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SUBSURFACE SOIL INVESTIGATION MERIDIAN RANCH - ROLLING HILLS RANCH EL PASO COUNTY, COLORADO

Prepared for:

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Respectfully Submitted,

ENTECH ENGINEERING, INC.

Reviewed by:

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DPS/ts

Encl.

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SUBSURFACE SOIL INVESTIGATION MERIDIAN RANCH - ROLLING HILLS RANCH, FILINGS 1 - 4 EL PASO COUNTY, COLORADO

1.0 INTRODUCTION

The project consists of the development of the site for the construction of single-family residences in Rolling Hills Ranch Filings 1 - 4. Development is expected to include site grading, installation of subsurface utilities, roadways, and drainage structures. The subdivision is in Meridian Ranch in the northern portion of El Paso County, Colorado. The approximate location of the project site is shown on the Vicinity Map, Figure 1. The test boring locations are shown on Figure 2, the Test Boring Location Plan, with the approximate delineation of soil types and potential groundwater areas depicted on the figures.

This report describes the subsurface investigation conducted for the site and provides recommendations for development design and construction. The Subsurface Soil Investigation included the drilling of forty-nine test borings across the site, collecting samples of soil, and conducting a geotechnical evaluation of the investigation findings. All drilling and subsurface investigation activities were performed by Entech Engineering, Inc. (Entech). The contents of this report, including the geotechnical evaluation and recommendations, are subject to the limitations and assumptions presented in Section 17.0.

2.0 PROJECT AND SITE DESCRIPTION

The project will consist of developing the site for single family residential structures. The planned lots are located in the Rolling Hills Ranch subdivision in Meridian Ranch. The investigation was performed at predetermined locations designated based on the roadway alignment and proposed grading on the site plan provided to us. At the time of drilling, the site was vacant and not developed. The site is not graded for the planned development. Site grading plans were provided to us with proposed cuts up to 13 feet and fills up to 15 feet. The majority of the cuts and fills are in the 2 to 10-foot range. The site has a gradual slope towards the southeast. Vegetation consisted of grasses and weeds. Existing residences and Falcon High School were located to the west and south of the site, undeveloped land immediately north, and Eastonville Road to the east. Natural earthen drainage trends to the southeast traversing the property from near the intersection of Rex Road and Sunrise Ridge Drive towards Eastonville Road at a point approximately 2000 feet northeast of Falcon High School. Fill piles of soil encompass approximately 3 acres in the northwest quadrant of the proposed subdivision, and approximately 20-acres of land south of this area was previously excavated, likely for nearby developments. The large area of soil removals and fill piles are not depicted on the topographic mapping for this site. Other smaller piles of manmade materials and straw bales were noted south and west of the natural drainage.

3.0 SUBSURFACE EXPLORATIONS AND LABORATORY TESTING

Subsurface conditions on the site were explored by drilling forty-nine test borings at the approximate locations shown on Figure 2. The boring locations were determined and staked by others. The borings were drilled within the proposed roadway alignments. The borings were drilled to depths of 20 to 25 feet below the existing ground surface (bgs). The drilling was performed using a truck-mounted, continuous flight auger-drilling rig supplied and operated by Entech. Boring logs descriptive of the subsurface conditions encountered during drilling are presented in Appendix A. At the conclusion and subsequent to drilling, observations for groundwater levels were made in each of the open boreholes.

Soil and bedrock samples were obtained from the borings utilizing the Standard Penetration Test (ASTM D-1586) using 2-inch O.D. split-barrel and California samplers. Results of the Standard Penetration Test (SPT) are included on the boring logs in terms of N-values

expressed in blows per foot (bpf). Soil and bedrock samples recovered from the borings were visually classified and recorded on the boring logs. The soil and bedrock classifications were later verified utilizing laboratory testing and grouped by soil type. The soil and bedrock type numbers are included on the boring logs. It should be understood that the soil and bedrock descriptions shown on the boring logs may vary between boring location and sample depth. It should also be noted that the lines of stratigraphic separation shown on the boring logs represent approximate boundaries between soil and bedrock types and the actual stratigraphic transitions may be more gradual or variable with location.

Water content testing (ASTM D-2216) was performed on the samples recovered from the borings, and the results are shown on the boring logs. Grain-Size Analysis (ASTM D-422) and Atterberg Limits testing (ASTM D-4318) were performed on selected samples to assist in classifying the materials encountered in the borings. Volume change testing was performed on selected samples using the Swell/Consolidation Test (ASTM D-4546) and the FHA Swell Test in order to evaluate potential expansion/compression characteristics of the soil and bedrock. Soluble sulfate testing was performed on select soil samples to evaluate the potential for below grade degradation of concrete due to sulfate attack. The Laboratory Testing Results are summarized on Table 1 and are presented in Appendix B.

4.0 SUBSURFACE CONDITIONS

One soil type and two bedrock types were encountered in the test borings drilled for the subsurface investigation: Type 1: native slightly silty to silty sand, clayey to very clayey sand, and sand (SM-SW, SM, SC, SW), Type 2: slightly silty to silty sandstone and clayey to very clayey sandstone (SM-SW, SM, SC), and Type 3: sandy to very sandy claystone (CL). The soil and bedrock were classified in accordance with the Unified Soil Classification System (USCS) and American Association of State Highway and Transportation Officials (AASHTO) System using the laboratory testing results and the observations made during drilling.

4.1 Soil and Bedrock

<u>Soil Type 1</u> classified as native slightly silty to silty sand, clayey to very clayey sand, and sand (SM-SW, SM, SC, SW). The sand was encountered in all of the test borings at the existing ground surface and extending to depth ranging from 1 to 14 feet below ground surface (bgs).

Standard Penetration Testing conducted on the sand resulted in SPT N-values ranging from 4 to 48 blows per foot (bpf), indicating loose to dense states. Water content and grain size testing of selected soil samples resulted in a water content range of 1 to 21 percent, and 5 to 48 percent of the soil particles passing the No. 200 sieve. Atterberg limits testing resulted in Liquid Limits of 26, 29, and no value and Plastic Indexes of 16, 10, and non-plastic, respectively. FHA Swell testing resulted in swell pressure between 70 and 2970 psf, indicating low to high expansion potentials. Swell/Consolidation testing on a sample of silty sand resulted in a volume change of -1.2 percent, indicating a low to moderate consolidation potential. Sulfate testing resulted in 0.00, less than 0.01, and 0.01 percent soluble sulfate by weight, which indicates a negligible potential for below grade concrete degradation due to sulfate attack.

Soil Type 2 classified as slightly silty to silty sandstone and clayey to very clayey sandstone (SM-SW, SM, SC). The sandstone was encountered in all test borings, but Test Boring No. 31, underlying Soil Types 1 and 3 at depths ranging from 1 to 20 feet bgs and extending to depths ranging from 12 to 24 feet bgs and to the termination of the borings (20 to 25 feet). Standard Penetration Testing conducted on the sandstone resulted in SPT N-values from 27 to greater than 50 bpf, which indicates medium dense to very dense states. Water content and grain size testing resulted in a water content range of 2 to 30, and 7 to 50 percent of the soil particles passing the No. 200 sieve. Atterberg Limits testing resulted in Liquid Limit between 26 and 41 and no value with Plastic Indexes between 12 and 20 and non-plastic. Swell/Consolidation testing on the sandstone resulted in volume changes of -1.9 to 3.2 percent, indicating low to moderate consolidation potentials and moderate to high expansion potentials. Sulfate testing on the sandstone resulted in 0.00 and less than 0.01 percent sulfate by weight indicating the sandstone exhibits a negligible potential for below grade concrete degradation due to sulfate attack.

<u>Soil Type 3</u> classified as sandy to very sandy claystone (CL). The claystone was encountered in Test Boring Nos. 2, 4, 5, 15, 16, 19 thru 24, 27, 31 thru 39, 41, 43, 46, and 48 underlying Soil Types 1 and 2 at depths ranging from 1 to 24 feet bgs and extending to depths ranging from 4 to 24 feet bgs or to the termination of the borings (20 to 25 feet). Standard Penetration Testing conducted on the claystone resulted in SPT N-values of 45 to greater than 50 bpf, which indicates very stiff to hard consistencies. Water content and grain size testing resulted in a water content range of 9 to 19, and 51 to 81 percent the soil size particles passing the No. 200 sieve. Atterberg limits testing resulted in Liquid Limits between 34 and 42 and Plastic Indexes

between 15 and 20. FHA Swell testing resulted in a swell pressure of 90 psf, indicating a low expansion potential. Swell/Consolidation testing on the claystone resulted in volume changes of -2.0 to 2.5 percent, indicating moderate to high consolidation and expansion potentials. Sulfate testing on the claystone resulted in 0.00 percent sulfate by weight indicating the claystone exhibits negligible degradation to concrete due to sulfate attack.

4.2 Groundwater

Depth to groundwater was measured in each of the borings at the conclusion of drilling and subsequent to drilling. Groundwater was encountered in thirty-eight of the forty-nine test borings, ranging from depths of 2 to 23 feet bgs. Groundwater may affect building foundation excavations, roadway and utilities construction on this site. It should be noted that groundwater levels could change due to seasonal variations, changes in land runoff characteristics and future development including nearby areas. Table 2 presents the estimated depths to bedrock and groundwater.

5.0 PRELIMINIARY DEVELOPMENT CONSIDERATIONS

The following discussion is based on the subsurface conditions encountered in the test borings drilled at the site. This investigation is for the site discussed in 2.0 Project and Site Description. If subsurface conditions different from those described herein are encountered during construction or if the project elements change from those described, Entech Engineering, Inc. should be notified so that the evaluation and recommendations presented can be reviewed and revised if necessary.

Subsurface soil conditions encountered in the test borings drilled on the site generally consisted of native slightly silty to silty sand, clayey to very clayey sand, and sand overlying slightly silty to silty sandstone, clayey to very clayey sandstone, and sandy to very sandy claystone. Bedrock was encountered at depths ranging from 1 to 14 feet bgs. Depths to bedrock are indicated on the test boring plan and in Table 2. Consideration should be given to several conditions on this site in planning and excavating the development including groundwater, expansive soils and sandstone/claystone materials.

5.1 Groundwater

Groundwater may impact the development. Table 2 presents the depth to groundwater measured in each boring. Subsequent to completion of overlot grading cuts per the grading plan presented to us, the measured water levels will be less than 10 feet in some areas of the site. Groundwater was measured as shallow as two feet in Test Boring No. 24. Fill is proposed in this area. The area may require stabilization prior to placing fill. Claystone was encountered at 4 feet. Unstable conditions should be expected where groundwater is shallow or close to excavated depths. Procedures and equipment to mitigate groundwater impact during and after construction should be anticipated. Pumps, cofferdams, wide area and localized drain systems and other procedures and equipment may be necessary. Shotrock and geotextiles may be appropriate for stabilizing excavations. An underdrain system can be considered for long term groundwater mitigation. Frequently, groundwater levels rise following development as result of increased irrigation and decreased potential area of evaporation.

5.2 Expansive Soils

Expansive soils [clayey sand, claystone, and potentially clay (not encountered in the test borings)] are present on the site exhibiting expansion potential from low to high. Expansive soils where encountered will require mitigation for residential construction. Damage to structures can occur due to expansive soils; occurrence and severity of distress can be reduced by moisture treatments and overexcavation mitigation approaches.

5.3 Sandstone and Claystone

Sandstone and claystone were encountered at shallow depths across the site. Excavation of sandstone and claystone should be expected to be moderate to difficult. Track type equipment likely will be needed to accomplish excavations particularly where harder materials or lenses are present. Upon completion of site grading per the plan provided to us, sandstone is expected to be exposed across the majority of the areas tested.

6.0 SITE GRADING

Shallow bedrock was encountered in approximately half of the test borings. Depth to bedrock in each boring is indicated on the Test Boring Plan, Figure 2. Excavation of dense and hard

materials on site is expected to be moderate to difficult with heavy duty earthmoving equipment. Claystone and sandstone materials may require track equipment and ripping teeth. For conditions with no groundwater seepage, cut and fill slopes no steeper than 3 to 1 (horizontal to vertical) should be considered. If seepage occurs, then flatter slopes or a drain system should be considered. Recommendations may be subject to change depending upon particular field conditions.

6.1 Stripping

Debris, topsoil and organic materials should be stripped from the ground surface of areas to be filled. Any uncontrolled fill materials should be completely removed. The materials may be used as fill pending approval if they are free of organic material and debris. Although soft areas are not expected any soft or loose soils should be stabilized or removed to expose suitable material prior to placement of fill. Topsoil may be stored in stock piles and placed at the surface in landscape areas.

6.2 Fill Preparation

Surfaces which will receive fill should be scarified to depths of 6 inches, moisture conditioned to within 0 to 3 percent of optimum moisture, and compacted to minimum of 95 percent of Standard Proctor Dry Density (ASTM D-698) for cohesive materials and within 2 percent of optimum moisture, and compacted to minimum of 95 percent of Modified Proctor Dry Density (ASTM D-1557) for cohesionless soils. On-site natural soils and bedrock are anticipated to be used as site grading fill. Bedrock must be processed and broken down to small gravel-sized materials where placed in the fill. Expansive materials used for fill should be placed at sufficient moisture content to mitigate potential swell. The fill quality will influence the performance of foundations, slabs-on-grade, and pavements. Fill settlement can be minimized by placing thin lifts at suitable moisture content and by verification of compaction with frequent density tests.

6.3 Compaction

Overlot grading fill consisting of granular soils should be placed in lifts to exceed 6 inches following compaction and compacted to at least 95 percent of the maximum dry density determined by Modified Proctor (ASTM D-1557). Clay materials should be placed in compacted lifts less than 6 inches thick compacted to at least 95 percent of maximum Standard Proctor (ASTM D 698) dry density. Fills below 10 feet in depth should be moisture conditioned as above

and compacted to 98 percent of Standard Proctor dry density (ASTM D 698) for cohesive materials or 98 percent of maximum modified Proctor Dry Density (ASTM D 1557) for granular materials. The soil materials should be placed at a moisture content conducive to adequate compaction, usually within ±2 percent of optimum moisture content. Fill placement and compaction should be observed and tested by Entech during construction to verify that adequate moisture and density has been achieved.

7.0 UNDERGROUND UTILITY CONSTRUCTION

Generally excavation is expected to be moderate to difficult utilizing heavy-duty track hoes. Rock buckets and rock teeth will likely be required where excavations extend into very hard sandstone or cemented materials. Special procedures or equipment may be required to remove water and/or achieve stability in utility trenches where excavations approach or intercept groundwater.

Utilities including water and sewer lines are usually constructed beneath paved roads. Placement of fill and degree of compaction applied to trench backfill will influence performance of overlying structures including pavements. Fill placed into utility trenches should be compacted according to requirements of the local jurisdiction. Fill should be placed in horizontal lifts having compacted thickness of six inches or less and at a water content conducive adequate compaction, usually within ±2 percent of optimum water content. Typical compaction specifications would be similar to specifications in the Site Grading section. Mechanical methods should be used for fill placement; however, heavy equipment should be kept at a distance away from structures to avoid damage. No water flooding techniques of any type should be used for compaction or placement of utility trench backfill.

Trench backfill should be performed in accordance with El Paso County specifications and requirements. Excavations and excavation shoring/bracing should be performed in accordance with OSHA guidelines.

8.0 UNDERDRAIN SYSTEM

Depending on final site grading anticipated depths of excavations and structure foundations relative to groundwater occurrence, an underdrain system may be considered to be included as part of sewer system design and installation. The underdrain system drain pipe shall consist of

smooth wall non perforated rigid PVC pipe placed at a minimum slope of 2 percent. Shallower pipe grades can be considered for larger diameter underdrain pipes and areas to daylight the drainage systems. Concrete or clay material fill may be strategically placed at the manhole locations to slow the water flow down the trench. The underdrain below sewer should be constructed with adequate depth to allow connection of residence foundation drain systems. Drain elements should be of appropriate slopes and sizes for anticipated flows. Maintenance of the underdrain system should be anticipated. Gravity outlet should be planned such that other developments and properties are not adversely affected.

9.0 PAVEMENT CONSIDERATIONS

Materials exposed at pavement subgrade elevations will be dependent upon native materials exposed at final overlot grading and the specific materials placed as fill at and near finish grade elevations. The predominate materials are generally expected to be silty sand, sandstone, clayey sand, and clay. Materials anticipated at subgrade elevation generally would be rated as good, but some areas likely would be rated as poor AASHTO classifications of A-1-b, A-2-6, and A-4 were determined for the sandstone and upper granular soils. Based on depth to claystone and estimated cut, claystone with AASHTO classification of A-6 and associated poor rating is likely not to be encountered. The claystone classifies as A-6 which has poor asphalt support characteristics. Thickness of asphalt pavements to be anticipated generally range between 4 to 5 inches of asphalt overlying 6 to 10 inches of basecourse depending on specific subgrade materials and Roadway Classification of each particular street. Cement treated subgrade thickness of 10 to 12 inches are common. Actual thickness may exceed anticipated thickness at some areas. For specific thickness determinations, a subsurface investigation and pavement design should be completed after completion of overlot grading.

10.0 ANTICIPATED RESIDENTIAL FOUNDATION SYSTEMS

Subsurface soil conditions consisted of granular materials with some areas of expansive clayey soils and claystone materials. We anticipate conventional spread footing foundation systems will be appropriate for residences constructed on the majority of the site. Where expansive materials are encountered at or near foundation grades, use of spread footings with overexcavation and replacement with non-expansive fill should be expected. Drilled pier foundations may be a suitable alternative where expansive soils are encountered. A Subsurface Soils Investigation

report should be prepared after completion of overlot grading to address appropriate foundation systems. Perimeter below grade drain systems should be anticipated for all structures with basements. Overexcavation drains may also be recommended. Figures 3 and 4 present typical details. Shallow groundwater was encountered in numerous test borings. Temporary and permanent dewatering systems may be necessary at various foundation excavations. Shotrock and geotextiles may be appropriate for stabilizing excavations. An area wide subdrain may be considered for discharge of collected water.

11.0 RESIDENCE ON-GRADE FLOOR SLABS

On-grade floor slabs for the planned structures could be supported by on-site non-expansive soils or compacted, non-expansive, structural fill. Loose or expansive soils encountered at or near floor slab grade should be penetrated or overexcavated a distance below slab subgrade and replaced with a non-expansive structural fill to improve floor slab performance. If slab movement and cracks cannot be tolerated a structural floor system should be used. Evaluation of subgrade materials should be included within a Subsurface Soils Investigation for each specific lot.

12.0 CONCRETE DEGRADATION DUE TO SULFATE ATTACK

Sulfate solubility testing was conducted on eight samples recovered from the test borings to evaluate the potential for sulfate attack on concrete placed below surface grade. The test results indicated 0.00 to 0.01 percent soluble sulfate (by weight). The test results indicate the sulfate component of the in-place soils presents a negligible exposure threat to concrete placed below the site grade. Type II cement is recommended for the on-site soils. Additional testing should be conducted following completion of overlot grading.

13.0 EXCAVATION STABILITY

Excavation walls must be properly sloped/benched or otherwise supported in order to maintain stable conditions. All excavation openings and work execution shall conform to OSHA standards as in CFR 29, Part 1926.650-652 (Subport D).

14.0 SURFACE AND SUBSURFACE DRAINAGE

Surface drainage will influence performance of structures at the site including streets and residences. Drainage is recommended around each building perimeter at a minimum slope of 5 percent in the first 10 feet adjacent to exterior foundation walls and for unpaved areas, where possible. For paved areas and other impervious surfaces, a minimum slope of 2 percent is recommended. Drainage should be planned to avoid ponding of water. Collected water and irrigation should discharge well beyond foundation backfill zones. Surface runoff should be designed to avoid sheet flow and erosion. Slopes should be protected from erosion by materials such as mulch or appropriate plants or other methods. All fills and backfills should be properly compacted. Unprotected surfaces may be subject to undesirable, heavy erosion.

15.0 WINTER CONSTRUCTION

In the event construction occurs during winter, concrete and soil materials should be protected from freezing conditions. Concrete should not be placed on frozen soil and once concrete has been placed, it should not be allowed to freeze. Similarly, once exposed, the soil subgrades should not be allowed to freeze. During grading operations and subgrade preparation, care should be taken to avoid burial of snow, ice or frozen material within the planned construction area.

16.0 CONSTRUCTION OBSERVATIONS

It is recommended that Entech observe and document the following activities during construction of the building foundations.

- Excavated subgrades and subgrade preparation.
- Placement of foundation perimeter drains (if installed).
- Placement/compaction of fill materials.
- Placement/compaction of utility bedding and trench backfill.

17.0 CLOSURE

The subsurface investigation, geotechnical evaluation and preliminary recommendations presented in this report are intended for use by Tech Contractors with application to the planned development of the single-family residential project site located in the Rolling Hills Ranch Filings 1 - 4 subdivision in Meridian Ranch in northern El Paso County, Colorado. In conducting the subsurface soil investigation, laboratory testing, engineering evaluation and reporting, Entech Engineering, Inc. endeavored to work in accordance with generally accepted professional geotechnical and geologic practices and principles consistent with the level of care and skill ordinarily exercised by members of the geotechnical profession currently practicing in same locality and under similar conditions. No other warranty, expressed or implied is made. Additional subsurface investigations and testing are recommended to further evaluate the individual sites and roadways after final development plans are prepared and after the site has been graded. During final design and/or construction, if conditions are encountered which appear different from those described in this report, Entech Engineering, Inc. requests that it be notified so that the evaluation and recommendations presented herein can be reviewed and modified as appropriate.

If there are any questions regarding the information provided herein or if Entech Engineering, Inc. can be of further assistance, please do not hesitate to contact us.

