# DRAINAGE LETTER REPORT 

# for <br> SMELKER-HCI BUILDING LOT 2, PUMP IT BABY SUBDIVISION 

Prepared for:<br>Hammers Construction Inc.<br>1411 Woolsey Heights<br>Colorado Springs, CO 80915

June 2, 2022
Revised August 17, 2022

Prepared by:


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JPS Project No. 042203
PCD File No. PPR-22-037

## SMELKER-HCI BUILDING LOT 2, PUMP YT BABY SUBDIVISION DRAINAGE REPORT STATEMENTS

## 1. Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision
 prepared according to
 report:

John P ASChwab rrs or omissions on my part in preparing this

## 2. Developer's Statement:

I, the developer, have read and will comply with all the requirements specified in this drainage report and plan.

By:


Printed Name: Elliot Smith
$\frac{170<122}{\text { Date }}$

Title: Project Manger
Hammers Construction, Inc., 1411 Woolsey Heights, Colorado Springs, CO 80915

## 3. El Paso County Statement:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.

## I. INTRODUCTION

## A. Property Location and Description

Smelker Schleder LLP is planning to construct a new 9,750 square-foot commercial building on the vacant 1 -acre lot a 7920 Industry Road in El Paso County. The property is platted as Lot 2, Pump it Baby Subdivision (El Paso County Assessor's Parcel No. 53320-01-012), located at the southeast corner of Industry Road and Marksheffel Road.

The site is zoned Industrial (I-3), and the property adjoins developed commercial / industrial properties on all sides. Marksheffel Road is a fully improved arterial public road along the west boundary of the site, and Industry Road is an improved local public road along the south frontage of the property. A shared private access drive adjoins the east boundary of the site, providing access to the developed mini-warehouse facility adjoining the north boundary of the property (Lot 1, Pump it Baby Subdivision).

The lot on the east side of the shared access drive (Lot 2, Marksheffel Industrial Park) is developed with an existing distribution / warehouse building. The lot on the south side of Industry Road (Lot 18, Marksheffel Industrial Park) across from this site is also developed with existing distribution / warehouse facilities.

The proposed Site Development Plan consists of a new 9,750 square-foot single-story commercial Office / Warehouse Building with associated parking and site improvements. Access will be provided by a driveway connection to Industry Road along the southern boundary and a second driveway connection to the existing shared private drive along the eastern property boundary.

The total disturbed area associated with this project is approximately 0.9 acres. Recognizing that the land disturbance is under one acre, water quality facilities are not required as the project is not classified as an "applicable construction activity" in accordance with Section I.6.1 of the El Paso County Engineering Criteria Manual (ECM).

## B. Scope

In support of the Site Development Plan submittal to El Paso County, this report is intended to meet the requirements of a Drainage Letter Report in accordance with El Paso County drainage criteria. This report will provide a summary of site drainage issues impacting the proposed development. The report is based on the guidelines and criteria presented in the City of Colorado Springs and El Paso County "Drainage Criteria Manual."

## C. References

City of Colorado Springs \& El Paso County "Drainage Criteria Manual, Volumes 1 and 2," revised May, 2014.

Colorado Engineering \& Geotechnical Group, Inc., "Drainage Letter, 5920 \& 5950 Industry Road (addresses incorrectly labeled; report refers to 7920 \& 7950 Industry Road), March 5, 2002.

El Paso County "Engineering Criteria Manual," December 13, 2016.
Oliver E. Watts, "Drainage Report, Lot 16, Marksheffel Industrial Park," March 12, 2001.

## II. EXISTING AND PROPOSED DRAINAGE CONDITIONS

According to the Natural Resources Conservation Service (NRCS) Soil Survey for this site, on-site soils are comprised of "Blendon sandy loam" soils, and these well drained soils are classified as hydrologic soils group "B" (high infiltration rate; see Appendix A).

