



Final Drainage Report

I68 Training Facility

+/-158.45 Acre Parcel

Project No. 61224

December 6, 2024

PCD File No. PPR2440

Final Drainage Report

for

I68 Training Facility

Project No. 61224

December 6, 2024

prepared for

K. Marc Fitzwater

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Peyton, CO 80831

prepared by

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61224-168 Training Facility-FDR.odt

Statements and Acknowledgments

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Charles C. Crum, P.E.
Colorado No. 13348
For and on Behalf of MVE, Inc.

Developer's Statement

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

K. Marc Fitzwater
Owner
9758 Vistas Park Dr.
Peyton, CO 80831

Date

El Paso County

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer
County Engineer / ECM Administrator

Date

Conditions:

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Final Drainage Report

The purpose of this Final Drainage Report is to identify drainage patterns and quantities within and affecting the proposed I68 Training Facility site. The I68 Training facility is approved as a 'Special Use AL249' on 08/08/24 has been split into four Phases. Phases 1, 2, & 3 will be composed of six Flat Shooting Ranges and one long distance range. Phase 4 will consist of the Connex City, Administrative Building, Lodging Building, Operational Support buildings, and Driving Track. The Final Drainage Report will address Phases 1, 2, & 3. Phase 4 will be addressed and submitted in the future as a separate Site Development Plan. The development project is to build an elite firearms training facility. The report will identify specific solutions to drainage concerns on-site and off-site resulting from the proposed project. The report and included maps present results of hydrologic and drainage facilities analyses. The report will discuss the recommended drainage improvements to the site and identify drainage requirements relative to the proposed project. This report has been prepared and submitted in accordance with the requirements of the El Paso County development approval process. An Appendix is included with this report with pertinent calculations and graphs used in the drainage analyses and design.

1 General Location and Description

1.1 Location

The proposed I68 Training Facility site is a tract of property located in Section 7, Township 13 South, Range 61 W of the 6th P.M. in El Paso County, Colorado. The 158.45 acre site is situated to the west of Calhan Highway, and this would be the road in which the site will be accessed from. The property is currently zoned as A-35.

The properties to the north and to the south of the site are also zoned as A-35 and are undeveloped. To the west of the site is Liberty Road.

A **Vicinity Map** is included in the **Appendix**. The entire site is located in El Paso County's Upper Big Springs Creek Drainage Basin.

1.2 Description of Property

The I68 Training Facility site 158.45 acres and is zoned A-35 (Agriculture). The property is undeveloped. El Paso County Tax Assessor's Schedule Number: 1300000712. The proposed I68 Training Facility includes a gravel access driveway, gravel parking areas, 6 shooting range areas each with a shooting overhead cover structure and one long distance shooting range.

The ground cover, which is in good condition, consists of native grasses. The land use is categorized as grazing.

The existing site topography slopes to the south-west with grades that range from 3% to 5%.

There is a large drainage path on the western portion of the I68 Training Facility site. Also, small drainage swales exist on the southern portion of said site and exiting at the southern site boundary. No construction is proposed in said large drainage path and small drainage swale areas. The will

remain undisturbed. For the entire site, all storm runoff flows drain to the south-west. There is no storm drain system in the surrounding area. The site is located in El Paso County's Upper Big Springs Creek Drainage Basin and the flows from the site flow south-west and eventually enter Big Springs Creek.

According to the National Resource Conservation Service, there are three (3) soil types in the I68 Training Facility site. Yoder gravelly-sandy loam (map unit 110) makes up about 80.9% of the site, Truckton sandy loam (map unit 97) makes up about 18.7% of the site and Bresser Sandy Loam (map unit 11) makes up about 0.3% of the soil on the site.

Yoder gravelly sandy loam is deep and somewhat excessively drained. Permeability is moderately rapid, surface runoff is medium to rapid, and the hazard of erosion is moderate. Yoder gravelly sandy loam is classified as being part of Hydrologic Soil Group A.

Truckton sandy loam is deep and well drained. Permeability is moderately rapid, surface runoff is slow to medium, and the hazard of erosion is moderate. Truckton sandy loam is classified as being part of Hydrologic Soil Group A.

The other soil type located on the site is Bresser sandy loam and this soil type makes up a very small portion of the site @ 0.3%. The soil is deep and well drained. Permeability is moderate, surface runoff is slow, and the hazard of erosion is moderate. Bresser sandy loam is classified as being part of Hydrologic Soil Group B.

A portion of the Soil Map and data tables from the National Cooperative Soil Survey and relevant Official Soil Series Descriptions (OSD) are included in the **Appendix**.^{1 2}

2 Drainage Basins and Sub-Basins

2.1 Major Basin Descriptions

The I68 Training Facility site is located in the Upper Big Springs Creek Drainage Basin (CHBG0400). No Drainage Basin Planning Studies are on file for this drainage basin.

The current Flood Insurance Study of the region includes Flood Insurance Rate Maps (FIRM), effective on December 7, 2018.³ The proposed training facility is included in the Community Panel Numbered 08041C0625 G of the Flood Insurance Rate Maps for the El Paso County. No part of the site is shown to be included in a 100-year flood hazard area as determined by FEMA. A portion of the current FEMA Flood Insurance Rate Maps with the site delineated is included in the **Appendix**.

2.2 Sub-Basin Description

The existing and developed drainage patterns of the I68 Training Facility project are described by four (4) on-site drainage basins and five (5) offsite basins. All of these basins are previously undisturbed. All existing basin delineations and data are depicted on the attached **Existing Drainage Map**.

2.2.1 Existing Drainage Patterns (Off-Site)

Off-site sub-basin OS-1 is located north and to the east end of the site, containing pasture/meadow areas, drains south onto the site. This flow enters the onsite sub-basin EX-A and continues through the site.

Off-site sub-basin OS-2 is located north of the site, containing pasture/meadow areas, drains south onto the site. This flow enters the onsite sub-basin EX-B and continues through the site.

Off-site sub-basin OS-3 is located north of the site and to the east of off-site sub-basin OS-2, containing pasture/meadow areas, drains south onto the site. This flow enters the onsite sub-basin EX-C and continues through the site.

1 WSS
2 OSD
3 FIRM

Off-site sub-basin OS-4 is located north and to the west end of the site, containing pasture/meadow areas, drains south onto the site. This flow enters the onsite sub-basin EX-D and continues through the site.

Off-site sub-basin OS-5 is located north and to the west end of the site, containing pasture/meadow areas, drains south onto the site. This flow enters the onsite sub-basin EX-D and continues through the site.

2.2.2 Existing Drainage Patterns (On-Site)

Sub-basin EX-A is to the eastern portion of the site, containing pasture/meadow, drains south. The combined flows of sub-basin OS-1 and EX-A drains to the south and exits the site into the adjacent property.

Sub-basin EX-B is to the eastern-middle portion of the site, containing pasture/meadow, drains south-west. The combined flows of sub-basin OS-2 and EX-B drains to the south-west and exits the site into the adjacent property.

Sub-basin EX-C is to the western-middle portion of the site, containing pasture/meadow, drains south. The combined flows of sub-basin OS-3 and EX-C drains to the south and exits the site into the adjacent property.

Sub-basin EX-D is to the western portion of the site, containing pasture/meadow, drains south-west. The combined flows of sub-basin OS-4 and EX-D drains to the south-west and exits the site into the adjacent property.

3 Drainage Design Criteria

3.1 Development Criteria Reference

This Final Drainage Report for I68 Training Facility has been prepared according to the report guidelines presented in the latest edition of *El Paso County Drainage Criteria Manual* (DCM)⁴. The County has also adopted portions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2, especially concerning the calculation of rainfall runoff flow rates.^{5 6} The hydrologic analysis is based on a collection of data from the DCM, the NRCS Web Soil Survey⁷, and existing topographic data by Polaris.

3.2 Previous Drainage Studies

No drainage reports were found for any of the surrounding developments.

3.3 Hydrologic Criteria

For this Final Drainage Report, the Rational Method as described in the *Drainage Criteria Manual* has been used for all Storm Runoff calculations, as the development and all sub-basins are consistent in ground cover with prairie type attributes. The larger off-site basin OS-4 drains into the future Phase 4 area which will be planned in the future with a Phase 4 Site Development Plan and a Final Drainage Report addressing calculation requirements. The calculations utilizing the Rational Method for this report are consistent with the western non-developed area of this submittal. "Colorado Springs Rainfall Intensity Duration Frequency" curves, Figure 6-5 in the DCM, was used to obtain the design rainfall values; a copy is included in the **Appendix**. The "Overland (Initial) Flow Equation" (Eq. 6-8) in the DCM, and Manning's equation with estimated depths were used in time of concentration calculations. "Runoff Coefficients for Rational Method", Table 6-6 in the DCM, was utilized as a guide in estimating runoff coefficient and Percent Impervious values; a copy is included in the **Appendix**. Peak runoff discharges were calculated for each drainage sub-basin for both the

4 DCM Section 4.3 and Section 4.4

5 CS DCM Vol 1

6 CS DCM Vol 2

7 WSS

5-year storm event and the 100-year storm event with the Rational Method formula, (Eq. 6-5) in the DCM.⁸

4 Drainage Facility Design

4.1 General Concept

The intent of the drainage concept presented in this Final Drainage Report is to allow for the development of the 158.45+/- acres while maintaining the existing drainage patterns on the site. The site will be in compliance with the County's Stormwater Management regulations without the need for permanent water quality treatment facilities. Major and minor storm flows will continue to be safely conveyed through the site and downstream.

The site is expected to be constructed in several Phases as detailed in the Site Development Plan. This Drainage Report reflects the ultimate build out conditions and the maximum impact of the project.

The existing and proposed drainage hydrologic conditions are described in more detail below. Input data and results for all calculations are included in the **Appendix**. A Drainage map for the hydrology are also included in the **Appendix**.

4.2 Existing Hydrologic Conditions

The I68 Training Facility site is impacted by nine (9) existing sub-basins, four (4) on-site and five (5) off-site. The site generally drains south and southwest. The sub-basins are described in more detail below.

Design Point 1 – DP1 Off-site sub-basin OS-1 (29.98 acres) is located north at the northeast end of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin EX-A (19.76 acres) containing pasture/meadow, and continue flowing southerly through the site. The combined flows of sub-basins OS-1 and EX-A are $Q_5 = 4.7$ cfs and $Q_{100} = 34.8$ cfs draining to the south and exiting the site at **DP1** into the adjacent property.

Design Point 2 – DP2 Off-site sub-basin OS-2 (111.10 acres) is located north of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin EX-B (55.08 acres) containing pasture/meadow, and continue flowing southerly through the site. The combined flows of sub-basins OS-2 and EX-B are $Q_5 = 11.5$ cfs and $Q_{100} = 84.0$ cfs draining to the southwest and exiting the site at **DP2** into the adjacent property.

Design Point 3 – DP3 Off-site sub-basin OS-3 (17.00 acres) is located north of the site and to the west of sub-basin OS-2, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin EX-C (48.04 acres) containing pasture/meadow, and continues flowing southerly through the site. The combined flows of sub-basins OS-3 and EX-C are $Q_5 = 10.6$ cfs and $Q_{100} = 77.8$ cfs draining to the southwest and exiting the site at **DP3** into the adjacent property.

Design Point 4 – DP4 Off-site sub-basins OS-4 (157.08 acres) and OS-5 (11.95 Acres) are located at the northwest end of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin EX-D (35.58 acres) containing pasture/meadow, and continues flowing southwesterly through the site. The combined flows of sub-basins OS-4, OS-5, and EX-D are $Q_5 = 10.0$ cfs and $Q_{100} = 73.3$ cfs draining to the southwest and exiting the site at **DP4** into the adjacent property.

8 DCM

Developed Hydrologic Conditions

The I68 Training Facility site is impacted by nine (9) sub-basins, eight (8) on-site and the existing five (5) off-site. The site generally drains south and southwest. The sub-basins are described in more detail below.

Design Point A1 – DPA1 Off-site sub-basin OS-1 (29.98 acres) is located north at the northeast end of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin PR-A1 (1.35 acres) containing pasture/meadow, and continues flowing southerly. The combined flows of sub-basin OS-1 and PR-A1 are $Q_5 = 3.4$ cfs and $Q_{100} = 25.0$ cfs draining to the proposed 24" CM Pipe w/ flared end sections. Said pipe to be placed under the proposed gravel driveway exiting said pipe via proposed 7'W x 13'L riprap outfall at **DPA1** into sub-basin PR-A2. Calculations for pipe and outfall riprap is included in the **Appendix**.

Design Point A2 – DPA2 On-site sub-basin PR-A2 (51.42 acres) is located along the eastern boundary of the site, containing pasture/meadow areas with no proposed construction activities, combining with flows of **DPA1** and draining southerly through the site. The combined flows of **DPA1** and sub-basin PR-A2 are $Q_5 = 5.1$ cfs and $Q_{100} = 34.9$ cfs drain southerly and exit the site at **DPA2** into the adjacent property.

Design Point B – DPB On-site sub-basin PR-B (40.00 acres) is located in the eastern-middle portion of the site. Sub-basin PR-B contains meadow/pasture, roofs from the shooting overhead cover structure, lawn/turf field, landscaping, gravel driveway, and gravel parking areas. The Hesco Barriers adjacent to the 'Long Distance Shooting Range' will be spaced 10' between sections to allow natural drainage flow. Sub-basin PR-B encompasses about 85% of sub-basin EX-B producing peak existing storm runoff rates of approximately $Q_5 = 8.4$ cfs and $Q_{100} = 61.9$ cfs. Sub-basin PR-B runoff rates of $Q_5 = 11.0$ cfs and $Q_{100} = 59.6$ cfs (developed flows) will drain southerly and onto the adjacent property over the length of the southern property line and the flow is not concentrated. This is an increase of $Q_5 = 2.6$ cfs and a decrease of $Q_{100} = 2.3$ cfs. There is less flow for the proposed 100-yr. flows in this basin due to a difference in the time of concentrations. The time of concentration in the proposed basin condition is longer, and this is due to the proposed site grading simply making a longer path. Based on the rational equation, the longer time of concentration value, resulted in less flow volume. By comparing the change in flows for the existing and proposed conditions in this sub-basin, the difference is minimal (and even reduced for the 100-yr event), thus, having no negative impact on downstream areas. The overland flows generally sheet flow off of the site to the south.

Design Point C1 – DPC1 OS-2 (114.90 acres) is located north of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin PR-C1 (4.49 acres) containing pasture/meadow, and the proposed shooting berm directing the flows westerly and then southerly via a proposed swale formed by the proposed shooting berms. The combined flows of sub-basin OS-2 and PR-C1 are $Q_5 = 8.7$ cfs and $Q_{100} = 63.9$ cfs draining to the proposed 2 - 24" CM Pipes w/ flared end sections. Said pipe to be placed under the proposed gravel driveway exiting the pipes via proposed 9'W x 13'L riprap outfall at **DPC1** into sub-basin PR-C2. Calculations for shooting berm swales, pipes and outfall riprap is included in the **Appendix**.

Design Point C2 – DPC2 On-site sub-basin PR-B (40.00 acres) is located in the middle portion of the site. Sub-basin PR-C2 contains meadow/pasture, roofs from the shooting overhead cover structure, lawn/turf field, landscaping, gravel driveway, and gravel parking areas. The Hesco Barriers adjacent to the 'Long Distance Shooting Range' will be spaced 10' between sections to allow natural drainage flow. Sub-basin PR-C2 encompasses about 15% of sub-basin EX-B reducing peak existing storm runoff rates to approximately $Q_5 = 1.5$ cfs and $Q_{100} = 11.0$ cfs, and also encompasses about 5% of sub-basin EX-C reducing peak existing storm runoff rates to approximately $Q_5 = 0.5$ cfs and $Q_{100} = 3.4$ cfs. PR-C2 runoff rates of $Q_5 = 3.9$ cfs and $Q_{100} = 21.4$ cfs (developed flows) which drain south and onto the adjacent property an existing swale. This is an increase of $Q_5 = 1.9$ cfs and an increase of $Q_{100} = 7.0$ cfs. There is less flow for the proposed 100-yr. flows in this basin due to there being a difference in the time of concentrations. The time of concentration in the proposed basin condition is 8.4 minutes longer, and this is due to the proposed site grading simply making a longer path. Based on the rational equation, the longer time of concentration value, resulted in less flow volume. By comparing the change in flows for the existing and proposed conditions in this sub-

basin, the difference is minimal (and even reduced for the 100-yr event), thus, having no negative impact on downstream areas. The flows leave the site to the south in an existing defined shallow swale which is not showing any signs of erosion. Calculation for this existing swale is included in the **Appendix**.

Design Point D1 – DPD1 OS-3 (17.00 acres) is located north of the site, containing pasture/meadow areas, draining south onto the site. This flow enters the on-site sub-basin PR-D1 (2.52 acres) containing pasture/meadow, and the proposed shooting berm directing the flows westerly via a proposed swale formed by the proposed shooting berm. The combined flows of sub-basin OS-3 and PR-D1 are $Q_5 = 3.7$ cfs and $Q_{100} = 27.0$ cfs draining within the proposed swale to outfall at **DPD1** into sub-basin PR-D2. Calculations for the shooting berm swale are included in the **Appendix**.

Design Point D2 – DPD2 On-site sub-basin PR-D2 (40.92 acres) is located along the western boundary of the site. Sub-basin PR-D2 contains meadow/pasture, roofs from the shooting overhead cover structure, lawn/turf field, landscaping, gravel driveway, and gravel parking areas combining with flows of **DPD1**, off-site basin OS-4 & OS-5 with all draining southerly through the site. These combined developed flows at **DPD2** are $Q_5 = 9.4$ cfs and $Q_{100} = 67.2$ cfs which drain southwesterly and onto the adjacent property via an existing drainageway. Sub-basin PR-D2 encompasses about 15% of sub-basin EX-C reducing peak existing storm runoff rates to approximately $Q_5 = 1.4$ cfs and $Q_{100} = 9.4$ cfs in the area of sub-basin PR-D2. This is an increase of $Q_5 = 0.8$ cfs and an increase of $Q_{100} = 3.4$ cfs. By comparing the change in flows for the existing and proposed conditions in this sub-basin, the difference is minimal, thus, having no negative impact on downstream areas. The flows are generally flow overland to the existing natural drainageway and off of the site to the south. There are no construction activities that would effect the existing drainageway in the western portion of the site. Flows leave the site southwesterly in the existing drainageway not showing any signs of erosion. Calculation for this existing drainageway is included in the **Appendix**.

Design Point E – DPE On-site sub-basin PR-E (36.66 acres) is located in the western-middle portion of the site. Sub-basin PR-E contains meadow/pasture, roofs from the shooting overhead cover structure, lawn/turf field, landscaping, gravel driveway, and gravel parking areas. The Hesco Barriers adjacent to the 'Long Distance Shooting Range' will be spaced 10' between sections to allow natural drainage flow. Sub-basin PR-E encompasses about 85% of sub-basin EX-C producing peak existing storm runoff rates of approximately $Q_5 = 7.8$ cfs and $Q_{100} = 53.1$ cfs. Sub-basin PR-E runoff rates of $Q_5 = 11.0$ cfs and $Q_{100} = 59.6$ cfs (developed flows) will drain southerly and onto the adjacent property over the length of the southern property line and the flow is not concentrated. This is an increase of $Q_5 = 3.2$ cfs and an increase of $Q_{100} = 6.5$ cfs. By comparing the change in flows for the existing and proposed conditions in this sub-basin, the difference is minimal, thus, having no negative impact on downstream areas. The overland flows generally sheet flow off of the site to the south.

4.3 Erosion Control

Proposed grading for the site will be associated with the shooting berms construction and gravel driveway and gravel parking area installations. Control measures (CM's) for each phase of the project shall be installed individually for each phase and shall include temporary silt fencing.

4.4 Four Step Process

The El Paso County Engineering Criteria Manual (Appendix I, Section I.7.2) requires the consideration of a "Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long term source controls". The Four Step Process is incorporated in this project and the elements are discussed below.

The entire site consists of low impact development which is excluded from Post Construction Stormwater Management requirements by ECM I.7.1.B.5 due to the low development density as an agricultural zoned land, greater than 2.5 acres and having a total tract impervious area of less than

10%. There is no public roadway being dedicated or constructed as part of this project. The site is not subject to Post Construction Stormwater Treatment requirements.

1) Runoff Reduction Practices are employed in this project. Impervious surfaces have been reduced as much as practically possible. There is only minimal hard surfaces proposed. Minimized Directly Connected Impervious Areas (MDCIA) is employed on the project because runoff passes through an open space pasture/meadow area before leaving the site.

2) There are no drainage paths on the site that are required to be stabilized as they are well vegetated with no visual erosion.

3) The project contains no potentially hazardous uses. The site is exempted from the use of WQCV CMs by ECM 1.7.1.B.5 by virtue of the large agricultural lands zoning of the site and having percent imperviousness of less than 10%. Phases 1, 2, & 3 have a imperviousness of 4.1%. As previously stated, this Final Drainage Report addresses Phases 1, 2, & 3. Phase 4 will be addressed and submitted in the future as a separate Site Development Plan with a Phase 4 Final Drainage report which may require WQCV CMs.

4) The agricultural tract of land is not anticipated to contain storage of potentially harmful substances or use of potentially harmful substances. No site specific or other source control CMs are required.

5 Drainage and Bridge Fees

The site is located within the Upper Big Springs Creek Drainage Basin, El Paso Basin Number CHBG0400, which which has no DBPS. There are no fees associated with this basin.

