Project No. 24-041



March 25, 2024

Mr. Shay Miles, PE Lodestar Engineering, LLC PB Box 88461 Colorado Springs, CO 80908

Subject: Memorandum for Pavement Thickness Design Fox Creek Lane Extension at Terra Ridge North Black Forest, El Paso County, Colorado

Dear Mr. Miles,

Granite Engineering Group, Inc. (GEG) has completed the engineering evaluation and prepare this memorandum to address the pavement thickness design for the Fox Creek Lane extension at the Terra Ridge North Community in El Paso County, Colorado.

Project Background

Based on the information provided to us, it is our understanding that the development consists of 13 new custom-home lots accessed via an approximate 1000' extension of Fox Creek Lane. The existing Fox Creek Lane is paved with Hot Mix Asphalt (HMA). At the time of exploration, the roadway extension was a graded, soil roadway and will be paved with HMA in the near future. Light gravel had been placed at the southern end of the extension.

It is our understanding that the proposed roadway will be a lightly trafficked, residential 2-way street consisting of HMA

1 FIELD EXPLORATION AND LABORATORY TESTING

A total of four (4) borings were performed at the approximate locations as shown in the Boring Location Plan. These borings were performed at approximately 250 feet spacing along the graded roadway extension. These borings were explored with hand auger to approximately 5 feet below existing ground surface (bgs) or hand auger refusal, whichever occurred first. Drive samples with hand driver were obtained in Borings D-1, D-3 and D-4. The strength of the existing subgrade was evaluated using Dynamic Cone Penetration (DCP) tests.

The samples were tested for soil classification and swell-consolidation tests. The boring logs and the laboratory test results are presented in Appendix B and C, respectively.

2 PAVEMENT THICKNESS RECOMMENDATIONS

The pavement thickness design was performed in accordance with El Paso County Engineering Criteria Manual.

2.1 SUBGRADE STRENGTH

Based on the results of the DCP and field exploration, a resilient modulus (Mr) value of 4,500 psi was used for the prepared subgrade along the new extension for the pavement thickness design.

2.2 TRAFFIC LOADING

Traffic information was not available at the time of writing this report. We estimate that the pavement will subject to 500 vehicles, 20 delivery trucks, and 2 trach or trailer truck per day. An ESAL of 31,620 was estimated based on the estimated traffic. The El Paso County Engineering Criteria Manual has a minimum ESAL of 36,500 for Local Road in Rural area, and it was used for the pavement thickness design.

2.3 PAVEMENT THICKNESS DESIGN

Pavement thickness design was performed using the WinPAS Version 12. The designs was performed in accordance with the 1993 AASHTO Pavement Design Guide and El Paso County Engineering Criteria Manual. Tables 1-1 and 1-2 present a summary of the design input parameters.

Parameter	Value
Design Period (year)	20
18-kip ESAL over design period	36,500 for flexible
Reliability (%)	75
Overall Standard Deviation	0.44 for flexible
Initial Serviceability Index	4.5
Terminal Serviceability Index	2.5

Table 1-1. Pavement Design Parameters

Table 1-2. Pavement Design Strength Coefficients

Parameter	Value
New Hot Mix Asphalt (HMA) Layer Coefficient	0.44
Drainage Coefficient	1.0
Aggregate Base Course (ABC) ¹ Layer Coefficient	0.11
Subgrade Soil Resilient Modulus (psi)	4,500

¹ ABC meeting El Paso County Engineering Criteria Manual

Based on the above design parameters, the recommended reconstruction sections for flexible pavements are presented in Table 1-3.

Table 1-3. Recommended Minimum Pavement Sections

Pavement Reconstruction	HMA Pavement Section
Fox Creek Lane Extension	-4.5 inches HMA -6.0 inches ABC -Subgrade ¹

PCC= Portland cement concrete HMA= Hot mixed asphalt

¹ Subgrade should be prepared in accordance with Section 3 of the report.

2.4 PAVEMENT MATERIALS

2.4.1 Base Course

We recommend CDOT Coarse Aggregate Type Class 5 or 6 to be used for the aggregate base materials. The material should be placed in a uniform layer without segregation of size and compacted in loose lifts not to exceed 8-inches.

