



The Cottages at Mesa Ridge Final Drainage Report

April 2022

HR Green Project No: 200541

PCD File No. PUDSP2111

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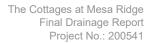
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HR GREEN: ADDRESSED

Please revise to SF2214





▷ ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by negligent acts, errors, or omission on my part in preparing this report.

	Ken Huhn, PE	Date		
	Registered Professional Engine	eer State of Colorado No	·	
	For and on behalf of HR Green	Development, LLC		
\triangleright	DEVELOPER'S STATEMENT			
	I, the developer, have read and	will comply with all of th	e requirements specified in this drain	age report and plan.
	Name of Developer		Authorized Signature	Date
	Printed Name	Title	Address	
\triangleright	EL PASO COUNTY			
	Filed in accordance with the red Manual, Volumes 1 and 2 and I	•	o County Land Development Code, Enual, as amended.)rainage Criteria
	Jennifer Irvine, P.E.			
	County Engineer/ECM Adminis	trator		



Table of Contents

١.	G	eneral Purpose, Location and Description	3
;	a.	Purpose	3
	b.	Location	3
	C.	Description of Property	3
	d.	Floodplain Statement	3
II.	Di	rainage Basins and Subbasins	3
;	a.	Major Basin Description	3
	b.	Existing Subbasin Description	4
	C.	Proposed Subbasin Description	4
III.		Drainage Design Criteria	5
;	a.	Development Criteria Reference	5
	b.	Hydrologic Criteria	5
IV.		Drainage Facility Design	6
;	a.	General Concept	6
	b.	Water Quality & Detention	6
	C.	Operation and Maintenance	9
	d.	Grading and Erosion Control Plan	9
	e.	Four Step Method to Minimize Adverse Impacts of Urbanization	9
1	f.	Drainage and Bridge Fees	9
9	g.	Opinion of Probable Cost	9
V.	Sı	ummary	. 10
VI.		Drawings	. 10
VII		References	. 10

Appendices

- A. Vicinity Map, FEMA Map, NRCS Soil Survey
- B. Hydrologic Analysis
- C. Hydraulic Analysis
- D. Water Quality and Detention Calculations
- E. Reference Material
- F. Drainage Maps



I. General Purpose, Location and Description

a. Purpose

The purpose of this Final Drainage Report (FDR) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure, and the planned stormwater management for The Cottages at Mesa Ridge. This report will support the development plan that is currently in review with El Paso County.

b. Location

The Cottages at Mesa Ridge, referred to as 'the site' herein, is in a portion of the northeast quarter of section 29, the southeast quarter of section 20, the southwest quarter of section 21, and the northwest quarter of section 28, township 15 south, range 65 west of the 6th P.M., County of El Paso, Colorado. The site is bound by S. Powers Boulevard to the east, multi-family residential development to the south, single-family residential development to the west and undeveloped land to the north. Surrounding platted developments include Mesa Ridge Filing 8 and 9 to the south, Sunrise Ridge to the west and the Glen at Widefield to the east. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 10.22 acres of undeveloped land with existing vegetation consisting of native grasses. Once developed, the site will include 122 dwelling units, a club house and open space tracts. The site will be platted as a single lot. In general, the site slopes south towards the Fountain Mutual Irrigation Co canal. Onsite elevations range from 5750' - 5795' with slopes ranging 1 - 33%. Per a NRCS soil survey, the site is made up of Type B Stoneham sandy loam and Type B Nelson-Tassel fine sand loams. The NRCS soil survey is presented in Appendix A.

There are no major drainageways or irrigation facilities that traverse the site nor does the site fall within the Streamside Overlay Zone. Onsite, existing utilities include water, sewer, fiberoptic, underground gas and underground electric/telecommunication. An existing drainage map is presented in Appendix F.

d. Floodplain Statement

Based on FEMA Firm map 08041C0956G dated December 8, 2018, the site is Zone X, which are areas determined to be outside the 0.2% annual chance flood.

II. Drainage Basins and Subbasins

a. Major Basin Description

The site is located within West Fork Jimmy Camp Creek Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

- 1. "West Fork Jimmy Camp Creek Drainage Basin Planning Study" prepared by Kiowa Engineering Corporation, October 2003, revised.
- 2. "Master Development Drainage Plan Mesa Ridge Development" prepared by Kiowa Engineering Corporation, December 17, 2006. (2006 MDDP)
- 3. "Mesa Ridge Development Master Development Drainage Plan Update" prepared by Kiowa Engineering Corporation, January 15, 2013. (2013 MDDP)

In the 2006 MDDP, the site was identified as Basin 1040 and Basin 1030. Basin 1040 was planned to be routed to Detention Basin D (located within Mesa Ridge Subdivision Filing 8) while Basin 1030 was routed to



Detention Basin 1031 (located on the east side of S. Powers Boulevard adjacent to the site). The 2013 MDDP did not alter the planned detention scenario for the site.

b. Existing Subbasin Description

The site's existing drainage is split into five basins. An existing drainage map is presented in Appendix B. See below for existing basin descriptions:

Basin EX1 is 5.69 acres of undeveloped area and existing single family residential lots. Existing stormwater from this basin ($Q_5 = 2.5$ cfs $Q_{100} = 13.7$ cfs) is conveyed onsite to DP1.

Basin EX2 is 3.12 acres of undeveloped area and a portion of S. Powers Boulevard. Existing stormwater from this basin ($Q_5 = 4.2$ cfs $Q_{100} = 12.4$ cfs) follows historic drainage patterns to an existing roadside swale to DP2. The flow is captured in an existing area inlet at DP2 and conveyed underneath S. Powers Boulevard in a 24" RCP culvert to an existing, temporary sediment basin.

Basin EX3 is 1.46 acres of undeveloped area. Existing stormwater from this basin ($Q_5 = 1.6$ cfs $Q_{100} = 5.1$ cfs) is conveyed to the existing irrigation canal to DP3.

Basin EX4 is 0.28 acres of undeveloped area. Existing stormwater from this basin ($Q_5 = 0.1$ cfs $Q_{100} = 0.8$ cfs) is conveyed in an existing roadside swale to DP4.

Basin EX5 is 3.38 acres of undeveloped area and existing single family residential lots. Existing stormwater from this basin ($Q_5 = 2.8$ cfs $Q_{100} = 11.9$ cfs) flows offsite along the site's southern boundary at DP5.

c. Proposed Subbasin Description

The proposed site has been divided into 9 subbasins for analysis. All storm sewer and appurtenances are private. A drainage map has been presented in Appendix F. See below for basin descriptions:

Basin 1 is 3.65 acres of single-family residential lots, duplex homes, roadway and landscaping. Stormwater from this basin ($Q_5 = 6.6$ cfs $Q_{100} = 14.6$ cfs) is conveyed in curb and gutter to a 15' Type R on-grade inlet at DP5. Basin 1 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 2 is 5.02 acres of single-family residential lots, duplex homes, roadway and landscaping. Stormwater from this basin ($Q_5 = 8.7$ cfs $Q_{100} = 19.3$ cfs) is conveyed in curb and gutter to a 15' Type R on-grade inlet at DP1. Basin 2 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 3 is 3.03 acres of existing roadway (S. Powers Boulevard), a compacted breeze trail and undeveloped area. Stormwater from this basin ($Q_5 = 3.4$ cfs $Q_{100} = 9.7$ cfs) follows historic drainage patterns in an existing roadside swale to an existing Type C inlet at DP2. An existing 24" RCP culvert conveys to flow to an existing, temporary sediment basin. Per Section I.7.1.B.7 and I.7.1.B.9 of the EPCDCM Appendix I – Stormwater Quality Policy and Procedures, Basin 3 will not be routed to a permanent stormwater control measure. The trail improvements associated with Basin 3 will not increase existing stormwater flows.

Basin 4 is 0.48 acres of landscaping and undeveloped area. Stormwater from this basin ($Q_5 = 0.4$ cfs $Q_{100} = 1.8$ cfs) follows historic drainage patterns towards the Fountain Irrigation Ditch at DP3. From there, flow is conveyed under S. Powers Blvd in an existing box culvert (size unknown) to an existing, temporary sediment



basin. Per Section I.7.1.B.7 and I.7.1.B.9 of the El Paso County Appendix I – Stormwater Quality Policy and Procedures, Basin 4 will not be routed to a permanent stormwater control measure. The basin will remain mostly undeveloped with a proposed trail and retaining wall. The trail and retaining wall improvements associated with Basin 4 will not increase existing stormwater flows.

Basin 5 is 1.61 acres of landscaping and a fire access road. Stormwater from this basin ($Q_5 = 2.1$ cfs $Q_{100} = 5.6$ cfs) is captured in a grass-lined swale and captured in a Type C inlet at DP4. Basin 5 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 6 is 0.60 acres of undeveloped area. Stormwater from this basin ($Q_5 = 0.2$ cfs $Q_{100} = 1.2$ cfs) follows historic drainage patterns in an existing roadside swale along S. Powers Boulevard at DP6 and continues south along S. Powers in a roadside ditch that outfalls into existing Detention Basin D. The land disturbance associated with Basin 6 will not increase existing stormwater flows.

Basin 7 is 0.45 acres of landscaping and existing single family residential. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 1.6$ cfs) follows historic drainage patterns towards DP7. From there, the flow continues into Mesa Ridge Subdivision Filing 8 where it is captured and detained in Basin D. See Basin 1040 from the Mesa Ridge Filing No. 8 FDR for additional detail.

Basin 8 is 0.21 acres of roadway. Stormwater from this basin ($Q_5 = 1.1$ cfs $Q_{100} = 2.0$ cfs) is conveyed in curb and gutter down Landover Lane to a 15' Type R inlet at DP8. Basin 8 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 9 is 0.16 acres of roadway. Stormwater from this basin ($Q_5 = 0.7$ cfs $Q_{100} = 1.2$ cfs) is conveyed in curb and gutter down Landover Lane to a 5' Type R inlet at DP9. Basin 9 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

III. Drainage Design Criteria

a. Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "*Drainage Criteria Manual of EL Paso County, Colorado*" Volumes 1 and 2 (EPCDCM), current adopted version, and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CCSDCM), dated May 2014, as adopted by El Paso County, as well as the July 2019 El Paso County Engineering Criteria Manual update.

b. Hydrologic Criteria

Hydrologic data was obtained from the "City of Colorado Springs Drainage Criteria Manual – Chapter 6 Hydrology". Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from CCSDCM Table 6-2 below. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Full Spectrum Detention in addition to CUHP v.2.0.1 and EPA-SWMM v.5.1. Detention pond allowable release rate will be limited to less than or equal to those noted in the 2013 Mesa Ridge MDDP.



Table 6-2: Rainfall Depths for Colorado Springs									
Return Period (yr) 5 100									
1-hr Rainfall Depth (in)	1.50	2.52							

IV. Drainage Facility Design

a. General Concept

Onsite stormwater will be conveyed via Type 5 curb and gutter to Type R inlets. Captured stormwater will be piped to and detained in an existing, full spectrum detention pond located in Mesa Ridge Filing 9 south of the site. The full spectrum detention pond will outfall at less than historic values to the east side of S. Powers Boulevard and to the site's historic outfall. See below section regarding the existing detention basin analysis and retrofit. The ultimate outfall for the site is Jimmy Camp Creek, south of Hale Reservoir.

b. Water Quality & Detention

The Cottages at Mesa Ridge will utilize the existing regional Full Spectrum Detention Basin D for water quality and detention. Detailed analysis performed with this Report indicates that in its existing condition, there is adequate 100-year volume in the Detention Basin D for development of The Cottages at Mesa Ridge site. However, there are some concerns regarding the detention pond drain times. See discussion below for details on the analysis completed on Detention Basin D.

This pond was included originally as flood control in the 2006 MDDP and was updated to provide Full Spectrum detention with the 2013 MDDP. In addition, the record drawings for the retrofit of the pond confirmed the use of an orifice plate to control the full spectrum volume. Record documents are titled: Mesa Ridge Filings 8 & 9, Detention Basin 'D', Full Spectrum Detention Modifications, Final Design Drawings, by Kiowa Engineering Corporation, dated October 2011. Both MDDPs show Basin 1040 routed to Full Spectrum Detention Basin D. However, the basin characteristics provided with the most recent MDDP included The Cottages at Mesa Ridge site as historic.

In order to confirm that the existing Full Spectrum Detention Basin D has c HR GREEN: Cottages at Mesa Ridge, updated modeling with proposed basin 1040 chai ADDRESSED

of The

Hydrology and hydraulics included with the previous MDDPs utilized HEC-1 software to determine peak runoff quantities at specific design points and routing elements. These HEC-1 models were not available for use, so an effort was made to update them to the more current HEC-HMS program. However, there were too many unknown variables with the program to get it to provide reliable results.

Current CCSDCM V.1 CH.6 1.4 Selecting Methods for Estimating Design Flows notes in part that:

- For more complex drainage basins and routing requirements, the HEC-HMS model or the EPA SWMM method is better suited but requires more experience and expertise to properly apply. The EPA SWMM method also provides hydrographs, reservoir routing, and the ability to evaluate runoff reduction practices in detail.
- If detention facilities are to be sized based on hydrograph routing, or if hydrograph information is desired for any other reason, the EPA SWMM or the NRCS method must be used.





Therefore, CUHP and EPA SWMM methodology were selected as appropriate modeling programs to confirm volumes and release rates for Full Spectrum Detention Basin D are in line with the intent of the previous MDDPs and current CCSDCM criteria.

CUHP

A new CUHP model was prepared streamlined with only the MDDP basins being updated at this time and major basins tributary to Full Spectrum Detention Basin D. This includes Basin 1040, 6001, 6005, 6010, 6011 and 6020. Basin parameters included in the CUHP as follows:

- Basin parameters for Basin 1040 were updated based on the most current design information available and correspond to the Rational Method calculations noted elsewhere in this report. The area to Basin 1040 increased from what was accounted for in the previous MDDPs.
- Basins 6001, 6005, 6010, 6011 and 6020 used area and length parameters taken directly from the HEC-1 noted above.
- Basins 6001, 6005, 6010, 6011 and 6020 utilized percent impervious estimated from existing asconstructed land uses.
- All basins used the standard depression storage and infiltration parameters for Hydrologic Soil Type B.

Rainfall data was taken from NOAA Atlas 14 Point Precipitation for a 60-minute (1-hour) recurrence interval depth, 100=2.74 in. The 1-hour point precipitation was chosen in part because the MHFD-Detention worksheet uses the 1-hour depth as an input parameter to run the CUHP program in the background. This allows a more accurate review of the existing pond by using consistent storms across both the CUHP and MHFD-Detention software.

Input parameters and results for the 100-year event are included with Appendix D.

EPA SWMM

Similar to the CUHP modeling, a simplified hydraulic routing model was prepared. In this case, the U.S. Environmental Protection Agency Stormwater Management Model (EPA SWMM) software was used for the proposed conditions with the development of The Cottages at Mesa Ridge.

The model includes a stage-storage curve for Pond D extracted directly from the pond grading shown on the 2011 Full Spectrum Detention Modifications Plan noted above. The proposed Pond D stage-release curve was developed through an iterative process, described more in depth below.

The other separate existing pond (Detention Basin 6002) which is tributary to Pond D provides storage for Basin 6001. Parameters for modeling Detention Basin 6002 were taken directly from the 2013 MDDP HEC-1. Additionally, EPA SWMM element routing parameters such as channel length and size were taken directly from the previous HEC-1 model with the exception of elevations (not used in HEC-1). For this a reasonable starting (downstream) elevation was used from the Pond D plans, and slope/length parameters from HEC-1 used to set all other upstream elevations. A back-check was completed to ensure resultant upstream elevations seem reasonable given rough elevations on 2013 MDDP Exhibit.

Input parameters and results for the 100-year event are included with Appendix D.



Full Spectrum Detention Basin D

MHFD-Detention worksheets were set up using updated total watershed area and percent imperviousness for several reasons, they include:

- To confirm the updated full spectrum volume required within Pond D. Note, because an inflow hydrograph will be used for the 5-year and 100-year events only the resultant full spectrum volumes are relevant from this data.
- To review how the existing pond is functioning under the proposed condition by incorporating the as-built stage-storage and stage-release data into the workbook. Note, the release structure was surveyed to provide accurate structure parameters.
- To route the 5-year and 100-year hydrographs developed in the CUHP and EPA SWMM through the provided pond volume and as-built release structure.

MHFD-Detention (as-built) results from routing the proposed 100-year hydrograph through the as-built pond volume and release structure indicate that there is adequate 100-year volume in the existing pond for development of The Cottages at Mesa Ridge site. However, results also indicate that the existing pond is exceeding drain time limitations noted in current MHFD criteria and Colorado Revised Statute 37-92-602(8).

To rectify the drain times discrepancy a separate MHFD-Detention (proposed) worksheet was set up matching the previously noted stage-storage curve and input hydrograph but altering the release structure (and corresponding stage-release curve). The drain times were revised by enlarging the orifice areas and updating the detention stages to correlate with the new Full Spectrum volume. Once the 100-year peak release rate was confirmed to be at or below the threshold established with the 2013 MDDP (233 cfs) the resultant stage-release curve was transferred back to the prepared SWMM and re-run to confirm the same results as found with the MHFD-Detention (proposed) analysis. Note the existing structure box size becomes the limiting element controlling release in the 100-year event, not the restrictor plate.

Key pond parameters from the 2011 Full Spectrum Detention Modifications Plan along with the values determined with this Final Drainage Report are summarized below.

Full Spectrum Detention Basin D Summary											
	2011 Full Spectrum Modifications	As-Built Pond D without Modifications	As-Built Pond D with Proposed Modifications								
Tributary Area (acres)	not provided	98.8	98.9								
% Impervious (%)	not provided	48.8	49.1								
Full Spectrum Volume (acre-ft)	4.2	5.1	5.2								
Full Spectrum WSEL (ft)	5686.8	5687.2	5687.3								
Full Spectrum Drain Time (hrs)	not provided	> 120	71								
100-yr volume (acre-ft)	8.3	11.6	14.3								
Release Rate (cfs)	219	252	230								
100-yr WSEL (ft)	5690.2	5691.2	5692.7								
100-yr Drain Time (hrs)	not provided	> 120	70								



Conclusions from the analysis presented with this Report are that Full Spectrum Detention Basin D will function as intended in the proposed conditions taking into consideration the Basin 1040 changes (including increase in basin area) that will occur with development of The Cottages at Mesa Ridge. No modifications to the as-built volume are anticipated at this time. Modifications are required to the release structure to bring the existing pond in conformance with current drain time and stage-storage requirements. The detailed extent of modifications to the existing structure have been presented in Appendix E.

c. Operation and Maintenance

An Operation and Maintenance (O&M) manual was previously approved for Detention Basin D. The pond is privately maintained by Mesa Ridge Metropolitan District No. 1. The manual will be provided once made available. The manual specifies maintenance intervals and required actions to maintain the function of the extended detention basin and appurtenances.

d. Grading and Erosion Control Plan

Due to the project disturbance area, a separate Grading and Erosion Control plan will be required. The Grading and Erosion Control Plan has been submitted to El Paso County and City of Fountain in conjunction with the Final Drainage Report and Construction Drawings.

e. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Roof drains will route across landscape areas and grass lined swales are used for stormwater conveyance, whenever possible to promote infiltration.

Step 2 – Treat and slowly release the WQCV: An existing, regional full spectrum detention pond provides water quality for the site. The WQCV is released over a period of 41 hours.

Step 3 – Stabilize stream channels: Drainage swales will be lined with non-erosive soils and permanently seeded to provide stabilization. If required due to erosive velocities, additional protection will be provided in the form of riprap lining and drop structures to reduce stormwater velocities and provide stabilization.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

f. Drainage and Bridge Fees

Cottages at Mesa Ridge is located within the West Fork Jimmy Camp Creek drainage basin. See below for drainage fees associated with The Cottages at Mesa Ridge development. Fees are due at time of platting.

	2022 Drainage & Bridge Fees													
Site Acreage (ac)	Site Impervious (%)	Impervious Area (ac)	Drainage Fee/ Impervious Acre	Drainage Fee										
10.22	56	5.72	\$14,470	\$82,869	\$4,281	\$24,488								

g. Opinion of Probable Cost

The engineer's opinion of probable cost is presented in Appendix E.



V. Summary

The Cottages at Mesa Ridge development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest El Paso County Drainage criteria and is in accordance with the Mesa Ridge MDDP.

VI. Drawings

Please refer to the Appendix F for existing and proposed drainage maps.

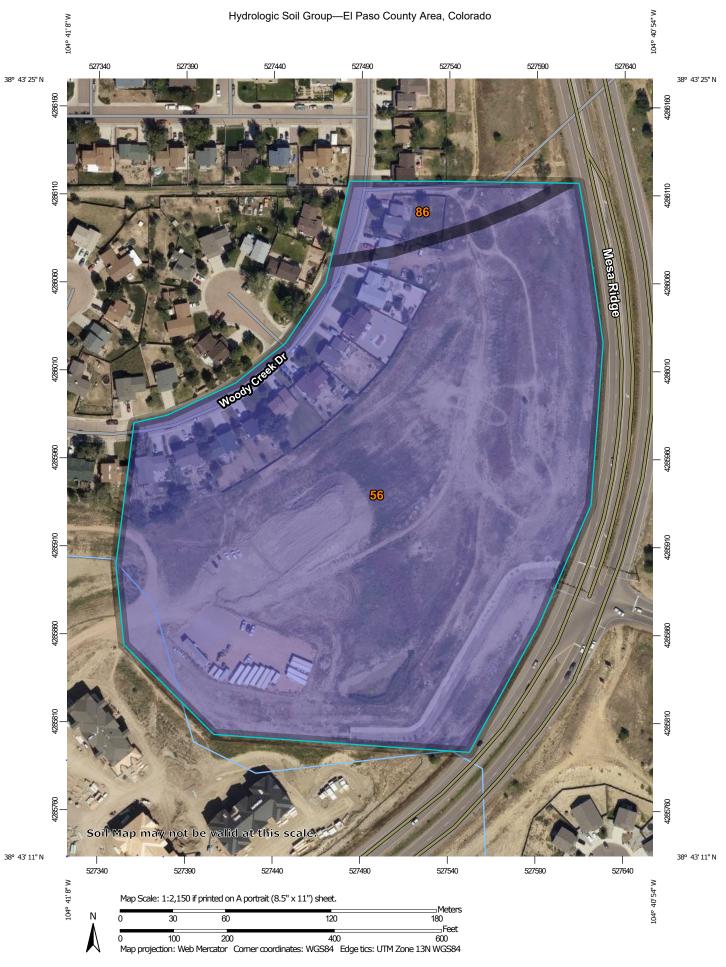
VII. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Urban Storm Drainage Criteria Manual, Mile High Flood District, January 2018.
- 3. *Master Development Drainage Plan Mesa Ridge Development*, Kiowa Engineering Corporation, December 17, 2006.
- 4. *Mesa Ridge Development Master Development Drainage Plan Update*, Kiowa Engineering Corporation, January 15, 2013.
- 5. *Mesa Ridge Filings* 8 & 9, *Detention Basin 'D'*, *Full Spectrum Detention Modifications, Final Design Drawings*, by Kiowa Engineering Corporation, October 2011.
- 6. Colorado Unit Hydrograph Procedure (CUHP), Version 2.0.1, October 2019.
- 7. Environmental Protection Agency Stormwater Management Model (EPA SWMM), Version 5.1, 2020.
- 8. Mile High Flood District Detention Basin Design Workbook (MHFD-Detention), Version 4.04, February 2021.





APPENDIX A - VICINITY MAP, SOIL MAP, FEMA MAP



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 17, Sep 13, 2019 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Aug 14, 2018—Sep 23. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

			_	
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	В	15.6	94.7%
86	Stoneham sandy loam, 3 to 8 percent slopes	В	0.9	5.3%
Totals for Area of Inter	est	16.5	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

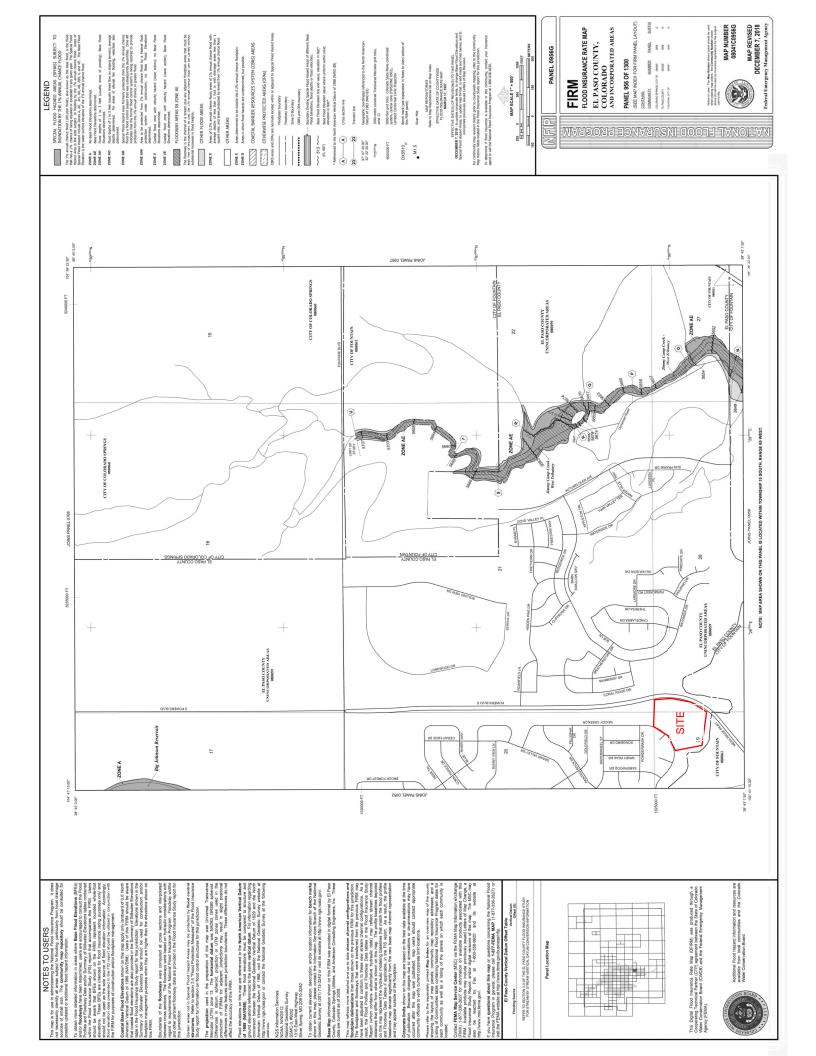
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





