

# **FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY, COLORADO**

**Prepared for:**

Doubletree Ventures  
106 S. Kyrene Road #2  
Chandler, AZ 85226  
(480) 313-2724

**Prepared by:**

M&S Civil Consultants  
212 N. Wahsatch Avenue  
Suite 305  
Colorado Springs, CO 80903 (719) 955-5485

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Project #10-020  
PCD Filing No.: **VR233**

**PCD FILING NO. VR233 ADDED**



# FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO

## DRAINAGE PLAN STATEMENTS

### ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

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Virgil A. Sanchez, P.E. #37160  
For and on Behalf of M&S Civil Consultants, Inc

### DEVELOPER'S STATEMENT

I, the developer(s) have read and will comply with all the requirements specified in this drainage report and plan.

BY: \_\_\_\_\_

TITLE: \_\_\_\_\_ DATE: \_\_\_\_\_

ADDRESS: Brian Zurek  
106 S. Kryene Road  
Chandler, AZ 85226

### EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Joshua Palmer, P.E.  
~~Interim~~ County Engineer / ECM Administrator

CONDITIONS.

Remove

INTERIM REMOVED

# **FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO**

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Move Ex & Pr Drainage Maps to back of report

**REVISED EX & PROP MAPS MOVED  
TO THE BACK OF THE REPORT.**

# **FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO**

## **Purpose**

This Final Drainage Report for Claremont Business Park 2 Filing No. 2 is in support of the Final Plat, Preliminary Plan, and Construction Drawings of the subject site. This report functions to identify the existing and proposed runoff patterns and recommend proposed drainage improvements which are intended to safely convey runoff through the proposed development, while minimizing impacts to downstream facilities and adjacent properties. The analysis has been prepared in accordance with the requirements set forth by El Paso County and remains in compliance with the Final Drainage Report for Claremont Business Park 2 Filing No. 1 by M&S Civil Consultants.

## **General Location and Description**

The Claremont Business Park 2 Filing No.2 is a Replat of Lots 8, 9 & 10 and Tract B of Claremont Business Park 2 Filing No.1. The site is located in the Northeast  $\frac{1}{4}$  of the Northeast  $\frac{1}{4}$  of Section 8, and the Southeast  $\frac{1}{4}$  of the Southeast  $\frac{1}{4}$  of Section 5, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The site is bordered to the southeast by U.S. Highway 24 and to the northeast by N. Marksheffel Road, to the north and west by Meadowbrook Parkway, and to the south by Claremont Business Park 2 Filing No. 1 (Lots 1-7). See Vicinity Map in Appendix for details.

The site consists of 4.988 acres which is currently vacant land. The replat will eliminate Tract B and redistribute the three (3) lots based around a newly aligned private roadway. The development project will construct a roadway and utilities through the site and into Filing 1. An existing access easement which is a portion of existing Lots 6 and 7 will allow for the proposed roadway to connect to the existing roadway (Gary Watson Point.) The Claremont Business Park 2 Filing 2 site is currently zoned "CS" and the proposed principal use for the site will be neighborhood commercial and light industrial.

In addition to the construction of the roadway and utilities, a storm sewer system will be constructed that will function to collect runoff from the future lots and a single (1) sand filter basin water quality pond will initially be provided to treat runoff from aforementioned improvements. The proposed storm sewer will tie into an existing system near Meadowbrook Parkway, which ultimately conveys runoff southwest into the East Fork of Sand Creek.

Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required. (refer to appendix).

Individual drainage letters and/or reports shall be required with the development of each lot not otherwise clearly analyzed by this report for Claremont Business Park 2 Filing No. 2.

## **Soils**

The Natural Resources Conservation Service, United States Department of Agriculture, Web Soil Survey, indicates that the soils for this project are: Blakeland Loamy Sand (8), Blendon Sandy Loam (10) and Ellicott Loamy Course Sand (28). These soils have been characterized as having Hydrologic Soil Types "A" & "B". The soils classification used for this study is "B". Refer to the Soils Map located in the Appendix of this report

## **Previous Studies**

The proposed site and surrounding existing drainage facilities have been included in multiple drainage letters and reports. The following is a list of existing documents that were pertinent to analyzing this site.

- Falcon Drainage Basin Planning Study, by Matrix Design Group, dated September 2015.
- Final Drainage Report for Claremont Business Park Filing No.2, by Matrix Design Group, Inc. dated November 2006.
- Final Drainage Report for Claremont Business Park 2 Filing No. 1, by M&S Civil Consultants, approved 2/11/2021.
- Final Drainage Letter for Lot 1 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 4/01/2021.
- Final Drainage Letter for Lot 2 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 5/19/2021.
- Final Drainage Letter for Lot 3 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 05/19/2021.
- Final Drainage Letter for Lot 4 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 05/19/2021.
- Final Drainage Letter for Lot 5 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 03/03/2021.
- Final Drainage Letter for Lot 6 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 07/08/2021.
- Final Drainage Letter for Lot 7 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 3/31/2021.

## **Drainage Criteria**

As required by El Paso County, Colorado, this report has been prepared in accordance to the criteria set forth in the El Paso County Drainage Criteria Manual Volume 1 & 2 (DCM), the El Paso County Engineering Criteria Manual (ECM), and El Paso County Resolutions 15-042 and 19-245.

## **Design Event Frequency**

The 100-year storm event was used as the major storm for the project, and the 5-year storm event was used as the minor storm.

## **Method of Analysis**

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres.

Where:  $Q=C*i*A$

$Q$  = Maximum runoff rate in cubic feet per second (cfs)

$C$  = Runoff coefficient

$i$  = Average rainfall intensity (inches per hour)

$A$  = Area of drainage sub-basin (acres)

## **Runoff Coefficient**

Rational Method coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. Composite percent impervious and C values were calculated using roofs, commercial areas, asphalt drives, landscaped areas and parks found within the aforementioned table.

## **Time of Concentration**

The time of concentration consists of the initial time of overland flow and the travel time (street or channel, etc) to a downstream structure or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas.

## **Rainfall Intensity**

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Drainage Criteria Manual.

Project 1-Hour Rainfall Depth Storm Recurrence Interval Rainfall Depth (inches)

5-year 1.50" 100-year 2.52"

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

## **Hydraulic Grade Line Analysis**

StormCAD was utilized to analyze the proposed storm sewer system and determine the Hydraulic Grade Line (HGL's) profiles for the major and minor storms. The standard method was used to calculate head loss in the system with K coefficients taken from Table 9-4 of the Colorado Springs DCM.

In addition to the DCM, The Mile High Flood District BMP Sizing (UD-BMPv.3.07) and Detention Design (MHFD Detention v4.06) worksheets were utilized for to check to verify the existing the water quality

ponds still functions with the revised tributary areas and impervious values. These spreadsheets were also utilized for the design of the proposed and future on-site water quality ponds. The MFHD-Inlet v5.02 worksheet was utilized to calculate both the street capacities and evaluate inlet capacities.

## Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0756G, revised December 7, 2018. No portion of this site is located within the 100 year floodplain. See Appendix.

## Existing Drainage Conditions

As the site has been graded previously with the development of Filing 1, the vegetation is sparse, consisting primarily of native grasses and weeds. Existing site terrain generally slopes from north to southwest at grade rates that vary between 1.2% and 2%. A soil retention wall runs along the eastside of the proposed site, next to U.S. Highway 24 and N. Marksheffel Road, and borders a large portion of the back of the proposed lots. A depression or sediment pond is located in the southwest corner of the site, which was to serve as a future singular water quality pond for the 3 future lots. An existing 24" ADS private storm drain has been constructed along the east side of Meadowbrook Parkway that extends to this existing sediment pond. This pipe will serve as the outfall for the proposed site development.

As the proposed project will construct street improvements within Lots 6 and 7 of Claremont Business Park Filing No. 1, the existing and proposed drainage analysis will be expanded to evaluate changes in drainage patterns to ensure no negative affects to downstream facilities. An existing conditions drainage map is included in the appendix of this report to accompany the following discussion.

### Existing Conditions Detailed Drainage Discussion

**Design Point 1** ( $Q_5 = 1.8 \text{ cfs}$ ,  $Q_{100} = 11.8 \text{ cfs}$ ) consists of runoff from undeveloped **Basins A, B, and C**. **Basins A** and **B** are 0.19 and 0.30 acres of existing roadway embankment located generally between the subject site and existing US. Hwy 24 and Marksheffel Road. **Basin C** consists of 4.90 acres of that generally consist of the remaining undeveloped portions of the subject site. Runoff from the three basins is conveyed to an existing sediment pond located in the southwest corner of the site at DP1.

An existing 24" ADS (Pipe 11) is located at the southwest corner of the pond which collects runoff.

**Design Point 2** was omitted.

**Design Point 3** ( $Q_5 = 2.2 \text{ cfs}$ ,  $Q_{100} = 4.4 \text{ cfs}$ ) consists of runoff from **Basin H1** and **Basin I1**. **Basin H1** is 0.18 acres of undeveloped roadway embankment and **Basin I1** consists 0.57 acres of roof top, asphalt paving and landscaped areas. Runoff from the two basins flow into an existing 3.0 foot wide x 6 inch high concrete chase with 6 inch curb heights which discharges into the cul-de-sac of Gary Watson Point.



CONCRETE CHASE LABELED.

**Design Point 4** ( $Q_5 = 1.8 \text{ cfs}$ ,  $Q_{100} = 4.1 \text{ cfs}$ ) consists of runoff from **Basin H2** and **Basin I2**. **Basin H2** is 0.40 acres of undeveloped roadway embankment and **Basin I2** consists 0.48 acres of asphalt paving and landscaped areas. Runoff from basins is collected in curb and gutter which discharges into the cul-de-sac of Gary Watson Point.

**Design Point 5** ( $Q_5 = 0.8 \text{ cfs}$ ,  $Q_{100} = 1.6 \text{ cfs}$ ) consists of runoff from **Basin H3** and **Basin I7**. **REVISED TO DP3-5** 0.04 acres of undeveloped roadway embankment and **Basin I7** consists 0.23 acres of asphalt paving and landscaped areas. Runoff from basins is collected in curb and gutter which discharges into the **DP3 thru 5 per hydrology spreadsheet** sac of Gary Watson Point. **REVISED TO EX WQ POND 2**

**Design Point 6** ( $Q_5 = 8.2 \text{ cfs}$ ,  $Q_{100} = 16.5 \text{ cfs}$ ) consists of runoff from **Basin I3, I4, I5, I6** and **DP1-3**. **Basins I3, I4, I5, and I6** are of 0.58, 0.43, 0.23, and 0.19 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the four basins combines with flows from **DP1-3** within the private street section of Gary Watson. Runoff is collected by a pair of existing 15' Type R at grade inlets located at **DP6**. Collected runoff is conveyed to the west underground via private 24" storm sewer to an existing WQ pond (**PR13-14**). **Inlet 3** collects  $Q_5=4.1$  and  $Q_{100}=7.9 \text{ cfs}$ , with  $Q_5=0.0 \text{ cfs}$  and  $Q_5=0.4 \text{ cfs}$  of flow-by in the respective storm events. **Inlet 4** collects  $Q_5=4.1$  and  $Q_{100}=8.0 \text{ cfs}$ , with  $Q_5=0.0 \text{ cfs}$  and  $Q_5=0.3 \text{ cfs}$  of flow-by in the respective storm events. Runoff bypassing the existing inlets continues westward to **Design Point 7** and **8**.

**Design Point 7** ( $Q_5 = 2.4 \text{ cfs}$ ,  $Q_{100} = 7.5 \text{ cfs}$ ) consists of flow-by runoff from **Inlet 3** and flows within **Basin J1**. **Basin J1** consists 0.76 acres of rooftop, asphalt paving and landscaped areas. Runoff from **Basin J1** and flow-by from the inlet is conveyed within the curb and gutter to an existing 15' Type R at grade inlets located at **DP7**. **Inlet 5** collects  $Q_5=2.4$  and  $Q_{100}=7.3 \text{ cfs}$ , with  $Q_5=0.0 \text{ cfs}$  and  $Q_5=0.2 \text{ cfs}$  of flow-by in the respective storm events. An existing 18" storm sewer (**PR15**) conveys the in**REVISED TO Q100** runoff underneath Gary Watson.

**Design Point 8** ( $Q_5 = 0.9 \text{ cfs}$ ,  $Q_{100} = 4.1 \text{ cfs}$ ) consists of flow-by runoff from **Inlet 4** and flows within **Basin J2 and J3**. **Basins J2 and J3** are of 0.25 and 0.01 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. Runoff from **Basins J2 and J3** and flow-by from the inlet is conveyed within the curb and gutter to an existing 15' Type R at grade inlets located at **DP8**. **Inlet 6** collects  $Q_5=0.9$  and  $Q_{100}=4.1 \text{ cfs}$ , with no flow-by in either of the storm events. An existing 18" storm sewer (**PR16**) conveys the intercepted runoff from the pair of inlets southward underground.

**Design Point 9** ( $Q_5 = 3.8 \text{ cfs}$ ,  $Q_{100} = 9.7 \text{ cfs}$ ) consists of runoff from **Basin H4, L and M4**. **Basin H4** and **L** are 0.10 and 1.32 acres of undeveloped roadway embankment and **Basin M4** consists of 0.98 acres of roof top, asphalt paving and landscaped areas. Runoff from the three basins flow into an existing a 2' foot trapezoidal channel located at the south end of the property.

**Design Point 10** ( $Q_5 = 5.3 \text{ cfs}$ ,  $Q_{100} = 12.3 \text{ cfs}$ ) consists of runoff from **Basin M2, M3 and DP9**. **Basins M2 and M3** are of 0.24 and 0.37 acres in size respectively and consist of roof top, asphalt paving and

landscaped areas within the development. Runoff from the two basins combine with **DP9** flows in an existing a 2' foot trapezoidal channel located at the south end of the property. Runoff at **DP10** will enter the existing Filing 1 **WQ Pond 2** via an existing trapezoidal grouted riprap rundown.

**Design Point 11** ( $Q_5 = 1.4 \text{ cfs}$ ,  $Q_{100} = 2.5 \text{ cfs}$ ) consists of runoff from **Basin M1** and **K4**. **Basins M1** and **K4** are of 0.28 and 0.05 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the two basins is directed into the existing **WQ Pond 2** via an existing concrete rundown at **DP11**.

**Design Point 12** ( $Q_5 = 1.1 \text{ cfs}$ ,  $Q_{100} = 2.0 \text{ cfs}$ ) consists of runoff from **Basin K2**, **K3** and **N1**. **Basins K2**, **K3** and **N1** are of 0.05, 0.15 and 0.06 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the **t3** basins is directed into the existing **WQ Pond 2** via an existing concrete rundown at **DP12**. **REVISED TO 3**

**Design Point 13** ( $Q_5 = 0.7 \text{ cfs}$ ,  $Q_{100} = 1.3 \text{ cfs}$ ) consists of runoff from **Basin K1**. **Basins K1** is 0.17 acres in size and consists of roof top, asphalt paving and landscaped areas within the development. The runoff from the basins is directed to an existing beehive grated manhole located in the southwest corner of the lot. Runoff collect by the inlet combines with flows conveyed by **PR12**, in **PR13** a private 24" storm sewer that outfalls into **WQ Pond 2**.

Is this Inlet 7 as labeled on the existing drainage map? If so, please include the name in the text.

**INSERT INLET 7  
INTO STATEMENT**

**Design Point 14** ( $Q_5 = 19.3 \text{ cfs}$ ,  $Q_{100} = 43.9 \text{ cfs}$ ) consists of runoff from **Basin N2** and **DP10-13**. **Basins N2** is 0.41 acres in size and consists of a sand filter water quality pond (**WQ Pond 2**).

#### **Basin D, O1, O2,**

**Basins D, O1, and O2** are 0.23, 0.12 and 0.06 acres in size and consist of asphalt, concrete, and landscaped areas along the western periphery of the development. The runoff from the three basins is directed to Existing Meadowbrook Parkway. The 5 year event and 100 year event peak runoff rates from Basin **D, 01**, and **O2** are  $Q_5 = 0.1 \text{ cfs}$ ,  $Q_{100} = 0.7 \text{ cfs}$ ,  $Q_5 = 0.1 \text{ cfs}$ ,  $Q_{100} = 0.4 \text{ cfs}$  and  $Q_5 = 0.1 \text{ cfs}$ ,  $Q_{100} = 0.3 \text{ cfs}$  respectively.

#### **Basin P**

**Basins P** ( $Q_5 = 0.0 \text{ cfs}$ ,  $Q_{100} = 0.3 \text{ cfs}$ ) is 0.11 acres in size and consists of landscaped and undeveloped areas along the southern periphery of the development. The runoff from the basins is directed to the adjacent development.

### **Four Step Process**

The development will follow the "Four Step Process" as outlined below:

#### **Step 1 - Employ Runoff Reduction Practices**

The proposed development uses Low Impact Development (LID) practices to reduce runoff. When possible runoff is to be directed to pervious areas to promote infiltration and limit directly connected impervious areas. .

### **Step 2 - Stabilize Drainageways**

There are no drainageways on-site to stabilize. The site is upstream of an existing 42"/48" RCP storm sewer system that discharges directly into the Sand Creek Channel via an outlet structure with wingwalls (privately owned and maintained by the Central Marksheffel Metropolitan District). The Claremont Commercial Filing No. 2 site proposes Sand Filter Water Quality Facilities that will treat runoff prior to discharging to the existing storm sewer system. There will be no adverse affects on downstream developments as a result of the development of this subdivision.

### **Step 3 - Provide Water Quality Capture Volume**

One (1) Sand Filter Basin water quality facility is proposed to provide WQCV at the time of the writing of this report. Up to four (4) future Sand Filter water quality facilities maybe required with the full build out of the parcel.

### **Step 4 - Consider Need for Industrial and Commercial BMP's**

This submittal provides a Preliminary Grading and Erosion Control plan. A Final GEC plan with BMP's in place shall be required with a Final Plat and Site Development applications. The proposed project will use silt fence, a vehicle tracking control pad, a concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site.

## **Proposed Drainage Characteristics**

### **General Concept Drainage Discussion**

The "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc. indicated that flows discharged from the subject site were to be collected and conveyed to the East Fork of Sand Creek Channel via a storm system that was to parallel Meadowbrook Parkway. As a portion of the construction of Claremont Business Park 2 Filing No.1 the existing storm sewer system was extended along the eastern side of Meadowbrook Parkway to collect runoff from the Lots 8, 9 & 10 and Tract B of Claremont Business Park 2 Filing No.1 and thus remain in compliance with the previous drainage plans and studies.

The Claremont Business Park 2 Filing No.2 project will Replat of Lots 8, 9 & 10 and Tract B of Claremont Business Park 2 Filing No.1, eliminate Tract B and redistribute the three (3) lots based around a newly aligned private roadway. The subject site is anticipated to continue to consist of neighborhood commercial and light industrial use and thus the properties will consist of asphalt, curb and gutter, parking areas, buildings, and landscaping.

A private storm sewer will be extended via drainage easements to collect runoff from each lot and the roadway. In lieu of a singular water quality pond (as previously anticipated by the CBP2, Filing 1 FDR) to treat the runoff from the subject site, each lot will be required to provide and maintain its own water quality facilities.

Pond 4 is shown as future on drainage map on pdf pg 126 below. Revise text and/or map to remove discrepancy.

## REVISED TO WQ POND 3

The initial construction of the project will include the construction of storm main to each lot, the construction of El Jefe Heights roadway and subsurface utilities such as water and wastewater to support future development. Temporary sediment basins will be constructed at the terminus of the storm sewers stubs to collect runoff from the undeveloped lots. A permanent water quality pond will be constructed at the southwest corner of Lot 2 to provide treatment for the proposed roadway and a portion of Lot 2. With the exception of the current permanent WQ Pond 4, no routing was considered when evaluating the discharge from the proposed lots to size the proposed storms sewer.

Individual drainage letters and/or reports shall be required with the development of each future lot not otherwise clearly analyzed by this report. A proposed conditions drainage map is included in the Appendix of this report to accompany the following discussion.

### Proposed Conditions Detailed Drainage Discussion

**Design Point 1** ( $Q_5 = 5.9 \text{ cfs}$ ,  $Q_{100} = 11.2 \text{ cfs}$ ) consists of runoff from **Basin A** and **Basin B**. **Basin A** is 0.21 acres of undeveloped roadway embankment and **Basin B** consists 1.50 acres of future roof top, asphalt paving and landscaped areas associated with commercial or industrial development. Runoff from the two basins will be directed to the southwest and collected by a private 18" ADS storm (**PR1**) at the southwest corner of the lot. A WQ facility or CDS unit will need to be provided upon development.

**Design Point 2** ( $Q_5 = 3.0 \text{ cfs}$ ,  $Q_{100} = 5.8 \text{ cfs}$ ) consists of runoff from **Basin C** and **Basin D**. **Basin C** is 0.12 acres of undeveloped roadway embankment and **Basin D** consists 0.77 acres of future roof top, asphalt paving and landscaped areas associated with commercial or industrial development within the northern half of Lot 2. Runoff from the basin will be directed to the southwest and collected by a private 18" ADS storm (**PR2**) at the middle of the western boundary of the lot. A WQ facility or CDS unit will need to be provided upon development.

**Design Point 3** ( $Q_5 = 1.2 \text{ cfs}$ ,  $Q_{100} = 2.3 \text{ cfs}$ ) consists of runoff from **Basin F**. **Basin F** consists 0.30 acres of future roof top, asphalt paving and landscaped areas associated with commercial or industrial development within the northeastern portion of Lot 3. Runoff from the basin will be directed to the southeast and collected by a private 18" ADS storm at the middle of the eastern boundary of the lot. A WQ facility or CDS Unit will need to be provided upon development.

**Design Point 4** ( $Q_5 = 1.0 \text{ cfs}$ ,  $Q_{100} = 1.7 \text{ cfs}$ ) consists of runoff from **Basin E2**. **Basin E2** consists 0.21 acres of asphalt paving, sidewalks, and landscaped areas associated with a portion of EL Jefe Heights. Runoff from the basin will be directed to the south and collected at low point by a private 5' Type R sump inlet. A proposed private 18" ADS Storm Drain will convey the collected runoff east under the roadway.

(Inlet 1)

**INLET 1 ADDED  
TO STATEMENT.**

**Design Point 5** ( $Q_5 = 1.2 \text{ cfs}$ ,  $Q_{100} = 2.2 \text{ cfs}$ ) consists of runoff from **Basin E1**. **Basin E1** consists 0.27 acres of asphalt paving, sidewalks, and landscaped areas associated with a portion of EL Jefe Heights. Runoff from the basin will be directed to the south and collected at low point by a private 5' Type I (Inlet 2)

**INLET 2 ADDED  
TO STATEMENT.**

sump inlet. Runoff collect by the inlet combines with flows conveyed by **PR5**, in **PR6** a private 18" storm sewer that outfalls into **WQ Pond 2**. In the event that the inlets at **DP4** and **DP5** were to become clogged runoff would overtop the localized high point of the road and continue south within El Jefe Heights.

**Design Point 6** ( $Q_5 = 5.1 \text{ cfs}$ ,  $Q_{100} = 9.6 \text{ cfs}$ ) consists of runoff from **Basin C1, D1 and Pipe Run 6 (PR6)**. **Basin C1** is 0.17 acres of undeveloped roadway embankment and **Basin D** consists 0.78 acres of future roof top, asphalt paving and landscaped areas associated with commercial or industrial development within the northern half of Lot 2. Runoff from the basin will be directed to the southwest to a permanent WQ facility and combine with flows conveyed within **PR6**. A permanent sand filter water quality facility will discharge runoff to the south where it will combine with flows conveyed within **PR4**, a private 24" ADS storm sewer (**PR8**) at peak flow rates of  $Q_5 = 5.9 \text{ cfs}$ ,  $Q_{100} = 13.1 \text{ cfs}$ .

**Design Point 7** ( $Q_5 = 4.7 \text{ cfs}$ ,  $Q_{100} = 8.7 \text{ cfs}$ ) consists of runoff from **Basin G2**. **Basin G2** consists 1.15 acres of future roof top, asphalt paving and landscaped areas associated with commercial or industrial development within the northeastern portion of Lot 3. Runoff from the basin will be directed to the southwest and collected by a private 24" ADS storm at the middle of the eastern boundary of the lot. A WQ facility or CDS unit will need to be provided upon development.

The subject site fully developed peak flow being discharge to an existing 24" ADS (**PR11**) which is located at the southwest corner of the site is estimated at  $Q_5 = 7.1 \text{ cfs}$ ,  $Q_{100} = 16.2 \text{ cfs}$ .

**Design Point 8** ( $Q_5 = 2.2 \text{ cfs}$ ,  $Q_{100} = 4.3 \text{ cfs}$ ) consists of runoff from **Basin H1** and **Basin I1**. **Basin H1** is 0.16 acres of undeveloped roadway embankment and **Basin I1** consists 0.55 acres of roof top, asphalt paving and landscaped areas. Runoff from the two basins flow into an existing 3.0 foot wide x 6 inch high concrete chase with 6 inch curb heights which discharges into the cul-de-sac of Gary Watson Point.

**Design Point 9** ( $Q_5 = 1.8 \text{ cfs}$ ,  $Q_{100} = 4.1 \text{ cfs}$ ) consists of runoff from **Basin H2** and **Basin I2**. **Basin H2** is 0.40 acres of undeveloped roadway embankment and **Basin I2** consists 0.48 acres of asphalt landscaped areas. Runoff from basins is collected in curb and gutter which discharges into the cul-de-sac of Gary Watson Point.

Label chase on  
drainage map

**Design Point 10** ( $Q_5 = 0.8 \text{ cfs}$ ,  $Q_{100} = 1.6 \text{ cfs}$ ) consists of runoff from **Basin H3** and **Basin I7**. **Basin H3** is 0.04 acres of undeveloped roadway embankment and **Basin I7** consists 0.23 acres of asphalt paving and landscaped areas. Runoff from basins is collected in curb and gutter which discharges into the cul-de-sac of Gary Watson Point.

DESIGN POINTS REVISED.

DP 3 thru 5

**Design Point 11** ( $Q_5 = 8.4 \text{ cfs}$ ,  $Q_{100} = 16.7 \text{ cfs}$ ) consists of runoff from **Basin I3, I4, I5, I6** and **DP1-3**. **Basins I3, I4, I5, and I6** are of 0.45, 0.55, 0.23, and 0.19 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the four basins combines with flows from **DP1-3** within the private street section of Gary Watson. Runoff is collected by a pair of existing 15' Type R at grade inlets located at **DP6**. Collected runoff is conveyed to the west underground via private 24" storm sewer to an existing WQ pond (Fil1Pond) (**PR13-14**). **Inlet 3** collects

Q100

REVISED TO Q100

Q5=4.1 cfs and Q100=7.9 cfs, with Q5=0.0 cfs and Q5=0.4 cfs of flow-by in the respective storm events.

**Inlet 4** collects Q5=4.2 cfs and Q100=8.0 cfs, with Q5=0.0 cfs and Q5=0.3 cfs of flow-by in the respective storm events. Runoff bypassing the existing inlets continues westward to **Design Point 12** and **13**.

**Design Point 12** (Q5 = 2.8 cfs, Q100 = 8.1 cfs) consists of flow-by runoff from **Inlet 3** and flows within **Basin J1**. **Basin J1** consists 0.69 acres of rooftop, asphalt paving and landscaped areas. Runoff from **Basin J1** and flow-by from the inlet is conveyed within the curb and gutter to an existing 15' Type R at grade inlets located at **DP7**. **Inlet 5** collects Q5=2.4 cfs and Q100=7.3 cfs, with Q5=0.0 cfs and Q5=0.2 cfs of flow-by in the respective storm events. An existing 18" storm sewer (**PR15**) conveys the intercepted runoff underneath Gary Watson.

Include O1 in DP12 and show flow arrows for O1

REVISED TO DP12 DP12

**Design Point 13** (Q5 = 1.0 cfs, Q100 = 5.0 cfs) consists of flow-by runoff from **Inlet 4** and flows within

PER THE APPROVED "FINAL

**Basin J2 and J3**. **Basins J2 and J3** are of 0.10 and 0.12 acres of undeveloped roadway embankment and

asphalt paving and landscaped areas within

DRAINAGE REPORT FOR CLAREMONT

asphalt paving and landscaped areas within

BUSINESS PARK 2 FILING NO. 1" BY MS CIVIL

by from the inlet is conveyed within the cur

CONSULTANTS, INC. DATED DECEMBER 2020

at **DP13**. **Inlet 6** collects Q5=1.0 cfs and C

AND SUBSEQUENT REPORT FOR LOT 7 BASIN O1

An existing 18" storm sewer (**PR16**) conve

WILL SHEET FLOW ONTO MEADOWBROOK PARKWAY.

FLOW ARROWS WILL BE ADDED.

**Design Point 14** (Q5 = 3.8 cfs, Q100 = 9.7 cfs) consists of runoff from **Basin H4, L and M4**. **Basin H4** and **L** are 0.10 and 1.32 acres of undeveloped roadway embankment and **Basin M4** consists of 0.98 acres of roof top, asphalt paving and landscaped areas. Runoff from the three basins flows into an existing a 2' foot trapezoidal channel located at the south end of the property.

REVISED TO DP14

**Design Point 15** (Q5 = 5.3 cfs, Q100 = 12.3 cfs) consists of runoff from **Basin M2, M3 and DP9**. **Basins M2 and M3** are of 0.24 and 0.37 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. Runoff from the two basins combine with **DP14** flows in an existing a 2' foot trapezoidal channel located at the south end of the property. Runoff at **DP15** will enter the existing Filing 1 **WQ Pond 2** via an existing trapezoidal grouted riprap rundown.

**Design Point 16** (Q5 = 1.4 cfs, Q100 = 2.5 cfs) consists of runoff from **Basin M1 and K4**. **Basins M1** and **K4** are of 0.28 and 0.05 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the two basins is directed into the existing **WQ Pond 2** via an existing concrete rundown.

**Design Point 17** (Q5 = 1.1 cfs, Q100 = 2.0 cfs) consists of runoff from **Basin K2, K3 and N1**. **Basins K2, K3 and N1** are of 0.05, 0.15 and 0.06 acres in size respectively and consist of roof top, asphalt paving and landscaped areas within the development. The runoff from the three basins is directed into the existing **WQ Pond 2** via an existing concrete rundown.

REVISED TO 3 BASINS

**Design Point 18** (Q5 = 0.7 cfs, Q100 = 1.3 cfs) consists of runoff from **Basin K1**. **Basin K1** is 0.17 acres in size and consists of roof top, asphalt paving and landscaped areas within the

development. The runoff from the basins is directed to an existing beehive grated manhole located in the southwest corner of the lot.

**REVISED TO DP15-17**

DP15-18

**Design Point 19** ( $Q_5 = 19.8 \text{ cfs}$ ,  $Q_{100} = 44.7 \text{ cfs}$ ) consists of runoff from **Basin N2** and **DP10-13**.

**Basins N2** is 0.41 acres in size and consists of a sand filter water quality pond (**WQ Pond 2**).

#### **Basin G1, O1, O2,**

**Basins G1, O1, and O2** are 0.27, 0.12 and 0.06 acres in size and consist of asphalt, concrete, and landscaped areas along the western periphery of the development. The runoff from the three basins is directed to Existing Meadowbrook Parkway. The 5 year event and 100 year event peak runoff rates from **Basin G1, O1, and O2** are  $Q_5 = 0.4 \text{ cfs}$ ,  $Q_{100} = 1.2 \text{ cfs}$ ,  $Q_5 = 0.1 \text{ cfs}$ ,  $Q_{100} = 0.4 \text{ cfs}$  and  $Q_5 = 0.1 \text{ cfs}$ ,  $Q_{100} = 0.3 \text{ cfs}$  respectively.

#### **Basin P**

**Basins P** ( $Q_5 = 0.0 \text{ cfs}$ ,  $Q_{100} = 0.3 \text{ cfs}$ ) is 0.11 acres in size and consists of landscaped and undeveloped areas along the southern periphery of the development. The runoff from the basins is directed to the adjacent development.

The Matrix "Final Drainage Report for Claremont Business Park Filing No. 2" calculated that DP 1 combining Sub Basins B1 and B2 generated of ( $Q_5=31.5 \text{ cfs}$  and  $Q_{100}=63.6$ ). The proposed developments (CBPF2 Filings 1 and 2) will release  $Q_5=19.8 \text{ cfs}$  and  $Q_{100}=44.7$  which is less than what was anticipated by the Matrix report. Therefore the proposed development shall not have a negative impact on the downstream storm system and is adequately sized to convey the proposed generated flows.

### **Water Quality Provision and Maintenance**

The subject site was previously analyzed within the Final Drainage Report for Claremont Business Park Filing No. 2 prepared by Matrix Design Group approved April 24, 2006. Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater full spectrum detention (refer FDR for Claremont Business Park Fil. 2). The water quality volume required for the site has been determined using the MHFD UD-Detention workbook per the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II.

As previously discussed water quality for the site (CBP2F2) will be provided by proposed Sand Filter Basins (SFB). Pond 3 is to be constructed initially and will function to treat runoff from the newly constructed improvements (roadway, sidewalks) and the western half of Lot 2 or approx 1.43 acres at 81.8 imperviousness.

Pond 3 will provide 0.032 acre-feet of water quality storage. Per ECM section 1.7.1.C.1, 20% of the project site (not to exceed 1.0 acre) may be excluded from the 100% WQ treatment requirement per El Paso County criteria. This report identifies that **Basins G1, O1, O2** and **P** is unable to reach one of the

## REVISED STATEMENT TO POND 3

Which two? This section only previously mentions Pond 3.

Lots 8-10 are being renamed with the subdivision. Please revise lot numbers.

proposed WQ ponds. Combined total acreage of the Basins is 0.56 AC, and doesn't exceed the 1.0 acre maximum allowance of acreage runoff allowed per EPC critera.

## REVISED LOT NUMBERS

Flows tributary to the two SFBs are released through outlet structures into an existing storm sewer system located along Meadowbrook Parkway. Water quality pond 1 will be private and shall be maintained by the property owners (equal shares determined by size of lots 8-10). Water quality pond 2 will be private and shall be maintained by the property owners (equal shares determined by size of lots 1-7). Access shall be granted to the owner and El Paso County for access and maintenance of the private WQCV facility. A private maintenance agreement document shall accompany the final drainage report(s) submittal(s) which construct the two ponds.

This paragraph only mentions Pond 1 and 2. What about Pond 4 and 5? (Pond 3 already previously discussed in this section)  
**Erosion Control**

The report identifies Pond 3 being built and Pond 5 (location of existing sediment basin on Tract B) being removed. Please revise paragraph for consistency.

## REVISED STATEMENT TO INCLUDE POND 4 & 5

It is the policy of the El Paso County that a grading and erosion contr EXISTING SEDIMENT BASIN TO report. The GEC incorporates silt fence, vehicle traffic control, inlet an REMAIN UNTIL LOT 3 IS DEVELOPED. and other best management practices (BMP's) as identified in the DCM Volume 2.

## Construction Cost Opinion

Private Drainage Facilities (NON-Reimbursable) Including Sand Filter WQ Pond 3:

Item	Description	Quantity	Unit Cost	Cost
1.	18" PP	394 LF	\$48 /LF	\$18,912.00
2.	18" RCP	50 LF	\$60 /LF	\$3,000.00
3.	18" RCP FES	2 LF	\$650 /LF	\$1,300.00
4.	24" PP	851 LF	\$75 /EA	\$63,825.00
5.	Type L Riprap	6 CY	\$75 /CY	\$450.00
6.	CDOT Type C Grated Inlet	1 EA	\$4,500 /EA	\$4,500.00
7.	CDOT Type R 5' Sump Inlet	2 EA	\$6,500 /EA	\$13,000.00
8.	Type II Manhole	7 EA	\$5,000 /EA	\$35,000.00
9.	WQCV Sand Filter Pond	1 EA	\$25,000 /EA	\$25,000.00
				<b>\$164,987.00</b>
	Engineering Costs (10%)			<b>16,498.70</b>
				<b>181,485.70</b>

Note: The required infrastructure (private) and future ponds (private) for Claremont Business Park 2 Filing 2, Lots 1-3 will be provided in subsequent drainage report and/or letters.

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost in 2023.

Provide an estimate of the proposed imperviousness of the site and difference from the previously approved drainage report.

## Drainage and Bridge Fees

## STATEMENT PROVIDED ON IMPERVIOUSNESS IN THE GENERAL CONCEPT DRAINAGE DISCUSSION SECTION.

This site is in the Sand Creek Drainage Basin. The site was previously subdivided into ten commercial lots as a portion of Claremont Business Park 2, Filing No.1. The proposed project will replat the existing Lot and create Claremont Business Park 2, Filing No.2

Drainage fees were paid at the time of the previous platting as Tract C of Claremont Business Park Filing No. 2 (Reception No. 207712506), therefore no additional Drainage Bridge and/or Pond fees are required.

## Summary

The proposed design meets the design assumptions utilized in the "Final Drainage Report for Claremont Business Park Filing No. 2", by Matrix Design Group, Inc that is included in Appendix. The Matrix "Final Drainage Report for Claremont Business Park Filing No. 2" calculated that DP 1 combining Sub Basins B1 and B2 generated of (Q5=31.5 cfs and Q100=63.6). The proposed developments (Filing 1 and Filing 2) will release Q5=19.8 cfs and Q100=44.7 which is less than what was anticipated by the Matrix report. Therefore the proposed development shall not have a negative impact on the downstream storm system and is adequately sized to convey the proposed generated flows. Thus the development of Claremont Business Park 2 Filing No.2 shall not adversely affect the surrounding development. The proposed drainage facilities will adequately convey, detain and route runoff from the onsite & offsite flows to existing facilities. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix) are subject to change being dependent upon individual lot development but owners/developer of the lots shall comply with this final drainage report that will be submitted with the final plat application. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions.

Completing a "Water Quality Treatment Summary Table" like the example provided below would greatly help us clearly see that WQ req's are being met for the whole site, if you could do one for this site.

Add rows for each basin within this filing.

Make a column for each of the 5 ponds.

delete this column if no RR is anticipated for this site.

The areas of Basin G1, O1, O2, and P would be in this column

From the PBMP Form, this column should be blank.

	Total Area (ac)	Total Proposed Disturbed Area (ac)	Area Trib to Pond A (ac)	Disturbed Area Treated via Runoff Reduction (ac)	Area Excluded from WQ per ECM App I.7.1.C.1 (ac)	Area Excluded from WQ per ECM App I.7.1.B.# (ac)	Applicable WQ Exclusions (App I.7.1.B.#)
4.50	4.50	4.50	-	-	-	-	
1.25	1.25	-	1.00	0.25	-	-	
-	6.00	4.00	-	-	-	4.00	ECM App I.7.1.B.5
D	2.50	2.50	1.00	-	0.50	1.00	ECM App I.7.1.B.7
E	3.00	-	3.00	-	-	-	
F	8.25	-	-	-	-	-	
Total	25.50	12.25	8.50	1.00	0.75	5.00	
Comments	[For each row, the sum of the values in Columns 4-7 must be greater than or equal to the value in Column 3 above.]	[Values in this column can be more than Column 3 if over-treating non-disturbed areas.]	See RR calc spreadsheet.	[Total must be <20% of site and <1ac.]			

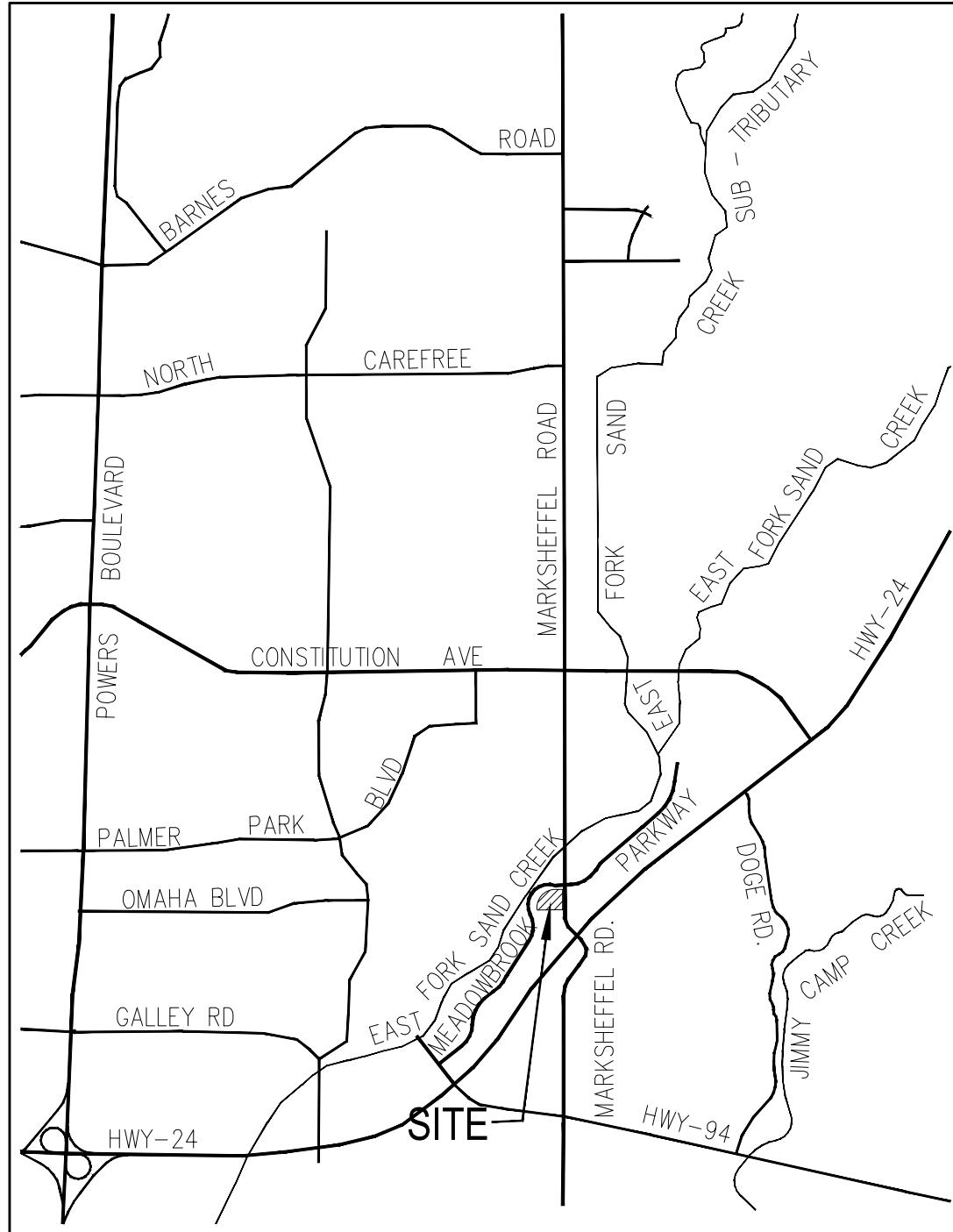
**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

## References

1. "El Paso County and City of Colorado Springs Drainage Criteria Manual".
2. "Urban Storm Drainage Criteria Manual"
3. Soil Survey Staff, Natural Resources Conservation Service, United States Department of Agriculture. Web Soil Survey. Available online at the following link: <http://websoilsurvey.sc.egov.usda.gov/>. Accessed: Febrary 02 , 2023.
4. Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective dated December 7, 2018.
5. "Final Drainage Report for Claremont Business Park Filing No. 2", by Matrix Design Group, Inc dated November 2006.
6. "Falcon Drainage Basin Planning Study", by Matrix Design Group, dated September 2015.
7. "Final Drainage Report for Claremont Business Park Filing No.2", by Matrix Design Group, Inc. dated November 2006.
8. "Final Drainage Report for Claremont Business Park 2 Filing No. 1", by M&S Civil Consultants, approved 2/11/2021.
9. "Final Drainage Letter for Lot 1 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 04/01/2021.
10. "Final Drainage Letter for Lot 2 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 05/19/2021.
11. "Final Drainage Letter for Lot 3 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 05/19/2021.
12. "Final Drainage Letter for Lot 4 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 05/19/2021.
13. "Final Drainage Letter for Lot 5 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 03/03/2021.
14. "Final Drainage Letter for Lot 6 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 07/08/2021.
15. "Final Drainage Letter for Lot 7 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 03/31/2021.