2.4.2 Hot Mix Asphalt

Hot mix asphalt materials, placement procedures, and testing should follow The Pike Peak Region Asphalt Specification. We recommend PG 58-28 HMA binder with Grading S or SX aggregate, and gyration of 75.

3. CONSTRUCTION RECOMMENDATIONS

3.1 SUBGRADE PREPARATION AND EARTHWORK

3.1.1 Site Preparation

Site preparation should begin by stripping and removal of vegetation, existing structures, and other deleterious materials. Clearing and Grubbing operations and removal of existing structure should be performed in accordance with Sections 201 and 202 of CDOT Standard Specifications for Road and Bridge Construction, 2022 (CDOT 2022) respectively. All exposed surfaces should be free of mounds and depressions, which may prevent uniform compaction. Stripped materials consisting of vegetation and organic materials should be removed from the site or be used to re-vegetate landscaped areas and exposed slopes after completion of grading operations. The site should be initially graded to create an appropriate surface to receive fill. All exposed areas which will receive fill, once properly cleared and benched, should be scarified to a minimum depth of 12 inches, moisture conditioned and recompacted in accordance with Section 4.2.4 of this report. Based upon the subsurface conditions encountered, subgrade soils exposed during construction are anticipated to be relatively stable. However, the stability of the subgrade may be affected by drainage and precipitation. If unstable conditions are encountered or develop during construction, stability may be improved by scarifying and drying the subgrade soils or with other ground improvement techniques. A typical stabilization method may include utilizing gravel with the combination of geo-grid (e.g. Tensar NX650) to create a stable base. Other stabilization methods may also be appropriate.

3.1.2 Fill Materials and Subgrade Preparation

Following initial excavation and subgrade preparation in the construction areas, visual inspection and proof rolling of the exposed subgrade is required to identify potential areas where the subgrade contains soft / loose soils. The proof roll should be performed in accordance with Section 203.08 of CDOT 2022. Areas which deform non-uniformly under heavy wheel loads should either be moisture conditioned and recompacted or excavated and replaced with properly compacted structural fill. The depth of over-excavation, if required, should be determined during construction. We recommend that the proof rolling activities and visual inspection of the foundation soils be observed and evaluated by an experienced geotechnical engineer or engineer's representative.

Fill placed on existing slopes that are steeper than 4H:1V should be properly benched in accordance with section 203.06 of CDOT 2022. All compaction efforts should be performed in horizontal lifts that are 8-inches or less in loose thickness, using equipment and procedures that will produce a uniform fill with the required moisture contents and densities throughout the lift. The required percent of relative compaction and moisture content for the fill materials are presented in Section 203 of CDOT 2022 and Section 4.2.4 of this report.

Fill materials should be tested for severity of sulfate exposure prior to placement. We recommend that the subgrade preparation process including soil excavation, the placement and compaction of materials, proof rolling and visual inspection of subgrade soils be observed and evaluated by the geotechnical engineer of record or the engineer's representative.

3.1.3 Excavation and Trench Grading

All site excavation and embankment grading should conform to Section 203 of CDOT 2022. Cut slopes should be protected from surface water runoff to prevent erosion and slope failure. Landscape sprinklers if present should be frequently checked for leaks and maintained in good working order. Surface drainage should be provided around all permanent cuts and fills to direct surface runoff away from the slope faces. Concentrated runoff should be prevented in areas susceptible to erosion or slope instability.

Excavations into the on-site soils will encounter a variety of conditions. All excavations must comply with the applicable local, State, and Federal safety regulations, and particularly with the excavation standards of the Occupational Safety and Health Administration (OSHA). Construction site safety, including excavation safety, is the sole responsibility of the Contractor as part of its overall responsibility for the means, methods, and sequencing of construction operations. GEG recommendations for excavation support is provided for the Client's sole use in planning the project, in no way do they relieve the Contractor of its responsibility to construct, support, and maintain safe slopes. Under no circumstances should the following recommendations be interpreted to mean that GEG is assuming responsibility for either construction site safety or the Contractor's activities.