NOAA Atlas 14, Volume 8, Version 2 Location name: Widefield, Colorado, USA* Latitude: 38.7212°, Longitude: -104.684° Elevation: 5774.67 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹														
Duration	Average recurrence interval (years)														
Daration	1	2	5	10	25	50	100	200	500	1000					
5-min	0.253 (0.208-0.313)	0.304 (0.250-0.377)	0.395 (0.323-0.491)	0.478 (0.388-0.596)	0.603 (0.476-0.792)	0.707 (0.541-0.940)	0.819 0.603-1.12)	0.940 (0.659-1.32)	1.11 (0.746-1.61)	1.25 (0.811-1.83)					
10-min	0.371 (0.305-0.459)	0.446 (0.366-0.552)	0.579 (0.473-0.719)	0.700 (0.569-0.873)	0.883 (0.696-1.16)	1.04 (0.793-1.38)	1.20 0.882-1.64)	1.38 (0.965-1.93)	1.63 (1.09-2.35)	1.83 (1.19-2.67)					
15-min	0.452 (0.372-0.559)	0.544 (0.446-0.673)	0.706 (0.577-0.877)	0.854 (0.694-1.07)	1.08 (0.849-1.42)	1.26 (0.967-1.68)	1.46 (1.08-2.00)	1.68 (1.18-2.36)	1.99 (1.33-2.87)	2.23 (1.45-3.26)					
30-min	0.655 (0.538-0.810)	0.785 (0.645-0.972)	1.02 (0.833-1.26)	1.23 (1.00-1.54)	1.55 (1.22-2.04)	1.82 (1.39-2.42)	2.11 (1.55-2.88)	2.42 (1.70-3.40)	2.87 (1.92-4.14)	3.23 (2.09-4.71)					
60-min	0.851 (0.699-1.05)	0.998 (0.819-1.24)	1.28 (1.04-1.59)	1.55 (1.25-1.93)	1.97 (1.56-2.61)	2.34 (1.80-3.13)	2.74 (2.02-3.77)	3.19 (2.25-4.51)	3.84 (2.58-5.58)	4.38 (2.84-6.39)					
2-hr	1.05 (0.865-1.29)	1.21 (1.00-1.49)	1.54 (1.26-1.90)	1.86 (1.52-2.31)	2.38 (1.92-3.16)	2.85 (2.21-3.81)	3.37 (2.52-4.62)	3.96 (2.81-5.57)	4.82 (3.27-6.97)	5.54 (3.62-8.03)					
3-hr	1.15 (0.955-1.41)	1.31 (1.09-1.61)	1.65 (1.36-2.02)	2.00 (1.64-2.46)	2.58 (2.09-3.43)	3.11 (2.43-4.16)	3.71 (2.79-5.09)	4.40 (3.15-6.19)	5.42 (3.70-7.82)	6.27 (4.12-9.06)					
6-hr	1.32 (1.10-1.60)	1.48 (1.24-1.81)	1.85 (1.54-2.26)	2.24 (1.85-2.75)	2.91 (2.38-3.87)	3.53 (2.79-4.71)	4.24 (3.21-5.79)	5.05 (3.65-7.08)	6.27 (4.33-9.00)	7.29 (4.84-10.5)					
12-hr	1.47 (1.23-1.77)	1.68 (1.41-2.03)	2.11 (1.77-2.56)	2.55 (2.12-3.11)	3.29 (2.70-4.31)	3.96 (3.13-5.21)	4.71 (3.59-6.36)	5.56 (4.04-7.71)	6.82 (4.74-9.71)	7.87 (5.27-11.2)					
24-hr	1.64 (1.39-1.97)	1.91 (1.62-2.30)	2.43 (2.05-2.93)	2.93 (2.46-3.55)	3.73 (3.06-4.80)	4.42 (3.52-5.75)	5.19 (3.97-6.91)	6.04 (4.41-8.27)	7.27 (5.09-10.2)	8.29 (5.60-11.7)					
2-day	1.85 (1.57-2.20)	2.19 (1.86-2.61)	2.80 (2.37-3.35)	3.36 (2.83-4.04)	4.22 (3.47-5.35)	4.94 (3.94-6.34)	5.72 (4.40-7.54)	6.57 (4.83-8.91)	7.79 (5.48-10.9)	8.77 (5.98-12.3)					
3-day	2.00 (1.71-2.37)	2.35 (2.01-2.79)	2.98 (2.54-3.56)	3.57 (3.02-4.27)	4.46 (3.68-5.63)	5.21 (4.17-6.65)	6.01 (4.64-7.89)	6.89 (5.09-9.30)	8.14 (5.77-11.3)	9.16 (6.28-12.8)					
4-day	2.14 (1.83-2.53)	2.49 (2.14-2.96)	3.14 (2.68-3.73)	3.74 (3.17-4.46)	4.64 (3.84-5.85)	5.41 (4.35-6.90)	6.25 (4.84-8.17)	7.15 (5.30-9.63)	8.44 (6.00-11.7)	9.49 (6.54-13.3)					
7-day	2.55 (2.20-3.00)	2.93 (2.52-3.45)	3.62 (3.10-4.28)	4.25 (3.62-5.05)	5.21 (4.34-6.52)	6.03 (4.88-7.63)	6.90 (5.38-8.97)	7.86 (5.87-10.5)	9.22 (6.60-12.7)	10.3 (7.16-14.4)					
10-day	2.91 (2.51-3.41)	3.33 (2.87-3.91)	4.07 (3.51-4.80)	4.75 (4.07-5.63)	5.78 (4.82-7.17)	6.63 (5.38-8.34)	7.55 (5.90-9.75)	8.53 (6.39-11.4)	9.93 (7.14-13.6)	11.1 (7.71-15.3)					
20-day	3.85 (3.35-4.49)	4.42 (3.85-5.16)	5.40 (4.68-6.32)	6.25 (5.38-7.35)	7.46 (6.24-9.14)	8.44 (6.88-10.5)	9.46 (7.44-12.1)	10.5 (7.93-13.8)	12.0 (8.69-16.3)	13.2 (9.25-18.1)					
30-day	4.62 (4.04-5.36)	5.32 (4.65-6.19)	6.50 (5.65-7.57)	7.48 (6.47-8.76)	8.86 (7.41-10.7)	9.94 (8.11-12.2)	11.0 (8.70-14.0)	12.1 (9.18-15.9)	13.6 (9.92-18.4)	14.8 (10.5-20.3)					
45-day	5.59 (4.91-6.46)	6.46 (5.66-7.48)	7.86 (6.87-9.13)	9.02 (7.83-10.5)	10.6 (8.86-12.7)	11.8 (9.63-14.4)	12.9 (10.2-16.3)	14.1 (10.7-18.3)	15.6 (11.4-20.9)	16.8 (11.9-22.9)					
60-day	6.43 (5.66-7.41)	7.43 (6.53-8.57)	9.02 (7.90-10.4)	10.3 (8.98-12.0)	12.0 (10.1-14.4)	13.3 (10.9-16.2)	14.5 (11.5-18.2)	15.7 (12.0-20.3)	17.3 (12.6-23.0)	18.4 (13.1-25.0)					

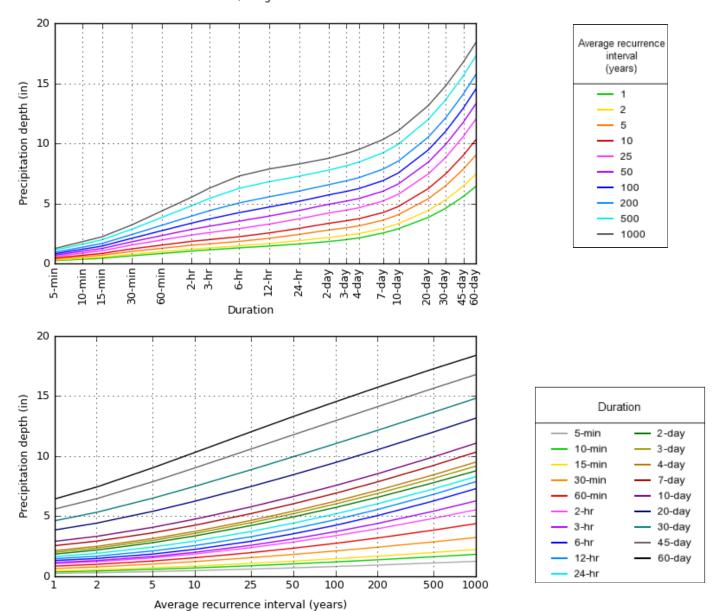
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

PDS-based depth-duration-frequency (DDF) curves Latitude: 38.7212°, Longitude: -104.6840°



NOAA Atlas 14, Volume 8, Version 2

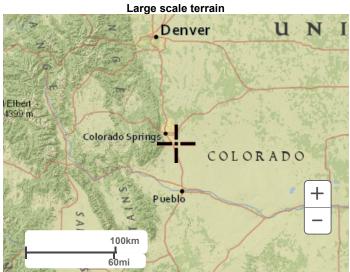
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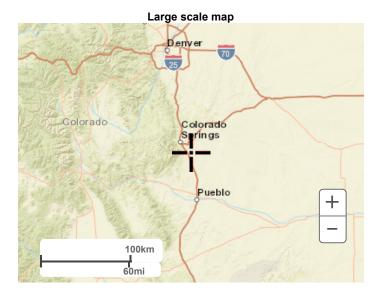
Back to Top

Maps & aerials

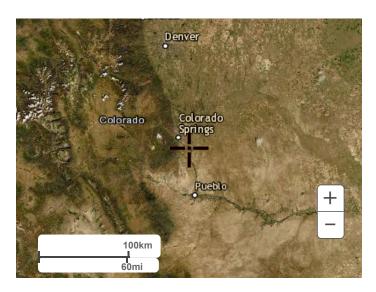
Small scale terrain







Large scale aerial



Back to Top

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National Weather Service
National Water Center
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Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

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APPENDIX B - HYDROLOGIC CALCULATIONS

1433	COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
	EXISTING CONDITIONS	Checked by:	!
HRGreen	LOCATION: COLORADO SPRINGS, COLORADO	Date:	12/6/2021

:	SUMMARY RUNOFF TABLE													
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)										
EX1	5.69	7	2.5	13.4										
EX2	3.12	28	3.5	10.0										
EX3	1.46	24	1.4	4.1										
EX4	0.28	2	0.1	0.5										
EX5	3.38	15	2.1	8.7										

DESIGN POINT SUMMARY TABLE												
DESIGN POINT	UPSTREAM BASIN	ΣQ ₅ (cfs)	ΣQ ₁₀₀ (cfs)									
1	EX1	2.5	13.4									
2	EX2	3.5	10.0									
3	EX3	1.4	4.1									
4	EX4	0.1	0.5									
5	EX5	21	8.7									



	COTTAGES AT MESA RIDGE	ИQJ	Calc'd by:
	EXISTING CONDITIONS		Checked by:
7	LOCATION: COLORADO SPRINGS, COLORADO	12/6/2021	Date:

	COMPOSITE 'C' FACTORS																	
BASIN	UNDEVELOPED	PAVED	SINGLE FAMILY LOT	TOTAL	SOIL						PAVE	D	SINC	LOT	MILY	CO IMPERV	MPOSI IOUSNE	
	ACRES				TYPE	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	
EX1	5.25	0.00	0.44	5.69	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	7	0.12	0.38	
EX2	2.28	0.84	0.00	3.12	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	28	0.31	0.52	
EX3	1.13	0.33	0.00	1.46	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	24	0.27	0.50	
EX4	0.28	0.00	0.00	0.28	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	2	0.09	0.36	
EX5	2.70	0.00	0.68	3.38	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	15	0.16	0.41	
Total				13.93											15.30			



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
EXISTING CONDITIONS	Checked by:	
LOCATION: COLORADO SPRINGS, COLORADO	Date:	12/6/2021

	TIME OF CONCENTRATION										
BAS	IN DATA		OVER	LAND TIM	E (T;)		TOTAL				
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C_{V}	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)
EX1	0.12	5.69	100	25.0	6.2	10	750	3.2	1.8	7.0	13.1
EX2	0.31	3.12	158	7.1	9.5	10	620	6.5	2.5	4.1	13.5
EX3	0.27	1.46	25	25.0	2.6	20	520	0.1	0.6	13.7	16.3
EX4	0.09	0.28	75	1.0	16.0	10	305	5.4	2.3	2.2	18.2
EX5	0.16	3.38	42	1.8	9.2	10	440	4.2	2.0	3.6	12.7



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
EXISTING CONDITIONS	Checked by:	
DESIGN STORM: 5-YEAR	Date:	12/6/2021

DIRECT RUNOFF				T	OTAL	RUNG	OFF	S	TREE	т		PIF	PΕ		TR	AVEL	TIME	REMARKS						
STREET	FNICO NO	DESIGN POINT	BASIN ID	AREA (ac)	C ₅	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	% alone	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mir	
		1	EX1	5.69	0.12	13.1	0.67	3.72	2.5															
		_	->																					
		2	EX2	3.12	0.31	13.5	0.96	3.67	3.5															
		3	EX3	1.46	0.27	16.3	0.40	2.40	1 1															
		3	EV9	1.40	0.27	10.3	0.40	3.40	1.4															
	4	4	EX4	0.28	0.09	18.2	0.03	3.23	0.1															
		1					,,,,,																	
	Ę	5	EX5	3.38	0.16	12.7	0.55	3.77	2.1															
																					·			



COTTAGES AT MESA RIDGE	Calc'd by:	ИФЛ
EXISTING CONDITIONS	Checked by:	
DESIGN STORM: 100-YEAR	Date:	8/10/2021

				DIF	RECT	RUNOF	F		TC	TAL I	RUNOI	FF	S	STREET			PIF	PE		TR	AVEL .		REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	t_c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	% SCOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1	EX1	5.69	0.39	13.1	2.19	6.24	13.7															
	2	EX2	3.12	0.63	12.9	1.97	6.28	12.4															
	3	EX3	1.46	0.61	16.1																		
	4	EX4	0.28	0.51	17.1	0.14																	
	5	EX5	3.38	0.55	12.2																		

コンフ	COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
	PROPOSED CONDITIONS	Checked by:	
HRGreen	LOCATION: EL PASO COUNTY, COLORADO	Date:	2/25/2022

SUMMARY RUNOFF TABLE							
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)			
1	3.65	61	7.3	15.2			
2	5.02	63	10.4	21.7			
3	3.03	29	3.4	9.7			
4	0.48	8	0.3	1.7			
5	1.61	38	2.6	6.6			
6	0.60	2	0.2	1.2			
7	0.45	26	0.4	1.3			
8	0.21	100	1.0	1.7			
9	0.16	100	0.7	1.3			

DESI	DESIGN POINT SUMMARY TABLE									
DESIGN POINT	UPSTREAM BASIN	ΣQ ₅ (cfs)	ΣQ ₁₀₀ (cfs)							
1	2	10.4	21.7							
2	3	3.4	9.7							
3	4	0.3	1.7							
4	5	2.6	6.6							
4.1	1 & 5	11.2	19.3							
5	1 & 2	7.3	21.8							
5.1	1, 2 & 5	18.0	33.7							
6	6	0.2	1.2							
7	7	0.4	1.3							
8	8	1.0	8.0							
9	9	0.7	1.4							
9.1	1, 2, 5, 8 & 9	19.1	42.0							



`	COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
1	PROPOSED CONDITIONS	Checked by:	
n	LOCATION: EL PASO COUNTY, COLORADO	Date:	2/25/2022

COMPOSITE 'C' FACTORS COMPOSITE SINGLE LANDSCAPING ROOFS ROOFS SINGLE FAMILY **PAVED TOTAL** SOIL LANDSCAPING **PAVED IMPERVIOUSNESS & C BASIN FAMILY TYPE** ACRES **%**I C₁₀₀ **%**I **%I** C₅ C₅ | C₁₀₀ **%**I C₅ C₁₀₀ C₅ C₁₀₀ **%**I C₅ C₁₀₀ 0.68 3.65 2 0.09 0.90 0.53 1.12 0.72 В 0.36 100 0.96 90 0.73 0.81 65 0.45 0.50 61 0.66 1 1.13 2 1.60 1.94 1.21 0.27 5.02 2 0.09 100 0.30 0.50 0.57 В 0.36 0.90 0.96 90 0.73 0.81 40 63 0.71 3 2.19 0.84 0.00 0.00 3.03 В 2 0.09 90 40 0.50 29 0.31 0.53 0.36 100 0.90 0.96 0.73 0.81 0.30 4 0.45 0.03 0.00 0.00 0.48 В 2 0.09 0.36 100 0.90 0.96 90 0.73 0.81 40 0.30 0.50 8 0.14 0.40 0.59 0.00 0.00 0.09 40 5 1.02 1.61 В 2 0.36 100 0.90 0.96 90 0.73 0.81 0.30 0.50 38 0.39 0.58 0.60 0.00 0.00 0.00 0.60 В 2 0.09 40 6 0.36 100 0.90 0.96 90 0.73 0.81 0.30 0.50 2 0.09 0.36 7 0.17 0.00 0.00 0.28 0.45 В 2 0.09 0.36 100 0.90 0.96 90 0.73 0.81 40 0.30 0.50 26 0.22 0.45 8 0.00 0.21 0.00 0.00 0.21 В 2 0.09 0.36 100 0.90 0.96 90 0.73 0.81 40 0.30 0.50 100 0.90 0.96 9 0.00 0.16 0.00 0.00 0.16 В 2 0.09 0.36 100 0.90 0.96 90 0.73 0.81 40 0.30 0.50 100 0.90 0.96 Pond 11.70 56 15.21 Total



COTTAGES AT MESA RIDGE	Calc'd by:	ИQJ
PROPOSED CONDITIONS	Checked by:	
LOCATION: EL PASO COUNTY, COLORADO	Date:	2/25/2022

TIME OF CONCENTRATION OVERLAND TIME (T_i) TRAVEL TIME (T_t) **TOTAL BASIN DATA** AREA (ac) LENGTH (ft) SLOPE % t_i (min) LENGTH (ft) SLOPE % V (ft/s) t_c (min) DESIGNATION C_5 C_V t_t (min) 0.53 3.65 100 2.0 8.3 20 900 2.9 3.4 4.4 12.7 100 20 3.2 2 0.57 5.02 2.0 7.7 1160 2.5 6.1 13.8 9.2 3 0.31 3.03 65 2.0 10 715 6.0 2.4 4.9 14.1 0.14 0.48 22 25.0 2.8 20 92 9.0 6.0 0.3 5.0 4 5 0.39 1.61 54 25.0 3.3 10 260 0.5 0.7 6.1 9.4 0.09 0.60 70 15.5 10 380 5.5 2.3 18.2 6 1.0 2.7 0.45 58 2.0 9.7 10 260 3.0 1.7 2.5 12.2 7 0.22 8 0.90 0.21 16 2.0 1.2 20 270 9.0 6.0 0.8 5.0 1.2 6.0 5.0 9 0.90 0.16 16 2.0 20 270 9.0 8.0



COTTAGES AT MESA RIDGE	Calc'd by:	ИОЛ
PROPOSED CONDITIONS	Checked by:	
DESIGN STORM: 5-YEAR	Date:	2/25/2022

	nkGreen																						
			DIRECT RUNOFF						TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	Cs	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	% 3LOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
		1	3.65	0.53	12.7	1.94	3.77	7.3															BASIN 1 FLOW, C&G FLOW TO DP1
																9.0	2.47	4.0	18	62	14.4	0.07	BASIN 2 FLOW @ DP1, CAPTURED IN ON GRADE 15' TYPE R INLET
	1	2	5.02	0.57	13.8	2.85	3.64	10.4					1.4	0.38	1.0					175	2.0	1.46	DP1 BYPASS FLOW, C&G FLOW TO DP5
	2	3	3.03	0.31	14.1	0.95	3.62	3.4															BASIN 3 FLOW, SWALE FLOW TO EX TYPE C INLET @ DP2
	3	4	0.48	0.14	5.0	0.07	5.17	0.3															BASIN 4 FLOW, FOLLOW HISTORIC DRAINAGE PATTERNS TO DP3
	3	-4	0.40	0.14	5.0	0.07	5.17	0.3								2.6	0.62	1.0	12	432	7.2	1.00	BASIN 5 FLOW @ DP4, CAPTURED IN TYPE C INLET, PIPE TO DP4.1
	4	5	1.61	0.39	9.4	0.62	4.22	2.6															
																11.2	3.09	1.0	18	205	7.2	0.47	COMBINED DP1 & DP4 FLOW @ DP4.1, PIPE TO DP5.1
	4.1								13.9	3.09	3.63	11.2							ļ.,				
	5								12.7	1.94	2 77	7.3				7.3	1.94	10.0	18	18	22.8	0.01	BASIN 1 FLOW @ DP5, CAPTURED IN ON GRADE 15' TYPE R INLET, PIPE TO DP5.1
	5								12.7	1.94	3.11	1.3				18.0	5.03	5.4	2/	105	16.7	0.19	COMBINED DP4.1 & DP5 @ DP5.1, PIPE TO DP9.1
	5.1								14.4	5.03	3.58	18.0				10.0	0.00	0.4		155	10.7	0.13	30MBH4EB B1 4.1 & B1 0 @ B1 0.1,1 II E 10 B1 0.1
	6	6	0.6	0.09	18.2	0.05	3.23	0.2															BASIN 6 FLOW @ DP6, FOLLOWS HISTORIC DRAINAGE PATTERNS
	7	7	0.45	0.00	40.0	0.40	0.00	0.4															DAGIN TELONICO DET FOLLONIO LIVETORIO DELIVILOS DATTERNO
	/	- /	0.45	0.22	12.2	0.10	3.83	0.4	-							1.0	0.19	2.0	19	16	10.2	0.03	BASIN 7 FLOW @ DP7, FOLLOWS HISTORIC DRAINAGE PATTERNS BASIN 8 FLOW @ DP8, CAPTURED IN 15' TYPE R INLET (ON GRADE), PIPE TO 9.1
	8	8	0.21	0.90	5.0	0.19	5.17	1.0								1.0	0.19	2.0	10	10	10.2	0.03	DP8 FLOW BY, C&G FLOW TO LANDOVER LANE SUMP INLETS
	Ť		0.2.	0.00	0.0	0.10	0.11									0.7	0.14	2.0	18	16	10.2	0.03	BASIN 9 AND DP2 FLOW BY, CAPTURED IN 10' TYPE R INLET (ON GRADE), PIPE TO DP9.1
	9	9	0.16	0.90	5.0	0.14	5.17	0.7															DP9 FLOW BY, C&G FLOW TO LANDOVER LANE SUMP INLETS
									44.0	5.07	0.50	40.1											COMPANIED DOS A DOS SI COMO DOS A DIOS TO SIVE DE LA COMO DOS A DIOS SI COMO DOS ADOS A DIOS SI COMO DOS A DIOS SI COMO DOS ADOS A DIOS A DI
<u> </u>	9.1								14.6	5.37	3.56	19.1	-						1	-	ļ	1	COMBINED DP5.1, DP8, & DP9 FLOW@ DP9.1, PIPE TO EX DETENTION POND D



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
PROPOSED CONDITIONS	Checked by:	
DESIGN STORM: 100-YEAR	Date:	2/25/2022

DIRECT RUNOFF **TOTAL RUNOFF** STREET PIPE TRAVEL TIME **REMARKS** E E DESIGN POINT C₁₀₀*A (ac) C100*A (ac) C100*A (ac) (in./ hr.) (in./ hr.) LENGTH Q (cfs) Q (cfs) BASIN 1 FLOW, C&G FLOW TO DP1 3.65 0.66 12.7 2.40 6.33 15.2 2.23 2.0 24 16 10.2 0.03 BASIN 2 FLOW @ DP1, CAPTURED IN ON GRADE 15' TYPE R INLET 6.11 1.33 5.02 0.71 13.8 3.55 21.7 8.1 280 6.0 DP1 BYPASS FLOW, C&G FLOW TO DP5 & DP9 0.78 3.03 0.53 14.1 1.59 6.07 9.7 BASIN 3 FLOW, SWALE FLOW TO EX TYPE C INLET @ DP2 3 4 0.48 0.40 0.19 8.68 BASIN 4 FLOW, FOLLOW HISTORIC DRAINAGE PATTERNS TO DP3 6.6 0.93 1.0 12 432 7.2 1.00 BASIN 5 FLOW @ DP4, CAPTURED IN TYPE C INLET, PIPE TO DP4.1 4 1.61 0.58 0.93 7.08 94 6.6 19.3 3.16 1.0 18 205 7.2 0.47 COMBINED DP1 & DP4 FLOW @ DP4.1, PIPE TO DP5.1 13.9 3.16 6.11 19.3 BASIN 1 & PORTION OF DP1 FLOW BY @ DP5, CAPTURED IN ON-GRADE 15' TYPE R INLET, PIPE TO DP5.1 14.8 2.48 10.0 18 22.8 0.01 5 14.6 3.65 5.97 21.8 7.0 1.17 9.0 250 6.0 0.69 DP5 FLOW-BY, C&G FLOW TO DP8 33.7 5.64 5.4 195 16.7 0.19 COMBINED DP4.1 & DP5 FLOW @ DP5.1, PIPE TO DP9.1 5.1 14.6 5.64 5.97 33. 6 0.6 0.36 18.2 0.22 5.42 BASIN 6 FLOW @ DP6, FOLLOWS HISTORIC DRAINAGE PATTERNS 0.45 0.45 12.2 0.20 6.42 BASIN 7 FLOW @ DP7, FOLLOWS HISTORIC DRAINAGE PATTERNS 7.7 1.31 9.0 16 21.6 0.01 BASIN 8 AND DP5 FLOW BY, CAPTURED IN ON-GRADE 15' TYPE R INLET 1.37 5.86 8.0 0.3 0.06 8 0.21 0.96 5.0 0.20 8.68 1.7 15.3 DP8 FLOW BY, C&G FLOW TO LANDOVER LANE SUMP INLETS 1.3 0.22 9.0 16 21.6 0.01 BASIN 9 AND REMAINING DP1 FLOW BY, CAPTURED IN ON-GRADE 5' TYPE R INLET, PIPE TO DP9.1 9 9 0.16 0.96 0.15 8.68 14.6 0.23 5.97 1.4 0.1 0.01 DP9 FLOW BY, C&G FLOW TO LANDOVER LANE SUMP INLETS 9.1 7.17 5.86 42. COMBINED DP2.1, DP8, & DP9 FLOW @DP9.1, PIPE TO EX DETENTION POND D



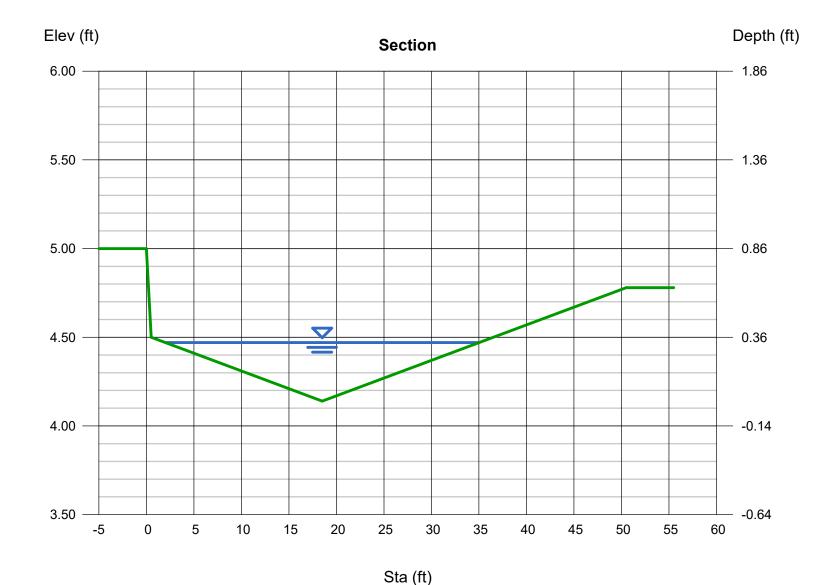


APPENDIX C - HYDRAULIC CALCULATIONS

STREET CAPACITY - APISHAPA HEIGHTS W/ BASIN 1 FLOW (Q100 = 15.0)

User-defined		Highlighted	
Invert Elev (ft)	= 4.14	Depth (ft)	= 0.33
Slope (%)	= 1.00	Q (cfs)	= 15.00
N-Value	= 0.016	Area (sqft)	= 5.44
		Velocity (ft/s)	= 2.75
Calculations		Wetted Perim (ft)	= 33.01
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.36
Known Q (cfs)	= 15.00	Top Width (ft)	= 33.00
, ,		EGL (ft)	= 0.45

(Sta, El, n)-(Sta, El, n)... (0.00, 5.00)-(0.50, 4.50, 0.016)-(18.50, 4.14, 0.016)-(50.50, 4.78, 0.016)



Channel Report

DP2 is located at the existing Box culvert. Should this be DP1 or basin 2? Please

Hydraflow Express Extension for Autodesk® Civil 3 Parify/revise accordingly.

Thursday, Feb 24 2022

= 0.43

= 3.47

= 3.00

= 0.47

= 18.95

= 10.40

MINOR STORM STREET CAPACITY HR GREEN: ADDRESSED, DP1 IS CORRECT. Let W DP2 FLOW (Q5 = 10.4) htted

Invert Elev (ft) = 9.39 Slope (%) = 1.00 N-Value = 0.016

1.00 Q (cfs)
0.016 Area (sqft)
Velocity (ft/s)
Wetted Perim (ft)
own Q Crit Depth, Yc (ft)

Compute by: Known Q Known Q (cfs) = 10.40

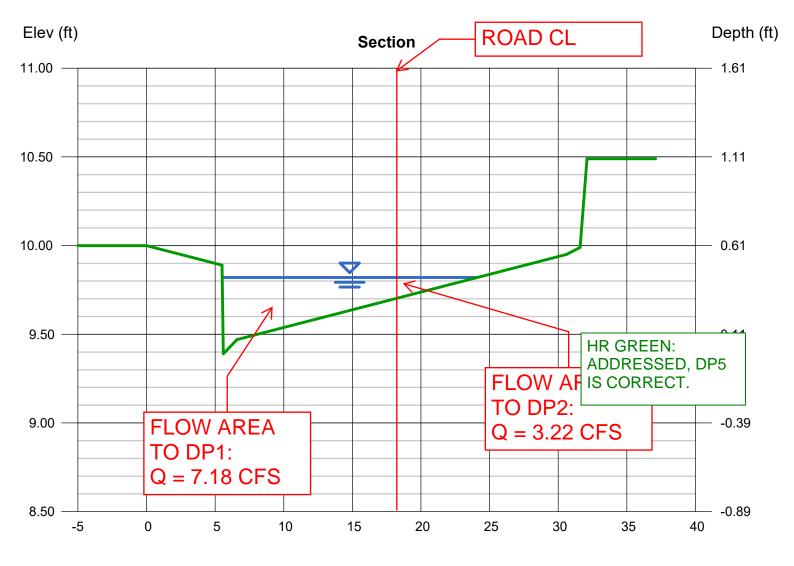
Top Width (ft) = 18.59 EGL (ft) = 0.57

ft)

(Sta, El, n)-(Sta, El, n)...

Calculations

(0.00, 10.00)-(5.50, 9.89, 0.016)-(5.60, 9.39, 0.016)-(6.60, 9.47, 0.016)-(30.60, 9.95, 0.016)-(31.60, 9.99, 0.016)-(32.10, 10.49, 0.016)



Channel Report

see comment above

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, and revise any other

sheets as necessary

HR GREEN: ADDRESSED, DP1 day, Feb 24 2022

(Q100 = 21.7)

MAJOR STORM STREET CAPACITY - SEGUNDO GRO IS CORRECT.