## Subdivision Drainage Report

Drainage planning for this site was previously addressed in the "Drainage Letter, 5920 \& 5950 Industry Road" by Colorado Engineering \& Geotechnical Group, Inc. dated March 5, 2002, which was prepared for the "Pump it Baby Subdivision" replat of a portion of Marksheffel Industrial Park (while the addresses are incorrectly listed, this drainage letter refers to the subject property addressed as 7920 \& 7950 Industry Road). The previously approved Drainage Letter by Mr. Paul R. Bryant, P.E., states:
"I have reviewed the existing, approved Final Drainage Plan for the Marksheffel Industrial Park, of which this lot is a portion (Subbasin A). This plan, authored by Simons, Li \& Associates, September 1985, calls for complete industrial development of all portions of the subdivision, with surface drainage of all flows (historic and developed) into the existing and improved drainage structures. The specified improvements appear to have been completed some years ago. The 100 -year flood is now fully contained within the improved drainage channel...."

The Colorado Engineering Drainage Letter further states the proposed drainage plan "directs the runoff into a new curb-and-gutter system along a private driveway into the existing curb and gutter system along Industry Road. This is in accordance with the approved Final Drainage Plan."

## Existing Site Drainage Conditions

As shown on the enclosed "Existing Conditions Drainage Plan" (Figure EX1), the majority of the existing Lot 2 site has been delineated as Basin A ( 0.94 acres), and surface drainage from Basin A flows southeasterly by sheet flow to Design Point \#1 at the southeast corner of the property. The Lot 2 site is impacted by off-site drainage from the parking area on the adjoining Lot 1 . The existing gravel parking area on the south side of the adjoining Lot 1 (delineated as Basin OA1 on Sh. EX1) sheet flows southeasterly towards the north boundary of the subject Lot 2. Drainage from Basins OA1 and A combines at Design Point \#1, with existing peak flows calculated as $\mathrm{Q}_{5}=3.8$ cfs and $\mathrm{Q}_{100}=9.1 \mathrm{cfs}$.

Drainage from Design Point \#1 flows easterly along the existing curb and gutter on the north side of Industry Road to the existing concrete-lined East Fork Sand Creek Subtributary Channel east of the property (east side of Lot 3, Marksheffel Industrial Park).

The west edge of the site has been delineated as Basin B ( 0.06 acres), and surface drainage from Basin B flows southwesterly to the existing 24" RCP culvert at Design Point \#2 at the southwest corner of the property. Existing peak flows at Design Point \#2 are calculated as $\mathrm{Q}_{5}=0.02 \mathrm{cfs}$ and $\mathrm{Q}_{100}=0.14 \mathrm{cfs}$.

## Proposed Site Drainage Conditions

As shown on the enclosed Drainage Plan (Figure D1), the developed area of this project is limited to approximately 0.9 acres. The majority of the developed site has been delineated as Basin A ( 0.83 acres), and surface drainage from Basin A will flow southeasterly by sheet flow, drainage swales, and curb and gutter to Design Point \#1 at the southeast corner of the property. Developed flows from Basins OA1 and A will combine at Design Point \#1, with developed peak flows calculated as $\mathrm{Q}_{5}=6.0 \mathrm{cfs}$ and $\mathrm{Q}_{100}=11.6 \mathrm{cfs}$.

Developed drainage from Design Point \#1 will continue to flow easterly along the existing curb and gutter on the north side of Industry Road to the existing concrete-lined East Fork Sand Creek Subtributary Channel east of the property. The Drainage Plan for Marksheffel Industrial Park identified peak flows of $\mathrm{Q}_{5}=14.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=24.5 \mathrm{cfs}$ for Design Point A (original Lots 1-3 of Marksheffel Industrial Park, which include the subject property). Industry Road provides an allowable street capacity of $\mathrm{Q}_{5}=14.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=127.5 \mathrm{cfs}$, providing a suitable outfall for drainage from this site with adequate capacity to convey the combined developed flows to the drainage channel.

