### PRELIMINARY DRAINAGE REPORT AND MDDP ADDENDUM FOR HOMESTEAD NORTH AT STERLING RANCH PRELIMINARY PLAN

**Engineering Review** 

04/23/2021 5:49:58 PM dsdrice JeffRice@elpasoco.com (719) 520-7877 EPC Planning & Community Development Department

See comment memo also.

**Prepared For:** 

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> February, 2021 Project No. 25188.00

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# PRELIMINARY DRAINAGE REPORT AND MDDP ADDENDUM FOR HOMESTEAD NORTH AT STERLING RANCH

February 2021

#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. 38861 For and On Behalf of JR Engineering, LLC

#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

**Business Name:** 

SR Land, LLC

By:

Title: Address:

20 Boulder Crescent, Suite 200 Colorado Springs, CO 80903

**El Paso County:** 

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. County Engineer/ ECM Administrator Date

Conditions:



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- Appendix B Hydrologic Calculations
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# PURPOSE

This document is the Preliminary Drainage Report and MDDP Addendum for Homestead North at Sterling Ranch. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert and inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities. It is important to note that Homestead North at Sterling Ranch is intended to be constructed in two phases with both phases being evaluated in this report. Assumptions have been made with regards to Phase 2 in order to size and evaluate the site drainage infrastructure. This report will be confirmed or amended in the event that the phase 2 lot configuration has significant changes.

# **GENERAL SITE DESCRIPTION**

## **GENERAL LOCATION**

Homestead North at Sterling Ranch and the undeveloped land to the north(hereby referred to as the "site") is a proposed development with a total area of approximately 88 acres.

The site is located in the northeast quarter of Section 33 and the southeast quarter of section 28, Township 12 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located immediately east of Vollmer Road. The site is bounded by Briargate Parkway to the south, an unplatted vacant residential parcel to the north, and Sand Creek borders the site to east. The parcels are planned to be platted after approval of the Preliminary Plan. Refer to the vicinity map in Appendix A for additional information.

## **DESCRIPTION OF PROPERTY**

The site is currently being designed to accommodate approximately 228 single-family residential lots and development is to be completed in two phases (totaling approximately 88 acres). The site is comprised of variable sloping grasslands that generally slope(s) downward to the east at 3 to 7% towards the Sand Creek tributary basin.

Soil characteristics are comprised of Type B hydrologic Soil groups. Refer to the soil survey map in Appendix A for additional information.

The Sand Creek is within the eastern portion of the site. Currently, Kiowa Engineering Corp. is performing studies and plans to address Sand Creek stabilization.

There are no known irrigation facilities located on the project site.



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#### FLOODPLAIN STATEMENT

Based on the FEMA Firm Maps Number 08041C0533G and 08041C0535G revised December 7, 2018, the vast majority of the development is located within Zone X, or areas area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. The eastern property boundary will be platted to the center of Sand creek placing a portion of the site within Zone AE. The area of disturbance for site grading is located outside of the delineated floodway within Zone X. The FEMA map containing the site has been presented in Appendix A.

# **EXISTING DRAINAGE CONDITIONS**

### MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into major sub-basins. The site is within the respective sub-basin is shown in Appendix E.

The Sand Creek DBPS assumed the Homestead North at Sterling Ranch property to have a "large lot residential" use for the majority of the site. However, the proposed Sterling Ranch master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. The site generally drains from north to south consisting of rolling hills. Currently, the site is used as pasture land for cattle. Sand Creek is located in the east portion of the site running north to south. This reach of drainage conveyance is not currently improved. There are a few stock ponds within the creek channel used for cattle watering. Currently, Kiowa is performing studies and plans to address Sand Creek stabilization adjacent to the site.

The proposed drainage on the site closely follows the approved "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. The MMDP "Developed Hydrologic Conditions Map" as shown within Appendix E, shows the estimated detention for the site. The site is tributary to basins SC3-18, SC3-17, and a portion of basin SC-322. Full-spectrum detention in the MMDP was previously analyzed and corresponds to ponds FSD18 and FSD17 for the site. Pond FSD17 is associated with ponds A and B within this report. Pond FSD18 is associated with ponds B and C within this report. Runoff as shown in the proposed M&S conduit RT-10A will drain offsite runoff parallel to the site as shown in the MDDP within a 5' conduit. The total estimated/projected detention and estimated outflows from the MDDP are shown in Table 1 below.



# PRELIMINARY DRAINAGE REPORT AND MDDP ADDENDUM FOR HOMESTEAD NORTH AT STERLING RANCH

FSD17						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	41.8	59.6	85.2	119.0	149.1	180.6
ALLOWABLE RELEASE (CFS)	0.7	11.1	22.5	52	67.2	86.3
MODELED RELEASE (CFS)	0.7	8.4	22.4	52	67.2	86.1
STORED VOLUME (AC-FT)	2.6	2.6	2.8	3.4	4.0	4.7

#### Table 1.

FSD18						
STORM EVENT (YR)	2	5	10	25	50	100
PEAK INFLOW (CFS)	49.3	67.1	91.0	121.2	147.3	174
ALLOWABLE RELEASE (CFS)	0.6	9.2	18.4	42.2	54.6	69.9
MODELED RELEASE (CFS)	0.6	6.3	18.4	42.2	54.6	69.6
STORED VOLUME (AC-FT)	3.2	3.2	3.4	4.0	4.7	5.3

The MMDP plans for additional detention to the north of the site as shown in appendix E. No future offsite detention is necessary for the site.

In summary, the site will have three detention ponds A, B, and C. Ponds A and B associated with pond FSD17 of the M&S MDDP and Ponds B and C associated with pond FSD18. The release rates of these ponds will be below 90% of the historic drainage in continuity with the approved M&S MDDP. The report remains in continuity with MDDP and conveys the existing offsite runoff from basin SC3-19 of the MDDP to Sand Creek via proposed storm pipe along Vollmer road and Briargate parkway. The total net detention being stored onsite in the 100 year event is 7.6 Acre-ft, as shown Tables 2.1-2.3 of this report. The total runoff released from the detention ponds is 87.7 cfs in the 100 year event for the three ponds, as shown Tables 2.1-2.3 of this report. The net allowed release rate for the site is 156.2 cfs, as shown in Table 1 above.

### **EXISTING SUB-BASIN DRAINAGE**

The existing/ predeveloped site consists of 3 onsite basins (H1, H2, and H3) and one offsite basin (2). This historic basins outfall to Sand Creek at 2 outfalls as shown in the Historic Drainage Map in Appendix D. A sub-division to the north of the site is being developed called "Retreat at Timberidge". Runoff from this sub-division will be detained and will not impact storm-water runoff on the Sterling Ranch Homestead site.

**Basin 2** (Q5 = 47.7 cfs, Q100 = 188.8 cfs) is a 184 acre area of undeveloped lands covered with native prairie grasses located to the northwest of Vollmer Road. The runoff from this basin is shown in basin SC3-19 as shown in the proposed M&S Drainage Map. The runoff from this basin will be conveyed via a 5" RCP pipe along Vollmer road and Briargate parkway and outfall into Sand Creek.

**Basin H1** (Q5 = 8.9 cfs, Q100 = 61.1 cfs) is 45.3 acres of undeveloped land covered in native prairie grass.

**Basin H2** (Q5 = 3.5 cfs, Q100 = 25.7 cfs) is 15.9 acres of undeveloped land covered in native prairie grass. This basin drains directly into Sand Creek. The basin is to the south east of Vollmer road. This basin drains directly into Sand Creek.

**Basin H3** (Q5 = 6.1 cfs, Q100 = 41.8 cfs) is 21.9 acres of undeveloped land covered in native prairie grass. This basin drains directly into Sand Creek. The basin is to the south east of Vollmer road and North of Briargate Parkway.

Address the existing basins around proposed Sterling Ranch Road and Briargate Pkwy.

# **INTERIM DRAINAGE CONDITIONS**

An Interim Condition Drainage map has been provided for the early grading area of Homestead, and a map is provided in Appendix D. The early grading area consists of the southern portion of Homestead as well as Briargate Parkway and Sterling Ranch Road. This area was split into 2 basins corresponding to the two proposed sediment basins and the areas tributary to them.

**Basin** C is 2% impervious and 24.2 Acres. This basin includes early grading from Sterling Ranch Homestead North. Runoff from this basin will drain into a temporary sediment basin at pond C.

**Basin** D is 2% impervious and 17.25 Acres. This basin includes Briargate Parkway and Sterling Ranch Road. Runoff from this basin will drain into a temporary sediment basin at pond D. The stormwater requirements for Briargate parkway and Sterling Ranch Road are included with the drainage report for Sterling Ranch Phase 3, and will be detailed and designed in the Final Drainage Report when it is time to plat the ROW.

If Briargate Pkwy and Sterling Ranch Road are included in early grading, details to the FDR level will be required. See comment letter.



# **PROPOSED DRAINAGE CONDITIONS**

#### **PROPOSED SUB-BASIN DRAINAGE**

The proposed site was broken up and delineated into three major basins: Basin A (upper-portion), Basin B (mid –portion), and Basin C (lower-portion) of the site. It should be noted that Basin A will be constructed as part of phase 2 of this development and Basins B and C will be constructed as part of Phase 1. Basin A is tributary to Pond A, Basin B is Tributary to Pond B and Basin C is tributary to Pond C. The proposed basin (and sub-basin) delineation is shown on the drainage basin map within Appendix D and is described as follows.

**Basin A1** 3.67 acres and 52% percent impervious is comprised of single-family residential lots, a residential road Jesse Evans Drive, and a Cul de Sac. Runoff ( $Q_5=6.9$  cfs,  $Q_{100}=14.7$  cfs)from this basin A1 drains to design point 1A to a 15' type R on-grade inlet. Runoff is then by-passed in the 100 year event to DP 3A.

**Basin A2** 3.27 acres and 56% percent impervious is comprised of single-family residential lots, a residential road Jesse Evans Drive, and a Cul de Sac. Runoff ( $Q_5$ =6.4 cfs,  $Q_{100}$ =13.3 cfs) from this basin drains to design point 2A to a 15' type R on-grade inlet. Runoff is then by-passed in the 100 year event to DP 4A.

**Basin A3** 4.79 acres and 50% percent impervious is comprised of single-family residential lots, a residential road David Rudabaugh Drive, and a Cul de Sac. Runoff ( $Q_5$ =8.5 cfs,  $Q_{100}$ =18.4 cfs) from this basin drains to design point 3A a 15'type R on-grade inlet in confluence with upstream by-pass flow from basin A1.

**Basin A4** 3.95 acres and 54% percent impervious is comprised of single-family residential lots, a residential road David Rudabaugh Drive, and a Cul de Sac. Runoff ( $Q_5=7.4$  cfs,  $Q_{100}=15.6$  cfs)from this basin drains to design point 4A a 15' type R on-grade inlet in confluence with upstream by-pass runoff from basin A2.

**Basin A5** 5.43 acres and 50% percent impervious is comprised of single-family residential lots, a residential road William Downing Drive, and an urban knuckle. Runoff ( $Q_5=10.5$  cfs,  $Q_{100}=22.6$  cfs)from this basin drains to design point 5A in confluence with upstream by-pass runoff from basin A3 and A1.

**Basin A6** 3.97 acres and 53% percent impervious is comprised of single-family residential lots, a residential road William Downing Drive, and a cul de sac. Runoff ( $Q_5=7.7$  cfs,  $Q_{100}=16.3$  cfs) from this basin drains to design point 6A at an on grade inlet in confluence with upstream by-pass runoff from basin A4 and A2.



**Basin A7** 1.97 acres and 15% percent impervious is comprised of open grass area, and a portion of a residential road Aspen Valley Road. The runoff ( $Q_5=1.3$  cfs,  $Q_{100}=4.8$  cfs)from this basin drains to design point 7A a 20' type R sump inlet. The runoff from the sump inlet collects tributary runoff basins A7, A5, A3, and A1.

**Basin A8** 0.42 acres and 57% percent impervious is comprised of a portion of a residential road Aspen Valley Road. The runoff ( $Q_5=1.2$  cfs,  $Q_{100}=2.5$  cfs)from this basin drains to design point 8A a 15' type R sump inlet. From here on runoff is piped for basin A1-A8 to detention pond A and detained for the water-quality event and up to the 100-year event.

#### — address the overflow conveyance

**Basin A9** 2.97 acres and 16% percent impervious is comprised of pond A, grass and walk-out lots facing the detention area. Runoff ( $Q_5=2.2$  cfs,  $Q_{100}=7.9$  cfs) generated in Basin A9 sheet flows into Pond A where it is treated for water-quality and is detained up until the 100 year-event. The UD Detention sheet for pond A is shown in Appendix C of this report.

**Pond A** has a total tributary area of 30.43 Acres, the net percent impervious area of pond A is 46.3%. Pond A has been conceptually graded in to fit the design volume, as shown in Appendix C of this report. This pond will be built in phase 2 of Homestead North at Sterling Ranch. Pond A will outfall directly into the Sand Creek basin. The WQCV, 5 year and 100 year volumes, releases rates and stages for pond A are shown in Table 2.1 below. These results correspond to the Routed Hydrograph results, as shown in Appendix C of this report.

	TABLE 2.1 Pond A											
	Stage –ft	Volume (Acres)	Release Rate (cfs)									
WQCV	2.58	0.503	0.2									
5 Year	4.70	1.774	3.9									
100 Year	6.00	2.708	32.2									

**Basin B1.1** 3.35 acres and 45% percent impervious is comprised of single-family residential lots, a local roads Billy Claiborne Drive, Perry Owens Drive and an urban knuckle. The runoff ( $Q_5=5.5$  cfs,  $Q_{100}=12.5$  cfs) from basin B1.1 drains to design point 1.1B.

**Basin B1.2** 1.81 acres and 54% percent impervious is comprised of single-family residential lots, a local roads Claiborne Drive, Perry Owens Drive and an urban knuckle. The runoff ( $Q_5=3.5$  cfs,  $Q_{100}=7.4$  cfs) from basin B1.2 drains to design point 1.2B.

**Basin B1.3** 0.47 acres and 47% percent impervious is comprised of single-family residential lots and a local roads Aspen Valley Road and Perry Owens Drive. The runoff ( $Q_5=1.0$  cfs,  $Q_{100}=2.2$  cfs) from basin B1.3 drains to design point 1.3B.

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J R ENGINEERING

Address the Vollmer Road basins, DPs and inlets

**Basin B2** 0.82 acres and 58% percent impervious is comprised of the northern portion of a local residential road Sam Bass Drive adjacent to the intersecting at Vollmer road. Runoff ( $Q_5=2.3$  cfs,  $Q_{100}=4.9$  cfs)from basin B2 drains to design point 2B and confluences with runoff from basin 1B.

**Basin B3** 0.24 acres and 79% percent impervious is comprised of the southern portion of a local residential road Sam Bass Drive adjacent to the intersection of Vollmer road. Runoff ( $Q_5=0.9$  cfs,  $Q_{100}=1.7$  cfs)from basin B3 drains to design point 3B.

**Basin B4** 3.98 acres and 40% percent impervious is comprised of single-family residential lots, a local residential road Wheatland Driveand a Cul de Sac. Runoff ( $Q_5=6.7$  cfs,  $Q_{100}=15.9$  cfs) from this basin drains to design point 4B.

**Basin B5** 1.75 acres and 58% percent impervious is comprised of single-family residential lots, a residential road Wheatland Drive, and a Cul de Sac. Runoff ( $Q_5$ =4.3 cfs,  $Q_{100}$ =8.9 cfs)from basin B5 drains to design point 5B.

**Basin B6** 3.66 acres and 57% percent impervious is comprised of single-family residential lots and a local residential roads Sam Bass Drive, Aspen Valley Road, Perry Owens Drive and Wheatland Drive. Runoff ( $Q_5=9.5$  cfs,  $Q_{100}=19.9$  cfs) from basin 6B drains to design point 6B. In total, the flow at design point 6B collects flow from basins B1, B2, B3, B4, and B6.

**Basin B7** 1.14 acres and 61% percent impervious is comprised of single-family lots, local roads and a Cul de Sac Robert Allison Circle. Runoff ( $Q_5=2.9$  cfs,  $Q_{100}=5.8$  cfs) from basin B7 drains to design point 7B in confluence with runoff from B5.

**Basin B8** 1.74 acres and 58% percent impervious is comprised of single-family lots, local road and a Cul de Sac. Runoff ( $Q_5$ =4.1 cfs,  $Q_{100}$ =8.5 cfs) from basin B8 drains to design point B8 in confluence with runoff from basins B8, B7 and B5.

**Basin B9** 3.69 acres and 65% percent impervious is comprised of single-family lots, and an urban knuckle, and local roads Willie Picket Drive and Wheatland Drive. Runoff ( $Q_5=6.9$  cfs,  $Q_{100}=14.8$  cfs)from Basin B9 drains to design point B9 in a 15' type R sump inlet. In total the runoff from the sump inlet collects runoff from basins B1, B2, B3, B4, B6 and B9.

**Basin B10** 0.22 acres and 80% percent impervious is comprised of the southeastern side of the local road Wheatland Drive. The runoff from this basin drains to design point B10 a 10' type R sump inlet. The total runoff ( $Q_5=0.8$  cfs,  $Q_{100}=1.6$  cfs) is collected at this site is from basins B7, B8, and B10. Runoff will over





**Basin B11** 1.77 acres and 14% percent impervious is comprised of pond B. Runoff ( $Q_5=0.9$  cfs,  $Q_{100}$ =3.9 cfs) generated in Basin B11 sheet flows into Pond B where it is treated for water-quality and is detained up until the 100 year-event. The UD Detention sheet for pond B is shown in Appendix C of this report.

**Pond B** has a tributary area 24.73 acres and is 51.1 % impervious. Pond B has been conceptually graded in to fit the design volume, as shown in Appendix C of this report. This pond will be built in phase 1 of Homestead North at Sterling Ranch. The pond B emergency overflow spillway will drain directly into Sand Creek. The WQCV, 5 year and 100 year volumes, releases rates and stages for pond B are shown in Table 2.2 below. These results correspond to the Routed Hydrograph results, as shown in Appendix C of this report.

	TABLE 2.2 Pond B										
	Stage –ft	Volume (Acres)	Release Rate (cfs)								
WQCV	3.06	0.435	0.2								
5 Year	4.31	1.577	2.9								
100 Year	5.09	2.455	31.2								
			spreadsheet								

**Basin C1** 2.82 acres and 69% percent impervious is comprised of single-family lots, and the northwestern side of the local residential roads Texas Jack Drive and Harvey Logan Drive. Runoff  $(Q_5=5.4 \text{ cfs}, Q_{100}=11.4 \text{ cfs})$  from basin C1 drains to design point 1C at Wheatland Drive.