User-defined	
Invert Elev (ft)	= 9.39
Slope (%)	= 1.00
N-Value	= 0.016

Calculations

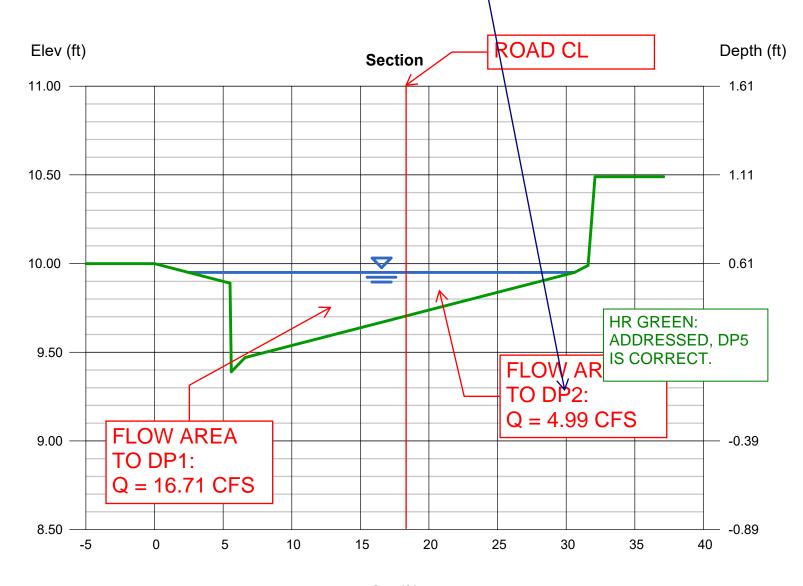
Compute by: Known Q Known Q (cfs) = 21.70

Highlighted

Depth (ft) = 0.56Q (cfs) = 21.70Area (sqft) = 6.40Velocity (ft/s) = 3.39Wetted Perim (ft) = 28.52Crit Depth, Yc (ft) = 0.61Top Width (ft) = 28.10EGL (ft) = 0.74

(Sta, El, n)-(Sta, El, n)...

(0.00, 10.00)-(5.50, 9.89, 0.016)-(5.60, 9.39, 0.016)-(6.60, 9.47, 0.016)-(30.60, 9.95, 0.016)-(\$1.60, 9.99, 0.016)-(32.10, 10.49, 0.016)



Sta (ft)

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

HR GREEN: ADDRESSED, DP1 IS CORRECT.

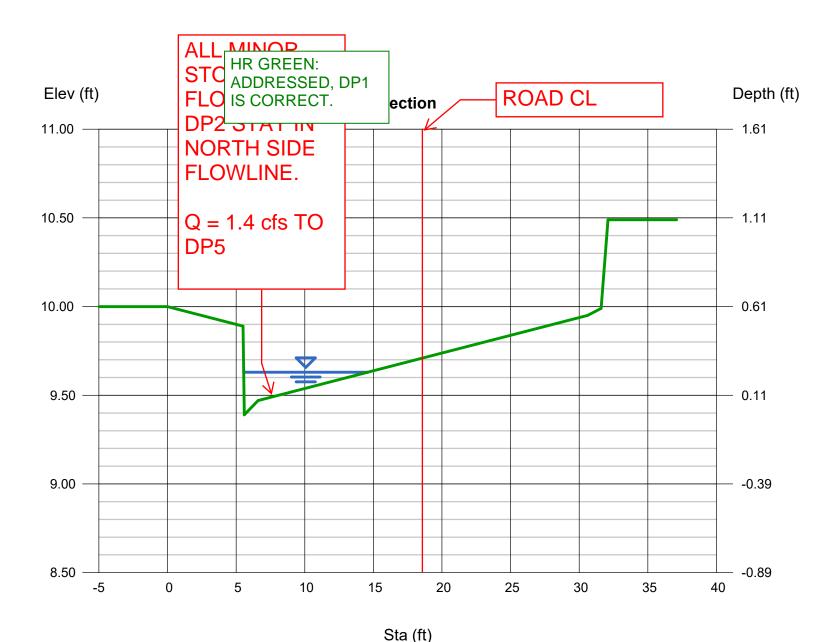
022

MINOR STORM STREET CAPACITY - SEGUNDO GROVE AFTER DP2 (Q5 = 1.4 cfs)

User-defined Highlighted Invert Elev (ft) = 9.39Depth (ft) = 0.24Slope (%) = 1.00Q (cfs) = 1.400N-Value = 0.016Area (sqft) = 0.85Velocity (ft/s) = 1.66Wetted Perim (ft) **Calculations** = 9.25Compute by: Known Q Crit Depth, Yc (ft) = 0.24Known Q (cfs) = 1.40Top Width (ft) = 9.05EGL (ft) = 0.28

(Sta, El, n)-(Sta, El, n)...

(0.00, 10.00)-(5.50, 9.89, 0.016)-(5.60, 9.39, 0.016)-(6.60, 9.47, 0.016)-(30.60, 9.95, 0.016)-(31.60, 9.99, 0.016)-(32.10, 10.49, 0.016)



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

HR GREEN: ADDRESSED, DP1 IS CORRECT.

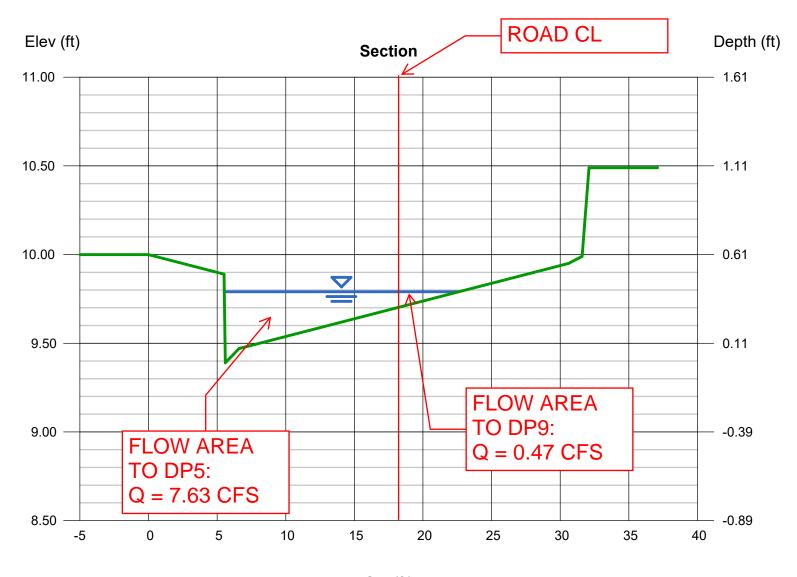
25 2022

MAJOR STORM STREET CAPACITY - SEGUNDO GROVE AFTER DP2 (Q100 = 8.1 cfs)

User-defined		Highlighted	w
Invert Elev (ft)	= 9.39	Depth (ft)	= 0.40
Slope (%)	= 1.00	Q (cfs)	= 8.100
N-Value	= 0.016	Area (sqft)	= 2.94
		Velocity (ft/s)	= 2.76
Calculations		Wetted Perim (ft)	= 17.41
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.43
Known Q (cfs)	= 8.10	Top Width (ft)	= 17.08
		EGL (ft)	= 0.52

(Sta, El, n)-(Sta, El, n)...

(0.00, 10.00)-(5.50, 9.89, 0.016)-(5.60, 9.39, 0.016)-(6.60, 9.47, 0.016)-(30.60, 9.95, 0.016)-(31.60, 9.99, 0.016)-(32.10, 10.49, 0.016)



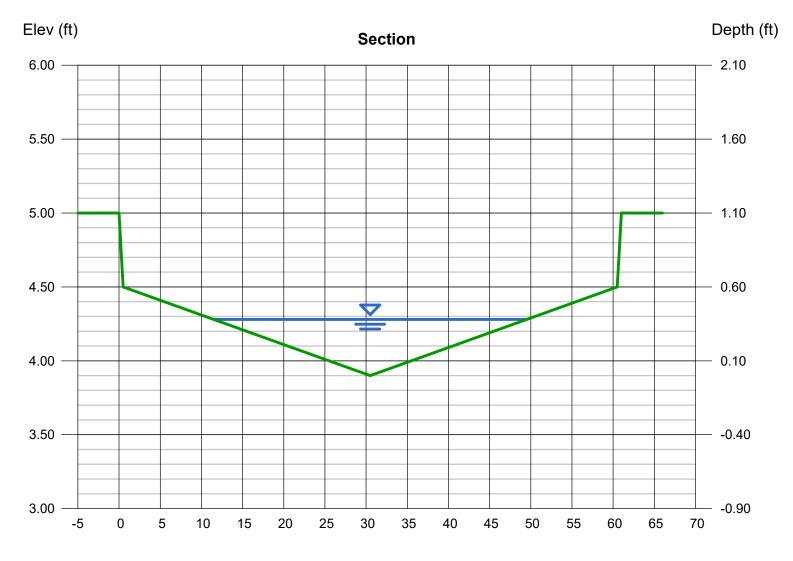
Sta (ft)

Thursday, Feb 24 2022

STREET CAPACITY - WAHATOYA POINT W/ BASIN 2 FLOW (Q100 = 21.7)

User-defined		Highlighted	
Invert Elev (ft)	= 3.90	Depth (ft)	= 0.38
Slope (%)	= 1.00	Q (cfs)	= 21.70
N-Value	= 0.016	Area (sqft)	= 7.22
		Velocity (ft/s)	= 3.01
Calculations		Wetted Perim (ft)	= 38.01
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.42
Known Q (cfs)	= 21.70	Top Width (ft)	= 38.00
		EGL (ft)	= 0.52

(Sta, EI, n)-(Sta, EI, n)... (0.00, 5.00)-(0.50, 4.50, 0.016)-(30.50, 3.90, 0.016)-(60.50, 4.50, 0.016)-(61.00, 5.00, 0.016)

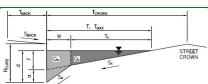


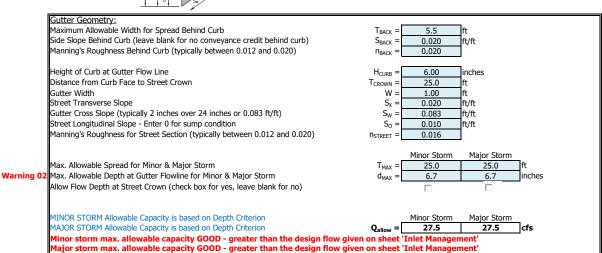
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: COTTAGES AT MESA RIDGE

Inlet ID: DP1

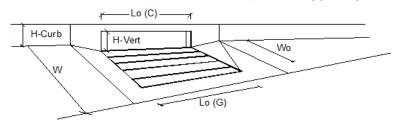




Warning 02: Max Allowable Depth for Minor Storm is greater than the Curb Height.

INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



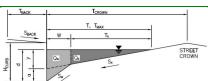
Design Information (Input) CDOT Type R Curb Opening	- [MINOR	MAJOR	1
Type of Inlet	Type =		Curb Opening	-
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - $C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	9.0	13.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	1.4	8.1	cfs
Capture Percentage = Q_a/Q_o =	C% =	87	63	%

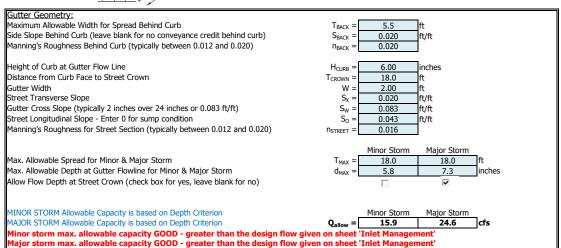
MHFD-Inlet_v5.01.xlsm, DP1 2/25/2022, 1:24 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

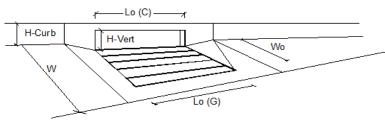
Project: COTTAGES AT MESA RIDGE Inlet ID: DP5





INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L ₀ =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	6.8	14.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	7.0	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	68	%

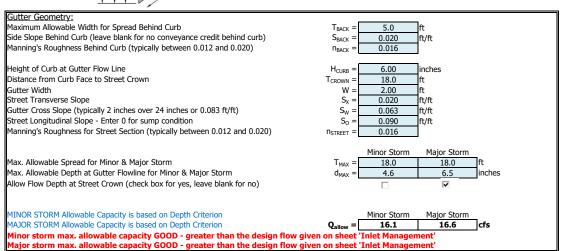
MHFD-Inlet_v5.01.xlsm, DP5 2/25/2022, 1:24 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

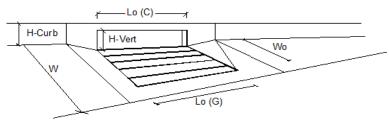
Project: COTTAGES AT MESA RIDGE Inlet ID: DP8

Tomore



INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) Type of Inlet CDOT Type R Curb Opening	Type =	MINOR CDOT Type R	MAJOR Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.0	7.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.3	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	97	%

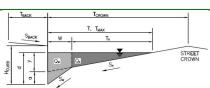
MHFD-Inlet_v5.01.xlsm, DP8 2/25/2022, 1:25 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: COTTAGES AT MESA RIDGE

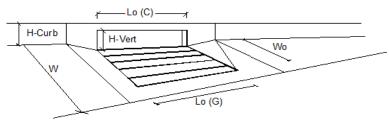
Inlet ID: DP9



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 5.0 TRACK : Side Slope Behind Curb (leave blank for no conveyance credit behind curb) ft/ft 0.020 SRACK Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 n_{rack} Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 18.0 Gutter Width 2.00 Street Transverse Slope S_X 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) $S_{W} \\$ 0.063 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S_0 0.046 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) $n_{\text{STREET}} \\$ Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 18.0 18.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm $d_{\text{MAX}} \\$ 4.6 6.5 inches Allow Flow Depth at Street Crown (check box for yes, leave blank for no) MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Major Storm Minor Storm 16.1 $Q_{allow} =$ 20.2 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management

INLET ON A CONTINUOUS GRADE

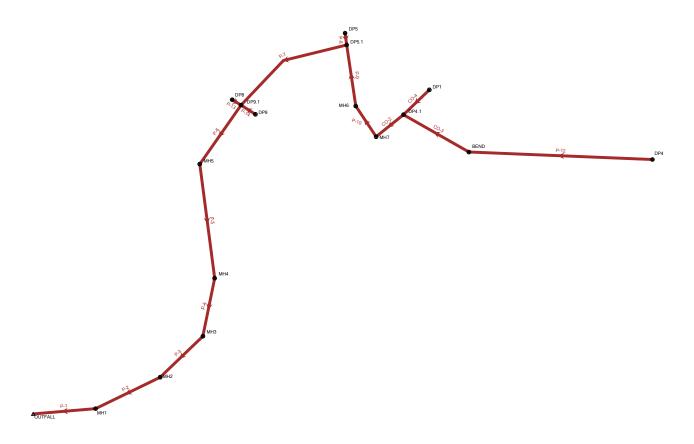
MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) Type of Inlet CDOT Type R Curb Opening	Type =	MINOR CDOT Type R	MAJOR Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.7	1.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.1	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	93	%

MHFD-Inlet_v5.01.xlsm, DP9 2/25/2022, 1:25 PM

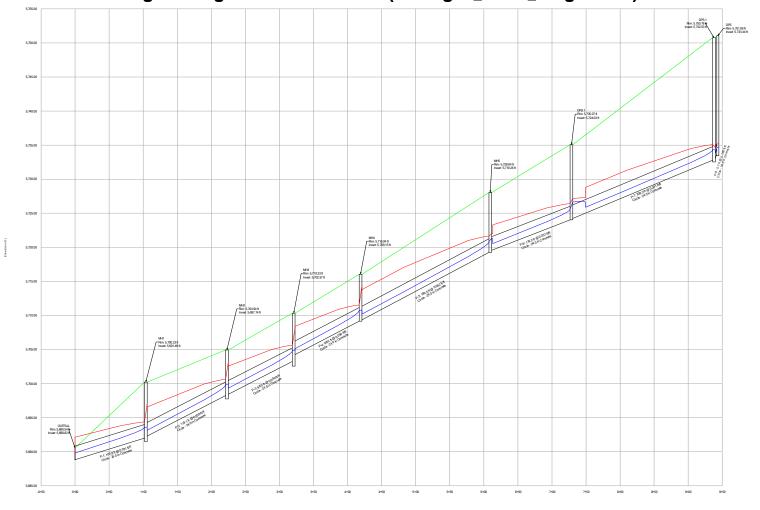
Scenario: 5-YR



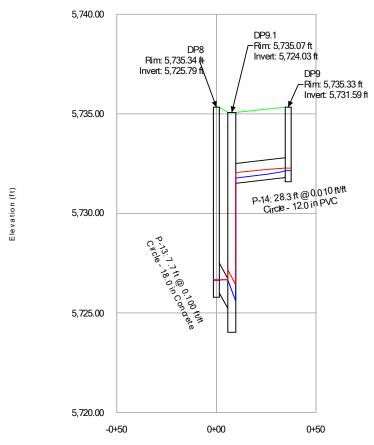
FlexTable: Conduit Table

Label	Diameter (in)	Length (Unified) (ft)	Flow (cfs)	Velocity (ft/s)	Invert (Start) (ft)	Invert (Stop) (ft)	Slope (Calculated) (ft/ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
P-10	24.0	93.9	11.20	9.46	5,736.83	5,734.85	0.021	5,738.03	5,735.66	5,738.53	5,737.03
P-9	24.0	67.8	10.80	9.47	5,734.55	5,733.08	0.022	5,735.73	5,734.31	5,736.22	5,734.75
P-8	18.0	5.7	7.30	15.09	5,733.65	5,733.08	0.100	5,734.70	5,734.31	5,735.17	5,734.65
P-12	12.0	304.5	2.60	6.66	5,743.85	5,740.70	0.010	5,744.54	5,741.20	5,744.85	5,741.89
P-13	18.0	7.7	1.00	8.41	5,726.00	5,725.23	0.100	5,726.65	5,726.67	5,726.67	5,726.67
P-14	12.0	28.3	0.70	4.29	5,731.80	5,731.51	0.010	5,732.15	5,731.77	5,732.28	5,732.05
P-6	24.0	119.2	19.10	13.46	5,724.03	5,719.56	0.037	5,725.60	5,721.35	5,726.41	5,721.99
P-5	24.0	190.5	19.10	15.19	5,719.26	5,709.35	0.052	5,720.83	5,710.19	5,721.64	5,713.78
P-4	24.0	98.0	19.10	14.98	5,709.15	5,704.25	0.050	5,710.72	5,705.12	5,711.53	5,708.40
P-3	24.0	98.0	19.10	14.87	5,703.25	5,698.44	0.049	5,704.82	5,699.32	5,705.63	5,702.55
P-2	24.0	119.1	19.10	14.98	5,698.24	5,692.29	0.050	5,699.81	5,693.15	5,700.62	5,696.58
P-1	24.0	103.8	19.10	12.47	5,691.99	5,688.82	0.031	5,693.56	5,689.82	5,694.37	5,692.12
P-7	24.0	209.2	18.00	13.69	5,732.78	5,724.23	0.041	5,734.31	5,726.67	5,735.07	5,727.18
CO-2	24.0	39.5	11.20	8.07	5,737.67	5,737.13	0.014	5,738.87	5,738.69	5,739.37	5,738.97
CO-3	18.0	117.8	2.60	6.53	5,740.20	5,738.67	0.013	5,740.81	5,739.38	5,741.04	5,739.54
CO-4	18.0	55.6	9.00	11.51	5,744.36	5,742.09	0.041	5,745.52	5,742.80	5,746.11	5,744.66

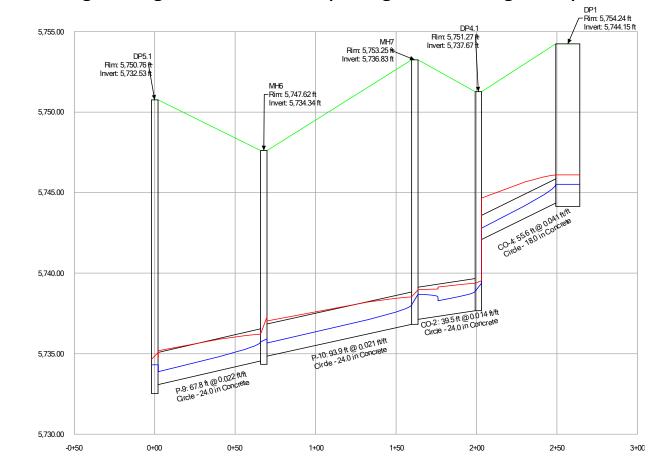
Profile Report
Engineering Profile - 02-Storm (Cottages_Mesa_Ridge.stsw)



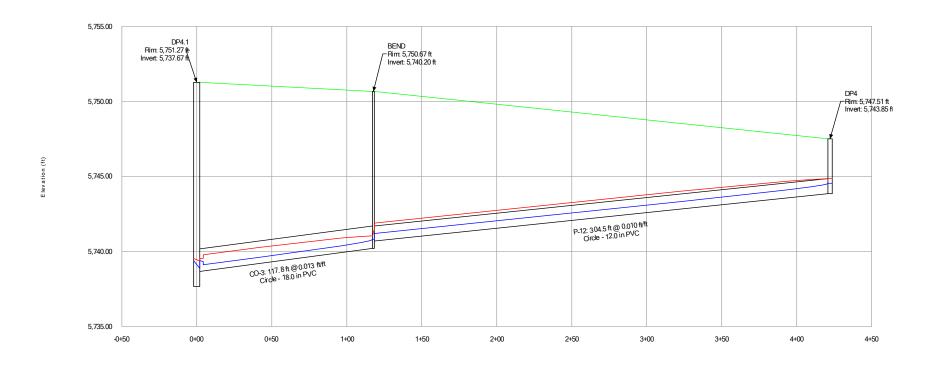
Profile Report Engineering Profile - 03-Storm (Cottages_Mesa_Ridge.stsw)



Profile Report
Engineering Profile - 04-Storm (Cottages_Mesa_Ridge.stsw)



Profile Report Engineering Profile - 05-Storm (Cottages_Mesa_Ridge.stsw)



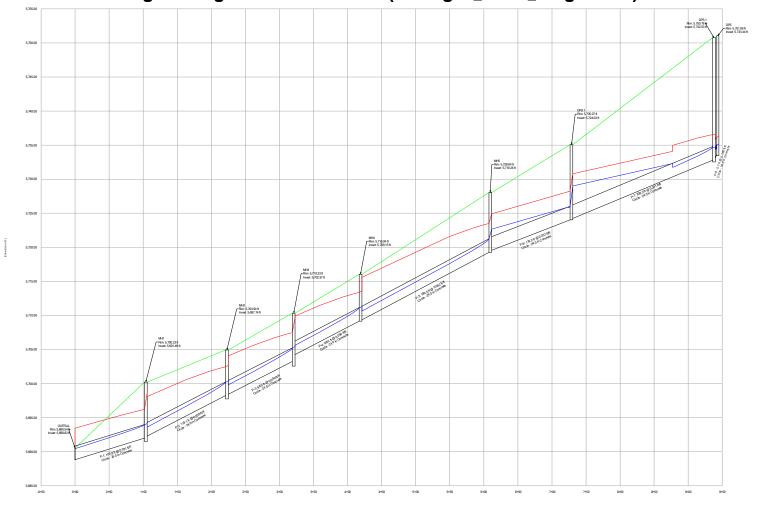
please provide label that this is the 100yr analysis.

FlexTable: Conduit Table

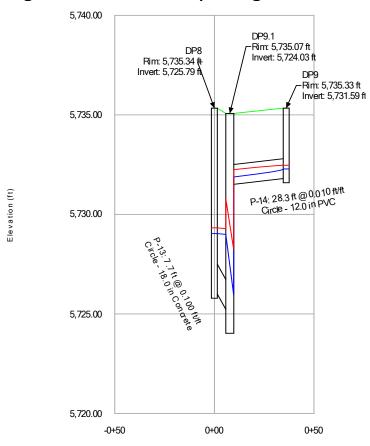
HR GREEN: ADDRESSED. MAJOR AND MINOR STORM LABELS ADDED

										LADELO	ADDED	
Label	Diameter	Length	Flow	Velocity	Invert	Invert (Stop)	Slope	Hydraulic		TO ALL		Energy
	(in)	(Unified)	(cfs)	(ft/s)	(Start)	(ft)	(Calculated)	Grade Line	9	_		Grade
		(ft)			(ft)		(ft/ft)	(In)		STORMO	JAD	Line
								(ft)		APPEND	IX	(Out)
										MATERIA		(ft)
P-10	24.0	93.9	19.30	10.88	5,736.83	5,734.85	0.021	5,738.41		WAIEKI	AL.	5,737.37
P-9	24.0	67.8	24.90	11.63	5,734.55	5,733.08	0.022	5,736.31		5,734.43	5,737.43	5,736.33
P-8	18.0	5.7	14.80	18.28	5,733.65	5,733.08	0.100	5,735.05		5,734.69	5,736.21	5,735.78
P-12	12.0	304.5	6.60	8.40	5,743.85	5,740.70	0.010	5,746.70		5,741.67	5,747.79	5,742.79
P-13	18.0	7.7	7.70	4.36	5,726.00	5,725.23	0.100	5,729.03		5,728.99	5,729.33	5,729.29
P-14	12.0	28.3	1.30	5.10	5,731.80	5,731.51	0.010	5,732.28		5,731.88	5,732.47	5,732.26
P-6	24.0	119.2	37.80	15.69	5,724.03	5,719.56	0.037	5,725.97		5,722.67	5,728.26	5,724.92
P-5	24.0	190.5	37.80	17.94	5,719.26	5,709.35	0.052	5,721.20		5,711.32	5,723.49	5,713.58
P-4	24.0	98.0	37.80	17.66	5,709.15	5,704.25	0.050	5,711.09		5,705.61	5,713.38	5,709.92
P-3	24.0	98.0	37.80	17.52	5,703.25	5,698.44	0.049	5,705.19		5,700.41	5,707.48	5,702.67
P-2	24.0	119.1	37.80	17.66	5,698.24	5,692.29	0.050	5,700.18		5,693.63	5,702.47	5,698.10
P-1	24.0	103.8	37.80	14.33	5,691.99	5,688.82	0.031	5,693.93		5,690.43	5,696.22	5,693.45
P-7	24.0	209.2	33.70	15.92	5,732.78	5,724.23	0.041	5,734.69		5,728.99	5,736.54	5,730.78
CO-2	24.0	39.5	19.30	6.14	5,737.67	5,737.13	0.014	5,739.78		5,739.49	5,740.36	5,740.07
CO-3	18.0	117.8	6.60	8.44	5,740.20	5,738.67	0.013	5,741.19		5,740.37	5,741.63	5,740.59
CO-4	18.0	55.6	13.60	12.74	5,744.36	5,742.09	0.041	5,745.73		5,743.01	5,746.73	5,745.23

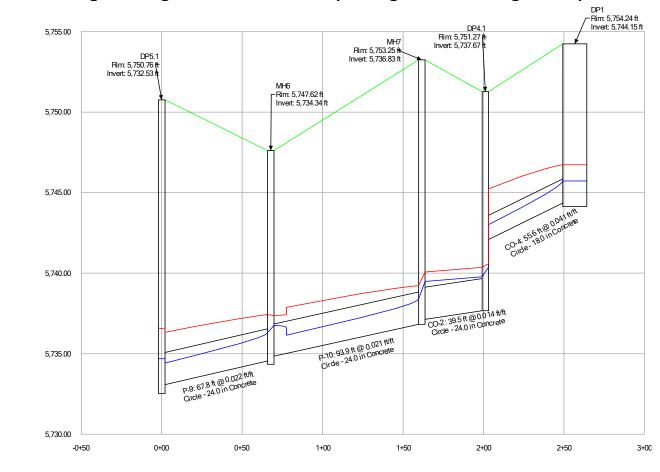
Profile Report
Engineering Profile - 02-Storm (Cottages_Mesa_Ridge.stsw)



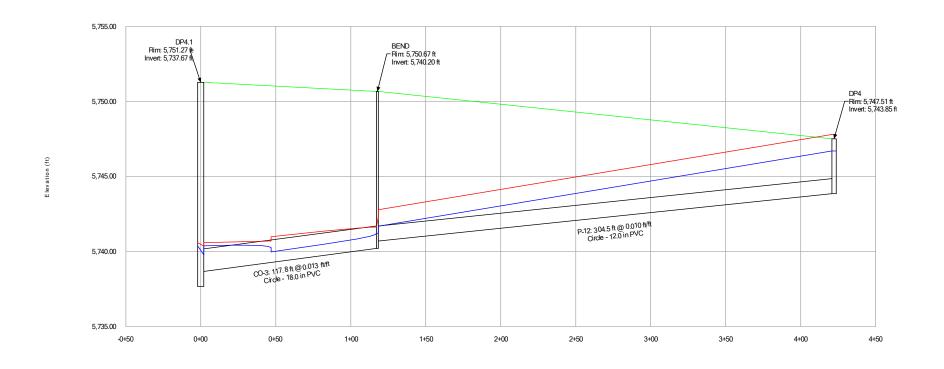
Profile Report Engineering Profile - 03-Storm (Cottages_Mesa_Ridge.stsw)



Profile Report
Engineering Profile - 04-Storm (Cottages_Mesa_Ridge.stsw)