## Appendix

## Vicinity Map



# VICINITY MAP

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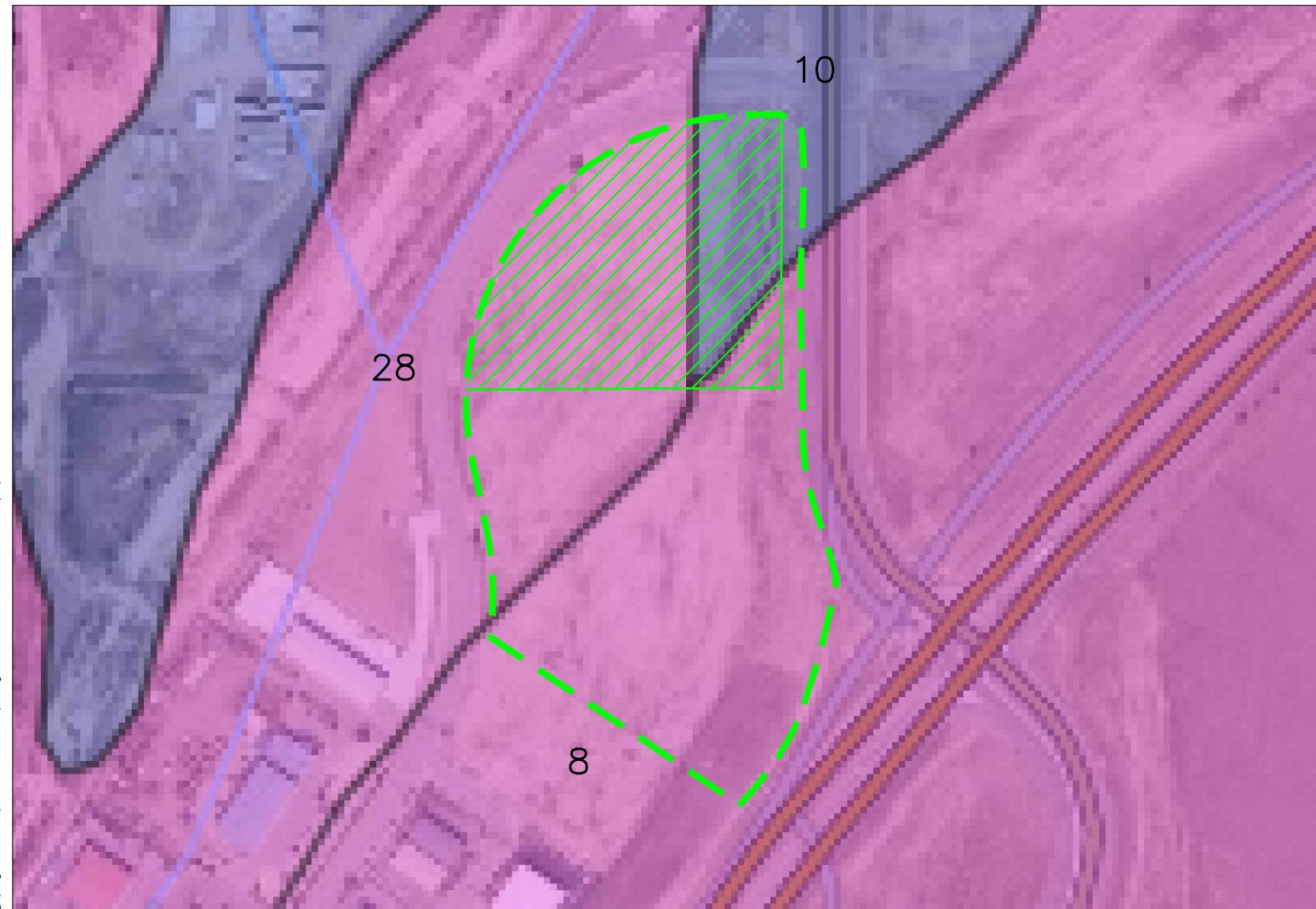
N.T.S.



## Soils Map

# CLAREMONT BUSINESS PARK 2 FILING NO. 2

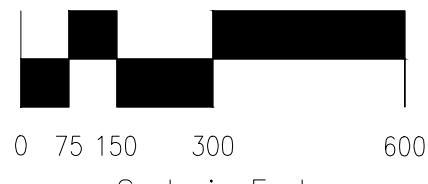
2/2/2023 11:50 AM



HYDROLOGIC TYPE A SOILS	
HYDROLOGIC TYPE B SOILS	
WATERSHED BOUNDARY	
SITE BOUNDARY	



1" = 300'



0 75 150 300 600

Scale in Feet

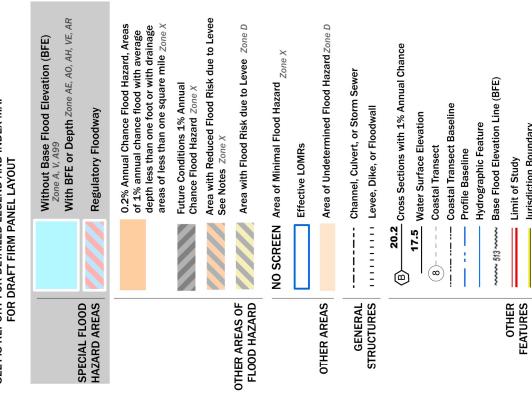
Map unit symbol	Map unit name	Rating
8	Blakeland loamy sand, 1 to 9 percent slopes	A
10	Blendon sandy loam, 0 to 3 percent slopes	B
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	A

## SOILS MAP



212 N. WAHSATCH AVE., STE 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.955.5485

## FEMA FIRM Panel

**FLOOD HAZARD INFORMATION**SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP  
FOR DRAFT FIRM PANEL LAYOUT**NOTES TO USERS**

For information and questions about this Flood Insurance Rate Map (FIRM), available products associated with this FIRM, including historic versions, the current map date at each FIRM panel, how to order products, and how to obtain a copy of the FIRM, contact the FEMA Flood Map Service Center at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA Flood Map Service Center website at [www.floodmaps.fema.gov](http://www.floodmaps.fema.gov). Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and other digital versions of the map. Many of these products can be ordered directly from the website.

Communities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well as the current FIRM Index. These may be ordered directly from the Flood Map Service Center at the number listed above.

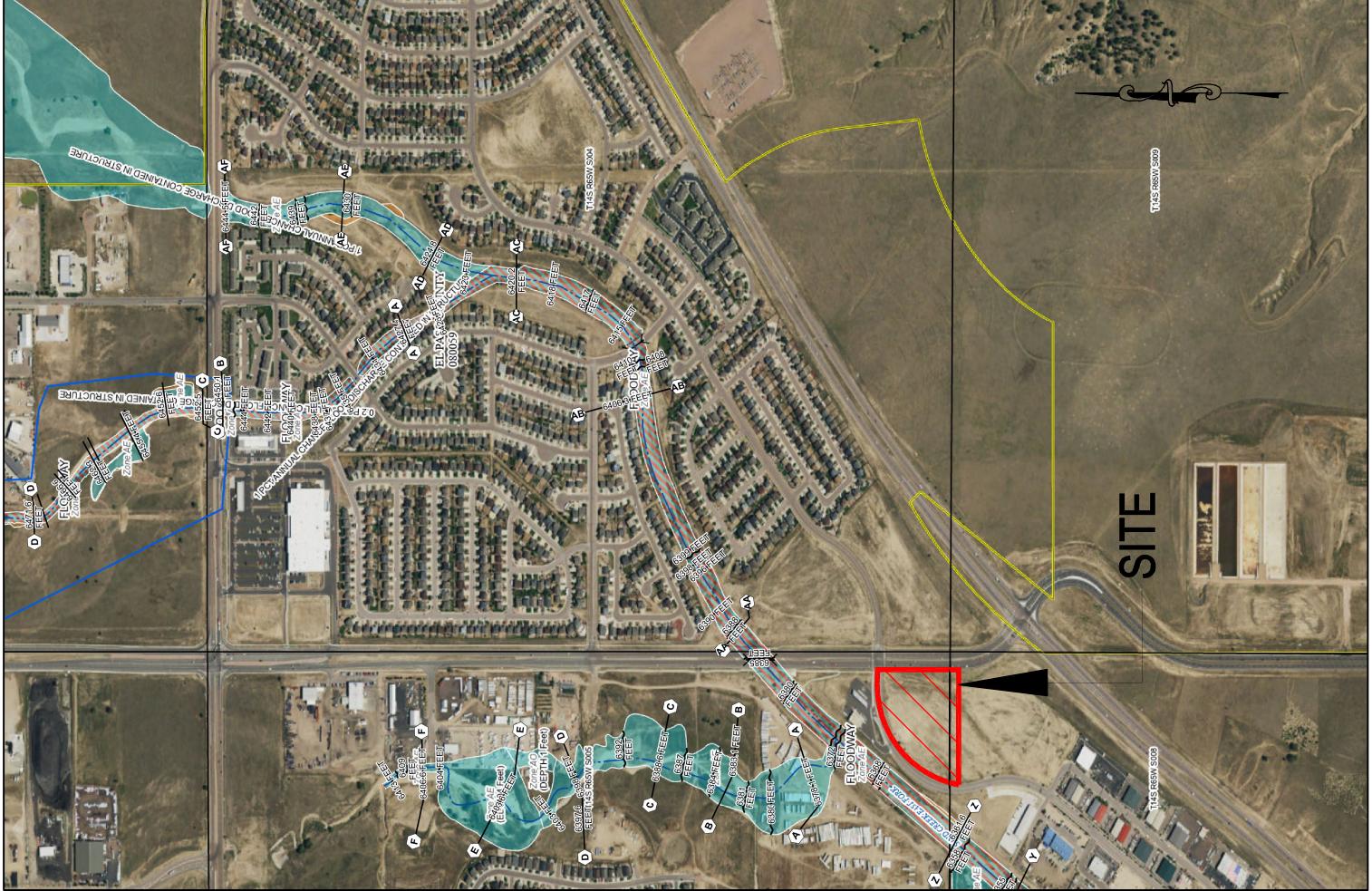
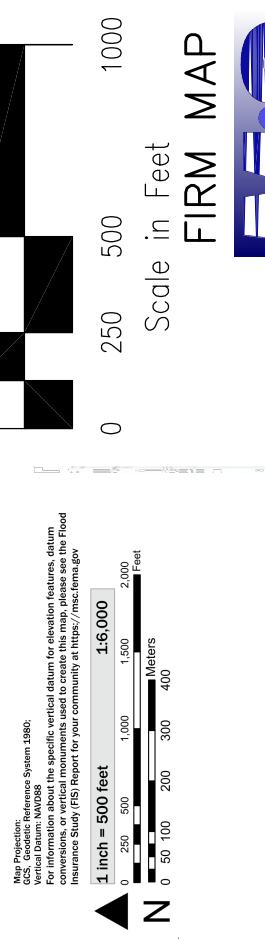
To determine if flood insurance is available in this community, contact your insurance agent or call National Flood Insurance Program at 1-800-638-6620.

The baseline shown is the USGS National Map. On November 20, 2020, the FIRM was provided by the United States Geological Survey (USGS).

This dataset is derived from FEMA's National Flood Hazard Layer (NFHL) as of April 2023. NFHL and base map data are subject to change or modification subsequent to the date and time. For additional information please see the Flood Hazard Mapping Update Fact Sheet at <https://www.fema.gov/flood-hazard-mapping-updates>.

This map complies with FEMA standards for the use of digital flood maps as of November 20, 2018. The baseline shows compliance with FEMA's National Flood Hazard Layer (NFHL) as of April 2023. NFHL and base map data are subject to change or modification subsequent to the date and time. For additional information please see the Flood Hazard Mapping Update Fact Sheet at <https://www.fema.gov/flood-hazard-mapping-updates>.

For information about the specific vertical datum for elevation features, datum conversions, or vertical monuments used to create this map, please see the Flood Insurance Study (FIS) Report for your community at <https://msc.fema.gov>.

**SCALE**

## **HYDROLOGIC CALCULATIONS**

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**EXISTING DRAINAGE CALCULATIONS**  
*(Area Runoff Coefficient Summary)*

			ROOFS 0.73-0.81 COMMERCIAL AREAS 0.81-0.88 ASPHALT DRIVES 0.90-0.96			LANDSCAPED AREAS 0.16-0.41 GRAVEL STORAGE YARD 0.30-0.50 LIGHT INDUST AREAS 0.59-0.70			PARKS 0.12-0.39 GREENBELTS/AGRI. 0.09-0.36			WEIGHTED	
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
A	8359.8	0.19	0.00	0.90	0.96	0.00	0.16	0.41	0.19	0.09	0.36	0.09	0.36
B	13279.6	0.30	0.00	0.81	0.88	0.00	0.30	0.50	0.30	0.09	0.36	0.09	0.36
C	213471.0	4.90	0.00	0.90	0.96	0.00	0.16	0.41	4.90	0.09	0.36	0.09	0.36
D	9961.3	0.23	0.00	0.90	0.96	0.00	0.16	0.41	0.23	0.09	0.36	0.09	0.36
H1	7641.7	0.18	0.00	0.90	0.96	0.00	0.73	0.81	0.18	0.09	0.36	0.09	0.36
H2	17510.6	0.40	0.00	0.90	0.96	0.00	0.73	0.81	0.40	0.09	0.36	0.09	0.36
H3	1583.1	0.04	0.00	0.90	0.96	0.00	0.73	0.81	0.04	0.09	0.36	0.09	0.36
H4	4363.6	0.10	0.00	0.81	0.88	0.00	0.30	0.50	0.10	0.09	0.36	0.09	0.36
I1	24996.2	0.57	0.33	0.90	0.96	0.21	0.73	0.81	0.03	0.16	0.41	0.80	0.88
I2	21018.4	0.48	0.32	0.90	0.96	0.12	0.73	0.81	0.05	0.16	0.41	0.79	0.87
I3	25471.7	0.58	0.32	0.90	0.96	0.08	0.73	0.81	0.18	0.16	0.41	0.65	0.77
I4	18732.1	0.43	0.28	0.90	0.96	0.11	0.73	0.81	0.03	0.16	0.41	0.80	0.88
I5	10207.0	0.23	0.12	0.90	0.96	0.08	0.73	0.81	0.04	0.16	0.41	0.73	0.83
I6	8155.2	0.19	0.12	0.90	0.96	0.00	0.73	0.81	0.07	0.16	0.41	0.62	0.75
I7	10159.6	0.23	0.19	0.90	0.96	0.00	0.73	0.81	0.04	0.16	0.41	0.77	0.87
J1	33120.0	0.76	0.45	0.90	0.96	0.12	0.73	0.81	0.19	0.16	0.41	0.69	0.80
J2	10980.0	0.25	0.14	0.90	0.96	0.08	0.73	0.81	0.04	0.16	0.41	0.73	0.83
J3	626.0	0.01	0.00	0.90	0.96	0.00	0.73	0.81	0.01	0.16	0.41	0.16	0.41
K1	7398.7	0.17	0.12	0.90	0.96	0.04	0.73	0.81	0.01	0.16	0.41	0.83	0.90
K2	2320.2	0.05	0.01	0.90	0.96	0.04	0.73	0.81	0.00	0.16	0.41	0.72	0.81
K3	6474.8	0.15	0.09	0.90	0.96	0.05	0.73	0.81	0.01	0.16	0.41	0.78	0.87
K4	2266.5	0.05	0.00	0.90	0.96	0.05	0.73	0.81	0.00	0.16	0.41	0.69	0.78
L	57315.2	1.32	0.00	0.90	0.96	0.00	0.73	0.81	1.32	0.09	0.36	0.09	0.36
M1	12396.2	0.28	0.19	0.90	0.96	0.08	0.73	0.81	0.02	0.16	0.41	0.81	0.88
M2	10573.8	0.24	0.00	0.90	0.96	0.20	0.73	0.81	0.05	0.16	0.41	0.62	0.73
M3	15906.8	0.37	0.33	0.90	0.96	0.00	0.73	0.81	0.04	0.16	0.41	0.83	0.91
M4	42578.8	0.98	0.77	0.90	0.96	0.11	0.73	0.81	0.10	0.12	0.39	0.80	0.89
N1	2827.1	0.06	0.06	0.90	0.96	0.00	0.73	0.81	0.00	0.16	0.41	0.90	0.96
N2	18017.7	0.41	0.00	0.90	0.96	0.00	0.30	0.50	0.41	0.12	0.39	0.12	0.39
O1	5318.2	0.12	0.01	0.90	0.96	0.00	0.30	0.50	0.12	0.12	0.41	0.16	0.44
O2	2824.6	0.06	0.01	0.90	0.96	0.00	0.30	0.50	0.06	0.12	0.41	0.22	0.48
P	4961.4	0.11	0.00	0.90	0.96	0.00	0.30	0.50	0.11	0.09	0.36	0.09	0.36

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**EXISTING DRAINAGE CALCULATIONS**  
*(Area Drainage Summary)*

From Area Runoff Coefficient Summary				OVERLAND			STREET / CHANNEL FLOW				Time of Travel ( $T_t$ )		INTENSITY *		TOTAL FLOWS		
BASIN	AREA TOTAL (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub> From DCM Table 5-1	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	*TOTAL (min)	CHECK (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)
A	0.19	0.09	0.36	0.09	40	5.0	5.0	0	0.0%	0.0	0.0	5.0	10.2	5.2	8.7	0.1	0.6
B	0.30	0.09	0.36	0.09	40	8.0	4.3	0	0.0%	0.0	0.0	4.3	10.2	5.2	8.7	0.1	1.0
C	4.90	0.09	0.36	0.09	100	2.0	14.5	637	1.7%	1.3	8.3	22.8	14.1	3.6	6.1	1.6	10.7
D	0.23	0.09	0.36	0.09	20	0.5	6.0	0	0.0%	0.0	0.0	6.0	10.1	4.9	8.2	0.1	0.7
H1	0.18	0.09	0.36	0.09	76	20.0	5.4	0	0.0%	0.0	0.0	5.4	10.4	5.1	8.5	0.1	0.5
H2	0.40	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	4.6	7.8	0.2	1.1
H3	0.04	0.09	0.36	0.09	100	17.0	7.2	0	2.0%	1.4	0.0	7.2	10.6	4.6	7.8	0.0	0.1
H4	0.10	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	4.6	7.8	0.0	0.3
I1	0.57	0.80	0.88	0.80	100	3.0	3.8	216	2.5%	3.2	1.1	5.0	11.8	5.2	8.7	2.4	4.4
I2	0.48	0.79	0.87	0.79	50	2.0	2.5	261	1.0%	2.0	2.2	5.0	11.7	5.2	8.7	2.0	3.6
I3	0.58	0.65	0.77	0.65	67	2.6	4.3	246	0.9%	1.8	2.2	6.5	11.7	4.8	8.0	1.8	3.6
I4	0.43	0.80	0.88	0.80	67	2.6	2.8	246	0.9%	1.8	2.2	5.0	11.7	5.2	8.7	1.8	3.3
I5	0.23	0.73	0.83	0.73	25	0.5	2.6	146	1.4%	2.4	1.0	5.0	11.0	5.2	8.7	0.9	1.7
I6	0.19	0.62	0.75	0.62	31	0.3	4.8	120	1.3%	2.3	0.9	5.7	10.8	5.0	8.3	0.6	1.2
I7	0.23	0.77	0.87	0.77	50	0.3	5.2	133	1.1%	2.1	1.1	6.2	11.0	4.8	8.1	0.9	1.6
J1	0.76	0.69	0.80	0.69	85	3.0	4.5	327	0.9%	1.9	2.8	7.4	12.3	4.6	7.7	2.4	4.7
J2	0.25	0.73	0.83	0.73	25	0.5	2.6	185	1.4%	2.3	1.3	5.0	11.2	5.2	8.7	1.0	1.8
J3	0.01	0.16	0.41	0.16	10	1.0	2.6	0	0.0%	0.0	0.0	5.0	10.1	5.2	8.7	0.0	0.1
K1	0.17	0.83	0.90	0.83	25	0.5	2.0	115	3.0%	3.5	0.5	5.0	10.8	5.2	8.7	0.7	1.3
K2	0.05	0.72	0.81	0.72	25	0.5	2.7	55	1.8%	2.7	0.3	5.0	10.4	5.2	8.7	0.2	0.4
K3	0.15	0.78	0.87	0.78	25	0.5	2.3	120	1.4%	2.4	0.8	5.0	10.8	5.2	8.7	0.6	1.1
K4	0.05	0.69	0.78	0.69	25	0.5	3.0	91	1.0%	2.0	0.8	5.0	10.6	5.2	8.7	0.2	0.4
L	1.32	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	4.6	7.8	0.5	3.7
M1	0.28	0.81	0.88	0.81	25	0.5	2.1	203	1.0%	2.0	1.7	5.0	11.3	5.2	8.7	1.2	2.2
M2	0.24	0.62	0.73	0.62	25	0.5	3.5	148	1.0%	1.5	1.6	5.1	11.0	5.1	8.6	0.8	1.5
M3	0.37	0.83	0.91	0.83	50	2.0	2.2	112	2.5%	3.2	0.6	5.0	10.9	5.2	8.7	1.6	2.9
M4	0.98	0.80	0.89	0.80	100	1.0	5.3	326	1.2%	2.2	2.4	7.8	12.4	4.5	7.6	3.5	6.6
N1	0.06	0.90	0.96	0.90	50	1.0	2.0	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.3	0.5
N2	0.41	0.12	0.39	0.12	60	1.2	10.9	30	33.0%	11.5	0.0	10.9	10.5	4.1	6.8	0.2	1.1
O1	0.12	0.16	0.44	0.16	32	0.5	8.3	0	0.0%	0.0	0.0	8.3	10.2	4.4	7.4	0.1	0.4
O2	0.06	0.22	0.48	0.22	25	0.5	6.3	0	0.0%	0.0	0.0	6.3	10.1	4.8	8.1	0.1	0.3
P	0.11	0.09	0.36	0.09	25	0.5	7.1	0	0.0%	0.0	0.0	7.1	10.1	4.6	7.8	0.0	0.3

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**EXISTING DRAINAGE CALCULATIONS**  
**(Basin Routing Summary)**

From Area Runoff Coefficient Summary				OVERLAND			PIPE / CHANNEL FLOW				Time of Travel ( $T_t$ )		INTENSITY *		TOTAL FLOWS		COMMENTS
DESIGN POINT	CONTRIBUTING BASINS DPS AND/OR PIPES	CA <sub>s</sub>	CA <sub>100</sub>	C <sub>s</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	*TOTAL (min)	I <sub>s</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>s</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)	
<b>I</b>	A, B, C	0.49	1.94		Basin C Tc used							14.1	3.6	6.1	<b>1.8</b>	<b>II.8</b>	Exist PVT 24" Storm Sewer
<b>2</b>					NOT USED												
<b>3</b>	H1, II	0.47	0.57		Basin H1 Tc used + Basin II routing							7.1	4.6	7.8	<b>2.2</b>	<b>4.4</b>	Existing Curb and Gutter
<b>4</b>	H2, I2	0.42	0.56		Basin H2 Tc used + Basin I2 routing							8.9	4.3	7.2	<b>1.8</b>	<b>4.1</b>	Existing Curb and Gutter
<b>5</b>	H3, I7	0.18	0.22		Basin H1 Tc used + Basin II routing							8.6	4.4	7.3	<b>0.8</b>	<b>1.6</b>	Existing Curb and Gutter
<b>6</b>	DP3, DP4, DP5 I3, I4, I5, I6	2.09	2.51		Basin H3 Tc used + Basin I7 Routing							11.5	3.9	6.6	<b>8.2</b>	<b>16.5</b>	2-Exist 15" CDOT Type R Inlet (assumed split flows 100-yr)
<b>7</b>	FB INLET 3, J1	0.52	0.97		Basin J1 Tc Used							7.4	4.6	7.7	<b>2.4</b>	<b>7.5</b>	Exist 15" CDOT Type R Inlet
<b>8</b>	FB INLET 4, J2, J3	0.18	0.47		Basin J2 Tc Used							5.0	5.2	8.7	<b>0.9</b>	<b>4.1</b>	Exist 15" CDOT Type R Inlet
<b>9</b>	H4, L, M4	0.91	1.38		Basin L Tc used + Basin M4 Routing							9.6	4.2	7.0	<b>3.8</b>	<b>9.7</b>	Existing Pvt Swale
<b>10</b>	DP9, M2, M3	1.37	1.88		Basin DP9 Tc used + Basin M3 Routing							11.7	3.9	6.5	<b>5.3</b>	<b>12.3</b>	Existing Pvt Swale/Concrete Riprap Rundown
<b>11</b>	M1, K4	0.27	0.29		Basin M1 Tc Used							5.0	5.2	8.7	<b>1.4</b>	<b>2.5</b>	Existing Conc. Rock Rundown
<b>12</b>	K2, K3, N1	0.21	0.23		Basin K3 Tc Used							5.0	5.2	8.7	<b>1.1</b>	<b>2.0</b>	Existing Conc. Rock Rundown
<b>13</b>	K1	0.14	0.15		Basin K1 Tc Used							5.0	5.2	8.7	<b>0.7</b>	<b>1.3</b>	Existing Inlet
<b>14</b>	DP10, DP11, DP12 DP13, N2, PR14, PR17	4.96	6.72		DP10 Tc Used							11.7	3.9	6.5	<b>19.3</b>	<b>43.9</b>	Existing Sand Filter FSD Pond 2

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

***FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2***  
***EXISTING DRAINAGE CALCULATIONS***  
***(Storm Sewer Routing Summary)***

PIPE RUN	Contributing Pipes/Design Points	Equivalent CA <sub>5</sub>	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	Intensity*		Flow		Pipe Size
					I <sub>5</sub>	I <sub>100</sub>	Q <sub>5</sub>	Q <sub>100</sub>	
11	DP1	0.49	1.94	14.1	3.6	6.1	1.8	11.8	EX 24" PP
12	PR11	0.49	1.94	14.1	3.6	6.1	1.8	11.8	EX 24" PP
13	INLET 3	1.05	1.20	11.5	3.9	6.6	4.1	7.9	EX 15" PP
14	PR13, INLET 4	2.09	2.42	11.5	3.9	6.6	8.2	15.9	EX 24" PP
15	INLET 5	0.52	0.95	7.4	4.6	7.7	2.4	7.3	EX 18" PP
16	PR15, INLET 6	0.70	1.42	7.4	4.6	7.7	3.2	11.0	EX 24" PP
17	PR16, DP13	0.84	1.57	7.4	4.6	7.7	3.9	12.1	EX 24" PP
18	POND 2 OUTFALL	5.52	5.75	30.0	2.5	4.2	13.7	23.9	EX 30" PP
19	PR12, PR18	6.01	7.69	22.0	2.9	4.9	17.7	38.0	EX 24" PP

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point

FB- Flow By from Design Point

PR - Pipe Run

INT- Intercepted Flow from Design Point

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**PROPOSED DRAINAGE CALCULATIONS**  
*(Area Runoff Coefficient Summary)*

			ROOFS 0.73-0.81 COMMERCIAL AREAS 0.81-0.88 ASPHALT DRIVES 0.90-0.96				LANDSCAPED AREAS 0.16-0.41 GRAVEL STORAGE YARD 0.30-0.50 LIGHT INDUST AREAS 0.59-0.70				PARKS 0.12-0.39 GREENBELTS/AGRI. 0.09-0.36				WEIGHTED		
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>2</sub>	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>2</sub>	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>2</sub>	C <sub>5</sub>	C <sub>100</sub>	C <sub>2</sub>	C <sub>5</sub>	C <sub>100</sub>
A	9300.8	0.21	0.00	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.21	0.03	0.09	0.36	0.03	0.09	0.36
B	65284.4	1.50	1.50	0.79	0.81	0.88	0.00	0.23	0.30	0.50	0.00	0.05	0.12	0.39	0.79	0.81	0.88
C	5372.3	0.12	0.00	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.12	0.03	0.09	0.36	0.03	0.09	0.36
C1	7457.3	0.17	0.00	0.89	0.90	0.96	0.00	0.07	0.16	0.41	0.17	0.03	0.09	0.36	0.03	0.09	0.36
D	33587.9	0.77	0.77	0.79	0.81	0.88	0.00	0.23	0.30	0.50	0.00	0.05	0.12	0.39	0.79	0.81	0.88
D1	34028.4	0.78	0.78	0.79	0.81	0.88	0.00	0.23	0.30	0.50	0.00	0.05	0.12	0.39	0.79	0.81	0.88
E1	11683.7	0.27	0.22	0.89	0.90	0.96	0.05	0.79	0.81	0.88	0.00	0.05	0.12	0.39	0.87	0.88	0.95
E2	9082.0	0.21	0.17	0.89	0.90	0.96	0.04	0.79	0.81	0.88	0.00	0.05	0.12	0.39	0.87	0.88	0.95
F	12955.1	0.30	0.30	0.79	0.81	0.88	0.00	0.07	0.16	0.41	0.00	0.05	0.12	0.39	0.79	0.81	0.88
G1	11586.1	0.27	0.06	0.89	0.90	0.96	0.00	0.57	0.59	0.70	0.21	0.05	0.12	0.39	0.25	0.30	0.52
G2	50180.3	1.15	0.00	0.89	0.90	0.96	1.15	0.79	0.81	0.88	0.00	0.03	0.09	0.36	0.79	0.81	0.88
H1	7154.6	0.16	0.00	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.16	0.03	0.09	0.36	0.03	0.09	0.36
H2	17510.6	0.40	0.00	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.40	0.03	0.09	0.36	0.03	0.09	0.36
H3	1583.1	0.04	0.00	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.04	0.03	0.09	0.36	0.03	0.09	0.36
H4	4363.6	0.10	0.00	0.79	0.81	0.88	0.00	0.23	0.30	0.50	0.10	0.03	0.09	0.36	0.03	0.09	0.36
II	23800.3	0.55	0.33	0.89	0.90	0.96	0.21	0.71	0.73	0.81	0.00	0.07	0.16	0.41	0.82	0.83	0.90
I2	21018.4	0.48	0.32	0.89	0.90	0.96	0.12	0.71	0.73	0.81	0.05	0.07	0.16	0.41	0.77	0.79	0.87
I3	19407.4	0.45	0.31	0.89	0.90	0.96	0.08	0.71	0.73	0.81	0.05	0.07	0.16	0.41	0.76	0.78	0.87
I4	23928.1	0.55	0.40	0.89	0.90	0.96	0.11	0.71	0.73	0.81	0.04	0.07	0.16	0.41	0.80	0.81	0.89
I5	10207.0	0.23	0.12	0.89	0.90	0.96	0.08	0.71	0.73	0.81	0.04	0.07	0.16	0.41	0.71	0.73	0.83
I6	8155.2	0.19	0.12	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.07	0.07	0.16	0.41	0.58	0.62	0.75
I7	10159.6	0.23	0.19	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.04	0.07	0.16	0.41	0.75	0.77	0.87
J1	30237.3	0.69	0.52	0.89	0.90	0.96	0.12	0.71	0.73	0.81	0.06	0.07	0.16	0.41	0.79	0.81	0.89
J2	10980.0	0.25	0.14	0.89	0.90	0.96	0.08	0.71	0.73	0.81	0.04	0.07	0.16	0.41	0.71	0.73	0.83
J3	626.0	0.01	0.00	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.01	0.07	0.16	0.41	0.07	0.16	0.41
K1	7398.7	0.17	0.12	0.89	0.90	0.96	0.04	0.71	0.73	0.81	0.01	0.07	0.16	0.41	0.81	0.83	0.90
K2	2320.2	0.05	0.01	0.89	0.90	0.96	0.04	0.71	0.73	0.81	0.00	0.07	0.16	0.41	0.70	0.72	0.81
K3	6474.8	0.15	0.09	0.89	0.90	0.96	0.05	0.71	0.73	0.81	0.01	0.07	0.16	0.41	0.76	0.78	0.87
K4	2266.5	0.05	0.00	0.89	0.90	0.96	0.05	0.71	0.73	0.81	0.00	0.07	0.16	0.41	0.66	0.69	0.78
L	57315.2	1.32	0.00	0.89	0.90	0.96	0.00	0.71	0.73	0.81	1.32	0.03	0.09	0.36	0.03	0.09	0.36
M1	12396.2	0.28	0.19	0.89	0.90	0.96	0.08	0.71	0.73	0.81	0.02	0.07	0.16	0.41	0.79	0.81	0.88
M2	10573.8	0.24	0.00	0.89	0.90	0.96	0.20	0.71	0.73	0.81	0.05	0.07	0.16	0.41	0.58	0.62	0.73
M3	15906.8	0.37	0.33	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.04	0.07	0.16	0.41	0.81	0.83	0.91
M4	42578.8	0.98	0.77	0.89	0.90	0.96	0.11	0.71	0.73	0.81	0.10	0.05	0.12	0.39	0.79	0.80	0.89
N1	2827.1	0.06	0.06	0.89	0.90	0.96	0.00	0.71	0.73	0.81	0.00	0.07	0.16	0.41	0.89	0.90	0.96
N2	18017.7	0.41	0.00	0.89	0.90	0.96	0.00	0.23	0.30	0.50	0.41	0.05	0.12	0.39	0.05	0.12	0.39
O1	5318.2	0.12	0.01	0.89	0.90	0.96	0.00	0.23	0.30	0.50	0.12	0.05	0.12	0.41	0.10	0.16	0.44
O2	2824.6	0.06	0.01	0.89	0.90	0.96	0.00	0.23	0.30	0.50	0.06	0.05	0.12	0.41	0.16	0.22	0.48
P	4961.4	0.11	0.00	0.89	0.90	0.96	0.00	0.23	0.30	0.50	0.11	0.03	0.09	0.36	0.03	0.09	0.36

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**PROPOSED DRAINAGE CALCULATIONS**  
*(Area Drainage Summary)*

From Area Runoff Coefficient Summary					OVERLAND			STREET / CHANNEL FLOW				Time of Travel ( $T_t$ )		INTENSITY *			TOTAL FLOWS			
BASIN	AREA TOTAL (Acres)	C <sub>2</sub>	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	*TOTAL (min)	CHECK (min)	I <sub>2</sub> (in/hr)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>2</sub> (c.f.s.)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)
<i>A</i>	0.21	0.03	0.09	0.36	0.09	40	5.0	5.0	0	0.0%	0.0	0.0	5.0	10.2	4.1	5.2	8.7	<b>0.0</b>	<b>0.1</b>	<b>0.7</b>
<i>B</i>	1.50	0.79	0.81	0.88	0.81	80	1.0	4.4	240	1.7%	2.6	1.5	5.9	11.8	3.9	4.9	8.3	<b>4.6</b>	<b>6.0</b>	<b>10.9</b>
<i>C</i>	0.12	0.03	0.09	0.36	0.09	40	16.0	3.4	0	0.0%	0.0	0.0	5.0	10.2	4.1	5.2	8.7	<b>0.0</b>	<b>0.1</b>	<b>0.4</b>
<i>C1</i>	0.17	0.03	0.09	0.36	0.09	60	22.0	4.3	0	0.0%	0.0	0.0	5.0	10.3	4.1	5.2	8.7	<b>0.0</b>	<b>0.1</b>	<b>0.5</b>
<i>D</i>	0.77	0.79	0.81	0.88	0.81	60	1.2	3.2	250	1.6%	2.5	1.6	5.0	11.7	4.1	5.2	8.7	<b>2.5</b>	<b>3.2</b>	<b>5.9</b>
<i>D1</i>	0.78	0.79	0.81	0.88	0.81	60	1.2	3.2	250	1.6%	2.5	1.6	5.0	11.7	4.1	5.2	8.7	<b>2.5</b>	<b>3.3</b>	<b>6.0</b>
<i>E1</i>	0.27	0.87	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.7	5.0	11.7	4.1	5.2	8.7	<b>1.0</b>	<b>1.2</b>	<b>2.2</b>
<i>E2</i>	0.21	0.87	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.7	5.0	11.7	4.1	5.2	8.7	<b>0.7</b>	<b>1.0</b>	<b>1.7</b>
<i>F</i>	0.30	0.79	0.81	0.88	0.81	60	1.2	3.2	150	1.3%	2.3	1.1	5.0	11.2	4.1	5.2	8.7	<b>1.0</b>	<b>1.2</b>	<b>2.3</b>
<i>G1</i>	0.27	0.25	0.30	0.52	0.30	30	1.0	5.3	0	0.0%	0.0	0.0	5.3	10.2	4.1	5.1	8.5	<b>0.3</b>	<b>0.4</b>	<b>1.2</b>
<i>G2</i>	1.15	0.79	0.81	0.88	0.81	60	0.6	4.1	400	1.0%	2.0	3.3	7.4	12.6	3.7	4.6	7.7	<b>3.3</b>	<b>4.3</b>	<b>7.8</b>
<i>H1</i>	0.16	0.03	0.09	0.36	0.09	76	20.0	5.4	0	0.0%	0.0	0.0	5.4	10.4	4.0	5.1	8.5	<b>0.0</b>	<b>0.1</b>	<b>0.5</b>
<i>H2</i>	0.40	0.03	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	3.7	4.6	7.8	<b>0.0</b>	<b>0.2</b>	<b>1.1</b>
<i>H3</i>	0.04	0.03	0.09	0.36	0.09	100	17.0	7.2	0	2.0%	1.4	0.0	7.2	10.6	3.7	4.6	7.8	<b>0.0</b>	<b>0.0</b>	<b>0.1</b>
<i>H4</i>	0.10	0.03	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	3.7	4.6	7.8	<b>0.0</b>	<b>0.0</b>	<b>0.3</b>
<i>I1</i>	0.55	0.82	0.83	0.90	0.83	100	3.0	3.4	216	2.5%	3.2	1.1	5.0	11.8	4.1	5.2	8.7	<b>1.8</b>	<b>2.3</b>	<b>4.3</b>
<i>I2</i>	0.48	0.77	0.79	0.87	0.79	50	2.0	2.5	261	1.0%	2.0	2.2	5.0	11.7	4.1	5.2	8.7	<b>1.5</b>	<b>2.0</b>	<b>3.6</b>
<i>I3</i>	0.45	0.76	0.78	0.87	0.78	67	2.6	3.0	246	0.9%	1.8	2.2	5.2	11.7	4.1	5.1	8.6	<b>1.4</b>	<b>1.8</b>	<b>3.3</b>
<i>I4</i>	0.55	0.80	0.81	0.89	0.81	67	2.6	2.7	246	0.9%	1.8	2.2	5.0	11.7	4.1	5.2	8.7	<b>1.8</b>	<b>2.3</b>	<b>4.2</b>
<i>I5</i>	0.23	0.71	0.73	0.83	0.73	25	0.5	2.6	146	1.4%	2.4	1.0	5.0	11.0	4.1	5.2	8.7	<b>0.7</b>	<b>0.9</b>	<b>1.7</b>
<i>I6</i>	0.19	0.58	0.62	0.75	0.62	31	0.3	4.8	120	1.3%	2.3	0.9	5.7	10.8	4.0	5.0	8.3	<b>0.4</b>	<b>0.6</b>	<b>1.2</b>
<i>I7</i>	0.23	0.75	0.77	0.87	0.77	50	0.3	5.2	133	1.1%	2.1	1.1	6.2	11.0	3.9	4.8	8.1	<b>0.7</b>	<b>0.9</b>	<b>1.6</b>
<i>J1</i>	0.69	0.79	0.81	0.89	0.81	85	3.0	3.2	327	0.9%	1.9	2.8	6.1	12.3	3.9	4.9	8.2	<b>2.1</b>	<b>2.7</b>	<b>5.1</b>
<i>J2</i>	0.25	0.71	0.73	0.83	0.73	25	0.5	2.6	185	1.4%	2.3	1.3	5.0	11.2	4.1	5.2	8.7	<b>0.7</b>	<b>1.0</b>	<b>1.8</b>
<i>J3</i>	0.01	0.07	0.16	0.41	0.16	10	1.0	2.6	0	0.0%	0.0	0.0	5.0	10.1	4.1	5.2	8.7	<b>0.0</b>	<b>0.0</b>	<b>0.1</b>
<i>K1</i>	0.17	0.81	0.83	0.90	0.83	25	0.5	2.0	115	3.0%	3.5	0.5	5.0	10.8	4.1	5.2	8.7	<b>0.6</b>	<b>0.7</b>	<b>1.3</b>
<i>K2</i>	0.05	0.70	0.72	0.81	0.72	25	0.5	2.7	55	1.8%	2.7	0.3	5.0	10.4	4.1	5.2	8.7	<b>0.2</b>	<b>0.2</b>	<b>0.4</b>
<i>K3</i>	0.15	0.76	0.78	0.87	0.78	25	0.5	2.3	120	1.4%	2.4	0.8	5.0	10.8	4.1	5.2	8.7	<b>0.5</b>	<b>0.6</b>	<b>1.1</b>
<i>K4</i>	0.05	0.66	0.69	0.78	0.69	25	0.5	3.0	91	1.0%	2.0	0.8	5.0	10.6	4.1	5.2	8.7	<b>0.1</b>	<b>0.2</b>	<b>0.4</b>
<i>L</i>	1.32	0.03	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	3.7	4.6	7.8	<b>0.1</b>	<b>0.5</b>	<b>3.7</b>
<i>M1</i>	0.28	0.79	0.81	0.88	0.81	25	0.5	2.1	203	1.0%	2.0	1.7	5.0	11.3	4.1	5.2	8.7	<b>0.9</b>	<b>1.2</b>	<b>2.2</b>
<i>M2</i>	0.24	0.58	0.62	0.73	0.62	25	0.5	3.5	148	1.0%	1.5	1.6	5.1	11.0	4.1	5.1	8.6	<b>0.6</b>	<b>0.8</b>	<b>1.5</b>
<i>M3</i>	0.37	0.81	0.83	0.91	0.83	50	2.0	2.2	112	2.5%	3.2	0.6	5.0	10.9	4.1	5.2	8.7	<b>1.2</b>	<b>1.6</b>	<b>2.9</b>
<i>M4</i>	0.98	0.79	0.80	0.89	0.80	100	1.0	5.3	326	1.2%	2.2	2.4	7.8	12.4	3.6	4.5	7.6	<b>2.8</b>	<b>3.5</b>	<b>6.6</b>
<i>N1</i>	0.06	0.89	0.90	0.96	0.90	50	1.0	2.0	0	0.0%	0.0	0.0	5.0	10.3	4.1	5.2	8.7	<b>0.2</b>	<b>0.3</b>	<b>0.5</b>
<i>N2</i>	0.41	0.05	0.12	0.39	0.12	60	1.2	10.9	30	33.0%	11.5	0.0	10.9	10.5	3.2	4.1	6.8	<b>0.1</b>	<b>0.2</b>	<b>1.1</b>
<i>O1</i>	0.12	0.10	0.16	0.44	0.16	32	0.5	8.3	0	0.0%	0.0	0.0	8.3	10.2	3.5	4.4	7.4	<b>0.0</b>	<b>0.1</b>	<b>0.4</b>
<i>O2</i>	0.06	0.16	0.22	0.48	0.22	25	0.5	6.3	0	0.0%	0.0	0.0	6.3	10.1	3.8	4.8	8.1	<b>0.0</b>	<b>0.1</b>	<b>0.3</b>
<i>P</i>	0.11	0.03	0.09	0.36	0.09	25	0.5	7.1	0	0.0%	0.0	0.0	7.1	10.1	3.7	4.6	7.8	<b>0.0</b>	<b>0.0</b>	<b>0.3</b>

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**PROPOSED DRAINAGE CALCULATIONS**  
*(Basin Routing Summary)*

DESIGN POINT	CONTRIBUTING BASINS DPS AND/OR PIPES	From Area Runoff Coefficient Summary			OVERLAND			PIPE / CHANNEL FLOW			Time of Travel ( $T_t$ )		INTENSITY*			TOTAL FLOWS			COMMENTS
		CA <sub>2</sub>	CA <sub>3</sub>	CA <sub>100</sub>	C <sub>4</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	*TOTAL (min)	I <sub>2</sub> (in/hr)	I <sub>3</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>2</sub> (c.f.s.)	Q <sub>3</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)
1	A, B	1.19	1.23	1.40		Basin A Tc used + Basin B routing						6.6	3.8	4.8	8.0	4.5	5.9	11.2	Proposed PVT 18" Storm Sewer
2	C, D	0.61	0.64	0.72		Basin C Tc used + Basin D routing						6.6	3.8	4.7	8.0	2.3	3.0	5.8	Proposed PVT 15" Storm Sewer
3	F	0.23	0.24	0.26		Basin F Tc used						5.0	4.1	5.2	8.7	1.0	1.2	2.3	Proposed PVT 15" Storm Sewer
4	E2	0.18	0.18	0.20		Basin E1 Tc used						5.0	4.1	5.2	8.7	0.7	1.0	1.7	Proposed 5' Type R Sump Inlet
5	E1	0.23	0.24	0.25		Basin E2 Tc used						5.0	4.1	5.2	8.7	1.0	1.2	2.2	Proposed 5' Type R Sump Inlet
6	C1, D1, PR6	1.04	1.07	1.20		Basin C1 Tc used + Basin D1 routing						6.6	3.8	4.7	8.0	3.9	5.1	9.6	Exist PVT 24" Storm Sewer
7	G2	0.91	0.93	1.01		TAKEN FROM BASIN G2						5.3	4.1	5.1	8.5	3.7	4.7	8.7	Existing Curb and Gutter
8	H1, II	0.45	0.47	0.55		Basin H1 Tc used + Basin II routing						7.1	3.7	4.6	7.8	1.7	2.2	4.3	Existing Curb and Gutter
9	H2, I2	0.38	0.42	0.56		Basin H2 Tc used + Basin I2 routing						8.9	3.4	4.3	7.2	1.3	1.8	4.1	Existing Curb and Gutter
10	H3, I7	0.18	0.18	0.22		Basin H1 Tc used + Basin II routing						8.6	3.5	4.4	7.3	0.6	0.8	1.6	Existing Curb and Gutter
11	DP3, DP4, DP5 I3, I4, I5, I6	2.06	2.15	2.54		Basin H3 Tc used + Basin I7 Routing						11.5	3.1	3.9	6.6	6.5	8.4	16.7	2-Exist 15' CDOT Type R Inlet  assumed split flows 100-yr
12	FB INLET 3, J1	0.55	0.58	0.98		Basin J1 Tc Used						6.1	3.9	4.9	8.2	2.1	2.8	8.1	Exist 15' CDOT Type R Inlet
13	FB INLET 4, J2, J3	0.18	0.19	0.58		Basin J2 Tc Used						5.0	4.1	5.2	8.7	0.7	1.0	5.0	Exist 15' CDOT Type R Inlet
14	H4, L, M4 DP14	0.81	0.91	1.38		Basin L Tc used + Basin M4 Routing						9.6	3.3	4.2	7.0	2.7	3.8	9.7	Existing Pvt Swale
15	M1, M2, M3	1.25	1.37	1.88		Basin DP9 Tc used + Basin M3 Routing						11.7	3.1	3.9	6.5	3.9	5.3	12.3	Existing Pvt Swale/Concrete Riprap Rundown
16	M1, K4	0.26	0.27	0.29		Basin M1 Tc Used						5.0	4.1	5.2	8.7	1.1	1.4	2.5	Existing Conc. Rock Rundown
17	K2, K3, N1	0.21	0.21	0.23		Basin K3 Tc Used						5.0	4.1	5.2	8.7	0.9	1.1	2.0	Existing Conc. Rock Rundown
18	K1	0.14	0.14	0.15		Basin K1 Tc Used						5.0	4.1	5.2	8.7	0.6	0.7	1.3	Existing Inlet
19	DP10, DP11, DP12 DP13, N2, PR14, PR17	2.74	5.09	6.84		DP10 Tc Used						11.7	3.1	3.9	6.5	8.5	19.8	44.7	Existing Sand Filter FSD Pond 2

**DESIGN POINT REVISED**

DP15 thru 18 instead  
of 10 thru 13

**DESIGN POINTS REVISED**

ons assume a minimum travel time of 5 minutes.