**Basin C2.1** 0.20 acres and 91% percent impervious is comprised of single-family lots, and the north western side of the residential road Texas Jack Drive. Runoff ( $Q_5=0.8$  cfs,  $Q_{100}=1.6$  cfs) from basin C2.1 drains to design point 2.1C a 5' on grade type R inlet.

**Basin C2.2** 4.69 acres and 73% percent impervious is comprised of local roads, single-family lots, and the north western side of the residential road Wheatland Drive. Runoff ( $Q_5=9.9$  cfs,  $Q_{100}=20.3$ cfs) from basin C2.2 drains to design point 2.2C in confluence with bypass runoff from basin C2.3. The runoff ultimately drains to design point 4C a 20' type R sump inlet. The total runoff from basins C1, C2.1, C2.2, C2.3 and C4.1 is collected within the sump inlet.

**Basin C2.3** 0.83 acres and 67% percent impervious is comprised of local roads Tom Ketchum Drive Jack Helm Drive and Harvey Logan Drive, single-family lots, and the north western side of the residential road Wheatland Drive. Runoff ( $Q_5=1.9$  cfs,  $Q_{100}=3.9$  cfs) from basin C2.3 drains to design point 2.3C in confluence with runoff from basin C1 at an on grade 15' Type R inlet.



**Basin C3.1** 0.35 acres and 73% percent impervious is comprised of single-family lots, and the southeastern side of the residential road Wheatland Drive. Runoff ( $Q_5=1.2$  cfs,  $Q_{100}=2.4$  cfs) from basin C3.1 drains to design point 3.1C.

**Basin C3.2** 1.46 acres and 71% percent impervious is comprised of local roads, single-family lots, and the southeastern side of the residential road Wheatland Drive and Tom Ketchum Drive. Runoff  $(Q_5=3.6 \text{ cfs}, Q_{100}=7.4 \text{ cfs})$  from basin C3.2 drains to design point 3.2C.

**Basin C4.1** 6.37 acres and 65% percent impervious is comprised of single-family lots, and the northwestern side of the local residential road Texas Jack Drive and Nat Love Drive. Runoff ( $Q_5=11.8$  cfs,  $Q_{100}=25.4$  cfs) from basin C4.1 drains to design point 4C a 20' type R sump inlet. The total runoff from basins C1, C2.1, C2.2, C2.3 and C4.1 is collected within the sump inlet.

**Basin C4.2** 3.47 acres and 55% percent impervious is comprised of a local road Texas Jack Drive and single-family lots. Runoff ( $Q_5$ =4.8 cfs,  $Q_{100}$ =11.2 cfs) from basin C4.2 drains to design point 4.2C a 15' type R on grade inlet.

**Basin C5** 0.16 acres and 81% percent impervious is comprised of the northwestern side of a residential road Wheatland Drive. Runoff ( $Q_5=0.6$  cfs,  $Q_{100}=1.1$  cfs) from basin C5 drains to design point 5C, a 5' type R sump inlet. Basin C5 collects runoff from basin C3.2 and C5. The runoff from basin C ultimately outfalls into pond C. In the event the inlet clogs at Basin C5 the runoff will overflow to pond C.

**Basin C6** 2.42 acres and 10% percent impervious is comprised of pond C and some single-family residential area. Runoff ( $Q_5=1.6$  cfs,  $Q_{100}=8.0$  cfs) generated in Basin B11 sheet flows into Pond C where it is treated for water-quality and is detained up until the 100 year-event. The MHFD Detention sheet for pond C is shown in Appendix C of this report.



**Pond C** has a tributary area of 22.77 acres and is 60.8 % impervious. Pond C has been conceptually graded in to fit the design volume, as shown in Appendix C of this report. This pond will be built in phase 1 of Homestead North at Sterling Ranch. The Pond C overflow emergency spillway will overflow into Sand Creek. The WQCV, 5 year and 100 year volumes, releases rates and stages for pond C are shown in Table 2.3 below. These results correspond to the Routed Hydrograph results, as shown in Appendix C of this report.

	TABLE 2.3 Pond C												
	Stage –ft	Volume (Acres)	Release Rate (cfs)										
WQCV	2.39	0.455	0.2										
5 Year	4.05	1.682	3.2										
100 Year	4.99	2.464	24.3										

# **DRAINAGE DESIGN CRITERIA**

## **DEVELOPMENT CRITERIA REFERENCE**

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

## HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.



Storm	Rainfall (in.)							
5-year	1.50							
100-year	2.52							

#### HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD MHFD-Detention v4.03 spreadsheet was utilized for evaluating proposed detention and water quality pond. Sump and on-grade inlets were sized using UDFCD UD-Inlet v2.07. Manning's equation was used to size the proposed pipes in this report and StormCAD will be used to model the proposed storm sewer system and to analyze the proposed HGL calculations for Construction Drawings.

# **DRAINAGE FACILITY DESIGN**

### FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The Homestead North at Sterling Ranch development project consists single -family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 – Stabilize Drainageways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the channel stabilization being designed by Kiowa adjacent to the site and on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek; therefore no downstream stabilization will be accomplished with this project.

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in three proposed full spectrum water quality detention ponds: Pond A, B, and Pond C. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours,



J-R ENGINEERING

This needs to be clarified. Also state the requirements of the Sterling Ranch Filing 1 SIA for Sand Creek channel construction.

Page | 11

and the extended urban runoff volume (EURV) for 72 hours. All flows released from the ponds will be reduced to less than historic rates. See my comment from Review 1. And per ECM Appendix 1.7.2, the heading for Step 4 still needs to be "Consider Need for Industrial and

Step 4 – Pollution Control BMPs: Bi protect the downstream receiving wate Appendix I), therefore specialized BMPs do not need to be considered. implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include asphalt drives and parking, storm inlets and storm pipe, three full spectrum water quality and detention ponds, and permanent vegetation.

## WATER QUALITY

The site is split into three major basins A, B, and C. Each major basin is serviced by an extended full spectrum water quality / detention pond. All the ponds have been designed per Section 13.3.2.1 of Resolution 15-042 of the El Paso County Drainage Criteria Manual. For additional information on pond storage and outlet characteristics see the MHFD sheets within appendix C.

#### **EROSION CONTROL PLAN**

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

#### **OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. We respectfully request that the Operation & Maintenance Manual be submitted in conjunction with the construction documents, prior to obtaining a grading permit.

## **DRAINAGE AND BRIDGE FEES**

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees will be provided at time of final drainage report and will be due at time of platting (depending on date of plat submittal):



# SUMMARY

The proposed Homestead North at Sterling Ranch drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development ponds are designed to release less than MDDP study associated with the subject site. The proposed development will not adversely affect the offsite drainageways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.



# PRELIMINARY DRAINAGE REPORT AND MDDP ADDENDUM FOR HOMESTEAD NORTH AT STERLING RANCH

## REFERENCES

- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2. El Paso County ECM, 2019
- 3. El Paso County DCM Vol. 1 Update, 2015
- 4. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- 5. <u>Upper Sand Creek Detention Evaluation Study</u>, Wilson and Company'
- 6. <u>Final Drainage Report For Retreat at Timberridge Filing No. 1</u>, Classic Consulting Engineers & Surveyors
- 7. Sand Creek Channel Design Report Kiowa, 2021

(This will be required prior to approval or conditions of approval restricting road and lot platting and construction east of Wheatland Drive will be needed.)



# Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map





N.T.S.

VICINITY MAP HOMESTEAD FIL. 3 JOB NO. 25188.00 04/20/20 SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

#### Hydrologic Soil Group-El Paso County Area, Colorado



National Cooperative Soil Survey

**Conservation Service** 

Page 1 of 4



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	90.2	100.0%
Totals for Area of Intere	st	90.2	100.0%	

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified Tie-break Rule: Higher





NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

			LEGEND
		SPECIAL FLOO INUNDATION B	d hazard areas (SFHAS) subject to Y the 1% annual chance flood
39' 22,50"	The 1% annu that has a 1%	al chance flood (100 6 chance of being eq	-year flood), also known as the base flood, is the flood ualed or exceeded in any given year. The Special Flood
38° 58' 7.50"	Hazard Area Special Flood	is the area subject Hazard include Zone	to flooding by the 1% annual chance flood. Areas of s A, AE, AH, AO, AR, A99, V, and VE. The Base Flood
	ZONE A	No Base Flood Eleva	ations determined.
	ZONE AE ZONE AH	Base Flood Elevatio Flood depths of 1	ns determined. . to 3 feet (usually areas of ponding); Base Flood
	ZONE AO	Flood depths of 1 to	ea. o 3 feet (usually sheet flow on sloping terrain); average
		depuis determined determined.	A real Sourceshy protected from the 194 annual chance
		flood by a flood co AR indicates that	the former flood control system is being restored to
4313000mN	ZONE A99	Area to be protection f	rom the 1% annual chance or greater flood. ed from 1% annual chance flood by a Federal flood
	ZONE V	determined.	under construction; no base Hood Elevations
	ZONE VE	Elevations determin	ed. e with velocity hazard (wave action): Base Flood
		Elevations determin	
	The floodway	is the channel of a	stream plus any adjacent floodplain areas that must be
	kept free of substantial in	encroachment so tha creases in flood heigh	it the 1% annual chance flood can be carried without its.
		OTHER FLOOD	AREAS
	ZONE X	Areas of 0.2% annu average depths of square mile: and ar	ai chance flood; areas of 1% annual chance flood with less than 1 foot or with drainage areas less than 1 eas protected by leves from 1% annual chance flood
		OTHER AREAS	
	ZONE X	Areas determined to	be outside the 0.2% annual chance floodplain.
	ZONE D	Areas in which flood	I hazards are undetermined, but possible.
		COASTAL BARR	IER RESOURCES SYSTEM (CBRS) AREAS
		OTHERWISE PR	OTECTED AREAS (OPAs)
	CBRS areas a	nd OPAs are normally Floodp	r located within or adjacent to Special Flood Hazard Areas. Iain boundary
	<b>.</b>	Floody	vay boundary
	******	CBRS a	and OPA boundary
		Bound Flood	ary dividing Special Flood Hazard Areas of different Base Elevations, flood depths or flood velocities.
	~~ 513	Base F	lood Elevation line and value; elevation in feet*
	(EL 98/	) Base r elevati	ood Elevation value where uniform within zone; on in feet*
<sup>43</sup> 12 <sup>000m</sup> N		- Cross :	n vertical Datum of 1988 (NAVD 88) section line
	<u></u>		rt line
5.	97° 07' 30	.00" Geogra	aphic coordinates referenced to the North American
5.	32° 22' 30 4275000m	.00" Datum N 1000-r	of 1983 (NAD 83) neter Universal Transverse Mercator grid ticks.
		zone 1	3 Kat arid Vislan Calaurila Cinto Dinan accustoria
235	600000	FI 5000-I system Lambe	n, central zone (FIPSZONE 0502); rt Conformal Conic Projection
INEL	DX5510	) Bench X this FI	mark (see explanation in Notes to Users section of RM panel)
N	• M1.5	5 River M	Иile
Ō		Poforio	MAP REPOSITORIES
		EFFE	
		FĻC	JOD INSURANCE RALE MAP MARCH 17, 1997
	DECEMI Special FI	EFFECTIVE D/ SER 7, 2018 - to upda ood Hazard Areas, to	ATE(S) OF REVISION(S) TO THIS PANEL te corporate limits, to change Base Flood Elevations and update map format, to add roads and road names, and to
		incorporate p	eviously issued Letters of Map Revision.
	For communi Map History 1	ty map revision histor able located in the Fl	y prior to countywide mapping, refer to the Community ood Insurance Study report for this jurisdiction.
	To determine agent or call	if flood insurance is the National Flood Ins	s available in this community, contact your insurance surance Program at 1-800-638-6620.
		J	MAP SCALE 1" = 500'
		250 0 <u>HHH</u>	500 1000 FEET
	1	50 0	METERS 150 300
	1	NIEIBI	
		<b>Ц</b> ŊЦЩЦЦ∏[]]	PANEL 0533G
		6	FLOOD INSURANCE RATE MAP
		Q	EL PASO COUNTY,
			AND INCORPORATED AREAS
		9	SEE MAD INDEX FOR FIDM DANEL LAYOUT
			COMMUNITY NUMBER PANEL SUFFIX
		6	EL PASO COUNTY 080059 0533 G.
		Q	
			Notice to User. The <b>Map Number</b> shown below should be
			used when placing map orders: the <b>Community Number</b> shown above should be used on insurance applications for the subject community.
		Ø	MAP NUMBER
38* 56' 15 00*		NI NI	08041C0533G
I4° 39' 22,50"			MAP REVISED
		W	DECEMBER 7, 2018
-	IE I		I Rederal Emergency Management Agency



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NOTES TO USERS

<sup>om</sup> N ' 15.00" '	NAMERONAL FLOOD	Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject community. MAP NUMBER 08041C05355G MAP REVISED DECEMBER 7, 2018 Federal Emergency Management Agency
υπΝ	DEINSURANGE PROGRAM	FIREL COUCC FIRM FLOOD INSURANCE RATE MAP FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS PANEL 535 OF 1300 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: <u>COMMUNITY</u> NUMBER PANEL SUFFIX COLORADO SPRINGS, CITY OF 080080 0535 G EL PASO COUNTY 080059 0535 G
тN	To determine if flood insurance agent or call the National Flood In 500 0 500 0 300	is available in this community, contact your insurance insurance Program at 1-800-638-6620. MAP SCALE 1" = 1000' 1000 2000 FEET METERS 0 300 600
"N	6000000 FT 5000 syste Lamb DX5510 Bencl this F M1.5 River Refer to EFFECTIVE I DECEMBER 7, 2018 - to upo Special Flood Hazard Areas, t incorporate to For community map revision hists Map History Table located in the I	I-foot grid ticks: Colorado State Plane coordinate Em, central zone (FIPSZONE 0502), pert Conformal Conic Projection th mark (see explanation in Notes to Users section of FIRM panel) • Mile MAP REPOSITORIES to Map Repositories list on Map Index ECTIVE DATE OF COUNTYWIDE LOOD INSURANCE RATE MAP MARCH 17, 1997 DATE(S) OF REVISION(S) TO THIS PANEL date corporate limits, to change Base Flood Elevations and to update map format, to add roads and road names, and to previously issued Letters of Map Revision. bory prior to countywide mapping, refer to the Community Flood Insurance Study report for this jurisdiction.
۳N	Boun         Boun           Flood         Flood           Image: State of the sta	idary dividing Special Flood Hazard Areas of different Base 1 Elevations, flood depths or flood velocities. Flood Elevation line and value; elevation in feet* Flood Elevation value where uniform within zone; ation in feet* can Vertical Datum of 1988 (NAVD 88) is section line sect line graphic coordinates referenced to the North American m of 1983 (NAD 83) I-meter Universal Transverse Mercator grid ticks, 13
۳N	ZONE X       Areas of 0.2% and average depths or square mile; and a	<ul> <li>AREAS</li> <li>nual chance flood; areas of 1% annual chance flood with of less than 1 foot or with drainage areas less than 1 areas protected by levees from 1% annual chance flood,</li> <li>to be outside the 0.2% annual chance floodplain.</li> <li>od hazards are undetermined, but possible.</li> <li>RIER RESOURCES SYSTEM (CBRS) AREAS</li> <li>PROTECTED AREAS (OPAs)</li> <li>Ily located within or adjacent to Special Flood Hazard Areas.</li> <li>tplain boundary</li> <li>to Boundary</li> <li>5 and OPA boundary</li> </ul>
۳N	ZONE AR       Special Flood Haze         flood by a flood c       AR         flood by a flood c       AR         provide protection       Some AR         ZONE A99       Area to be protection         ZONE A99       Area to be protection         ZONE V       Coastal flood zon         Elevations determined.       ZONE VE         ZONE VE       Coastal flood zon         Elevations determined.       FLOODWAY AF         The floodway is the channel of a kept free of encroachment so th substantial increases in flood heig	and Area Formerly protected from the 1% annual chance control system that was subsequently decertified. Zone is the former flood control system is being restored to inform the 1% annual chance or greater flood. cted from 1% annual chance flood by a Federal flood in under construction; no Base Flood Elevations he with velocity hazard (wave action); no Base Flood ined. REAS IN ZONE AE a stream plus any adjacent floodplain areas that must be hat the 1% annual chance flood can be carried without ghts.
.00*	SPECIAL FLOO INUNDATION I The 1% annual chance flood (10 that has a 1% chance of being e Hazard Area is the area subject Special Flood Hazard include Zon Elevation is the water-surface ele ZONE A No Base Flood Elevati ZONE AE Base Flood Elevati ZONE AH Flood depths of Elevations determi ZONE AO Flood depths of 1	LEGEND OD HAZARD AREAS (SFHAS) SUBJECT TO BY THE 1% ANNUAL CHANCE FLOOD 00-year flood), also known as the base flood, is the flood gualed or exceeded in any given year. The Special Flood to flooding by the 1% annual chance flood. Areas of tes A, AE, AH, AO, AR, A99, V, and VE. The Base Flood wation of the 1% annual chance flood. wations determined. ions determined. 1 to 3 feet (usually areas of ponding); Base Flood ined. to 3 feet (usually sheet flow on sloping terrain); average

# Appendix B Hydrologic Calculations



## COMPOSITE % IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Existing Conditions Homestead Fil. 3 El Paso County Project Name: Homestead North Project No.: 25188.00 Calculated By: ARJ Checked By: Date: 2/12/20

	Total	Street	Streets/Paved (100% Impervious) Residential (45%-65% Impervious)			mpervious)	Lawns (2% Impervious)				Basins Total Weighted C		Basins Total Weighted %			
Basin ID	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	Val C <sub>5</sub>	ues C <sub>100</sub>	Imp.
H1	45.30	0.90	0.96	0.38	0.8%	0.45	0.59	0.00	0.0%	0.08	0.35	44.92	2.0%	0.09	0.36	2.8%
H2	15.90	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	15.90	2.0%	0.08	0.35	2.0%
H3	29.10	0.90	0.96	0.22	0.7%	0.45	0.59	0.00	0.0%	0.08	0.35	28.88	2.0%	0.09	0.35	2.7%

Provide for the area east of Sand Creek that the proposed roads are in.

#### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Existing Conditions Homestead Fil. 3

Location: El Paso County

#### Project Name: Homestead North

Project No.: 25188.00

-	
Calculated By:	ARJ
Checked By:	
Date:	2/12/20

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	К	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
H1	45.30	В	3%	0.09	0.36	150	2.0%	17.8	1074	2.3%	7.0	1.1	16.9	34.7	1224.0	38.1	34.7
H2	15.90	В	2%	0.08	0.35	150	2.0%	17.9	425	2.0%	7.0	1.0	7.2	25.1	575.0	31.1	25.1
H3	29.10	В	3%	0.09	0.35	150	1.4%	20.3	645	1.9%	7.0	1.0	11.1	31.3	795.0	33.8	31.3

NOTES:

	$t_{\perp} = t_{\perp} + t_{\perp}$	Equation	$5.2 = 0.395(1.1 - C_5)\sqrt{L_i}$	Equation 6.2	Table 6-2. NRCS Conve	yance factors, K
	<i>c 1 1</i>	Equation	$L_i = \frac{S_o^{0.33}}{S_o^{0.33}}$	Equation 0-5	Type of Land Surface	Conveyance Factor, K
Where	ti in the second se		Where		Heavy meadow	2.5
	$t_c$ = computed time of concentration (minutes)		where.		Tillage/field	5
			$t_i$ = overland (initial) flow time (minutes)		Short pasture and lawns	7
	$t_i = \text{overland (initial) flow time (minutes)}$		$L_i = \text{length of overland flow (ft)}$		Nearly bare ground	10
	$t_t$ = channelized flow time (minutes).		$S_o$ = average slope along the overland flow path (ft/ft).		Grassed waterway	15
					Paved areas and shallow paved swales	20
	$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$	Equation 6-4	$t_c = (26 - 17i) + \frac{L_r}{60(14i + 9)\sqrt{S_r}}$	Equation 6-5		
Where	5		Where:			
	$t_t = \text{channelized flow time (travel time, min)}$ $L_t = waterway length (ft)$ $S_0 = waterway slope (ft/ft)$ $V_t = travel time velocity (ft/sec) = K \sqrt{S_0}$ K = NRCS conveyance factor (see Table 6-2).		$t_c = \minimum$ time of concentration for first design point when less than t $L_t = \text{length of channelized flow path (ft)}$ I = imperviousness (cxpressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$	from Equation 6-1.		

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Existing Conditions Homestead Fil. 3 Location: El Paso County Design Storm: 100-Year

Project Name: Ho	mestead North
------------------	---------------

Project No.: 25188.00 Calculated By: ARJ

Checked By:

Date: 2/12/21

				DIF	RECT R	UNOFF			T	OTAL R	UNOF	F	STRE	et/sw	VALE		PI	ΡE		TRAV	'EL TIN	ЛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	${ m t_c}$ (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1h	H1	45.30	0.36	34.7	16.08	3.80	61.1															Drains to swale
	2h	H2	15.90	0.35	25.1	5.57	4.61	25.7	34.7	21.65	3.80	82.2											Accepts runoff from H1 and H2
	3h	H3	29.10	0.35	31.3	10.32	4.05	41.8															Does not include upstream runoff
Netoci																							•

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Existing Conditions Homestead Fil. 3 Location: El Paso County Design Storm: 100-Year

Project Name: Ho	mestead North
------------------	---------------

Project No.: 25188.00 Calculated By: ARJ

Checked By:

Date: 2/12/21

				DIF	RECT R	UNOFF			T	OTAL R	UNOF	F	STRE	et/sw	VALE		PI	ΡE		TRAV	'EL TIN	ЛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	${ m t_c}$ (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1h	H1	45.30	0.36	34.7	16.08	3.80	61.1															Drains to swale
	2h	H2	15.90	0.35	25.1	5.57	4.61	25.7	34.7	21.65	3.80	82.2											Accepts runoff from H1 and H2
	3h	H3	29.10	0.35	31.3	10.32	4.05	41.8															Does not include upstream runoff
Netoci																							•

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### COMPOSITE % IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Homestead Fil. 3 El Paso County Project Name: Homestead North Project No.: 25188.00 Calculated By: ARJ Checked By:

Date: 2/12/21

	Total	Street	s/Paved	(100% In	npervious)	Reside	ntial (45	%-65% Ir	npervious)	L	awns (29	% Imper∖	vious)	Basins Weigh Val	Total nted C	Basins Total Weighted %
Basin ID	Ai ca (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp	C <sub>r</sub>	Can	Imp.
				(40)	70 mp.			(40)	70 mp.			(40)	70 mp.	-5	- 100	
A1	3.67	0.90	0.96	0.82	22.4%	0.45	0.59	2.41	29.5%	0.08	0.35	0.44	0.2%	0.51	0.64	52.2%
A2	3.27	0.90	0.96	0.84	25.6%	0.45	0.59	2.19	30.1%	0.08	0.35	0.24	0.1%	0.54	0.67	55.9%
A3	4.79	0.90	0.96	0.79	16.4%	0.45	0.59	3.56	33.4%	0.08	0.35	0.45	0.2%	0.49	0.63	50.0%
A4	3.95	0.90	0.96	0.77	19.6%	0.45	0.59	2.99	34.1%	0.08	0.35	0.18	0.1%	0.52	0.65	53.8%
A5	5.43	0.90	0.96	0.67	12.4%	0.45	0.59	4.47	37.0%	0.08	0.35	0.29	0.1%	0.49	0.62	49.5%
A6	3.97	0.90	0.96	0.67	17.0%	0.45	0.59	3.17	36.0%	0.08	0.35	0.12	0.1%	0.51	0.65	53.0%
A7	1.97	0.90	0.96	0.22	11.0%	0.45	0.59	0.12	2.7%	0.08	0.35	1.63	1.7%	0.19	0.43	15.4%
A8	0.42	0.90	0.96	0.21	50.4%	0.45	0.59	0.05	5.9%	0.08	0.35	0.15	0.7%	0.54	0.69	57.1%
A9	2.97	0.90	0.96	0.00	0.0%	0.45	0.59	0.99	14.9%	0.08	0.35	1.99	1.3%	0.20	0.43	16.3%
Pond A	30.44															46.3%
B1.1	3.35	0.90	0.96	0.48	14.2%	0.45	0.59	2.29	30.7%	80.0	0.35	0.59	0.4%	0.45	0.60	45.2%
B1.2	1.81	0.90	0.96	0.32	17.9%	0.45	0.59	1.43	35.5%	0.08	0.35	0.06	0.1%	0.52	0.65	53.5%
B1.3	0.47	0.90	0.96	0.20	41.4%	0.45	0.59	0.05	5.0%	0.08	0.35	0.22	0.9%	0.46	0.63	47.4%
B2	0.82	0.90	0.96	0.33	40.2%	0.45	0.59	0.32	17.3%	0.08	0.35	0.17	0.4%	0.55	0.69	57.9%
B3	0.24	0.90	0.96	0.19	78.7%	0.45	0.59	0.00	0.0%	0.08	0.35	0.05	0.4%	0.73	0.83	79.1%
B4	3.98	0.90	0.96	0.46	11.4%	0.45	0.59	2.47	27.9%	0.08	0.35	1.06	0.5%	0.40	0.57	39.9%
B5	1.75	0.90	0.96	0.44	25.1%	0.45	0.59	1.26	32.4%	0.08	0.35	0.05	0.1%	0.55	0.68	57.5%
B6	3.66	0.90	0.96	1.25	34.2%	0.45	0.59	1.85	22.8%	0.08	0.35	0.55	0.3%	0.55	0.68	57.3%
B7	1.14	0.90	0.96	0.38	33.7%	0.45	0.59	0.69	27.4%	0.08	0.35	0.06	0.1%	0.58	0.70	61.2%
B8	1.74	0.90	0.96	0.53	30.2%	0.45	0.59	1.07	27.7%	0.08	0.35	0.14	0.2%	0.56	0.68	58.1%
B9	3.69	0.90	0.96	0.80	21.7%	0.45	0.59	2.43	42.7%	0.08	0.35	0.47	0.3%	0.50	0.64	64.6%
B10	0.22	0.90	0.96	0.18	79.1%	0.45	0.59	0.00	0.0%	0.08	0.35	0.05	0.4%	0.73	0.83	79.5%
B11	1.77	0.90	0.96	0.00	0.0%	0.45	0.59	0.35	12.7%	0.08	0.35	1.42	1.6%	0.15	0.40	14.3%
Pond B	24.64															51.1%
C1	2.82	0.90	0.96	0.49	17.2%	0.45	0.59	2.25	51.7%	0.08	0.35	0.09	0.1%	0.52	0.65	69.0%
C2.1	0.20	0.90	0.96	0.18	90.5%	0.45	0.59	0.00	0.0%	0.08	0.35	0.02	0.2%	0.82	0.90	90.7%
C2.2	4.69	0.90	0.96	1.26	26.9%	0.45	0.59	3.33	46.1%	0.08	0.35	0.10	0.0%	0.56	0.68	73.0%
C2.3	0.83	0.90	0.96	0.28	34.1%	0.45	0.59	0.41	32.4%	0.08	0.35	0.13	0.3%	0.54	0.68	66.9%
C3.1	0.35	0.90	0.96	0.25	72.8%	0.45	0.59	0.00	0.0%	0.08	0.35	0.09	0.5%	0.68	0.79	73.3%
C3.2	1.46	0.90	0.96	0.42	28.4%	0.45	0.59	0.96	42.8%	0.08	0.35	0.08	0.1%	0.56	0.68	71.3%
C4.1	6.37	0.90	0.96	1.04	16.4%	0.45	0.59	4.76	48.6%	0.08	0.35	0.57	0.2%	0.49	0.63	65.1%
C4.2	3.47	0.90	0.96	0.45	13.1%	0.45	0.59	2.20	41.2%	0.08	0.35	0.81	0.5%	0.42	0.58	54.8%
C5	0.16	0.90	0.96	0.13	80.9%	0.45	0.59	0.00	0.0%	0.08	0.35	0.03	0.4%	0.74	0.84	81.3%
C6	2.42	0.90	0.96	0.00	0.0%	0.45	0.59	0.32	8.7%	0.08	0.35	2.10	1.7%	0.13	0.38	10.4%
Pond C	22.77															60.8%

#### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Homestead Fil. 3

Location: El Paso County

Project Name: Homestead North

Project No.: 25188.00

Calculated By: ARJ Checked By:

Date: 2/12/21

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	$C_5$	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	3.67	В	52%	0.51	0.64	150	2.0%	10.4	589	3.0%	20.0	3.5	2.8	13.3	739.0	20.6	13.3
A2	3.27	В	56%	0.54	0.67	150	2.0%	9.9	595	1.6%	20.0	2.5	3.9	13.8	745.0	21.2	13.8
A3	4.79	В	50%	0.49	0.63	150	2.0%	10.7	645	2.9%	20.0	3.4	3.2	13.9	795.0	21.5	13.9
A4	3.95	В	54%	0.52	0.65	150	2.0%	10.2	653	1.9%	20.0	2.7	4.0	14.2	803.0	21.7	14.2
A5	5.43	В	50%	0.49	0.62	187	7.0%	8.0	531	2.1%	20.0	2.9	3.1	11.1	718.0	21.5	11.1
A6	3.97	В	53%	0.51	0.65	230	4.5%	9.8	435	1.6%	20.0	2.6	2.8	12.6	665.0	20.4	12.6
A7	1.97	В	15%	0.19	0.43	240	4.9%	15.1	125	0.6%	20.0	1.5	1.4	16.5	365.0	25.9	16.5
A8	0.42	В	57%	0.54	0.69	9.5	2.0%	2.5	230	1.9%	20.0	2.8	1.4	3.9	239.5	17.9	5.0
A9	2.97	В	16%	0.20	0.43	30	2.0%	7.1	535	0.5%	20.0	1.4	6.3	13.4	565.0	34.4	13.4
B1.1	3.35	В	45%	0.45	0.60	125	2.0%	10.5	610	3.1%	20.0	3.5	2.9	13.4	735.0	22.1	13.4
B1.2	1.81	В	54%	0.52	0.65	150	2.0%	10.2	577	3.4%	20.0	3.7	2.6	12.8	727.0	20.1	12.8
B1.3	0.47	В	47%	0.46	0.63	50	2.0%	6.5	270	2.0%	20.0	2.8	1.6	8.1	320.0	20.0	8.1
B2	0.82	В	58%	0.55	0.69	9.5	2.0%	2.4	368	3.4%	20.0	3.7	1.7	4.1	377.5	18.1	5.0
B3	0.24	В	79%	0.73	0.83	9.5	2.0%	1.7	360	3.7%	20.0	3.9	1.6	3.2	369.5	14.1	5.0
B4	3.98	В	40%	0.40	0.57	25	2.0%	5.0	680	1.6%	20.0	2.5	4.5	9.5	705.0	25.4	9.5
B5	1.75	В	58%	0.55	0.68	25	2.0%	3.9	590	1.6%	20.0	2.6	3.8	7.8	615.0	20.7	7.8
B6	3.66	В	57%	0.55	0.68	9.5	2.0%	2.4	855	3.0%	20.0	3.5	4.1	6.6	864.5	21.1	6.6
B7	1.14	В	61%	0.58	0.70	50	1.0%	6.6	315	1.5%	20.0	2.4	2.1	8.8	365.0	18.0	8.8
B8	1.74	В	58%	0.56	0.68	50	1.0%	6.9	280	1.0%	20.0	2.0	2.4	9.3	330.0	18.9	9.3
B9	3.69	В	65%	0.50	0.64	140	2.0%	10.2	600	2.9%	20.0	3.4	2.9	13.1	740.0	18.3	13.1
B10	0.22	В	80%	0.73	0.83	9.5	2.0%	1.6	200	0.5%	20.0	1.4	2.4	4.1	209.5	14.9	5.0
B11	1.77	В	14%	0.15	0.40	30	2.0%	7.5	250	0.1%	20.0	0.4	9.3	16.8	280.0	40.5	16.8
C1	2.82	В	69%	0.52	0.65	130	2.0%	9.6	690	2.6%	20.0	3.2	3.6	13.1	820.0	18.1	13.1
C2.1	0.20	В	91%	0.82	0.90	7.5	2.0%	1.1	300	1.0%	20.0	2.0	2.5	3.6	307.5	12.9	5.0
C2.2	4.69	В	73%	0.56	0.68	150	2.0%	9.5	630	2.5%	20.0	3.2	3.3	12.8	780.0	17.0	12.8
C2.3	0.83	В	67%	0.54	0.68	100	2.0%	8.0	462	3.3%	20.0	3.6	2.1	10.1	562.0	16.9	10.1
C3.1	0.35	В	73%	0.68	0.79	9.5	2.0%	1.9	460	2.6%	20.0	3.2	2.4	4.2	469.5	16.0	5.0

#### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Homestead Fil. 3

Location: El Paso County

#### Project Name: Homestead North

Project No.: 25188.00

Calculated By: ARJ Checked By:

Date: 2/12/21

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
C3.2	1.46	В	71%	0.56	0.68	50	2.0%	5.5	365	1.1%	20.0	2.1	2.9	8.4	415.0	16.9	8.4
C4.1	6.37	В	65%	0.49	0.63	150	2.0%	9.6	633	2.8%	20.0	3.3	3.2	12.7	783.0	17.2	12.7
C4.2	3.47	В	55%	0.42	0.58	150	2.0%	10.7	1010	1.7%	20.0	2.6	6.5	17.2	1160.0	22.1	17.2
C5	0.16	В	81%	0.74	0.84	9.5	2.0%	2.7	200	0.6%	20.0	1.5	2.2	4.9	209.5	17.4	5.0
C6	2.42	В	10%	0.13	0.38	15	2.0%	2.0	160	0.5%	20.0	1.4	1.9	3.9	175.0	14.0	5.0

#### NOTES:

$t_c = t_i + t_t$	Equation	$5-2$ = 0.395(1.1- $C_5$ ) $\sqrt{L_i}$	Fountion 6.3	Table 6-2. NRCS Conve	yance factors, K
Where		$u_i = \frac{1}{S_o^{0.33}}$	Equation 0-5	Type of Land Surface	Conveyance Factor, K
where.		Wheee		Heavy meadow	2.5
$t_c$ = computed time of concentration (minutes)		where.		Tillage/field	5
$t_i$ = overland (initial) flow time (minutes)		$t_i$ = overland (initial) flow time (minutes)		Short pasture and lawns	7
t = the set of the time (minutes)		$L_i = \text{length of overland flow (ft)}$		Nearly bare ground	10
$t_t = \text{channelized now time (minutes)}.$		$S_o$ = average slope along the overland flow path (ft/ft).		Grassed waterway	15
$L_r$ $L_r$	-			Paved areas and shallow paved swales	20
$I_t = \frac{1}{60K\sqrt{S_o}} = \frac{1}{60V_t}$	Equation 6-4	$l_{r} = (26 - 1/l) + \frac{1}{60(14l + 9)\sqrt{S_{r}}}$	Equation 6-5		
Where:		Where:			
$t_r$ = channelized flow time (travel time, min) $L_r$ = waterway length (ft) $S_o$ = waterway slope (ft)ft $V_r$ = travel time velocity (ft/sc) = K $\sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2).		$t_e = \minimum$ time of concentration for first design point when less than to $L_i = \text{length of channelized flow path (ft)}$ i = imperviousness (expressed as a decimal) $S_r = \text{slope of the channelized flow path (ft/ft)}.$	from Equation 6-1.		

