



May 22, 2024
Project No. 24-041

PCD File NO. PAV 244

Mr. Shay Miles, PE
Lodestar Engineering, LLC
PB Box 88461
Colorado Springs, CO 80908

**Subject: Memorandum for Pavement Thickness Design
Fox Creek Lane Extension at Terra Ridge North
Black Forest, El Paso County, Colorado**

Dear Mr. Miles,

Granite Engineering Group, Inc. (GEG) has completed the engineering evaluation and prepared this memorandum to address the pavement thickness design for the Fox Creek Lane extension at the Terra Ridge North Community in El Paso County, Colorado.

Project Background

Based on the information provided to us, it is our understanding that the development consists of 13 new custom-home lots accessed via an approximate 1000' extension of Fox Creek Lane. The existing Fox Creek Lane is paved with Hot Mix Asphalt (HMA). At the time of exploration, the roadway extension was a graded, soil roadway and will be paved with HMA in the near future. Light gravel had been placed at the southern end of the extension.

It is our understanding that the proposed roadway will be a lightly trafficked, residential 2-way street consisting of HMA

1 FIELD EXPLORATION AND LABORATORY TESTING

A total of four (4) borings were performed at the approximate locations as shown in the Boring Location Plan. These borings were performed at approximately 250 feet spacing along the graded roadway extension. These borings were explored with hand auger to approximately 5 feet below existing ground surface (bgs) or hand auger refusal, whichever occurred first. Drive samples with hand driver were obtained in Borings D-1, D-3 and D-4. The strength of the existing subgrade was evaluated using Dynamic Cone Penetration (DCP) tests. The DCP apparatus consists of a 5/8" diameter steel rod with a 60 degrees conical tip. The rod is topped with an anvil that is connected to a second rod. The rod is used as a guide to allow an 8kg hammer to be repeatedly raised and dropped from a height of 575 mm. The connection between the two rods consists of an anvil to allow for quick connections between the rods and for efficient energy transfer from the falling weight to the penetrating rod. The penetration of the rod is measured after each drop. The penetration value can be correlated to the common engineering parameters.

All borings were dry at the completion of testing.

The samples were tested for soil classification and swell-consolidation tests. Analytical testing was not performed since hot mix asphalt will be used for the pavement and Portland cement concrete is not planned. The boring logs and the laboratory test results are presented in Appendix B and C, respectively.

2 PAVEMENT THICKNESS RECOMMENDATIONS

The pavement thickness design was performed in accordance with El Paso County Engineering Criteria Manual.

2.1 SUBGRADE STRENGTH

The subgrade strength is evaluated using DCP tests. The blow counts and penetration of the DCP are used to calculate the DCP index. The DCP index paired with the soil type were correlated to the CBR of the in-situ subgrade soils based on the correlations published by US Army Corp of Engineers. The calculated CBR values and the DCP results are attached to this memo. Based on the results of the DCP and field exploration, a CBR of 3 is selected, which is correlated to a resilient modulus (Mr) value of 4,500 psi and was used for the prepared subgrade along the new extension for the pavement thickness design. Laboratory testing of subgrade strength including R-value or CBR was not performed since DCP was used to test the in-place pavement subgrade strength.

2.2 TRAFFIC LOADING

Traffic information was provided in the Terra Ridge North Transportation Memorandum dated February 9, 2023 prepared by LSC Transportation Consultants, Inc. based on the report, it is estimated that the pavement will subject to 104 vehicles per day. We also estimate that 20 delivery trucks and 2 trash or trailer truck per day. An ESAL of 27,277 was estimated based on the traffic. The El Paso County Engineering Criteria Manual has a minimum ESAL of 36,500 for Local Road in Rural area, and it was used for the pavement thickness design.

2.3 PAVEMENT THICKNESS DESIGN

Pavement thickness design was performed using the WinPAS Version 12. The designs was performed in accordance with the 1993 AASHTO Pavement Design Guide and El Paso County Engineering Criteria Manual. Tables 1-1 and 1-2 present a summary of the design input parameters.

Table 1-1. Pavement Design Parameters

| Parameter | Value |
|--------------------------------|---------------------|
| Design Period (year) | 20 |
| 18-kip ESAL over design period | 36,500 for flexible |
| Reliability (%) | 75 |
| Overall Standard Deviation | 0.44 for flexible |
| Initial Serviceability Index | 4.5 |
| Terminal Serviceability Index | 2.5 |

Table 1-2. Pavement Design Strength Coefficients

| Parameter | Value |
|---|-------|
| New Hot Mix Asphalt (HMA) Layer Coefficient | 0.44 |

| | |
|--|-------|
| Drainage Coefficient | 1.0 |
| Aggregate Base Course (ABC) ¹ Layer Coefficient | 0.11 |
| Subgrade Soil Resilient Modulus (psi) | 4,500 |

¹ ABC meeting El Paso County Engineering Criteria Manual

Based on the above design parameters, the recommended reconstruction sections for flexible pavements are presented in Table 1-3.

Table 1-3. Recommended Minimum Pavement Sections

| Pavement Reconstruction | HMA Pavement Section |
|--------------------------|--|
| Fox Creek Lane Extension | -4.5 inches HMA -6.0 inches ABC -Subgrade ¹ |

PCC= Portland cement concrete HMA= Hot mixed asphalt

¹ Subgrade should be prepared in accordance with Section 3 of the report.

2.4 PAVEMENT MATERIALS

2.4.1 Base Course

We recommend aggregate meetings Class 5 or Class 6 of the El Paso County Engineering Criteria Manual, Appendix D, Table D-6 to be used for the aggregate base materials. The material should be placed in a uniform layer without segregation of size and compacted in loose lifts not to exceed 8-inches.

2.4.2 Hot Mix Asphalt

Hot mix asphalt materials, placement procedures, and testing should follow The Pike Peak Region Asphalt Specification. We recommend PG 58-28 HMA binder with Grading S or SX aggregate, and gyration of 75.

3. CONSTRUCTION RECOMMENDATIONS

3.1 SUBGRADE PREPARATION AND EARTHWORK

3.1.1 Site Preparation

Site preparation should begin by stripping and removal of vegetation, existing structures, and other deleterious materials. Clearing and Grubbing operations and removal of existing structure should be performed in accordance with El Paso County Engineering Criteria Manual (EPCECM). All exposed surfaces should be free of mounds and depressions, which may prevent uniform compaction. Stripped materials consisting of vegetation and organic materials should be removed from the site or be used to re-vegetate landscaped areas and exposed slopes after completion of grading operations. The site should be initially graded to create an appropriate surface to receive fill. All exposed areas which will receive fill, once properly cleared and benched, should be scarified to a minimum depth of 12 inches, moisture conditioned and recompacted in accordance with Section 4.2.4 of this report. Based upon the subsurface conditions encountered, subgrade soils exposed during construction are anticipated to be relatively stable. However, the stability of the subgrade may be affected by drainage and precipitation. If unstable conditions are encountered or develop during construction, stability may be improved by scarifying and drying the subgrade soils or with other ground improvement techniques. A typical stabilization method may include utilizing gravel with the combination of

geo-grid (e.g. Tensar NX650) to create a stable base. Other stabilization methods may also be appropriate.

3.1.2 Fill Materials and Subgrade Preparation

Following initial excavation and subgrade preparation in the construction areas, visual inspection and proof rolling of the exposed subgrade is required to identify potential areas where the subgrade contains soft / loose soils. The proof roll should be performed in accordance with EPCECM. Areas which deform non-uniformly under heavy wheel loads should either be moisture conditioned and recompacted or excavated and replaced with properly compacted structural fill. The depth of over-excavation, if required, should be determined during construction. We recommend that the proof rolling activities and visual inspection of the foundation soils be observed and evaluated by an experienced geotechnical engineer or engineer's representative.

Fill placed on existing slopes that are steeper than 4H:1V should be properly benched in accordance with EPCECM. All compaction efforts should be performed in horizontal lifts that are 8-inches or less in loose thickness, using equipment and procedures that will produce a uniform fill with the required moisture contents and densities throughout the lift. The required percent of relative compaction and moisture content for the fill materials are presented in the EPCECM.

Fill materials should be tested for severity of sulfate exposure prior to placement. We recommend that the subgrade preparation process including soil excavation, the placement and compaction of materials, proof rolling and visual inspection of subgrade soils be observed and evaluated by the geotechnical engineer of record or the engineer's representative.

3.1.3 Excavation and Trench Grading

All site excavation and embankment grading should conform to EPCECM. Cut slopes should be protected from surface water runoff to prevent erosion and slope failure. Landscape sprinklers if present should be frequently checked for leaks and maintained in good working order. Surface drainage should be provided around all permanent cuts and fills to direct surface runoff away from the slope faces. Concentrated runoff should be prevented in areas susceptible to erosion or slope instability.

Excavations into the on-site soils will encounter a variety of conditions. All excavations must comply with the applicable local, State, and Federal safety regulations, and particularly with the excavation standards of the Occupational Safety and Health Administration (OSHA). Construction site safety, including excavation safety, is the sole responsibility of the Contractor as part of its overall responsibility for the means, methods, and sequencing of construction operations. GEG recommendations for excavation support is provided for the Client's sole use in planning the project, in no way do they relieve the Contractor of its responsibility to construct, support, and maintain safe slopes. Under no circumstances should the following recommendations be interpreted to mean that GEG is assuming responsibility for either construction site safety or the Contractor's activities.

