

**FINAL DRAINAGE REPORT
FOR
PLATTE SELF STORAGE
COLORADO SPRINGS, COLORADO**

MAY 2024

Prepared For:
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TNE Job No. 2419.00

County Job No. ###

Please include project No.
PPR2418

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FOR
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COLORADO SPRINGS, COLORADO**

TABLE OF CONTENTS

Engineer's Statement	Page 3
Purpose	Page 4
General Description	Page 4
Existing Drainage Conditions	Page 5
Proposed Drainage Conditions	Page 6
Hydrologic Calculations	Page 9
Hydraulic Calculations	Page 9
Floodplain Statement	Page 10
Water Quality	Page 10
Construction Cost Opinion	Page 10
Drainage Fees	Page 11
Maintenance	Page 11
Summary	Page 11
Bibliography	Page 12

APPENDICIES

VICINITY MAP

NRCS SOILS MAP

FEMA FIRM MAP

HYDROLOGIC CALCULATIONS

HYDRAULIC CALCULATIONS

DETENTION CALCULATIONS

DRAINAGE PLAN

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DESIGN ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Dane Frank, P.E. 50207
On behalf of Terra Nova Engineering, Inc.

Date

OWNER/DEVELOPER'S STATEMENT:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

Authorized Signature

Date

Printed Name, Title

Business Name

Address

EL PASO COUNTY:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E.
County Engineer / ECM Administrator

Date

Conditions:

Joshua Palmer

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PURPOSE

The purpose of this Final Drainage Report is to identify and analyze the proposed drainage patterns, determine proposed runoff quantities, size drainage structures for conveyance of developed runoff, and present solutions to drainage impacts on-site and off-site resulting from this development. The site has not previously been platted or studied.

GENERAL DESCRIPTION

This Final Drainage Report (FDR) is an analysis of approximately 17.22 acres of developed land located at 6001 E Platte Ave. The site is currently in use as and landscaping materials yard and is being developed as a mini storage facility. The site is in the northwest quarter of Section 18, Township 14 South, Range 65 West of the 6th Principal Meridian within El Paso County. The parcels are bounded to the north by Motel Road and E Platte Ave, to the east by two unplatted lots, to the south by an unplatted lot and LOT 2 COLORADO SPRINGS AIRPORT FIL NO 1B, and to the west by unplatted lots. (see vicinity map in appendix).

The site lies within the Sand Creek Basin, with storm runoff surface draining west across the site, before flowing onto the neighboring property where Sand Creek East Fork is located.

Soils for this project are delineated by the map in the appendix as Blakeland loamy sand (8), 1 to 9 percent slopes. Soils in the study area are shown as mapped by NRCS in the “Soils Survey of El Paso County Area” and contains soils of Hydrologic Group A.

The site is currently developed with mostly dirt surfaces, some gravel and asphalt areas, and minimal vegetation that is mostly native grasses around the perimeter. The site drains to the west, with an average slope of 6.6%.

EXISTING DRAINAGE CONDITIONS

There are multiple existing buildings, a weight scale, miles of retaining or freestanding walls being used to create material storage areas, and a pond (low area that doesn't drain) on the site. Most of the west side of the site is bermed up before an embankment drops down, which results in little runoff leaving the site. The existing pond area is said to be largely paved (unconfirmed), so most runoff would leave the site by evaporation.

There are ten drainage basins, four of which are offsite. See attached Existing Drainage Map in the appendix.

Offsite Basins

Basin OS-Z is 6.34 acres and drains to Design Point Z on the east property line of the site. This basin is offsite and drains onto the site and into Basin EX-C. The basin surfaces are primarily dirt and gravel (construction yard). Basin OS-Z has flows of $Q_5 = 6.1$ cfs and $Q_{100} = 16.7$ cfs.

Basin OS-Y is 8.15 acres and drains to Design Point Y on the east property line of the site. This basin is offsite and drains onto the site and into Basin EX-C. The basin surfaces are primarily dirt and gravel (construction yard), with some native grass area. Basin OS-Y has flows of $Q_5 = 3.6$ cfs and $Q_{100} = 15.4$ cfs.

Basin OS-X is 1.20 acres and drains to Design Point X on the south property line of the site. This basin is offsite and drains onto the site and into Basin EX-C. The basin surfaces are native grass (undeveloped land). Basin OS-X has flows of $Q_5 = 0.4$ cfs and $Q_{100} = 2.3$ cfs.

Basin OS-W is 0.45 acres and drains to Design Point W on the north property line of the site. This basin is offsite and drains onto the site and into Basin EX-B. The basin surfaces are native grass and asphalt (area beside Motel Road and the site's driveway). Basin OS-W has flows of $Q_5 = 0.5$ cfs and $Q_{100} = 1.3$ cfs.

Onsite Basins

Basin EX-A is 0.30 acres and drains to Design Point A at the site's north property line. Runoff

flows off the site and onto the Motel Road right of way. This basin consists of landscaping areas and buildings. Basin EX-A has flows of $Q_5 = 0.2$ cfs and $Q_{100} = 0.8$ cfs.

Basin EX-B is 0.64 acres and drains to Design Point B at the at the site's north property line. Runoff flows off the site and onto the Motel Road right of way. This basin consists of landscaping areas, buildings, some pavement, and a swale. Basin EX-A has flows of $Q_5 = 1.1$ cfs and $Q_{100} = 2.6$ cfs.

Basin EX-C is 15.4 acres and drains to Design Point C at the existing pond on the site. Runoff doesn't appear to leave this pond other than by evaporation. This basin includes the bulk of the site and includes buildings, roads, storage areas, and parking areas. The surfaces are primarily dirt, gravel, or paved. Basin EX-C has flows of $Q_5 = 29.0$ cfs and $Q_{100} = 65.0$ cfs.

Basin EX-D is 1.05 acres and drains to Design Point D at the site's south/west property line. Runoff flows off the site and onto the adjacent property. This basin is primarily a dirt storage/stockpile area. Basin EX-D has flows of $Q_5 = 0.3$ cfs and $Q_{100} = 1.9$ cfs.

Indicate that this flow travels through Basin OS-X and enters back onto the site at DP X, combining flows with OS-X.

Basin EX-E is 0.16 acres and drains to Design Point E at the site's west property line. Runoff flows off the site and onto the adjacent property. This basin consists an earth embankment. Basin EX-E has flows of $Q_5 = 0.1$ cfs and $Q_{100} = 0.5$ cfs.

Basin EX-F is 0.23 acres and drains to Design Point F at the site's northwest property line. Runoff flows off the site and onto the adjacent property. This basin consists an earth embankment. Basin EX-F has flows of $Q_5 = 0.1$ cfs and $Q_{100} = 0.7$ cfs.

PROPOSED DRAINAGE CONDITIONS

Runoff in the developed conditions consists of 14 basins, four of which are offsite. Below is a description of the runoff in the developed conditions and how it will be safely routed, treated and detained. Basins on the west half of the site are proposed as undeveloped, but the proposed detention pond has been sized to account for their future commercial development.

Discuss how water quality is being addressed for each sub-basin.

Offsite Basins

The offsite basins remain the same as in the existing condition.

Please describe the path of runoff flow at each Design Point. Once collected at these points, where will the runoff flow next? How will these flows interact with the storm infrastructure (including proposed or existing pipes, culverts, inlets, swales, ponds, etc.)? Additional comments may be added after addressing these points.

Include what basins are being combined at each DP location

Onsite Basins

Basin PR-1 is 0.07 acres and drains to Design Point 1 at the site's north property line. Basin PR-1 is a landscaping area behind proposed Building B. Basin PR-1 has flows of $Q_5 = 0.0$ cfs and $Q_{100} = 0.2$ cfs.

Basin PR-2 is 0.13 acres and drains to Design Point 2 at the site's north property line. Basin PR-2 is a landscaping area behind proposed Building A. Basin PR-2 has flows of $Q_5 = 0.1$ cfs and $Q_{100} = 0.4$ cfs.

Basin PR-3 is 5.12 acres and drains to Design Point 3 at the west edge of the proposed mini-storage area. This area consists almost entirely of buildings and pavement that drain to an inlet. Basin PR-3 has flows of $Q_5 = 23.1$ cfs and $Q_{100} = 41.4$ cfs.

Basin PR-4 is 3.66 acres and drains to Design Point 4 at the west edge of a gravel parking area. This area is a gravel yard, and the two future canopies have been included in the drainage calculation. Basin PR-4 has flows of $Q_5 = 8.2$ cfs and $Q_{100} = 16.8$ cfs.

Please specify this inlet with private/public, proposed/existing, type, size. If it is a sump inlet, please discuss emergency path if it gets clogged.

Basin PR-5 is 0.56 acres and drains to Design Point 5 at the site's south property line. The swale in this basin catches offsite flow and carries it west and back offsite. Basin PR-5 has flows of $Q_5 = 0.1$ cfs and $Q_{100} = 0.9$ cfs.

Basin PR-6 is 6.64 acres and drains to Design Point 6 at the northeast corner of the site. This basin is most of the western portion of the site and will remain undeveloped. The **propoeed** detention pond is located in this basin. Basin PR-6 has flows of $Q_5 = 3.1$ cfs and $Q_{100} = 13.1$ cfs.

Basin PR-7 is 0.34 acres and drains to Design Point 7 at the northwest edge of the site. This basin is an earth embankment area that sheet flows offsite to the adjacent property. Basin PR-7 has flows of $Q_5 = 0.2$ cfs and $Q_{100} = 1.1$ cfs.

Basin PR-8 is 0.30 acres and drains to Design Point 8 at the west edge of the site. This basin is an earth embankment area that sheet flows offsite to the adjacent property. Basin PR-8 has flows of $Q_5 = 0.2$ cfs and $Q_{100} = 1.0$ cfs.

Basin PR-9 is 0.59 acres and drains to Design Point 9 at the west edge of the site. This basin is an earth embankment and flatter area that sheet flows offsite to the adjacent property. Basin PR-9 has flows of $Q_5 = 0.2$ cfs and $Q_{100} = 1.5$ cfs.

Basin PR-10 is 0.40 acres and drains to Design Point 10 at the east edge of the site. This basin is between the east property line and proposed buildings that is largely embankment with a concrete drain trench to collect runoff from offsite. The drain trench discharges into a storm sewer. Basin PR-10 has flows of $Q_5 = 0.3$ cfs and $Q_{100} = 1.4$ cfs.

List all the basins that contribute to DP 6.

At Design Point 6 the combined flow of the currently proposed development and future commercial development will be captured in a 2.657 acre-foot Extended Detention Basin. Runoff entering the pond through the storm sewer system will be routed into a 702 cu-ft concrete lined forebay with a 1.5 feet high concrete cutoff wall. A 3 inch notch in the wall drains the flow to a 2' concrete trickle channel, then the runoff is routed to the 3.0' deep micropool which has a 6" deep initial surcharge area. The 32.96 acres tributary to the EDB are 44% impervious. Based upon this we need a WQCV of 0.523 ac-ft, an EURV volume of 1.091 ac-ft and 100-year volume of 1.044 ac-ft for a total volume needed of 2.657 ac-ft. The bottom of the micropool elevation is at 6199.50 while the top of the ISV elevation is at 6202.50. The WQCV orifice starts at 6202.00 with two 1-5/8 inch diameter holes spaced 20.40 inches apart, then one 1-1/2 inch diameter hole spaced 20.40 inches apart, then one 3.00" diameter spaced 8.40 inches apart. A 4'x4' outlet structure is set at 6210.00. The 100-year water elevation tops out at 6210.54. A 18" HDPE storm pipe will release $Q_5=0.5$ cfs and $Q_{100}=11.3$ cfs discharge to a stilling basin at the west property line, which will outfall onto the adjacent property.

Please compare the runoff at the design point (DP) between the existing and proposed conditions as they leave the site.

There is one storm sewer system proposed on the site. This system collects runoff from the drain trench along the east property line and the two curb inlets in the mini-storage area and pipes the

The existing flow at this point appears to sheet flow, will a stilling basin be sufficient to ensure a suitable outfall and matching the existing condition?

runoff to the detention pond. There are a series of area inlets along the storm pipe in the mini-storage area that are not required to capture runoff, but will lessen the surface flow along the central drive aisle. The storm pipes on the west side of the site have been sized to have some extra capacity so that the future commercial development can tie into them as well.

In an effort to protect receiving water and as part of the “four-step process to minimize adverse impacts of urbanization” this site was analyzed in the following manner:

1. Reduce Runoff- There is no runoff reduction in the proposed mini-storage area. The proposed parking area south of the mini-storage has been surfaced with gravel, which will reduce runoff. These items will reduce the volume of runoff using ponding and infiltration.
2. Stabilize Drainageways- There are no existing or proposed drainageways onsite. The Sand Creek East Fork is located west of the site; however, channel improvements have previously been constructed there.
3. Provide Water Quality Capture Volume (WQCV)- The Extended Detention Basin has been sized and designed to sufficiently capture the required WQCV and slowly release it through the outlet structure, thereby allowing solids and contaminants to settle out.
4. Consider Need for Industrial and Commercial BMPs- The proposed development is an indoor mini storage facility; therefore, no Industrial and Commercial BMPs have been proposed.

Discuss exclusions to areas that do not drain to the proposed EDB

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County Storm Drainage Design Criteria Manual - Volumes 1 & 2, latest editions. The Rational Method was used to estimate storm water runoff anticipated from design storms with 5-year and 100-year recurrence intervals. The Urban Drainage Criteria Manual was used to calculate the detention and water quality volume.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning’s Formula and the methods described in the El Paso County Storm Drainage Design Criteria Manual – Volumes 1 & 2, latest editions. The pertinent data sheets are included in the appendix of this report.

A culvert is proposed at one of the site entrances. Design calculations have been included for the proposed culvert.

Street runoff capacity calculations for the onsite drive isles have been included.

FLOODPLAIN STATEMENT

No portion of this site is within a designated FEMA floodplain, as determined by FIRM Number 08041C0754 G, dated December 7, 2018 (see appendix).

WATER QUALITY

The proposed detention basin provides water quality treatment for nearly all of the proposed development.

Runoff from basins PR-1, PR-2, PR-5, PR-7, PR-8, and PR-9 are not captured by the proposed detention pond. Basins PR-1 and PR-2 are landscaping areas along the property line with no impervious area. Basin PR-5 is an undeveloped area with a swale that directs offsite flow back offsite, with no impervious area. Basins PR-7 and PR-8 are earth embankments on the downstream edge of the site that drop 10-15 feet in elevation, with no impervious area. Basin PR-9 is part flatter undeveloped area and part earth embankment on the downstream edge of the site that doesn't flow toward the detention pond, with no impervious area. The combined area of these basins is 1.69 acres, with zero impervious area. **As there is no impervious area in these basins, no WQCV treatment is required for them.** Additionally, as all of these basins are landscaping or undeveloped areas, they would qualify as water quality treatment areas (grass buffers).

CONSTRUCTION COST OPINION

Public Reimbursable

None

Public Non-Reimbursable

None

All disturbed areas are required to be accounted for with treatment or water quality exclusions, not impervious areas.

If the areas are proposed to as "runoff reduction" water quality treatment areas as stated in the sentence after, they need to be identified as separate pervious areas with supporting calculations and identified clearly on the plans. Vegetation in RPAs and SPAs should have a uniform density of at least 80%. In the Drainage Report, runoff reduction calculations (UD-BMP spreadsheet or equivalent) shall be included. In the Drainage Report, include a figure delineating all proposed UIA, RPA, and SPA areas to be utilized for runoff reduction. All RPAs and SPAs are considered PCMs and therefore require a signed PCM Maintenance Agreement and an O&M Manual.

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under "Permanent Pond/BMP (provide engineer's estimate)" in Section 1. The total should not include grading, which is a separate line item in Section 1: "Earthwork." The cost estimate should include labor costs (as a separate line item or added into the cost of each component).

Private Non-Reimbursable

1. 48" RCP	260 LF	\$ 245	\$ 63,700
2. 42" RCP	80 LF	\$ 201	\$ 16,080
3. 36" RCP	385 LF	\$ 151	\$ 58,135
4. 30" RCP	170 LF	\$ 123	\$ 20,910
5. 24" RCP	115 LF	\$ 98	\$ 11,270
6. 18" HDPE	36 LF	\$ 50	\$ 1,800
7. 6' Manhole	1 EA	\$ 10,000	\$ 10,000
8. 7' Manhole	1 EA	\$ 14,000	\$ 14,000
9. CDOT Type C Area Inlet	9 EA	\$ 6,037	\$ 54,333
10. 16' D-10-R Curb Inlet	1 EA	\$ 13,835	\$ 13,835
11. 20' D-10-R Curb Inlet	1 EA	\$ 20,000	\$ 20,000
12. Concrete Drain Trench	710 LF	\$ 200	\$ 142,000
13. EDB	1 EA	\$ 100,000	<u>\$ 100,000</u>
Total \$			426,063

DRAINAGE FEES

This drainage report is part of a site development application; therefore, no drainage fees are due.

MAINTENANCE

The Extended Detention Basin is private and will be maintained by the property owner. The proposed storm sewers are private and will be maintained by the property owner.

SUMMARY

Development of this site will not adversely affect the surrounding development. This report is in general conformance with the **previous reports** which included this site. Site runoff and storm drain appurtenances from the development will not adversely affect the downstream and surrounding developments and will be safely routed to the proposed extended detention basin and runoff reduced to the allowable pre-developed rates while slowly treating the water quality capture volume.

Please include name, date of approval and prepared by whom of the previous reports. Also, please include them in the reference part.

Provide discussion earlier in report discussing suitable outfall location. Provide comparison of existing flow rates to developed/released flow rates.

**PREPARED BY:
TERRA NOVA ENGINEERING, INC.**

Dane Frank, P.E.
Project Engineer

Jobs/2419.00/Drainage/241900 FDR.doc

BIBLIOGRAPHY

El Paso County Drainage Criteria Manual-Volumes 1 & 2, latest edition

VICINITY MAP



6001 E Platte Ave Subdivision - Location Map

Image Date Oct 2022



E Platte Ave / HWY 24

Motel Rd

Sand Creek

SITE

Google Earth

700 ft



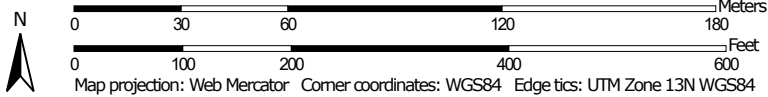
NRCS SOILS MAP

Soil Map—El Paso County Area, Colorado



Soil Map may not be valid at this scale.

Map Scale: 1:2,120 if printed on A portrait (8.5" x 11") sheet.



MAP LEGEND




















Area of Interest (AOI)


Area of Interest (AOI)

Soils


-  Soil Map Unit Polygons
-  Soil Map Unit Lines
-  Soil Map Unit Points

Special Point Features






-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

Water Features

-  Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

-  Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 21, Aug 24, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	16.5	100.0%
Totals for Area of Interest		16.5	100.0%

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v
Elevation: 4,600 to 5,800 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 48 degrees F
Frost-free period: 125 to 145 days
Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent
Minor components: 2 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats
Landform position (three-dimensional): Side slope, talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand
AC - 11 to 27 inches: loamy sand
C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e
Land capability classification (nonirrigated): 6e
***Hydrologic Soil Group:* A**
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent

Landform: Depressions

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 21, Aug 24, 2023

FEMA FIRM MAP

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only to landward of 0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, horizontal projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional inaccuracies in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1993 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
 NOAA, NNGS-12
 National Geodetic Survey
 SSMC-3, #9202
 1315 East-West Highway
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3420 or visit its website at <http://www.ngs.noaa.gov>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. This data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or dis-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

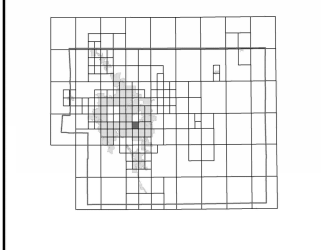
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/fip>.

El Paso County Vertical Datum Offset Table

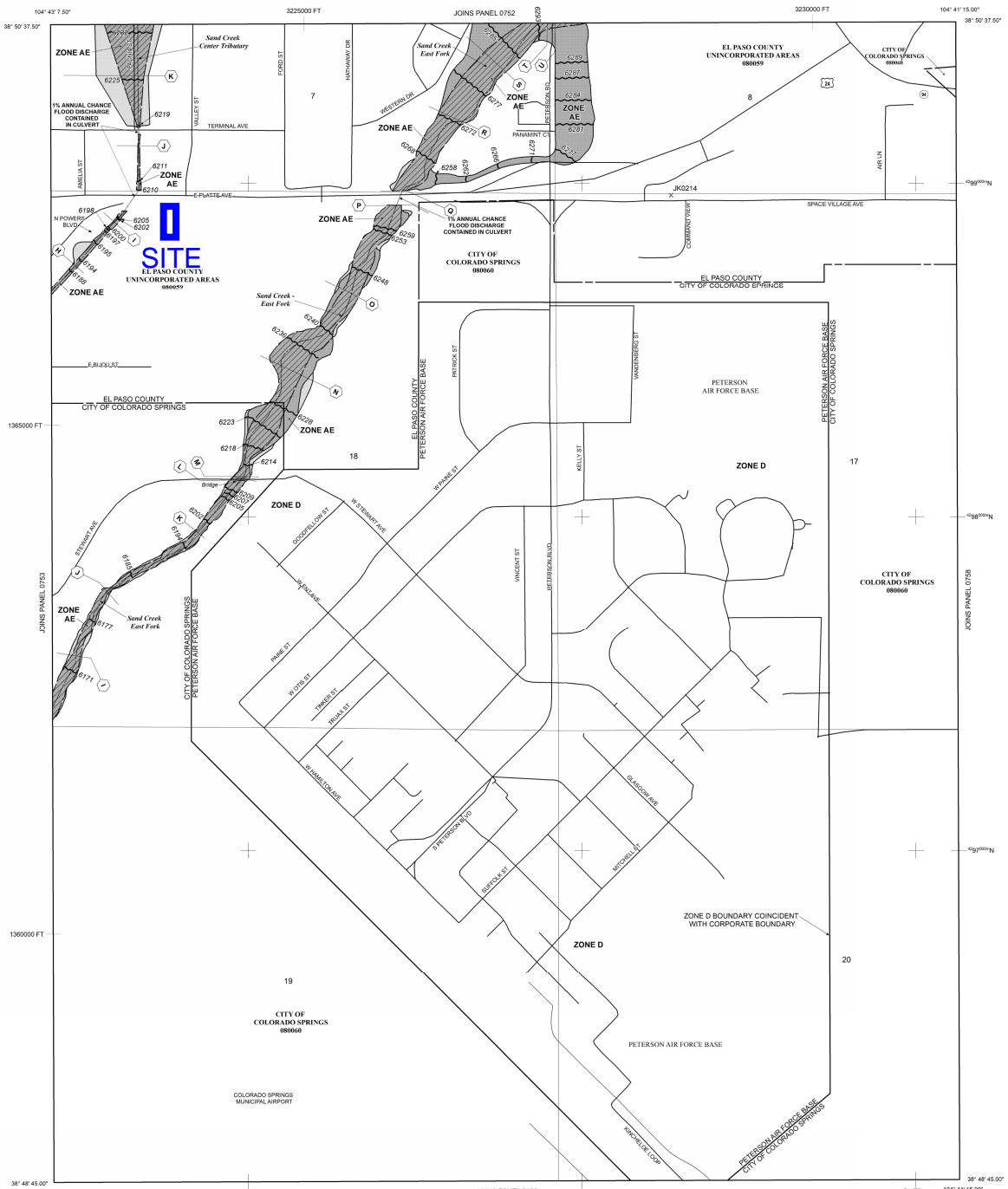
Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM-BY-STREAM VERTICAL DATUM CONVERSION INFORMATION.	