The landscaped area along the west boundary of the site has been delineated as Basin B ( 0.17 acres), and surface drainage from Basin $B$ will flow southwesterly to the existing $24 "$ RCP culvert at Design Point \#2 at the southwest corner of the property. Developed peak flows at Design Point \#2 are calculated as $\mathrm{Q}_{5}=0.05 \mathrm{cfs}$ and $\mathrm{Q}_{100}=0.39 \mathrm{cfs}$, representing a negligible flow contribution to the existing 24 -inch RCP public Storm Sewer in the southwest corner of the site. As noted on Sh. D1, a riprap apron will be installed to dissipate flows from the proposed drainage swale at the northwest corner of the new building, and the project will re-seed the existing ditch area for stabilization along the west edge of the property.

The calculated impervious area of the proposed site development is 0.72 acres ( 72.0 percent of the overall site), which is below the presumed impervious percentage of 80 percent for light industrial areas in DCM Table 6-6. As such, the proposed development is fully consistent with the "complete industrial development" planned for the Marksheffel Industrial Park, with a slightly lower drainage impact based on the reduced impervious area.

Hydrologic calculations for the site are detailed in the attached spreadsheets (Appendix A), and peak flows are identified on Figures EX1 and D1 (Appendix A).

## III. DRAINAGE PLANNING FOUR STEP PROCESS

El Paso County Drainage Criteria require drainage planning to include a Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls. The Four Step Process has been implemented as follows in the planning of this project:

## Step 1: Employ Runoff Reduction Practices

- Minimize Impacts: The proposed site development consists of a new commercial building on a previously platted commercial lot which has been planned for full industrial development. This infill project will have minimal drainage impacts in comparison to new development of an unplatted site.


## Step 2: Stabilize Drainageways

- There are no drainage channels directly adjacent to this project site. The existing drainage ditch along the west side of the property will be re-seeded for stabilization.
- The existing East Fork Sand Creek Subtributary Channel downstream of this property is a stable, concrete-lined channel.


## Step 3: Provide Water Quality Capture Volume (WQCV)

- This site is excluded from permanent Water Quality control measure requirements based on the disturbed area remaining under one acre.


## Step 4: Consider Need for Industrial and Commercial BMPs

- The Owner is responsible for maintaining proper housekeeping practices and spill containment procedures.


## IV. FLOODPLAIN IMPACTS

Floodplain limits in vicinity of this site are delineated in the applicable Flood Insurance Rate Map, FIRM Panel No. 08041C0543G dated December 7, 2018 (FIRM exhibit enclosed in Appendix A), which has been revised by Letter of Map Revision (LOMR) 20-08-0548P dated June 1, 2021. This site is not impacted by the delineated 100-year FEMA floodplain.

## V. STORMWATER DETENTION AND WATER QUALITY

No stormwater detention is required based on the previous drainage planning for this industrial park having accounted for higher impervious areas than currently proposed. As previously discussed, this site is excluded from water quality control measure requirements based on the disturbed area being smaller than one acre. A future change in I-3 Industrial zoning special or allowed use type may result in future water quality facilities or permanent control measures being required.

## VI. DRAINAGE BASIN FEES

The site lies within the Sand Creek Drainage Basin. No public drainage improvements are required for development of this site. Required drainage fees have been paid during the previous subdivision platting process, so there are no applicable drainage fees required with the Site Development Plan.

## VII. SUMMARY

The developed drainage patterns associated with the proposed Smelker-HCI Building at 7920 Industry Road (Lot 2, Pump it Baby Subdivision) will remain consistent with the established drainage conditions for this subdivision. The existing stormwater outfalls are functioning properly, including the drainage ditch and 24 " RCP public storm sewer along the west boundary of the site and the existing street and drainage system along Industry Road flowing east to the East Fork Sand Creek Subtributary Channel. Proper establishment and maintenance of positive drainage within the site, in conjunction with proper erosion control practices, will ensure that this developed site has no significant adverse impact on downstream or surrounding areas.