We believe the overburden soil encountered at this site will classify as a Type C material, using OSHA criteria. OSHA requires that unsupported cuts be no steeper than 1½:1 for Type C for unbraced excavations up to 20 feet in height. In general, we believe that these slope ratios will be temporarily stable under unsaturated conditions. Flattened slopes may be required if excavations encounter groundwater or the slopes will be exposed for an extended period of time. Please note that the Contractor's OSHA-qualified "competent person" must make the actual determination of soil type and allowable sloping in the field.

The soils encountered by the proposed excavations may vary significantly across the site. The preliminary classifications presented above are based solely on the materials encountered in

widely spaced exploratory test borings. The contractor should verify that similar conditions exist throughout the proposed area of excavation.

As a safety measure, it is recommended that all vehicles and soil piles be kept to a lateral distance equal to at least the depth of the excavation from the crest of the slope. The exposed slope face should be protected against the elements and monitored by the contractor on at least a daily basis.

3.2 DRAINAGE CONSIDERATIONS

During construction, grade the site such that surface water can drain readily away from the pavement areas. Promptly pump out or otherwise remove water that accumulates in the excavations or on subgrade surfaces and allow these areas to dry before resuming construction. The use of berms, ditches, and similar means may be used to prevent stormwater from entering the work area and to convey water off site efficiently.

Limitations

The findings and recommendations presented in this memorandum are based upon data obtained from available information and previous studies, our understanding of the proposed construction, and other sources of information referenced in this memorandum. It is possible that subsurface conditions may vary between or beyond the locations explored. If subsurface conditions are encountered that vary from those described herein, we should be notified immediately so a review may be made, and any supplemental recommendations provided.

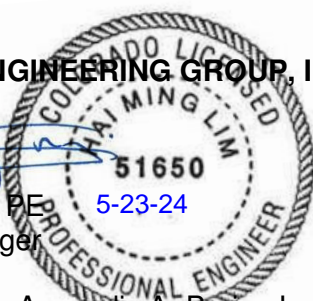
This memorandum was prepared in a manner consistent with that level of care and skill ordinarily exercised by other members of GEG's profession practicing in the same locality, under similar conditions and at the date the services are provided. GEG makes no other representation, guarantee, or warranty, express or implied, regarding the services, communication (oral or written), report, opinion, or instrument of service provided.

The scope of services for this geotechnical memorandum did not include environmental assessments or evaluations regarding the presence or absence of wetlands or hazardous substances in the soil, surface water, or groundwater.

This memorandum may be used only by the Client and the registered design professional in responsible charge and only for the purposes stated for this specific engagement within a reasonable time from its issuance, but in no event later than three years from the date of the report.

Respectfully,
GRANITE ENGINEERING GROUP, INC.


Hai Ming Lim PE
Project Manager

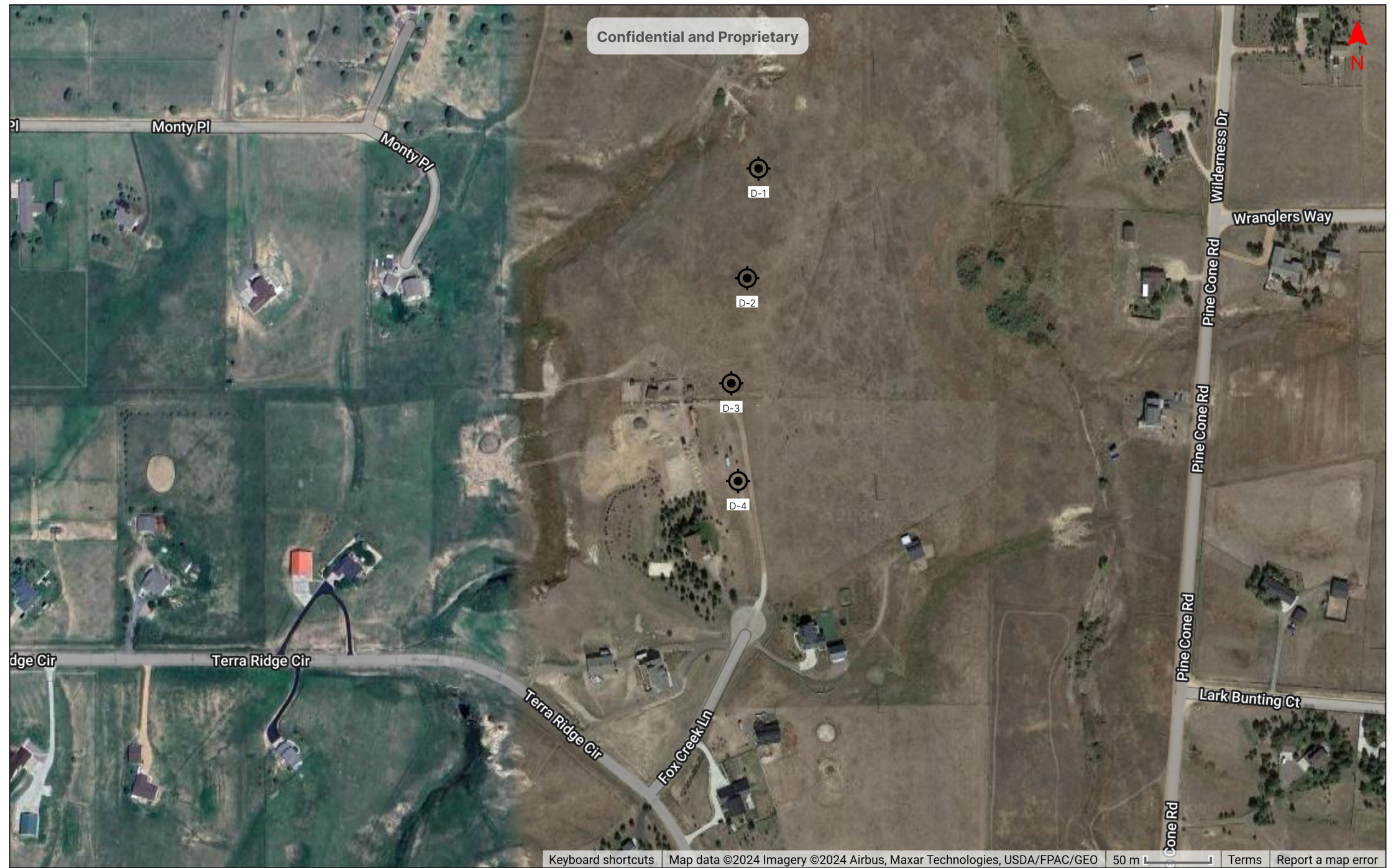


Attachment: Appendix A- Boring Location Plan
Appendix B- Boring Logs
Appendix C- Lab Results
Appendix D- Pavement Design Output

Appendix A

BORING LOCATION PLAN

Confidential and Proprietary



Keyboard shortcuts | Map data ©2024 Imagery ©2024 Airbus, Maxar Technologies, USDA/FPAC/Geo | 50 m | Terms | Report a map error



PREPARED BY

Granite Engineering Group
Colorado Springs, Colorado

PROJECT

Name: Terra Ridge North Pavement
Number: 24-041

LOCATION

39.05935, -104.69314
Colorado Springs, CO

SYMBOL KEY

 Soil Borings

Appendix B

BORING LOGS

Legend for Symbols Used on Borehole Logs

Sample Types



Bulk Sample of
auger/odex cuttings



Modified California
Sampler
(2.5 inch OD, 2.0
inch ID)

Lithology Symbols (see Boring Logs for complete descriptions)



USCS Low Plasticity
Clay



USCS Low Plasticity
Sandy Clay



Sandstone



USCS Clayey Sand



USCS Silty Sand

Lab Test Standards

| | |
|--|-------------------------------------|
| Moisture Content | ASTM D2216 |
| Dry Density | ASTM D7263 |
| Sand/Fines Content | ASTM D421, ASTM C136, ASTM D1140 |
| Atterberg Limits | ASTM D4318 |
| AASHTO Class. | AASHTO M145, ASTM D3282 |
| USCS Class. | ASTM D2487 |
| (Fines = % Passing #200 Sieve Sand = % Passing #4 Sieve, but not passing #200 Sieve) | |

Other Lab Test Abbreviations

| | |
|----------|--|
| pH | Soil pH (AASHTO T289-91) |
| S | Water-Soluble Sulfate Content (AASHTO T290-91, ASTM D4327) |
| Chl | Water-Soluble Chloride Content (AASHTO T291-91, ASTM D4327) |
| S/C | Swell/Consolidation (ASTM D4546) |
| UCCS | Unconfined Compressive Strength (ASTM D2166) |
| R-Value | Resistance R-Value (ASTM D2844) |
| DS (C) | Direct Shear cohesion (ASTM D3080) |
| DS (phi) | Direct Shear friction angle (ASTM D3080) |
| Re | Electrical Resistivity (AASHTO T288-91) |
| PtL | Point Load Strength Index (ASTM D5731) |

Notes

- "Penetration Resistance" on the Boring Logs refers to the uncorrected N value for SPT samples only, as per ASTM D1586. For samples obtained with a Modified California (MC) sampler, drive depth is 12 inches, and "Penetration Resistance" refers to the sum of all blows. Where blow counts were > 50 for the 3rd increment (SPT) or 2nd increment (MC), "Penetration Resistance" combines the last and 2nd-to-last blows and lengths; for other increments with > 50 blows, the blows for the last increment are reported.
- The Modified California sampler used to obtain samples is a 2.5-inch OD, 2.0-inch ID (1.95-inch ID with liners), split-barrel sampler with internal liners, as per ASTM D3550. Sampler is driven with a 140-pound hammer, dropped 30 inches per blow.
- "ER" for the hammer is the Reported Calibrated Energy Transfer Ratio for that specific hammer, as provided by the drilling company.