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 14 SOUTH, RANGE 65 WEST.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. This Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zone AE, AH, AO, AV, A, and V. The base flood elevation is the water-surface elevation of the 1% annual chance flood.

NO BASE FLOOD ELEVATIONS DETERMINED

ZONE AE Base Flood Elevations determined.

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of shallow fan flooding, velocities also determined.

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system (e.g., levee) that was subsequently identified. Zone AR indicates that the former flood control system is being retained to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot in any given year. This Special Flood Hazard Area is less than 1 square mile, and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain.

ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary
 Floodway boundary
 Zone D boundary
 CBRS and OPA boundary

Boundary, dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
 Base Flood Elevation line and value; elevation in feet*
 Base Flood Elevation value where uniform within zone; elevation in feet*
 * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross-section line
 Transient line
 Geographic coordinates refer to the North American Datum of 1983 (NAD 83)
 1000-meter Universal Transverse Mercator grid ticks, zone 13
 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (PROJZONE 020), Lambert Conformal Conic Projection
 Bench mark (see explanation in Notes to Users section of this FIRM report)
 M1.5 River Mile

MAP REPOSITORIES
 Refer to Map Repositories List on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
 MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
 DECEMBER 7, 2018. To update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Change.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'
 250 0 500 1000
 FEET
 150 0 150 300
 METERS

NFP

NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0754G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS

PANEL 754 OF 1300
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COUNTY	COMMUNITY	NUMBER	DATUM	SUFFIX
COLORADO SPRINGS, CITY OF	88000	0754	G	
EL PASO COUNTY	88000	0754	G	

Note: This map was released on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice to User Letter that accompanied this correction for details.

Note to User: The Map Number shown below should be used when showing map status. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
0841C0754G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

HYDROLOGIC CALCULATIONS

**PLATTE SELF STORAGE
AREA RUNOFF COEFFICIENT (C) SUMMARY**

EXISTING

BASIN	TOTAL AREA (Acres)	DEVELOPED / IMPERVIOUS			UNDEVELOPED / NON-IMPERVIOUS			WEIGHTED		WEIGHTED CA	
		AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀	CA ₅	CA ₁₀₀
<i>OS-Z</i>	6.34	1.90	0.90	0.96	4.44	0.08	0.35	0.33	0.53	2.07	3.38
<i>OS-Y</i>	8.15	0.82	0.90	0.96	7.33	0.08	0.35	0.16	0.41	1.32	3.35
<i>OS-X</i>	1.20	0.02	0.90	0.96	1.18	0.08	0.35	0.09	0.36	0.11	0.43
<i>OS-W</i>	0.45	0.11	0.90	0.96	0.34	0.08	0.35	0.28	0.50	0.13	0.22
<i>EX-A</i>	0.30	0.05	0.90	0.96	0.25	0.08	0.35	0.22	0.45	0.07	0.14
<i>EX-B</i>	0.64	0.29	0.90	0.96	0.35	0.08	0.35	0.45	0.63	0.29	0.40
<i>EX-C</i>	15.4	7.70	0.90	0.96	7.70	0.08	0.35	0.49	0.66	7.55	10.09
<i>EX-D</i>	1.05	0.02	0.90	0.96	1.03	0.08	0.35	0.10	0.36	0.10	0.38
<i>EX-E</i>	0.16	0.00	0.90	0.96	0.16	0.08	0.35	0.08	0.35	0.01	0.06
<i>EX-F</i>	0.23	0.00	0.90	0.96	0.23	0.08	0.35	0.08	0.35	0.02	0.08
Total	33.92	10.91									
										Calc:	DLF
										Date:	4/29/2024
										Checked:	

**PLATTE SELF STORAGE
AREA RUNOFF COEFFICIENT (C) SUMMARY**

PROPOSED

BASIN	TOTAL AREA (Acres)	DEVELOPED / IMPERVIOUS			UNDEVELOPED / NON-IMPERVIOUS			WEIGHTED		WEIGHTED CA	
		AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀	CA ₅	CA ₁₀₀
<i>OS-Z</i>	6.34	1.90	0.90	0.96	4.44	0.08	0.35	0.33	0.53	2.07	3.38
<i>OS-Y</i>	8.15	0.82	0.90	0.96	7.33	0.08	0.35	0.16	0.41	1.32	3.35
<i>OS-X</i>	1.20	0.02	0.90	0.96	1.18	0.08	0.35	0.09	0.36	0.11	0.43
<i>OS-W</i>	0.45	0.11	0.90	0.96	0.34	0.08	0.35	0.28	0.50	0.13	0.22
<i>1</i>	0.07	0.00	0.90	0.96	0.07	0.08	0.35	0.08	0.35	0.01	0.02
<i>2</i>	0.13	0.00	0.90	0.96	0.13	0.08	0.35	0.08	0.35	0.01	0.05
<i>3</i>	5.12	5.12	0.90	0.96	0.00	0.08	0.35	0.90	0.96	4.61	4.92
<i>4</i>	3.66	2.38	0.90	0.96	1.28	0.08	0.35	0.61	0.75	2.24	2.73
<i>5</i>	0.56	0.01	0.90	0.96	0.55	0.08	0.35	0.09	0.36	0.05	0.20
<i>6</i>	6.64	0.66	0.90	0.96	5.98	0.08	0.35	0.16	0.41	1.07	2.73
<i>7</i>	0.34	0.01	0.90	0.96	0.33	0.08	0.35	0.10	0.37	0.04	0.13
<i>8</i>	0.30	0.01	0.90	0.96	0.29	0.08	0.35	0.11	0.37	0.03	0.11
<i>9</i>	0.59	0.01	0.90	0.96	0.58	0.08	0.35	0.09	0.36	0.06	0.21
<i>10</i>	0.40	0.04	0.90	0.96	0.36	0.08	0.35	0.16	0.41	0.06	0.16
Total	33.95	11.09									

Calc:	DLF
Date:	4/29/2024
Checked:	0

Use same labeling convention as in report and on drainage map

PLATTE SELF STORAGE RUNOFF SUMMARY

EXISTING

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _t (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		<small>* For Calcs See Runoff Summary</small>														
OS-Z	6.34	0.33	0.53	0.33	300	0.02	19.3	230	2.0%	1.4	2.7	22.0	2.9	4.9	6.1	16.7
OS-Y	8.15	0.16	0.41	0.16	300	0.03	20.4	505	3.0%	1.7	4.9	25.3	2.7	4.6	3.6	15.4
OS-X	1.20	0.09	0.36	0.09	300	0.05	18.5	0	5.0%	2.2	0.0	18.5	3.2	5.4	0.4	2.3
OS-W	0.45	0.28	0.50	0.28	300	0.07	13.5	160	7.0%	2.6	1.0	14.5	3.6	6.0	0.5	1.3
EX-A	0.30	0.22	0.45	0.22	300	0.07	14.5	0	7.0%	2.6	0.0	14.5	3.6	6.0	0.2	0.8
EX-B	0.64	0.45	0.63	0.45	300	0.07	10.7	250	7.0%	2.6	1.6	12.2	3.8	6.4	1.1	2.6
EX-C	15.4	0.49	0.66	0.49	300	0.07	10.0	330	7.0%	2.6	2.1	12.1	3.8	6.4	29.0	65.0
EX-D	1.05	0.10	0.36	0.10	300	0.03	21.9	40	3.0%	1.7	0.4	22.2	2.9	4.9	0.3	1.9
EX-E	0.16	0.08	0.35	0.08	30	0.40	3.0	0	40.0%	6.3	0.0	5.0	5.2	8.7	0.1	0.5
EX-F	0.23	0.08	0.35	0.08	35	0.24	3.8	0	24.0%	4.9	0.0	5.0	5.2	8.7	0.1	0.7

Calc:	DLF
Date:	4/29/2024
Checked:	0

PLATTE SELF STORAGE RUNOFF SUMMARY

PROPOSED

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _t (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		* For Calcs See Runoff Summary														
OS-Z	6.34	0.33	0.53	0.33	300	0.02	19.3	230	2.0%	1.4	2.7	22.0	2.9	4.9	6.1	16.7
OS-Y	8.15	0.16	0.41	0.16	300	0.03	20.4	505	3.0%	1.7	4.9	25.3	2.7	4.6	3.6	15.4
OS-X	1.20	0.09	0.36	0.09	300	0.05	18.5	0	5.0%	2.2	0.0	18.5	3.2	5.4	0.4	2.3
OS-W	0.45	0.28	0.50	0.28	300	0.07	13.5	160	7.0%	2.6	1.0	14.5	3.6	6.0	0.5	1.3
1	0.07	0.08	0.35	0.08	100	0.08	9.3	0	8.0%	2.8	0.0	9.3	4.2	7.1	0.0	0.2
2	0.13	0.08	0.35	0.08	45	0.25	4.3	0	25.0%	5.0	0.0	5.0	5.2	8.7	0.1	0.4
3	5.12	0.90	0.96	0.90	100	0.02	2.9	450	2.0%	2.8	2.7	5.5	5.0	8.4	23.1	41.4
4	3.66	0.61	0.75	0.61	100	0.02	7.0	400	2.0%	1.0	6.7	13.7	3.7	6.1	8.2	16.8
5	0.56	0.09	0.36	0.09	300	0.02	25.0	0	2.0%	1.0	0.0	25.0	2.8	4.6	0.1	0.9
6	6.64	0.16	0.41	0.16	300	0.02	23.3	0	2.0%	1.0	0.0	23.3	2.9	4.8	3.1	13.1
7	0.34	0.10	0.37	0.10	25	0.33	2.8	0	33.0%	4.0	0.0	5.0	5.2	8.7	0.2	1.1
8	0.30	0.11	0.37	0.11	35	0.33	3.3	0	33.0%	4.0	0.0	5.0	5.2	8.7	0.2	1.0
9	0.59	0.09	0.36	0.09	100	0.06	10.1	0	6.0%	1.7	0.0	10.1	4.1	6.9	0.2	1.5
10	0.40	0.16	0.41	0.16	10	0.33	1.7	350	1.0%	2.0	2.9	5.0	5.2	8.7	0.3	1.4

Calc:	DLF
Date:	4/29/2024
Checked:	0

Use same labeling convention as in report and on drainage map

PLATTE SELF STORAGE SURFACE ROUTING SUMMARY

EXISTING

<i>Design Point(s)</i>	<i>Contributing Basins</i>	<i>Area (ac)</i>	<i>Flow (cfs)</i>	
			<i>Q₅</i>	<i>Q₁₀₀</i>
Z	OS-Z	6.34	6.1	16.7
Y	OS-Y	8.15	3.6	15.4
X	OS-X,EX-D	2.25	0.7	4.2
W	OS-W	0.45	0.5	1.3
A	EX-A	0.30	0.2	0.8
B	EX-B	0.64	1.1	2.6
C	OS-Z,OS-Y,OS-X,EX-C,EX-D	32.14	39.4	101.4
D	EX-D	1.05	0.3	1.9
E	EX-E	0.16	0.1	0.5
F	EX-F	0.23	0.1	0.7

Calc:	DLF
Date:	4/29/2024
Checked:	0

PLATTE SELF STORAGE SURFACE ROUTING SUMMARY

PROPOSED

Design Point(s)	Contributing Basins	Area (ac)	Flow (cfs)	
			Q_5	Q_{100}
1	PR-1	0.07	0.0	0.2
2	PR-2	0.13	0.1	0.4
3	PR-3	5.12	23.1	41.4
4	OS-Y,PR-4	11.81	11.8	32.2
5	OX-X,PR-5	1.76	0.5	3.3
6	PR-6	6.64	3.1	13.1
7	PR-7	0.34	0.2	1.1
8	PR-8	0.30	0.2	1.0
9	PR-9	0.59	0.2	1.5
10	OS-Z,PR-10	6.74	6.4	18.1

Calc:	DLF
Date:	4/29/2024
Checked:	0

Include design points W, X, Y & Z

This should include all basins which end up in detention pond

PLATTE SELF STORAGE PIPE ROUTING SUMMARY

<i>Pipe Run</i>	<i>Inlet #</i>	<i>Contributing Flow Sources</i>	<i>5 Year Flow (cfs)</i>	<i>100 Year Flow (cfs)</i>	<i>Slope</i>	<i>Pipe Size & Type</i>	<i>Owner</i>
<i>PR#1</i>	-	PR#2	41.4	91.7	2.7%	48" RCP	PVT
<i>PR#2</i>	-	PR#3	41.4	91.7	2.2%	48" RCP	PVT
<i>PR#3</i>	#1	PR#4,PR-3	41.4	91.7	2.2%	42" RCP	PVT
<i>PR#4</i>	#2	PR#5	18.3	50.3	1.7%	42" RCP	PVT
<i>PR#5</i>	#3	PR#6,PR#11	18.3	50.3	2.1%	42" RCP	PVT
<i>PR#6</i>	#4	PR#7	6.4	18.1	5.0%	30" RCP	PVT
<i>PR#7</i>	#5	PR#8	6.4	18.1	1.9%	30" RCP	PVT
<i>PR#8</i>	#6	PR#9	6.4	18.1	1.9%	30" RCP	PVT
<i>PR#9</i>	#7	PR#10	6.4	18.1	1.9%	24" RCP	PVT
<i>PR#10</i>	#10	PR#13	6.4	18.1	1.7%	24" RCP	PVT
<i>PR#13</i>	#11	OS-Z,PR-10	6.4	18.1	1.9%	24" RCP	PVT
<i>PR#11</i>	#8	PR#12	11.8	32.2	1.0%	36" RCP	PVT
<i>PR#12</i>	#9	OS-Y,PR-4	11.8	32.2	1.0%	36" RCP	PVT
<i>PR#90</i>	-	Pond outlet	0.5	11.3	1.4%	18" HDPE	PVT

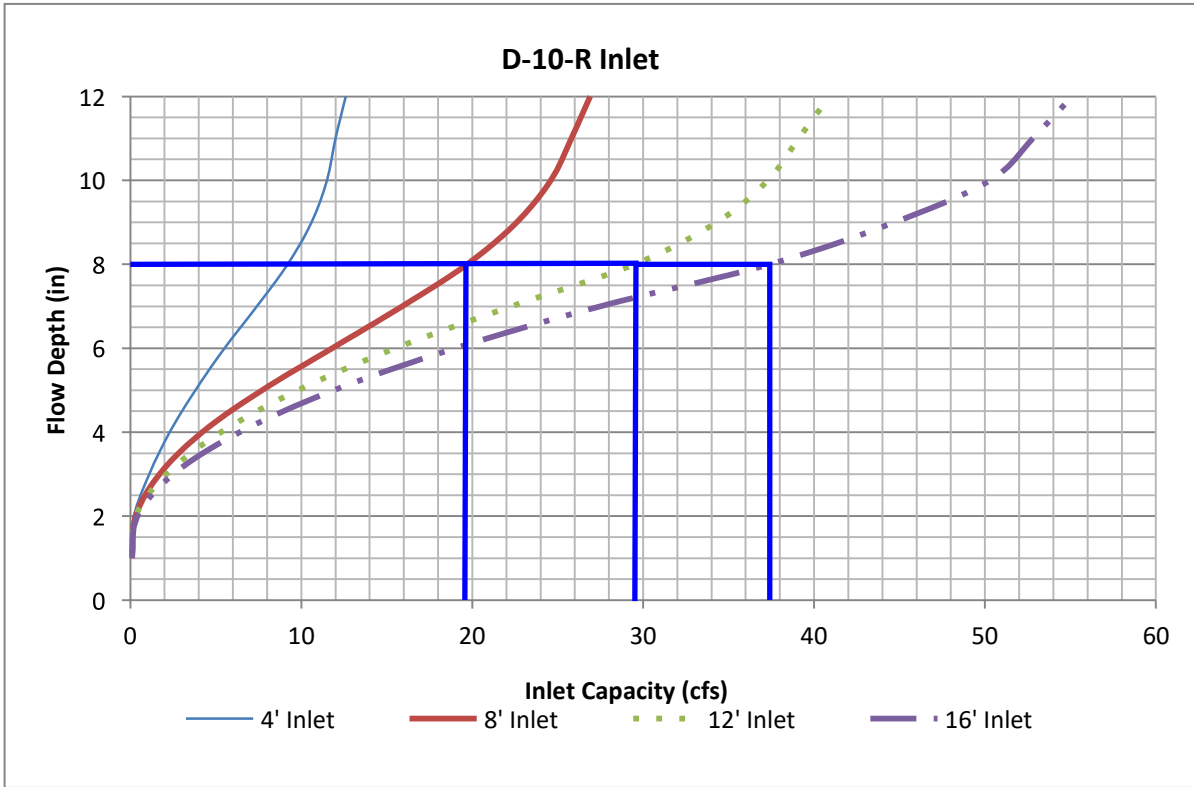
Calc:	DLF
Date:	4/29/2024
Checked:	0

HYDRAULIC CALCULATIONS

Please include inlet
management tab, and
inlet calculations.

Also include calculations for
riprap outlet protection

Figure 8-12. Inlet Capacity Chart Sump Conditions, Curb Opening (D-10-R) Inlet



- A 8' inlet has a capacity of 19.5 cfs.
- A 12' inlet has a capacity of 29.5 cfs.
- A 16' inlet has a capacity of 37.0 cfs.
- Combining 8' and 12' inlets would give a capacity of 49 cfs for a 20' inlet.

Please provide swale ID. Please ensure IDs match the ID labeled on the proposed drainage map.