## APPENDIX A

DRAINAGE CALCULATIONS \& FIGURES





## Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| :--- | :---: | :---: | ---: | ---: |
| 10 | Blendon sandy loam, 0 <br> to 3 percent slopes | B | 0.9 | $100.0 \%$ |
| Totals for Area of Interest | $\mathbf{0 . 9}$ | $\mathbf{1 0 0 . 0 \%}$ |  |  |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

| Land Use or Surface Characteristics | Percent Impervious | Runoff Coefficients |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2-year |  | 5-year |  | 10-year |  | 25-year |  | 50-year |  | 100-year |  |
|  |  | HSG A\&B | HSG C\&D | HSG A\&B | HSG C\&D | HSG A\&B | HSG C\&D | HSG A\&B | HSG C\&D | HSG A\&B | HSG C\&D | HSG A\&B | HSG C\&D |
| Business |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Commercial Areas | 95 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.87 | 0.88 | 0.88 | 0.89 |
| Neighborhood Areas | 70 | 0.45 | 0.49 | 0.49 | 0.53 | 0.53 | 0.57 | 0.58 | 0.62 | 0.60 | 0.65 | 0.62 | 0.68 |
| Residential |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1/8 Acre or less | 65 | 0.41 | 0.45 | 0.45 | 0.49 | 0.49 | 0.54 | 0.54 | 0.59 | 0.57 | 0.62 | 0.59 | 0.65 |
| 1/4 Acre | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
| 1/3 Acre | 30 | 0.18 | 0.22 | 0.25 | 0.30 | 0.32 | 0.38 | 0.39 | 0.47 | 0.43 | 0.52 | 0.47 | 0.57 |
| 1/2 Acre | 25 | 0.15 | 0.20 | 0.22 | 0.28 | 0.30 | 0.36 | 0.37 | 0.46 | 0.41 | 0.51 | 0.46 | 0.56 |
| 1 Acre | 20 | 0.12 | 0.17 | 0.20 | 0.26 | 0.27 | 0.34 | 0.35 | 0.44 | 0.40 | 0.50 | 0.44 | 0.55 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Industrial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Light Areas | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
| Heavy Areas | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Parks and Cemeteries | 7 | 0.05 | 0.09 | 0.12 | 0.19 | 0.20 | 0.29 | 0.30 | 0.40 | 0.34 | 0.46 | 0.39 | 0.52 |
| Playgrounds | 13 | 0.07 | 0.13 | 0.16 | 0.23 | 0.24 | 0.31 | 0.32 | 0.42 | 0.37 | 0.48 | 0.41 | 0.54 |
| Railroad Yard Areas | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Undeveloped Areas |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Historic Flow Analysis-Greenbelts, Agriculture | 2 | 0.03 | 0.05 | 0.09 | 0.16 | 0.17 | 0.26 | 0.26 | 0.38 | 0.31 | 0.45 | 0.36 | 0.51 |
| Pasture/Meadow | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Forest | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Exposed Rock | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Offsite Flow Analysis (when landuse is undefined) | 45 | 0.26 | 0.31 | 0.32 | 0.37 | 0.38 | 0.44 | 0.44 | 0.51 | 0.48 | 0.55 | 0.51 | 0.59 |
| Streets |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Paved | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Gravel | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drive and Walks | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Roofs | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
| Lawns | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |

### 3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration $\left(t_{c}\right)$ consists of an initial time or overland flow time $\left(t_{i}\right)$ plus the travel time $\left(t_{t}\right)$ in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time $\left(t_{i}\right)$ plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion $\left(t_{t}\right)$ of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$
\begin{equation*}
t_{c}=t_{i}+t_{t} \tag{Eq.6-7}
\end{equation*}
$$

Where:
$t_{c}=$ time of concentration (min)
$t_{i}=$ overland (initial) flow time (min)
$t_{t}=$ travel time in the ditch, channel, gutter, storm sewer, etc. (min)

### 3.2.1 Overland (Initial) Flow Time

The overland flow time, $t_{i}$, may be calculated using Equation 6-8.

$$
\begin{equation*}
t_{i}=\frac{0.395\left(1.1-C_{5}\right) \sqrt{L}}{S^{0.33}} \tag{Eq.6-8}
\end{equation*}
$$