We believe the overburden soil encountered at this site will classify as a Type C material, using OSHA criteria. OSHA requires that unsupported cuts be no steeper than 1½:1 for Type C for unbraced excavations up to 20 feet in height. In general, we believe that these slope ratios will be temporarily stable under unsaturated conditions. Flattened slopes may be required if excavations encounter groundwater or the slopes will be exposed for an extended period of time. Please note that the Contractor's OSHA-qualified "competent person" must make the actual determination of soil type and allowable sloping in the field.

The soils encountered by the proposed excavations may vary significantly across the site. The preliminary classifications presented above are based solely on the materials encountered in widely spaced exploratory test borings. The contractor should verify that similar conditions exist throughout the proposed area of excavation.

As a safety measure, it is recommended that all vehicles and soil piles be kept to a lateral distance equal to at least the depth of the excavation from the crest of the slope. The exposed slope face should be protected against the elements and monitored by the contractor on at least a daily basis.

3.2 DRAINAGE CONSIDERATIONS

During construction, grade the site such that surface water can drain readily away from the pavement areas. Promptly pump out or otherwise remove water that accumulates in the excavations or on subgrade surfaces and allow these areas to dry before resuming construction. The use of berms, ditches, and similar means may be used to prevent stormwater from entering the work area and to convey water off site efficiently.

Limitations

The findings and recommendations presented in this memorandum are based upon data obtained from available information and previous studies, our understanding of the proposed construction, and other sources of information referenced in this memorandum. It is possible

that subsurface conditions may vary between or beyond the locations explored. If subsurface conditions are encountered that vary from those described herein, we should be notified immediately so a review may be made, and any supplemental recommendations provided.

This memorandum was prepared in in a manner consistent with that level of care and skill ordinarily exercised by other members of GEG's profession practicing in the same locality, under similar conditions and at the date the services are provided. GEG makes no other representation, guarantee, or warranty, express or implied, regarding the services, communication (oral or written), report, opinion, or instrument of service provided.

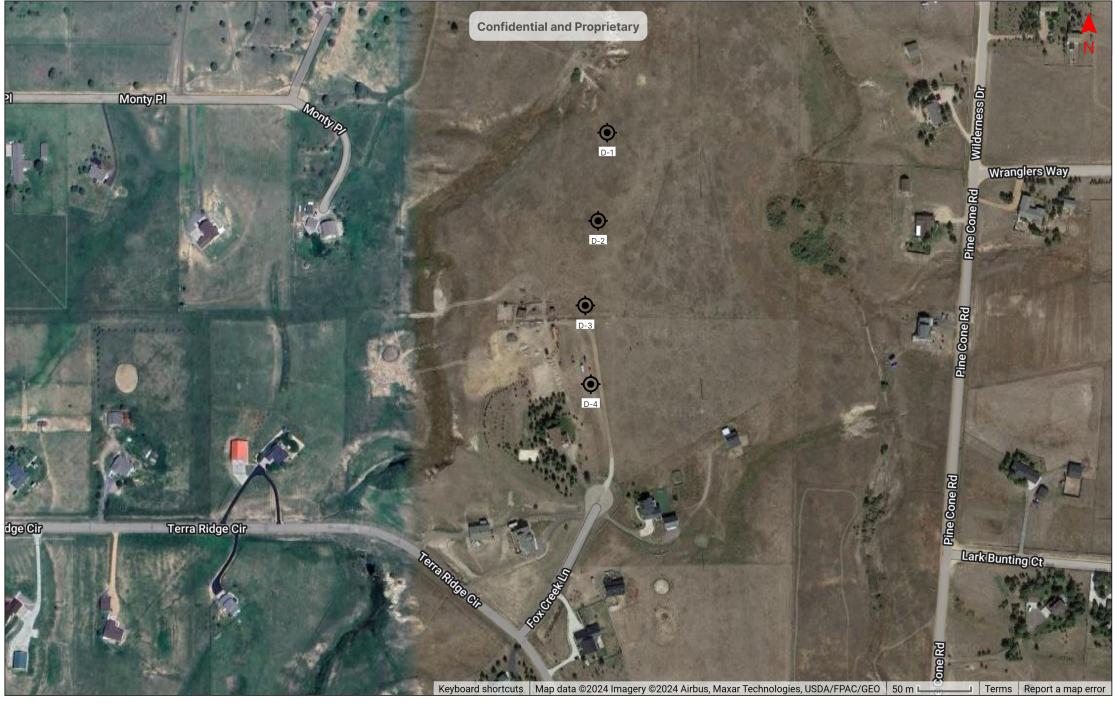
The scope of services for this geotechnical memorandum did not include environmental assessments or evaluations regarding the presence or absence of wetlands or hazardous substances in the soil, surface water, or groundwater.