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **Mini-Storage 30' V Drive Aisles at 1% - Capacity**
 By: **Dane Frank** Date: **4/2/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

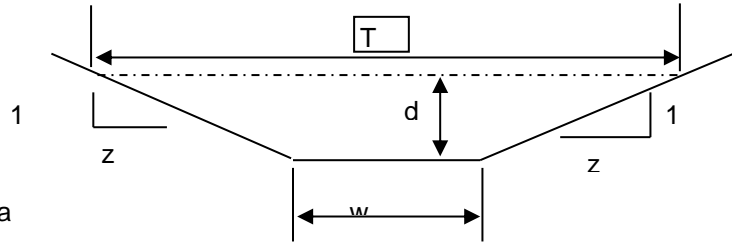
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 20
 z (sideslope)= 20
 b (btm width, ft)= 0
 d (depth, ft)= 0.25
 S (slope, ft/ft) 0.01
 n_{low} = 0.013
 n_{high} = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.25	1.25	10.01	0.12	2.85511683	3.5689	2.855117	3.5689	10	0.125

Sc low = 0.0049 Sc high = 0.0049

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.0035	0.0064	0.0035	0.0064

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **Mini-Storage Drive Aisles at 2% - Capacity**
 By: **Dane Frank** Date: **3/27/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

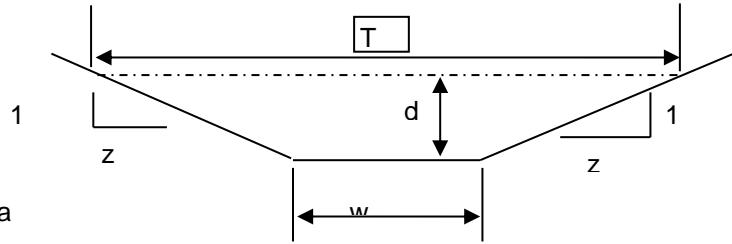
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 33.3
 z (sideslope)= 33.3
 b (btm width, ft)= 0
 d (depth, ft)= 0.35
 S (slope, ft/ft) 0.02
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.35	4.08	23.32	0.17	5.0558412	20.624	5.055841	20.624	23.31	0.175

Sc low = 0.0044 Sc high = 0.0044

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.0031	0.0057	0.0031	0.0057

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **East Drain Trench (need Q=9.1 cfs)**
 By: **John Fornander** Date: **4/19/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

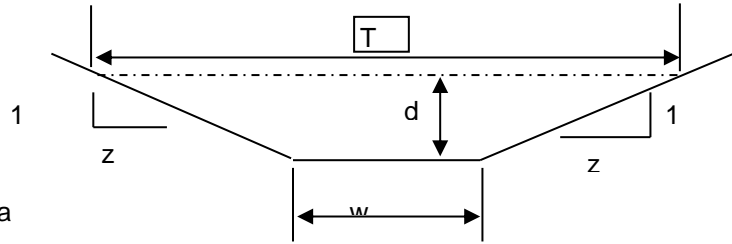
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 0
 b (btm width, ft)= 1.5
 d (depth, ft)= 1
 S (slope, ft/ft) 0.01
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
1	1.50	3.50	0.43	6.49748573	9.74623	6.497486	9.74623	1.5	1.000
Sc low =				0.0076	Sc high =		0.0076		
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc		
				0.0053	0.0099	0.0053	0.0099		

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

Created by: Mike O'Shea

Please provide erosion protection for this open channel as velocity is above the standard velocity per DCM vol.1, chapter 10, table 10-4

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **Bldg AH Drive Aisle (need Q=3.6 cfs)**
 By: **John F** Date: **4/2/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

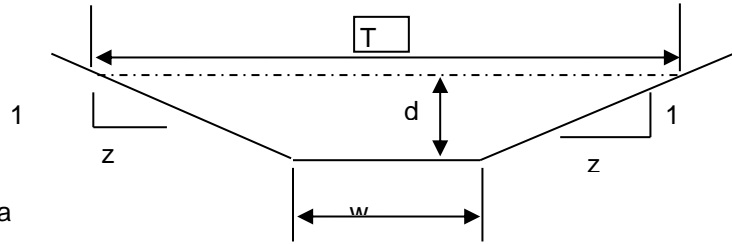
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 14.3
 z (sideslope)= 16
 b (btm width, ft)= 0
 d (depth, ft)= 0.35
 S (slope, ft/ft) 0.01
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.35	1.86	10.63	0.17	3.570899	6.62714	3.570899	6.62714	10.605	0.175

Sc low = 0.0044 Sc high = 0.0044

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.0031	0.0057	0.0031	0.0057

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **Bldg N+RV Drive Aisel (need Q=31 cfs)**
 By: **John F** Date: **4/2/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

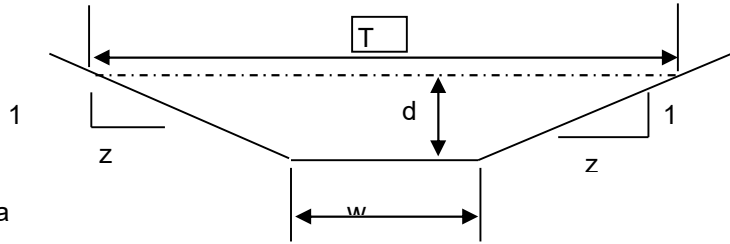
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 7.1
 z (sideslope)= 14.7
 b (btm width, ft)= 0
 d (depth, ft)= 0.7
 S (slope, ft/ft) 0.01
 n_{low} = 0.013
 n_{high} = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.7	5.34	15.33	0.35	5.65883356	30.2238	5.658834	30.2238	15.26	0.350
Sc low =				0.0035	Sc high =		0.0035		
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc		
				0.0025	0.0046	0.0025	0.0046		

s_c = critical slope ft / ft
 T = top width of the stream
 d_m = a/T = mean depth of flow

Created by: Mike O'Shea

Please provide erosion protection for this open channel as velocity is above the standard velocity per DCM vol.1, chapter 10, table 10-4

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **Bldg Central Drive Aisel (need Q=41.3 cfs)**
 By: **John F** Date: **4/2/2024**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

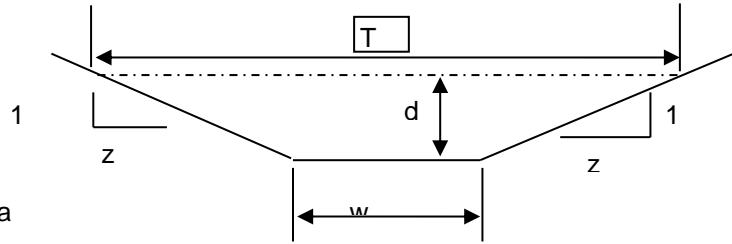
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 33
 z (sideslope)= 33
 b (btm width, ft)= 0
 d (depth, ft)= 0.5
 S (slope, ft/ft) 0.02
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.5	8.25	33.02	0.25	6.41304341	52.9076	6.413043	52.9076	33	0.250
Sc low =				0.0039	Sc high =		0.0039		
.7 Sc				0.0027	1.3 Sc		0.0051		
.7 Sc				0.0027	1.3 Sc		0.0051		

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

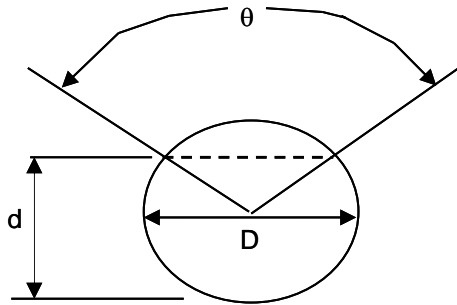
Created by: Mike O'Shea

Please provide erosion protection for this open channel as velocity is above the standard velocity per DCM vol.1, chapter 10, table 10-4

MANNING'S EQUATION FOR PIPE FLOW

Project: Platte Self Storage Location: Driveway Culvert (need Q=2 cfs)
 By: Dane Frank Date: 4/5/2024
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

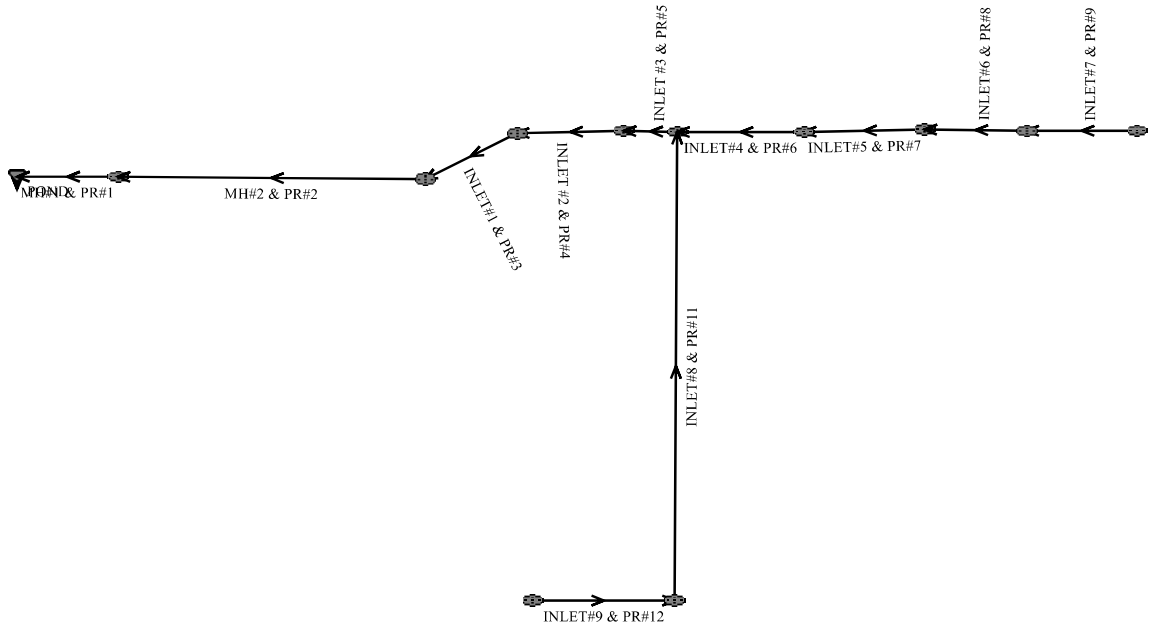
D= 18 inches
 d= 18 inches
 n= 0.013 mannings coeff
 theta= 0.0 degrees
 S= 0.04 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

Solution to Mannings Equation					Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
1.77	4.71	0.38	11.89	21.01	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea



2419.00 6001 E Platte Ave Storage
East System Layout

Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 4/26/2024 2:19:34 PM	<h2>UDSewer Results Summary</h2> <p>Project Title: 6001 E Platte Storage - 5 Year Project Description: East System</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in): 1.50
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 300
Maximum Urban Overland Len. (ft): 100
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 6.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 3.0

Backwater Calculations:

Tailwater Elevation (ft): 6209.00

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
POND	6211.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MH#1 & PR#1	6220.00	41.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MH#2 & PR#2	6223.50	41.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#1 & PR#3	6233.50	41.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET #2 & PR#4	6234.00	18.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET #3 & PR#5	6234.40	18.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#8 & PR#11	6237.45	11.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#9 & PR#12	6236.85	11.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#4 & PR#6	6235.60	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#5 & PR#7	6236.80	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#6 & PR#8	6238.10	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#7 & PR#9	6239.30	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#10 & PR#10	6239.85	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
TRENCH & PR#13	6240.35	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
POND	0.00	0.00	0.00	0.00	0.00	5.97	6.91	0.15	41.30	
MH#1 & PR#1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	41.30	
MH#2 & PR#2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	41.30	
INLET#1 & PR#3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	41.30	
INLET #2 & PR#4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.20	
INLET #3 & PR#5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.20	
INLET#8 & PR#11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	11.80	
INLET#9 & PR#12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	11.80	
INLET#4 & PR#6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	
INLET#5 & PR#7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	
INLET#6 & PR#8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	
INLET#7 & PR#9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	
INLET#10 & PR#10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	
TRENCH & PR#13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.40	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
MH#1 & PR#1	30.00	6205.00	2.7	6205.80	0.013	0.03	0.00	CIRCULAR	48.00 in	48.00 in
MH#2 & PR#2	227.00	6211.00	2.2	6216.00	0.013	0.05	0.00	CIRCULAR	48.00 in	48.00 in
INLET#1 & PR#3	45.00	6216.80	2.2	6217.80	0.013	0.24	0.00	CIRCULAR	42.00 in	42.00 in
INLET #2 & PR#4	24.00	6225.50	1.7	6225.90	0.013	0.24	0.00	CIRCULAR	42.00 in	42.00 in
INLET #3 & PR#5	7.00	6226.00	2.1	6226.15	0.013	0.05	0.00	CIRCULAR	42.00 in	42.00 in
INLET#8 & PR#11	352.00	6227.75	1.0	6231.25	0.013	1.00	0.25	CIRCULAR	36.00 in	36.00 in
INLET#9 & PR#12	31.00	6231.55	1.0	6231.85	0.013	1.00	0.00	CIRCULAR	36.00 in	36.00 in
INLET#4 & PR#6	47.00	6228.15	5.0	6230.50	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#5 & PR#7	57.00	6230.60	1.9	6231.70	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#6 & PR#8	62.00	6231.80	1.9	6233.00	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#7 & PR#9	57.00	6233.60	1.9	6234.70	0.013	0.05	0.00	CIRCULAR	24.00 in	24.00 in
INLET#10 & PR#10	24.00	6235.00	1.7	6235.40	0.013	0.11	0.00	CIRCULAR	24.00 in	24.00 in
TRENCH & PR#13	32.00	6235.70	1.9	6236.30	0.013	0.11	0.00	CIRCULAR	24.00 in	24.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow						
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
MH#1 & PR#1	235.17	18.71	23.03	6.93	13.62	14.08	2.75	Supercritical	41.30	0.00	
MH#2 & PR#2	213.76	17.01	23.03	6.93	14.30	13.15	2.50	Supercritical	41.30	0.00	
INLET#1 & PR#3	150.38	15.63	24.00	7.27	15.04	13.34	2.45	Supercritical	41.30	0.00	
INLET #2 & PR#4	130.22	13.53	15.64	5.57	10.61	9.54	2.12	Supercritical	18.20	0.00	
INLET #3 & PR#5	146.19	15.19	15.64	5.57	10.01	10.36	2.38	Supercritical	18.20	0.00	
INLET#8 & PR#11	66.69	9.43	13.08	5.09	10.25	7.11	1.60	Supercritical	11.80	0.00	
INLET#9 & PR#12	65.82	9.31	13.08	5.09	10.32	7.05	1.58	Supercritical	11.80	0.00	
INLET#4 & PR#6	91.96	18.73	10.05	4.44	5.36	10.77	3.41	Supercritical	6.40	0.00	
INLET#5 & PR#7	57.14	11.64	10.05	4.44	6.78	7.69	2.15	Supercritical	6.40	0.00	
INLET#6 & PR#8	57.22	11.66	10.05	4.44	6.77	7.70	2.15	Supercritical	6.40	0.00	
INLET#7 & PR#9	31.51	10.03	10.75	4.70	7.34	7.87	2.09	Supercritical	6.40	0.00	

INLET#10 & PR#10	29.28	9.32	10.75	4.70	7.62	7.46	1.94	Supercritical	6.40	0.00	
TRENCH & PR#13	31.05	9.88	10.75	4.70	7.39	7.78	2.06	Supercritical	6.40	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	
MH#1 & PR#1	41.30	CIRCULAR	48.00 in	48.00 in	27.00 in	27.00 in	48.00 in	48.00 in	12.57	
MH#2 & PR#2	41.30	CIRCULAR	48.00 in	48.00 in	27.00 in	27.00 in	48.00 in	48.00 in	12.57	
INLET#1 & PR#3	41.30	CIRCULAR	42.00 in	42.00 in	27.00 in	27.00 in	42.00 in	42.00 in	9.62	
INLET #2 & PR#4	18.20	CIRCULAR	42.00 in	42.00 in	21.00 in	21.00 in	42.00 in	42.00 in	9.62	
INLET #3 & PR#5	18.20	CIRCULAR	42.00 in	42.00 in	21.00 in	21.00 in	42.00 in	42.00 in	9.62	
INLET#8 & PR#11	11.80	CIRCULAR	36.00 in	36.00 in	21.00 in	21.00 in	36.00 in	36.00 in	7.07	
INLET#9 & PR#12	11.80	CIRCULAR	36.00 in	36.00 in	21.00 in	21.00 in	36.00 in	36.00 in	7.07	
INLET#4 & PR#6	6.40	CIRCULAR	30.00 in	30.00 in	12.00 in	12.00 in	30.00 in	30.00 in	4.91	
INLET#5 & PR#7	6.40	CIRCULAR	30.00 in	30.00 in	15.00 in	15.00 in	30.00 in	30.00 in	4.91	
INLET#6 & PR#8	6.40	CIRCULAR	30.00 in	30.00 in	15.00 in	15.00 in	30.00 in	30.00 in	4.91	
INLET#7 & PR#9	6.40	CIRCULAR	24.00 in	24.00 in	15.00 in	15.00 in	24.00 in	24.00 in	3.14	
INLET#10 & PR#10	6.40	CIRCULAR	24.00 in	24.00 in	15.00 in	15.00 in	24.00 in	24.00 in	3.14	
TRENCH & PR#13	6.40	CIRCULAR	24.00 in	24.00 in	15.00 in	15.00 in	24.00 in	24.00 in	3.14	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6209.00

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
MH#1 & PR#1	6205.00	6205.80	0.00	0.00	6209.00	6209.00	6209.21	0.01	6209.23
MH#2 & PR#2	6211.00	6216.00	0.01	0.00	6212.19	6217.92	6214.88	3.79	6218.66

INLET#1 & PR#3	6216.80	6217.80	0.07	0.00	6218.05	6220.34	6220.82	0.00	6220.82
INLET #2 & PR#4	6225.50	6225.90	0.01	0.00	6226.50	6227.20	6227.50	0.19	6227.69
INLET #3 & PR#5	6226.00	6226.15	0.00	0.00	6227.21	6228.38	6228.50	0.00	6228.50
INLET#8 & PR#11	6227.75	6231.25	0.04	0.04	6228.60	6232.34	6229.39	3.35	6232.74
INLET#9 & PR#12	6231.55	6231.85	0.04	0.00	6232.41	6232.94	6233.18	0.16	6233.34
INLET#4 & PR#6	6228.15	6230.50	0.00	0.00	6228.60	6231.34	6230.40	1.25	6231.64
INLET#5 & PR#7	6230.60	6231.70	0.00	0.00	6231.34	6232.54	6232.08	0.76	6232.84
INLET#6 & PR#8	6231.80	6233.00	0.00	0.00	6232.54	6233.84	6233.29	0.86	6234.14
INLET#7 & PR#9	6233.60	6234.70	0.00	0.00	6234.21	6235.60	6235.17	0.77	6235.94
INLET#10 & PR#10	6235.00	6235.40	0.01	0.00	6235.64	6236.30	6236.50	0.14	6236.64
TRENCH & PR#13	6235.70	6236.30	0.01	0.00	6236.32	6237.20	6237.26	0.28	6237.54

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 1.00 ft

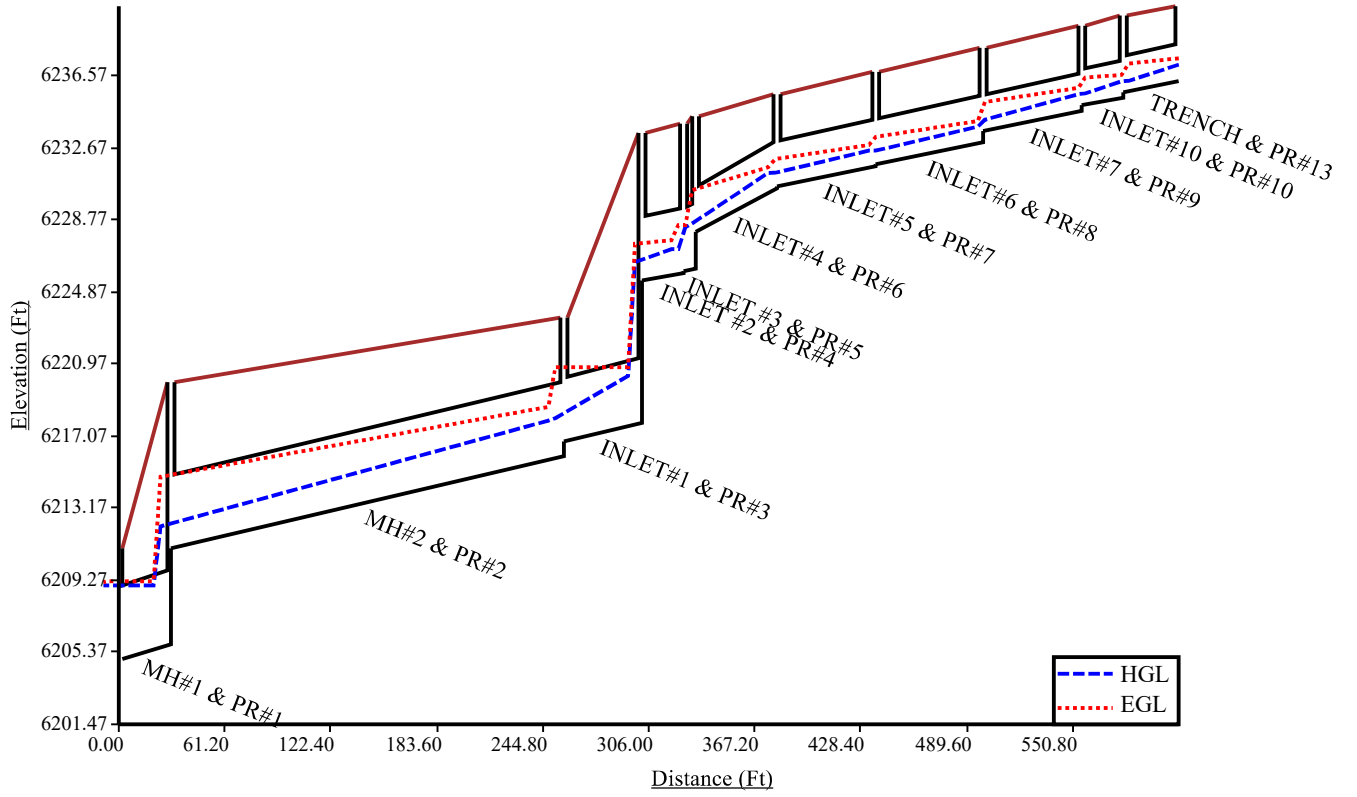
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
MH#1 & PR#1	30.00	5.00	6.00	7.83	9.00	6.92	1.58	25.40	15.12	9.78	138.93	
MH#2 & PR#2	227.00	5.00	6.00	7.83	15.00	9.92	4.58	12.00	8.42	3.08	675.92	
INLET#1 & PR#3	45.00	4.50	6.00	7.25	10.90	7.58	2.83	28.90	16.58	11.83	246.33	
INLET #2 & PR#4	24.00	4.50	6.00	7.25	13.50	8.87	4.12	13.70	8.98	4.23	66.48	
INLET #3 & PR#5	7.00	4.50	6.00	7.25	13.49	8.87	4.12	14.00	9.13	4.38	19.65	
INLET#8 & PR#11	352.00	4.00	6.00	6.67	11.30	7.48	3.32	10.40	7.03	2.87	688.55	
INLET#9 & PR#12	31.00	4.00	6.00	6.67	9.80	6.73	2.57	8.00	5.83	1.67	49.76	
INLET#4 & PR#6	47.00	3.50	6.00	6.08	11.00	7.04	3.46	8.70	5.89	2.31	75.23	
INLET#5 & PR#7	57.00	3.50	6.00	6.08	8.50	5.79	2.21	8.70	5.89	2.31	78.37	
INLET#6 & PR#8	62.00	3.50	6.00	6.08	8.50	5.79	2.21	8.70	5.89	2.31	85.25	

INLET#7 & PR#9	57.00	3.00	4.00	5.50	8.00	5.08	2.25	8.20	5.18	2.35	63.18	
INLET#10 & PR#10	24.00	3.00	4.00	5.50	7.60	4.88	2.05	7.90	5.03	2.20	25.37	
TRENCH & PR#13	32.00	3.00	4.00	5.50	7.30	4.73	1.90	7.10	4.63	1.80	31.39	

