PRELIMINARY DRAINAGE REPORT

for WINDERMERE FILING NO. 2

Colorado Springs, CO

August 2024

Prepared for:

Colo Windermere #2, LLC

4164 Austin Bluffs Parkway, #361 Colorado Springs, CO 80918 Contact: James Todd Stephens

Prepared by:

Drexel, Barrell & Co.

101 Sahwatch St, Suite 100 Colorado Springs, CO 80903 Contact: Tim McConnell, P.E. (719) 260-0887

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PRELIMINARY DRAINAGE REPORT

for WINDERMERE FILING NO. 2 Colorado Springs, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E. Colorado P.E. License No. 33797 For and on Behalf of Drexel, Barrell & Co.

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name:

Colo Windermere #2, LLC

By:

Title: Address: James Todd Stephens Owner 4164 Austin Bluffs Parkway, #361 Colorado Springs, CO 80918

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

County Engineer/ECM Administrator

Date

Date

Date

CONDITIONS

PRELIMINARY DRAINAGE REPORT

for WINDERMERE FILING NO. 2

Colorado Springs, Colorado

2.0 PURPOSE

This report is prepared by Drexel, Barrel & Co in support of the Windermere Filing No. 2 subdivision. This preliminary drainage report is presented in order to determine the adequacy of the existing drainage facilities based upon the anticipated development. This report is associated with a preliminary plan amendment, which triggered the need for this drainage analysis. This development is in the concept stage and as such no site work, grading or drainage and utility installation is to occur at this time. The drainage report will be required to be updated upon final layout, grading and drainage design.

3.0 GENERAL SITE DESCRIPTION

<u>Location</u>

The site is located at the northwest corner of N. Carefree Cir. and Marksheffel Rd. - the E 1/2 of Section 29, Township 13 S, Range 65 W of the 6th P.M., El Paso County, Colorado.

The site is bound on the west by Antelope Ridge Dr., on the north by the Windermere Filing No. 1 subdivision (Pronghorn Meadows Circle), on the east by Marksheffel Rd., and on the south by N. Carefree Cir.

Site Conditions

The site is approximately 9.26 acres in size and is proposed as a multi-family home subdivision. The proposed site development includes approximately 200 multi-family units. The site has recently been overlot graded, seeded and mulched as part of the Windermere Filing No. 1 development to the north. The site is located within the Sand Creek Drainage Basin. Historically, this site drains to the southeast towards the intersection of N. Carefree Circle and Marksheffel Road.

This site was studied as part of the approved Preliminary Drainage Report for Windermere & Final Drainage Report for Windermere Filing No. 1, by Classic Consulting (October 2014) and the more recently approved Final Drainage Report for Windermere Filing No. 1, by Drexel, Barrell & Co. (April 2022).

Soils

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S. Department of Agriculture Soil Conservation Service, the site is underlain by Truckton sandy loam, a type 'A' hydrologic soil. See appendix for map.

<u>Climate</u>

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers

relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel #08041C0543 G (December 7, 2018) the project site is within a designated Zone X area described as "area of minimal hazard". A firmette map is included in the appendix.

4.0 HISTORIC HYDROLOGY

The existing condition described in the previously approved Preliminary Drainage Report for Windermere & Final Drainage Report for Windermere Filing No. 1, by Classic Consulting (October 2014) of the project area is presented View for references, spectrically to the project area is presented view for references, spectrically to the project area is presented view for the project area view for

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5.0 EXISTING HYDROLOGY 🖌

delineation of the subject project on excerpt map, text discussion, and calculations of the basin that match the historical conditions of the proposed project.

As described above, the Windermere Filing No.2 in the Windermere Filing No.1 development and stociate to state the windermere filing No.1 development and stociate to state the state of th

The following basin descriptions are pulled directly from the previously approved Windermere Filing No. 1 Final Drainage Report.