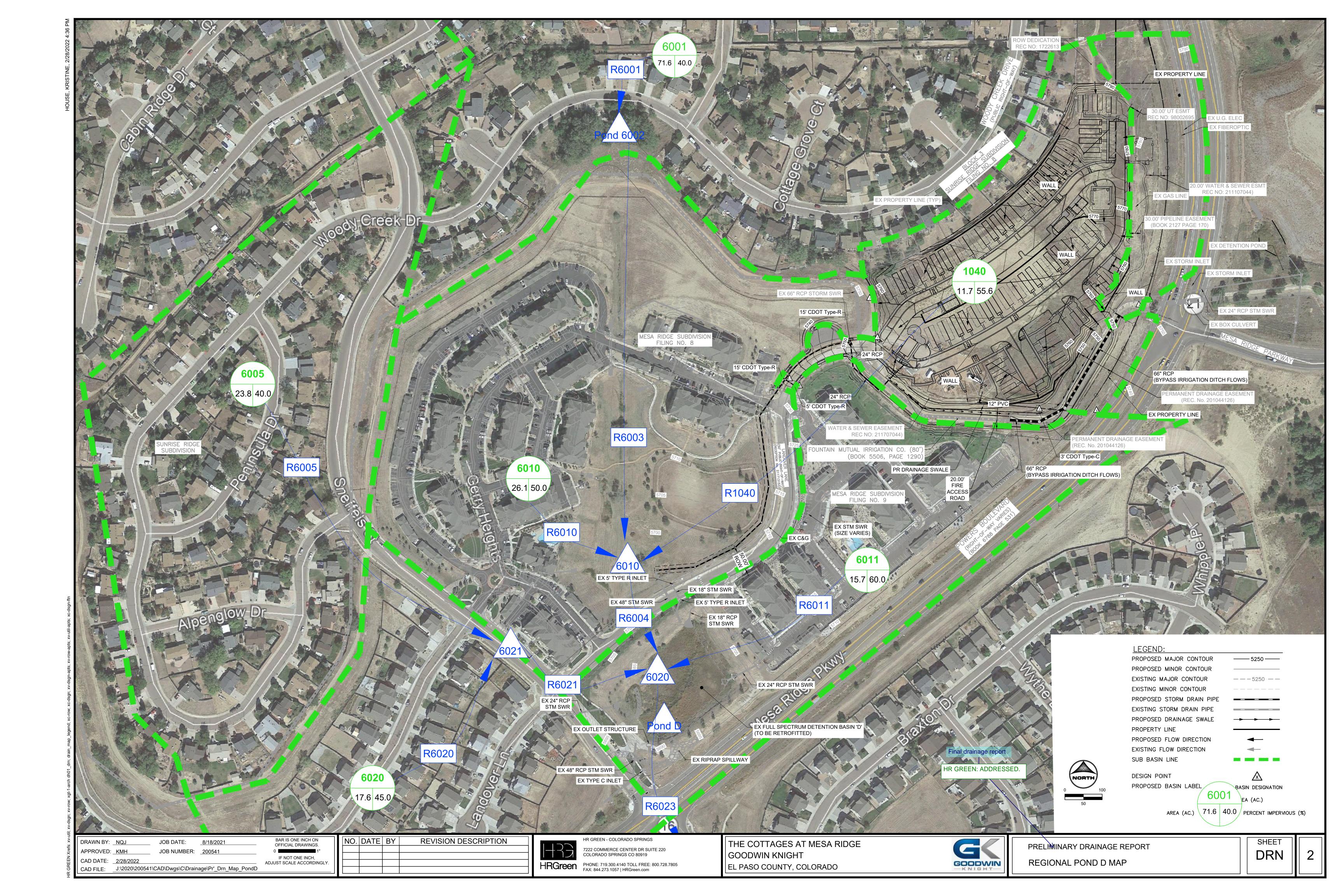
Profile Report Engineering Profile - 05-Storm (Cottages_Mesa_Ridge.stsw)







APPENDIX D - WATER QUALITY & DETENTION



Columns with this color heading are for required user-input Columns with this color heading are for optional override values Columns with this color heading are for program-calculated value

								Maximum Depression Storage (Watershed inches)			Horton's Infiltration Parameters						
Subcatchment Name	EPA SWMM Target Node	Raingage	Area (mi²)	Length to Centroid (mi)	Length (mi)	Slope (ft/ft)	Percent Imperviousness	Pervious	Impervious	Initial Rate (in/hr)	Decay Coefficient (1/seconds)	Rate	Level 0, 1, or 2	Comment			
6001	E6001	5-YR	0.112	0.2178	0.4356	0.012	40.0	0.35	0.1	4.5	0.0018	0.6	0				
6005	E6005	5-YR	0.0362	0.0786	0.2235	0.030	40.0	0.35	0.1	4.5	0.0018	0.6	0				
6010	E6010	5-YR	0.0433	0.1009	0.2216	0.049	50.0	0.35	0.1	4.5	0.0018	0.6	0	Updated imperviousness to include open space			
6011	E6011	5-YR	0.0267	0.1621	0.3136	0.036	60.0	0.35	0.1	4.5	0.0018	0.6	0				
6020	E6020	5-YR	0.0300	0.1345	0.2083	0.050	45.0	0.35	0.1	4.5	0.0018	0.6	0	Updated to single-family imperviousness			
1040	E1040	5-YR	0.0183	0.0758	0.1894	0.022	55.6	0.35	0.1	4.5	0.0018	0.6	0	Updated for new size and imperviousness			

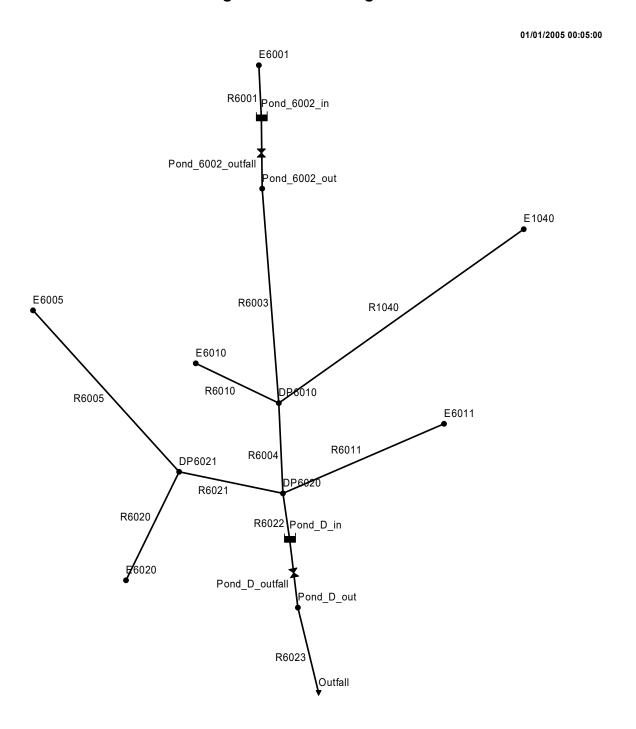
Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

			Unit Hydrograph Parameters and Results				Excess	Precip.		Storm H	ydrograph					
Catchment Name/ID	User Comment for Catchment	СТ	Ср	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
6,001		0.094	0.175	23.6	3.47	12.3	2.45	5.8	142	260,198	0.56	145,367	34.0	45	145,362	0.62
6,005		0.094	0.105	14.0	1.43	7.3	1.01	2.4	77	84,100	0.56	46,985	31.0	21	46,984	0.89
6,010	Updated imperviousness to include open space	0.089	0.130	10.7	1.37	5.6	0.97	2.3	121	100,595	0.68	68,520	30.0	33	68,523	1.21
6,011		0.085	0.114	18.5	1.92	9.6	1.35	3.2	43	62,029	0.81	49,990	31.0	17	49,984	0.99
6,020	Updated to single-family imperviousness	0.092	0.104	15.2	1.52	7.9	1.07	2.5	59	69,696	0.62	43,184	31.0	17	43,176	0.91
1,040	Updated for new size and imperviousness	0.087	0.093	14.2	1.32	7.4	0.93	2.2	39	42,515	0.75	31,912	31.0	13	31,917	1.10

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

			Unit Hydrograph Parameters and Results			Excess	Precip.		Storm H	ydrograph						
Catchment Name/ID	User Comment for Catchment	ст	Ср	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
6,001		0.094	0.178	23.1	3.45	12.0	2.44	5.7	146	260,198	2.09	542,819	40.0	173	542,806	2.41
6,005		0.094	0.107	13.7	1.42	7.1	1.01	2.4	79	84,100	2.09	175,447	36.0	77	175,455	3.32
6,010	Updated imperviousness to include open space	0.089	0.131	10.5	1.36	5.5	0.96	2.3	123	100,595	2.22	223,481	35.0	110	223,473	3.96
6,011		0.084	0.115	18.3	1.91	9.5	1.35	3.2	44	62,029	2.36	146,231	37.0	51	146,214	2.99
6,020	Updated to single-family imperviousness	0.091	0.105	15.0	1.51	7.8	1.07	2.5	60	69,696	2.15	150,108	36.0	62	150,075	3.21
1,040	Updated for new size and imperviousness	0.086	0.094	14.1	1.31	7.3	0.93	2.2	39	42,515	2.30	97,677	35.0	40	97,703	3.45

The Cottages at Mesa Ridge



SWMM 5.1 Page 1

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

WARNING 04: minimum elevation drop used for Conduit R6022

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units ... CFS
Process Models:
 Rainfall/Runoff NO
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO

Antecedent Dry Days 0.0
Report Time Step 00:05:00
Routing Time Step 60.00 sec

All links are stable.

Minimum Time Step : 60.00 sec
Average Time Step : 60.00 sec
Maximum Time Step : 60.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.12
Percent Not Converging : 0.00

| Node | Type | Peet |

should be final drainage report

HR GREEN: ADDRESSED



EPA SWMM Results - 100-

DP6010	JUNCTION	0.48	3.15	5691.34	0	00:42	3.09
DP6021	JUNCTION	0.18	2.13	5693.32	0	00:37	2.09
DP6020	JUNCTION	0.48	3.15	5686.84	0	00:42	3.07
Pond D out	JUNCTION	0.19	1.04	5683.63	0	01:14	1.04
Pond 6002 out	JUNCTION	0.18	1.25	5749.71	0	00:59	1.24
Outfall	OUTFALL	0.19	1.04	5673.88	0	01:14	1.04
Pond 6002 in	STORAGE	4.90	9.61	5759.07	0	00:59	9.61
Pond_D_in	STORAGE	5.51	10.37	5694.06	0	01:14	10.37

Node Inflow Summary

		Maximum	Maximum			Lateral	Total	Flow
		Lateral	Total	Time	of Max	Inflow	Inflow	Balance
		Inflow	Inflow	0cci	rrence	Volume	Volume	Error
Node	Type	CFS	CFS	days	hr:min	10^6 gal	10^6 gal	Percent
E6005	JUNCTION	76.91	76.91		00:37	1.31	1.31	0.000
E6010	JUNCTION	109.76	109.76	0	00:36	1.67	1.67	0.000
				•				
E6001	JUNCTION	172.95	172.95	0	00:41	4.06	4.06	0.000
E1040	JUNCTION	40.35	40.35	0	00:36	0.731	0.731	0.000
E6011	JUNCTION	51.06	51.06	0	00:38	1.09	1.09	0.000
E6020	JUNCTION	61.62	61.62	0	00:37	1.12	1.12	0.000
DP6010	JUNCTION	0.00	232.79	0	00:42	0	6.28	0.000
DP6021	JUNCTION	0.00	138.54	0	00:37	0	2.43	0.000
DP6020	JUNCTION	0.00	413.44	0	00:41	0	9.8	0.000
Pond_D_out	JUNCTION	0.00	228.07	0	01:14	0	8.19	0.000
Pond_6002_out	JUNCTION	0.00	136.68	0	00:59	0	3.87	0.000
Outfall	OUTFALL	0.00	228.05	0	01:14	0	8.18	0.000
Pond_6002_in	STORAGE	0.00	172.95	0	00:41	0	4.06	0.152
Pond_D_in	STORAGE	0.00	413.44	0	00:41	0	9.8	0.048

No nodes were flooded.

Storage Unit	Average Volume 1000 ft3	_	Pcnt	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CFS
Pond_6002_in Pond D in	45.849 277.085	16 36	0	0 0	126.976 631.133	45 82	0 00:59 0 01:13	136.68

	Flow Freq	Avg Flow	Max Flow	Total Volume
Outfall Node	Pont	CFS	CFS	10^6 gal
Outfall	98.06	25.83	228.05	8.184
System	98.06	25.83	228.05	8.184

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
R1040	CONDUIT	40.05	0 00:38	6.12	0.01	0.11
R6003	CONDUIT	136.55	0 01:01	8.00	0.06	0.25

EPA SWMM Results - 100-y

/e	HR GREEN:
	ADDRESSED

R6004	CONDUIT	232.57	0	00:42	19.57	0.84	0.70
R6005	CONDUIT	76.92	0	00:37	17.52	0.67	0.60
R6011	DUMMY	51.06	0	00:38			
R6010	DUMMY	109.76	0	00:36			
R6021	CONDUIT	138.54	0	00:37	20.33	0.56	0.53
R6020	DUMMY	61.62	0	00:37			
R6001	DUMMY	172.95	0	00:41			
R6022	DUMMY	413.44	0	00:41			
R6023	CONDUIT	228.05	0	01:14	18.27	0.10	0.17
Pond_6002_outfall	DUMMY	136.68	0	00:59			
Pond_D_outfall	DUMMY	228.07	0	01:14			

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Mon Feb 28 16:14:51 2022 Analysis ended on: Mon Feb 28 16:14:51 2022 Total elapsed time: < 1 sec

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

pond bottom

5682.4

Optional User Overrides acre-feet acre-feet

inches

inches

inches

inches

inches

inches

inches

1.00

1.28

1.55

1.97

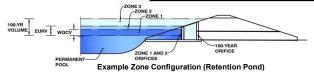
2.34

2.74

3.84

Project: Mesa Ridge Cottages

Basin ID: Existing Pond D Sizing Confirmation



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	98.80	acres
Watershed Length =	4,090	ft
Watershed Length to Centroid =	2,000	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	48.80%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.							
1.671	acre-feet						
5.144	acre-feet						
3.741	acre-feet						
5.462	acre-feet						
7.357	acre-feet						
11.295	acre-feet						
14.367	acre-feet						
18.116	acre-feet						
27.672	acre-feet						
3.247	acre-feet						
4.538	acre-feet						
6.263	acre-feet						
7.639	acre-feet						
8.436	acre-feet						
9.873	acre-feet						
	1.671 5.144 3.741 5.462 7.357 11.295 14.367 18.116 27.672 3.247 4.538 6.263 7.639 8.436						

Define Zones and Basin Geometry

Zone 1 Volume (User Defined) =	5.14	acre-feet
Zone 2 Volume (User Defined - Zone 1) =	0.32	acre-feet
Zone 3 Volume (User Defined - Zones 1 & 2) =	6.10	acre-feet
Total Detention Basin Volume =	11.57	acre-feet

100 VP FC01 16 0 76	11.57	
Depth Increment = ft 100-YR 5691.16 8.76		
Optional Optional	-	I
Stage - Storage Stage Override Length Width Area Override Description (ft) Stage (ft) (ft) (ft) (ft ²) Area (ft ²)	Area (acre)	

Elevation

EURV (FSV) 5687.18

Stage

4.78

Volume

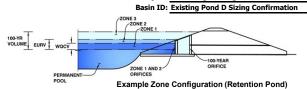
5.14

Depth Increment =		ft		100-YR	5691.16	8.76	11.57		
		Optional				Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft 2)	(acre)	(ft ³)	(ac-ft)
Top of Micropool		0.00				0	0.000		
5684.00		1.60				50,745	1.165	40,595	0.932
5685.00		2.60				55,231	1.268	93,583	2.148
5686.00		3.60				58,662	1.347	150,529	3.456
5687.00		4.60				64,191	1.474	211,956	4.866
5688.00		5.60				67,213	1.543	277,658	6.374
5689.00		6.60				70,292	1.614	346,410	7.952
5690.00		7.60				73,458	1.686	418,285	9.603
5691.00		8.60				73,831	1.695	491,930	11.293
5692.00		9.60				80,094	1.839	568,892	13.060
5693.00		10.60				83,415	1.915	650,647	14.937
5694.00		11.60				87,173	2.001	735,941	16.895
		-						-	

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Mesa Ridge Cottages



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (User)	4.79	5.144	Orifice Plate
Zone 2 (User)	5.01	0.318	Orifice Plate
Zone 3 (User)	8.76	6.104	Weir&Pipe (Rect.)
•	Total (all zones)	11.566	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = inches

11.500	1		
		Calculated Parame	ters for Underdrain
Underdi	rain Orifice Area =		ft ²
Underdrain	Orifice Centroid =		feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = 4.46 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parame	ters for Plate
N/A	ft ²
N/A	feet
N/A	feet
N/A	ft ²
	N/A N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.85	1.19	1.52	1.85	2.19	2.52	2.85	3.19
Orifice Area (sq. inches)	3.93	3.93	3.93	3.93	3.93	3.93	3.93	3.93

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		0.00	0.00	0.00	0.00	0.00	0.00	0.00
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A

Calculated Parameters for Vertical Orifice Not Selected Not Selected ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = inches

User Input: Overflow Weir (Dropbox with Flat o	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.46	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t =	6.46	N/A	feet
Overflow Weir Front Edge Length =	12.00	N/A	feet Overflow Weir Slope Length =	6.32	N/A	feet
Overflow Weir Grate Slope =	3.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	3.34	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Grate Open Area w/o Debris =	60.03	N/A	ft ²
Overflow Grate Type =	Close Mesh Grate	N/A	Overflow Grate Open Area w/ Debris =	60.03	N/A	ft ²
Debris Clogging % =	0%	N/A	%			-

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, R	estrictor Plate, or	Rectangular Orifice)	rs for Outlet Pipe w/ Flow Restriction Plate			
	Zone 3 Rectangulai	Not Selected			Zone 3 Rectangular	Not Selected	
Depth to Invert of Outlet Pipe =	1.21	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	18.00	N/A	ft ²
Rectangular Orifice Width =	72.00	N/A	inches	Outlet Orifice Centroid =	1.50	N/A	feet
Rectangular Orifice Height =	36.00		inches Half-Central Angle o	of Restrictor Plate on Pipe =	N/A	N/A	radians

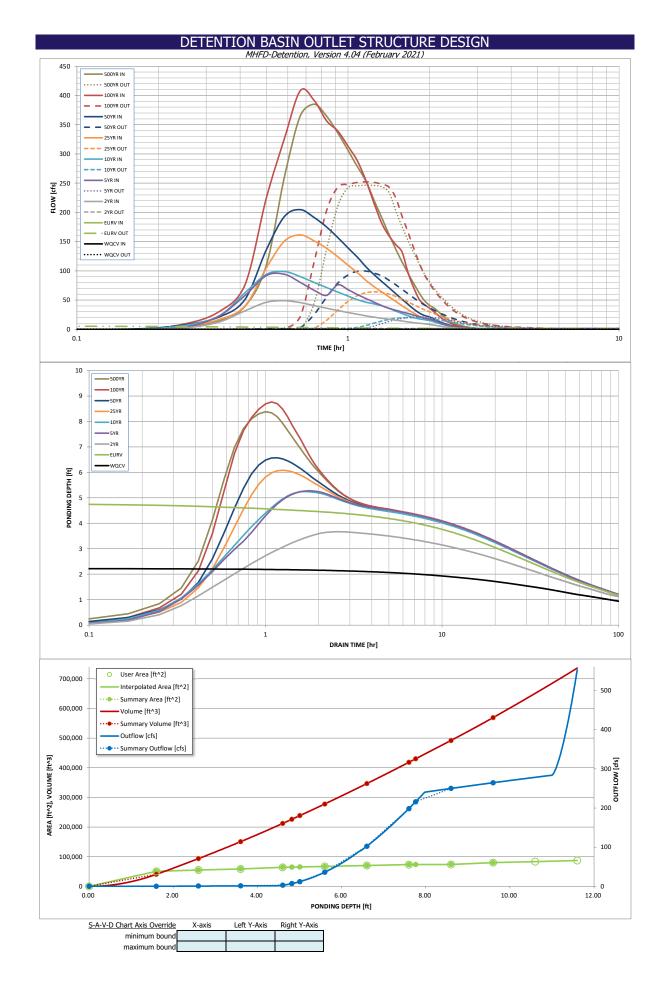
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	11.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	185.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.40	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth= 0.59 feet Stage at Top of Freeboard = 11.99 feet Basin Area at Top of Freeboard 2.00 acres Basin Volume at Top of Freeboard = 16.89 acre-ft

Routed Hydrograph Results	The user can over	rride the default CUI	HP hydrographs ar	nd runoff volumes b	y entering new valt	ues in the Inflow H	ydrographs table (C	Columns W through	h AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.00	1.28	1.55	1.97	2.34	2.74	3.84
CUHP Runoff Volume (acre-ft) =	1.671	5.144	3.741	5.462	7.357	11.295	14.367	18.116	27.672
User Override Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	3.741	7.663	7.357	11.295	14.367	29.508	27.672
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	11.3	25.6	67.8	94.1	127.9	209.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.11	0.26	0.69	0.95	1.29	2.12
Peak Inflow Q (cfs) =	N/A	N/A	48.9	94.1	98.7	161.4	204.6	407.9	385.0
Peak Outflow Q (cfs) =	0.5	6.0	1.3	21.3	20.1	64.1	99.5	252.3	246.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.9	0.8	0.9	1.1	2.0	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	0.08	N/A	0.3	0.3	1.0	1.6	4.2	4.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	>120	>120	>120	>120	>120	>120	116	71	74
Time to Drain 99% of Inflow Volume (hours) =	>120	>120	>120	>120	>120	>120	>120	>120	>120
Maximum Ponding Depth (ft) =	2.22	4.79	3.66	5.27	5.24	6.08	6.57	8.76	8.38
Area at Maximum Ponding Depth (acres) =	1.23	1.49	1.35	1.52	1.52	1.58	1.61	1.72	1.69
Maximum Volume Stored (acre-ft) =	1.674	5.147	3.537	5.869	5.823	7.107	7.888	11.566	10.904
Equivalent Elevation (ft) =		5687.19	5686.06	5687.67	5687.64	5688.48	5688.97	5691.16	
Pond Bottom (ft) =	5682.400								



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	USER	CUHP	CUHP	CUHP	USER	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]		50 Year [cfs]	100 Year [cfs]	
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 111111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.70	0.00	3.09
	0:15:00	0.00	0.00	2.43	3.68	6.53	5.30	7.67	9.15	14.49
	0:20:00	0.00	0.00	12.29	22.29	22.28	16.37	20.88	29.83	38.98
	0:25:00	0.00	0.00	31.51	57.69	62.37	39.54	50.87	75.72	109.68
	0:30:00	0.00	0.00	46.16	91.81	93.76	105.05	136.02	224.60	260.83
	0:35:00	0.00	0.00	48.87	94.12	98.66	150.75	193.05	326.49	365.14
	0:40:00	0.00	0.00	45.61	80.25	90.11	161.36	204.64	407.93	385.04
	0:45:00	0.00	0.00	40.59	66.76	80.26	151.30	191.18	391.67	364.86
	0:50:00 0:55:00	0.00	0.00	35.99 32.15	58.09	71.47 63.78	138.64	175.05	356.83	336.13
	1:00:00	0.00	0.00	28.77	76.08 67.82	56.86	124.09 109.79	157.03 139.37	339.23 313.47	306.19 278.30
	1:05:00	0.00	0.00	25.79	59.43	50.69	96.85	123.27	288.08	252.85
	1:10:00	0.00	0.00	23.01	52.50	46.30	83.54	106.61	253.54	220.13
	1:15:00	0.00	0.00	20.74	46.35	43.41	72.79	93.34	214.87	190.34
	1:20:00	0.00	0.00	18.86	40.52	40.10	63.61	81.64	180.99	162.52
	1:25:00	0.00	0.00	17.22	36.01	35.76	55.52	71.12	160.14	137.32
	1:30:00	0.00	0.00	15.66	32.65	31.27	47.74	60.92	145.01	115.32
	1:35:00	0.00	0.00	14.12	29.66	27.06	40.42	51.35	132.08	95.75
	1:40:00	0.00	0.00	12.62	27.15	23.26	33.66	42.55	96.68	77.90
	1:45:00 1:50:00	0.00	0.00	11.30	24.16	19.99 17.80	27.50	34.55	70.46	61.83
	1:55:00	0.00	0.00	10.40 9.39	21.51 19.21	16.39	22.22 18.85	27.75 23.57	50.89 42.17	48.98 41.05
	2:00:00	0.00	0.00	8.38	17.41	15.05	16.81	20.99	36.08	35.98
	2:05:00	0.00	0.00	7.01	14.97	12.69	13.93	17.36	29.63	29.23
	2:10:00	0.00	0.00	5.61	11.89	10.11	10.84	13.48	22.74	22.26
	2:15:00	0.00	0.00	4.44	9.04	7.93	8.34	10.34	16.89	16.62
	2:20:00	0.00	0.00	3.50	7.02	6.20	6.43	7.94	12.61	12.36
	2:25:00	0.00	0.00	2.75	5.27	4.81	4.94	6.07	9.30	9.21
	2:30:00	0.00	0.00	2.14	4.09	3.67	3.78	4.62	6.83	6.99
	2:35:00	0.00	0.00	1.67	3.12	2.78	2.86	3.48	4.99	5.26
	2:40:00 2:45:00	0.00	0.00	1.28 0.98	2.39 1.78	2.10 1.61	2.16 1.65	2.62	3.71 2.77	4.01 3.10
	2:50:00	0.00	0.00	0.72	1.76	1.01	1.05	1.51	2.77	2.33
	2:55:00	0.00	0.00	0.51	1.22	0.86	0.90	1.09	1.53	1.67
	3:00:00	0.00	0.00	0.34	1.11	0.58	0.61	0.74	1.24	1.12
	3:05:00	0.00	0.00	0.20	1.06	0.35	0.38	0.45	1.11	0.67
	3:10:00	0.00	0.00	0.10	1.03	0.18	0.20	0.24	1.05	0.34
	3:15:00	0.00	0.00	0.04	1.02	0.07	0.08	0.09	1.03	0.12
	3:20:00	0.00	0.00	0.01	1.02	0.01	0.01	0.01	1.02	0.00
	3:25:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.02	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:40:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:45:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:50:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:55:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:00:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:05:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:20:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:25:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:40:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:45:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	1.00 1.00	0.00	0.00	0.00	1.00	0.00
	5:00:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

The aser should grapmeany t	,	,	bic to the fail 5			iiiiiii ic captares	_
Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
	0.00	0	0.000	0	0.000	0.00	Foi
		50,745	1.165	40,595	0.932	0.24	sta
	1.60	55,231	1.268	93,583	2.148	0.70	cha
	2.60	58,662	1.347		3.456	1.28	fro
	3.60			150,529 211,956	4.866		_Sh
FUD: ((50)	4.60	64,191 64,856	1.474 1.489	· ·	5.192	2.89 7.01	
EURV (FS)	4.82	65,430	1.502	226,151 238,528	5.192	12.09	Als
5-Year	5.01					35.96	ove
	5.60	67,213 70,292	1.543 1.614	277,658 346,410	6.374 7.952	102.27	wh
	6.60 7.60	73,458	1.686	418,285	9.603	198.34	+
100 Voor	7.76	73,518	1.688	430,043	9.872	215.81	-
100-Year	8.60	73,831	1.695	491,930	11.293	249.84	-
	9.60	80,094	1.839	568,892	13.060	264.45	-
	9.00	00,054	1.055	300,032	15.000	204.43	
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or best results, include the tages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on heet 'Basin'.