Calculated by: DLM  
 Date: 2/20/2023  
 Checked by: VAS

**FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.2**  
**PROPOSED DRAINAGE CALCULATIONS**  
*(Storm Sewer Routing Summary)*

PIPE RUN	Contributing Pipes/Design Points	Equivalent CA <sub>5</sub>	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	Intensity*				Pipe Size
					I <sub>5</sub>	I <sub>100</sub>	Q <sub>5</sub>	Q <sub>100</sub>	
1	FUTURE POND 1 OUTFALL	0.98	1.37	30.0	2.5	4.2	2.4	5.7	PROP 18" PP
2	FUTURE POND 2 OUTFALL	0.42	0.58	30.0	2.5	4.2	1.0	2.4	PROP 18" PP
3	FUTURE POND 4 OUTFALL	0.18	0.24	30.0	2.5	4.2	0.4	1.0	PROP 18" PP
4	PR1, PR2, PR3	1.58	2.19	30.0	2.5	4.2	3.9	9.1	PROP 24" PP
5	DP4	0.18	0.20	5.0	5.2	8.7	1.0	1.7	PROP 24" PP
6	PR5, DP5	0.42	0.45	5.0	5.2	8.7	2.2	3.9	PROP 18" PP
6A	C1 90%D1	0.56	0.58	5.0	5.2	8.7	2.9	5.1	PROP 18" PP
7	POND 3 OUTFALL	0.78	0.96	30.0	2.5	4.2	1.9	4.0	PROP 24" PP
8	PR4, PR7	2.36	3.15	30.0	2.5	4.2	5.9	13.1	PROP 18" PP
9	FUTURE POND 5 OUTFALL	0.52	0.73	30.0	2.5	4.2	1.3	3.0	PROP 24" PP
10	PR8, PR9	2.88	3.88	30.0	2.5	4.2	7.1	16.2	PROP 24" PP
11	PR10	2.88	3.88	30.0	2.5	4.2	7.1	16.2	EX 24" PP
12	PR11	2.88	3.88	30.0	2.5	4.2	7.1	16.2	EX 24" PP
13	INLET 3	1.07	1.22	11.5	3.9	6.6	4.2	8.0	PROP 15" PP
14	PR13, INLET 4	2.15	2.43	11.5	3.9	6.6	8.4	16.0	PROP 24" PP
15	INLET 5	0.58	0.95	6.1	4.9	8.2	2.8	7.8	PROP 24" PP
16	PR15, INLET 6	0.77	1.53	6.1	4.9	8.2	3.7	12.6	PROP 18" PP
17	PR16, DP18	0.91	1.69	6.1	4.9	8.2	4.4	13.8	EXIST 24" PP
18	POND 2 OUTFALL	5.52	5.72	30.0	2.5	4.2	13.7	23.8	EXIST 24" PP
19	PR18, PR12	8.40	9.60	30.0	2.5	4.2	20.8	40.0	EXIST 42" RCP

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point

PR - Pipe Run

FB- Flow By from Design Point

INT- Intercepted Flow from Design Point

Calculated by: DLM

Date: 2/20/2023

Checked by: VAS

\*\*Existing undeveloped

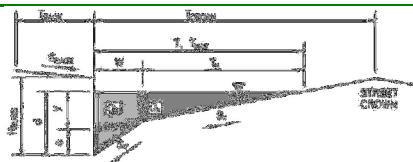
\*\*\*Ultimate build out, developed. Used to size future pond 1 and storm sewer.

## **HYDRAULIC CALCULATIONS / SFB WQCV CALCULATIONS**

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
**Inlet ID:** Inlet 3 DP 6 (North)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
Distance from Curb Face to Street Crown  
Gutter Width  
Street Transverse Slope  
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
Street Longitudinal Slope - Enter 0 for sump condition  
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>X</sub> =	0.020	ft/ft
S <sub>W</sub> =	0.083	ft/ft
S <sub>O</sub> =	0.012	ft/ft
n <sub>STREET</sub> =	0.015	

Max. Allowable Spread for Minor & Major Storm  
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

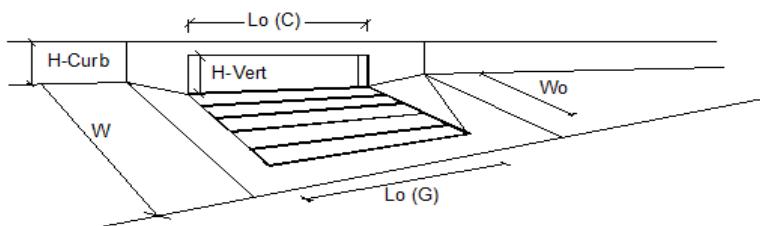
Minor Storm		Major Storm	
T <sub>MAX</sub> =	15.8	17.0	ft
d <sub>MAX</sub> =	4.6	7.8	inches

MINOR STORM Allowable Capacity is based on Depth Criterion  
MAJOR STORM Allowable Capacity is based on Spread Criterion  
**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.10 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.30 cfs on sheet 'Inlet Management'**

Minor Storm		Major Storm	
Q <sub>allow</sub> =	6.5	12.7	cfs

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

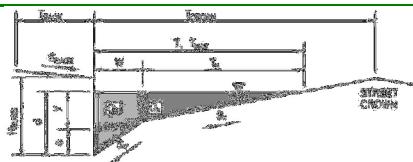


<b>Design Information (Input)</b>	CDOT Type R Curb Opening
Type of Inlet	
Local Depression (additional to continuous gutter depression 'a')	
Total Number of Units in the Inlet (Grate or Curb Opening)	
Length of a Single Unit Inlet (Grate or Curb Opening)	
Width of a Unit Grate (cannot be greater than W, Gutter Width)	
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	
Street Hydraulics: OK - Q < Allowable Street Capacity'	
Total Inlet Interception Capacity	
Total Inlet Carry-Over Flow (flow bypassing inlet)	
Capture Percentage = $Q_b/Q_a$	
<b>MINOR</b>	
<b>MAJOR</b>	
Type =	
$a_{LOCAL} =$	MINOR      MAJOR
$N_o =$	3.0      3.0
$L_o =$	inches
$W_o =$	5.00      5.00
$C_f(G) =$	ft
$C_f(C) =$	N/A      N/A
$C_f(C) =$	ft
<b>MINOR</b>	
<b>MAJOR</b>	
Q =	
$Q_b =$	4.1      7.9
$C\% =$	cfs
0.0      0.4	
100      96	
%cfs	

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
**Inlet ID:** Inlet 4 DP6 (South)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
Distance from Curb Face to Street Crown  
Gutter Width  
Street Transverse Slope  
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
Street Longitudinal Slope - Enter 0 for sump condition  
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>X</sub> =	0.020	ft/ft
S <sub>W</sub> =	0.083	ft/ft
S <sub>O</sub> =	0.011	ft/ft
n <sub>STREET</sub> =	0.016	

Max. Allowable Spread for Minor & Major Storm  
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

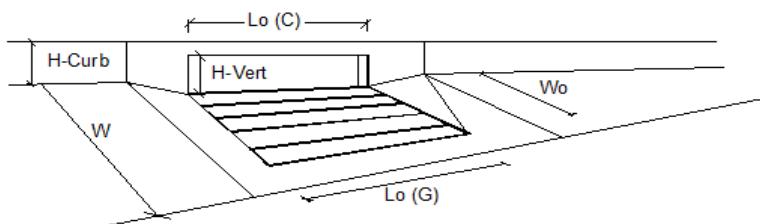
Minor Storm		Major Storm	
T <sub>MAX</sub> =	15.8	17.0	ft
d <sub>MAX</sub> =	4.6	7.8	inches

MINOR STORM Allowable Capacity is based on Depth Criterion  
MAJOR STORM Allowable Capacity is based on Spread Criterion  
**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.10 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.30 cfs on sheet 'Inlet Management'**

Minor Storm		Major Storm	
Q <sub>allow</sub> =	5.8	11.4	cfs

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

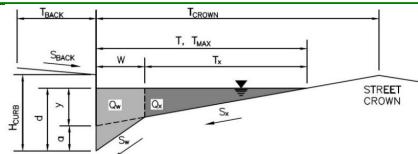


<b>Design Information (Input)</b>	CDOT Type R Curb Opening
Type of Inlet	
Local Depression (additional to continuous gutter depression 'a')	
Total Number of Units in the Inlet (Grate or Curb Opening)	
Length of a Single Unit Inlet (Grate or Curb Opening)	
Width of a Unit Grate (cannot be greater than W, Gutter Width)	
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	
Street Hydraulics: OK - Q < Allowable Street Capacity'	
Total Inlet Interception Capacity	
Total Inlet Carry-Over Flow (flow bypassing inlet)	
Capture Percentage = $Q_c/Q_o$	
<b>MINOR                    MAJOR</b>	
<b>Type = CDOT Type R Curb Opening</b>	
$a_{LOCAL} =$	3.0                    3.0
$N_o =$	3                    3
$L_o =$	5.00                    5.00
$W_o =$	N/A                    N/A
$C_f (G) =$	N/A                    N/A
$C_f (C) =$	0.10                    0.10
<b>MINOR                    MAJOR</b>	
<b><math>Q =</math></b>	
$Q =$	4.1                    8.0
$Q_b =$	0.0                    0.3
$C\% =$	100                    96
<b>cfs                    cfs                    %</b>	

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
 Inlet ID: Inlet 5 DP7 (North)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>x</sub> =	0.020	ft/ft
S <sub>w</sub> =	0.083	ft/ft
S <sub>0</sub> =	0.010	ft/ft
n <sub>STREET</sub> =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
T <sub>MAX</sub> =	15.8	17.0
d <sub>MAX</sub> =	4.6	7.8

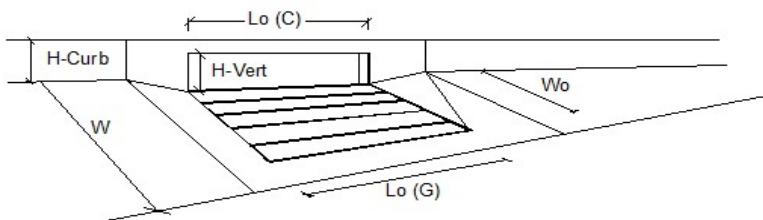
MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

Minor Storm	Major Storm
Q <sub>allow</sub> =	5.9      11.6
cfs	

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 2.40 cfs on sheet 'Inlet Management'  
 Major storm max. allowable capacity GOOD - greater than the design peak flow of 7.50 cfs on sheet 'Inlet Management'

## INLET ON A CONTINUOUS GRADE

*MHFD-Inlet, Version 5.02 (August 2022)*

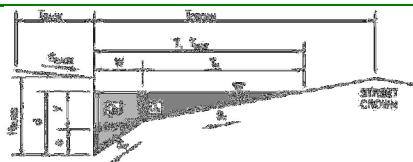


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	inches	
Local Depression (additional to continuous gutter depression 'a')		a <sub>local</sub> =	3.0	3.0	
Total Number of Units in the Inlet (Grate or Curb Opening)		N <sub>o</sub> =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>f</sub> (G) =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>f</sub> (C) =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity'</b>					
Total Inlet Interception Capacity		MINOR	MAJOR		
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q =	2.4	7.3	cfs
Capture Percentage = Q <sub>b</sub> /Q <sub>a</sub>		Q <sub>b</sub> =	0.0	0.2	cfs
		C% =	100	98	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
 Inlet ID: Inlet 6 DP7 (South)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>X</sub> =	0.020	ft/ft
S <sub>W</sub> =	0.083	ft/ft
S <sub>O</sub> =	0.010	ft/ft
n <sub>STREET</sub> =	0.016	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

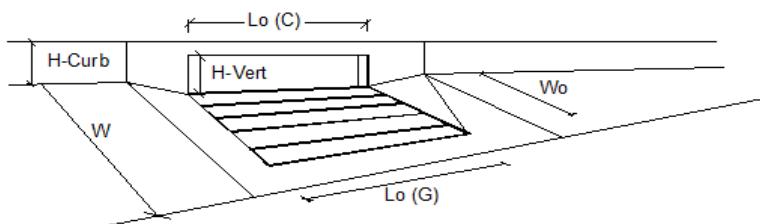
Minor Storm		Major Storm	
T <sub>MAX</sub> =	15.8	17.0	ft
d <sub>MAX</sub> =	4.6	7.8	inches

MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion  
**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 0.90 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 4.10 cfs on sheet 'Inlet Management'**

Minor Storm		Major Storm	
Q <sub>allow</sub> =	5.5	10.9	cfs

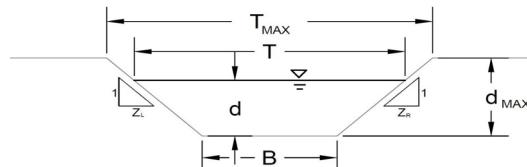
## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)



<b>Design Information (Input)</b>	CDOT Type R Curb Opening
Type of Inlet	
Local Depression (additional to continuous gutter depression 'a')	
Total Number of Units in the Inlet (Grate or Curb Opening)	
Length of a Single Unit Inlet (Grate or Curb Opening)	
Width of a Unit Grate (cannot be greater than W, Gutter Width)	
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	
Street Hydraulics: OK - Q < Allowable Street Capacity'	
Total Inlet Interception Capacity	
Total Inlet Carry-Over Flow (flow bypassing inlet)	
Capture Percentage = $Q_c/Q_o$	
<b>MINOR                    MAJOR</b>	
<b>Type = CDOT Type R Curb Opening</b>	
$a_{LOCAL} =$	3.0                    3.0
$N_o =$	3                    3
$L_o =$	5.00                    5.00
$W_o =$	N/A                    N/A
$C_f (G) =$	N/A                    N/A
$C_f (C) =$	0.10                    0.10
<b>MINOR                    MAJOR</b>	
<b><math>Q =</math>      <math>Q_b =</math>      <math>C\% =</math></b>	
<b>0.9                    4.1                    cfs</b>	
<b>0.0                    0.0                    cfs</b>	
<b>100                    100                    %</b>	

## AREA INLET IN A SWALE

Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
Inlet 7 (DP13)

This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see  
Section 7.2.3 of the USDCM.

## Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

A, B, C, D, or E = 

Manning's n (Leave cell D16 blank to manually enter an n value)

n = 

Channel Invert Slope

S<sub>0</sub> =  ft/ft

Bottom Width

B =  ft

Left Side Slope

Z<sub>L</sub> =  ft/ft

Right Side Slope

Z<sub>R</sub> =  ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V <sub>MAX</sub> )	Max Froude No. (F <sub>MAX</sub> )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:

- Non-Cohesive
- Cohesive
- Paved

	Minor Storm	Major Storm	
T <sub>MAX</sub> =	1.92	2.40	ft
d <sub>MAX</sub> =	0.32	0.40	ft

Maximum Allowable Top Width of Channel for Minor &amp; Major Storm

	Minor Storm	Major Storm	
Q <sub>allow</sub> =	1.8	3.3	cfs
d <sub>allow</sub> =	0.32	0.40	ft

Maximum Allowable Water Depth in Channel for Minor &amp; Major Storm

	Minor Storm	Major Storm	
Q <sub>o</sub> =	0.7	1.3	cfs
d =	0.22	0.28	ft

## Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

Minor Storm      Major Storm

MAJOR STORM Allowable Capacity is based on Depth Criterion

d<sub>allow</sub> =  ft

## Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Q<sub>o</sub> =  cfs

Water Depth

d =  ft**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'****Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## AREA INLET IN A SWALE

Claremont Business Park 2 Filing No. 2 (Existing Conditions)  
Inlet 7 (DP13)

Inlet Design Information (Input)											
Type of Inlet	CDOT Type C (Depressed)										
Inlet Type =	CDOT Type C (Depressed)										
Angle of Inclined Grate (must be <= 30 degrees)											
Width of Grate	W = 3.00 ft										
Length of Grate	L = 3.00 ft										
Open Area Ratio	A <sub>RATIO</sub> = 0.70										
Height of Inclined Grate	H <sub>B</sub> = 0.00 ft										
Clogging Factor	C <sub>f</sub> = 0.50										
Grate Discharge Coefficient	C <sub>d</sub> = 0.84										
Orifice Coefficient	C <sub>o</sub> = 0.56										
Weir Coefficient	C <sub>w</sub> = 1.81										
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)											
Total Inlet Interception Capacity (assumes clogged condition)											
Bypassed Flow											
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub>											
<table border="1"> <thead> <tr> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>d = 1.22</td> <td>1.28</td> </tr> <tr> <td>Q<sub>a</sub> = 15.7</td> <td>16.1</td> </tr> <tr> <td>Q<sub>b</sub> = 0.0</td> <td>0.0</td> </tr> <tr> <td>C% = 100</td> <td>100</td> </tr> </tbody> </table>		MINOR	MAJOR	d = 1.22	1.28	Q <sub>a</sub> = 15.7	16.1	Q <sub>b</sub> = 0.0	0.0	C% = 100	100
MINOR	MAJOR										
d = 1.22	1.28										
Q <sub>a</sub> = 15.7	16.1										
Q <sub>b</sub> = 0.0	0.0										
C% = 100	100										

**Warning 04:** Froude No. exceeds USDCM Volume I recommendation.

CLAREMONT COMMERCIAL FILING NO. 2 (EXISTING CONDITIONS)

<i><b>Weighted Percent Imperviousness of Ex Fil1 WQ Sand Filter Pond 2</b></i>				
<i><b>Contributing Basins</b></i>	<i><b>Area (Acres)</b></i>	<i><b>C<sub>5</sub></b></i>	<i><b>Impervious % (I)</b></i>	<i><b>(Acres)*(I)</b></i>
<i><b>H1</b></i>	0.18	0.09	2	0.35
<i><b>H2</b></i>	0.40	0.09	2	0.80
<i><b>H3</b></i>	0.04	0.09	2	0.07
<i><b>H4</b></i>	0.10	0.09	2	0.20
<i><b>I1</b></i>	0.57	0.80	94.4	54.17
<i><b>I2</b></i>	0.48	0.79	93.8	45.26
<i><b>I3</b></i>	0.58	0.65	84.3	49.29
<i><b>I4</b></i>	0.43	0.80	94.4	40.59
<i><b>I5</b></i>	0.23	0.73	90	21.09
<i><b>I6</b></i>	0.19	0.62	82.1	15.37
<i><b>I7</b></i>	0.23	0.77	92.5	21.57
<i><b>J1</b></i>	0.76	0.69	87.1	66.22
<i><b>J2</b></i>	0.25	0.73	90	22.69
<i><b>J3</b></i>	0.01	0.16	13	0.19
<i><b>K1</b></i>	0.17	0.83	96.1	16.32
<i><b>K2</b></i>	0.05	0.72	89.3	4.76
<i><b>K3</b></i>	0.15	0.78	93.1	13.84
<i><b>K4</b></i>	0.05	0.69	87.1	4.53
<i><b>L</b></i>	1.32	0.09	2	2.63
<i><b>M1</b></i>	0.28	0.81	95	27.03
<i><b>M2</b></i>	0.24	0.62	82.1	19.93
<i><b>M3</b></i>	0.37	0.83	96.1	35.09
<i><b>M4</b></i>	0.98	0.80	94.4	92.27
<i><b>N1</b></i>	0.06	0.90	100	6.49
<i><b>N2</b></i>	0.41	0.12	7	2.90
<i><b>Totals</b></i>	<b>8.55</b>			<b>563.68</b>
<i><b>Imperviousness of WQ Pond 2</b></i>	<b>65.9</b>			

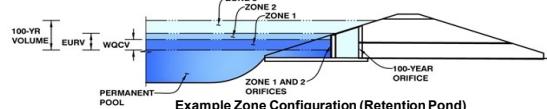
8.55    B soils  
 8.55 total area

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.02 (February 2020)*

**Project: CLAREMONT COMMERCIAL FILING N**

**Basin ID: WOCV POND 2 (Remodeled Existing Conditions**



## Watershed Information

Selected BMP Type =	<b>SF</b>
Watershed Area =	8.55
Watershed Length =	665
Watershed Length to Centroid =	325
Watershed Slope =	0.018
Watershed Imperviousness =	65.90%
Percentage Hydrologic Soil Group A =	0.0%
Percentage Hydrologic Soil Group B =	100.0%
Percentage Hydrologic Soil Groups C/D =	0.0%
Target WQV Rainfall Duration =	12.0
Location for 1-hr Rainfall Depths =	User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.147	acre-feet
Excess Urban Runoff Volume (EURV) =	0.616	acre-feet
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) =	0.539	acre-feet
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) =	0.733	acre-feet
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) =	0.899	acre-feet
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) =	1.100	acre-feet
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) =	1.274	acre-feet
100-yr Runoff Volume ( $P_1 = 2.5 \text{ in.}$ ) =	1.485	acre-feet
500-yr Runoff Volume ( $P_1 = 2.53 \text{ in.}$ ) =	1.492	acre-feet
Approximate 2-yr Detention Volume =	0.478	acre-feet
Approximate 5-yr Detention Volume =	0.640	acre-feet
Approximate 10-yr Detention Volume =	0.815	acre-feet
Approximate 25-yr Detention Volume =	0.877	acre-feet
Approximate 50-yr Detention Volume =	0.913	acre-feet
Approximate 100-yr Detention Volume =	0.986	acre-feet

## Define Zones and Basin Geometry

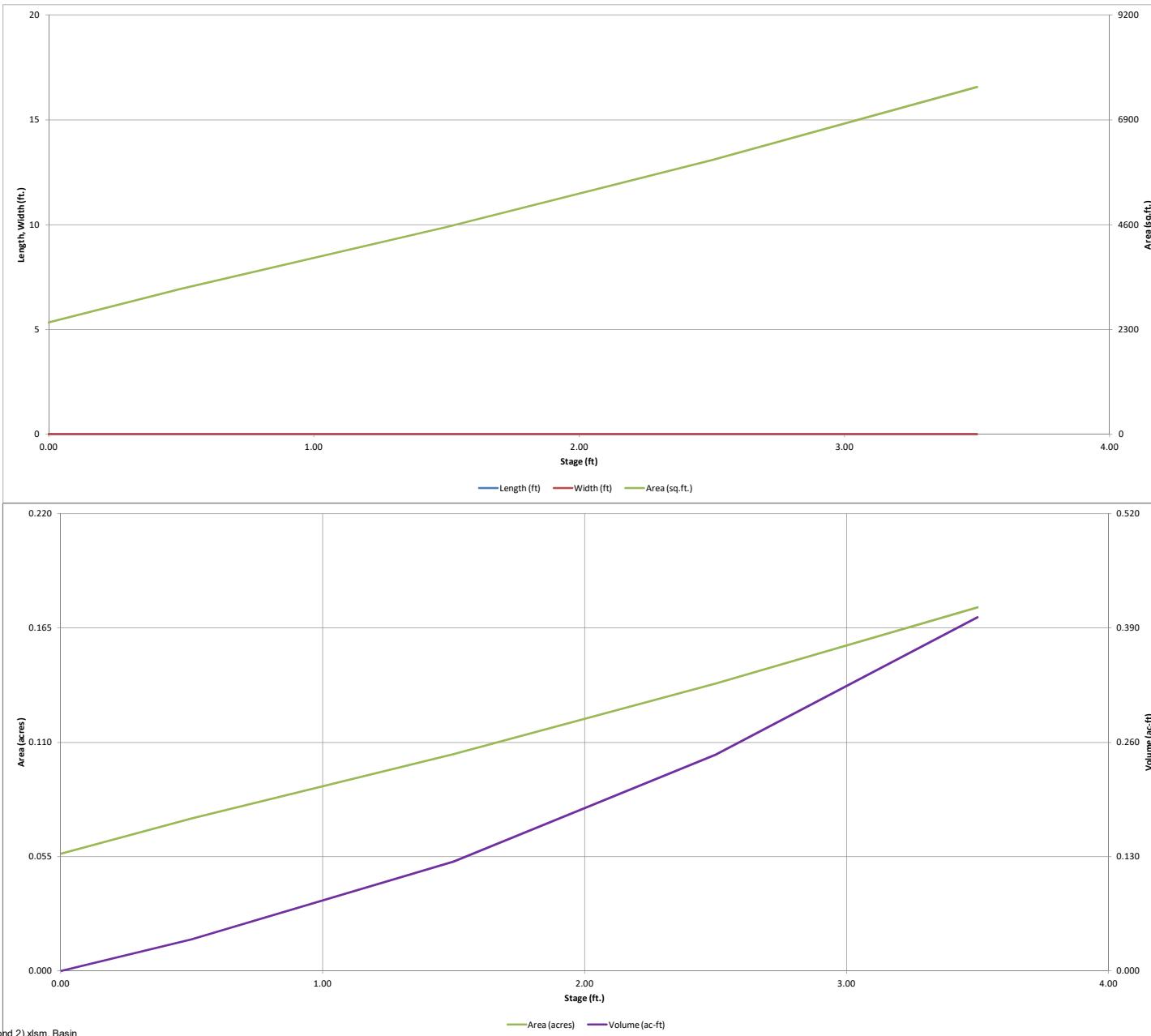
Zone 1 Volume (WQCV) =	0.147	acre-feet
Zone 2 Volume (100-year - Zone 1) =	0.839	acre-feet
Select Zone 3 Storage Volume (Optional) =		acre-feet
Total Detention Basin Volume =	0.986	acre-feet
Initial Surge Charge Volume (ISV) =	N/A	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth ( $H_{total}$ ) =	user	ft
Depth of Trickle Channel ( $H_{TC}$ ) =	N/A	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	N/A	ft/ft
Slopes of Main Basin Sides ( $S_{man}$ ) =	user	H:V
Basin Length-to-Width Ratio ( $R_{LW}$ ) =	user	

Initial Surcharge Area ( $A_{SV}$ ) =	user	$\text{ft}^2$
Surcharge Volume Length ( $L_{SV}$ ) =	user	$\text{ft}$
Surcharge Volume Width ( $W_{SV}$ ) =	user	$\text{ft}$
Depth of Basin Floor ( $H_{FLOOR}$ ) =	user	$\text{ft}$
Length of Basin Floor ( $L_{FLOOR}$ ) =	user	$\text{ft}$
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	$\text{ft}$
Area of Basin Floor ( $A_{FLOOR}$ ) =	user	$\text{ft}^2$
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	$\text{ft}^3$
Depth of Main Basin ( $H_{MAIN}$ ) =	user	$\text{ft}$
Length of Main Basin ( $L_{MAIN}$ ) =	user	$\text{ft}$
Width of Main Basin ( $W_{MAIN}$ ) =	user	$\text{ft}$
Area of Main Basin ( $A_{MAIN}$ ) =	user	$\text{ft}^2$
Volume of Main Basin ( $V_{MAIN}$ ) =	user	$\text{ft}^3$
Calculated Total Basin Volume (V...) =	user	acre-feet

6364

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.02 (February 2020)*



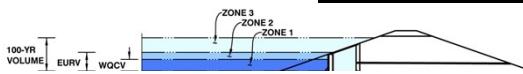
Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

Define "Remodeled Existing Conditions." How is this different for the other calcs for this same pond shown on pdf page 60 below? Please discuss in the FDR text above.

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention Version 4.02 (February 2022)

Project: CLAREMONT COMMERCIAL FILING NO.2  
Basin ID: WQCV POND 2 (Remodeled Existing Conditions)



Estimated Stage (ft)  
Zone 1 (WQCV) 1.76

**SHEET LABELED EXISTING CONDITION AND CORRESPONDING SHEET LABEL PROPOSED CONDITION EXTENTION OF EL JEFE HT.**

**TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT**

Calculated Parameters for Underdrain  
Underdrain Orifice Area = 0.0 ft<sup>2</sup>  
Underdrain Orifice Centroid = 0.07 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

Calculated Parameters for Plate  
WQ Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Stage of Orifice Centroid (ft)	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Stage of Orifice Centroid (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

Not Selected	Not Selected
Invert of Vertical Orifice =	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = Not Selected ft<sup>2</sup>  
Vertical Orifice Centroid = Not Selected feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Zone 2 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.75	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	7.00	feet
Overflow Weir Grate Slope =	0.00	H:V
Horiz. Length of Weir Sides =	2.91	feet
Overflow Grate Open Area % =	70%	%, grate open area/total area
Debris Clogging % =	50%	%

Calculated Parameters for Overflow Weir  
Zone 2 Weir = Not Selected feet  
Height of Grate Upper Edge, H<sub>t</sub> = 1.75 feet  
Overflow Weir Slope Length = 2.91 feet  
Grate Open Area / 100-yr Orifice Area = 6.47 ft<sup>2</sup>  
Overflow Grate Open Area w/o Debris = 14.26 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 7.13 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 2 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.75	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	inches
Restrictor Plate Height Above Pipe Invert =	13.80	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 2 Restrictor = Not Selected ft<sup>2</sup>  
Outlet Orifice Area = 2.20 feet  
Outlet Orifice Centroid = 0.67 feet  
Half-Central Angle of Restrictor Plate on Pipe = 1.49 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	3.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	12.50	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth= 0.75 feet  
Stage at Top of Freeboard = 4.75 feet  
Basin Area at Top of Freeboard = 0.18 acres  
Basin Volume at Top of Freeboard = 0.40 acre-ft

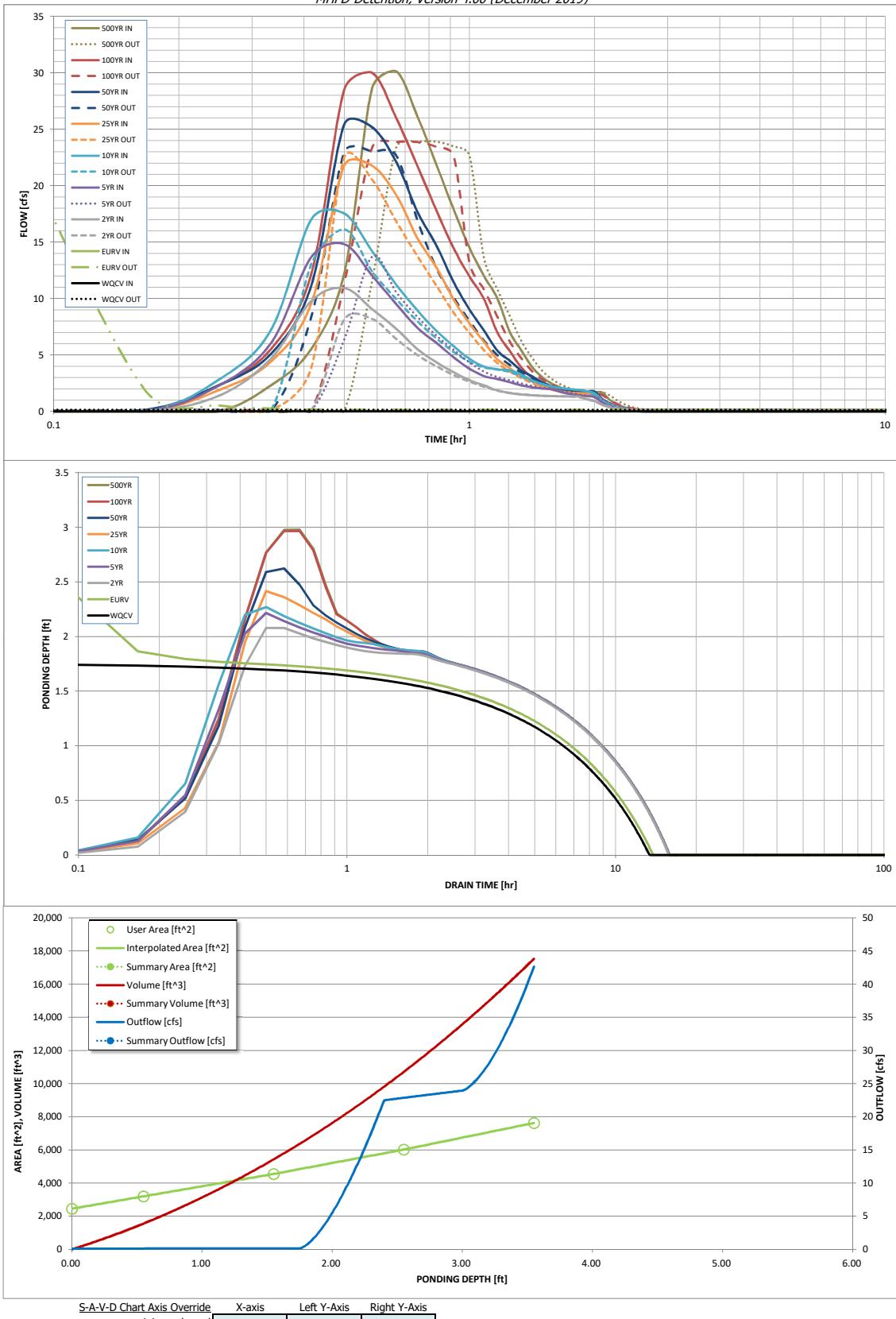
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	2.53
One-Hour Rainfall Depth (in) =	0.147	0.616	0.539	0.733	0.899	1.100	1.274	1.485	1.492
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.539	0.733	0.899	1.100	1.274	1.485	1.492
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A							
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.2	3.2	4.8	8.5	10.6	13.3	13.4
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.14	0.38	0.56	0.99	1.24	1.55	1.56
Peak Inflow Q (cfs) =	N/A	N/A	10.9	14.8	17.5	21.8	25.4	30.0	30.1
Peak Outflow Q (cfs) =	0.2	42.6	8.2	13.7	16.1	22.5	23.0	23.9	23.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	4.3	3.4	2.7	2.2	1.8	1.8
Structure Controlling Flow =	Overflow Weir 1	Outlet Plate 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	0.00	1.59	0.57	1.0	1.1	1.6	1.6	1.7	1.7
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	13	12	14	14	13	13	12	12	11
Time to Drain 99% of Inflow Volume (hours) =	13	13	15	15	15	15	15	14	14
Maximum Ponding Depth (ft) =	1.76	2.54	2.08	2.22	2.27	2.42	2.62	2.97	2.98
Area at Maximum Ponding Depth (acres) =	0.11	0.14	0.12	0.13	0.13	0.13	0.14	0.15	0.15
Maximum Volume Stored (acre-ft) =	0.147	0.243	0.183	0.201	0.207	0.227	0.256	0.306	0.307

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



S-A-V-D Chart Axis Override	X-axis	Left Y-axis	Right Y-axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*Outflow Hydrograph Workbook Filename:*

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)

<i><b>Weighted Percent Imperviousness of Proposed WQ Sand Filter Pond 1</b></i>				
<i><b>Contributing Basins</b></i>	<i><b>Area (Acres)</b></i>	<i><b>C<sub>s</sub></b></i>	<i><b>Impervious % (I)</b></i>	<i><b>(Acres)*(I)</b></i>
<i><b>A</b></i>	0.21	0.09	2	0.43
<i><b>B</b></i>	1.50	0.81	90	134.89
<i><b>Totals</b></i>	<i><b>1.71</b></i>			<i><b>135.31</b></i>
<i><b>Imperviousness % to FSD</b></i>	<i><b>79.0</b></i>			

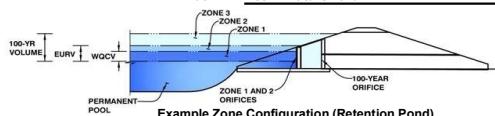
A soils            35%  
 B soils            65%

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Claremont Business Park 2 Filing No. 2

**Basin ID: Lot 1 - Future Pond**



## Watershed Information

Selected BMP Type =	<b>SF</b>
Watershed Area =	1.71
Watershed Length =	300
Watershed Length to Centroid =	150
Watershed Slope =	0.017
Watershed Imperviousness =	79.00%
Percentage Hydrologic Soil Group A =	35.0%
Percentage Hydrologic Soil Group B =	65.0%
Percentage Hydrologic Soil Groups C/D =	0.0%
Target WOCV Drain Time =	12.0

Location for 1-hr Rainfall Depths = User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

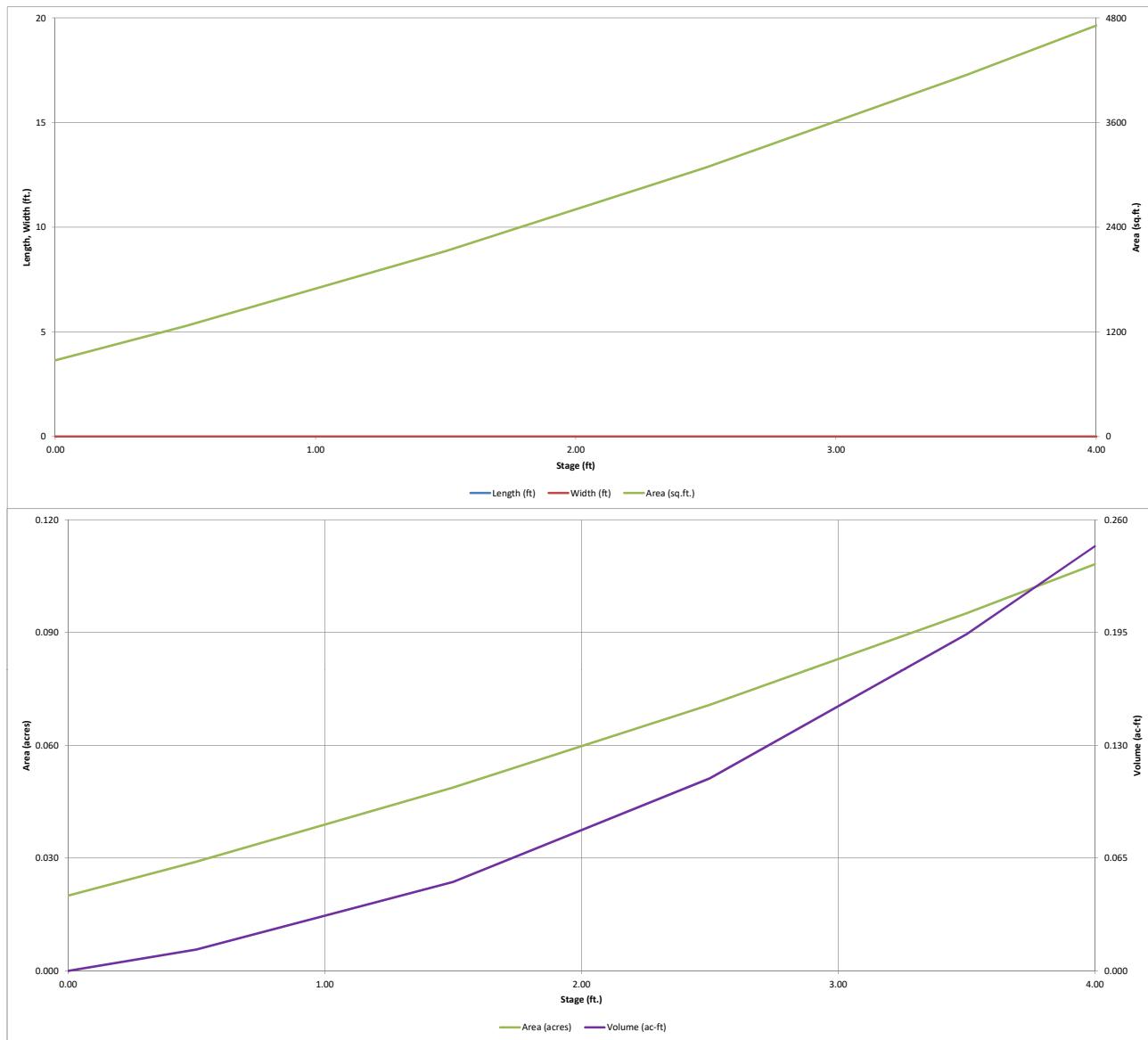
Water Quality Capture Volume (WQCV) =	0.037	acre-feet
Excess Urban Runoff Volume (EURV) =	0.159	acre-feet
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) =	0.121	acre-feet
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) =	0.159	acre-feet
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) =	0.192	acre-feet
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) =	0.229	acre-feet
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) =	0.263	acre-feet
100-yr Runoff Volume ( $P_1 = 2.5 \text{ in.}$ ) =	0.303	acre-feet
500-yr Runoff Volume ( $P_1 = 3.14 \text{ in.}$ ) =	0.388	acre-feet
Approximate 2-yr Detention Volume =	0.118	acre-feet
Approximate 5-yr Detention Volume =	0.155	acre-feet
Approximate 10-yr Detention Volume =	0.190	acre-feet
Approximate 25-yr Detention Volume =	0.211	acre-feet
Approximate 50-yr Detention Volume =	0.223	acre-feet
Approximate 100-yr Detention Volume =	0.237	acre-feet

## Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.037	acre-feet
Zone 2 Volume (100-year - Zone 1) =	0.200	acre-feet
Select Zone 3 Storage Volume (Optional) =		acre-feet
Total Detention Basin Volume =	0.237	acre-feet
Initial Surcharge Volume (ISV) =	N/A	ft. <sup>3</sup>
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth (H <sub>TOTAL</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	N/A	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	N/A	ft/ft
Slopes of Main Basin Sides (S <sub>MAIN</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>LW</sub> ) =	user	
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft. <sup>2</sup>
Surcharge Volume Length (L <sub>ISV</sub> ) =	user	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft
Length of Basin Floor (L <sub>FLOOR</sub> ) =	user	ft
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft. <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft. <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft
Length of Main Basin (L <sub>MAIN</sub> ) =	user	ft
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft. <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft. <sup>3</sup>
Calculated Total Basin Volume (V <sub>TOTAL</sub> ) =	user	acre-feet

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.06 (July 2022)*



Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

# TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT

PERMANENT  
POOL

ORIFICES

### Example Zone Configuration (Retention Pond)

Zone 3

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	2.50	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	0.89	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Underdrain Orifice Centroid =	0.04	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate	WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
	Elliptical Half-Width =	N/A	feet
	Elliptical Slot Centroid =	N/A	feet
	Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =	Not Selected	Not Selected	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =			inches

Calculated Parameters for Vertical Orif	Not Selected	Not Selected
Vertical Orifice Area =		
Vertical Orifice Centroid =		

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Zone 2 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	1.19
Overflow Weir Front Edge Length =	2.91
Overflow Weir Grate Slope =	0.00
Horiz. Length of Weir Sides =	2.91
Overflow Grate Type =	Type C Grate
Debris Clogging % =	50%

