

Apex Waste Solutions Final Drainage Report

El Paso County, Colorado

October 2024

Completed By:

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APPENDIX



STATEMENT SHEET

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Brett Louk, P.E. #_____

Developer's Statement:

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Scott Lukach, President

Owner: <u>Apex Waste Solutions, Scott Lukach - President</u>

Address: 11681 Progress Lane

Parker, CO 80134

El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended

Joshua Palmer, P.E. County Engineer

Conditions:



Engineer stamp, date and sign Owner sign and date

Date

2

Date

Date

1. GENERAL LOCATION AND DESCRIPTION

The owner of 560 and 570 Air Lane has asked SMH Consultants, P.A. (SMH) to conduct a stormwater drainage analysis for the proposed Apex Waste Solutions site improvements to satisfy the El Paso County drainage criteria manual requirements. This analysis will determine potential impacts resulting from expanding the existing asphalt millings parking lot and replacing the existing modular office building with two new modular office buildings.

a. Development Location

The property is located in the SE and SW ¼ of Section 8, Township 14 South, Range 65 West in El Paso County, Colorado. The site is currently platted as lots 4 and 5 of the Hillcrest Acres Subdivision. The site is 7.6-acres in size and consists of existing asphalt millings parking lot, a modular office unit, and shipping containers used as storage. The lot is bordered by commercial and industrial properties on all sides. The site is zoned I-2 (light industrial). The lots are also located within an Airport Overlay (CAD-O) district. The site is accessed via the public road Air Lane. A vicinity map of the site and adjacent properties has been included in the appendix of this report.

b. Description of Property

The existing site consists of an asphalt millings parking lot, shipping containers being used as storage, outdoor storage, and a modular office unit. A majority of the site is covered with native vegetation, including light grasses, shrubs, and some trees. With this site plan, approximately 1.62 acres will be disturbed for an improved asphalt millings parking lot, two trailers to be used for office and operations space, and a proposed sand filter basin.

Based on a Custom Soil Resource Report, obtained from the USDA NRCS Web Soil Survey (accessed April 18, 2024) for the site, the native soil consists of *Blakeland loamy sand* with slopes ranging from 1-9 percent. This native soil is classified in Hydrologic Soil Group A. Group A soils are typically classified as a well-drained soil, with a low runoff class. The Custom Soil Report is included in the appendix of this report.

The nearest major drainageway is Sand Creek, which is located approximately 0.7 miles west of the site. Sand Creek travels southwest until it joins Fountain Creek, which continues to travel south.

2. DRAINAGE BASINS AND SUB-BASINS

a. Major Basin Descriptions

The subject site is entirely in the Peterson Field drainage basin. The Peterson Field drainage basin was studied as part of the Peterson Field Drainage Master Plan prepared by URS/NES and approved on December 11, 1985. The project is in line with the results from the Drainage Basin Planning Study. Runoff from the site historically flowed south along historic drainage routes towards the existing Peterson Field Regional Detention Ponds #1 and #2. Proposed



runoff on the site will now be detained via an on-site sand filter basin. Because of the existing topography of the site and lack of adjacent storm sewer infrastructure to connect to, there are no outlet structures proposed for the sand filter basin. Runoff on the site will now be detained in the basin and leave the site through subsurface infiltration. This will slightly reduce the total inflow to Peterson Field Regional Detention Ponds #1 and #2.

b. Sub-Basin Descriptions

Because the site is infiltrating storms greater than the WQCV please provide proof of approval from the state that the project site has the water rights to do so.

Offsite Drainage Area OS-1 is approximately 2.84 acres located north and east of the site. Stormwater runoff flows south onto the site at slopes ranging from 3-25 percent and flows along existing terrain patterns to EX-1. OS-1 consists of both native vegetation and paved roads. This sub-basin has existing 5-yr and 100-yr flows of 1.92 cfs and 8.28 cfs, respectively.

EX-1 is approximately 7.60 acres and contains the extents of the site. Stormwater runoff flows south/southwest at slopes ranging from 4-6 percent and flows along existing terrain patterns to Design Point 1 south of the site. EX-1 receives offsite runoff from sub-basin OS-1. EX-1 consists of native vegetation, sand/gravel areas, an office trailer and storage containers, and asphalt millings. This sub-basin has existing 5-yr and 100-yr flows of 6.55 cfs and 21.54 cfs, respectively.

Existing Design Point 1 (DP-1) has 5-yr and 100-yr flows of 7.76 cfs and 26.68 cfs, respectively.

3. DRAINAGE DESIGN CRITERIA

a. Development Criteria Reference

Pre- and post-development drainage characteristics were reviewed, studied, and analyzed using the *El Paso County Drainage Criteria Manual Volumes 1 and 2*, Federal Emergency Management Agency's Flood Insurance Rate Map and USDA NRCS Web Soil Survey.

b. Hydrologic Criteria

Hydrology calculations in this report were performed following the methodologies outlined in the El Paso County Engineering Criteria Manual and the El Paso County Drainage Criteria Manual (DCM) Volumes 1 and 2. Drainage characteristics were delineated based on existing topographic information from surface LIDAR data and USGS topographical maps. The existing and proposed drainage maps have been included in the appendix of this report.

Since the watershed area encompassing the development site is less than 100 acres, the Rational Method was used to determine peak flows for the 5-year and 100-year storm events. Weighted C values were determined for each drainage area within the proposed site based on the amount of impervious and pervious areas. A runoff coefficient (C) was chosen from Table 6-6 of the *El Paso County Drainage Criteria Manual, Volume 1 update*. As mentioned earlier, the site consists of Hydrological Soil Group A. The Weighted C values are shown in the



appendix of this report.

The time of concentration was calculated for each drainage area based off methods found in Chapter 6, Section 3.2 of the *El Paso County Drainage Criteria Manual, Volume 1 update.* The first 100 feet of unconcentrated overland flow time was calculated and added to the subsequent channelized flow times. Channelized flow times were calculated using channel flow time equation. All onsite and offsite sub-basins were analyzed under developed flow conditions. All times of concentration for the existing and proposed sub-basins have been included in the appendix of this report.

Rainfall intensity was calculated for each drainage area based off methods found in Chapter 6, Section 3.3 of the *El Paso County Drainage Criteria Manual, Volume 1 update.* The intensity value for each basin was determined using the equations from Figure 6-5. Each drainage area's time of concentration was used to determine the respective intensity. All rainfall intensity calculations for existing and proposed sub-basins have been included in the appendix of this report.

4. DRAINAGE FACILITY DESIGN

a. General Concept

Proposed improvements to the site include enlarging the existing asphalt millings parking area and adding two new 24'x56' modular units to be used as an office and operations area. The existing shipping containers on-site will remain, however, the existing modular unit in the southeast corner of the site will be removed. The C-values for the site will increase due to the addition of impervious area. All offsite flow will be allowed to enter the site as it currently does. The 5-year and 100-year runoff calculations for the proposed site can be seen in the appendix.

Drainage Area P-1 is approximately 7.60 acres and contains the extents of the site. Stormwater flows south/southwest at slopes ranging from 4-6 percent and flows along existing terrain patterns to Design Point 1 in the southwest corner of the site. P-1 receives offsite runoff from sub-basin OS-1. The planned improvements for this sub-basin include expansion of an asphalt millings parking lot and driveway and two new modular units. This sub-basin has proposed 5-year and 100-year flows of 8.62 cfs and 25.10 cfs, respectively.

Proposed Design Point 1 (DP-1) has 5-yr and 100-yr flows of 9.93 cfs and 31.46 cfs, respectively.

Table 1 below shows a comparison between existing and proposed runoff rates at Design Point 1.



Design Point Summary										
Design Point	Area (ac)	Q5 (cfs)	Q100 (cfs)							
DP-1 (Existing)	10.44	7.76	26.68							
DP-1 (Proposed)	10.44	9.93	31.46							

Table 1. Existing and Proposed Design Point Summary

To address the increase in runoff from the site, a full-infiltration sand filter basin has been designed to provide water quality treatment and detention up to the 100-yr storm. The proposed sand filter basin will be 4.5 feet in depth, with the top of the filter media at an elevation of 6294.50' and a top of basin elevation of 6299.00'. The minimum filter surface area and design volume per the El Paso County Drainage Criteria Manual are 1,322 sq. ft and 3,964 cu. ft., respectively. The minimum filter surface area and design volume are specified for basins that treat and store the WQCV only, while the proposed basin will treat and store up to the 100-year event. The proposed sand filter basin will be approximately 14,150 sq. ft. in size, and have a filter surface area of 6710 sq. ft. The proposed basin will have approximately 46,165 cu. ft. of total storage throughout the full depth of the basin. The filter media will be 18 inches in thickness. The WOCV and EURV for the basin are 0.091 and 0.204 acre-feet, respectively. The water surface elevation for the WQCV and 100-year events are 6295.06' and 6297.70', respectively. The sand filter basin will have a spillway crest on the south side, with an elevation of 6297.75'. The spillway crest length is approximately 30.0 feet, 4:1 side slopes, and a design flow depth of 0.47 feet at 31.46 cfs. All runoff beyond the 100-year event will leave the sand filter basin and travel south along historic drainage paths. Percolation tests were performed on the existing soils in the proposed location of the sand filter basin and show the infiltration rate to be 1.5 in/hr. Calculations for the water surface elevations, runoff volumes, and percolation testing can be seen in the appendix of this report.

5. FOUR STEP PROCESS

Clarify change in discharge point. The existing and proposed discharge points appear different so this sentence does not appear accurate based on the drainage maps.

El Paso County requires a four-step process for stormwater quality management: reducing runoff volumes, treating the water quality capture volume, stabilizing streams, and implementing long-term source controls. These steps are further outlined in Volumes 1 and 2 of the County's Drainage Criteria Manual.

Step 1: Employ Runoff Reduction Practices. The site has been designed so that runoff flows over vegetated areas prior to entering the sand filter basin and eventually leaving the site. This will minimize directly connected impervious areas within the site. The site will also have a full-infiltration sand filter basin that will help reduce runoff from the site.