This memorandum may be used only by the Client and the registered design professional in responsible charge and only for the purposes stated for this specific engagement within a reasonable time from its issuance, but in no event later than three years from the date of the report.

Respectfully. GRANITE ENGINE Hai Ming Lim P 3-26-24 Project Manage Appendix AA Boring Location Plan Attachment: Appendix B- Boring Logs Appendix C- Lab Results Appendix D- Pavement Design Output

Appendix A

BORING LOCATION PLAN



PREPARED BY	PROJECT	LOCATION	SYMBOL KEY
Granite Engineering Group Colorado Springs, Colorado	Name: Terra Ridge North Pavement Number: 24-041	39.05935, -104.69314 Colorado Springs, CO	• Soil Borings

Appendix B

BORING LOGS

S	OIL CLAS	SSIFICATIO	N C	HART PER	RAS	TM D 2488			GRAII			
				SECON	IDAR	Y DIVISIONS					APPROXIMAT	
PRI	MARY DIVIS	SIONS	GI	ROUP SYMB	OL	GROUP NAME	DESCF	RIPTION	SIEVE SIZE	GRAIN SIZE	SIZE	
		CLEAN GRAVEL		GW		well-graded GRAVEL	Bou	lders	> 12"	> 12"	Larger than basketball-sized	
		less than 5% fines		GP		poorly-graded GRAVEL						
	GRAVEL more		, D°C	GW-GM	٧	vell-graded GRAVEL with silt	Cob	bles	3 - 12"	3 - 12"	Fist-sized to basketball-sized	
	than 50% of	GRAVEL with DUAL		GP-GM	ро	oorly-graded GRAVEL with silt						
	coarse fraction retained on No.	CLASSIFICATIONS 5% to 12% fines	, D°C	GW-GC	w	vell-graded GRAVEL with clay			- / · · ·		Thumb-sized to	
	4 sieve			GP-GC	ро	orly-graded GRAVEL with clay		Coarse	3/4 - 3"	3/4 - 3"	fist-sized	
		GRAVEL with FINES more than 12% fines		GM		silty GRAVEL	Gravel					
004005				GC		clayey GRAVEL		Fine	#4 - 3/4"	0.19 - 0.75"	Pea-sized to thumb-sized	
COARSE- GRAINED SOILS				GC-GM		silty, clayey GRAVEL						
more than 50% retained on No. 200 sieve		CLEAN SAND less		SW		well-graded SAND	Coarse		#10 - #4	0.079 - 0.19"	Rock-salt-sized to pea-sized	
		than 5% fines		SP		poorly-graded SAND	Sand	Medium	#40 - #10	0.017 - 0.079"	Sugar-sized to rock-salt-sized	
	SAND 50%			SW-SM		well-graded SAND with silt						
	or more of	SAND with DUAL		SP-SM	F	poorly-graded SAND with silt		Fine	#200 - #40	0.0029 - 0.017"	Flour-sized to	
	coarse fraction retained on No. 4 sieve	CLASSIFICATIONS 5% to 12% fines		SW-SC		well-graded SAND with clay		Fille	#200 - #40	0.0029 - 0.017	sugar-sized	
	4 Sieve			SP-SC	р	oorly-graded SAND with clay						
				SM		silty SAND	Fi	nes	Passing #200	< 0.0029"	Flour-sized and smaller	
		SAND with FINES more than 12% fines		SC		clayey SAND						
				SC-SM		silty, clayey SAND			PLASTICI	TY CHART		
				CL		lean CLAY	70 r					
		INORGANIC		ML		SILT						
	SILT and CLAY liquid limit less			CL-ML		silty CLAY	60					
	than 50%	ORGANIC	(×, ×', (×, ''/×, \)	OL (PI > 4)		organic CLAY	* 50					
FINE-		ORGANIC	× × ×	OL (PI < 4)		organic CLAY	(id) X3 40			CH or OH		
GRAINED SOILS 50% or more				СН		fat CLAY	IQN ∠ 30					
passes No. 200 sieve	SILT and CLAY	INORGANIC	Ĭ	МН		elastic SILT	PLASTICITY INDEX (PI), 00 00 00 00 00		CL dr O		MH or OH	
	liquid limit 50% or more			OH (plots on or above 'A'-line)		organic CLAY	רב 10					
		ORGANIC		OH (plots below 'A'-line)		organic SILT	0					
	Highly O	organic Soils		PT		Peat	0	10	20 30 40 LIQUIE	50 60 70 D LIMIT (LL), %	80 90 10	