Calculated Parameters for Overflow W	Zone 2 Weir	Not Selected
Height of Grate Upper Edge, Ht =	1.19	
Overflow Weir Slope Length =	2.91	
Grate Open Area / 100-yr Orifice Area =	3.34	
Overflow Grate Open Area w/o Debris =	5.89	
Overflow Grate Open Area w/ Debris =	2.95	

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 2 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	2.75
Outlet Pipe Diameter =	18.00
Restrictor Plate Height Above Pipe Invert =	18.00

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl	Zone 2 Restrictor	Not Selected
Outlet Orifice Area =	1.77	
Outlet Orifice Centroid =	0.75	
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	2.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	20.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway	0.21	feet
Stage at Top of Freeboard =	3.21	feet
Basin Area at Top of Freeboard =	0.09	acres
Basin Volume at Top of Freeboard =	0.17	acre-ft

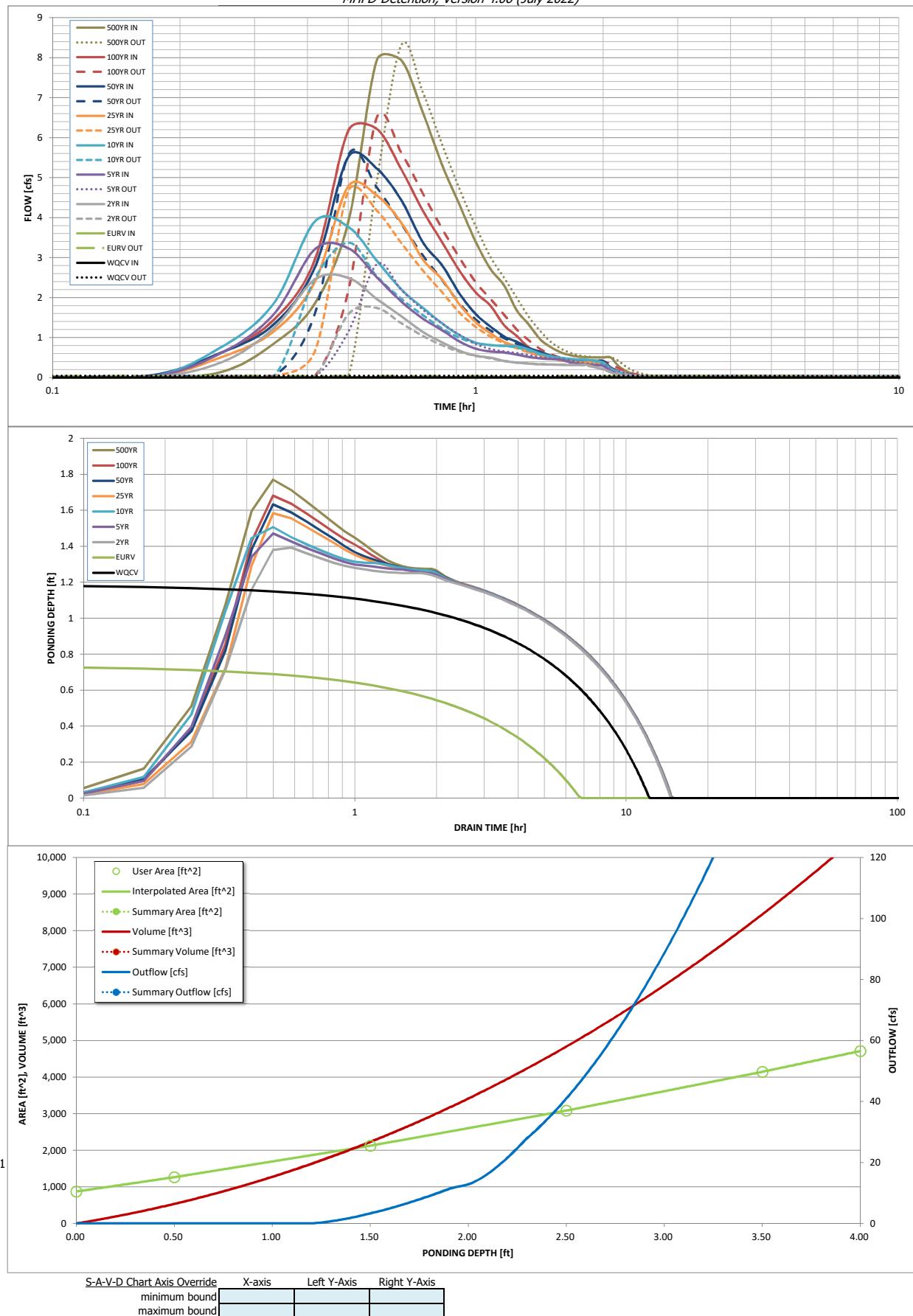
### Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through Al)

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
One-Hour Rainfall Depth (in) =								
CUHP Runoff Volume (acre-ft) =	0.037	0.159	0.121	0.159	0.192	0.229	0.263	0.303
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.121	0.159	0.192	0.229	0.263	0.303
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.3	0.7	1.3	1.8	2.3
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.02	0.20	0.38	0.78	1.03	1.34
Peak Inflow Q (cfs) =	N/A	N/A	2.5	3.2	3.9	4.8	5.5	6.2
Peak Outflow Q (cfs) =	0.0	20.3	1.7	2.8	3.4	4.7	5.6	6.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	8.1	5.1	3.5	3.2	2.8
Structure Controlling Flow =	Overflow Weir 1	Spillway	Overflow Weir 1					
Max Velocity through Grate 1 (fps) =	N/A	3.26	0.28	0.5	0.6	0.8	0.9	1.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	12	6	13	13	13	12	12	12
Time to Drain 99% of Inflow Volume (hours) =	12	7	14	14	14	14	14	14
Maximum Ponding Depth (ft) =	1.19	3.12	1.39	1.47	1.51	1.58	1.63	1.68
Area at Maximum Ponding Depth (acres) =	0.04	0.09	0.05	0.05	0.05	0.05	0.05	0.05
Maximum Volume Stored (acre-ft) =	0.037	0.160	0.046	0.050	0.051	0.055	0.058	0.060

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MFHD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-axis	Right Y-axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.00	0.14
	0:15:00	0.00	0.00	0.38	0.61	0.76	0.51	0.62	0.62	0.85
	0:20:00	0.00	0.00	1.24	1.59	1.86	1.16	1.34	1.45	1.86
	0:25:00	0.00	0.00	2.45	3.21	3.90	2.40	2.76	2.95	3.90
	0:30:00	0.00	0.00	2.49	3.23	3.76	4.79	5.53	6.17	7.93
	0:35:00	0.00	0.00	1.96	2.51	2.92	4.56	5.23	6.22	7.93
	0:40:00	0.00	0.00	1.53	1.90	2.20	3.87	4.43	5.21	6.62
	0:45:00	0.00	0.00	1.14	1.47	1.74	2.95	3.38	4.17	5.30
	0:50:00	0.00	0.00	0.87	1.18	1.35	2.45	2.80	3.38	4.30
	0:55:00	0.00	0.00	0.67	0.90	1.05	1.82	2.09	2.66	3.39
	1:00:00	0.00	0.00	0.55	0.72	0.87	1.38	1.59	2.13	2.71
	1:05:00	0.00	0.00	0.50	0.65	0.81	1.11	1.27	1.80	2.30
	1:10:00	0.00	0.00	0.42	0.63	0.79	0.89	1.03	1.31	1.68
	1:15:00	0.00	0.00	0.37	0.57	0.79	0.78	0.90	1.04	1.33
	1:20:00	0.00	0.00	0.35	0.52	0.71	0.65	0.74	0.76	0.97
	1:25:00	0.00	0.00	0.33	0.48	0.60	0.57	0.65	0.61	0.77
	1:30:00	0.00	0.00	0.32	0.46	0.53	0.48	0.55	0.50	0.64
	1:35:00	0.00	0.00	0.32	0.45	0.49	0.43	0.49	0.45	0.56
	1:40:00	0.00	0.00	0.32	0.39	0.47	0.40	0.45	0.42	0.52
	1:45:00	0.00	0.00	0.32	0.35	0.45	0.39	0.44	0.41	0.51
	1:50:00	0.00	0.00	0.32	0.33	0.44	0.38	0.42	0.40	0.50
	1:55:00	0.00	0.00	0.25	0.31	0.42	0.37	0.42	0.40	0.50
	2:00:00	0.00	0.00	0.21	0.29	0.37	0.37	0.42	0.40	0.50
	2:05:00	0.00	0.00	0.13	0.17	0.22	0.22	0.25	0.24	0.30
	2:10:00	0.00	0.00	0.07	0.10	0.13	0.13	0.15	0.14	0.18
	2:15:00	0.00	0.00	0.04	0.06	0.07	0.07	0.08	0.08	0.10
	2:20:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:25:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

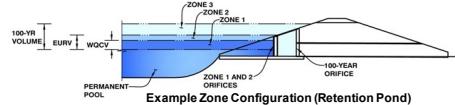
CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)

<i><b>Weighted Percent Imperviousness of Proposed WQ Sand Filter Pond 2</b></i>				
<i><b>Contributing Basins</b></i>	<i><b>Area (Acres)</b></i>	<i><b>C<sub>5</sub></b></i>	<i><b>Impervious % (I)</b></i>	<i><b>(Acres)*(I)</b></i>
<b>C</b>	0.12	0.09	2	0.25
<b>D</b>	0.77	0.81	90	69.40
<b>Totals</b>	<b>0.89</b>			<b>69.64</b>
<i><b>Imperviousness of WQ Pond 2</b></i>	<b>77.9</b>			

A soils            48%  
 B soils            52%

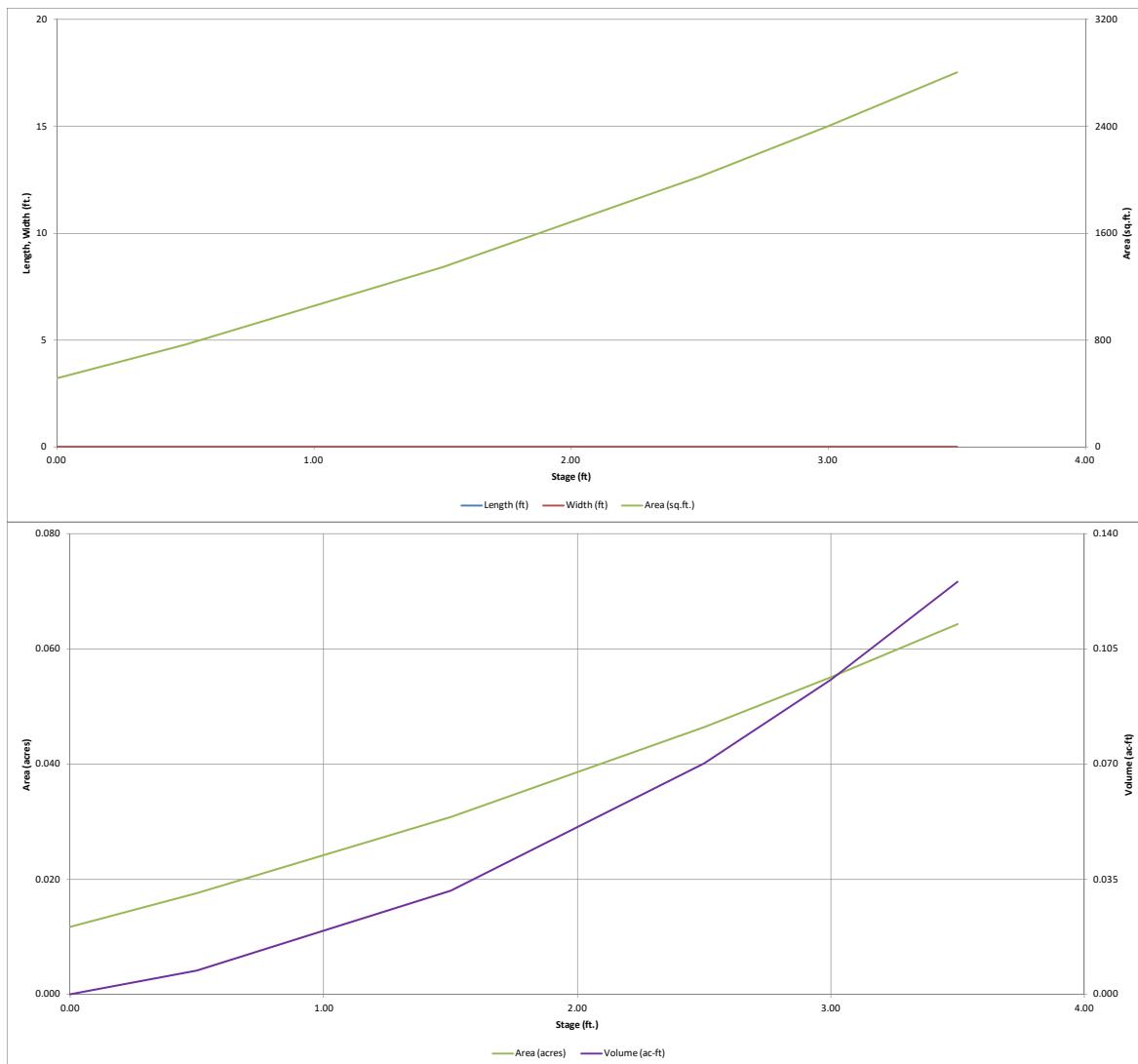
# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Claremont Business Park 2 Filing No. 2 Basin ID: Lot 2 - Future Pond 2									
 <p><b>Example Zone Configuration (Retention Pond)</b></p>									
Watershed Information	Depth Increment = <input type="text" value="ft"/> ft								
	Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft <sup>2</sup> )	Optional Override Area (ft <sup>2</sup> )	Area (acre)	Volume (ft <sup>3</sup> )
Selected BMP Type = <input type="text" value="SF"/>	<input type="text" value="--"/>	<input type="text" value="0.00"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="513"/>	<input type="text" value="0.012"/>	<input type="text" value="319"/>	<input type="text" value="0.007"/>
Watershed Area = <input type="text" value="0.83"/>	<input type="text" value="--"/>	<input type="text" value="0.50"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="765"/>	<input type="text" value="0.018"/>	<input type="text" value="319"/>	<input type="text" value="0.007"/>
Watershed Length = <input type="text" value="310"/>	<input type="text" value="--"/>	<input type="text" value="1.50"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="1,344"/>	<input type="text" value="0.031"/>	<input type="text" value="1,374"/>	<input type="text" value="0.032"/>
Watershed Length to Centroid = <input type="text" value="150"/>	<input type="text" value="--"/>	<input type="text" value="2.50"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="2,023"/>	<input type="text" value="0.046"/>	<input type="text" value="3,057"/>	<input type="text" value="0.070"/>
Watershed Slope = <input type="text" value="0.016"/>	<input type="text" value="--"/>	<input type="text" value="3.00"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="2,400"/>	<input type="text" value="0.055"/>	<input type="text" value="4,163"/>	<input type="text" value="0.096"/>
Watershed Imperviousness = <input type="text" value="77.90%"/>	<input type="text" value="--"/>	<input type="text" value="3.50"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="2,803"/>	<input type="text" value="0.064"/>	<input type="text" value="5,464"/>	<input type="text" value="0.125"/>
Percentage Hydrologic Soil Group A = <input type="text" value="48.0%"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>
Percentage Hydrologic Soil Group B = <input type="text" value="52.0%"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>
Percentage Hydrologic Soil Groups C/D = <input type="text" value="0.0%"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>
Target WQCV Drain Time = <input type="text" value="12.0"/>	<input type="text" value="--"/>	<input type="text" value="hours"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>	<input type="text" value="--"/>
Location for 1-hr Rainfall Depths = User Input									
After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.									
Optional User Overrides									
Water Quality Capture Volume (WQCV) = <input type="text" value="0.017"/>									
Water Quality Capture Volume (WQCV) = <input type="text" value="0.017"/>									
Excess Urban Runoff Volume = <input type="text" value="0.075"/>									
Excess Urban Runoff Volume = <input type="text" value="0.075"/>									
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) = <input type="text" value="0.059"/>									
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) = <input type="text" value="0.059"/>									
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) = <input type="text" value="0.077"/>									
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) = <input type="text" value="0.077"/>									
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) = <input type="text" value="0.093"/>									
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) = <input type="text" value="0.093"/>									
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) = <input type="text" value="0.111"/>									
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) = <input type="text" value="0.111"/>									
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) = <input type="text" value="0.128"/>									
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) = <input type="text" value="0.128"/>									
100-yr Runoff Volume ( $P_1 = 2.52 \text{ in.}$ ) = <input type="text" value="0.148"/>									
100-yr Runoff Volume ( $P_1 = 2.52 \text{ in.}$ ) = <input type="text" value="0.148"/>									
500-yr Runoff Volume ( $P_1 = 3.14 \text{ in.}$ ) = <input type="text" value="0.190"/>									
500-yr Runoff Volume ( $P_1 = 3.14 \text{ in.}$ ) = <input type="text" value="0.190"/>									
Approximate 2-yr Detention Volume = <input type="text" value="0.056"/>									
Approximate 2-yr Detention Volume = <input type="text" value="0.056"/>									
Approximate 5-yr Detention Volume = <input type="text" value="0.073"/>									
Approximate 5-yr Detention Volume = <input type="text" value="0.073"/>									
Approximate 10-yr Detention Volume = <input type="text" value="0.095"/>									
Approximate 10-yr Detention Volume = <input type="text" value="0.095"/>									
Approximate 25-yr Detention Volume = <input type="text" value="0.101"/>									
Approximate 25-yr Detention Volume = <input type="text" value="0.101"/>									
Approximate 50-yr Detention Volume = <input type="text" value="0.108"/>									
Approximate 50-yr Detention Volume = <input type="text" value="0.108"/>									
Approximate 100-yr Detention Volume = <input type="text" value="0.115"/>									
Approximate 100-yr Detention Volume = <input type="text" value="0.115"/>									
Define Zones and Basin Geometry									
Zone 1 Volume (WQCV) = <input type="text" value="0.017"/>									
Zone 2 Volume (100-year - Zone 1) = <input type="text" value="0.098"/>									
Select Zone 3 Storage Volume (Optional)									
Total Detention Basin Volume = <input type="text" value="0.115"/>									
Initial Surcharge Volume (ISV) = <input type="text" value="N/A"/>									
Initial Surcharge Depth (ISD) = <input type="text" value="N/A"/>									
Total Available Detention Depth ( $H_{total}$ ) = <input type="text" value="user"/>									
Depth of Trickle Channel ( $H_{trickle}$ ) = <input type="text" value="N/A"/>									
Slope of Trickle Channel ( $S_{trickle}$ ) = <input type="text" value="N/A"/>									
Slopes of Main Basin Sides ( $S_{main}$ ) = <input type="text" value="user"/>									
Basin Length-to-Width Ratio ( $R_{L/W}$ ) = <input type="text" value="user"/>									
Initial Surcharge Area ( $A_{SV}$ ) = <input type="text" value="user"/>									
Surcharge Volume Length ( $L_{SV}$ ) = <input type="text" value="user"/>									
Surcharge Volume Width ( $W_{SV}$ ) = <input type="text" value="user"/>									
Depth of Basin Floor ( $H_{FLOOR}$ ) = <input type="text" value="user"/>									
Length of Basin Floor ( $L_{FLOOR}$ ) = <input type="text" value="user"/>									
Width of Basin Floor ( $W_{FLOOR}$ ) = <input type="text" value="user"/>									
Area of Basin Floor ( $A_{FLOOR}$ ) = <input type="text" value="user"/>									
Volume of Basin Floor ( $V_{FLOOR}$ ) = <input type="text" value="user"/>									
Depth of Main Basin ( $H_{MAIN}$ ) = <input type="text" value="user"/>									
Length of Main Basin ( $L_{MAIN}$ ) = <input type="text" value="user"/>									
Width of Main Basin ( $W_{MAIN}$ ) = <input type="text" value="user"/>									
Area of Main Basin ( $A_{MAIN}$ ) = <input type="text" value="user"/>									
Volume of Main Basin ( $V_{MAIN}$ ) = <input type="text" value="user"/>									
Calculated Total Basin Volume ( $V_{total}$ ) = <input type="text" value="user"/>									

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

## DETENTION BASIN OUTLET STRUCTURE DESIGN

Project: Claremont Business Park 2 Eiling No. 3  
MHFD-Detention, Version 4.06 (July 2022)

### TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT

PERMANENT  
POOL

ORIFICES

#### Example Zone Configuration (Retention Pond)

Zone 3

Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
0.99	0.017	Filtration Media
3.34	0.098	Weir&Pipe (Restrict)
Total (all zones)	0.115	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Underdrain Orifice Area = <input type="text" value="0.0"/>	ft <sup>2</sup>
Underdrain Orifice Centroid = <input type="text" value="0.03"/>	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches

WQ Orifice Area per Row = <input type="text" value="N/A"/>	ft <sup>2</sup>
Elliptical Half-Width = <input type="text" value="N/A"/>	feet
Elliptical Slot Centroid = <input type="text" value="N/A"/>	feet
Elliptical Slot Area = <input type="text" value="N/A"/>	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft) <input type="text" value="N/A"/>	<input type="text" value="N/A"/>						
Orifice Area (sq. inches) <input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft) <input type="text" value="N/A"/>	<input type="text" value="N/A"/>						
Orifice Area (sq. inches) <input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Vertical Orifice Area = <input type="text" value="Not Selected"/>	ft <sup>2</sup>
Vertical Orifice Centroid = <input type="text" value="Not Selected"/>	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, Ho =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Height of Grate Upper Edge, Ht = <input type="text" value="0.99"/>	ft
Overflow Weir Slope Length = <input type="text" value="3.00"/>	feet
Grate Open Area / 100-yr Orifice Area = <input type="text" value="5.01"/>	ft <sup>2</sup>
Overflow Grate Open Area w/o Debris = <input type="text" value="6.26"/>	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris = <input type="text" value="1.88"/>	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Outlet Orifice Area = <input type="text" value="1.25"/>	ft <sup>2</sup>
Outlet Orifice Centroid = <input type="text" value="0.56"/>	feet
Half-Central Angle of Restrictor Plate on Pipe = <input type="text" value="1.91"/>	degrees
	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Spillway Design Flow Depth= <input type="text" value="0.18"/>	feet
Stage at Top of Freeboard = <input type="text" value="3.18"/>	feet
Basin Area at Top of Freeboard = <input type="text" value="0.06"/>	acres
Basin Volume at Top of Freeboard = <input type="text" value="0.11"/>	acre-ft

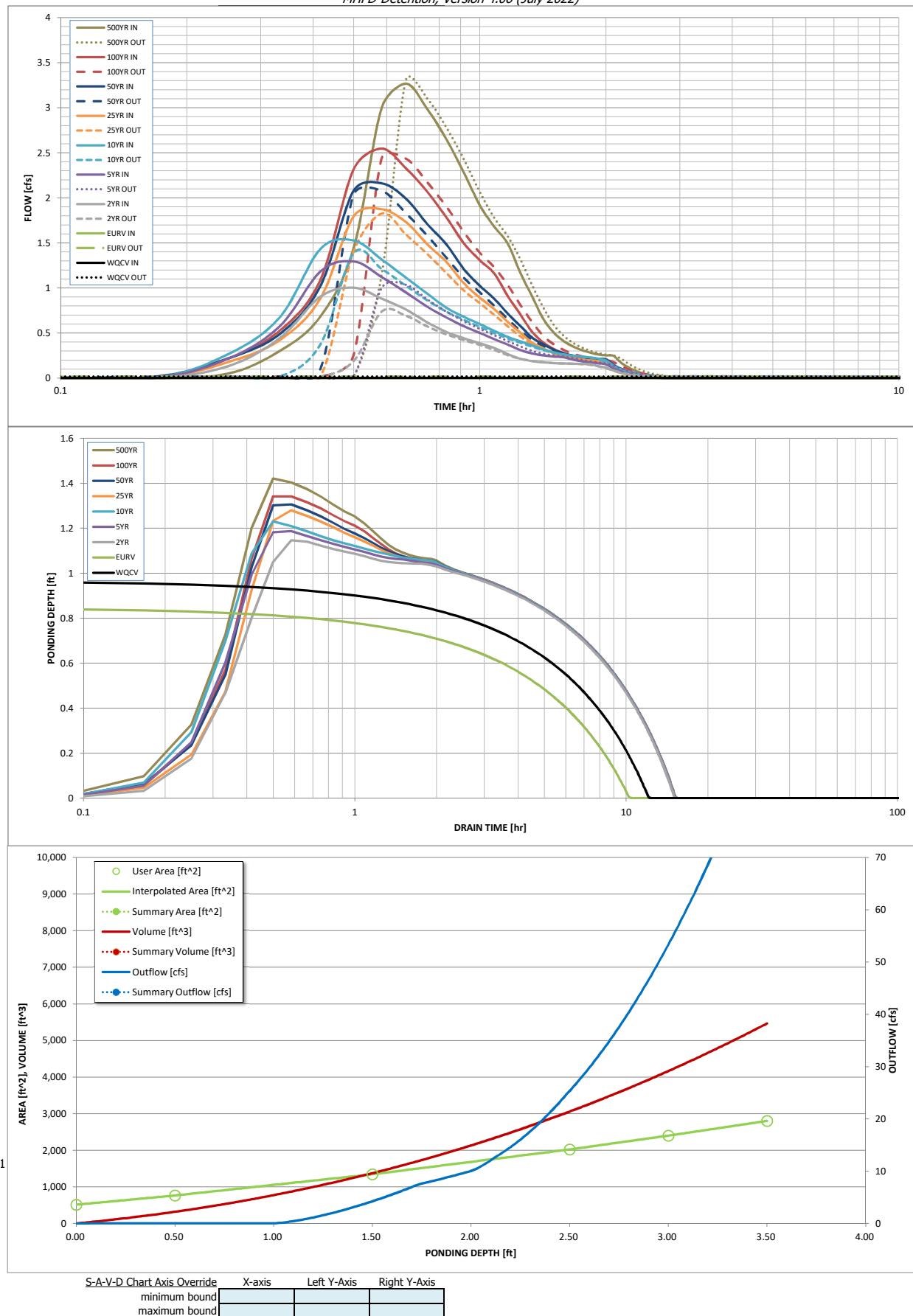
#### Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through Al)

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.017	0.078	0.059	0.077	0.093	0.111	0.128	0.148
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.059	0.077	0.093	0.111	0.128	0.148
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.2	0.4	0.6	0.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.09	0.22	0.52	0.71	0.96
Peak Inflow Q (cfs) =	N/A	N/A	1.0	1.3	1.5	1.9	2.2	2.5
Peak Outflow Q (cfs) =	0.0	9.3	0.7	1.0	1.4	1.8	2.1	2.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	13.6	7.5	4.2	3.5	3.0
Structure Controlling Flow =	Filtration Media	Spillway	Overflow Weir 1					
Max Velocity through Grate 1 (fps) =	N/A	2.12	0.12	0.2	0.2	0.3	0.3	0.4
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	12	9	14	13	13	13	12	12
Time to Drain 99% of Inflow Volume (hours) =	12	10	15	15	15	14	14	14
Maximum Ponding Depth (ft) =	0.97	2.67	1.15	1.19	1.23	1.28	1.31	1.34
Area at Maximum Ponding Depth (acres) =	0.02	0.05	0.03	0.03	0.03	0.03	0.03	0.03
Maximum Volume Stored (acre-ft) =	0.017	0.078	0.021	0.022	0.024	0.025	0.026	0.027

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.05
	0:15:00	0.00	0.00	0.13	0.21	0.26	0.18	0.22	0.21	0.30
	0:20:00	0.00	0.00	0.44	0.58	0.67	0.42	0.49	0.53	0.68
	0:25:00	0.00	0.00	0.90	1.18	1.43	0.89	1.02	1.09	1.44
	0:30:00	0.00	0.00	1.00	1.29	1.53	1.79	2.08	2.31	3.00
	0:35:00	0.00	0.00	0.88	1.12	1.32	1.88	2.16	2.54	3.27
	0:40:00	0.00	0.00	0.76	0.95	1.11	1.73	1.99	2.33	2.98
	0:45:00	0.00	0.00	0.62	0.79	0.94	1.48	1.71	2.07	2.65
	0:50:00	0.00	0.00	0.51	0.67	0.78	1.29	1.48	1.78	2.28
	0:55:00	0.00	0.00	0.44	0.58	0.68	1.05	1.21	1.50	1.92
	1:00:00	0.00	0.00	0.39	0.50	0.60	0.89	1.02	1.31	1.68
	1:05:00	0.00	0.00	0.33	0.43	0.52	0.77	0.88	1.16	1.49
	1:10:00	0.00	0.00	0.27	0.37	0.46	0.62	0.72	0.91	1.17
	1:15:00	0.00	0.00	0.22	0.31	0.41	0.51	0.58	0.71	0.91
	1:20:00	0.00	0.00	0.19	0.27	0.36	0.39	0.45	0.52	0.66
	1:25:00	0.00	0.00	0.18	0.25	0.32	0.33	0.38	0.40	0.51
	1:30:00	0.00	0.00	0.17	0.24	0.29	0.28	0.32	0.32	0.41
	1:35:00	0.00	0.00	0.16	0.23	0.26	0.25	0.28	0.28	0.35
	1:40:00	0.00	0.00	0.16	0.21	0.25	0.22	0.25	0.25	0.31
	1:45:00	0.00	0.00	0.16	0.19	0.24	0.21	0.23	0.22	0.28
	1:50:00	0.00	0.00	0.16	0.17	0.23	0.20	0.22	0.21	0.26
	1:55:00	0.00	0.00	0.13	0.16	0.22	0.19	0.21	0.20	0.25
	2:00:00	0.00	0.00	0.12	0.15	0.20	0.19	0.21	0.20	0.25
	2:05:00	0.00	0.00	0.08	0.11	0.14	0.13	0.15	0.14	0.18
	2:10:00	0.00	0.00	0.06	0.08	0.10	0.09	0.10	0.10	0.12
	2:15:00	0.00	0.00	0.04	0.05	0.07	0.07	0.07	0.07	0.09
	2:20:00	0.00	0.00	0.03	0.03	0.05	0.04	0.05	0.05	0.06
	2:25:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:30:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
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	2:40:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
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	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

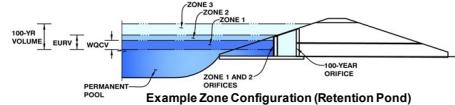
CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)

<i>Weighted Percent Imperviousness of Proposed WQ Sand Filter Pond 3</i>				
<i>Contributing Basins</i>	<i>Area (Acres)</i>	<i>C<sub>5</sub></i>	<i>Impervious % (I)</i>	<i>(Acres)*(I)</i>
<i>C1</i>	0.17	0.09	2	0.34
<i>D1</i>	0.78	0.81	90	70.31
<i>E1</i>	0.27	0.88	97	26.02
<i>E2</i>	0.21	0.88	97	20.22
<b>Totals</b>	<b>1.43</b>			<b>116.89</b>
<i>Imperviousness of WQ Pond 2</i>	<b>81.8</b>			

A soils            85%  
 B soils            15%

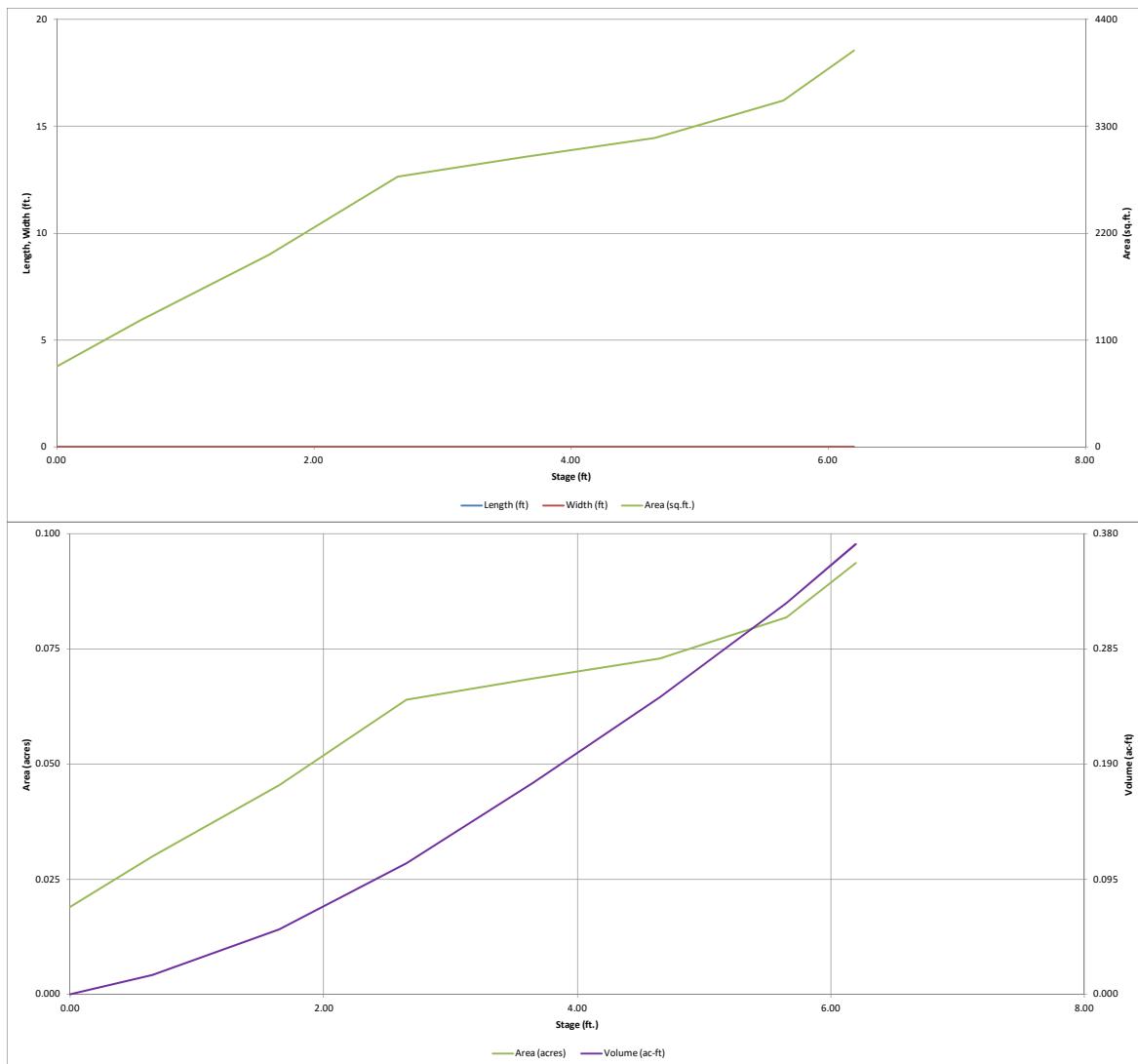
# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Claremont Business Park 2 Filing No. 2 Basin ID: Lot 2 - Pond 3									
 <p><b>Example Zone Configuration (Retention Pond)</b></p>									
Watershed Information	Depth Increment = <input type="text" value="ft"/> ft								
	Selected BMP Type = <input type="text" value="SF"/>	Stage - Storage Description	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft <sup>2</sup> )	Optional Override Area (ft <sup>2</sup> )	Area (acres)	Volume (ft <sup>3</sup> )
Media Surface	--	0.00	--	--	--	828	0.019	--	--
Watershed Area = <input type="text" value="1.43"/> acres	--	0.65	--	--	--	1,305	0.030	693	0.016
Watershed Length = <input type="text" value="310"/> ft	--	1.65	--	--	--	1,980	0.045	2,336	0.054
Watershed Length to Centroid = <input type="text" value="150"/> ft	--	2.65	--	--	--	2,785	0.064	4,718	0.108
Watershed Slope = <input type="text" value="0.016"/> ft/ft	--	3.65	--	--	--	2,990	0.069	7,606	0.175
Watershed Imperviousness = <input type="text" value="81.80%"/> percent	--	4.65	--	--	--	3,178	0.073	10,690	0.245
Percentage Hydrologic Soil Group A = <input type="text" value="85.0%"/> percent	--	5.65	--	--	--	3,568	0.082	14,063	0.323
Percentage Hydrologic Soil Group B = <input type="text" value="15.0%"/> percent	--	6.20	--	--	--	4,078	0.094	16,165	0.371
Percentage Hydrologic Soil Groups C/D = <input type="text" value="0.0%"/> percent	--	--	--	--	--	--	--	--	--
Target WQCV Drain Time = <input type="text" value="12.0"/> hours	--	--	--	--	--	--	--	--	--
Location for 1-hr Rainfall Depths = User Input	--	--	--	--	--	--	--	--	--
After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.									
Optional User Overrides									
Water Quality Capture Volume (WQCV) = <input type="text" value="0.032"/> acre-feet									
Excess Urban Runoff Volume (EURV) = <input type="text" value="0.151"/> acre-feet									
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) = <input type="text" value="0.105"/> acre-feet									
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) = <input type="text" value="0.135"/> acre-feet									
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) = <input type="text" value="0.160"/> acre-feet									
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) = <input type="text" value="0.191"/> acre-feet									
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) = <input type="text" value="0.219"/> acre-feet									
100-yr Runoff Volume ( $P_1 = 2.52 \text{ in.}$ ) = <input type="text" value="0.251"/> acre-feet									
500-yr Runoff Volume ( $P_1 = 3.14 \text{ in.}$ ) = <input type="text" value="0.323"/> acre-feet									
Approximate 2-yr Detention Volume = <input type="text" value="0.102"/> acre-feet									
Approximate 5-yr Detention Volume = <input type="text" value="0.133"/> acre-feet									
Approximate 10-yr Detention Volume = <input type="text" value="0.159"/> acre-feet									
Approximate 25-yr Detention Volume = <input type="text" value="0.186"/> acre-feet									
Approximate 50-yr Detention Volume = <input type="text" value="0.202"/> acre-feet									
Approximate 100-yr Detention Volume = <input type="text" value="0.216"/> acre-feet									
Define Zones and Basin Geometry									
Zone 1 Volume (WQCV) = <input type="text" value="0.032"/> acre-feet									
Zone 2 Volume (100-year - Zone 1) = <input type="text" value="0.184"/> acre-feet									
Select Zone 3 Storage Volume (Optional)									
Total Detention Basin Volume = <input type="text" value="0.216"/> acre-feet									
Initial Surcharge Volume (ISV) = <input type="text" value="N/A"/> ft <sup>3</sup>									
Initial Surcharge Depth (ISD) = <input type="text" value="N/A"/> ft									
Total Available Detention Depth ( $H_{TOTAL}$ ) = <input type="text" value="user"/> ft									
Depth of Trickle Channel ( $H_{TICKLE}$ ) = <input type="text" value="N/A"/> ft									
Slope of Trickle Channel ( $S_{TICKLE}$ ) = <input type="text" value="N/A"/> ft/ft									
Slopes of Main Basin Sides ( $S_{MAIN}$ ) = <input type="text" value="user"/> H:V									
Basin Length-to-Width Ratio ( $R_{L/W}$ ) = <input type="text" value="user"/>									
Initial Surcharge Area ( $A_{ISV}$ ) = <input type="text" value="user"/> ft <sup>2</sup>									
Surcharge Volume Length ( $L_{ISV}$ ) = <input type="text" value="user"/> ft									
Surcharge Volume Width ( $W_{ISV}$ ) = <input type="text" value="user"/> ft									
Depth of Basin Floor ( $H_{FLOOR}$ ) = <input type="text" value="user"/> ft									
Length of Basin Floor ( $L_{FLOOR}$ ) = <input type="text" value="user"/> ft									
Width of Basin Floor ( $W_{FLOOR}$ ) = <input type="text" value="user"/> ft									
Area of Basin Floor ( $A_{FLOOR}$ ) = <input type="text" value="user"/> ft <sup>2</sup>									
Volume of Basin Floor ( $V_{FLOOR}$ ) = <input type="text" value="user"/> ft <sup>3</sup>									
Depth of Main Basin ( $H_{MAIN}$ ) = <input type="text" value="user"/> ft									
Length of Main Basin ( $L_{MAIN}$ ) = <input type="text" value="user"/> ft									
Width of Main Basin ( $W_{MAIN}$ ) = <input type="text" value="user"/> ft									
Area of Main Basin ( $A_{MAIN}$ ) = <input type="text" value="user"/> ft <sup>2</sup>									
Volume of Main Basin ( $V_{MAIN}$ ) = <input type="text" value="user"/> ft <sup>3</sup>									
Calculated Total Basin Volume ( $V_{total}$ ) = <input type="text" value="user"/> acre-feet									

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

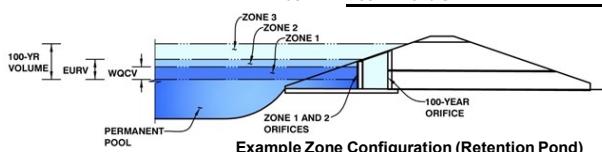
MHFD-Detention, Version 4.06 (July 2022)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Project: Claremont Business Park 2 Filing No. 2  
MHFD-Detention, Version 4.06 (July 2022)

Basin ID: Lot 2 - Pond 3



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.14	0.032	Filtration Media
Zone 2 (100-year)	4.25	0.184	Weir&Pipe (Restrict)
Zone 3			
Total (all zones)		0.216	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.50 ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter = 0.84 inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	0.0 ft <sup>2</sup>
Underdrain Orifice Centroid =	0.04 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A sq. inches

Calculated Parameters for Plate	
WQ Orifice Area per Row =	N/A ft <sup>2</sup>
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = Not Selected ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = Not Selected ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = Not Selected inches

Calculated Parameters for Vertical Orif	
Not Selected	Not Selected
Vertical Orifice Area =	
Vertical Orifice Centroid =	

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, Ho = 1.14 ft (relative to basin bottom at Stage = 0 ft)  
 Overflow Weir Front Edge Length = 3.00 feet  
 Overflow Weir Grate Slope = 0.00 H:V  
 Horiz. Length of Weir Sides = 3.00 feet  
Overflow Grate Type = Type C Grate  
Debris Clogging % = 70% %

Calculated Parameters for Overflow W	
Zone 2 Weir	Not Selected
Height of Grate Upper Edge, Ht =	1.14
Overflow Weir Slope Length =	3.00
Grate Open Area / 100-yr Orifice Area =	15.64
Overflow Grate Open Area w/o Debris =	6.26
Overflow Grate Open Area w/ Debris =	1.88

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = Zone 2 Restrictor Not Selected ft (distance below basin bottom at Stage = 0 ft)  
 Outlet Pipe Diameter = 2.75 inches  
 Restrictor Plate Height Above Pipe Invert = 18.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl	
Zone 2 Restrictor	Not Selected
Outlet Orifice Area =	0.40
Outlet Orifice Centroid =	0.25
Half-Central Angle of Restrictor Plate on Pipe =	1.11 N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 5.00 ft (relative to basin bottom at Stage = 0 ft)  
 Spillway Crest Length = 18.00 feet  
 Spillway End Slopes = 4.00 H:V  
 Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway	
Spillway Design Flow Depth=	0.19 feet
Stage at Top of Freeboard =	6.19 feet
Basin Area at Top of Freeboard =	0.09 acres
Basin Volume at Top of Freeboard =	0.37 acre-ft