Step 2: Implement BMPs that Provide Water Quality Capture Volume (WQCV) with Slow Release. A sand filter basin has been designed for the site to provide water quality capture volume and detention volume. Since there is no underground storm sewer adjacent to the site, the sand filter basin was designed as a full-infiltration section. To confirm the infiltration capacity of the existing soils onsite, Entech Engineering was hired to perform percolation tests in the area of the planned sand filter basin. These tests were completed on September 19, 2024 and show the existing soil has an infiltration rate of 1.5 in/hr. Based on this infiltration rate, and the site runoff characteristics, the sand filter basin was designed to have



Per MHFD Criteria for full infiltration systems the control measure should be approximately 3 feet or more above groundwater levels. Discuss if this site characteristic is met.

a minimum filter surface area of 6710 sq. ft., side slopes of 4:1, and a maximum ponding depth of 3.20'. The bottom of the sand filter basin will be at an elevation of 6294.50' and the top, including 1' of freeboard, will be at an elevation of 6299.00'. The WQCV water surface elevation is at 6295.06' and the 100-year water surface elevation is at 6297.70'. When fullinfiltration sections are used for WQCV and detention, minimum drain times are not applicable. Full-infiltration permanent control measures must be designed to drain fast enough to meet the required drain times for Colorado water rights. Because full-infiltration permanent control measures tend to drain slower than the original design rates, a safety factor of 2 is applied for the EURV and WQCV drain rates. The EURV must be designed to drain in a maximum of 36 hours and the WQCV must be designed to drain in a maximum of 20 hours. The sand filter basin for this site has an EURV and WQCV drain rate of 93 and 4.4 hours, respectively. With an applied safety factor of 2, the sand filter basin has EURV and WQCV drain rates of 18.6 and 8.8 hours, respectively. All calculations for the sand filter basin, and percolation testing, can be seen in the appendix of this report.

Step 3: Stabilize Drainageways. Since runoff from the site is being detained and infiltrated into the soil, runoff leaving the site will be decreased from historical rates. This, coupled with MHFD. It the existing vegetated swale on the adjacent property to the south, provides a stabilized outfall for runoff from the site. Runoff flows down the vegetated swale to a roadside ditch along Space Village Ave., through a culvert under Space Village Ave., over undeveloped land and vegetated land until it ultimately ends up in the regional detention pond on Peterson below, but Air Force Base. Because of the path runoff takes, no downstream drainageway improvements please clarify are required.

Step 4: Implement Site Specific and Other Source Control BMPs. Soil erosion control measures will be implemented during improvements of the parking lot and site. Erosion control measures such as silt fence and vehicle tracking control will be utilized to reduce the disturbance of existing soil and vegetation during construction. The full soil erosion control measures to be utilized during construction of the site are shown in the erosion control plan for the site development plans.

6. FLOODPLAIN STATEMENT

No portion of the site is located within a 100-year floodplain as determined by the Flood Insurance Rate Map (FIRM) number 08041C0754G effective date December 7, 2018. The corresponding FEMA flood map can be seen in the appendix.

7. DRAINAGE BASIN FEES

The site is located entirely within the Peterson Field Drainage Basin. The total amount of disturbance in the Peterson Field Drainage Basin is 1.62 acres. Since the property has been previously platted, no drainage basin fees are required.

> Add engineer estimate for SFB design cost to match FAE.



The SFB sizing should be based on a WQCV drain time of 12 hours per appears this is met based on results stated this sentence.

8. SUMMARY

A drainage analysis was conducted for the proposed parking lot expansion and site improvements to the 7.6-acre industrial site located at 560 & 570 Air Lane. The site is located in the Peterson Field drainage basin. Based on the analysis, the 5-year & 100-year post-development stormwater peak flow rates will be slightly higher than the pre-developed stormwater peak flow rates. A sand filter basin will be implemented into the site to capture and infiltrate runoff generated from the proposed site. Runoff will no longer leave the site through historic drainageways. Development of the site should not adversely impact surrounding or downstream properties.

Design and statement must indicate "will not adversely impact".



References

El Paso County Assessor (2020). *El Paso County Assessor's Real Property Search*. Retrieved from: <u>https://www.elpasoco.com/search-el-paso-county/</u>

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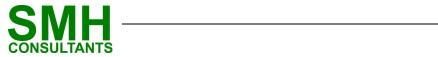
United States Department of Agriculture Natural Resources Conservation Service (2024, April 17). *Web Soil Survey*. Retrieved from: <u>https://websoilsurvey.sc.egov.usda.gov/App/WebSoilSurvey.aspx</u>

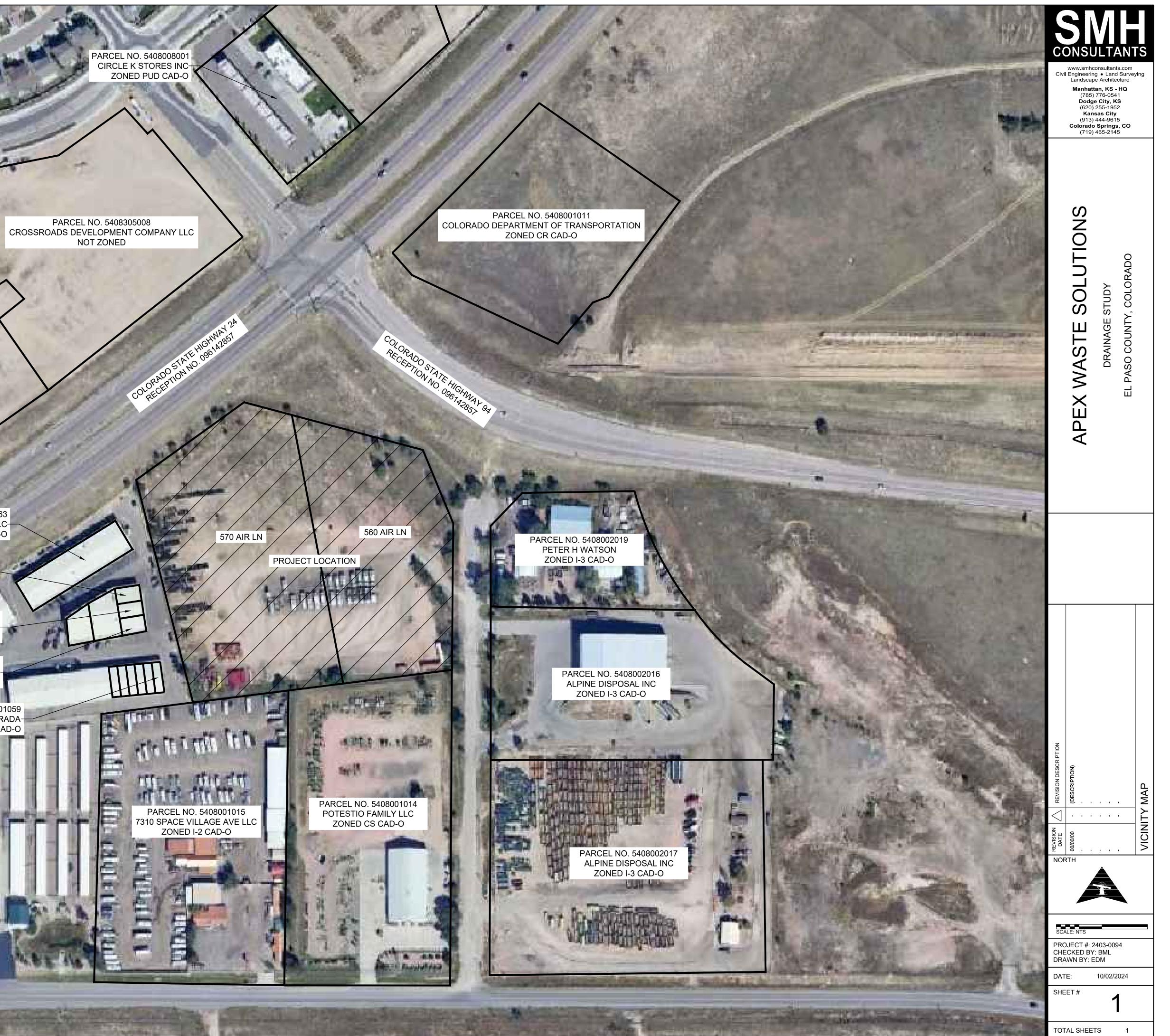


APPENDIX



VICINITY MAP





PARCEL NO. 5408305007 CROSSROADS DEVELOPMENT COMPANY LLC-NOT ZONED

Sality.