South area – tributary to existing N. Carefree/Marksheffel storm system

Basin C3 covers an area of 0.63 acres of pond embankment and is located along the southeasterly project boundary along N. Marksheffel Road. This basin generates flows of $Q_5=0.5$ cfs and $Q_{100}=2.5$ cfs that travel offsite to the east and ultimately south along N. Marksheffel Road towards the existing storm inlet at DP-S. As this basin is to remain undeveloped, the discharge of flows offsite is acceptable under MS4 criteria.

Existing Design Point 4 covers runoff from Bosin D-16 of the Pronghorn Meadows Subdivision to the west of this project development. An existing 8' sump curb inlet intercepts the runoff (Q_5 =4.9 cfs and Q_{100} =10.7 cfs) and directs it via existing 24" RCP across Antelope Ridge Drive, where it currently discharges into a roadside swale along N. Carefree Circle. Design and extension of this storm system to the east and connection to the existing storm sewer system of press with the completed of the tully reviewed without existing drainage and extension of this draw of east and connection to the existing drainage and extension of this storm system to the east and connection to the existing drainage and extension of this storm system to the east and connection to the existing drainage and extension of this storm system to the east and connection to the existing drainage and extension of the east and connection to the existing drainage map is

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Circle and generates flows of $Q_5=2.1$ cfs and $Q_{100}=6.9$ cfs that travel to the south and ultimately combine with flows from Design Point 4 in a roadside swale traveling east along N. Carefree Circle towards DP-S.

A portion of basin C4 (0.72-acres) is conservatively assumed to cover future development of Tract B that will drain offsite and will not be treated for Water Quality. As per El Paso County ECM App I.7.1.C.1, this area is less than 20% of site area or 1-acre, and is due to grading restrictions (an exclusion listed in ECM App I.7.1.B), the discharge of these flows offsite to the southern drainageway is permitted under County MS4 criteria. This assumption of grading and future use will be required to be reviewed at the time of replat for future development of Tract B. To meet this criteria, this area will be required to remain impervious, or be redirected to drain to the detention pond.

DP-S is located at the existing area inlet in Basin C3. The flows leave this inlet via an existing 24" storm pipe that connects to the existing storm system in N. Carefree Cir., which then carries the flows to the south. This design point reflects the flows from Basins C3 & C4, detained flows released by the south detention facility, offsite Basin EXR, and offsite Basin D-16. The combined flows at DP-S are $Q_5=10.0$ cfs and $Q_{100}=33.7$ cfs, which is less than the existing condition at Ex. DP-6 of $Q_5=18.4$ cfs and $Q_{100}=42.6$ cfs.

Existing Design Point 19 represents the flows generated by offsite Basin NC2 ($Q_5=5.1$ cfs and $Q_{100}=9.8$ cfs), these flows are picked up by the existing 15' triple at-grade inlet just west of the intersection with N. Marksheffel Road. The flows then leave this inlet via an existing 18" storm pipe to the east, ultimately converging with the flows from DP-S at an existing manhole at existing design point J1.

Flows of $Q_5=15.1$ cfs and $Q_{100}=43.5$ cfs leave DP-J1 via an existing 24" storm pipe and are carried to the existing 10' sump inlet at Existing DP-20 in offsite Basin NC1. The flows leave this existing inlet via an existing 30" storm pipe ultimately traveling to the south via the Marksheffel Road storm system. Developed runoff rates at DP-20 ($Q_5=17.0$ cfs and $Q_{100}=46.9$ cfs) are less than those in the existing condition ($Q_5=24.2$ cfs and $Q_{100}=53.3$ cfs, thereby reducing impact to the existing storm sewer system.

6.0 PROPOSED HYDROLOGY

This preliminary drainage report is presented in order to determine the adequacy of the existing drainage facilities based upon the anticipated development. This report is associated with a preliminary plan amendment, which triggered the need for this drainage analysis. This development is in the concept stage and as such no site work, grading or drainage and utility installation is to occur at this time. The drainage report will be required to be updated upon final layout, grading and drainage design.

The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals, and Mile High Flood District design software (MHFD-Detention v.4.03) for pond analysis. See below for a summary runoff table and description of each design point.