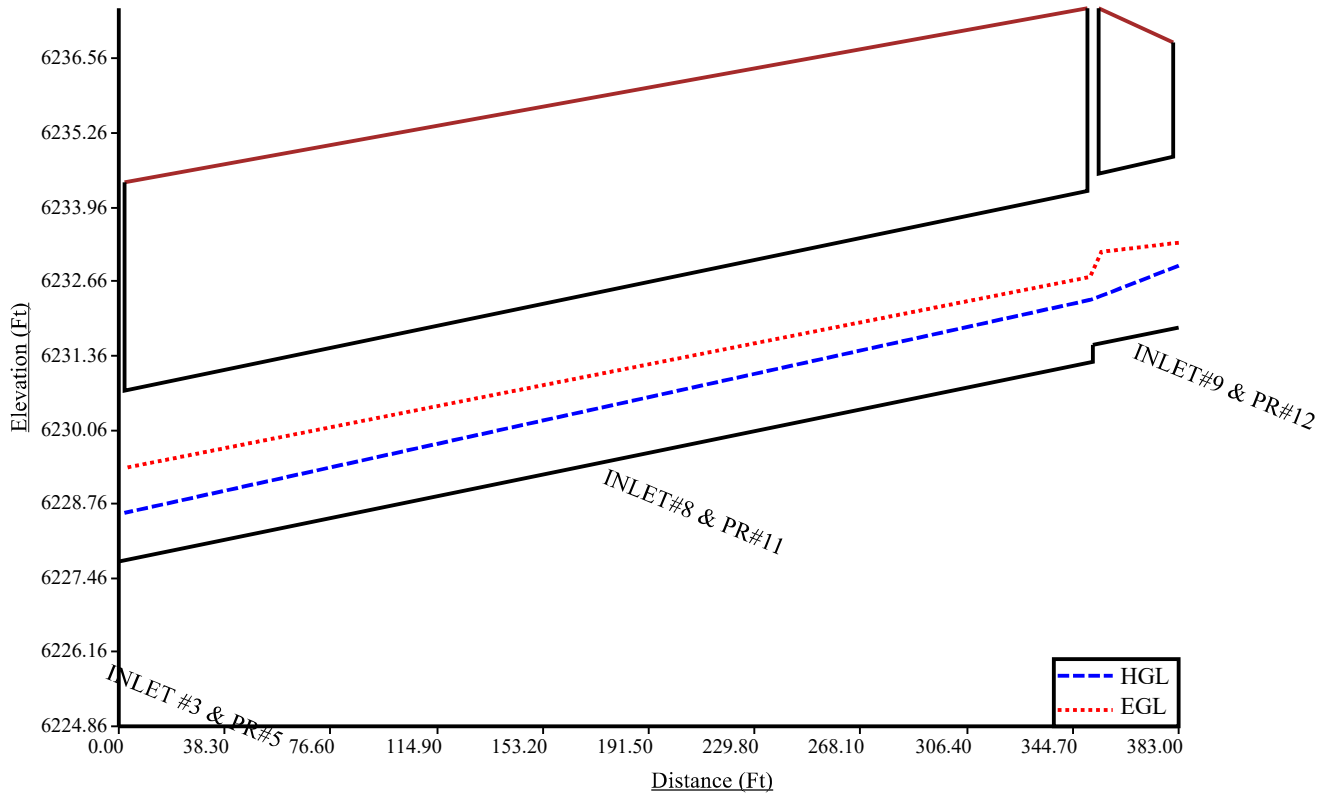
Total earth volume for sewer trenches = 2244 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

Main Run



South Run



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 4/26/2024 10:31:41 AM	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p style="margin: 0;">Project Title: 6001 E Platte Storage - 100 Year Project Description: East System</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in): 2.52
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 300
Maximum Urban Overland Len. (ft): 100
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 6.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 3.0

Backwater Calculations:

Tailwater Elevation (ft): 6212.00

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
POND	6211.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
MH#1 & PR#1	6220.00	91.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MH#2 & PR#2	6223.50	91.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#1 & PR#3	6233.50	91.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET #2 & PR#4	6234.00	50.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET #3 & PR#5	6234.40	50.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#8 & PR#11	6237.45	32.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#9 & PR#12	6236.85	32.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#4 & PR#6	6235.60	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#5 & PR#7	6236.80	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#6 & PR#8	6238.10	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#7 & PR#9	6239.30	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INLET#10 & PR#10	6239.85	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
TRENCH & PR#13	6240.35	18.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
POND	0.00	0.00	0.00	0.00	0.00	7.84	11.69	0.07	91.70	Surface Water Present (Upstream)
MH#1 & PR#1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	91.70	Surface Water Present (Downstream)
MH#2 & PR#2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	91.70	
INLET#1 & PR#3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	91.70	
INLET #2 & PR#4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	50.30	
INLET #3 & PR#5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	50.30	
INLET#8 & PR#11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	32.20	
INLET#9 & PR#12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	32.20	
INLET#4 & PR#6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	

INLET#5 & PR#7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	
INLET#6 & PR#8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	
INLET#7 & PR#9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	
INLET#10 & PR#10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	
TRENCH & PR#13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	18.10	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
MH#1 & PR#1	30.00	6205.00	2.7	6205.80	0.013	0.03	0.00	CIRCULAR	48.00 in	48.00 in
MH#2 & PR#2	227.00	6211.00	2.2	6216.00	0.013	0.05	0.00	CIRCULAR	48.00 in	48.00 in
INLET#1 & PR#3	45.00	6216.80	2.2	6217.80	0.013	0.24	0.00	CIRCULAR	42.00 in	42.00 in
INLET #2 & PR#4	24.00	6225.50	1.7	6225.90	0.013	0.24	0.00	CIRCULAR	42.00 in	42.00 in
INLET #3 & PR#5	7.00	6226.00	2.1	6226.15	0.013	0.05	0.00	CIRCULAR	42.00 in	42.00 in
INLET#8 & PR#11	352.00	6227.75	1.0	6231.25	0.013	1.00	0.25	CIRCULAR	36.00 in	36.00 in
INLET#9 & PR#12	31.00	6231.55	1.0	6231.85	0.013	1.00	0.00	CIRCULAR	36.00 in	36.00 in
INLET#4 & PR#6	47.00	6228.15	5.0	6230.50	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#5 & PR#7	57.00	6230.60	1.9	6231.70	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#6 & PR#8	62.00	6231.80	1.9	6233.00	0.013	0.05	0.00	CIRCULAR	30.00 in	30.00 in
INLET#7 & PR#9	57.00	6233.60	1.9	6234.70	0.013	0.05	0.00	CIRCULAR	24.00 in	24.00 in
INLET#10 & PR#10	24.00	6235.00	1.7	6235.40	0.013	0.11	0.00	CIRCULAR	24.00 in	24.00 in
TRENCH & PR#13	32.00	6235.70	1.9	6236.30	0.013	0.11	0.00	CIRCULAR	24.00 in	24.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
MH#1 & PR#1	235.17	18.71	34.84	9.39	20.81	17.55	2.69	Pressurized	91.70	30.00	
MH#2 & PR#2	213.76	17.01	34.84	9.39	21.96	16.36	2.43	Supercritical	91.70	0.00	
INLET#1 & PR#3	150.38	15.63	35.59	10.55	23.69	16.40	2.28	Supercritical	91.70	0.00	
INLET #2 & PR#4	130.22	13.53	26.60	7.83	18.12	12.66	2.09	Supercritical	50.30	0.00	
INLET #3 & PR#5	146.19	15.19	26.60	7.83	16.99	13.79	2.36	Supercritical	50.30	0.00	

INLET#8 & PR#11	66.69	9.43	22.09	7.08	17.64	9.35	1.54	Supercritical	32.20	0.00	
INLET#9 & PR#12	65.82	9.31	22.09	7.08	17.77	9.26	1.52	Supercritical	32.20	0.00	
INLET#4 & PR#6	91.96	18.73	17.29	6.18	9.02	14.56	3.49	Supercritical	18.10	0.00	
INLET#5 & PR#7	57.14	11.64	17.29	6.18	11.60	10.33	2.15	Supercritical	18.10	0.00	
INLET#6 & PR#8	57.22	11.66	17.29	6.18	11.59	10.34	2.15	Supercritical	18.10	0.00	
INLET#7 & PR#9	31.51	10.03	18.39	7.01	13.04	10.38	1.95	Supercritical	18.10	0.00	
INLET#10 & PR#10	29.28	9.32	18.39	7.01	13.65	9.81	1.79	Supercritical	18.10	0.00	
TRENCH & PR#13	31.05	9.88	18.39	7.01	13.16	10.26	1.92	Supercritical	18.10	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	
MH#1 & PR#1	91.70	CIRCULAR	48.00 in	48.00 in	36.00 in	36.00 in	48.00 in	48.00 in	12.57	
MH#2 & PR#2	91.70	CIRCULAR	48.00 in	48.00 in	36.00 in	36.00 in	48.00 in	48.00 in	12.57	
INLET#1 & PR#3	91.70	CIRCULAR	42.00 in	42.00 in	36.00 in	36.00 in	42.00 in	42.00 in	9.62	
INLET #2 & PR#4	50.30	CIRCULAR	42.00 in	42.00 in	30.00 in	30.00 in	42.00 in	42.00 in	9.62	
INLET #3 & PR#5	50.30	CIRCULAR	42.00 in	42.00 in	30.00 in	30.00 in	42.00 in	42.00 in	9.62	
INLET#8 & PR#11	32.20	CIRCULAR	36.00 in	36.00 in	30.00 in	30.00 in	36.00 in	36.00 in	7.07	
INLET#9 & PR#12	32.20	CIRCULAR	36.00 in	36.00 in	30.00 in	30.00 in	36.00 in	36.00 in	7.07	
INLET#4 & PR#6	18.10	CIRCULAR	30.00 in	30.00 in	18.00 in	18.00 in	30.00 in	30.00 in	4.91	
INLET#5 & PR#7	18.10	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
INLET#6 & PR#8	18.10	CIRCULAR	30.00 in	30.00 in	21.00 in	21.00 in	30.00 in	30.00 in	4.91	
INLET#7 & PR#9	18.10	CIRCULAR	24.00 in	24.00 in	21.00 in	21.00 in	24.00 in	24.00 in	3.14	
INLET#10 & PR#10	18.10	CIRCULAR	24.00 in	24.00 in	21.00 in	21.00 in	24.00 in	24.00 in	3.14	
TRENCH & PR#13	18.10	CIRCULAR	24.00 in	24.00 in	21.00 in	21.00 in	24.00 in	24.00 in	3.14	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6212.00

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
MH#1 & PR#1	6205.00	6205.80	0.00	0.00	6212.00	6212.12	6212.83	0.12	6212.95
MH#2 & PR#2	6211.00	6216.00	0.04	0.00	6212.83	6218.90	6216.99	3.29	6220.27
INLET#1 & PR#3	6216.80	6217.80	0.34	0.00	6219.24	6221.54	6222.95	0.00	6222.95
INLET #2 & PR#4	6225.50	6225.90	0.10	0.00	6227.01	6229.02	6229.50	0.00	6229.50
INLET #3 & PR#5	6226.00	6226.15	0.02	0.00	6229.04	6229.95	6230.37	0.00	6230.37
INLET#8 & PR#11	6227.75	6231.25	0.32	0.34	6230.71	6233.09	6231.04	2.83	6233.87
INLET#9 & PR#12	6231.55	6231.85	0.32	0.00	6233.41	6233.69	6234.36	0.11	6234.47
INLET#4 & PR#6	6228.15	6230.50	0.01	0.00	6229.96	6231.94	6232.19	0.34	6232.53
INLET#5 & PR#7	6230.60	6231.70	0.01	0.00	6231.95	6233.14	6233.22	0.51	6233.73
INLET#6 & PR#8	6231.80	6233.00	0.01	0.00	6233.15	6234.44	6234.43	0.61	6235.03
INLET#7 & PR#9	6233.60	6234.70	0.03	0.00	6234.69	6236.23	6236.36	0.64	6236.99
INLET#10 & PR#10	6235.00	6235.40	0.06	0.00	6236.29	6236.93	6237.63	0.06	6237.69
TRENCH & PR#13	6235.70	6236.30	0.06	0.00	6236.99	6237.83	6238.43	0.16	6238.59

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft
 The minimum trench width is 1.00 ft

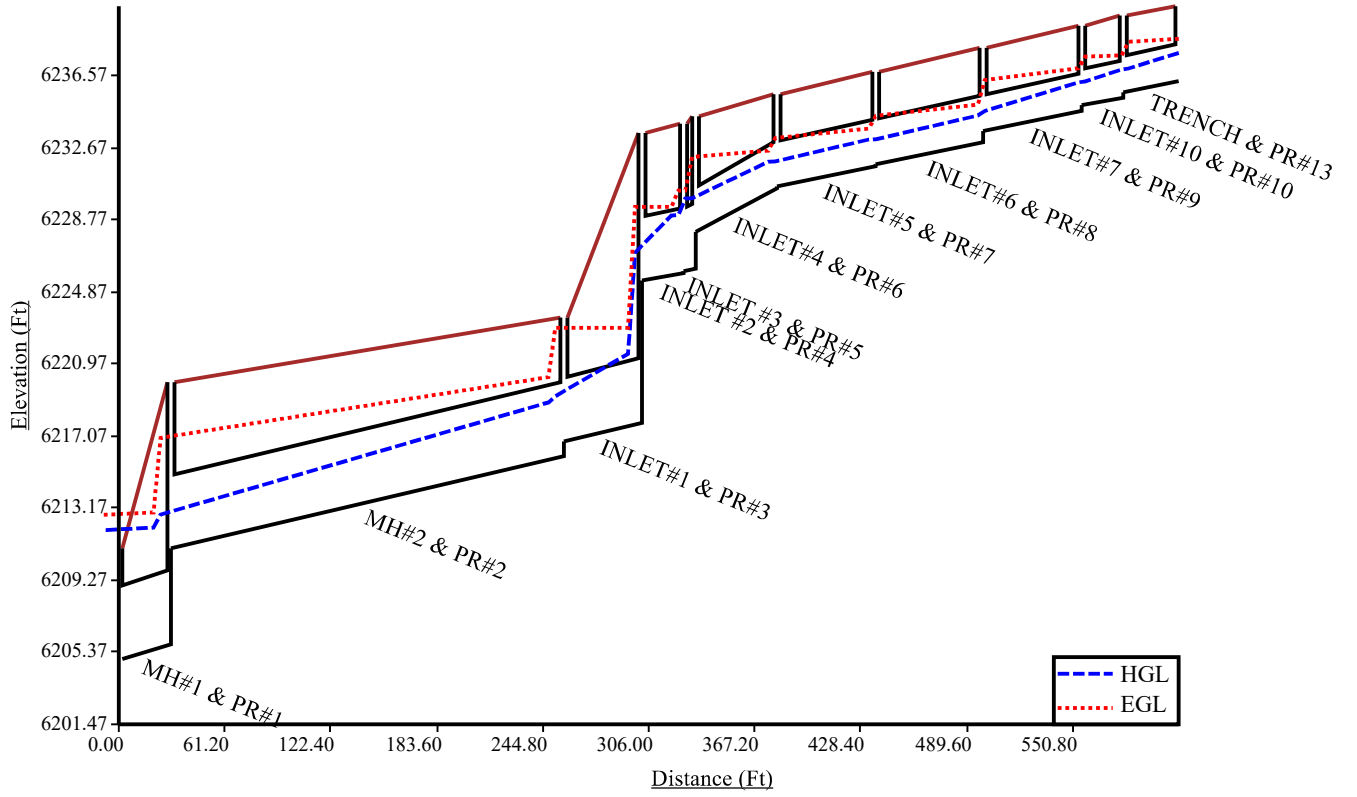
Element Name	Downstream				Upstream			Volume (cu. yd)	Comment			
	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)					
MH#1 & PR#1	30.00	5.00	6.00	7.83	9.00	6.92	1.58	25.40	15.12	9.78	138.93	
MH#2 & PR#2	227.00	5.00	6.00	7.83	15.00	9.92	4.58	12.00	8.42	3.08	675.92	

INLET#1 & PR#3	45.00	4.50	6.00	7.25	10.90	7.58	2.83	28.90	16.58	11.83	246.33	
INLET #2 & PR#4	24.00	4.50	6.00	7.25	13.50	8.87	4.12	13.70	8.98	4.23	66.48	
INLET #3 & PR#5	7.00	4.50	6.00	7.25	13.49	8.87	4.12	14.00	9.13	4.38	19.65	
INLET#8 & PR#11	352.00	4.00	6.00	6.67	11.30	7.48	3.32	10.40	7.03	2.87	688.55	
INLET#9 & PR#12	31.00	4.00	6.00	6.67	9.80	6.73	2.57	8.00	5.83	1.67	49.76	
INLET#4 & PR#6	47.00	3.50	6.00	6.08	11.00	7.04	3.46	8.70	5.89	2.31	75.23	
INLET#5 & PR#7	57.00	3.50	6.00	6.08	8.50	5.79	2.21	8.70	5.89	2.31	78.37	
INLET#6 & PR#8	62.00	3.50	6.00	6.08	8.50	5.79	2.21	8.70	5.89	2.31	85.25	
INLET#7 & PR#9	57.00	3.00	4.00	5.50	8.00	5.08	2.25	8.20	5.18	2.35	63.18	
INLET#10 & PR#10	24.00	3.00	4.00	5.50	7.60	4.88	2.05	7.90	5.03	2.20	25.37	
TRENCH & PR#13	32.00	3.00	4.00	5.50	7.30	4.73	1.90	7.10	4.63	1.80	31.39	

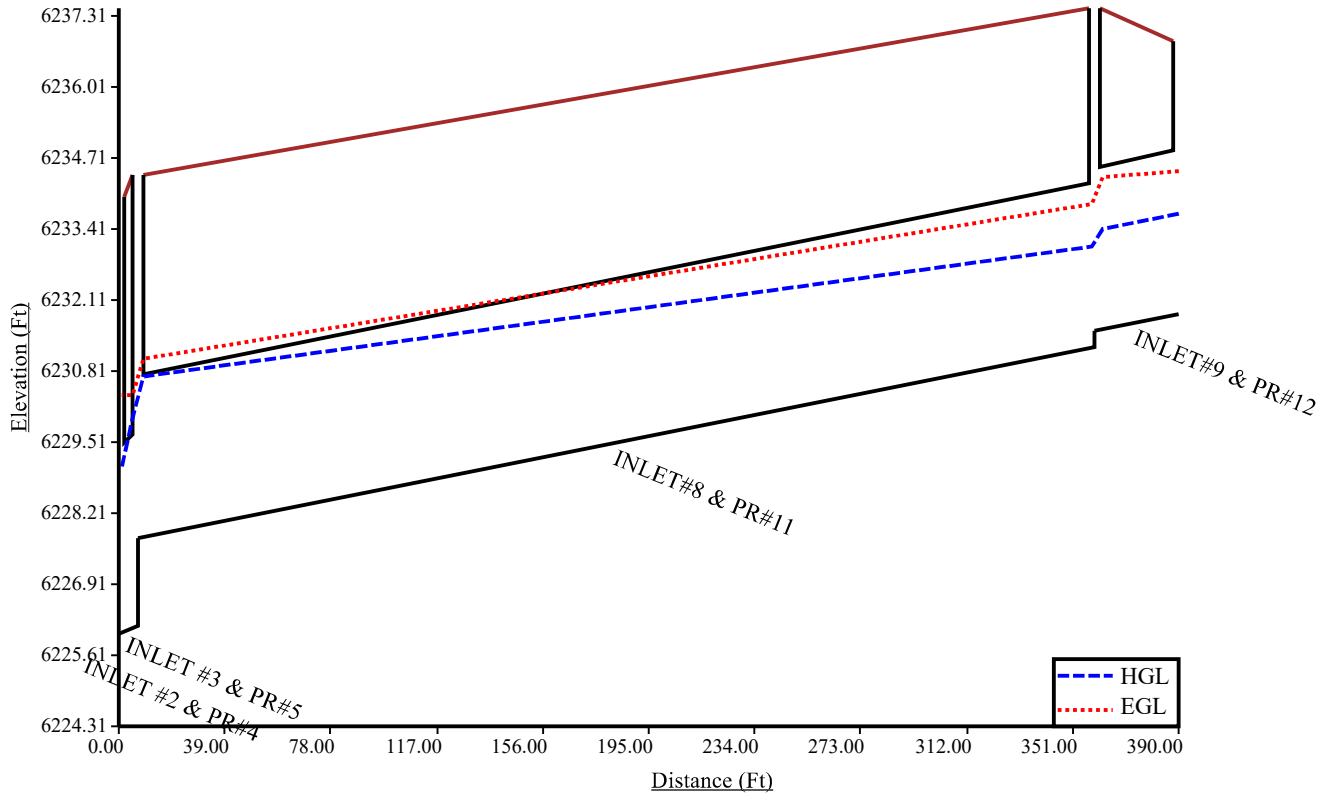
Total earth volume for sewer trenches = 2244 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

Main Run



South Run





STIPONING OUTLET & PR#90

Stilling Basin

Pond Outlet & PR#90

2419.00 6001 E Platte Ave Storage
Pond Outlet Layout

Please fix this error.

Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 4/26/2024 2:34:34 PM	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p>Project Title: 6001 E Platte Storage - 5 Year Project Description: Pond Outlet System</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in): 1.50
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 300
Maximum Urban Overland Len. (ft): 100
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 6.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 3.0

Backwater Calculations:

Tailwater Elevation (ft): 6201.00

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
STILLING BASIN	6201.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

POND OUTLET & PR#90	6209.00	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
STILLING BASIN	0.00	0.00	0.00	0.00	0.00	0.08	6.02	2.12	0.50	
POND OUTLET & PR#90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.50	Surface Water Present (Downstream)

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
POND OUTLET & PR#90	36.00	6201.00	1.4	6201.50	0.012	0.03	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
POND OUTLET & PR#90	13.50	7.64	3.14	2.42	2.37	3.64	1.74	Supercritical	0.50	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft^2)	
POND OUTLET & PR#90	0.50	CIRCULAR	18.00 in	18.00 in	6.00 in	6.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available

size.