PARCEL NO. 5408001063 7235 E HWY 24 LLC-ZONED CS CAD-O

PARCEL NO. 5408001070 KENT ESTATES LLC-ZONED CS CAD-O

PARCEL NO. 5408001069 KENT ESTATES LLC ZONED CS CAD-O

PARCEL NO. 5408001068 KENT ESTATES LLC-ZONED CS CAD-O

> PARCEL NO. 5408001059 LARRY OURADA ZONED CS CAD-O

SOILS REPORT





United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

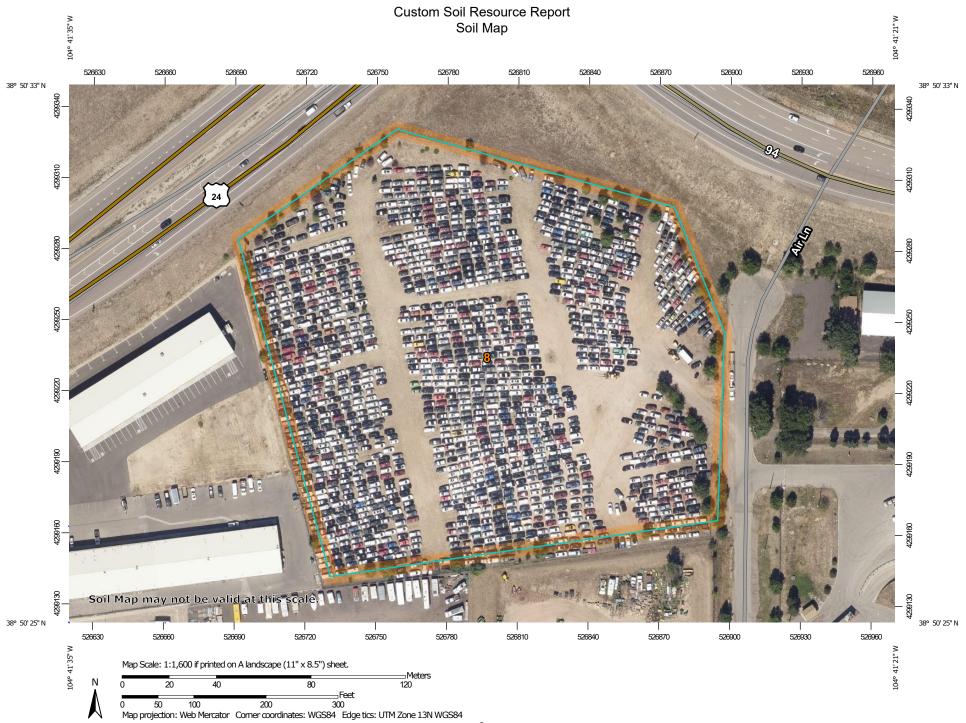
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND		MAP INFORMATION
	terest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils	Soil Map Unit Polygons Soil Map Unit Lines	Ø V	Very Stony Spot Wet Spot	Warning: Soil Map may not be valid at this scale.
	Soil Map Unit Points Point Features		Other Special Line Features	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of
ල හ	Blowout Borrow Pit	Water Fea	tures Streams and Canals	contrasting soils that could have been shown at a more detailed scale.
⊠ ₩ ◇	Clay Spot Closed Depression	Transport	Rails	Please rely on the bar scale on each map sheet for map measurements.
×	Gravel Pit Gravelly Spot	~	Interstate Highways US Routes	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
 Θ Λ.	Landfill Lava Flow	~	Major Roads Local Roads	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts
人 小 次	Marsh or swamp Mine or Quarry	Backgrou	Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
0	Miscellaneous Water Perennial Water			This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
~ +	Rock Outcrop Saline Spot			Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 21, Aug 24, 2023
··· •·	Sandy Spot Severely Eroded Spot			Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.
 ۵	Sinkhole Slide or Slip			Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018
ju K	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
8	Blakeland loamy sand, 1 to 9 percent slopes	7.3	100.0%		
Totals for Area of Interest		7.3	100.0%		

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8-Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats Landform position (three-dimensional): Side slope, talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

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FEMA FLOODPLAIN MAP



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

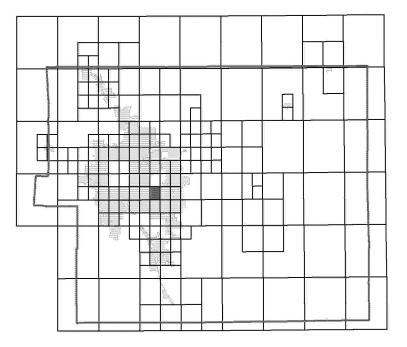
> El Paso County Vertical Datum Offset Table Vertical Datum

Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Offset (ft)

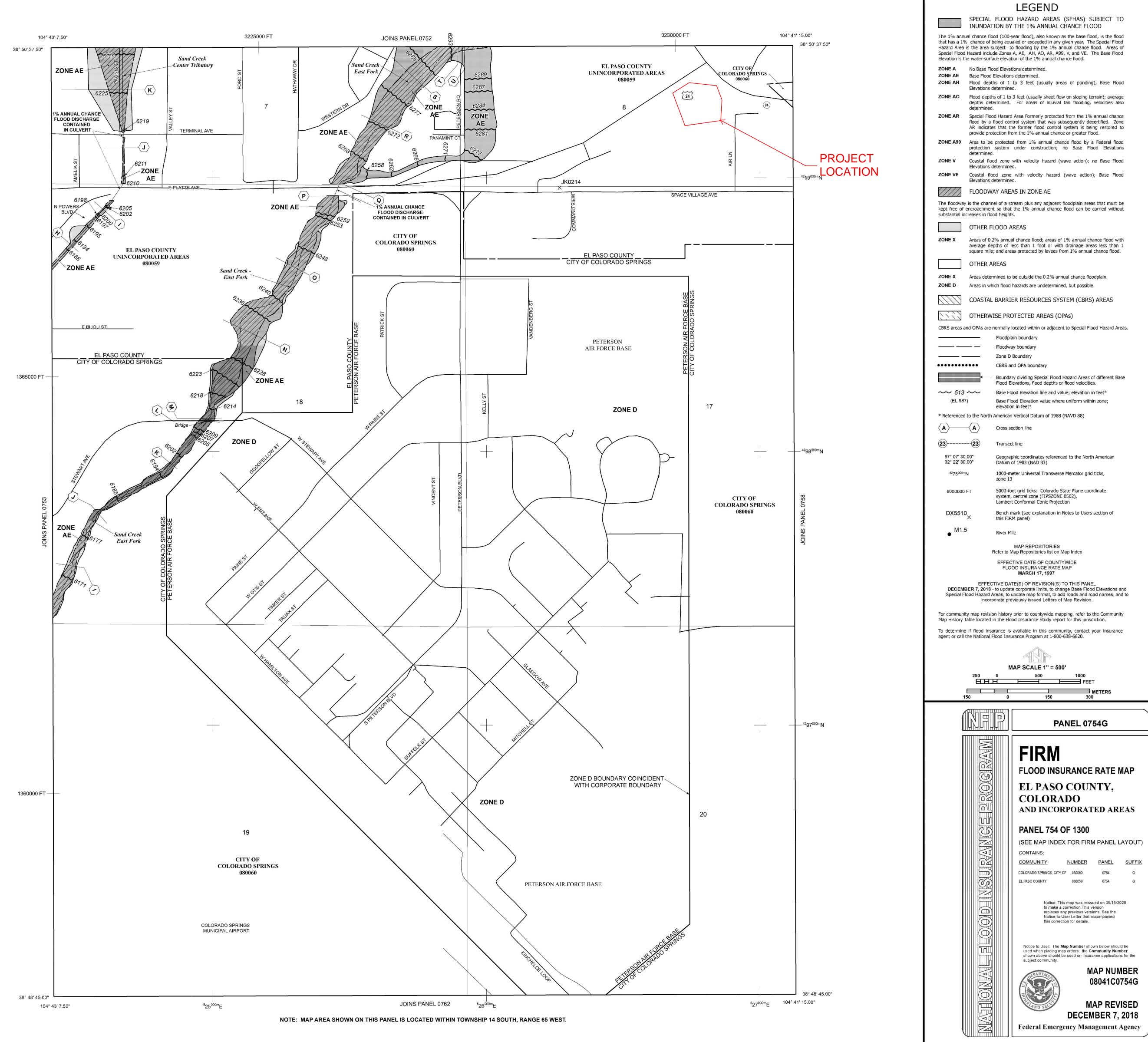
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



HYDROLOGIC CALCULATIONS



			Existing (C-Calcs (HSO	G:A)				
Basin	Land Use	Area (sf)	Area (ac)	C5	C100	C5 x A	C100 x A	Weighted C5	Weighted C100
	Pavement	11990	0.28	0.9	0.96	0.248	0.264		
OS-1	Pasture/Meadow	111896	2.57	0.08	0.35	0.206	0.899	0.16	0.41
	Total	123886	2.84			0.453	1.163		
Basin	Land Use	Area (sf)	Area (ac)	C5	C100	C5 x A	C100 x A	Weighted C5	Weighted C100
	Pavement	63163	1.45	0.9	0.96	1.305	1.392		
FV 1	Building	800	0.02	0.73	0.81	0.013	0.015	0.24	0.47
EX-1	Pasture/Meadow	266933	6.13	0.08	0.35	0.490	2.145	0.24	
	Total	330896	7.60			1.809	3.552		
	<u>. </u>							•	
Basin	Land Use	Area (sf)	Area (ac)	C5	C100	C5 x A	C100 x A	Weighted C5	Weighted C100
	Pavement	75153	1.73	0.9	0.96	1.553	1.656		0.45
	Building	800	0.02	0.73	0.81	0.013	0.015	0.22	
DP-1 (EX-1, OS-1)	Pasture/Meadow	378829	8.70	0.08	0.35	0.696	3.044	0.22	
	Total	454782	10.44			2.262	4.715		
						•		•	
			Proposed	C-Calcs (HS	G:A)				
Basin	Land Use	Area (sf)	Area (ac)	C5	C100	C5 x A	C100 x A	Weighted C5	Weighted C100
	Pavement	11990	0.28	0.9	0.96	0.248	0.264		
OS-1	Pasture/Meadow	111896	2.57	0.08	0.35	0.206	0.899	0.16	0.41
	Total	123886	2.84			0.453	1.163	1	
	I								
Basin	Land Use	Area (sf)	Area (ac)	C5	C100	C5 x A	C100 x A	Weighted C5	Weighted C100

1.935

0.061

1.927

3.923

C100 x A

2.199

0.061

2.826

5.086

0.30

0.26

0.52

0.49

Weighted C5 Weighted C100

87791

3288

239817

330896

Area (sf)

99781

3288

351713

454782

2.02

0.08

5.51

7.60

Area (ac)

2.29

0.08

8.07

10.44

0.9

0.73

0.08

C5

0.9

0.73

0.08

0.96

0.81

0.35

C100

0.96

0.81

0.35

1.814

0.055

0.440

2.309

C5 x A

2.062

0.055

0.646

2.763

Pavement

Building

Pasture/Meadow

Total

Land Use

Pavement Building

Pasture/Meadow

Total

P-1

Basin

DP-1 (P-1, OS-1)

	Existing Time of Concentration																	
S	Sub Basin Data Initial/Overland Time (t _i)				Travel Time (t _t)										Final Time (t _c)			
Basin	Area (ac)	C5	Length (ft)	Slope (ft/ft)	t _i (min)	Length (ft)	Slope (ft/ft)	Land Type	Cv	Velocity (ft/sec)	t _t (min)	Length (ft)	Slope (ft/ft)	Land Type	Cv	Velocity (ft/sec)	t _t (min)	Final t_{c}
OS-1	2.84	0.16	100	0.110	7.7	171	0.062	SP	7	1.75	1.63							9.32
EX-1	7.60	0.24	100	0.056	8.8	144	0.020	PV	20	2.83	0.85	339	0.03	SP	7	1.21	4.66	14.32
DP-1	10.44	0.22	100	0.110	7.2	144	0.020	PV	20	2.83	0.85	610	0.03	SP	7	1.21	8.39	16.46