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN

#### (RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	Home: El Paso 5-Year	stead F o Coun	il. 3 ty									•				Proj P Calc Cł	ect Na Project sulated necked	me: <u>Hc</u> No.: <u>25</u> By: <u>AR</u> By:	mestea 188.00	ad No	rth		
																	D	ate: 2/	12/21				
				DIRE	CT RUI	NOFF			T	OTAL	RUNOF	F	STRE	ET/SW	ALE		PIP	E	TRA	VEL 1	FIME		
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Length (ft)	Velocity (fps)	forder formation	t <sub>t</sub> (min)	REMARKS
	1a	A1	3.67	0.51	13.3	1.86	3.70	6.9					0.00	0	2.84				33	5 3	.4	1.7	On-grade Type R Inlet, Bypass to DP 3a
	3a	A3	4.79	0.49	13.9	2.34	3.63	8.5	14.9	2.34	3.53	8.3	0.20	0.06	2.8				11	0 3	.3	0.5	On-grade Type R Inlet, Bypass to DP 5a
	5a	A5	5.43	0.49	11.1	2.64	3.98	10.5	14.9	2.70	3.53	9.5											Street Flow
	7a	A7	1.97	0.19	16.5	0.38	3.38	1.3	16.5	3.08	3.38	10.4											Flow Confluences at sump inlet
	2a	A2	3.27	0.54	13.8	1.76	3.64	6.4					0.00	0	2.84				33	5 3	.4	1.7	On-grade Type R Inlet, Bypass to DP 4a
	4a	A4	3.95	0.52	14.2	2.06	3.61	7.4	15.5	2.06	3.47	7.2	3.60	1.04	2.8				11	0 3	.3	0.5	On-grade Type R Inlet, Bypass to DP 6a
	6a	A6	3.97	0.51	12.6	2.04	3.79	7.7	15.5	3.08	3.47	10.7											Street Flow
	8a	A8	0.42	0.54	5.0	0.23	5.17	1.2	16.0	3.31	3.42	11.3											Flow Confluences at sump inlet
	9A	A9	2.97	0.20	13.4	0.60	3.69	2.2	16.5	6.38	3.38	21.6											Flows into Pond A. All of Pond A.
	1.1b	B1.1	3.35	0.45	13.4	1.50	3.69	5.5					0.00	0	2.6				21	0 3	.2	1.1	On-grade Type R Inlet, Bypass to DP 2B
	1.2b	B1.2	1.81	0.52	12.8	0.94	3.75	3.5					0.00	0	2.6				23	5 3	.2	1.2	On-grade Type R Inlet, Bypass to DP 2B
	1.3b	B1.3	0.47	0.46	8.1	0.22	4.45	1.0															Street flow
	2b	B2	0.82	0.55	5.0	0.45	5.17	2.3	14.4	0.67	3.58	2.40											Street flow
	3b	B3	0.24	0.73	5.0	0.18	5.17	0.9															Street flow
	4b	B4	3.98	0.40	9.5	1.60	4.20	6.7					0.1	0.02	2.5				34	0 3	.2	1.8	Type R Inlet, Bypass to DP 6B
	6b	B6	3.66	0.55	6.6	2.00	4.76	9.5	14.4	2.87	3.58	10.28											Recives by-pass flows from Basins (B1.1, B1.2 and B4 ), Direct Runoff from B1.3, B2, B3, and B6
	9b	B9	3.69	0.50	13.1	1.85	3.72	6.9	14.4	3.37	3.58	12.07											Sump inlet Recives by-pass flows from (B1.1, B1.2 and B4) Direct Runoff from B1.3,82,83, B6 and B9
					Ţ		T			T				T		T	T					Ī	
	5b	B5	1.75	0.55	7.8	0.96	4.51	4.3															Street flow
	7b	B7	1.14	0.58	8.8	0.66	4.33	2.9	8.8	1.62	4.33	7.0	0.1	0.06	1.6				34	0 2	.5	2.2	On-grade Type R Inlet, Bypass to DP 8B
	8b	B8	1.74	0.56	9.3	0.97	4.24	4.1	11.0	1.03	3.99	4.1											Street Flow, Recives bypass flow from DP 7B
	10b	B10	0.22	0.73	5.0	0.16	5.17	0.8	11.0	1.19	3.99	4.7											Sump inlet revices by-pass flow from 7b and runoff from 5b,8b, and 10b

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Homestead Fil. 3     Project Name: Homestead North       Location: ElPaso County     Project Name: Homestead North       Location: ElPaso County     Calculated By: ARI       Design Storm:     5-Year       Date:     2/12/21																							
	DIRECT RUNOFF TOTAL RUNOFF													STREET/SWALE				PIPE			L TIM	E	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	11b	B11	1.77	0.15	16.8	0.27	3.35	0.9	14.4	4.83	3.58	17.3											Flow confluences into Pond B. All of Basin B
	1c	C1	2.82	0.52	13.1	1.46	3.72	5.4															
	2.3c	C2.3	0.83	0.54	10.1	0.45	4.11	1.9	13.1	1.91	3.72	7.1	0.1	0.03	1.6				1	185	2.5	1.2	On-Grade Type R Inlet, Street runoff from basin C1 and basin C2.3
	2.1C	C2.1	0.20	0.82	5.0	0.16	5.17	0.8					0.0	0	2.83				e	630	3.4	3.1	On-Grade Type R Inlet
	2.2C	C2.2	4.69	0.56	12.8	2.64	3.76	9.9	13.1	2.64	3.72	9.8											Runoff from basins 1c, 2.3c, 2.1c and 2.2c
	4.2c	C4.2	3.47	0.42	17.2	1.46	3.31	4.8					0.00	0	2.84				10	010	3.4	5.0	On-Grade Type R Inlet, by pass to 4.2c
	4C	C4.1	6.37	0.49	12.7	3.13	3.77	11.8	22.2	5.77	2.93	16.9											Sump Inlet
	3.1c	C3.1	0.35	0.68	5.0	0.24	5.17	1.2					0.00	0	2.84				1	200	3.4	1.0	On-Grade Type R inlet, By pass flow to DP 3.2c
	3.2c	C3.2	1.46	0.56	8.4	0.82	4.39	3.6	8.4	0.82	4.39	3.6											Recives by-pass flow from DP 3.1c
	5C	C5	0.16	0.74	5.0	0.12	5.17	0.6	8.4	0.94	4.39	4.1											Sump Inlet
	6C	C6	2.42	0.13	5.0	0.31	5.17	1.6	22.2	7.02	2.93	20.6											Conluenced flow for Pond C

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	Subdivision: Homestead Fil. 3 Location: El Paso County ssign Storm: 100-Year															Proj F Calc Cl	ect Nar Project N culated necked Da	ne: <u>H</u> No.: <u>2</u> By: <u>A</u> By: <u></u> Ite: <u>2</u>	omestead North 5188.00 RJ 712/21					
		DIRECT RUNOFF TOTAL RUNOFF												T/SWAI	F		PIPF			TRAVE	I TIN	ЛF		
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street/swale</sub> (cfs)	C*A (ac)	slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS	
	1a	A1	3.67	0.64	13.3	2.36	6.22	14.7					2.80	0.45 2	2.84					335	3.4	1.7	On-grade Type R Inlet, Bypass to DP 3a	
	3a	A3	4.79	0.63	13.9	3.01	6.10	18.4	14.9	3.46	5.92	20.5	6.10	1.03	2.8					110	3.3	0.5	On-grade Type R Inlet, Bypass to DP 5a	
	5a	A5	5.43	0.62	11.1	3.38	6.67	22.6	14.9	4.41	5.92	26.1											Street Flow	
	7a	A7	1.97	0.43	16.5	0.85	5.68	4.8	16.5	5.26	5.68	29.9											Flow Confluences at sump inlet	
	2a	A2	3.27	0.67	13.8	2.18	6.12	13.3					1.60	0.26 2	2.84					335	3.4	1.7	On-grade Type R Inlet, Bypass to DP 4a	
	4a	A4	3.95	0.65	14.2	2.57	6.05	15.6	15.5	2.83	5.83	16.5	3.60	0.62	2.8					110	3.3	0.5	On-grade Type R Inlet, Bypass to DP 6a	
	6a	A6	3.97	0.65	12.6	2.56	6.35	16.3	15.5	3.18	5.83	18.5											Street Flow	
	8a	A8	0.42	0.69	5.0	0.29	8.68	2.5	16.0	3.47	5.75	19.9											Flow Confluences at sump inlet	
	9A	A9	2.97	0.43	13.4	1.28	6.20	7.9	16.5	8.73	5.68	49.5											Flows into Pond A. All of Pond A.	
	1.1b	B1.1	3.35	0.60	13.4	2.01	6.20	12.5					1.50	0.24	2.6					210	3.2	1.1	On-grade Type R Inlet, Bypass to DP 2B	
	1.2b	B1.2	1.81	0.65	12.8	1.17	6.30	7.4					0.20	0.03	2.6					235	3.2	1.2	On-grade Type R Inlet, Bypass to DP 2B	
	1.3b	B1.3	0.47	0.63	8.1	0.30	7.47	2.2															Street flow	
	2b	B2	0.82	0.69	5.0	0.56	8.68	4.9	14.4	1.13	6.01	6.81											Street flow, Recives bypass flow from 1.1b, 1.2b and direct runoff from basin 1.3b	
	3b	B3	0.24	0.83	5.0	0.20	8.68	1.7															Street flow	
	4b	B4	3.98	0.57	9.5	2.26	7.06	15.9					4.1	0.58	2.5					340	3.2	1.8	Type R Inlet, Bypass to DP 6B	
	6b	B6	3.66	0.68	6.6	2.49	8.00	19.9	14.4	4.40	6.01	26.5											Recives by-pass flows from Basins (B1.1, B1.2 and B4 ), Direct Runoff from B1.3,B2,B3, and B6	
	9b	B9	3.69	0.64	13.1	2.36	6.25	14.8	14.4	5.04	6.01	30.3											Sump inlet kecives by-pass flows from [61.1, 81.2 and 84] Direct Runoff from B1.3,B2,B3, B6 and B9	
	5b	B5	1 75	0.68	7.8	1 18	7 57	89															Street flow	
#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision:	Home	stead F	il. 3													Pro	oject N Projec	ame: t No.:	Home 2518	estea 8.00	d North	1	
Location: Design Storm:	El Pas 100-Y	o Coun ear	ty													Cal (	culate Checke	ed By: ed By:	ARJ				
														Date:	2/12/	/21							
				DIF	RECT R	UNOFF			Т	OTAL R	UNOF	F	STRE	et/sw/	ALE		PI	PE	-	TRA	VEL TIN	1E	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	7b	B7	1.14	0.70	8.8	0.80	7.27	5.8	8.8	1.98	7.27	14.4	3.2	0.44	1.6					340	0 2.5	2.2	On-grade Type R Inlet, Bypass to DP 8B
	8b	B8	1.74	0.68	9.3	1.19	7.12	8.5	11.0	1.63	6.69	10.9											Street Flow, Recives bypass flow from DP 7B
	10b	B10	0.22	0.83	5.0	0.19	8.68	1.6	11.0	1.82	6.69	12.2											Sump inlet revices by-pass flow from 7b and runoff from 5b,8b, and 10b
	11b	B11	1.77	0.40	16.8	0.70	5.63	3.9	14.4	7.56	6.01	45.4											Flow confluences into Pond B. All of Basin B
	1c	C1	2.82	0.65	13.1	1.82	6.25	11.4															
	2.3c	C2.3	0.83	0.68	10.1	0.56	6.91	3.9	13.1	2.38	6.25	14.9	3.6	0.58	1.6					185	5 2.5	1.2	On-Grade Type R Inlet, Street runoff from basin C1 and basin C2.3
	2.1C	C2.1	0.20	0.90	5.0	0.18	8.68	1.6					0.1	0.01	2.83					630	0 3.4	3.1	On-Grade Type R Inlet
	2.2C	C2.2	4.69	0.68	12.8	3.21	6.32	20.3	13.1	3.22	6.25	20.1											Runoff from basins 1c, 2.3c, 2.1c and 2.2c
	4.2c	C4.2	3.47	0.58	17.2	2.02	5.56	11.2					0.70	0.13	2.84					1010	0 3.4	5.0	On-Grade Type R Inlet, by pass to 4.2c
	4C	C4.1	6.37	0.63	12.7	4.01	6.32	25.4	22.2	7.36	4.92	36.2											Sump Inlet
	3.1c	C3.1	0.35	0.79	5.0	0.28	8.68	2.4					0.60	0.07	2.84					200	0 3.4	1.0	On-Grade Type R inlet, By pass flow to DP 3.2c
	3.2c	C3.2	1.46	0.68	8.4	1.00	7.37	7.4	8.4	1.07	7.37	7.9											Recives by-pass flow from DP 3.1c
-																							
	5C	C5	0.16	0.84	5.0	0.13	8.68	1.1	8.4	1.20	7.37	8.8									+		Sump Inlet
	6C	C6	2.42	0.38	5.0	0.92	8.68	8.0	22.2	9.48	4.92	46.6											Conluenced flow for Pond C
																				<u> </u>			
	1								1											1			

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

# Appendix C Hydraulic Calculations



MHFD-Detention, Version 4.03 (May 2020)

Project: Homestead North at Sterling Ranch
Basin ID: Pond A
PERMANENT ORIFICES
POOL Example Zone Configuration (Retention Pond)

Watershed Information

ersneu miormation		
Selected BMP Type =	EDB	
Watershed Area =	30.44	acres
Watershed Length =	1,963	ft
Watershed Length to Centroid =	1,178	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	46.30%	percen
Percentage Hydrologic Soil Group A =	0.0%	percen
Percentage Hydrologic Soil Group B =	100.0%	percen
Percentage Hydrologic Soil Groups C/D =	0.0%	percen
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	re.	Optional User	Ove
Water Quality Capture Volume (WQCV) =	0.498	acre-feet		acre
Excess Urban Runoff Volume (EURV) =	1.497	acre-feet		acre
2-yr Runoff Volume (P1 = 1.19 in.) =	1.440	acre-feet	1.19	inch
5-yr Runoff Volume (P1 = 1.5 in.) =	2.088	acre-feet	1.50	inch
10-yr Runoff Volume (P1 = 1.75 in.) =	2.661	acre-feet	1.75	inch
25-yr Runoff Volume (P1 = 2 in.) =	3.451	acre-feet	2.00	inch
50-yr Runoff Volume (P1 = 2.25 in.) =	4.081	acre-feet	2.25	inch
100-yr Runoff Volume (P1 = 2.52 in.) =	4.888	acre-feet	2.52	inch
500-yr Runoff Volume (P1 = 4 in.) =	8.806	acre-feet	4.00	inch
Approximate 2-yr Detention Volume =	1.121	acre-feet		
Approximate 5-yr Detention Volume =	1.546	acre-feet		
Approximate 10-yr Detention Volume =	2.074	acre-feet		
Approximate 25-yr Detention Volume =	2.285	acre-feet		
Approximate 50-yr Detention Volume =	2.392	acre-feet		
Approximate 100-yr Detention Volume =	2.695	acre-feet		

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.498	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.999	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.197	acre-feet
Total Detention Basin Volume =	2.695	acre-feet
Initial Surcharge Volume (ISV) =	65	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.50	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel $(H_{TC})$ =	0.50	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	0.005	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	4	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	130	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	11.4	ft
Surcharge Volume Width ( $W_{ISV}$ ) =	11.4	ft
Depth of Basin Floor $(H_{FLOOR}) =$	0.95	ft
Length of Basin Floor $(L_{FLOOR}) =$	205.2	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	106.4	ft
Area of Basin Floor $(A_{FLOOR})$ =	21,836	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	7,490	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	4.05	ft
Length of Main Basin $(L_{MAIN}) =$	237.6	ft
Width of Main Basin ( $W_{MAIN}$ ) =	138.8	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	32,983	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	110,235	ft <sup>3</sup>
Calculated Total Basin Volume (V <sub>total</sub> ) =	2.706	acre-feet

8		Г		1							
		Depth Increment =	0.10	ft Optional	1		1	Optional		1	
n Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
		Top of Micropool	0.00		11.4	11.4	130		0.003		
		ISV	0.50		11.4	11.4	130		0.003	65	0.001
			0.60		11.4	11.4	130		0.003	78	0.002
			0.70		11.4	11.4	130		0.003	91	0.002
			0.80		11.4	11.4	130		0.003	104	0.002
			0.90		11.4	11.4	130		0.003	117	0.003
			1.00		11.4	11.4	130		0.003	130	0.003
			1 10		31.8	21.4	681		0.016	167	0.004
			1.10		52.2	31.4	1.640		0.038	280	0.006
			1.20		72.4	41.4	2 007		0.050	500	0.000
			1.30		72.0	41.4	3,007		0.007	307	0.012
			1.40		93.0	51.4	4,782		0.110	895	0.021
			1.50		113.4	61.4	6,964		0.160	1,479	0.034
			1.60		133.8	71.4	9,555		0.219	2,301	0.053
			1.70		154.2	81.4	12,554		0.288	3,404	0.078
Optional Use	r Overrides		1.80		174.6	91.4	15,961		0.366	4,826	0.111
	acre-feet		1.90		195.0	101.4	19,776		0.454	6,609	0.152
	acre-feet	Floor	1.95		205.2	106.4	21,836		0.501	7,649	0.176
1.19	inches		2.00		205.6	106.8	21,961		0.504	8,744	0.201
1.50	inches		2.10		206.4	107.6	22,212		0.510	10,953	0.251
1.75	inches		2.20		207.2	108.4	22,464		0.516	13,187	0.303
2.00	inches		2.30		208.0	109.2	22,717		0.522	15,446	0.355
2.25	inches		2.40		208.8	110.0	22,971		0.527	17,730	0.407
2.52	inches		2.50		209.6	110.8	23.227		0.533	20.040	0.460
4.00	inches	Zone 1 (WOCV)	2.58		210.2	111.4	23.432		0.538	21.906	0.503
	<b>1</b>	(	2.60		210.4	111.6	23.484		0.539	22.375	0.514
			2 70		211.7	112 /	23 742		0.545	24 727	0.569
			2.10		211.2	112.4	23,142		0.040	27,137	0.008
			2.00		212.0	114.0	24,002		0.001	21,124	0.023
			2.90		212.8	114.0	24,262		0.55/	29,53/	0.678
		<u>├</u>	3.00		213.6	114.8	24,525		0.563	31,976	U./34
			3.10		214.4	115.6	24,788		0.569	34,442	0.791
			3.20		215.2	116.4	25,053		0.575	36,934	0.848
			3.30		216.0	117.2	25,318		0.581	39,452	0.906
			3.40		216.8	118.0	25,586		0.587	41,998	0.964
			3.50		217.6	118.8	25,854		0.594	44,570	1.023
			3.60		218.4	119.6	26,124		0.600	47,169	1.083
			3.70		219.2	120.4	26,395		0.606	49,794	1.143
			3.80		220.0	121.2	26,667		0.612	52,448	1.204
			3.90		220.8	122.0	26.941		0.618	55,128	1.266
			4.00		221.6	122.8	27.216		0.625	57.836	1.328
			4 10		222.4	123.6	27 492		0.631	60.571	1 391
			1.10		222.1	124.4	27,760		0.637	63 334	1.071
		Zopo 2 (ELIDV)	4.27		220.2	125.0	27,064		0.642	45 295	1.400
		ZONE Z (LONV)	4.20		223.0	125.0	20,049		0.644	44 125	1.477
			4.30		224.0	123.2	20,040		0.044	00,125	1.510
			4.40		224.0	126.0	20,320		0.650	06,944	1.563
			4.50		225.6	126.8	28,610		0.657	/1,/91	1.648
			4.60		226.4	127.6	28,892		0.663	/4,666	1./14
			4.70		227.2	128.4	29,176		0.670	77,569	1.781
			4.80		228.0	129.2	29,461		0.676	80,501	1.848
			4.90		228.8	130.0	29,748		0.683	83,462	1.916
			5.00		229.6	130.8	30,035		0.690	86,451	1.985
			5.10		230.4	131.6	30,324		0.696	89,469	2.054
			5.20		231.2	132.4	30,614		0.703	92,516	2.124
			5.30		232.0	133.2	30,906		0.710	95,592	2.194
			5.40		232.8	134.0	31,199		0.716	98,697	2.266
			5.50		233.6	134.8	31,493		0.723	101,831	2.338
			5.60		234.4	135.6	31,788		0.730	104,995	2.410
			5.70		235.2	136.4	32,085		0.737	108,189	2.484
			5.80		236.0	137.2	32,383		0.743	111,412	2.558
			5.90		236.8	138.0	32,682		0.750	114,666	2.632
		Zone 3 (100-year)	5.99		237.5	138.7	32,952		0.756	117,619	2.700
		<u> </u>	6.10		237.0	139.6	33,284		0.764	121,262	2.784
		L	6.20		239.2	140.4	33,587		0.771	124,606	2.861
			6.30		240.0	141.2	33,892		0.785	127,980	2.938
			6.50		241.6	142.8	34,504		0.792	134,819	3.095
			6.60		242.4	143.6	34,812		0.799	138,285	3.175
			6.80		243.2 244.0	144.4	35,122		0.806	141,/82	3.255
			6.90		244.8	146.0	35,745		0.821	148,868	3.418
		$\vdash$	7.00		245.6	146.8	36,058		0.828	152,459	3.500
			7.20		246.4	147.6	36,373		0.835	156,080	3.583
			7.30		248.0	149.2	37,006		0.850	163,418	3.752
		<u> </u>	7.40		248.8	150.0	37,324		0.857	167,134	3.837
			7.60		249.0 250.4	150.8	37.965		0.804	174.663	3.923
			7.70		251.2	152.4	38,287		0.879	178,476	4.097
			7.80		252.0	153.2	38,610		0.886	182,320	4.185
			8.00		252.8	154.0	30,935		0.894	190,198	4.275
			8.10		254.4	155.6	39,589		0.909	194,050	4.455
		<b>⊢</b>	8.20		255.2	156.4	39,917		0.916	198,025	4.546
			8.40		256.0 256.8	157.2	40,247		0.924	202,033	4.038
			8.50		257.6	158.8	40,911		0.939	210,149	4.824
			8.60		258.4	159.6	41,245		0.947	214,257	4.919
			8.80		259.2 260.0	160.4	41,580 41.916		0.962	218,398 222.573	5.014
			8.90		260.8	162.0	42,254		0.970	226,781	5.206
		L	9.00		261.6	162.8	42,593		0.978	231,024	5.304
			9.10		262.4	163.6	42,933 43.274		0.986	235,300	5.402
			9.30		264.0	165.2	43,617		1.001	243,955	5.600
		<u> </u>	9.40		264.8	166.0	43,961		1.009	248,334	5.701
			9.60		266.4	167.6	44,653		1.025	257.195	5.902
			9.70		267.2	168.4	45,001		1.033	261,678	6.007
		1	9.80		268.0	169.2	45,350		1.041	266,195	6.111