APPARENT DENSITY - COARSE-GRAINED SOIL

	SPOOLING CABI	LE OR CATHEAD	AUTOMATIC 1	RIP HAMMER
APPARENT DENSITY	SPT (blows/foot)	MODIFIED SPLIT BARREL (blows/foot)	SPT (blows/foot)	MODIFIED SPLIT BARREL (blows/foot)
Very Loose	≤ 4	≤ 8	≤ 3	≤ 5
Loose	5 - 10	9 - 21	4 - 7	6 - 14
Medium Dense	11 - 30	22 - 63	8 - 20	15 - 42
Dense	31 - 50	64 - 105	21 - 33	43 - 70
Very Dense	> 50	> 105	> 33	> 70

CONSISTENCY - FINE-GRAINED SOIL

	SPOOLING CAB	LE OR CATHEAD	AUTOMATIC 1	RIP HAMMER		
CONSISTENCY	SPT (blows/foot)	MODIFIED SPLIT BARREL (blows/foot)	SPT (blows/foot)	MODIFIED SPLIT BARREL (blows/foot)		
Very Soft	< 2	< 3	< 1	< 2		
Soft	2 - 4	3 - 5	1 - 3	2 - 3		
Firm	5 - 8	6 - 10	4 - 5	4 - 6		
Stiff	9 - 15	11 - 20	6 - 10	7 - 13		
Very Stiff	16 - 30	21 - 39	11 - 20	14 - 26		
Hard	> 30	> 39	> 20	> 26		

							Soil	Borir	g								
	GRA		NGINEERIN) P		Terra Ridge 15630 Fox Cr Springs, C	eek Ln	Cold	orad		S F	ROJ		NO.:	NO.: D-1 1 of 24-0 Joel	
Log	ged By	: Joel	h: 03/12/ Shekosk anite Enç	k i			Rig Type: CME-75 Method: Auger Tooling: 4" Solid Stem Auger	Depth: 4' Ground S Coordina					2				
	mer Ty mer W						Other Comments: Elevation is approximated Google Maps location	d from	Dat - -	e	T	Gr ime - -		water [tab Tin		ft) Water 0.999 0.999	Casing
Ham	mer Fa	all: -				1			1							1	1
Elevation (ft)	Depth (ft)	Sample Graphic	Samples Blow Counts Blow Counts	Uncorrected N-Value	Graphic Log		Materials Description	on	Dry Density (PCF)	Moisture Content (%)	_ab R % Lines	Eiquid Limit	Plasticity Index	% Shrink/Swell Potential	NSCS	AASHTO	Remarks
	-					LE CL bro	LTY SAND , brown, dry. EAN CLAY , brown, moist. AYEY SAND , light yellowish own, moist. AYEY SANDSTONE , gray to	1.3									-
	-						y, low plasticity.	, white,	92.5	17.8	49	41	25		SC	A-7-6	
							iger Refusal at 4'. Boring minated.	4.0									