6 Conclusion

This Final Drainage Report presents existing and proposed drainage conditions for the proposed I68 Training Facility project. The development will have negligible and inconsequential effects on the existing site drainage and drainage conditions downstream. The site is exempted from the use of WQCV CMs by ECM 1.7.1.B.5 by virtue low development density as an agricultural zoned land, greater than 2.5 acres and having a total tract impervious area of less than 10%. The entire site upon final development of Phases 1, 2, & 3 is 4.1% impervious. The site is not subject to Post Construction Stormwater Treatment requirements. With such a negligible increase in stormwater flows from the site, detention will not be necessary for the proposed development and will not be provided. The proposed project will not, with respect to stormwater runoff, negatively impact the adjacent properties and downstream properties.

References

NRCS Web Soil Survey. United States Department of Agriculture, Natural Resources Conservation Service ("<http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx>", accessed March, 2018).

NRCS Official Soil Series Descriptions. United States Department of Agriculture, Natural Resources Conservation Service ("<http://soils.usda.gov/technical/classification/osd/index.html>", accessed March, 2018).

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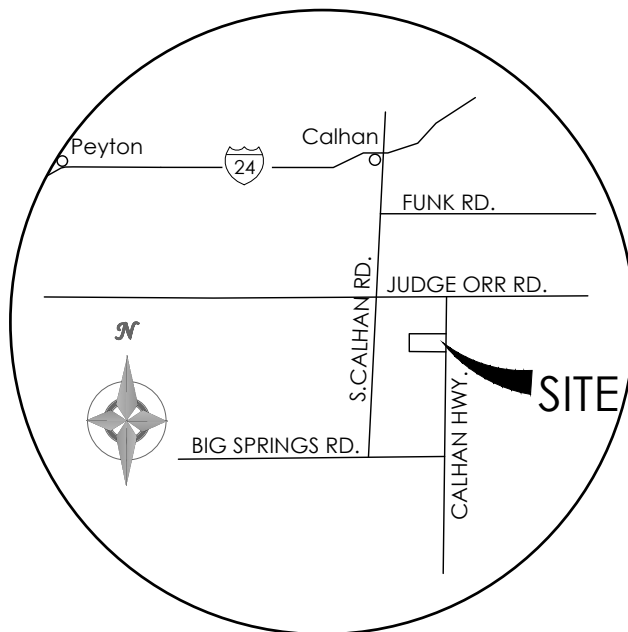
City of Colorado Springs/El Paso County Drainage Criteria Manual. City of Colorado Springs, Department of Public Works, Engineering Division; HDR Infrastructure, Inc.; El Paso County, Department of Public Works, Engineering Division (Colorado Springs: City of Colorado Springs, Revised November 1991).

City of Colorado Springs Drainage Criteria Manual Volume 1. City of Colorado Springs Engineering Division with Matrix Design Group and Wright Water Engineers (Colorado Springs, Colorado: , May 2014).

| Appendices

1 General Maps and Supporting Data

- Vicinity Map
- Portions of Flood Insurance Rate Map
- NRCS Soil Map and Tables
- SCS Soil Type Descriptions
- Hydrologic Soil Group Map and Tables



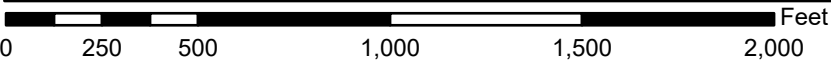
VICINITY MAP

NOT TO SCALE

National Flood Hazard Layer FIRMMette



104°16'22"W 38°56'11"N



1:6,000

104°15'45"W 38°55'43"N

Basemap Imagery Source: USGS National Map 2023

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone D
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5 Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
		Profile Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **10/9/2024 at 4:58 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

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ENTIRE SITE BOUNDARY



United States
Department of
Agriculture

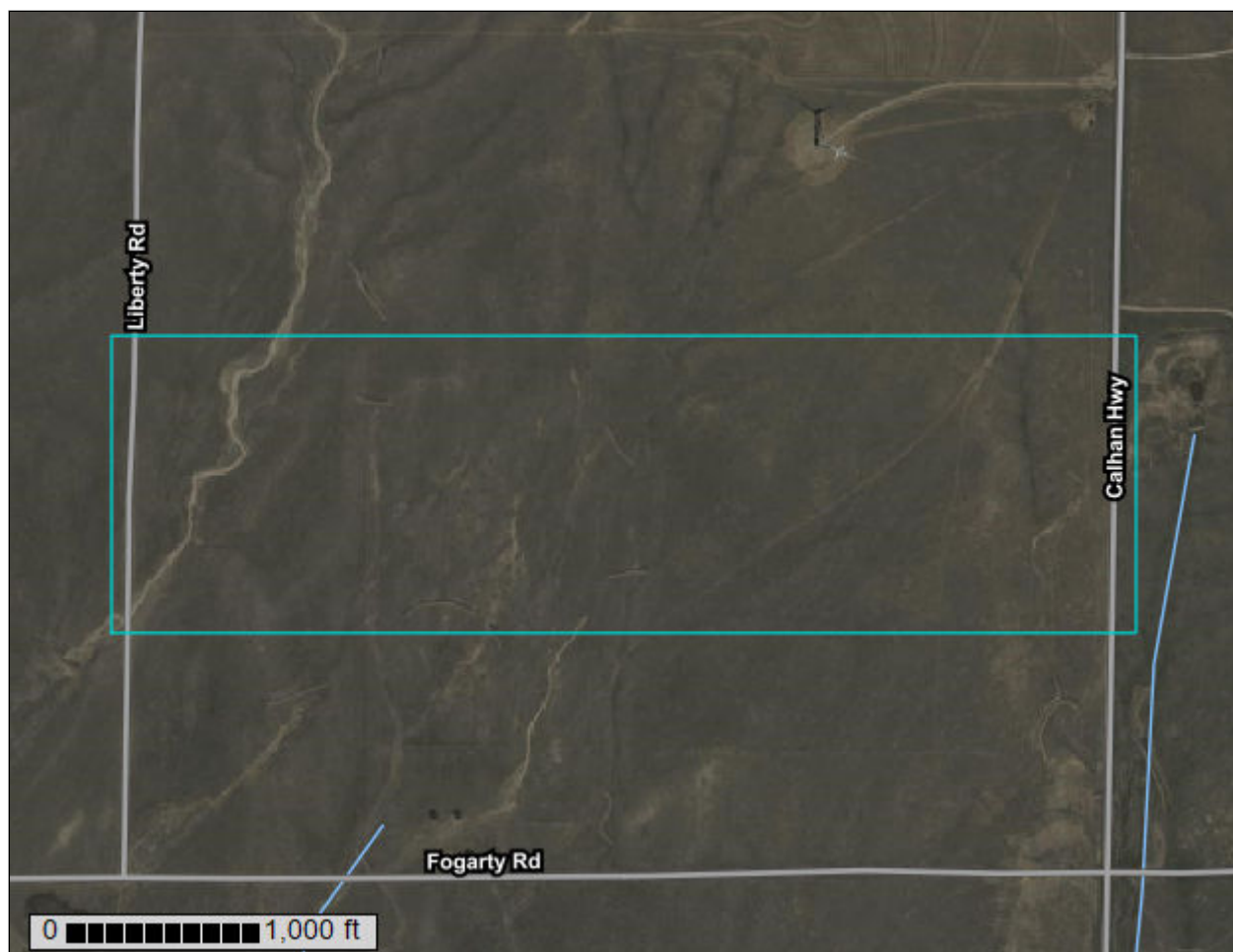
NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for **El Paso County Area, Colorado**

168 Training Facility



October 9, 2024

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

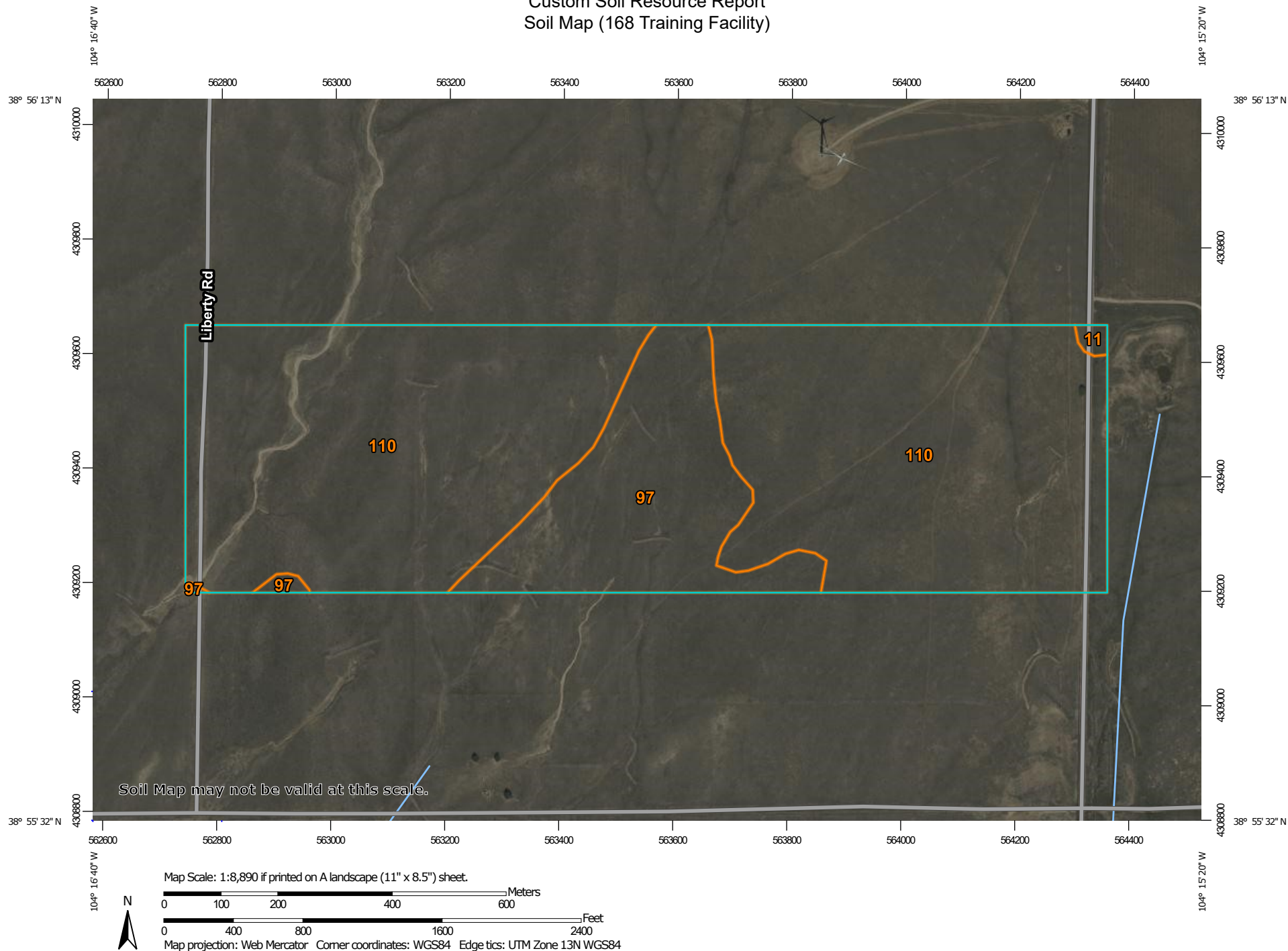
Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map (168 Training Facility)



Custom Soil Resource Report

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

 Blowout

 Borrow Pit

 Clay Spot

 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop

 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

Water Features

 Streams and Canals

Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 22, Sep 3, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Oct 20, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend (168 Training Facility)

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
11	Bresser sandy loam, cool, 0 to 3 percent slopes	0.6	0.3%
97	Truckton sandy loam, 3 to 9 percent slopes	35.2	18.7%
110	Yoder gravelly sandy loam, 8 to 25 percent slopes	151.8	80.9%
Totals for Area of Interest		187.6	100.0%

Map Unit Descriptions (168 Training Facility)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate

pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

11—Bresser sandy loam, cool, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2tlph

Elevation: 5,850 to 6,880 feet

Mean annual precipitation: 15 to 19 inches

Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 100 to 130 days

Farmland classification: Prime farmland if irrigated and the product of I (soil erodibility) x C (climate factor) does not exceed 60

Map Unit Composition

Bresser, cool, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Bresser, Cool

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Convex

Parent material: Tertiary aged alluvium derived from arkose

Typical profile

Ap - 0 to 5 inches: sandy loam

Bt1 - 5 to 8 inches: sandy loam

Bt2 - 8 to 27 inches: sandy clay loam

Bt3 - 27 to 36 inches: sandy loam

C - 36 to 80 inches: loamy coarse sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent

Maximum salinity: Nonsaline to very slightly saline (0.1 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.4 inches)

Interpretive groups

Land capability classification (irrigated): 3e

Land capability classification (nonirrigated): 4c

Hydrologic Soil Group: B

Ecological site: R049XB210CO - Sandy Foothill

Hydric soil rating: No

Minor Components

Truckton

Percent of map unit: 10 percent
Landform: Interfluves
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Yoder

Percent of map unit: 5 percent
Landform: Alluvial fans
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: R049XY214CO - Gravelly Foothill
Hydric soil rating: No

97—Truckton sandy loam, 3 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2x0j2
Elevation: 5,300 to 6,850 feet
Mean annual precipitation: 14 to 19 inches
Mean annual air temperature: 48 to 52 degrees F
Frost-free period: 85 to 155 days
Farmland classification: Not prime farmland

Map Unit Composition

Truckton and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Truckton

Setting

Landform: Hillslopes, interfluves
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Re-worked alluvium derived from arkose

Typical profile

A - 0 to 4 inches: sandy loam
Bt1 - 4 to 12 inches: sandy loam
Bt2 - 12 to 19 inches: sandy loam
C - 19 to 80 inches: sandy loam

Properties and qualities

Slope: 3 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 1 percent
Maximum salinity: Nonsaline (0.1 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 6.6 inches)

Interpretive groups

Land capability classification (irrigated): 6e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Minor Components

Blakeland

Percent of map unit: 8 percent
Landform: Hillslopes, interfluves
Landform position (two-dimensional): Shoulder, backslope, summit
Landform position (three-dimensional): Side slope, crest
Down-slope shape: Convex, linear
Across-slope shape: Convex, linear
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Bresser

Percent of map unit: 7 percent
Landform: Low hills, interfluves
Landform position (two-dimensional): Footslope, toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

110—Yoder gravelly sandy loam, 8 to 25 percent slopes

Map Unit Setting

National map unit symbol: 367f
Elevation: 6,200 to 6,900 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F

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Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Yoder and similar soils: 95 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Yoder

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Noncalcareous alluvium derived from arkose

Typical profile

A - 0 to 6 inches: gravelly sandy loam

Bt - 6 to 12 inches: gravelly sandy clay loam

2C - 12 to 60 inches: very gravelly loamy coarse sand

Properties and qualities

Slope: 8 to 25 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XY214CO - Gravelly Foothill

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 4 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent

Landform: Depressions

Hydric soil rating: Yes

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United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs142p2_052290.pdf

Typically, the surface layer is dark grayish brown sandy loam about 10 inches thick. The subsoil is dark grayish brown and brown sandy loam about 26 inches thick. The substratum is light brownish gray gravelly sandy loam.

Included with this soil in mapping are small areas of Blakeland loamy sand, 1 to 9 percent slopes; Bresser sandy loam, 0 to 3 percent slopes; Truckton sandy loam, 0 to 3 percent slopes; Ellicott loamy coarse sand, 0 to 5 percent slopes; and Ustic Torrifluvents, loamy.

Permeability of this Blendon soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazards of erosion and soil blowing are moderate.

Most areas of this soil are used as rangeland, but some small areas are cultivated. Some homesite development has taken place on this soil.

Native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of plant cover from the soil. Interseeding improves the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Proper location of livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the principal limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is well suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, the provision of undisturbed nesting cover is vital and should be included in plans for habitat development. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for homesites. The main limitation for the construction of local roads and streets is a moderate frost action potential. Roads can be designed to overcome this limitation. Capability subclass IIIe.

11—Bresser sandy loam, 0 to 3 percent slopes. This deep, well drained soil formed in arkosic alluvium and residuum on terraces and uplands. Elevation ranges from 6,000 to 6,800 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The subsoil is brown sandy clay loam about 31 inches thick. The substratum is light yellowish brown loamy coarse sand to a depth of 60 inches.

Included with this soil in mapping are small areas of Truckton sandy loam, 0 to 3 percent slopes; Ascalon sandy loam, 1 to 3 percent slopes; Fort Collins loam, 0 to 3 percent slopes; and Yoder gravelly sandy loam, 1 to 8 percent slopes. Some areas of Ustic Torrifluvents, loamy, occur along narrow drainageways.

Permeability of this Bresser soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, the hazard of erosion is slight to moderate, and the hazard of soil blowing is moderate.

Most areas of this soil are cultivated. The remaining acreage is used as rangeland.

A rotation of winter wheat and fallow is used because precipitation is insufficient for annual cropping. A feed-grain crop such as millet or sorghum can be substituted for wheat in some years. Crop residue management and minimum tillage are needed to control erosion.

Native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of plant cover from the soil. Interseeding improves the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Proper location of livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the principal limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is well suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, the provision of undisturbed nesting cover is vital and should be included in plans for habitat development. This is especially true in areas of intensive farming. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for homesites. Limiting the disturbance of the soil and the removal of existing plant cover during construction helps to control erosion. Capability subclass IIIC.

Almost all areas of this soil are used as rangeland. A few areas of crops such as alfalfa and corn are grown under sprinkler irrigation.

This soil is well suited to the production of native vegetation suitable for grazing. It is best suited to deep-rooted grasses. The native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover. Interseeding is used to improve the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Properly locating livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are fairly well suited to this soil. Blowing sand is the main limitation for the establishment of trees and shrubs. The soil is so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to openland and rangeland wildlife habitat. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. The main limitation of this soil for roads and streets is frost action potential. Special designs for roads are needed to minimize this limitation. Practices are needed to control soil blowing and water erosion on construction sites where the plant cover has been removed. Capability subclass VIe, nonirrigated.

96—Truckton sandy loam, 0 to 3 percent slopes. This deep, well drained soil formed in alluvium and residuum derived from arkosic sedimentary rock on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The next layer is dark grayish brown sandy loam about 3 inches thick. The subsoil is brown sandy loam about 16 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Blakeland loamy sand, 1 to 9 percent slopes; Bresser sandy loam, 0 to 3 percent slopes; Ellicott loamy coarse sand, 0 to 5 percent slopes; and Ustic Torrifluvents, loamy.

Permeability of this Truckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazards of erosion and soil blowing are moderate.

This soil is used mainly for cultivated crops. It is also used for livestock grazing, for wildlife habitat, and as homesites.

Crops are commonly grown in combination with summer fallow because moisture is insufficient for annual cropping. Alfalfa can also be grown on this soil. When this soil is used as cropland, crop residue management and minimum tillage are necessary conservation practices.

This soil is well suited to the production of native vegetation suitable for grazing (fig. 7). It favors deep-rooted grasses. The native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover. Interseeding is used to improve the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Properly locating livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings generally are suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, undisturbed nesting cover is vital and should be provided in plans for habitat development. This is especially true in areas of intensive farming. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. The main limitation of this soil for roads and streets is frost-action potential. Special designs for roads are needed to overcome this limitation. Capability subclasses IIIe, nonirrigated, and IIe, irrigated.

97—Truckton sandy loam, 3 to 9 percent slopes. This deep, well drained soil formed in alluvium and residuum derived from arkosic sedimentary rock on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The next layer is dark grayish brown sandy loam about 3 inches thick. The subsoil is brown sandy loam about 16 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Blakeland loamy sand, 1 to 9 percent slopes; Bresser sandy loam, 3 to 5 percent slopes; and Truckton sandy loam, 0 to 3 percent slopes. Also included are small areas of soils that have arkosic sandstone or shale at a depth of less than 40 inches.

Permeability of this Truckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow to medium, and the hazards of erosion and soil blowing are moderate.

More than half of this soil is used as rangeland, for wildlife habitat, and as homesites. The rest, consisting of the less sloping areas, is used for wheat and sorghum. Rangeland or pastureland is the most suitable use because the permanent plant cover protects the soil.

This soil is well suited to the production of native vegetation suitable for grazing. Native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover from this soil. Interseeding improves the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Properly locating livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings generally are well suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, undisturbed nesting cover is vital and should be provided for in plans for habitat development. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

The main limitation of this soil for construction is frost-action potential. Special designs for roads are needed to overcome this limitation. Because of the sandy nature of the soil, practices must be provided to minimize surface runoff and thus keep erosion to a minimum. Access roads must have adequate cut-slope grade and be provided with drains to control surface runoff. Capability subclasses VIe, nonirrigated, and IVe, irrigated.

98—Truckton-Blakeland complex, 9 to 20 percent slopes. These strongly sloping to moderately steep soils

are on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

The Truckton soil makes up about 60 percent of the complex, the Blakeland soil about 25 percent, and other soils about 15 percent.

Included with these soils in mapping are areas of Bresser sandy loam, 5 to 9 percent slopes, and Yoder gravelly sandy loam, 8 to 25 percent slopes.

The Truckton soil is deep and well drained. It formed in alluvium and residuum weathered from arkosic sedimentary rock. Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The next layer is dark grayish brown sandy loam about 3 inches thick. The subsoil is brown sandy loam about 16 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of 60 inches or more.

Permeability of the Truckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is medium to rapid, and the hazard of erosion is moderate to high. Soil slippage is common on the upper part of slopes.

The Blakeland soil is deep and somewhat excessively drained. It formed in arkosic sandy alluvium and eolian sediment derived from arkosic sedimentary rock. Typically, the surface layer is dark grayish brown loamy sand about 11 inches thick. The underlying material is brown loamy sand about 16 inches thick; it grades to pale brown sand that extends to a depth of 60 inches or more.

Permeability of the Blakeland soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Surface runoff is medium, and the hazard of erosion is moderate to high, and the hazard of soil blowing is high. Soil slippage is common on the upper part of slopes.