	Proposed Time of Concentration																	
S	Sub Basin Data Initial/Overland Time (t _i)					Travel Time (t _t)										Final Time (t _c)		
Basin	Area (ac)	C5	Length (ft)	Slope (ft/ft)	t _i (min)	Length (ft)	Slope (ft/ft)	Land Type	C _v	Velocity (ft/sec)	t _t (min)	Length (ft)	Slope (ft/ft)	Land Type	C _v	Velocity (ft/sec)	t _t (min)	Final t _c
OS-1	2.84	0.16	100	0.110	7.7	171	0.062	SP	7	1.75	1.63							9.32
P-1	7.60	0.30	100	0.056	8.1	221	0.025	PV	20	3.16	1.16	240	0.03	SP	7	1.21	3.30	12.60
DP-1	10.44	0.26	100	0.110	6.8	221	0.025	PV	20	3.16	1.16	410	0.03	SP	7	1.21	5.64	13.63

Conveyance Coeffecient C_v									
Type of Land Surface	Land Type	Cv							
Heavy Meadow	HM	2.5							
Tillage/Fields	TF	5							
Riprap (Not Buried)	RR	6.5							
Short Pasture/Lawns	SP	7							
Nearly Bare Ground	NBG	10							
Grassed Waterway	GW	15							
Paved Areas & Shallow Paved Swales	PV	20							

Equations:

$$\begin{split} t_i & (\text{overland}) = 0.395(1.1\text{-}C5)\text{L}^{0.5}\text{S}^{\cdot 0.333} \\ \text{C} = \text{Runoff Coeffecient} \\ \text{L} = \text{Length of overland flow (Max 100ft developed)} \\ \text{S} = \text{Slope} \\ \text{Travel Time: V} = C_v\text{S}^{0.5} \\ \text{V} = \text{Velocity (ft/s)} \\ \text{C}_v = \text{Conveyance Coeffecient} \\ \text{S} = \text{Slope} \\ t_c \text{ Check} = (\text{L}/180)\text{+}10 & \text{(first design point to storm inlet only)} \\ \text{L} = \text{Overall Length} \end{split}$$

E	Existing Intensity Calculations											
Basin	D = t _c (min)	15 (in/hr)	1100 (in/hr)									
OS-1	9.32	4.23	7.11									
EX-1	14.32	3.59	6.03									
DP-1	16.46	3.38	5.68									

Pr	Proposed Intensity Calculations											
Basin	D = t _c (min)	15 (in/hr)	1100 (in/hr)									
OS-1	9.32	4.23	7.11									
P-1	12.60	3.78	6.35									
DP-1	13.63	3.66	6.15									

	Existing Runoff Calculations (Q = CIA)												
Basin	C5	C100	A (ac)	15 (in/hr)	1100 (in/hr)	Q5 (cfs)	Q100 (cfs)						
OS-1	0.16	0.41	2.84	4.23	7.11	1.92	8.28						
EX-1	0.24	0.47	7.60	3.59	6.03	6.55	21.54						
DP-1	0.22	0.45	10.44	3.38	5.68	7.76	26.68						

	Proposed Runoff Calculations (Q = CIA)							
ľ	Basin	C5	C100	A (ac)	15 (in/hr)	1100 (in/hr)	Q5 (cfs)	Q100 (cfs)
	OS-1	0.16	0.41	2.84	4.23	7.11	1.92	8.28
	P-1	0.30	0.52	7.60	3.78	6.35	8.62	25.10
	DP-1	0.26	0.49	10.44	3.66	6.15	9.93	31.46

I5 = -1.50ln(D) + 7.583 I100 = -2.52ln(D) + 12.735 (Figure 6-5 El Paso Co DCM)

PERCOLATION TESTING



October 9, 2024

ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599

SMH Consultants 620 North Tejon Street, Suite 201 Colorado Springs, Colorado 80903

- Attn: Brett Louk
- Re: Geotechnical Data Report Infiltration Testing 560-570 Air Lane El Paso County, Colorado Entech Job No. 241513

Dear Mr. Louk:

As requested, personnel of Entech Engineering, Inc. performed infiltration testing using the percolation testing method at the above referenced site to evaluate the site soils to determine the infiltration rates for proposed detention pond.

The test holes were drilled on September 19, 2024, and the testing was performed on September 20, 2024. The test locations are shown on Site and Exploration Plan, Figure 1. Profile hole PH-1 was drilled in the center of proposed detention pond with the percolation holes (designated P1 – P3) were drilled across the pond. The profile hole log, laboratory test results, percolation test results, and infiltration rates are presented in Figures 2 through 5. Soils encountered in the profile and percolation holes consisted of silty sand. Bedrock and groundwater were not encountered in the profile hole which was drilled to a depth of 10 feet. Results are summarized in the table below.

Test Location	Percolation Rate (min./inch)	Infiltration Rate (inch/hour)	Average Infiltration Rate (inch/hour)	Discuss if groundwater
P1	8	1.935		was encountered and if
P2	20	0.774	1.5	so at what elevation.
P3	13	1.161		

We trust that this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

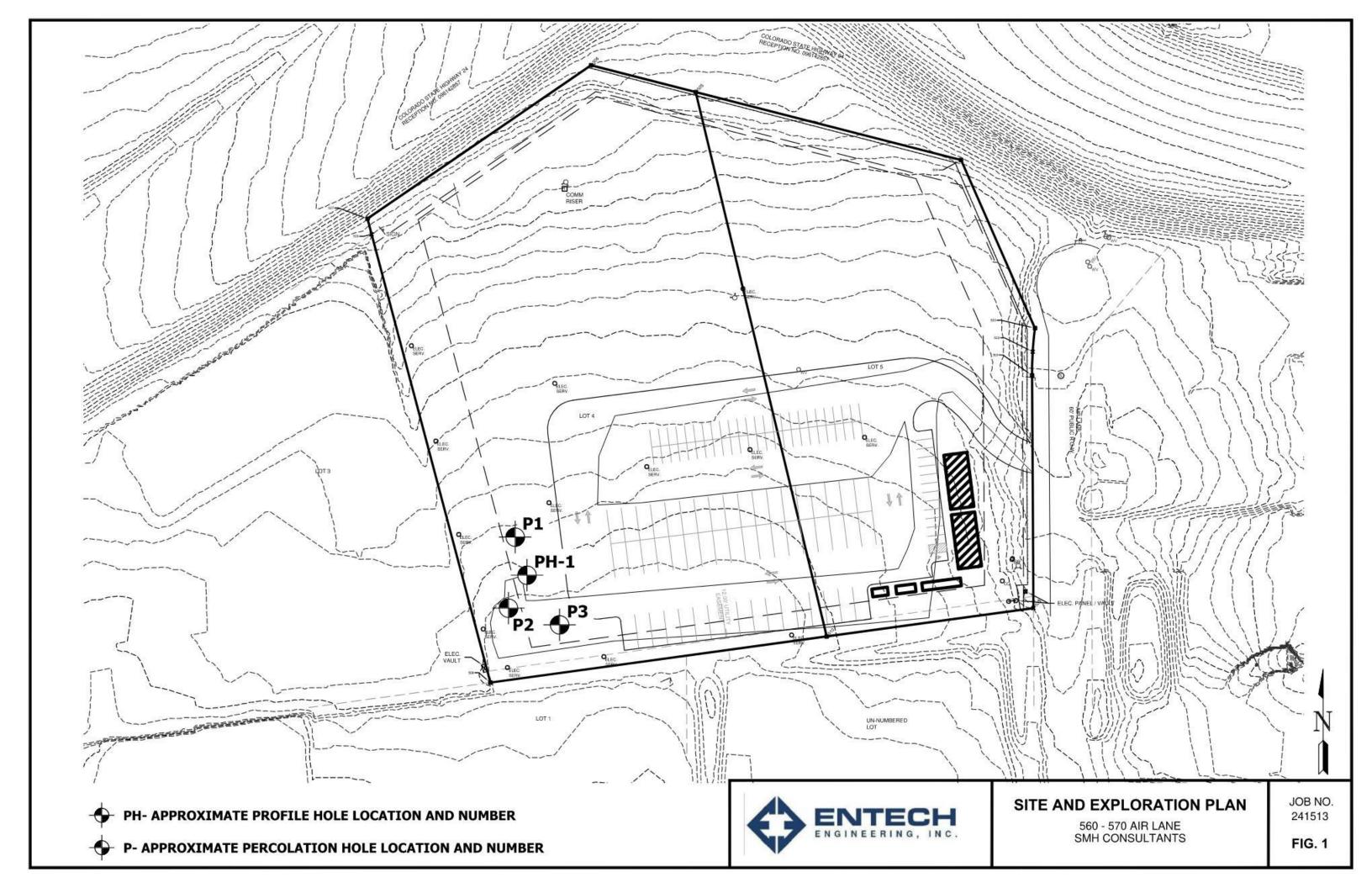
Logan L. Langford, P.G. Sr. Geologist

Reviewed by:



Digitally signed by Joseph C Goode III Date: 10/09/24

Joseph C. Goode III, P.E. Sr. Engineer



TEST BORING DATE DRILLED 9/19/202 REMARKS	1 24				%	
	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	
DRY TO 10', 9/19/24	Δ	0	S	В	5	
SAND, SILTY, LIGHT BROWN to		111				
OLIVE, LOOSE, MOIST				7	5.1	
	5			5	4.7	
	10 15 20			9	9.8	



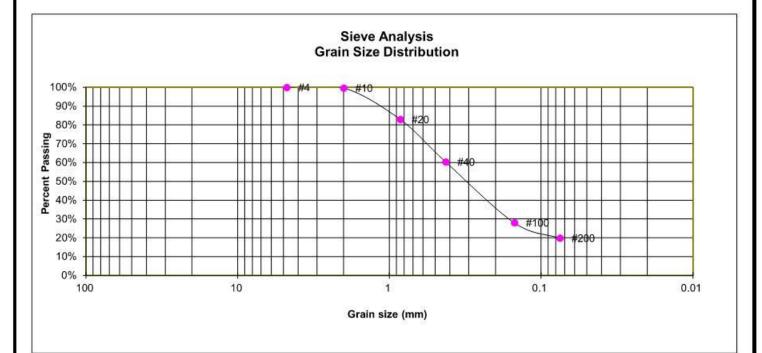
TEST BORING LOGS

560-570 AIR LANE SMH CONSULTANTS JOB NO. 241513

FIG. 2

<u>TEST BORING</u> DEPTH (FT)

1 2-3



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	Finer
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	
4	100.0%
10	99.7%
20	83.0%
40	60.3%
100	28.0%
200	19.8%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM