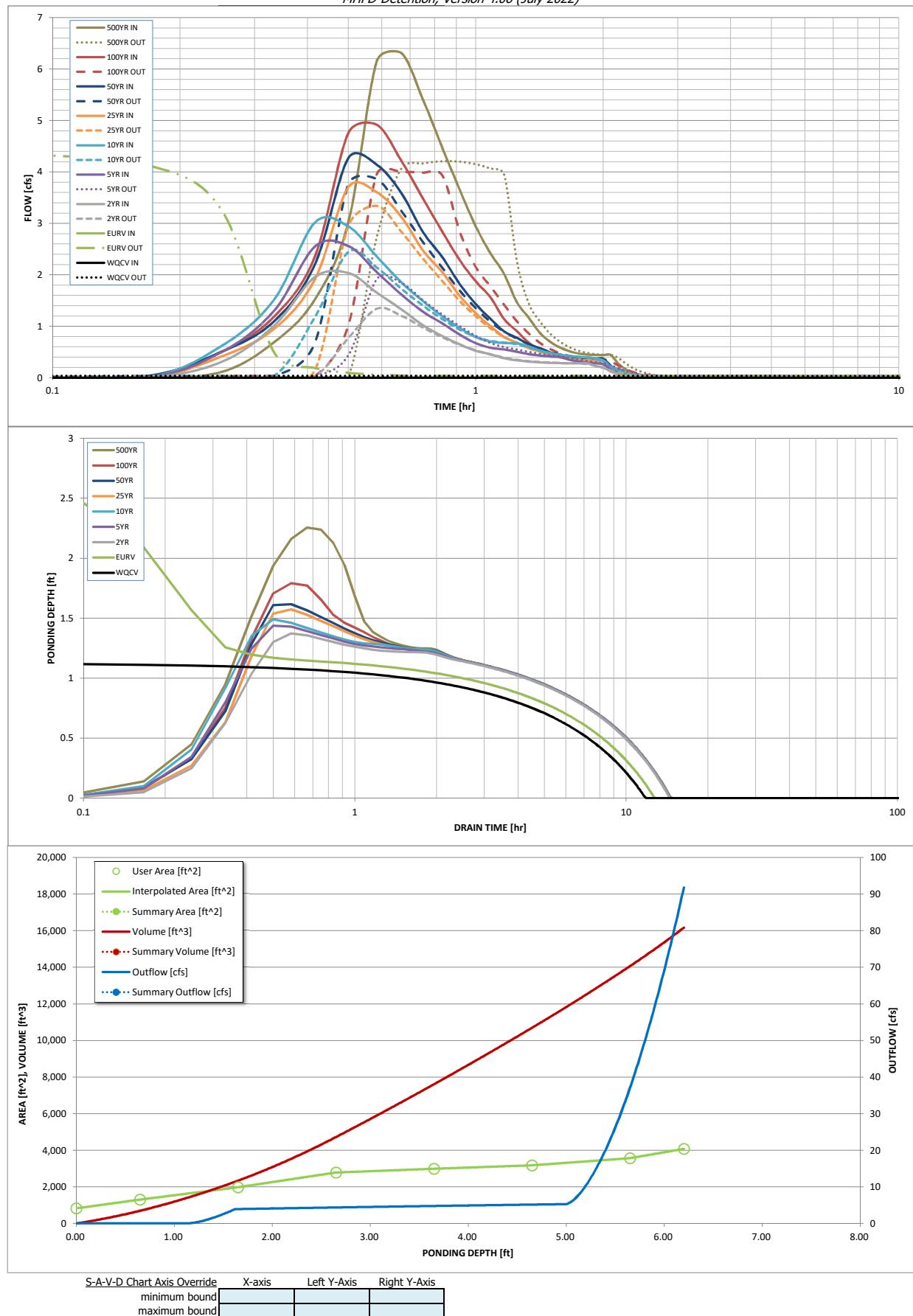
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through Al)

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.032	0.151	0.105	0.135	0.160	0.191	0.219	0.251
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.105	0.135	0.160	0.191	0.219	0.251
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.0	0.0	0.5	0.8	1.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.03	0.36	0.57	0.83
Peak Inflow Q (cfs) =	N/A	N/A	2.0	2.6	3.0	3.7	4.3	4.9
Peak Outflow Q (cfs) =	0.0	4.6	1.3	1.9	2.4	3.3	3.9	4.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	68.8	49.5	6.4	4.8	3.4
Structure Controlling Flow =	Filtration Media	Outlet Plate 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	0.74	0.20	0.3	0.4	0.5	0.6	0.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	11	11	13	13	13	12	12	12
Time to Drain 99% of Inflow Volume (hours) =	12	12	14	14	14	14	14	14
Maximum Ponding Depth (ft) =	1.13	3.31	1.37	1.44	1.49	1.57	1.62	1.79
Area at Maximum Ponding Depth (acres) =	0.04	0.07	0.04	0.04	0.04	0.04	0.04	0.05
Maximum Volume Stored (acre-ft) =	0.032	0.152	0.042	0.044	0.047	0.050	0.052	0.060

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.11
	0:15:00	0.00	0.00	0.30	0.49	0.61	0.41	0.50	0.50	0.69
	0:20:00	0.00	0.00	1.01	1.30	1.51	0.95	1.09	1.18	1.52
	0:25:00	0.00	0.00	1.96	2.55	3.02	1.92	2.21	2.35	3.03
	0:30:00	0.00	0.00	2.03	2.56	2.94	3.71	4.27	4.76	6.15
	0:35:00	0.00	0.00	1.65	2.05	2.36	3.61	4.14	4.92	6.31
	0:40:00	0.00	0.00	1.33	1.62	1.85	3.13	3.59	4.22	5.41
	0:45:00	0.00	0.00	1.02	1.28	1.49	2.48	2.83	3.49	4.47
	0:50:00	0.00	0.00	0.81	1.06	1.20	2.05	2.35	2.84	3.65
	0:55:00	0.00	0.00	0.65	0.84	0.97	1.59	1.82	2.28	2.94
	1:00:00	0.00	0.00	0.52	0.67	0.79	1.25	1.43	1.87	2.42
	1:05:00	0.00	0.00	0.45	0.58	0.70	1.00	1.14	1.56	2.02
	1:10:00	0.00	0.00	0.38	0.55	0.68	0.79	0.90	1.14	1.47
	1:15:00	0.00	0.00	0.34	0.50	0.67	0.68	0.78	0.91	1.17
	1:20:00	0.00	0.00	0.31	0.46	0.61	0.58	0.65	0.68	0.87
	1:25:00	0.00	0.00	0.30	0.43	0.53	0.51	0.58	0.55	0.70
	1:30:00	0.00	0.00	0.29	0.41	0.48	0.44	0.49	0.46	0.59
	1:35:00	0.00	0.00	0.28	0.40	0.44	0.39	0.44	0.41	0.51
	1:40:00	0.00	0.00	0.28	0.35	0.42	0.36	0.41	0.38	0.47
	1:45:00	0.00	0.00	0.28	0.32	0.40	0.35	0.39	0.36	0.45
	1:50:00	0.00	0.00	0.28	0.29	0.39	0.34	0.38	0.36	0.44
	1:55:00	0.00	0.00	0.23	0.28	0.38	0.33	0.37	0.35	0.44
	2:00:00	0.00	0.00	0.20	0.26	0.34	0.33	0.37	0.35	0.44
	2:05:00	0.00	0.00	0.12	0.16	0.21	0.21	0.23	0.23	0.28
	2:10:00	0.00	0.00	0.08	0.10	0.13	0.13	0.15	0.14	0.18
	2:15:00	0.00	0.00	0.04	0.06	0.08	0.08	0.09	0.09	0.11
	2:20:00	0.00	0.00	0.02	0.04	0.05	0.05	0.05	0.05	0.06
	2:25:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.03	0.03
	2:30:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

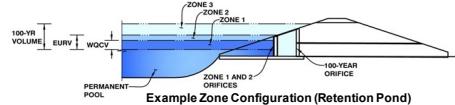
CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)

<i><b>Weighted Percent Imperviousness of Proposed WQ Sand Filter Pond 4</b></i>				
<i><b>Contributing Basins</b></i>	<i><b>Area (Acres)</b></i>	<i><b>C<sub>5</sub></b></i>	<i><b>Impervious % (I)</b></i>	<i><b>(Acres)*(I)</b></i>
<i><b>F</b></i>	<i><b>0.30</b></i>	<i><b>0.81</b></i>	<i><b>90</b></i>	<i><b>26.77</b></i>
<i><b>Totals</b></i>	<i><b>0.30</b></i>			<i><b>26.77</b></i>
<i><b>Imperviousness of WQ Pond 2</b></i>	<i><b>90.0</b></i>			

A soils      100%  
 B soils      0%

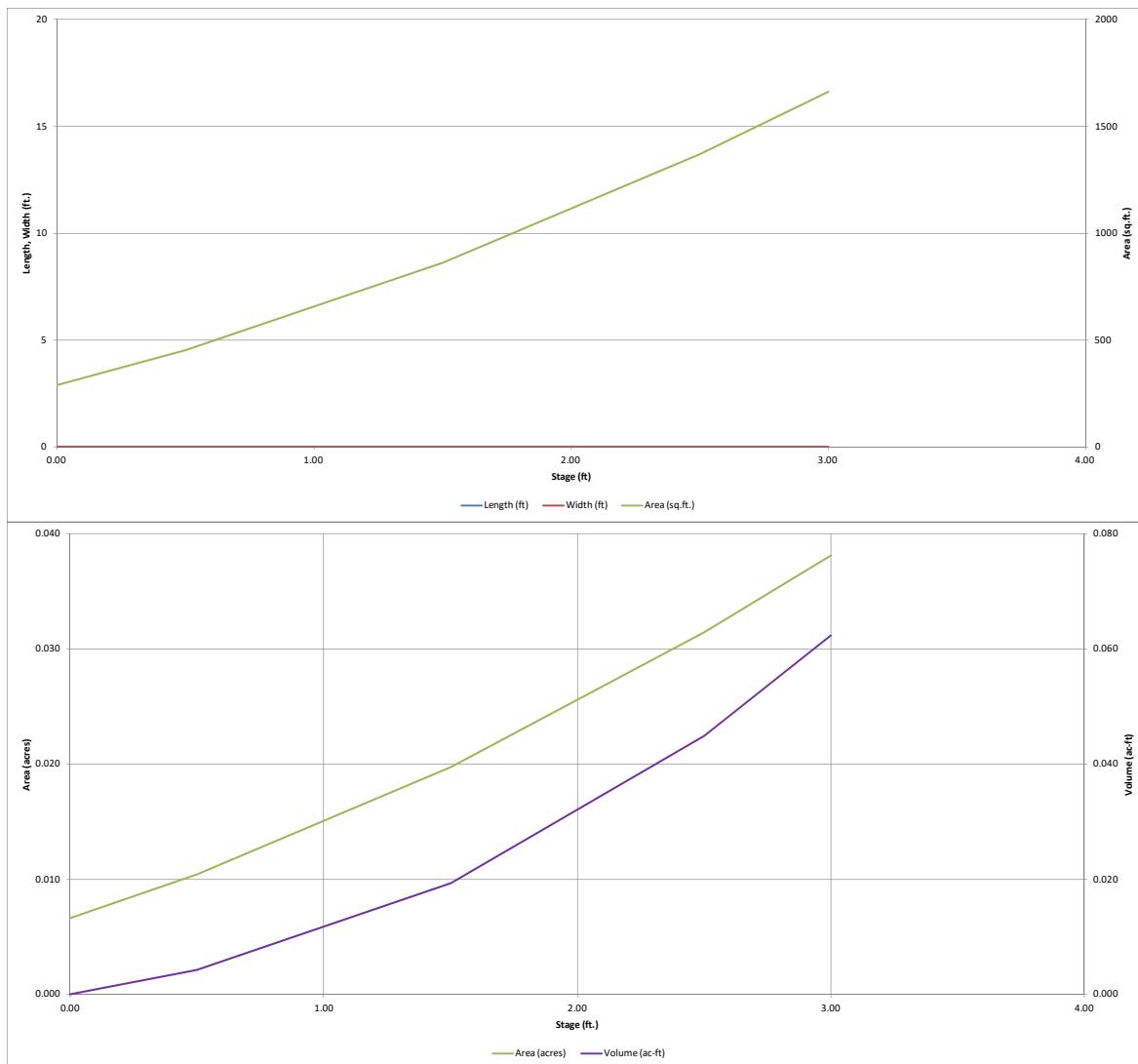
# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

<b>Project:</b> Claremont Business Park 2 Filing No. 2 <b>Basin ID:</b> Lot 3 - Pond 4																																																																																																																									
 <p><b>Example Zone Configuration (Retention Pond)</b></p>																																																																																																																									
<b>Watershed Information</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 15%;">Selected BMP Type =</td> <td style="width: 15%; text-align: center;"><b>SF</b></td> <td style="width: 10%;">Depth Increment =</td> <td style="width: 10%; text-align: center;">ft</td> </tr> <tr> <td>Watershed Area =</td> <td>0.30 acres</td> <td>Optional Stage Description</td> <td>Optional Stage (ft)</td> </tr> <tr> <td>Watershed Length =</td> <td>200 ft</td> <td>Stage</td> <td>Length (ft)</td> </tr> <tr> <td>Watershed Length to Centroid =</td> <td>100 ft</td> <td>Width (ft)</td> <td>Area (ft<sup>2</sup>)</td> </tr> <tr> <td>Watershed Slope =</td> <td>0.013 ft/ft</td> <td>Optional Override Area (ft<sup>2</sup>)</td> <td>Area (acre)</td> </tr> <tr> <td>Watershed Imperviousness =</td> <td>90.00% percent</td> <td>Volume (ft<sup>3</sup>)</td> <td>Volume (ac-ft)</td> </tr> <tr> <td>Percentage Hydrologic Soil Group A =</td> <td>100.0% percent</td> <td colspan="3"></td> </tr> <tr> <td>Percentage Hydrologic Soil Group B =</td> <td>0.0% percent</td> <td colspan="3"></td> </tr> <tr> <td>Percentage Hydrologic Soil Groups C/D =</td> <td>0.0% percent</td> <td colspan="3"></td> </tr> <tr> <td>Target WQCV Drain Time =</td> <td>12.0 hours</td> <td colspan="3"></td> </tr> <tr> <td>Location for 1-hr Rainfall Depths = User Input</td> <td></td> <td colspan="3"></td> </tr> </table> <p>After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.</p>		Selected BMP Type =	<b>SF</b>	Depth Increment =	ft	Watershed Area =	0.30 acres	Optional Stage Description	Optional Stage (ft)	Watershed Length =	200 ft	Stage	Length (ft)	Watershed Length to Centroid =	100 ft	Width (ft)	Area (ft <sup>2</sup> )	Watershed Slope =	0.013 ft/ft	Optional Override Area (ft <sup>2</sup> )	Area (acre)	Watershed Imperviousness =	90.00% percent	Volume (ft <sup>3</sup> )	Volume (ac-ft)	Percentage Hydrologic Soil Group A =	100.0% percent				Percentage Hydrologic Soil Group B =	0.0% percent				Percentage Hydrologic Soil Groups C/D =	0.0% percent				Target WQCV Drain Time =	12.0 hours				Location for 1-hr Rainfall Depths = User Input																																																																											
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## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

### TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT



**Example Zone Configuration (Retention Pond)**

Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
0.82	0.008	Filtration Media
2.70	0.043	Weir&Pipe (Restrict)
Total (all zones)	0.051	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	2.50	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	0.42	inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	0.0 ft <sup>2</sup>
Underdrain Orifice Centroid =	0.02 feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Centroid of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate	
WQ Orifice Area per Row =	N/A ft <sup>2</sup>
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

**User Input: Vertical Orifice (Circular or Rectangular)**

Invert of Vertical Orifice =	Not Selected	Not Selected	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =			feet
Vertical Orifice Diameter =			inches

Calculated Parameters for Vertical Orif	
Vertical Orifice Area =	Not Selected
Vertical Orifice Centroid =	Not Selected

**User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)**

Zone 2 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	0.82
Overflow Weir Front Edge Length =	3.00
Overflow Weir Grate Slope =	0.00
Horiz. Length of Weir Sides =	3.00
Overflow Grate Type =	Type C Grate
Debris Clogging % =	70%

Calculated Parameters for Overflow W	
Zone 2 Weir	Not Selected
Height of Grate Upper Edge, Ht =	0.82
Overflow Weir Slope Length =	3.00
Grate Open Area / 100-yr Orifice Area =	5.10
Overflow Grate Open Area w/o Debris =	6.26
Overflow Grate Open Area w/ Debris =	1.88

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

Depth to Invert of Outlet Pipe =	Zone 2 Restrictor	Not Selected	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	2.75		inches
Restrictor Plate Height Above Pipe Invert =	15.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl	
Zone 2 Restrictor	Not Selected
Outlet Orifice Area =	1.23
Outlet Orifice Centroid =	0.63
Half-Central Angle of Restrictor Plate on Pipe =	3.14
	N/A

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage=	1.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	6.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

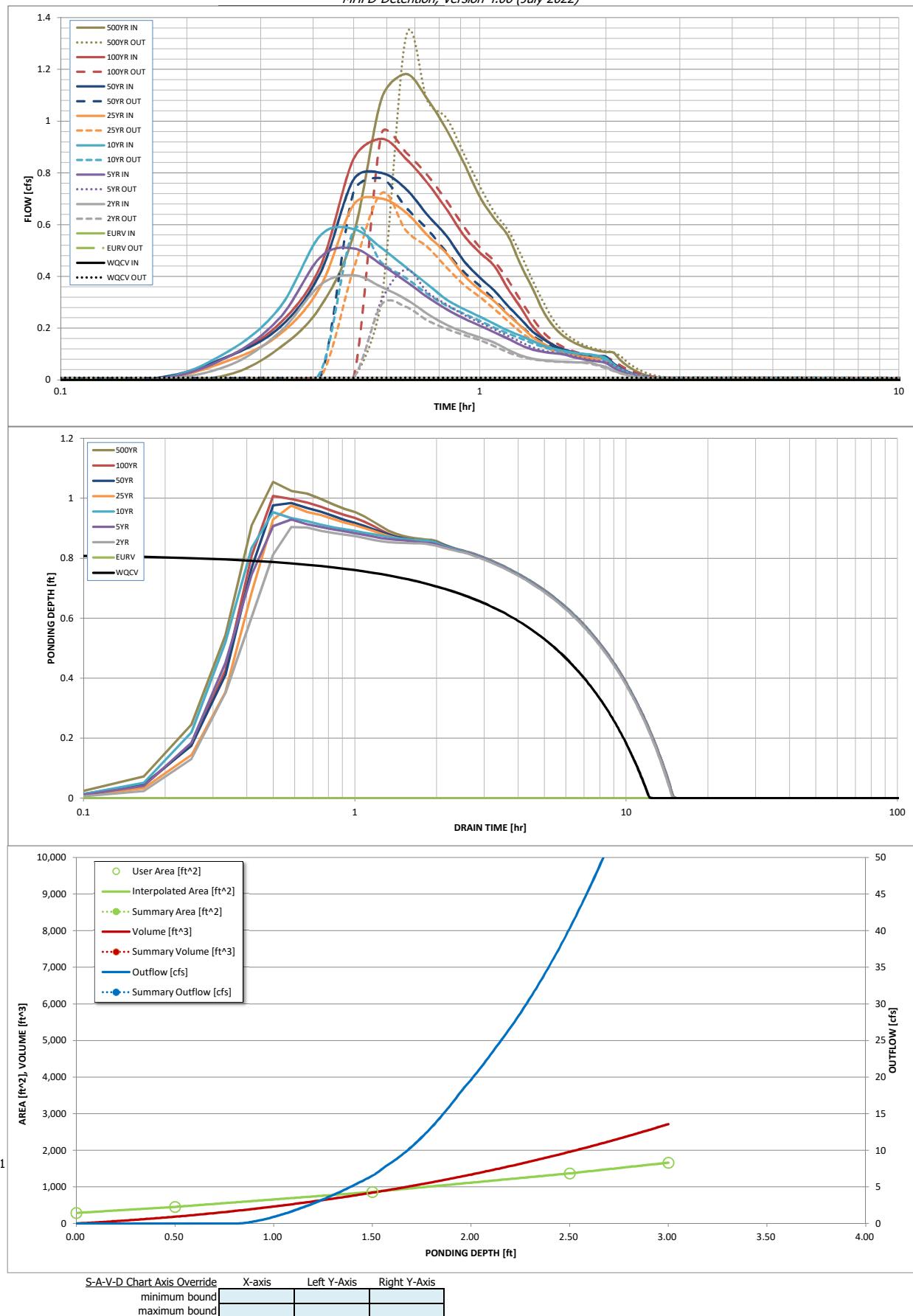
Calculated Parameters for Spillway	
0.13	feet
2.63	feet
0.03	acres
0.05	acre-ft

#### Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through Al)								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.008	0.037	0.025	0.037	0.044	0.050	0.057	
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.025	0.032	0.037	0.044	0.050	0.057
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.0	0.0	0.0	0.1	0.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.00	0.00	0.13	0.28	0.47
Peak Inflow Q (cfs) =	N/A	N/A	0.4	0.5	0.6	0.7	0.8	0.9
Peak Outflow Q (cfs) =	0.0	5.5	0.3	0.4	0.6	0.7	0.8	1.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	#DIV/0!	#DIV/0!	18.9	9.3	6.8
Structure Controlling Flow =	Overflow Weir 1	Spillway	Overflow Weir 1					
Max Velocity through Grate 1 (fps) =	N/A	1.97	0.04	0.1	0.1	0.1	0.1	0.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	12	0	14	13	13	13	13	12
Time to Drain 99% of Inflow Volume (hours) =	12	0	15	14	14	14	14	14
Maximum Ponding Depth (ft) =	0.82	2.24	0.90	0.93	0.95	0.98	0.98	1.01
Area at Maximum Ponding Depth (acres) =	0.01	0.03	0.01	0.01	0.01	0.01	0.01	0.02
Maximum Volume Stored (acre-ft) =	0.008	0.037	0.009	0.009	0.010	0.010	0.010	0.011

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-axis	Right Y-axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.02
	0:15:00	0.00	0.00	0.05	0.09	0.11	0.07	0.09	0.09	0.12
	0:20:00	0.00	0.00	0.18	0.24	0.28	0.18	0.20	0.22	0.28
	0:25:00	0.00	0.00	0.37	0.47	0.56	0.36	0.41	0.44	0.56
	0:30:00	0.00	0.00	0.40	0.51	0.58	0.68	0.77	0.85	1.09
	0:35:00	0.00	0.00	0.36	0.44	0.51	0.70	0.80	0.93	1.18
	0:40:00	0.00	0.00	0.31	0.38	0.44	0.65	0.74	0.86	1.09
	0:45:00	0.00	0.00	0.26	0.32	0.37	0.56	0.64	0.76	0.97
	0:50:00	0.00	0.00	0.21	0.27	0.31	0.49	0.56	0.66	0.84
	0:55:00	0.00	0.00	0.19	0.24	0.27	0.40	0.46	0.56	0.71
	1:00:00	0.00	0.00	0.16	0.21	0.24	0.35	0.40	0.49	0.62
	1:05:00	0.00	0.00	0.14	0.18	0.22	0.30	0.34	0.44	0.56
	1:10:00	0.00	0.00	0.12	0.16	0.19	0.25	0.29	0.35	0.45
	1:15:00	0.00	0.00	0.10	0.14	0.17	0.21	0.24	0.28	0.36
	1:20:00	0.00	0.00	0.08	0.12	0.15	0.17	0.19	0.21	0.27
	1:25:00	0.00	0.00	0.08	0.11	0.13	0.14	0.16	0.16	0.21
	1:30:00	0.00	0.00	0.07	0.10	0.12	0.12	0.13	0.14	0.17
	1:35:00	0.00	0.00	0.07	0.10	0.11	0.10	0.12	0.12	0.15
	1:40:00	0.00	0.00	0.07	0.09	0.11	0.10	0.11	0.10	0.13
	1:45:00	0.00	0.00	0.07	0.08	0.10	0.09	0.10	0.10	0.12
	1:50:00	0.00	0.00	0.07	0.08	0.10	0.08	0.10	0.09	0.11
	1:55:00	0.00	0.00	0.06	0.07	0.09	0.08	0.09	0.09	0.11
	2:00:00	0.00	0.00	0.05	0.07	0.08	0.08	0.09	0.08	0.11
	2:05:00	0.00	0.00	0.04	0.05	0.06	0.06	0.06	0.06	0.08
	2:10:00	0.00	0.00	0.03	0.03	0.04	0.04	0.05	0.04	0.05
	2:15:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:20:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	2:25:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.01	0.02
	2:30:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

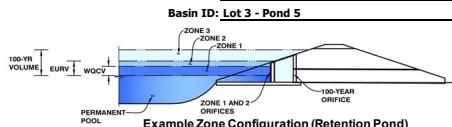
**CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)**

A soils 100%  
B soils 0%

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

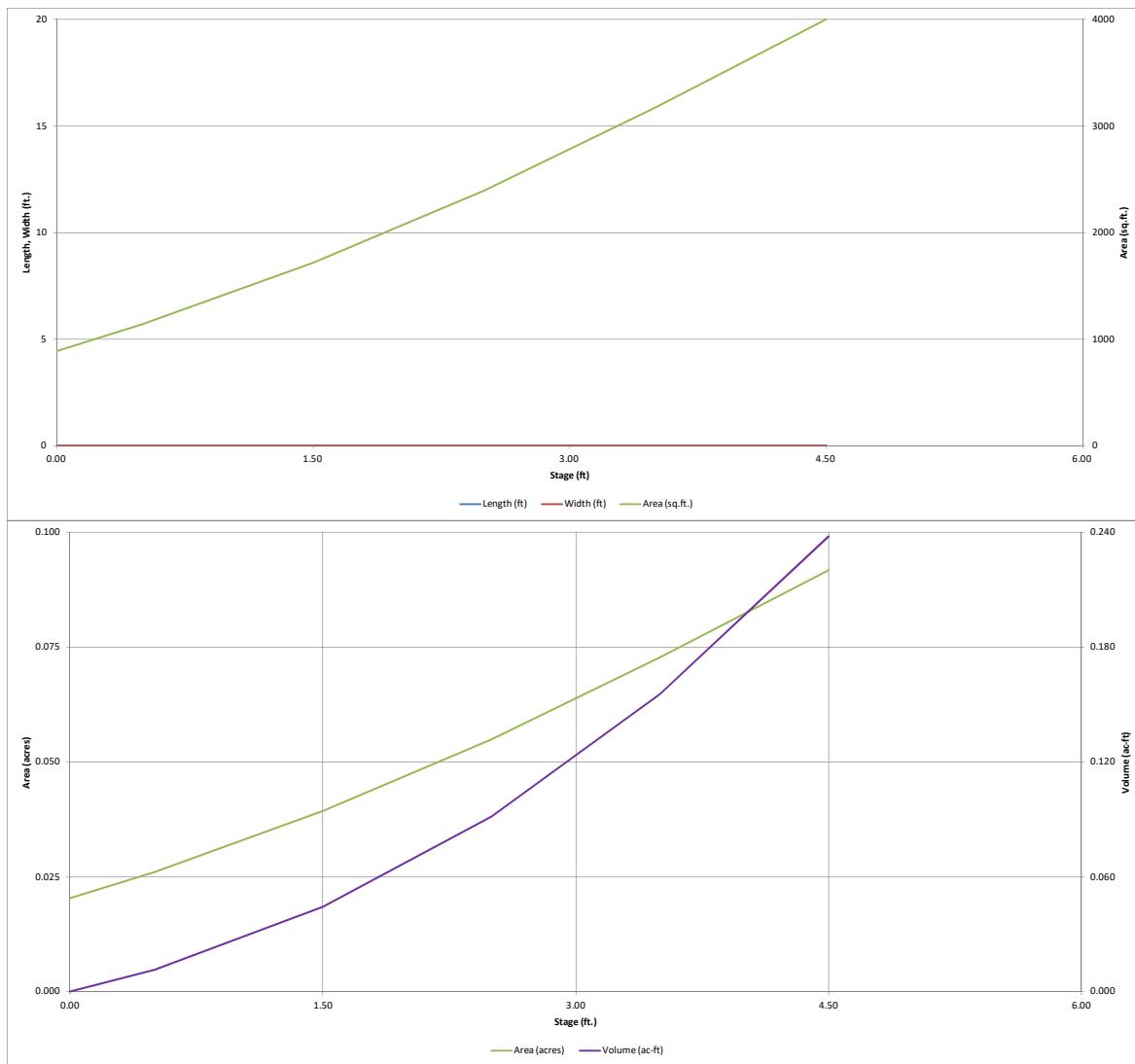
Project: Claremont Business Park 2 Filing No.



#### **Example Zone Configuration (Retention Pond)**

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: Claremont Business Park 2 Filing No. 2

### TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT

#### Example Zone Configuration (Retention Pond)

Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
1.14	0.031	Filtration Media
4.03	0.165	Weir&Pipe (Restrict)
Total (all zones)		0.196

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	2.50	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	0.82	inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	0.0 ft <sup>2</sup>
Underdrain Orifice Centroid =	0.03 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate	
WQ Orifice Area per Row =	N/A ft <sup>2</sup>
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =	Not Selected	Not Selected	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =			feet
Vertical Orifice Diameter =			inches

Calculated Parameters for Vertical Orif	
Vertical Orifice Area =	Not Selected
Vertical Orifice Centroid =	Not Selected

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Zone 2 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	1.15
Overflow Weir Front Edge Length =	3.00
Overflow Weir Grate Slope =	0.00
Horiz. Length of Weir Sides =	3.00
Overflow Grate Type =	Type C Grate
Debris Clogging % =	70%

Calculated Parameters for Overflow W	
Zone 2 Weir	Not Selected
Height of Grate Upper Edge, Ht =	1.15
Overflow Weir Slope Length =	3.00
Grate Open Area / 100-yr Orifice Area =	5.10
Overflow Grate Open Area w/o Debris =	6.26
Overflow Grate Open Area w/ Debris =	1.88

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =	Zone 2 Restrictor	Not Selected	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	2.75		inches
Restrictor Plate Height Above Pipe Invert =	15.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl	
Zone 2 Restrictor	Not Selected
Outlet Orifice Area =	1.23
Outlet Orifice Centroid =	0.63
Half-Central Angle of Restrictor Plate on Pipe =	3.14
	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	2.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	10.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

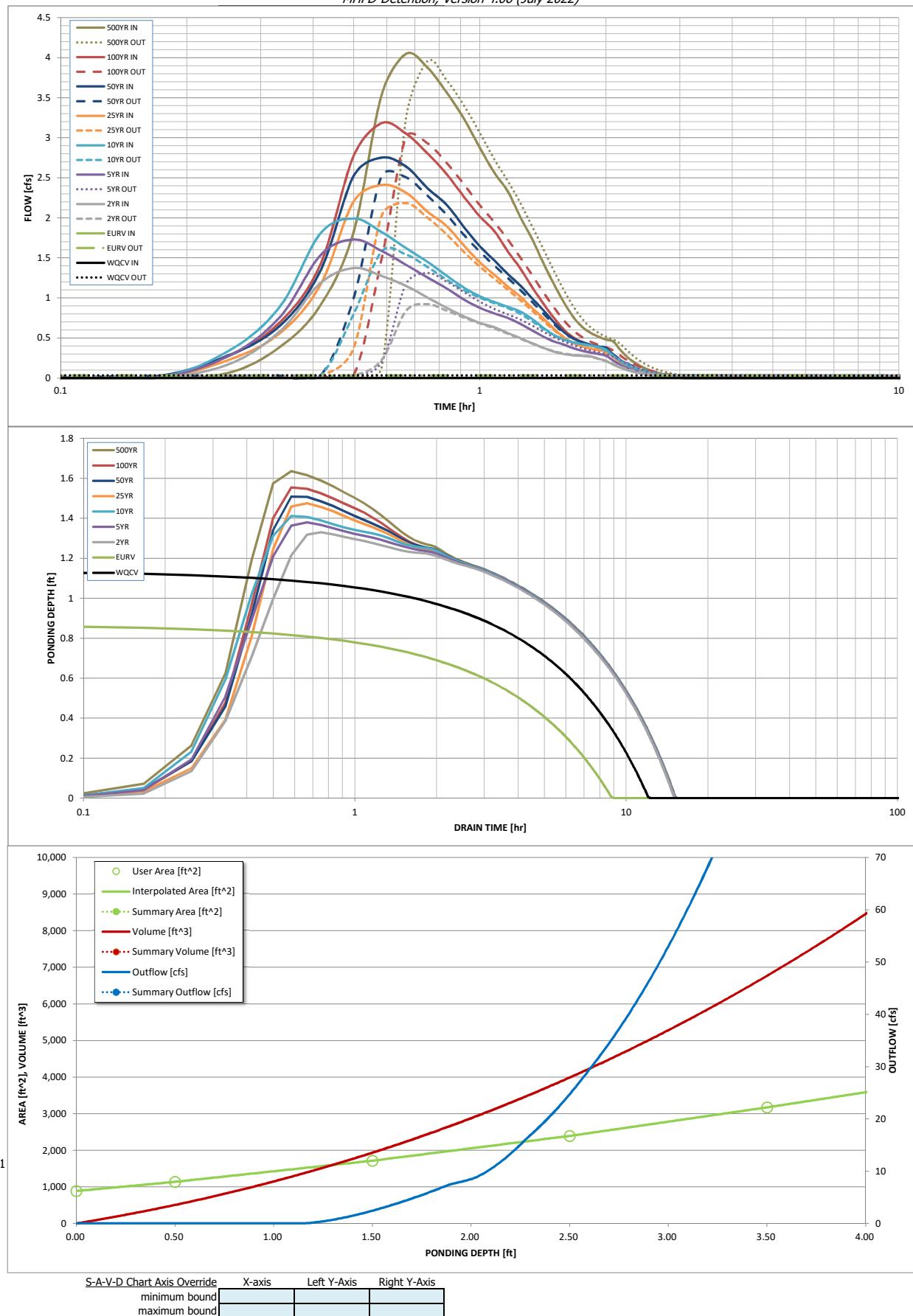
Calculated Parameters for Spillway	
0.21	feet
3.21	feet
0.07	acres
0.14	acre-ft

#### Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through Al)								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.031	0.141	0.097	0.125	0.148	0.172	0.196	0.223
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.097	0.125	0.148	0.172	0.196	0.223
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.0	0.0	0.1	0.3	0.5
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.01	0.01	0.12	0.25	0.40
Peak Inflow Q (cfs) =	N/A	N/A	1.4	1.7	2.0	2.4	2.8	3.2
Peak Outflow Q (cfs) =	0.0	17.3	0.9	1.3	1.6	2.2	2.5	3.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	120.0	104.1	15.6	8.9	6.5
Structure Controlling Flow =	Filtration Media	Spillway	Overflow Weir 1					
Max Velocity through Grate 1 (fps) =	N/A	2.19	0.14	0.2	0.2	0.4	0.4	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	12	8	14	14	13	13	13	12
Time to Drain 99% of Inflow Volume (hours) =	12	9	15	15	15	15	14	14
Maximum Ponding Depth (ft) =	1.14	3.30	1.33	1.38	1.41	1.48	1.51	1.55
Area at Maximum Ponding Depth (acres) =	0.03	0.07	0.04	0.04	0.04	0.04	0.04	0.04
Maximum Volume Stored (acre-ft) =	0.031	0.141	0.038	0.039	0.041	0.043	0.044	0.046

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-axis	Right Y-axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.06
	0:15:00	0.00	0.00	0.16	0.27	0.33	0.22	0.28	0.27	0.38
	0:20:00	0.00	0.00	0.58	0.76	0.89	0.56	0.65	0.70	0.91
	0:25:00	0.00	0.00	1.18	1.53	1.80	1.16	1.34	1.42	1.82
	0:30:00	0.00	0.00	1.37	1.73	1.99	2.20	2.52	2.77	3.53
	0:35:00	0.00	0.00	1.27	1.59	1.82	2.41	2.75	3.18	4.05
	0:40:00	0.00	0.00	1.15	1.41	1.62	2.31	2.64	3.05	3.88
	0:45:00	0.00	0.00	1.00	1.26	1.45	2.08	2.37	2.81	3.57
	0:50:00	0.00	0.00	0.88	1.12	1.28	1.90	2.16	2.55	3.24
	0:55:00	0.00	0.00	0.77	0.98	1.13	1.66	1.88	2.27	2.88
	1:00:00	0.00	0.00	0.69	0.88	1.02	1.45	1.65	2.02	2.56
	1:05:00	0.00	0.00	0.63	0.81	0.95	1.29	1.47	1.84	2.33
	1:10:00	0.00	0.00	0.56	0.75	0.89	1.14	1.30	1.58	2.01
	1:15:00	0.00	0.00	0.50	0.68	0.83	1.02	1.15	1.37	1.73
	1:20:00	0.00	0.00	0.43	0.59	0.74	0.88	0.99	1.14	1.44
	1:25:00	0.00	0.00	0.38	0.52	0.63	0.75	0.85	0.93	1.18
	1:30:00	0.00	0.00	0.33	0.46	0.54	0.62	0.70	0.76	0.96
	1:35:00	0.00	0.00	0.30	0.42	0.48	0.51	0.58	0.61	0.77
	1:40:00	0.00	0.00	0.28	0.37	0.45	0.44	0.50	0.51	0.64
	1:45:00	0.00	0.00	0.28	0.34	0.42	0.40	0.45	0.45	0.57
	1:50:00	0.00	0.00	0.27	0.32	0.41	0.37	0.41	0.41	0.52
	1:55:00	0.00	0.00	0.24	0.30	0.39	0.35	0.39	0.38	0.48
	2:00:00	0.00	0.00	0.21	0.28	0.36	0.33	0.38	0.36	0.45
	2:05:00	0.00	0.00	0.17	0.22	0.28	0.26	0.29	0.28	0.35
	2:10:00	0.00	0.00	0.13	0.16	0.21	0.20	0.22	0.21	0.26
	2:15:00	0.00	0.00	0.10	0.13	0.16	0.15	0.17	0.16	0.20
	2:20:00	0.00	0.00	0.07	0.09	0.12	0.11	0.13	0.12	0.15
	2:25:00	0.00	0.00	0.05	0.07	0.09	0.08	0.09	0.09	0.11
	2:30:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.07	0.08
	2:35:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	2:40:00	0.00	0.00	0.02	0.03	0.03	0.03	0.04	0.04	0.04
	2:45:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.02	0.03
	2:50:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.02
	2:55:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

CLAREMONT BUSINESS PARK 2 FILING NO. 2 (PROPOSED CONDITIONS)

<i><b>Weighted Percent Imperviousness of Ex Fil 1 WQ Sand Filter Pond 2</b></i>				
<i><b>Contributing Basins</b></i>	<i><b>Area (Acres)</b></i>	<i><b>C<sub>5</sub></b></i>	<i><b>Impervious % (I)</b></i>	<i><b>(Acres)* (I)</b></i>
<i><b>H1</b></i>	0.16	0.09	2	0.33
<i><b>H2</b></i>	0.40	0.09	2	0.80
<i><b>H3</b></i>	0.04	0.09	2	0.07
<i><b>H4</b></i>	0.10	0.09	2	0.20
<i><b>I1</b></i>	0.55	0.83	96.1	52.51
<i><b>I2</b></i>	0.48	0.79	93.8	45.26
<i><b>I3</b></i>	0.45	0.78	93.1	41.48
<i><b>I4</b></i>	0.55	0.81	95	52.18
<i><b>I5</b></i>	0.23	0.73	90	21.09
<i><b>I6</b></i>	0.19	0.62	82.1	15.37
<i><b>I7</b></i>	0.23	0.77	92.5	21.57
<i><b>J1</b></i>	0.69	0.81	95	65.94
<i><b>J2</b></i>	0.25	0.73	90	22.69
<i><b>J3</b></i>	0.01	0.16	13	0.19
<i><b>K1</b></i>	0.17	0.83	96.1	16.32
<i><b>K2</b></i>	0.05	0.72	89.3	4.76
<i><b>K3</b></i>	0.15	0.78	93.1	13.84
<i><b>K4</b></i>	0.05	0.69	87.1	4.53
<i><b>L</b></i>	1.32	0.09	2	2.63
<i><b>M1</b></i>	0.28	0.81	95	27.03
<i><b>M2</b></i>	0.24	0.62	82.1	19.93
<i><b>M3</b></i>	0.37	0.83	96.1	35.09
<i><b>M4</b></i>	0.98	0.80	94.4	92.27
<i><b>N1</b></i>	0.06	0.90	100	6.49
<i><b>N2</b></i>	0.41	0.12	7	2.90
<i><b>Totals</b></i>	<b>8.43</b>			<b>565.48</b>
<i><b>Imperviousness of WQ Pond 2</b></i>	<b>67.1</b>			

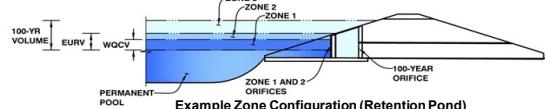
A soils      100%  
 B soils      0%

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.02 (February 2020)*

**Project: CLAREMONT COMMERCIAL FILING N**

**Basin ID: WQCV POND 2 (Remodeled Proposed Conditions)**



Watershed Information

<b>Selected BMP Type =</b>	<b>SF</b>
Watershed Area =	8.43
Watershed Length =	665
Watershed Length to Centroid =	325
Watershed Slope =	0.018
Watershed Imperviousness =	67.10%
Percentage Hydrologic Soil Group A =	0.0%
Percentage Hydrologic Soil Group B =	100.0%
Percentage Hydrologic Soil Groups C/D =	0.0%
Target WQV Drain Time =	12.0
Location for 1-hr Rainfall Depths =	User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.148	acre-feet
Excess Urban Runoff Volume (EURV) =	0.619	acre-feet
2-yr Runoff Volume ( $P_1 = 1.19 \text{ in.}$ ) =	0.541	acre-feet
5-yr Runoff Volume ( $P_1 = 1.5 \text{ in.}$ ) =	0.734	acre-feet
10-yr Runoff Volume ( $P_1 = 1.75 \text{ in.}$ ) =	0.897	acre-feet
25-yr Runoff Volume ( $P_1 = 2 \text{ in.}$ ) =	1.095	acre-feet
50-yr Runoff Volume ( $P_1 = 2.25 \text{ in.}$ ) =	1.267	acre-feet
100-yr Runoff Volume ( $P_1 = 2.5 \text{ in.}$ ) =	1.474	acre-feet
500-yr Runoff Volume ( $P_1 = 2.53 \text{ in.}$ ) =	1.481	acre-feet
Approximate 2-yr Detention Volume =	0.482	acre-feet
Approximate 5-yr Detention Volume =	0.644	acre-feet
Approximate 10-yr Detention Volume =	0.818	acre-feet
Approximate 25-yr Detention Volume =	0.880	acre-feet
Approximate 50-yr Detention Volume =	0.916	acre-feet
Approximate 100-yr Detention Volume =	0.986	acre-feet

## Define Zones and Basin Geometry

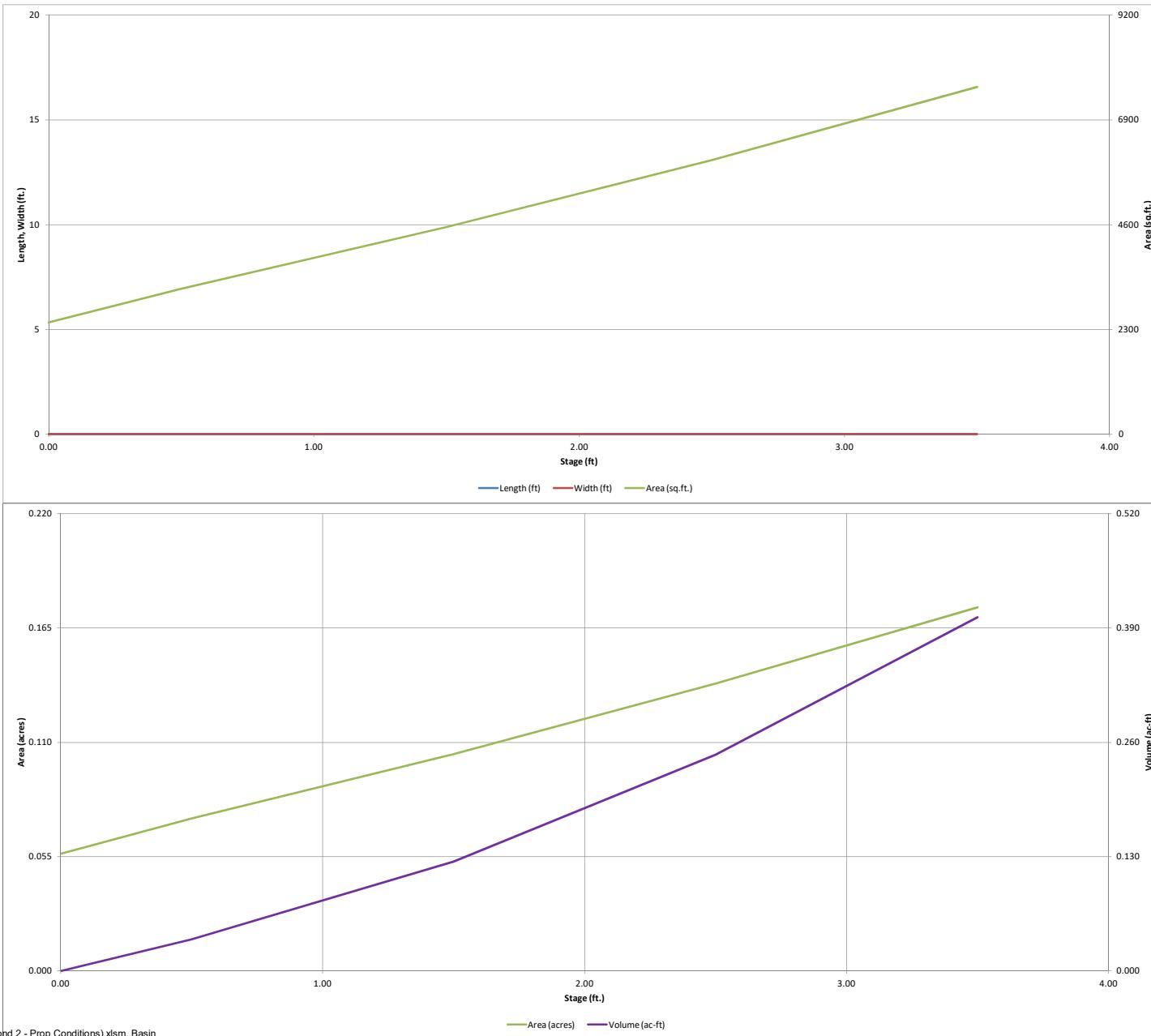
Zone 1 Volume (WQCV) =	0.148	acre-feet
Zone 2 Volume (100-year - Zone 1) =	0.838	acre-feet
Select Zone 3 Storage Volume (Optional) =		acre-feet
Total Detention Basin Volume =	0.986	
Initial Surcharge Volume (ISV) =	N/A	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth ( $H_{total}$ ) =	user	ft
Depth of Trickle Channel ( $H_{rc}$ ) =	N/A	ft
Slope of Trickle Channel ( $S_{rc}$ ) =	N/A	ft/ft
Slopes of Main Basin Sides ( $S_{main}$ ) =	user	ft/V
Basin Length-to-Width Ratio ( $R_{LW}$ ) =	user	

Initial Surcharge Area ( $A_{SV}$ ) =	<input type="text"/>	user	$\text{ft}^2$
Surcharge Volume Length ( $L_{SV}$ ) =	<input type="text"/>	user	ft
Surcharge Volume Width ( $W_{SV}$ ) =	<input type="text"/>	user	ft
Depth of Basin Floor ( $H_{FLOOR}$ ) =	<input type="text"/>	user	ft
Length of Basin Floor ( $L_{FLOOR}$ ) =	<input type="text"/>	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	<input type="text"/>	user	ft
Area of Basin Floor ( $A_{FLOOR}$ ) =	<input type="text"/>	user	$\text{ft}^2$
Volume of Basin Floor ( $V_{FLOOR}$ ) =	<input type="text"/>	user	$\text{ft}^3$
Depth of Main Basin ( $H_{MAIN}$ ) =	<input type="text"/>	user	ft
Length of Main Basin ( $L_{MAIN}$ ) =	<input type="text"/>	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	<input type="text"/>	user	ft
Area of Main Basin ( $A_{MAIN}$ ) =	<input type="text"/>	user	$\text{ft}^2$
Volume of Main Basin ( $V_{MAIN}$ ) =	<input type="text"/>	user	$\text{ft}^3$
Calculated Total Basin Volume ( $V_{...}$ ) =	<input type="text"/>	user	acre-feet

6364

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.02 (February 2020)*



Define "Remodeled Proposed Conditions."  
How is this different for the other calcs for this  
same pond shown on pdf page 60 above?  
Please discuss in the FDR text above.