Also include the inverts of all butlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

pond bottom

5682.4

Project: Mesa Ridge Cottages

Basin ID: Existing Pond D Sizing Confirmation - with Structure Modifications

Optional User Overrides

1.00

1.28

1.55

1.97

2.34

2.74

3.84

acre-feet

inches

inches

inches

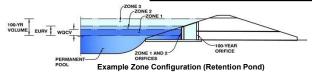
inches

inches

inches

inches

acre-feet



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	98.90	acres
Watershed Length =	4,090	ft
Watershed Length to Centroid =	2,000	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	49.08%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Denths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) = 1.679 acre-feet Excess Urban Runoff Volume (EURV) = 5.181 acre-feet 2-yr Runoff Volume (P1 = 1 in.) = 3.768 acre-feet 5-yr Runoff Volume (P1 = 1.28 in.) = 5.495 acre-feet 10-yr Runoff Volume (P1 = 1.55 in.) = 7.395 acre-feet 25-yr Runoff Volume (P1 = 1.97 in.) = 11.334 acre-feet 50-yr Runoff Volume (P1 = 2.34 in.) = 14.409 acre-feet 100-yr Runoff Volume (P1 = 2.74 in.) = 18.159 acre-feet 500-vr Runoff Volume (P1 = 3.84 in.) = 27.727 acre-feet Approximate 2-yr Detention Volume = 3.272 acre-feet Approximate 5-yr Detention Volume = 4.571 acre-feet Approximate 10-yr Detention Volume = 6.303 acre-feet 7.685 Approximate 25-yr Detention Volume = acre-feet Approximate 50-yr Detention Volume = 8.485 acre-feet Approximate 100-yr Detention Volume =

Define Zones and Basin Geometry

Zone 1 Volume (User Defined) =	5.19	acre-feet
Zone 2 Volume (User Defined - Zone 1) =	1.37	acre-feet
Zone 3 Volume (User Defined - Zones 1 & 2) =	7.93	acre-feet
Total Detention Basin Volume =	14.49	acre-feet

				5-Yr	5688.19	5.79	6.56	
Depth Increment =		ft		100-YR	5692.82	10.42	14.49	
		Optional				Optional		T
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	ı
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft 2)	(acre)	l
		0.00				•	0.000	I

Volume

5.19

Elevation

EURV (FSV) 5687.29

Stage

4.89

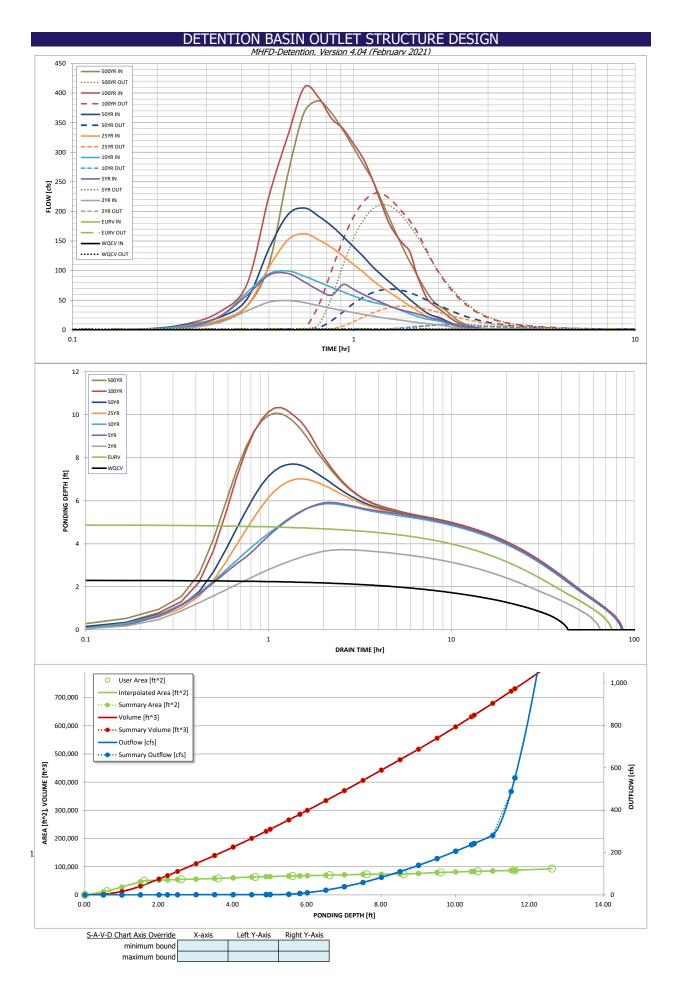
Depth Increment =		ft		100-YR	5692.82	10.42	14.49		
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool		0.00				0	0.000	(17)	(23.13)
5683.0		0.60	-		-	13,215	0.303	3,964	0.091
5684.0		1.60			-	50,745	1.165	35,944	0.825
5685.0		2.60				55,231	1.268	88,932	2.042
5686.0		3.60				58,662	1.347	145,878	3.349
5687.0		4.60				64,191	1.474	207,305	4.759
5688.0		5.60				67,213	1.543	273,007	6.267
5689.0		6.60			-	70,292	1.614	341,759	7.846
5690.0		7.60				73,458	1.686	413,634	9.496
5691.0		8.60				73,831	1.695	487,279	11.186
5692.0		9.60				80,094	1.839	564,241	12.953
5693.0		10.60	-		-	83,808	1.924	646,192	14.835
5694.0	-	11.60	-		-	87,413	2.007	731,803	16.800
5695.0	-	12.60	-		-	93,285	2.142	822,152	18.874

DETENTION BASIN OUTLET STRUCTU HR GREEN: MHFD-Detention, Version 4.04 (February 202 ADDRESSED This does not match Project: Mesa Ridge Cottages Basin ID: Existing Pond D Sizing Confirmation - with Structure Modifications OUTLET he orifices shown on Estimated **STRUCTURE** the modified orifice Volu Stage (ft) Zone 1 (User) 4.89 **DETAIL HAS** plate on the CD's as it -100-YEAR Zone 2 (User) 5.80 **BEEN UPDATED** still shows the Zone 3 (User) 10.43 AND REFLECTS existing nine rows. Example Zone Configuration (Retention Pond) Total (all zones) <u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u> **UD-DETENTION** Please for Endistrain Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) **AS SHOWN** accordingly so that Underdrain Orifice Diameter = they match User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) WQ Orifice Area per Row Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) N/A ft2 Depth at top of Zone using Orifice Plate = 5.80 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = N/A feet Orifice Plate: Orifice Vertical Spacing = N/A inches Elliptical Slot Centroid N/A feet Elliptical Slot Area Orifice Plate: Orifice Area per Row = N/A inches N/A ft² User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 5 (optional) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid 0.00 0.81 Orifice Area (sq. inches) 7.60 5.00 5.00 5.00 2.00 Aow 9 (optional) Row 10 (optional) Row 10 (optional) Row 12 (optional) 1 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft' Orifice Area (sq. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected SEE CONSTRUCTION Invert of Vertical Orifice = N/A N/A ft (relative to basin bottom at e Area N/A N/A ft² **DOCUMENTS FOR** Depth at top of Zone using Vertical Orifice = N/A N/A ft (relative to basin bottom at entroid = N/A N/A feet MODIFICATIONS TO Vertical Orifice Diameter = N/A N/A inches **EX ORIFICE PLATE** User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Zone 3 Weir Not Selected Not Selected Overflow Weir Front Edge Height, Ho = 5.24 Height of Grate Upper Edge, Ht = 7.24 N/A feet N/A ft (relative to basin bottom at Stage = 0 ft) Overflow Weir Front Edge Length = 12.00 N/A feet Overflow Weir Slope Length = 6.32 N/A feet 3.00 H:V Grate Open Area / 100-yr Orifice Area = Overflow Weir Grate Slope = N/A 2.93 N/A Horiz. Length of Weir Sides = 6.00 N/A feet n Area w/o Debris : 52.82 N/A SEE CONSTRUCTION Type C Grate Overflow Grate Type = N/A en Area w/ Debris = 52.82 N/A ft^2 **DOCUMENTS FOR** Debris Clogging % = 0% N/A **MODIFICATIONS TO** EX OUTLET STRUCT. User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Rectangular Not Selected Zone 3 Rectangular Not Selected Depth to Invert of Outlet Pipe 1.21 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area 18.00 N/A Outlet Orifice Centroid Rectangular Orifice Width : 72.00 N/A 1.50 linches N/A feet Rectangular Orifice Height = 36.00 inches Half-Central Angle of Restrictor Plate on Pipe = N/A N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 11.00 0.80 feet Spillway Crest Length = 185.00 Stage at Top of Freeboard = 12.20 feet feet Spillway End Slopes = 4.00 lH:V Basin Area at Top of Freeboard : 2.09 acres Freeboard above Max Water Surface = Basin Volume at Top of Freeboard = 0.40 feet 18.03 acre-ft Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF) EURV Design Storm Return Period WOCV 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year 2 Year One-Hour Rainfall Depth (in) : N/A N/A 1.00 1.28 1.55 1.97 CUHP Runoff Volume (acre-ft) 1.679 5.181 3.768 5.495 305 11.334 14.40 18.159 User Override Inflow Hydrograph Volume (acre-ft) = N/A N/A 3.768 7.701 11.334 14,409 209.5 CUHP Predevelopment Peak O (cfs) = N/A N/A 1.1 11.4 25.6 67.9 94.3 128.0 OPTIONAL Override Predevelopment Peak Q (cfs) : N/A N/A

N/A 2.36 Predevelopment Unit Peak Flow, q (cfs/acre) = N/A 0.01 0.11 0.26 0.69 0.95 Peak Inflow Q (cfs) : N/A N/A 49.4 95.1 99.4 162.3 205.7 409.3 Peak Outflow Q (cfs) : 1.0 9 4 8.4 40.0 68.7 230. Ratio Peak Outflow to Predevelopment Q = N/A N/A N/A 0.8 0.3 0.7 1.0 Structure Controlling Flow Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir 1)verflow Weir Plate Plate Plate erflow Weir 1 Max Velocity through Grate 1 (fps) = N/A N/A N/A 0.7 0.1 N/A N/A N/A Max Velocity through Grate 2 (fps) N/A N/A Time to Drain 97% of Inflow Volume (hours) = 39 64 56 65 56 Time to Drain 99% of Inflow Volume (hours) = 41 71 61 79 79 76 70 70 Maximum Ponding Depth (ft) : 4.89 3.73 5.93 5.87 7,71 10.34 10.08 1.36 3.51 1.90 14.318 1.88 13.83 Area at Maximum Ponding Depth (acres) = 1.24 1.49 1.57 1.6 6.765 1.69 5.189 9.68 Maximum Volume Stored (acre-ft) = 6.67 5687.29 5686.13 5688.33 5692.74 Equivalent Elevation (ft) = 5682 400 Pond Bottom (ft) = 100 YR PEAK RELEASE SET

> RESULTS FROM CROSSED OUT STORM EVENTS ARE NOT VALID, ONLY THE 5-YR & 100-YR HYDROGRAPHS WERE REPLACED (FROM SWMM) IN THIS WORKSHEET

BELOW VALUE PERSCRIBED IN 2013 MDDP (233 CFS)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	USER	CUHP	CUHP	CUHP	USER	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 111111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.71	0.00	3.14
	0:15:00	0.00	0.00	2.47	3.68	6.63	5.38	7.78	9.16	14.70
	0:20:00	0.00	0.00	12.47	22.38	22.59	16.60	21.16	30.17	39.47
	0:25:00	0.00	0.00	31.93	58.18	63.06	40.04	51.48	76.34	110.68
	0:30:00	0.00	0.00	46.70	92.37	94.61	106.01	137.18	225.91	262.70
	0:35:00	0.00	0.00	49.37	95.06	99.39 90.69	151.87 162.30	194.38 205.75	328.10 409.27	367.29
	0:45:00	0.00	0.00	46.03 40.94	81.06 67.14	80.71	152.06	192.06	392.65	386.82 366.24
	0:50:00	0.00	0.00	36.27	58.35	71.85	139.22	175.69	357.50	337.13
	0:55:00	0.00	0.00	32.38	76.39	64.07	124.55	157.55	339.61	306.95
	1:00:00	0.00	0.00	28.94	68.07	57.07	110.10	139.70	313.76	278.78
	1:05:00	0.00	0.00	25.93	59.52	50.84	97.03	123.44	288.18	253.04
	1:10:00	0.00	0.00	23.16	52.37	46.49	83.62	106.66	253.61	220.11
	1:20:00	0.00	0.00	20.87 18.97	46.48 40.58	43.61 40.25	72.92 63.71	93.46 81.72	214.82 181.11	190.38 162.48
	1:25:00	0.00	0.00	17.30	36.06	35.86	55.57	71.14	160.14	137.12
	1:30:00	0.00	0.00	15.71	32.72	31.31	47.71	60.85	144.84	114.99
	1:35:00	0.00	0.00	14.15	30.00	27.04	40.32	51.19	132.05	95.27
	1:40:00	0.00	0.00	12.63	27.33	23.21	33.50	42.32	96.69	77.32
	1:45:00	0.00	0.00	11.31	24.24	19.93	27.30	34.26	70.46	61.23
	1:50:00 1:55:00	0.00	0.00	10.44 9.44	21.59 19.30	17.82 16.47	22.02 18.80	27.48	50.93 42.23	48.56 40.85
	2:00:00	0.00	0.00	8.43	17.47	15.13	16.82	20.98	36.01	35.90
	2:05:00	0.00	0.00	7.05	15.04	12.75	13.95	17.37	29.84	29.18
	2:10:00	0.00	0.00	5.64	11.93	10.14	10.84	13.47	22.81	22.20
	2:15:00	0.00	0.00	4.45	9.21	7.94	8.34	10.33	16.90	16.56
	2:20:00	0.00	0.00	3.51	7.03	6.20	6.42	7.92	12.51	12.29
	2:25:00	0.00	0.00	2.75	5.27	4.80	4.93	6.05	9.31	9.17
	2:35:00	0.00	0.00	2.14 1.66	4.09 3.12	3.66 2.76	3.77 2.85	4.60 3.46	6.83 5.01	6.96 5.24
	2:40:00	0.00	0.00	1.28	2.39	2.09	2.15	2.60	3.71	3.99
	2:45:00	0.00	0.00	0.97	1.78	1.60	1.64	1.98	2.77	3.08
	2:50:00	0.00	0.00	0.72	1.41	1.19	1.24	1.49	2.07	2.31
	2:55:00	0.00	0.00	0.50	1.22	0.85	0.89	1.07	1.53	1.65
	3:00:00 3:05:00	0.00	0.00	0.33	1.11	0.56	0.60	0.72	1.23	1.09
	3:10:00	0.00	0.00	0.19 0.10	1.06 1.03	0.34 0.17	0.37 0.19	0.44	1.10 1.05	0.65
	3:15:00	0.00	0.00	0.04	1.02	0.06	0.07	0.08	1.03	0.11
	3:20:00	0.00	0.00	0.01	1.02	0.01	0.01	0.01	1.02	0.00
	3:25:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.02	0.00
	3:30:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:35:00 3:40:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:45:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:50:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.01	0.00
	3:55:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:00:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:15:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:20:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:35:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:40:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00 1.00	0.00
	4:55:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	5:00:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

<u>Summary Stage-Area-Volume-Discharge Relationships</u>

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

The user should graphically co	inpure the builtin	141,071,000				Total	
Stage - Storage	Stage	Area	Area	Volume	Volume	Outflow	1
Description	[ft]	[ft²]	[acres]	[ft ³]	[ac-ft]	[cfs]	4
	0.00	0	0.000	0	0.000	0.00	T
		11,013	0.253	2,752	0.063	0.18	٦,
	0.50			-			4
	1.00	28,227	0.648	12,252	0.281	0.33	- 1
	1.50	46,992	1.079	31,057	0.713	0.58	4
	2.00	52,539	1.206	56,600	1.299	0.85	4
WQCV	2.23	53,571	1.230	68,803	1.580	0.94	ď
	2.50	54,782	1.258	83,431	1.915	1.04	-Ľ
	3.00	56,603	1.299	111,298	2.555	1.20	-[ˈ,
	3.50	58,319	1.339	140,029	3.215	1.33	4
	4.00	60,874	1.397	169,785	3.898	1.45	4
	4.50	63,638	1.461	200,913	4.612	1.57	4
EURV	4.89	65,067	1.494	226,047	5.189	1.65	4
	5.00	65,400	1.501	233,223	5.354	1.67	4
	5.50	66,911	1.536	266,300	6.113	3.41	4
5-YEAR	5.80	67,829	1.557	286,511	6.577	7.29	4
	6.00	68,445	1.571	300,138	6.890	10.82	4
	6.50	69,984	1.607	334,745	7.685	22.72	4
	7.00	71,558	1.643	370,129	8.497	39.06	4
	7.50	73,141	1.679	406,304	9.327	58.97	_
	8.00	73,607	1.690	443,047	10.171	83.01	4
	8.50	73,794	1.694	479,897	11.017	110.04	4
	9.00	76,336	1.752	517,312	11.876	139.71	\perp
	9.50	79,468	1.824	556,263	12.770	171.79	╛
	10.00	81,580	1.873	596,576	13.695	206.11	\rfloor
100-YEAR	10.43	83,177	1.909	631,998	14.509	237.31	╛
	10.50	83,437	1.915	637,830	14.643	242.53	╛
	11.00	85,250	1.957	680,004	15.611	280.92	
	11.50	87,052	1.998	723,079	16.600	488.10	╛
	11.60	87,413	2.007	731,803	16.800	552.09	
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For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

Stormwater Detention and Infiltration Design Data Sheet

Workhook Protected

Worksheet Protected

Stormwater Facility Name: EXISTING DETENTION BASIN D W/ PROPOSED OUTLET STRUCTURE MODIFICATIONS

Facility Location & Jurisdiction: LOCATED: NW CORNER OF SNEFFLES ST & MESA RIDGE PKWY; JURISDCTION: MESA RDIGE METRO DIST, NO. 1

User Input: Watershed Characteristics

Watershed Slope =	0.035	ft/ft
Watershed Length =	4090	ft
Watershed Area =	98.90	acres
Watershed Imperviousness =	49.1%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
rcentage Hydrologic Soil Groups C/D =	0.0%	percent
_		

Location for 1-hr Rainfall Depths (use dropdown):

User Input

Pe

WQCV Treatment Method = Extended Detention

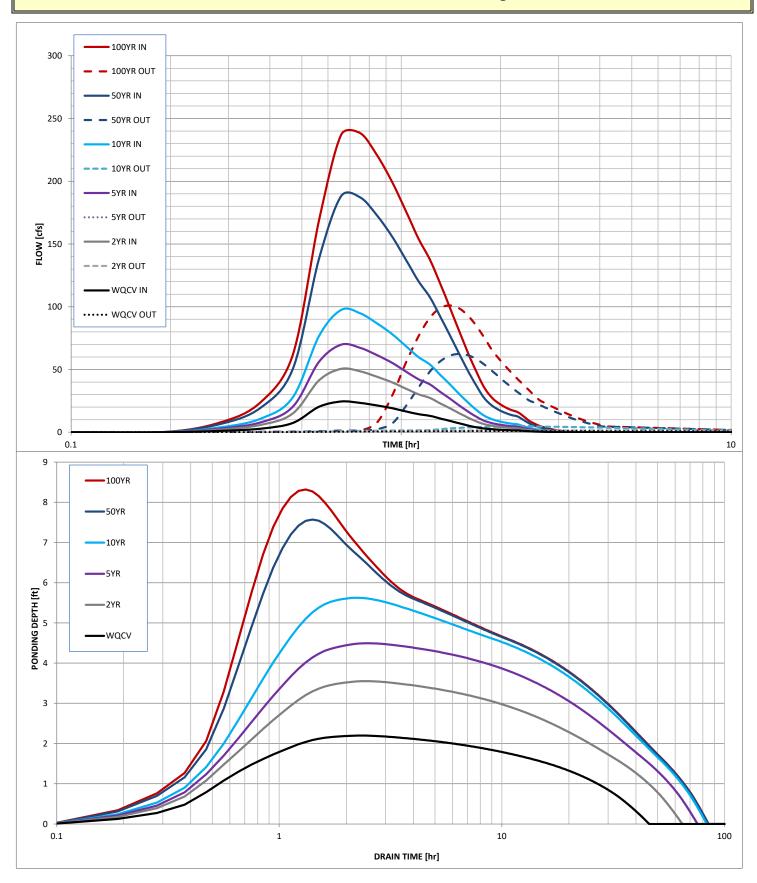
Stage [ft] Area [ft^2] Stag 0.00 0 0.0 0.60 13,215 0. 1.60 50,745 1. 2.60 55,231 2. 3.60 58,662 3. 4.60 64,191 4.	00 0.00 60 0.20 60 0.64 60 1.07 60 1.36
0.60 13,215 0. 1.60 50,745 1. 2.60 55,231 2. 3.60 58,662 3.	60 0.20 60 0.64 60 1.07 60 1.36
1.60 50,745 1. 2.60 55,231 2. 3.60 58,662 3.	60 0.64 60 1.07 60 1.36
2.60 55,231 2. 3.60 58,662 3.	60 1.07 60 1.36
3.60 58,662 3.	60 1.36
4.60 64,191 4.	60 1.59
5.60 67,213 5.	60 4.51
6.60 70,292 6.	60 25.63
7.60 73,458 7.	60 63.52
8.60 73,831 8.	60 115.77
9.60 80,094 9.	178.48
10.60 83,808 10.	60 250.05
11.60 87,413 11	60 552.09
12.60 93,285 12	60 1458.41

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

Routed Hydrograph Results

	Routeu Hydrograph Results						_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.00	1.28	1.55	2.34	2.74	in
Calculated Runoff Volume =	1.680	3.506	4.870	6.863	13.542	17.231	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	1.680	3.505	4.869	6.862	13.535	17.224	acre-ft
Time to Drain 97% of Inflow Volume =	37.7	52.8	61.7	66.9	62.0	59.4	hours
Time to Drain 99% of Inflow Volume =	41.2	57.8	67.6	73.7	71.2	69.7	hours
Maximum Ponding Depth =	2.20	3.55	4.49	5.63	7.57	8.32	ft
Maximum Ponded Area =	1.23	1.34	1.46	1.54	1.68	1.69	acres
Maximum Volume Stored =	1.532	3.276	4.601	6.300	9.440	10.693	acre-ft

Stormwater Detention and Infiltration Design Data Sheet









APPENDIX E - REFERENCE MATERIAL

Mesa Ridge Development Master Development Drainage Plan Update

Fountain, Colorado

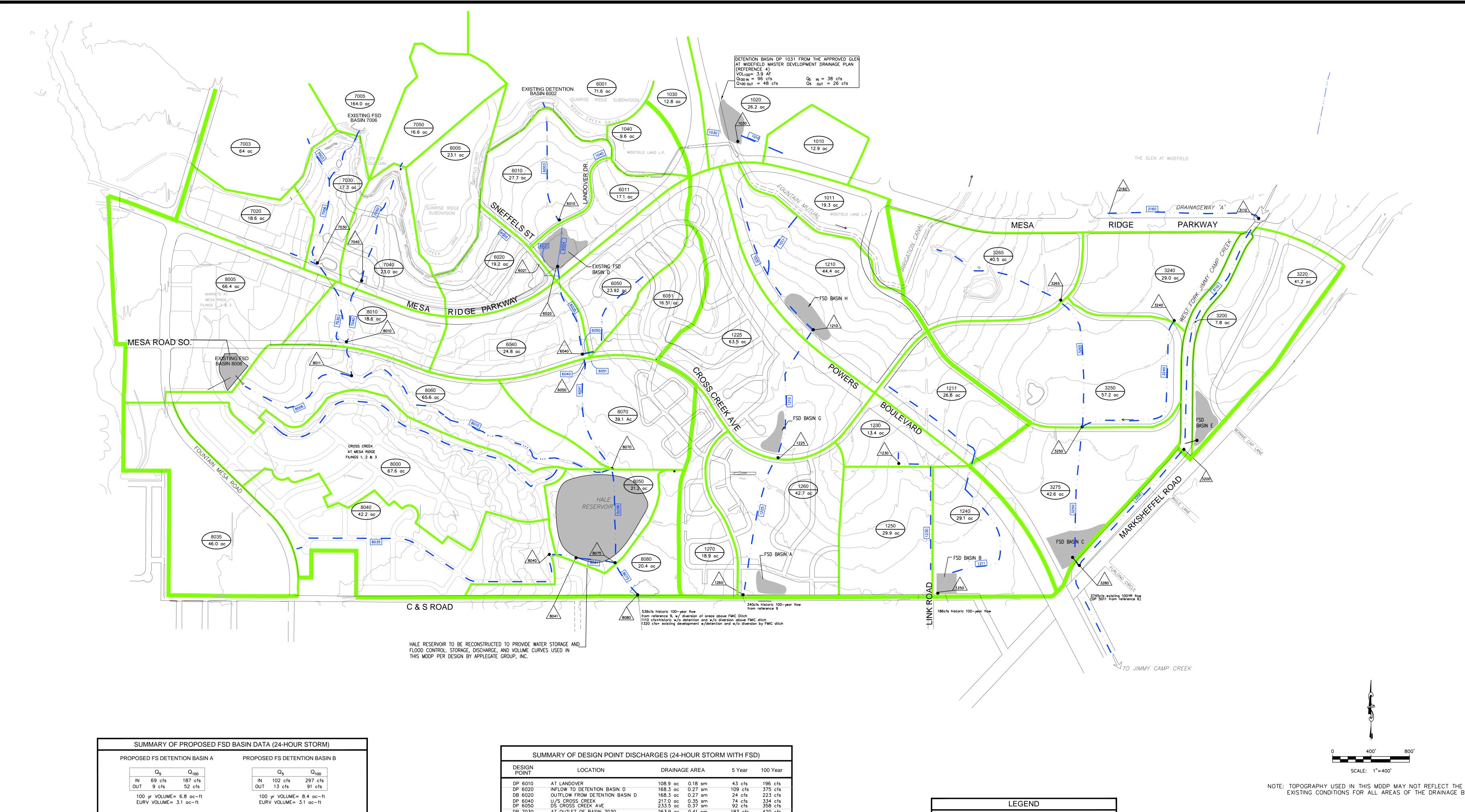
Prepared for:
Nor'wood Development
111 South Tejon Suite 222
Colorado Springs, Colorado 80903

Prepared by:



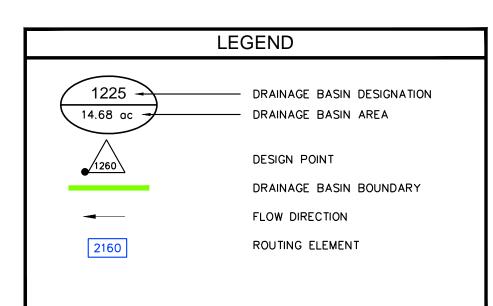
1604 South 21st Street Colorado Springs, Colorado 80904 (719) 630-7342

Kiowa Project No. 11045 January 15, 2013



PROPOSED FS DETENTION BASIN A	PROPOSED FS DETENTION BASIN B
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 69 cfs 187 cfs OUT 9 cfs 52 cfs	IN 102 cfs 297 cfs OUT 13 cfs 91 cfs
100 yr VOLUME= 6.8 ac-ft EURV VOLUME= 3.1 ac-ft	100 yr VOLUME= 8.4 ac-ft EURV VOLUME= 3.1 ac-ft
PROPOSED FS DETENTION BASIN C	AS-BUILT FS DETENTION BASIN D
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 158 cfs 490 cfs OUT 9 cfs 145 cfs	IN 109 cfs 375 cfs OUT 24 cfs 233 cfs
100 yr VOLUME= 14.8 ac-ft EURV VOLUME= 8.3 ac-ft	100 yr VOLUME= 8.0 ac-ft 5 yr VOLUME= 4.1 ac-ft
PROPOSED FS DETENTION BASIN E	RECONSTRUCTED DAM & RESERVOIR BASIN
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 41 cfs 120 cfs OUT 5 cfs 24 cfs	IN 540 cfs 1540 cfs OUT 7 cfs 255 cfs
100 yr VOLUME= 3.9 ac-ft	100 yr VOLUME= 95.9 ac-ft 5 yr VOLUME= 50.0 ac-ft
EURV VOLUME = 1.3 ac-ft	5 yr VOLUME = 50.0 dc-ft
EURV VOLUME= 1.3 ac-ft	PROPOSED FS DETENTION BASIN H
EURV VOLUME= 1.3 ac-ft PROPOSED FS DETENTION BASIN G	•
EURÝ VOLUME= 1.3 ac-ft PROPOSED FS DETENTION BASIN G	PROPOSED FS DETENTION BASIN H

DESIGN POINT					
	LOCATION	DRAINAC	GE AREA	5 Year	100 Year
DP 6010	AT LANDOVER	108.9 ac	0.18 sm	43 cfs	196 cfs
DP 6020	INFLOW TO DETENTION BASIN D	168.3 ac	0.27 sm	109 cfs	375 cfs
DB 6020	OUTFLOW FROM DETENTION BASIN D	168.3 ac	0.27 sm	24 cfs	223 cfs
DP 6040 DP 6050	U/S CROSS CREEK DS CROSS CREEK AVE	217.0 ac 233.5 ac	0.35 sm 0.37 sm	74 cfs 92 cfs	334 cfs 358 cfs
DP 7030	AT OUTLET OF BASIN 7030	263.9 ac	0.41 sm	183 cfs	420 cfs
DP 7040	AT OUTLET OF BASIN 7040	39.6 ac	0.06 sm	30 cfs	110 cfs
DP 8010	AT OUTLET OF BASIN 8010	322.1 ac	0.50 sm	241 cfs	603 cfs
DP 8070	U/S OF HALE RESERVOIR	726.7 ac	1,15 sm	446 cfs	1259 cfs
DP 8075	INFLOW TO HALE RESERVOIR	908.8 ac	1.42 sm	540 cfs	1540 cfs
DB 8075	OUTFLOW FROM HALE RESERVOIR	908.8 ac	1.42 sm	7 cfs	255 cfs
DP 8080	C&S ROAD	928 ac	1.45 sm	13 cfs	257 cfs
DP 1031	D/S POWERS BOULEVARD	51.0 ac	0.08 sm	28 cfs	55 cfs
DP 1211	INFLOW TO DET. BASIN H	108.8 ac	0.17 sm	161 cfs	323 cfs
DB 1210	OUTLOW FROM DET. BASIN H	108.8 ac	0.17 sm	23 cfs	36 cfs
SB 1225	INFLOW TO DETENTION BASIN G	70.4 ac	0.11 sm	74 cfs	216 cfs
DP 1225	AT CROSS CREEK AVENUE	185.6 ac	0.29 sm	33 cfs	104 cfs
DP 1250	INFLOW TO DETENTION BASIN B	96.0 ac	0.15 sm	102 cfs	297 cfs
DB 1250	OUTFLOW FROM DETENTION BASIN B	96.0 ac	0.15 sm	13 cfs	91 cfs
DP 1265	INFLOW TO DETENTION BASIN A	64 ac	0.10 sm	69 cfs	187 cfs
DP 1260	AT C & S ROAD	243 ac	0.38 sm	41 cfs	156 cfs
DP 2160	DESIGN POINT 2160	448 ac	0.70 sm	188 cfs	640 cfs
DP 3110	AT MESA RIDGE PARKWAY	2163.2 ac	3.38 sm	766 cfs	3095 cfs
DP 3200	DESIGN POINT 3200	2208 ac	3.44 sm	764 cfs	3089 cfs
DP 3250	AT COLLECTOR ROAD	126.7 ac	0.20 sm	130 cfs	380 cfs
DP 3265	AT OUTLET OF BASIN 3265	40.5 ac	0.06 sm	52 cfs	135 cfs
DP 3275	INFLOW TO DET. BASIN C	172.8 ac	0.27 sm	158 cfs	490 cfs
DB 3280	OUTFLOW FROM DETENTION BASIN C	172.8 ac	0.27 sm	9 cfs	145 cfs



SUMMARY OF HISTORIC DISCHARGES								
DESIGN POINT	LOCATION	5 Year	100 Year					
3280	WF JIMMY CAMP CREEK MARKSHEFFEL ROAD	992 cfs	3745 cfs					
1250	@ C & S ROAD	35 cfs	186 cfs					
1260	@ C & S ROAD	48 cfs	340 cfs					
8080 (1)	@ C & S ROAD	152 cfs	1110 cfs					

(1) AREA ABOVE FOUNTAIN MUTUAL IRRIGATION CANAL ASSUMED TRIBUTARY TO THIS DESIGN POINT. FMIC CANAL ASSUMED TO CONVEY IRRIGATION FLOW ONLY.

