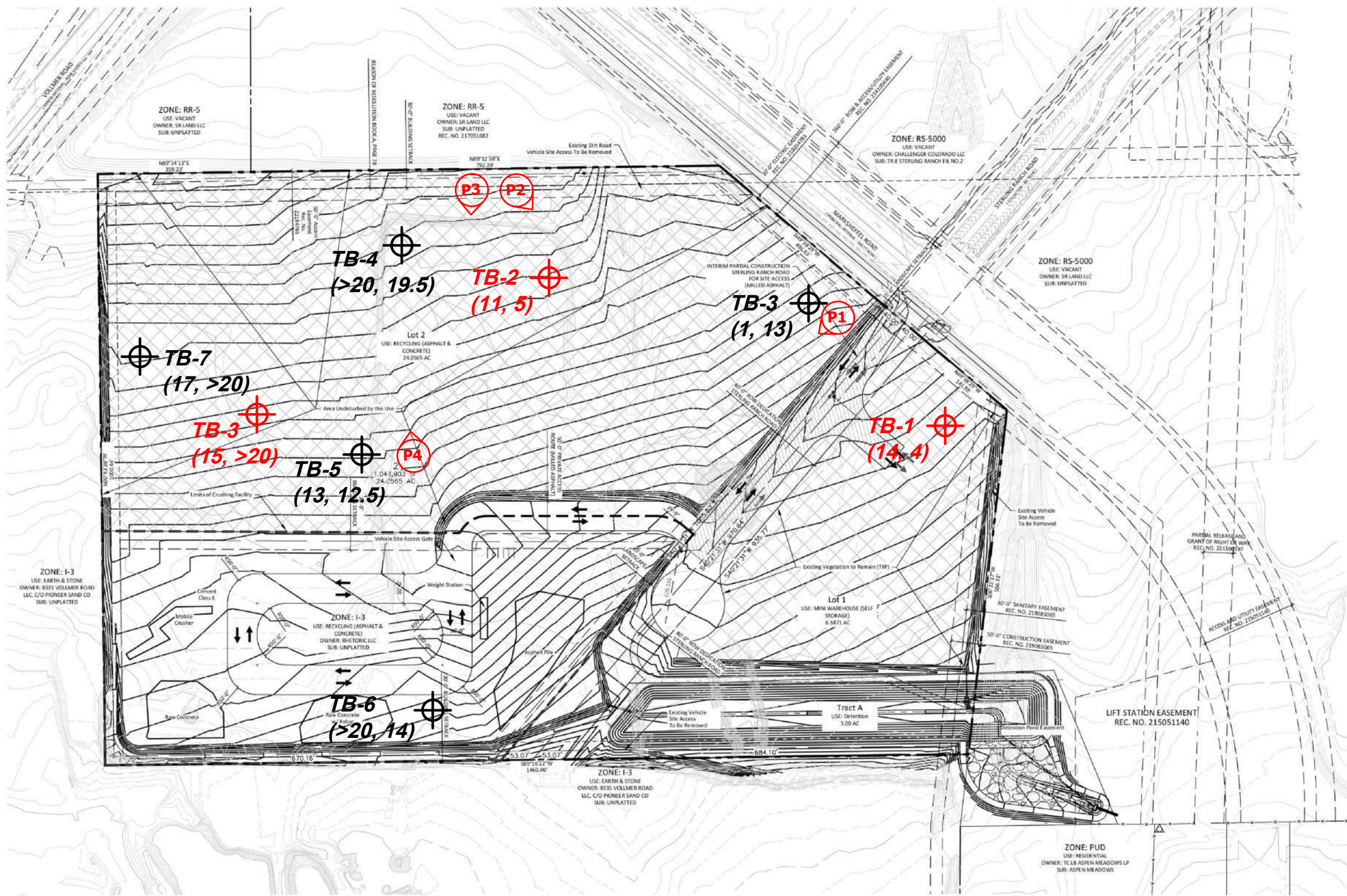
SECTION 5 IN TOWNSHIP 12 SOUTH RANGE 65 WEST OF THE 6TH PRINCIPAL MERIDIAN EL PASO COUNTY, CO  
SITE DEVELOPMENT PLAN

| REVISION | BY |
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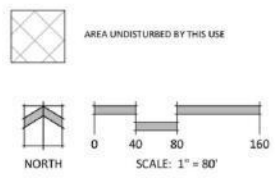