The basins and design points described below are based on a preliminary concept site design. Grading and subsequent areas tributary to the detention facility are subject to change and any areas not tributary to the detention facility will be assessed for water quality treatment in adherence to County drainage criteria at the final drainage report stage.

BASIN	AREA (AC)	Q5 (cfs)	Q100 (cfs)
A1	6.79	12.6	27.9
B1	3.33	7.2	16.0
B2	0.49	1.0	2.3
B4	0.16	0.4	0.8
P1	1.00	0.5	2.7
D16	2.73	4.9	10.7
A2	0.92	0.7	3.4
NC2	1.61	6.3	12.1
EXR	0.53	2.4	4.4
C3	0.63	0.5	2.5
Pond Release	1.00	0.3	10.6
NC1	0.43	1.9	3.4

Rational Method Runoff Summary

The proposed runoff of A1 is higher than that of B3 in the excerpts (SF2126). Please clarify whether the south pond will still have sufficient capacity to accommodate this increase. This comment arises because the excerpts were not included in Review C3.

Design Point 1 represents the flows generated by basin A1 ($Q_5=12.6$ cfs and $Q_{100}=27.9$ cfs). These flows sheet flow across the site, from northwest to southeast, before being discharged into the existing detention facility. No early grading is proposed with this concept design, and it is acknowledged that prior to any grading an adequate method will need to be provided for flows to discharge into the existing detention facility.

Design Point 2 covers flow from offsite basins B1 and B2. Flows of $Q_5=8.1$ cfs and $Q_{100}=17.7$ cfs travel via the existing private 24" RCP storm sewer to the east and discharge into the north end of the existing detention facility.

Design Point 3 represents all flows reaching the existing detention facility (Basins B4, P1, DP1, and DP2) for a total flow of $Q_5=19.8$ cfs and $Q_{100}=45.8$ cfs. The existing detention facility and modifications for this developed condition are described further below.

Design Point 4 is identical to DP-4-EX in the historic and existing condition, and represents flows (Q_5 = 4.9cfs and Q_{100} =10.7cfs) from offsite basin D16 which discharges on to the Windermere property. In the developed condition, it is proposed that the roadside ditch be continued to capture flows that are not able to be captured by the detention facility due to grading restraints. This swale would allow flows to continue to the east to be captured by the existing Type D area inlet at the intersection of N. Carefree Cir. and Marksheffel Road. As the grading for the site is refined, the area tributary to the detention facility will be maximized to the extent possible given the site grading constraints. Appropriate erosion control measures will be provided at the terminus of the swale to aid in erosion and scour mitigation.

Design Point 19 is equivalent to DP-19-EX from the historic and existing condition, and The existing condition discussion is the blass begin have with a flow of the property of the existing condition in Static and the difference of the property of the existing storm of the condition in SF2126. Please clarify whether the existing storm pipe, existing inlets have sufficient capacity to handle the increased runoff. Pipe, and inlet capacity calculations will be required in the FDR. This comment arises because the excerpts were not included in Review C3. and Marksheffel Road intercepts a portion of this runoff ($Q_5=4.8$ cfs and $Q_{100}=8.1$ cfs) and discharges to the east via public 18" RCP storm sewer.

Design Point S is located at the same existing area inlet as DP-6-EX. In the developed condition flows reaching this point, from basins EXR, A2, C3, DP4, in addition to the proposed pond release rate will equal $Q_5=7.8$ cfs and $Q_{100}=29.2$ cfs. Flows exit this area inlet by public 24" RCP to the south.

Design Point J1 is located at the existing manhole on the north side of N. Carefree Circle and represents the combining of flows from DP-19 and DP-S. Flows of Q_5 =12.4 cfs and Q_{100} =38.0 cfs continue to the south via the existing public 30" RCP towards DP-20.

Design Point 20 (equivalent to DP-EX-20) as in the existing condition consists of surface runoff from basin NC-1, flowby from the at-grade inlet at DP-19 and pipe flow from DP-J1. An existing public 10' Type R sump inlet intercepts all the surface runoff and combines it with the upstream flows from DP-J1 and DP-19 existing at-grade inlet capture. Total developed runoff at this location is $Q_5=13.7$ cfs and $Q_{100}=40.4$ cfs. This runoff continues within the existing Marksheffel Road storm system to the south. Should the inlet be clogged, the resulting runoff will continue east via the neighboring curb and gutter.