Project Name: Terra Ridge North Pavement
 Fox Creek Lane, Colorado Springs, CO
 Project Number: 24-041 Boring No.: D1

Boring Began: 3/12/2024
 Boring Completed: 3/12/2024
 Drilling Method(s): Hand Auger
 Driller:
 Drill Rig:
 Hammer Type: , ER: %

Total Depth: 4.0 ft
 Ground Elevation:
 Coordinates: Lat: 39.0617 Long: -104.69312
 Location:
 Logged By: J. Shekoski
 Final By: HML

Weather Notes: Mostly Sunny
 Inclination from Horiz.: Vertical
 Night Work:

| | | | |
|----------------------------------|---|---|---|
| Groundwater Levels: Not Observed | | | |
| Symbol | - | - | - |
| Depth | - | - | - |
| Date | - | - | - |

| Elevation (feet) | Depth (feet) | Sample Type/ Advancement Method | Soil Samples | | Lithology | Material Description | Moisture Content (%) | Dry Density (pcf) | Gravel Content (%) | Sand Content (%) | Fines Content (%) | Atterberg Limits | | AASHTO & USCS Classifications | Field Notes and Other Lab Tests |
|------------------|--------------|------------------------------------|----------------|------------------------|-----------|---|----------------------|-------------------|--------------------|------------------|-------------------|------------------|------------------|-------------------------------|---------------------------------|
| | | | Blows per 6 in | Penetration Resistance | | | | | | | | Liquid Limit | Plasticity Index | | |
| | | | | | | 0.0 - 0.2 ft. SILTY SAND, brown, low to no plasticity, dry. | | | | | | | | | |
| | | | | | | 0.2 - 0.3 ft. LEAN CLAY w/ SAND, brown, medium plasticity, moist, stiff. | | | | | | | | | |
| | | | | | | 0.3 - 1.3 ft. CLAYEY SAND, light yellowish brown, medium plasticity, moist, hard. | | | | | | | | | |
| | | | | | | 1.3 - 4.0 ft. CLAYEY SANDSTONE, SC, gray to white, low plasticity, dry. | 15.9 | 92.5 | | | | | | | S/C=0% @ 250 psf |
| | | | | | | | 17.8 | | 11 | 40 | 49.1 | 41 | 25 | A-7-6 (8) SC | |

Bottom of Hole at 4.0 ft.



Project Name: Terra Ridge North Pavement
 Fox Creek Lane, Colorado Springs, CO
 Project Number: 24-041 Boring No.: D2

Boring Began: 3/12/2024
 Boring Completed: 3/12/2024
 Drilling Method(s): Hand Auger
 Driller:
 Drill Rig:
 Hammer Type: , ER: %

Total Depth: 5.0 ft
 Ground Elevation:
 Coordinates: Lat: 39.06095 Long: -104.69322
 Location:
 Logged By: J. Shekoski
 Final By: HML

Weather Notes: Mostly Sunny
 Inclination from Horiz.: Vertical
 Night Work:

| | | | |
|----------------------------------|---|---|---|
| Groundwater Levels: Not Observed | | | |
| Symbol | - | - | - |
| Depth | - | - | - |
| Date | - | - | - |

| Elevation (feet) | Depth (feet) | Sample Type/ Advancement Method | Soil Samples | | Lithology | Material Description | Moisture Content (%) | Dry Density (pcf) | Fines Content (%) | Atterberg Limits | | AASHTO & USCS Classifications | Field Notes and Other Lab Tests |
|------------------|--------------|------------------------------------|----------------|------------------------|-----------|---|----------------------|-------------------|-------------------|------------------|------------------|-------------------------------|---------------------------------|
| | | | Blows per 6 in | Penetration Resistance | | | | | | Liquid Limit | Plasticity Index | | |
| | | | | | | 0.0 - 0.1 ft. CLAYEY SAND, brown, low to no plasticity, dry, organics observed. | | | | | | | |
| | | | | | | 0.1 - 5.0 ft. SILTY SAND, brown, medium plasticity, moist, stiff. | | | | | | | |

Bottom of Hole at 5.0 ft.



Project Name: Terra Ridge North Pavement
 Fox Creek Lane, Colorado Springs, CO
 Project Number: 24-041 Boring No.: D3

Boring Began: 3/12/2024 Total Depth: 4.5 ft Weather Notes: Mostly Sunny
 Boring Completed: 3/12/2024 Ground Elevation: Inclination from Horiz.: Vertical
 Drilling Method(s): Hand Auger Coordinates: Lat: 39.06023 Long: -104.69336
 Driller: Location: Night Work:
 Drill Rig: Hammer Type: , ER: % Logged By: J. Shekoski
 Final By: HML

| Groundwater Levels: Not Observed | | | |
|----------------------------------|-------|------|---|
| Symbol | Depth | Date | |
| - | - | - | - |
| - | - | - | - |

| Elevation (feet) | Depth (feet) | Sample Type/ Advancement Method | Soil Samples | | Lithology | Material Description | Moisture Content (%) | Dry Density (pcf) | Gravel Content (%) | Sand Content (%) | Fines Content (%) | Atterberg Limits | | AASHTO & USCS Classifications | Field Notes and Other Lab Tests |
|---------------------------|--------------|------------------------------------|----------------|------------------------|-----------|--|----------------------|-------------------|--------------------|------------------|-------------------|------------------|------------------|-------------------------------|---------------------------------|
| | | | Blows per 6 in | Penetration Resistance | | | | | | | | Liquid Limit | Plasticity Index | | |
| | | | | | | | | | | | | | | | |
| | | | | | | 0.0 - 4.5 ft. SANDY LEAN CLAYfill. RAP and organics observed at 4'. CL, brown, low plasticity, dry to moist. | 12.2 | 112.3 | | | | | | | S/C=0.5% @ 250 psf |
| | | | | | | | 11.2 | | 1 | 38 | 60.5 | 32 | 15 | A-6 (6) CL | |
| Bottom of Hole at 4.5 ft. | | | | | | | | | | | | | | | |

BORING LOG 24-041 TERRA RIDGE BORELOGS.GPJ GEG BORING LOGS TEMPLATE.GDT GEG LIBRARY 9-3-21.GLB 5/23/24



Project Name: Terra Ridge North Pavement
 Fox Creek Lane, Colorado Springs, CO
 Project Number: 24-041 Boring No.: D4

Boring Began: 3/12/2024 Total Depth: 2.7 ft Weather Notes: Mostly Sunny
 Boring Completed: 3/12/2024 Ground Elevation: Inclination from Horiz.: Vertical
 Drilling Method(s): Hand Auger Coordinates: Lat: 39.05956 Long: -104.6933
 Driller: Location: Night Work:
 Drill Rig: Groundwater Levels: Not Observed
 Hammer Type: , ER: % Logged By: J. Shekoski
 Final By: HML

| Groundwater Levels: Not Observed | | | |
|----------------------------------|-------|------|---|
| Symbol | Depth | Date | |
| - | - | - | - |
| - | - | - | - |

| Elevation (feet) | Depth (feet) | Sample Type/ Advancement Method | Soil Samples | | Lithology | Material Description | Moisture Content (%) | Dry Density (pcf) | Gravel Content (%) | Sand Content (%) | Fines Content (%) | Atterberg Limits | | AASHTO & USCS Classifications | Field Notes and Other Lab Tests |
|---------------------------|--------------|------------------------------------|----------------|------------------------|-----------|---|----------------------|-------------------|--------------------|------------------|-------------------|------------------|------------------|-------------------------------|---------------------------------|
| | | | Blows per 6 in | Penetration Resistance | | | | | | | | Liquid Limit | Plasticity Index | | |
| | | | | | | 0.0 - 2.0 ft. LEAN CLAY w/ SAND, CL, brown, low to no plasticity, dry. | 14.3 | | 1 | 27 | 71.9 | 42 | 28 | A-7-6 (18) CL | S/C=-0.3% @ 250 psf |
| | | | | | | 2.0 - 2.6 ft. SILTY SAND, brown, medium plasticity, moist, stiff. | 11.7 | 88.2 | | | | | | | |
| | | | | | | 2.6 - 2.7 ft. SILTY SANDSTONE coarse grained, gray to white, no plasticity, dry, auger refusal. | | | | | | | | | |
| Bottom of Hole at 2.7 ft. | | | | | | | | | | | | | | | |