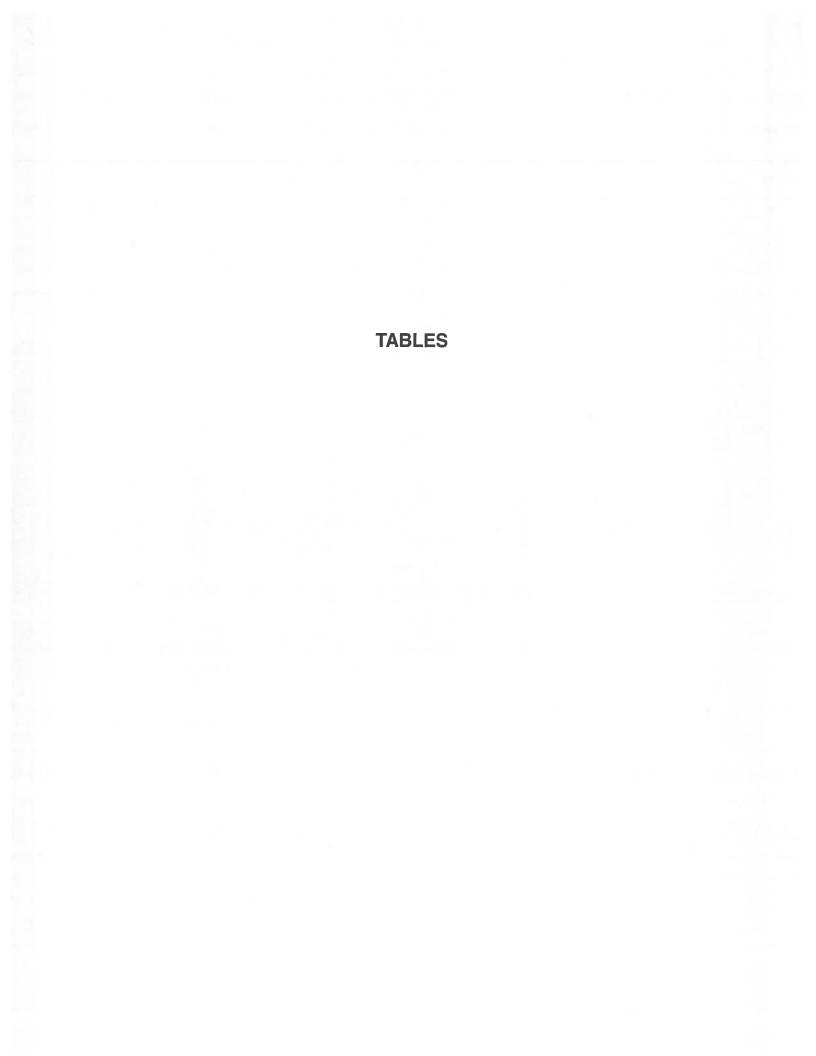


TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS
JOB NO. 190300

	_	_		T	_		_	_	_					_	_	_	_	_						_			_	_	_	_	_	_	_	_		_
SOIL DESCRIPTION	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, CLAYEY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND SILTY	SAND, VERY CLAYEY	SAND	SAND, CLAYEY	SAND	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND	SAND, CLAYEY	CLAY, SANDY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SAND, SILTY	SAND, SLIGHTLY SILTY	SANDSTONE, CLAYEY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY
UNIFIED CLASS.	SM-SW	SM-SW	SC	SM	SM-SW	SM	SM	SM	SC	SW	SC	SW	SM	SM-SW	SM	SM-SW	SW	SC	7	SM-SW	SM-SW	SM-SW	SM	SM	SM-SW	SM	SM-SW	SC	SM-SW	SM	SC	SM	SM	SM	SC	SM
SWELL/ CONSOL (%)															-1.2																					
FHA SWELL (PSF)				370					460					70					2970							220										
AASHTO CLASS.	A-1-b		A-2-6			A-1-b				A-1-b	A-2-4		A-1-b			A-1-b	A-1-b					A-1-b			A-1-b			A-2-6	A-1-b		A-2-6				A-6	A-1-b
SULFATE (WT %)	<0.01		0.01			0.00																													<0.01	<0.01
PLASTIC INDEX (%)	NP		16			NP				ΝP	10		NP			NP	NP					NP			P.			14	NP		20				13	₽ N
LIQUID LIMIT (%)	Ν		29			N				NV	56		N			N	N					NV			2			32	N<		37				26	N
PASSING NO. 200 SIEVE (%)	8.1	6.1	14.0	15.2	8.4	17.0	18.0	15.6	48.3	4.7	13.3	4.8	13.2	5.9	34.7	11.5	4.9	12.1		6.9	5.4	8.6	17.8	19.6	6.0	20.7	7.3	18.6	7.3	14.2	17.1	12.5	16.0	14.3	38.9	17.5
DRY DENSITY (PCF)															112.9																					
WATER (%)															10.0					1																
ОЕРТН (FT)	2-3	5	5	2-3	2-3	2-3	2-3	10	5	2-3	2-3	2-3	2	D.	2-3	2	2-3	2	က	2	2	2-3	2	2	2-3	2-3	5	9	9	2	2	9	9	9	20	15
TEST BORING NO.	9	8	9	11	2	23	24	32	27	-	2	13	14	16	19	56	28	30	30	30	31	38	33	42	43	47	49	7	17	18	20	21	41	4	9	6
SOIL	-	-	-	-	1	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	2	2	7	2	2	2	2	2	2

TABLE 1 (cont.)

SOIL DESCRIPTION	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, VERY CLAYEY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY	CLAYSTONE, VERY SANDY	CLAYSTONE, SANDY					
UNIFIED CLASS.	SM	SM	SC	SM	SM	SM-SW	SM-SW	SM	SM	SC	SC	SM	SC	SC	SM	SC	SC	သွင	SM	SC	ر ا	ر ا	ر ا	ರ	ರ	占	ರ	덩	ರ	占
SWELL/ CONSOL (%)			-0.4							-1.9				3.2			-0.4					1.0	0.0			-0.7			0.7	2.5
FHA SWELL (PSF)																												06		
AASHTO CLASS.				A-1-b	A-2-4					A-2-6	A-6			A-6		A-2-6								A-6	A-6					A-7-6
SULFATE (WT %)			0.00	<0.01																										
PLASTIC INDEX (%)				NP	NP					12	14			14		17								15	17					20
LIQUID LIMIT (%)				N	N					29	31			28		41								34	34					42
PASSING NO. 200 SIEVE (%)	15.5	26.1	35.4	12.3	28.7	11.6	10.1	16.2	15.5	20.3	48.5	17.8	19.9	49.7	21.2	28.3	49.6	41.1	13.4	45.5	65.1	56.1	58.8	54.2	59.6	51.1	59.7	63.6	56.0	80.8
DRY DENSITY (PCF)			116.5							110.3				84.0			119.9					126.8	120.5	99.3		103.3		i	114.3	115.0
WATER (%)			11.4							9.3				7.4			4.5					7.2	9.5	12.7		12.5			11.5	16.5
DEPTH (FT)	10	5	5	10	15	10	2	10	15	50	25	20	15	20	25	15	10	15	20	15	2	9	20	10	15	50	15	5	9	우
TEST BORING NO.	12	က	37	40	25	23	35	27	-	4	5	14	15	50	21	28	59	39	45	46	19	15	16	22	38	48	36	24	34	33
SOIL	2	2	2	2	5	2	2	5	2	2	2	2	5	2	5	2	2	2	2	2	ဇ	က	ဗ	3	ဇ	3	ဗ	က	က	33

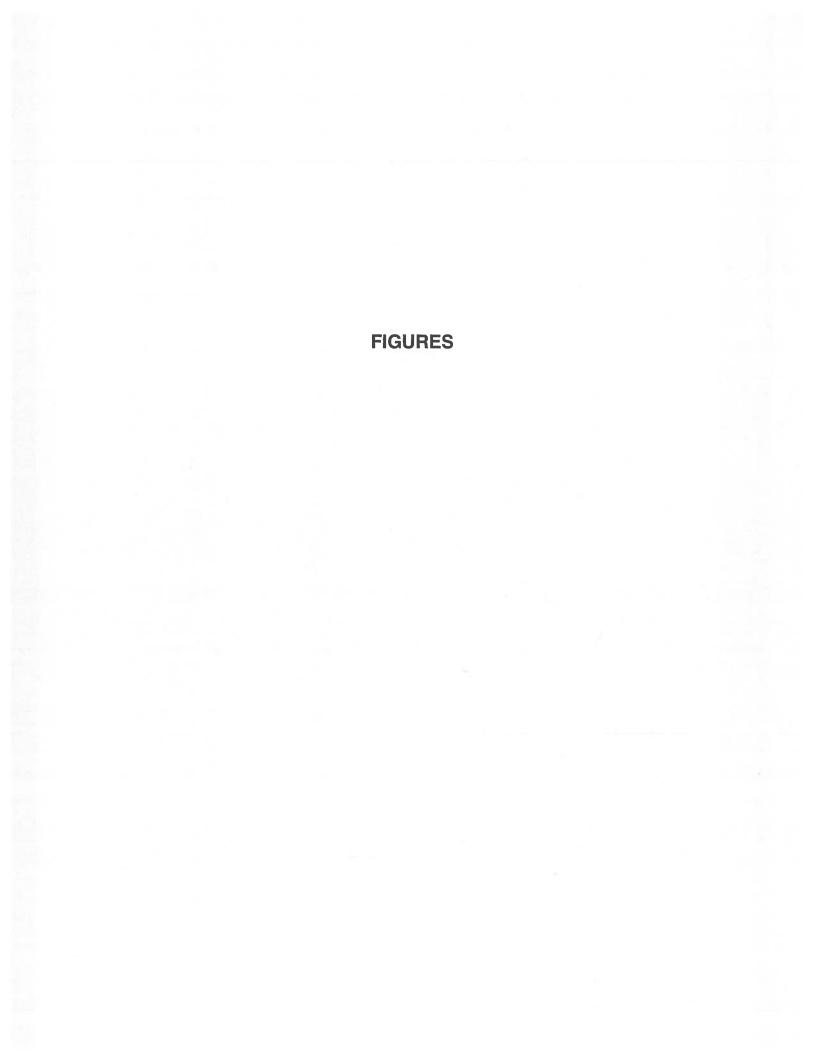
Table 2: Summary of Test Borings and Water Measurements*

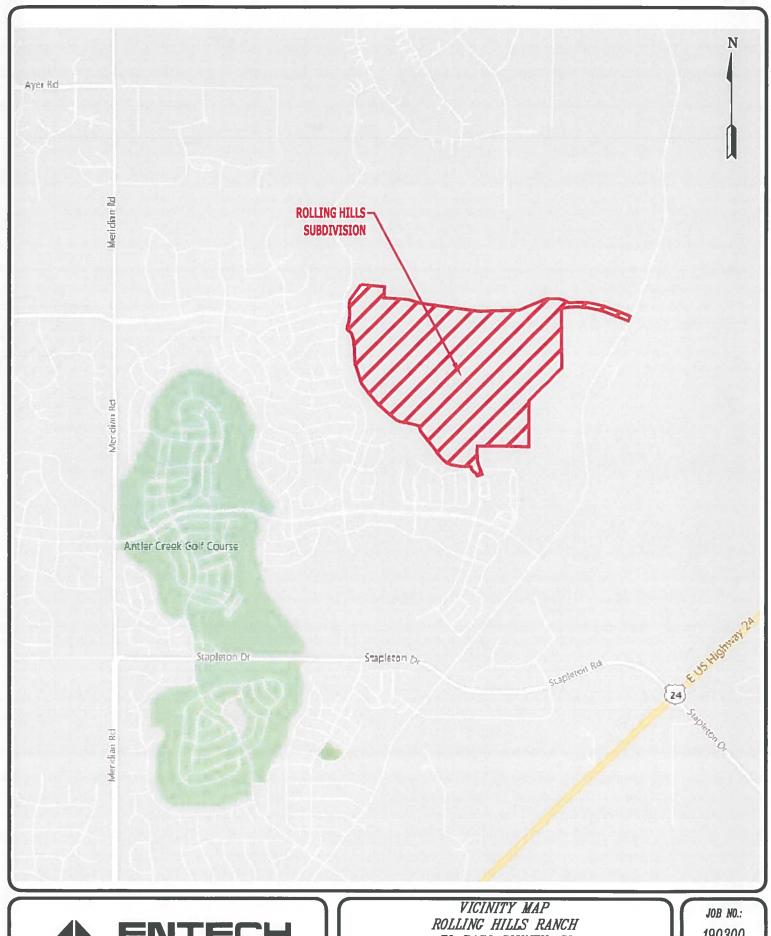
Test	Depth of	Depth to	Depth to	Cut & Fill**	Estimated	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
1	20.0	9.0	9.0	0 to -2	7021.3	7012.3
2	25.0	9.0	13.0	-2 to -4	7031.5	7018.5
3	25.0	1.0	15.0	-2 to -4	7032.3	7017.3
4	20.0	1.0	dry	-2 to -4	7044.0	dry
5	25.0	4.0	14.0	-2 to -4	7044.8	7030.8
6	25.0	14.0	10.0	0 to +2	7054.7	7044.7
7	20.0	1.0	16.5	+2 to +4	7058.6	7042.6
8	20.0	9.0	13.0	0 to -2	7060.1	7047.1
9	20.0	14.0	10.0	+4 to +6	7069.7	7059.7
10	20.0	14.0	14.0	0 to -2	7077.5	7063.5
11	20.0	9.0	9.0	0 to +2	7071.6	7062.6
12	20.0	9.0	14.0	0 to -2	7087.3	7073.3
13	20.0	9.0	14.0	0 to -2	7092.0	7078.0
14	25.0	14.0	18.5	-6 to -8	7105.3	7086.8
15	20.0	9.0	18.0	0 to -2	7108.4	7090.4
16	25.0	9.0	16.0	0 to -2	7110.9	7094.9
17	20.0	1.0	17.5	0 to -2	7121.7	7104.2
18	20.0	4.0	dry	0 to +2	7120.7	dry
19	20.0	4.0	dry	+2 to +4	7126.5	dry
20	20.0	1.0	dry	outside cut/fill	7125.4	dry
21	25.0	1.0	10.0	-6 to -8	7105.7	7095.7
22	20.0	4.0	18.5	-6 to -8	7106.0	7087.5
23	20.0	9.0	dry	+2 to +4	7092.3	dry
24	25.0	4.0	2.0	0 to +2	7072.9	7070.9

Table 2: (Continued)

Test	Depth of	Depth to	Depth to	Cut & Fill**	Est.	Estimated
Boring No.	Boring (ft.)	Bedrock	Groundwater	(-/+, ft.)	Ground	Groundwater
		(ft.)	(ft.)		Elevation	Elevation
25	20.0	1.0	12.0	0 to +2	7068.8	7056.8
26	20.0	1.0	17.0	-6 to -8	7049.2	7032.2
27	20.0	9.0	8.0	0 to +2	7071.2	7063.2
28	20.0	9.0	13.5	0 to -2	7082.9	7069.4
29	25.0	4.0	12.0	outside cut/fill	7084.4	7072.4
30	20.0	10.0	8.0	0 to +2	7066.7	7058.7
31	20.0	14.0	dry	0 to -2	7057.5	dry
32	25.0	14.0	13.0	0 to -2	7045.4	7032.4
33	25.0	9.0	7.0	0 to -2	7052.7	7045.7
34	20.0	1.0	9.0	+2 to +4	7042.0	7033.0
35	20.0	3.0	dry	0 to -2	7065.4	dry
36	25.0	1.0	23.0	-6 to -8	7049.4	7026.4
37	20.0	1.0	dry	-2 to -4	7038.8	dry
38	25.0	12.0	10.0	-6 to -8	7032.4	7022.4
39	20.0	9.0	4.0	-6 to -8	7032.5	7028.5
40	20.0	9.0	10.0	+12 to +14	7032.1	7022.1
41	20.0	1.0	17.0	outside cut/fill	7039.1	7022.1
42	25.0	9.0	14.0	outside cut/fill	7046.0	7032.0
43	25.0	4.0	19.0	outside cut/fill	7049.0	7030.0
44	20.0	1.0	dry	outside cut/fill	7064.0	dry
45	25.0	4.0	11.0	outside cut/fill	7072.1	7061.1
46	25.0	4.0	22.0	outside cut/fill	7065.0	7043.0
47	20.0	1.0	dry	outside cut/fill	7058.7	dry
48	20.0	1.0	dry	outside cut/fill	7047.6	dry
49	25.0	14.0	12.0	outside cut/fill	7029.5	7017.5

Measurement taken subsequent to drillingCut and Fill estimates based on map provided by the client







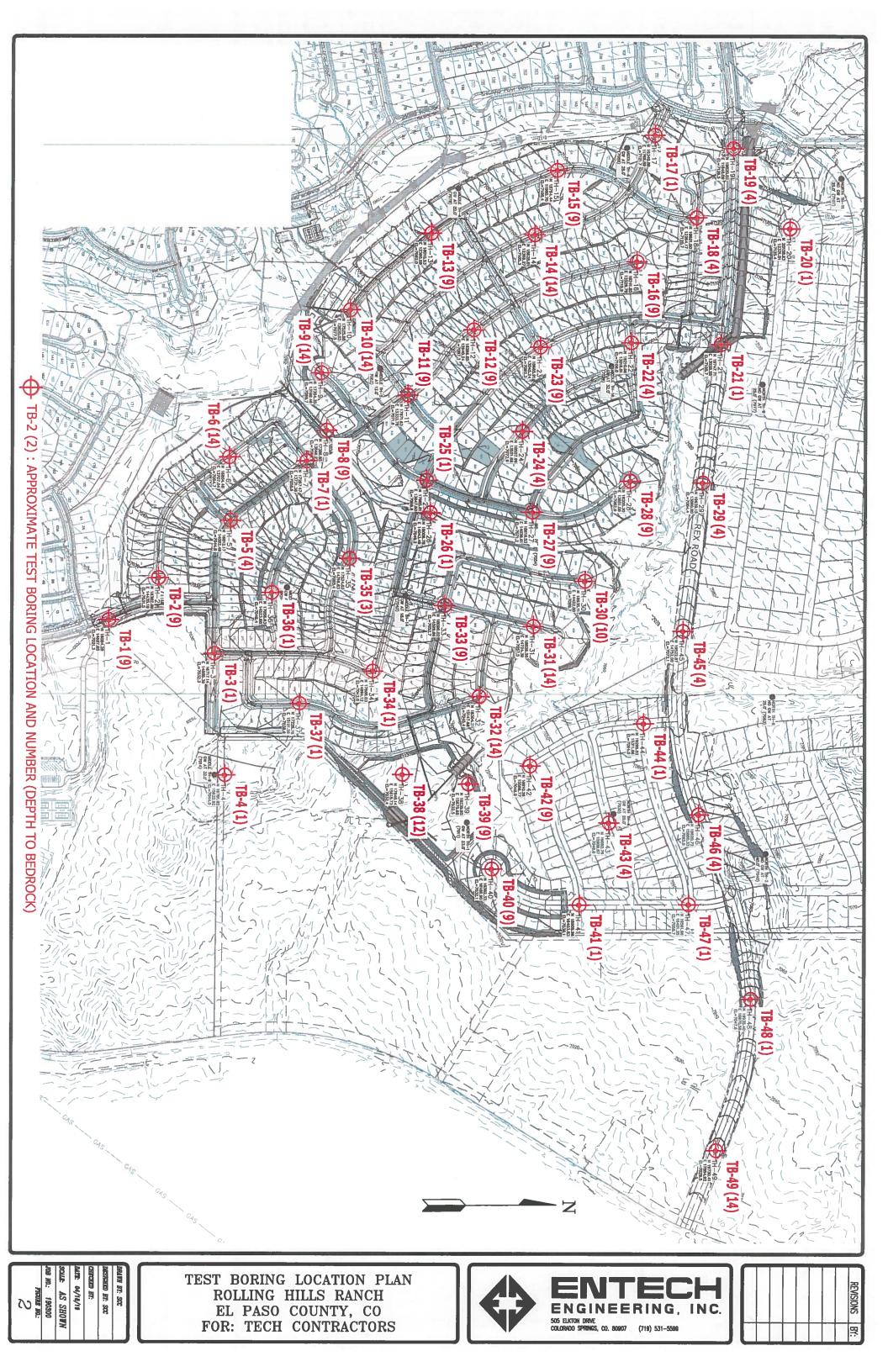
	VICINITY MAP												
	ROLLING HILLS RANCH												
	EL	PASO	COUNTY,	CO									
	FOR:	TECH	CONTRAC	TORS									
\neg													

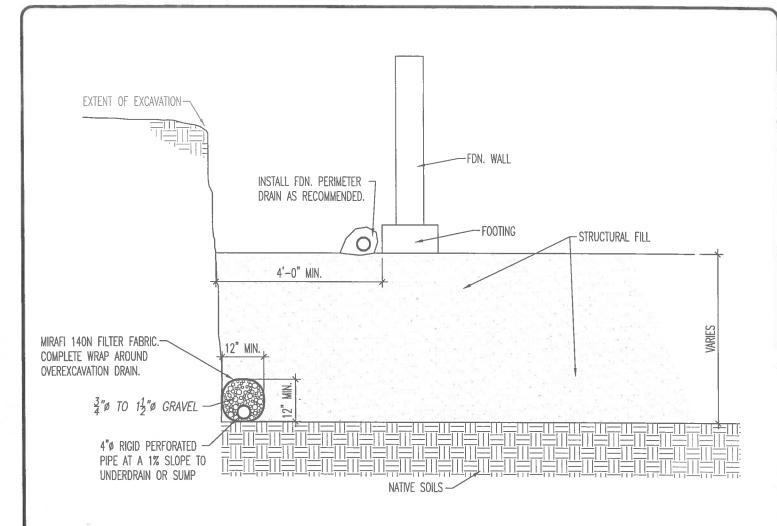
DRAWN BY: SC DATE DRAWN: 04/18/19

DESIGNED BY: SC

CHECKED: SC

190300 FIG. NO.:





OVEREXCAVATION DRAIN DETAIL

N.T.S.