EXISTING CONDITIONS FOR ALL AREAS OF THE DRAINAGE BASINS.

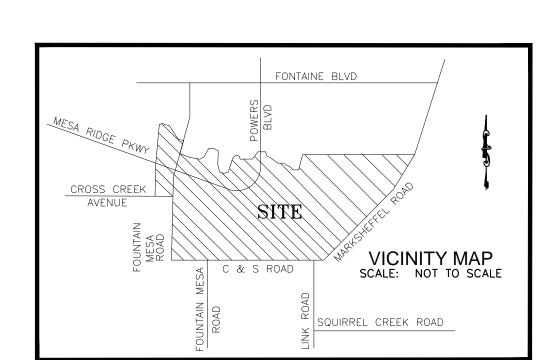
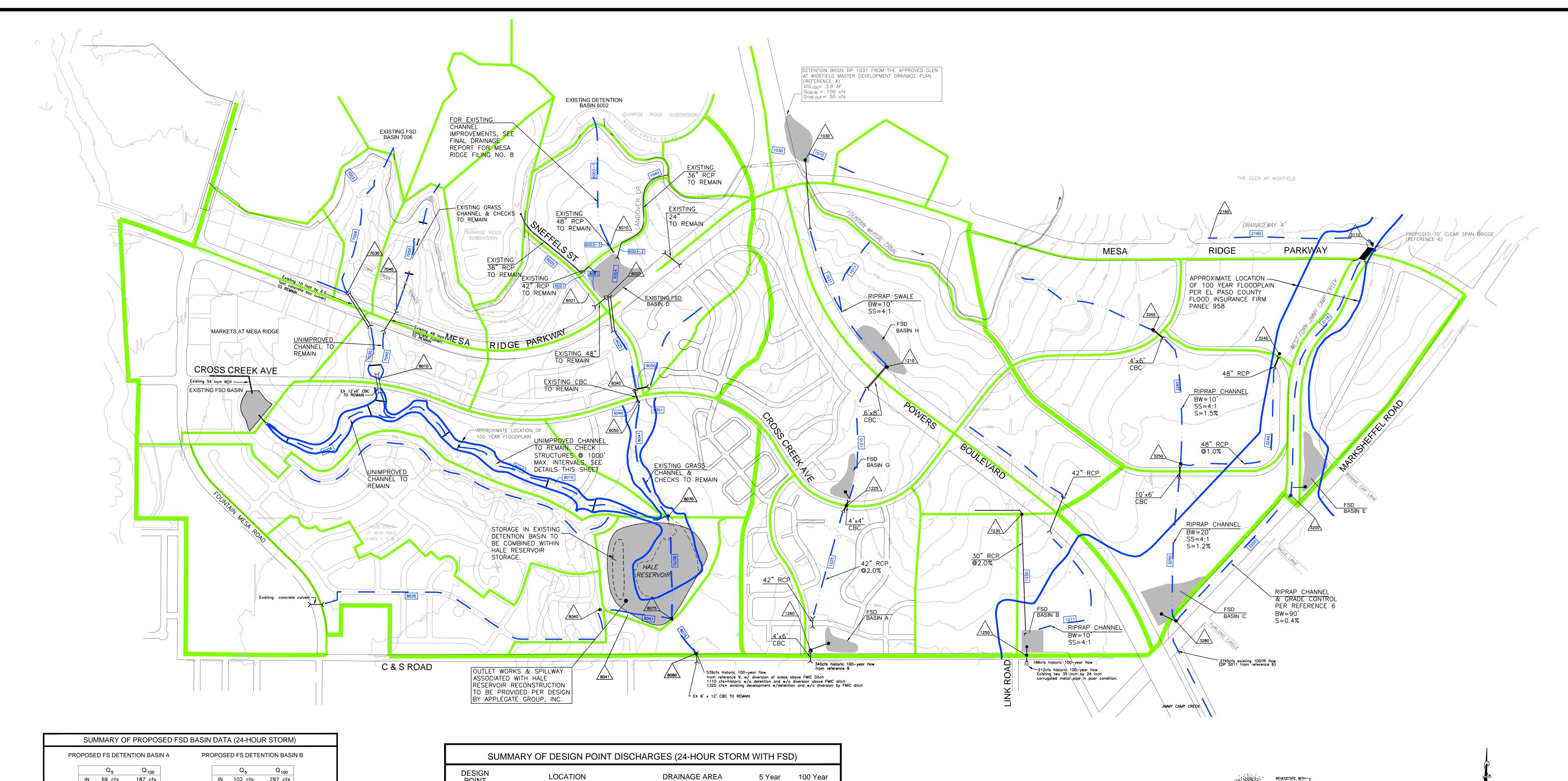


EXHIBIT 1 MESA RIDGE DEVELOPMENT MASTER DEVELOPMENT DRAINAGE PLAN UPDATE HYDROLOGIC SUB-BASIN MAP DEVELOPED WITH EXISTING & PROPOSED DETENTION FOUNTAIN, COLORADO

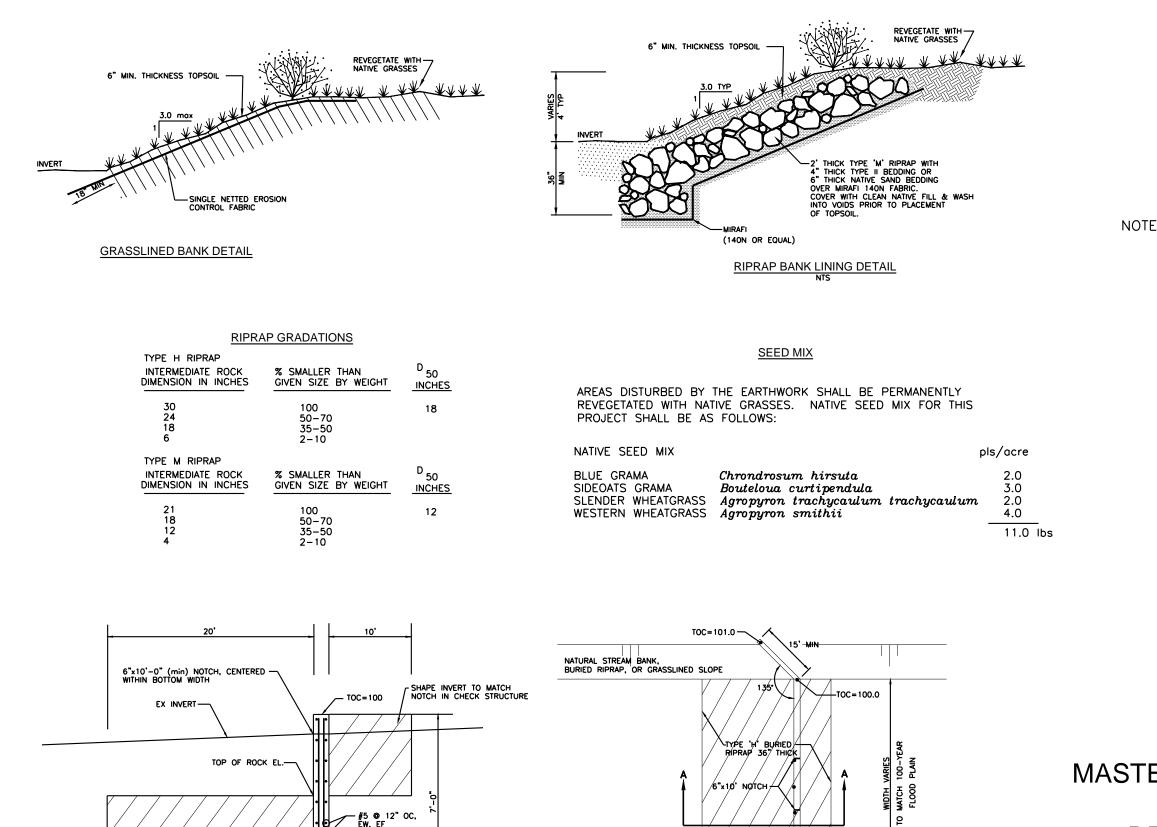
Kiowa Engineering Corporation 1604 South 21st Street Colorado Springs, Colorado 80904 - 4208 (719) 630-7342



PROPOSED FS DETENTION BASIN A	PROPOSED FS DETENTION BASIN B
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 69 cfs 187 cfs OUT 9 cfs 52 cfs	IN 102 cfs 297 cfs OUT 13 cfs 91 cfs
100 yr VOLUME= 6.8 ac-ft EURV VOLUME= 3.1 ac-ft	100 yr VOLUME= 8.4 ac-ft EURV VOLUME= 3.1 ac-ft
PROPOSED FS DETENTION BASIN C	AS-BUILT FS DETENTION BASIN D
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 158 cfs 490 cfs OUT 9 cfs 145 cfs	IN 109 cfs 375 cfs OUT 24 cfs 233 cfs
100 yr VOLUME= 14.8 ac-ft EURV VOLUME= 8.3 ac-ft	100 yr VOLUME= 8.0 ac-ft 5 yr VOLUME= 4.1 ac-ft
PROPOSED FS DETENTION BASIN E	RECONSTRUCTED DAM & RESERVOIR BAS
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 41 cfs 120 cfs OUT 5 cfs 24 cfs	IN 540 cfs 1540 cfs OUT 7 cfs 255 cfs
100 yr VOLUME= 3.9 ac-ft EURV VOLUME= 1.3 ac-ft	100 yr VOLUME= 95.9 ac-ft 5 yr VOLUME= 50.0 ac-ft
PROPOSED FS DETENTION BASIN G	PROPOSED FS DETENTION BASIN H
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 74 cfs 216 cfs OUT 10 cfs 51 cfs	IN 161 cfs 323 cfs OUT 23 cfs 56 cfs

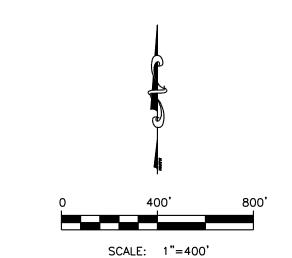
LEGEND						
	100-YEAR FLOODPLAIN					
1250	DESIGN POINT					
	MAJOR DRAINAGE BASIN BOUNDARY					
-	FLOW DIRECTION					
	DRAINAGEWAY & CHECK/DROP STRUCTURE					

	JMMARY OF DESIGN POINT DISCH	HARGES (24-F	100K STOR	(IVI VVIIII FSI	ט)
DESIGN POINT	LOCATION	DRAINAG	GE AREA	5 Year	100 Year
DP 6010	AT LANDOVER	108.9 ac	0.18 sm	43 cfs	196 cfs
DP 6020	INFLOW TO DETENTION BASIN D	168.3 ac	0.27 sm	109 cfs	375 cfs
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DP 6040 DP 6050	U/S CROSS CREEK DS CROSS CREEK AVE	217.0 ac 233.5 ac	0.35 sm 0.37 sm	74 cfs 92 cfs	334 cfs 358 cfs
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DP 8080	C&S ROAD	928 ac	1.45 sm	13 cfs	257 cfs
DP 1031	D/S POWERS BOULEVARD	51.0 ac	0.08 sm	28 cfs	55 cfs
DP 1211	INFLOW TO DET. BASIN H 1210, POWERS	BLVD 108.8 ac	0.17 sm	161 cfs	323 cfs
DP 1210	OUTLOW FROM DET. BASIN H	108.8 ac	0.17 sm	23 cfs	36 cfs
SB 1225	INFLOW TO DETENTION BASIN G	70.4 ac	0.11 sm	74 cfs	216 cfs
DP 1225	AT CROSS CREEK AVENUE	185.6 ac	0.29 sm	33 cfs	104 cfs
DP 1250	INFLOW TO DETENTION BASIN B	96.0 ac	0.15 sm	102 cfs	297 cfs
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DP 2160	DESIGN POINT 2160	448 ac	0.70 sm	188 cfs	640 cfs
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DP 3200	DESIGN POINT 3200	2208 ac	3.44 sm	764 cfs	3089 cfs
DP 3250	AT COLLECTOR ROAD	126.7 ac	0.20 sm	130 cfs	380 cfs
DP 3265	AT OUTLET OF BASIN 3265	40.5 ac	0.06 sm	52 cfs	135 cfs
DP 3281	INFLOW TO DET. BASIN C	172.8 ac	0.27 sm	158 cfs	490 cfs
DB 3281	OUTFLOW FROM DETENTION BASIN C	172.8 ac	0.27 sm	9 cfs	145 cfs
DP 3280	AT MARKSHEFFEL ROAD	2381.0 ac	3.72 sm	772 cfs	3215 cfs



TYPICAL CHECK STRUCTURE PLAN
NO SCALE

SECTION A-A



NOTE: TOPOGRAPHY USED IN THIS MDDP MAY NOT REFLECT THE EXISTING CONDITIONS FOR ALL AREAS OF THE DRAINAGE BASINS.

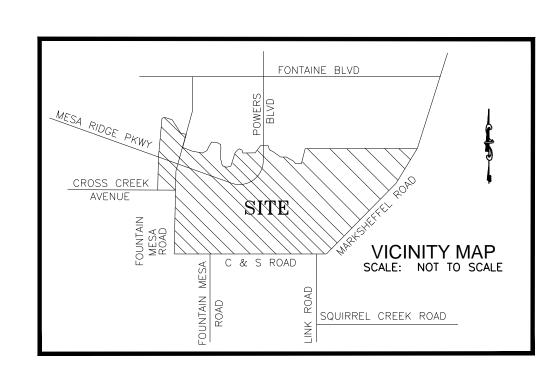


EXHIBIT 2
MESA RIDGE DEVELOPMENT
MASTER DEVELOPMENT DRAINAGE PLAN UPDATE
PROPOSED FACILITIES PLAN
DEVELOPED WITH REGIONAL DETENTION
FOUNTAIN, COLORADO

Kiowa Engineering Corporation

1604 South 21st Street
Colorado Springs, Colorado
80904 - 4208
[719] 630-7342



Master Development Drainage Plan Mesa Ridge Development

City of Fountain, Colorado

Prepared For:

Norwood Development 111 South Tejon #222 Colorado Springs, CO 80903

Prepared By:

Kiowa Engineering Corporation 1604 South 21st Street Colorado Springs, Colorado 80904

Project Number 05011 December 17, 2006

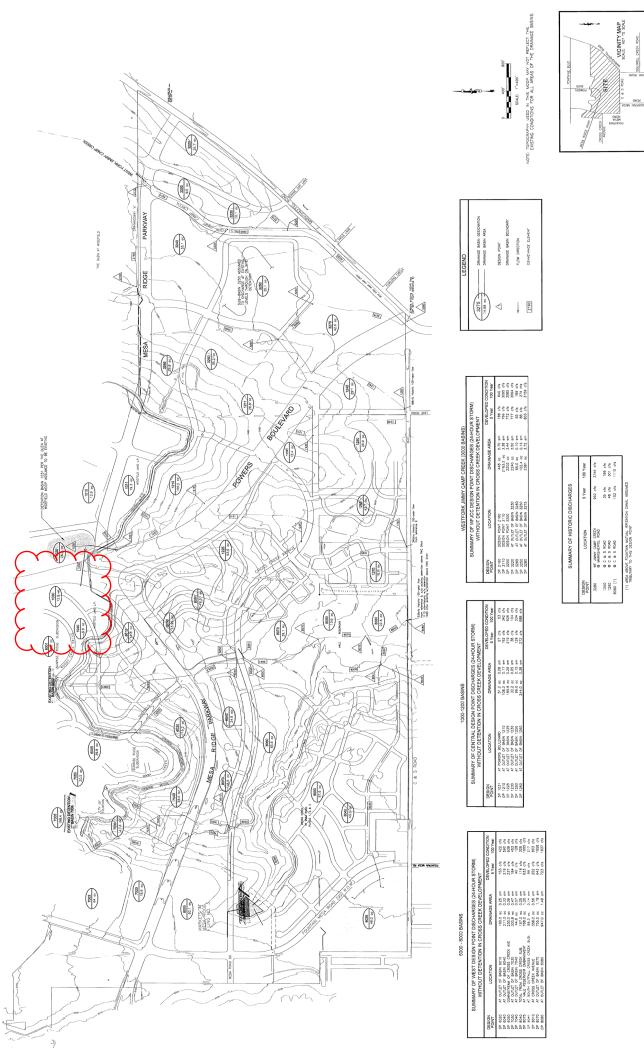


EXHIBIT 1

MESA RIDGE DEVELOPMENT

MASTER DEVELOPMENT DRAINAGE PLAN UPDATE

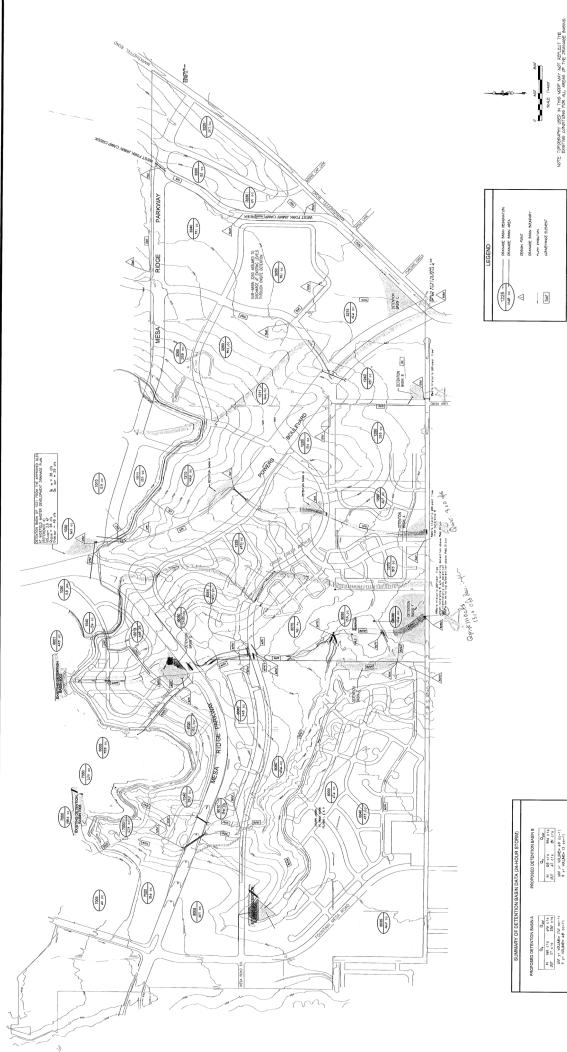
HYDROLOGIC SUB-BASIN MAP

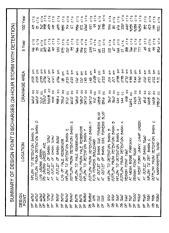
DEVELOPED WITHOUT REGIONAL DETENTION

& DRAINAGEWAY IMPROVEMENTS

FOUNTAIN, COLORADO

JINTAIN, COLORADO
Kitowa Engineering Corporation
1604 South 21 et Street
Corporate Springs, Colorado
1799 660-7942
(719) 660-7942





Q₅ Q₆₀ N @9 cts A40 cts QIT 80 cts 165 cts 100 yr vQLD4E= 156 cc-tt 5 yr vQLD4E= 54 cc-tt ROPOSED DETENTION BASIN G

04 0wo N 145 cts 415 cts OUT 99 cts 199 cts 100 yr VOLINE= 108 cc-1t 5 yr VOLINE= 58 cc-1t

POSED DETENTION BASIN C

04 0 099 N RD cis 344 cis 041 79 cis 121 cis 120 yr VOLUNE= 69 cc-1t 5 yr VOLUNE= 69 cc-1t

		PATE STATES	NOTE: TOPOGRAPHY USED IN THIS INDIP I EXISTING CANTENIS FOR ALL ARE	Z SESWOOD		CHOSS CHEEK	//// See
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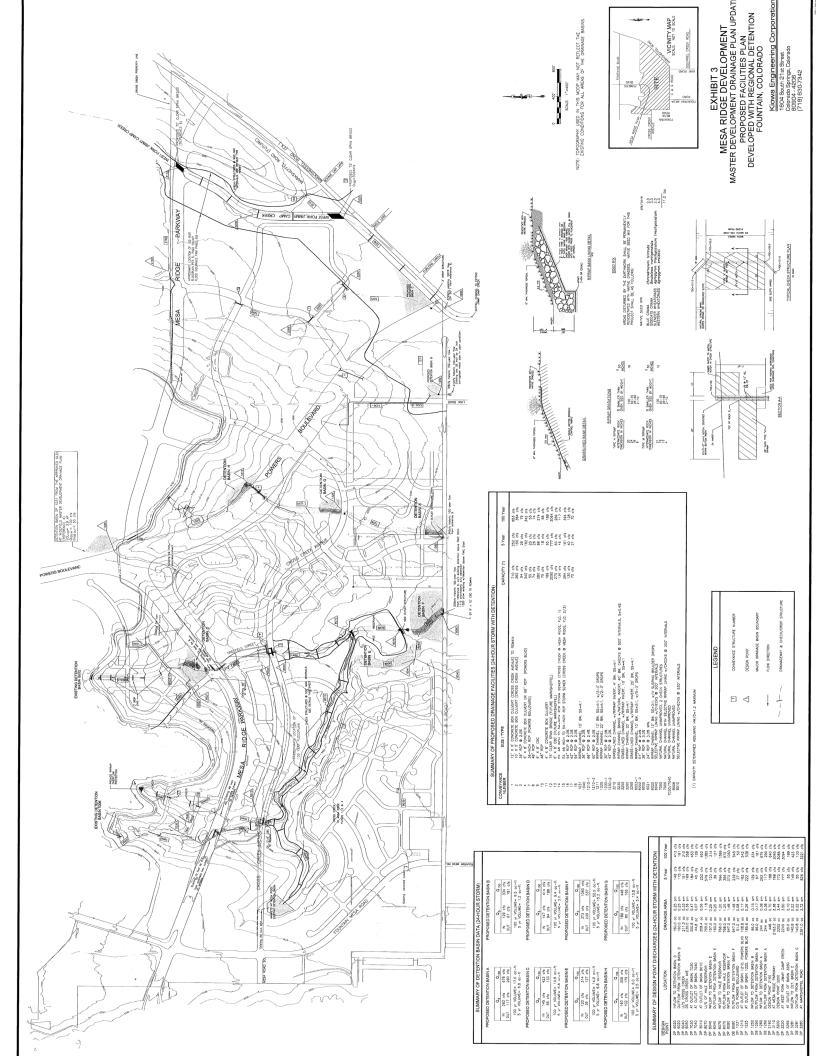
GANE SUNTANCY	OATB SH3WOd	SOBOS CREEK	FOUNTAME OF THE PARTY AND TO SEAT TO S	OWORR SHILL OWN SHILL
		CROSS		

SUMMARY OF HISTORIC DISCHARGES

5 Year

WF JAMY CAMP CR # MARKSTETEL RC # C & 5 ROW # C & 5 ROW

EXHIBIT 2
MESA RIDGE DEVELOPMENT
MASTER DEVELOPMENT DRAINAGE PLAN UPDAT
HYDROLOGIC SUB-BASIN MAP
DEVELOPED WITH DETENTION
FOUNTAIN, COLORADO Klowa Engineering Corporation 1604 South 21st Street Cobrado Springs, Colorado 80904 - 4208 (719) 630-7342



GENERAL NOTES

- 1. ALL WORK REQUIRED OF THESE PLANS SHALL BE COMPLETED IN ACCORDANCE WITH CITY OF COLORADO SPRINGS, ENGINEERING DIVISION, STANDARD SPECIFICATIONS, AND WITH THE APPLICABLE SECTIONS OF THE COLORADO DEPARTMENT OF TRANSPORTATION. STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION.
- 2. THE CONTRACTOR IS RESPONSIBLE FOR THE FIELD VERIFICATION OF ALL PUBLIC AND PRIVATE UTILITIES PRIOR TO THE COMMENCEMENT OF WORK. THE UTILITIES SHOWN ON THESE PLANS HAVE BEEN LOCATED USING THE BEST AVAILABLE INFORMATION. SHOULD A UTILITY BE DAMAGED AS A RESULT OF THIS CONSTRUCTION, IT SHALL BE REPAIRED IMMEDIATELY BY EITHER THE CONTRACTOR OR THE AFFECTED UTILITY OWNER. THE FULL COST OF SUCH A REPAIR SHALL BE THE RESPONSIBILITY OF THE
- 3. SURFACE AND GROUNDWATER AT THE SITE MAY CREATE A NEED FOR DEWATERING DURING THE CONSTRUCTION OF THE DRAINAGEWAY FACILITIES. CONTRACTOR SHALL BE RESPONSIBLE FOR THE MAINTENANCE OF TEMPORARY DEWATERING STRUCTURES, AND PROVIDE FOR THE SAFE AND STABLE DISCHARGE OF WATER FROM THE CONSTRUCTION SITE. THE COST OF DEWATERING IS CONSIDERED INCIDENTAL TO THE CONSTRUCTION AND WILL NOT BE PAID FOR UNDER A SPECIFIC ITEM IN THE BID DOCUMENTS.
- 4. CLASS III RCP SHALL BE USED FOR ALL STORM SEWERS UNLESS OTHERWISE SPECIFIED.
- 5. THE CONTRACTOR SHALL NOTIFY THE CITY OF FOUNTAIN DEPARTMENT OF PUBLIC WORKS 48 HOURS PRIOR TO THE START OF CONSTRUCTION TO OUTLINE METHODS OF CONSTRUCTION, SCHEDULING, AND ISSUING OF INSPECTION PERMITS.

STRUCTURAL CONCRETE NOTES

- 1. ALL CONSTRUCTION INVOLVING THE PLACEMENT OF STRUCTURAL CONCRETE SHALL BE COMPLETED IN ACCORDANCE WITH SECTION 600 OF THE CITY OF COLORADO SPRINGS ENGINEERING DIVISION STANDARD SPECIFICATIONS.
- 2. STEEL REINFORCING SHALL BE GRADE 60 FOR ALL REINFORCING STEEL GREATER THAN #4. A TABLE SPECIFYING MINIMUM SPLICE LENGTHS HAS BEEN PROVIDED ON THE STRUCTURAL DETAIL SHEETS. ALL REINFORCING SHALL HAVE A 2-INCH MINIMUM COVER UNLESS OTHERWISE SPECIFIED. REBAR SHOP DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW
- 3. CAST-IN-PLACE CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH (F'C) OF 4,000 PSI AT 28 DAYS. ALL CONCRETE PLACED AGAINST SOIL SHALL BE TYPE II/V PORTLAND CEMENT. ALL EXPOSED CORNERS SHALL BE FORMED WITH A 3/4" CHAMFER UNLESS OTHERWISE SPECIFIED.
- 4. EXPANSION JOINT MATERIAL SHALL MEET AASHTO SPECIFICATION M-213.
- 5. BACKFILL AGAINST STRUCTURES SHALL NOT COMMENCE UNTIL ALL SUPPORTING DIAPHRAGMS ARE IN PLACE AND CONCRETE HAS OBTAINED ITS FULL SEVEN DAY STRENGTH. BACKFILL SHALL BE PLACED EQUALLY ON EACH SIDE OF CHECK STRUCTURES AND CUTOFF WALLS UNTIL THE FINAL GRADE IS REACHED.
- 6. FOOTING EXCAVATIONS SHALL BE EXAMINED BY THE GEOTECHNICAL ENGINEER PRIOR TO THE FORMING AND PLACING OF CONCRETE.
- 7. CONTRACTOR IS RESPONSIBLE FOR PROVIDING THE ENGINEER AND GEOTECHNICAL ENGINEER WITH A 24-HOUR MINIMUM NOTIFICATION FOR REBAR OBSERVATION, SOIL AND/OR CONCRETE TESTING. PLACEMENT OF CONCRETE IN THE ABSENCE OF TESTING SHALL BE COMPLETED AT THE SOLE RISK OF THE CONTRACTOR.

- A. NO ADMIXTURES PERMITTED WITHOUT THE REVIEW OF ENGINEER. SUBMIT DESIGN MIX FOR ENGINEER APPROVAL.
- B. CONTRACTOR IS RESPONSIBLE FOR THE ADEQUACY OF FORMS AND SHORING AND FOR SAFE PRACTICE IN THEIR USE AND REMOVAL. C. COMPRESSIVE STRENGTH SHALL BE 4,000 psi, MIN.