**SITE PLAN/TESTING LOCATION MAP**  
 LOT 1, STERLING RECYCLING FACILITY  
 EL PASO COUNTY, COLORADO  
 RHETORIC LLC

JOB NO.  
 231252  
**FIG. 3**



- ⊕ - APPROXIMATE TEST BORING LOCATION AND NUMBER (BEDROCK, GROUNDWATER DEPTHS FT.) EEI JOB NO. 231252
- ⊕ - APPROXIMATE TEST BORING LOCATION AND NUMBER (BEDROCK, GROUNDWATER DEPTHS FT.) EEI JOB NO. 220402
- P1 - APPROXIMATE PHOTOGRAPH LOCATION AND NUMBER

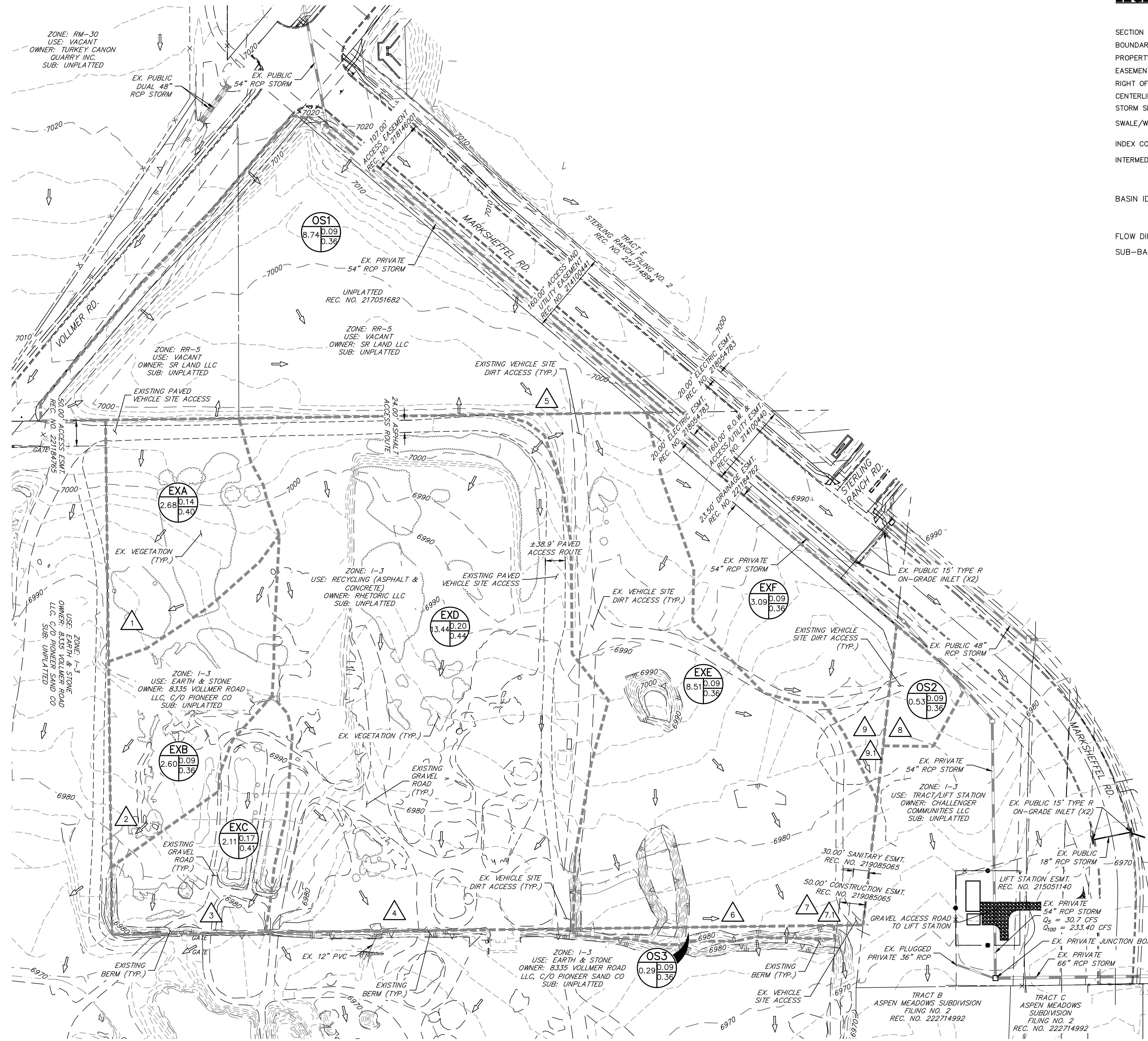


## **Appendix E**

### **Drainage Maps**

# STERLING RANCH RECYCLING FACILITY

## EXISTING DRAINAGE MAP



### LEGEND

|                          | EXISTING | PROPOSED |
|--------------------------|----------|----------|
| SECTION LINE             | -----    | -----    |
| BOUNDARY LINE            | -----    | -----    |
| PROPERTY LINE            | -----    | -----    |
| EASEMENT LINE            | -----    | -----    |
| RIGHT OF WAY             | -----    | -----    |
| CENTERLINE               | -----    | -----    |
| STORM SEWER              | -----    | -----    |
| SWALE/WATERWAY FLOWLINE  | -----    | -----    |
| INDEX CONTOUR            | -----    | -----    |
| INTERMEDIATE CONTOUR     | -----    | -----    |
| BASIN ID                 |          |          |
| DESIGN POINT DESIGNATION |          |          |
| FLOW DIRECTION           |          |          |
| SUB-BASIN DRAINAGE AREA  | -----    | -----    |

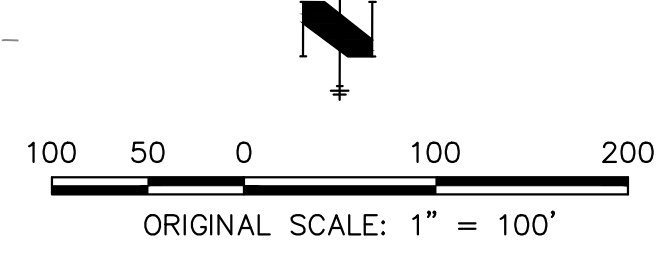
#### BASIN SUMMARY TABLE

| Tributary Sub-basin | Area (acres) | Percent Impervious | C <sub>s</sub> | C <sub>100</sub> | t <sub>c</sub> (min) | Q <sub>s</sub> (cfs) | Q <sub>100</sub> (cfs) |
|---------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| EXA                 | 2.68         | 8%                 | 0.14           | 0.40             | 21.1                 | 1.1                  | 5.4                    |
| EXB                 | 2.60         | 2%                 | 0.09           | 0.36             | 25.9                 | 0.6                  | 4.3                    |
| EXC                 | 2.11         | 14%                | 0.17           | 0.41             | 22.4                 | 1.0                  | 4.3                    |
| EXD                 | 13.44        | 17%                | 0.20           | 0.44             | 23.4                 | 7.6                  | 28.1                   |
| EXE                 | 8.51         | 2%                 | 0.09           | 0.36             | 27.7                 | 2.0                  | 13.4                   |
| EXF                 | 3.09         | 2%                 | 0.09           | 0.36             | 24.1                 | 0.8                  | 5.2                    |
| OS1                 | 8.74         | 2%                 | 0.09           | 0.36             | 49.4                 | 1.4                  | 9.2                    |
| OS2                 | 0.53         | 2%                 | 0.09           | 0.36             | 15.8                 | 0.2                  | 1.1                    |
| OS3                 | 0.29         | 2%                 | 0.09           | 0.36             | 5.0                  | 0.2                  | 0.9                    |