7.0 EXISTING DETENTION/WATER QUALITY FACILITY

As part of the overlot design for Windermere Filing No. 1, the detention pond located in the southeast corner of the property was designed as a full-spectrum detention facility to capture flows from the Windermere Filing No. 2 basins.

In order to minimize future grading within the detention facility area, the volume was based on an assumed final build-out watershed imperviousness of 68.0%, which considered Windermere Filing No. 2 (Windermere Filing No. 1 – Tract B) as potentially higher density than single-family residential. As part of the Windermere Filing 1 overlot grading, the pond was excavated to full volume and the outlet structure and associated piping installed. An interim orifice plate (assuming full developed condition within the street right-of-way, but no further development) was installed to allow for appropriate WQCV drain time. Once the design is finalized at the final drainage report stage, the orifice plate will need to be switched out to allow for discharge of the developed flows. It is anticipated based on this preliminary design that the restrictor plate will need to be raised to 7.80" above the invert of the 18" outfall pipe. No other portion of the detention facility will need to be modified.

Based on the analysis in this preliminary report, the developed condition encompasses a total of 12.79 acres that is tributary to this existing facility, with a composite imperviousness of 54.9% for the final fully developed condition. Required volumes are listed below.

		Required Volume					
	Imperviousness	WQCV EURV 100-YR					
FINAL	54.9%	0.24	0.83	1.29			

The actual pond volume at the proposed spillway stage is 1.15 acre-feet. A concrete forebay with an energy dissipater has been installed where the flows enter the pond. The volume of the forebay was designed for 3% of the WQCV volume for the pond, as is still within that limit for this concept design condition. The flows exit the forebay through a notch, discharging into the concrete trickle channel at the bottom of the pond. The trickle channel conveys the flows to the micropool. The outlet structure then releases the flows at a reduced flow rate with the use of a plate with orifice holes, into a proposed 18" pipe with restrictor plate, discharging into an existing storm inlet at the corner of N. Carefree Circle and Marksheffel Rd, after which the flows continue to the south via the existing storm sewer system.

In accordance with El Paso County criteria, the modified Type C outlet structure with a permanent micropool will release the WQCV over a 40-hour period. Switching out of the orifice plate will ensure that the WQCV release rate remains within criteria for the final developed condition. The outlet structure will remain in place and in this preliminary stage will result in release rates of $Q_5=0.3$ cfs and $Q_{100}=10.6$ cfs. For comparison, the existing basin EX-A released flow rates of $Q_5=11.3$ cfs and $Q_{100}=28.2$ cfs.

A 27-ft wide riprap emergency spillway is located on the south side of the pond. In the event that water overtops the spillway, flow will discharge into existing area inlet at the intersection of N. Carefree Cir and Marksheffel Rd, where it is then picked up by the existing storm system.

All detention facility calculations, including excerpts for forebay volumes, micropool surface areas, outlet structures, discharge pipes and spillway design are provided in the appendix.

The pond has a 15' wide maintenance access that provides access to the pond bottom, forebay and outlet structure per ECM 3.3.3.K. A private maintenance agreement and O&M manual has been established for this pond as required by the County. Necessary modifications to this maintenance access will be provided with the final drainage report.

8.0 FOUR-STEP PROCESS

This project conforms to the City of Colorado Springs/El Paso County Four Step Process. The process focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

- 1. **Employ Runoff Reduction Practices:** Proposed impervious areas on this site (roofs, asphalt/sidewalk) will sheet flow across landscaped ground as much as possible to slow runoff and increase time of concentration prior to being conveyed to the proposed public streets and storm sewer system. This will minimize directly connected impervious areas within the project site.
- 2. Implement BMP's that provide a Water Quality Capture Volume with slow release: Runoff from this project will be treated through capture and slow release of the WQCV in apermanent Extended Detention Basin designed per current City of El Paso County drainage criteria.