9. REINFORCING STEEL:

- A. TO BE BILLET STEEL CONFORMING TO THE LATEST A.S.T.M/ A615 GRADE 60 SPECIFICATION, FABRICATED IN ACCORDANCE WITH MANUAL OF STANDARD PRACTICE OF THE C.R.S.I. AND PLACED IN ACCORDANCE WITH A.C.I. 315 AND A.C.I. MANUAL OF PRACTICE.
- B. MINIMUM OF CONCRETE COVER UNLESS OTHERWISE DETAILED ON DRAWINGS: FOOTINGS 3 INCHES, WALLS 3 INCHES, SLABS EXPOSED TO WEATHER 1-1/12 INCHES, SLABS ON GRADE 1-1/2 INCHES MEASURED FROM TOP OF SLAB.
- C. SLAB REINFORCEMENT: LAPPED 36 BAR DIAMETER OR MINIMUM 18 INCHES. BOTTOM BARS SPLICED ONLY AT SUPPORTS, TOP BARS SPLICED ONLY AT MID-SPAN. ALL TOP BARS HOOKED AT NON-CONTINUOUS EDGES (U.O.N.) ALL HOOKS TO BE STANDARD 90 DEGREE OR 180 DEGREE HOOKS AS REQUIRED (U.O.N.), DOWELS IN FOUNDATION TO MATCH REINFORCING ABOVE.
- D. SUBMIT SHOP DRAWINGS FOR REINFORCING PRIOR TO FABRICATION.

10. FOUNDATIONS:

- A. STRUCTURES SHALL BEAR ON SOIL HAVING A MINIMUM BEARING CAPACITY OF 2,000 P.S.F. COMPACTION FOR SUBGRADE PREPARATION SHALL BE IN ACCORDANCE WITH REQUIREMENTS OF THE SOILS REPORT. SUBGRADE PREPARATION SHALL BE MONITORED BY THE SOILS ENGINEER.
- .11. BACKFILL AND STABILIZATION MATERIAL
- A. BACKFILL MATERIAL CONSISTING OF SELECT, GRANULAR, NON-SWELLING MATERIAL TO BE PLACED ALONG THE SIDES OF THE VAULTS EXTENDING 3 FEET OUTSIDE THE VAULT WALLS.
- B. 3/4-INCH ROCK, 12-INCHES DEEP, TO BE PLACED UNDER ALL VAULTS. C. 2-INCH TO 4-INCH STABILIZATION MATERIAL SHALL BE PLACED UNDER THE 3/4" ROCK IF SUBGRADE STABILIZATION IS REQUIRED.

12. ABBREVIATIONS

E.C -- EPOXY COATED O.F. -- OUTSIDE FACE E.F. -- EACH FACE I.F. -- INSIDE FACE N.F. -- NEAR FACE T.O.C. -- TOP OF CONCRETE B.O.C. -- BOTTOM OF CONCRETE CONT. -- CONTINUOUS

INDEX OF SHEETS

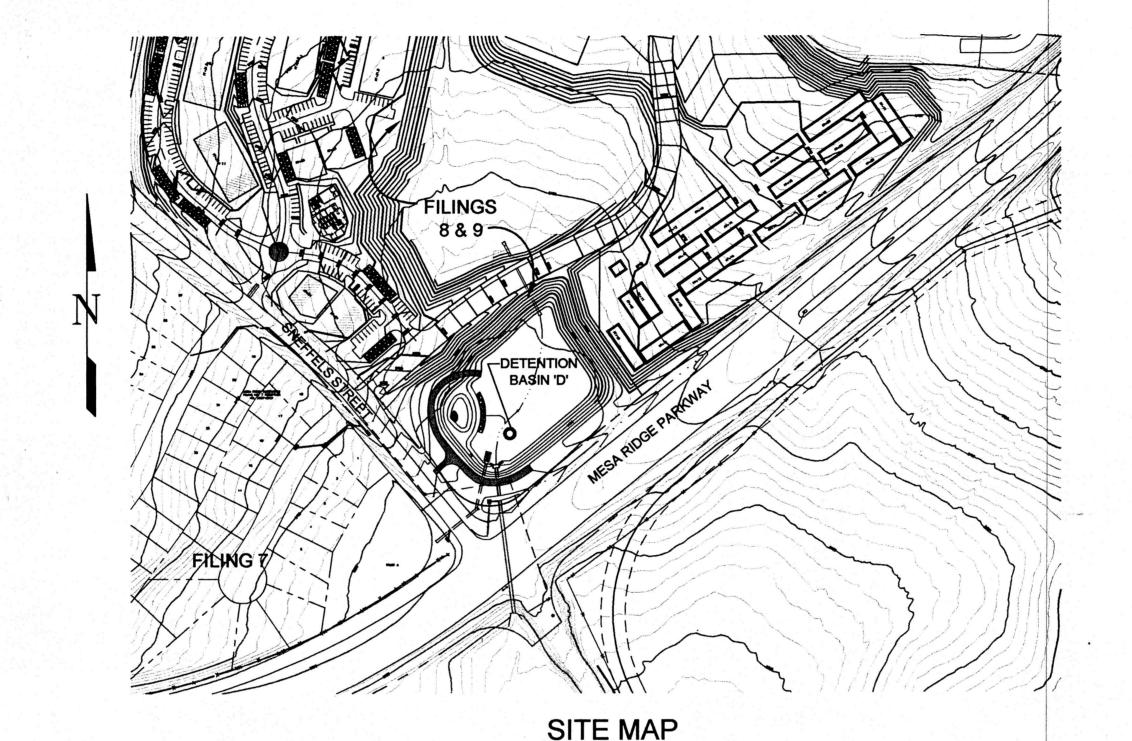
- COVER SHEET
- 2 GRADING AND EROSION CONTROL PLAN & STORM PROFILE
- 3 OUTLET STRUCTURE DETAILS

ABBREVIATIONS PVC = POINT OF VERTICAL CURVATURE ASSY = ASSEMBLYHORIZ.= HORIZONTAL PVI = POINT OF VERTICAL INTERSECTION BNDY = BOUNDARY HYD = HYDRANTPVT = POINT OF VERTICAL TANGENCY B.O.P. = BOTTOM OF PIPEI.D. = INSIDE DIAMETER RCB = REINFORCED CONCRETE BOX = LEFT CL = CENTERLINE RCP = REINFORCED CONCRETE PIPE CRA = CONCRETE REVERSE ANCHOR LF = LINEAR FEET ROW = RIGHT OF WAY LP = LOW POINT CTRB = CONCRETE THRUST BLOCK RT = RIGHT CR = POINT OF CURB RETURN MAX. = MAXIMUM SHT = SHEET DIP = DUCTILE IRON PIPE M.H. = MANHOLE SS = SANITARY SEWER MIN. = MINIMUM EL = ELEVATION STA. = STATION ESMT = EASEMENTNTS = NOT TO SCALE O.D. = OUTSIDE DIAMETER STD. = STANDARD EX. = EXISTING T.O.P. = TOP OF PIPE FC = FACE OF CURB PC = POINT OF HORIZONTAL CURVATURE PCHC = POINT OF CURVATURE ON HORIZ. CURVE TYP. = TYPICAL FES = FLARED END SECTION VC = VERTICAL CURVE FLG = FLANGE PT = POINT OF HORIZONTAL TANGENCY VERT. = VERTICAL FL = FLOWLINE PTHC = POINT OF TANGENCY ON HORIZ. CURVE GB = GRADE BREAK HP = HIGH POINT PVC = POLY VINYL CHLORIDE PIPE

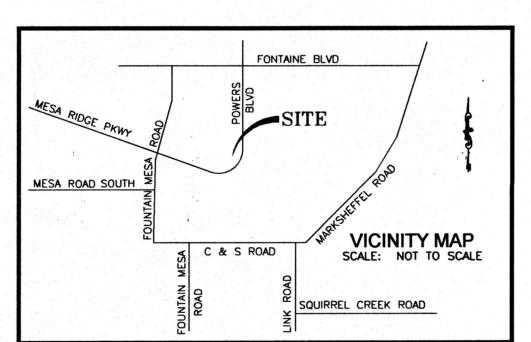
MESA RIDGE FILINGS 8 & 9

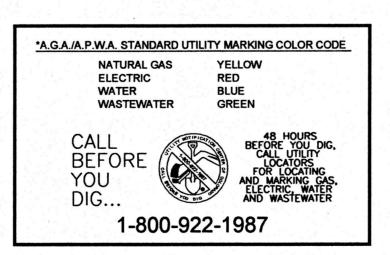
DETENTION BASIN 'D' FULL SPECTRUM DETENTION MODIFICATIONS FINAL DESIGN DRAWINGS

FOUNTAIN, COLORADO



SCALE: 1"=200'





DUANE GREENWOOD, PUBLIC WORKS DIR./CITY ENGINEER DETAILED DRAINAGE CONSTRUCTION PLANS & SPECIFICATIONS **ENGINEER'S STATEMENT:** THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE CITY FOR DETAILED DRAINAGE PLANS AND SPECIFICATIONS SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY(S) IS DESIGNED. I ACCEPT RESPONSIBILITY FOR LIABILITY CAUSED BY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS. RICHARD N. WRAY P.E. #19310 DEVELOPER \ NOR'WOOD DEVELOPMENT PLAZA OF THE ROCKIES 11 S. TEJON STREET, SUITE 222 COLORADO SPRINGS, COLORADO 80903

CITY OF FOUNTAIN ACCEPTANCE:

STATEMENTS

THE PLANS OR REPORT SUBMITTED APPEAR TO BE IN CONFORMANCE WITH THE CITY OF

PRACTICES APPEAR TO HAVE BEEN FOLLOWED. THE PROFESSIONAL ENGINEER SUBMITTING

AND SEALING THE PLANS OR REPORT IS SOLELY RESPONSIBLE FOR THEIR ACCURACY AND

DATE

DEVELOPER:

NOR'WOOD DEVELOPMENT

PLAZA OF THE ROCKIES

11 S. TEJON STREET, SUITE 222

COLORADO SPRINGS, COLORADO 80903

FOUNTAIN SUBMITTAL REQUIREMENTS AND STANDARD ENGINEERING PRINCIPALS AND

VALIDITY. THIS REVIEW IS ONLY VALID FOR ONE (1) YEAR FROM THE DATE BELOW.

Kiowa Project No. 09061 October 25, 2011

PROJECT SPECIFIC GRADING AND EROSION CONTROL NOTES

- 1. All earthwork required of this construction shall be completed in accordance with all applicable sections of the Project
- Specifications and Soil Investigation Report (Geotechnical Report). 2. Rubbish including timber, concrete rubble, trees, brush, and asphalt shall not be backfilled adjacent to any of the structures or be in the placement of any unclassified fill. The Contractor shall be responsible for the removal and hauling of such materials to a suitable spoil area. Costs associated with the removal of such materials shall be paid for as documented in the Project
- 3. Excess excavation shall become the property of the Contractor and shall be disposed of at the Contractor's expense. The cost of
- haulage and spoiling of excess excavated materials shall be paid for as documented in the Project Specifications. 4. Water shall be used as a dust palliative as required and shall be included in the cost for earthwork item(s). No separate payment will be made for dust control associated with the site construction.
- 5. The road grades shall be cleared of vegetation and the topsoil stockpiled for later use.
- 6. All grading shall be in conformance with the Geotechnical Report for the area. . Placement of fill for roadway embankments shall be completed in conformance with the Geotechnical Report.
- 8. Grading contours shown on this plan are to final grade.
- 9. Compaction under filled areas, including roadway and detention basin embankments, shall be 95 percent of the maximum
- Standard Proctor Density (ASTM D698) at two (2) percent of optimum moisture content. 10. No rubble or debris shall be placed in the backfill under any of the proposed buildings, streets, curb & gutter, sidewalk and drainage structures or within five (5) feet of a building footprint. Properly graded rubble may be used in some locations as
- specified and verified by the Geotechnical Engineer. 11. Contractor is responsible for reviewing the site prior to bidding to verify site conditions.
- 12. Contractor is responsible for providing erosion control measures as approved by the City of Fountain Dept. of Public Works
- Division and as may be required by the El Paso County Inspector. 13. All slopes equal to or greater than 3:1 shall require erosion control blanket, single netted fabric, American Excelsior or equal.
- 14. The Developer is responsible for maintaining erosion control measures until a mature stage of vegetation is established.
- 15. All soils used for fill must be approved by a representative of the Geotechnical Engineer.
- 16. All natural ground to receive fill must be properly scarified, watered and compacted prior to placing fill.
- 17. The Contractor is solely responsible for the design, maintenance and operation of any required dewatering system. The Contractor shall perform such independent investigation as he deems necessary to satisfy himself as to the subsurface groundwater conditions and unstable soil conditions to be encountered throughout the construction.
- 18. No fill shall be placed, spread or rolled while it is frozen, thawing or during unfavorable weather conditions. When the work is interrupted by heavy rain, fill operations shall not be resumed until a representative of the Geotechnical Engineer indicates that the moisture content and density of the previously placed fill are as specified. Fill surfaces may be scarified and recompacted after rainfall if necessary, to obtain proper moisture density relation.
- 19. Additional erosion control structures and/or grading may be required at the time of construction.
- 20. Sediment removal for erosion control facilities shall be performed continuously for proper function.
- 21. Base mapping was provided by Rockwell Consulting. The date of the survey was January 2008. 22. Proposed Construction Schedule: Begin Construction: 60-TO GER 25, 2011
- End Construction: FEBRUARY 28, 2017 Total Site Area = 3.6 Acres
- 23. Area to be disturbed = 3.6 Acres (est.) Existing 100-year runoff coefficient = 0.40 Proposed 100-year runoff coefficient = 0.40
- Existing Hydrological Soil Groups: B & C 24. Site is currently undeveloped and covered with native grasses on mild slopes (2%-7%).
- 25. Site is located in the Jimmy Camp Creek Drainage Basin.
- 26. All grading and erosion control shall be completed in accordance with the City of Fountain Municipal Code Sections 12.04.160

GRADING AND EROSION CONTROL NOTES

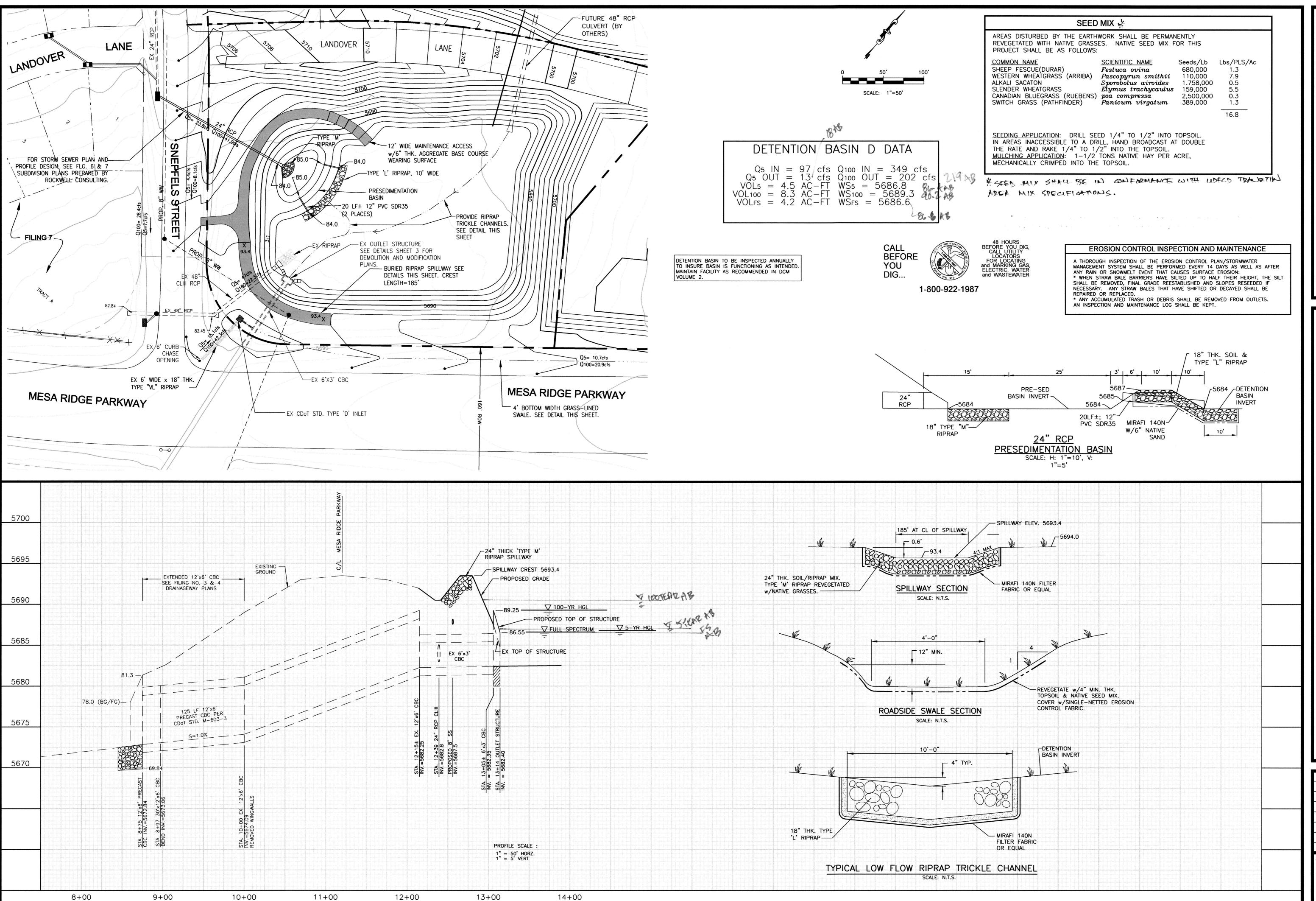
- 1. ALL GRADING AND EROSION CONTROL SHALL BE COMPLETED IN ACCORDANCE WITH THE CITY OF FOUNTAIN
- MUNICIPAL CODE SECTIONS 12.04.160 AND 12.10.
- 2. ALL FILL AREAS SHALL BE COMPACTED IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS.
- SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN TWENTY ONE (21) CALENDAR DAYS AFTER FINAL GRADING, OR FINAL EARTH DISTURBANCE HAS BEEN COMPLETED. AN AREA THAT IS GOING TO REMAIN IN AN INTERIM STATE FOR MORE THAN 60 DAYS SHALL ALSO BE SEEDED. ALL TEMPORARY SOIL EROSION CONTROL MEASURES AND BMPS SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED.
- 4. EROSION CONTROL SHALL CONSIST OF SILT FENCES AND HAY BALES AS SHOWN ON THE DRAWING, AND TOPSOIL WITH GRASS SEED WHICH WILL BE WATERED UNTIL VEGETATION HAS BEEN REESTABLISHED.
- 5. EROSION CONTROL BALES OR SILT FENCE SHALL BE PLACED AT THE TOE AND DRAINAGE OUTFALL POINTS OF ALL SLOPES 4:1 OR STEEPER TO PREVENT SILTATION ON STREETS. REFER TO STORM WATER MANAGEMENT PLAN FOR DETAIL AND LOCATION OF EROSION CONTROL MEASURES.
- 6. CONTRACTOR SHALL COMPLY WITH ALL LOCAL, COUNTY AND STATE REGULATIONS PERTAINING TO GRADING, DUST
- NATURAL VEGETATION SHALL BE RETAINED AND PROTECTED WHEREVER POSSIBLE. EXPOSURE OF SOIL TO EROSION BY REMOVAL OR DISTURBANCE OF VEGETATION SHALL BE LIMITED TO THE AREA REQUIRED FOR
- IMMEDIATE CONSTRUCTION OPERATIONS AND FOR THE SHORTEST PRACTICAL PERIOD OF TIME. 8. TOPSOIL SHALL BE STOCKPILED TO THE EXTENT PRACTICABLE ON THE SITE FOR USE ON AREAS TO BE
- REVEGETATED. ANY AND ALL STOCKPILES SHALL BE LOCATED AND PROTECTED FROM EROSIVE ELEMENTS. AT ALL TIMES, THE PROPERTY SHALL BE MAINTAINED AND/OR WATERED TO PREVENT WIND-CAUSED EROSION.
- EARTHWORK OPERATIONS SHALL BE DISCONTINUED WHEN FUGITIVE DUST SIGNIFICANTLY IMPACTS ADJACENT PROPERTY. IF EARTHWORK IS COMPLETE OR DISCONTINUED AND DUST FROM THE SITE CONTINUES TO CREATE PROBLEMS, THE OWNER/DEVELOPER SHALL IMMEDIATELY INSTITUTE MITIGATIVE MEASURES AND SHALL CORRECT DAMAGE TO ADJACENT PROPERTY. 10. ALL PERSONS ENGAGED IN EARTH DISTURBANCE SHALL IMPLEMENT AND MAINTAIN ACCEPTABLE SOIL EROSION
- AND SEDIMENT CONTROL MEASURES INCLUDING BMPS IN CONFORMANCE WITH THE EROSION CONTROL TECHNICAL STANDARDS OF THE MANUAL AND IN ACCORDANCE WITH THE EROSION AND STORMWATER QUALITY CONTROL PLAN APPROVED BY THE CITY OF FOUNTAIN, IF REQUIRED.
- 11. ALL EARTH DISTURBANCE SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY REDUCE ACCELERATED SOIL EROSION.
- 12. ALL EARTH DISTURBANCE SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED IN SUCH A MANNER SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME.
- 13. ALL EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE
- 14. SUSPENDED SEDIMENT CAUSED BY ACCELERATED SOIL EROSION SHALL BE MINIMIZED IN RUNOFF WATER BEFORE
- 15. TEMPORARY SOIL EROSION CONTROL FACILITIES SHALL BE REMOVED AND EARTH DISTURBANCE AREAS GRADED AND STABILIZED WITH PERMANENT SOIL EROSION CONTROL MEASURES PURSUANT TO THE STANDARDS AND SPECIFICATIONS PRESCRIBED IN THE MANUAL, AND IN ACCORDANCE WITH THE PERMANENT EROSION CONTROL FEATURES SHOWN ON THE EROSION AND STORMWATER CONTROL PLANS APPROVED BY THE CITY OF FOUNTAIN, IF
- ANY STREET OR DRAINAGE FACILITY WHICH HAS HAD EROSION SEDIMENT DEPOSITED IN IT DUE TO CONSTRUCTION, GRADING, OR OTHER DEVELOPMENT ACTIVITY, MUST BE CLEANED IMMEDIATELY AT THE EXPENSE OF THE CONTRACTOR, DEVELOPER, HOMEBUILDER, OR WHOEVER IS RESPONSIBLE FOR THE CONSTRUCTION, GRADING, OR LAND DEVELOPMENT ACTIVITY. IF THE FACILITY IS NOT CLEANED IMMEDIATELY OR WITHIN A RESPONSIBLE PERIOD OF TIME AFTER NOTIFICATION BY THE CITY, THE CITY MAY PERFORM THE WORK OR HAVE THE WORK DONE AND
- BILL THE RESPONSIBLE PARTY. 17. IT IS THE RESPONSIBILITY OF THE OWNER TO ENSURE THAT VEHICLE TRACKING CONTROL IS IN PLACE,
- FUNCTIONAL, AND MAINTAINED THROUGHOUT THE CONSTRUCTION PHASE OF THIS PROJECT. 18. INDIVIDUALS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33USC 1344), REGULATIONS PROMULGATED, CERTIFICATIONS OR PERMITS ISSUED, IN ADDITION TO CITY OF FOUNTAIN REQUIREMENTS. IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS,

THE MORE RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL APPLY.

PREPARED BY:

Kiowa Engineering Corporation

1604 South 21st Street Colorado Springs, Colorado 80904-4208 [719] 630-7342



9 - DETENTION BASIN 'D'
TION MODIFICATIONS
OL PLAN AND STORM PROFILE

Kiowa Engineerin
1604 South 21st Street
Colorado Springs, Colorad
719] 630-7342

ESA RIDGE FILINGS 8 & 9 - DETENTION BASIN FULL SPECTRUM DETENTION MODIFICATIONS RADING AND EROSION CONTROL PLAN AND STORM PROF FOUNTAIN, COLORADO

Project No.: 09061

Date: October 17, 2011

Design: RNW

Drawn: JGD

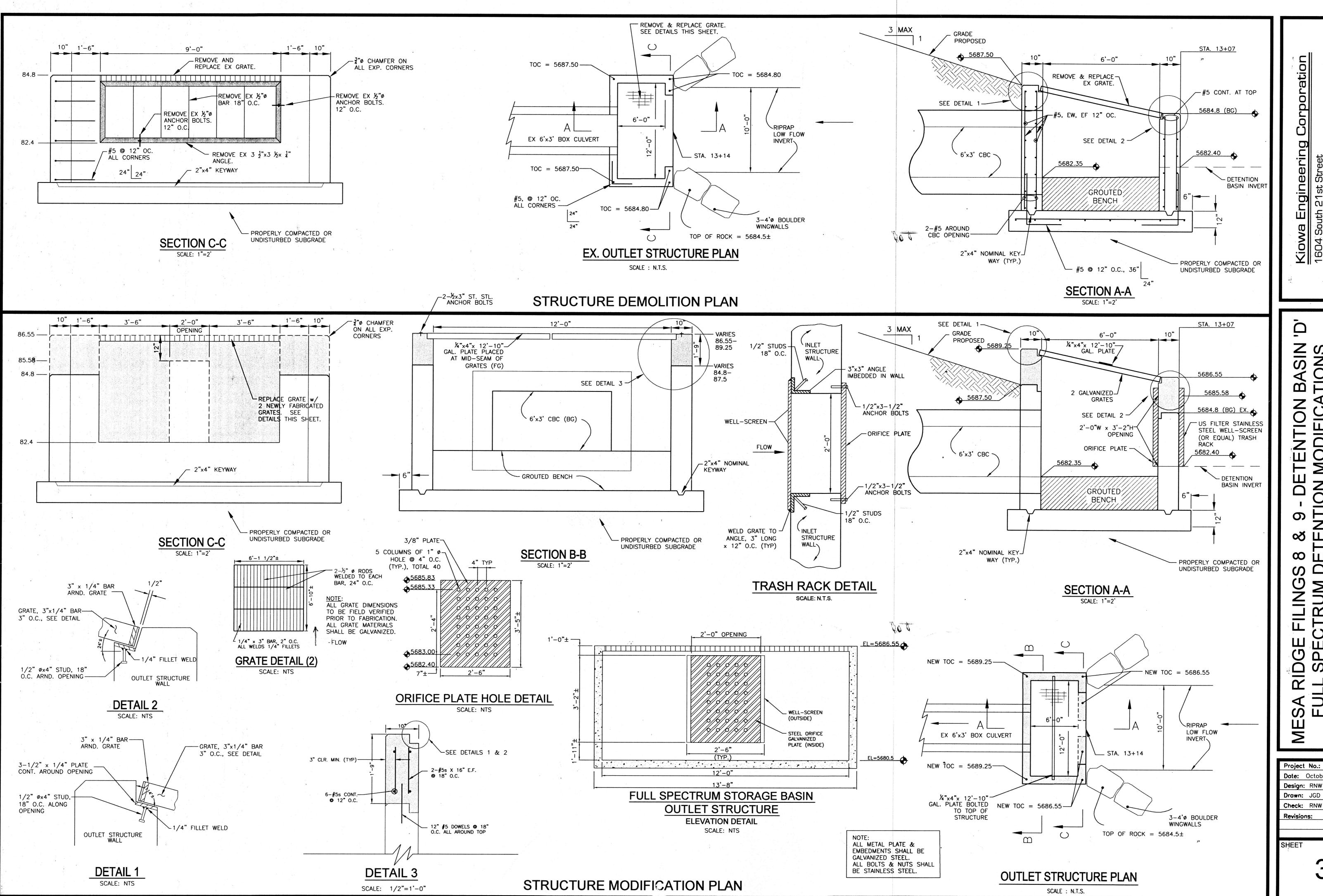
Check: RNW

Revisions:

SHEET

OF 3 SHEETS

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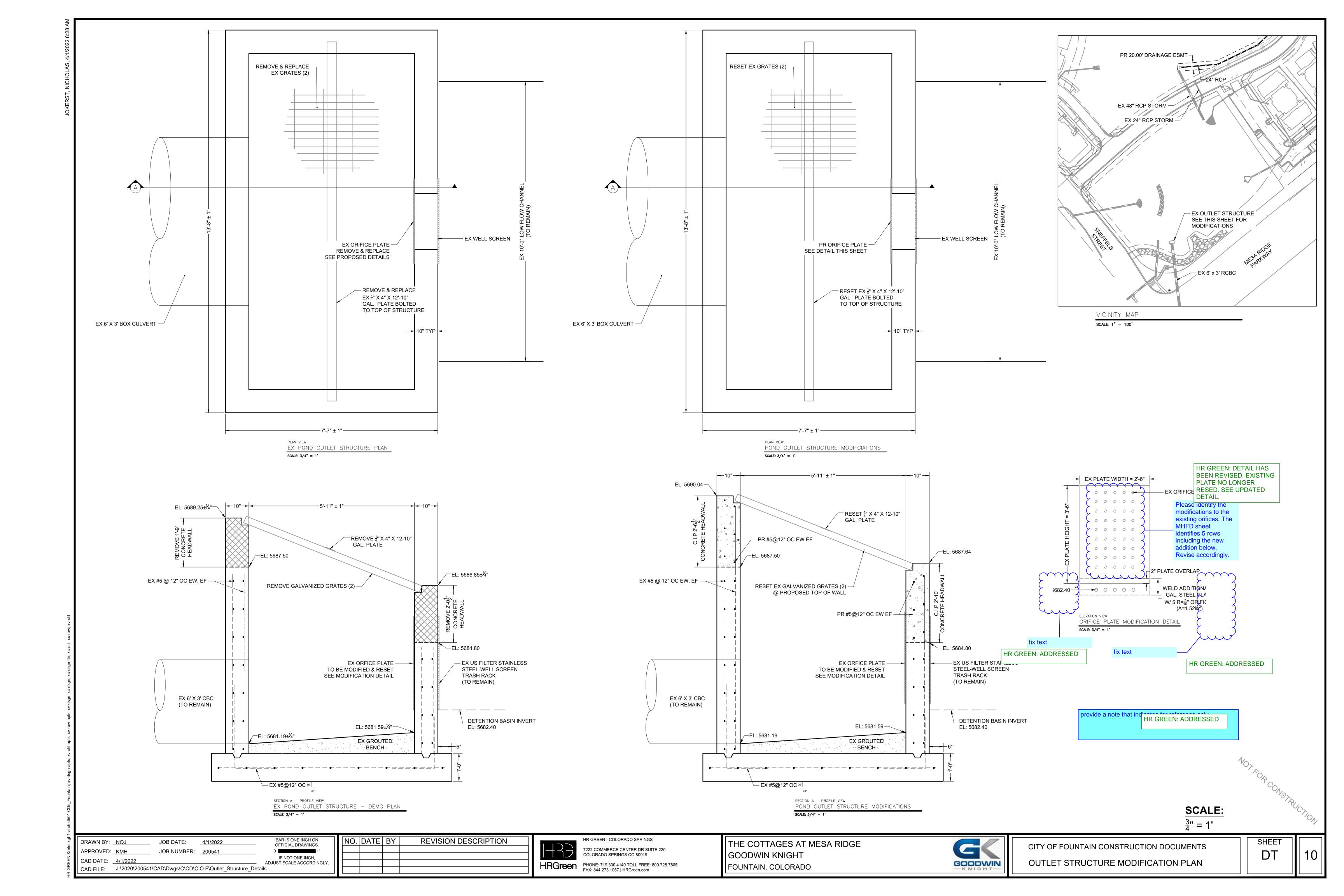


1604 South 21st S Colorado Springs, (80904-4208 (719) 630-7342 FILING RIDGE LL SPE(

Project No.: 09061 Date: October 24, 2011 Design: RNW Drawn: JGD Check: RNW Revisions: SHEET

OF 3 SHEETS

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Please remove the FAE form from HR GREEN: ADDRESSED report.