**DETENTION BASIN OUTLET STRU**  
*MHFD-Detention Version 4.02 (February 2012)*  
**Project: CLAREMONT COMMERCIAL FILING NO.2**  
**Basin ID: WQCV POND 2 (Remodeled Proposed Conditions)**

**SHEET LABELED EXISTING CONDITION  
AND CORRESPONDING SHEET LABEL  
PROPOSED CONDITION EXTENTION  
OF EL JEFE HT.**

**Example Zone Configuration (Retention Pond)**

Zone	Estimated Stage (ft)	Flow Rate (ft³/s)	Notes
Zone 1 (WQCV)	1.77	0.128	PERMANENT POOL
Zone 2 (100-year)	#VALUE!	0.838	Weir&Pipe (Restrict)
Zone 3			
Total (all zones)	0.986		

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft²  
 Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing =  inches  
 Orifice Plate: Orifice Area per Row =  inches

Calculated Parameters for Plate

WQ Orifice Area per Row =  ft²  
 Elliptical Half-Width =  feet  
 Elliptical Slot Centroid =  feet  
 Elliptical Slot Area =  ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A						
Orifice Area (sq. inches)	N/A						

Calculated Parameters for Vertical Orifice

Vertical Orifice Area =  ft²  
 Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, Ho =  ft (relative to basin bottom at Stage = 0 ft)  
 Overflow Weir Front Edge Length =  feet  
 Overflow Weir Grate Slope =  H:V  
 Horiz. Length of Weir Sides =  feet  
 Overflow Grate Open Area % =  %, grate open area/total area  
 Debris Clogging % =  %

Calculated Parameters for Overflow Weir

Height of Grate Upper Edge, H<sub>t</sub> =  feet  
 Overflow Weir Slope Length =  feet  
 Grate Open Area / 100-yr Orifice Area =  ft²  
 Overflow Grate Open Area w/o Debris =  ft²  
 Overflow Grate Open Area w/ Debris =  ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
 Outlet Pipe Diameter =  inches  
 Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area =  ft²  
 Outlet Orifice Centroid =  feet  
 Half-Central Angle of Restrictor Plate on Pipe =  radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
 Spillway Crest Length =  feet  
 Spillway End Slopes =  H:V  
 Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =  feet  
 Stage at Top of Freeboard =  feet  
 Basin Area at Top of Freeboard =  acres  
 Basin Volume at Top of Freeboard =  acre-ft

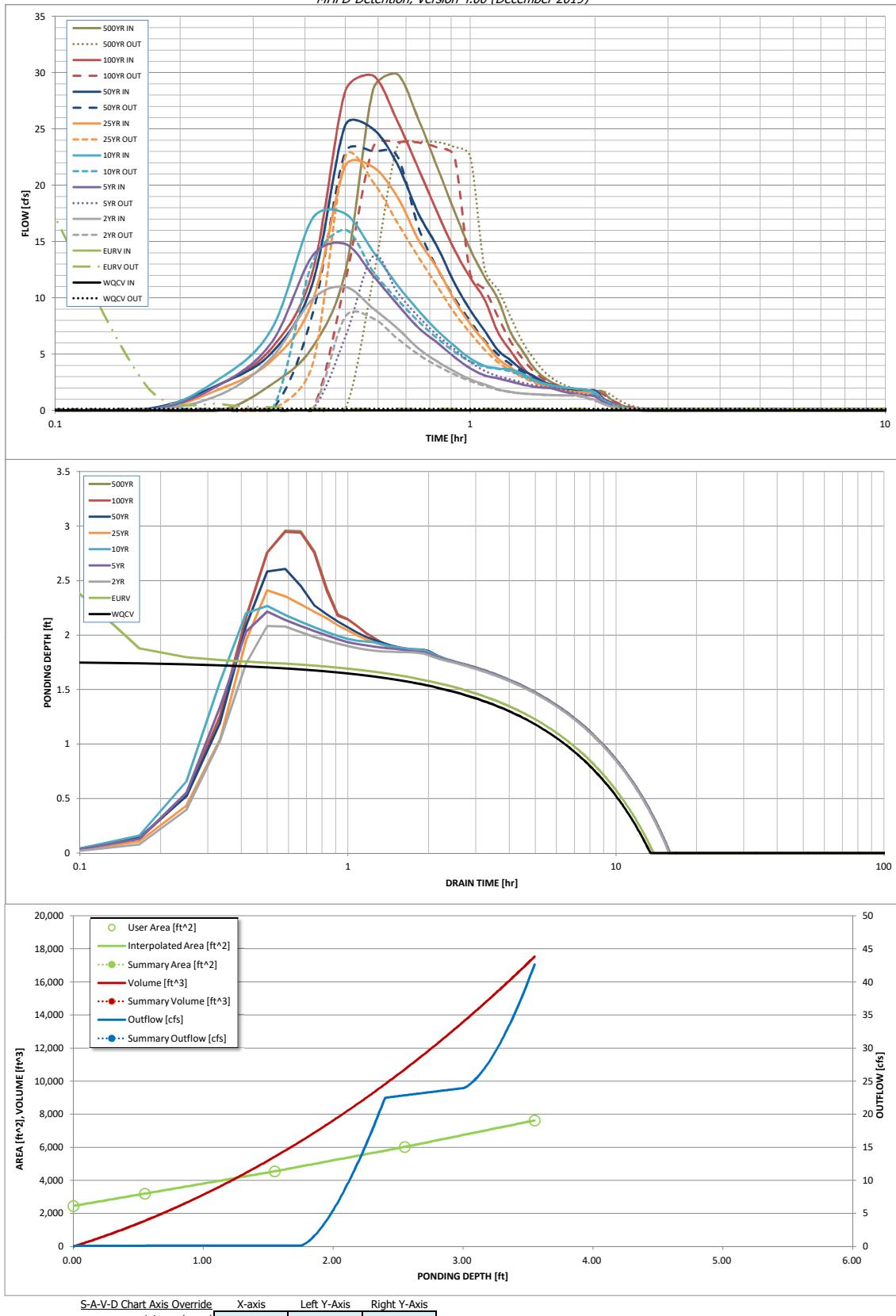
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	2.53
CUHP Runoff Volume (acre-ft) =	0.148	0.619	0.541	0.734	0.897	1.095	1.267	1.474	1.481
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.541	0.734	0.897	1.095	1.267	1.474	1.481
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	3.2	4.7	8.3	10.4	13.0	13.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.14	0.37	0.56	0.99	1.24	1.55	1.56
Peak Inflow Q (cfs) =	N/A	N/A	11.0	14.8	17.5	21.7	25.3	29.7	29.9
Peak Outflow Q (cfs) =	0.2	42.6	8.3	13.7	16.0	22.5	23.0	23.8	23.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	4.3	3.4	2.7	2.2	1.8	1.8
Structure Controlling Flow =	Overflow Weir 1	Outlet Plate 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	0.01	1.59	0.57	0.9	1.1	1.6	1.6	1.7	1.7
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	13	12	14	14	13	13	12	12	12
Time to Drain 99% of Inflow Volume (hours) =	13	13	15	15	15	15	15	14	14
Maximum Ponding Depth (ft) =	1.77	2.56	2.08	2.21	2.27	2.41	2.61	2.95	2.96
Area at Maximum Ponding Depth (acres) =	0.11	0.14	0.12	0.13	0.13	0.13	0.14	0.15	0.15
Maximum Volume Stored (acre-ft) =	0.148	0.246	0.185	0.201	0.207	0.227	0.253	0.302	0.304

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



S-A-V-D Chart Axis Override	X-axis	Left Y-axis	Right Y-axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*Outflow Hydrograph Workbook Filename:*

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lo1 Pond 1 (Future)  
**Location:** Lot 1 - Claremont Buisness Park 2 - Filing No. 2

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math>            (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time  <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume  <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region,            Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume            (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{83.4} \%$ $i = \boxed{0.834}$ $WQCV = \boxed{0.28}$ watershed inches $Area = \boxed{74,372}$ sq ft $V_{WQCV} = \boxed{\phantom{000}}$ cu ft $d_6 = \boxed{0.60}$ in $V_{WQCV\ OTHER} = \boxed{2,426}$ cu ft $V_{WQCV\ USER} = \boxed{\phantom{000}}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	$D_{WQCV} = \boxed{1.2}$ ft $Z = \boxed{4.00}$ ft / ft $A_{Min} = \boxed{775}$ sq ft $A_{Actual} = \boxed{873}$ sq ft $V_T = \boxed{\phantom{000}}$ cu ft
<p>3. Filter Material</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain):  <hr/><hr/></p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p><math>y = \boxed{2.5}</math> ft</p> <p><math>Vol_{12} = \boxed{2,426}</math> cu ft</p> <p><math>D_o = \boxed{1 1/16}</math> in</p>

## Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lo1 Pond 1 (Future)  
**Location:** Lot 1 - Claremont Buisness Park 2 - Filing No. 2

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES  NO

6. Inlet / Outlet Works

- A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

TBD

Concrete Outlet Box with Unrestricted 18" RCP

Notes:

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## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 2 Pond 2 (Future)  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math>            (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time  <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume  <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume            (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{77.9} \%$ $i = \boxed{0.779}$ $WQCV = \boxed{0.25}$ watershed inches $Area = \boxed{38,960}$ sq ft $V_{WQCV} = \boxed{\phantom{000}}$ cu ft $d_6 = \boxed{0.60}$ in $V_{WQCV\ OTHER} = \boxed{1,144}$ cu ft $V_{WQCV\ USER} = \boxed{\phantom{000}}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	$D_{WQCV} = \boxed{1.0}$ ft $Z = \boxed{4.00}$ ft / ft $A_{Min} = \boxed{379}$ sq ft $A_{Actual} = \boxed{513}$ sq ft $V_T = \boxed{\phantom{000}}$ cu ft
<p>3. Filter Material</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain):  <hr/><hr/></p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p><math>y = \boxed{2.5}</math> ft</p> <p><math>Vol_{12} = \boxed{1,144}</math> cu ft</p> <p><math>D_o = \boxed{3/4}</math> in</p>

## Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 2 Pond 2 (Future)  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES  NO

6. Inlet / Outlet Works

- A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

TBD

Concrete Outlet Box with Unrestricted 18" RCP

Notes:

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## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 2 Pond 3  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{81.8} \%$ $i = \boxed{0.818}$ $WQCV = \boxed{0.27}$ watershed inches $Area = \boxed{62,251}$ sq ft $V_{WQCV} = \boxed{\quad}$ cu ft $d_6 = \boxed{0.60}$ in $V_{WQCV\ OTHER} = \boxed{\quad}$ cu ft $V_{WQCV\ USER} = \boxed{1,393}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	$D_{WQCV} = \boxed{1.3}$ ft $Z = \boxed{4.00}$ ft / ft $A_{Min} = \boxed{637}$ sq ft $A_{Actual} = \boxed{784}$ sq ft $V_T = \boxed{\quad}$ cu ft
<p>3. Filter Material</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain): _____ _____</p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p><math>y = \boxed{2.5}</math> ft</p> <p><math>Vol_{12} = \boxed{1,393}</math> cu ft</p> <p><math>D_o = \boxed{13/16}</math> in</p>

## Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: Darin Moffett  
Company: M&S Civil Consultants  
Date: February 23, 2023  
Project: Lot 2 Pond 3  
Location: Lot 2 - Claremont Business Park 2 - Filing No. 2

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES  NO

6. Inlet / Outlet Works

- A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

TBD

Concrete Outlet Box with Restricted 18" RCP

Notes:

## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 3 Pond 4  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{90.0} \%$ $i = \boxed{0.900}$ $WQCV = \boxed{0.32}$ watershed inches $Area = \boxed{12,955}$ sq ft $V_{WQCV} = \boxed{\phantom{000}}$ cu ft $d_6 = \boxed{0.60}$ in $V_{WQCV\ OTHER} = \boxed{\phantom{000}}$ cu ft $V_{WQCV\ USER} = \boxed{349}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	$D_{WQCV} = \boxed{0.8}$ ft $Z = \boxed{4.00}$ ft / ft $A_{Min} = \boxed{146}$ sq ft $A_{Actual} = \boxed{288}$ sq ft $V_T = \boxed{350}$ cu ft
<p>3. Filter Material</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain): _____ _____</p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p><math>y = \boxed{2.5}</math> ft</p> <p><math>Vol_{12} = \boxed{349}</math> cu ft</p> <p><math>D_o = \boxed{7/16}</math> in</p>

## Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 3 Pond 4  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES  NO

6. Inlet / Outlet Works

- A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

TBD

Concrete Outlet Box with Unrestricted 18" RCP

Notes:

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## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 3 Pond 5  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math display="block">WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math display="block">V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	$I_a = \boxed{90.0} \%$ $i = \boxed{0.900}$ $WQCV = \boxed{0.32}$ watershed inches $Area = \boxed{50,180}$ sq ft $V_{WQCV} = \boxed{\phantom{000}}$ cu ft $d_6 = \boxed{0.60}$ in $V_{WQCV\ OTHER} = \boxed{1,874}$ cu ft $V_{WQCV\ USER} = \boxed{\phantom{000}}$ cu ft
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	$D_{WQCV} = \boxed{0.8}$ ft $Z = \boxed{4.00}$ ft / ft $A_{Min} = \boxed{565}$ sq ft $A_{Actual} = \boxed{887}$ sq ft $V_T = \boxed{\phantom{000}}$ cu ft
<p>3. Filter Material</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain): _____</p>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p>	<p>Choose One –</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p><math>y = \boxed{2.5}</math> ft</p> <p><math>Vol_{12} = \boxed{1,874}</math> cu ft</p> <p><math>D_o = \boxed{15/16}</math> in</p>

## Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

**Designer:** Darin Moffett  
**Company:** M&S Civil Consultants  
**Date:** February 23, 2023  
**Project:** Lot 3 Pond 5  
**Location:** Lot 2 - Claremont Business Park 2 - Filing No. 2

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

- A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES  NO

6. Inlet / Outlet Works

- A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

TBD

Concrete Outlet Box with Unrestricted 18" RCP

Notes:

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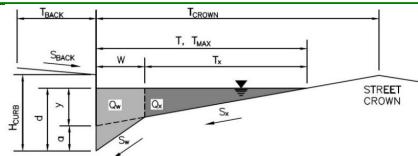


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## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 1 (DP5)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$ =	7.5	ft
$S_{BACK}$ =	0.020	ft/ft
$n_{BACK}$ =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$ =	6.00	inches
$T_CROWN$ =	18.0	ft
$W$ =	2.00	ft
$S_x$ =	0.020	ft/ft
$S_w$ =	0.083	ft/ft
$S_0$ =	0.000	ft/ft
$n_{STREET}$ =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm
$T_{MAX}$ =	15.8	18.0
$d_{MAX}$ =	4.6	7.8



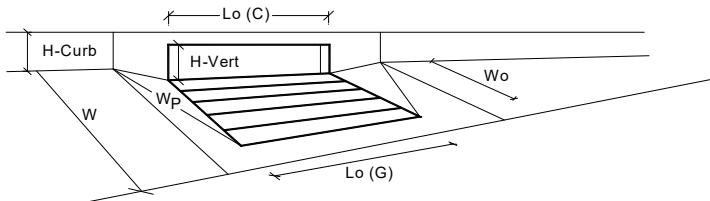
MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

	Minor Storm	Major Storm
$Q_{allow}$ =	SUMP	SUMP

cfs

## INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)



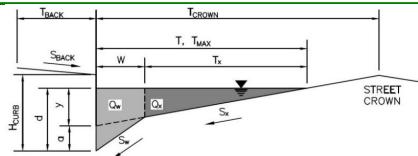
<b>Design Information (Input)</b>	CDOT Type R Curb Opening
Type of Inlet	
Local Depression (additional to continuous gutter depression 'a' from above)	
Number of Unit Inlets (Grate or Curb Opening)	
Water Depth at Flowline (outside of local depression)	
<b>Grate Information</b>	
Length of a Unit Grate	
Width of a Unit Grate	
Open Area Ratio for a Grate (typical values 0.15-0.90)	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	
Grate Weir Coefficient (typical value 2.15 - 3.60)	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	
<b>Curb Opening Information</b>	
Length of a Unit Curb Opening	
Height of Vertical Curb Opening in Inches	
Height of Curb Orifice Throat in Inches	
Angle of Throat (see USDCM Figure ST-5)	
Side Width for Depression Pan (typically the gutter width of 2 feet)	
Clogging Factor for a Single Curb Opening (typical value 0.10)	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	
<b>Low Head Performance Reduction (Calculated)</b>	
Depth for Grate Midwidth	
Depth for Curb Opening Weir Equation	
Grated Inlet Performance Reduction Factor for Long Inlets	
Curb Opening Performance Reduction Factor for Long Inlets	
Combination Inlet Performance Reduction Factor for Long Inlets	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>	
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
$d_{local}$ =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	4.6	5.8	inches
		<input type="checkbox"/> Override Depths	
$L_o (G)$ =	N/A	N/A	feet
$W_o$ =	N/A	N/A	feet
$A_{ratio}$ =	N/A	N/A	
$C_f (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
		<input type="checkbox"/> Override Depths	
$L_o (C)$ =	5.00	5.00	feet
$H_{vert}$ =	6.00	6.00	inches
$H_{throat}$ =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
$W_p$ =	2.00	2.00	feet
$C_f (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
		<input type="checkbox"/> Override Depths	
$d_{Grate}$ =	N/A	N/A	ft
$d_{Curb}$ =	0.22	0.32	ft
$RF_{Grate}$ =	N/A	N/A	
$RF_{Curb}$ =	1.00	1.00	
$RF_{Combination}$ =	N/A	N/A	
		<input type="checkbox"/> Override Depths	
$Q_a$ =	2.8	5.0	cfs
$Q_{PEAK\ REQUIRED}$ =	1.2	2.2	cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 2 (DP5)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$ =	7.5	ft
$S_{BACK}$ =	0.020	ft/ft
$n_{BACK}$ =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$ =	6.00	inches
$T_{CROWN}$ =	18.0	ft
$W$ =	2.00	ft
$S_x$ =	0.020	ft/ft
$S_w$ =	0.083	ft/ft
$S_0$ =	0.000	ft/ft
$n_{STREET}$ =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm
$T_{MAX}$ =	15.8	18.0
$d_{MAX}$ =	4.6	7.8

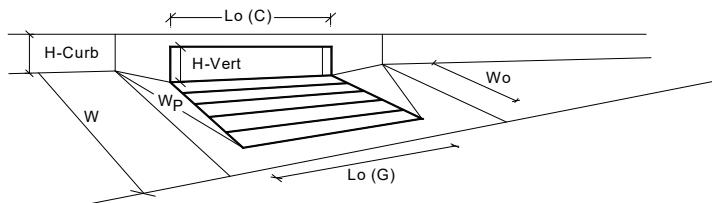
MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

Minor Storm	Major Storm
SUMP	SUMP

cfs

## **INLET IN A SUMP OR SAG LOCATION**

*MHFD-Inlet, Version 5.02 (August 2022)*

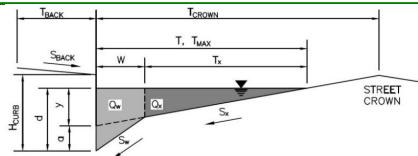


<b>Design Information (Input)</b>	
Type of Inlet	CDOT Type R Curb Opening
Local Depression (additional to continuous gutter depression 'a' from above)	
Number of Unit Inlets (Grate or Curb Opening)	
Water Depth at Flowline (outside of local depression)	
<b>Grate Information</b>	
Length of a Unit Grate	
Width of a Unit Grate	
Open Area Ratio for a Grate (typical values 0.15-0.90)	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	
Grate Weir Coefficient (typical value 2.15 - 3.60)	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	
<b>Curb Opening Information</b>	
Length of a Unit Curb Opening	
Height of Vertical Curb Opening in Inches	
Height of Curb Orifice Throat in Inches	
Angle of Throat (see USDCM Figure ST-5)	
Side Width for Depression Pan (typically the gutter width of 2 feet)	
Clogging Factor for a Single Curb Opening (typical value 0.10)	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	
<b>Low Head Performance Reduction (Calculated)</b>	
Depth for Grate Midwidth	
Depth for Curb Opening Weir Equation	
Grated Inlet Performance Reduction Factor for Long Inlets	
Curb Opening Performance Reduction Factor for Long Inlets	
Combination Inlet Performance Reduction Factor for Long Inlets	
Total Inlet Interception Capacity (assumes clogged condition)	
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 3 (DP11 North)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$ =	7.5	ft
$S_{BACK}$ =	0.020	ft/ft
$n_{BACK}$ =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$ =	6.00	inches
$T_{CROWN}$ =	17.0	ft
$W$ =	2.00	ft
$S_x$ =	0.020	ft/ft
$S_w$ =	0.083	ft/ft
$S_0$ =	0.012	ft/ft
$n_{STREET}$ =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
$T_{MAX}$ =	15.8	17.0
$d_{MAX}$ =	4.6	7.8



MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

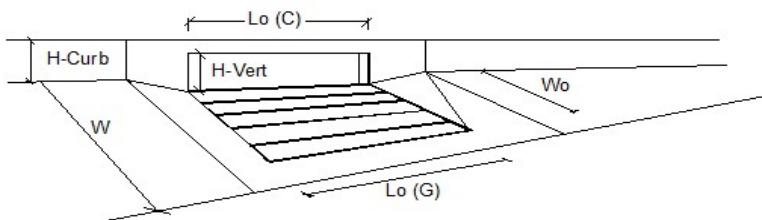
	Minor Storm	Major Storm
$Q_{allow}$ =	6.5	12.7

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.20 cfs on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.40 cfs on sheet 'Inlet Management'

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

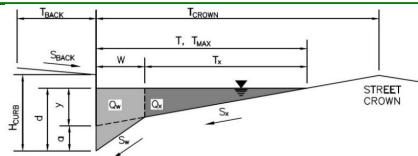


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a <sub>local</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		N <sub>o</sub> =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>f</sub> (G) =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>f</sub> (C) =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity					
Total Inlet Interception Capacity		Q =	4.2	8.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	0.0	0.4	cfs
Capture Percentage = Q <sub>b</sub> /Q <sub>a</sub>		C% =	100	95	%

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 4 (DP11 South)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$ =	7.5	ft
$S_{BACK}$ =	0.020	ft/ft
$n_{BACK}$ =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$ =	6.00	inches
$T_{CROWN}$ =	17.0	ft
$W$ =	2.00	ft
$S_x$ =	0.020	ft/ft
$S_w$ =	0.083	ft/ft
$S_0$ =	0.011	ft/ft
$n_{STREET}$ =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
$T_{MAX}$ =	15.8	17.0
$d_{MAX}$ =	4.6	7.8

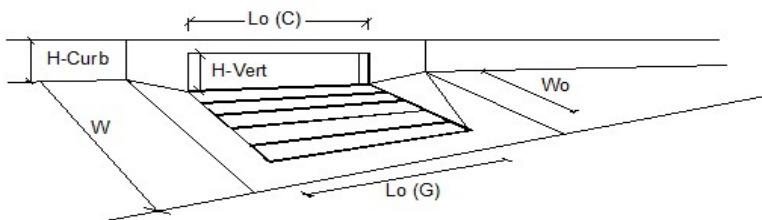
MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

	Minor Storm	Major Storm
$Q_{allow}$ =	6.2	12.2

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.20 cfs on sheet 'Inlet Management'  
 Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.40 cfs on sheet 'Inlet Management'

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

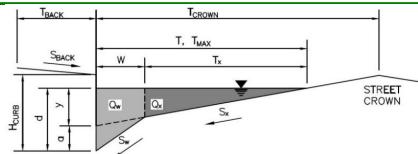


<b>Design Information (Input)</b>	CDOT Type R Curb Opening	
Type of Inlet	Type = <b>CDOT Type R Curb Opening</b>	
Local Depression (additional to continuous gutter depression 'a')	<b>a<sub>local</sub> = 3.0</b>	<b>3.0 inches</b>
Total Number of Units in the Inlet (Grate or Curb Opening)	<b>No = 3</b>	<b>3 ft</b>
Length of a Single Unit Inlet (Grate or Curb Opening)	<b>Lo = 5.00</b>	<b>5.00 ft</b>
Width of a Unit Grate (cannot be greater than W, Gutter Width)	<b>W<sub>o</sub> = N/A</b>	<b>N/A ft</b>
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	<b>C<sub>f</sub> (G) = N/A</b>	<b>N/A</b>
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	<b>C<sub>f</sub> (C) = 0.10</b>	<b>0.10</b>
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		
Total Inlet Interception Capacity	<b>Q = 4.2</b>	<b>8.0 cfs</b>
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q<sub>b</sub> = 0.0</b>	<b>0.4 cfs</b>
Capture Percentage = Q <sub>b</sub> /Q <sub>a</sub>	<b>C% = 100</b>	<b>95 %</b>

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 5 (DP12)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>x</sub> =	0.020	ft/ft
S <sub>w</sub> =	0.083	ft/ft
S <sub>0</sub> =	0.010	ft/ft
n <sub>STREET</sub> =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
T <sub>MAX</sub> =	15.8	17.0
d <sub>MAX</sub> =	4.6	7.8

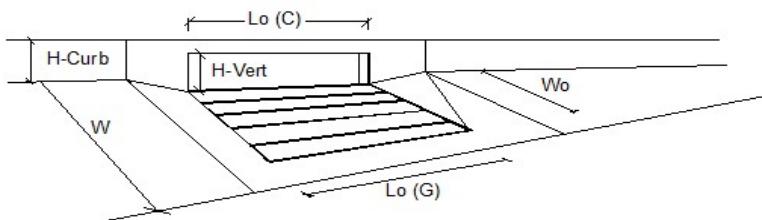
MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion  
**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 2.80 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.10 cfs on sheet 'Inlet Management'**

	Minor Storm	Major Storm
Q <sub>allow</sub> =	5.9	11.6

cfs

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

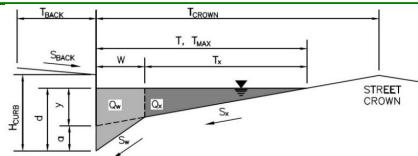


<b>Design Information (Input)</b> Type of Inlet: CDOT Type R Curb Opening Local Depression (additional to continuous gutter depression 'a') Total Number of Units in the Inlet (Grate or Curb Opening) Length of a Single Unit Inlet (Grate or Curb Opening) Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity'</b> Total Inlet Interception Capacity Total Inlet Carry-Over Flow (flow bypassing inlet) Capture Percentage = Q <sub>b</sub> /Q <sub>a</sub>	<b>MINOR</b> <b>MAJOR</b>	Type = CDOT Type R Curb Opening a <sub>local</sub> = 3.0      3.0      inches N <sub>o</sub> = 3      3 L <sub>o</sub> = 5.00      5.00      ft W <sub>o</sub> = N/A      N/A      ft C <sub>f</sub> (G) = N/A      N/A C <sub>f</sub> (C) = 0.10      0.10  <b>MINOR</b> <b>MAJOR</b> Q = 2.8      7.8      cfs Q <sub>b</sub> = 0.0      0.3      cfs C% = 100      96      %
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## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor &amp; Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Claremont Business Park 2 Filing 2 (Proposed Conditions)  
 Inlet ID: Inlet 6 (DP13)

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T <sub>BACK</sub> =	7.5	ft
S <sub>BACK</sub> =	0.020	ft/ft
n <sub>BACK</sub> =	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H <sub>CURB</sub> =	6.00	inches
T <sub>CROWN</sub> =	17.0	ft
W =	2.00	ft
S <sub>x</sub> =	0.020	ft/ft
S <sub>w</sub> =	0.083	ft/ft
S <sub>0</sub> =	0.010	ft/ft
n <sub>STREET</sub> =	0.015	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm
T <sub>MAX</sub> =	15.8	17.0
d <sub>MAX</sub> =	4.6	7.8

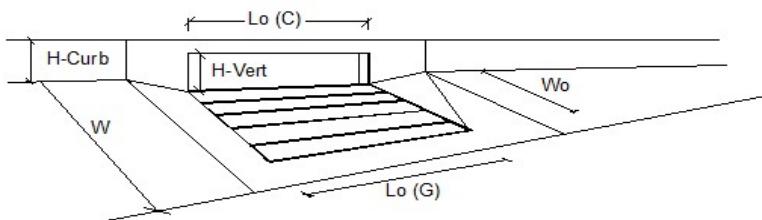
MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion  
**Minor storm max. allowable capacity GOOD - greater than the design peak flow of 1.00 cfs on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design peak flow of 5.00 cfs on sheet 'Inlet Management'**

	Minor Storm	Major Storm
Q <sub>allow</sub> =	5.9	11.6

cfs

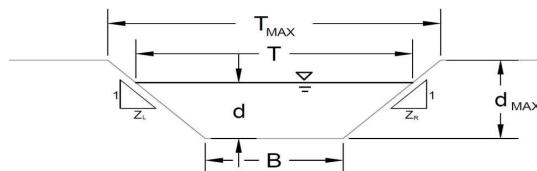
## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)



<b>Design Information (Input)</b> Type of Inlet: CDOT Type R Curb Opening Local Depression (additional to continuous gutter depression 'a') Total Number of Units in the Inlet (Grate or Curb Opening) Length of a Single Unit Inlet (Grate or Curb Opening) Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) <b>Street Hydraulics:</b> OK - Q < Allowable Street Capacity	<table style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;"></th> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <th></th> </tr> </thead> <tbody> <tr> <td>Type =</td> <td colspan="2" style="text-align: center;">CDOT Type R Curb Opening</td> <td></td> </tr> <tr> <td>a<sub>local</sub> =</td> <td style="text-align: center;">3.0</td> <td style="text-align: center;">3.0</td> <td>inches</td> </tr> <tr> <td>N<sub>o</sub> =</td> <td style="text-align: center;">3</td> <td style="text-align: center;">3</td> <td></td> </tr> <tr> <td>L<sub>o</sub> =</td> <td style="text-align: center;">5.00</td> <td style="text-align: center;">5.00</td> <td>ft</td> </tr> <tr> <td>W<sub>o</sub> =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>ft</td> </tr> <tr> <td>C<sub>f</sub> (G) =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>C<sub>f</sub> (C) =</td> <td style="text-align: center;">0.10</td> <td style="text-align: center;">0.10</td> <td></td> </tr> <tr> <td colspan="4" style="text-align: right; padding-top: 10px;"><b>MINOR                    MAJOR</b></td> </tr> <tr> <td>Total Inlet Interception Capacity</td> <td style="text-align: center;">Q =</td> <td style="text-align: center;">1.0</td> <td style="text-align: center;">5.0</td> <td>cfs</td> </tr> <tr> <td>Total Inlet Carry-Over Flow (flow bypassing inlet)</td> <td style="text-align: center;">Q<sub>b</sub> =</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> <td>cfs</td> </tr> <tr> <td>Capture Percentage = Q<sub>b</sub>/Q<sub>a</sub></td> <td style="text-align: center;">C% =</td> <td style="text-align: center;">100</td> <td style="text-align: center;">100</td> <td>%</td> </tr> </tbody> </table>		MINOR	MAJOR		Type =	CDOT Type R Curb Opening			a <sub>local</sub> =	3.0	3.0	inches	N <sub>o</sub> =	3	3		L <sub>o</sub> =	5.00	5.00	ft	W <sub>o</sub> =	N/A	N/A	ft	C <sub>f</sub> (G) =	N/A	N/A		C <sub>f</sub> (C) =	0.10	0.10		<b>MINOR                    MAJOR</b>				Total Inlet Interception Capacity	Q =	1.0	5.0	cfs	Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.0	cfs	Capture Percentage = Q <sub>b</sub> /Q <sub>a</sub>	C% =	100	100	%
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## AREA INLET IN A SWALE

Claremont Business Park 2 Filing 2 (Proposed Conditions)  
Inlet 7 (DP18)

This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

## Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

A, B, C, D, or E =	<input type="text"/>
n =	<input type="text"/> 0.025
$S_0$ =	<input type="text"/> 0.1200 ft/ft
B =	<input type="text"/> 0.00 ft
$Z_1$ =	<input type="text"/> 3.00 ft/ft
$Z_2$ =	<input type="text"/> 3.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity ( $V_{MAX}$ )	Max Froude No. ( $F_{MAX}$ )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Choose One:

 Non-Cohesive  
 Cohesive  
 Paved

Minor Storm	Major Storm
$T_{MAX} =$ <input type="text"/> 1.92	<input type="text"/> 2.40
$d_{MAX} =$ <input type="text"/> 0.32	<input type="text"/> 0.40

## Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

Minor Storm	Major Storm
$Q_{allow} =$ <input type="text"/> 1.8	<input type="text"/> 3.3 cfs
$d_{allow} =$ <input type="text"/> 0.32	<input type="text"/> 0.40 ft

## Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

$Q_o =$	0.7	1.3	cfs
$d =$	0.22	0.28	ft

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'****Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

**AREA INLET IN A SWALE****Claremont Business Park 2 Filing 2 (Proposed Conditions)**  
**Inlet 7 (DP18)**

Inlet Design Information (Input)																
Type of Inlet	CDOT Type C (Depressed)															
Inlet Type	CDOT Type C (Depressed)															
Angle of Inclined Grate (must be <= 30 degrees)																
Width of Grate	W = 3.00 ft															
Length of Grate	L = 3.00 ft															
Open Area Ratio	A <sub>RATIO</sub> = 0.70															
Height of Inclined Grate	H <sub>B</sub> = 0.00 ft															
Clogging Factor	C <sub>f</sub> = 0.50															
Grate Discharge Coefficient	C <sub>d</sub> = 0.84															
Orifice Coefficient	C <sub>o</sub> = 0.56															
Weir Coefficient	C <sub>w</sub> = 1.81															
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)																
Total Inlet Interception Capacity (assumes clogged condition)																
Bypassed Flow																
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub>																
<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>d =</td> <td>1.22</td> <td>1.28</td> </tr> <tr> <td>Q<sub>a</sub> =</td> <td>15.7</td> <td>16.1</td> </tr> <tr> <td>Q<sub>b</sub> =</td> <td>0.0</td> <td>0.0</td> </tr> <tr> <td>C% =</td> <td>100</td> <td>100</td> </tr> </tbody> </table>			MINOR	MAJOR	d =	1.22	1.28	Q <sub>a</sub> =	15.7	16.1	Q <sub>b</sub> =	0.0	0.0	C% =	100	100
	MINOR	MAJOR														
d =	1.22	1.28														
Q <sub>a</sub> =	15.7	16.1														
Q <sub>b</sub> =	0.0	0.0														
C% =	100	100														

**Warning 04: Froude No. exceeds USDCM Volume I recommendation.**



CIVIL CONSULTANTS, INC.

2-11-23

212 N. Wahsatch Ave., Ste. 305  
Colorado Springs, CO  
719.955.5485

Project: Claremont Business Park 2 Phase 2  
Date: Right of Way Curb

Proposed 18" RCP (Future Dev. Lot)

$$n = 0.013 \quad D = 1.5'$$

$$S = 0.01 \text{ (Assumed)} \quad Q_{100} = 6.0 \text{ cfs} \quad \text{Basins C & D}$$

$$TW = m \cdot n = 0.4 \times 1.5 = 0.6$$

Flow is supercritical (Flowmeter)  $U_0 = 0.808$   
 $U_0 = 6.14$

$$D' = \frac{D + y_0}{2}$$

$$D' = (1.5 + 0.81)/2 = 1.16$$

$$D_{50} = 0.2 (1.16) \left( \frac{6.0}{\sqrt{32.2} \cdot (1.16)^{25}} \right)^{1/3} \left( \frac{1.16}{0.6} \right) = .009 < 1"$$

$$\text{Use } D_{50} = 9" \quad \text{Depth} = 2.0 \times D_{50} = 18"$$

$$L = 4.0 \times 1.5 = 6.0$$

$$\begin{aligned} \text{End width} &= 3.0 \times 0 + \frac{2}{3} L \\ &= 3.0 \times 1.5 + \frac{2}{3} (6.0) \end{aligned}$$

$$4.5 + 4 = 8.5$$



212 N. Wahsatch Ave., Ste. 305  
Colorado Springs, CO  
719.955.5485

Project: Currington Business Park 2 Phase 2  
Date: R. prop. Aron Ctr.