The soils in this complex are used for grazing livestock and wildlife habitat.

These soils are suited to the production of native vegetation suitable for grazing. The native vegetation is dominantly western wheatgrass, side-oats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover from these soils. Interseeding improves the existing vegetation. Deferment of grazing in spring improves plant vigor and soil stability. Properly locating livestock watering facilities helps to control grazing.

Soil blowing is the main limitation for the establishment of trees and shrubs on these soils. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Trees need to be planted in shallow furrows on the Blakeland soil because of its loose, sandy surface layer. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac and lilac.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

The main limitation of this soil for excavations is the high gravel content, which causes cut banks to cave in. Excavations for underground utilities need to be designed to overcome this limitation. Capability subclass VIe.

110—Yoder gravelly sandy loam, 8 to 25 percent slopes. This deep, well drained, gravelly soil formed in noncalcareous alluvium derived from arkosic deposits on uplands. Elevation ranges from 6,200 to 6,900 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown gravelly sandy loam about 6 inches thick. The subsoil is brown gravelly sandy clay loam about 6 inches thick. The substratum is very gravelly loamy coarse sand to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Louviers silty clay loam, 3 to 18 percent slopes, and Truckton-Bresser complex, 5 to 20 percent slopes.

Permeability of this Yoder soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Surface runoff is medium to rapid, and the hazard of erosion is moderate. Some gullies have developed along drainageways, and there is some soil slippage on the steeper slopes.

This soil is used as rangeland and for wildlife habitat.

The native vegetation is mainly western wheatgrass, side-oats grama, needleandthread, and little bluestem. The most prominent shrub on this soil is true mountain-mahogany.

Vegetation is very difficult to reestablish on this soil if the native vegetation is destroyed. Properly locating livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are suited to this soil. Low available water capacity is the main limitation for the establishment of tree and shrub plantings. Summer fallow a year in advance and continued cultivation for weed control are needed to insure the establishment and survival of plantings. Supplemental irrigation may also be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac and lilac.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly

managing livestock grazing, and reseeding range where needed.

The main limitation of this soil for homesites is slope. The high gravel content can cause some excavation problems, such as unstable cut banks. Special designs for buildings and roads are required to overcome this limitation. Access roads must have adequate cut-slope grade and be provided with drains to control surface runoff and keep soil losses to a minimum. Capability subclass VIe.

Use and management of the soils

The soil survey is a detailed inventory and evaluation of the most basic resource of the survey area—the soil. It is useful in adjusting land use, including urbanization, to the limitations and potentials of natural resources and the environment. Also, it can help avoid soil-related failures in uses of the land.

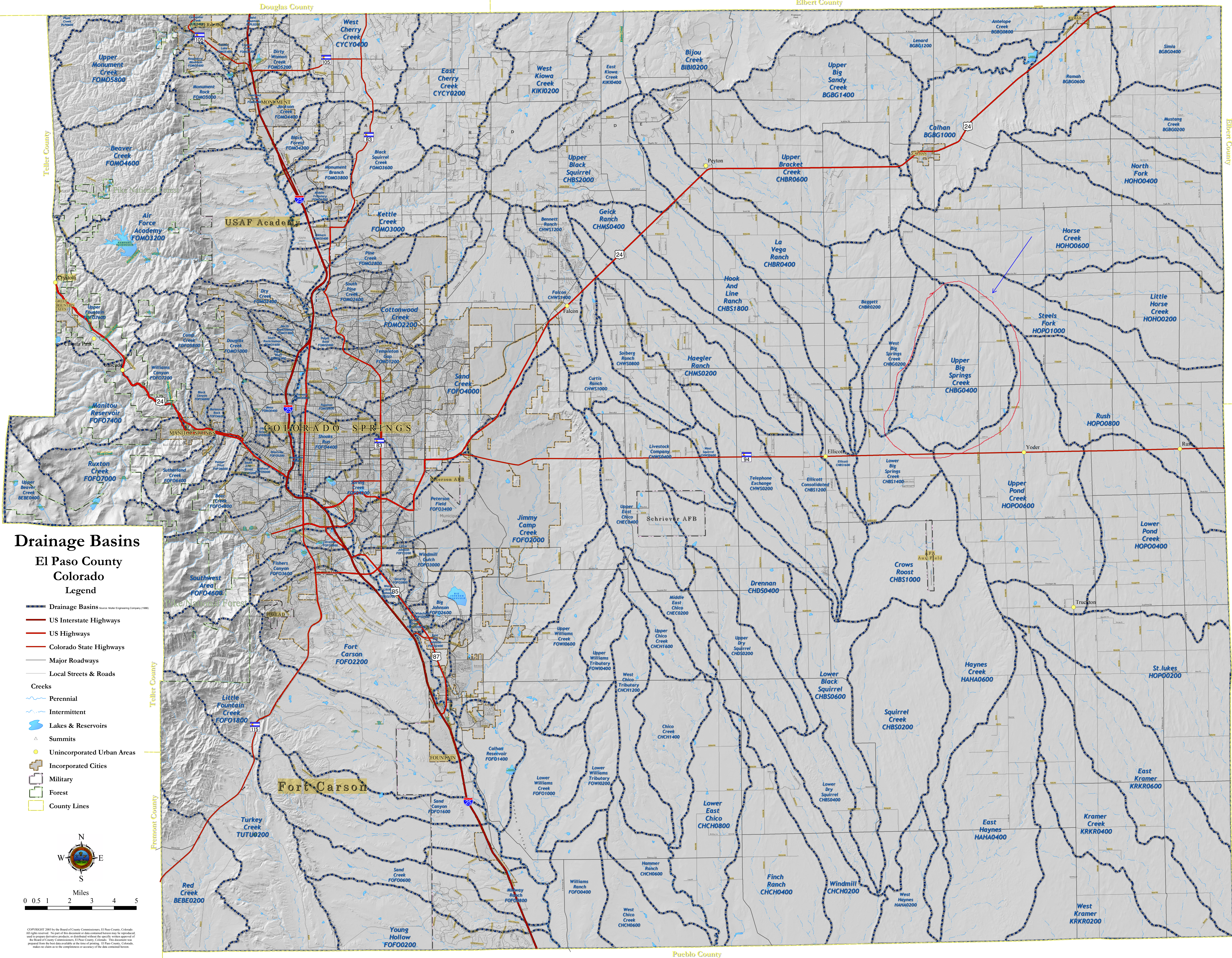
While a soil survey is in progress, soil scientists, conservationists, engineers, and others keep extensive notes about the nature of the soils and about unique aspects of behavior of the soils. These notes include data on erosion, drought damage to specific crops, yield estimates, flooding, the functioning of septic tank disposal systems, and other factors affecting the productivity, potential, and limitations of the soils under various uses and management. In this way, field experience and measured data on soil properties and performance are used as a basis for predicting soil behavior.

Information in this section is useful in planning use and management of soils for crops and pasture, rangeland, and woodland; as sites for buildings, highways and other transportation systems, sanitary facilities, and parks and other recreation facilities; and for wildlife habitat. From the data presented, the potential of each soil for specified land uses can be determined, soil limitations to these land uses can be identified, and costly failures in houses and other structures, caused by unfavorable soil properties, can be avoided. A site where soil properties are favorable can be selected, or practices that will overcome the soil limitations can be planned.

Planners and others using the soil survey can evaluate the impact of specific land uses on the overall productivity of the survey area or other broad planning area and on the environment. Productivity and the environment are closely related to the nature of the soil. Plans should maintain or create a land-use pattern in harmony with the natural soil.

Contractors can find information that is useful in locating sources of sand and gravel, roadfill, and topsoil. Other information indicates the presence of bedrock, wetness, or very firm soil horizons that cause difficulty in excavation.

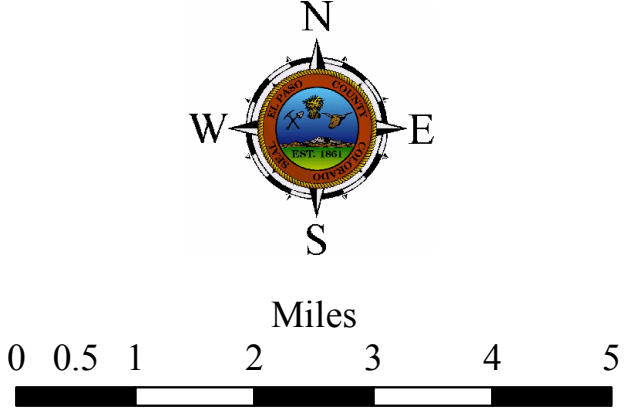
Health officials, highway officials, engineers, and many other specialists also can find useful information in this soil survey. The safe disposal of wastes, for example, is closely related to properties of the soil. Pavements, sidewalks, campsites, playgrounds, lawns, and trees and shrubs are influenced by the nature of the soil.



Drainage Basins

El Paso County
Colorado
Legend

- Drainage Basins (Source: Muter Engineering Company 1988)
- US Interstate Highways
- US Highways
- Colorado State Highways
- Major Roadways
- Local Streets & Roads
- Creeks
 - Perennial
 - Intermittent
- Lakes & Reservoirs
- Summits
- Unincorporated Urban Areas
- Incorporated Cities
- Military
- Forest
- County Lines



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2 Hydrologic Calculations

Runoff Coefficients and Percent Imperviousness Table 6-6

Colorado Springs Rainfall Intensity Duration Frequency Table 6-5

Hydrologic Calculations Summary Form SF-1 for Existing & Developed Conditions

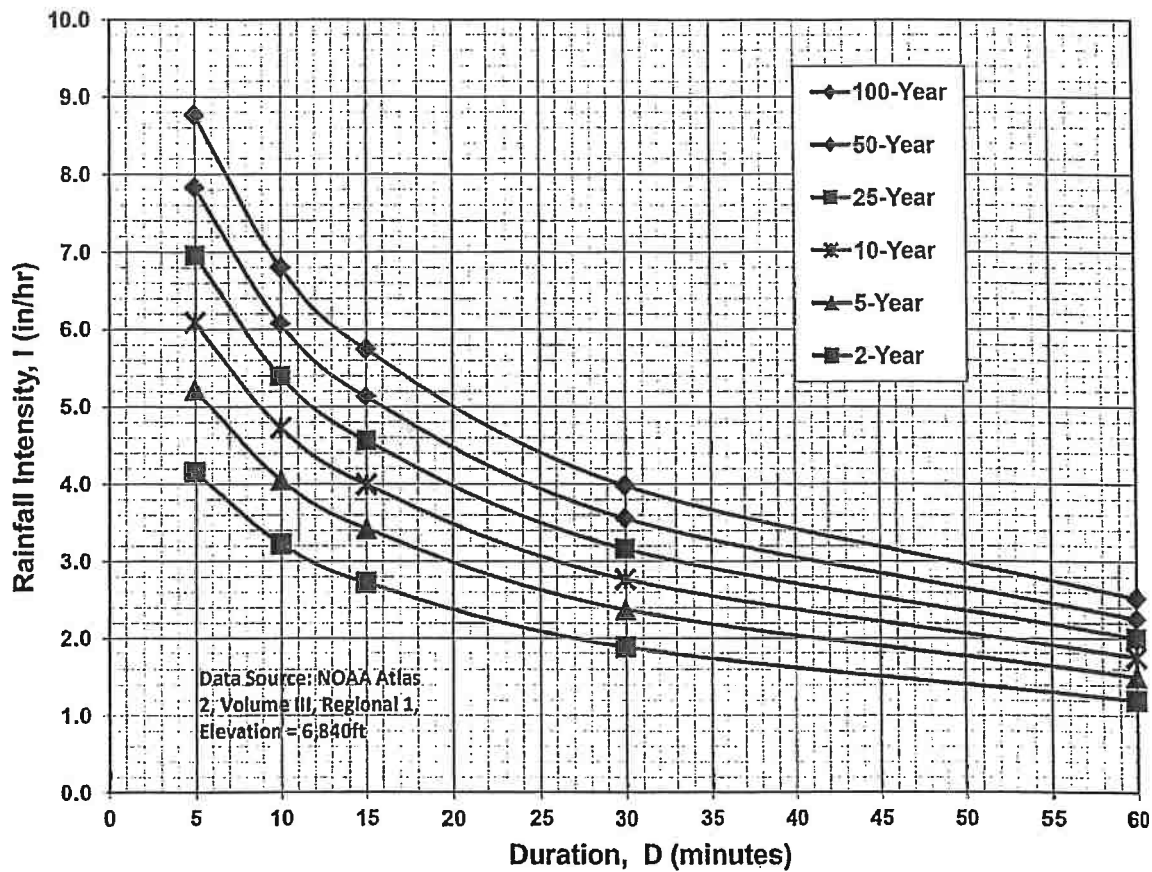
Hydrologic Calculations Summary 5-yr Form SF-2 for Existing & Developed Conditions

Hydrologic Calculations Summary 100-yr Form SF-2 for Existing & Developed Conditions

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis--	2												
Greenbelts, Agriculture		0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Job No.: **61224**
 Project: **168 Training Facility**

Date: **12/6/2024 13:36**
 Calcs By: **SLB**
 Checked By: _____

Time of Concentration (Modified from Standard Form SF-1)

Sub-Basin	Sub-Basin Data				Overland			Shallow Channel				Channelized				t _c Check		t _c
	Area (Acres)	C ₅	C ₁₀₀ /CN	% Imp.	L ₀ (ft)	S ₀ (%)	t _i (min)	L _{0t} (ft)	S _{0t} (ft/ft)	v _{0sc} (ft/s)	t _t (min)	L _{0c} (ft)	S _{0c} (ft/ft)	v _{0c} (ft/s)	t _c (min)	L (min)	t _{c,alt} (min)	
EX-A	19.76	0.08	0.35	0%	300	5%	18.8	1073	0.042	1.4	12.5	0	0.000	0.0	0.0	1373	N/A	31.2
EX-B	55.08	0.08	0.35	0%	300	6%	17.3	1596	0.046	1.5	17.6	0	0.000	0.0	0.0	1896	N/A	35.0
EX-C	48.04	0.08	0.35	0%	300	6%	17.7	1125	0.036	1.3	14.2	0	0.000	0.0	0.0	1425	N/A	31.9
EX-D	35.58	0.08	0.35	0%	300	5%	18.8	1101	0.035	1.3	13.9	267	0.026	2.9	1.5	1668	N/A	34.2
PR-A1	1.35	0.08	0.35	0%	50	8%	6.6	30	0.033	1.3	0.4	0	0.000	0.0	0.0	80	N/A	6.9
PR-A2	18.41	0.10	0.36	2%	300	5%	18.1	464	0.047	1.5	5.1	505	0.028	1.5	5.8	1269	N/A	28.9
PR-B	40.00	0.12	0.38	6%	300	4%	19.5	1221	0.051	1.6	12.9	0	0.000	0.0	0.0	1521	N/A	32.4
PR-C1	4.49	0.09	0.36	1%	300	3%	21.3	1374	0.044	1.5	15.7	422	0.038	4.8	1.5	2096	N/A	38.4
PR-C2	14.10	0.11	0.37	5%	300	12%	13.6	1229	0.031	1.2	16.6	187	0.053	3.8	0.8	1716	N/A	31.1
PR-D1	2.52	0.09	0.36	2%	300	1%	31.6	1030	0.038	1.4	12.6	172	0.041	1.5	1.9	1502	N/A	46.1
PR-D2	40.92	0.09	0.36	1%	300	7%	16.9	1289	0.040	1.4	15.3	267	0.030	3.2	1.4	1856	N/A	33.6
PR-E	36.66	0.10	0.37	4%	300	7%	16.1	1295	0.037	1.3	16.0	0	0.000	0.0	0.0	1595	N/A	32.2

Job No.: **61224**
 Project: **168 Training Facility**
 Design Storm: **5-Year Storm (20% Probability)**
 Jurisdiction: **DCM**

Date: **12/6/2024 13:36**
 Calcs By: **SLB**
 Checked By: _____

Sub-Basin and Combined Flows (Modified from Standard Form SF-2)

DP	Sub-Basin	Area (Acres)	C5	Direct Runoff				Combined Runoff				Streetflow			Pipe Flow					Travel Time		
				t _c	CA	I5	Q5	t _c	CA	I5	Q5	Slope	Length	Q	Q	Slope	Mnngs	Length	D _{Pipe}	Length	V _{0.5C}	t _t
				(min)	(Acres)	(in/hr)	(cfs)	(min)	(Acres)	(in/hr)	(cfs)	(%)	(ft)	(cfs)	(cfs)	(%)	n	(ft)	(in)	(ft)	(ft/s)	(min)
	OS-1	25.98	0.08	54.8	2.08	1.58	3.28															
	OS-2	111.10	0.08	80.1	8.89	1.01	8.95															
	OS-3	17.00	0.08	31.7	1.36	2.40	3.26															
	OS-4	157.08	0.08	92.4	12.57	0.79	9.97															
DP-1	EX-A	19.76	0.08	31.2	1.58	2.42	3.83															
		45.75	0.08					66.1	3.66	1.30	4.7											
DP-2	EX-B	55.08	0.08	35.0	4.41	2.25	9.91															
		166.18	0.08					88.3	13.29	0.86	11.5											
DP-3	EX-C	48.04	0.08	31.9	3.84	2.39	9.19															
		65.05	0.08					40.4	5.20	2.04	10.6											
DP-4	EX-D	35.58	0.08	34.2	2.85	2.28	6.50															
		204.61	0.08					104.3	16.37	0.61	10.0											
DP-A1	PR-A1	1.35	0.08	6.9	0.11	4.68	0.50															
		27.33	0.08					55.5	2.19	1.56	3.4											
DP-A2	PR-A2	18.41	0.10	28.9	1.77	2.54	4.49															
		45.75	0.09					66.7	3.96	1.28	5.1											
DP-B	PR-B	40.00	0.12	32.4	4.63	2.37	10.97															
	PR-C1	4.49	0.09	38.4	0.39	2.11	0.83															
DP-C1		115.60	0.08					83.7	9.28	0.94	8.7											
	PR-C2	14.10	0.11	31.1	1.59	2.43	3.86															
DP-C2		129.69	0.08					91.4	10.87	0.81	8.8											
	PR-D1	2.52	0.09	46.1	0.23	1.84	0.41															
DP-D1		19.52	0.08					32.7	1.59	2.35	3.7											
	PR-D2	40.92	0.09	33.6	3.63	2.31	8.40															
DP-D2		212.47	0.08					109.5	17.38	0.54	9.4											

DCM: $I = C1 * \ln(tc) + C2$
 C1: 1.5
 C1: 7.583

Job No.: **61224**
 Project: **168 Training Facility**
 Design Storm: **100-Year Storm (1% Probability)**
 Jurisdiction: **DCM**

Date: **12/6/2024 13:36**
 Calcs By: **SLB**
 Checked By: _____

Sub-Basin and Combined Flows (Modified from Standard Form SF-2)

DP	Sub-Basin	Area (Acres)	C100	Direct Runoff				Combined Runoff				Streetflow			Pipe Flow					Travel Time		
				t _c	CA	I100	Q100	t _c	CA	I100	Q100	Slope (%)	Length (ft)	Q (cfs)	Q (cfs)	Slope (%)	Mnngs n	Length (ft)	D _{Pipe} (in)	Length (ft)	V _{0.5C} (ft/s)	t _t (min)
				(min)	(Acres)	(in/hr)	(cfs)	(min)	(Acres)	(in/hr)	(cfs)											
DP-1	OS-1	25.98	0.35	54.8	9.09	2.65	24.07															
	OS-2	111.10	0.35	80.1	38.89	1.69	65.62															
	OS-3	17.00	0.35	31.7	5.95	4.02	23.94															
	OS-4	157.08	0.35	92.4	54.98	1.33	73.01															
DP-1	EX-A	19.76	0.35	31.2	6.92	4.06	28.10															
		45.75	0.35					66.1	16.01	2.17	34.8											
DP-2	EX-B	55.08	0.35	35.0	19.28	3.78	72.79															
		166.18	0.35					88.3	58.16	1.44	84.0											
DP-3	EX-C	48.04	0.35	31.9	16.81	4.01	67.46															
		65.05	0.35					40.4	22.77	3.42	77.8											
DP-4	EX-D	35.58	0.35	34.2	12.45	3.83	47.73															
		204.61	0.35					104.3	71.61	1.02	73.3											
DP-A1	PR-A1	1.35	0.35	6.9	0.47	7.85	3.71															
		27.33	0.35					55.5	9.57	2.62	25.0											
DP-A2	PR-A2	18.41	0.36	28.9	6.65	4.26	28.31															
		45.75	0.35					66.7	16.22	2.15	34.9											
DP-B	PR-B	40.00	0.38	32.4	15.01	3.97	59.60															
	PR-C1	4.49	0.36	38.4	1.60	3.54	5.68															
DP-C1		115.60	0.35					83.7	40.49	1.58	63.9											
	PR-C2	14.10	0.37	31.1	5.26	4.08	21.43															
DP-C2		129.69	0.35					91.4	45.75	1.36	62.1											
	PR-D1	2.52	0.36	46.1	0.91	3.08	2.79															
DP-D1		19.52	0.35					32.7	6.86	3.94	27.0											
	PR-D2	40.92	0.36	33.6	14.58	3.88	56.58															
DP-D2		212.47	0.35					109.5	74.65	0.90	67.2											

DCM: $I = C1 * \ln(t_c) + C2$
 C1: 2.52
 C1: 12.735

Sub-Basin OS-1 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	1131832.821	25.98	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,131,833	25.98	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,755	32	-	-	-	-	
Initial Time	300	3	0.010	-	31.9	N/A	DCM Eq. 6-8
Shallow Channel	990	15	0.015	0.9	19.1	-	DCM Eq. 6-9
Channelized	465	14	0.030	2.1	3.7	-	Trap Ditch
				t_c	54.8 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.27	1.58	1.84	2.10	2.37	2.65
Runoff (cfs)	0.7	3.3	7.2	13.7	18.5	24.1
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.7	3.3	7.2	13.7	18.5	24.1