- 3. **Stabilize Drainage Ways:** Flows from the detention facility are released directly into the existing storm sewer system and no stabilization will be necessary.
- 4. Implement Site Specific and Other Source Control BMP's: The site is proposed as a residential development, and as such standard household source control will be utilized in order to minimize potential pollutants entering the storm system. Example source control measures consist of: garages for storage of household chemicals, trash receptacles for individual households and in common areas for pet waste. The need for Industrial and Commercial BMP's was considered, however per ECM 1.7.2.A the need for industrial and commercial BMPs are not applicable for this project.

9.0 GEOTECHNICAL HAZARDS

In accordance with geotechnical recommendations, the project design is intended to direct runoff away from structures, and into the receiving storm sewer system and water quality/detention basins. This will be accomplished by a variety of means, i.e. curb and gutter and storm sewer. Per "Soils and Geology Study, Windermere Subdivision" by RMG, October 26, 2020 (Revised January 18, 2021), and updated with an addendum for Tract B (March 30, 2022)

10.0 FACILITY MAINTENANCE

Ownership and maintenance of all public facilities, generally located within the public right-of-way will be by El Paso County. Ownership and maintenance of all tracts and private facilities will be by the Sands Metropolitan District #4.

11.0 CONSTRUCTION COST ESTIMATE

Construction cost estimate will be provided with the Final Drainage Report.

12.0 DRAINAGE/BRIDGE FEES

Tract B was considered as an open space tract for the drainage fee calculation for Windermere Filing No. 1. Development of this tract will require payment of drainage and bridge fees associated with the proposed impervious acreage. This will be determined with the Final Drainage Report for this development as site imperviousness is confirmed.

13.0 CONCLUSIONS

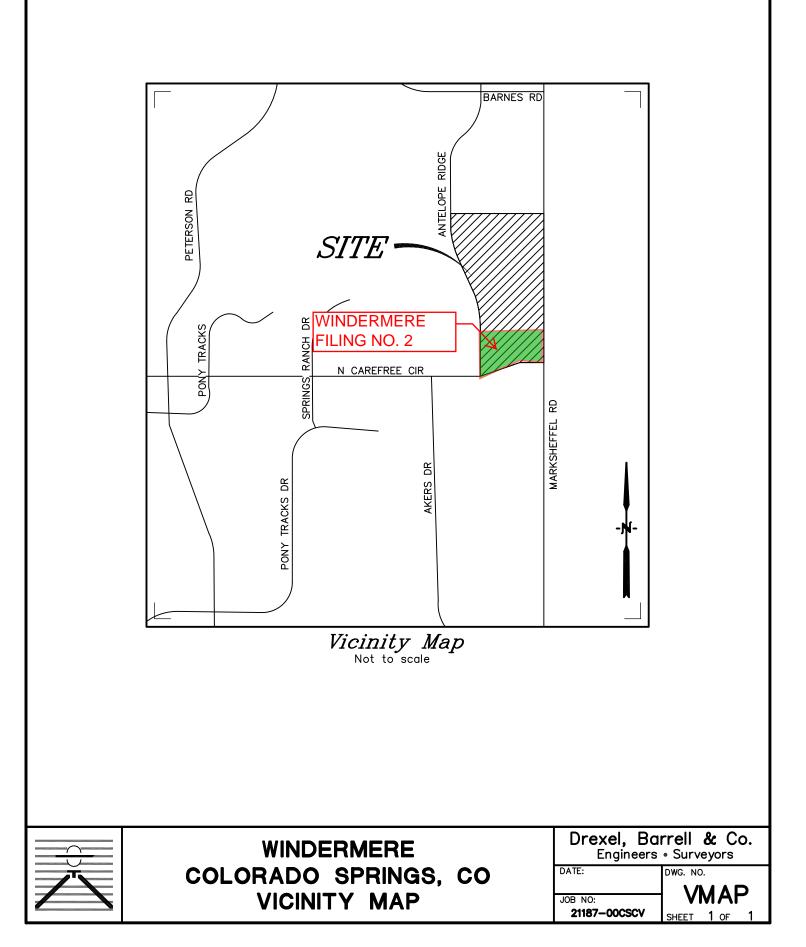
The Windermere Filing No. 2 project has been designed in accordance with El Paso County criteria. The detention facility has been designed to limit the release of storm runoff to historic conditions. This development will not negatively impact or increase flows in the downstream facilities.