							Soil	Borir	ng									
	GRA		NGINEERIN	G GROU)		Terra Ridge 15630 Fox Ci Springs, C	reek Ln	, C	olo	orad		S F	SHEE PROJ		NO.:	NO.: D-2 1 of 24-0 Joel	
Date	Start	- Fins	sh: 03/12/	/24 - 03	8/12/24	4	Rig Type: -	Depth: 5	•									
Log	ged By	: Joe	l Shekosk	ki			Method: Hand Auger	Ground	Surf	ace	Elev.	(ft): ~	7486	.2'				
Drill	ing Fir	m: G	ranite Eng	gineerir	ng Gro	oup	Tooling: 3" Hand Auger	Coordina	nates: 39.06095, -104.69322									
Ham	mer T	ype: -					Other Comments:			Date	9	т	Gi ime		water I tab Tir	Depth ((ft) Water	Casing
Ham	mer W	/eight	t: -				Elevation is approximate Google Maps location	d from		-			-				0.999	
	mer F	-											_				0.000	1
			Sample	s			•				l	_ab R	esult	s				
Elevation (ft) 27882	Depth (ft)	Sample Graphic	Blow Counts	Uncorrected N-Value	Graphic Log		Materials Descripti		Dry Density (PCF)	Moisture Content (%)	% Fines	Liquid Limit	Plasticity Index	% Shrink/Swell Potential	nscs	AASHTO	Remarks	
-7485	-					SIL	ganics observed LTY SAND , tan-brown, mois	5.0										

							Soil	Borir	ng								
	GRA		NGINEERIN	G GROU	P		Terra Ridge 15630 Fox Cr Springs, C	eek Ln	, Colc	orad		S F	SHEE PROJ		NO.:		
Date	Start	- Fins	sh: 03/12/	/24 - 03	3/12/24	4	Rig Type: -	Depth: 5'									
Log	ged By	: Joe	l Shekosk	ci			Method: Hand Auger	Ground §									
Drill	ing Fir	m: Gi	ranite Eng	gineerir	ng Gro	bup	Tooling: 3" Hand Auger	Coordina	ates: 39	.0602	3, -10						
Ham	mer T	ype: -					Other Comments: Elevation is approximated	d from	Dat	е	Т	Gi ïme		water [tab Tin		Water	Casing
Ham	mer W	/eight	t: -				Google Maps location									0.999 0.999	
Ham	mer F	all: -															
			Sample	s						l	_ab R	lesults					
Elevation (ft) (ft)	Depth (ft)	Sample Graphic	Blow Counts	Uncorrected N-Value	Graphic Log		Materials Description	on	Dry Density (PCF)	Moisture Content (%)	% Fines	Liquid Limit	Plasticity Index	% Shrink/Swell Potential	NSCS	AASHTO	Remarks
7490						to	ANDY LEAN CLAY , FILL, bro moist, low plasticity.	5.0	112.3	11.2	61	32	15	0.5	CL	A-6	Organics and RAP encountered at 4'

							Soil	Borir	g								
	GRA			G GROU	P		Terra Ridge 15630 Fox Cr Springs, C	eek Ln	, Col	ora		S F	SHEE PROJ		NO.:		
Log		: Joe	sh: 03/12/ I Shekosk		3/12/2	4	Rig Type: - Method: Hand Auger Tooling: 3" Regular Auger	Method: Hand Auger Ground Su Tooling: 3" Regular Coordinate									
	imer T						Other Comments: Elevation is approximated Google Maps location	d from		ate -		īme -		water [Stab Tin		(ft) Water -1.999	Casing
	imer W Imer F								03/1	3/24	0	6:00				3	
			Samples	S							Lab F	Result	sults				
Elevation (ft)	C B B N								Dry Density (PCF)	Moisture Content (%)	% Fines	Liquid Limit	Plasticity Index	% Shrink/Swell Potential	NSCS	AASHTO	Remarks
7505						SII SII	EAN CLAY with Sand, FILL, own, dry. LTY SAND, tan-brown, moist LTY SANDSTONE, white, dr astic, coarse grained. uger Refusal at 3.75'. Boring	2.7							CL		
						ter	minated.										