DCP TEST DATA

Test#: D1 39.06170, -104.69312

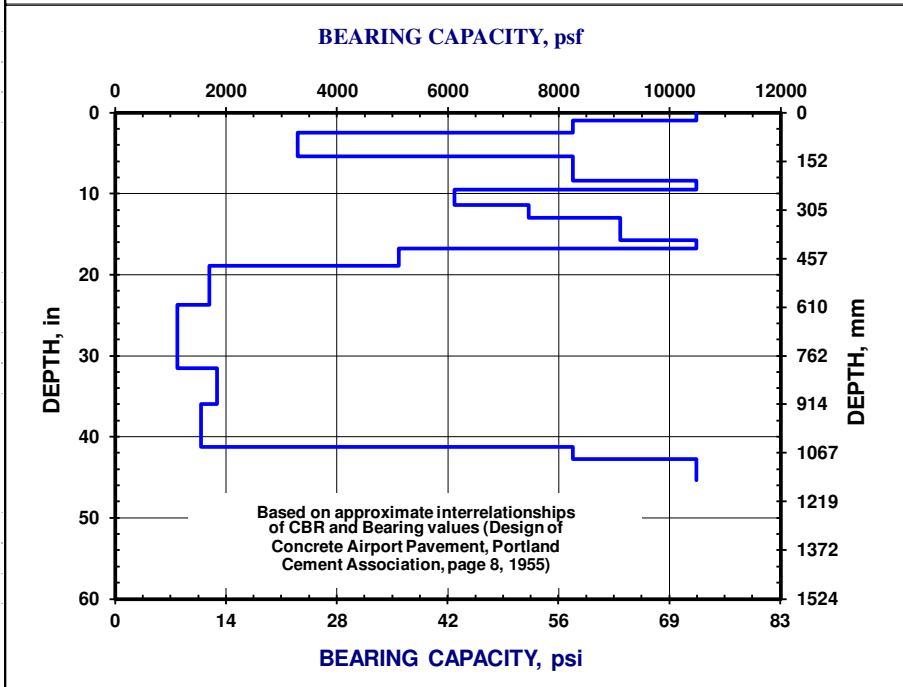
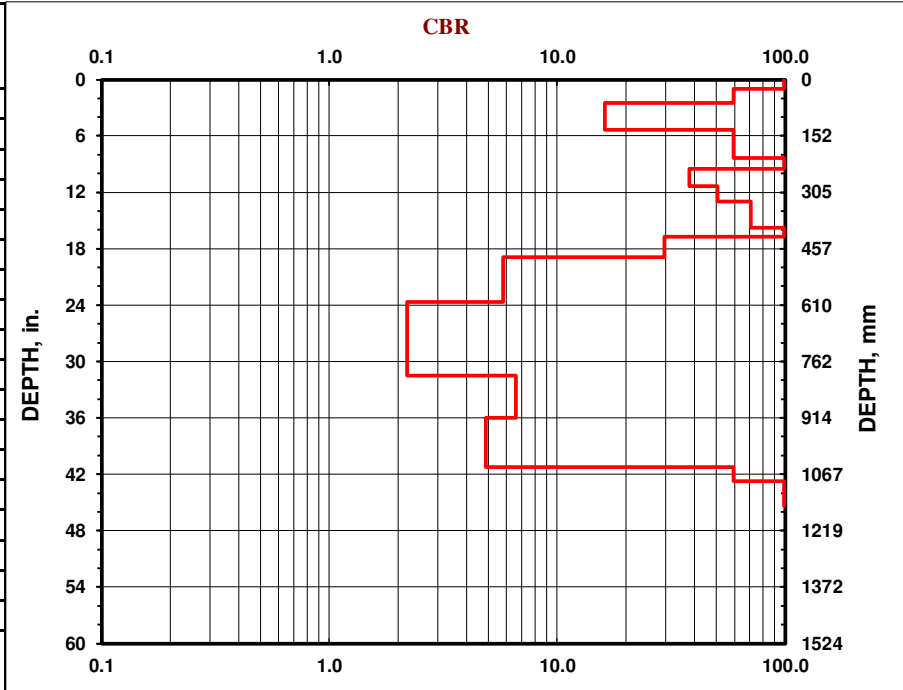
Project: Terra Ridge North Pavement
Location: Black Forest, CO

Date: 12-Mar-24
Soil Type(s): Low plasticity Clay with CBR<10

Hammer
 10.1 lbs.
 17.6 lbs.
 Both hammers used

Soil Type
 CH
 CL
 All other soils

| No. of Blows | Accumulative Penetration (mm) | Type of Hammer |
|--------------|-------------------------------|----------------|
| 0 | 0 | 1 |
| 5 | 25.4 | 1 |
| 5 | 63.5 | 1 |
| 5 | 136.525 | 1 |
| 5 | 174.625 | 1 |
| 5 | 212.725 | 1 |
| 5 | 241.3 | 1 |
| 5 | 288.925 | 1 |
| 5 | 330.2 | 1 |
| 5 | 365.125 | 1 |
| 5 | 400.05 | 1 |
| 5 | 425.45 | 1 |
| 5 | 479.425 | 1 |
| 5 | 601.6625 | 1 |
| 5 | 800.1 | 1 |
| 5 | 914.4 | 1 |
| 5 | 1047.75 | 1 |
| 5 | 1085.85 | 1 |
| 5 | 1103.3125 | 1 |
| 5 | 1120.775 | 1 |
| 5 | 1130.3 | 1 |
| 5 | 1146.175 | 1 |
| 5 | 1152.525 | 1 |

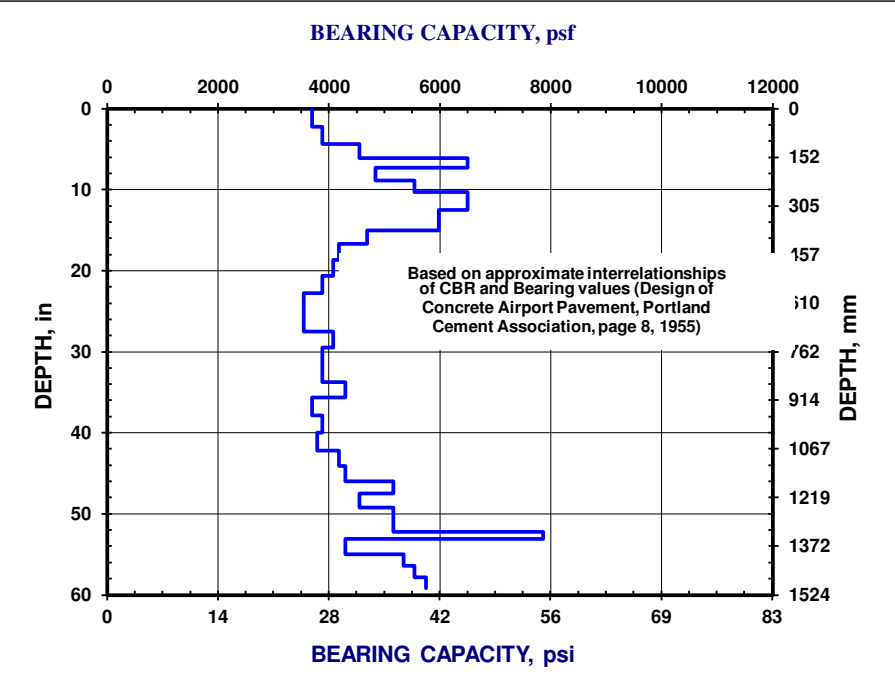
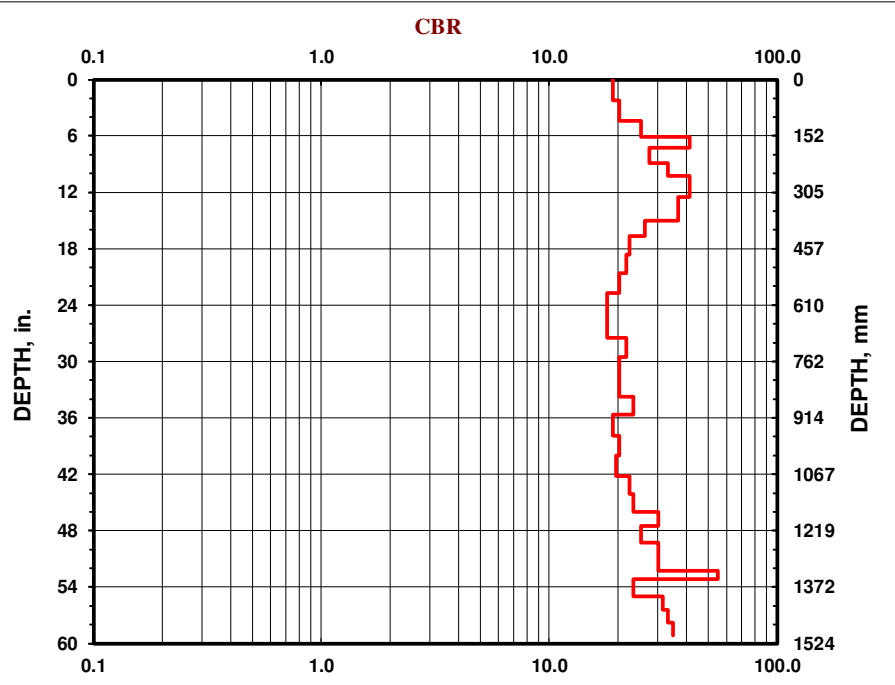