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Sub-Basin OS-2 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	4839623.914	111.10	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	4,839,624	111.10	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	4,135	113	-	-	-	-	
Initial Time	300	5	0.017	-	26.9	N/A	DCM Eq. 6-8
Shallow Channel	3,635	100	0.028	1.2	52.2	-	DCM Eq. 6-9
Channelized	200	8	0.040	3.3	1.0	-	V-Ditch
				t_c	80.1 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.82	1.01	1.18	1.34	1.51	1.69
Runoff (cfs)	1.8	9.0	19.6	37.3	50.4	65.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.8	9.0	19.6	37.3	50.4	65.6

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Sub-Basin OS-3 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	740706.1153	17.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	740,706	17.00	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{max, Overland}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,512	75	-	-	-	-	
Initial Time	300	15	0.050	-	18.8	N/A	DCM Eq. 6-8
Shallow Channel	1,212	60	0.050	1.6	13.0	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	V-Ditch
				t_c	31.7 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.92	2.40	2.80	3.20	3.60	4.02
Runoff (cfs)	0.7	3.3	7.1	13.6	18.3	23.9
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.7	3.3	7.1	13.6	18.3	23.9

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Sub-Basin OS-4 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	6842233.529	157.08	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	6,842,234	157.08	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	5,348	175	-	-	-	-	
Initial Time	300	5	0.017	-	26.9	N/A	DCM Eq. 6-8
Shallow Channel	5,048	170	0.034	1.3	65.5	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	V-Ditch
				t_c	92.4 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.65	0.79	0.93	1.06	1.19	1.33
Runoff (cfs)	2.0	10.0	21.8	41.5	56.1	73.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	2.0	10.0	21.8	41.5	56.1	73.0

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Sub-Basin OS-5 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	520704.0662	11.95	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	520,704	11.95	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{max, Overland}$		300 ft	C_v		7		
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,062	49	-	-	-	-	
Initial Time	300	15	0.050	-	18.8	N/A DCM Eq. 6-8	
Shallow Channel	762	34	0.045	1.5	8.6	- DCM Eq. 6-9	
Channelized			0.000	0.0	0.0	- 0	
					t_c	27.3 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.10	2.62	3.06	3.49	3.93	4.40
Runoff (cfs)	0.5	2.5	5.5	10.4	14.1	18.4
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.5	2.5	5.5	10.4	14.1	18.4

$$DCM: I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Sub-Basin EX-A Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	860850.524	19.76	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	860,851	19.76	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,373	60	-	-	-	-	
Initial Time	300	15	0.050	-	18.8	N/A	DCM Eq. 6-8
Shallow Channel	1,073	45	0.042	1.4	12.5	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	0
				t_c	31.2 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.94	2.42	2.82	3.23	3.63	4.06
Runoff (cfs)	0.8	3.8	8.4	15.9	21.5	28.1
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.8	3.8	8.4	15.9	21.5	28.1

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-1)

Includes Basins OS-1 EX-A

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	1,992,683	45.75	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,992,683	45.75	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-1	-	1,755	32	-	-	-	-	54.8
Channelized-1	Trap Ditch	2	1,372	60	28	40	13	2.0	11.3
Channelized-2									
Channelized-3									
Total			3,127	92					
2 = Natural, Winding, minimal vegetation/shallow grass									
									t_c (min) 66.1

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.05	1.30	1.51	1.73	1.95	2.17
Site Runoff (cfs)	0.96	4.75	10.38	19.78	26.71	34.82
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	4.7	-	-	-	34.8

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin EX-B Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	2399118.903	55.08	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	2,399,119	55.08	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300 ft	C_v		7		
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,896	93	-	-	-	-	
Initial Time	300	19	0.063	-	17.3	N/A DCM Eq. 6-8	
Shallow Channel	1,596	74	0.046	1.5	17.6	- DCM Eq. 6-9	
Channelized			0.000	0.0	0.0	- 0	
					t_c	35.0 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.80	2.25	2.63	3.00	3.38	3.78
Runoff (cfs)	2.0	9.9	21.7	41.3	55.8	72.8
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	2.0	9.9	21.7	41.3	55.8	72.8

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-2)

Includes Basins OS-2 EX-B

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	7,238,743	166.18	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	7,238,743	166.18	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-2	-	4,135	113	-	-	-	-	80.1
Channelized-1	Trap Ditch	2	1,402	60	73	40	13	2.9	8.2
Channelized-2									
Channelized-3									
Total			5,537	173					
2 = Natural, Winding, minimal vegetation/shallow grass									
									t_c (min) 88.3

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.70	0.86	1.01	1.15	1.29	1.44
Site Runoff (cfs)	2.34	11.46	25.07	47.76	64.48	83.96
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	11.5	-	-	-	84.0

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin EX-C Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	2092668.557	48.04	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	2,092,669	48.04	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns				
	$L_{\max, \text{Overland}}$	300 ft			C_v	7	
	L (ft)	ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,425	58	-	-	-	-	
Initial Time	300	18	0.060	-	17.7	N/A	DCM Eq. 6-8
Shallow Channel	1,125	40	0.036	1.3	14.2	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	0
				t_c	31.9 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.92	2.39	2.79	3.19	3.59	4.01
Runoff (cfs)	1.8	9.2	20.1	38.3	51.7	67.5
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.8	9.2	20.1	38.3	51.7	67.5

DCM: $I = C1 * \ln(tc) + C2$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-3)

Includes Basins OS-3 EX-C

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	2,833,375	65.05	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	2,833,375	65.05	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-3	-	1,512	75	-	-	-	-	31.7
Channelized-1	Trap Ditch	2	1,425	58	68	40	13	2.7	8.7
Channelized-2									
Channelized-3									
Total			2,937	133					

2 = Natural, Winding, minimal vegetation/shallow grass

t_c (min) 40.4

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.63	2.04	2.37	2.71	3.05	3.42
Site Runoff (cfs)	2.13	10.59	23.17	44.14	59.59	77.75
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	10.6	-	-	-	77.8

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin EX-D Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	1549895.891	35.58	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,549,896	35.58	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{max, Overland}$		300	ft	C_v		7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,668	61	-	-	-	-	
Initial Time	300	15	0.050	-	18.8	N/A	DCM Eq. 6-8
Shallow Channel	1,101	39	0.035	1.3	13.9	-	DCM Eq. 6-9
Channelized	267	7	0.026	2.9	1.5	-	V-Ditch
				t_c	34.2 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.83	2.28	2.66	3.05	3.43	3.83
Runoff (cfs)	1.3	6.5	14.2	27.1	36.6	47.7
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.3	6.5	14.2	27.1	36.6	47.7

$$DCM: I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-4)

Includes Basins OS-4 OS-5 EX-D

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	8,912,833	204.61	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	8,912,833	204.61	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-4	-	5,348	175	-	-	-	-	92.4
Channelized-1	Trap Ditch	2	1,667	62	48	40	13	2.3	11.8
Channelized-2									
Channelized-3									
Total			7,015	237					

2 = Natural, Winding, minimal vegetation/shallow grass

t_c (min) **104.3**

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.50	0.61	0.71	0.82	0.92	1.02
Site Runoff (cfs)	2.07	10.02	21.93	41.77	56.40	73.34
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	10.0	-	-	-	73.3

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-A1 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	58779.0444	1.35	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	58,779	1.35	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{\max, \text{Overland}}$		300	ft		C_v	7	
	L (ft)	ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	80	5	-	-	-	-	
Initial Time	50	4	0.080	-	6.6	N/A	DCM Eq. 6-8
Shallow Channel	30	1	0.033	1.3	0.4	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	0
					t_c	6.9 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.73	4.68	5.45	6.23	7.01	7.85
Runoff (cfs)	0.1	0.5	1.1	2.1	2.8	3.7
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.1	0.5	1.1	2.1	2.8	3.7

$$\text{DCM: } I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-A1)

Includes Basins OS-1 PR-A1

Job No.: **61224** Date: **12/6/2024 13:36**
Project: **168 Training Facility** Calcs by: **SLB**
Checked by: _____
Jurisdiction **DCM** Soil Type **A**
Runoff Coefficient **Surface Type** Urbanization **Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	1,190,612	27.33	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,190,612	27.33	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-1	-	1,755	32	-	-	-	-	54.8
Channelized-1	Trap Ditch	2	81	4	24	40	13	2.0	0.7
Channelized-2									
Channelized-3									
Total			1,836	36					
2 = Natural, Winding, minimal vegetation/shallow grass									
									t_c (min) 55.5

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.26	1.56	1.82	2.08	2.34	2.62
Site Runoff (cfs)	0.69	3.41	7.46	14.21	19.18	25.02
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	3.4	-	-	-	25.0

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-A2 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Gravel	21892.7062	0.50	0.57	0.59	0.63	0.66	0.68	0.7	80%
Pasture/Meadow	778,034	17.86	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved	2,145	0.05	0.89	0.9	0.92	0.94	0.95	0.96	100%
Combined	802,072	18.41	0.04	0.10	0.17	0.26	0.31	0.36	2.5%

802071.4796

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns			
	L _{max, Overland}	300	ft		C _v	7
	L (ft)	ΔZ ₀ (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)
Total	1,269	52	-	-	-	-
Initial Time	300	16	0.053	-	18.1	N/A DCM Eq. 6-8
Shallow Channel	464	22	0.047	1.5	5.1	- DCM Eq. 6-9
Channelized	505	14	0.028	1.5	5.8	- V-Ditch
				t _c	28.9 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.03	2.54	2.96	3.38	3.80	4.26
Runoff (cfs)	1.4	4.5	9.0	16.4	21.9	28.3
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.4	4.5	9.0	16.4	21.9	28.3

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-A2)

Includes Basins OS-1 PR-A1 PR-A2

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	1,968,646	45.19	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	-	0.00	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	21,893	0.50	0.57	0.59	0.63	0.66	0.68	0.7	80%
Paved	2,145	0.05	0.89	0.9	0.92	0.94	0.95	0.96	100%
Combined	1,992,684	45.75	0.03	0.09	0.16	0.26	0.30	0.35	1.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-1	-	1,755	32	-	-	-	-	54.8
Channelized-1	Trap Ditch	2	81	4	24	40	13	2.0	0.7
Channelized-2	Trap Ditch	2	1,236	40	28	40	15	1.8	11.2
Channelized-3									
Total			3,072	76					
		2 = Natural, Winding, minimal vegetation/shallow grass						t_c	66.7
		2 = Natural, Winding, minimal vegetation/shallow grass						(min)	

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.04	1.28	1.50	1.71	1.93	2.15
Site Runoff (cfs)	1.28	5.08	10.69	19.98	26.85	34.89
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	5.1	-	-	-	34.9

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-B Runoff Calculations (DP B)

Job No.:61224

Date:12/6/2024 13:36

Project:168 Training Facility

Calcs by:SLB

JurisdictionDCM

Soil TypeA

Runoff CoefficientSurface Type

UrbanizationNon-Urban

Checked by:

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	9480	0.22	0.71	0.73	0.75	0.78	0.8	0.81	90%
Lawns	255,352	5.86	0.02	0.08	0.15	0.25	0.30	0.35	0%
Gravel	105,176	2.41	0.57	0.59	0.63	0.66	0.68	0.7	80%
Landscaping	263,540	6.05	0.03	0.09	0.17	0.26	0.31	0.36	2%
Pasture/Meadow	1,108,981	25.46	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,742,529	40.00	0.06	0.12	0.19	0.28	0.33	0.38	5.6%

1742529.011

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
L _{max,Overland}		300	ft	C _v		7	
L (ft)		ΔZ ₀ (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)	
Total	1,521	74	-	-	-	-	
Initial Time	300	12	0.040	-	19.5	N/A	DCM Eq. 6-8
Shallow Channel	1,221	62	0.051	1.6	12.9	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	0
				t _c	32.4 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.90	2.37	2.76	3.16	3.55	3.97
Runoff (cfs)	4.4	11.0	20.5	35.2	46.5	59.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	4.4	11.0	20.5	35.2	46.5	59.6

DCM: I = C1 * ln (tc) + C2

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Sub-Basin PR-C1 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction: **DCM**
Runoff Coefficient: **Surface Type**

Checked by: _____

Soil Type: **A**
Urbanization: **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Landscaping	138248.5587	3.17	0.03	0.09	0.17	0.26	0.31	0.36	2%
Pasture/Meadow	57,549	1.32	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	195,798	4.49	0.03	0.09	0.16	0.26	0.31	0.36	1.4%

195797.7016

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns				
	$L_{\max, \text{Overland}}$	300 ft			C_v	7	
	L (ft)	ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	2,096	86	-	-	-	-	
Initial Time	300	10	0.033	-	21.3	N/A	DCM Eq. 6-8
Shallow Channel	1,374	60	0.044	1.5	15.7	-	DCM Eq. 6-9
Channelized	422	16	0.038	4.8	1.5	-	V-Ditch
					t_c	38.4 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.69	2.11	2.46	2.81	3.17	3.54
Runoff (cfs)	0.2	0.8	1.8	3.3	4.4	5.7
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.2	0.8	1.8	3.3	4.4	5.7

DCM: $I = C1 * \ln(tc) + C2$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-C1)

Includes Basins OS-2 PR-C1

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	4,897,173	112.42	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	138,249	3.17	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	5,035,422	115.60	0.02	0.08	0.15	0.25	0.30	0.35	0.1%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-2	-	4,135	113	-	-	-	-	80.1
Channelized-1	V-Ditch	2	614	16	6	0	3	2.8	3.6
Channelized-2									
Channelized-3									
Total			4,749	129					
2 = Natural, Winding, minimal vegetation/shallow grass									
									t_c (min) 83.7

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

Q_{Minor} (cfs) - 5-year Storm

Q_{Major} (cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.77	0.94	1.10	1.26	1.41	1.58
Site Runoff (cfs)	1.80	8.74	19.12	36.32	49.03	63.86
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	8.7	-	-	-	63.9

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-C2 Runoff Calculations

Job No.: **61224**

Date: **12/6/2024 13:36**

Project: **168 Training Facility**

Calcs by: **SLB**

Jurisdiction **DCM**
Runoff Coefficient **Surface Type**

Checked by: _____

Soil Type **A**
Urbanization **Non-Urban**

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	2528	0.06	0.71	0.73	0.75	0.78	0.8	0.81	90%
Gravel	34,318	0.79	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	103,855	2.38	0.02	0.08	0.15	0.25	0.30	0.35	0%
Landscaping	88,163	2.02	0.03	0.09	0.17	0.26	0.31	0.36	2%
Pasture/Meadow	385,119	8.84	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	613,983	14.10	0.06	0.11	0.18	0.28	0.32	0.37	5.1%

613983.1099

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns				
	$L_{\max, \text{Overland}}$	300 ft			C_v	7	
	L (ft)	ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,716	84	-	-	-	-	
Initial Time	300	36	0.120	-	13.6	N/A	DCM Eq. 6-8
Shallow Channel	1,229	38	0.031	1.2	16.6	-	DCM Eq. 6-9
Channelized	187	10	0.053	3.8	0.8	-	V-Ditch
				t_c	31.1 min.		

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.95	2.43	2.83	3.24	3.64	4.08
Runoff (cfs)	1.5	3.9	7.3	12.6	16.7	21.4
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.5	3.9	7.3	12.6	16.7	21.4

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-C2)

Includes Basins OS-2 PR-C1 PR-C2

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	5,282,292	121.26	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	2,528	0.06	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	226,412	5.20	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	34,318	0.79	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	103,855	2.38	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	5,649,405	129.69	0.02	0.08	0.15	0.25	0.30	0.35	0.6%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-2	-	4,135	113	-	-	-	-	80.1
Channelized-1	V-Ditch	2	614	16	6	0	3	2.8	3.6
Channelized-2	Trap Ditch	2	822	34	21	40	13	1.8	7.6
Channelized-3									
Total			5,571	163					
		2 = Natural, Winding, minimal vegetation/shallow grass						t_c	91.4
		2 = Natural, Winding, minimal vegetation/shallow grass						(min)	

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.66	0.81	0.95	1.08	1.22	1.36
Site Runoff (cfs)	2.07	8.81	18.89	35.49	47.79	62.09
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	8.8	-	-	-	62.1

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-D1 Runoff Calculations

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Non-Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	3258	0.07	0.02	0.08	0.15	0.25	0.3	0.35	0%
Landscaping	106,417	2.44	0.03	0.09	0.17	0.26	0.31	0.36	2%
Combined	109,675	2.52	0.03	0.09	0.17	0.26	0.31	0.36	1.9%

109674.7669

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns			
	L _{max, Overland}	300	ft		C _v	7
	L (ft)	ΔZ ₀ (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)
Total	1,502	49	-	-	-	-
Initial Time	300	3	0.010	-	31.6	N/A DCM Eq. 6-8
Shallow Channel	1,030	39	0.038	1.4	12.6	- DCM Eq. 6-9
Channelized	172	7	0.041	1.5	1.9	- V-Ditch
				t _c	46.1 min.	

Storage Volume

		40 -hr release time		Detention is NOT required			
EURV	0.00 (in)	a = 1		Water Quality is NOT required			
WQCV	0.00 (in)						
i (return period)	5-year	10-year	100-year	Design Volume (ft³)			
K _i (ft)	0.0000	0.0000	0	% Storage	100-year	WQCV	Total
V _i (acre-ft)	0.000	0.000	-0.01295	EURV	0%	0	0
V _i (ft³)	0	0	-564	WQCV	0%	0	0

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.48	1.84	2.14	2.45	2.76	3.08
Runoff (cfs)	0.1	0.4	0.9	1.6	2.1	2.8
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.1	0.4	0.9	1.6	2.1	2.8

DCM: $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-D1)

Includes Basins OS-3 PR-D1

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	743,964	17.08	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	106,417	2.44	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	-	0.00	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	850,381	19.52	0.02	0.08	0.15	0.25	0.30	0.35	0.3%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-3	-	1,512	75	-	-	-	-	31.7
Channelized-1	V-Ditch	2	172	7	3	0	3	2.8	1.0
Channelized-2									
Channelized-3									
Total			1,684	82					
2 = Natural, Winding, minimal vegetation/shallow grass									
									t_c (min) 32.7

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.88	2.35	2.74	3.13	3.53	3.94
Site Runoff (cfs)	0.78	3.73	8.16	15.37	20.73	27.04
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	3.7	-	-	-	27.0

DCM: $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-D2 Runoff Calculations

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Non-Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Landscaping	151064	3.47	0.03	0.09	0.17	0.26	0.31	0.36	2%
Roofs	2,528	0.06	0.71	0.73	0.75	0.78	0.8	0.81	90%
Gravel	24,308	0.56	0.57	0.59	0.63	0.66	0.68	0.7	80%
Pasture/Meadow	1,604,773	36.84	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,782,673	40.92	0.03	0.09	0.16	0.26	0.31	0.36	1.4%

1782672.76

Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{max, Overland}$		300	ft		C_v	7	
L (ft)		ΔZ_0 (ft)	S_0 (ft/ft)	v (ft/s)	t (min)	t_{Alt} (min)	
Total	1,856	80	-	-	-	-	
	300	20	0.067	-	16.9	N/A	DCM Eq. 6-8
Shallow Channel	1,289	52	0.040	1.4	15.3	-	DCM Eq. 6-9
Channelized	267	8	0.030	3.2	1.4	-	V-Ditch
				t_c	33.6 min.		