Appendix C

LAB RESULTS

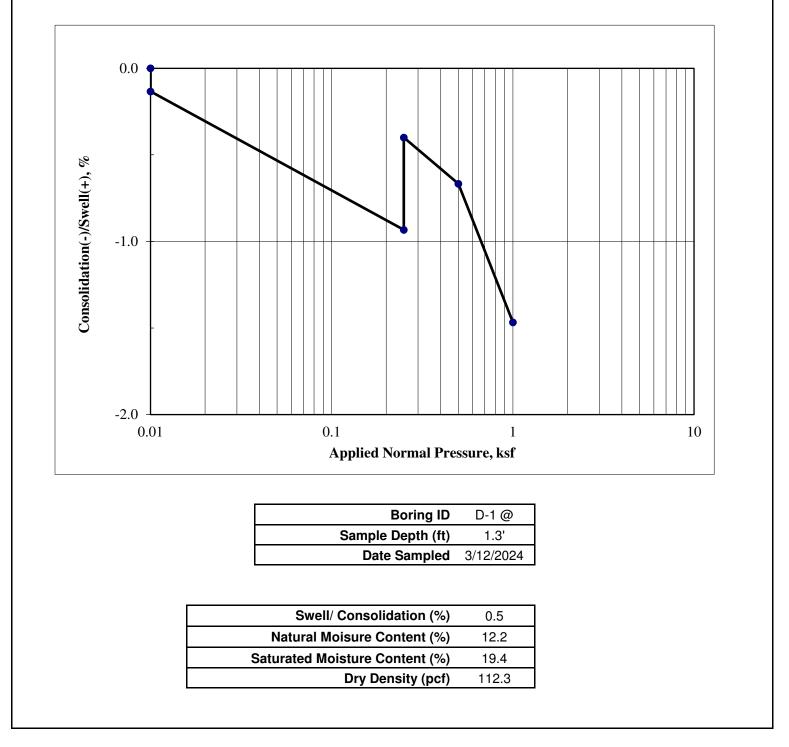


Laboratory Results Summary

Terra Ridge North Pavement El Paso County, CO

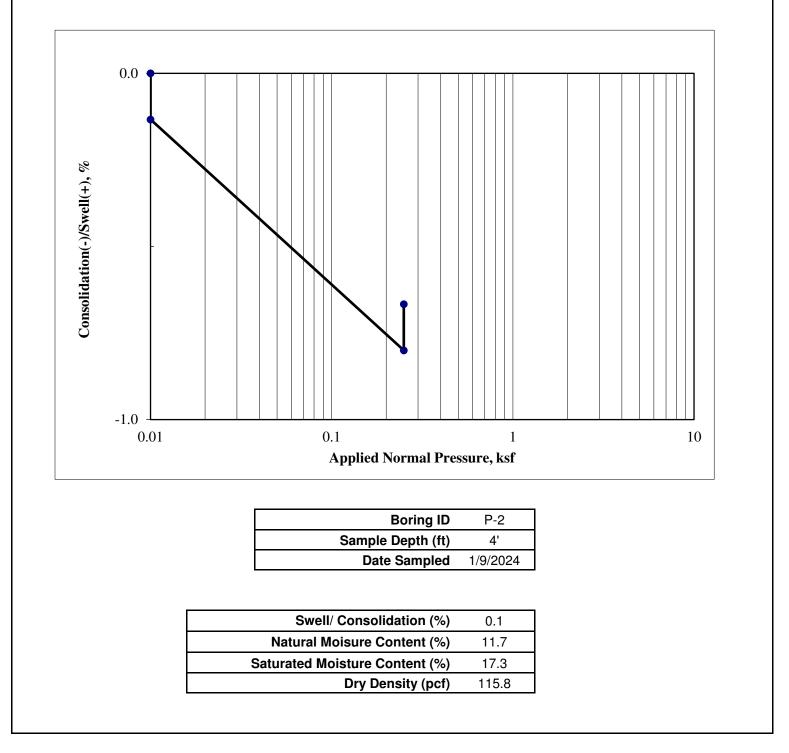
Boring ID	Sample ID	Depth	Moisture Content	LL	PL	Ы	%Gravel	% Sand	% Fines	Dry Density	% Finer than 0.02mm	USCS Classification	USCS Description
D-1	D1@1.3-3.5	1.3	17.79	42	16	26							
D-3	D-3 0'-4.5'	0	11.24	31	17	14							
D-4	D-4 0'-2'	0	14.34	41	14	27							