Where:
$t_{i}=$ overland (initial) flow time (min)
$C_{5}=$ runoff coefficient for 5-year frequency (see Table 6-6)
$L=$ length of overland flow ( $300 \mathrm{ft} \underline{\text { maximum }}$ for non-urban land uses, $100 \mathrm{ft} \underline{\text { maximum }}$ for urban land uses)
$S=$ average basin slope ( $\mathrm{ft} / \mathrm{ft}$ )
Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

### 3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, $t_{t}$, which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, $t_{t}$, can be estimated with the help of Figure 625 or Equation 6-9 (Guo 1999).

$$
\begin{equation*}
V=C_{v} S_{w}^{0.5} \tag{Eq.6-9}
\end{equation*}
$$

Where:
$V=$ velocity ( $\mathrm{ft} / \mathrm{s}$ )
$C_{v}=$ conveyance coefficient (from Table 6-7)
$S_{w}=$ watercourse slope ( $\mathrm{ft} / \mathrm{ft}$ )

Table 6-7. Conveyance Coefficient, $C_{v}$

| Type of Land Surface | $\boldsymbol{C}_{\boldsymbol{v}}$ |
| :--- | :---: |
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried) |  |
| Short pasture and lawns | 6.5 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |

${ }^{*}$ For buried riprap, select $\mathrm{C}_{\mathrm{v}}$ value based on type of vegetative cover.
The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration $\left(t_{c}\right)$ is then the sum of the overland flow time $\left(t_{i}\right)$ and the travel time $\left(t_{t}\right)$ per Equation 6-7.

### 3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation $6-10$. The first design point is defined as the point where runoff first enters the storm sewer system.

$$
\begin{equation*}
t_{c}=\frac{L}{180}+10 \tag{Eq.6-10}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& t_{c}=\text { maximum time of concentration at the first design point in an urban watershed (min) } \\
& L=\text { waterway length }(\mathrm{ft})
\end{aligned}
$$

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

### 3.2.4 Minimum Time of Concentration

If the calculations result in a $t_{c}$ of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum $t_{c}$ for urbanized areas is 5 minutes.

### 3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency


| IDF Equations |
| :---: |
| $\mathbf{I}_{100}=\mathbf{- 2 . 5 2} \ln (D)+\mathbf{1 2 . 7 3 5}$ |
| $\mathbf{I}_{50}=\mathbf{- 2 . 2 5} \ln (D)+\mathbf{1 1 . 3 7 5}$ |
| $\mathbf{I}_{25}=\mathbf{- 2 . 0 0} \ln (D)+\mathbf{1 0 . 1 1 1}$ |
| $\mathbf{I}_{\mathbf{1 0}}=\mathbf{- 1 . 7 5} \ln (D)+\mathbf{8 . 8 4 7}$ |
| $\mathbf{I}_{\mathbf{5}}=\mathbf{- 1 . 5 0} \ln (\mathrm{D})+\mathbf{7 . 5 8 3}$ |
| $\mathbf{I}_{\mathbf{2}}=\mathbf{- 1 . 1 9} \ln (\mathrm{D})+\mathbf{6 . 0 3 5}$ |
| Note: Values calculated by |
| equations may not precisely |
| duplicate values read from figure. |