Storage Volume

		40 -hr release time		Detention is NOT required			
EURV	0.00 (in)	a = 1		Water Quality is NOT required			
WQCV	0.00 (in)						
i (return period)	5-year	10-year	100-year	Design Volume (ft ³)			
K _i (ft)	0.0000	0.0000	0	% Storage	100-year	WQCV	Total
V _i (acre-ft)	0.000	0.000	-0.2669	EURV	0%	0	0
V _i (ft ³)	0	0	-11,626	WQCV	0%	0	0

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.85	2.31	2.70	3.08	3.47	3.88
Runoff (cfs)	2.2	8.4	17.6	32.5	43.5	56.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	2.2	8.4	17.6	32.5	43.5	56.6

DCM: $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Combined Sub-Basin Runoff Calculations (DP-D2)

Includes Basins OS-5 OS-4 PR-D1 PR-D2

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Pasture/Meadow	8,970,969	205.95	0.02	0.08	0.15	0.25	0.3	0.35	0%
Roofs	2,528	0.06	0.71	0.73	0.75	0.78	0.8	0.81	90%
Landscaping	257,481	5.91	0.03	0.09	0.17	0.26	0.31	0.36	2%
Gravel	24,308	0.56	0.57	0.59	0.63	0.66	0.68	0.7	80%
Lawns	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	9,255,286	212.47	0.02	0.08	0.15	0.25	0.30	0.35	0.3%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q_i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-4	-	5,348	175	-	-	-	-	92.4
Channelized-1	V-Ditch	2	172	7	3	0	3	2.8	1.0
Channelized-2	Trap Ditch	2	1,656	75	21	40	13	2.8	1.0
Channelized-3								1.8	15.1
Total			7,176	257					
								t_c (min)	109.5

2 = Natural, Winding, minimal vegetation/shallow grass

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
Q_{Minor}	(cfs) - 5-year Storm
Q_{Major}	(cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	0.45	0.54	0.63	0.72	0.81	0.90
Site Runoff (cfs)	2.08	9.36	20.30	38.40	51.77	67.22
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	9.4	-	-	-	67.2

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin PR-E Runoff Calculations (DP-E)

Job No.:	61224	Date:	12/6/2024 13:36
Project:	168 Training Facility	Calcs by:	SLB
Jurisdiction	DCM	Checked by:	
Runoff Coefficient	Surface Type	Soil Type	A
		Urbanization	Non-Urban

Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Landscaping	169217	3.88	0.03	0.09	0.17	0.26	0.31	0.36	2%
Roofs	2,528	0.06	0.71	0.73	0.75	0.78	0.8	0.81	90%
Gravel	68,041	1.56	0.57	0.59	0.63	0.66	0.68	0.7	80%
Pasture/Meadow	1,356,978	31.15	0.02	0.08	0.15	0.25	0.3	0.35	0%
Combined	1,596,764	36.66	0.05	0.10	0.17	0.27	0.32	0.37	3.8%

1596764.322

Basin Travel Time

Shallow Channel Ground Cover			Short Pasture/Lawns			
	L _{max, Overland}	300	ft		C _v	7
	L (ft)	ΔZ ₀ (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)
Total	1,595	70	-	-	-	-
Initial Time	300	22	0.073	-	16.1	N/A DCM Eq. 6-8
Shallow Channel	1,295	48	0.037	1.3	16.0	- DCM Eq. 6-9
Channelized			0.000	0.0	0.0	- 0
				t _c	32.2 min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	1.90	2.38	2.77	3.17	3.57	3.99
Runoff (cfs)	3.2	9.0	17.6	31.3	41.6	53.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	3.2	9.0	17.6	31.3	41.6	53.6

DCM: $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

3 Hydraulic Calculations

Swale Calculations
Culvert Calculations
Conditions at Site Outfall Locations Calculations

Channel Report

Channel C1 (North) - 5yr = 8.7 cfs

Triangular

Side Slopes (z:1) = 3.00, 12.00
Total Depth (ft) = 3.00

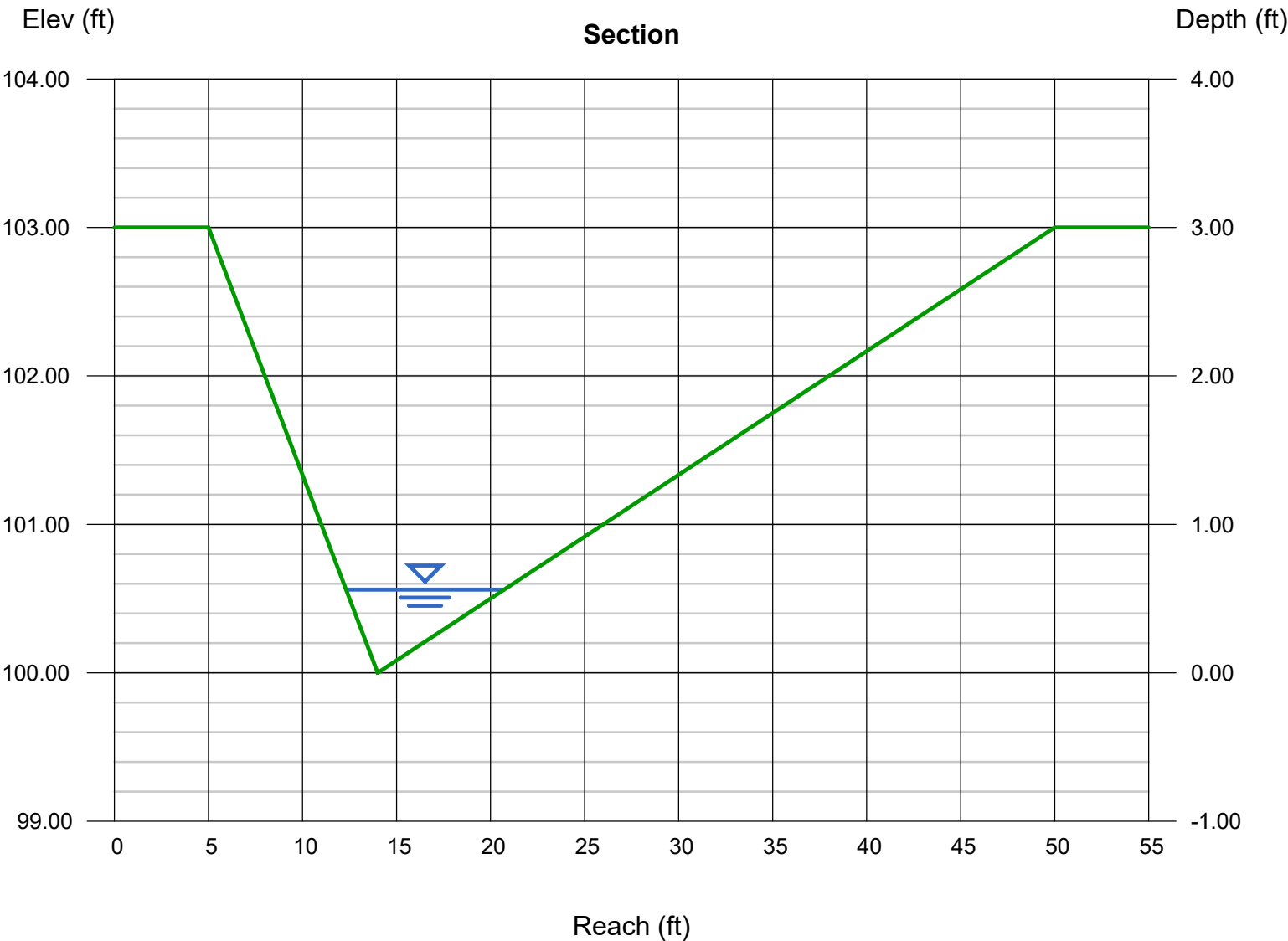
Invert Elev (ft) = 100.00
Slope (%) = 4.00
N-Value = 0.034

Calculations

Compute by: Known Q
Known Q (cfs) = 8.70

Highlighted

Depth (ft) = 0.56
Q (cfs) = 8.700
Area (sqft) = 2.35
Velocity (ft/s) = 3.70
Wetted Perim (ft) = 8.51
Crit Depth, Yc (ft) = 0.61
Top Width (ft) = 8.40
EGL (ft) = 0.77



Channel Report

Channel C1 (North) - 100yr = 63.9 cfs

Triangular

Side Slopes (z:1) = 3.00, 12.00
Total Depth (ft) = 3.00

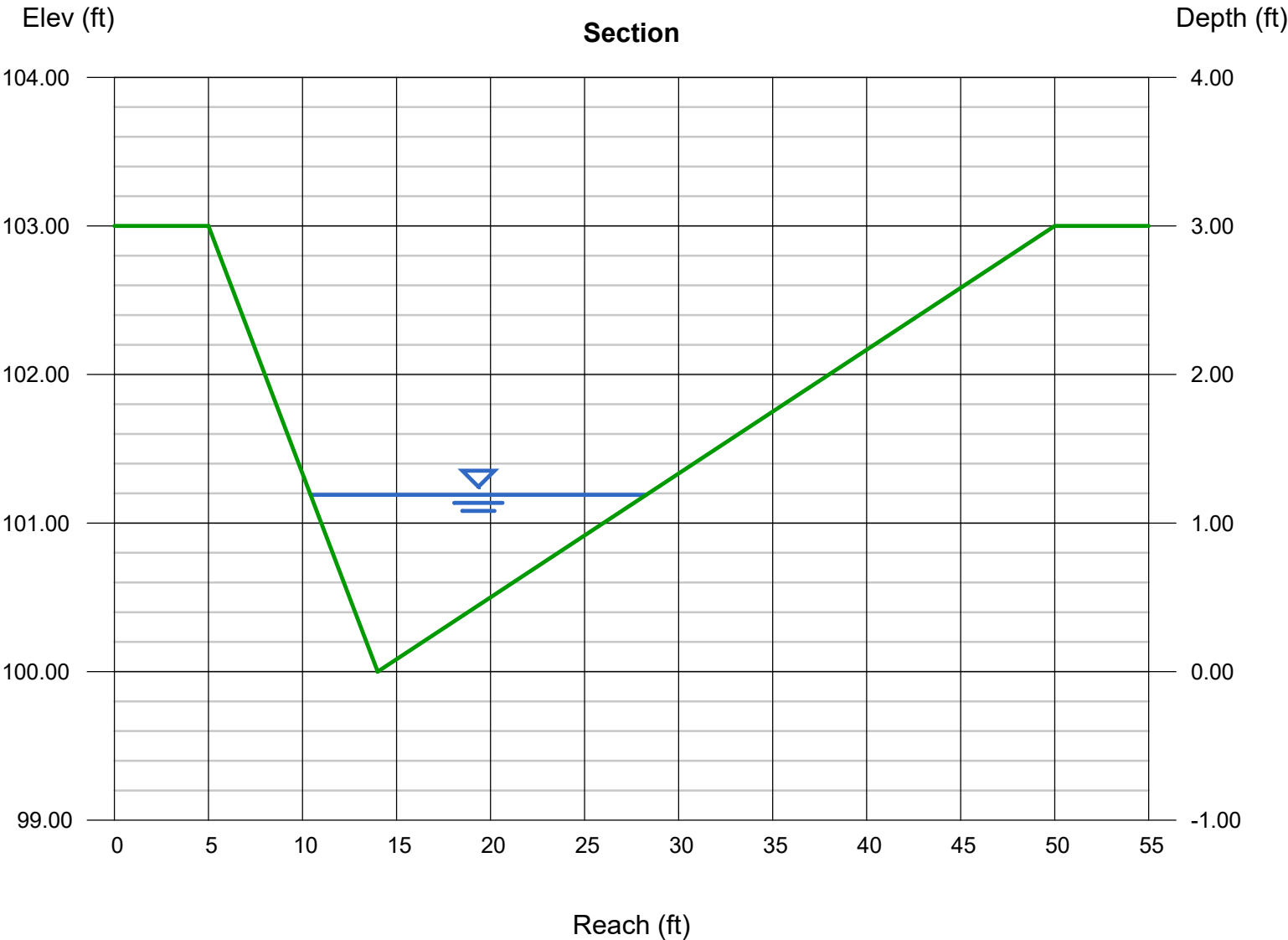
Invert Elev (ft) = 100.00
Slope (%) = 4.00
N-Value = 0.034

Calculations

Compute by: Known Q
Known Q (cfs) = 63.90

Highlighted

Depth (ft) = 1.19
Q (cfs) = 63.90
Area (sqft) = 10.62
Velocity (ft/s) = 6.02
Wetted Perim (ft) = 18.09
Crit Depth, Yc (ft) = 1.36
Top Width (ft) = 17.85
EGL (ft) = 1.75



Channel Report

Channel C1 (Central) - 5yr = 8.7 cfs

Trapezoidal

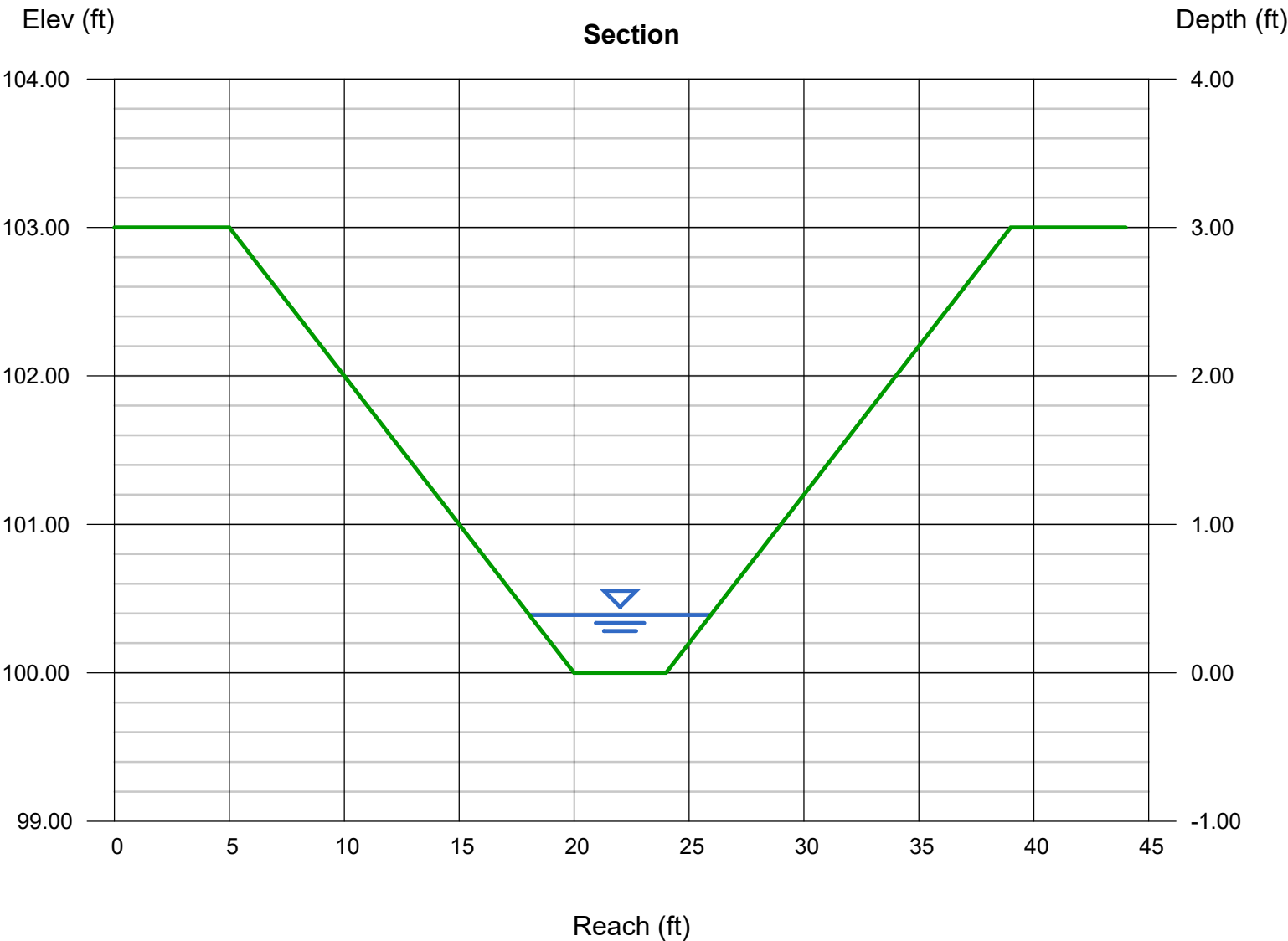
Bottom Width (ft)	= 4.00
Side Slopes (z:1)	= 5.00, 5.00
Total Depth (ft)	= 3.00
Invert Elev (ft)	= 100.00
Slope (%)	= 4.00
N-Value	= 0.034

Highlighted

Depth (ft)	= 0.39
Q (cfs)	= 8.700
Area (sqft)	= 2.32
Velocity (ft/s)	= 3.75
Wetted Perim (ft)	= 7.98
Crit Depth, Yc (ft)	= 0.44
Top Width (ft)	= 7.90
EGL (ft)	= 0.61

Calculations

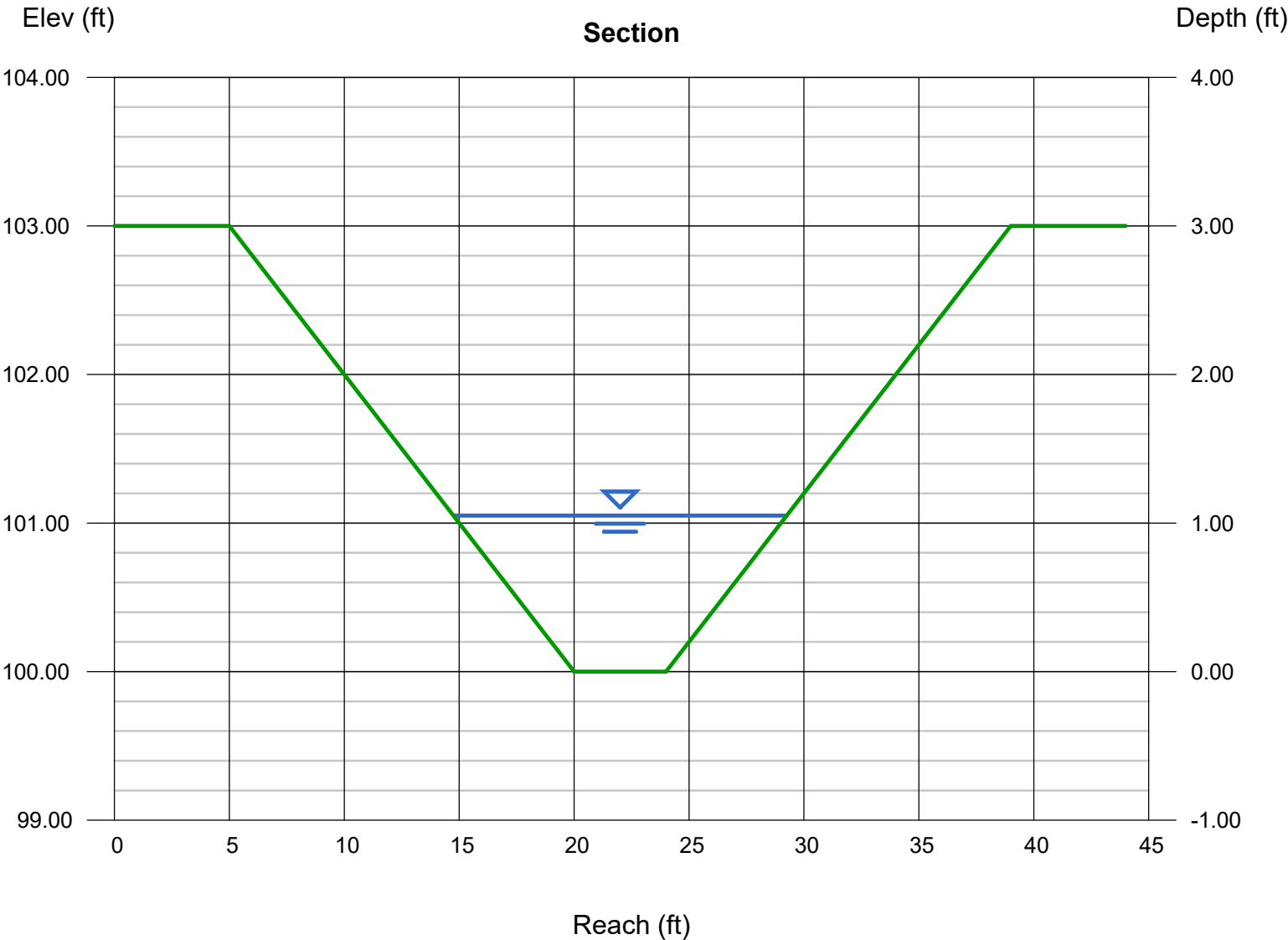
Compute by:	Known Q
Known Q (cfs)	= 8.70



Channel Report

Channel C1 (Central) - 100yr = 63.9 cfs

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.00	Depth (ft)	= 1.05
Side Slopes (z:1)	= 5.00, 5.00	Q (cfs)	= 63.90
Total Depth (ft)	= 3.00	Area (sqft)	= 9.71
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 6.58
Slope (%)	= 4.00	Wetted Perim (ft)	= 14.71
N-Value	= 0.034	Crit Depth, Yc (ft)	= 1.25
Calculations		Top Width (ft)	= 14.50
Compute by:	Known Q	EGL (ft)	= 1.72
Known Q (cfs)	= 63.90		



Channel Report

Channel D1 (North) - 5yr = 3.7 cfs

Triangular

Side Slopes (z:1) = 3.00, 4.00
Total Depth (ft) = 3.00

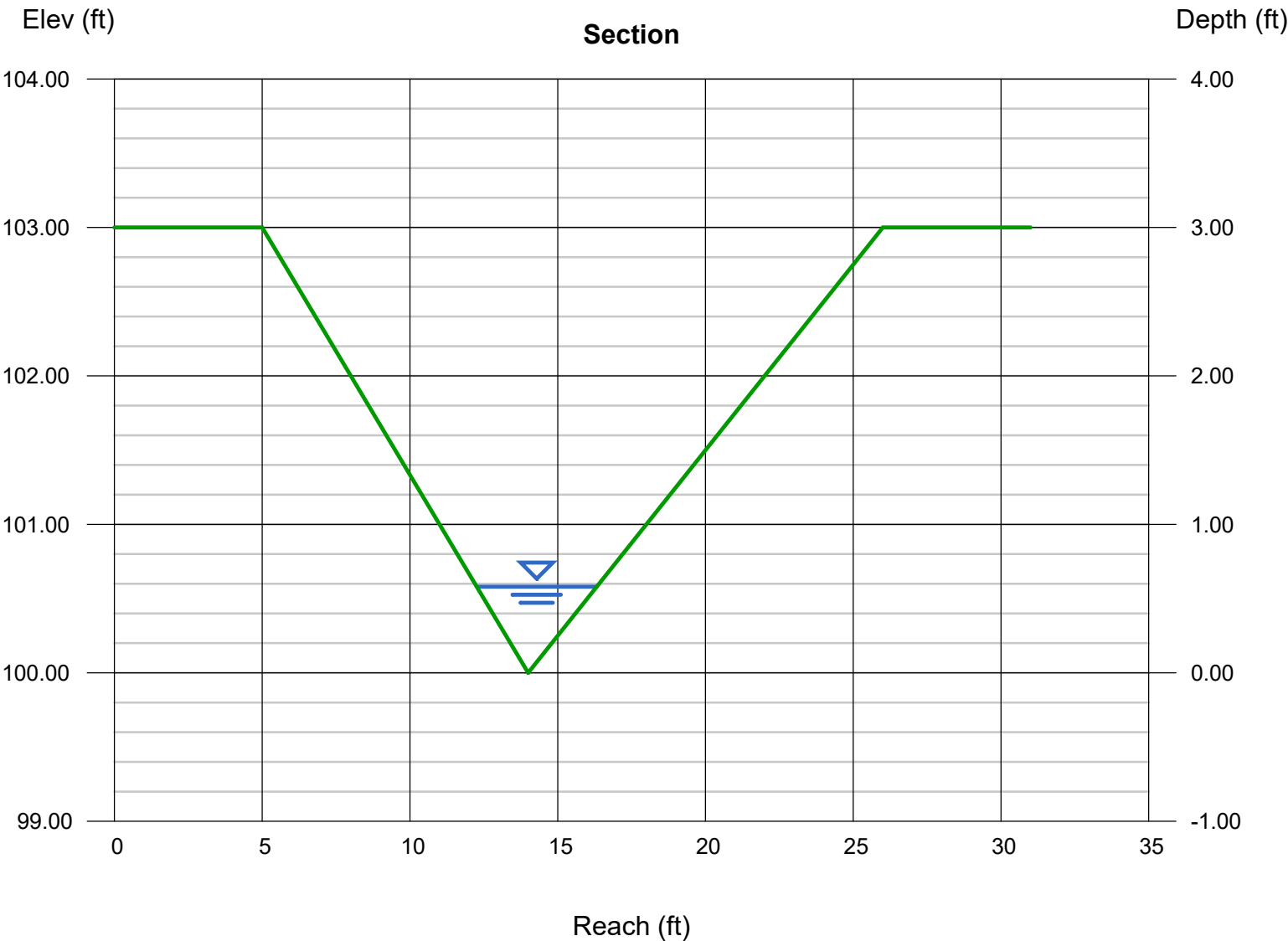
Invert Elev (ft) = 100.00
Slope (%) = 3.00
N-Value = 0.034