MHFD-Detention, Version 4.03 (May 2020)



MHFD-Detention, Version 4.03 (May 2020 Project: Homestead North at Sterling Ranch Basin ID: Pond A Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type 2.58 0.498 Orifice Plate 4.27 0.999 Orifice Plate 100-YEAR V. ZONE 1 AND 2 ORIFICES Weir&Pipe (Restrict) 5.99 1.197 Ir) Example Zone Configuration Total (all zones) 2.695 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain Underdrain Orifice Area Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) ft<sup>2</sup> Underdrain Orifice Centroid Underdrain Orifice Diameter inches feet User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row N/A  $ft^2$ Depth at top of Zone using Orifice Plate 4.27 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width N/A feet Orifice Plate: Orifice Vertical Spacing N/A inches Elliptical Slot Centroid N/A feet ft<sup>2</sup> Orifice Plate: Orifice Area per Row N/A inches Elliptical Slot Area N/A User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (required)Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) 0.00 1.42 2.85 3.85 Orifice Area (sq. inches) 2.11 2 11 2 11 24 00 Row 9 (optional) low 10 (optional Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A N/A N/A N/A Depth at top of Zone using Vertical Orifice N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid feet Vertical Orifice Diameter N/A N/A inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho 4.30 N/A ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, Ht = 5.55 N/A feet Overflow Weir Front Edge Length 5.00 N/A feet Overflow Weir Slope Length 5.15 N/A feet Overflow Weir Grate Slope 4.00 N/A H:V Grate Open Area / 100-yr Orifice Area 7.74 N/A Horiz, Length of Weir Sides 19.33 ft<sup>2</sup> 5.00 N/A feet Overflow Grate Open Area w/o Debris N/A Overflow Grate Open Area % 75% N/A %. grate open area/total area Overflow Grate Open Area w/ Debris 9.66 N/A Debris Clogging % = 50% N/A User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate one 3 Restricto Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe 2.00 N/A Outlet Orifice Area 2.50 ft (distance below basin bottom at Stage = 0 ft) N/A Outlet Pipe Diameter : 24.00 N/A inches Outlet Orifice Centroid 0.82 N/A feet Restrictor Plate Height Above Pipe Invert = 17.80 Half-Central Angle of Restrictor Plate on Pipe N/A radians inches 2.08 User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= 6 10 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.91 feet Stage at Top of Freeboard Spillway Crest Length 23.00 feet 8.01 feet 4.00 H:V Basin Area at Top of Freeboard 0.90 Spillway End Slopes acres Freeboard above Max Water Surface = Basin Volume at Top of Freeboard 1.00 feet 4.37 acre-ft Routed Hydrograph Results The user can override the de ult CUHP hydrog phs and runoff volumes by entering new values in the Inflow Hydrographs ta Columns W thro uah AF 50 Year Design Storm Return Period WOCY FUR\ Yea S Ye 10 Year 5 Ye 100 Ye 500 Yea One-Hour Rainfall Depth (in) N/A N/A 1.19 1.50 1.75 2.00 2.52 4.00 2.25 CUHP Runoff Volume (acre-ft) 0.498 1.497 1.440 2.088 2.661 3.451 4.081 4.888 8.806 Inflow Hydrograph Volume (acre-ft) N/A 1.440 3.451 N/A 2.088 4.888 8.806 2.661 4.081 CUHP Predevelopment Peak Q (cfs) N/A N/A 7.9 12.0 21.6 34.8 2.8 27.2 68.5 PTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.09 0.26 0.40 0.71 0.89 1.14 2.25 Peak Inflow Q (cfs) N/A N/A 48.4 119.5 19.2 28.5 35.5 57.1 67.9 Peak Outflow Q (cfs) 0.2 0.9 0.7 3.9 9.0 18.4 25.7 89.8 32.2 Ratio Peak Outflow to Predevelopment Q N/A N/A N/A 05 07 0.8 0.9 0.9 Structure Controlling Flow Plate Plate Plate Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Outlet Plate 1 Spillway Max Velocity through Grate 1 (fps) N/A N/A N/A 0.1 0.4 0.9 1.7 1.2 1.6 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 38 75 76 74 73 71 62 19 182 Time to Drain 99% of Inflow Volume (hours) 40 79 82 81 80 80 76 Maximum Ponding Depth (ft) 4.27 2.584.04 4.70 5.01 5.38 5.61 6.00 6.91 Area at Maximum Ponding Depth (acres) 0.54 0.64 0.63 0.67 0.69 0.71 0.73 0.76 0.82 1 353 Maximum Volume Stored (acre-ft) 0 503 1 4 9 9 1.774 1 985 2 251 2 708

3 418

2 418



minimum bound maximum bound

Outflow Hydrograph Workbook Filename:

	he user can o	verride the calcul	lated inflow hydr	ographs from thi	is workbook with	inflow hydrogra	phs developed in	a separate progr	am.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	0.02	1.31
	0:15:00	0.00	0.00	1.51	2.47	3.07	2.06	2.60	2.52	5.34
	0:20:00	0.00	0.00	5.58	7.43	9.27	5.55	6.50	6.93	13.75
	0.25.00	0.00	0.00	13.54	20.45	20.80	37.38	15.84	50.89	40.83 94.87
	0:35:00	0.00	0.00	19.23	28.10	34.63	47.43	56.27	66.87	119.06
	0:40:00	0.00	0.00	17.82	25.57	31.54	48.41	57.08	67.89	119.48
	0:45:00	0.00	0.00	15.70	22.67	28.33	45.04	53.05	64.60	113.15
	0:50:00	0.00	0.00	13.89	20.40	25.35	41.53	48.88	59.57	104.45
	1:00:00	0.00	0.00	12.41	16.19	22.73	37.06	43.72	54.26	95.34
	1:05:00	0.00	0.00	9.87	14.23	20.33	29.14	34 52	49.52	79.33
	1:10:00	0.00	0.00	8.69	12.90	16.77	24.93	29.58	38.26	68.10
	1:15:00	0.00	0.00	7.78	11.78	15.82	21.83	26.00	32.76	59.21
	1:20:00	0.00	0.00	7.05	10.64	14.45	19.06	22.70	27.89	50.52
10	) 1:25:00	0.00	0.00	6.39	9.57	12.74	16.67	19.83	23.67	42.77
	1:30:00	0.00	0.00	5.76	8.56	0.50	14.32	16.98	20.04	36.10
	1:40:00	0.00	0.00	4.54	6.43	8.20	10.12	11.91	13.66	24.45
	1:45:00	0.00	0.00	4.01	5.36	6.99	8.27	9.68	10.88	19.41
	1:50:00	0.00	0.00	3.63	4.59	6.17	6.66	7.75	8.53	15.37
	1:55:00	0.00	0.00	3.18	4.15	5.61	5.60	6.52	6.97	12.82
	2:00:00	0.00	0.00	2.83	3.81	5.07	4.96	5.77	6.01	11.19
	2:03:00	0.00	0.00	2.32	3.12	4.15	3.95	4.59	4.68	8.77
	2:15:00	0.00	0.00	1.47	1.95	2.61	2.38	2.75	2.66	5.00
	2:20:00	0.00	0.00	1.16	1.54	2.04	1.84	2.11	1.97	3.72
	2:25:00	0.00	0.00	0.91	1.21	1.58	1.42	1.62	1.47	2.77
	2:30:00	0.00	0.00	0.71	0.93	1.20	1.08	1.24	1.12	2.10
	2:35:00	0.00	0.00	0.56	0.71	0.91	0.82	0.93	0.85	1.58
	2:40:00	0.00	0.00	0.43	0.54	0.69	0.62	0.71	0.65	0.94
	2:50:00	0.00	0.00	0.24	0.30	0.40	0.36	0.41	0.39	0.71
	2:55:00	0.00	0.00	0.17	0.21	0.28	0.26	0.30	0.28	0.51
	3:00:00	0.00	0.00	0.11	0.14	0.19	0.18	0.20	0.19	0.34
	3:05:00	0.00	0.00	0.07	0.09	0.11	0.11	0.13	0.12	0.21
	3:10:00	0.00	0.00	0.03	0.05	0.06	0.06	0.07	0.06	0.11
	3:20:00	0.00	0.00	0.00	0.02	0.02	0.02	0.00	0.02	0.04
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
250	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
200	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
150 5	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
No	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
LI LI	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 100	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 50	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10.00	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

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Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Агеа	Area	Volume	Volume	Total	
Description	[ft]	[ft <sup>2</sup> ]	[acres]	[ft <sup>3</sup> ]	[ac-ft]	[cfs]	
							For best results, include the
							changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverte of all
							outlets (e.g. vertical orifice
							overflow grate, and spillway,
							where applicable).
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ORIFICE

Depth Increment = 0.10 ft ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond)

Watershed	Information
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Selected BMP Type =	EDB	
Watershed Area =	24.73	acres
Watershed Length =	1,290	ft
Watershed Length to Centroid =	775	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	51.10%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.431	acre-feet
Excess Urban Runoff Volume (EURV) =	1.353	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.273	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.812	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.284	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.915	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.428	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.078	acre-feet
500-yr Runoff Volume (P1 = 4 in.) =	7.262	acre-feet
Approximate 2-yr Detention Volume =	1.023	acre-feet
Approximate 5-yr Detention Volume =	1.400	acre-feet
Approximate 10-yr Detention Volume =	1.848	acre-feet
Approximate 25-yr Detention Volume =	2.020	acre-feet
Approximate 50-yr Detention Volume =	2.111	acre-feet
Approximate 100-yr Detention Volume =	2.350	acre-feet

Define	Zones	and	Basi	n	Geome	etry
		7	one	1	Volume	(W

Zone 1 Volume (WQCV) =	0.431	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.922	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.997	acre-feet
Total Detention Basin Volume =	2.350	acre-feet
Initial Surcharge Volume (ISV) =	56	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.50	ft
Total Available Detention Depth (H <sub>total</sub> ) =	5.00	ft
Depth of Trickle Channel $(H_{TC}) =$	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.010	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	113	ft 2
Surcharge Volume Length $(L_{ISV}) =$	10.6	ft
Surcharge Volume Width $(W_{ISV}) =$	10.6	ft
Depth of Basin Floor $(H_{FLOOR}) =$	2.81	ft
Length of Basin Floor $(L_{FLOOR}) =$	302.9	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	151.1	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	45,767	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	45,101	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	1.19	ft
Length of Main Basin ( $L_{MAIN}$ ) =	312.4	ft
Width of Main Basin ( $W_{MAIN}$ ) =	160.6	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	50,179	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	57,068	ft <sup>3</sup>

Calculated Total Basin Volume (Vtotal) = 2.348 acre-feet

on Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		Description Top of Micropool	(ft)	Stage (ft)	(ft) 10.6	(ft)	(ft <sup>2</sup> )	Area (ft ')	(acre)	(ft ')	(ac-ft)
			0.00		10.0	10.0	113		0.003	57	0.001
		150	0.50		10.0	10.6	113		0.003	00	0.001
			0.60		10.6	10.6	113		0.003	68 70	0.002
			0.80		10.6	10.6	113		0.003	90	0.002
			0.90		10.6	10.6	113		0.003	101	0.002
			1.00		10.6	10.6	113		0.003	113	0.003
			1.10		21.0	15.6	328		0.008	134	0.003
			1.20		31.4	20.6	648		0.015	182	0.004
			1.30		41.8	25.6	1,071		0.025	267	0.006
			1.40		52.2	30.6	1,599		0.037	400	0.009
			1.50		72.0	30.0	2,230		0.069	840	0.014
			1.00		83.4	40.0	3,805		0.087	1,187	0.019
Optional Use	r Overrides		1.80		93.8	50.6	4,749		0.109	1,614	0.037
	acre-feet		1.90		104.2	55.6	5,796		0.133	2,140	0.049
	acre-feet		2.00		114.6	60.6	6,948		0.159	2,776	0.064
1.19	inches		2.10		125.0	65.6	8,203		0.188	3,533	0.081
1.50	inches		2.20		135.4	70.6	9,563		0.220	4,420	0.101
1.75	inches		2.30		145.8	75.6	11,026		0.253	5,449	0.125
2.00	inches		2.40		156.2	80.6	12,594		0.289	0,029	0.152
2.23	inches		2.50		177.0	90.6	16.041		0.327	9.486	0.183
4.00	inches		2.00		187.4	95.6	17.920		0.411	11.183	0.257
	1		2.80		197.8	100.6	19,904		0.457	13,073	0.300
			2.90		208.2	105.6	21,991		0.505	15,167	0.348
			3.00		218.6	110.6	24,183		0.555	17,475	0.401
		Zone 1 (WQCV)	3.06		224.9	113.6	25,548		0.586	18,967	0.435
			3.10		229.0	115.6	26,478		0.608	20,007	0.459
			3.20		239.4	120.6 12F 4	28,878		0.663	22,114	0.523
			3.30		249.8	125.0	31,381		0.720	29,780	0.592
			3.50		270.6	135.6	36,700		0.843	32.587	0.748
			3.60		281.0	140.6	39,516		0.907	36,397	0.836
			3.70		291.4	145.6	42,435		0.974	40,494	0.930
			3.80		301.8	150.6	45,459		1.044	44,888	1.030
		Floor	3.81		302.9	151.1	45,767		1.051	45,344	1.041
		-	3.90		303.6	151.8	46,094		1.058	49,477	1.136
			4.00		304.4	152.6	46,459		1.067	54,105	1.242
		Zope 2 (FLIRV)	4.10		305.2	153.4	46,825		1.075	59,769	1.349
		20110 2 (20111)	4.20		306.0	154.2	47,193		1.070	63 470	1.457
			4.30		306.8	155.0	47,562		1.092	68,208	1.566
			4.40		307.6	155.8	47,932		1.100	72,983	1.675
			4.50		308.4	156.6	48,303		1.109	77,794	1.786
			4.60		309.2	157.4	48,676		1.117	82,643	1.897
			4.70		310.0	158.2	49,050		1.126	87,530	2.009
			4.80		310.8	159.0	49,425		1.135	92,453	2.122
		Zone 3 (100-year)	4.90		312.4	160.6	50.179		1.143	102.414	2.230
			5.10		313.2	161.4	50,558		1.161	107,450	2.467
			5.20		314.0	162.2	50,939		1.169	112,525	2.583
			5.30		314.8	163.0	51,320		1.178	117,638	2.701
			5.40		315.6	163.8	51,703		1.187	122,789	2.819
			5.50		316.4	164.6	52,087		1.196	127,979	2.938
			5.60		317.2	165.4	52,473		1.205	133,207	3.058
			5.80		318.8	167.0	53.247		1.222	143.779	3.301
			5.90		319.6	167.8	53,637		1.231	149,123	3.423
			6.00		320.4 321.2	168.6 169.4	54,027 54,419		1.240	154,506	3.547 3.671
			6.20		322.0	170.2	54,812		1.258	165,390	3.797
			6.30		322.8 323.6	171.0 171.8	55,207 55,602		1.267	170,891 176,431	3.923 4.050
			6.50		324.4	172.6	55,999		1.286	182,012	4.178
			6.70		325.2 326.0	174.2	56,797		1.295	193,291	4.437
			6.80		326.8	175.0	57,198		1.313	198,991	4.568
			7.00		328.4	176.6	58,003		1.332	210,511	4.833
			7.10		329.2	177.4	58,408 58,814		1.341	216,332	4.966
			7.30		330.8	179.0	59,221		1.360	228,094	5.236
			7.40		331.6 332.4	179.8	59,630 60.039		1.369	234,037 240.020	5.373
			7.60		333.2	181.4	60,451		1.388	246,045	5.648
			7.70		334.0 334.8	182.2	61,276		1.397	252,110	5.928
			7.90		335.6	183.8	61,691		1.416	264,366	6.069
			8.10		337.2	185.4	62,525		1.435	276,787	6.354
			8.20		338.0 338.8	186.2 187.0	62,944 63.364		1.445	283,061 289,376	6.498
			8.40		339.6	187.8	63,785		1.464	295,734	6.789
			8.50		340.4 341.2	188.6 189.4	64,208 64,631		1.474	302,133 308,575	6.936 7.084
			8.70		342.0	190.2	65,057		1.493	315,060	7.233
			8.80		342.8 343.6	191.0 191.8	65,483 65,911		1.503	321,587 328,156	7.383
			9.00		344.4	192.6	66,340		1.523	334,769	7.685
			9.10		345.2 346.0	193.4 194.2	67,201		1.533	341,424 348,123	7.992
			9.30		346.8	195.0	67,634		1.553	354,864	8.147
			9.40 9.50		347.0	195.8	68,504		1.563	368,478	8.459
			9.60		349.2	197.4	68,940		1.583	375,350	8.617
			9.80		350.8	199.0	69,818		1.603	389,226	8.935
		1	9.90		351.6	199.8	70,258		1.613	396.230	9.096