- Sewer sizes should not decrease downstream.
- All hydraulics where calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6201.00

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
POND OUTLET & PR#90	6201.00	6201.50	0.00	0.00	6201.19	6201.76	6201.40	0.45	6201.85

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

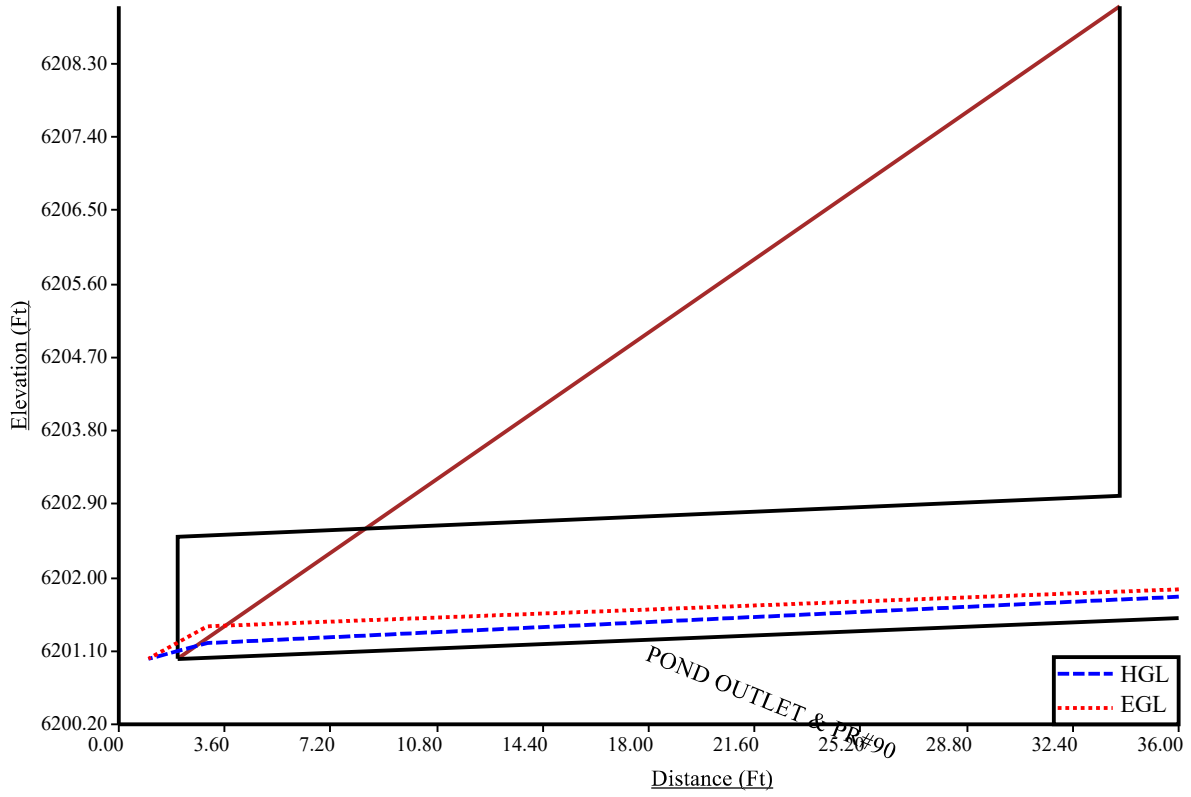
The minimum trench width is 1.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
POND OUTLET & PR#90	36.00	2.50	4.00	4.92	0.00	0.55	0.00	14.50	8.04	5.79	43.45	Sewer Too Shallow

Total earth volume for sewer trenches = 43 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

Pond Outlet



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 4/26/2024 2:28:37 PM	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p>Project Title: 6001 E Platte Storage - 100 Year Project Description: Pond Outlet System</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in): 2.52
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 300
Maximum Urban Overland Len. (ft): 100
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 6.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 3.0

Backwater Calculations:

Tailwater Elevation (ft): 6201.00

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
STILLING BASIN	6201.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

POND OUTLET & PR#90	6209.00	11.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
STILLING BASIN	0.00	0.00	0.00	0.00	0.00	0.97	11.67	0.09	11.30	
POND OUTLET & PR#90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	11.30	Surface Water Present (Downstream)

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
POND OUTLET & PR#90	36.00	6201.00	1.4	6201.50	0.012	0.03	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
POND OUTLET & PR#90	13.45	7.61	15.41	7.02	12.64	8.53	1.53	Supercritical	11.30	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment	
			Rise	Span	Rise	Span	Rise	Span	Area (ft^2)		
POND OUTLET & PR#90	11.30	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available

size.

- Sewer sizes should not decrease downstream.
- All hydraulics where calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6201.00

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
POND OUTLET & PR#90	6201.00	6201.50	0.00	0.00	6202.05	6202.78	6203.18	0.37	6203.55

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

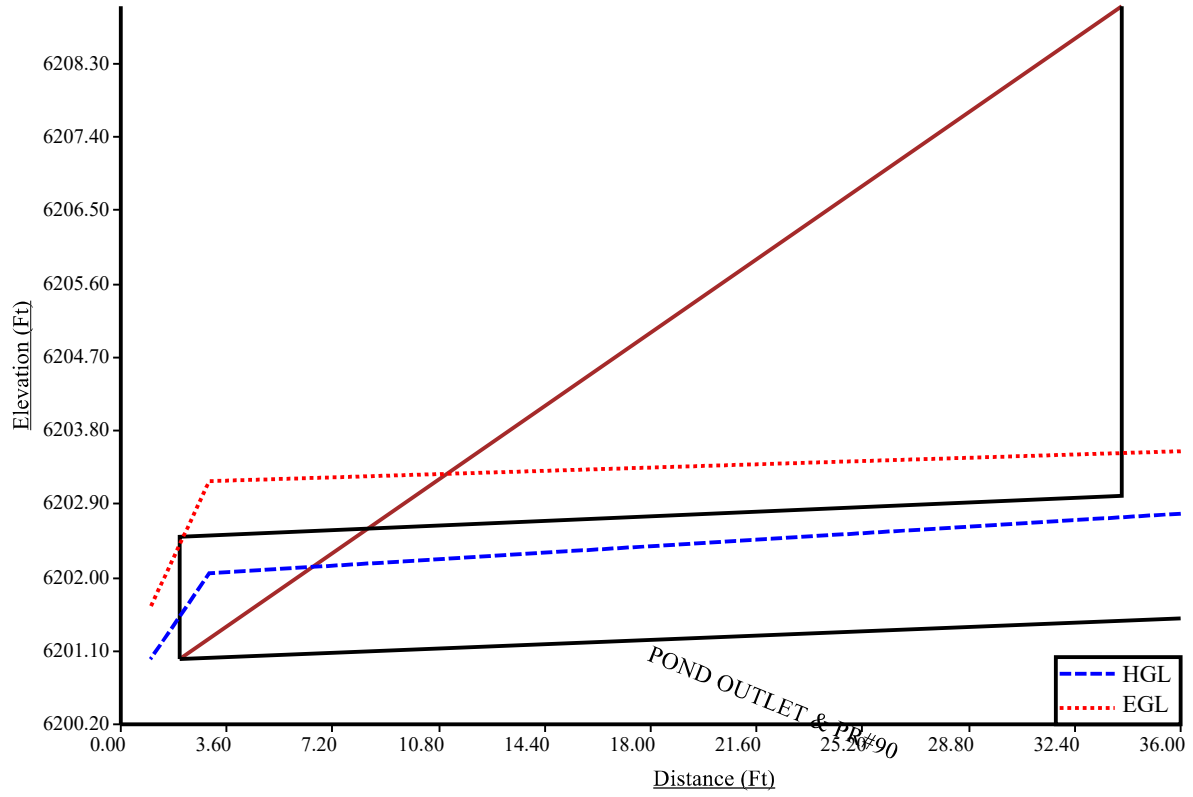
The minimum trench width is 1.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
POND OUTLET & PR#90	36.00	2.50	4.00	4.92	0.00	0.54	0.00	14.50	8.04	5.79	43.44	Sewer Too Shallow

Total earth volume for sewer trenches = 43 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

Pond Outlet



DETENTION CALCULATIONS

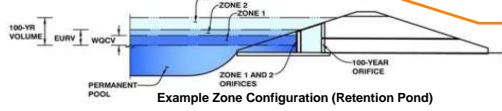
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD- Detention, Version 4.04 (February 2021)

Project: **Platte Self Storage**

Basin ID: **Stormwater Pond**

Provide pond identifier, see GEC Plan comments



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB
Watershed Area =	32.96 acres
Watershed Length =	1,610 ft
Watershed Length to Centroid =	730 ft
Watershed Slope =	0.035 ft/ft
Watershed Imperviousness =	44.00% percent
Percentage Hydrologic Soil Group A =	100.0% percent
Percentage Hydrologic Soil Group B =	0.0% percent
Percentage Hydrologic Soil Groups C/D =	0.0% percent
Target WQCV Drain Time =	40.0 hours
Location for 1-hr Rainfall Depths =	User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.523	acre-feet
Excess Urban Runoff Volume (EURV) =	1.613	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.211	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.620	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.947	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.517	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.072	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.789	acre-feet
500-yr Runoff Volume (P1 = 3 in.) =	4.970	acre-feet
Approximate 2-yr Detention Volume =	1.032	acre-feet
Approximate 5-yr Detention Volume =	1.363	acre-feet
Approximate 10-yr Detention Volume =	1.673	acre-feet
Approximate 25-yr Detention Volume =	2.063	acre-feet
Approximate 50-yr Detention Volume =	2.320	acre-feet
Approximate 100-yr Detention Volume =	2.657	acre-feet

Optional User Overrides

		acre-feet
		acre-feet
	1.19	inches
	1.50	inches
	1.75	inches
	2.00	inches
	2.25	inches
	2.52	inches
	3.00	inches

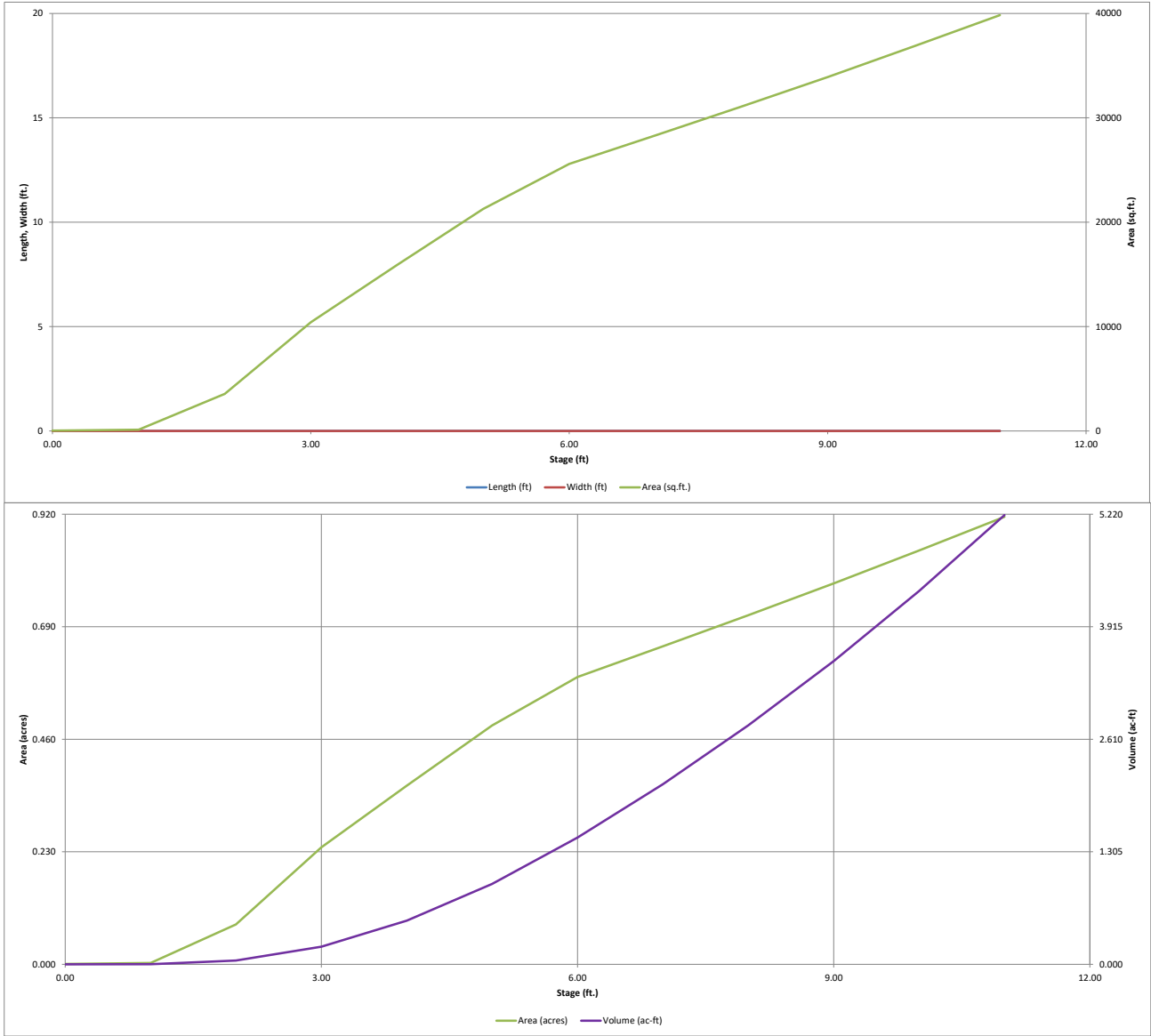
Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.523	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.091	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.044	acre-feet
Total Detention Basin Volume =	2.657	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (L _{FLOOR}) =	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V _{total}) =	user	acre-feet

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	35	0.001	--	--
6203	--	1.00	--	--	--	119	0.003	77	0.002
6204	--	2.00	--	--	--	3,553	0.082	1,913	0.044
6205	--	3.00	--	--	--	10,414	0.239	8,896	0.204
6206	--	4.00	--	--	--	15,905	0.365	22,056	0.506
6207	--	5.00	--	--	--	21,269	0.488	40,643	0.933
6208	--	6.00	--	--	--	25,579	0.587	64,067	1.471
6209	--	7.00	--	--	--	28,311	0.650	91,012	2.089
6210	--	8.00	--	--	--	31,084	0.714	120,709	2.771
6211	--	9.00	--	--	--	33,911	0.778	153,207	3.517
6212	--	10.00	--	--	--	36,847	0.846	188,586	4.329
6213	--	11.00	--	--	--	39,841	0.915	226,930	5.210

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

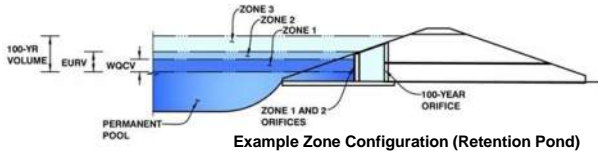


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: **Platte Self Storage**

Basin ID: **Stormwater Pond**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.05	0.523	Orifice Plate
Zone 2 (EURV)	6.24	1.091	Orifice Plate
Zone 3 (100-year)	7.84	1.044	Weir&Pipe (Restrict)
Total (all zones)		2.657	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = inches

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.70	3.40	4.10				
Orifice Area (sq. inches)	1.64	1.64	1.50	3.00				
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice

	Not Selected	Not Selected
Vertical Orifice Area =	N/A	N/A
Vertical Orifice Centroid =	N/A	N/A

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, H _o =	8.00	N/A
Overflow Weir Front Edge Length =	4.00	N/A
Overflow Weir Grate Slope =	0.00	N/A
Horiz. Length of Weir Sides =	4.00	N/A
Overflow Grate Type =	Close Mesh Grate	N/A
Debris Clogging % =	50%	N/A

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected
Height of Grate Upper Edge, H _g =	8.00	N/A
Overflow Weir Slope Length =	4.00	N/A
Grate Open Area / 100-yr Orifice Area =	10.11	N/A
Overflow Grate Open Area w/o Debris =	12.66	N/A
Overflow Grate Open Area w/ Debris =	6.33	N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.50	N/A
Outlet Pipe Diameter =	18.00	N/A
Restrictor Plate Height Above Pipe Invert =	12.00	N/A

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected
Outlet Orifice Area =	1.25	N/A
Outlet Orifice Centroid =	0.56	N/A
Half-Central Angle of Restrictor Plate on Pipe =	1.91	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = feet
 Spillway End Slopes = H:V
 Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.93	feet
Stage at Top of Freeboard =	10.93	feet
Basin Area at Top of Freeboard =	0.91	acres
Basin Volume at Top of Freeboard =	5.15	acre-ft

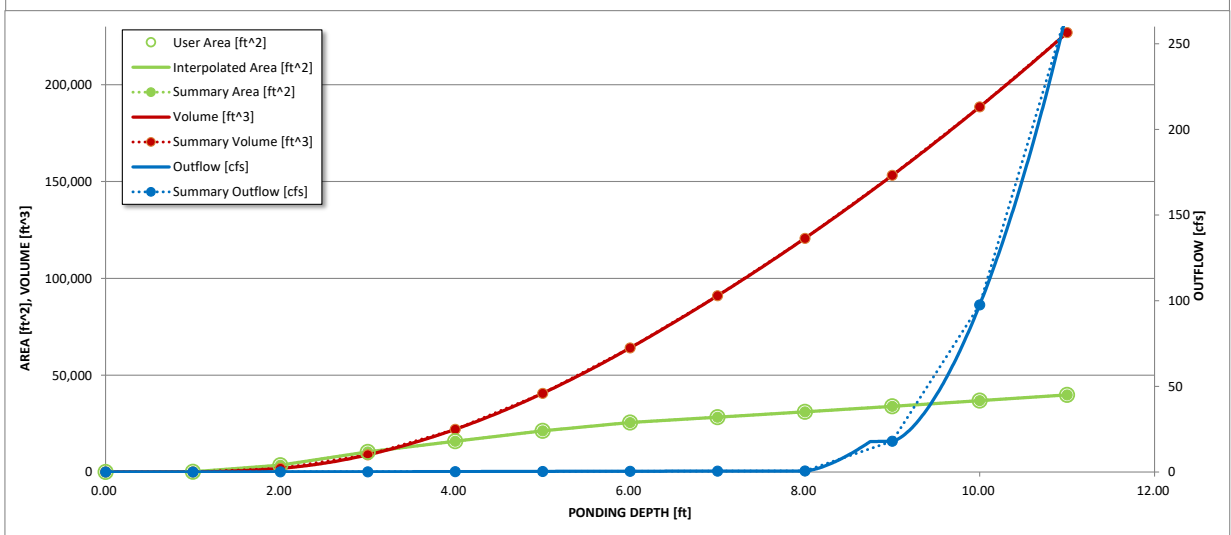
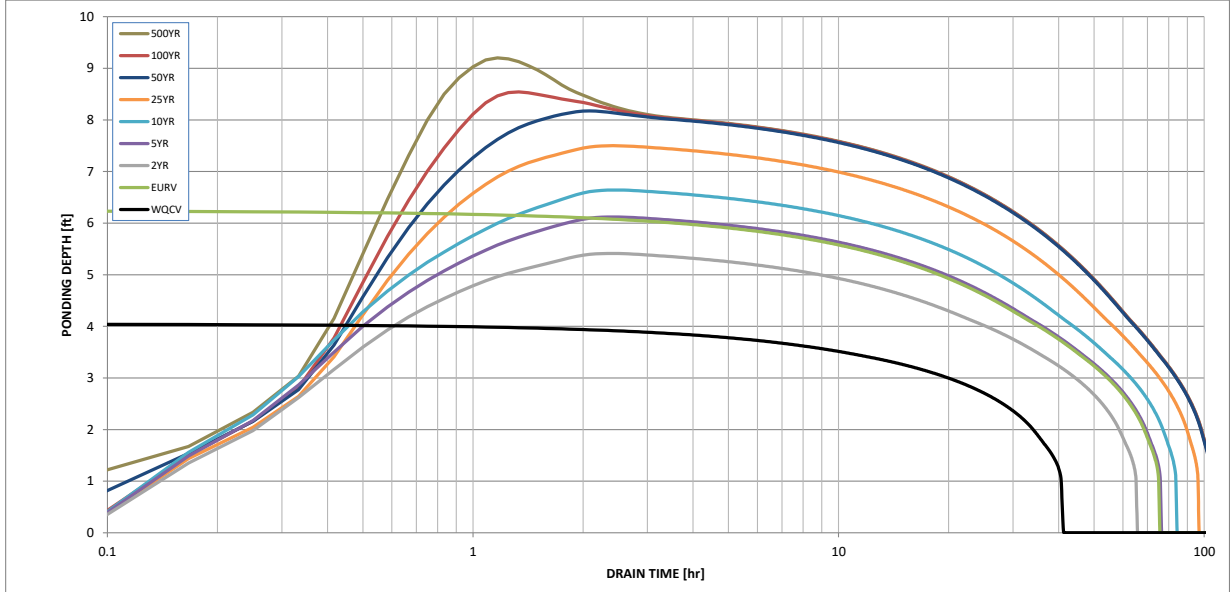
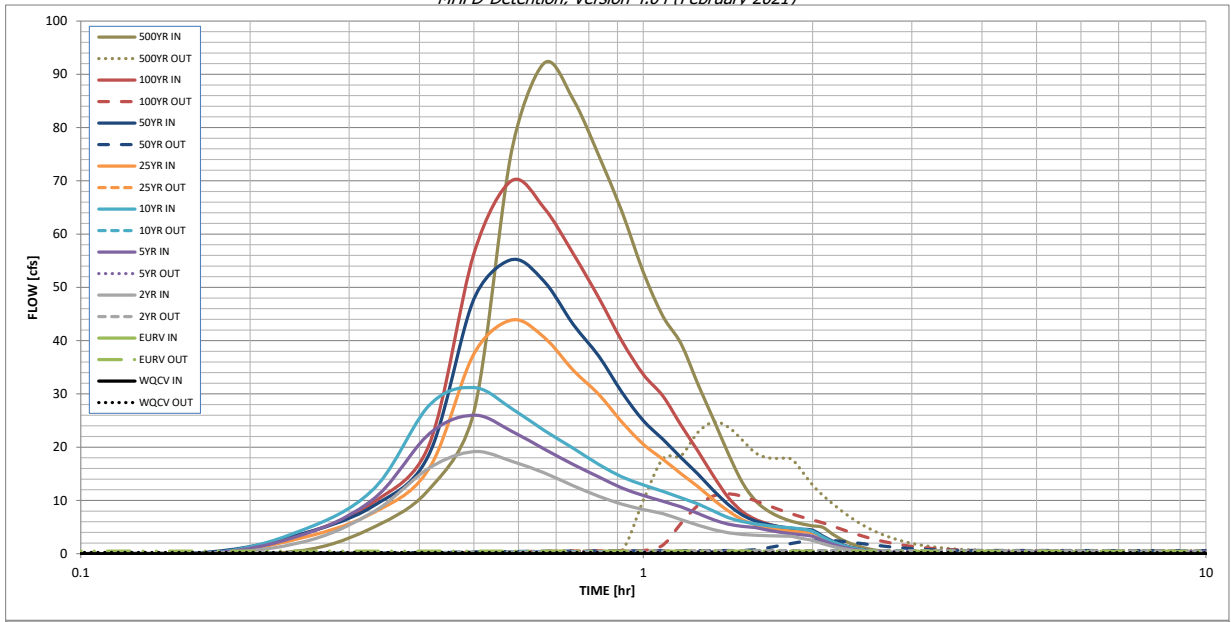
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
One-Hour Rainfall Depth (in) =	0.523	1.613	1.211	1.620	1.947	2.517	3.072	3.789	4.970
CUHP Runoff Volume (acre-ft) =	N/A	N/A	1.211	1.620	1.947	2.517	3.072	3.789	4.970
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.3	0.6	0.8	7.3	14.6	23.9	38.1
OPTIONAL CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.02	0.02	0.22	0.44	0.72	1.16
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	19.2	26.0	31.2	43.9	55.2	70.0	92.1
Peak Inflow Q (cfs) =	0.2	0.5	0.4	0.5	0.5	0.6	2.6	11.3	24.7
Peak Outflow Q (cfs) =	N/A	N/A	N/A	0.8	0.6	0.1	0.2	0.5	0.6
Ratio Peak Outflow to Predevelopment Q =	Plate	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Spillway
Structure Controlling Flow =	N/A	N/A	N/A	N/A	N/A	N/A	0.2	0.8	1.4
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Max Velocity through Gate 2 (fps) =	38	68	60	69	76	87	93	92	89
Time to Drain 97% of Inflow Volume (hours) =	40	72	63	73	81	92	100	99	98
Time to Drain 99% of Inflow Volume (hours) =	4.05	6.24	5.41	6.12	6.64	7.50	8.18	8.54	9.20
Maximum Ponding Depth (ft) =	0.37	0.60	0.53	0.59	0.63	0.68	0.72	0.75	0.79
Area at Maximum Ponding Depth (acres) =	0.525	1.614	1.142	1.536	1.859	2.415	2.893	3.166	3.674
Maximum Volume Stored (acre-ft) =									