DCP TEST DATA

Test#: D2 39.06095, -104.69322

| | |
|--|---|
| Project: <u>Terra Ridge North Pavement</u> Location: <u>Black Forest, CO</u> | Date: <u>12-Mar-24</u> Soil Type(s): <u>Type in the soil type</u> |
| Hammer <input type="radio"/> 10.1 lbs. <input checked="" type="radio"/> 17.6 lbs. <input type="radio"/> Both hammers used | Soil Type <input type="radio"/> CH <input type="radio"/> CL <input checked="" type="radio"/> All other soils |

| No. of Blows | Accumulative Penetration (mm) | Type of Hammer |
|--------------|-------------------------------|----------------|
| 0 | 0 | 1 |
| 5 | 57.15 | 1 |
| 5 | 111.125 | 1 |
| 5 | 155.575 | 1 |
| 5 | 184.15 | 1 |
| 5 | 225.425 | 1 |
| 5 | 260.35 | 1 |
| 5 | 288.925 | 1 |
| 5 | 317.5 | 1 |
| 5 | 349.25 | 1 |
| 5 | 381 | 1 |
| 5 | 423.8625 | 1 |
| 5 | 473.075 | 1 |
| 5 | 523.875 | 1 |
| 5 | 577.85 | 1 |
| 5 | 638.175 | 1 |
| 5 | 698.5 | 1 |
| 5 | 749.3 | 1 |
| 5 | 803.275 | 1 |
| 5 | 857.25 | 1 |
| 5 | 904.875 | 1 |
| 5 | 962.025 | 1 |
| 5 | 1016 | 1 |
| 5 | 1071.5625 | 1 |
| 5 | 1120.775 | 1 |
| 5 | 1168.4 | 1 |
| 5 | 1206.5 | 1 |
| 5 | 1250.95 | 1 |
| 5 | 1289.05 | 1 |
| 5 | 1327.15 | 1 |
| 5 | 1349.375 | 1 |
| 5 | 1397 | 1 |
| 5 | 1433.5125 | 1 |
| 5 | 1468.4375 | 1 |
| 5 | 1501.775 | 1 |
| | | |
| | | |
| | | |
| | | |
| | | |



DCP TEST DATA

Test#: D3 39.06023, -104.69336

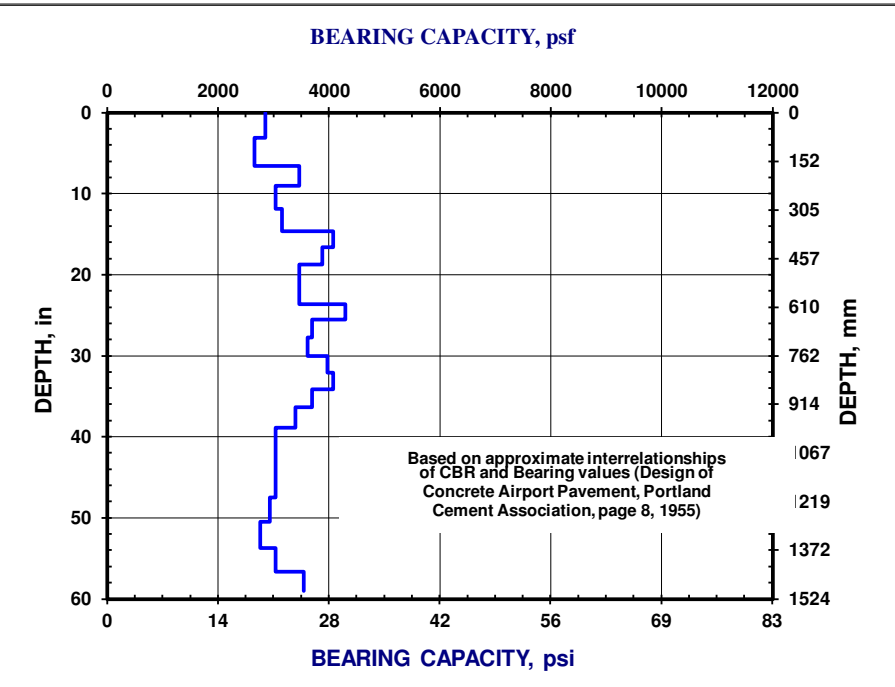
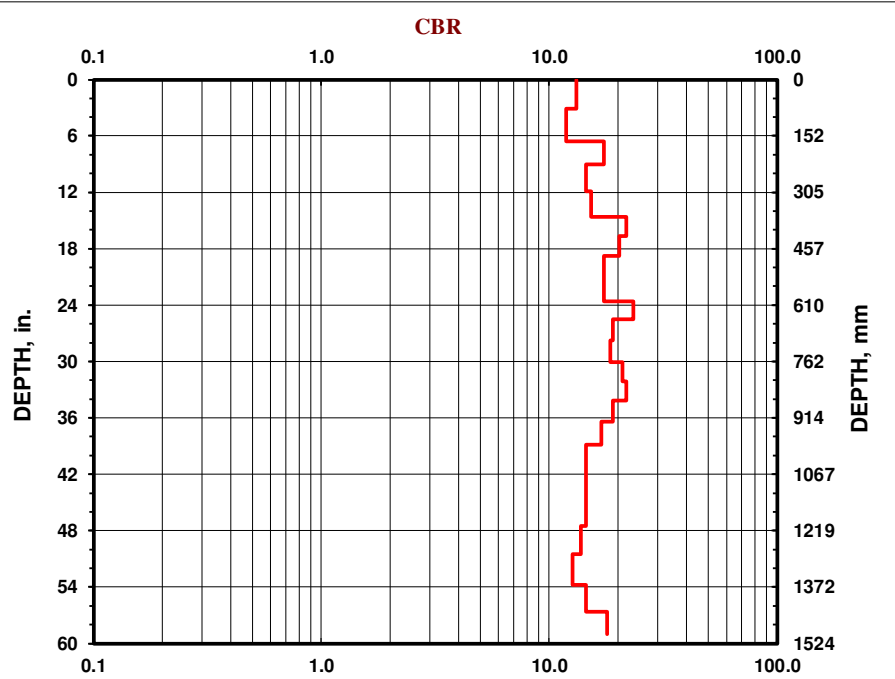
Project: Terra Ridge North Pavement
 Location: Black Forest, CO

Date: 12-Mar-24
 Soil Type(s): Type in the soil type

Hammer
 10.1 lbs.
 17.6 lbs.
 Both hammers used

Soil Type
 CH
 CL
 All other soils

| No. of Blows | Accumulative Penetration (mm) | Type of Hammer |
|--------------|-------------------------------|----------------|
| 0 | 0 | 1 |
| 5 | 79.375 | 1 |
| 5 | 166.6875 | 1 |
| 5 | 228.6 | 1 |
| 5 | 301.625 | 1 |
| 5 | 371.475 | 1 |
| 5 | 422.275 | 1 |
| 5 | 476.25 | 1 |
| 5 | 538.1625 | 1 |
| 5 | 600.075 | 1 |
| 5 | 647.7 | 1 |
| 5 | 704.85 | 1 |
| 5 | 763.5875 | 1 |
| 5 | 815.975 | 1 |
| 5 | 866.775 | 1 |
| 5 | 923.925 | 1 |
| 5 | 987.425 | 1 |
| 5 | 1060.45 | 1 |
| 5 | 1133.475 | 1 |
| 5 | 1206.5 | 1 |
| 5 | 1282.7 | 1 |
| 5 | 1365.25 | 1 |
| 5 | 1438.275 | 1 |
| 5 | 1498.6 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |
| 5 | 0 | 1 |



DCP TEST DATA

Test#: D4 39.05956, -104.69330

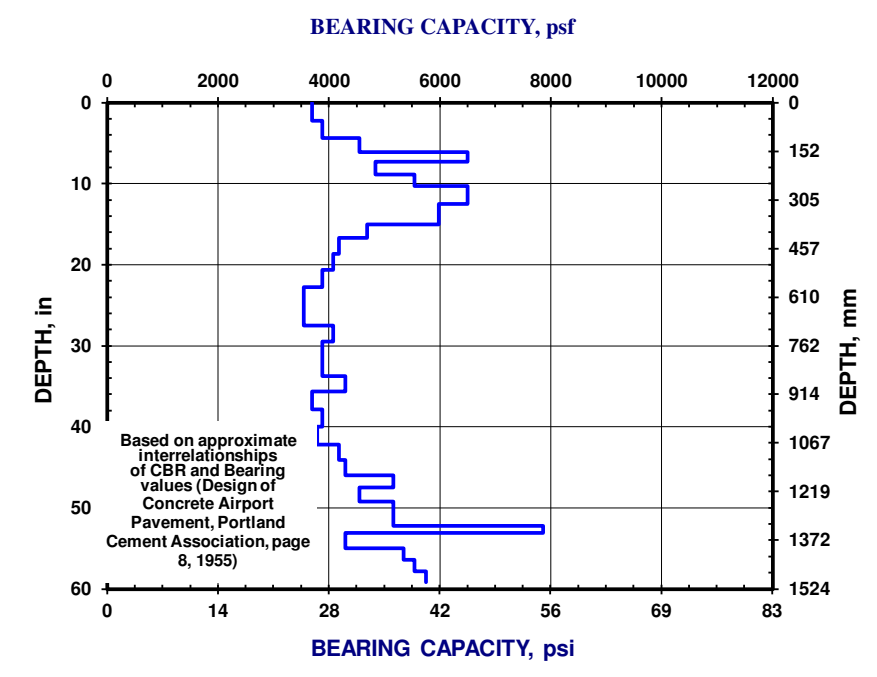
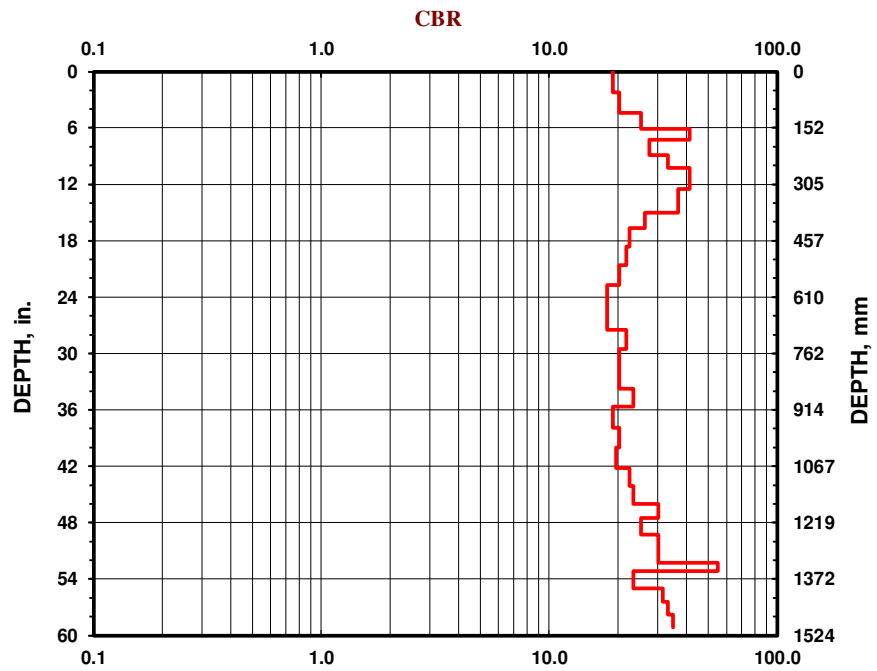
Project: Terra Ridge North Pavement
Location: Black Forest, CO