Calculations

Compute by: Known Q
Known Q (cfs) = 3.70

Highlighted

Depth (ft) = 0.58
Q (cfs) = 3.700
Area (sqft) = 1.18
Velocity (ft/s) = 3.14
Wetted Perim (ft) = 4.23
Crit Depth, Yc (ft) = 0.59
Top Width (ft) = 4.06
EGL (ft) = 0.73



Channel Report

Channel D1 (North) - 100yr = 27.0 cfs

Triangular

Side Slopes (z:1) = 3.00, 4.00
Total Depth (ft) = 3.00

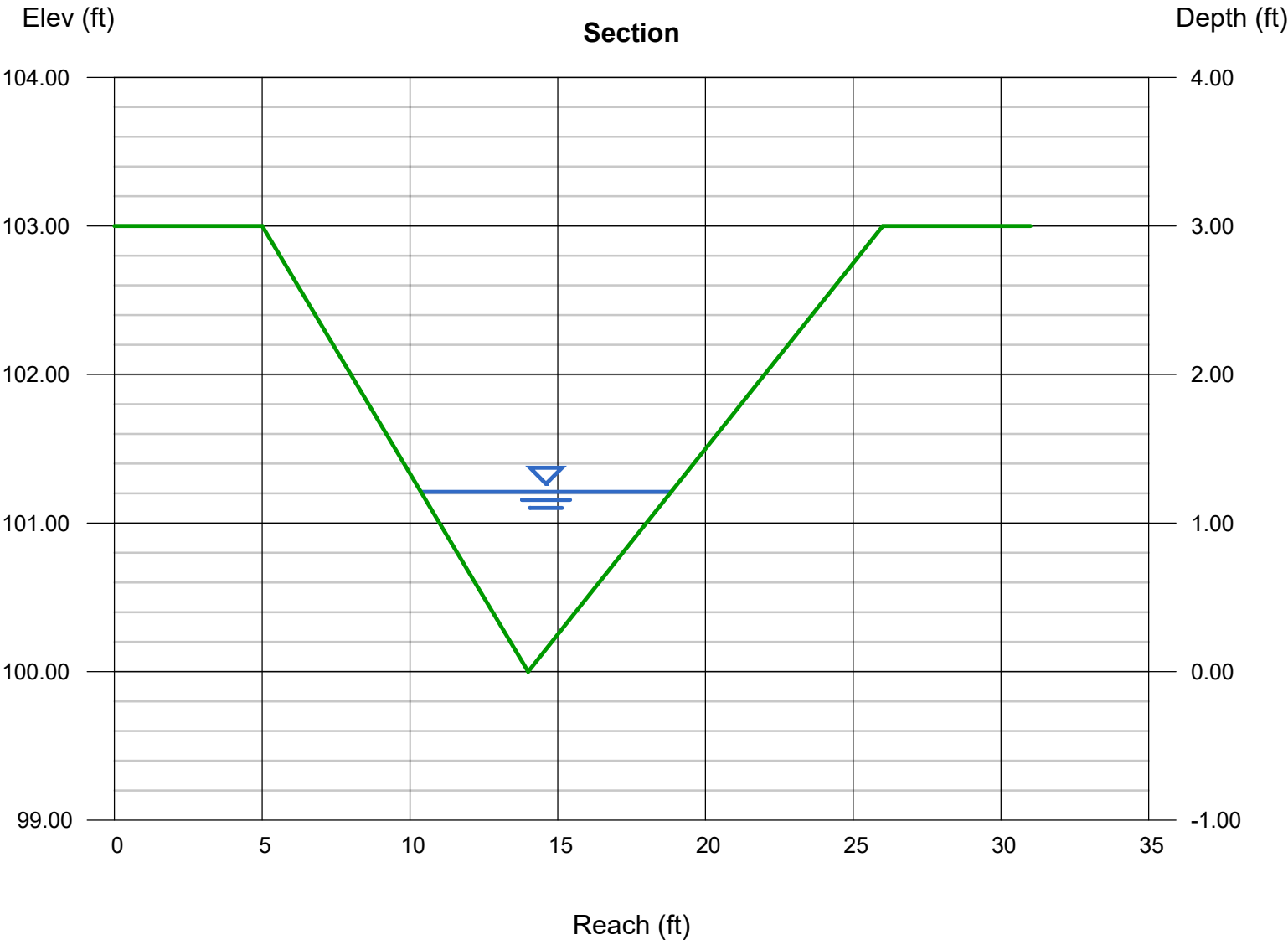
Invert Elev (ft) = 100.00
Slope (%) = 3.00
N-Value = 0.034

Calculations

Compute by: Known Q
Known Q (cfs) = 27.00

Highlighted

Depth (ft) = 1.21
Q (cfs) = 27.00
Area (sqft) = 5.12
Velocity (ft/s) = 5.27
Wetted Perim (ft) = 8.82
Crit Depth, Yc (ft) = 1.30
Top Width (ft) = 8.47
EGL (ft) = 1.64



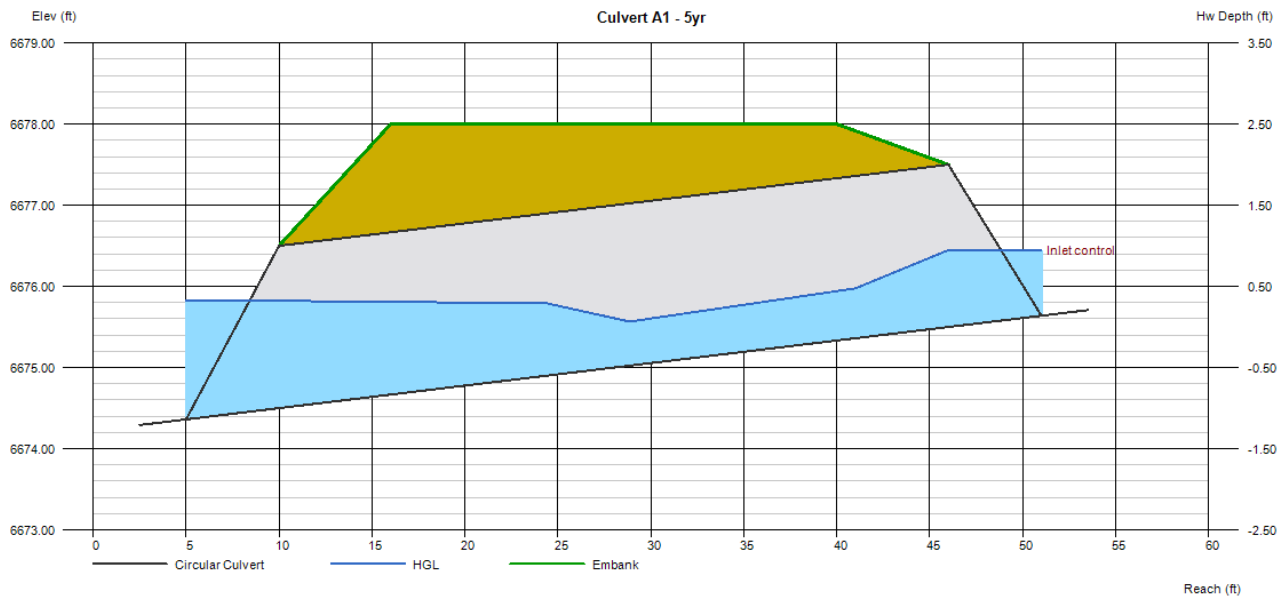
Culvert Report

Culvert A1 - 5yr

Invert Elev Dn (ft)	= 6674.50
Pipe Length (ft)	= 36.00
Slope (%)	= 2.78
Invert Elev Up (ft)	= 6675.50
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.023
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Mitered to slope (C)
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7

Embankment	
Top Elevation (ft)	= 6678.00
Top Width (ft)	= 24.00
Crest Width (ft)	= 100.00

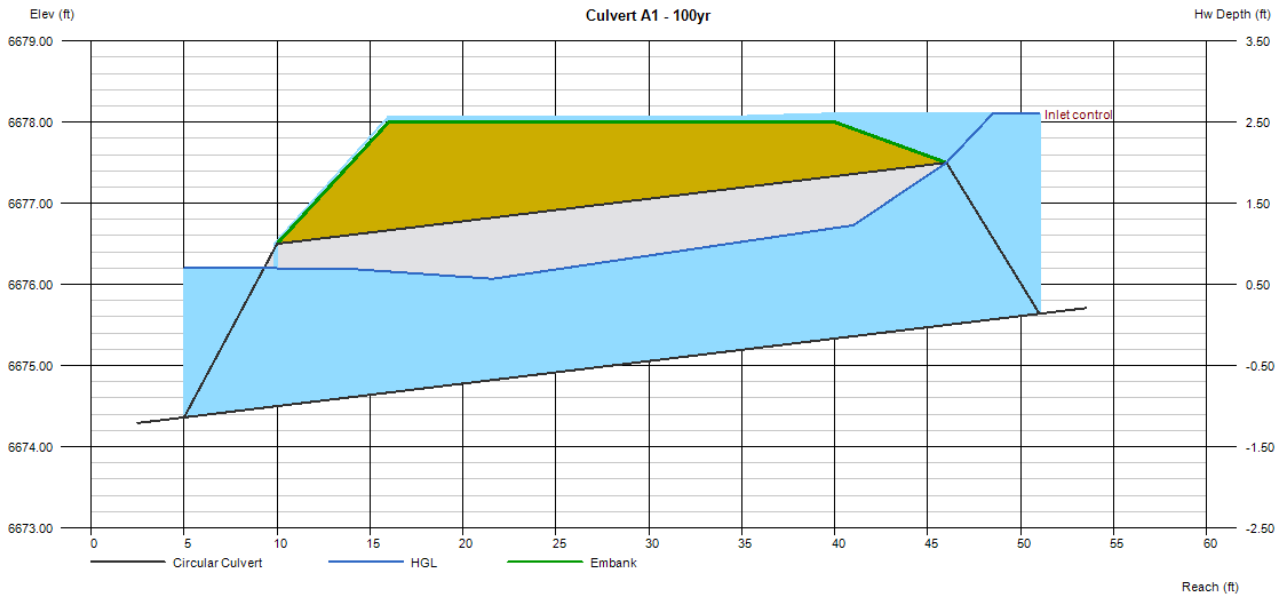
Calculations	
Qmin (cfs)	= 3.40
Qmax (cfs)	= 3.40
Tailwater Elev (ft)	= (dc+D)/2
Highlighted	
Qtotal (cfs)	= 3.40
Qpipe (cfs)	= 3.40
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 1.54
Veloc Up (ft/s)	= 3.89
HGL Dn (ft)	= 6675.82
HGL Up (ft)	= 6676.14
Hw Elev (ft)	= 6676.45
Hw/D (ft)	= 0.47
Flow Regime	= Inlet Control



Culvert Report

Culvert A1 - 100yr

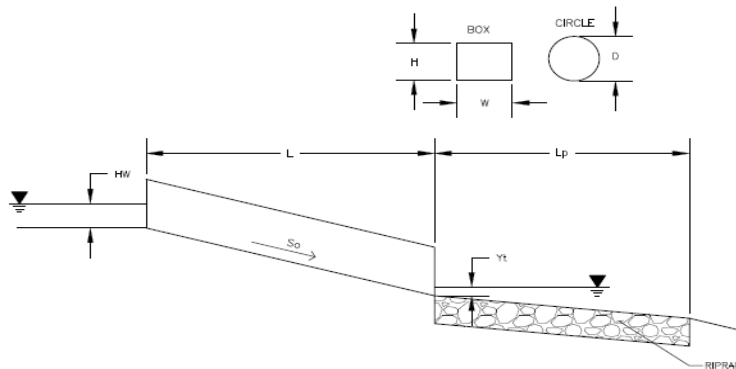
Invert Elev Dn (ft)	= 6674.50	Calculations	
Pipe Length (ft)	= 36.00	Qmin (cfs)	= 25.00
Slope (%)	= 2.78	Qmax (cfs)	= 25.00
Invert Elev Up (ft)	= 6675.50	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 25.00
No. Barrels	= 1	Qpipe (cfs)	= 15.08
n-Value	= 0.023	Qovertop (cfs)	= 9.92
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 5.30
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 6.43
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 6676.20
		HGL Up (ft)	= 6676.90
		Hw Elev (ft)	= 6678.11
		Hw/D (ft)	= 1.30
		Flow Regime	= Inlet Control
Embankment			
Top Elevation (ft)	= 6678.00		
Top Width (ft)	= 24.00		
Crest Width (ft)	= 100.00		



Determination of Culvert Headwater and Outlet Protection

Project: **61224 - I68 Ranges**

Basin ID: **Culvert A1 - 100yr**



Soil Type:

Choose One:

☒ Sandy

☐ Non-Sandy

Design Information (Input):

Design Discharge

Q = 25 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 24 inches

Inlet Edge Type (Choose from pull-down list)

1.5 : 1 Beveled Edge

OR

Box Culvert:

Barrel Height (Rise) in Feet

Height (Rise) =

Barrel Width (Span) in Feet

Width (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

No = 1

Inlet Elevation

Elev IN = 6675.5 ft

Outlet Elevation **OR** Slope

Elev OUT = 6674.5 ft

Culvert Length

L = 36 ft

Manning's Roughness

n = 0.023

Bend Loss Coefficient

k_b = 0

Exit Loss Coefficient

k_x = 1

Tailwater Surface Elevation

Elev Y_t =

Max Allowable Channel Velocity

V = 5 ft/s

Required Protection (Output):

Tailwater Surface Height

Y_t = 0.80 ft

Flow Area at Max Channel Velocity

A_t = 5.00 ft²

Culvert Cross Sectional Area Available

A = 3.14 ft²

Entrance Loss Coefficient

k_e = 0.20

Friction Loss Coefficient

k_f = 1.39

Sum of All Losses Coefficients

k_s = 2.59

Culvert Normal Depth

Y_n = 1.41 ft

Culvert Critical Depth

Y_c = 1.76 ft

Tailwater Depth for Design

d = 1.88 ft

Adjusted Diameter **OR** Adjusted Rise

D_a = - ft

Expansion Factor

1/(2*tan(Θ)) = 3.04

Flow/Diameter^{2.5} **OR** Flow/(Span * Rise^{1.5})

Q/D^{2.5} = 4.42 ft^{0.5}/s

Froude Number

Fr = -

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

Y_t/D = 0.40

Pressure flow!

Inlet Control Headwater

HW_i = 3.20 ft

Outlet Control Headwater

HW_o = 3.43 ft

Design Headwater Elevation

HW = 6,678.93 ft

Headwater/Diameter **OR Headwater/Rise Ratio**

HW/D = 1.71 **HW/D > 1.5!**

Minimum Theoretical Riprap Size

d₅₀ = 7 in

Nominal Riprap Size

d₅₀ = 9 in

UDFCD Riprap Type

Type = L

Length of Protection

L_p = 13 ft

Width of Protection

T = 7 ft

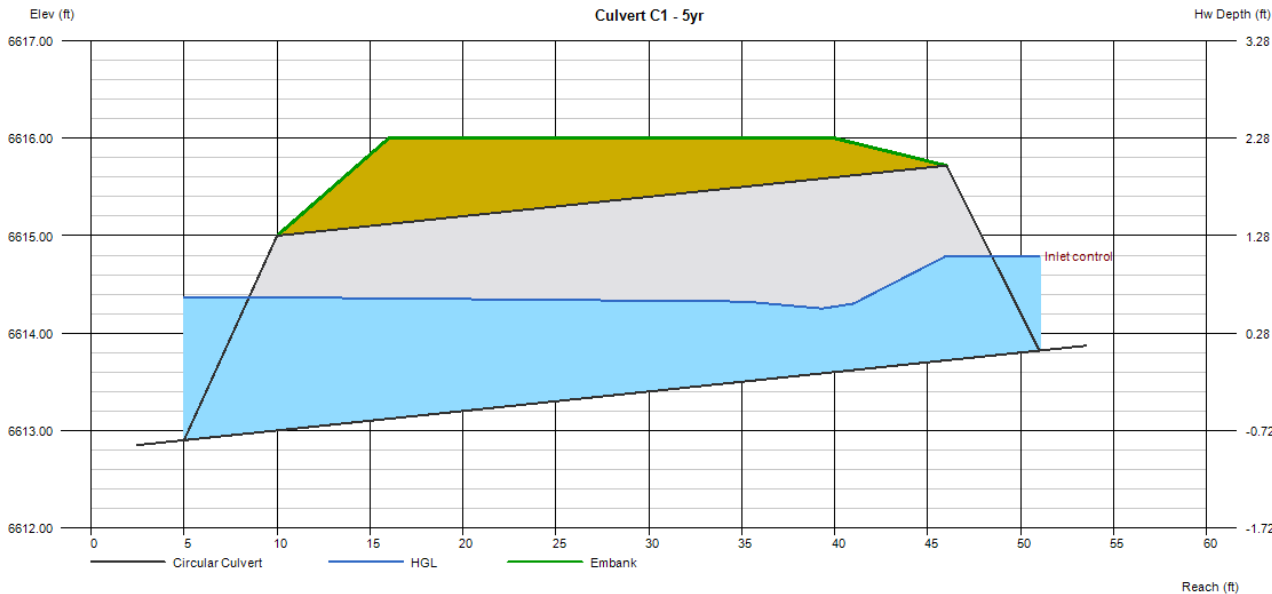
Culvert Report

Culvert C1 - 5yr

Invert Elev Dn (ft)	= 6613.00
Pipe Length (ft)	= 36.00
Slope (%)	= 2.00
Invert Elev Up (ft)	= 6613.72
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 2
n-Value	= 0.023
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Mitered to slope (C)
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7

Embankment	
Top Elevation (ft)	= 6616.00
Top Width (ft)	= 24.00
Crest Width (ft)	= 100.00

Calculations	
Qmin (cfs)	= 8.70
Qmax (cfs)	= 8.70
Tailwater Elev (ft)	= (dc+D)/2
Highlighted	
Qtotal (cfs)	= 8.70
Qpipe (cfs)	= 8.70
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 1.90
Veloc Up (ft/s)	= 4.18
HGL Dn (ft)	= 6614.37
HGL Up (ft)	= 6614.45
Hw Elev (ft)	= 6614.79
Hw/D (ft)	= 0.54
Flow Regime	= Inlet Control



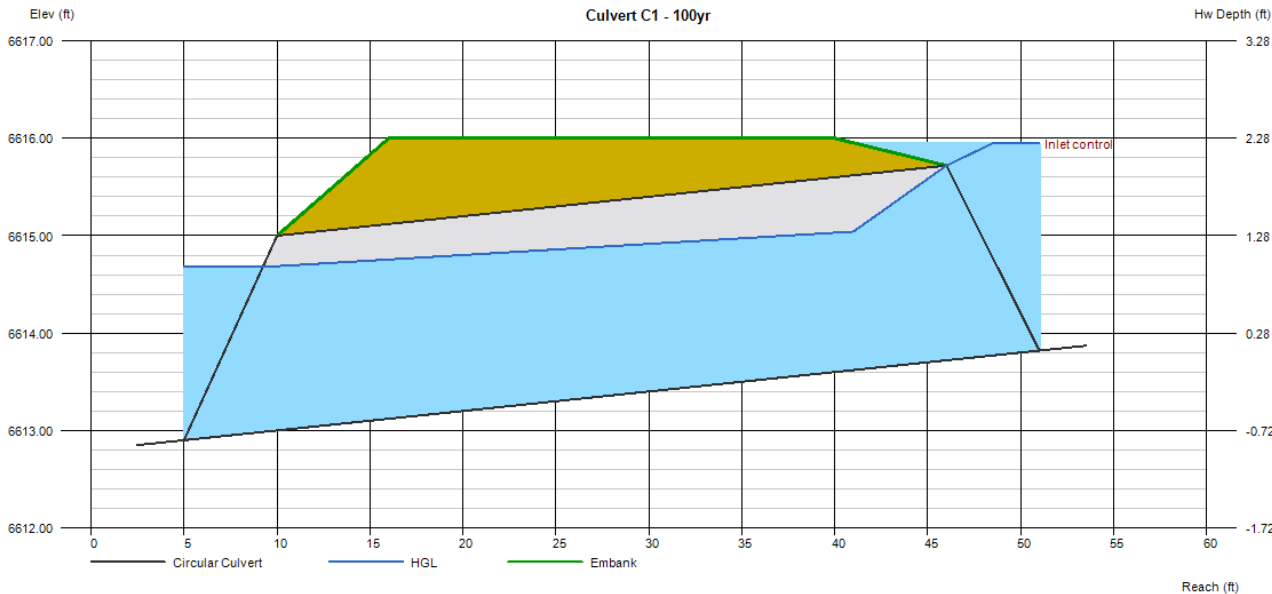
Culvert Report

Culvert C1 - 100yr

Invert Elev Dn (ft)	=	6613.00
Pipe Length (ft)	=	36.00
Slope (%)	=	2.00
Invert Elev Up (ft)	=	6613.72
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	2
n-Value	=	0.023
Culvert Type	=	Circular Corrugate Metal Pipe
Culvert Entrance	=	Mitered to slope (C)
Coeff. K,M,c,Y,k	=	0.021, 1.33, 0.0463, 0.75, 0.7