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

Forebay Wall Notch

Notch to releae 2% of the undetained 100-year peak discharge.

$$\begin{aligned} 100\text{-y peak discharge} &= \mathbf{23.9} \text{ cfs} \\ 2.0\% &= \mathbf{0.48} \text{ cfs} \end{aligned}$$

The general form of the equation for horizontal crested weirs is $Q = CLH^{3/2}$ where:

Q = Weir flow discharge (cfs)	0.48	
C = Weir flow coefficient	3.4	
H = Depth of flow over the weir (ft)	1.50	Opening Height
L = Length of the weir (ft)	0.08	Length
L = Length of the weir (in)	1	

Minimim notch length is 3" per standards

Notch to releae 2% of the undetained 100-year peak discharge is 3" wide by 18" high (min allowed)

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Platte Self Storage** Location: **2' TRICKEL CHANNEL**
 By: **JS** Date: **4/29/2024**
 Chk By: **DF** Date: **4/29/2024** version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

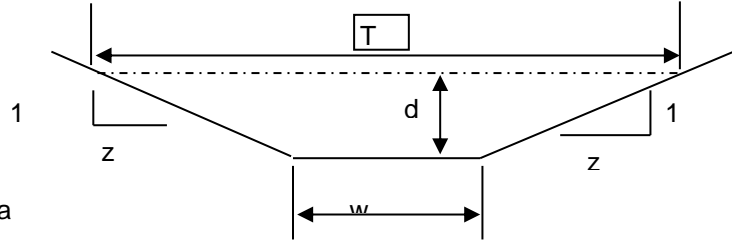
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 0
 b (btm width, ft)= 2
 d (depth, ft)= 0.5
 S (slope, ft/ft) 0.01
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.5	1.00	3.00	0.33	5.49513943	5.49514	5.495139	5.49514	2	0.500
Sc low =				0.0053	Sc high =		0.0053		
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc		
				0.0037	0.0069	0.0037	0.0069		

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

Created by: Mike O'Shea

Please provide erosion protection for this open channel as velocity is above the standard velocity per DCM vol.1, chapter 10, table 10-4

Please include calculations for trickle channel, emergency spillway, ripraps, stilling basin.

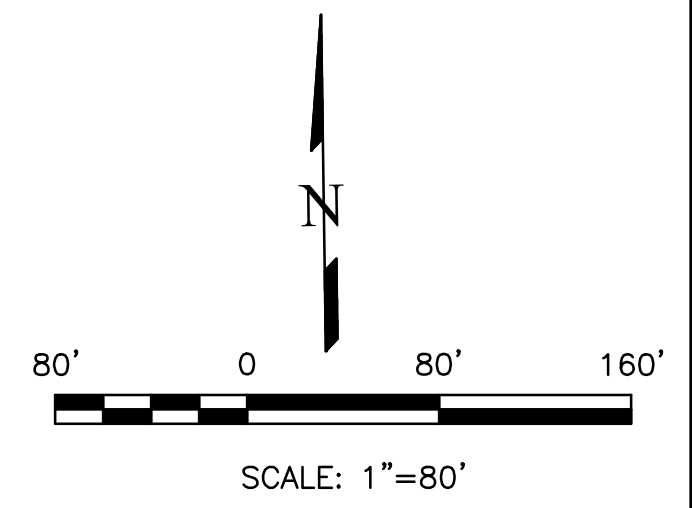
Per DCMv2 – Chap 4.2, trickle channel should at a minimum provide capacity equal to twice the release capacity at the upstream forebay outlet. Provide these calcs in the drainage report and revise plans as needed.

We need to know how much of the proposed area of disturbance (not just the impervious surfaces) is treated vs untreated and if there are any exclusions that apply to the untreated areas. So please create a basic overview map (or modify an existing drainage map) with color shading/hatching that shows areas tributary to each PBMP (pond, runoff reduction, etc.) and those disturbed areas that are not treated by a PBMP, with the applicable exclusion labeled (ex: 20% up to 1ac of development can be excluded per ECM App I.7.1.C.1 and exclusions listed in ECM App I.7.1.B.#). An accompanying summary table on this map would also be very helpful (example provided):

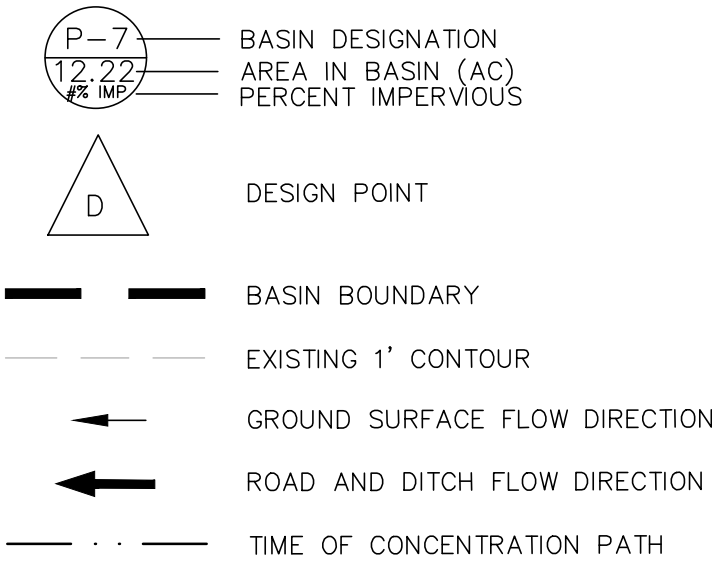
DRAINAGE MAPS

Water Quality Treatment Summary Table							
Basin ID	Total Area (ac)	Total Proposed Disturbed Area (ac)	Area Trib to Pond A (ac)	Disturbed Area Treated via Runoff Reduction (ac)	Disturbed Area Excluded from WQ per ECM App I.7.1.C.1 (ac)	Disturbed Area Excluded from WQ per ECM App I.7.1.B.# (ac)	Applicable WQ Exclusions (App I.7.1.B.#)
A	4.50	4.50	4.50				
B	1.25	1.25		1.25			
C	6.00	4.00				4.00	ECM App I.7.1.B.5
D	2.50	2.50	1.00		0.50	1.00	ECM App I.7.1.B.7
E	3.00		3.00				
F	8.25						
Total	25.50	12.25	8.50	1.25	0.50	5.00	
<i>Comments</i>		<i>[For each row, the sum of the values in Columns 4-7 must be greater than or equal to the value in Column 3 above.]</i>	<i>[Values in this column can be more than Column 3 if over-treating non-disturbed areas of the same land-use.]</i>	<i>[See RR calc spreadsheet.]</i>	<i>[Total must be <20% of site and <1ac.]</i>		
		Total Proposed Disturbed Area (ac)	Total Proposed Treated Area (ac)	Total Proposed Disturbed Area Excluded from WQ (ac)	Minimum Area to be Treated (ac)		
		12.25	9.75	5.50	6.75		

PLATTE SELF STORAGE SITE DEVELOPMENT PLAN EXISTING DRAINAGE MAP MAY 2024



LEGEND



NOTES

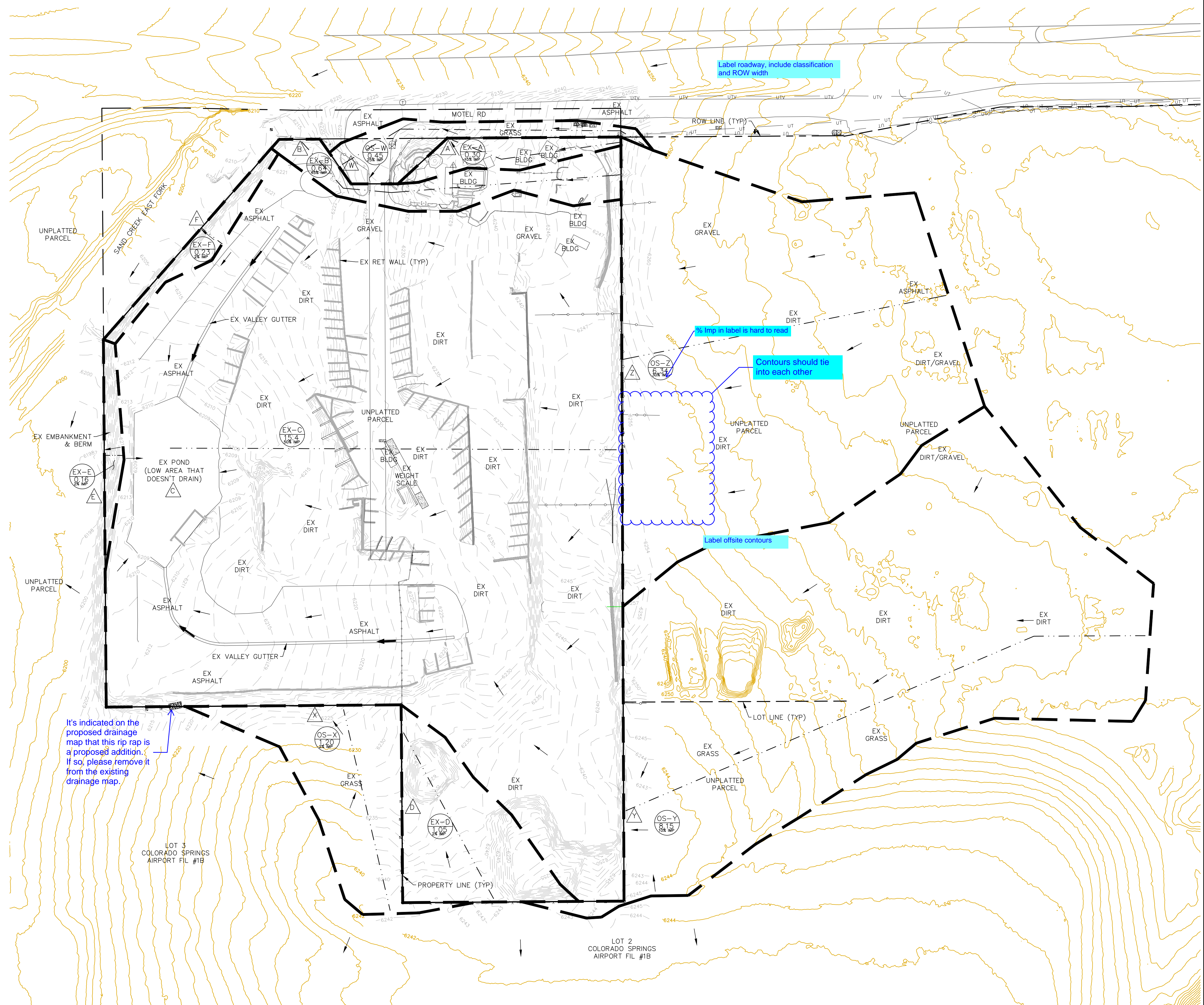
1. BROWN GROUND SURFACE CONTOURS ARE LIDAR DATA DOWNLOADED FROM THE COLORADO HAZARD MAPPING & RISK MAP PORTAL, DATA SET: 2018 3DEP EAST CO EL PASO. THIS DATA IS APPROXIMATE. LIDAR DATA IS FROM 2018 AND AT 2' INTERVALS.
2. THE EXISTING SITE IS A LANDSCAPING MATERIALS YARD. GROUND SURFACES ARE DIRT, GRAVEL, AND ASPHALT. THE EDGE OF ASPHALT IS OFTEN COVERED BY DIRT/GRAVEL AND IT'S EXTENTS ARE ONLY ROUGHLY KNOWN.

BASIN SUMMARY

BASIN	AREA TOTAL (Acres)	TOTAL FLOWS	
		Q _s (cfs)	Q ₁₀₀ (cfs)
OS-Z	6.34	6.1	16.7
OS-Y	8.15	3.6	15.4
OS-X	1.20	0.4	2.3
OS-W	0.45	0.5	1.3
EX-A	0.30	0.2	0.8
EX-B	0.64	1.1	2.6
EX-C	15.4	29.0	65.0
EX-D	1.05	0.3	1.9
EX-E	0.16	0.1	0.5
EX-F	0.23	0.1	0.7

DESIGN POINT SUMMARY

Design Point(s)	Contributing Basins	Area (ac)	Flow (cfs)	
			Q _s	Q ₁₀₀
Z	OS-Z	6.34	6.1	16.7
Y	OS-Y	8.15	3.6	15.4
X	OS-X, EX-D	2.25	0.7	4.2
W	OS-W	0.45	0.5	1.3
A	EX-A	0.30	0.2	0.8
B	EX-B	0.64	1.1	2.6
C	OS-Z, OS-Y, OS-X, EX-C, EX-D	32.14	39.4	101.4
D	EX-D	1.05	0.3	1.9
E	EX-E	0.16	0.1	0.5
F	EX-F	0.23	0.1	0.7



It's indicated on the proposed drainage map that this rip rap is a proposed addition. If so, please remove it from the existing drainage map.

REVISIONS

NO.	DESCRIPTION	DATE

UNTI SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE FOLLOWING AGENCIES: TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT AND FOR THE MOST PART BY WRITTEN AUTHORIZATION.

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RMG-ROCKY MOUNTAIN GROUP
ATTN:
5085 LIST DR, #200
COLORADO SPRINGS, CO 80919
719.548.0600

Terra Nova
Engineering, Inc.
Civil/Environmental Engineers

721 S. ZABO STREET
COLORADO SPRINGS, CO 80904
OFFICE: 719-635-6422
FAX: 719-635-6426
www.tninc.com

DESIGNED BY DLF
DRAWN BY DLF
CHECKED BY LD

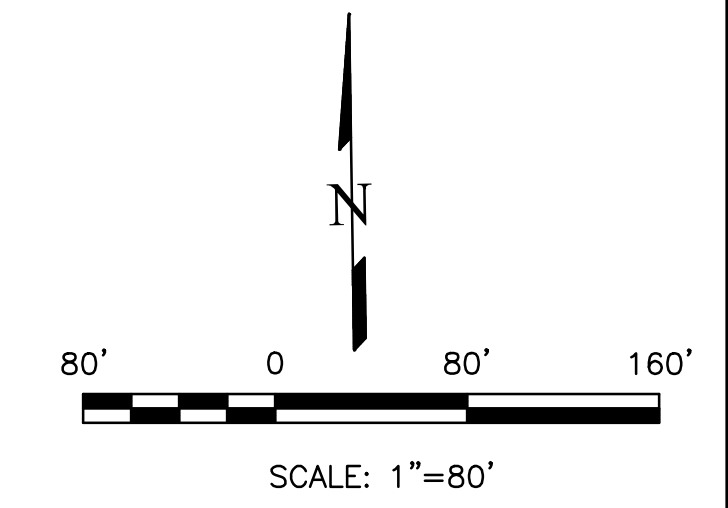
PLATTE SELF STORAGE
EXISTING DRAINAGE MAP

H-SCALE AS SHOWN
V-SCALE N/A

JOB NO. 2419.00
DATE ISSUED 05/07/24
SHEET NO. 1 OF 4

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PLATTE SELF STORAGE SITE DEVELOPMENT PLAN PROPOSED DRAINAGE MAP MAY 2024



LEGEND

- BASIN DESIGNATION
AREA IN BASIN (AC)
PERCENT IMPERVIOUS
- DESIGN POINT
- BASIN BOUNDARY
- EXISTING 1' CONTOUR
- GROUND SURFACE FLOW DIRECTION
- ROAD AND DITCH FLOW DIRECTION
- PROPOSED RETAINING WALL
- TIME OF CONCENTRATION PATH

NOTES

1. BROWN GROUND SURFACE CONTOURS ARE LIDAR DATA DOWNLOADED FROM THE COLORADO HAZARD MAPPING & RISK MAP PORTAL, DATA SET: 2018 3DEP EAST CO EL PASO. THIS DATA IS APPROXIMATE. LIDAR DATA IS FROM 2018 AND AT 2' INTERVALS.

BASIN	AREA TOTAL (Acres)	TOTAL FLOWS	
		Q _s (cfs)	Q ₁₀₀ (cfs)
OS-Z	6.34	6.1	16.7
OS-Y	8.15	3.6	15.4
OS-X	1.20	0.4	2.3
OS-W	0.45	0.5	1.3
1	0.07	0.0	0.2
2	0.13	0.1	0.4
3	5.12	23.1	41.4
4	3.66	8.2	16.8
5	0.56	0.1	0.9
6	6.64	3.1	13.1
7	0.34	0.2	1.1
8	0.30	0.2	1.0
9	0.59	0.2	1.5
10	0.40	0.3	1.4

DESIGN POINT SUMMARY

Design Point(s)	Contributing Basins	Area (ac)	Flow (cfs)	
			Q _s	Q ₁₀₀
1	PR-1	0.07	0.0	0.2
2	PR-2	0.13	0.1	0.4
3	PR-3	5.12	23.1	41.4
4	OS-Y, PR-4	11.81	11.8	32.2
5	OS-X, PR-5	1.76	0.5	3.3
6	PR-6	6.64	3.1	13.1
7	PR-7	0.34	0.2	1.1
8	PR-8	0.30	0.2	1.0
9	PR-9	0.59	0.2	1.5
10	OS-Z, PR-10	6.74	6.4	18.1

See comments on summary table in report

Please display more off-site contour 50'-200 feet beyond the boundary or drainage basin delineation line to illustrate how the runoff diverges from the site.

Please show and label all side slope of the pond. Side slope cannot be steeper than 3:1.

Please consider the distance between inlet and outlet. Distance measured along the trickle channel (from inlet to outlet) to the average basin width is at least 1.5:1, and greater than 2:1 is preferred. USDCM, Chapter 4, T-6.