Date: 12-Mar-24
Soil Type(s): Type in the soil type

Hammer
○ 10.1 lbs.
● 17.6 lbs.
○ Both hammers used

Soil Type
○ CH
○ CL
● All other soils

| No. of Blows | Accumulative Penetration (mm) | Type of Hammer |
|--------------|-------------------------------|----------------|
| 0 | 0 | 1 |
| 5 | 57.15 | 1 |
| 5 | 111.125 | 1 |
| 5 | 155.575 | 1 |
| 5 | 184.15 | 1 |
| 5 | 225.425 | 1 |
| 5 | 260.35 | 1 |
| 5 | 288.925 | 1 |
| 5 | 317.5 | 1 |
| 5 | 349.25 | 1 |
| 5 | 381 | 1 |
| 5 | 423.8625 | 1 |
| 5 | 473.075 | 1 |
| 5 | 523.875 | 1 |
| 5 | 577.85 | 1 |
| 5 | 638.175 | 1 |
| 5 | 698.5 | 1 |
| 5 | 749.3 | 1 |
| 5 | 803.275 | 1 |
| 5 | 857.25 | 1 |
| 5 | 904.875 | 1 |
| 5 | 962.025 | 1 |
| 5 | 1016 | 1 |
| 5 | 1071.5625 | 1 |
| 5 | 1120.775 | 1 |
| 5 | 1168.4 | 1 |
| 5 | 1206.5 | 1 |
| 5 | 1250.95 | 1 |
| 5 | 1289.05 | 1 |
| 5 | 1327.15 | 1 |
| 5 | 1349.375 | 1 |
| 5 | 1397 | 1 |
| 5 | 1433.5125 | 1 |
| 5 | 1468.4375 | 1 |
| 5 | 1501.775 | 1 |
| | | |
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Appendix C

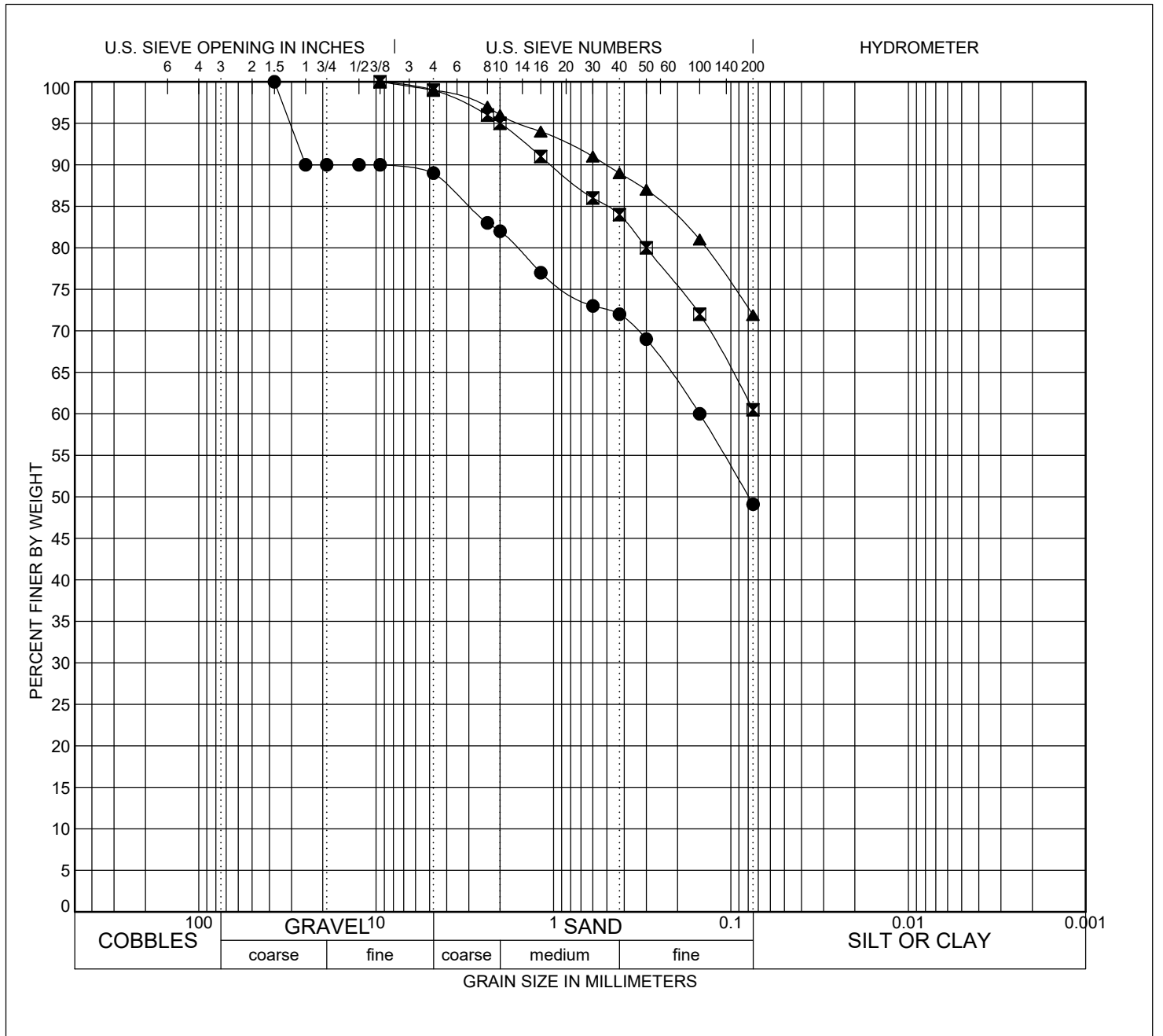
LAB RESULTS

Summary of Laboratory Test Results




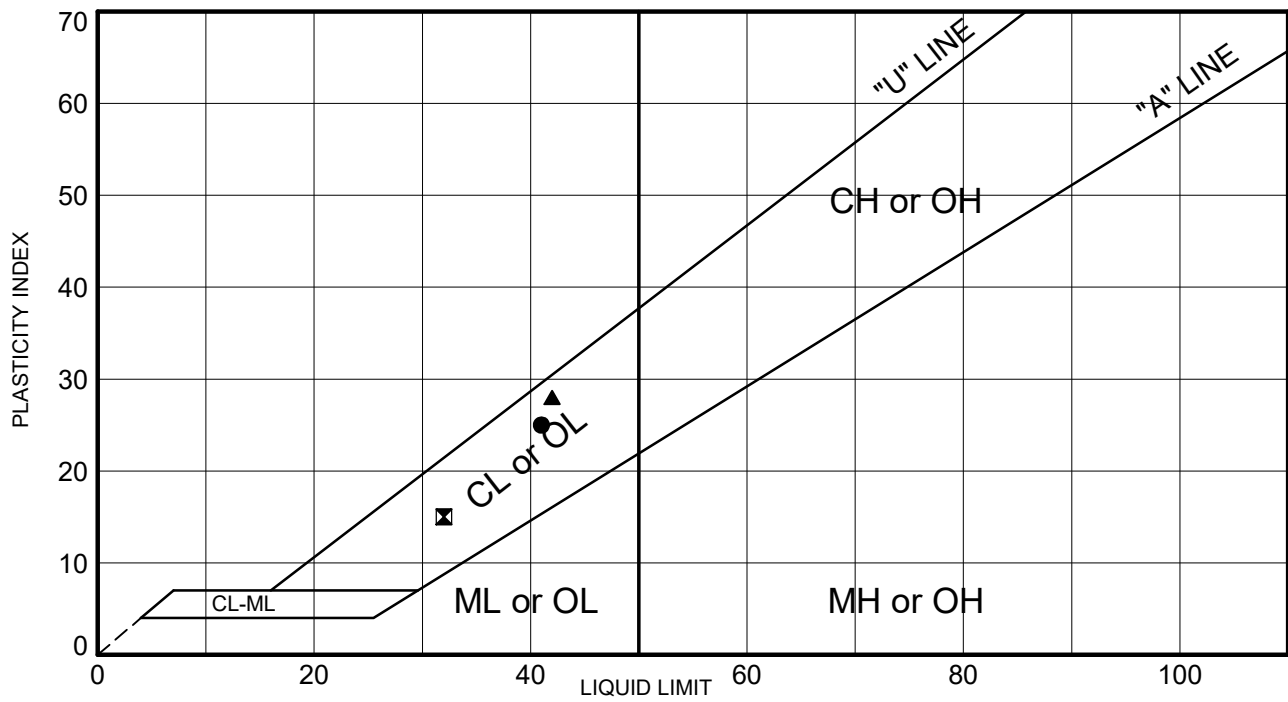
Project No: 24-041 Project Name: Terra Ridge North Pavement, Fox Creek Lane, Colorado Springs, CO