LABORATORY TEST RESULTS

560-570 AIR LANE SMH CONSULTANTS JOB NO. 241513

FIG. 3

PERCOLATION HOLES

Date Hole	s Prepared:	9/19/2024			Date Hole	Completed:	9/2	0/2024
Hole No. Depth:	1 58"		Hole No. Depth:	. 2 47"		Hole No. 3 Depth:	47"	
	æ.	Water			Water			Water
T	Time	Level	75-2-21	Time	Level	70-1-1	Time	Level
<u>Trial</u> 1	<u>(min.)</u> 10	<u>Change (in.)</u> 2 1/4	<u>Trial</u> 1	<u>(min.)</u> 10	<u>Change (in.)</u> 3/4	<u>Trial</u> 1	<u>(min.)</u> 10	Change (in.) 1
	10			10	3/4		10	1
2 3	10	2 1 1/4	2 3	10	1/2	2 3	10	3/4
Perc Rate	(min./in.):	8	Perc Rate	e (min./in.):	20	Perc Rate ((min./in.):	13
		Average Per	rc Rate (mi	n./in.)	14			
PROFII	LE HOLE				Date Profile Hole	Completed:	9/1	9/2024
Depth		Visual Classification				Remarks		
0-10'		Sand, with silt, light b	rown to oli	ive				
						No Bedroc No Ground		
	7 Blows / ft.	@ 2'				No Oround	Iwater	
	5 Blows / ft.	@ 4'						
	9 Blows / ft.	@ 9'						
Observer:	S. Wood							
\bigcirc					560-570 AIR LA	NE	S	JOB NO. 241513 FIG. 4

SMH CONSULTANTS

Infiltration Rate (I) = Percolation Rate (P)/ Reduction Factor(RF) I=P/RF

 $R_{f} = [(2d_{1} - \Delta d) / dia] + 1$

d₁ = initial water depth (in.)

∆d = final water level drop (in.)

dia = diameter of the percolation hole (in.)

Test No. P1			Test No. F	2		Test No. P3		
Perc Rate diameter		0 in/hr in	Perc Rate diameter	3.00 8) in/hr in	Perc Rate diameter) in/hr in
<u>P1</u> d ₁ =	(inches) 12.0		<u>P1</u> d ₁ =	(inches) 12.0		<u>P1</u> d ₁ =	(inches) 12.0	
∆d = R _f =	1.00 3.9		∆d = R _f =	1.00 3.9		$\Delta d = R_f =$	1.00 3.9	
(P1) I =	1.935	in/hr	(P2) I =	0.774	in/hr	(P3) I =	1.161	in/hr
			I AVG=	1.5	in/hr			



INFILTRATION RATE

560-570 AIR LANE SMH CONSULTANTS

FIG. 5

PERMANENT BMP CALCULATIONS



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Pond No. 1 - SAND FILTER BASIN

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 6294.50 ft

Stage / Storage Table

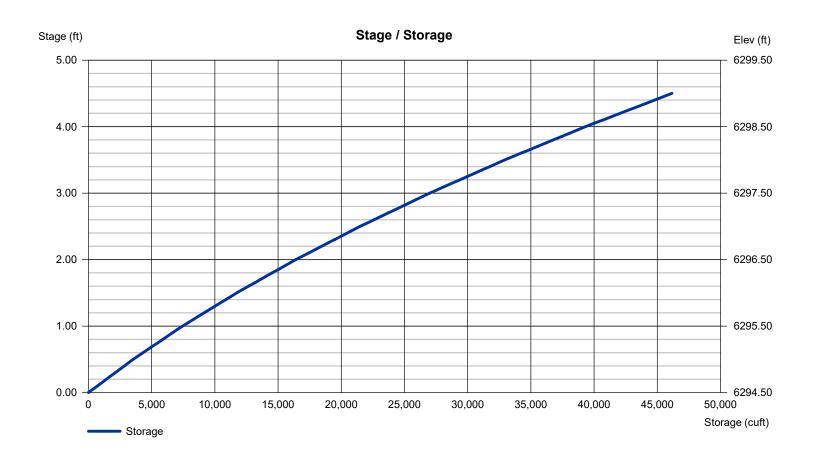
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	6294.50	6,710	0	0
0.50	6295.00	7,436	3,535	3,535
1.00	6295.50	8,188	3,904	7,439
1.50	6296.00	8,964	4,286	11,725
2.00	6296.50	9,766	4,681	16,405
2.50	6297.00	10,592	5,088	21,493
3.00	6297.50	11,444	5,507	27,000
3.50	6298.00	12,321	5,939	32,939
4.00	6298.50	13,223	6,384	39,323
4.50	6299.00	14,150	6,841	46,165

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.500 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



	Infiltration Calculations						
Elevation (ft)	Stage (ft)	Contour Area A (sf)	Discharge Q (cfs)				
6294.5	0	6710	0.23				
6295	0.5	7436	0.26				
6295.5	1	8188	0.28				
6296	1.5	8964	0.31				
6296.5	2	9766	0.34				
6297	2.5	10592	0.37				
6297.5	3	11444	0.40				
6298	3.5	12321	0.43				
6298.5	4	13223	0.46				
6299	4.5	14150	0.49				

Is this the exfiltration Q as calculated to the side? Please make sure the names match. If not please identify what the discharge represents/what storm event.

in/hr Percolation Rate R = 1.5

Extiltration Q (cfs)= (R in/hr x A sf) / (12 in/ft x 3600 s/hr)

Imperviousness i = 27.5%

WQCV = a	a(0.91i [°] -	1.19i ²	+ 0.7

iper riousiless i	27.370	
WQCV = a	(0.91i ³ - 1.19	i ² + 0.78i)
a =	1	(note - a = 1 corresponds to 40 hr minimum drain time, infiltration sections do not have a minmum drain time, but a maximum drain time of 20 hrs)
WQCV =	0.143	watershed inches
WQCV =	0.091	ac-ft
EURV (HSG A) = 1	.68i ^{1.28}	USDCM Vol 2 - EQ 12-1
EURV =	0.322	watershed inches
EURV =	0.204	ac-ft

From El Paso Co DCM Vol 2, Section 4.2					
Design Volume = (WQCV/12) * Basin Area [ac-ft]					
Design Volume = (0.143/12) * 7.60					
Design Volume = 0.091 ac-ft					
Design Volume = 3964 cu. ft.					
Min. Filter Surface Area = Design Vol / 3 * 43560 [sq. ft.]					
Min. Filter Surface Area = (0.091/3) * 43560					
Min. Filter Surface Area = 1322 sq. ft.					

Note - EPC design equations for sand filter basin storage and mimimum filter surface area are specified for sand filter basins that only store and treat the WQCV. Because the proposed basin will store and release up to the 100-year event, the proposed basin storage and filter surface are are much larger than the EPC design equations specify.

Provide calculations of drain times for design storm events. WQCV, EURV, 5-year, 100-year.

Because these volumes and surface areas aren't use - show calculated volumes/surface area based on the 100-year and clearly show drain times based on the actual designed dimensions.

SDI-Design Data v2.00, Released January 2020

Stormwater Facility Name: 560-570 Air Lane Infiltration Pond

Facility Location & Jurisdiction: El Paso County, CO

User Input: Watershed Characteristics Sand Filter (SF) SF 7.60 Watershed Area = acres 600 Watershed Length = ft Watershed Length to Centroid = 540 ft 0.030 Watershed Slope = ft/ft Watershed Imperviousness = 27.5% percent Percentage Hydrologic Soil Group A = 100.0% percent 0.0% Percentage Hydrologic Soil Group B = percent 0.0% Percentage Hydrologic Soil Groups C/D = percent Target WQCV Drain Time = 40.0 hours Location for 1-hr Rainfall Depths (use dropdown): User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Once CUHP has been run and the Stage-Area-Discharge information has been provided, click 'Process Data' to interpolate the Stage-Area-Volume-Discharge data and generate summary results in the table below. Once this is complete, click 'Print to PDF'.

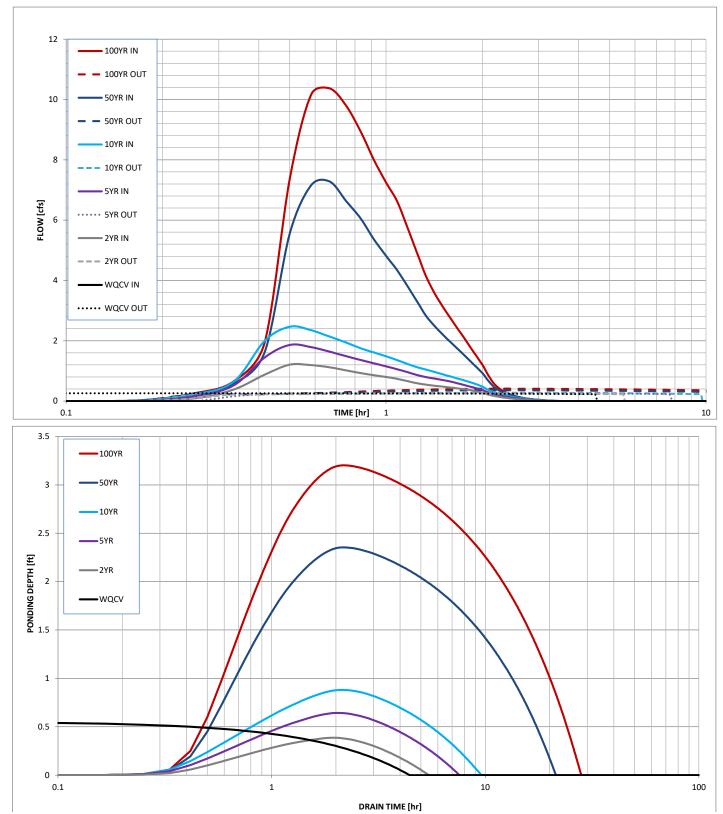
User Defined	User Defined	User Defined	User Defined
Stage [ft]	Area [ft^2]	Stage [ft]	Discharge [cfs]
0.00	6,710	0.00	0.23
0.50	7,436	0.50	0.26
1.00	8,188	1.00	0.28
1.50	8,964	1.50	0.31
2.00	9,766	2.00	0.34
2.50	10,592	2.50	0.37
3.00	11,444	3.00	0.40
3.50	12,321	3.50	0.43
4.00	13,223	4.00	0.46
4.50	14,150	4.50	0.49

After completing and printing this worksheet to a pdf, go to: <u>https://maperture.digitaldataservices.com/gvh/?viewer=cswdif</u> Create a new stormwater facility, and attach the PDF of this worksheet to that record.