#### DESIGN POINT

| DP  | Q5    |       | Q100  |       |
|-----|-------|-------|-------|-------|
|     | Total | Total | Total | Total |
| 1   | 1.1   | 5.4   |       |       |
| 2   | 0.6   | 4.3   |       |       |
| 3   | 1.0   | 4.3   |       |       |
| 4   | 7.6   | 28.1  |       |       |
| 5   | 1.4   | 9.2   |       |       |
| 6   | 0.2   | 0.9   |       |       |
| 7   | 2.0   | 13.4  |       |       |
| 7.1 | 2.8   | 18.3  |       |       |
| 8   | 0.2   | 1.1   |       |       |
| 9   | 0.8   | 5.2   |       |       |
| 9.1 | 0.9   | 6.1   |       |       |

PCD FILE NO. PPR2341 & SF2325  
 STERLING RANCH RECYCLING FACILITY  
 EXISTING DRAINAGE MAP  
 JOB NO. 25188.14  
 01/19/2024  
 SHEET 1 OF 1



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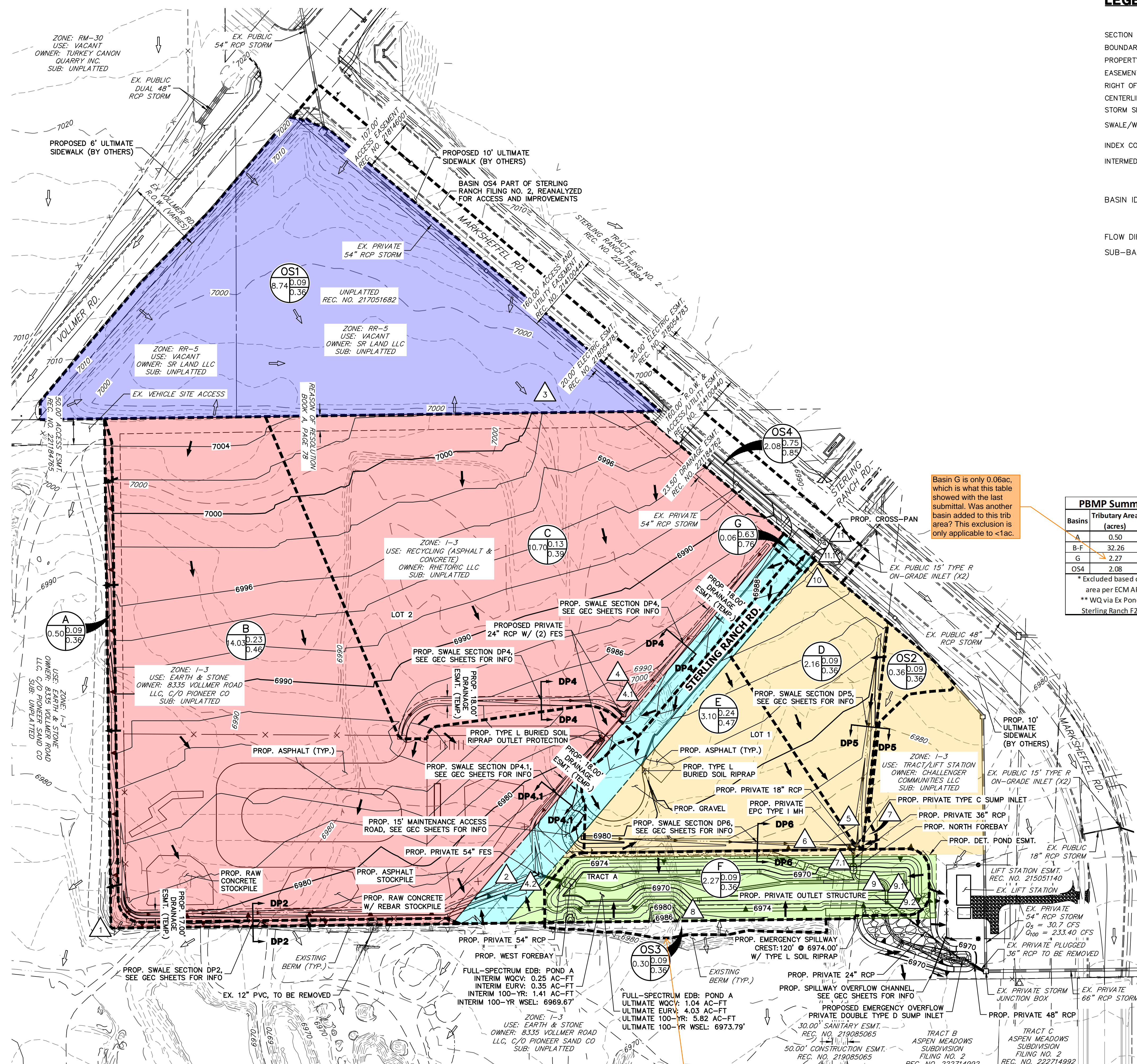
# STERLING RANCH RECYCLING FACILITY PROPOSED DRAINAGE MAP