NOTE:

EXTEND DRAIN TO SUMP AS REQ'D.



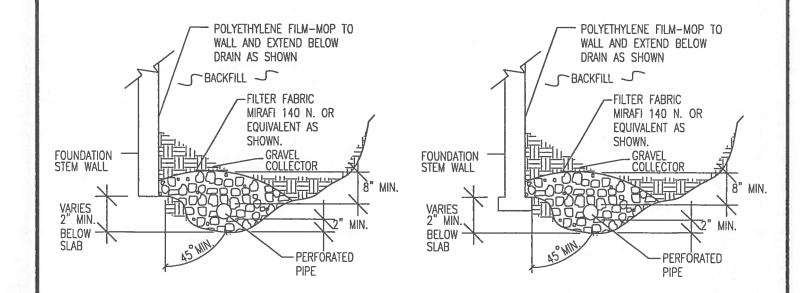
OVEREXCAVATION DRAIN DETAIL

DRAWN BY: M. WELLS

DATE DRAWN:

DESIGNED BY: D. STEGMAN CHECKED:

JOB NO.: 190300 FIG. NO.:



NOTES:

- -GRAVEL SIZE IS RELATED TO DIAMETER OF PIPE PERFORATIONS-85% GRAVEL GREATER THAN 2x PERFORATION DIAMETER.
- -PIPE DIAMETER DEPENDS UPON EXPECTED SEEPAGE. 4-INCH DIAMETER IS MOST OFTEN USED.
- -ALL PIPE SHALL BE PERFORATED PLASTIC. THE DISCHARGE PORTION OF THE PIPE SHOULD BE NON-PERFORATED PIPE.
- -FLEXIBLE PIPE MAY BE USED UP TO 8 FEET IN DEPTH, IF SUCH PIPE IS DESIGNED TO WITHSTAND THE PRESSURES. RIGID PLASTIC PIPE WOULD OTHERWISE BE REQUIRED.
- -MINIMUM GRADE FOR DRAIN PIPE TO BE 1% OR 3 INCHES OF FALL IN 25 FEET.
- -DRAIN TO BE PROVIDED WITH A FREE GRAVITY OUTFALL, IF POSSIBLE. A SUMP AND PUMP MAY BE USED IF GRAVITY OUT FALL IS NOT AVAILABLE.



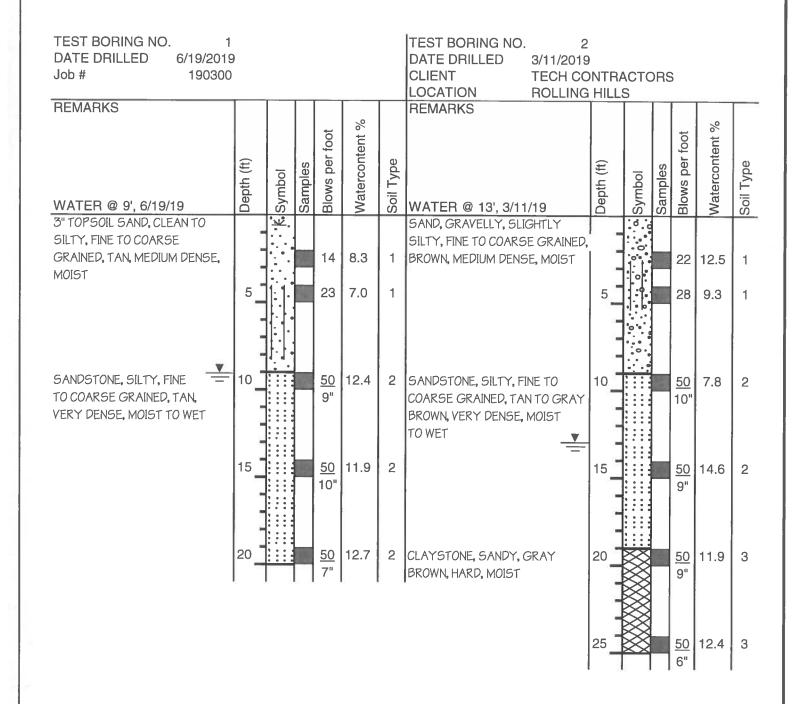
PERIMETER	DRAIN	DETAIL
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DRAWN: DATE: DESIGNED: CHECKED:

JOB NO.: 190300

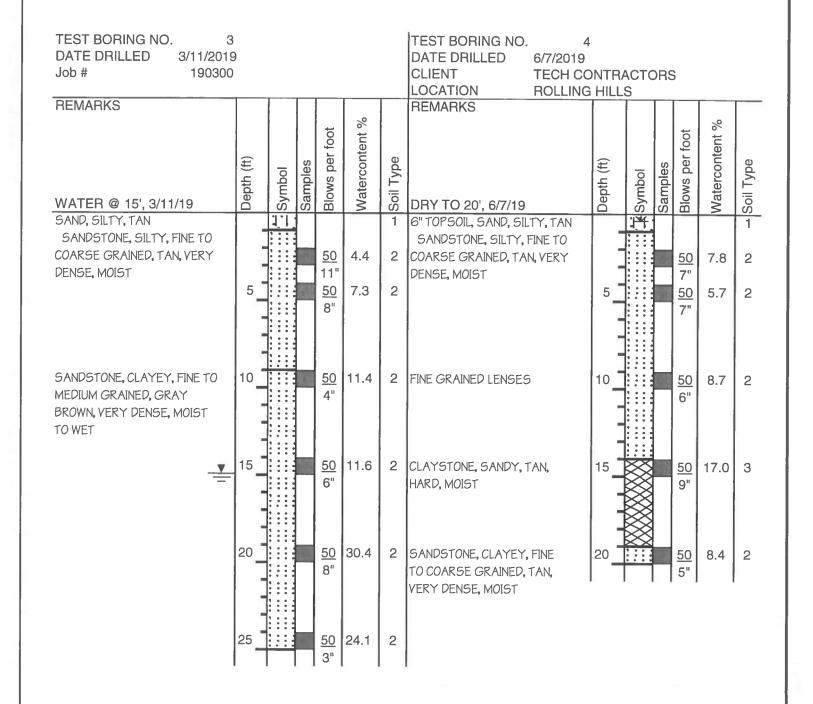
FIG NO.:

APPENDIX A: Test Boring Logs





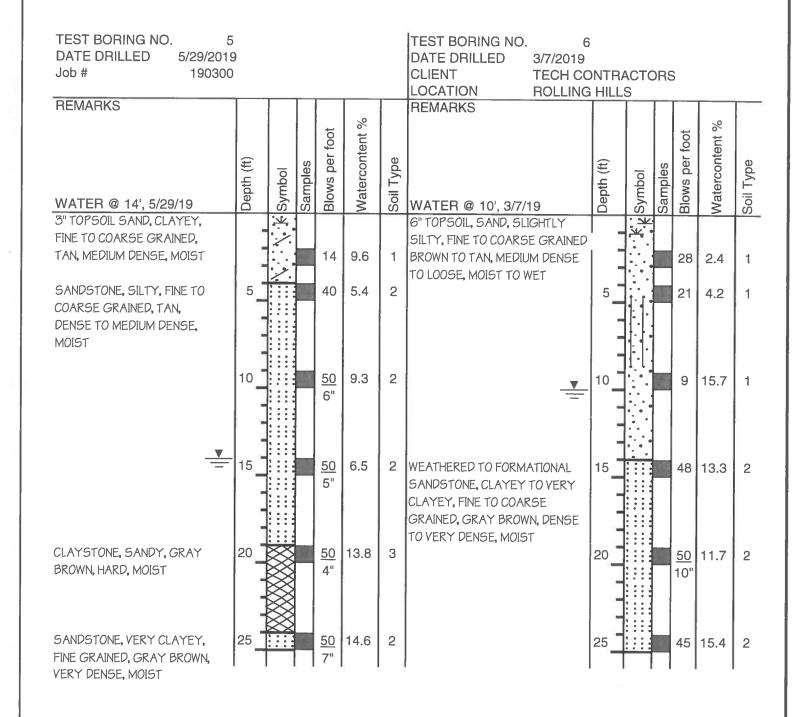
	TE	ST BORING LO	G
DRAWN:	DATE	CHECKED:	DATE: 7/11/9





	TES	ST BORING LOC	3
DRAWN:	DATE:	CHECKED:	DATE:

FIG NO.: A- 2





	TEST	BORING LOG	ì	
DRAWN:	DATE:	CHECKED:	7/1/19	

FIG NO.:

TEST BORING NO. 7 TEST BORING NO. 8 DATE DRILLED 5/29/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Watercontent Blows per foot Watercontent Soil Type Depth (ft) \equiv Samples Soil Type Symbol Samples Symbol Depth WATER @ 16.5', 5/29/19 WATER @ 13', 3/7/19 6" TOPSOIL, SAND, SILTY, TAN 6" TOPSOIL, SAND, SLIGHTLY WEATHERED SANDSTONE. SILTY, FINE TO COARSE GRAINED. SILTY, FINE TO COARSE 46 4.8 2 BROWN, MEDIUM DENSE, MOIST 23 4.1 1 GRAINED, DENES, MOIST 45 9.0 2 11 6.0 1 SANDSTONE, CLAYEY TO 10 50 8.1 SANDSTONE, SILTY, FINE TO 10 50 8.5 2 SILTY, FINE TO COARSE 6" COARSE GRAINED, TAN, VERY 9" GRAINED, TAN, VERY DENSE, DENSE, MOIST TO WET MOIST TO WET 15 2 <u>50</u> 10.7 15 50 17.8 2 FINE GRAINED LENSES 3" 20 <u>50</u> 2 11.1 <u>50</u> 16.6 2



DRAWN:	DATE	CHECKED:	7/1/19

TEST BORING LOG

JOB NO.: 190300 FIG NO.:

TEST BORING NO. 9 TEST BORING NO. 10 DATE DRILLED 3/7/2019 DATE DRILLED 3/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS **REMARKS** Blows per foot Watercontent Natercontent Blows per Soil Type Depth (ft) Soil Type Samples Depth (ft) Samples Symbol Symbol WATER @ 10', 3/7/19 WATER @ 14', 3/7/19 6" TOPSOIL, SAND, SILTY, FINE 6" TOPSOIL, SAND, SILTY TO <u> 4</u> TO COARSE GRAINED, BROWN, CLAYEY, FINE TO COARSE MEDIUM DENSE, DRY TO MOIST 16 2.7 1 GRAINED, TAN, MEDIUM DENSE, 26 6.2 1 MOIST 5 11 6.6 1 5 19 7.8 SAND, CLAYEY, FINE TO 10 5 18.0 1 27 10 12.4 COARSE GRAINED, GRAY BROWN, LOOSE, WET 15 SANDSTONE, SILTY, FINE TO <u>50</u> 8.7 SANDSTONE, CLAYEY. 15 2 50 12.5 COARSE GRAINED, TAN, VERY FINE TO COARSE GRAINED, 10" DENSE, MOIST BRPOWN, VERY DENSE TO DENSE, WET 2 <u>50</u> 10.9 WEATHERED ZONE 45 | 13.8 2



	1231	DORING	LOG	l
DATE:		CHECKED:	2	DATE: 7/19

DRAWN:

TECT DODING LOC

JOB NO.: 190300 FIG NO.:

TEST BORING NO. 11 TEST BORING NO. 12 DATE DRILLED 3/7/2019 DATE DRILLED 3/7/2019 Job# 190300 **CLIENT TECH CONTRACTORS** LOCATION **ROLLING HILLS REMARKS REMARKS** Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Soil Type Samples Samples Symbol Symbol WATER @ 9', 3/7/19 WATER @ 14', 3/7/19 <u>*</u> SAND, SILTY, FINE TO COARSE 6" TOPSOIL, SAND, SILTY, FINE GRAINED, TAN, LOOSE TO TO COARSE GRAINED, BROWN, MEDIUM DENSE, VERY MOIST 7 21.3 1 LOOSE TO MEDIUM DENSE, 6 3.6 1 MOIST 5 15.1 16 1 23 8.6 SANDSTONE, SILTY, FINE 10 <u>50</u> 17.5 WEATHERED TO FORMATIONAL 10 2 36 | 11.3 TO COARSE GRAINED, TAN, 11" SANDSTONE, SILTY, FINE TO VERY DENSE, WET COARSE GRAINED, BROWN, DENSE TO VERY DENSE, MOIST TO WET 15 2 <u>50</u> 12.6 **CLAYEY LENSES** 15 2 <u>50</u> 20.2 8" 11" 20 <u>50</u> 12.7 <u>50</u> 12.8 2



TEST BORING LOG					
DRAWN:	DATE:	CHECKED:	7/1/19		

TEST DODING LOC

JOB NO.: 190300

FIG NO.: 6

TEST BORING NO. 13 TEST BORING NO. 14 DATE DRILLED 5/29/2019 DATE DRILLED 5/29/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS **REMARKS** Blows per foot Blows per foot **Natercontent** Watercontent Soil Type Depth (ft) Soil Type Samples Depth (ft) Samples Symbol Symbol WATER @ 14', 5/29/19 WATER @ 18.5', 5/29/19 6" TOPSOIL, SAND, CLEAN TO 6" TOPSOIL, SAND, SILTY, FINE SILTY, FINE TO COARSE TO COARSE GRAINED, TAN. GRAINED, TAN, LOOSE TO 11 1.4 1 LOOSE TO MEDIUM DENSE. 13 1.8 1 MEDIUM DENSE, MOIST DRY TO MOIST 5 14 6.3 1 7 2.3 WEATHERED TO FORMATIONAL 10 45 8.4 2 FINE GRAINED LENSES 10 24 9.1 1 SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, DENSE TO VERY DENSE. MOIST TO WET 15 48 8.9 SANDSTONE, SILTY, FINE TO 15 6.7 2 50 COARSE GRAINED, TAN, 11" VERY DENSE, MOIST TO WET 2 <u>50</u> 11.5 20 <u>50</u> 10.6 2 11" <u>50</u> 12.6 2

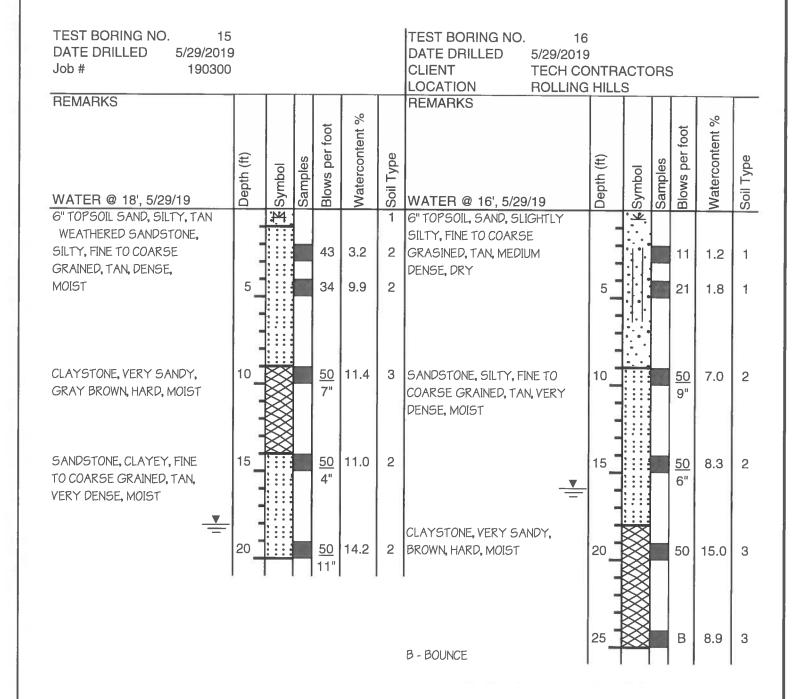


TEST BO	RING	LOG
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DRAWN: DATE: CHECKED: 17 7/11/19

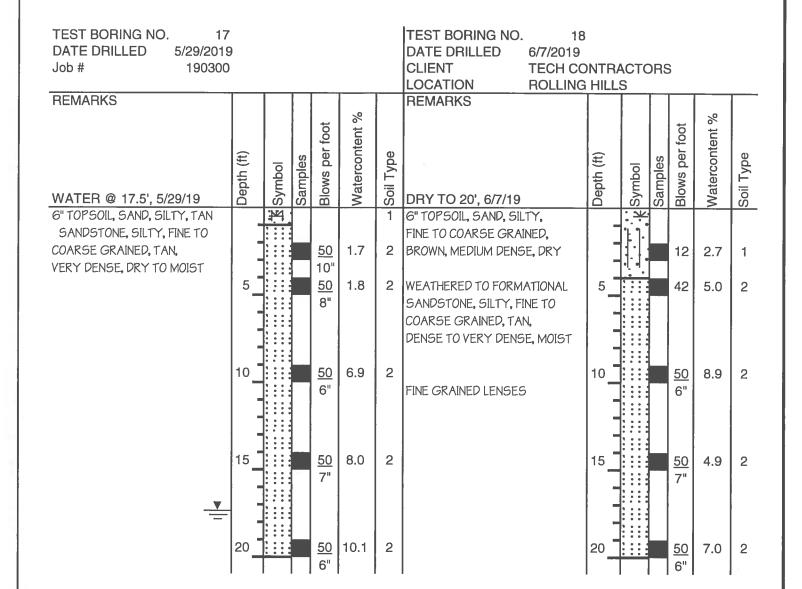
JOB NO.: 190300

FIG NO.: 7





	TEST BORING LOG				
DRAWN:	DATE:	CHECKED:	7/1/19		





TEST BORING LOG			
DRAWN:	DATE:	CHECKED:	7/1/19

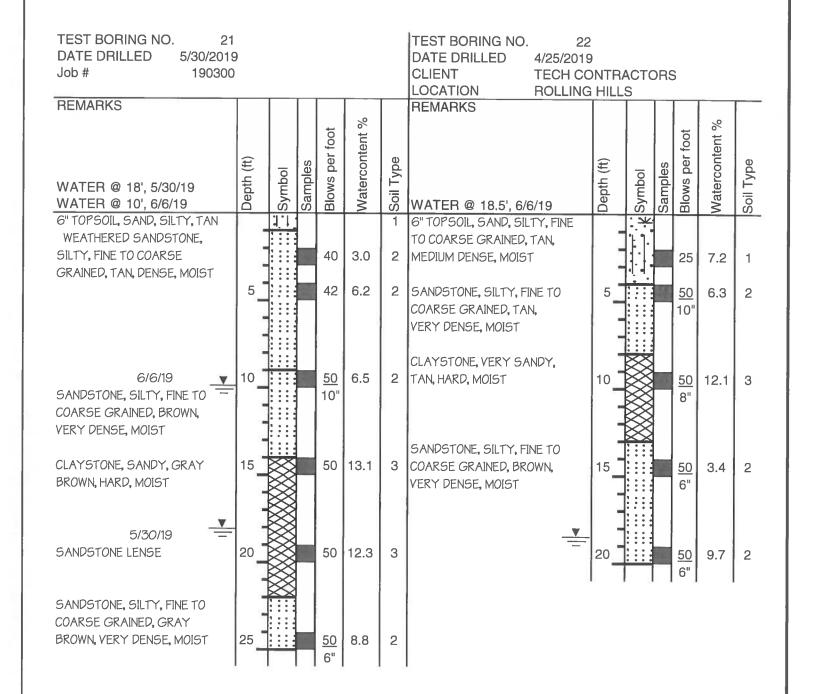
JOB NO.: 190300 FIG NO.:

TEST BORING NO. 19 TEST BORING NO. 20 DATE DRILLED 6/7/2019 DATE DRILLED 5/30/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS % Blows per foot Natercontent Watercontent Blows per Depth (ft) Samples Soil Type Samples Symbol Symbol DRY TO 20', 5/30/19 DRY TO 20', 6/7/19 CAVED TO 19', 6/6/19, DRY 6" TOPSOIL SAND, SILTY, FINE 6" TOPSOIL, SAND, SILTY, TAN 14 TO COARSE GRAINED, GRAY SANDSTONE, SILTY TO BROWN, MEDIUM DENSE, MOIST 21 7.8 1 CLAYEY, FINE TO COARSE 50 2 4.8 10" GRAINED, TAN, VERY DENSE, CLAYSTONE, SANDY, GRAY 3 <u>50</u> 10.9 DRY TO MOIST 5 50 8.6 2 BROWN, HARD, MOIST 9" 9" SANDSTONE, SILTY, FINE TO 10 <u>50</u> 7.8 2 10 50 6.5 2 8" COARSE GRAINED, TAN, 9" VERY DENSE, MOIST 15 <u>50</u> 5.7 2 CLAYSTONE, SANDY, GRAY 15 50 10.4 3 8" BROWN, HARD, MOIST 20 <u>50</u> 8.9 2 SANDSTONE, VERY CLAYEY, 2 <u>50</u> 8.0 6" 2" FINE TO COARSE GRAINED. BROWN, VERY DENSE, MOIST



TEST BORING LOG				
DRAWN:	DATE:	CHECKED:	6	DATE:/19

JOB NO.: 190300 FIG NO.:



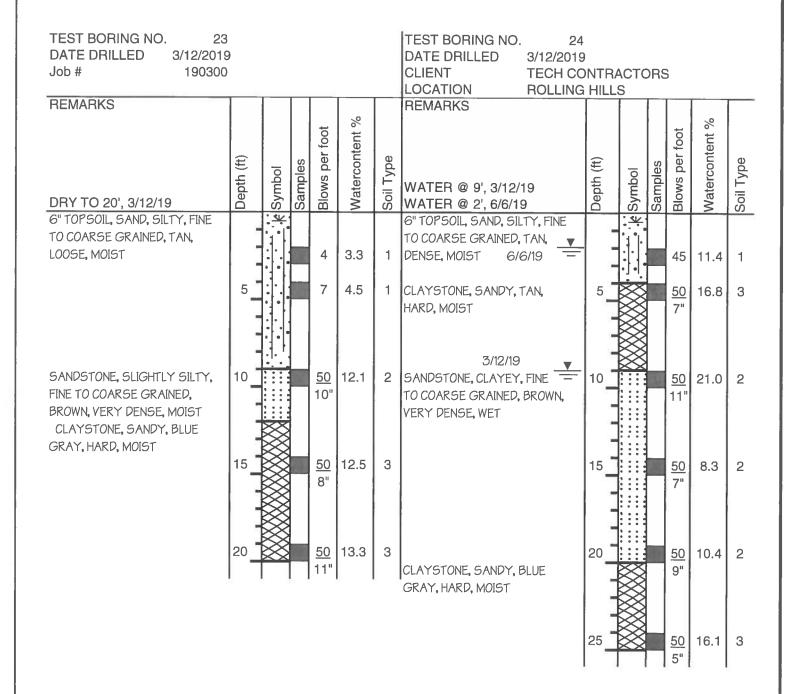
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DATE	CHECKED	h	75	ATE 19

TEST BORING LOG

JOB NO.: 190300

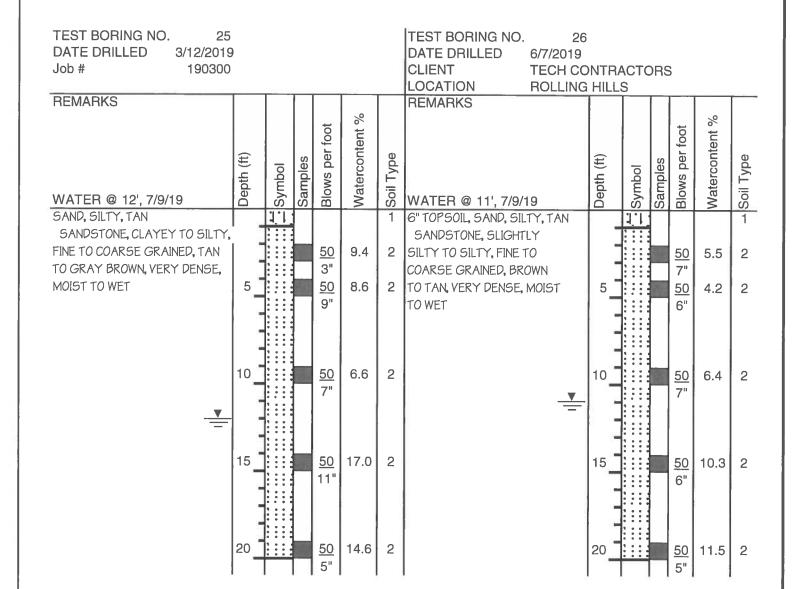




	TES	T BORING LO	3
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JOB NO.: 190300

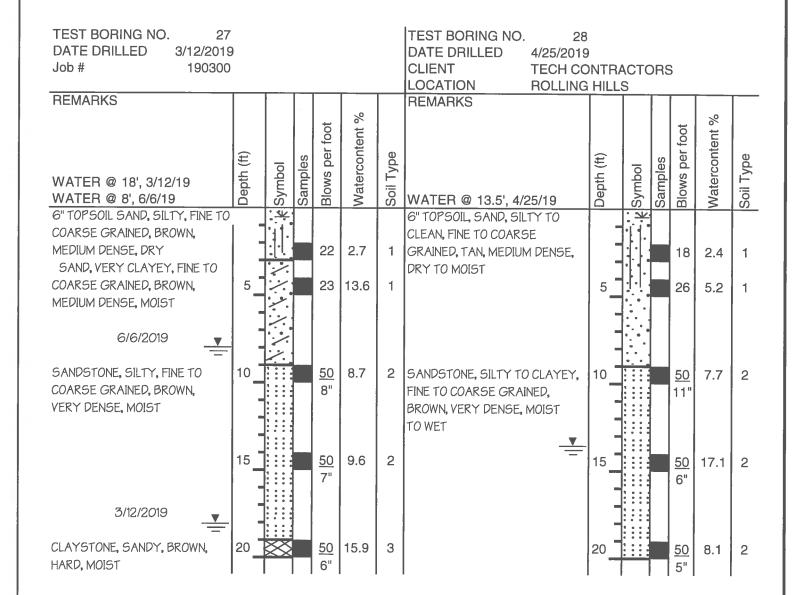
A- 12





TEST BORING LOG			
DRAWN:	DATE:	CHECKED:	DATE: 7.12.19

JOB NO.: 190300 FIG NO.: A- 13



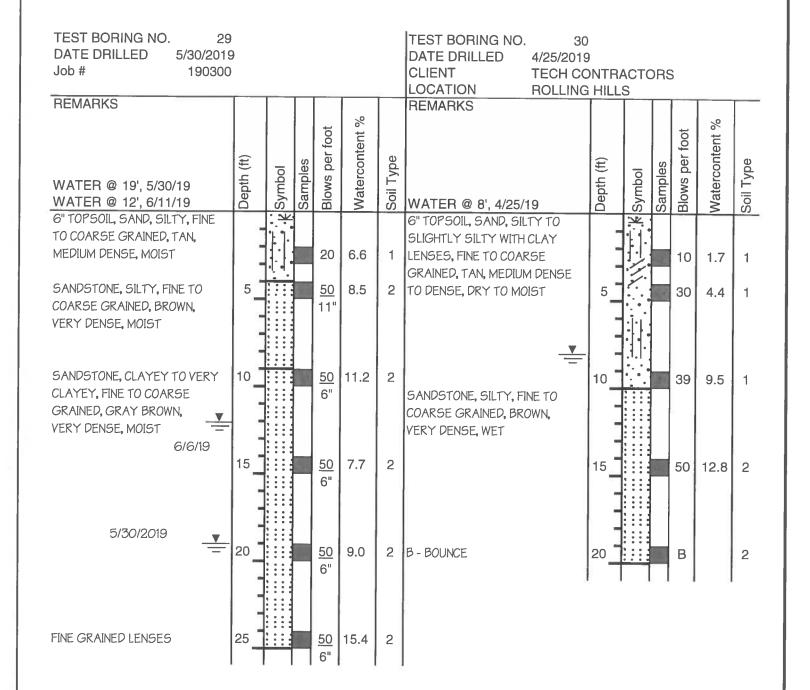


DRAWN:	DATE:	CHECKED:	DATE: 19

TEST BORING LOG

JOB NO.: 190300 FIG NO.:

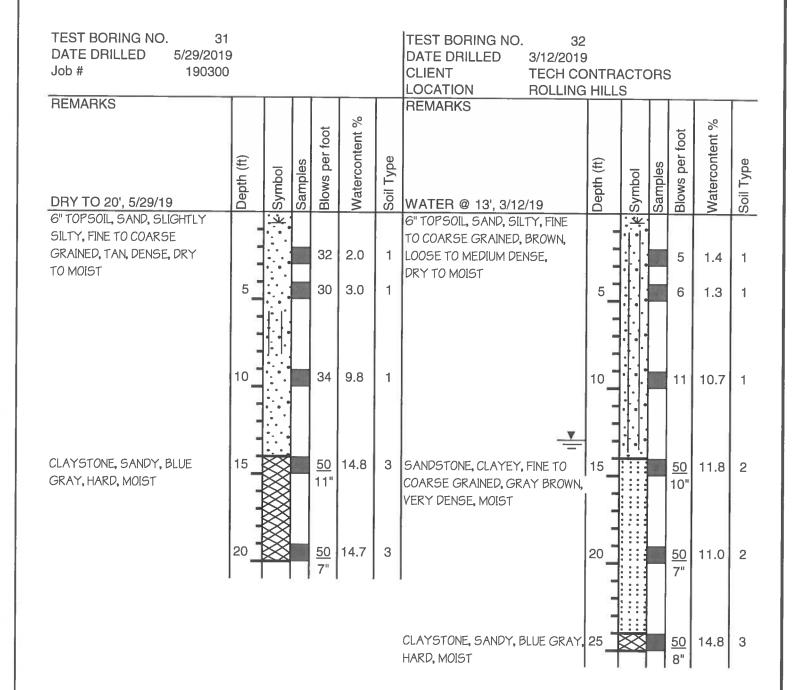
A- 14





	TES	ST BORING LOG	ì
DRAWN:	DATE:	CHECKED	DATE: 7:12.19

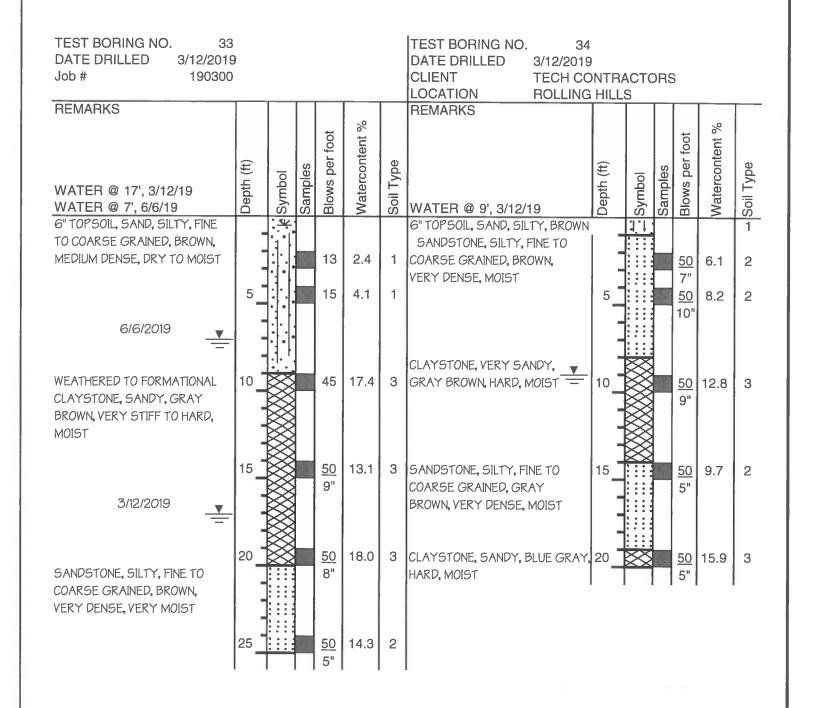
JOB NO.: 190300 FIG NO.: A- 15





	TE	ST BORING LOG	· ·
DRAWN:	DATE:	CHECKED:	DATE: 7/12/19

JOB NO.: 190300 FIG NO.: A- 16





	TES	T BORING LOC	à
DRAWN:	DATE:	CHECKED:	7/12/19

JOB NO.: 190300

FIG NO.: A- 17

TEST BORING NO. 35 TEST BORING NO. 36 DATE DRILLED 3/12/2019 DATE DRILLED 3/11/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Soil Type Samples Samples Symbol Symbol Depth (DRY TO 20', 3/12/19 WATER @ 13.5', 7/9/19 <u>. 44</u> 6" TOPSOIL SAND, SILTY, FINE SAND, SILTY, TAN 1.1 TO COARSE GRAINED, TAN, SANDSTONE, SILTY, FINE TO DENSE, MOIST 48 3.6 1 COARSE GRAINED, TAN, VERY <u>50</u> 3.1 2 SANDSTONE, SLIGHTLY SILTY 7" DENSE, MOIST TO SILTY, FINE TO COARSE 5 50 6.0 2 50 3.7 2 GRAINED, BROWN, VERY DENSE, 6" MOIST 10 <u>50</u> 8.9 2 10 50 10.9 2 9" 15 50 9.7 CLAYSTONE, VERY SANDY, BLUE 15 3 50 12.2 GRAY, HARD, MOIST 6" CLAYSTONE, SANDY, BLUE GRAY, HARD, MOIST <u>50</u> 11.7 SANDSTONE, CLAYEY, FINE TO 20 13.4 2 50 COARSE GRAINED, GRAY BROWN 10" TO BROWN, VERY DENSE, MOIST TO WET <u>50</u> 16.8 2

DRAWN:



TEST	BORING LOG	ì	
DATE	CHECKED:	-PATE/10	

JOB NO.: 190300

TEST BORING NO. 37 TEST BORING NO. 38 DATE DRILLED 3/12/2019 DATE DRILLED 6/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Soil Type Samples Samples Symbol Symbol Depth (DRY TO 20', 3/12/19 WATER @ 18', 7/9/19 SAND, SILTY, BROWN 1.1 6" TOPSOIL, SAND, GRAVELLY. 9/ CLAYSTONE, SANDY, BROWN, SILTY TO SLIGHTLY SILTY. HARD, MOIST <u>50</u> 11.6 FINE TO COARSE GRAINED. 1.7 1 11" BROWN, LOOSE TO MEDIUM SANDSTONE, CLAYEY, FINE TO 5 50 10.1 2 DENSE, MOIST 12 0.7 1 COARSE GRAINED, TAN, VERY 10" DENSE, MOIST 10 <u>50</u> 2 :: 11.3 10 -7.6 CLAYSTONE, SANDY, BROWN, MOIST 15 <u>50</u> 9.2 2 15 3 19.1 7"

<u>50</u>

6"

9.3

2

* - BULK SAMPLE TAKEN

GRAY, HARD, MOIST

SANDSTONE, SILTY, FINE TO

COARSE GRAINED, BROWN, VERY DENSE, MOIST

CLAYSTONE, SANDY, BLUE

20

B-BOUNCE



	TEST	BORING LOG	
DRAWN:	DATE:	CHECKED:	7/12/19

JOB NO.: 190300

12.1

9.4

50

В

2

3

FIG NO.: A- 19

TEST BORING NO. 39 TEST BORING NO. 40 DATE DRILLED 5/29/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Samples Depth (ft) Soil Type Samples Symbol Symbol WATER @ 11', 7/9/19 WATER @ 10', 3/12/19 6" TOPSOIL, SAND, SILTY, FINE 6" TOPSOIL, SAND, SILTY, FINE <u> 4</u> TO COARSE GRAINED, TAN, TO COARSE GRAINED, TAN. MEDIUM DENSE, MOIST TO 13 10.7 DENSE TO MEDIUM DENSE. 32 4.8 1 WET MOIST 5 21 11.7 1 6.2 27 1 10 CLAYSTONE, SANDY, GRAY 50 10.2 SANDSTONE, SILTY, FINE TO ____ 10 50 12.9 2 BROWN, HARD, MOIST COARSE GRAINED, GRAY BROWN, VERY DENSE, MOIST TO WET SANDSTONE, VERY CLAYEY, 15 14.8 2 15 2 50 | 12.9 FINE TO COARSE GRAINED. 8" CLAYEY LENSES BROWN, WET

18.4

WET

CLAYSTONE, SANDY, BROWN,



	TE	ST BORING LOG	
DRAWN:	DATE:	CHECKED:	7/12/19

JOB NO.: 190300
FIG NO.: A- 20

<u>50</u> 15.2

^{* -} BULK SAMPLE TAKEN

TEST BORING NO. 41 TEST BORING NO. 42 DATE DRILLED 6/7/2019 DATE DRILLED 3/12/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Soil Type Samples Samples Symbol Symbol WATER @ 17', 6/7/19 WATER @ 14', 6/7/19 14 6" TOPSOIL, SAND, SILTY, TAM 6" TOPSOIL, SAND, CLAYEY, * SANDSTONE, SILTY, FINE FINE TO COARSE GRAINED. TO COARSE GRAINED, BROWN, <u>50</u> 5.2 BROWN, MEDIUM DENSE, 10 9.2 1 7" VERY DENSE, MOIST MOIST CLAYSTONE, SANDY, BROWN, 3 <u>50</u> 10.3 5 29 7.8 HARD, MOIST 6" 10 SANDSTONE, CLAYEY TO 2 50 10.1 SANDSTONE, SILTY, FINE TO 10 <u>50</u> 10.0 2 SILTY, FINE TO COARSE 6" COARSE GRAINED, BROWN, 10" GRAINED, BROWN, VERY VERY DENSE, MOIST TO WET DENSE, MOIST TO WET 15 <u>50</u> 2 11.9 15 <u>50</u> 10.2 2 6" <u>50</u> 15.5 2 CLAYEY LENSES 20 9.3 50 2 <u>50</u> 14.0 2 6"

DRAWN:



IESI	BORING LOC	À
DATE:	CHECKED:	DATE:

JOB NO.: 190300

> FIG NO.: A- 21

TEST BORING NO. TEST BORING NO. 43 44 DATE DRILLED 5/30/2019 DATE DRILLED 5/30/2019 Job# 190300 **TECH CONTRACTORS CLIENT** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Samples Soil Type Samples Symbol Symbol WATER @ 19', 5/30/19 DRY TO 20', 5/30/19 6" TOPSOIL, SAND, SLIGHTLY 11 6" TOPSOIL, SAND, SILTY, TAN SILTY, FINE TO COARSE WEATHERED SANDSTONE, GRAINED, TAN, MEDIUM 14 3.4 1 SILTY, FINE TO COARSE :: 32 2 3.0 DENSE, MOIST GRAINED, TAN, DENSE, MOIST 32 WEATHERED SANDSTONE. 8.3 2 35 10.3 2 SILTY, FINE TO COARSE CLAYEY LENSES GRAINED, BROWN, DENSE. MOIST 10 CLAYSTONE, SANDY, GRAY <u>50</u> 14.1 3 SANDSTONE, SILTY, FINE TO 10 <u>50</u> 9.8 2 BROWN, HARD, MOIST COARSE GRAINED, BROWN, 11" VERY DENSE, MOIST 15 3 50 12.5 15 50 8.8 2 8" 8" SANDSTONE, CLAYEY, FINE 20 <u>50</u> 12.2 2 CLAYEY LENSES <u>50</u> 10.6 TO COARSE GRAINED, TAN, 5" VERY DENSE, MOIST CLAYSTONE, SANDY, BLUE GRAY, 25 50 16.8 3 HARD, MOIST 6"

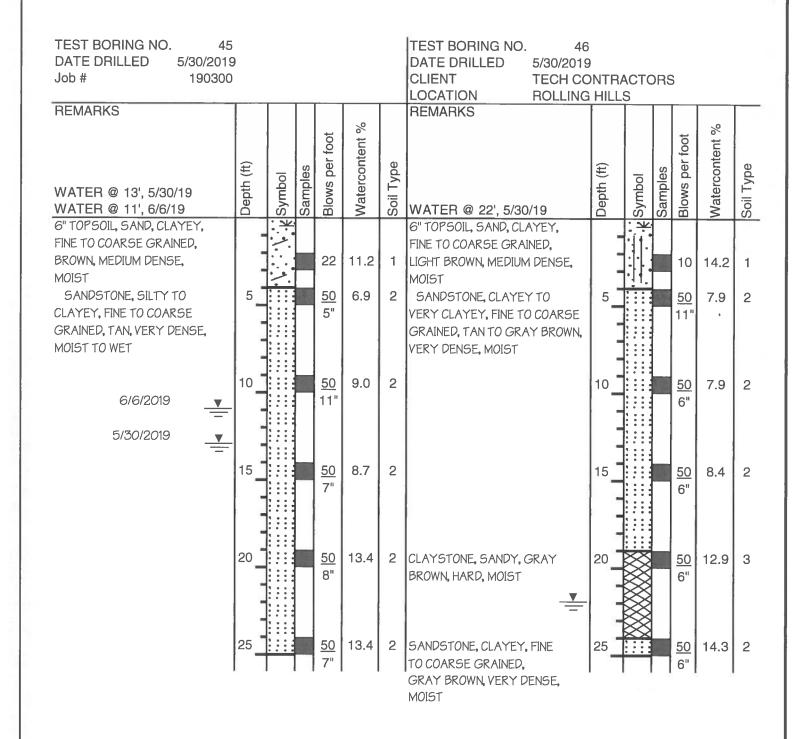
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	TEST	BORING	LOG	à	
DATE:		CHECKED:	h	2 PATE 9	

JOB NO.: 190300

FIG NO.: A- 22





	TES	ST BORING LOG
DRAWN:	DATE:	CHECKED: 1 DATE 19

JOB NO.:

FIG NO.: A- 23

TEST BORING NO. 47 TEST BORING NO. 48 DATE DRILLED 5/30/2019 DATE DRILLED 6/7/2019 Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Depth (ft) Soil Type Soil Type Samples Samples Symbol Symbol DRY TO 20', 6/7/19 DRY TO 20', 5/30/19 CAVED TO 14', 7/9/19, DRY 14 6" TOPSOIL, SAND, SILTY, TAN 6" TOPSOIL, SAND, SILTY, TAN 1.1 SANDSTONE, SILTY, FINE TO SANDSTONE, CLAYEY TO COARSE GRAINED, BROWN, <u>50</u> 9.0 SILTY, FINE TO COARSE 32 8.9 2 VERY DENSE, MOIST 9" GRAINED, BROWN, VERY DENSE, 5 50 8.7 2 MOIST 27 7.8 2 10" 10 50 2 9.4 CLAYSTONE, SANDY, BROWN, 10 <u>50</u> 9.6 3 10" HARD, MOIST 9" 15 50 8.8 2 SANDSTONE, SILTY, FINE TO 15 2 50 5.4 10" 8" COARSE GRAINED, TAN, VERY DENSE, MOIST CLAYSTONE, VERY SANDY, <u>50</u> 8.5 GRAY BROWN, HARD, MOIST <u>50</u> 9.4 3 9"



	TEST	BORING LOG	
DRAWN:	DATE:	CHECKED:	DATE: 7/12/19

JOB NO.: 190300 FIG NO.:

A- 24

TEST BORING NO. 49 TEST BORING NO. DATE DRILLED 6/7/2019 DATE DRILLED Job# 190300 CLIENT **TECH CONTRACTORS** LOCATION **ROLLING HILLS** REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Soil Type Depth (ft) Samples Samples Symbol Symbol WATER @ 12', 6/7/19 ंक 6" TOPSOIL, SAND, SLIGHTLY SILTY TO SILTY, FINE TO COARSE GRAINED, TAN, 15 5.2 1 MEDIUM DENSE TO DENSE, 5 MOIST 20 10.3 1 10 33 10.1 1 15 SANDSTONE, SILTY, FINE TO 11.9 2 <u>50</u> COARSE GRAINED, TAN, VERY DENSE, MOIST TO WET 20 2 <u>50</u> 15.5 6" <u>50</u> 15.5 5"

DRAWN:

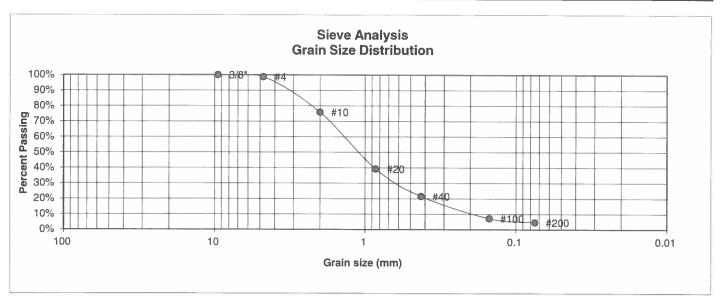


TES	FBORING LO	G
DATE:	CHECKED:	7/12/19

JOB NO.: 190300

FIG NO.: A- 25 **APPENDIX B: Laboratory Test Results**

UNIFIED CLASSIFICATION	SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	1	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



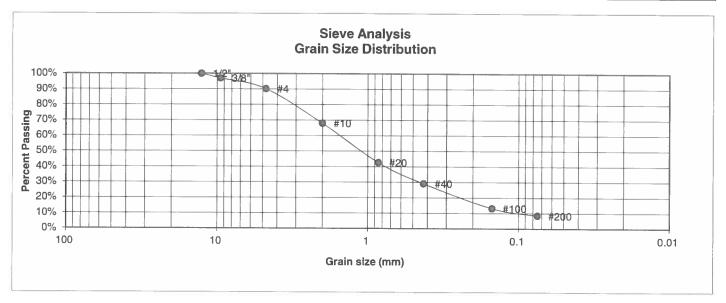
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	98.7%	<u>Swell</u>
10	75.9%	Moisture at start
20	39.2%	Moisture at finish
40	21.4%	Moisture increase
100	7.2%	Initial dry density (pcf)
200	4.7%	Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE	CHECKED:	DATE: //

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	2	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



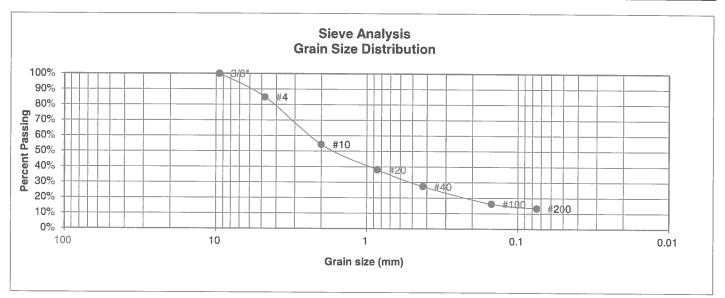
U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8" 4 10 20 40 100	Percent Finer 100.0% 97.0% 90.2% 67.9% 42.7% 29.0% 13.2%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf)
100	13.2%	Initial dry density (pcf)
200	8.4%	Swell (psf)



LABORATORY TEST RESULTS			
	DATE:	CHECKED:	DATE:) 7 / 1 / 19

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	5	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



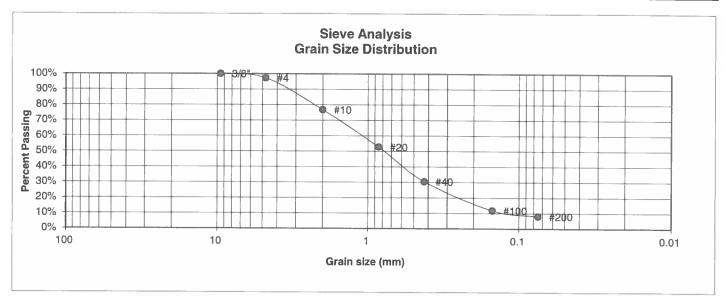
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit 16 Liquid Limit 26 Plastic Index 10
4	84.9% 54.4%	Swell Moisture et etert
20 40	38.1% 27.3%	Moisture at start Moisture at finish Moisture increase
100 200	16.2% 13.3%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE:	CHECKED:	DATE:

JOB NO: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	6	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



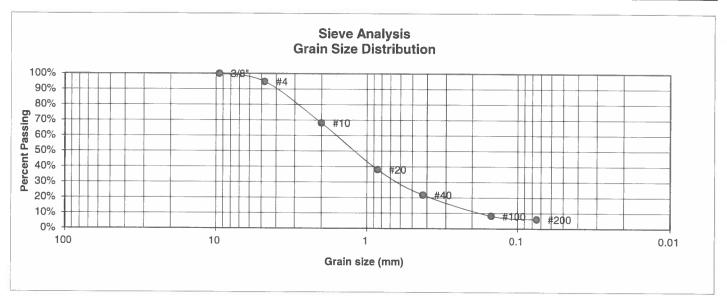
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4 10 20 40 100 200	97.3% 76.8% 52.8% 30.4% 11.8% 8.1%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY TEST
DATE:	CHECKED:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	8	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



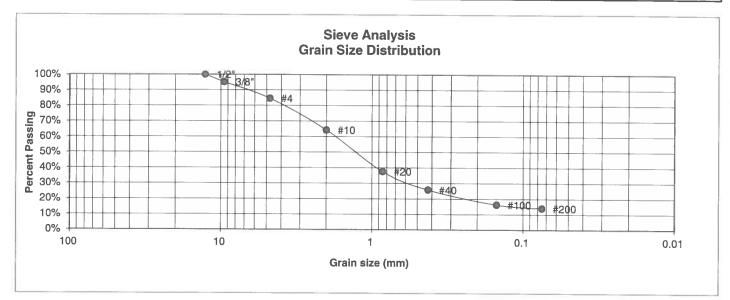
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	94.8%	Swell
10	68.1%	Moisture at start
20 40	38.0% 21.8%	Moisture at finish Moisture increase
100 200	8.2% 6.1%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS			
DATE:	CHECKED:	h	DATE: 1/19

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1 =	PROJECT	ROLLING HILLS
TEST BORING #	10	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer 100.0% 95.1%	Atterberg <u>Limits</u> Plastic Limit 13 Liquid Limit 29 Plastic Index 16
4	84.6% 64.3%	<u>Swell</u> Moisture at start
20	37.5%	Moisture at finish
40	25.8%	Moisture increase
100	16.3%	Initial dry density (pcf)
200	14.0%	Swell (psf)

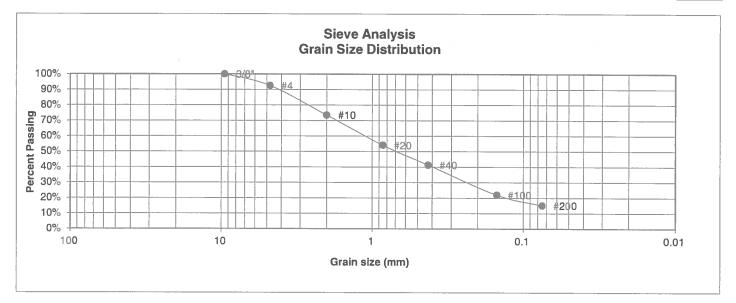


LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: 1 DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	11	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



Percent	Atterberg
<u>Finer</u>	<u>Limits</u>
	Plastic Limit
	Liquid Limit
	Plastic Index
100.0%	
92.6%	<u>Swell</u>
73.5%	Moisture at start 12.1%
54.1%	Moisture at finish 19.1%
41.3%	Moisture increase 6.9%
22.0%	Initial dry density (pcf) 110
15.2%	Swell (psf) 370
	Finer 100.0% 92.6% 73.5% 54.1% 41.3% 22.0%



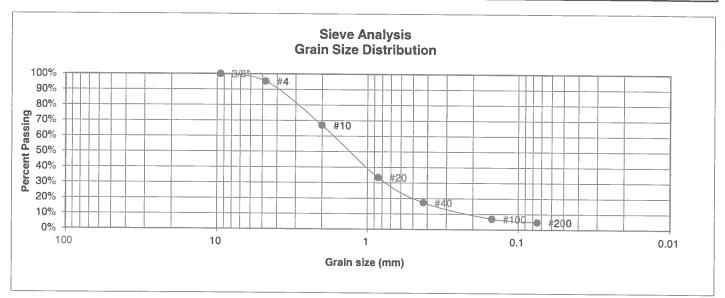
LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: L. DATE: 7/1/19

JOB NO.: 190300

FIG NO

UNIFIED CLASSIFICATION	SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	13	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	95.2%	<u>Swell</u>
10	67.0%	Moisture at start
20	33.4%	Moisture at finish
40	17.3%	Moisture increase
100	7.0%	Initial dry density (pcf)
200	4.8%	Swell (psf)

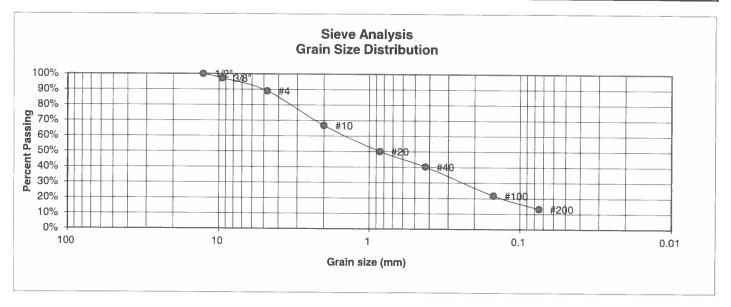


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	14	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 97.2%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	89.0%	<u>Swell</u>
10	66.8%	Moisture at start
20	50.1%	Moisture at finish
40	40.2%	Moisture increase
100	21.8%	Initial dry density (pcf)
200	13.2%	Swell (psf)

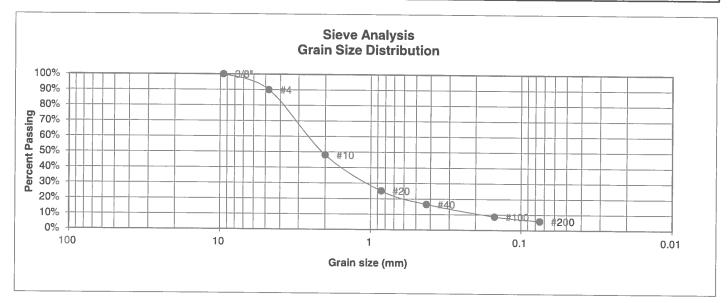


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE: 1/0

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	16	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



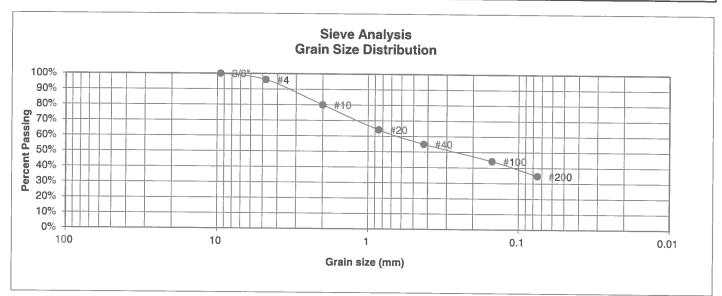
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	89.9%	Swell
10	48.1%	Moisture at start 13.5%
20	25.1%	Moisture at finish 21.9%
40	16.5%	Moisture increase 8.4%
100	8.7%	Initial dry density (pcf) 100
200	5.9%	Swell (psf) 70



LABORATORY TEST RESULTS		
DATE:	CHECKED:	7/1/19

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UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	19	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	96.1%	<u>Swell</u>
10	80.0%	Moisture at start
20	64.1%	Moisture at finish
40	55.0%	Moisture increase
100	44.2%	Initial dry density (pcf)
200	34.7%	Swell (psf)

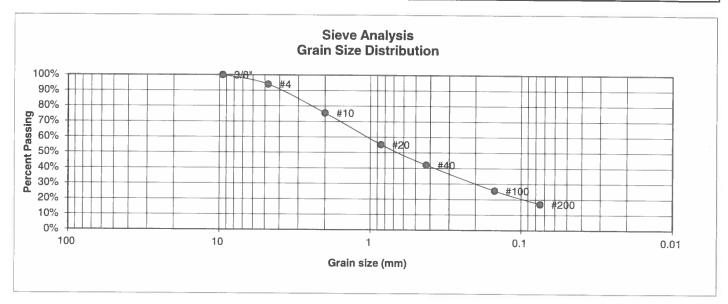


LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	23	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	94.0%	<u>Swell</u>
10	75.5%	Moisture at start
20	55.2%	Moisture at finish
40	42.1%	Moisture increase
100	25.6%	Initial dry density (pcf)
200	17.0%	Swell (psf)



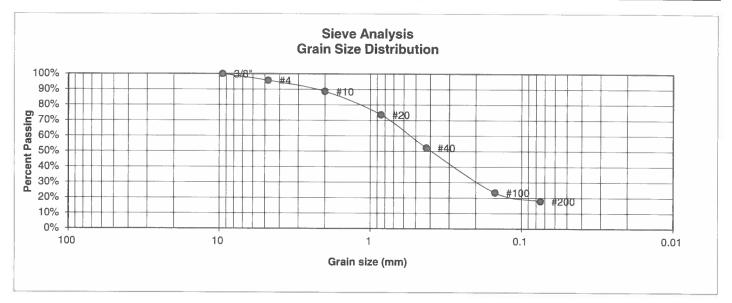
	LABORAT	ORY TEST		
	RESULTS			
ĺ	DATE:	CHECKED:	DATE/	_

JOB NO.: 190300

FIG NO.:

DATE! //a

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	24	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	95.8% 88.7%	<u>Swell</u> Moisture at start
20	73.6%	Moisture at finish
40	52.3%	Moisture increase
100	23.5%	Initial dry density (pcf)
200	18.0%	Swell (psf)

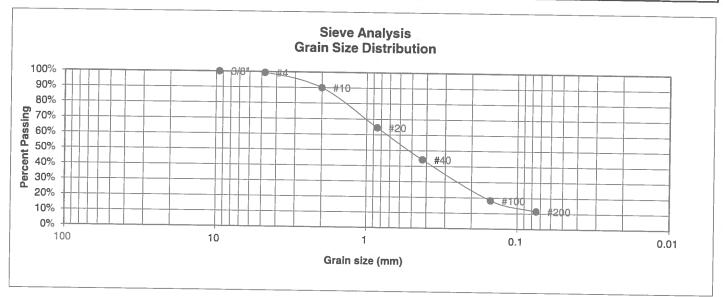


LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE: 7/1/19

JOB NO.:
190300

UNIFIED CLASSIFICATION SM-SW CLIENT TECH CONTRACTORS SOIL TYPE # 1 PROJECT ROLLING HILLS TEST BORING # 26 JOB NO. 190300 DEPTH (FT) 5 TEST BY BL	
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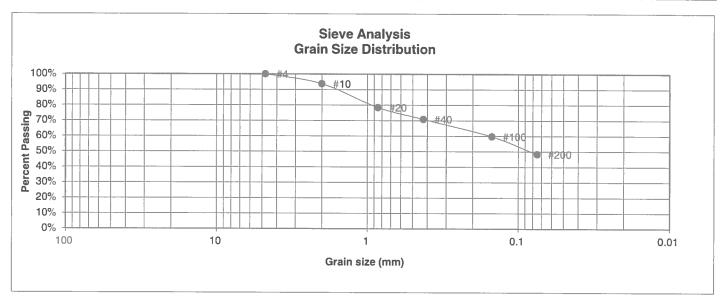
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4 10 20 40 100 200	99.3% 90.0% 64.6% 44.2% 18.3% 11.5%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORAT RESULTS	ORY TEST	
DATE:	CHECKED:	DATE

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	27	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



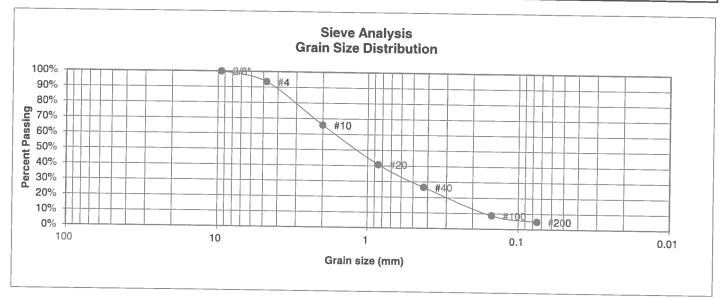
U.S.	Percent	Atterberg	
Sieve #	<u>Finer</u>	<u>Limits</u>	
3"		Plastic Limit	
1 1/2"		Liquid Limit	
3/4"		Plastic Index	
1/2"			
3/8"			
4	100.0%	<u>Swell</u>	
10	93.7%	Moisture at start 14.09	6
20	78.5%	Moisture at finish 20.99	6
40	70.9%	Moisture increase 6.99	6
100	59.7%	Initial dry density (pcf) 10	3
200	48.3%	Swell (psf) 46	0



RESULTS	ORY TEST	
DATE:	CHECKED:	DATE:

JOB NO.: 190300

TEST BORING # 28 JOB NO. 190300 DEPTH (FT) 2-3 TEST BY BL	UNIFIED CLASSIFICATION SOIL TYPE # TEST BORING # DEPTH (FT)	1 28		
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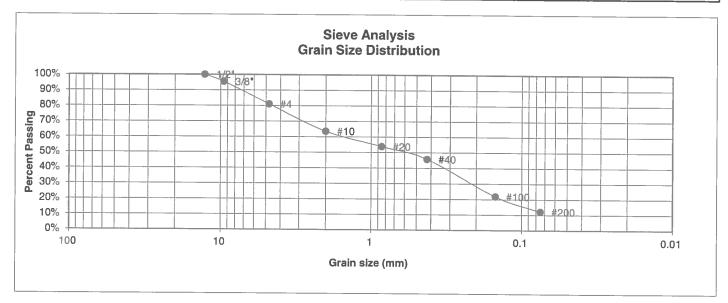
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	93.4% 65.9%	<u>Swell</u> Moisture at start
20 40 100 200	40.8% 26.4% 8.7% 4.9%	Moisture at finish Moisture increase Initial dry density (pcf)
		Swell (psf)



	LABORATORY TEST RESULTS		
DRAWN:	DATE:	CHECKED:	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	30	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



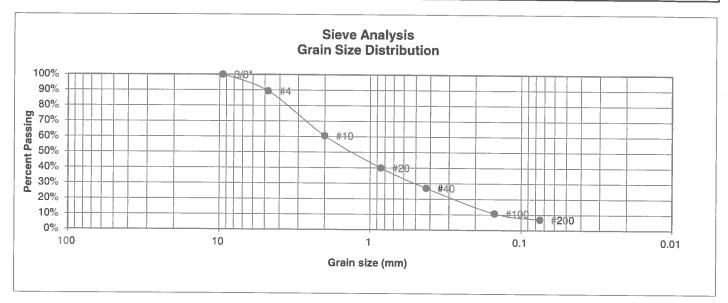
U.S.	Percent	Atterberg
Sieve #	<u>Finer</u>	<u>Limits</u>
3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"	100.0%	
3/8"	95.5%	
4	81.0%	<u>Şwell</u>
10	63.6%	Moisture at start 13.1%
20	53.9%	Moisture at finish 19.6%
40	45.8%	Moisture increase 6.5%
100	21.9%	Initial dry density (pcf) 97
200	12.1%	Swell (psf) 2970



LABORATORY TEST RESULTS			
DRAWN:	DATE:	CHECKED:	DATE 119

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	30	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/0 4	100.0% 89.3%	Swell
10	60.6%	Moisture at start
20 40	40.0% 26.9%	Moisture at finish Moisture increase
100 200	10.8% 6.9%	Initial dry density (pcf) Swell (psf)

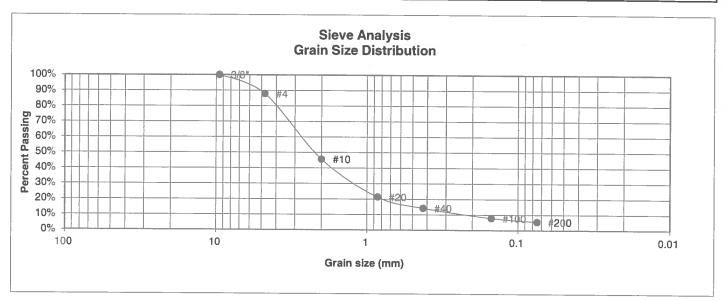


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	31	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100	87.9% 45.6% 21.3% 14.2% 7.8%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf)
200	5.4%	Swell (psf)

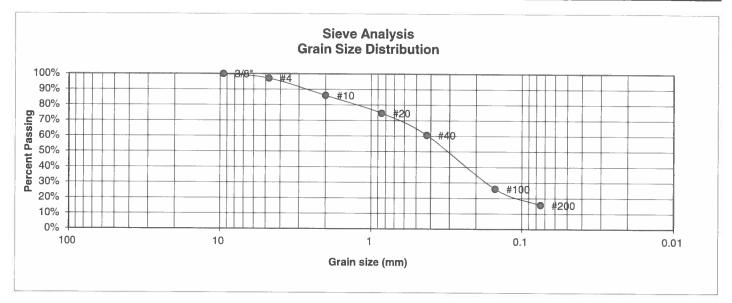


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE: 1/4

JOB NO.:: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	32	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	97.1%	Swell
10	86.1%	Moisture at start
20	74.7%	Moisture at finish
40	60.6%	Moisture increase
100	26.1%	Initial dry density (pcf)
200	15.6%	Swell (psf)