2-12-22

Prop 18" RCP

$$n = 0.013 \quad D = 1.5'$$

$$S = 0.005 \quad Q_{100} = 3.9 \text{ cfs}$$

$$Tw = \text{max} = 0.4 \quad D = 0.4(1.5) = 0.6$$

Flow is supercritical  $y_0 = 9.3'' = 0.775$   
 $W_0 = 4.25$

$$D' = \frac{(D + y_0)}{2}$$

$$D' = (1.5 + .78)/2 = 1.14'$$

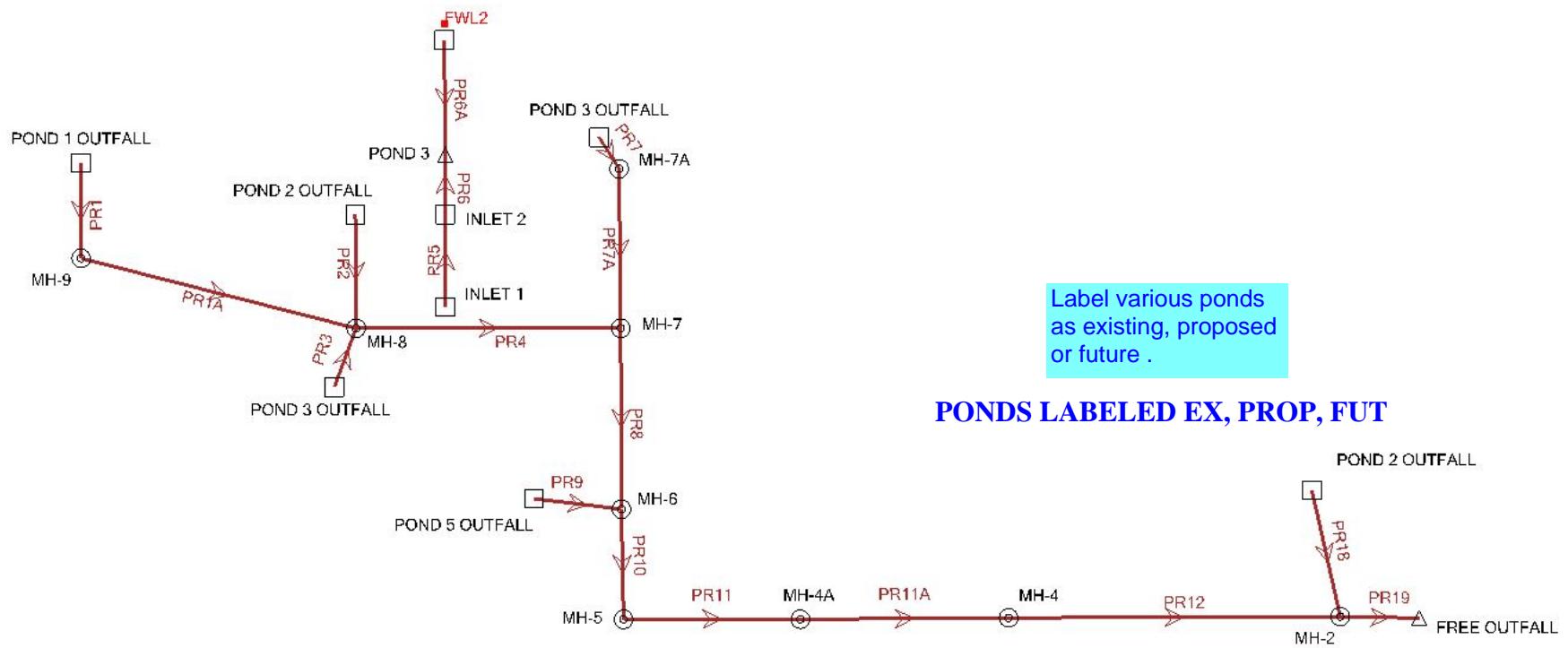
$$D_{50} = 0.2(1.14) \left( \frac{3.9}{\sqrt{132.2 \cdot (1.14)^{2.5}}} \right)^{4/3} / 0.6 = 0.005 \approx 1''$$

$$\text{Use } D_{50} = 9'' \quad \text{Depth} = 2.0 \times D_{50} = 1.5'$$

$$L = 4.0 \times D = 6.0'$$

$$End Water = 3.0 + D + 2/3 L$$

$$= 8.5'$$



**STORM CAD INFORMATION  
PRINTED ON ONE SHEET**

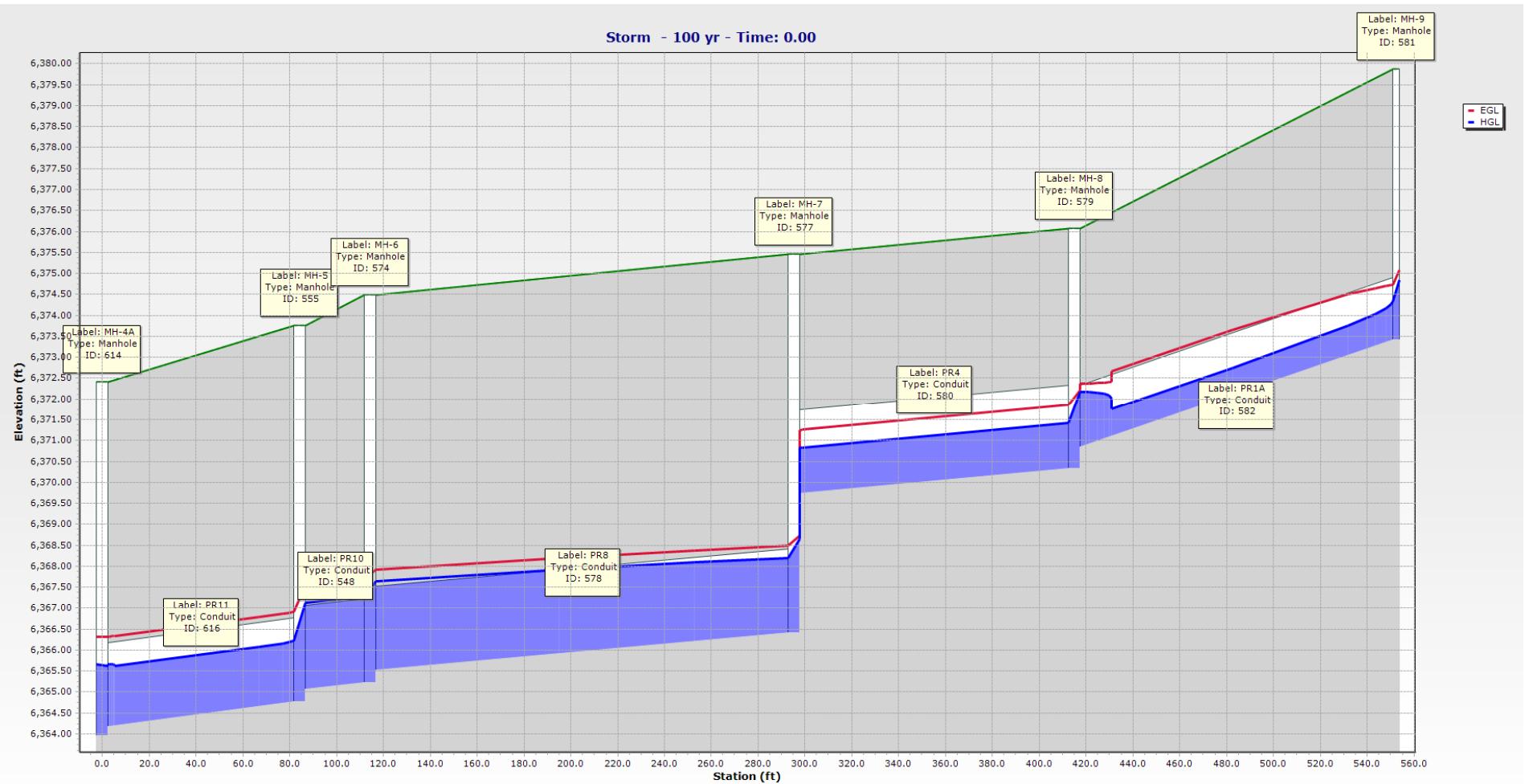
Try to print all of stormcad table on one sheet, or include "Label" column with second sheet

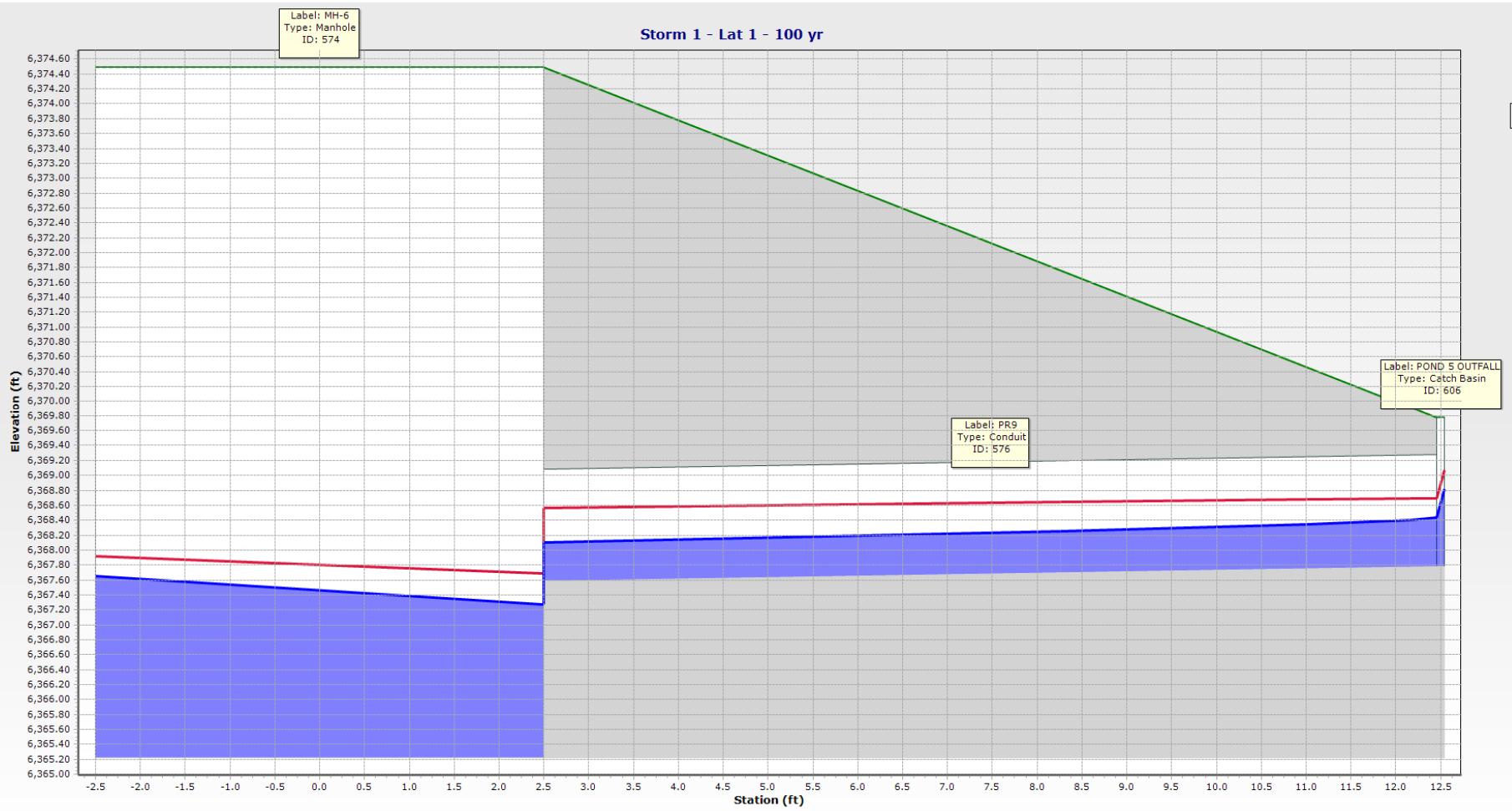
**Conduit FlexTable: STRM 1,2,3 - 100YR**

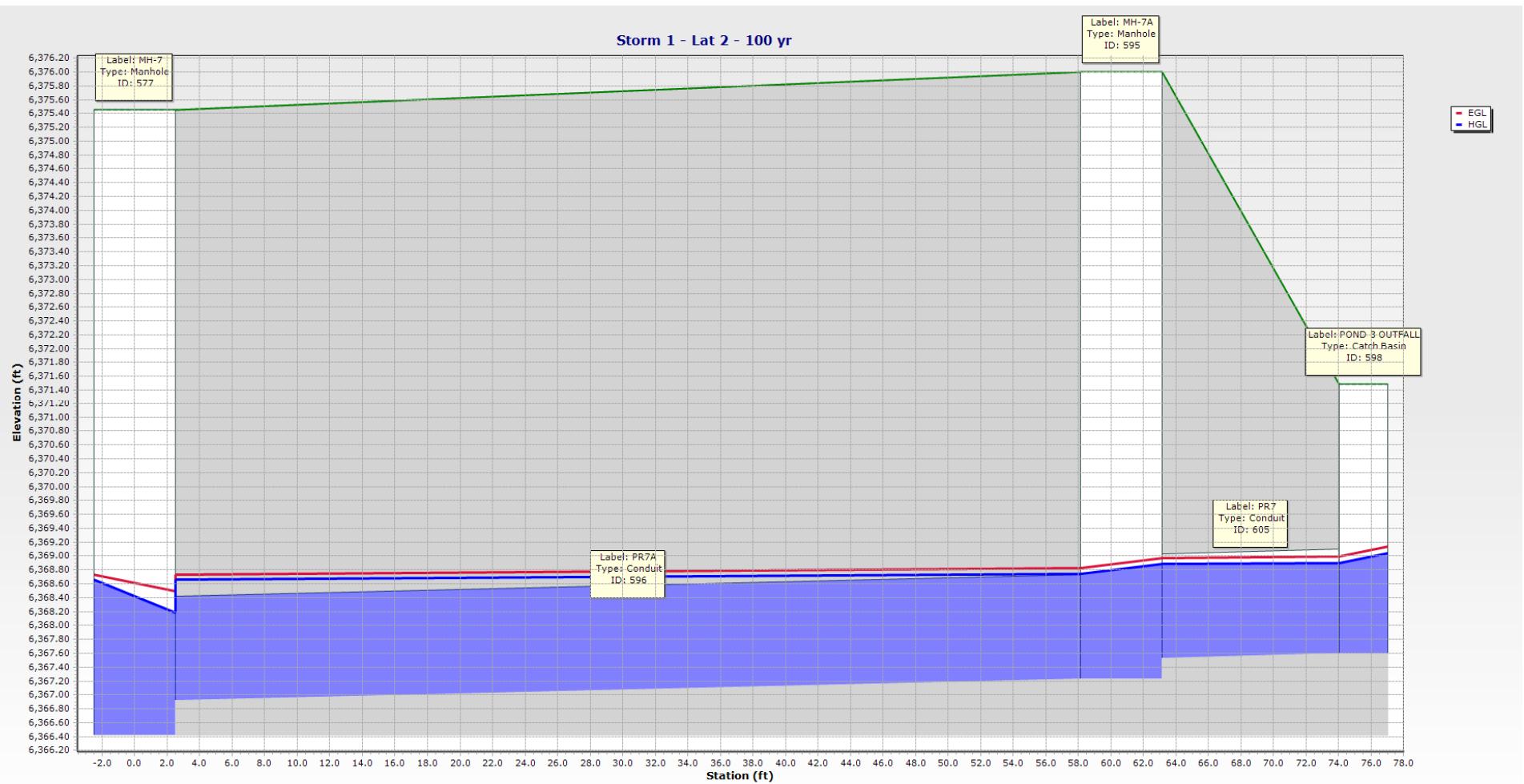
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	
PR1	601	POND 1 OUTFALL	5.70	76.9	57.1	
PR1A	582	MH-9	5.70	39.7	137 ?	
PR2	603	POND 2 OUTFALL	2.40	32.5	56	
PR3	613	POND 3 OUTFALL	1.00	13.1	11	
PR4	580	MH-8	9.10	56.8	119.5	
PR5	604	INLET 1	1.70	22.7	37.3	
PR6	608	INLET 2	3.90	38.3	20.2	
PR6A	631	FWL2	5.10	44.4	30.1	
PR7	605	POND 3 OUTFALL	4.00	55.5	14.9	
PR7A	596	MH-7A	4.00	53.3	60.6	
PR8	578	MH-7	13.10	82.1	181.1	
PR9	576	POND 5 OUTFALL	3.00	22.6	12.5	Length does not match CD's
PR10	548	MH-6	16.20	101.3	30.0	LENGTHS REVISED
PR11	616	MH-5	16.20	85.6	84.3	
PR11A	615	MH-4A	16.20	39.1	115.8	
PR12	568	MH-4	16.20	88.5	239.6	
PR18	570	POND 2 OUTFALL	23.80	23.0	39.7	
PR19	567	MH-2	40.00	36.2	23.2	
Velocity (ft/s)	Froude Number	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	
4.63	(N/A)	0.99	0.92	6,375.32	6,375.09	
7.66	(N/A)	0.66	0.92	6,374.72	6,372.36	
3.74	(N/A)	0.59	0.59	6,372.25	6,372.21	
2.98	(N/A)	0.37	0.37	6,372.19	6,372.19	
5.26	(N/A)	1.08	1.08	6,371.85	6,371.25	
3.43	(N/A)	0.49	0.49	6,372.28	6,372.27	
2.21	(N/A)	0.64	0.76	6,372.24	6,372.22	
2.89	(N/A)	0.70	0.87	6,372.34	6,372.27	
4.18	(N/A)	0.80	0.77	6,368.99	6,368.97	
2.26	(N/A)	0.78	0.77	6,368.83	6,368.74	
5.67	(N/A)	1.38	1.30	6,368.50	6,367.92	
6.07	(N/A)	0.48	0.66	6,368.69	6,368.57	
5.16	(N/A)	1.66	1.45	6,367.69	6,367.54	
6.77	(N/A)	1.42	1.45	6,366.91	6,366.32	
12.37	(N/A)	0.87	1.45	6,366.32	6,363.52	
6.58	(N/A)	1.46	1.45	6,362.21	6,360.64	
17.12	(N/A)	0.82	1.66	6,362.92	6,360.41	
10.56	(N/A)	1.46	1.97	6,359.77	6,359.62	

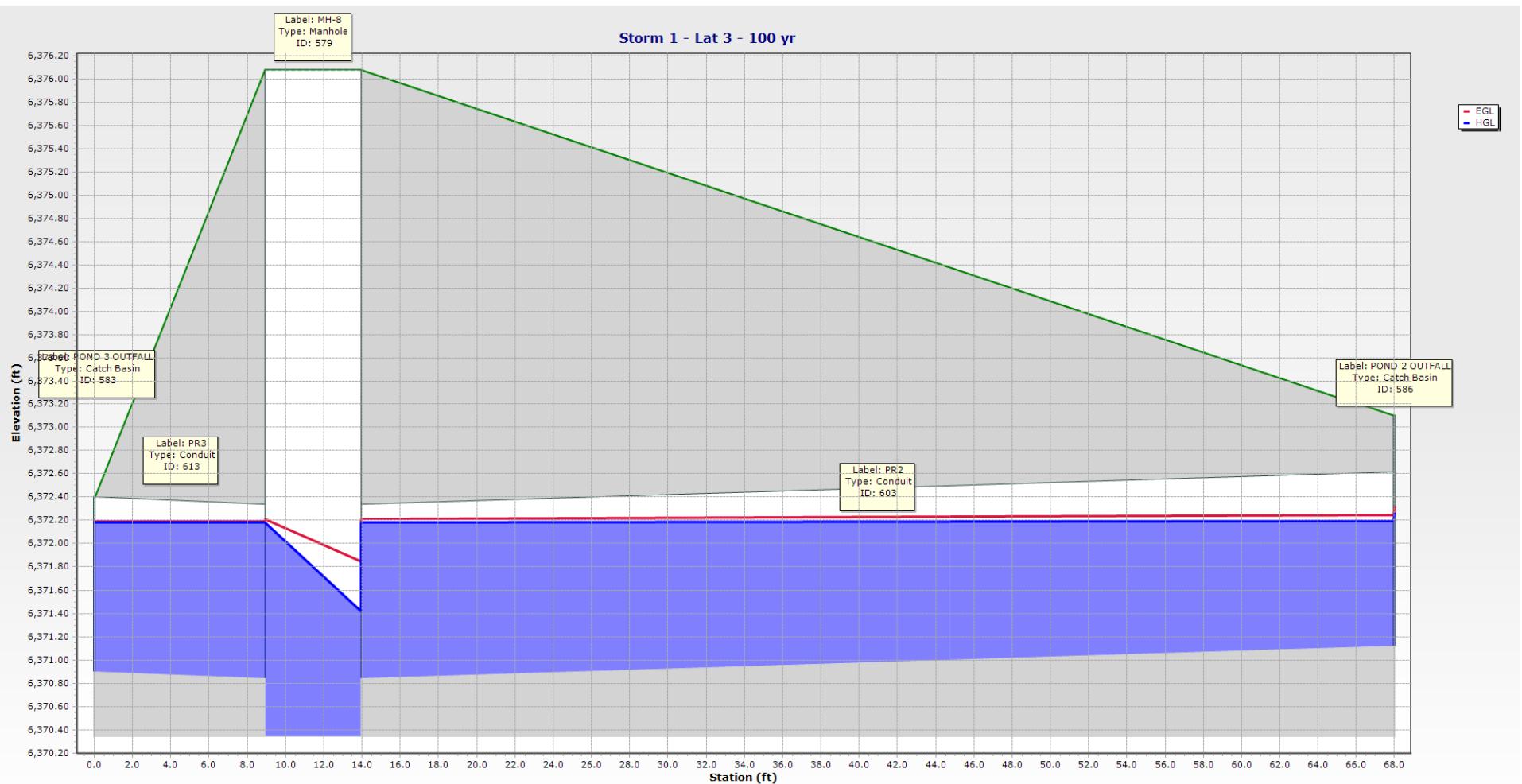
## Conduit FlexTable: STRM 1,2,3 - 100YR

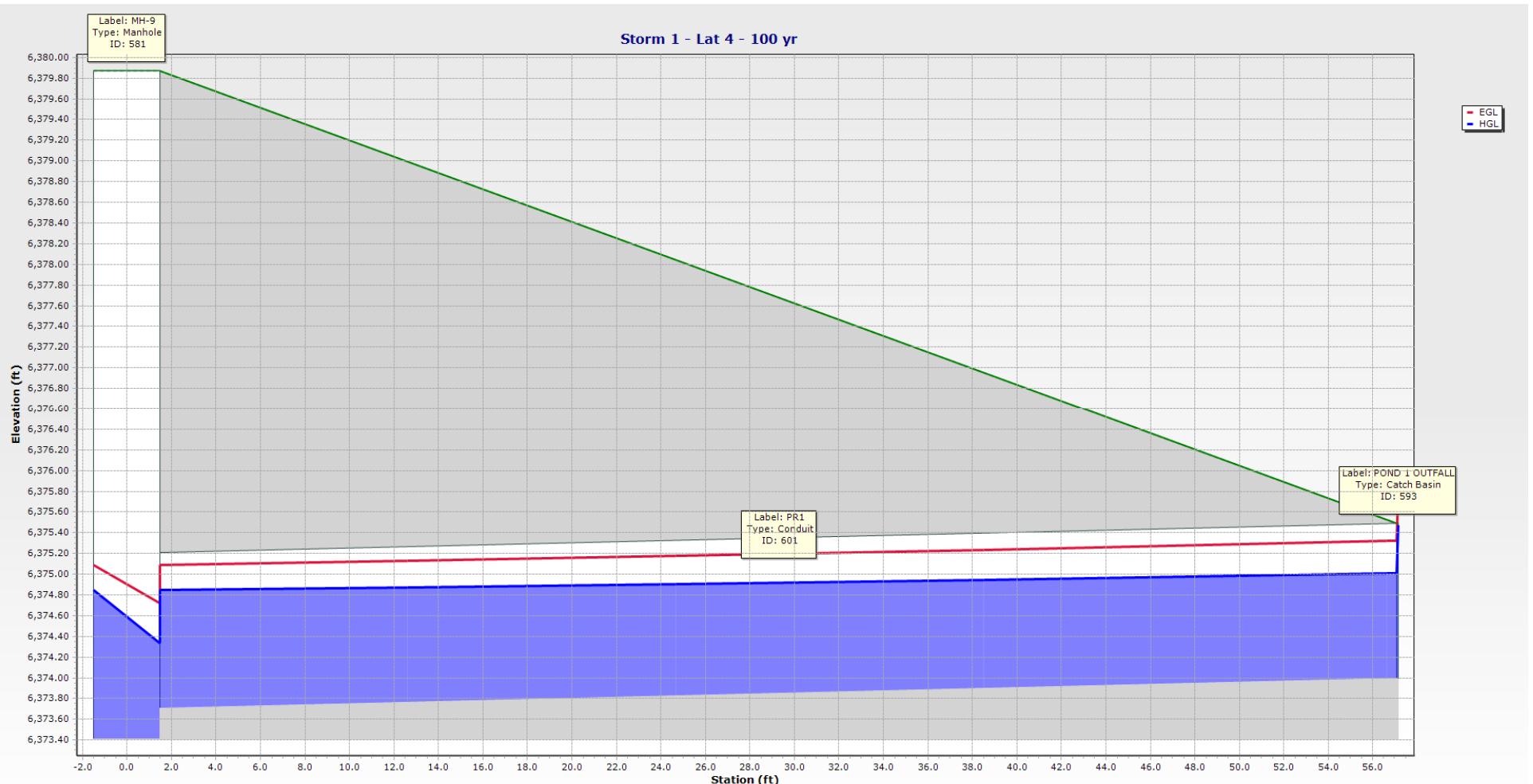
Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In-Governing) (ft/s)	Upstream Structure Headloss Coefficient
6,375.01	6,374.85	0.16	6,375.48	4.48	1.500
6,374.33	6,372.18	2.15	6,374.85	3.97	1.320
6,372.20	6,372.18	0.02	6,372.27	1.77	1.500
6,372.18	6,372.18	0.00	6,372.19	0.62	1.500
6,371.42	6,370.82	0.60	6,372.18	1.44	1.770
6,372.26	6,372.25	0.01	6,372.28	1.10	1.500
6,372.17	6,372.14	0.03	6,372.25	0.99	1.100
6,372.21	6,372.14	0.07	6,372.40	2.89	1.500
6,368.90	6,368.89	0.01	6,369.04	2.46	1.500
6,368.75	6,368.66	0.09	6,368.89	2.38	1.770
6,368.19	6,367.65	0.54	6,368.66	2.26	1.520
6,368.44	6,368.10	0.34	6,368.81	4.02	1.500
6,367.28	6,367.12	0.15	6,367.65	4.17	0.900
6,366.22	6,365.67	0.56	6,367.12	5.16	1.320
6,365.63	6,361.17	4.46	6,365.67	6.47	0.050
6,361.53	6,359.95	1.58	6,361.57	12.30	0.050
6,362.19	6,359.79	2.41	6,363.29	6.87	1.500
6,358.97	6,358.37	0.60	6,359.79	6.35	1.020
Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description
0.47	6,375.49	6,379.87	6,373.99	6,373.71	Circle - 18.0 in
0.51	6,379.87	6,376.08	6,373.41	6,370.84	Circle - 18.0 in
0.07	6,373.10	6,376.08	6,371.12	6,370.84	Circle - 18.0 in
0.01	6,376.08	6,372.40	6,370.84	6,370.90	Circle - 18.0 in
0.76	6,376.08	6,375.45	6,370.34	6,369.74	Circle - 24.0 in
0.03	6,375.11	6,375.11	6,371.03	6,370.84	Circle - 18.0 in
0.08	6,375.11	6,370.35	6,370.54	6,370.35	Circle - 18.0 in
0.19	6,370.35	6,372.21	6,370.35	6,370.71	Circle - 18.0 in
0.14	6,371.49	6,376.00	6,367.60	6,367.53	Circle - 18.0 in
0.14	6,376.00	6,375.45	6,367.23	6,366.92	Circle - 18.0 in
0.47	6,375.45	6,374.49	6,366.42	6,365.52	Circle - 24.0 in
0.38	6,369.78	6,374.49	6,367.78	6,367.58	Circle - 18.0 in
0.37	6,373.76	6,374.49	6,365.07	6,365.22	Circle - 24.0 in
0.90	6,372.41	6,373.76	6,364.18	6,364.77	Circle - 24.0 in
0.03	6,370.58	6,372.41	6,360.30	6,364.18	Circle - 24.0 in
0.03	6,367.74	6,370.58	6,358.50	6,360.07	Circle - 24.0 in
1.10	6,366.20	6,367.74	6,360.53	6,358.00	Circle - 30.0 in
0.82	6,367.70	6,367.74	6,356.72	6,357.00	Circle - 42.0 in

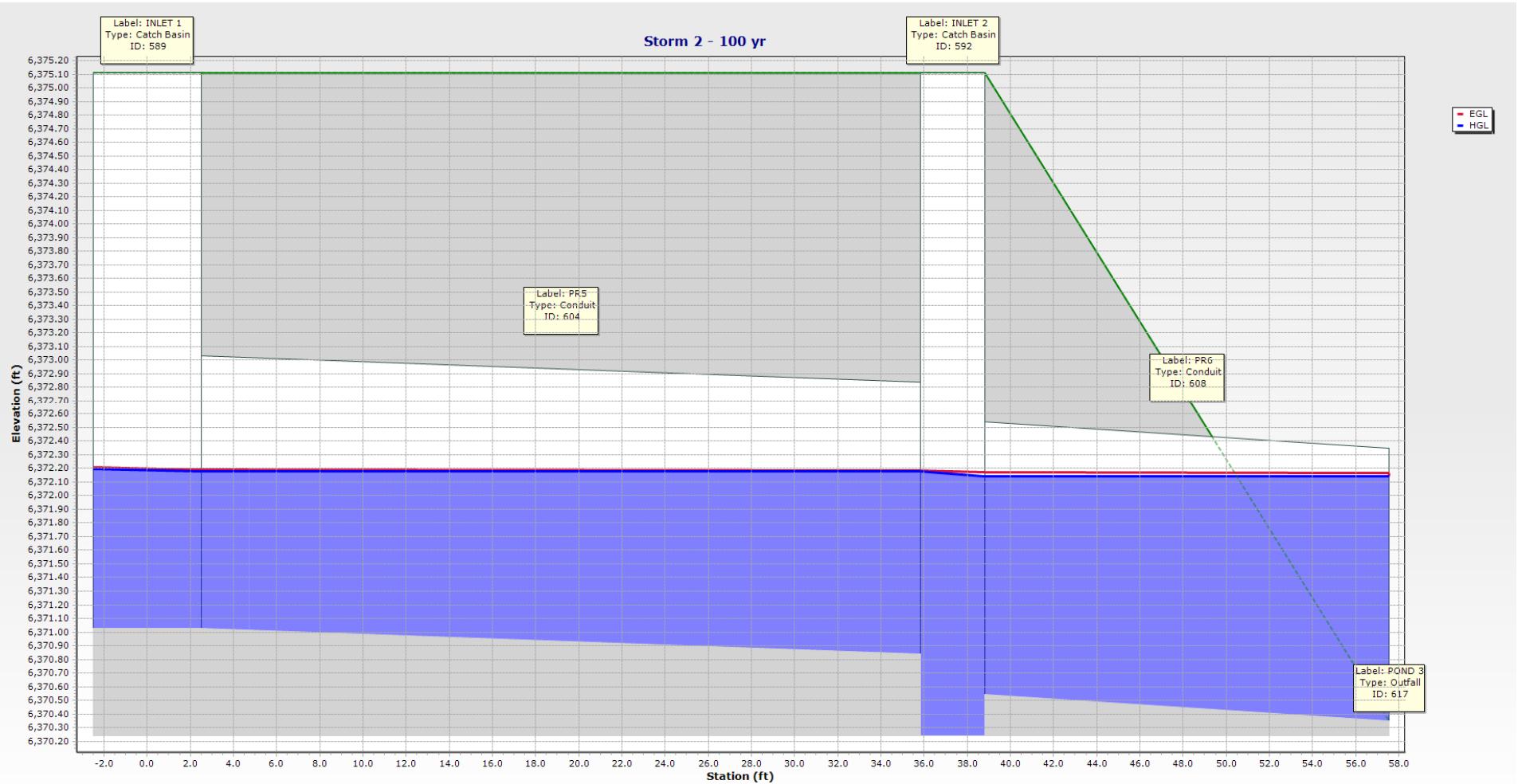












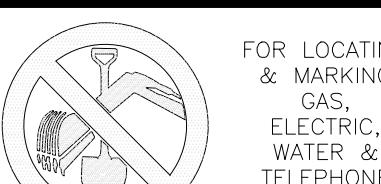
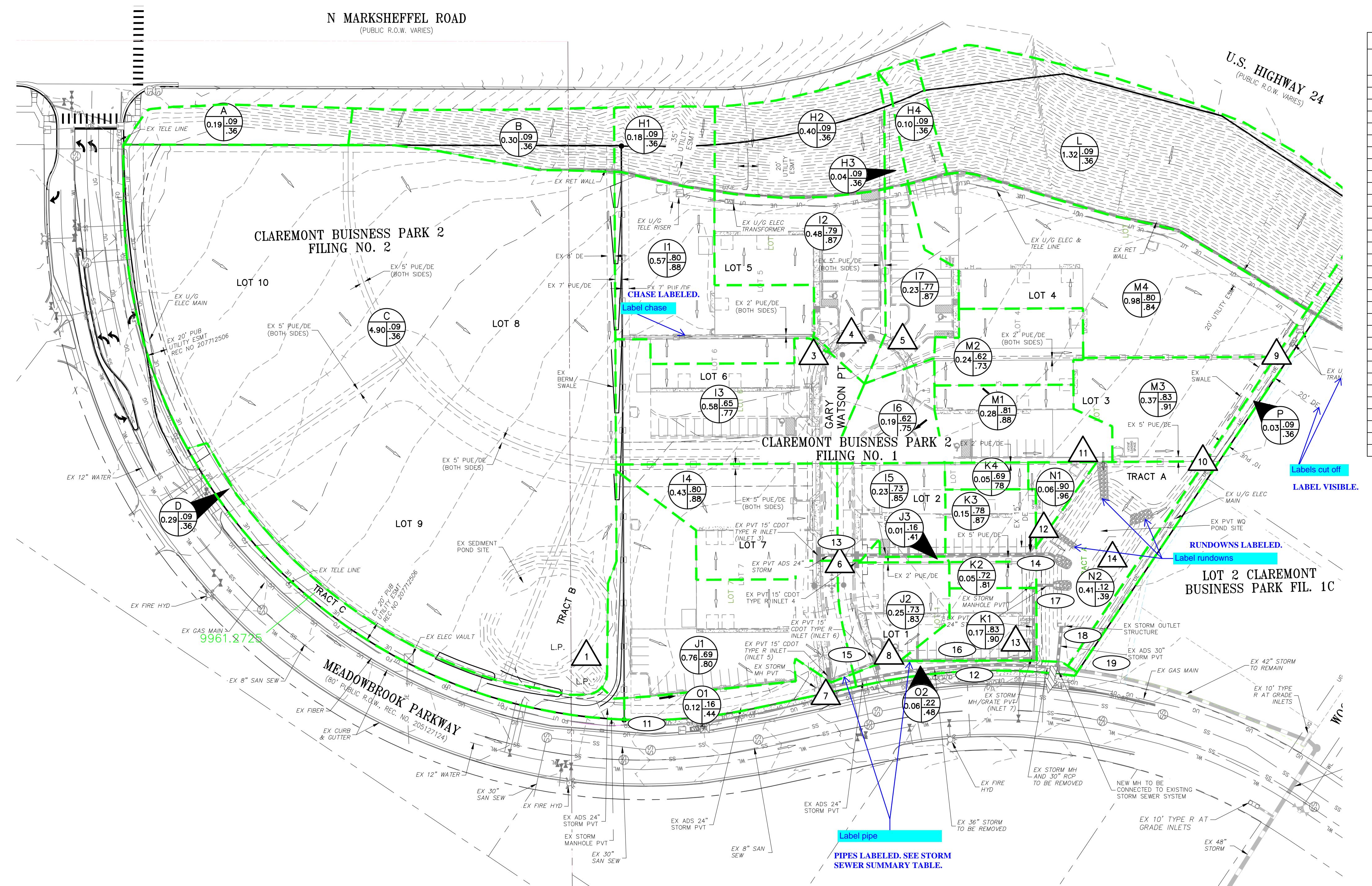
### Storm 3 - 100 yr



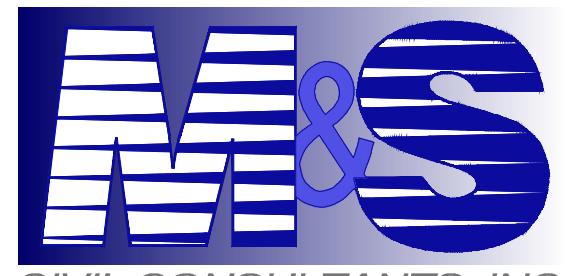
## **EXISTING DRAINAGE MAP**

**FINAL DRAINAGE REPORT FOR  
CLAREMONT BUSINESS PARK 2 FILING NO.2  
COUNTY OF EL PASO, STATE OF COLORADO  
EXISTING CONDITIONS DRAINAGE MAP**

# FEBRUARY 2023



FOR LOCATING  
& MARKING  
GAS,  
ELECTRIC,  
WATER &  
TELEPHONE  
LINES



The logo consists of the letters 'M' and 'S' in a stylized font. The 'M' is on the left, composed of several vertical bars of varying heights, creating a striped effect. The 'S' is on the right, also with vertical bars, and it features a small white bird perched on its top bar. A blue ampersand symbol (&) is positioned between the two letters.

CLAREMONT BUSINESS PARK 2 FLOOR NO.2

## EXISTING CONDITIONS DRAINAGE MAP

OBJECT NO. 10-022A FILE: \dwg\Eng Exhibits\10020 EDM.dwg

SIGNED BY:	DLM	SCALE	DATE: 02-23-2023
AWM, BY:	DLM	"	

AWN BY: DLM HORIZ: 1'-60' SHEET 1 OF 1  
ECKED BY: VAS VERT: N/A EDM01

$$1'' = 60'$$


Scale in Feet

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q <sub>5</sub>	Q <sub>100</sub>
A	0.19	0.1	0.6
B	0.30	0.1	1.0
C	4.90	1.6	10.7
D	0.23	0.1	0.7
H1	0.18	0.1	0.5
H2	0.40	0.2	1.1
H3	0.04	0.0	0.1
H4	0.10	0.0	0.3
I1	0.57	2.4	4.4
I2	0.48	2.0	3.6
I3	0.58	1.8	3.6
I4	0.43	1.8	3.3
I5	0.23	0.9	1.7
I6	0.19	0.6	1.2
I7	0.23	0.9	1.6
J1	0.76	2.4	4.7
J2	0.25	1.0	1.8
J3	0.01	0.0	0.1
K1	0.17	0.7	1.3
K2	0.05	0.2	0.4
K3	0.15	0.6	1.1
K4	0.06	0.2	0.4
L	1.32	0.5	3.7
M1	0.28	1.2	2.2
M2	0.24	0.8	1.5
M3	0.37	1.6	2.9
M4	0.98	3.5	6.6
N1	0.06	0.3	0.5
N2	0.41	0.2	1.1
O1	0.12	0.1	0.4
O2	0.06	0.1	0.3
P	0.11	0.0	0.3

DESIGN POINT SUMMARY				
DESIGN POINT	Q <sub>5</sub>	Q <sub>100</sub>	BASIN	STRUCTURE
1	1.8	11.8	A, B, C	24" PP
2		NOT	USED	
3	2.2	4.4	H1, I1	EX STREET
4	1.8	4.1	H2, I2	EX STREET
5	0.8	1.6	H3, I7	EX STREET
6	8.2	16.5	DP3-5, I3-I6	EX 15' INLETS
7	2.4	7.5	FB INLET3, J1	EX 15' INLET
8	0.9	4.1	FB INLET4, J2, J3	EX 15' INLET
9	3.8	9.7	H3, L, M4	EX SWALE
10	5.3	12.3	DP9, M2, M3	EX SWALE/RD
11	1.4	2.5	M1, K4	EX CONC. RD
12	1.1	2.0	K2, K3, N1	EX CONC. RD
13	0.7	1.3	K1	EX AREA INLET
14	19.3	43.9	DP10-13, N2, DP14, DP17	EX FSD POND

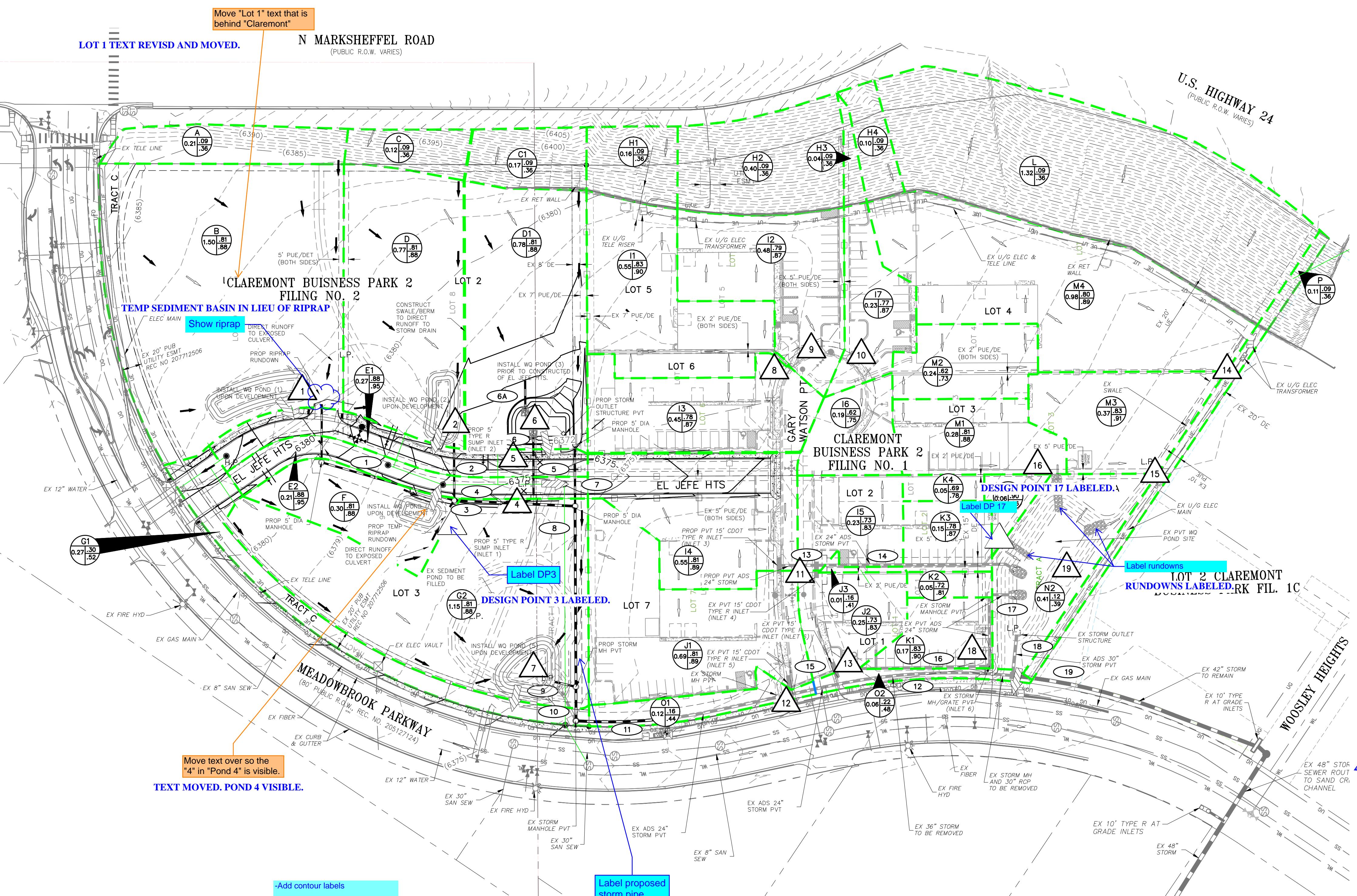
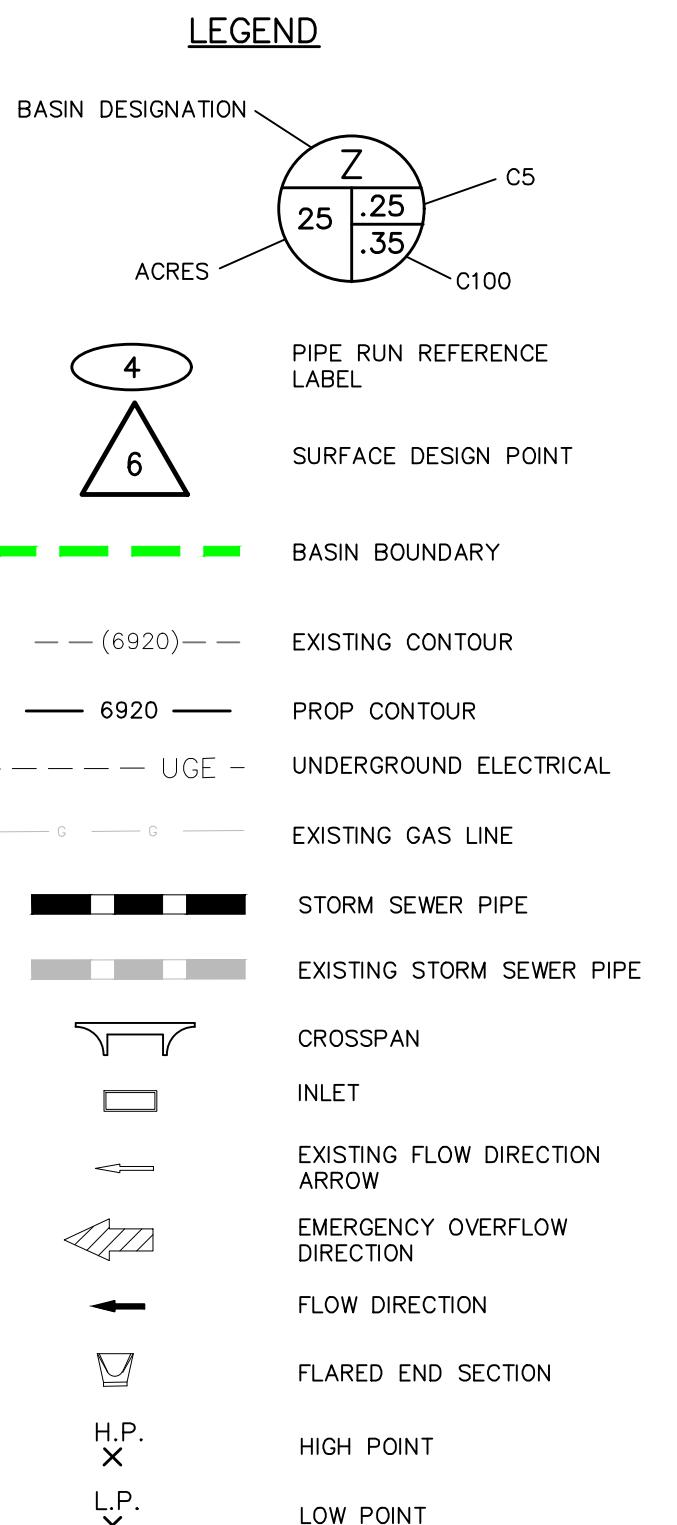
STORM SEWER SUMMARY				
PIPE RUN	Q <sub>5</sub>	Q <sub>100</sub>	PIPE SIZE	CONTRIBUTING DP/BASIN/PIPES
11	1.8	11.8	EX 24"	DP1
12	1.8	11.8	EX 24"	PR11
13	4.1	7.9	EX 15"	INLET 3
14	8.2	15.9	EX 24"	PR13, INLET 4
15	2.4	7.3	EX 18"	INLET 5
16	3.2	11.0	EX 24"	PR15, INLET 6
17	3.9	12.1	EX 24"	PR16, DP13
18	13.7	23.9	EX 30"	POND 2 OUTFALL

## PROPOSED DRAINAGE MAP

# FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO.1

COUNTY OF EL PASO, STATE OF COLORADO  
PROPOSED CONDITIONS DRAINAGE MAP

FEBRUARY 2023



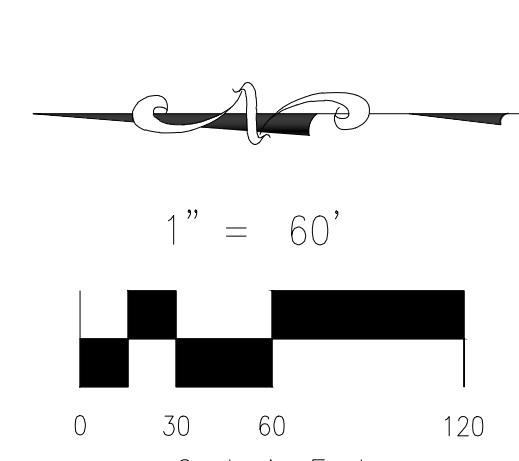
BASIN SUMMARY			
BASIN	AREA (ACRES)	$Q_5$	$Q_{100}$
A	0.21	0.1	0.7
B	1.50	6.0	10.9
C	0.12	0.1	0.4
C1	0.17	0.1	0.5
D	0.77	3.2	5.9
D1	0.78	3.3	6.0
E1	0.27	1.2	2.2
E2	0.21	1.0	1.7
F	0.30	1.2	2.3
G1	0.27	0.4	1.2
G2	1.15	4.3	7.8
H1	0.16	0.1	0.5
H2	0.40	0.2	1.1
H3	0.04	0.0	0.1
H4	0.10	0.0	0.3
I1	0.55	2.3	4.3
I2	0.48	2.0	3.6
I3	0.45	1.8	3.3
I4	0.55	2.3	4.2
I5	0.23	0.9	1.7
I6	0.19	0.6	1.2
I7	0.23	0.9	1.6
J1	0.69	2.7	5.1
J2	0.25	1.0	1.8
J3	0.01	0.0	0.1
K1	0.17	0.7	1.3
K2	0.05	0.2	0.4
K3	0.15	0.6	1.1
K4	0.05	0.2	0.4
L	1.32	0.5	3.7
M1	0.28	1.2	2.2
M2	0.24	0.8	1.5
M3	0.37	1.6	2.9
M4	0.98	3.5	6.6
N1	0.06	0.3	0.5
N2	0.41	0.2	1.1
O1	0.12	0.1	0.4
O2	0.06	0.1	0.3
P	0.11	0.0	0.3

DESIGN POINT SUMMARY			
DESIGN POINT	$Q_5$	$Q_{100}$	BASIN STRUCTURE
1	5.9	11.2	A, B 18" PP
2	3.0	5.8	C, D 18" PP
3	1.2	2.3	F 18" PP
4	1.0	1.7	E2 PROP 5' INLET
5	1.2	2.2	E1 PROP 5' INLET
6	5.1	9.6	C1, D1, PR6 24" PP
7	4.7	8.7	G2 EX STREET
8	2.2	4.3	H1, H2 EX STREET
9	1.8	4.1	H2, I2 EX STREET
10	0.8	1.6	H3, I7 EX STREET
11	8.4	16.7	DP3-5, I3-16 EX 15' INLETS
12	2.8	8.1	FB INLET3, J1 EX 15' INLET
13	1.0	5.0	FB INLET4, J2, J3 EX 15' INLET
14	3.8	9.7	H4, L, M4 EX SWALE
15	5.3	12.3	DP2, M2, M3 EX SWALE/RD
16	1.4	2.5	M1, K4 EX CONC. RD
17	1.1	2.0	K2, K3, N1 EX CONC. RD
18	0.7	1.3	K1 EX AREA INLET
19	19.8	44.7	DP10-13, N2, PR14, PR17 EX FSD POND 2

REVISED TO DP 15-17 MMARY			
PIPE RUN	$Q_5$	$Q_{100}$	PIPE SIZE CONTRIBUTING DP/BASIN/PIPES
1	2.4	5.7	18" FUT POND 1 OUTFALL
2	1.0	2.4	18" FUT POND 2 OUTFALL
3	0.4	1.0	18" FUT POND 4 OUTFALL
4	3.9	9.1	24" PR1-PR3
5	1.0	1.7	18" DP4
6	2.2	3.9	18" PR5, DP5
6A	2.9	5.1	18" C1, 90% D1
7	1.9	4.0	18" POND 3 OUTFALL
8	5.9	13.1	24" PR4, PR7
9	1.3	3.0	18" FUT POND 5 OUTFALL
10	7.1	16.2	24"/EX24" PR8, PR9
11	7.1	16.2	EX 24" PR10
12	4.2	8.0	EX 15" INLET 3
13	8.4	16.0	EX 24" PR13, INLET 4
14	2.8	7.8	EX 18" INLET 5
15	3.7	12.6	EX 24" PR15, INLET 6
16	4.4	13.8	EX 24" PR16, DP18
17	13.7	23.8	EX 30" DP17
18	20.8	40.0	EX 42" DP18, PR12

SF WQCV FUTURE PONDS SUMMARY			
PIPE RUN	$Q_5$	$Q_{100}$	PIPE SIZE
1	2.4	5.7	18" FUT POND 1 OUTFALL
2	1.0	2.4	18" FUT POND 2 OUTFALL
3	0.4	1.0	18" FUT POND 4 OUTFALL
4	3.9	9.1	24" PR1-PR3
5	1.0	1.7	18" DP4
6	2.2	3.9	18" PR5, DP5
6A	2.9	5.1	18" C1, 90% D1
7	1.9	4.0	18" POND 3 OUTFALL
8	5.9	13.1	24" PR4, PR7
9	1.3	3.0	18" FUT POND 5 OUTFALL
10	7.1	16.2	24"/EX24" PR8, PR9
11	7.1	16.2	EX 24" PR10
12	4.2	8.0	EX 15" INLET 3
13	8.4	16.0	EX 24" PR13, INLET 4
14	2.8	7.8	EX 18" INLET 5
15	3.7	12.6	EX 24" PR15, INLET 6
16	4.4	13.8	EX 24" PR16, DP18
17	13.7	23.8	EX 30" DP17
18	20.8	40.0	EX 42" DP18, PR12

SF WQCV POND 3 SUMMARY			
PIPE RUN	$Q_5$	$Q_{100}$	PIPE SIZE
1	0.06	0.48	18" EPC/URBAN DRAINAGE SAND FILTER BASIN-SEE STD. DET.
2	0.06	0.48	18" EPC/URBAN DRAINAGE SAND FILTER BASIN-SEE STD. DET.