## LEGEND

|                          | EXISTING | PROPOSED |
|--------------------------|----------|----------|
| SECTION LINE             | ---      | ---      |
| BOUNDARY LINE            | ---      | ---      |
| PROPERTY LINE            | ---      | ---      |
| EASEMENT LINE            | ---      | ---      |
| RIGHT OF WAY             | ---      | ---      |
| CENTERLINE               | ---      | ---      |
| STORM SEWER              | ---      | ---      |
| SWALE/WATERWAY FLOWLINE  | ---      | ---      |
| INDEX CONTOUR            | ---      | ---      |
| INTERMEDIATE CONTOUR     | ---      | ---      |
| BASIN ID                 |          |          |
| DESIGN POINT DESIGNATION |          |          |
| FLOW DIRECTION           |          |          |
| SUB-BASIN DRAINAGE AREA  |          |          |

## ULTIMATE LAND USE LEGEND

|  |  |
|--|--|
| INDUSTRIAL—HEAVY AREAS<br>(90% IMPERVIOUS)                       |  |
| BUSINESS COMMERCIAL AREAS<br>(90% IMPERVIOUS)                    |  |
| RESIDENTIAL—1/8 ACRE OR LESS<br>(65% IMPERVIOUS)                 |  |
| NON-RESIDENTIAL COLLECTOR—80' R.O.W.<br>(100% AND 2% IMPERVIOUS) |  |
| HISTORICAL ANALYSIS<br>(2% IMPERVIOUS)                           |  |



Basin G is only 0.06ac, which is what this table showed with the last submittal. Was another basin added to this tributary area? This exclusion is only applicable to <1ac.

### PBMP Summary Table

| Basins | Tributary Area (acres) | PBMP       |
|--------|------------------------|------------|
| A      | 0.50                   | Excluded*  |
| B-F    | 32.26                  | Pond A     |
| G      | 2.27                   | Excluded** |
| OS4    | 2.08                   | Excluded** |