| Sample Location | | | Natural Moisture Content (%) | Natural Dry Density (pcf) | Gradation | | | Atterberg | | | pH | Water Soluble Sulfate (%) | % Swell (+) / Consolidation (-) | Unconf. Comp. Strength (psf) | R-Value | Classification | |
|-----------------|------------|-------------|------------------------------|---------------------------|-----------------|----------|------------------|-----------|----|----|----|---------------------------|---------------------------------|------------------------------|-----------|----------------|------|
| Boring No. | Depth (ft) | Sample Type | | | Gravel > #4 (%) | Sand (%) | Fines < #200 (%) | LL | PL | PI | | | | | | AASHTO | USCS |
| D1 | 1.3~1.8 | MC | 15.9 | 92.5 | | | | | | | | 0.0% @ 250 psf | | -- | -- | -- | |
| D1 | 3.5~4.0 | BULK | 17.8 | | 11.0 | 39.9 | 49.1 | 41 | 16 | 25 | | | | | A-7-6(8) | SC | |
| D1 | 6.0~ | AUGER | | | | | | | | | | | | | -- | -- | |
| D3 | 0.0~4.5 | BULK | 11.2 | | 1.0 | 38.5 | 60.5 | 32 | 17 | 15 | | | | | A-6(6) | CL | |
| D3 | 1.0~1.5 | MC | 12.2 | 112.3 | | | | | | | | 0.5% @ 250 psf | | -- | -- | -- | |
| D4 | 0.0~2.0 | BULK | 14.3 | | 1.0 | 27.1 | 71.9 | 42 | 14 | 28 | | | | | A-7-6(18) | CL | |
| D4 | 1.0~1.5 | MC | 11.7 | 88.2 | | | | | | | | -0.3% @ 250 psf | | -- | -- | -- | |



| BOREHOLE | DEPTH | AASHTO Classification | USCS Classification | LL | PL | PI | %Gravel | %Sand | %Fines | |
|----------|-------|-----------------------|---------------------|----|----|----|---------|-------|--------|-------|
| | | | | | | | | | %Silt | %Clay |
| ● D1 | 3.5 | A-7-6(8) | SC | 41 | 16 | 25 | 11.0 | 39.9 | 49.1 | |
| ☒ D3 | 0.0 | A-6(6) | CL | 32 | 17 | 15 | 1.0 | 38.5 | 60.5 | |
| ▲ D4 | 0.0 | A-7-6(18) | CL | 42 | 14 | 28 | 1.0 | 27.1 | 71.9 | |
| | | | | | | | | | | |
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|---|-----------------|--|-------------------------|-----------------|
|  | | | <h2>SIEVE ANALYSIS</h2> | <h2>FIGURE</h2> |
| Project No. 24-041 | Date: 5/23/2024 | Terra Ridge North Pavement Fox Creek Lane, Colorado Springs, CO | | <h2>C-1</h2> |
| Drawn By: EC | | | | |
| Checked By: HML | | | | |



| BOREHOLE | DEPTH | LL | PL | PI | Passing #200 | USCS Sample Description | AASHTO Class. |
|----------|-------|----|----|----|--------------|-------------------------|---------------|
| ● D1 | 3.5 | 41 | 16 | 25 | 49 | CLAYEY SAND(SC) | A-7-6(8) |
| ☒ D3 | 0.0 | 32 | 17 | 15 | 61 | SANDY LEAN CLAY(CL) | A-6(6) |
| ▲ D4 | 0.0 | 42 | 14 | 28 | 72 | LEAN CLAY with SAND(CL) | A-7-6(18) |
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ATTERBERG LIMITS

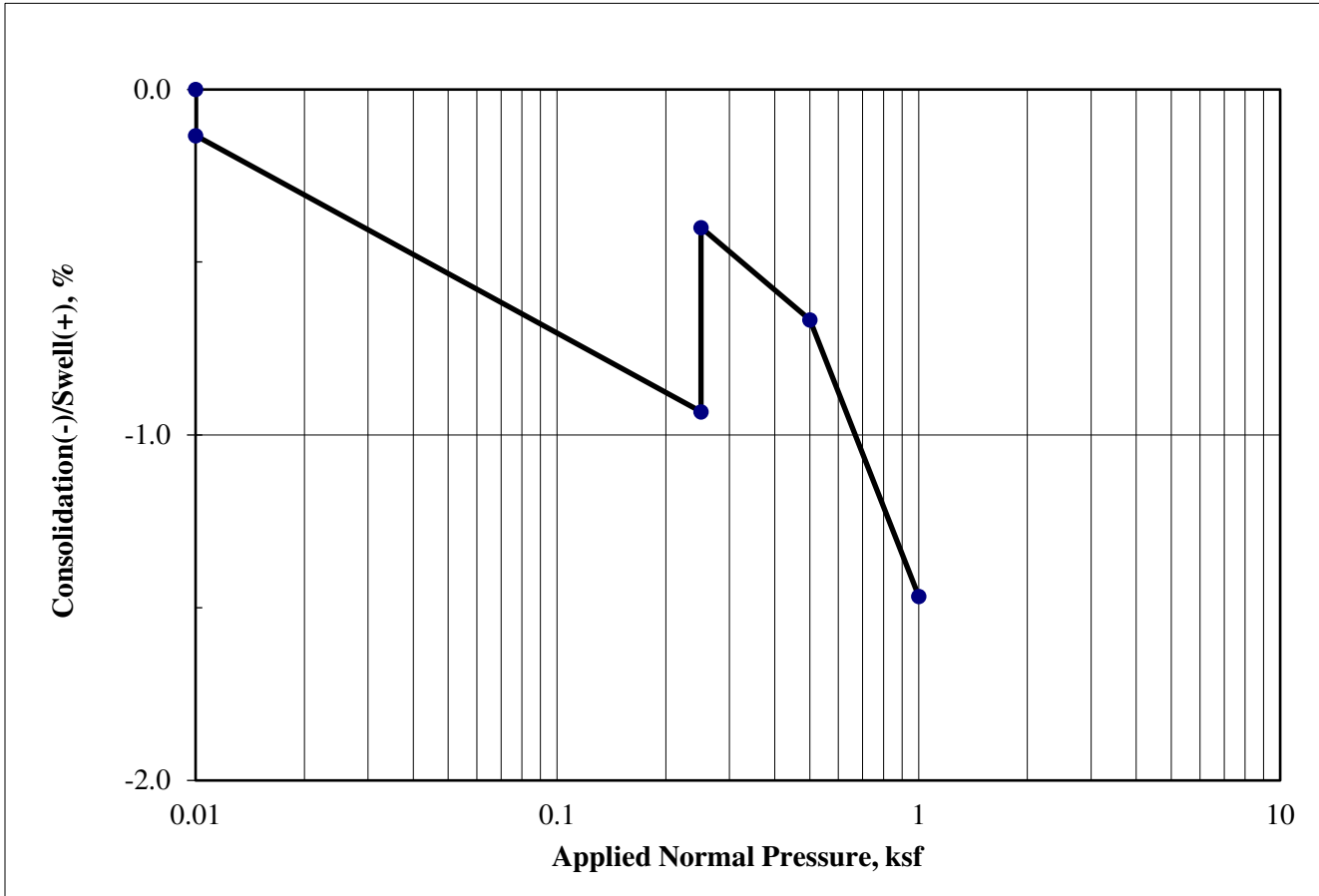
FIGURE

Project No. 24-041 Date: 5/23/2024
 Drawn By: EC
 Checked By: HML

Terra Ridge North Pavement
 Fox Creek Lane, Colorado
 Springs, CO

C - 2

SWELL/CONSOLIDATION TEST - ASTM D 4546



| | |
|--------------------------|-----------|
| Boring ID | D-1 @ |
| Sample Depth (ft) | 1.3' |
| Date Sampled | 3/12/2024 |

| | |
|---------------------------------------|-------|
| Swell/ Consolidation (%) | 0.5 |
| Natural Moisture Content (%) | 12.2 |
| Saturated Moisture Content (%) | 19.4 |
| Dry Density (pcf) | 112.3 |