MHFD-Detention, Version 4.03 (May 2020)





Elliptical Slot Centroid =

Elliptical Slot Area =

feet

ft<sup>2</sup>

N/A

N/A

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

0.91

1.34

4.93

Calculated Parameters for Spillway 0.91 feet

feet

acres

acre-ft

Underdrain Orifice Area = N/A ft (distance below the filtration media surface) ft<sup>2</sup> Underdrain Orifice Invert Depth N/A Underdrain Orifice Diameter = N/A inches Underdrain Orifice Centroid = N/A feet User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row N/A ft<sup>2</sup> 0.00 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = N/A feet

inches

inches

Depth at top of Zone using Orifice Plate = 4.11 Orifice Plate: Orifice Vertical Spacing = N/A Orifice Plate: Orifice Area per Row = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	low 4 (optional	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	ow 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.37	2.74	3.20				
Orifice Area (sq. inches)	1.40	1.40	1.40	9.00				
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	ow 12 (optiona	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	ow 16 (optional
Stage of Orifice Centroid (ft)								
Orifice Area (sg. inches)								

User Input: Vertical Orifice (Circular or Rectangula	Calculated Parameters for Vertical Orific					
	Not Selected	Not Selected		Not Selected	Not Selected	
Invert of Vertical Orifice =		N/A	ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area =		N/A 1	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid =		N/A 1	feet
Vertical Orifice Diameter =		N/A	inches			

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).										
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected					
Overflow Weir Front Edge Height, Ho =	4.11	N/A	ft (relative to basin bottom at Stage = $0Hp$ ight of Grate Upper Edge, H <sub>t</sub> =	4.11	N/A	feet				
Overflow Weir Front Edge Length =	5.00	N/A	feet Overflow Weir Slope Length =	5.00	N/A	feet				
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	5.76	N/A					
Horiz. Length of Weir Sides =	5.00	N/A	feet Overflow Grate Open Area w/o Debris =	17.50	N/A	ft <sup>2</sup>				
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Overflow Grate Open Area w/ Debris =	5.25	N/A	ft <sup>2</sup>				
Debris Clogging % =	70%	N/A	%							

User Ir	nput:	Outlet	Pipe \	N/ F	low	Restriction	Plate	(Circular	Orifice,	Restrictor	Plate,	or	Rectang	ular	Orifice)	

	one 3 Restricto	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft) Outlet Orific	ce Area =	3.04	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	33.00	N/A	inches Outlet Orifice C	entroid =	0.80	N/A	feet
Restrictor Plate Height Above Pipe Invert =	16.80		inches Half-Central Angle of Restrictor Plate	on Pipe =	1.59	N/A	radians

## User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	5.16	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	
Spillway Crest Length =	23.00	feet	Stage at Top of Freeboard =	
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	
		-	-	

Bouted Hydrograph Bosults	The user can	ovorrido the defau	It CHUD bydrograp	he and runoff	volumos hv ontorini	a now values in the	Inflow Hydrograph	be table (Colur	pps (4/ through AE)
Rouled Hydrograph Results	The user carro		п соне пушоўгар.	ns and runon	volumes by emering	Thew values in the	е ттом нушоўгарі	is lable (Colui	nns w unouyn Ar).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	4.00
CUHP Runoff Volume (acre-ft) =	0.431	1.353	1.273	1.812	2.284	2.915	3.428	4.078	7.262
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.273	1.812	2.284	2.915	3.428	4.078	7.262
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	2.7	7.7	11.6	20.6	25.8	33.0	64.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.31	0.47	0.83	1.04	1.34	2.62
Peak Inflow Q (cfs) =	N/A	N/A	21.0	30.6	37.5	49.0	57.7	68.7	119.9
Peak Outflow Q (cfs) =	0.2	0.5	0.5	2.9	6.5	13.8	19.3	26.7	71.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.7	0.8	1.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	verflow Weir	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	verflow Weir	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.3	0.8	1.1	1.5	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	68	68	72	70	68	67	65	55
Time to Drain 99% of Inflow Volume (hours) =	42	72	71	76	76	75	75	74	70
Maximum Ponding Depth (ft) =	3.06	4.11	3.96	4.31	4.48	4.75	4.91	5.15	5.80
Area at Maximum Ponding Depth (acres) =	0.59	1.08	1.06	1.09	1.11	1.13	1.14	1.17	1.22
Maximum Volume Stored (acre-ft) =	0.435	1.360	1.189	1.577	1.764	2.055	2.248	2.525	3.288







Outflow Hydrograph Workbook Filename:

		Inflow Hydrog	<u>irapns</u>								
		The user can ov	verride the calcul	ated inflow hydr	ographs from thi	s workbook with	inflow hydrogra	phs developed in	a separate progra	am.	
		SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	me Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
	5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		0.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		0.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.23	0.02	1.70
		0:15:00	0.00	0.00	1.98	3.24	4.02	2.70	3.37	3.29	6.71
		0:20:00	0.00	0.00	7.03	9.26	11.39	6.86	7.99	8.56	16.49
		0:25:00	0.00	0.00	16.22	23.99	31.04	15.92	18.80	20.87	46.11
		0:30:00	0.00	0.00	21.04	30.58	37.52	42.14	50.19	56.78	102.80
		0:35:00	0.00	0.00	19.65	27.93	33.93	49.02	57.73	68.74	119.90
		0:40:00	0.00	0.00	17.24	23.97	29.19	46.99	55.03	65.36	113.04
		0:45:00	0.00	0.00	14.41	20.36	25.26	41.20	48.24	59.02	102.02
		0:50:00	0.00	0.00	12.07	17.45	21.34	36.87	43.17	52.57	90.73
		0:55:00	0.00	0.00	10.18	14.61	18.05	30.88	36.21	45.31	78.28
		1:00:00	0.00	0.00	8.92	12.71	16.03	25.78	30.32	39.24	68.31
		1:05:00	0.00	0.00	8.04	11.38	14.57	22.52	26.59	35.44	61.90
		1:10:00	0.00	0.00	6.85	10.17	13.19	19.04	22.51	29.22	51.57
		1:15:00	0.00	0.00	5.75	8.68	11.82	15.96	18.93	23.67	42.36
		1:20:00	0.00	0.00	4.75	7.12	9.91	12.79	15.14	18.24	32.54
2		1:25:00	0.00	0.00	3.94	5.85	7.86	10.05	11.86	13.58	24.18
J		1:30:00	0.00	0.00	3.45	5.14	6.63	7.51	8.85	9.83	17.81
		1:35:00	0.00	0.00	3.23	4.79	5.92	6.04	7.09	7.62	13.97
	1	1:40:00	0.00	0.00	3.11	4.26	5.41	5.13	5.99	6.29	11.58
		1:45:00	0.00	0.00	3.05	3.84	5.05	4.54	5.27	5.36	9.90
		1:50:00	0.00	0.00	3.00	3.54	4.80	4.14	4.78	4.72	8.75
		1:55:00	0.00	0.00	2.63	3.31	4.49	3.88	4.45	4.27	7.92
		2:00:00	0.00	0.00	2.31	3.05	4.03	3.70	4.22	3.96	7.34
		2:05:00	0.00	0.00	1.75	2.30	3.02	2.78	3.17	2.93	5.42
		2:10:00	0.00	0.00	1.30	1.69	2.19	2.03	2.30	2.13	3.92
		2:15:00	0.00	0.00	0.95	1.23	1.58	1.48	1.67	1.56	2.85
		2:20:00	0.00	0.00	0.69	0.89	1.15	1.08	1.22	1.15	2.09
		2:25:00	0.00	0.00	0.50	0.63	0.82	0.76	0.86	0.82	1.49
		2:30:00	0.00	0.00	0.35	0.43	0.58	0.54	0.61	0.58	1.05
		2:35:00	0.00	0.00	0.24	0.30	0.40	0.38	0.43	0.41	0.74
		2:40:00	0.00	0.00	0.15	0.20	0.26	0.25	0.29	0.27	0.49
		2:45:00	0.00	0.00	0.08	0.12	0.15	0.15	0.17	0.16	0.29
		2:50:00	0.00	0.00	0.04	0.06	0.07	0.07	0.08	0.08	0.14
		2:55:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.03	0.04
		3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3.20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0		3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5.20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	]	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond)

ORIFICE

Depth Increment = 0.10 ft

Watershed	Information

PERMA

itersned information		
Selected BMP Type =	EDB	
Watershed Area =	22.77	acres
Watershed Length =	1,580	ft
Watershed Length to Centroid =	948	ft
Watershed Slope =	0.021	ft/ft
Watershed Imperviousness =	60.80%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	3.1	
Water Quality Capture Volume (WQCV) =	0.453	acre-feet
Excess Urban Runoff Volume (EURV) =	1.503	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.395	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.923	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.376	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.946	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.429	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.022	acre-feet
500-yr Runoff Volume (P1 = 4 in.) =	6.989	acre-feet
Approximate 2-yr Detention Volume =	1.158	acre-feet
Approximate 5-yr Detention Volume =	1.561	acre-feet
Approximate 10-yr Detention Volume =	2.008	acre-feet
Approximate 25-yr Detention Volume =	2.170	acre-feet
Approximate 50-yr Detention Volume =	2.262	acre-feet
Approximate 100-yr Detention Volume =	2.465	acre-feet

Define	Zones	and	Basi	n	Geome	etry
		7	one	1	Volume	(W

Zone 1 Volume (WQCV) =	0.453	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.050	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.962	acre-feet
Total Detention Basin Volume =	2.465	acre-feet
Initial Surcharge Volume (ISV) =	59	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.50	ft
Total Available Detention Depth (H <sub>total</sub> ) =	5.00	ft
Depth of Trickle Channel $(H_{TC}) =$	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	118	ft 2
Surcharge Volume Length ( $L_{ISV}$ ) =	10.9	ft
Surcharge Volume Width (WISV) =	10.9	ft
Depth of Basin Floor $(H_{FLOOR}) =$	1.11	ft
Length of Basin Floor $(L_{FLOOR}) =$	237.3	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	121.9	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	28,926	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	11,431	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	2.89	ft
Length of Main Basin ( $L_{MAIN}$ ) =	260.4	ft
Width of Main Basin ( $W_{MAIN}$ ) =	145.0	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	37,765	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	96,086	ft <sup>3</sup>

Area of Main Basin (A <sub>MAIN</sub> ) =	37,765	n -
Volume of Main Basin ( $V_{MAIN}$ ) =	96,086	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	2.471	acre-feet

ion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		Description Top of Micropool	(ft)	stage (ff)	(ft) 10.9	(ft) 10.9	(Π <sup>-</sup> ) 119	Area (ft *)	(acre)	(π-)	(ac-π)
			0.00		10.7	10.7	110		0.003	50	0.004
		ISV	0.50		10.9	10.9	118		0.003	59	0.001
			0.60		10.9	10.9	118		0.003	71	0.002
			0.70		10.9	10.9	118		0.003	83	0.002
			0.80		10.9	10.9	118		0.003	95	0.002
			0.90		10.9	10.9	118		0.003	107	0.002
			1.00		10.9	10.9	118		0.003	118	0.003
			1.10		31.3	20.9	003		0.015	104	0.004
			1.20		72.1	40.9	2 947		0.057	203	0.000
			1.30		92.5	40.9	4 706		0.008	400	0.011
			1.50		112.9	60.9	6.873		0.158	1 441	0.033
			1.60		133.3	70.9	9.448		0.217	2.254	0.052
			1.70		153.7	80.9	12,431		0.285	3,344	0.077
Optional Use	er Overrides		1.80		174.1	90.9	15,821		0.363	4,754	0.109
	acre-feet		1.90		194.5	100.9	19,620		0.450	6,522	0.150
	acre-feet		2.00		214.9	110.9	23,827		0.547	8,691	0.200
1.19	inches		2.10		235.3	120.9	28,442		0.653	11,301	0.259
1.50	inches	Floor	2.11		237.3	121.9	28,926		0.664	11,588	0.266
1.75	inches		2.20		238.0	122.6	29,185		0.670	14,203	0.326
2.00	inches	7 4 (1100) 0	2.30		238.8	123.4	29,474		0.677	17,136	0.393
2.25	inches	Zone T (WQCV)	2.39		239.6	124.1	29,736		0.683	19,801	0.455
4.00	inches		2.40		240.4	124.2	30.056		0.690	23,099	0.530
4.00	indires.		2.60		241.2	125.8	30,349		0.697	26,109	0.599
			2.70		242.0	126.6	30,644		0.703	29,159	0.669
			2.80		242.8	127.4	30,939		0.710	32,238	0.740
			2.90		243.6	128.2	31,236		0.717	35,347	0.811
			3.00		244.4	129.0	31,534		0.724	38,485	0.884
			3.10		245.2	129.8	31,834		0.731	41,654	0.956
			3.20		246.0	130.6	32,134		0.738	44,852	1.030
			3.30		246.8	131.4	32,436		0.745	48,081	1.104
			3.40		247.6	132.2	32,740		0.752	51,340	1.179
			3.50		248.4	133.0	33,044		0.759	54,629	1.254
			3.60		249.2	133.8	33,350		0.766	57,948	1.330
			3.70		250.0	134.0	33,037		0.7790	64.690	1.407
		Zone 2 (ELIRV)	3.83		250.0	135.4	34.058		0.782	65 700	1.403
		2010 2 (2010)	3.90		251.6	136.2	34,275		0.782	68.092	1.563
			4.00		252.4	137.0	34,586		0.794	71,535	1.642
			4.10		253.2	137.8	34,898		0.801	75,009	1.722
			4.20		254.0	138.6	35,212		0.808	78,515	1.802
			4.30		254.8	139.4	35,526		0.816	82,051	1.884
			4.40		255.6	140.2	35,842		0.823	85,620	1.966
			4.50		256.4	141.0	36,160		0.830	89,220	2.048
			4.60		257.2	141.8	36,478		0.837	92,852	2.132
			4.70		258.0	142.6	36,798		0.845	96,516	2.216
			4.80		208.8	143.4	37,119		0.852	100,211	2.301
		Zone 3 (100 year)	4.90		259.0	144.2	37,442		0.860	103,939	2.380
		Lone o (roo year)	5.10		261.2	145.8	38,090		0.874	111,493	2.560
			5.20		262.0	146.6	38,417		0.882	115,318	2.647
			5.30		262.8	147.4	38,744		0.889	119,176	2.736
			5.40		263.6	148.2	39,073		0.897	123,067	2.825
			5.50		264.4	149.0	39,403		0.905	126,991	2.915
			5.60		265.2	149.8	39,735		0.912	130,948	3.006
			5.70		266.0	150.6	40,067		0.920	134,938	3.098
			5.80		266.8	151.4	40,401		0.927	138,961	3.190
			6.00		268.4	153.0	40,730		0.933	147,108	3.377
			6.10		269.2	153.8	41,411		0.951	151,233	3.472
			6.30		270.8	155.4	42,090		0.966	159,583	3.664
			6.40		271.6	156.2	42,432		0.974	163,809	3.761
			6.60		273.2	157.8	43,119		0.990	172,364	3.957
			6.70		274.0	158.6	43,464		0.998	176,693	4.056
			6.90		275.6	160.2	44,159		1.014	185,455	4.257
			7.00		276.4	161.0	44,509		1.022	189,889	4.359
			7.20		278.0	162.6	45,211		1.038	198,860	4.565
			7.30		278.8	163.4	45,564		1.046	203,399	4.669
			7.50		280.4	165.0	46,274		1.062	212,583	4.880
			7.60		281.2 282.0	165.8 166.6	46,631		1.071	217,228 221.909	4.987
			7.80		282.8	167.4	47,349		1.087	226,626	5.203
			7.90		283.6 284.4	168.2 169.0	47,710 48,072		1.095	231,379 236,168	5.312 5.422
			8.10		285.2	169.8	48,436		1.112	240,994	5.532
			8.20		286.0	170.6	48,800		1.120	245,855 250,754	5.644
			8.40		287.6	172.2	49,533		1.137	255,689	5.870
			8.50		288.4	173.0	49,902		1.146	260,660	5.984
			8.70		290.0	174.6	50,643		1.163	270,715	6.215
			8.80		290.8 291.6	175.4	51,015 51,389		1.171	275,798 280,918	6.331
			9.00		292.4	177.0	51,764		1.188	286,076	6.567
			9.10		293.2 294.0	177.8	52,140 52,517		1.197	291,271 296,504	6.687
			9.30		294.8	179.4	52,896		1.214	301,774	6.928
			9.40		295.6 296.4	180.2	53,276 53,658		1.223	307,083	7.050
			9.60		297.2	181.8	54,040		1.241	317,814	7.296
			9.70		298.0 298.8	182.6 183.4	54,424 54,809		1.249	323,238 328,699	7.421
			9.90		299.6	184.2	55,196		1.267	334,200	7.672

Optional

MHFD-Detention, Version 4.03 (May 2020)