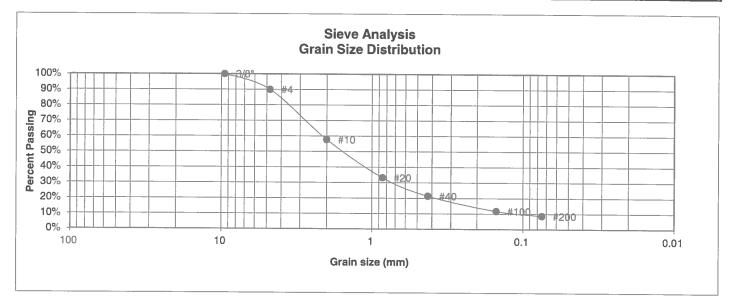


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: L DATE: 7/1/19

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	38	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



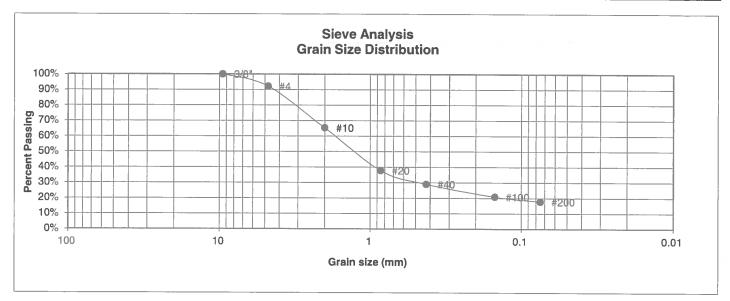
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	90.0%	<u>Şwell</u>
10	57.7%	Moisture at start
20	33.2%	Moisture at finish
40	21.4%	Moisture increase
100 200	11.7% 8.6%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS					
DATE:	CHECKED:	DATE:			

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	39	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



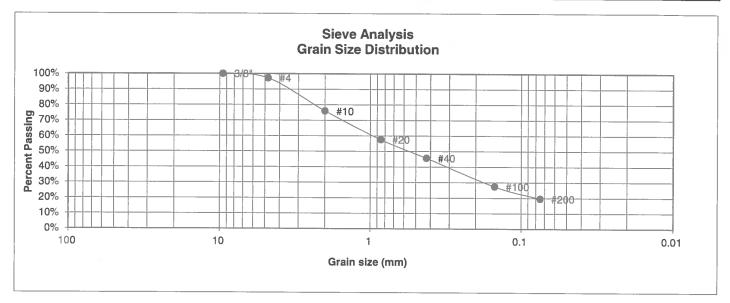
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	92.2%	<u>Swell</u>
10	65.3%	Moisture at start
20	37.7%	Moisture at finish
40	29.0%	Moisture increase
100	20.8%	Initial dry density (pcf)
200	17.8%	Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE:	OUTOKED!	DATE

JOB NO.::190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	42	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2" 3/8" 4 10	100.0% 97.2% 76.1%	<u>Swell</u> Moisture at start
20 40 100 200	57.5% 45.6% 27.4% 19.6%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



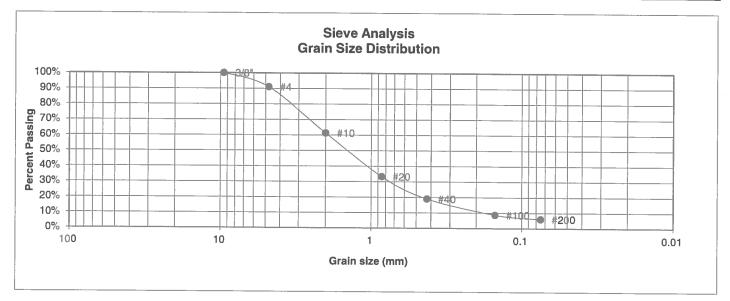
LABORATORY	TEST
RESULTS	

DATE: CHECKED: DATE:

JOB NO.: 190300

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UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	43	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



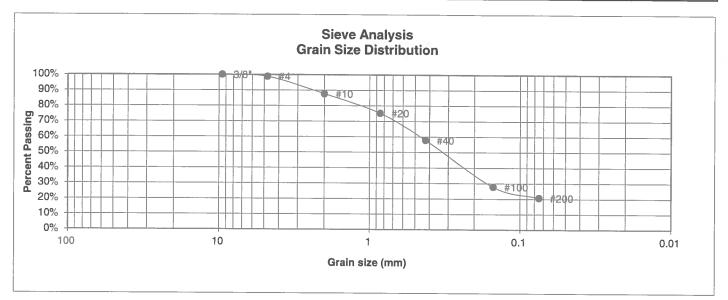
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	91.1%	<u>Swell</u>
10	61.3%	Moisture at start
20	33.3%	Moisture at finish
40	19.0%	Moisture increase
100	8.7%	Initial dry density (pcf)
200	6.0%	Swell (psf)



LABORAT RESULTS	ORY TEST	
DATE:	CHECKED:	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	47	JOB NO.	190300
DEPTH (FT)	2-3	TEST BY	BL



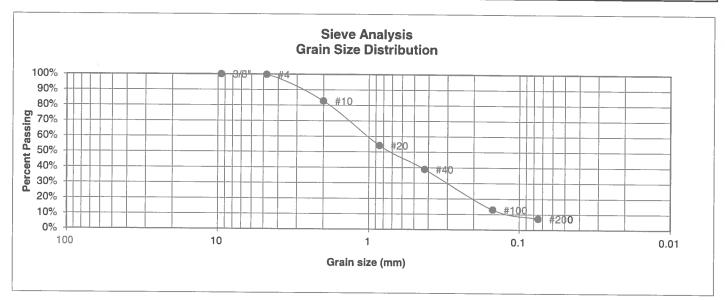
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index	
3/8"	100.0%		
4	98.8%	Swell	
10	87.7%	Moisture at start	13.9%
20	75.2%	Moisture at finish	18.6%
40	57.8%	Moisture increase	4.8%
100	27.8%	Initial dry density (pcf)	103
200	20.7%	Swell (psf)	220



LABORATO RESULTS	ORY TEST	
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	1	PROJECT	ROLLING HILLS
TEST BORING #	49	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



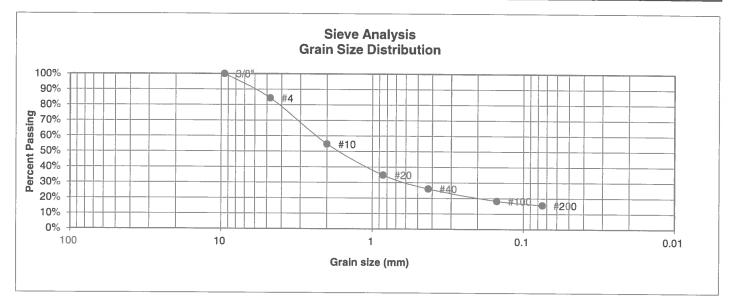
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.8%	Swell
10	82.8%	Moisture at start
20 40	54.2% 38.9%	Moisture at finish Moisture increase
100 200	13.0% 7.3%	Initial dry density (pcf) Swell (psf)



RESULTS	ORY TEST	
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	1	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



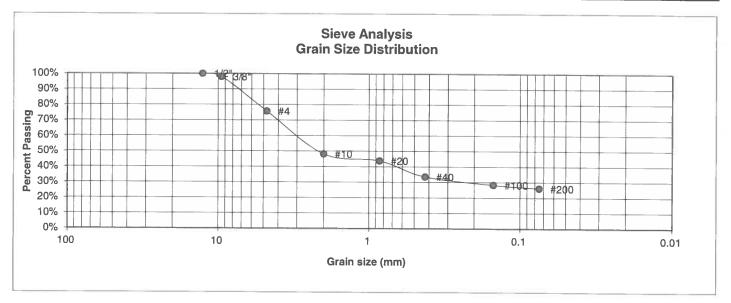
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	84.4%	<u>Swell</u>
10	54.8%	Moisture at start
20	34.9%	Moisture at finish
40	26.0%	Moisture increase
100	18.2%	Initial dry density (pcf)
200	15.5%	Swell (psf)



RESULTS	ORY TEST	
DATE:	CHECKED:	DATE:

JOB NO.:190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	3	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 98.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	75.7%	<u>Swell</u>
10	48.2%	Moisture at start
20 40	43.8% 33.5%	Moisture at start Moisture at finish Moisture increase
100	28.3%	Initial dry density (pcf)
200	26.1%	Swell (psf)

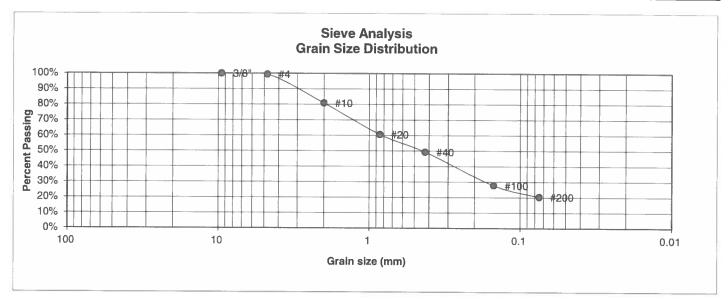


LABORATORY TEST	
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	4	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



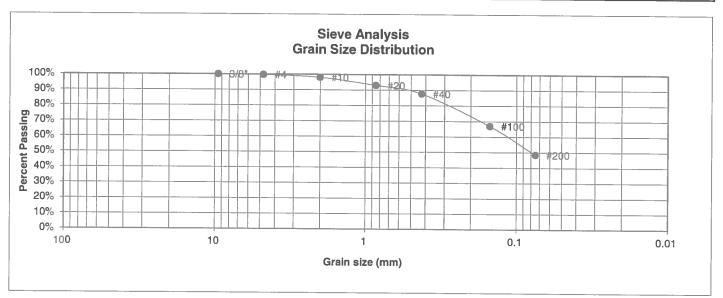
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 29 Plastic Index 12
3/8"	100.0%	
4	99.4%	Swell
10	80.9%	Moisture at start
20	60.6%	Moisture at finish
40	49.3%	Moisture increase
100 200	27.7% 20.3%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS	ORY TEST	
DATE:	CHECKED:	2/1/19

JOB NO.::

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	5	JOB NO.	190300
DEPTH (FT)	25	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 31 Plastic Index 14
3/6 4	100.0% 99.7%	Swell
10	98.0%	<u>Swell</u> Moisture at start
20 40	93.0% 87.6%	Moisture at finish Moisture increase
100 200	67.0% 48.5%	Initial dry density (pcf) Swell (psf)

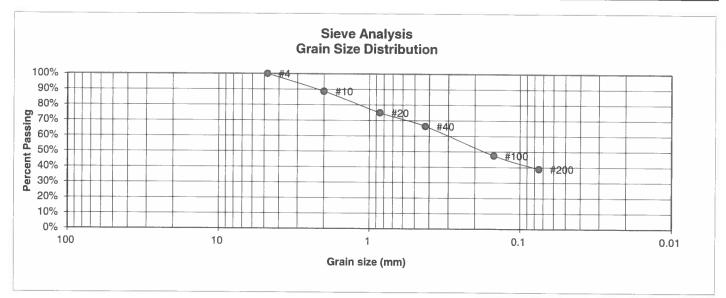


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DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	6	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 13 Liquid Limit 26 Plastic Index 13
4	100.0%	<u>Swell</u>
10	88.7%	Moisture at start
20	75.0%	Moisture at finish
40	66.3%	Moisture increase
100 200	47.5% 38.9%	Initial dry density (pcf) Swell (psf)
		ν (μ.,)

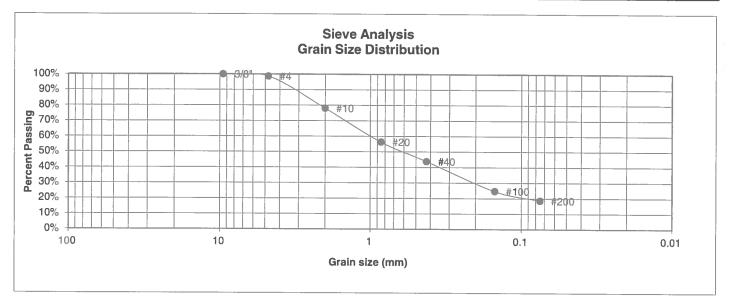


LABORATORY	TEST
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	7	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 18 Liquid Limit 32 Plastic Index 14
3/8"	100.0%	
4	98.7%	Swell
10	78.1%	Moisture at start
20	56.3%	Moisture at finish
40	43.8%	Moisture increase
100 200	24.6% 18.6%	Initial dry density (pcf) Swell (psf)

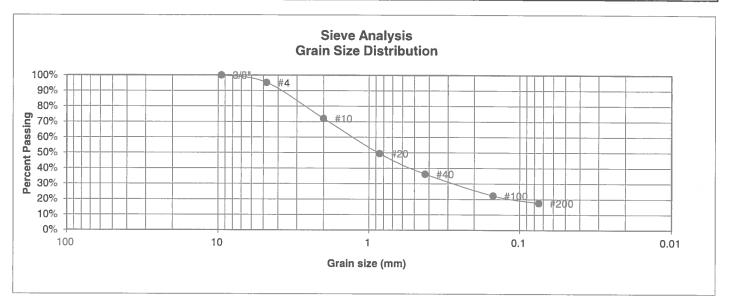


LABORATORY	TEST
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	N SM	CLIENT TECH CONTRACTORS
SOIL TYPE #	2	PROJECT ROLLING HILLS
TEST BORING #	9	JOB NO. 190300
DEPTH (FT)	15	TEST BY BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	95.3% 72.0%	<u>Swell</u> Moisture at start
20 40	49.5% 36.2%	Moisture at start Moisture at finish Moisture increase
100 200	22.3% 17.5%	Initial dry density (pcf) Swell (psf)

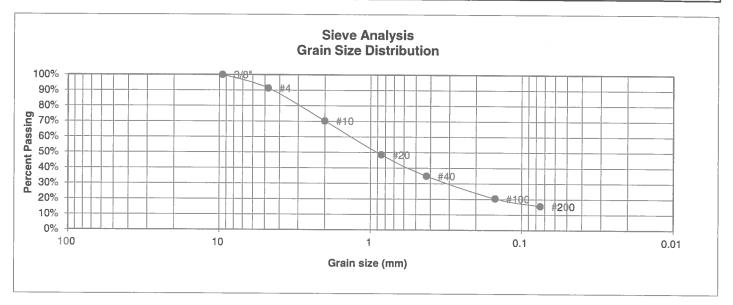


LABORATORY TEST RESULTS				
DRAWN:	DATE:	CHECKED:	7/1/19	

JOB NO.: 190300

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UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	12	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



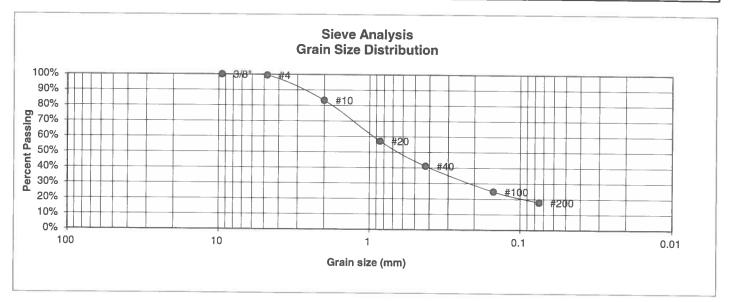
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	0 "
4	91.3%	Swell
10	70.3%	Moisture at start
20	48.5%	Moisture at finish
40	34.9%	Moisture increase
100 200	20.4% 15.5%	Initial dry density (pcf) Swell (psf)



	LABOR RESUL	ATORY TEST	
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JOB NO.:: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	14	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20	99.5% 83.3% 57.2%	<u>Swell</u> Moisture at start Moisture at finish
40 100 200	41.1% 24.8% 17.8%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORATORY	TEST
RESULTS	

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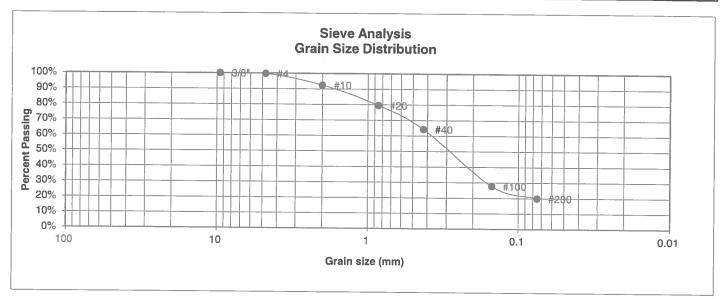
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JOB NO.: 190300

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UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	15	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



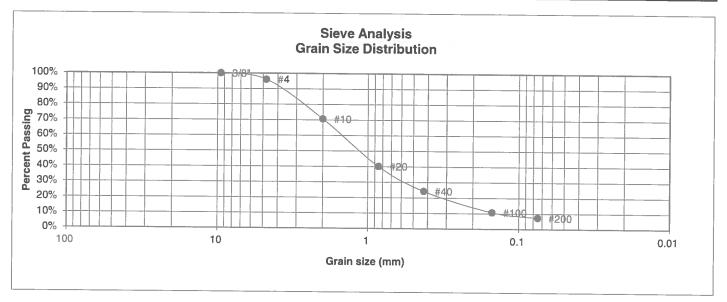
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	99.7%	<u>Swell</u>
10	92.5%	Moisture at start
20	79.5%	Moisture at finish
40	64.2%	Moisture increase
100	27.7%	Initial dry density (pcf)
200	19.9%	Swell (psf)



	LABORAT RESULTS	ORY TE	EST	
1	DATE:	CHECKED:	Λ	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	17	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



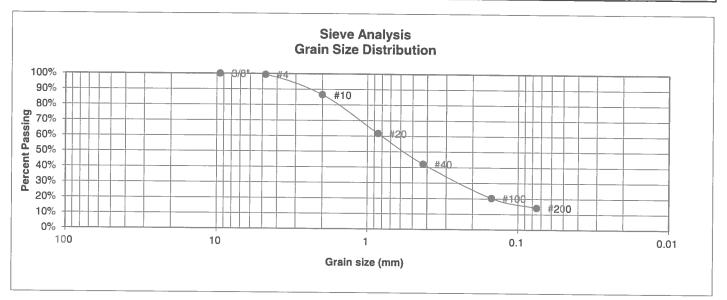
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	96.1%	<u>Swell</u>
10	70.6%	Moisture at start
20	40.1%	Moisture at finish
40	24.3%	Moisture increase
100	10.8%	Initial dry density (pcf)
200	7.3%	Swell (psf)



LABORATORY TEST RESULTS				
DRAWN:	DATE:	CHECKED:	DATE:	

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	18	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



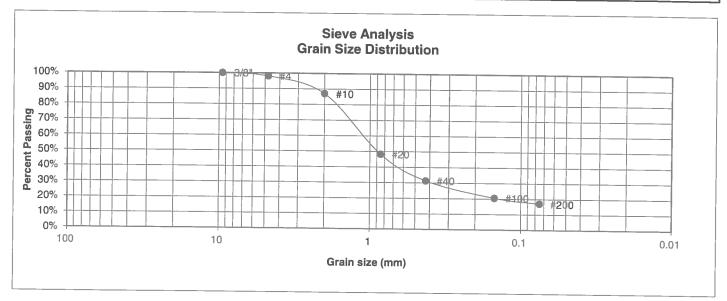
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100 200	99.4% 86.5% 61.7% 42.1% 20.3% 14.2%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORAT RESULTS	ORY TEST	
DATE:	CHECKED:	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	20	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100 200	98.1% 87.0% 48.2% 31.3% 20.5% 17.1%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

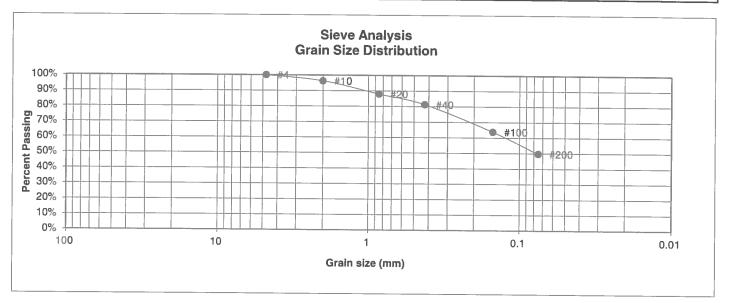


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DATE:	CHECKED:	10	DATE:	1

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> JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	20	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



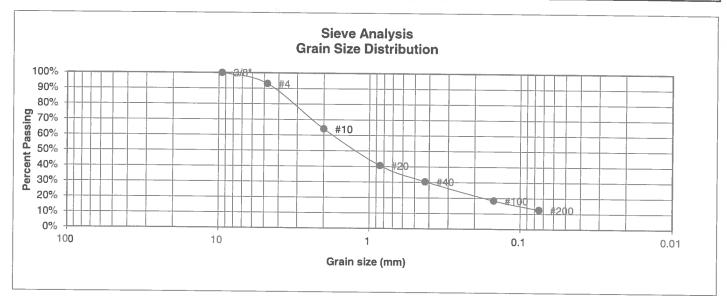
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 14 Liquid Limit 28 Plastic Index 14
4	100.0%	<u>Swell</u>
10	96.3%	Moisture at start
20	88.0%	Moisture at finish
40	81.3%	Moisture increase
100	63.8%	Initial dry density (pcf)
200	49.7%	Swell (psf)



LABORAT RESULTS	ORY TEST	
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UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	21	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	93.0%	Swell
10	64.1%	Moisture at start
20	40.6%	Moisture at finish
40	30.4%	Moisture increase
100	18.4%	Initial dry density (pcf)
200	12.5%	Swell (psf)