**EXCERPT OF "FINAL DRAINAGE REPORT FOR CLAREMONT  
BUSINESS PARK FIL NO. 2 ", BY MATRIX DESIGN DATED  
NOVEMBER 2006  
&  
EXISTING DRAINAGE MAP**



**FINAL DRAINAGE REPORT  
For  
“Claremont Business Park Filing No. 2”**

Prepared for:  
**El Paso County**  
**Department of Public Works**  
**Engineering Division**

On Behalf of:  
**Claremont Development, Inc.**

Prepared by:



2435 Research Parkway, Suite 300  
Colorado Springs, CO 80920  
(719) 575-0100  
fax (719) 572-0208

Revised November 2006

**Engineer's Statement:**

The *revisions* (changes made to the base Final Drainage Report since July, 2006) to the attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. The revisions encompassed adding additional right of way to the study area at the County's request, the handling of offsite drainage due to the additional right of way, a breakdown of private drainage within lot numbers 10 through 25 of Filing No. 2 due to cross-lot drainage (contrary to note # 25 on the recorded plat), profiling additional inlets along the channel edge, and rip-rap sizing for outlet structures along the channel. The Final Drainage Report dated July, 2006 was prepared under the direct supervision of Richard G. Gallegos, Jr. in July, 2006 and stamped (see next sheet).

The Final Drainage Report was prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing the *revisions* to this report.

SEAL

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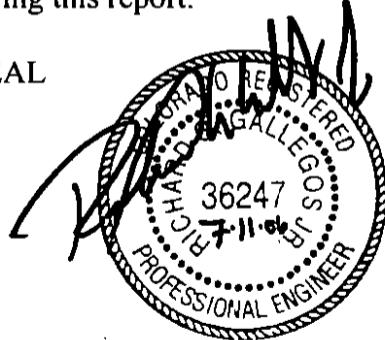
Brady A. Shyrock  
Registered Professional Engineer  
State of Colorado  
No. 38164



**Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SEAL



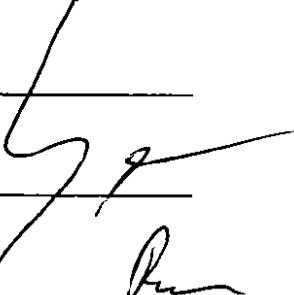
Richard G. Gallegos, Jr.  
Registered Professional Engineer  
State of Colorado  
No. 36247

**Developer's Statement:**

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Claremont Development, Inc.

Business Name

By: 

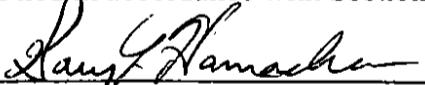
Title: 

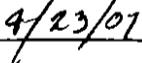
Address: 3460 Capital Drive

Colorado Springs, CO 80915

**El Paso County:**

Filed in accordance with Section 51.1 of the El Paso Land Development Code, as amended.

 Fox Mr. John McCarty, County Engineer/Director

 Date 4/23/07

Conditions:

#### **D. Drainage and Bridge Fees**

Claremont Business Park Filing No. 2 has not been previously platted. The drainage basin and bridge fees have been determined per the El Paso County Drainage Basin Fees Sheet, dated February 3, 2006, Resolution No. 06-31. The site is located entirely within the Sand Creek Drainage Basin. The fees are based upon the percent impervious of the development, which have been included within the appendix of this report. The fees due have been calculated as follows.

#### **Claremont Business Park Filing No. 2**

#### Final Drainage Report Drainage and Bridge Fees

	Area (ac.)	Fee/Imp. Acre	% Imp.	Fee Due	Reimbursable Const. Costs	Fee Credit	Fee Due at Platting	Fee Credit Remaining
Drainage Fee	62.967	\$15,000.00	80%	\$755,604.00	\$0.00	\$1,225,355.45	\$0.00	\$469,751.45
Bridge Fee	62.967	\$1,503.00	80%	\$75,711.52	\$75,711.52	\$0.00	\$0.00	\$0.00
<i>Total Fee Due at Platting</i>								<b>\$0.00</b>

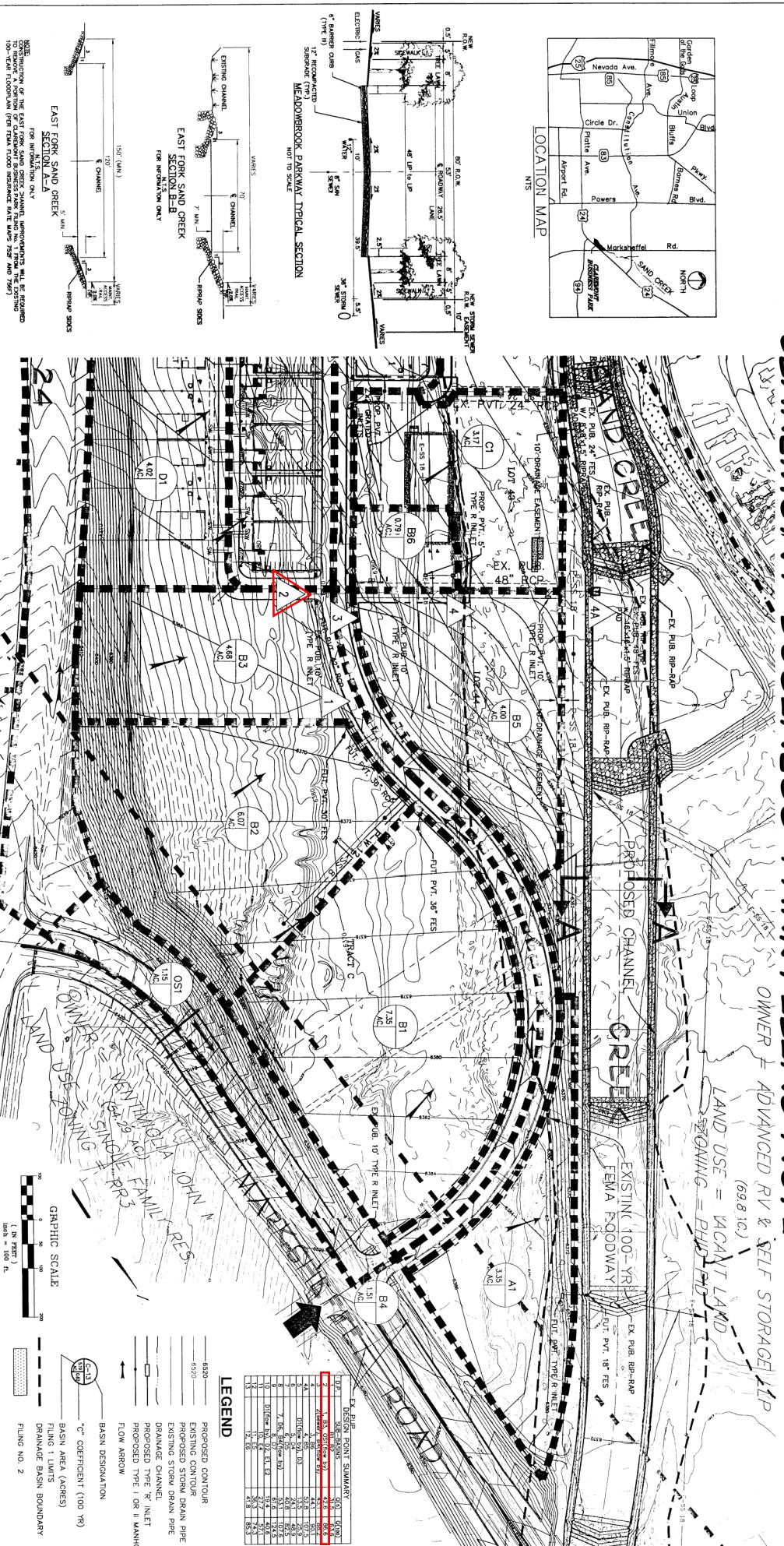
The developer of Claremont Business Park is completing the construction of the channel improvements on behalf of the Central Marksheffel Metropolitan District. The construction costs for both Filing 1 and Filing 2 combined exceed the drainage fees due for the site. No drainage fees will be required at the time of platting.

It should be noted that the Central Marksheffel Business District is reimbursing the developer of Claremont Business Park Filing 2 for the construction costs of the channel minus the drainage fees due for the site. The District has \$1,225,355.45 of drainage credits available within the Sand Creek Basin. This credit amount is based upon the construction cost estimate for the channel minus the drainage fees assessed for Claremont Business Park Filing No. 1. The District will use an additional \$755,604.00 of the drainage credits for the platting of Claremont Business Park Filing No. 2. The District will have \$469,751.45 of drainage credits left within the Sand Creek Fee basin.

The Central Marksheffel Business District has also constructed the Marksheffel Road Bridge over East Fork Sand Creek. This structure has been identified as a needed public improvement within the Drainage Basin Planning Study for Sand Creek and is eligible for reimbursement. Since the construction of the Marksheffel Bridge is in excess of the \$75,711.52 in bridge fees due for this site, no bridge fees are required at the time of platting. The fee will be deducted from the eligible reimbursable construction costs of the bridge and the remaining credits will be utilized or reimbursement applied for by the Central Marksheffel Business District.

**CLAREMONT DRAINAGE PLAN BUSINESS PARK FILING No. 2**

OWNER OF ADVANCED RV & SELF STORAGE



**SUBDIVER**  
HAMMERS CONSTRUCTION INC.  
3460 CAPITAL DRIVE  
COLORADO SPRINGS, CO 80915-9710



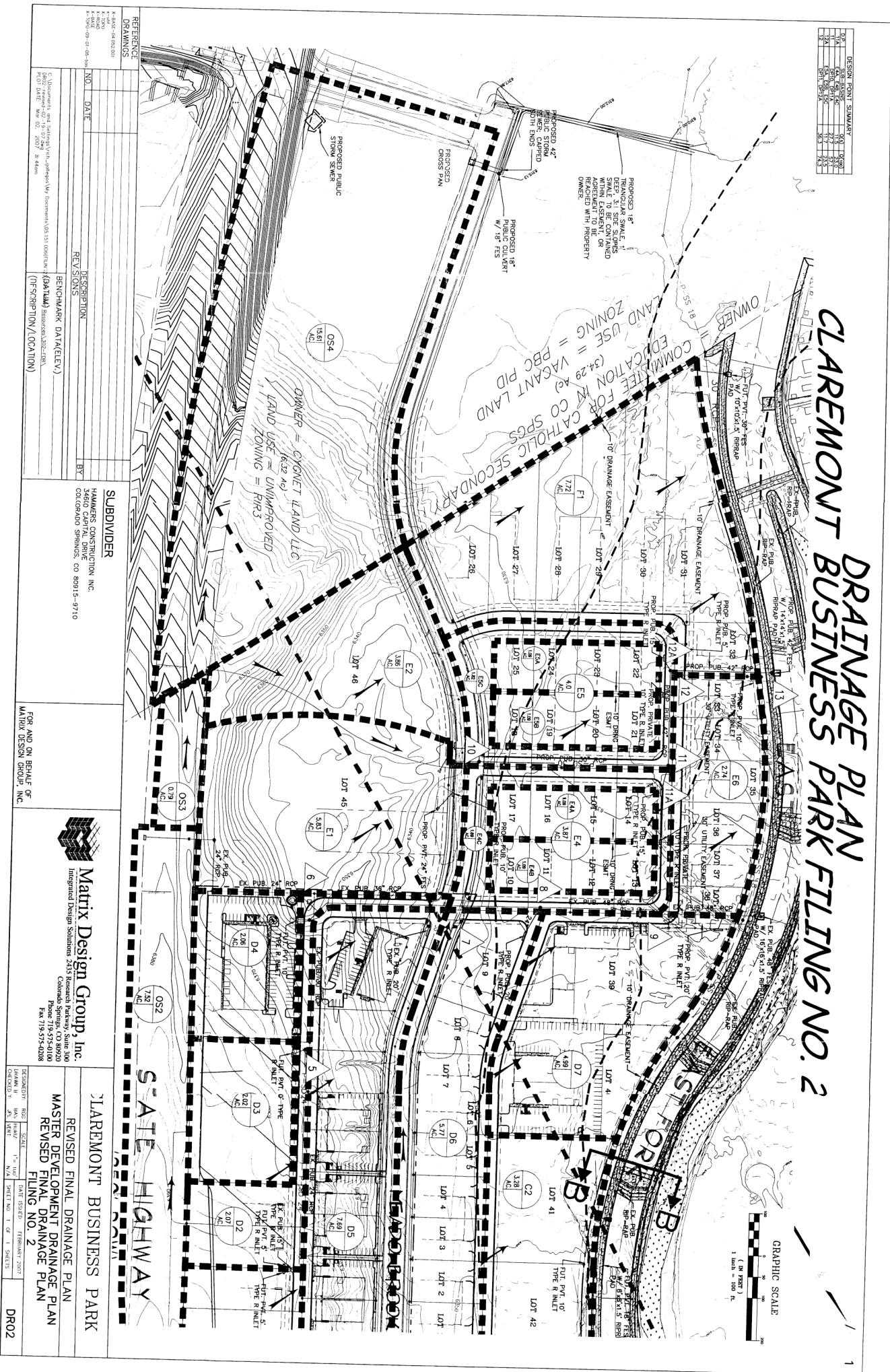
**Matrix Design Group, Inc.**  
Integrated Design Solutions 2435 Research Parkway, Suite 30  
Colorado Springs, CO 80906 Phone 719-575-0300

**CLOVERWOOD BLDG**

BUSINESS PARK

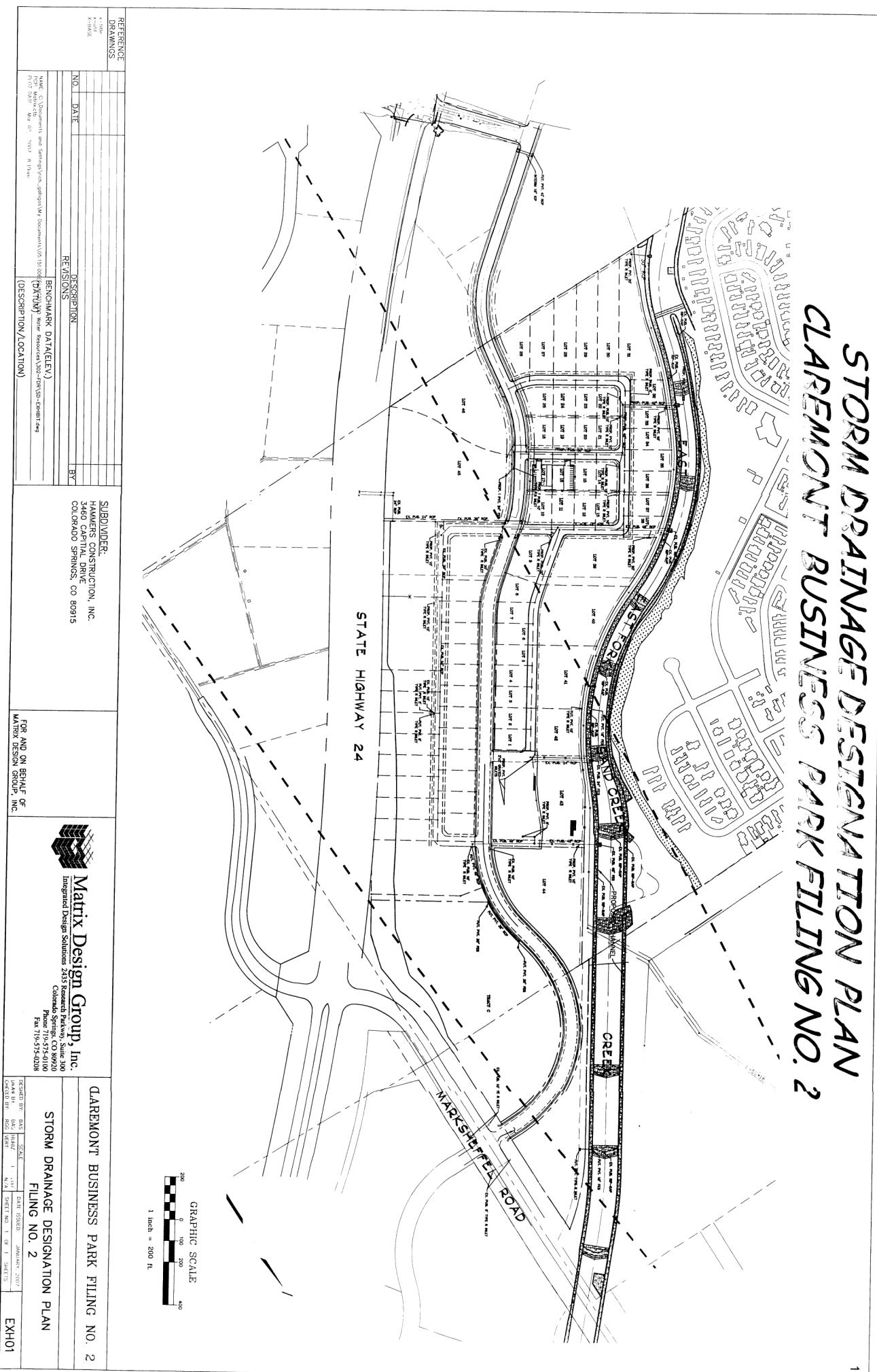
CLAREMONT DRAINAGE PLAN  
BUSINESS PARK FILING NO 2

DESIGN POINT SUMMARY			
D.P.	SUB-BASINS	Q(0)	Q(100)
I/A	EAA, EAB, EAC	11.5	23.0
II	DP10, DP11	27.7	57.1
IIA	EBA, EBB, EBC	11.7	23.5
III	DP11, DP12A	36.3	74.3



**STORM DRAINAGE DESIGNATION PLAN  
CLAREMONT BUSINESS PARK FILING NO. 2**

→



## **BOCC RESOLUTION 16-426**

500  
Chuck Broerman  
11/28/2016 11:50:04 AM  
Doc \$0.00 2  
Rec \$0.00 Pages

El Paso County, CO



216137149

**RESOLUTION NO. 16- 426**

**BOARD OF COUNTY COMMISSIONERS  
COUNTY OF EL PASO, STATE OF COLORADO**

**Resolution Denying an Appeal by Hammers Construction LLC (APP-16-002) of the Administrative Determination made by the Planning and Community Development Department Executive Director regarding the requirement for permanent/post construction Water Quality (permanent stormwater quality best management practices or BMP's).**

**WHEREAS**, pursuant to §§30-11-101(1)(e) and 30-11-107(1)(e), C.R.S., the Board of County Commissioners of El Paso County, Colorado (hereinafter "Board) has the legislative authority to manage the concerns of El Paso County when deemed by the Board to be in the best interests of the County and its inhabitants; and

**WHEREAS**, after consultation with the County Attorney's Office, the Executive Director of Planning and Community Development on August 4, 2016 issued an administrative determination finding made an administrative determination that all undeveloped lots within the Claremont Business Park are subject to installation of permanent stormwater management best management practices (BMP's) associated with development, and that the terms of a 2008 approved deviation relieving the developer of the requirements have not been met.; and

**WHEREAS**, an appeal of the administrative determination was filed by Hammers Construction on August 10, 2016, and a hearing date was set for September 27, 2016 to hear the appeal; and

**WHEREAS**, the hearing was continued to a date certain of November 22, 2016; and

**WHEREAS**, at the Applicant's appeal hearing on November 22, 2016, testimony from the Applicant and the Applicant's representatives was heard by the Board in favor of the appeal, testimony from representatives of Planning and Community Development Department and was presented, and such testimony and associated evidence was weighed by the Board; and

**WHEREAS**, the Board, having reviewed the testimony and evidence, hereby finds and determines that the requested appeal of the administrative determination by the Planning and Community Development Executive Director by the Applicant did not satisfy the criteria of approval to overturn the administrative determination.

**NOW, THEREFORE, BE IT RESOLVED** that the Board of County Commissioners of El Paso County, Colorado, hereby denies the appeal of the administrative determination by Hammers Construction and determines that permanent stormwater management best management practices (BMP's) are required with new development within the Claremont Business Park: and

**BE IT FURTHER RESOLVED** that Sallie Clark, duly elected, qualified member and Chair of the Board of County Commissioners, or Darryl Glenn, duly elected, qualified member and Vice Chair of the Board of County Commissioners, be and is hereby authorized on behalf of the Board to execute any and all documents necessary to carry out the intent of the Board as described herein.

**DONE THIS 22<sup>nd</sup> day of November, 2016, at Colorado Springs Colorado.**

BOARD OF COUNTY COMMISSIONERS  
EL PASO COUNTY, COLORADO



By:

  
Sallie Clark  
Chair of the Board

# V1\_Final Drainage Report Redlines.pdf Markup Summary

## Glenn Reese - EPC Stormwater (33)

**Subject:** SW - Textbox with Arrow

**Page Label:** 11

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 3:36:12 PM

**Length:** 0

**Area:** 0

**Volume:** 0

Pond 4 is shown as future on drainage map on pdf pg 126 below. Revise text and/or map to remove discrepancy.

**REVISED TO WQ POND 3**

**Subject:** SW - Textbox with Arrow

**Page Label:** 15

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 3:48:58 PM

**Length:** 0

**Area:** 0

**Volume:** 0

Which two? This section only previously mentions Pond 3.

**REVISED STATEMENT TO POND 3**

dwance of acreage run

ry to the two SFBs are  
id along Meadowbrook  
y the property owners

**Subject:** SW - Highlight

**Page Label:** 15

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 3:47:36 PM

**Length:** 0

**Area:** 0

**Volume:** 0

the two SFBs

**REVISED STATEMENT TO POND 3**

**Subject:** SW - Textbox with Arrow

**Page Label:** 15

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 3:49:06 PM

**Length:** 0

**Area:** 0

**Volume:** 0

This paragraph only mentions Pond 1 and 2. What about Pond 4 and 5? (Pond 3 already previously discussed in this section)

**REVISED STATEMENT TO INCLUDE POND 4 & 5**

**Subject:** Image

**Page Label:** 16

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 3:54:55 PM

**Length:** 0

**Area:** 0

**Volume:** 0

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

**Subject:** SW - Textbox with Arrow

**Page Label:** 16

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 4:21:45 PM

**Length:** 0

**Area:** 0

**Volume:** 0

Make a column for each of the 5 ponds.

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

Make a column for  
each of the 5 ponds.

delete this column if  
no RR is anticipated  
for this site.

**Subject:** SW - Textbox with Arrow

**Page Label:** 16

**Author:** Glenn Reese - EPC Stormwater

**Date:** 3/28/2023 4:21:48 PM

**Length:** 0

**Area:** 0

**Volume:** 0

delete this column if no RR is anticipated for this site.

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

**Subject:** SW - Textbox with Arrow  
**Page Label:** 16  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:21:43 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Add rows for each basin within this filing.

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

**Subject:** SW - Textbox  
**Page Label:** 16  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:22:36 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Completing a "Water Quality Treatment Summary Table" like the example provided below would greatly help us clearly see that WQ req's are being met for the whole site, if you could do one for this site.

**PER GLENN REESE TABLE NOT REQUIRED.  
MORE CLARIFICATION PROVIDED IN TEXT.**

**Subject:** SW - Textbox with Arrow  
**Page Label:** 16  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:21:52 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

From the PBMP Form, this column should be blank.

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

**Subject:** SW - Textbox with Arrow  
**Page Label:** 16  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:21:50 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

The areas of Basin G1, O1, O2, and P would be in this column

**PER GLENN REESE TABLE  
NOT REQUIRED. MORE  
CLARIFICATION PROVIDED  
IN TEXT.**

**Subject:** SW - Textbox with Arrow  
**Page Label:** 48  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/29/2023 7:53:46 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

**SHEET LABELED EXISTING CONDITION AND CORRESPONDING SHEET  
LABEL PROPOSED CONDITION EXTENTION OF EL JEFE HT.**

**Subject:** SW - Textbox  
**Page Label:** 48  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:31:23 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0 **TEXT ADDED**

Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE

**Subject:** SW - Textbox  
**Page Label:** 54  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:31:37 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

**DESIGN**  
Add text to the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

**TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT**



**Subject:** SW - Textbox  
**Page Label:** 60  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:31:43 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT"

**TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT**

User Input: Orifice at Und  
✓ Underdrain  
Underdrain  
Unc  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:52:01 PM  
**Length:** 0  
**Area:** 0      **NOTED**  
**Volume:** 0

Input: Orifice at Und  
Underdrain  
✓ Underdrain  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:53:39 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

User Input: Ov  
✓ Overflc  
Ov  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:54:08 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Overflow Weir Fr  
Overflow We  
✓ Overfl  
Horiz.  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:54:28 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Overflow Weir  
Overflc  
✓ Horiz. L  
C  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:54:30 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

User Input: Outlet Pipe  
✓ Depth  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:54:55 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Depth to Inver  
 Outlet  
ector Plate Height Ab  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:54:57 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Restrict  
  
 User Input:  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:58:14 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Emergency Spillwa  
 Spillw  
Spillwa  
cill.  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:59:34 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Emergency Spillway  
Spillwa  
 Spillwa  
Spillw  
reeboard above Max  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:59:36 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Spillway  
Spillway C  
 Spillway  
eboard above Max W  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:59:37 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

Freeboa  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:59:39 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0

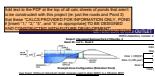
Time to I  
 Time to I  
Area  
  
**Subject:** Checkmark  
**Page Label:** 66  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 5:05:26 PM  
**Length:** 0      **NOTED**  
**Area:** 0  
**Volume:** 0



**Subject:** SW - Textbox  
**Page Label:** 72  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:32:05 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE

## **TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT**



**Subject:** SW - Textbox  
**Page Label:** 78  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:32:11 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Add text to the PDF at the top of all calc sheets of ponds that aren't to be constructed with this project (ie: just the roads and Pond 3) that these "CALCS PROVIDED FOR INFORMATION ONLY, POND # [insert "1," "2," "4", and "5" as appropriate] TO BE

## **TEXT ADDED TO REPORT, EX POND NOT TO BE MODIFIED OR CALCS PROVIDED FOR INFORMATION ONLY, POND# TO BE DESIGNED AND CONSTRUCTED WITH FUTURE DEVELOPMENT**



**Subject:** SW - Textbox  
**Page Label:** 84  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/29/2023 7:53:32 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Define "Remodeled Proposed Conditions." How is this different for the other calcs for this same pond shown on pdf page 60 above? Please discuss in the FDR text above.

## **SHEET LABELED EXISTING CONDITION AND CORRESPONDING SHEET LABEL PROPOSED CONDITION EXTENTION OF EL JEFE HT.**



**Subject:** SW - Textbox with Arrow  
**Page Label:** 126  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 3:36:29 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Move text over so the "4" in "Pond 4" is visible.

## **TEXT MOVED. POND 4 VISIBLE.**

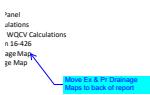


**Subject:** SW - Textbox with Arrow  
**Page Label:** 126  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 3/28/2023 4:05:52 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Move "Lot 1" text that is behind "Claremont"

## **LOT 1 TEXT REVISD AND MOVED.**

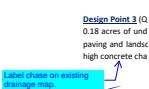
### **CDurham (38)**



**Subject:** Callout  
**Page Label:** 3  
**Author:** CDurham  
**Date:** 3/30/2023 9:55:19 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Move Ex & Pr Drainage Maps to back of report

## **REVISED EX & PROP MAPS MOVED TO THE BACK OF THE REPORT.**



**Subject:** Callout  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 3/30/2023 10:02:27 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label chase on existing drainage map.

## **CONCRETE CHASE LABELED.**

7. Basin H3 is  
half past the  
DP3 thru 5 per  
hydrology spreadsheet  
  
I6 and DP1.3.  
list of roof top,

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 3/30/2023 10:09:50 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP3 thru 5 per hydrology spreadsheet

**REVISED TO DP3-5**

e inlets located at DP6. Collected runoff  
over to an existing WQ pond (PR13-14)  
d QS=0.4 cfs of flow-by in the respective  
h QS=0.0 cfs and QS=0.3 cfs of flow-by  
inlets continues westward to Design Point  
Q100  
7.5 cfs) consists of flow-by runoff from  
as of rooftop, asphalt paving and landside  
remained within the curb and gutter to

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 3/30/2023 10:12:56 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Q100

**REVISED TO Q100**

flows within  
Runoff from  
15' Type R at  
id QS=0.2 cfs  
e intercepted

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 3/30/2023 10:18:20 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Q100

**REVISED TO Q100**

is collected in curb and gutter which discharges  
WQ Pond 2  
= 16.5 cfs) consists of runoff from Basin 13,  
43, 30, 23, and 0.19 acres in size respectively an  
as within the development. The runoff from  
the private street section of Gary Watson  
drainage area is collected at DP6. Collected runoff is  
over to an existing WQ pond (PR13-14). Inlet  
QS=0.4 cfs of flow-by in the respective st

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 3/30/2023 11:20:00 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

WQ Pond 2

**REVISED TO EX WQ POND 2**

t 3 b

**Subject:** Text Box  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 3/30/2023 11:23:36 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

3

**REVISED TO 3**

iX1 is 0.17  
whole  
flows  
Is this Inlet 7 as labeled on  
the existing drainage map?  
If so, please include the  
name in the text.

**Subject:** Callout  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 3/30/2023 11:25:50 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Is this Inlet 7 as labeled on the existing drainage  
map? If so, please include the name in the text.

**INSERT INLET 7  
INTO STATEMENT**

(Inlet 1)

**Subject:** Text Box  
**Page Label:** 11  
**Author:** CDurham  
**Date:** 3/30/2023 11:53:27 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

(Inlet 1)

**INLET 1 ADDED  
TO STATEMENT.**

ts.

ts. (Inlet 2)

**Subject:** Text Box  
**Page Label:** 11  
**Author:** CDurham  
**Date:** 3/30/2023 11:54:32 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

(Inlet 2)

**INLET 2 ADDED  
TO STATEMENT.**

asphalt  
x 6 inch  
on Point.  
Label chase on  
drainage map  
asin H2 is  
aving and  
e cul-de-

**Subject:** Callout  
**Page Label:** 12  
**Author:** CDurham  
**Date:** 3/30/2023 12:01:58 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label chase on drainage map

**LABELED ON MAP.**

ilt paving  
o the cul-  
DP 3 thru 5  
id DP1-3.  
roof top,

**Subject:** Callout  
**Page Label:** 12  
**Author:** CDurham  
**Date:** 3/30/2023 12:10:39 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP 3 thru 5

**DESIGN POINTS REVISED.**

and Q5=0.4 cfs of flow-by in the respect  
ith Q5=0.0 cfs and Q5=0.3 cfs of flow-b  
lets continues westward to Design Point

**Subject:** Callout  
**Page Label:** 13  
**Author:** CDurham  
**Date:** 3/30/2023 12:11:46 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Q100

**REVISED TO Q100**

1 and flow-by from the inlet  
nlets located at DP7. Inlet  
flow-by in the respective :  
pted runoff underneath Gan

DP12  
Point 13 (Q5 = 1.0 cfs, Q10

**Subject:** Callout  
**Page Label:** 13  
**Author:** CDurham  
**Date:** 3/30/2023 12:14:01 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP12

**REVISED TO DP12**

s flow into an  
DP14  
I DP9. Basins  
salt paving and

**Subject:** Callout  
**Page Label:** 13  
**Author:** CDurham  
**Date:** 3/30/2023 12:17:08 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP14

**REVISED TO DP14**

ts. 3

**Subject:** Text Box  
**Page Label:** 13  
**Author:** CDurham  
**Date:** 3/30/2023 12:19:57 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

3

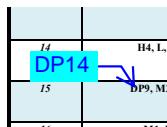
**REVISED TO 3 BASINS**

manhole  
nd DP10-13.  
Pond 2).

**Subject:** Callout  
**Page Label:** 14  
**Author:** CDurham  
**Date:** 3/30/2023 12:22:24 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP15-18

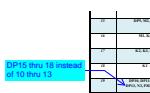
**REVISED TO DP15-17**



**Subject:** Callout  
**Page Label:** 32  
**Author:** CDurham  
**Date:** 3/30/2023 12:29:19 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP14

**DESIGN POINT REVISED**



**Subject:** Callout  
**Page Label:** 32  
**Author:** CDurham  
**Date:** 3/30/2023 12:30:21 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

DP15 thru 18 instead of 10 thru 13

**DESIGN POINTS REVISED**

Label various ponds  
as existing, proposed  
or future .

**Subject:** Text Box  
**Page Label:** 113  
**Author:** CDurham  
**Date:** 3/30/2023 4:16:44 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label various ponds as existing, proposed or  
future .

**PONDS LABELED EX, PROP, FUT**

Try to print all of stormcad  
table on one sheet, or include  
"Label" column with second  
sheet

Length (ft)

**Subject:** Text Box  
**Page Label:** 114  
**Author:** CDurham  
**Date:** 3/30/2023 4:18:28 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Try to print all of stormcad table on one sheet, or  
include "Label" column with second sheet

**STORM CAD INFORMATION  
PRINTED ON ONE SHEET**

Include pipe slope in  
table. ID, Fr #, %  
Flow/Capacity,critical depth, & EGL's is not  
needed in table.

**Subject:** Text Box  
**Page Label:** 114  
**Author:** CDurham  
**Date:** 3/30/2023 4:32:48 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Include pipe slope in table. ID, Fr #, %  
Flow/Capacity,critical depth, & EGL's is not needed  
in table.

**LABELS OMITTED.  
PIPE SLOPE IS  
SLOPE CALCULATED**

30.1  
14.9  
60.6  
181.1  
12.5  
30.0  
84.3  
115.8  
239.6

**Subject:** Callout  
**Page Label:** 114  
**Author:** CDurham  
**Date:** 3/30/2023 4:50:00 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Length does not match CD's

**LENGTHS REVISED**

4	1.0	1.0	HQ. 12
5	0.9	1.0	HQ. 17
6	0.2	1.0	DRIVE 12
7	0.2	1.0	DRIVE 13
8	0.9	1.0	PN PROJECT
9	0.8	0.7	HQ. 14
10	1.0	1.0	DRIVE 14
11	1.0	0.8	W1. 04
12	1.0	2.0	W2. 04
13	1.0	2.0	W3. 04
14	1.0	2.0	W4. 04

**Subject:** Callout  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:38:08 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

H4

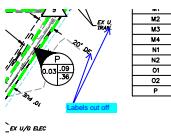
**BASIN LABEL REVISED..**

Add Contour Labels

**Subject:** Text Box  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:38:23 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Add Contour Labels

**MAJOR CONTOURS LABELED.**



**Subject:** Callout  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:38:44 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Labels cut off

**LABEL VISIBLE.**



**Subject:** Callout  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:39:09 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

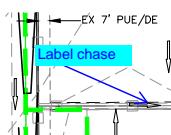
Label rundowns  
**RUNDOWNS LABELED.**



**Subject:** Callout  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:40:03 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label pipe

**PIPES LABELED. SEE STORM  
SEWER SUMMARY TABLE.**



**Subject:** Callout  
**Page Label:** 124  
**Author:** CDurham  
**Date:** 3/30/2023 12:39:41 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label chase

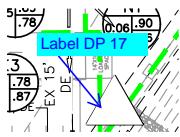
**CHASE LABELED.**



**Subject:** Cloud+  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:40:37 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Show riprap

**TEMP SEDIMENT BASIN IN LIEU OF RIPRAP**



**Subject:** Callout  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:41:02 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label DP 17

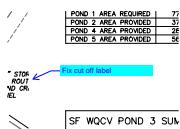
## DESIGN POINT 17 LABELED.



**Subject:** Callout  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:42:39 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label rundowns

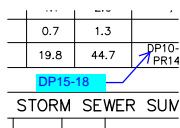
## RUNDOWNS LABELED.



**Subject:** Callout  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:42:50 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Fix cut off label

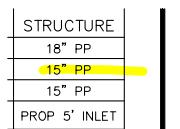
## LABEL VISIBLE.



**Subject:** Callout  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:43:06 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

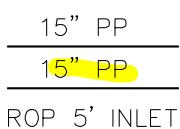
DP15-18

## REVISED TO DP 15-17



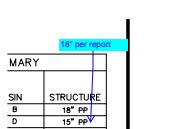
**Subject:** Highlight  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:43:14 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

## REVISED TO 18"



**Subject:** Highlight  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:43:16 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

## REVISED TO 18"



**Subject:** Callout  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:43:28 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

18" per report

## REVISED TO 18"

-Add contour labels  
- Indicate if facilities are public or private

**Subject:** Text Box  
**Page Label:** 126  
**Author:** CDurham  
**Date:** 3/30/2023 12:44:07 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

-Add contour labels  
- Indicate if facilities are public or private

## **PROPOSED AND EXISTING CONTOUR LABELS ADDED. FACILITIES LABEL PRIVATE.**

Carlos (10)

I20

.. VR233

**Subject:** Text Box  
**Page Label:** 1  
**Author:** Carlos  
**Date:** 3/28/2023 3:03:19 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

VR233

**PCD FILING NO. VR233 ADDED**

Joshua Palmer  
~~Interim Co~~

~~Conditions~~

**Subject:** Line  
**Page Label:** 2  
**Author:** Carlos  
**Date:** 3/20/2023 9:40:33 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

**INTERIM REMOVED**

Joshua Palmer, P.E.  
Interim County Engineer / ECM Administra  
~~Conditions~~  
~~Remove~~

**Subject:** Callout  
**Page Label:** 2  
**Author:** Carlos  
**Date:** 3/28/2023 3:03:37 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Remove

**INTERIM REMOVED**

Existing storm continues westward to Basin Ponds 12 and 13.  
I-20 (I-20) consists of flow from Basin 12 and flow which is conveyed within the curb and gutter to an existing STP (I-20) at approximately 100' upstream of the proposed outlet structure. Water is being released from Basin 12 and flow is being directed to Basin 13. An existing STP storm sewer (PSS) connects the two basins.

**Subject:** Text Box  
**Page Label:** 13  
**Author:** Carlos  
**Date:** 3/28/2023 11:29:53 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Include O1 in DP12 and show flow arrows for O1

**PER THE APPROVED "FINAL DRAINAGE REPORT FOR CLAREMONT BUSINESS PARK 2 FILING NO. 1" BY MS CIVIL CONSULTANTS, INC. DATED DECEMBER 2020 AND SUBSEQUENT REPORT FOR LOT 7 BASIN O1 WILL SHEET FLOW ONTO MEADOWBROOK PARKWAY.  
FLOW ARROWS WILL BE ADDED.**

(equal shares determined by size of lots 8-10)

**REVISED LOT NUMBERS**

Basin total acreage of the Basins is 0.56 AC, and doesn't exceed usage runoff allowed per EPC criteria.  
I-20Bs are released through outlet structures into an existing storm drain Meadowbrook Parkway. Water quality pond 1 will be private and shall be maintained by the owner of the property. Water quality pond 2 will be maintained by the property owners (equal shares) and shall be maintained by the owner of the El Paso County for access and maintenance. A maintenance agreement document shall accompany the final draw off the last ponds.

**Subject:** Highlight  
**Page Label:** 15  
**Author:** Carlos  
**Date:** 3/28/2023 11:36:50 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Lots 8-10 are being renamed with the subdivision.  
Please revise lot numbers.

**REVISED LOT NUMBERS**

**Subject:** Callout  
**Page Label:** 15  
**Author:** Carlos  
**Date:** 3/28/2023 11:37:22 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Lot 8-10 are being renamed with the subdivision.  
Please revise lot numbers.

At structures into an existing storm sewer  
The point it will be private and shall be  
the point of connection to the existing pond 2  
area (equal shares determined by size of lots  
and area of lot) and shall be located such that  
shall be connecting the first drainage report  
  
The report identifies Pond 3 being built and Pond 5  
(location of existing sediment basin on Tract B)  
being removed. Please revise paragraph for  
consistency.

**Subject:** Text Box  
**Page Label:** 15  
**Author:** Carlos  
**Date:** 3/28/2023 3:58:49 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

The report identifies Pond 3 being built and Pond 5  
(location of existing sediment basin on Tract B)  
being removed. Please revise paragraph for  
consistency.

## EXISTING SEDIMENT BASIN TO REMAIN UNTIL LOT 3 IS DEVELOPED.

**Subject:** Text Box  
**Page Label:** 16  
**Author:** Carlos  
**Date:** 3/28/2023 5:01:52 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Provide an estimate of the proposed  
imperviousness of the site and difference from the  
previously approved drainage report.

## STATEMENT PROVIDED ON IMPERVIOUSNESS IN THE GENERAL CONCEPT DRAINAGE DISCUSSION SECTION.



**Subject:** Callout  
**Page Label:** 126  
**Author:** Carlos  
**Date:** 3/27/2023 4:34:08 PM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label DP3

## DESIGN POINT 3 LABELED.



**Subject:** Callout  
**Page Label:** 126  
**Author:** Carlos  
**Date:** 3/28/2023 11:26:03 AM  
**Length:** 0  
**Area:** 0  
**Volume:** 0

Label proposed storm pipe.

## STORM SEWER HAS PIPE ROUTING LABEL. SEE STORM SUMMARY TABLE FOR SIZE.