Embankment	
Top Elevation (ft)	= 6616.00
Top Width (ft)	= 24.00
Crest Width (ft)	= 100.00

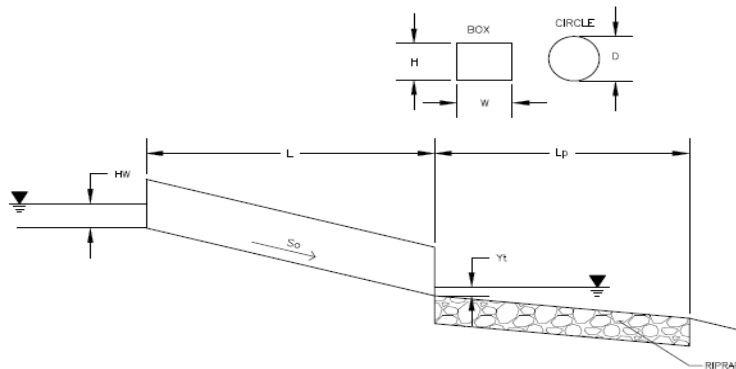
Calculations	
Qmin (cfs)	= 63.90
Qmax (cfs)	= 63.90
Tailwater Elev (ft)	= (dc+D)/2
Highlighted	
Qtotal (cfs)	= 63.90
Qpipe (cfs)	= 29.15
Qovertop (cfs)	= 34.75
Veloc Dn (ft/s)	= 5.15
Veloc Up (ft/s)	= 6.31
HGL Dn (ft)	= 6614.69
HGL Up (ft)	= 6615.10
Hw Elev (ft)	= 6615.95
Hw/D (ft)	= 1.11
Flow Regime	= Inlet Control



Determination of Culvert Headwater and Outlet Protection

Project: **61224 - I68 Ranges**

Basin ID: **Culvert C1 - 100yr**



Soil Type:

Choose One:

☒ Sandy

☐ Non-Sandy

Design Information (Input):

Design Discharge

Q = 63.9 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 24 inches

Inlet Edge Type (Choose from pull-down list)

1.1 : 1 Beveled Edge

OR

Box Culvert:

Barrel Height (Rise) in Feet

Height (Rise) =

Barrel Width (Span) in Feet

Width (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

No = 2

Inlet Elevation

Elev IN = 6613.72 ft

Outlet Elevation **OR** Slope

Elev OUT = 6613 ft

Culvert Length

L = 36 ft

Manning's Roughness

n = 0.023

Bend Loss Coefficient

k_b = 0

Exit Loss Coefficient

k_x = 1

Tailwater Surface Elevation

Elev Y_t =

Max Allowable Channel Velocity

V = 5 ft/s

Required Protection (Output):

Tailwater Surface Height

Y_t = 0.80 ft

Flow Area at Max Channel Velocity

A_t = 6.39 ft²

Culvert Cross Sectional Area Available

A = 3.14 ft²

Entrance Loss Coefficient

k_e = 0.20

Friction Loss Coefficient

k_f = 1.39

Sum of All Losses Coefficients

k_s = 2.59

Culvert Normal Depth

Y_n = 0.69 ft

Culvert Critical Depth

Y_c = 1.89 ft

Tailwater Depth for Design

d = 1.94 ft

Adjusted Diameter **OR** Adjusted Rise

D_a = - ft

Expansion Factor

1/(2*tan(Θ)) = 2.04

Flow/Diameter^{2.5} **OR** Flow/(Span * Rise^{1.5})

Q/D^{2.5} = 5.65 ft^{0.5}/s

Froude Number

Fr = -

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

Y_t/D = 0.40

Pressure flow!

Inlet Control Headwater

HW_i = 4.96 ft

Outlet Control Headwater

HW_o = 5.39 ft

Design Headwater Elevation

HW = 6.619.11 ft

Headwater/Diameter **OR Headwater/Rise Ratio**

HW/D = 2.69 **HW/D > 1.5!**

Minimum Theoretical Riprap Size

d₅₀ = 9 in

Nominal Riprap Size

d₅₀ = 12 in

UDFCD Riprap Type

Type = M

Length of Protection

L_p = 13 ft

Width of Protection

T = 9 ft

Channel Report

Design Point A2 - 100yr = 34.9cfs

Trapezoidal

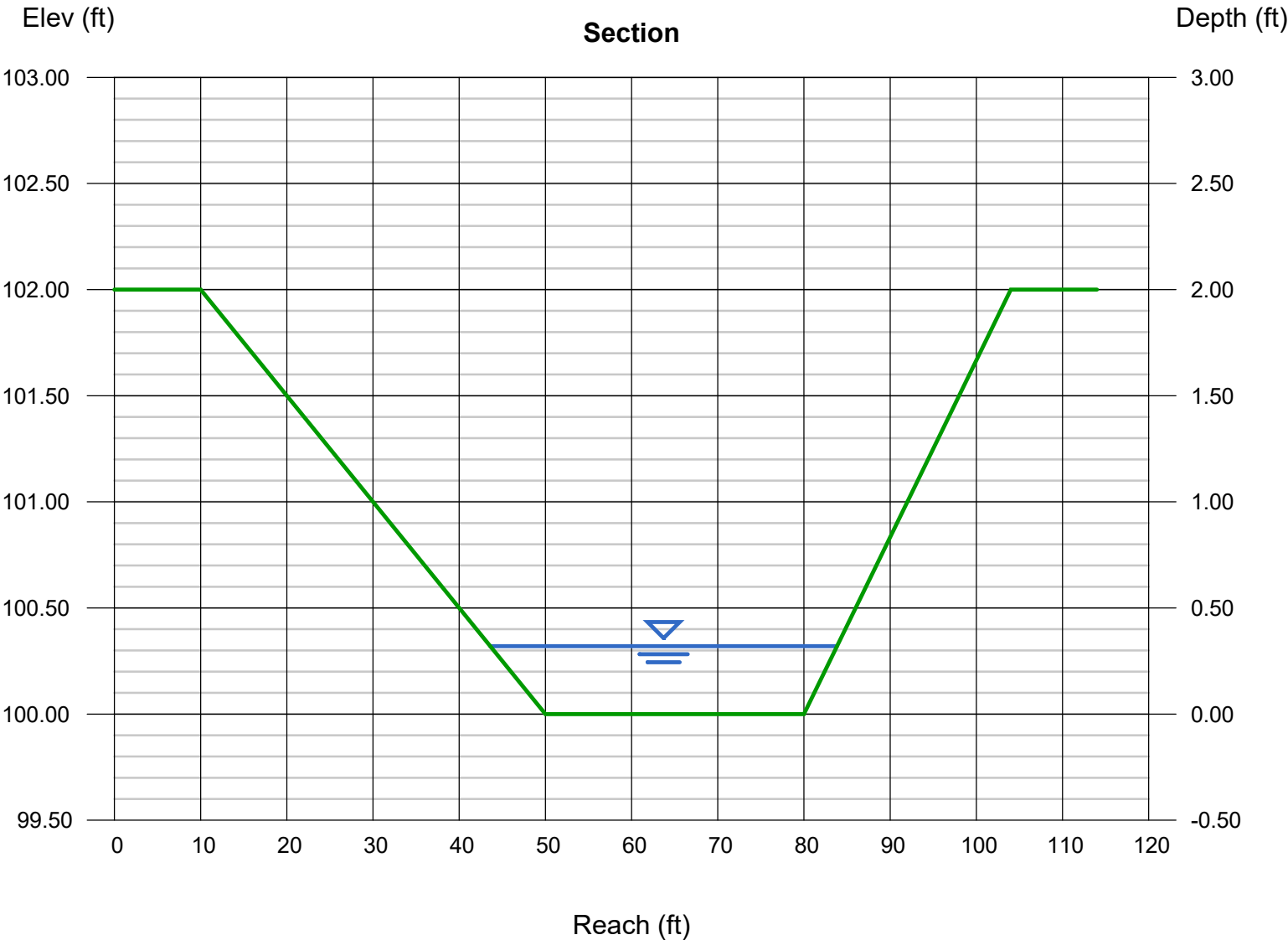
Bottom Width (ft)	= 30.00
Side Slopes (z:1)	= 20.00, 12.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 100.00
Slope (%)	= 3.00
N-Value	= 0.034

Highlighted

Depth (ft)	= 0.32
Q (cfs)	= 34.90
Area (sqft)	= 11.24
Velocity (ft/s)	= 3.11
Wetted Perim (ft)	= 40.26
Crit Depth, Yc (ft)	= 0.33
Top Width (ft)	= 40.24
EGL (ft)	= 0.47

Calculations

Compute by:	Known Q
Known Q (cfs)	= 34.90



Channel Report

Design Point C2 - 100yr = 62.1cfs

Trapezoidal

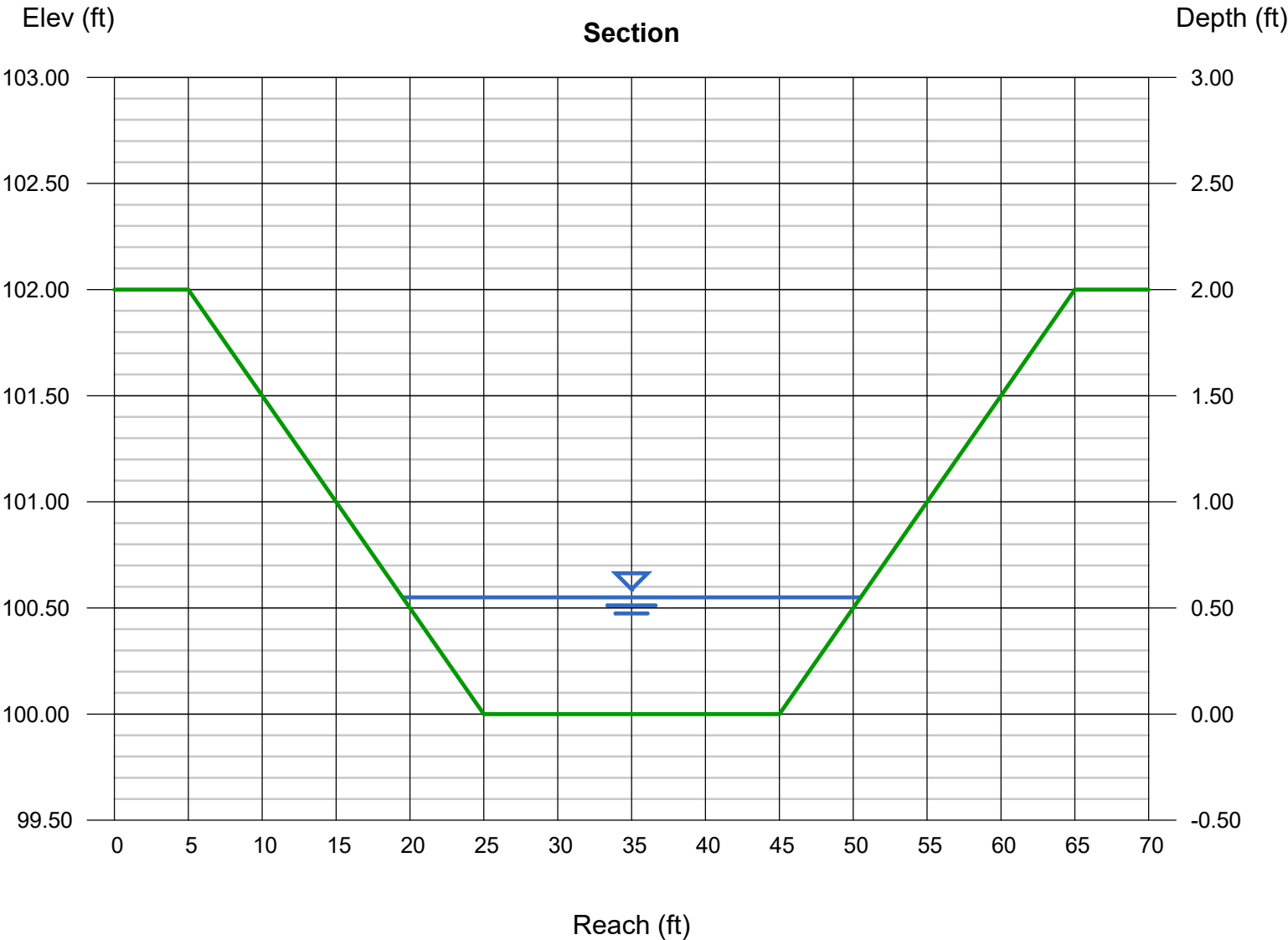
Bottom Width (ft)	= 20.00
Side Slopes (z:1)	= 10.00, 10.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 100.00
Slope (%)	= 3.00
N-Value	= 0.034

Highlighted

Depth (ft)	= 0.55
Q (cfs)	= 62.10
Area (sqft)	= 14.02
Velocity (ft/s)	= 4.43
Wetted Perim (ft)	= 31.05
Crit Depth, Yc (ft)	= 0.61
Top Width (ft)	= 31.00
EGL (ft)	= 0.85

Calculations

Compute by:	Known Q
Known Q (cfs)	= 62.10



Channel Report

Design Point D2 - 100yr = 67.2cfs

Trapezoidal

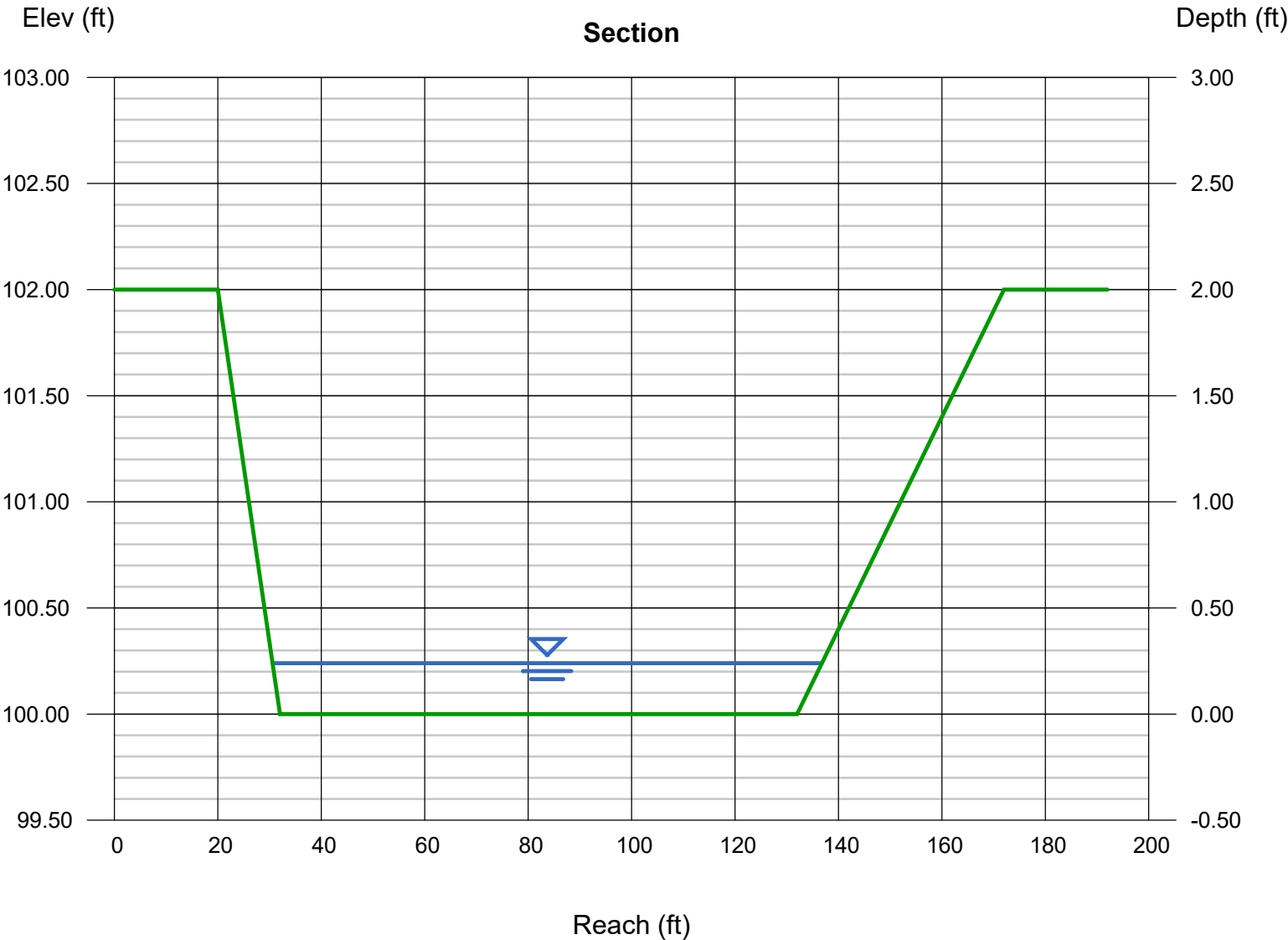
Bottom Width (ft)	= 100.00
Side Slopes (z:1)	= 6.00, 20.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 100.00
Slope (%)	= 3.00
N-Value	= 0.034

Highlighted

Depth (ft)	= 0.24
Q (cfs)	= 67.20
Area (sqft)	= 24.75
Velocity (ft/s)	= 2.72
Wetted Perim (ft)	= 106.27
Crit Depth, Yc (ft)	= 0.24
Top Width (ft)	= 106.24
EGL (ft)	= 0.35

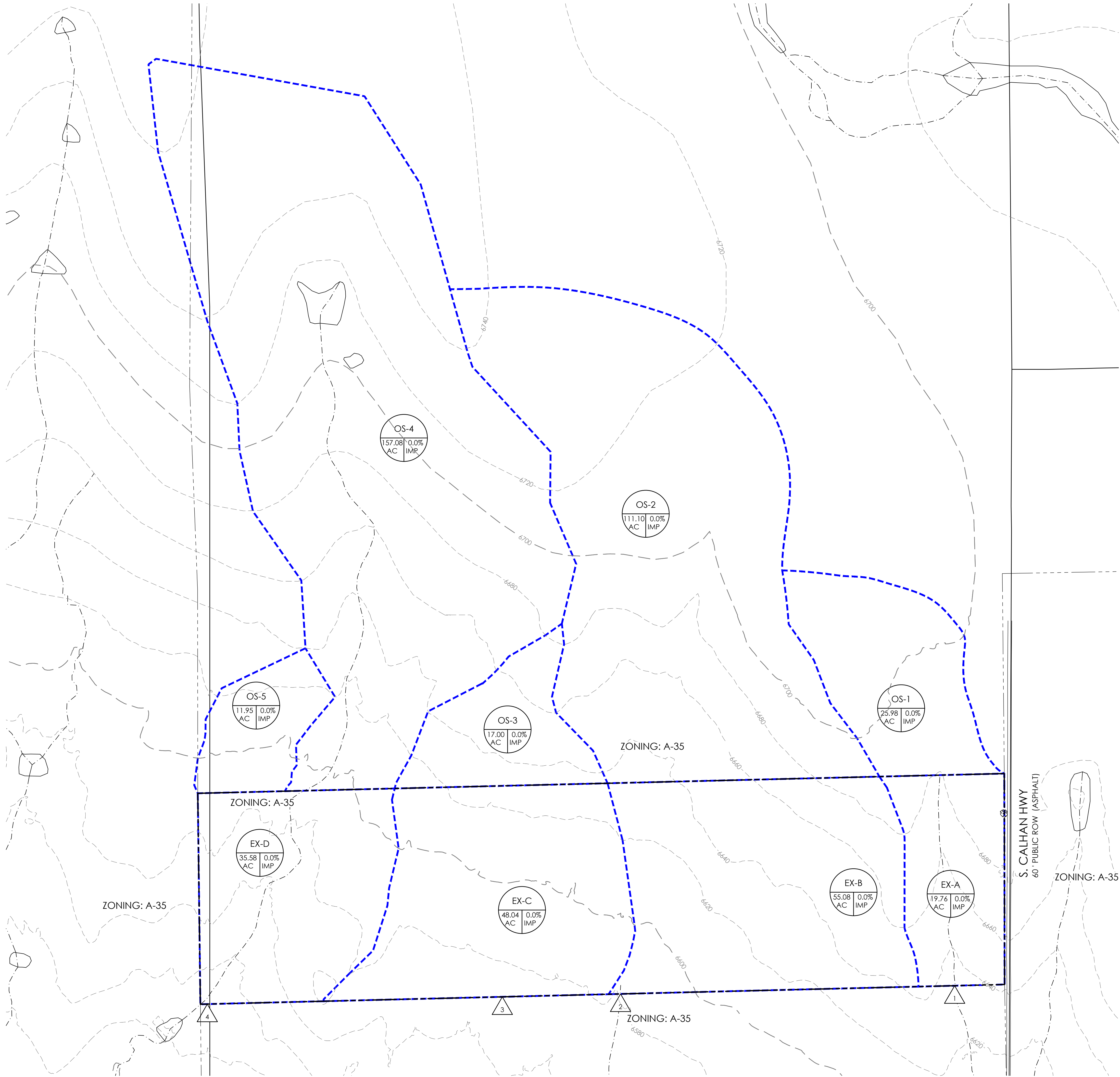
Calculations

Compute by:	Known Q
Known Q (cfs)	= 67.20



4 Report Maps

Existing Drainage Map (Map Pocket)
Proposed Drainage Map (Map Pocket)