2022 Financial Assurance Estimate Form (with pre-plat construction)

(with pre-plat construction)				Updated: 11/4/2021
	PROJECT I	NFORMATIO	ON	
The Cottages at Mesa Ridge	-	Date	4/1/2022	PCD File No.

				Unit				,	-Plat Construction)
Description	Quantity	Units		Cost			Total	% Complete	Remaining
SECTION 1 - GRADING AND EROSION CONTR	OL (Construction	on and Perm	nanen	t BMPs)					
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less than 1,000; \$5,300 min		CY	\$	6.00	=	\$			4
1,000-5,000; \$8,000 min 5,001-20,000; \$30,000 min		CY	\$	5.00		\$			4
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greater than 200,000; \$500,000 min		CY	\$	2.00		\$			\$ -
* Permanent Seeding (inc. noxious weed mgmnt.)		AC	\$	886.00		\$			\$ -
* Mulching		AC	\$	831.00		\$			\$ -
* Permanent Erosion Control Blanket		SY	\$	7.00		\$			\$ -
* Permanent Pond/BMP Construction		CY	\$	22.00		\$			\$ -
* Permanent Pond/BMP (provide engineer's estimate)		EA	Ψ	22.00		\$			\$ -
Porticinent Portar Divin (provide originate)		EA				\$			\$ -
Safety Fence		LF	\$	3.00		\$			\$ -
Temporary Erosion Control Blanket		SY	\$	3.00	=	\$			\$ -
Vehicle Tracking Control		EA		2,625.00	=	\$			\$ -
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Temporary Seeding		AC	\$	695.00	=	\$			\$ -
Temporary Mulch		AC	\$	831.00		\$			\$ -
Erosion Bales		EA	\$	28.00		\$	_		\$ -
Erosion Logs/Straw Wattles		LF	\$	6.00		\$			\$ -
Rock Check Dams		EA	\$	554.00		\$			\$ -
Inlet Protection		EA	\$	185.00		\$			\$ -
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[insert items not listed but part of construction plans]						\$			\$ -
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- Subject to defect warranty financial assurance. A minimum of 20% shall	iti Enance (55	70 OI COIISCI	ucc.o.	5 5,		Ψ			Ψ
be retained until final acceptance (MAXIMUM OF 80% COMPLETE		Section	n 1 C	O L. 4 4 1		-	_		\$ -
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Construction Traffic Control Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (8" thick, 6' wide to include return) Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return)		LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY SY SY SY SY EA	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 26.00 221.00 32.00 32.00 32.00 53.00 66.00 106.00 1,273.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (4" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) —" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return) Curb Chase		LS Tons CY SY SY Tons SF EA EA LF LF LF SY SY SY SY LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 26.00 221.00 32.00 32.00 32.00 53.00 66.00 80.00 1,273.00 67.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return)		LS Tons CY SY SY Tons SF EA EA LF LF SY SY SY LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 26.00 221.00 27.00 32.00 32.00 32.00 66.00 80.00 106.00 1,273.00 67.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Construction Traffic Control Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement Architage (147 lbs/cf) Asphalt Pavement Pavement Architag		LS Tons CY SY SY Tons SF EA EA LF LF LF SY SY SY SY LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 221.00 27.00 32.00 32.00 32.00 53.00 66.00 80.00 106.00 1,273.00 107.00 107.00 107.00 107.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Aspold Pavement Marking Barricade - Type 1 Curb and Gutter, Type 8 Curb and Gutter, Type 8 Curb and Gutter, Type C Cross Pan, local (8" thick, 6' wide to include return) Curb Cross Pan, collector (9" thick, 8' wide to include return) Curb Chase Guardrail Type 3 (W-Beam)		LS Tons CY SY SY Tons SF EA EA LF LF SY SY SY LF EA LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 221.00 27.00 32.00 32.00 53.00 66.00 80.00 106.00 1,273.00 67.00 102.00 1,639.00 55.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf)" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (6" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return) Curb Chase Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete)		LS Tons CY SY SY SY Tons SF EA EA LF LF SY SY SY LF EA LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 26.00 221.00 27.00 32.00 32.00 53.00 66.00 80.00 106.00 1,273.00 67.00 102.00 102.00 102.00 103.00 80.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ - \$ \$ \$ -
Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) —" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 8" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Curb Chase Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete) Guardrail End Anchorage		LS Tons CY SY SY SY Tons SF EA EA SF EA LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 221.00 32.00 32.00 32.00 53.00 66.00 106.00 1,273.00 67.00 102.00 1,639.00 55.00 80.00 2,324.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) —" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 8" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return) Curb Chase Guardrail Type 7 (Concrete) Guardrail Impact Attenuator		LS Tons CY SY SY SY Tons SF EA EA SF SF EA LF LF LF LF LF LF SY SY SY SY SY SY LF LF LF EA LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 9.00 333.00 15.00 221.00 32.00 32.00 32.00 53.00 66.00 80.00 106.00 1,273.00 67.00 102.00 1,639.00 55.00 80.00 2,324.00 4,172.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -
Construction Traffic Control Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement Marking Berricade - Type 3 Belineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) A" Sidewalk (common areas only) 5" Sidewalk B" Sidewalk B" Sidewalk Bedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return) Curb Chase Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete) Guardrail Impact Attenuator Sound Barrier Fence (CMU block, 6' high)		LS Tons CY SY SY SY Tons EA EA LF LF LF SY SY SY LF LF EA LF	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	31.00 56.00 16.00 21.00 32.00 97.00 3333.00 15.00 221.00 221.00 32.00 32.00 32.00 32.00 66.00 80.00 1,273.00 67.00 102.00 1,639.00 55.00 80.00 2,324.00 4,172.00 87.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			\$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ - \$ -

	PROJECT I	NFORMAT	ION	
The Cottages at Mesa Ridge	•	Date	4/1/2022	PCD File No.

			Unit			(with Pre-Plat Construction)		
Description	Quantity	Units	Cost		Total	% Complete	Remaining	
				=	\$ -		Т	-
[insert items not listed but part of construction plans]				=	\$ -		\$	-
STORM DRAIN IMPROVEMENTS								
Concrete Box Culvert (M Standard), Size (W x H)		LF		=	\$ -		\$	-
18" Reinforced Concrete Pipe		LF	\$ 70.00	=	\$ -		\$	-
24" Reinforced Concrete Pipe		LF	\$ 83.00	=	\$ -		\$	-
30" Reinforced Concrete Pipe		LF	\$ 104.00	=	\$ -		\$	-
36" Reinforced Concrete Pipe		LF	\$ 128.00	=	\$ -		\$	-
42" Reinforced Concrete Pipe		LF	\$ 171.00	=	\$ -		\$	-
48" Reinforced Concrete Pipe		LF	\$ 209.00	=	\$ -		\$	-
54" Reinforced Concrete Pipe		LF	\$ 272.00	=	\$ -		\$	-
60" Reinforced Concrete Pipe		LF	\$ 319.00	=	\$ -		\$	-
66" Reinforced Concrete Pipe		LF	\$ 368.00	=	\$ -		\$	-
72" Reinforced Concrete Pipe		LF	\$ 421.00	=	\$ -		\$	-
18" Corrugated Steel Pipe		LF	\$ 90.00	=	\$ -		\$	-
24" Corrugated Steel Pipe		LF	\$ 103.00	=	\$ -		\$	-
30" Corrugated Steel Pipe		LF	\$ 131.00	=	\$ -		\$	-
36" Corrugated Steel Pipe		LF	\$ 157.00	=	\$ -		\$	-
42" Corrugated Steel Pipe		LF	\$ 180.00	=	\$ -		\$	-
48" Corrugated Steel Pipe		LF	\$ 190.00	=	\$ -		\$	-
54" Corrugated Steel Pipe		LF	\$ 278.00	=	\$ -		\$	-
60" Corrugated Steel Pipe		LF	\$ 300.00	=	\$ -		\$	-
66" Corrugated Steel Pipe		LF	\$ 364.00	=	\$ -		\$	-
72" Corrugated Steel Pipe		LF	\$ 428.00	=	\$ -		\$	-
78" Corrugated Steel Pipe		LF	\$ 492.00	=	\$ -		\$	-
84" Corrugated Steel Pipe		LF	\$ 588.00	=	\$ -		\$	-
Flared End Section (FES) RCP Size = (unit cost = 6x pipe unit cost)		EA		=	\$ -		\$	-
Flared End Section (FES) CSP Size =				_	\$ _		\$	_
(unit cost = 6x pipe unit cost)		EA		_				
End Treatment- Headwall		EA		=	\$ -		Ψ	-
End Treatment- Wingwall		EA		=	\$ -		Ψ	-
End Treatment - Cutoff Wall		EA		=	\$ -		Ψ	-
Curb Inlet (Type R) L=5', Depth < 5'		EA	\$ 6,138.00	=	\$ -		Ψ	-
Curb Inlet (Type R) L=5', 5'≤ Depth < 10'		EA	\$ 7,981.00	=	\$ -		Ψ	-
Curb Inlet (Type R) L =5', 10'≤ Depth < 15'		EA	\$ 9,242.00	=	\$ -		Ψ	-
Curb Inlet (Type R) L =10', Depth < 5'		EA	\$ 8,447.00	=	\$ -		Ψ	-
Curb Inlet (Type R) L =10', 5'≤ Depth < 10'		EA	\$ 8,706.00	=	\$ -		Ψ	-
Curb Inlet (Type R) L =10', 10'≤ Depth < 15'		EA	\$ 10,898.00	=	\$ -		т	-
Curb Inlet (Type R) L =15', Depth < 5'		EA	\$ 10,984.00	=	\$ -		\$	-
Curb Inlet (Type R) L =15', 5'≤ Depth < 10'	1	EA	\$ 11,775.00	=	\$ 11,775.00		\$ 11,775	
Curb Inlet (Type R) L =15', 10'≤ Depth < 15'	1	EA	\$ 12,876.00	=	\$ 12,876.00		\$ 12,876	6.00
Curb Inlet (Type R) L =20', Depth < 5'		EA	\$ 11,706.00	=	\$ -		\$	-
Curb Inlet (Type R) L =20', 5'≤ Depth < 10'		EA	\$ 12,920.00	=	\$ -		Ψ	-
Grated Inlet (Type C), Depth < 5'	1	EA	\$ 5,138.00	=	\$ 5,138.00		\$ 5,138	8.00
Grated Inlet (Type D), Depth < 5'		EA	\$ 6,347.00	=	\$ -		\$	-
Storm Sewer Manhole, Box Base		EA	\$ 12,876.00	=	\$ -		Ψ	-
Storm Sewer Manhole, Slab Base	4	EA	\$ 7,082.00	=	\$ 28,328.00		\$ 28,328	8.00
Geotextile (Erosion Control)		SY	\$ 7.00	=	\$ -		\$	-
Rip Rap, d50 size from 6" to 24"		Tons	\$ 89.00	=	\$ -		\$	-
Rip Rap, Grouted		Tons	\$ 105.00	=	\$ -		\$	-
Drainage Channel Construction, Size (W x H)		LF	\$ -	=	\$ -		т	-
Drainage Channel Lining, Concrete		CY	\$ 631.00	=	\$ -		\$	-
Drainage Channel Lining, Rip Rap		CY	\$ 124.00	=	\$ -		\$	-
Drainage Channel Lining, Grass		AC	\$ 1,626.00	=	\$ -		\$	-
Drainage Channel Lining, Other Stabilization				=	\$ -		\$	-
				=	\$ -		\$	-
[insert items not listed but part of construction plans]				=	\$ -		\$	-
 Subject to defect warranty financial assurance. A minimum of 20% shall be retained until final acceptance (MAXIMUM OF 80% COMPLETE 		Soction	n 2 Subtotal	=	\$ 58,117.00		\$ 58,117.	00

	PROJECT INFORMATION										
The Cottages at Mesa Ridge	-	Date	4/1/2022		PCD File No.						

				Unit				(with Pre	-Plat	Construction)
Description	Quantit	y Ur	nits	Cost			Total	% Complete		Remaining
SECTION 3 - COMMON DEVELOPMEN	IT IMPROVEMENTS	(Private	or Dis	trict and I	NOT Mai	ntained	by EPC)**			
ROADWAY IMPROVEMENTS										
Thermoplastic Pavement Marking			SF :	\$ 26.00	=	\$	-		\$	-
Asphalt Pavement (6" thick)			SY :	\$ 32.00	=	\$	-		\$	-
Curb and Gutter, Type A (6" Vertical)		L	.F :	\$ 32.00	=	\$	-		\$	-
Curb and Gutter, Type C (Ramp)		L	F S	\$ 32.00	=	\$	-		\$	-
Pedestrian Ramp		E	A	\$ 1,273.00	=	\$	-		\$	-
4" Sidewalk (common areas only)		5	SY :	\$ 53.00	=	\$	-		\$	-
STORM DRAIN IMPROVEMENTS	(Exception: Permaner	nt Pond/BMF	shall be	itemized und	der Section	1)				
12" PVC STORM PIPE		315 L	.F :	\$ 60.00	=	\$	18,900.00		\$	18,900.00
18" RCP STORM PIPE		178 l	.F :	\$ 70.00	=	\$	12,460.00		\$	12,460.00
24" RCP STORM PIPE		214 l	.F :	\$ 83.00	=	\$	17,762.00		\$	17,762.00
Curb Inlet (Type R) L =15', 5'≤ Depth < 10'		1 E	A S	\$ 11,775.00	=	\$	11,775.00		\$	11,775.00
Curb Inlet (Type R) L =15', 10'≤ Depth < 15'		1 E	Α :	\$ 12,876.00	=	\$	12,876.00		\$	12,876.00
Grated Inlet (Type C)		1 E	A	\$ 5,138.00	=	\$	5,138.00		\$	5,138.00
Outlet Structure Modifciations		1 l	S !	\$ 10,000.00	=	\$	10,000.00		\$	10,000.00
					=	\$	-		\$	-
WATER SYSTEM IMPROVEMENTS										
Water Main Pipe (PVC), Size 4"		L	.F _	\$ 60.00	=	\$	-		\$	-
Water Main Pipe (PVC), Size 8"		L	.F :	\$ 71.00	=	\$	-		\$	-
Water Main Pipe (Ductile Iron), Size 8"		l l	.F _	\$ 83.00	=	\$	-		\$	-
Gate Valves, 8"		E	Α :	\$ 2,058.00		\$	-		\$	-
Fire Hydrant Assembly, w/ all valves		E	Α :	\$ 7,306.00	=	\$	-		\$	-
Water Service Line Installation, inc. tap and valv	/es	E	Α :	\$ 1,466.00	=	\$	-		\$	-
Fire Cistern Installation, complete		E	A		=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction p	lans]				=	\$	-		\$	-
SANITARY SEWER IMPROVEMENTS										
Sewer Main Pipe (PVC), Size 8"		L		\$ 71.00	=	\$	-		\$	-
Sanitary Sewer Manhole, Depth < 15 feet		E		\$ 4,858.00	=	\$	-		\$	-
Sanitary Service Line Installation, complete				\$ 1,553.00	=	\$	-		\$	-
Sanitary Sewer Lift Station, complete		E	A		=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction p	•				=	\$	-		\$	-
LANDSCAPING IMPROVEMENTS	(For subdivision			of approval, o	r PUD)					
			A		=	\$	-		\$	-
			A		=	\$	-		\$	-
		_	A		=	\$	-		\$	-
			A		=	\$	-		\$	-
		_	A		=	\$	-		\$	-
** - Section 3 is not subject to defect warranty requirements		S	ection	3 Subtotal	=	\$	88,911.00		\$	88,911.00

	PROJECT I	NFORMATIO	N		
The Cottages at Mesa Ridge		Date	4/1/2022	PCD File No.	

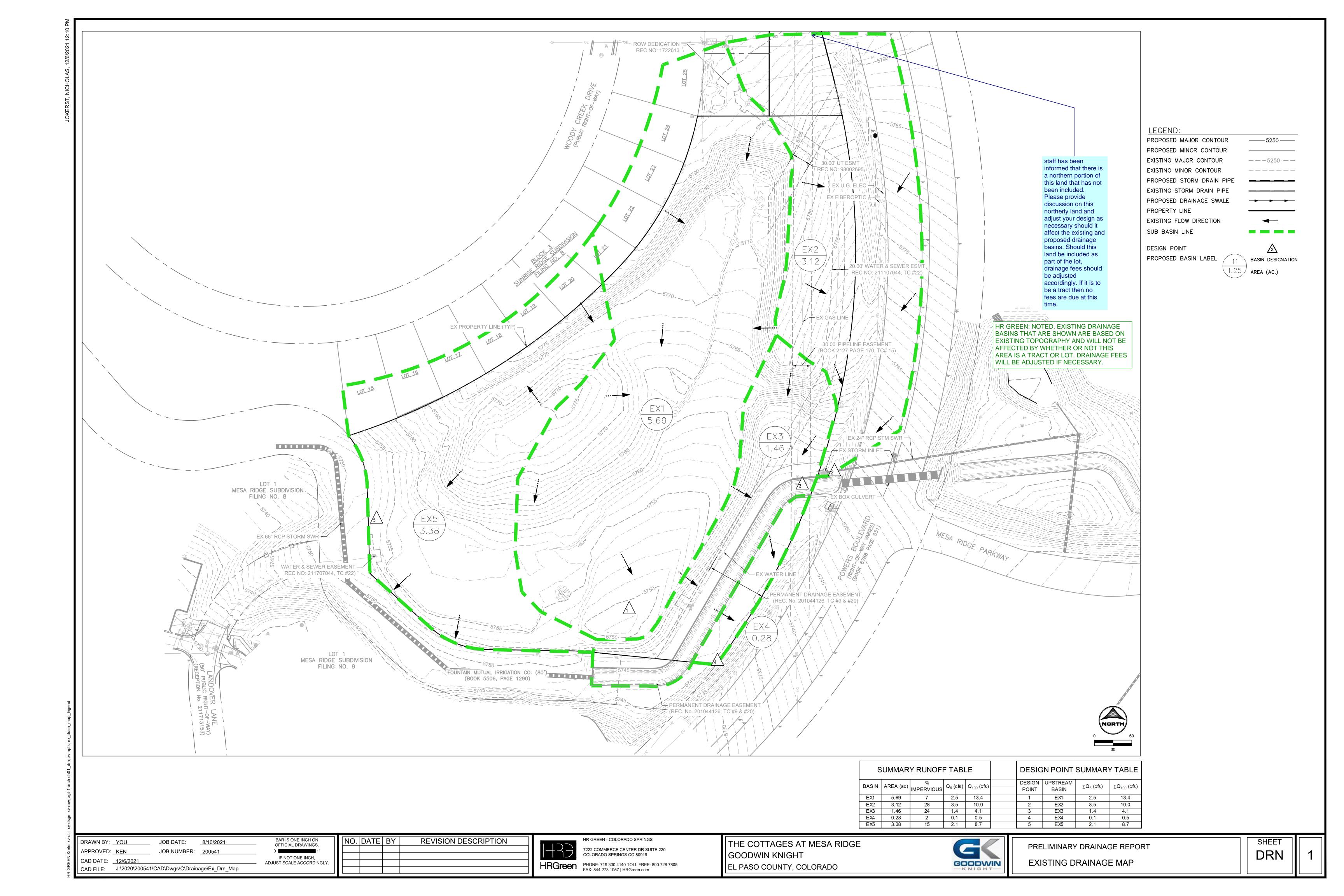
			Unit				(with Pre-F	Plat Construction)
Description	Quantity	Units	Cost		Total		% Complete	Remaining
AS-BUILT PLANS (Public Improvements inc. Perman	ant WOCV RMPs)	LS		_	¢			
POND/BMP CERTIFICATION (inc. elevations and volu		LS		=	\$	-	3	-
				Total	Construction F	inancia	I Assurance	\$ 147,028.00
			(Sum of all se	ction subtot	als plus as-builts ar	nd pond/B	MP certification)	
	Total Remain	ing Constr	uction Final	ncial Ass	urance (with Pr	e-Plat C	onstruction)_	\$ 147,028.00
	(Sum of all	section totals	less credit for i	tems compl	ete plus as-builts ar	nd pond/B	MP certification)	-
				Total De	efect Warranty F	inancia	I Assurance	\$ 11,623.40
	(2	20% of all items	s identified as (*). To be co	llateralized at time	of prelimin	arv acceptance)	•

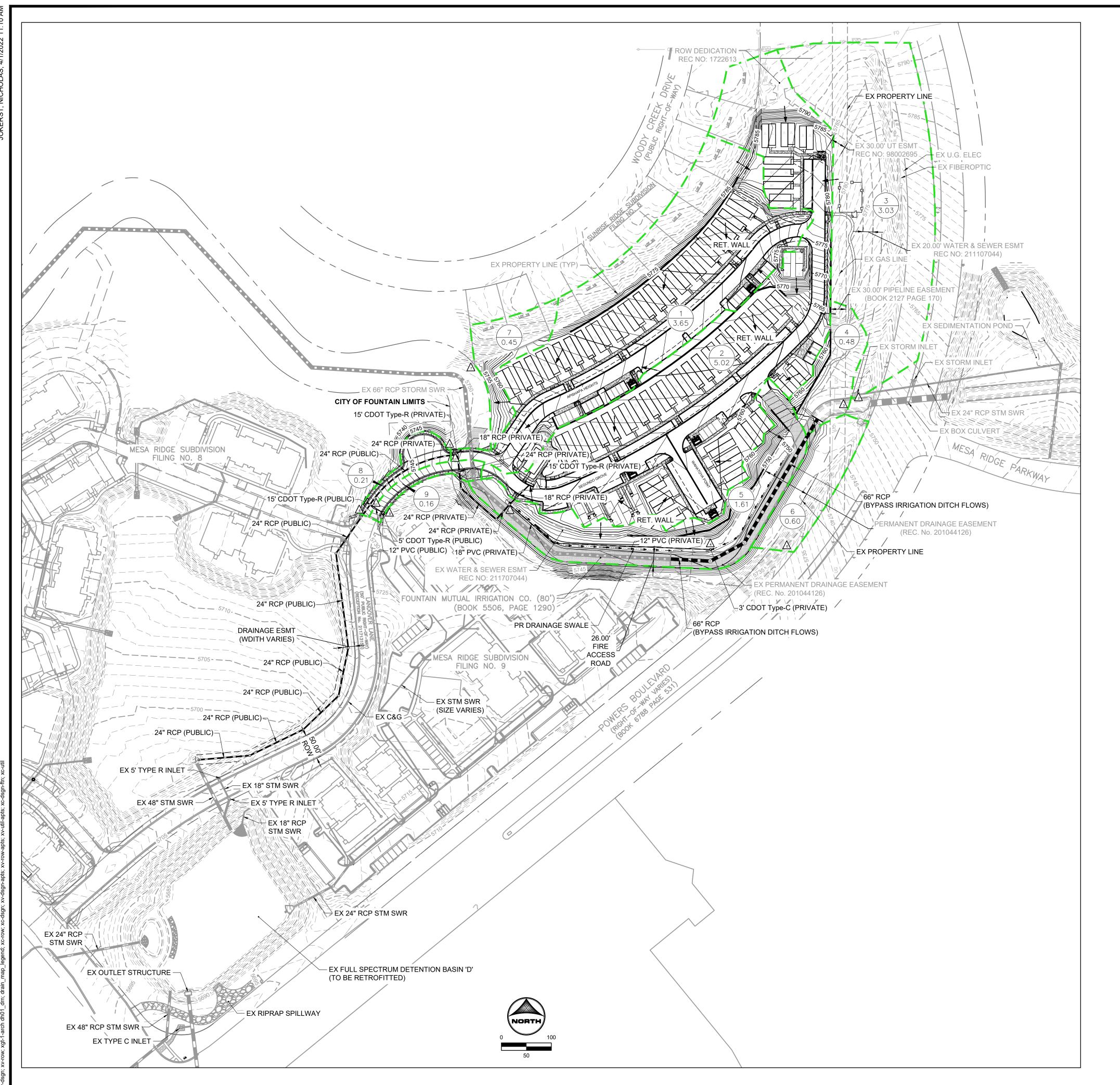
Approvals	
I hereby certify that this is an accurate and complete estimate of costs for the work as shown	n on the Grading and Erosion Control Plan and Construction Drawings associated with the Project.
Engineer (P.E. Seal Required)	
Approved by Owner / Applicant	Date
Approved by El Paso County Engineer / ECM Administrator	Date





APPENDIX F - DRAINAGE MAPS





LEGEND:	
PROPOSED MAJOR CONTOUR	 5250
PROPOSED MINOR CONTOUR	
EXISTING MAJOR CONTOUR	——————————————————————————————————————
EXISTING MINOR CONTOUR	
PROPOSED STORM DRAIN PIPE	
EXISTING STORM DRAIN PIPE	
PROPOSED DRAINAGE SWALE	
PROPERTY LINE	
PROPOSED FLOW DIRECTION	←
EXISTING FLOW DIRECTION	—
SUB BASIN LINE	
DESIGN POINT	\triangle
PROPOSED BASIN LABEL 11	BASIN DESIGNATION
1.25	AREA (AC.)

S	SUMMARY RUNOFF TABLE			_E	DESIGN POINT SUMMARY TABL			
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)	DESIGN POINT	UPSTREAM BASIN	ΣQ_5 (cfs)	ΣQ ₁₀₀ (cfs)
1	3.56	56	6.6	14.6	1	1	6.6	14.6
2	4.99	54	8.7	19.3	2	2	8.7	19.3
3	3.03	29	3.4	9.7	2.1	1 & 2	16.2	28.8
4	0.52	8	0.4	1.8	3	3 & 9	3.4	9.7
5	1.45	33	2.1	5.6	4	4	0.4	1.8
6	0.63	2	0.2	1.2	5	5	2.1	5.6
7	0.56	26	0.5	1.6	6	6	0.2	1.2
8	0.24	100	1.1	2.0	7	7	0.5	1.6
9	0.14	100	0.7	1.2	8	8	1.1	4.5
					9	9	0.9	6.6
					9.1	1, 2, 8 & 9	17.1	37.8

NO. DATE BY REVISION DESCRIPTION

HR GREEN - COLORADO SPRINGS 7222 COMMERCE CENTER DR SUITE 220 COLORADO SPRINGS CO 80919 HRGreen PHONE: 719.300.4140 TOLL FREE: 800.728.7805 FAX: 844.273.1057 | HRGreen.com

THE COTTAGES AT MESA RIDGE GOODWIN KNIGHT EL PASO COUNTY, COLORADO



PRELIMINARY DRAINAGE REPORT PROPOSED DRAINAGE MAP

DRN