SWELL/CONSOLIDATION TEST - ASTM D 4546



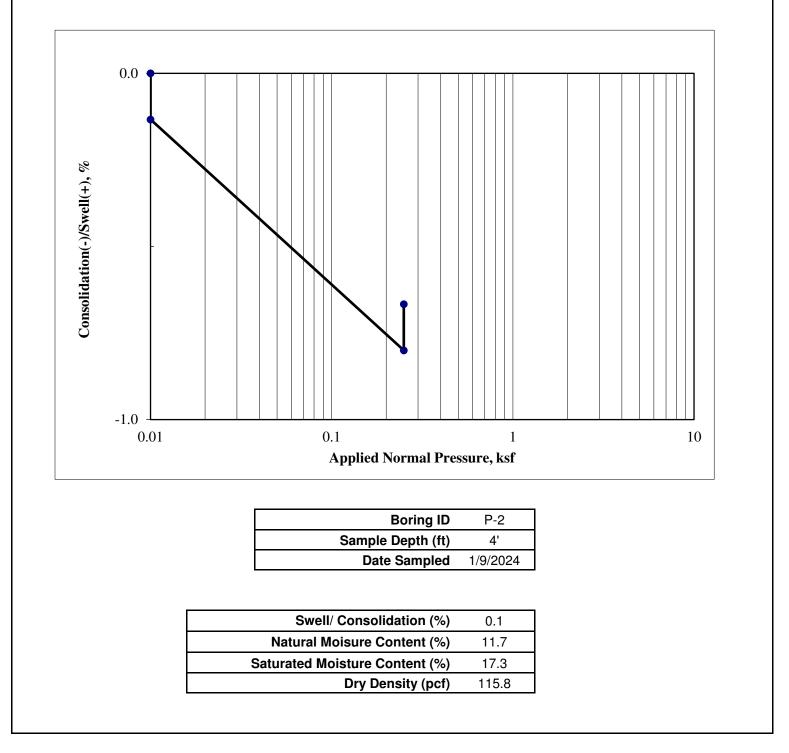
GREEGG GRANITE ENGINEERING GROUP				SWELL/ CONSOLIDATION TEST RESULTS	FIGURE
Project No.	24-041	Date:	3/12/2024	Terra Ridge North	C-1
Report By:	JLS			Black Forest, CO	
Checked By:	HML				





GRANITE ENGINEERING GROUP				SWELL/ CONSOLIDATION TEST RESULTS	FIGURE
Project No.	24-041	Date:	3/12/2024	Terra Ridge North	C-2
Report By:	JLS			Black Forest, CO	
Checked By	: HML				





GRANITE ENGINEERING GROUP				SWELL/ CONSOLIDATION TEST RESULTS	FIGURE
Project No.	24-041	Date:	3/12/2024	Terra Ridge North	C-3
Report By:	JLS			Black Forest, CO	
Checked By	: HML				

Appendix D

PAVEMENT DESIGN OUTPUT

WinPAS

Pavement Thickness Design According to

1993 AASHTO Guide for Design of Pavements Structures

American Concrete Pavement Association

Flexible Design Inputs

Project Name: Route: Location: Owner/Agency: Design Engineer:

Flexible Pavement Design/Evaluation

Structural Number Total Flexible ESALs Reliability Overall Standard Deviation	2.64 36,500 75.00 0.45	percent	Subgrade Resilient Modulus Initial Serviceabilitv Terminal Serviceability	4,500.00 psi 4.50 2.50
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Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN
Asphalt Cement Concrete	0.44	1.00	4.50	1.98
Graded Stone Base	0.11	1.00	6.00	0.66
	-		ΣSN	2.64