LEGEND

— PROPERTY LINE
- - - EASEMENT LINE
— LOT LINE

EXISTING

— 5985 INDEX CONTOUR
— 84 INTERMEDIATE CONTOUR

PROPOSED

— 5985 INDEX CONTOUR
— 84 INTERMEDIATE CONTOUR

■ BASIN BOUNDARY

2 = 19.0 cfs
3 = 40.0 cfs
FLOW AMOUNTS

▲ SLOPE DIRECTION AND GRADE

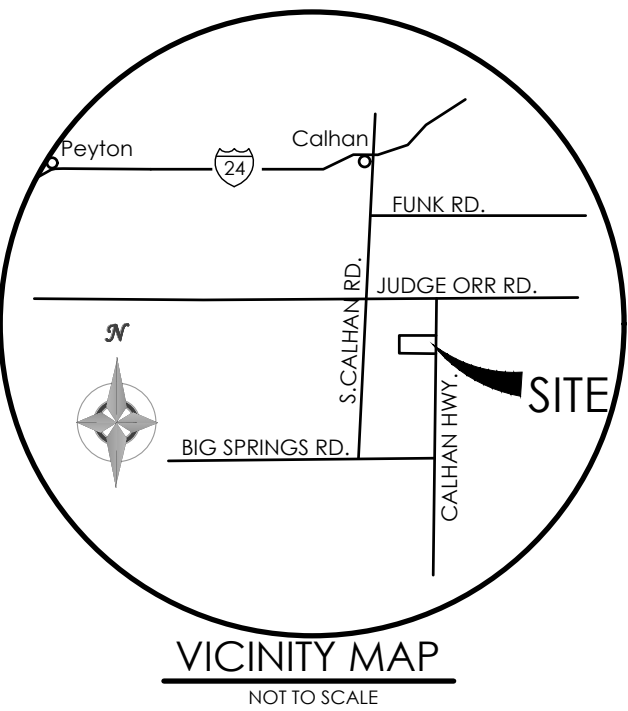
A1
1.0 AC 50% IMP
BASIN LABEL
AREA IN ACRES
PERCENT IMPERVIOUS

▲ DESIGN POINT

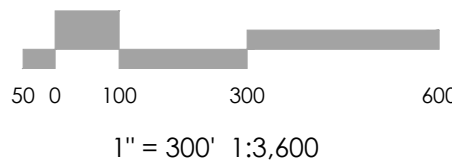
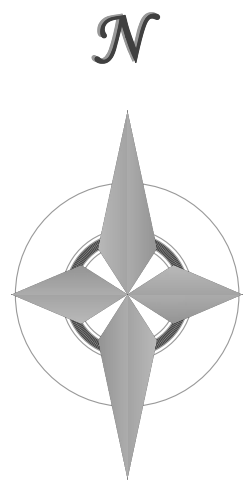
← TIME OF CONCENTRATION

→ FLOW DIRECTION

EXISTING DRAINAGE SUMMARY TABLE						
DESIGN POINTS	INCLUDED BASINS	AREA (AC)	Tc (MIN.)	RUNOFF		METHOD
				Q5 (CFS)	Q100 (CFS)	
	OS-1	25.98	54.8	3.3	24.1	RATIONAL
	OS-2	111.10	80.1	9.0	65.6	RATIONAL
	OS-3	17.00	31.7	3.3	23.9	RATIONAL
	OS-4	157.08	92.4	10.0	73.0	RATIONAL
	OS-5	11.95	27.3	2.5	18.4	RATIONAL
	EX-A	19.76	31.2	3.8	28.1	RATIONAL
DP-1	OS-1, EX-A	45.75	66.1	4.7	34.8	RATIONAL
	EX-B	55.08	35.0	9.9	72.8	RATIONAL
DP-2	OS-2, EX-B	166.18	88.3	11.5	84.0	RATIONAL
	EX-C	48.04	31.9	9.2	67.5	RATIONAL
DP-3	OS-3, EX-C	65.05	40.4	10.6	77.8	RATIONAL
	EX-D	35.58	34.2	6.5	47.7	RATIONAL
DP-4	OS-4&5, EX-D	204.61	104.3	10.0	73.3	RATIONAL



BENCHMARK



MVE, INC.
ENGINEERS & SURVEYORS

1903 Idaray Street, Suite 200 Colorado Springs CO 80909 719.635.5736

REVISIONS

DESIGNED BY _____
DRAWN BY _____
CHECKED BY _____
AS-BUILT BY _____
CHECKED BY _____

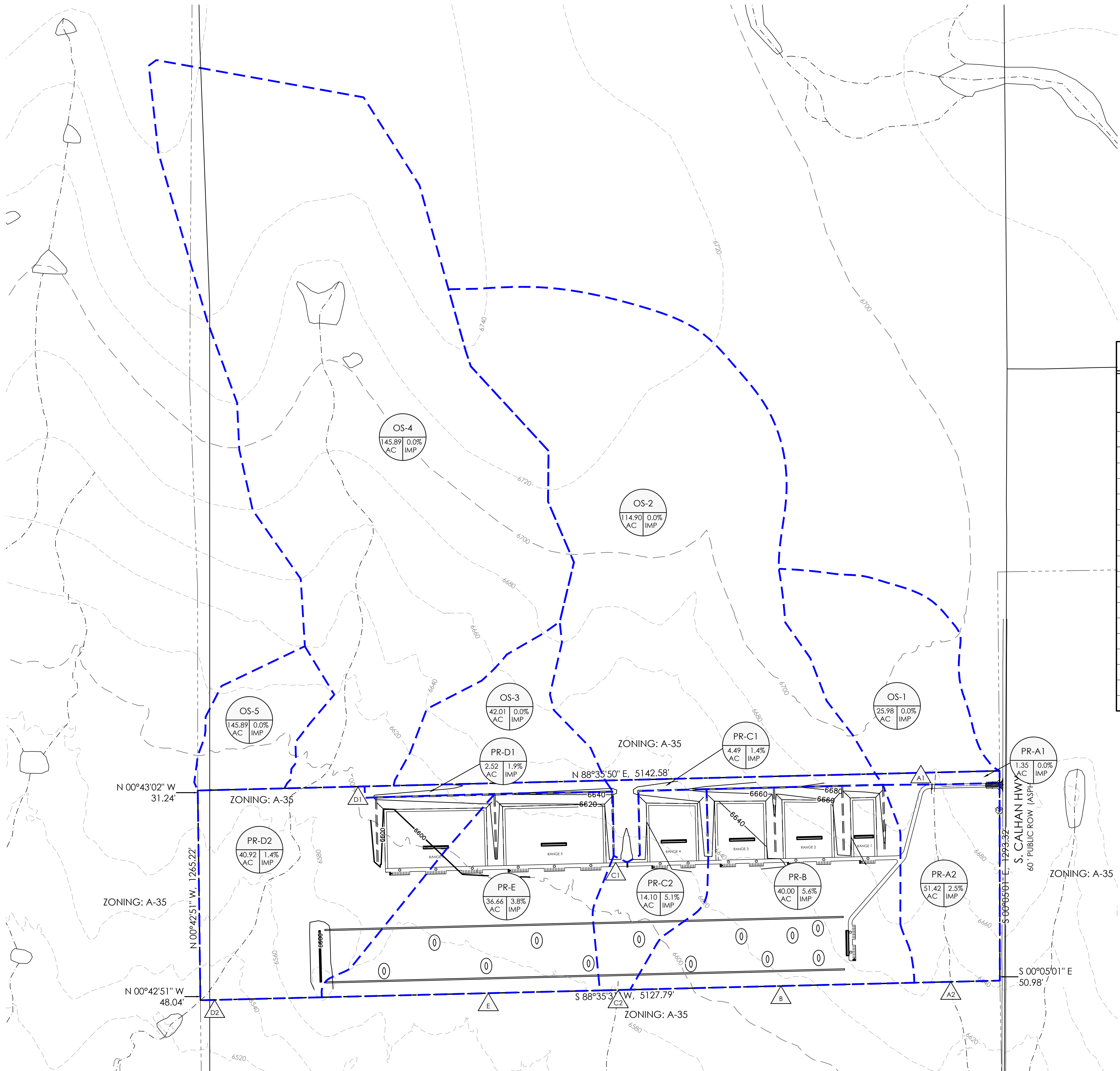
+158 Acre Parcel
168 Training Facility

DRAINAGE REPORT

EX OVERALL MAP

MVE PROJECT 61224
MVE DRAWING EXDRAIN MAP

DECEMBER 6, 2024
SHEET 1 OF 3



LEGEND

PROPERTY LINE
EASEMENT LINE
LOT LINE

EXISTING

INDEX CONTOUR
INTERMEDIATE CONTOUR

PROPOSED

INDEX CONTOUR
INTERMEDIATE CONTOUR

BASIN BOUNDARY

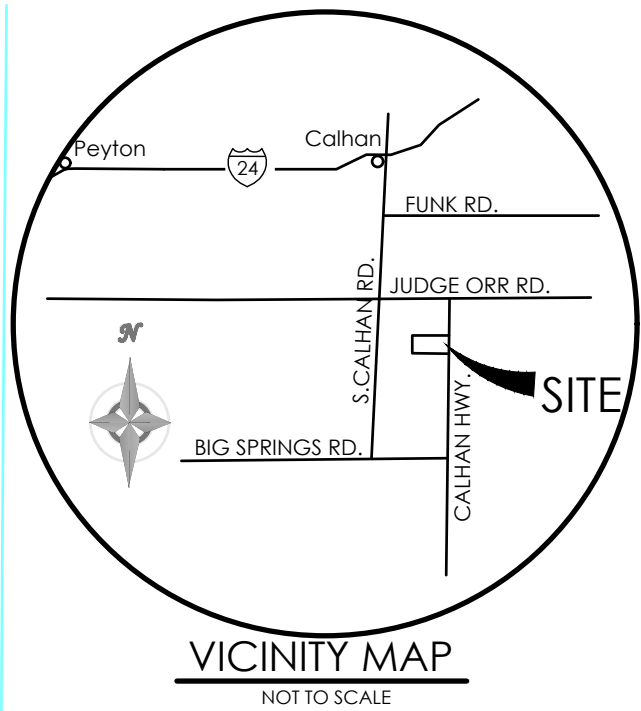
FLOW AMOUNTS
SLOPE DIRECTION AND GRADE

BASIN LABEL
AREA IN ACRES
PERCENT IMPERVIOUS

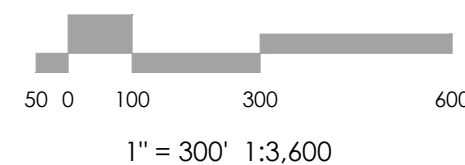
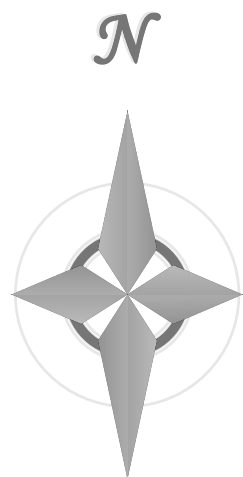
DESIGN POINT

TIME OF CONCENTRATION
FLOW DIRECTION

PROPOSED DRAINAGE SUMMARY TABLE						
DESIGN POINTS	INCLUDED BASINS	AREA (AC)	Tc (MIN.)	RUNOFF		METHOD
				Q5 (CFS)	Q100 (CFS)	
	OS-1	25.98	54.8	3.3	24.1	RATIONAL
	OS-2	111.10	80.1	9.0	65.6	RATIONAL
	OS-3	17.00	31.7	3.3	23.9	RATIONAL
	OS-4	157.08	92.4	10.0	73.0	RATIONAL
	OS-5	11.95	27.3	2.5	18.4	RATIONAL
	PR-A1	1.35	6.9	0.5	3.7	RATIONAL
DP-A1	OS-1, PR-A1	27.33	55.5	3.4	25.0	RATIONAL
	PR-A2	18.41	28.9	4.5	28.3	RATIONAL
DP-A2	OS-1, PR-A1&2	45.75	66.7	5.1	34.9	RATIONAL
DP-B	PR-B	40.00	32.4	11.0	59.6	RATIONAL
	PR-C1	4.49	38.4	0.8	5.7	RATIONAL
DP-C1	OS-2, PR-C1	115.60	83.7	8.7	63.9	RATIONAL
	PR-C2	14.10	31.1	3.9	21.4	RATIONAL
DP-C2	OS-2, PR-C1&2	129.69	91.4	8.8	62.1	RATIONAL
	PR-D1	2.52	46.1	0.4	2.8	RATIONAL
DP-D1	OS-3, PR-D1	19.52	32.7	3.7	27.0	RATIONAL
	PR-D2	40.92	33.6	8.4	56.6	RATIONAL
DP-D2	OS-4&5, D1&2	212.47	109.5	9.4	67.2	RATIONAL
DP-E	PR-E	36.66	32.2	9.0	53.6	RATIONAL



BENCHMARK



MVE, INC.
ENGINEERS & SURVEYORS

1903 Idelay Street, Suite 200 Colorado Springs CO 80909 719.635.5736

REVISIONS

DESIGNED BY _____
DRAWN BY _____
CHECKED BY _____
AS-BUILT BY _____
CHECKED BY _____

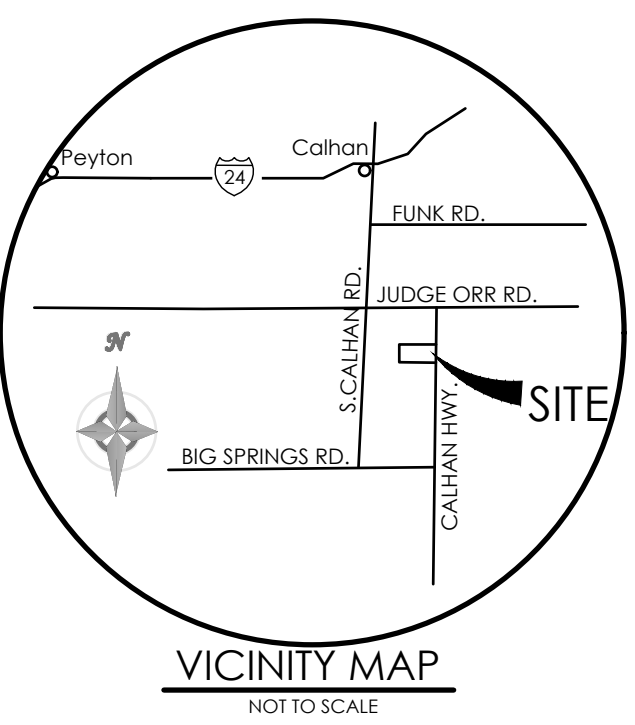
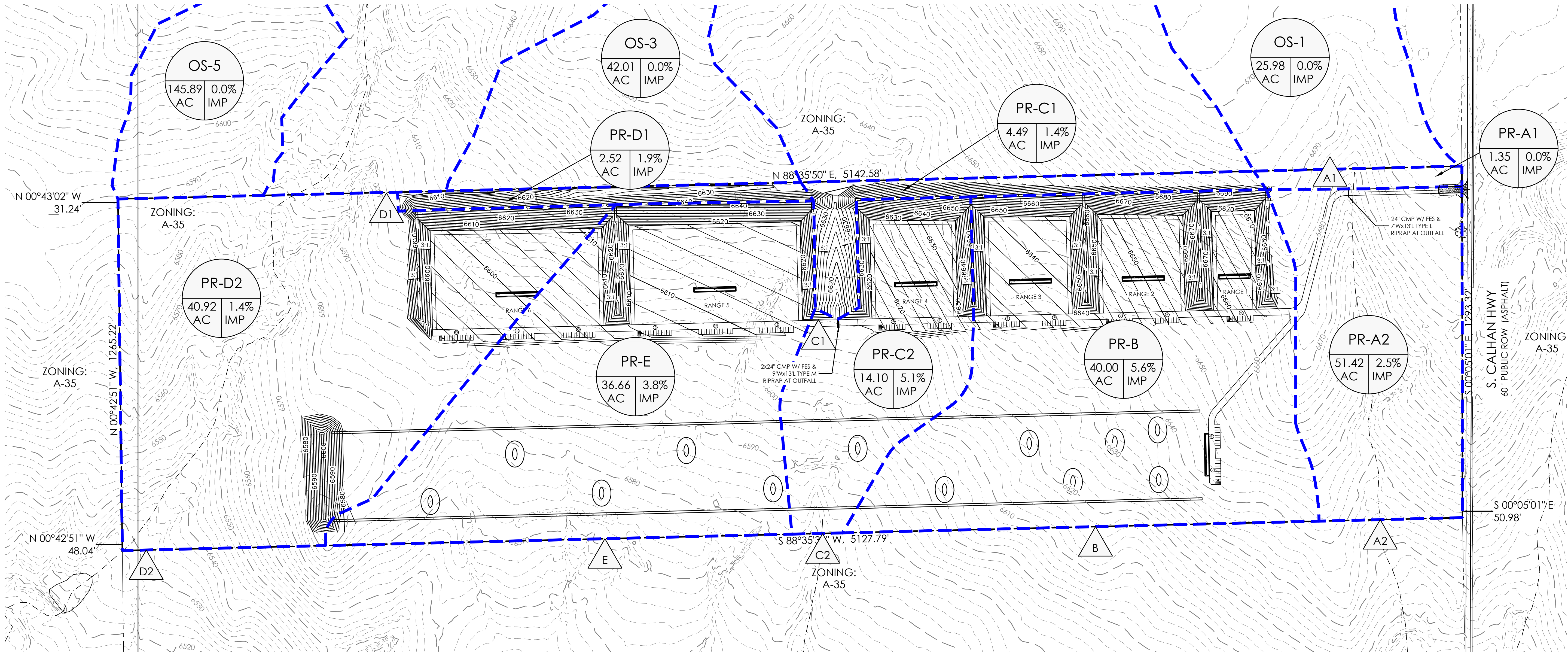
+158 Acre Parcel
168 Training Facility

DRAINAGE REPORT

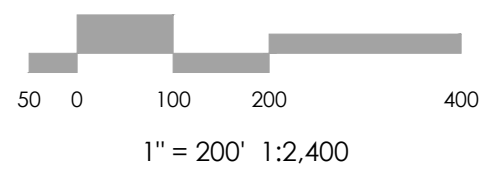
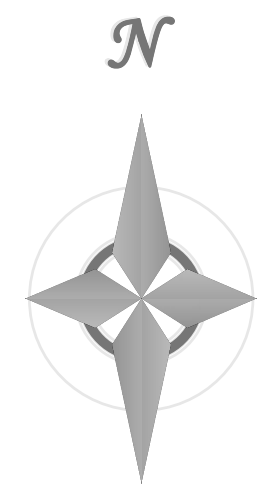
OVERALL DRAINAGE MAP

MVE PROJECT 61224
MVE DRAWING PRDRAIN MAP

DECEMBER 6, 2024
SHEET 2 OF 3



BENCHMARK



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ENGINEERS & SURVEYORS
1903 Idarway Street, Suite 200 Colorado Springs CO 80909 719.635.5736

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168 Training Facility

DRAINAGE REPORT

ONSITE DRAINAGE MAP

MVE PROJECT 61224
MVE DRAWING PRDRAIN MAP

DECEMBER 6, 2024
SHEET 3 OF 3

PROPOSED DRAINAGE SUMMARY TABLE						
DESIGN POINTS	INCLUDED BASINS	AREA (AC)	Tc (MIN.)	RUNOFF		METHOD
				Q5 (CFS)	Q100 (CFS)	
	OS-1	25.98	54.8	3.3	24.1	RATIONAL
	OS-2	111.10	80.1	9.0	65.6	RATIONAL
	OS-3	17.00	31.7	3.3	23.9	RATIONAL
	OS-4	157.08	92.4	10.0	73.0	RATIONAL
	OS-5	11.95	27.3	2.5	18.4	RATIONAL
	PR-A1	1.35	6.9	0.5	3.7	RATIONAL
DP-A1	OS-1, PR-A1	27.33	55.5	3.4	25.0	RATIONAL
	PR-A2	18.41	28.9	4.5	28.3	RATIONAL
DP-A2	OS-1, PR-A1&2	45.75	66.7	5.1	34.9	RATIONAL
DP-B	PR-B	40.00	32.4	11.0	59.6	RATIONAL
	PR-C1	4.49	38.4	0.8	5.7	RATIONAL
DP-C1	OS-2, PR-C1	115.60	83.7	8.7	63.9	RATIONAL
	PR-C2	14.10	31.1	3.9	21.4	RATIONAL
DP-C2	OS-2, PR-C1&2	129.69	91.4	8.8	62.1	RATIONAL
	PR-D1	2.52	46.1	0.4	2.8	RATIONAL
DP-D1	OS-3, PR-D1	19.52	32.7	3.7	27.0	RATIONAL
	PR-D2	40.92	33.6	8.4	56.6	RATIONAL
DP-D2	OS-4&5, D1&2	212.47	109.5	9.4	67.2	RATIONAL
DP-E	PR-E	36.66	32.2	9.0	53.6	RATIONAL