Routed Hydrograph Results

= WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
= N/A	1.02	1.30	1.57	2.35	2.74	in
= 0.091	0.106	0.154	0.200	0.522	0.743	acre-ft
= N/A	0.106	0.154	0.200	0.522	0.743	acre-ft
= 4.3	5.3	7.3	9.3	20.7	27.0	hours
= 4.4	5.4	7.5	9.5	21.2	27.8	hours
= 0.56	0.39	0.64	0.88	2.35	3.20	ft
= 0.17	0.17	0.18	0.18	0.24	0.27	acres
= 0.092	0.062	0.106	0.148	0.458	0.674	acre-ft
	= N/A = 0.091 = N/A = 4.3 = 4.4 = 0.56 = 0.17	$= \frac{N/A}{0.091} \frac{1.02}{0.106}$ $= \frac{N/A}{0.106} \frac{0.106}{0.106}$ $= \frac{4.3}{5.3} \frac{5.3}{0.106}$ $= \frac{4.4}{5.4} \frac{5.4}{0.56} \frac{0.39}{0.17}$ $= 0.17 0.17$	$= \frac{N/A}{0.091} \frac{1.02}{0.106} \frac{1.30}{0.154}$ $= \frac{N/A}{0.106} \frac{0.154}{0.154}$ $= \frac{4.3}{5.3} \frac{7.3}{7.3}$ $= \frac{4.4}{5.4} \frac{5.4}{7.5}$ $= \frac{0.56}{0.39} \frac{0.64}{0.64}$ $= 0.17 \frac{0.17}{0.18}$	$= \frac{N/A}{0.091} \frac{1.02}{0.106} \frac{1.30}{0.154} \frac{1.57}{0.200}$ $= \frac{N/A}{0.106} \frac{0.154}{0.154} \frac{0.200}{0.200}$ $= \frac{4.3}{0.3} \frac{5.3}{0.3} \frac{7.3}{0.3} \frac{9.3}{0.56}$ $= \frac{0.56}{0.39} \frac{0.64}{0.64} \frac{0.88}{0.88}$ $= \frac{0.17}{0.17} \frac{0.17}{0.18} \frac{0.18}{0.18}$	N/A 1.02 1.30 1.57 2.35 0.091 0.106 0.154 0.200 0.522 N/A 0.106 0.154 0.200 0.522 + 4.3 5.3 7.3 9.3 20.7 + 4.4 5.4 7.5 9.5 21.2 - 0.56 0.39 0.64 0.88 2.35 - 0.17 0.17 0.18 0.18 0.24	N/A 1.02 1.30 1.57 2.35 2.74 0.091 0.106 0.154 0.200 0.522 0.743 N/A 0.106 0.154 0.200 0.522 0.743 4.3 5.3 7.3 9.3 20.7 27.0 4.4 5.4 7.5 9.5 21.2 27.8 0.56 0.39 0.64 0.88 2.35 3.20 0.17 0.17 0.18 0.18 0.24 0.27

Were these the volume design values chosen for the full spectrum of storms?



SDI-Design Data v2.00, Released January 2020

Stormwater Facility Name: 560-570 Air Lane Infiltration Pond

Facility Location & Jurisdiction: El Paso County, CO

User Input: Watershed Characteristics Sand Filter (SF) SF Watershed Area = 7.60 acres 600 Watershed Length = ft Watershed Length to Centroid = 540 ft 0.030 Watershed Slope = ft/ft Watershed Imperviousness = 27.5% percent Percentage Hydrologic Soil Group A = 100.0% percent 0.0% Percentage Hydrologic Soil Group B = percent 0.0% Percentage Hydrologic Soil Groups C/D = percent 40.0 Target WQCV Drain Time = hours Location for 1-hr Rainfall Depths (use dropdown): User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

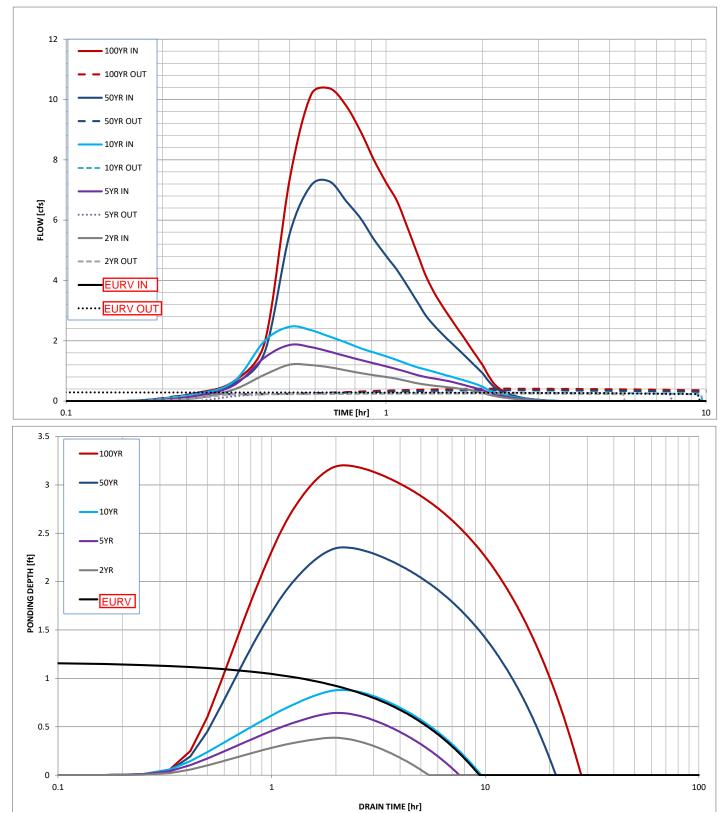
Once CUHP has been run and the Stage-Area-Discharge information has been provided, click 'Process Data' to interpolate the Stage-Area-Volume-Discharge data and generate summary results in the table below. Once this is complete, click 'Print to PDF'.

User Defined	User Defined	User Defined	User Defined
Stage [ft]	Area [ft^2]	Stage [ft]	Discharge [cfs]
0.00	6,710	0.00	0.23
0.50	7,436	0.50	0.26
1.00	8,188	1.00	0.28
1.50	8,964	1.50	0.31
2.00	9,766	2.00	0.34
2.50	10,592	2.50	0.37
3.00	11,444	3.00	0.40
3.50	12,321	3.50	0.43
4.00	13,223	4.00	0.46
4.50	14,150	4.50	0.49

After completing and printing this worksheet to a pdf, go to: <u>https://maperture.digitaldataservices.com/gvh/?viewer=cswdif</u> Create a new stormwater facility, and attach the PDF of this worksheet to that record.

Routed Hydrograph Results

Design Storm Return Period =	EURV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	N/A	1.02	1.30	1.57	2.35	2.74	in
CUHP Runoff Volume =	0.204	0.106	0.154	0.200	0.522	0.743	acre-ft
Inflow Hydrograph Volume =	N/A	0.106	0.154	0.200	0.522	0.743	acre-ft
Time to Drain 97% of Inflow Volume =	9.1	5.3	7.3	9.3	20.7	27.0	hours
Time to Drain 99% of Inflow Volume =	9.3	5.4	7.5	9.5	21.2	27.8	hours
Maximum Ponding Depth =	1.18	0.39	0.64	0.88	2.35	3.20	ft
Maximum Ponded Area =	0.19	0.17	0.18	0.18	0.24	0.27	acres
Maximum Volume Stored =	0.204	0.062	0.106	0.148	0.458	0.674	acre-ft



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

560-570 AIR LANE SPILLWAY CREST

Trapezoidal Weir

Crest	= Sharp
Bottom Length (ft)	= 30.00
Total Depth (ft)	= 1.25
Side Slope (z:1)	= 4.00

Calculations

Weir Coeff. Cw Compute by: Known Q (cfs) = 3.10 Known Q = 31.46

Provide calculation for spillway riprap sizing.

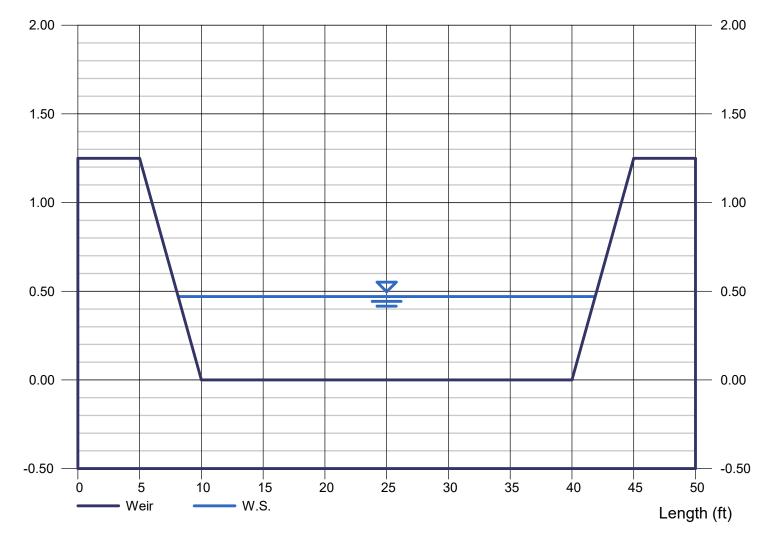
Highlighted

Depth (ft)	=	0.47
Q (cfs)	=	31.46
Area (sqft)	=	14.98
Velocity (ft/s)	=	2.10
Top Width (ft)	=	33.76

Depth (ft)

560-570 AIR LANE SPILLWAY CREST

Depth (ft)