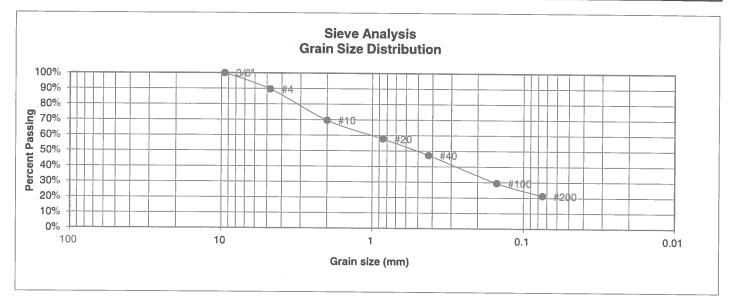


LABORATORY TEST	
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	21	JOB NO.	190300
DEPTH (FT)	25	TEST BY	BL



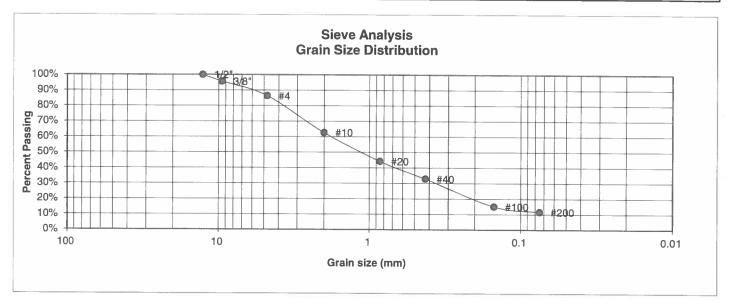
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20	89.6% 69.6% 57.7%	<u>Swell</u> Moisture at start Moisture at finish
40 100 200	47.2% 29.5% 21.2%	Moisture at initial Moisture increase Initial dry density (pcf) Swell (psf)



LABORAT	ORY T	EST	
RESULTS			
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	23	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



4 86.4% Swell 10 62.6% Moisture at start 20 44.2% Moisture at finish 40 32.8% Moisture increase 100 15.0% Initial dry density (pc 200 11.6% Swell (psf)	U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer 100.0% 95.7%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
20 44.2% Moisture at finish 40 32.8% Moisture increase 100 15.0% Initial dry density (pc	4		
initial ary density (pe	— -		Moisture at finish
			Initial dry density (pcf) Swell (psf)

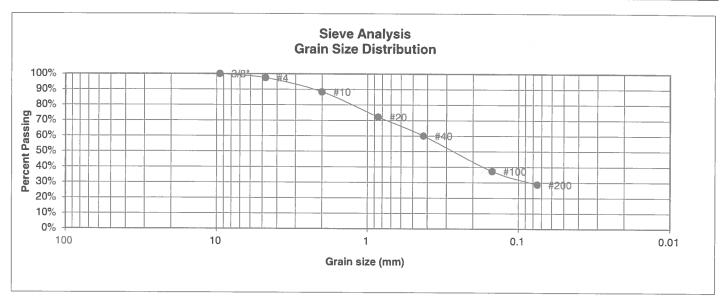


LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	25	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



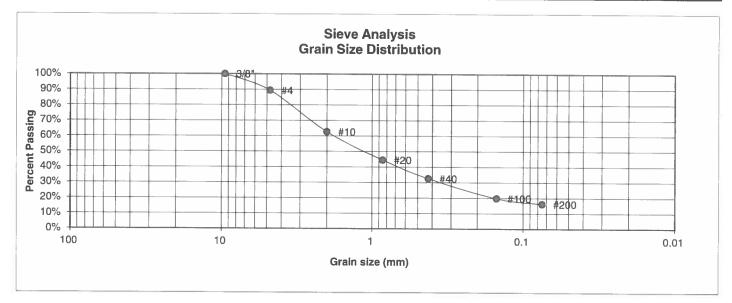
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.4% 88.4%	<u>Swell</u> Moisture at start
20 40	72.2% 60.1%	Moisture at start Moisture at finish Moisture increase
100 200	37.4% 28.7%	Initial dry density (pcf) Swell (psf)



LABORATO RESULTS		
DATE:	CHECKED:	DATE 10

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	27	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



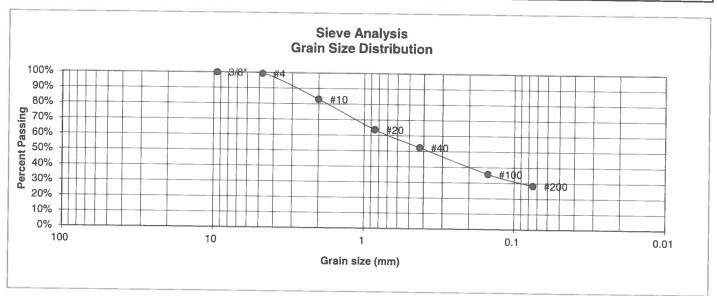
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	89.4%	<u>Swell</u>
10	62.7%	Moisture at start
20	44.5%	Moisture at finish
40	32.5%	Moisture increase
100	19.8%	Initial dry density (pcf)
200	16.2%	Swell (psf)



LABORATORY TEST RESULTS				
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JOB NO.: 190300

UNIFIED CLASSIFICATION SC	<u>CLIENT</u> TECH CONTRACTORS
SOIL TYPE # 2	PROJECT ROLLING HILLS
TEST BORING # 28	JOB NO. 190300
<u>DEPTH (FT)</u> 15	TEST BY BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.4% 83.0%	<u>Swell</u> Moisture at start
20 40 100 200	63.6% 52.4% 35.7% 28.3%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

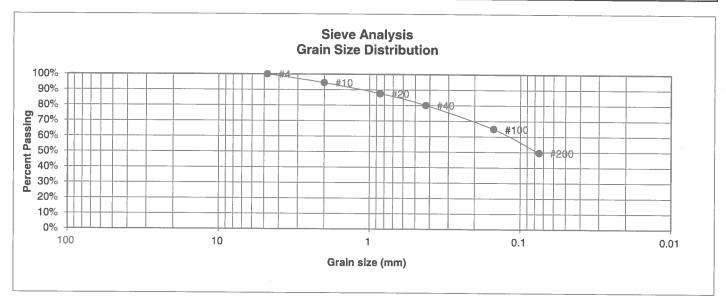


LABORATO RESULTS	ORY TEST	
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> JOB NO.: 190300

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	29	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	94.5%	Moisture at start
20	87.6%	Moisture at finish
40	80.1%	Moisture increase
100 200	64.9% 49.6%	Initial dry density (pcf) Swell (psf)

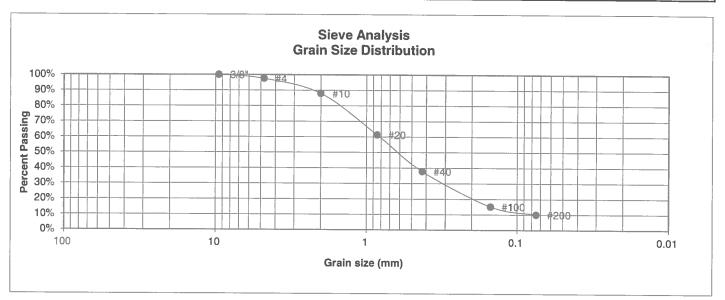


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM-SW	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	35	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2" 3/8" 4 10	100.0% 97.5% 87.9%	<u>Swell</u> Moisture at start
20 40 100 200	61.3% 37.8% 15.2% 10.1%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

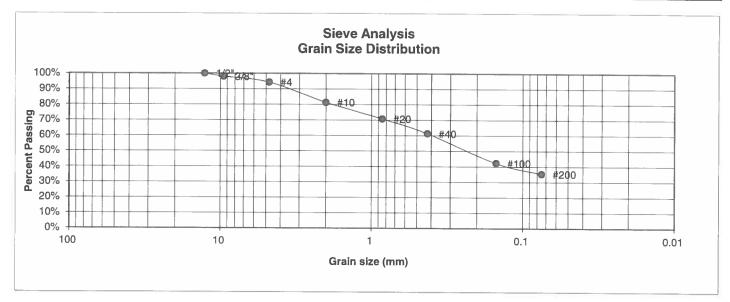


LABORATORY	TEST
RESULTS	

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JOB NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	37	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 98.1%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	94.3%	<u>Swell</u>
10	81.4%	Moisture at start
20	70.8%	Moisture at finish
40	61.3%	Moisture increase
100	42.3%	Initial dry density (pcf)
200	35.4%	Swell (psf)

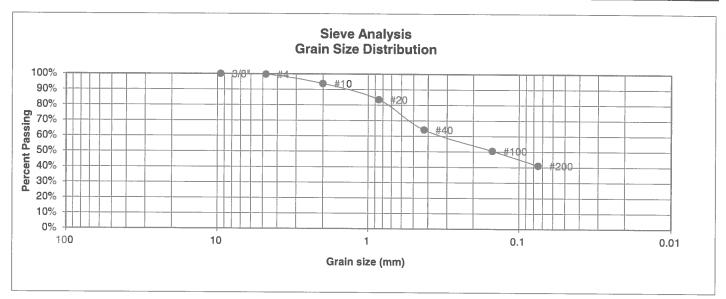


LABORATORY	TEST
RESULTS	

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UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	39	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



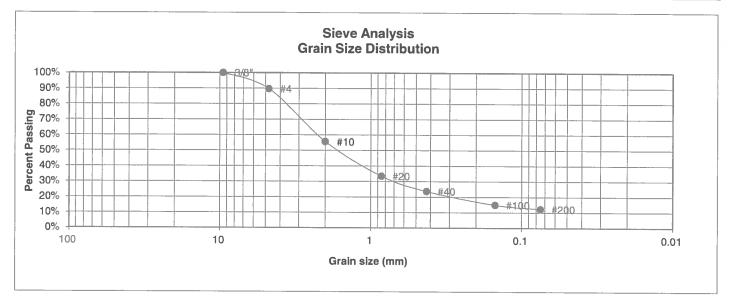
3/8" 100.0% 4 99.7% Swell 10 93.8% Moisture at star 20 83.5% Moisture at finis	
40 64.1% Moisture increa 100 50.5% Initial dry densi	sh se
200 41.1% Swell (psf)	y (pci)



LABORATORY TEST RESULTS				
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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	40	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	89.7%	Swell
10	55.7%	Moisture at start
20	33.4%	Moisture at finish
40	23.7%	Moisture increase
100	14.9%	Initial dry density (pcf)
200	12.3%	Swell (psf)

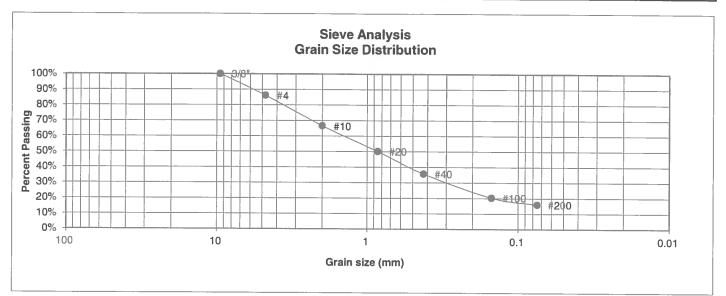


LABORATORY	TEST
RESULTS	

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JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	41	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	86.2%	<u>Swell</u>
10	66.5%	Moisture at start
20	50.2%	Moisture at finish
40	35.7%	Moisture increase
100	20.3%	Initial dry density (pcf)
200	16.0%	Swell (psf)

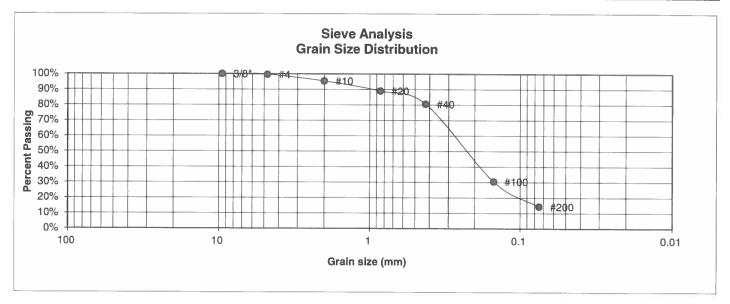


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	44	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



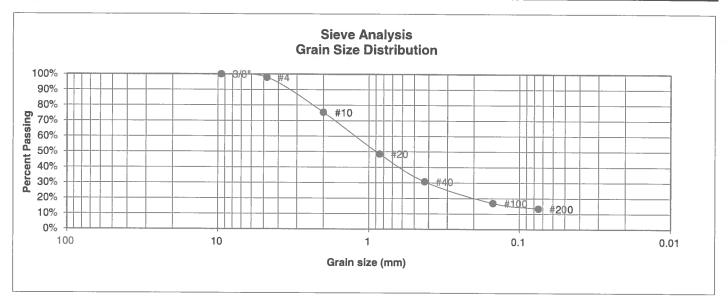
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4 10 20 40 100 200	99.6% 95.4% 89.0% 80.6% 30.5% 14.3%	Swell Moisture at start Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



RESULTS				
	DATE:	CHECKED:	1	DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	SM	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	45	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	97.9%	<u>Swell</u>
10	75.4%	Moisture at start
20 40	48.6% 30.7%	Moisture at finish Moisture increase
100	16.9%	Initial dry density (pcf)
200	13.4%	Swell (psf)

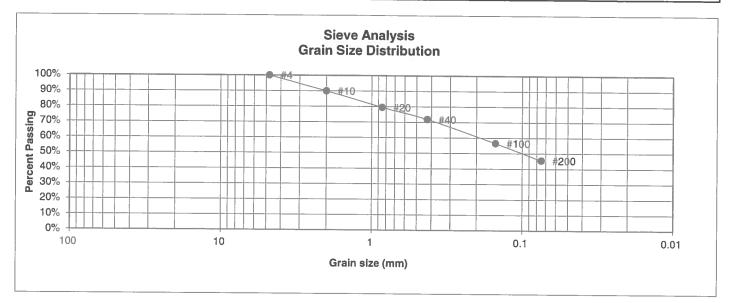


LABORATORY TEST RESULTS			
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JOB NO.: 190300

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UNIFIED CLASSIFICATION	SC	CLIENT	TECH CONTRACTORS
SOIL TYPE #	2	PROJECT	ROLLING HILLS
TEST BORING #	46	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



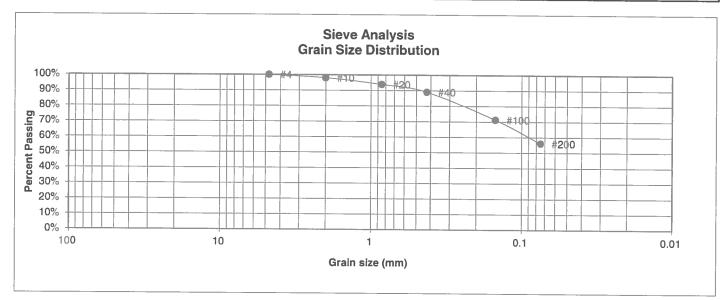
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	<u>Swell</u>
10	89.9%	Moisture at start
20	79.5%	Moisture at finish
40	71.8%	Moisture increase
100	56.5%	Initial dry density (pcf)
200	45.5%	Swell (psf)



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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	15	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	Swell
10	98.1%	Moisture at start
20	93.9%	Moisture at finish
40	89.0%	Moisture increase
100 200	71.3% 56.1%	Initial dry density (pcf) Swell (psf)

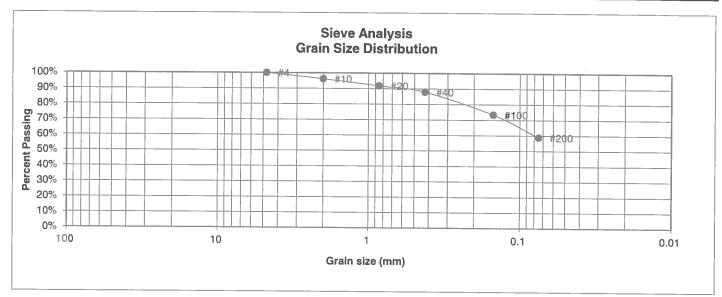


LABORATORY TEST RESULTS			
	DATE:	CHECKED:	DATE

JOB NO.: 190300

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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	16	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	100.0%	Swell
10	96.2%	Moisture at start
20	91.8%	Moisture at finish
40	87.9%	Moisture increase
100 200	73.5% 58.8%	Initial dry density (pcf) Swell (psf)



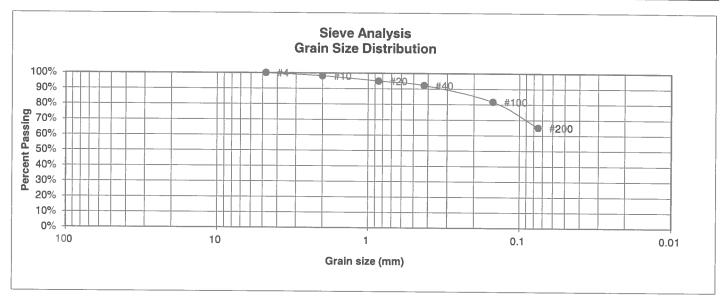
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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	19	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit
3/4 1/2" 3/8" 4	100.0%	Plastic Index <u>Swell</u>
10 20 40	98.2% 95.0% 92.2%	Moisture at start Moisture at finish Moisture increase
100 200	81.7% 65.1%	Initial dry density (pcf) Swell (psf)

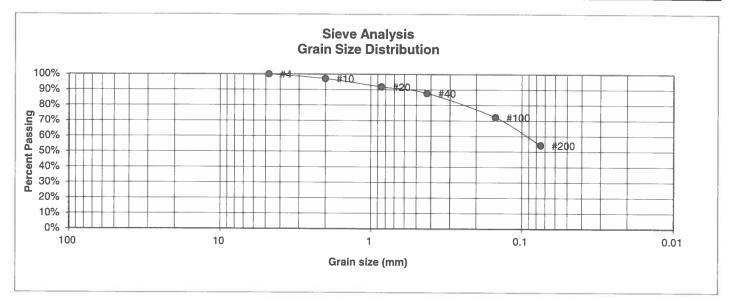


LABORATORY TEST	
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	22	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. Percent Atterberg Sieve # Finer Limits 3" Plastic Limit 1 1/2" Liquid Limit 3/4" Plastic Index 1/2" 3/8"	19 34 15
4 100.0% <u>Swell</u>	
10 97.1% Moisture at star	t
20 91.9% Moisture at finis	sh
40 87.7% Moisture increa	se
100 72.3% Initial dry densit 200 54.2% Swell (psf)	ty (pcf)

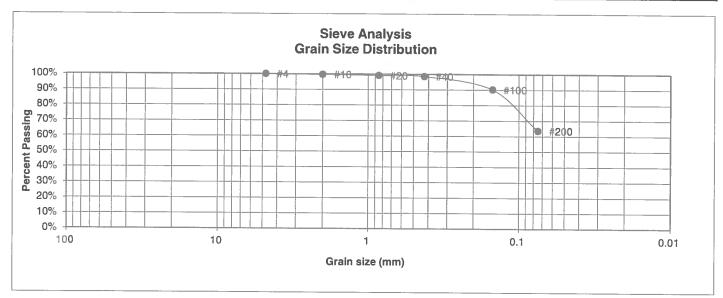


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: DATE:

JOB NO.:: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	24	JOB NO.	190300
DEPTH (FT)	5	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index	
4	100.0%	<u>Swell</u>	
10	99.7%	Moisture at start 14.5%	
20	99.1%	Moisture at finish 24.3%	
40	98.5%	Moisture increase 9.8%	
100	90.2%	Initial dry density (pcf) 90	
200	63.6%	Swell (psf) 90	

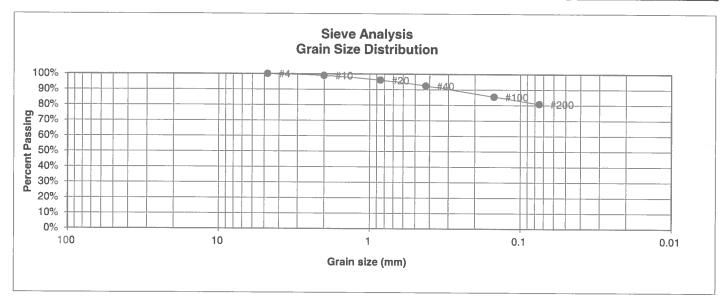


LABORATORY	TEST
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DRAWN: DATE: CHECKED: DATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	33	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 22 Liquid Limit 42 Plastic Index 20
4	100.0%	<u>Swell</u>
10	99.0%	Moisture at start
20	96.0%	Moisture at finish
40	92.5%	Moisture increase
100 200	85.5% 80.8%	Initial dry density (pcf) Swell (psf)

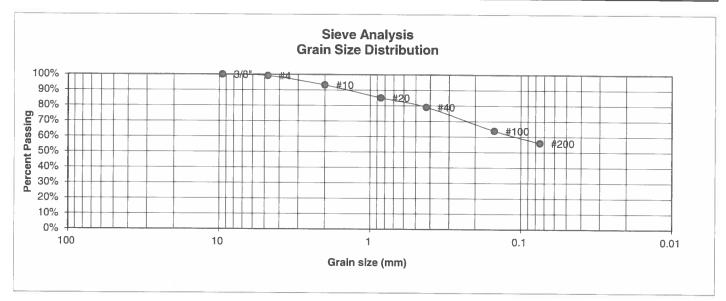


LABORATORY	TEST
RESULTS	

DRAWN: DATE: CHECKED: PATE:

JOB NO.: 190300

UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	34	JOB NO.	190300
DEPTH (FT)	10	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.2% 93.2%	<u>Swell</u> Moisture at start
20 40 100 200	85.1% 79.1% 63.9% 56.0%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