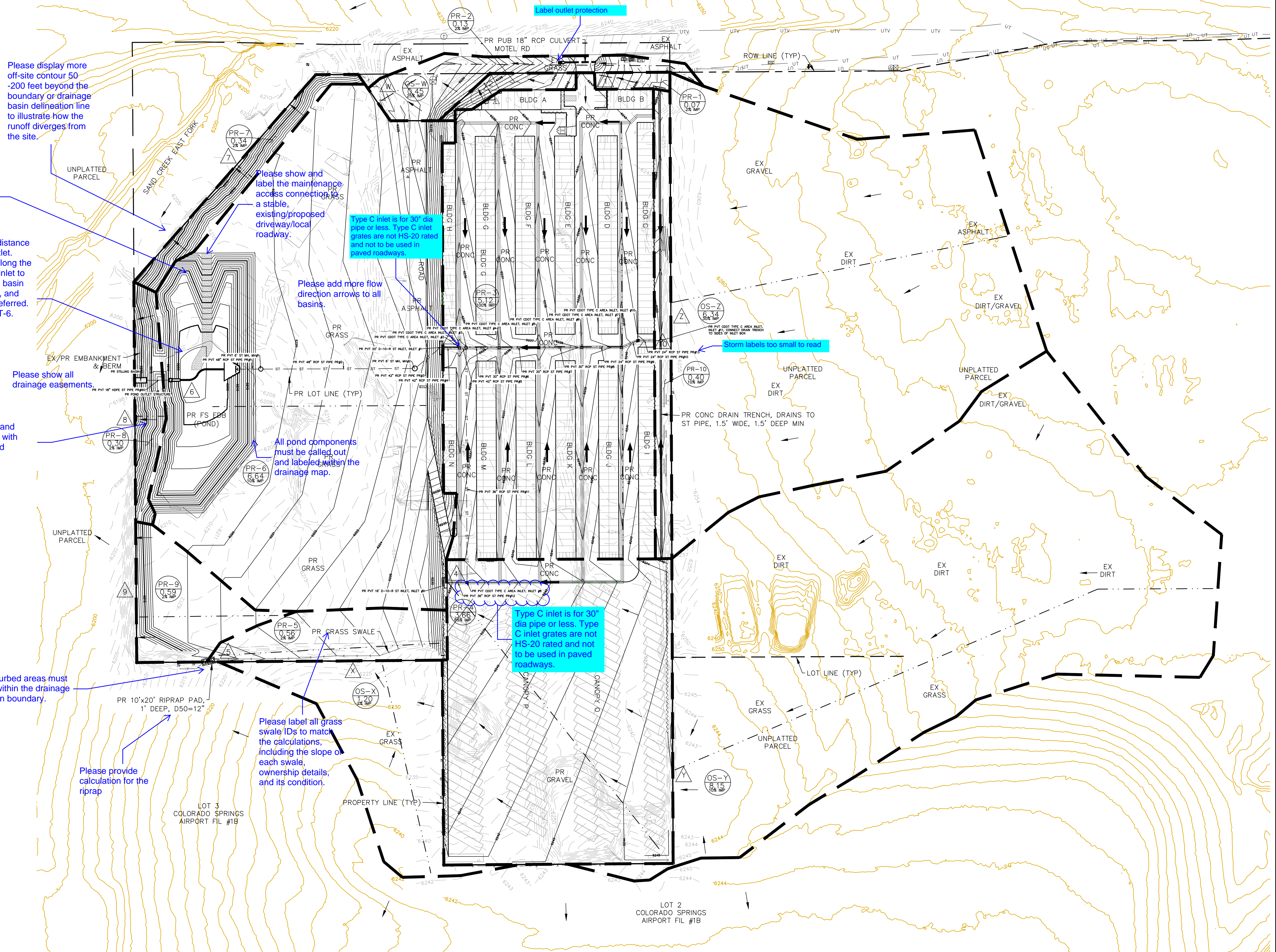
Please show all drainage easements.

Please show and label spillway with type, size, and condition.

Disturbed areas must be within the drainage basin boundary.

Please provide calculation for the riprap

Please label all grass swale IDs to match the calculations, including the slope of each swale, ownership details, and its condition.



<p>REVISIONS</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 5%;">NO.</th> <th style="width: 85%;">DESCRIPTION</th> <th style="width: 10%;">DATE</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DESCRIPTION	DATE										<p>UNTL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE REVIEWING AGENCIES, THE TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT AND FOR THE MOST PART BY WRITTEN AUTHORIZATION.</p> <p>PREPARED FOR: RMG-ROCKY MOUNTAIN GROUP ATTN: 5085 LIST DR, #200 COLORADO SPRINGS, CO 80919 719.548.0600</p> <div style="text-align: center;"> <p>Terra Nova Engineering, Inc. Civil/Environmental Engineers</p> </div> <p>721 S. ZABO STREET COLORADO SPRINGS, CO 80904 OFFICE: 719-635-6422 FAX: 719-635-6426 www.tninc.com</p> <p style="text-align: center;">PLATTE SELF STORAGE PROPOSED DRAINAGE MAP</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>DESIGNED BY DLF</td> </tr> <tr> <td>DRAWN BY DLF</td> </tr> <tr> <td>CHECKED BY LD</td> </tr> <tr> <td>H-SCALE AS SHOWN</td> </tr> <tr> <td>V-SCALE N/A</td> </tr> <tr> <td>JOB NO. 2419.00</td> </tr> <tr> <td>DATE ISSUED 05/07/24</td> </tr> <tr> <td>SHEET NO. 2 OF 4</td> </tr> </table>	DESIGNED BY DLF	DRAWN BY DLF	CHECKED BY LD	H-SCALE AS SHOWN	V-SCALE N/A	JOB NO. 2419.00	DATE ISSUED 05/07/24	SHEET NO. 2 OF 4
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PLATTE SELF STORAGE

SITE DEVELOPMENT PLAN

PROPOSED DETENTION POND

MAY 2024

FOR REFERENCE ONLY
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NOTES

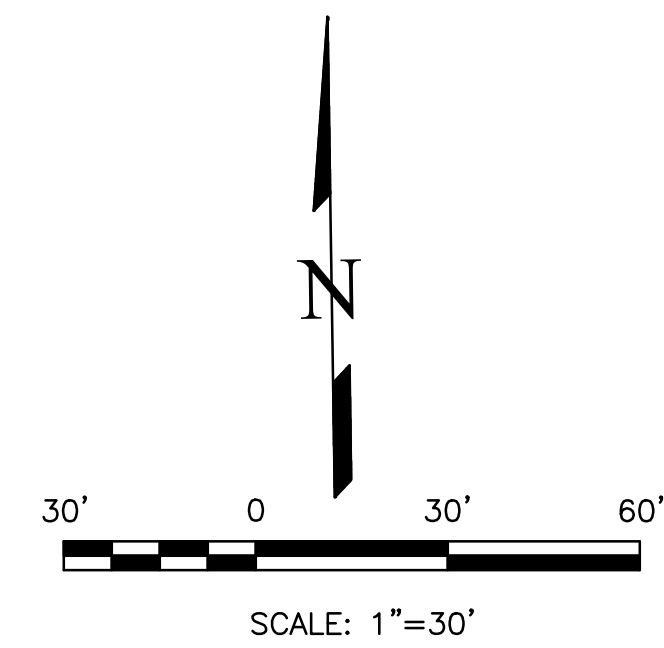
1. ALL HDPE STORM PIPE IS TO BE SMOOTH INTERIOR PIPE.
2. LARGE BLOCKS OF TEXT QUOTING STANDARD DRAWINGS OR DETAILS ARE INCLUDED AS A REQUIREMENT OF COUNTY REVIEWERS.

BENCHMARKS

#5 REBAR WITH ORANGE PLASTIC CAP MARKED "CSAM, LLC PLS 32439", FLUSH WITH GROUND - ELEV.=6513.85 (NAVD-1988) [NORTHWEST PROPERTY CORNER]

GRADING LEGEND

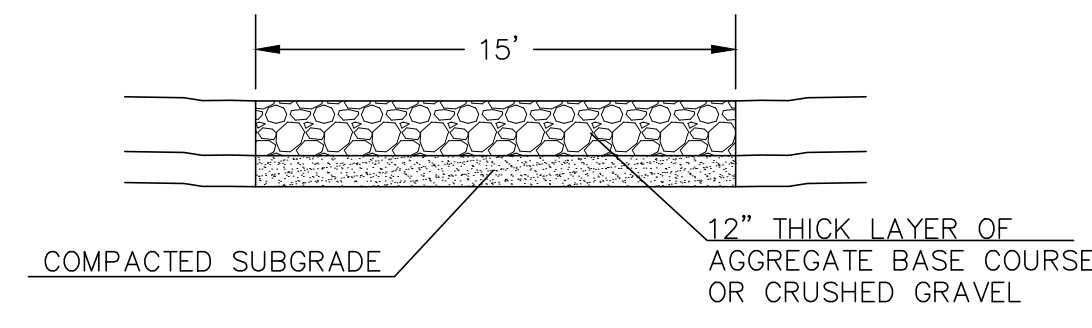
PROPOSED	PR	EXISTING CONTOURS - MINOR	---	6231
EXISTING	EX	EXISTING CONTOURS - MAJOR	---	6230
FINISHED SURFACE	FS	PROPOSED CONTOURS - 1'	---	6231
FINISHED GROUND	FG	EXISTING PROPERTY LINE	---	
TOP OF CURB	TC	PROPOSED RET WALL	---	
FLOWLINE	FL	PROPOSED RIPRAP	---	
FINISH GROUND AT TOP OF WALL	TW	WATER LINE	---	
FINISH GROUND AT BOTTOM OF WALL	BW	SANITARY SEWER LINE	---	
LOW POINT	LP	GAS LINE	---	
HIGH POINT	HP	UNDERGROUND ELECTRICAL LINE	---	
FLOW ARROW		TELEPHONE LINE	---	
PROPOSED CONTOURS (LIDAR)	8130	FIBER OPTIC LINE	---	
		STORM SEWER LINE	---	
		LIMIT OF CONSTRUCTION	---	
		LIMIT OF SOIL DISTURBANCE	---	
		PROPOSED FENCE	---	
		FIRE HYDRANT	---	



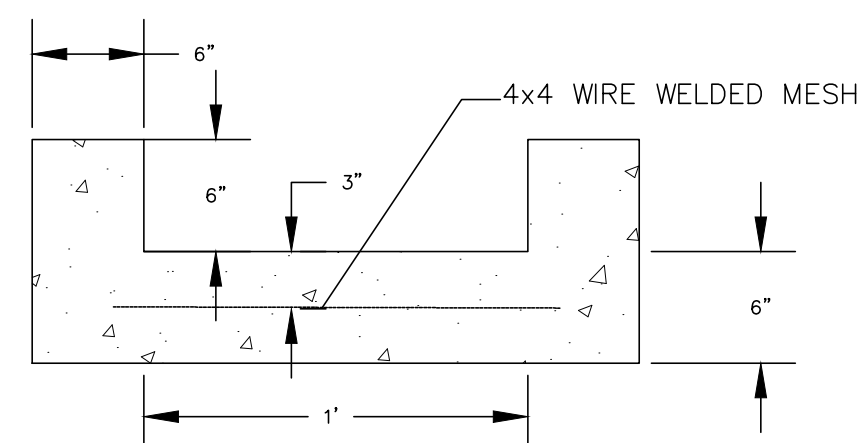
POND WATER LEVEL ELEVS

WOCV: 6206.05
EURV: 6208.24
100-YR: 6210.54

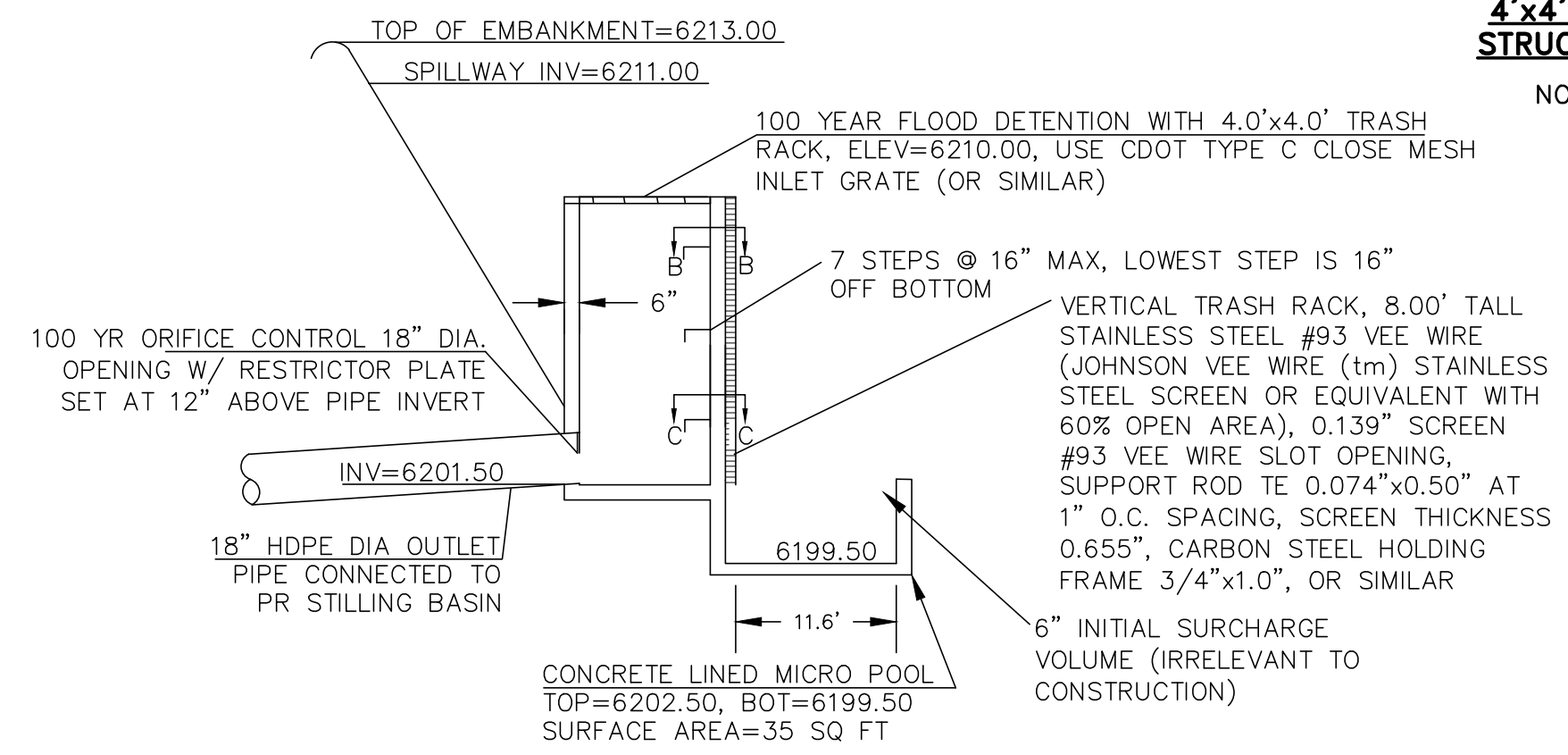
Construction plans are not reviewed within the drainage report. Please remove.



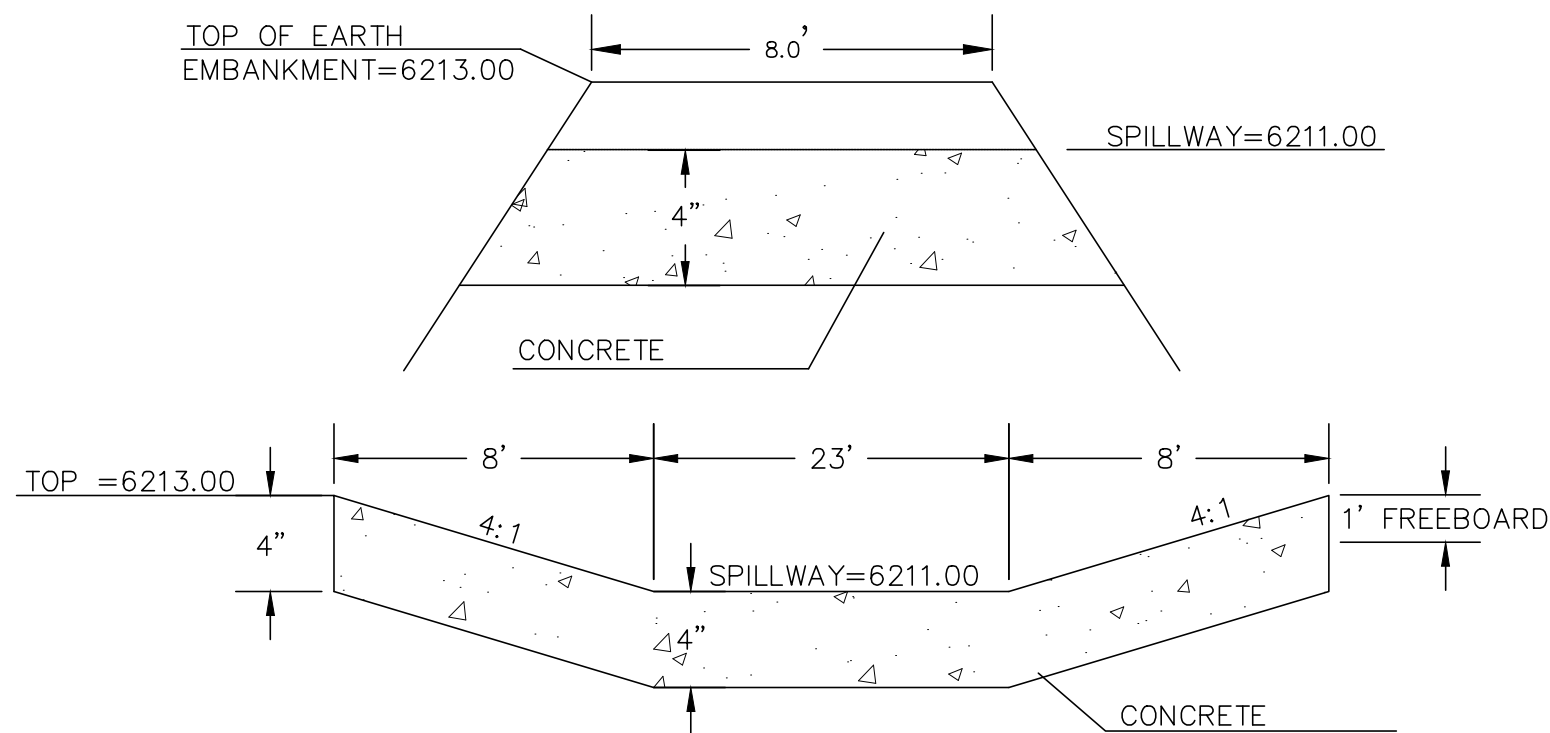
15' MAINTENANCE ACCESS ROAD SECTION
NOT TO SCALE



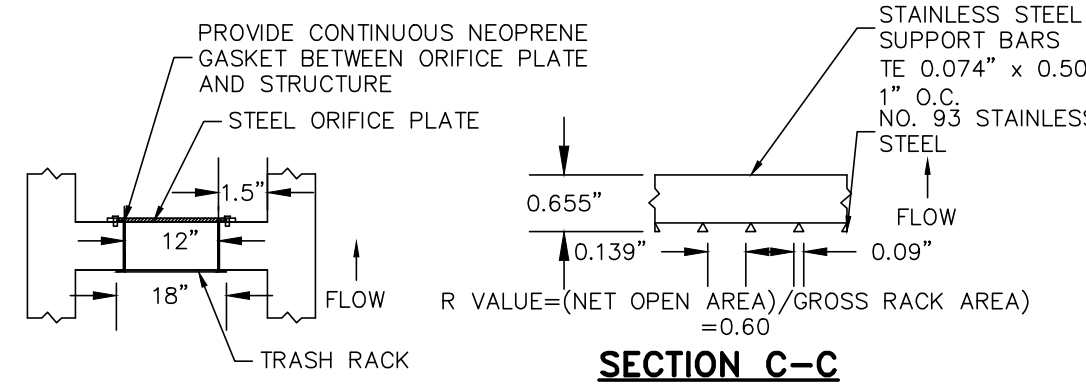
1' CONCRETE TRICKLE CHANNEL
NOT TO SCALE



OUTLET STRUCTURE
NOT TO SCALE

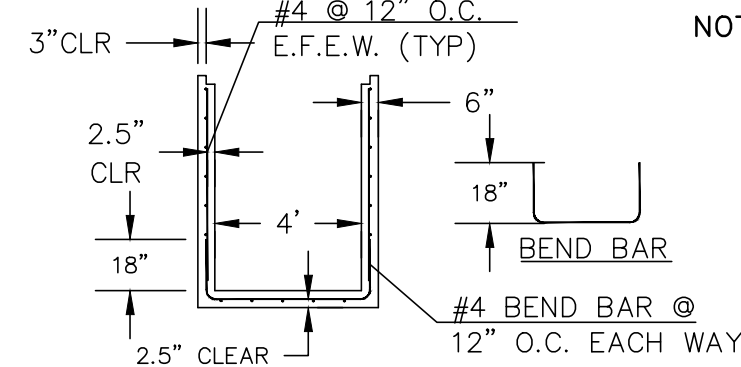


EDB EMERGENCY WEIR
NOT TO SCALE

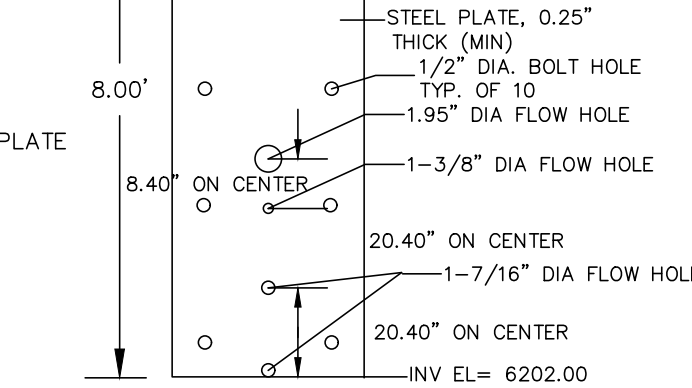
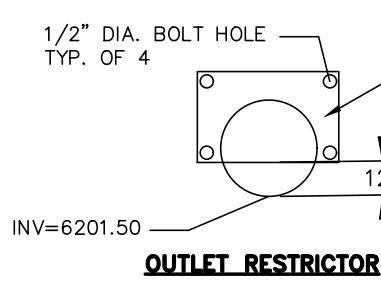