NOAA Atlas 14, Volume 8, Version 2 Location name: Cimarron Hills, Colorado, USA* Latitude: 38.8415°, Longitude: -104.6912° Elevation: 6304 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

		based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹ Average recurrence interval (years)								
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.238 (0.200-0.286)	0.289 (0.242-0.348)	0.378 (0.315-0.456)	0.457 (0.379-0.554)	0.573 (0.461-0.728)	0.669 (0.523-0.860)	0.771 (0.579-1.02)	0.880 (0.631-1.19)	1.03 (0.708-1.44)	1.15 (0.767-1.62)
10-min	0.349 (0.292-0.419)	0.423 (0.354-0.509)	0.553 (0.461-0.667)	0.669 (0.554-0.811)	0.839 (0.675-1.07)	0.980 (0.766-1.26)	1.13 (0.848-1.49)	1.29 (0.924-1.74)	1.51 (1.04-2.10)	1.69 (1.12-2.38)
15-min	0.425 (0.357-0.511)	0.516 (0.432-0.621)	0.674 (0.563-0.814)	0.815 (0.676-0.989)	1.02 (0.823-1.30)	1.20 (0.934-1.54)	1.38 (1.03-1.81)	1.57 (1.13-2.13)	1.84 (1.26-2.57)	2.06 (1.37-2.90)
30-min	0.647 (0.543-0.778)	0.783 (0.656-0.943)	1.02 (0.852-1.23)	1.23 (1.02-1.50)	1.55 (1.24-1.96)	1.80 (1.41-2.32)	2.08 (1.56-2.74)	2.37 (1.70-3.21)	2.78 (1.91-3.88)	3.11 (2.07-4.38)
60-min	0.863 (0.724-1.04)	1.02 (0.853-1.22)	1.30 (1.09-1.58)	1.57 (1.30-1.91)	1.99 (1.61-2.55)	2.35 (1.84-3.04)	2.74 (2.07-3.64)	3.17 (2.28-4.32)	3.79 (2.61-5.30)	4.30 (2.86-6.04)
2-hr	1.08 (0.912-1.29)	1.25 (1.06-1.50)	1.59 (1.34-1.90)	1.92 (1.60-2.31)	2.44 (2.00-3.12)	2.90 (2.30-3.74)	3.40 (2.59-4.50)	3.97 (2.88-5.39)	4.80 (3.33-6.68)	5.48 (3.67-7.66)
3-hr	1.19 (1.01-1.42)	1.36 (1.15-1.62)	1.70 (1.44-2.04)	2.06 (1.73-2.47)	2.64 (2.18-3.38)	3.16 (2.52-4.08)	3.74 (2.87-4.95)	4.41 (3.22-5.98)	5.39 (3.77-7.50)	6.21 (4.18-8.65)
6-hr	1.36 (1.17-1.61)	1.54 (1.32-1.82)	1.92 (1.63-2.28)	2.31 (1.96-2.76)	2.98 (2.49-3.82)	3.59 (2.90-4.62)	4.28 (3.32-5.64)	5.07 (3.74-6.86)	6.25 (4.40-8.66)	7.24 (4.91-10.0)
12-hr	1.51 (1.30-1.77)	1.73 (1.49-2.03)	2.18 (1.87-2.57)	2.63 (2.24-3.11)	3.37 (2.83-4.26)	4.03 (3.27-5.13)	4.77 (3.72-6.23)	5.61 (4.16-7.51)	6.85 (4.86-9.40)	7.88 (5.38-10.8)
24-hr	1.68 (1.46-1.96)	1.95 (1.70-2.28)	2.48 (2.15-2.90)	2.99 (2.57-3.51)	3.78 (3.18-4.72)	4.48 (3.65-5.63)	5.24 (4.10-6.75)	6.08 (4.54-8.06)	7.31 (5.21-9.94)	8.32 (5.72-11.4)
2-day	1.91 (1.68-2.22)	2.24 (1.96-2.59)	2.83 (2.47-3.29)	3.38 (2.94-3.95)	4.22 (3.57-5.20)	4.94 (4.05-6.15)	5.72 (4.50-7.29)	6.57 (4.93-8.61)	7.78 (5.58-10.5)	8.77 (6.08-11.9)
3-day	2.08 (1.84-2.40)	2.44 (2.15-2.82)	3.08 (2.70-3.56)	3.66 (3.19-4.25)	4.53 (3.83-5.53)	5.26 (4.32-6.49)	6.04 (4.77-7.65)	6.89 (5.18-8.97)	8.09 (5.82-10.8)	9.06 (6.30-12.2)
4-day	2.23 (1.97-2.56)	2.61 (2.30-3.00)	3.27 (2.88-3.78)	3.87 (3.39-4.49)	4.77 (4.04-5.79)	5.51 (4.54-6.78)	6.30 (4.99-7.95)	7.15 (5.40-9.28)	8.35 (6.03-11.1)	9.31 (6.50-12.6)
7-day	2.60 (2.32-2.98)	3.02 (2.69-3.46)	3.75 (3.33-4.30)	4.40 (3.87-5.07)	5.35 (4.56-6.44)	6.13 (5.08-7.48)	6.96 (5.54-8.72)	7.84 (5.95-10.1)	9.08 (6.59-12.0)	10.1 (7.07-13.5)
10-day	2.93 (2.63-3.34)	3.39 (3.03-3.86)	4.17 (3.71-4.77)	4.86 (4.30-5.58)	5.87 (5.02-7.03)	6.69 (5.56-8.12)	7.55 (6.04-9.41)	8.47 (6.45-10.9)	9.74 (7.10-12.9)	10.8 (7.59-14.4)
20-day	3.87 (3.50-4.38)	4.45 (4.01-5.04)	5.41 (4.86-6.15)	6.24 (5.57-7.12)	7.41 (6.37-8.76)	8.34 (6.98-10.0)	9.29 (7.47-11.5)	10.3 (7.88-13.0)	11.6 (8.53-15.2)	12.7 (9.02-16.8)
30-day	4.66 (4.23-5.25)	5.35 (4.85-6.03)	6.48 (5.85-7.33)	7.43 (6.66-8.44)	8.74 (7.53-10.3)	9.76 (8.19-11.6)	10.8 (8.70-13.2)	11.8 (9.09-14.9)	13.2 (9.71-17.1)	14.3 (10.2-18.9)
45-day	5.65 (5.16-6.34)	6.50 (5.92-7.30)	7.86 (7.13-8.85)	8.97 (8.08-10.1)	10.5 (9.04-12.2)	11.6 (9.76-13.7)	12.7 (10.3-15.4)	13.8 (10.6-17.2)	15.2 (11.2-19.6)	16.2 (11.7-21.4)
60-day	6.50 (5.95-7.27)	7.49 (6.85-8.38)	9.05 (8.24-10.2)	10.3 (9.32-11.6)	12.0 (10.3-13.8)	13.2 (11.1-15.5)	14.3 (11.6-17.3)	15.5 (12.0-19.3)	16.9 (12.5-21.7)	17.9 (12.9-23.5)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

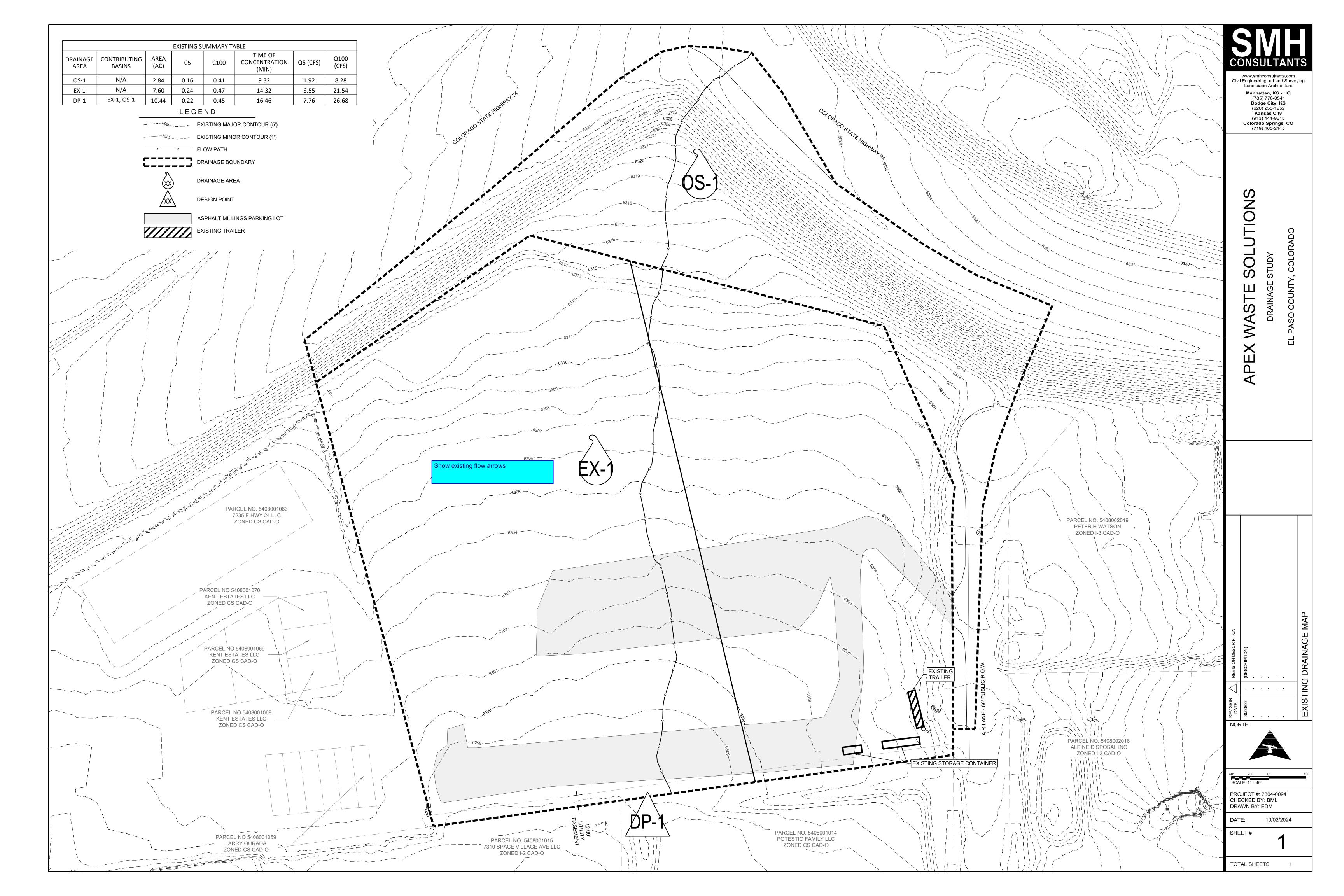
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