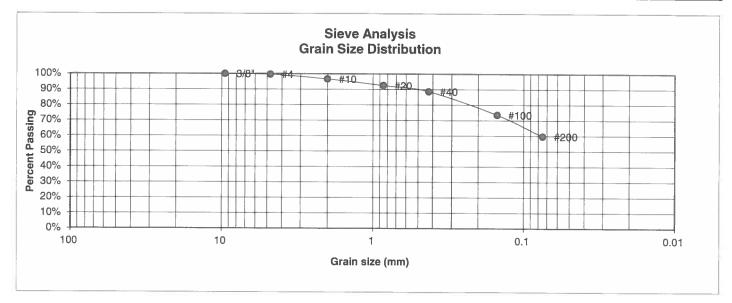


LABORATORY	TEST
RESULTS	

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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	36	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	99.6% 96.7%	<u>Swell</u> Moisture at start
20	92.5%	Moisture at finish
40	88.6%	Moisture increase
100	73.6%	Initial dry density (pcf)
200	59.7%	Swell (psf)

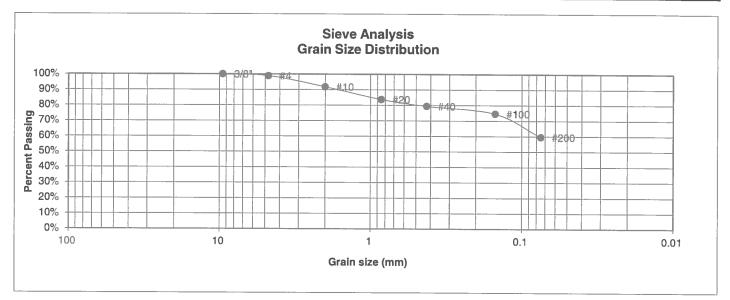


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RESULTS	

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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	38	JOB NO.	190300
DEPTH (FT)	15	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg Limits Plastic Limit 17 Liquid Limit 34 Plastic Index 17
4	98.9%	Swell
10	91.9%	Moisture at start
20 40	83.7% 79.3%	Moisture at finish Moisture increase
100 200	74.6% 59.6%	Initial dry density (pcf) Swell (psf)

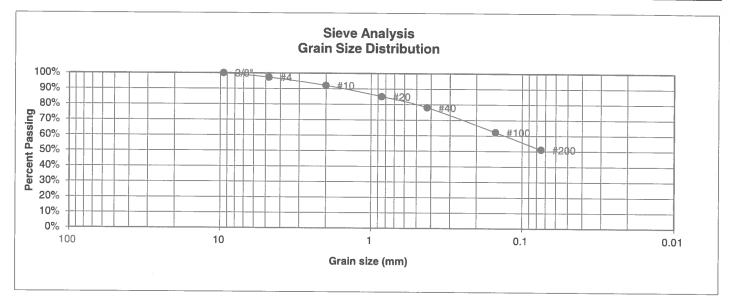
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DATE:	CHECKED:	DATE:		

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UNIFIED CLASSIFICATION	CL	CLIENT	TECH CONTRACTORS
SOIL TYPE #	3	PROJECT	ROLLING HILLS
TEST BORING #	48	JOB NO.	190300
DEPTH (FT)	20	TEST BY	BL



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
4	97.3%	<u>Swell</u>
10	92.1%	Moisture at start
20	85.1%	Moisture at finish
40	78.1%	Moisture increase
100	62.2%	Initial dry density (pcf)
200	51.1%	Swell (psf)



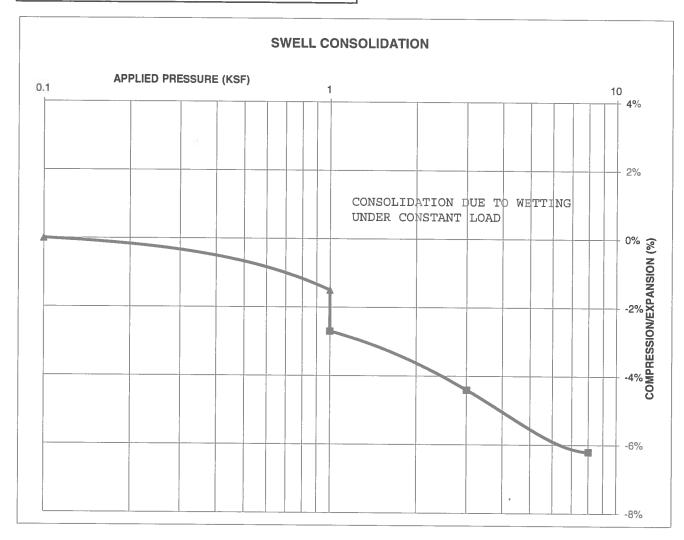
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RESULTS	

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TEST BORING #	19	DEPTH(ft)	2-3
DESCRIPTION	SM	SOIL TYPE	1
NATURAL UNIT DRY	WEIGH	HT (PCF)	113
NATURAL MOISTURE CONTENT		10.0%	
SWELL/CONSOLIDA	TION (9	%)	-1.2%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

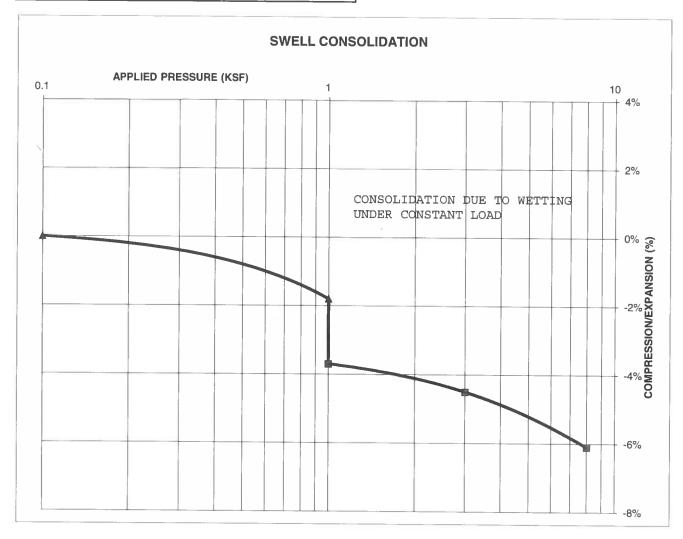
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JOB NO.: 190300

TEST BORING #	4	DEPTH(ft)	20
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	WEIGI	HT (PCF)	110
NATURAL MOISTURE CONTENT		9.3%	
SWELL/CONSOLIDA	NOIT	%)	-1.9%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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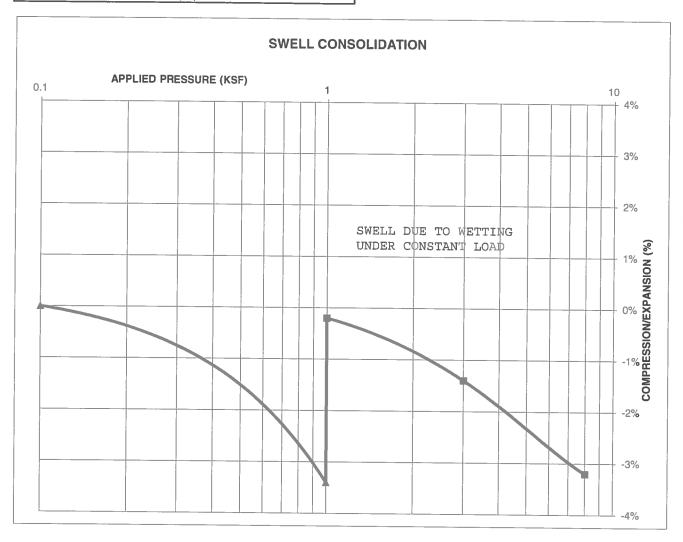
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JOB NO.: 190300

TEST BORING #	20	DEPTH(ft)	20
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	/ WEIGI	HT (PCF)	84
NATURAL MOISTURE CONTENT			7.4%
SWELL/CONSOLIDA	ATION (9	%)	3.2%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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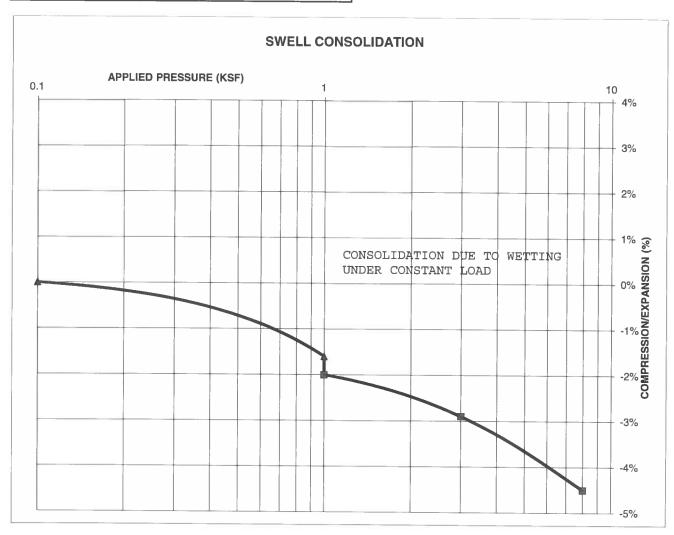
DATE:

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29	DEPTH(ft)	10	
SC	SOIL TYPE	2	
Y WEIGH	HT (PCF)	120	
NATURAL MOISTURE CONTENT		4.5%	
SWELL/CONSOLIDATION (%)		-0.4%	
	SC Y WEIGH RE CON	SC SOIL TÝPÉ Y WEIGHT (PCF) RE CONTENT	SC SOIL TYPE 2 Y WEIGHT (PCF) 120 RE CONTENT 4.5%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

DRAWN: DATE: CHECKED:

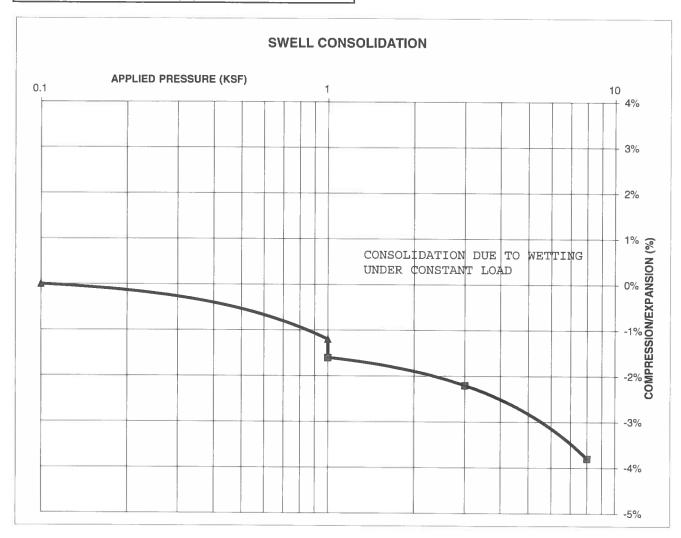
JOB NO.: 190300

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DATE: 7/14/19

TEST BORING #	37	DEPTH(ft)	5
DESCRIPTION	SC	SOIL TYPE	2
NATURAL UNIT DRY	WEIGI	HT (PCF)	117
NATURAL MOISTURE CONTENT			11.4%
SWELL/CONSOLIDA	TION (%)	-0.4%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

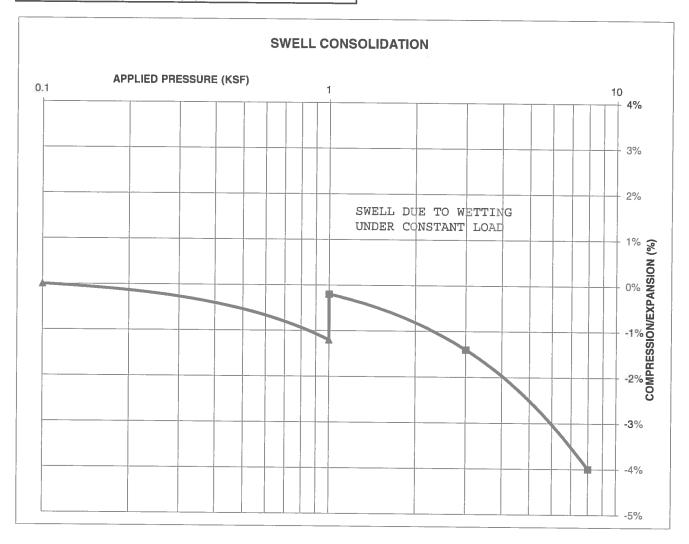
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JOB NO.: 190300

- 1					
	TEST BORING #	15	DEPTH(ft)	10	
	DESCRIPTION	CL	SOIL TYPE	3	
	NATURAL UNIT DRY	WEIG	HT (PCF)	127	
	NATURAL MOISTURE	E CON	TENT	7.2%	
	SWELL/CONSOLIDAT	TION (%)	1.0%	

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

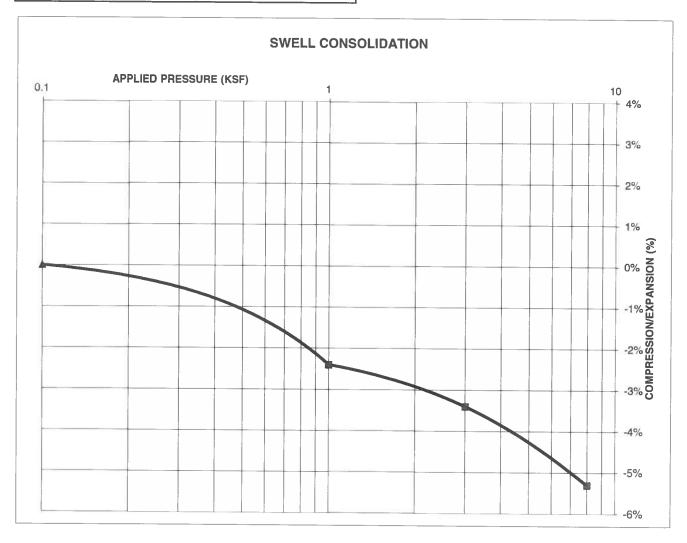
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TEST BORING #	16	DEPTH(ft)	20
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY WEIGHT (PCF)		121	
NATURAL MOISTURE CONTENT		9.5%	
SWELL/CONSOLIDA			0.0%

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CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL	CONSOLIDATION
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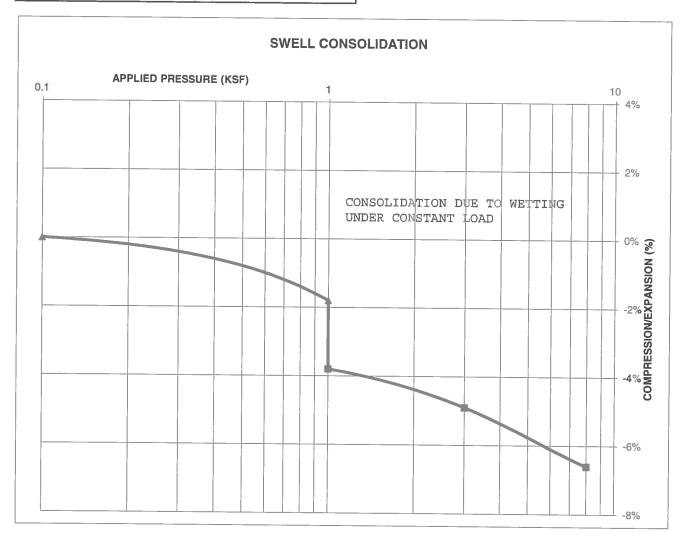
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DATE:

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TEAT DOON IS			
TEST BORING #	22	DEPTH(ft)	10
DE0.00100101		٠,	
DESCRIPTION	CL	SOIL TYPE	3
			3
INATURAL UNIT DRY	′ WEIGH	IT (PCF)	99
			//
NATURAL MOISTURE CONTENT			12.7%
TWITTE WOIST STILL SOLVIENT			12.770
SWELL/CONSOLIDA	TION (%	6)	-2.0%
		٠,	-2.070

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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DATE:

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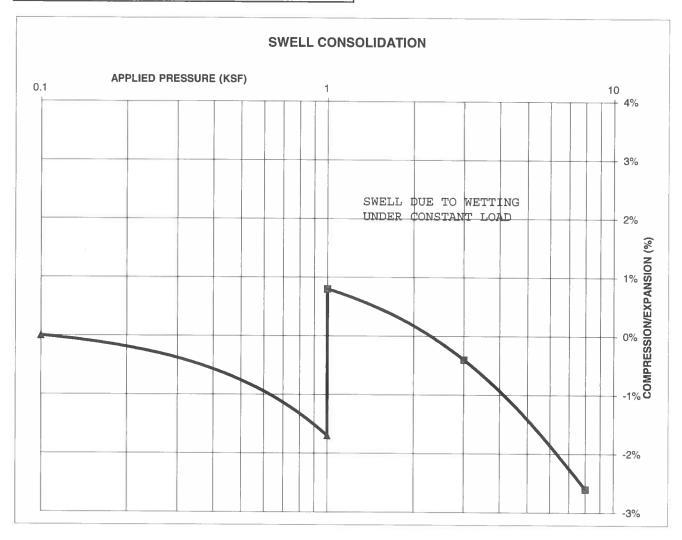
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JOB NO.:

TEST BORING #	33	DEPTH(ft)	10
DESCRIPTION	_	SOIL TYPE	3
NATURAL UNIT DI	RY WEIGH	T (PCF)	115
NATURAL MOISTU	JRE CONTI	ENT	16.5%
SWELL/CONSOLI	DATION (%) —	2.5%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

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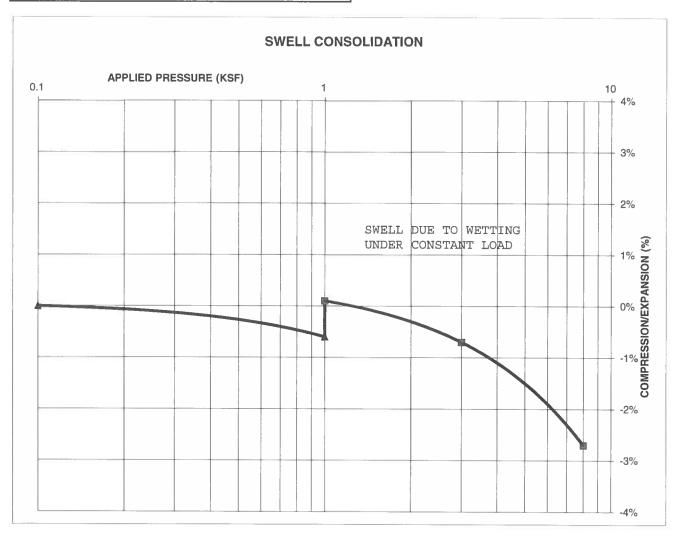
DATE:

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JOB NO.: 190300

TEST BORING #	34	DEPTH(ft)	10
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY	WEIGI	HT (PCF)	114
NATURAL MOISTUR	E CON	TENT	11.5%
SWELL/CONSOLIDA	TION (%)	0.7%

JOB NO. 190300
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PROJECT ROLLING HILLS





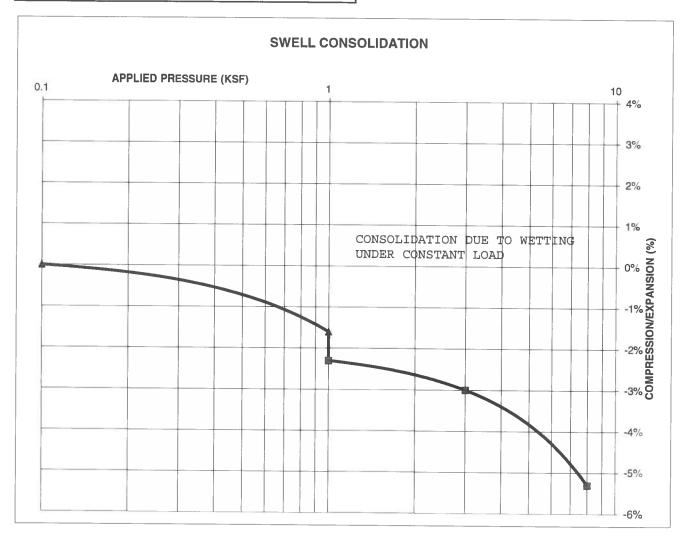
SWELL	CONSOLIDATION	J
TEST R	ESULTS	

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JOB NO.: 190300

TEST BORING #	48	DEPTH(ft)	20
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY WEIGHT (PCF)			103
NATURAL MOISTURE CONTENT			12.5%
SWELL/CONSOLIDATION (%)			-0.7%

JOB NO. 190300
CLIENT TECH CONTRACTORS
PROJECT ROLLING HILLS





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

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JOB NO.:

CLIENTTECH CONTRACTORSJOB NO.190300PROJECTROLLING HILLSDATE3/28/2019LOCATIONROLLING HILLSTEST BYBL

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-6	2-3	1	SM-SW	<0.01
TB-10	5	1 +	SC	0.01
TB-6	20	2	SC	<0.01
TB-9	15	2	SM	<0.01
TB-23	2-3	1	SM	0.00
TB-37	5	2	SC	0.00
TB-40	10	2	SM	<0.01
TB-13	2-3	1	SW	0.00
TB-14	20	2	SM	<0.01
TB-15	10	3	CL	<0.01
TB-31	5	1	SM-SW	<0.01
TB-39	5	1 1	SM	<0.01
TB-39	15	2	SC	<0.01
TB-22	10	3	CL	<0.01
TB-28	2-3	1	SW	<0.01
TB-28	15	2	SC	0.00
TB-26	5	1	SM-SW	<0.01
TB-38	2-3	1	SM-SW	<0.01
TB-38	15	3	CL	0.03
TB-48	20	3	CL	0.00

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QC BLANK PASS



LABORATORY TEST SULFATE RESULTS					
DATE:	CHECKED:	7/10ATE:			

JOB NO.: 190300