SMELKER-HCI BUILDING - LOT 2, PUMP IT BABY SUBDIVISION


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|  |  |  |  | c |  |  |  | CHANNEL | CONVEYANCE |  | SCS ${ }^{(2)}$ |  | TOTAL | TOTAL | INTE | ITY ${ }^{(5)}$ | PEAK | OW |
| BASIN | $\begin{gathered} \text { DESIGN } \\ \text { POINT } \\ \hline \end{gathered}$ | AREA $(\mathrm{AC})$ | 5-YEAR | 100-YEAR | $\begin{array}{\|c\|} \hline \text { LENGTH } \\ \text { (FT) } \\ \hline \end{array}$ | SLOPE (FT/FT) | $\begin{aligned} & \text { Tco }^{(1)} \\ & \text { (MIN) } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { LENGTH } \\ (\mathrm{FT}) \\ \hline \end{gathered}$ | $\begin{gathered} \text { COEFFICIENT } \\ \text { C } \\ \hline \end{gathered}$ | SLOPE <br> (FT/FT) | $\begin{gathered} \text { VELOCITY } \\ \text { (FT/S) } \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{Tt}^{(3)} \\ & \text { (MIN) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{Tc}^{(4)} \\ & (\mathrm{MIN}) \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{Tc}^{(4)} \\ & \text { (MIN) } \\ & \hline \end{aligned}$ | $\begin{gathered} 5-\mathrm{YR} \\ \text { (IN/HR) } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { 100-YR } \\ & \text { (IN/HR) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Q5 }^{(6)} \\ & \text { (CFS) } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { Q100 }^{(6)} \\ \text { (CFS) } \\ \hline \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| OA1 | OA1 | 1.59 | 0.590 | 0.700 | 100 | 0.010 | 9.3 | 200 | 20 | 0.01 | 2.00 | 1.7 | 11.0 | 11.0 | 3.99 | 6.69 | 3.74 | 7.45 |
| A | A | 0.94 | 0.080 | 0.350 | 40 | 0.020 | 9.4 | 255 | 20 | 0.013 | 2.28 | 1.9 | 11.2 | 11.2 | 3.95 | 6.64 | 0.30 | 2.18 |
| OA1,A | 1 | 2.53 | 0.401 | 0.570 |  |  |  |  |  |  |  |  | 12.9 | 12.9 | 3.75 | 6.30 | 3.81 | 9.08 |
| B | 2 | 0.06 | 0.080 | 0.350 | 40 | 0.020 | 9.4 | 210 | 15 | 0.015 | 1.84 | 1.9 | 11.3 | 11.3 | 3.95 | 6.63 | 0.02 | 0.14 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

DEVELOPED FLOWS

|  |  |  |  |  |  | erland FI |  |  | Cha | nel flow |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | c |  |  |  | CHANNEL | CONVEYANCE |  | SCS ${ }^{(2)}$ |  | TOTAL | TOTAL | INTEN | ITY ${ }^{(5)}$ | PEAK | OW |
| BASIN | $\begin{array}{\|c\|} \hline \text { DESIGN } \\ \text { POINT } \\ \hline \end{array}$ | AREA $(\mathrm{AC})$ | 5-YEAR | 100-YEAR | $\begin{gathered} \text { LENGTH } \\ \text { (FT) } \\ \hline \end{gathered}$ | SLOPE <br> (FT/FT) | Tco ${ }^{(1)}$ <br> (MIN) | $\begin{gathered} \text { LENGTH } \\ \text { (FT) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { COEFFICIENT } \\ \text { C } \\ \hline \end{gathered}$ | SLOPE (FT/FT) | $\begin{gathered} \text { VELOCITY } \\ \text { (FT/S) } \\ \hline \end{gathered}$ | $\mathrm{Tt}^{(3)}$ <br> (MIN) | $\begin{aligned} & \mathrm{Tc}^{(4)} \\ & (\mathrm{MIN}) \\ & \hline \end{aligned}$ | Tc ${ }^{(4)}$ (MIN) | $\begin{gathered} \text { 5-YR } \\ \text { (IN/HR) } \end{gathered}$ | 100-YR <br> (IN/HR) | $\begin{aligned} & \text { Q5 }{ }^{(6)} \\ & \text { (CFS) } \end{aligned}$ | $\begin{gathered} \text { Q100 }^{(6)} \\ \text { (CFS) } \\ \hline \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| OA1 | OA1 | 1.59 | 0.590 | 0.700 | 100 | 0.010 | 9.3 | 200 | 20 | 0.01 | 2.00 | 1.7 | 11.0 | 11.0 | 3.99 | 6.69 | 3.74 | 7.45 |
| A | A | 0.83 | 0.791 | 0.879 | 40 | 0.020 | 2.8 | 255 | 20 | 0.013 | 2.28 | 1.9 | 4.7 | 5.0 | 5.17 | 8.68 | 3.39 | 6.33 |
| OA1,A | 1 | 2.42 | 0.659 | 0.761 |  |  |  |  |  |  |  |  | 12.9 | 12.9 | 3.75 | 6.30 | 5.98 | 11.60 |
| B | 2 | 0.17 | 0.080 | 0.350 | 40 | 0.020 | 9.4 | 210 | 15 | 0.015 | 1.84 | 1.9 | 11.3 | 11.3 | 3.95 | 6.63 | 0.05 | 0.39 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