	DETE	ENTION BAS	<u>SIN OUTLE</u>	ISTRUCT	JRE DESIGI	N			
		MHFD	-Detention, Versio	n 4.03 (May 2020)					
Project: Basin ID:	Homestead North	at Sterling Ranch							
ZONE 3	Tond C			E attac at a d	E attac at a d				
ZONE 2 ZONE 1				Estimated Stago (ft)	Volumo (ac.ft)	Outlot Typo			
			Zama 1 (110001/)	2 20	0.452		1		
T T			Zone T (WQCV)	2.39	0.453	Onlice Plate			
ZONE 1 AND 2	ORIFICE		Zone 2 (EURV)	3.83	1.050	Orifice Plate	-		
PERMANENT ORIFICES POOL Example Zono	Configuration (Pot	ontion Bond)	Zone 3 (100-year)	5.00	0.962	Weir&Pipe (Restrict)			
	configuration (Red	ention Fond)		Total (all zones)	2.465				
User Input: Orifice at Underdrain Outlet (typically	used to drain WQCV	in a Filtration BMP)					Calculated Paramet	ers for Unde	erdrain
Underdrain Orifice Invert Depth =	N/A	ft (distance below t	he filtration media	surface)	Under	drain Orifice Area =	N/A	ft <sup>2</sup>	
Underdrain Orifice Diameter =	N/A	inches			Underdrai	n Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifice	or Elliptical Slot W	air (typically used to	drain WOCV and/o	r FLIRV in a sodimor	tation BMP)		Colculated Paramet	ore for Dioto	
Invert of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage =	0 ft)	WO Ori	fice Area per Row =		ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	3.83	ft (relative to basin	bottom at Stage =	0 ft)	EI	liptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	9	,	Ellip	tical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	inches				Elliptical Slot Area =	N/A	ft <sup>2</sup>	
		-						-	
User Input: Stage and Total Area of Each Orifice	Row (numbered from	n lowest to highest)				1			
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	ow 8 (optiona	al)
Stage of Orifice Centroid (ft)	0.00	1.30	2.00	3.00					
Orifice Area (sq. inches)	0.75	3.10	3.50	10.00					
			5 11 ( 11 B	5 46 ( H N	5 46 ( H B	-			
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	w 16 (option	al)
Orifice Area (cg. inches)									
Unite Area (sq. incres)									
User Input: Vertical Orifice (Circular or Rectangul	ar)						Calculated Paramet	ers for Verti	cal Orifice
· · ·	Not Selected	Not Selected					Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basir	h bottom at Stage =	0 ft) Ve	ertical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basir	n bottom at Stage =	0 ft) Vertica	al Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and Ou	utlet Pipe OR Rectan	gular/Trapezoidal \	Neir (and No Outlet	Pipe)		Calculated Paramet	ers for Over	flow Weir
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and Ou Zone 3 Weir	Not Selected	gular/Trapezoidal \	Neir (and No Outlet	Pipe)	to Linnor Edgo, H	Calculated Paramet	ers for Over Not Selected	flow Weir I
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho =	Sloped Grate and Or Zone 3 Weir 3.83	Not Selected	gular/Trapezoidal \ ft (relative to basin I	<u>Neir (and No Outlet</u> bottom at Stage = 0 ft	Pipe) ) Height of Gra	te Upper Edge, H <sub>t</sub> =	Calculated Paramet Zone 3 Weir 3.83	ers for Over Not Selected N/A	flow Weir I feet
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	Sloped Grate and Ou Zone 3 Weir 3.83 5.00 0.00	utlet Pipe OR Rectan Not Selected N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin l feet H·V	<u>Weir (and No Outlet</u> bottom at Stage = 0 fi	Pipe) ) Height of Gra Overflow \ Grate Open Area / 1	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area =	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91	ers for Over Not Selected N/A N/A N/A	flow Weir I feet feet
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz, Length of Weir Sides =	Sloped Grate and Or           Zone 3 Weir           3.83           5.00           0.00           5.00	utlet Pipe OR Rectan Not Selected N/A N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin I feet H:V feet	<u>Neir (and No Outlet</u> bottom at Stage = 0 ff (	Pipe) ) Height of Gra Overflow \ Grate Open Area / 1 Overflow Grate Oper	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris =	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75	ers for Over Not Selected N/A N/A N/A N/A	flow Weir I feet feet ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 5.00 75%	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A	gular/Trapezoidal V ft (relative to basin I feet H:V feet %, grate open are	Weir (and No Outlet bottom at Stage = 0 fl ( a/total area	Pipe) ) Height of Gra Overflow \ Grate Open Area / 1 Overflow Grate Open Overflow Grate Open	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75 4.69	ers for Over N/A N/A N/A N/A N/A N/A	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 5.00 75% 75%	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are %	Weir (and No Outlet bottom at Stage = 0 fl ( c a/total area	Pipe) Height of Gra Overflow \ Grate Open Area / 1 Overflow Grate Open Overflow Grate Open	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris =	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75 4.69	ers for Over N/A N/A N/A N/A N/A N/A	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 5.00 75% 75%	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are %	Weir (and No Outlet bottom at Stage = 0 fl ( a/total area	Pipe) Height of Gra Overflow \ Grate Open Area / 1 Dverflow Grate Open Overflow Grate Open	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris =	Calculated Paramet           Zone 3 Weir           3.83           5.00           7.91           18.75           4.69	ers for Over N/A N/A N/A N/A N/A N/A	flow Weir I feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (	Sloped Grate and Ot           Zone 3 Weir           3.83           5.00           0.00           5.00           75%           75%           Circular Orifice, Res	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are % angular Orifice)	Weir (and No Outlet bottom at Stage = 0 fl ( c a/total area	Pipe) ) Height of Gra Overflow \ Grate Open Area / 1 Dverflow Grate Open Overflow Grate Open Overflow Grate Open	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris = Calculated Parameter	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75 4.69 s for Outlet Pipe w/	ers for Over N/A N/A N/A N/A N/A N/A Flow Restric	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ction Plate
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 5.00 75% 75% Circular Orifice, Res Zone 3 Restrictor	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are % angular Orifice)	Weir (and No Outlet bottom at Stage = 0 fl ( c a/total area	Pipe) ) Height of Gra Overflow V Grate Open Area / 1 Overflow Grate Open Overflow Grate Open Overflow Grate Open <u>C</u>	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris = Calculated Parameter	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75 4.69 s for Outlet Pipe w/ Zone 3 Restrictor	ers for Over N/A N/A N/A N/A N/A N/A Flow Restric	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate ( Depth to Invert of Outlet Pipe =	Sloped Grate and Ot           Zone 3 Weir           3.83           5.00           0.00           5.00           75%           75%           Circular Orifice, Res           Zone 3 Restrictor           0.25	ttlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected N/A	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are % angular Orifice) ft (distance below b	Weir (and No Outlet bottom at Stage = 0 fl ( a/total area asin bottom at Stage =	Pipe) ) Height of Gra Overflow V Grate Open Area / 1 Overflow Grate Open Overflow Grate Open Overflow Grate Open <u>C</u> = 0 ft) <u>C</u>	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris = Calculated Parameter Dutlet Orifice Area =	Calculated Paramet Zone 3 Weir 3.83 5.00 7.91 18.75 4.69 s for Outlet Pipe w/ Zone 3 Restrictor 2.37	ers for Over N/A N/A N/A N/A N/A N/A Flow Restric N/A	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ction Plate ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate ( Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	Sloped Grate and Ot           Zone 3 Weir           3.83           5.00           0.00           5.00           75%           75%           Circular Orifice, Res           Zone 3 Restrictor           0.25           30.00	Itlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are % angular Orifice) ft (distance below b inches	Weir (and No Outlet bottom at Stage = 0 ff ( a/total area asin bottom at Stage =	Pipe) ) Height of Gra Overflow V Grate Open Area / 1 Overflow Grate Open Overflow Grate Open Overflow Grate Open C C C Outing Outin	te Upper Edge, H <sub>t</sub> = Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris = Calculated Parameter Dutlet Orifice Area = et Orifice Centroid =	Calculated Paramet           Zone 3 Weir           3.83           5.00           7.91           18.75           4.69           s for Outlet Pipe w/           Zone 3 Restrictor           2.37           0.70	ers for Over N/A N/A N/A N/A N/A N/A Flow Restric N/A N/A N/A	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ction Plate ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate ( Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Sloped Grate and Ot           Zone 3 Weir           3.83           5.00           0.00           5.00           75%           75%           Zone 3 Restrictor           0.25           30.00           14.60	utlet Pipe OR Rectan N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected N/A N/A	gular/Trapezoidal \ ft (relative to basin l feet H:V feet %, grate open are % angular Orifice) ft (distance below b inches inches	Weir (and No Outlet bottom at Stage = 0 fl c a/total area asin bottom at Stage = Half-Cer	Pipe) ) Height of Gra Overflow V Grate Open Area / 1 Overflow Grate Open Overflow Grate Open Overflow Grate Open Overflow Grate Open C C Outling outling	te Upper Edge, $H_t =$ Neir Slope Length = 00-yr Orifice Area = n Area w/o Debris = en Area w/ Debris = Calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe =	Calculated Paramet           Zone 3 Weir           3.83           5.00           7.91           18.75           4.69           s for Outlet Pipe w/           Zone 3 Restrictor           2.37           0.70           1.54	ers for Over N/A N/A N/A N/A N/A N/A Flow Restric N/A N/A N/A N/A	flow Weir feet feet ft <sup>2</sup> ft <sup>2</sup> <u>ction Plate</u> ft <sup>2</sup> feet radians
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Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate ( Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or T Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 75% 75% Zone 3 Restrictor 0.25 30.00 14.60 rapezoidal) 5.00 21.00 4.00 1.00 7 <i>The user can overr</i> WOCV N/A 0.453 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	ttlet Pipe OR Rectan Not Selected N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected N/A N/A N/A ft (relative to basin feet H:V feet H:V feet de <i>the default CUHI</i> EURV N/A 1.503 N/A N/A N/A N/A Overflow Weir 1 N/A Overflow Weir 1 N/A N/A N/A N/A N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin I feet %, grate open are % ft (distance below b inches inches bottom at Stage = <i>P hydrographs and</i> . 2 Year 1.19 1.395 2.1 0.09 21.1 0.6 N/A Plate N/A N/A 68 72	Weir (and No Outlet           bottom at Stage = 0 ft           control           a/total area           asin bottom at Stage =           asin bottom at Stage =           Half-Cer           0 ft)           runoff volumes by en           5 Year           1.50           1.923           5.9           0.26           29.3           3.2           0.5           Overflow Weir 1           N/A           71	Pipe). ) Height of Gra Overflow Grate Open Area / 1 Verflow Grate Oper Overflow Grate Oper Overflow Grate Oper Overflow Grate Oper ()  ()  ()  ()  ()  ()  ()  ()  ()  ()	te Upper Edge, $H_t =$ Neir Slope Length = 00-yr Orifice Area = h Area w/o Debris = en Area w/ Debris = calculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 10 of Freeboard = 2.946 2.946 2.946 16.0 0.70 45.2 14.0 0.9 Overflow Weir 1 0.7 N/A 68	Calculated Paramet           Zone 3 Weir           3.83           5.00           7.91           18.75           4.69           s for Outlet Pipe w/           Zone 3 Restrictor           2.37           0.70           1.54           Calculated Paramet           0.90           6.90           1.01           4.26           raphs table (Column           50 Year           2.25           3.429           20.1           0.88           52.7           19.4           1.0           Overflow Weir 1           1.0           N/A           66           75	ers for Over N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	flow Weir i feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> if ft <sup>2</sup> feet radians <u>vay</u> <u>vay</u> <u>vay</u> <u>vay</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> <u>tags</u> 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User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate ( Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or T Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Inflow Volume (acreft) = CUHP Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) =	Sloped Grate and Ot Zone 3 Weir 3.83 5.00 0.00 75% 75% Zone 3 Restrictor 0.25 30.00 14.60 rapezoidal) 5.00 21.00 4.00 1.00 7 <i>The user can overr</i> WOCV N/A 0.453 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	ttlet Pipe OR Rectan Not Selected N/A N/A N/A N/A N/A N/A N/A trictor Plate, or Rect Not Selected N/A N/A N/A ft (relative to basin feet H:V feet de the default CUHI EURV N/A 1.503 N/A N/A N/A N/A N/A Overflow Weir 1 N/A Overflow Weir 1 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	gular/Trapezoidal \ ft (relative to basin I feet %, grate open are % ft (distance below b inches inches bottom at Stage = Phydrographs and 2 Year 1.19 1.395 2.1 0.09 21.1 0.6 N/A Plate N/A N/A 68 73 3 57	Weir (and No Outlet           bottom at Stage = 0 ft           (C)           (a/total area           asin bottom at Stage =           asin bottom at Stage =           Half-Cer           0 ft)           runoff volumes by en           5 Year           1.50           1.923           5.9           0.26           29.3           3.2           0.5           Overflow Weir 1           N/A           71           77           4 05	Pipe). ) Height of Gra Overflow Grate Open Area / 1 Verflow Grate Oper Overflow Grate Oper Overflow Grate Oper Overflow Grate Oper ()  ()  ()  ()  ()  ()  ()  ()  ()  ()	te Upper Edge, $H_t =$ Neir Slope Length = 00-yr Orifice Area = h Area w/o Debris = en Area w/ Debris = calculated Parameter: Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 10 of Freeboard = 2.946 2.946 2.946 16.0 0.70 45.2 14.0 0.9 Overflow Weir 1 0.7 N/A 68 76 4.52	Calculated Paramet           Zone 3 Weir           3.83           5.00           7.91           18.75           4.69           s for Outlet Pipe w/           Zone 3 Restrictor           2.37           0.70           1.54           Calculated Paramet           0.90           6.90           1.01           4.26           raphs table (Column           50 Year           2.25           3.429           20.1           0.88           52.7           19.4           1.0           Overflow Weir 1           1.0           N/A           66           75           4 69	ers for Over N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	flow Weir feet feet ff <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians <u>vay</u> <u>b AF).</u> 500 Year 4.00 6.989 50.8 <u>2.23</u> 106.3 68.4 1.3 Spillway 1.3 Spillway N/A 55 70 5,71
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Pond C MHFD-Detention\_v4 03.xlsm, Outlet Structure



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

i i	The user can by	entue the calcul	ateu innow nyun	ographs nom m		innow nyurograp	ns developed in	a separate progra	ann.	
-	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.23	0.02	1.76
	0:15:00	0.00	0.00	2.07	3.38	4.18	2.80	3.51	3.42	7.04
	0:20:00	0.00	0.00	7.44	9.81	11.74	7.28	8.48	9.07	16.75
	0:25:00	0.00	0.00	16.50	23.35	29.31	16.19	18.96	20.73	41.98
	0:30:00	0.00	0.00	21.06	29.32	35.40	38.54	45.30	50.76	89.72
	0:35:00	0.00	0.00	19.96	27.28	32.63	45.18	52.70	62.01	106.34
	0:40:00	0.00	0.00	17.86	23.95	28.68	43.85	50.93	59.93	102.03
	0:45:00	0.00	0.00	15.32	20.84	25.31	39.25	45.55	55.00	93.50
	0:50:00	0.00	0.00	13.15	18.30	21.97	35.57	41.28	49.72	84.52
	0:55:00	0.00	0.00	11.34	15.74	19.04	30.68	35.65	43.89	74.61
	1:00:00	0.00	0.00	9.96	13.74	16.87	26.25	30.55	38.70	65.94
	1:05:00	0.00	0.00	9.02	12.40	15.46	22.96	26.77	34.84	59.61
	1:10:00	0.00	0.00	7.92	11.36	14.33	19.88	23.21	29.50	50.89
	1:15:00	0.00	0.00	6.90	10.08	13.22	17.25	20.17	24.83	43.18
	1:20:00	0.00	0.00	5.96	8.65	11.54	14.49	16.93	20.14	34.99
	1:25:00	0.00	0.00	5.09	7.36	9.55	12.02	14.02	16.04	27.76
	1:30:00	0.00	0.00	4.37	6.30	7.88	9.59	11.14	12.47	21.51
	1:35.00	0.00	0.00	3.92	5.64	6.85	7.54	8.71	9.51	16.50
	1.40.00	0.00	0.00	3.09	5.00	6.24 E.00	6.27 E.40	1.23	1.07	13.42
	1.40.00	0.00	0.00	3.58	4.52 4.19	5.82	5.49 4 00	5 71	5.77	10.14
	1:55:00	0.00	0.00	3.52	3 92	5.20	4.77	5.28	5.23	9.19
	2:00:00	0.00	0.00	2 77	3.63	4 73	4.04	5.00	4.84	8.50
	2:05:00	0.00	0.00	2.17	2.83	3.67	3.42	3.88	3.68	6.45
	2:10:00	0.00	0.00	1.63	2.12	2.75	2.55	2.88	2.69	4.71
	2:15:00	0.00	0.00	1.23	1.60	2.05	1.91	2.16	2.01	3.51
	2:20:00	0.00	0.00	0.93	1.20	1.52	1.43	1.61	1.51	2.62
	2:25:00	0.00	0.00	0.69	0.88	1.11	1.05	1.18	1.12	1.94
	2:30:00	0.00	0.00	0.50	0.63	0.81	0.76	0.85	0.82	1.42
	2:35:00	0.00	0.00	0.36	0.45	0.59	0.56	0.62	0.60	1.03
	2:40:00	0.00	0.00	0.25	0.31	0.42	0.40	0.45	0.43	0.74
	2:45:00	0.00	0.00	0.16	0.21	0.28	0.27	0.30	0.29	0.50
	2:50:00	0.00	0.00	0.09	0.13	0.16	0.17	0.19	0.18	0.30
	2:55:00	0.00	0.00	0.04	0.07	0.08	0.09	0.10	0.09	0.16
	3:00:00	0.00	0.00	0.02	0.03	0.03	0.03	0.04	0.03	0.06
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.30.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0,00	0.00	0.00	0,00	0,00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



(Only the sump inlets were checked)

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Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =			
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =			
		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =			cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =			%



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Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.1	12.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	2.8	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	81	%



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Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.2	14.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.2	6.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	98	70	%



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Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =			
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =			
		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =			cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =			%



### INLET IN A SUMP OR SAG LOCATION

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Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	4	4	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	8.3	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	0.78	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.79	0.91	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	18.2	39.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	10.5	29.7	cfs



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Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.4	11.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	1.7	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	87	%







Design Information (Input)	CDOT Time D Curt Organiza			MINOR	MAJOR	_
Type of Inlet	CDOT Type R Curb Opening	<u> </u>	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)		No =	3	3	
Length of a Single Unit Inlet (Grate	or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be gr	eater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit C	Grate (typical min. value = 0.5)		C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)		C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allov	vable Street Capacity'			MINOR	MAJOR	-
Total Inlet Interception Capacity			Q =	7.0	12.6	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)		Q <sub>b</sub> =	0.0	3.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =			C% =	100	78	%



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Design Information (Input)	N	MINOR MAJOR	
Type of Inlet	Type =		
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =		inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =		
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =		ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =		ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =		
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =		
	M	1INOR MAJOR	
Total Inlet Interception Capacity	Q =		cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =		cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =		%



### INLET IN A SUMP OR SAG LOCATION

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Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.8	8.3	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>0</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.32	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.55	0.78	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.78	0.91	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	12.5	29.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	11.3	19.9	cfs