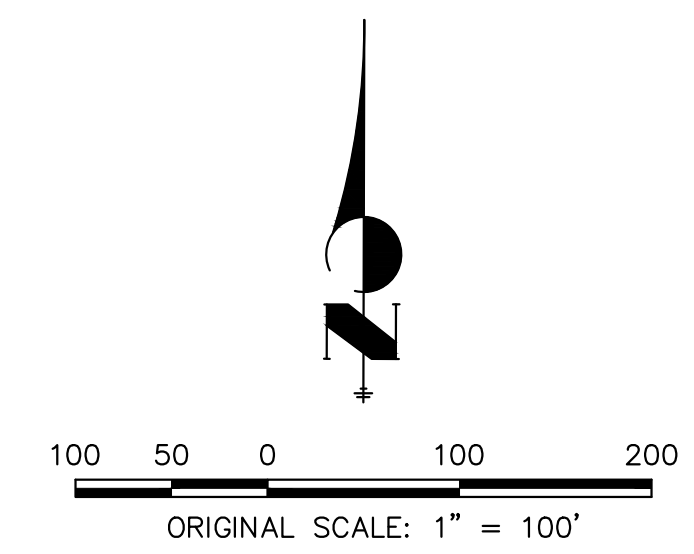
\* Excluded based on <1 acres of area per ECM APP. 1.7.C.1.a  
\*\* WQ via Ex Pond W-5 within Sterling Ranch F2 (SF-20-015)

### BASIN SUMMARY TABLE

| Tributary Sub-basin | Area (acres) | Percent Impervious | C <sub>s</sub> | C <sub>100</sub> | t <sub>c</sub> (min) | Q <sub>s</sub> (cfs) | Q <sub>100</sub> (cfs) |
|---------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| A                   | 0.50         | 2%                 | 0.09           | 0.36             | 5.0                  | 0.3                  | 1.6                    |
| B                   | 14.03        | 19%                | 0.23           | 0.46             | 34.1                 | 7.4                  | 25.1                   |
| C                   | 10.70        | 6%                 | 0.13           | 0.39             | 28.6                 | 3.4                  | 17.7                   |
| D                   | 2.16         | 2%                 | 0.09           | 0.36             | 24.1                 | 0.5                  | 3.7                    |
| E                   | 3.10         | 22%                | 0.24           | 0.47             | 22.8                 | 2.2                  | 7.1                    |
| F                   | 2.27         | 2%                 | 0.09           | 0.36             | 18.5                 | 0.6                  | 4.4                    |
| G                   | 0.06         | 67%                | 0.63           | 0.76             | 5.3                  | 0.2                  | 0.4                    |
| OS1                 | 8.74         | 2%                 | 0.09           | 0.36             | 49.4                 | 1.4                  | 9.2                    |
| OS2                 | 0.36         | 2%                 | 0.09           | 0.36             | 16.5                 | 0.1                  | 0.7                    |
| OS3                 | 0.30         | 2%                 | 0.09           | 0.36             | 5.0                  | 0.2                  | 1.0                    |
| OS4                 | 2.08         | 82%                | 0.75           | 0.85             | 9.0                  | 6.7                  | 12.8                   |

### DESIGN POINT

| DP   | Q5    |       | Q100  |       |
|------|-------|-------|-------|-------|
|      | Total | Total | Total | Total |
| 1    | 0.3   | 1.6   |       |       |
| 2    | 7.4   | 25.1  |       |       |
| 3    | 1.4   | 9.2   |       |       |
| 4    | 3.4   | 17.7  |       |       |
| 4.1  | 3.7   | 21.1  |       |       |
| 4.2  | 9.3   | 40.1  |       |       |
| 5    | 0.5   | 3.7   |       |       |
| 6    | 2.2   | 7.1   |       |       |
| 7    | 0.1   | 0.7   |       |       |
| 7.1  | 2.8   | 11.2  |       |       |
| 8    | 0.2   | 1.0   |       |       |
| 9    | 0.6   | 4.4   |       |       |
| 9.1  | 11.4  | 49.4  |       |       |
| 9.2  | 0.1   | 8.3   |       |       |
| 10   | 0.2   | 0.4   |       |       |
| 11   | 6.7   | 12.8  |       |       |
| 11.1 | 6.9   | 13.1  |       |       |



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PROPOSED DRAINAGE MAP  
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I believe we previously discussed on the phone or via email that the CSU Easement should be shown on these plans, since it is unclear how that will be accessed once this pond is installed (as shown on this plan).