1) $\operatorname{OVERLAND~FLOW~} \operatorname{Tco}=\left(0.395^{*}(1.1-R U N O F F \operatorname{COEFFICIENT})^{\star}\left(O V E R L A N D ~ F L O W ~ L E N G T H \wedge(0.5) /\left(\operatorname{SLOPE}^{\wedge}(0.333)\right)\right.\right.$
2) SCS VELOCITY $=C^{*}$ ((SLOPE(FT/FT)^0.5)
$=5$ FOR TILLAGE/FIELD
$C=5$ FOR TILLAGE/FIELD
$C=7$ FOR SHORT PASTURE AND LAWNS
$C=10$ FOR NEARLY BARE GROUND
$C=15$ FOR GRASSED WATERWAY
$C=20$ FOR PAVED AREAS AND SHALIOW PAV
$C=15$ FOR GRASSED WATERWAY
$C=20$ FOR PAVED AREAS AND SHALLOW PAVED SWALES
EXISTING CONDITION FLOWS
3) $\operatorname{SCS}$ VELOCITY $=C^{*}\left(\left(S L O P E(F T / F T)^{\wedge} 0.5\right)\right.$
[^0]Version 4.05 Released March 2017


## National Flood Hazard Layer FIRMette

10441'13"W 3853'6"N


## Legend

SEE PIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT
$\left.\begin{array}{l|l|l|}\hline \begin{array}{l|l}\text { SPECIAL FLOOD } \\ \text { HAZARD AREAS }\end{array} & \begin{array}{l}\text { Without Base Flood Elevation (BFE) } \\ \text { Zone A, } V \text {, A99 } \\ \text { With BFE or Depth Zone AE, AO, AH, VE, AR }\end{array} \\ \text { Regulatory Floodway }\end{array}\right]$

B- 20.2 Cross Sections with 1\% Annual Chance
17.5 Water Surface Elevation
mu 513 mm Base Flood Elevation Line (BFE)
Limit of Study
__ Jurisdiction Boundary
--- --- Coastal Transect Baseline
OTHER
FEATURES $\qquad$ Profile Baseline
$\qquad$

MAP PANELS

## 6 Digital Data Available

$\square$ No Digital Data Available
 Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The baseman shown complies with FEMA's baseman accuracy standards
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/2/2022 at 1:24 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: baseman imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.




[^0]:    3) MANNING'S CHANNEL TRAVEL TIME = L/V (WHEN CHANNEL VELOCITY IS KNOWN)

    4** IF TOTAL TIME OF CONCENTRATION IS LESS THAN 5 MINUTES, THEN 5 MINUTES IS USED
    5) INTENSITY BASED ON I-D-F EQUATIONS IN CITY OF COLORADO SPRINGS DRAINAGE CRITERIA MANUAL
    $\begin{array}{rl} & \mathrm{I}_{5}=-1.5 * \ln (\mathrm{Tc})+7.583 \\ \mathrm{I}_{100}=-2.52 & * \ln (\mathrm{Tc})+12.735 \\ \text { 6) } \mathrm{Q}= & \mathrm{CiA}\end{array}$

    $$
    \begin{aligned}
    & \mathrm{I}_{100}=-2.52 * \ln (\mathrm{Tc})+12.735 \\
    & \text { 6) } \mathrm{Q}=\mathrm{CiA}
    \end{aligned}
    $$