**SWELL/ CONSOLIDATION
TEST RESULTS**

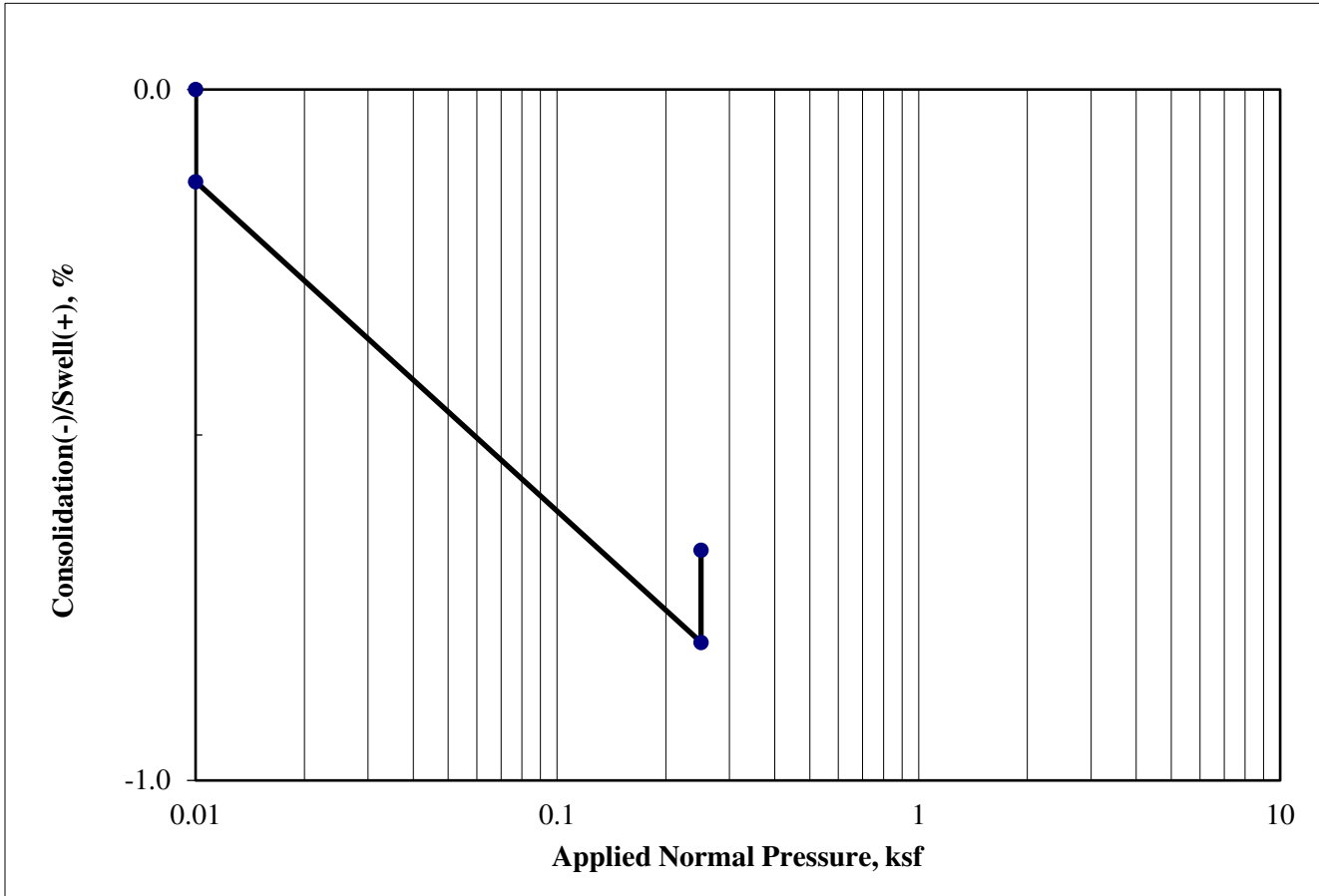
FIGURE

Project No. 24-041 Date: 3/12/2024
 Report By: JLS
 Checked By: HML

Terra Ridge North
 Black Forest, CO


C-1

SWELL/CONSOLIDATION TEST - ASTM D 4546

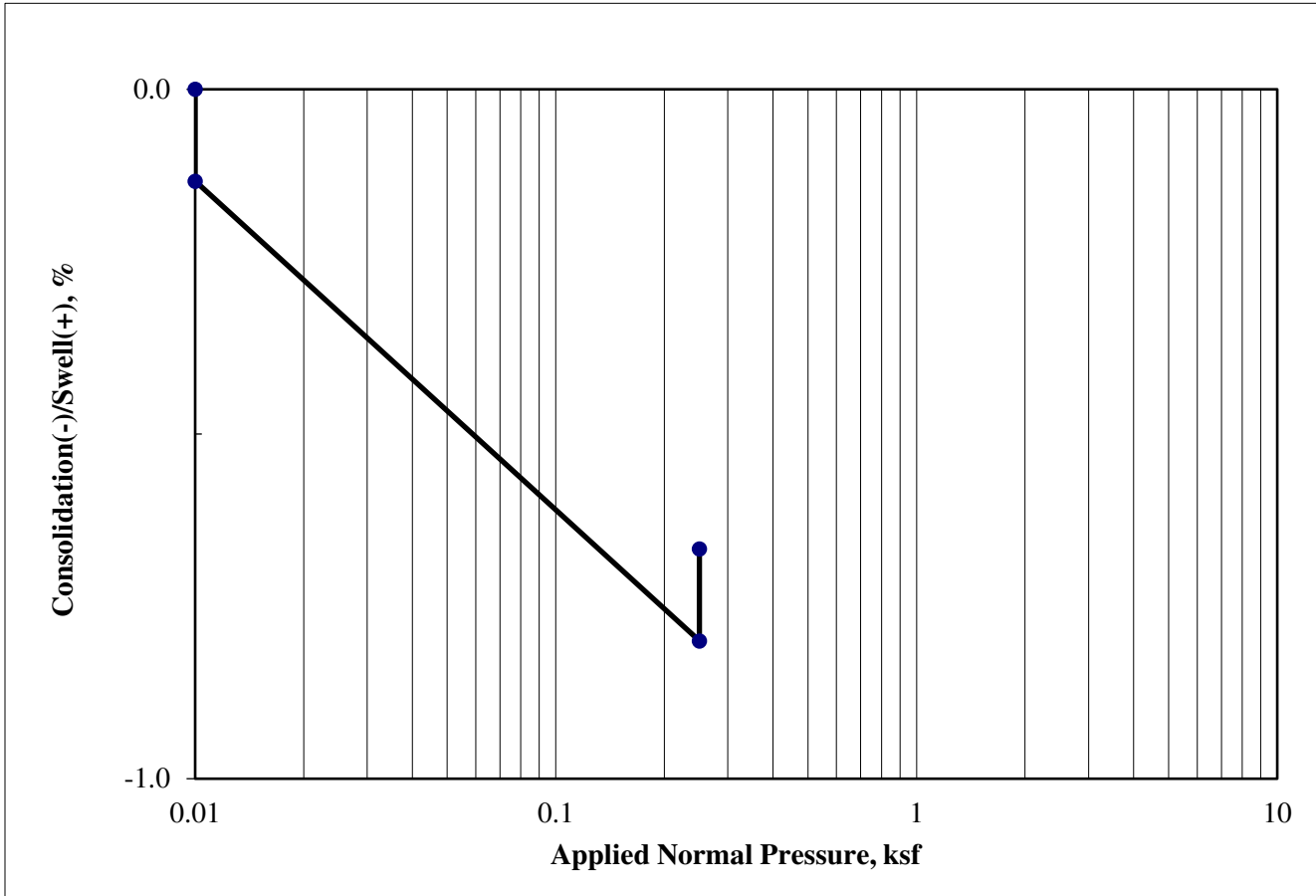


| | |
|--------------------------|----------|
| Boring ID | P-2 |
| Sample Depth (ft) | 4' |
| Date Sampled | 1/9/2024 |

| | |
|---------------------------------------|-------|
| Swell/ Consolidation (%) | 0.1 |
| Natural Moisture Content (%) | 11.7 |
| Saturated Moisture Content (%) | 17.3 |
| Dry Density (pcf) | 115.8 |

| | | |
|---|--|---------------|
|  GEG <small>GRANITE ENGINEERING GROUP</small> | SWELL/ CONSOLIDATION TEST RESULTS | FIGURE |
| Project No. 24-041 Date: 3/12/2024 Report By: JLS Checked By: HML | Terra Ridge North Black Forest, CO | C-2 |

SWELL/CONSOLIDATION TEST - ASTM D 4546



| | |
|--------------------------|----------|
| Boring ID | P-2 |
| Sample Depth (ft) | 4' |
| Date Sampled | 1/9/2024 |

| | |
|---------------------------------------|-------|
| Swell/ Consolidation (%) | 0.1 |
| Natural Moisture Content (%) | 11.7 |
| Saturated Moisture Content (%) | 17.3 |
| Dry Density (pcf) | 115.8 |



**SWELL/ CONSOLIDATION
TEST RESULTS**

FIGURE

Project No. 24-041 Date: 3/12/2024
 Report By: JLS
 Checked By: HML

Terra Ridge North
 Black Forest, CO

C-3

Appendix D

PAVEMENT DESIGN OUTPUT

WinPAS

Pavement Thickness Design According to
1993 AASHTO Guide for Design of Pavements Structures
American Concrete Pavement Association

Flexible Design Inputs

Project Name:
Route:
Location:
Owner/Agency:
Design Engineer:

Flexible Pavement Design/Evaluation

| | | | |
|-----------------------------------|---------------|-----------------------------------|--------------|
| Structural Number | 2.64 | Subgrade Resilient Modulus | 4,500.00 psi |
| Total Flexible ESALs | 36,500 | Initial Serviceability | 4.50 |
| Reliability | 75.00 percent | Terminal Serviceability | 2.50 |
| Overall Standard Deviation | 0.45 | | |

Layer Pavement Design/Evaluation

| Layer Material | Layer Coefficient | Drainage Coefficient | Layer Thickness | Layer SN |
|-------------------------|-------------------|----------------------|-----------------|----------|
| Asphalt Cement Concrete | 0.44 | 1.00 | 4.50 | 1.98 |
| Graded Stone Base | 0.11 | 1.00 | 6.00 | 0.66 |
| | | | Σ SN | 2.64 |