SECTION B-B
NOT TO SCALE

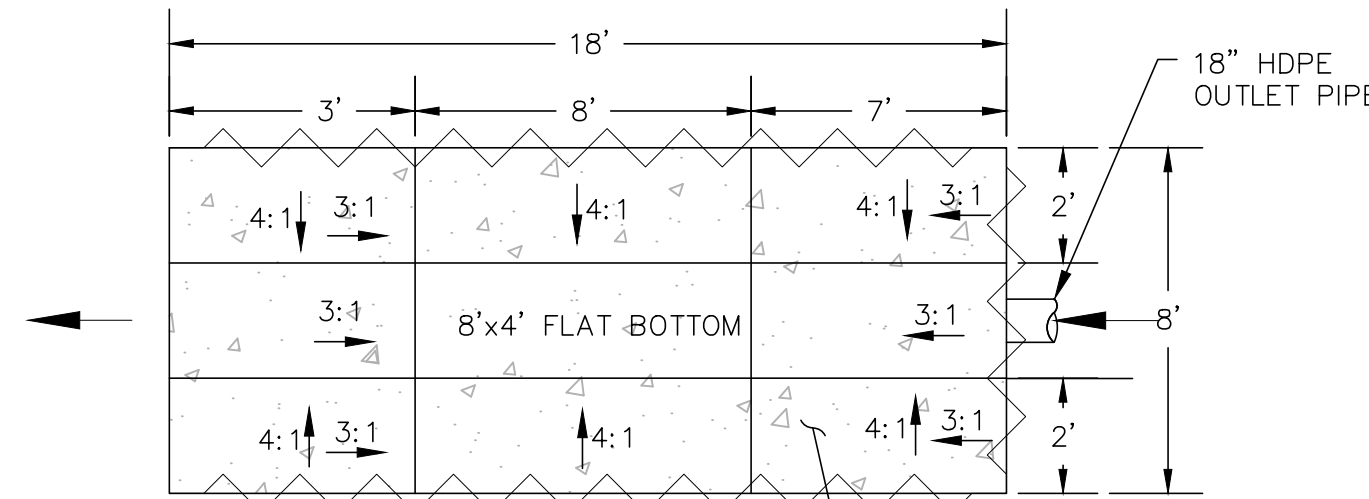
SECTION C-C
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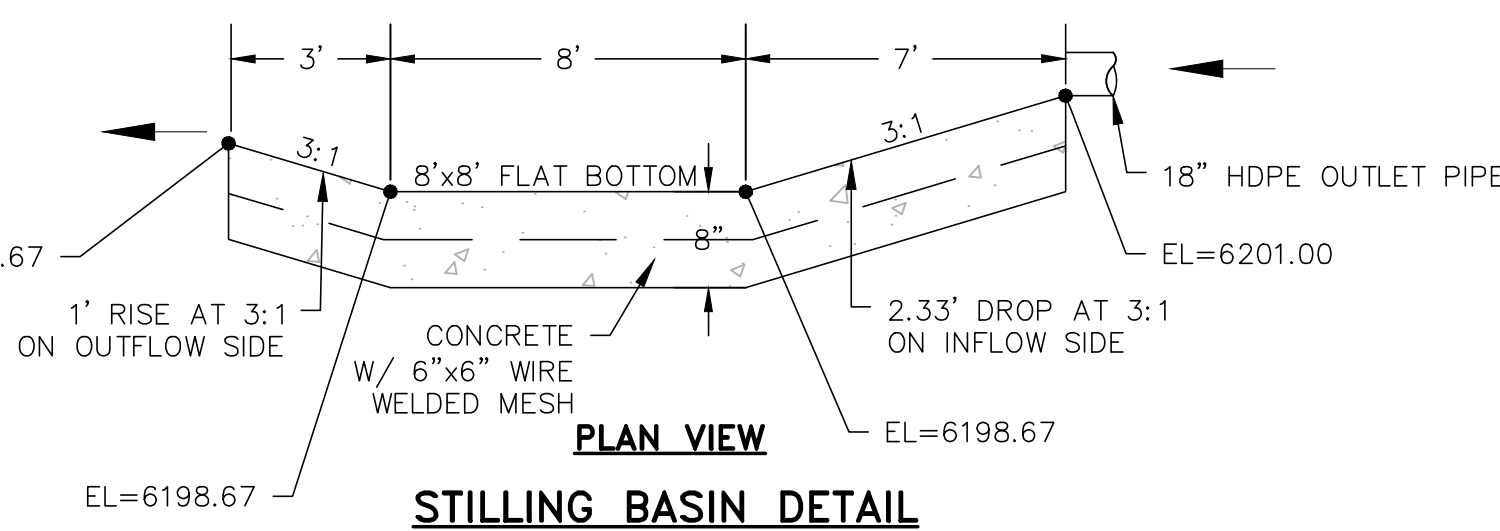
4'x4' OUTLET BOX STRUCTURAL DETAIL
NOT TO SCALE



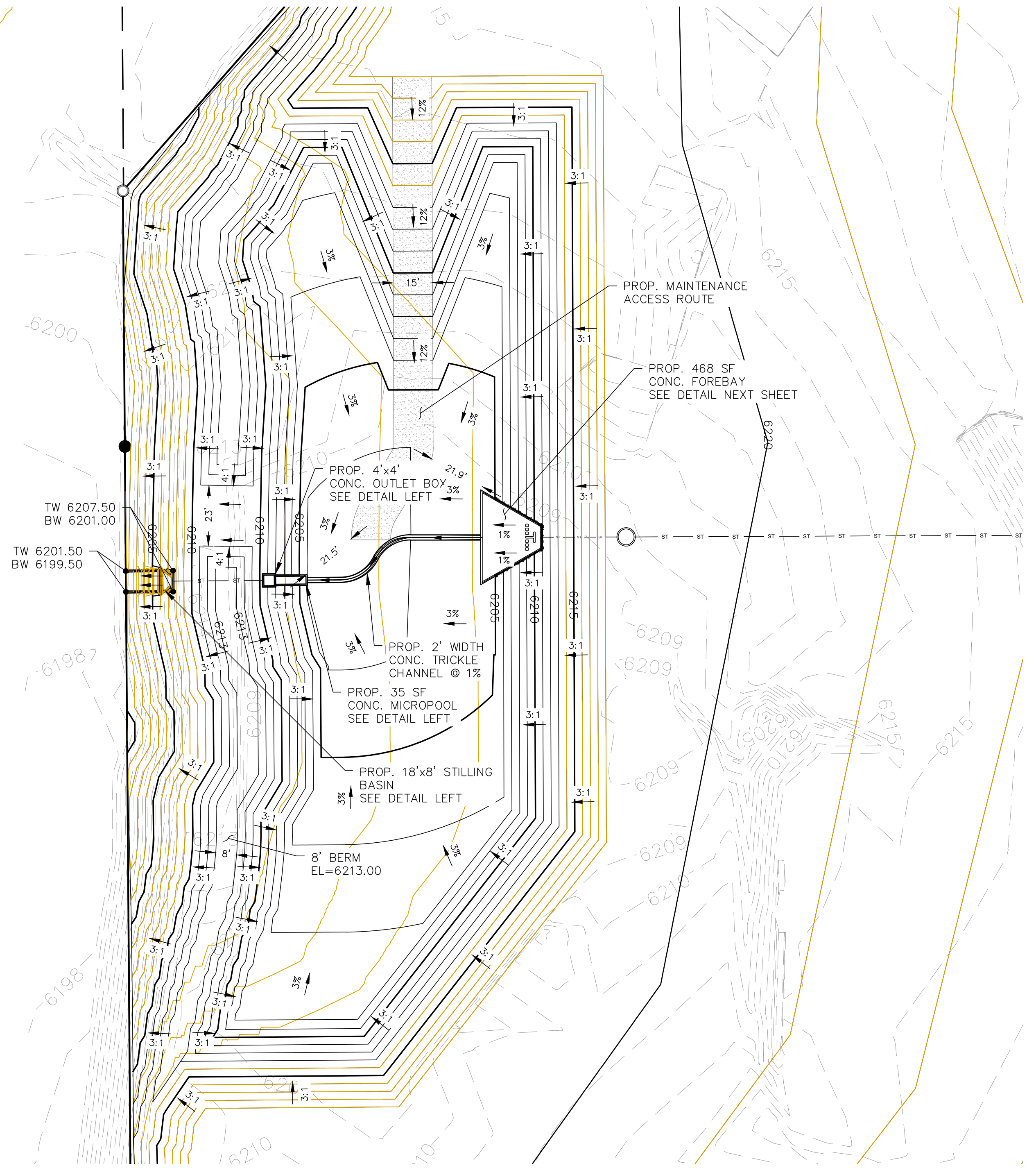
INLET ORIFICE PLATE PERFORATED HOLE PATTERN
NOT TO SCALE



PROFILE VIEW



STILLING BASIN DETAIL
NOT TO SCALE



<p>DESIGNED BY DLF DRAWN BY DLF CHECKED BY LD</p> <p>H-SCALE AS SHOWN V-SCALE N/A</p> <p>JOB NO. 2419.00 DATE ISSUED 05/07/24 SHEET NO. 3 OF 4</p>	<p>PLATTE SELF STORAGE</p> <p>PROPOSED DETENTION POND</p>	<p>REVISIONS</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 5%;">NO.</th> <th style="width: 95%;">DESCRIPTION</th> </tr> <tr> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> </tr> </table>	NO.	DESCRIPTION							<p>DATE</p> <p>UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE ENGINEER, THE REVIEWING AGENCIES, THE TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT AND FOR THE MOST PART BY WRITTEN AUTHORIZATION.</p> <p>PREPARED FOR: RMG-ROCKY MOUNTAIN GROUP ATTN: 5085 LEST DR, #200 COLORADO SPRINGS, CO 80919 719.548.0600</p> <p style="text-align: center;"> Terra Nova Engineering, Inc. Civil/Environmental Engineering </p> <p>721 S. ZARO STREET COLORADO SPRINGS, CO 80904 OFFICE: 719-635-6422 FAX: 719-635-6426 www.tnainc.com</p>
NO.	DESCRIPTION										

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PLATTE SELF STORAGE SITE DEVELOPMENT PLAN PROPOSED DETENTION POND MAY 2024

GRADING LEGEND

PROPOSED	PR	EXISTING CONTOURS - MINOR	---6231---
EXISTING	EX	EXISTING CONTOURS - MAJOR	---6230---
FINISHED SURFACE	FS	PROPOSED CONTOURS - 1'	---6231---
FINISHED GROUND	FG	EXISTING PROPERTY LINE	_____
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FLOWLINE	FL	PROPOSED RIPRAP	XXXXXX
FINISH GROUND AT TOP OF WALL	TW	WATER LINE	—v—v—
FINISH GROUND AT BOTTOM OF WALL	BW	SANITARY SEWER LINE	—ss—ss—
LOW POINT	LP	GAS LINE	—ug—ug—
HIGH POINT	HP	UNDERGROUND ELECTRICAL LINE	—ue—ue—
FLOW ARROW	←	TELEPHONE LINE	—ut—ut—
PROPOSED CONTOURS (LIDAR)	8130	FIBER OPTIC LINE	—fo—fo—
		STORM SEWER LINE	—st—st—
		LIMIT OF CONSTRUCTION	-----
		LIMIT OF SOIL DISTURBANCE	- - - - -
		PROPOSED FENCE	□ □ □ □
		FIRE HYDRANT	⊕

POND WATER LEVEL ELEVS

WQCV: 6206.05
EURV: 6208.24
100-YR: 6210.54

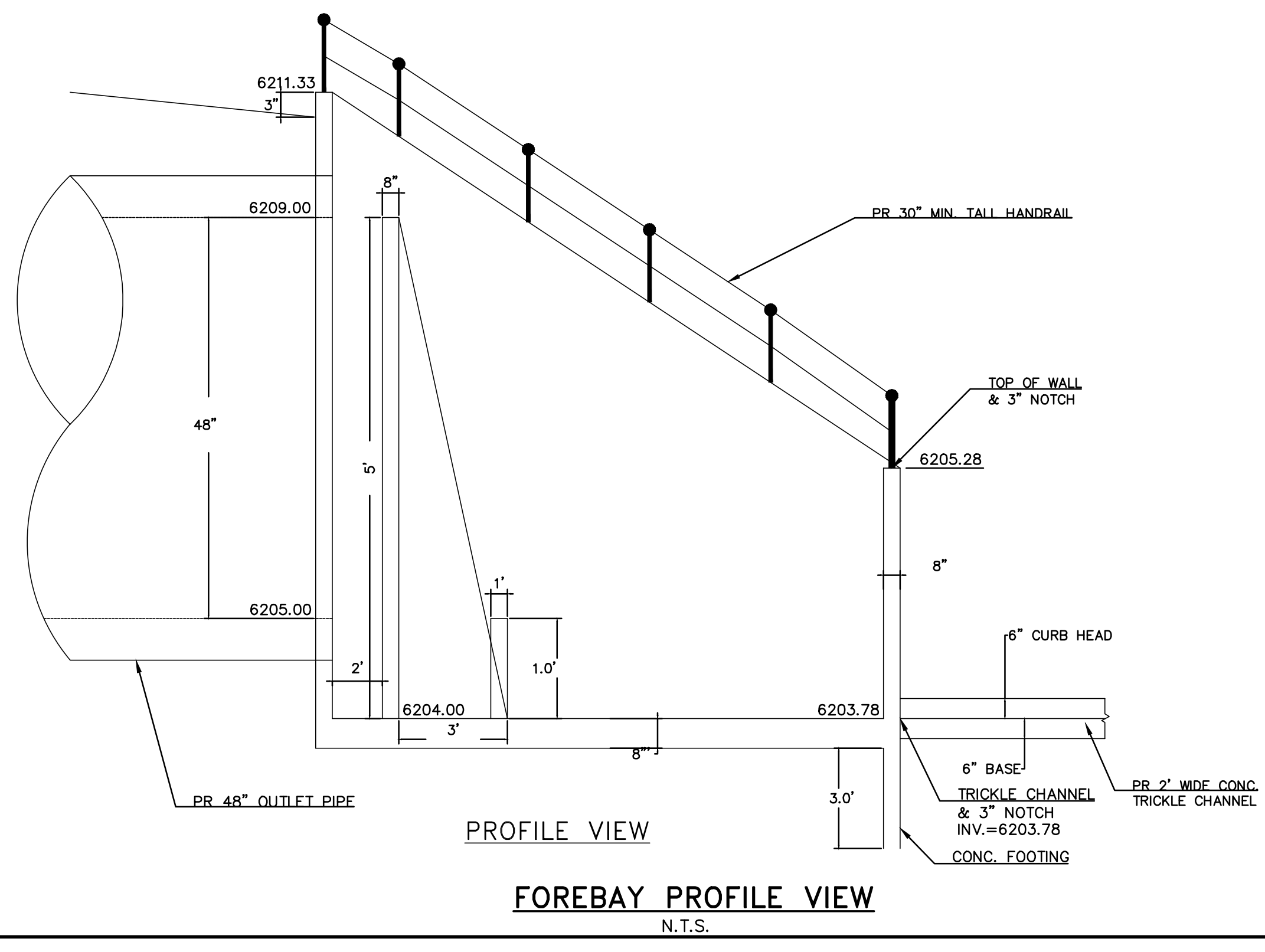
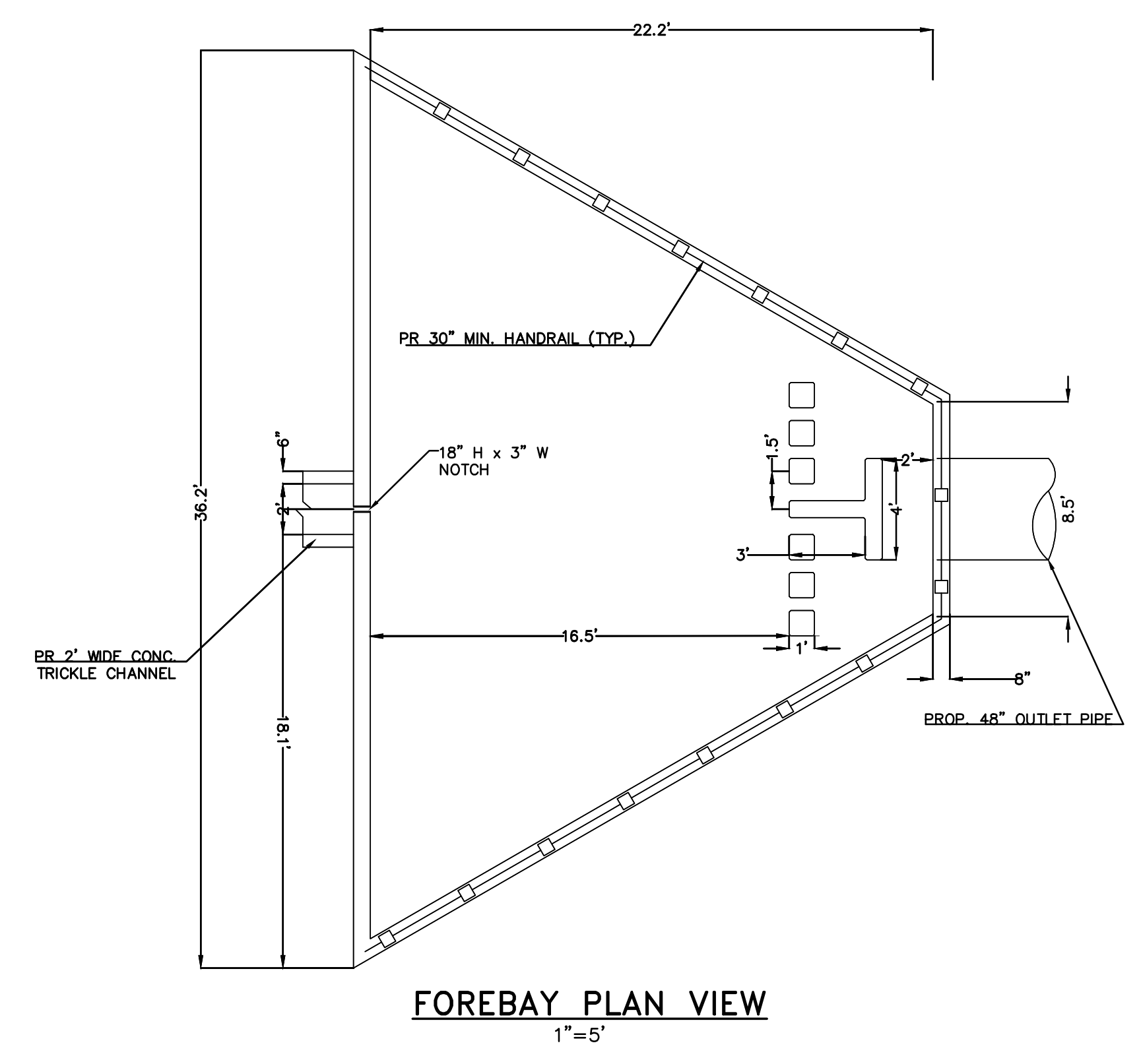
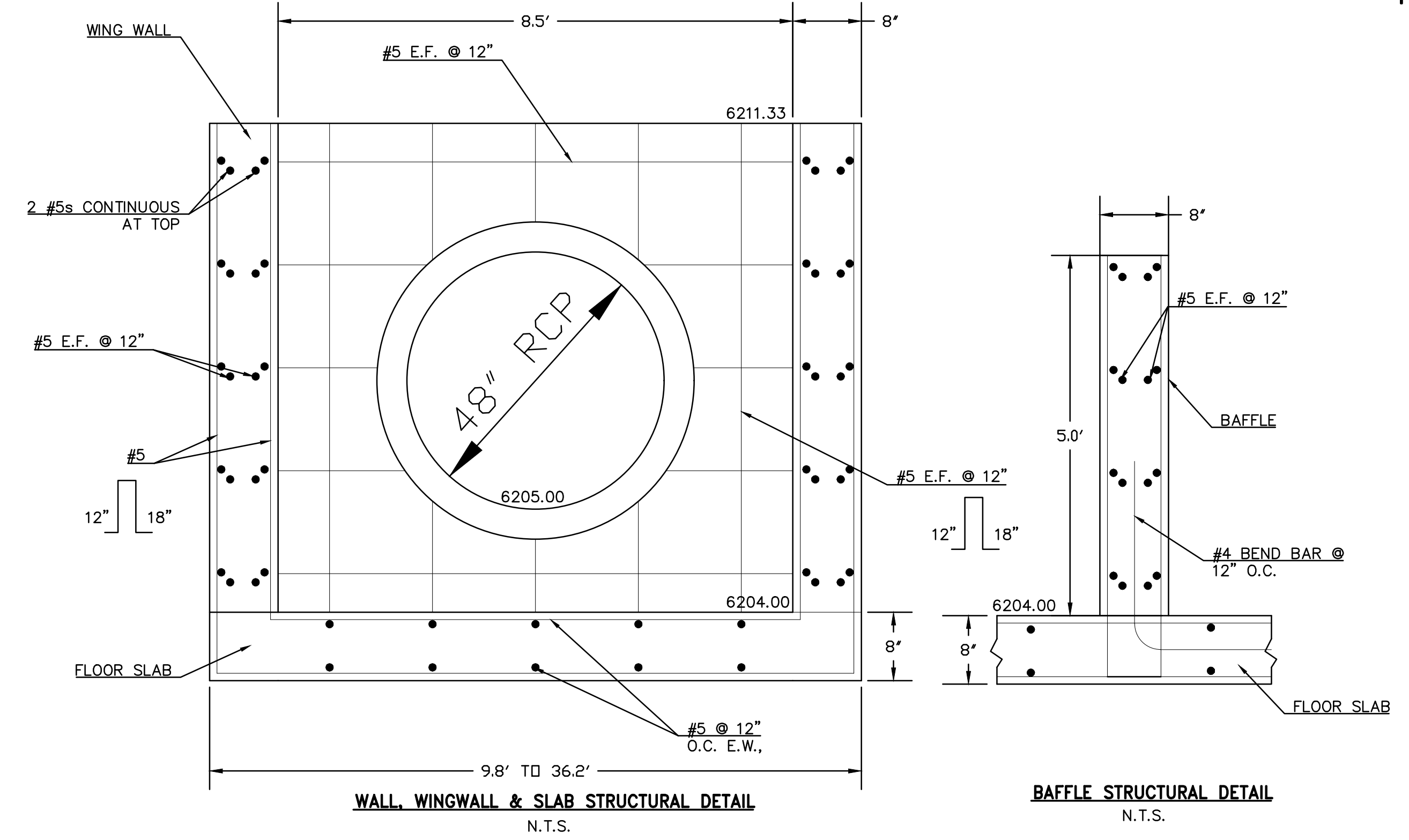
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PLATTE SELF STORAGE

PROPOSED DETENTION POND

DESIGNED BY	DLF
DRAWN BY	DLF
CHECKED BY	LD
H-SCALE	AS SHOWN
V-SCALE	N/A
JOB NO.	2419.00
DATE ISSUED	05/07/24
SHEET NO.	4 OF 4

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