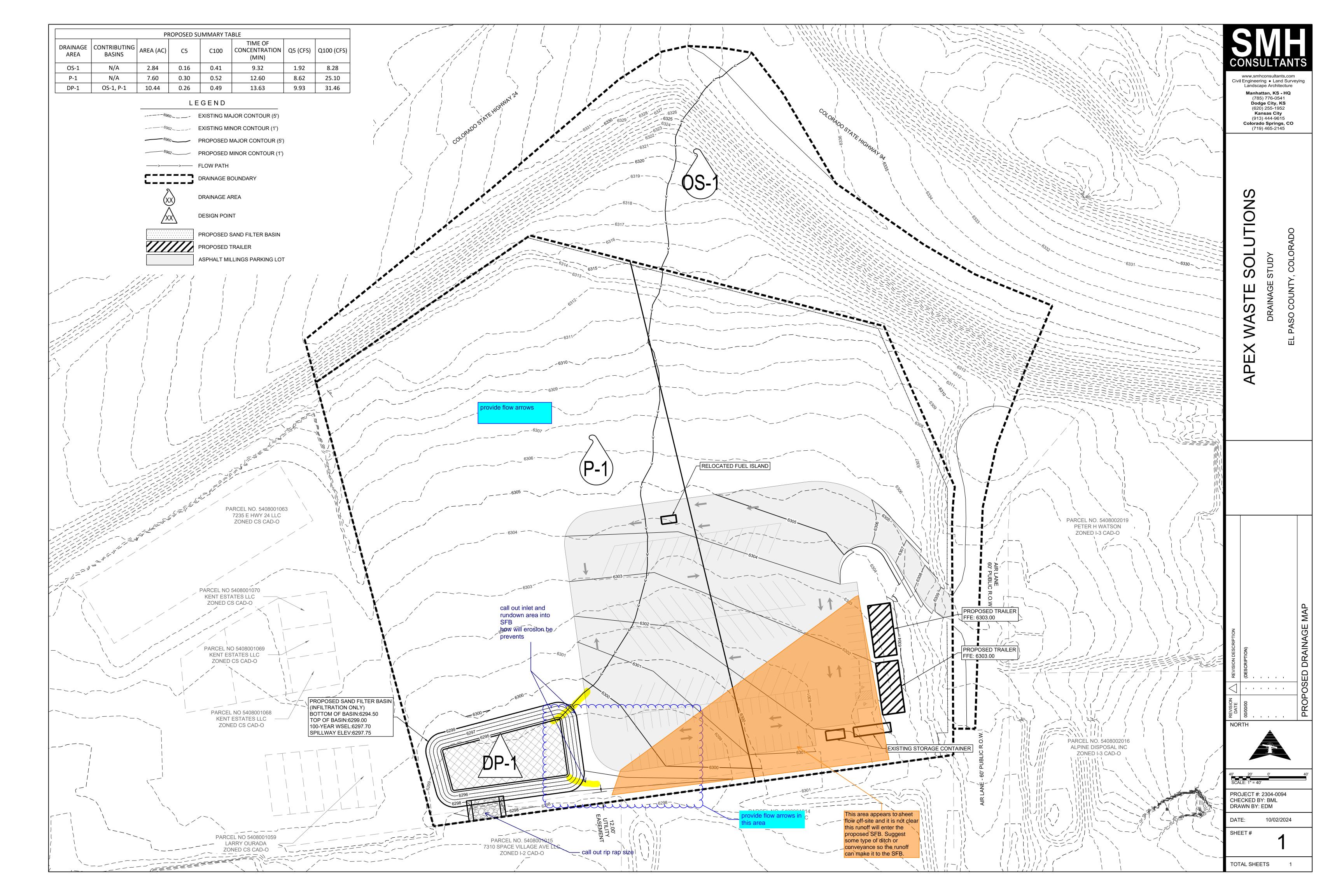
Back to Top

PF graphical

DRAINAGE MAPS







V1_Drainage Letter.pdf Markup Summary

eschoenheit (11		
Engineer stamp, date and sign Owner says and date property and engineering and approximate the block? Said dataset and approximate block? Said dataset and approximate block? Said dataset and approximate said block. The same state of the same state same base. I accept representation for any labelity	Author: eschoenheit Page Index: 3 Date: 12/10/2024 2:29:09 PM Color: Layer:	Engineer stamp, date and sign Owner sign and date
AND INCOMPLETED	Author: eschoenheit Page Index: 8 Date: 12/10/2024 11:32:55 AM Color: Layer:	Add engineer estimate for SFB design cost to match FAE.
flow rates will be slightly higher than the pr filter hists will be implemented into the sit the proposed sjectNardf "Mittime, longer the elegeneant of their is should not adversely in files. Design and slatement most indexes "will not adversely implect."	Author: eschoenheit Page Index: 9 Date: 12/9/2024 2:54:48 PM Color:	Design and statement must indicate "will not adversely impact".
te. Runoff will n sit <mark>e should n</mark> ot :	Author: eschoenheit Page Index: 9 Date: 12/9/2024 2:54:51 PM Color: Layer:	
The strange to a strange	Author: eschoenheit Page Index: 54 Date: 12/10/2024 11:44:55 AM Color: Layer:	Show existing flow arrows
	Author: eschoenheit Page Index: 55 Date: 12/10/2024 11:47:36 AM Color: Layer:	call out rip rap size
	Author: eschoenheit Page Index: 55 Date: 12/10/2024 11:44:21 AM Color: Layer:	provide flow arrows in this area
provide flow arrows	Author: eschoenheit Page Index: 55 Date: 12/10/2024 11:44:50 AM Color: Layer:	provide flow arrows
	Author: eschoenheit Page Index: 55 Date: 12/10/2024 2:57:43 PM Color: Layer:	



Author: eschoenheit Page Index: 55 Date: 12/10/2024 2:57:45 PM Color: Layer:



Author: eschoenheit Page Index: 55 Date: 12/10/2024 3:00:02 PM Color: Layer:

call out inlet and rundown area into SFB how will erosion be prevents

Mikayla Hartford (18)

Mikayla Hartioic		
() Apex V Fin	Author: Mikayla Hartford Page Index: 1 Date: 12/10/2024 9:27:22 AM Color: Color: Color	
), PPR2441	Author: Mikayla Hartford Page Index: 1 Date: 12/10/2024 9:27:34 AM Color: ■ Layer:	PPR2441
	Author: Mikayla Hartford Page Index: 5 Date: 12/11/2024 11:30:51 AM Color: Layer:	Runoff on the site will now be detained in the basin and leave the site through subsurface infiltration.
 A state of the sta	Author: Mikayla Hartford Page Index: 5 Date: 12/11/2024 11:36:19 AM Color: Layer:	Because the site is infiltrating storms greater than the WQCV please provide proof of approval from the state that the project site has the water rights to do so.
<text><text><section-header><text></text></section-header></text></text>	Author: Mikayla Hartford Page Index: 7 Date: 12/11/2024 11:33:13 AM Color: Layer:	event will leave the sand filter basin and travel south along historic drainage paths.
And Aling the Aling and the Aling	Author: Mikayla Hartford Page Index: 7 Date: 12/11/2024 11:33:52 AM Color: ■ Layer:	Clarify change in discharge point. The existing and proposed discharge points appear different so this sentence does not appear accurate based on the drainage maps.
Note a state of the state of th	Author: Mikayla Hartford Page Index: 7 Date: 12/11/2024 12:01:22 PM Color: Layer:	Per MHFD Criteria for full infiltration systems the control measure should be approximately 3 feet or more above groundwater levels. Discuss if this site characteristic is met.
NEXT PAYLOR IN CALL NO. A SUBJECT AND A SUBJ	Author: Mikayla Hartford Page Index: 8 Date: 12/11/2024 11:34:32 AM Color: Layer:	The EURV must be designed to drain in a maximum of 36 hours and the WQCV must be designed to drain in a maximum of 20 hours.
A is 19 values many having a sub- transmission of the sub- sub-sub-sub-sub-sub-sub-sub-sub-sub-sub-	Author: Mikayla Hartford Page Index: 8 Date: 12/11/2024 11:59:23 AM Color: ■ Layer:	The SFB sizing should be based on a WQCV drain time of 12 hours per MHFD. It appears this is met based on results stated below, but please clarify this sentence.

m . The set of the strain way before the the strain way before the strain way befor	Author: Mikayla Hartford Page Index: 38 Date: 12/11/2024 12:04:38 PM Color: ■ Layer:	Discuss if groundwater was encountered and if so at what elevation.
	Author: Mikayla Hartford Page Index: 46 Date: 12/11/2024 12:06:45 PM Color: ■ Layer:	Is this the exfiltration Q as calculated to the side? Please make sure the names match. If not please identify what the discharge represents/what storm event.
ung in angewa in ang	Author: Mikayla Hartford Page Index: 46 Date: 12/11/2024 12:08:57 PM Color: ■ Layer:	Provide calculations of drain times for design storm events. WQCV, EURV, 5-year, 100-year.
and an one of the state of the	Author: Mikayla Hartford Page Index: 46 Date: 12/11/2024 12:09:38 PM Color: ■ Layer:	Because these volumes and surface areas aren't use - show calculated volumes/surface area based on the 100-year and clearly show drain times based on the actual designed dimensions.
Please submit SDI form as a legarate slot as well in EDARP Stormwater D Stormwater Facility Name: 560-570	Author: Mikayla Hartford Page Index: 47 Date: 12/11/2024 8:01:43 AM Color: ■ Layer:	Please submit SDI form as a separate slot as well in EDARP.
	Author: Mikayla Hartford Page Index: 47 Date: 12/11/2024 12:11:30 PM Color: ■ Layer:	Were these the volume design values chosen for the full spectrum of storms?
1(0) - 1.60	Author: Mikayla Hartford Page Index: 51 Date: 12/11/2024 12:12:16 PM Color: ■ Layer:	Provide calculation for spillway riprap sizing.
	Author: Mikayla Hartford Page Index: 55 Date: 12/11/2024 12:12:45 PM Color: Layer:	
	Author: Mikayla Hartford Page Index: 55 Date: 12/11/2024 12:13:10 PM Color: ■ Layer:	This area appears to sheet flow off-site and it is not clear this runoff will enter the proposed SFB. Suggest some type of ditch or conveyance so the runoff can make it to the SFB.