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Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.3	9.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	1.5	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	87	%



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Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate	or Curb Opening)	$L_0 =$	5.00	5.00	ft
Width of a Unit Grate (cannot be g	reater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit C	Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allow	vable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity		Q =	3.6	7.4	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q <sub>b</sub> =	0.0	0.2	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	100	97	%



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Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.7	11.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.1	4.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	99	74	%



#### INLET IN A SUMP OR SAG LOCATION

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Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.8	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	•
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)	-	MINOR	MAJOR	-
Depth for Grate Midwidth	d <sub>Grote</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.32	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.55	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.78	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Intercention Canacity (assumes clogged condition)	Q =	12.5	39.1	cfs
Total met merception capacity (assumes clogged condition)	• • • • • •	12.5	39.1	013 afa
WARNING: Inlet Capacity less than Q Peak for Minor Storm	✓ PEAK REQUIRED =	12.5	30.9	cis



Version 4.05 Released March 2017



Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate	or Curb Opening)	$L_0 =$	5.00	5.00	ft
Width of a Unit Grate (cannot be gr	reater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit C	Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allov	vable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity		Q =	7.0	11.3	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q <sub>b</sub> =	0.1	3.2	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	98	78	%



#### INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.8	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>0</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	•
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)	-	MINOR	MAJOR	-
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.32	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.55	0.75	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.78	0.89	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	12.5	27.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	5.0	12.5	cfs



Version 4.05 Released March 2017



Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate	or Curb Opening)	$L_o =$	5.00	5.00	ft
Width of a Unit Grate (cannot be gr	reater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit C	Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allov	vable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity		Q =	7.2	11.6	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q <sub>b</sub> =	0.1	3.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	98	76	%



Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.8	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	91	%



Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.4	8.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	0.7	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	92	%



Version 4.05 Released March 2017



Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate	or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be g	reater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit (	Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allow	vable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity		Q =	1.3	2.0	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q <sub>b</sub> =	0.0	0.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	97	79	%



#### INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	4	4	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	8.3	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	•
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	0.78	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.79	0.91	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	18.2	39.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	16.9	35.5	cfs



#### INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.8	5.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>0</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.32	0.32	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.55	0.55	1
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.92	0.92	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	9.7	9.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.2	9.0	cfs

February 2021

# Appendix D Drainage Maps



# **EXISTING DRAINAGE MAP HOMESTEAD NORTH**



BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (acres)	Percent Impervious	C₅	C <sub>100</sub>	t <sub>c</sub> (min)	Q₅ (cfs)	Q <sub>100</sub> (cfs)
H1	45.30	3%	0.09	0.36	34.7	8.9	61.1
H2	15.90	2%	0.08	0.35	25.1	3.5	25.7
H3	29.10	3%	0.09	0.35	31.3	6.1	41.8





# EARLY GRADING - DRAINAGE MAP

SEE SHEET 2

LEGEND	
BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT PROPOSED FLOW DIRECTION	
BASIN DRAINAGE AREA	
EXISTING STORM SEWER	
STORM SEWER PROPOSED PROPOSED R.O.W PROPOSED PROPERTY LINES PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING FL EXISTING SIDEWALK EXISTING	
DRAINAGE ACCESS & MAINTER EASEMENT	NANCE

# EXISTING

Small

EXISTING	PROPOSED
6100	6100

# BASIN SUMMARY TABLE

Temporary	Contributing	Area	Percent	Contributing	Area	Percent	<b>Required Volume</b>	Provided Volume
Sediment Basin	On-site Basin	(acres)	Impervious	Off-site Basin	(acres)	Impervious	(cf)	(cf)
1	С	24.27	2%				87,372	108,900
2	D	17.29	2%	OS	160.00	2%	142,244	196,020

Provide basin and DP summary tables



EARLY GRADING – DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 02/12/21 SHEET 1 OF 1



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# LEGEND

BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT PROPOSED FLOW DIRECTION	
BASIN DRAINAGE AREA	
EXISTING STORM SEWER	
STORM SEWER PROPOSED	
PROPOSED R.O.W	
PROPOSED PROPERTY LINES	
PROPOSED SIDEWALK	
EXISTING PROPERTY LINE	
ROW EXISTING	
SIDEWALK EXISTING	
DRAINAGE ACCESS & MAINTEN EASEMENT	JANCE — — — —

# EXISTING

6100	6100

PROPOSED

Provide basin and DP summary tables



EARLY GRADING – DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 02/12/21 SHEET 2 OF 4



# J·R ENGINEERING A Westrian Company



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LEGEND

BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT PROPOSED FLOW DIRECTION	<u>↓</u> #
BASIN DRAINAGE AREA EXISTING STORM SEWER	
STORM SEWER PROPOSED PROPOSED R.O.W PROPOSED PROPERTY LINES PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING FL EXISTING SIDEWALK EXISTING	
DRAINAGE ACCESS & MAINTEN EASEMENT	IANCE — — — —

EXISTING

PROPOSED 6100

Provide basin and DP summary tables

EARLY GRADING – DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 02/12/21 SHEET 3 OF 4



J·R ENGINEERING A Westrian Company



# EARLY GRADING - DRAINAGE MAP

	LEGEND	
	BASIN ID A: BASIN LABEL B: AREA C: C —100 YR D: C—5 YR	
	DESIGN POINT PROPOSED FLOW DIRECTION	
	BASIN DRAINAGE AREA	
	EXISTING STORM SEWER	
	STORM SEWER PROPOSED PROPOSED R.O.W PROPOSED PROPERTY LINES PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING FL EXISTING SIDEWALK EXISTING DRAINAGE ACCESS & MAINTENANC	
	EASEMENT	
	EXISTING	PROPOSED
	6100	6100
N	Provide basin and DP summary tabl	es
T		
н Р		
S		

			BASI	N SUMMAR	RY TABL	E		
Temporary Sediment Basin	Contributing On-site Basin	Area (acres)	Percent Impervious	Contributing Off-site Basin	Area (acres)	Percent Impervious	Required Volume (cf)	Provided Volum (cf)
		(			(		(~~)	
1	С	24.27	2%				87,372	108,900

OS 160.00 2% 142,244

196,020

17.29 2%

D

2



EARLY GRADING – DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 02/12/21 SHEET 4 OF 4



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SEE SHEET 2



# EXISTING

PROPOSED

- 0100-	
	-

DE	SIGN PO	INT			BASI			<b>SLE</b>		
SUN	IMARY T	ABLE	Tributory		<b>_</b>				05	0100
DP	Q5	Q100		Area	Percent			tc (min)	Q5	Q100
	Total	Total	Sub-basin	(acres)	Impervious	C5	C100	(min)	(CTS)	(CTS)
1a	6.9	14.6								
2a	6.5	13.4	A1	3.67	52%	0.51	0.64	13.4	6.9	14.6
3a	8.2	20.4	A2	3.27	56%	0.54	0.67	13.6	6.5	13.4
4a	7.2	16.6	A3	4.79	50%	0.49	0.63	13.9	8.5	18.4
5a	9.5	26.1	A4	3.95	54%	0.52	0.65	14.1	7.4	15.6
6a	10.7	18.6	A5	5.43	50%	0.49	0.62	11.1	10.5	22.6
7a	10.4	29.9	A6	3.96	53%	0.52	0.65	12.6	7.7	16.3
8a	11.4	20.0	A7	1.97	15%	0.19	0.43	16.5	1.3	4.8
9a	21.6	49.5	A8	0.42	57%	0.54	0.69	5.0	1.2	2.5
1.1b	5.5	12.5	A9	2.97	16%	0.20	0.43	13.4	2.2	7.9
1.2b	3.5	7.4	B1.1	3.35	45%	0.45	0.60	13.4	5.5	12.5
1.3b	1.0	2.2	B1.2	1.81	54%	0.52	0.65	12.8	3.5	7.4
2b	2.4	6.8	B1.3	0.47	47%	0.46	0.63	8.1	1.0	2.2
3b	0.9	1.7	B2	0.82	58%	0.55	0.69	5.0	2.3	4.9
4b	6.7	15.9	B3	0.24	79%	0.73	0.83	5.0	0.9	1.7
5b	4.3	8.9	B4	3.98	40%	0.40	0.57	9.5	6.7	15.9
6b	10.4	26.5	B5	1.75	58%	0.55	0.68	7.8	4.3	8.9
7b	7.0	14.4	B6	3.66	58%	0.55	0.68	6.5	9.6	20.0
8b	4.1	10.9	B7	1.14	61%	0.58	0.70	8.8	2.9	5.8
9b	12.1	30.4	B8	1.74	58%	0.56	0.68	9.3	4.1	8.5
10b	4.7	12.2	B9	3.69	65%	0.50	0.64	13.1	6.9	14.8
11b	17.4	45.5	B10	0.22	80%	0.73	0.83	5.0	0.8	1.6
1c	5.4	11.4	B11	1.77	14%	0.15	0.40	16.8	0.9	3.9
2.1c	0.8	1.6	C1	2.82	69%	0.52	0.65	13.1	5.4	11.4
2.2c	9.8	20.1	C2.1	0.20	91%	0.82	0.90	5.0	0.8	1.6
2.3c	7.1	14.9	C2.2	4.69	73%	0.56	0.68	12.8	9.9	20.3
3.1c	1.2	2.4	C2.3	0.83	67%	0.54	0.68	10.1	1.9	3.9
3.2c	3.6	7.9	C3.1	0.35	73%	0.68	0.79	5.0	1.2	2.4
4c	16.9	36.2	C3.2	1.46	71%	0.56	0.68	8.4	3.6	7.4
4.2c	4.8	11.2	C4.1	6.37	65%	0.49	0.63	12.7	11.8	25.4
5c	4.1	8.8	C4.2	3.47	55%	0.42	0.58	17.2	4.8	11.2
6c	20.6	46.6	C5	0.16	81%	0.74	0.84	5.0	0.6	1.1
			C6	2.42	10%	0.13	0.38	5.0	1.6	8.0
						-				
			L	1	1		1	I	I	1



DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 2/15/21 SHEET 1 OF 2



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LEGEND	
BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT PROPOSED FLOW DIRECTION	
BASIN DRAINAGE AREA	
EXISTING STORM SEWER	
STORM SEWER PROPOSED PROPOSED R.O.W PROPOSED PROPERTY LINES PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING FL EXISTING SIDEWALK EXISTING	
DRAINAGE ACCESS & MAINTEN EASEMENT	NANCE

PROPOSED

- 6100

# EXISTING



DESIGN POINT										
			BASIN SUMMARY TABLE							
3010			Tributary	Area	Percent			tc	05	0100
DP	US Tatal		Sub basin	(acres)	Impervious	<b>CE</b>	C100	(min)	(cfs)	(cfs)
1 -	lotal	Iotal	Sub-basiii	(46165)		65		()		
1a	6.9	14.6		2.67	F 20/	0.51	0.04	12.4	6.0	14.0
2a	6.5	13.4	AI	3.67	52%	0.51	0.64	13.4	6.9	14.0
3a	8.2	20.4	A2	3.27	56%	0.54	0.67	13.6	6.5	13.4
4a	7.2	16.6	A3	4.79	50%	0.49	0.63	13.9	8.5	18.4
5a	9.5	26.1	A4	3.95	54%	0.52	0.65	14.1	7.4	15.6
6a	10.7	18.6	A5	5.43	50%	0.49	0.62	11.1	10.5	22.6
7a	10.4	29.9	A6	3.96	53%	0.52	0.65	12.6	7.7	16.3
8a	11.4	20.0	A7	1.97	15%	0.19	0.43	16.5	1.3	4.8
9a	21.6	49.5	A8	0.42	57%	0.54	0.69	5.0	1.2	2.5
1.1b	5.5	12.5	A9	2.97	16%	0.20	0.43	13.4	2.2	7.9
1.2b	3.5	7.4	B1.1	3.35	45%	0.45	0.60	13.4	5.5	12.5
1.3b	1.0	2.2	B1.2	1.81	54%	0.52	0.65	12.8	3.5	7.4
2b	2.4	6.8	B1.3	0.47	47%	0.46	0.63	8.1	1.0	2.2
3b	0.9	1.7	B2	0.82	58%	0.55	0.69	5.0	2.3	4.9
4b	6.7	15.9	B3	0.24	79%	0.73	0.83	5.0	0.9	1.7
5b	4.3	8.9	B4	3.98	40%	0.40	0.57	9.5	6.7	15.9
6b	10.4	26.5	B5	1.75	58%	0.55	0.68	7.8	4.3	8.9
7b	7.0	14.4	B6	3.66	58%	0.55	0.68	6.5	9.6	20.0
8b	4.1	10.9	B7	1.14	61%	0.58	0.70	8.8	2.9	5.8
9b	12.1	30.4	B8	1.74	58%	0.56	0.68	9.3	4.1	8.5
10b	4.7	12.2	В9	3.69	65%	0.50	0.64	13.1	6.9	14.8
11b	17.4	45.5	B10	0.22	80%	0.73	0.83	5.0	0.8	1.6
1c	5.4	11.4	B11	1.77	14%	0.15	0.40	16.8	0.9	3.9
2.1c	0.8	1.6	C1	2.82	69%	0.52	0.65	13.1	5.4	11.4
2.2c	9.8	20.1	C2.1	0.20	91%	0.82	0.90	5.0	0.8	1.6
2.3c	7.1	14.9	C2.2	4.69	73%	0.56	0.68	12.8	9.9	20.3
3.1c	1.2	2.4	C2.3	0.83	67%	0.54	0.68	10.1	1.9	3.9
3.2c	3.6	7.9	C3.1	0.35	73%	0.68	0.79	5.0	1.2	2.4
4c	16.9	36.2	C3.2	1.46	71%	0.56	0.68	8.4	3.6	7.4
4.2c	4.8	11.2	C4.1	6.37	65%	0.49	0.63	12.7	11.8	25.4
5c	4.1	8.8	C4.2	3.47	55%	0.42	0.58	17.2	4.8	11.2
6c	20.6	46.6	C5	0.16	81%	0.74	0.84	5.0	0.6	1.1
-			C6	2.42	10%	0.13	0.38	5.0	1.6	8.0



DRAINAGE MAP HOMESTEAD NORTH JOB NO. 25188.00 2/15/21 SHEET 2 OF 2



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POND A 30.43 ACRES, 46.3% IMPERVIOUS

POND B 24.64 ACRES, 51.1% IMPERVIOUS

POND C 22.77 ACRES, 60.8% IMPERVIOUS



February 2021

Appendix E Reference Material



# SAND CREEK DRAINAGE BASIN PLANNING STUDY

# PRELIMINARY DESIGN REPORT

# CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO



PREPARED FOR:

City of Colorado Springs Department of Comprehensive Planning, Development and Finance Engineering Division 30 S. Nevada Colorado Springs, Colorado 80903

# PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903

#### **STUDY AREA DESCRIPTION** II.

The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

# **Basin Description**

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence in most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

# Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about 30°F in the winter to 75° in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

# Soils and Geology

Soils within the Sand Creek basin vary between soil types A through D, as identified by the U.S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residium, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

# Property Ownership and Impervious Land Densities

Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within


HISTORIC CONDITION <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN 5UMARY</u> <u>BASIN 5UMARY</u> <u>BASIN 450 450 000 135 0000</u> <u>EX-12 23 71 2561 14955555555555555555555555555555555555</u>	Runoff in attenuated in an existing poind.     DESIGN POINTS       Runoff in attenuated in a mexisting poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Provide the state is 16 cfs     DESIGN POINTS       • 0.05     12     197     137     255     53       • 0.05     13     149     474     46     474 <t< th=""><th></th><th>Image: State factor STERLING RANCH MDDP   STERLING RANCH MDDP   Image: Sterright factor   Image: Sterright factor</th></t<>		Image: State factor STERLING RANCH MDDP   STERLING RANCH MDDP   Image: Sterright factor   Image: Sterright factor



HISTORIC CONDITION <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN SUMMARY</u> <u>BASIN 5UMARY</u> <u>BASIN 5UMARY</u> <u>BASIN 450 450 000 135 0000</u> <u>EX-12 23 71 2561 14955555555555555555555555555555555555</u>	Runoff in attenuated in an existing poind.     DESIGN POINTS       Runoff in attenuated in a mexisting poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Point Mine existing poind.     DESIGN POINTS       Provide the state is 16 cfs     DESIGN POINTS       • 0.05     12     197     137     255     53       • 0.05     13     149     474     46     474 <t< th=""><th></th><th>Image: State factor STERLING RANCH MDDP   STERLING RANCH MDDP   Image: Sterright factor   Image: Sterright factor</th></t<>		Image: State factor STERLING RANCH MDDP   STERLING RANCH MDDP   Image: Sterright factor   Image: Sterright factor



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UP-73     Z.471     H.D.     GO.O     91.0     136.8     176.2     Z.11.7     POCO ROAD X-ING       DP-71     2.757     46.3     70.0     104.3     151.3     194.5     216.7     216.7     POCO ROAD X-ING       DP-70     2.867     49.5     74.5     110.6     160.1     205.4     254.0     BRIARGATE PARKWAY X-ING       DP-69     3.238     57.5     86.1     127.4     183.8     235.3     290.6     BRIARGATE PARKWAY X-ING       DP-64     4.312     81.8     123.7     183.9     245.1     209.1     267.1     329.1     UPSTREAM OF POND W3       DP-64     5.17     111.0     168.6     209.1     267.7     352.8     433.5     STERLING RANCH SOUTHERN BNDRY       DP-64     5.17     111.0     168.6     250.4     359.5     457.7     561.5     SAND GREIK AND POND 3       DP-16     0.247     3.1     16.2     23.4     36.1     47.4     59.3     SOLORAD SPRINCS/EL PASO BNDRY       DP-26     1.079     8.0 <th></th>	
EFSC DBPS DESIGN NUMARY (PEAK FLOW)       DPS DESIGN     ARE A (point)     Quantity     ARE A (point)     Quantity     ARE A (point)     Quantity     ARE A (point)     Quantity     Quant	
PEAK     INFLOW     GES     141.6     189.4     252.5     331.4     398.9     46       ALLOWABLE RELEASE (GFS)     0.2     1.9     3.2     13.4     398.9     46       STORED RELEASE (GFS)     0.2     0.9     3.2     37.4     77.3     12       PND-E7     2     5     10     25.2     46.5     75.4     121.2     285.2     402.4     51       STORED VOLUME (AC-FT)     1.0     1.8     4.6     101.5     108.3     45.1     51       MODELED RELEASE (GFS)     23.1     35.3     71.5     108.3     152.1     51	Image: Provide and analysis of the provide analysis