14.0 REFERENCES

The sources of information used in the development of this study are listed below:

- 1. City of Colorado Springs "Drainage Criteria Manual", 2016.
- 2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised October 2019.
- 3. Soil Survey for Colorado Springs and El Paso County, Colorado, U.S. Department of Agriculture, Soil Conservation Service, June 1980.
- 4. "Flood Insurance Studies for Colorado Springs and El Paso County, Colorado", prepared by the Federal Emergency Management Agency (FEMA), 2018.
- 5. "Soils and Geology Study, Windermere Subdivision", prepared by RMG, October 26, 2020, Revised January 18, 2021.
- 6. "Preliminary Drainage Report for Windermere & Final Drainage Report for Windermere Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, October 2014.
- 7. "Final Drainage Report Marksheffel Road from Constitution Ave. to Dublin Rd.," by CH2M Hill, dated May 2008 and Marksheffel Road Construction Drawings by Wilson & Company.
- 8. "Final Drainage Report for Windermere Filing No. 1" prepared by Drexel, Barrell & Co., March 8, 2022.

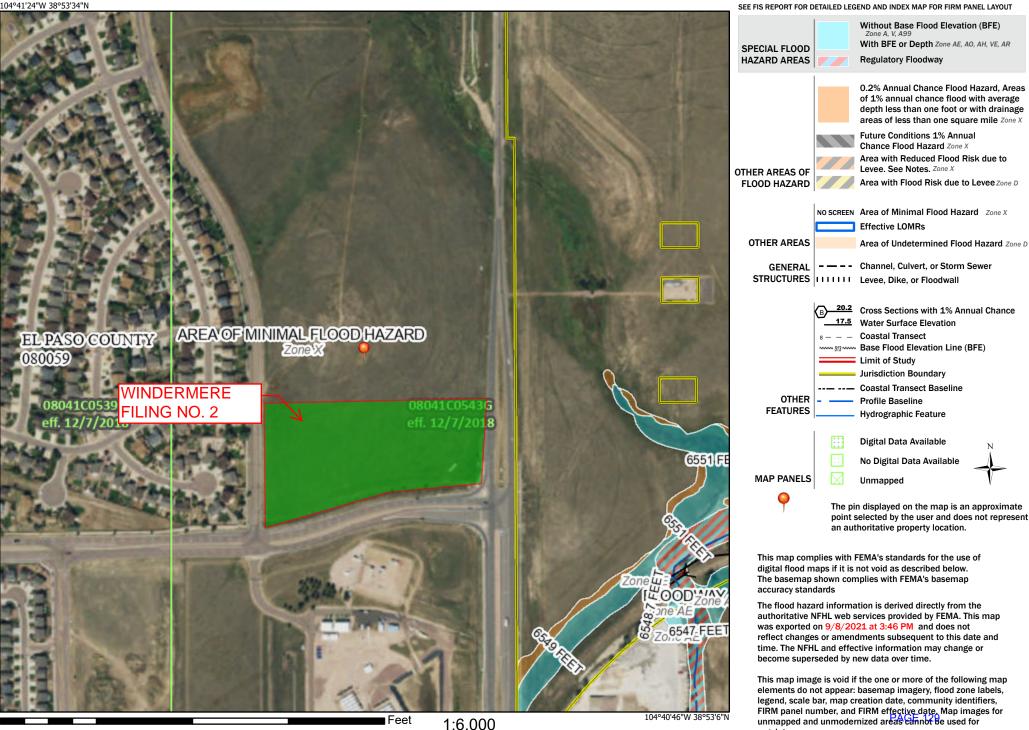
APPENDIX



National Flood Hazard Layer FIRMette



Legend



250 n

1,000

500

1,500

2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

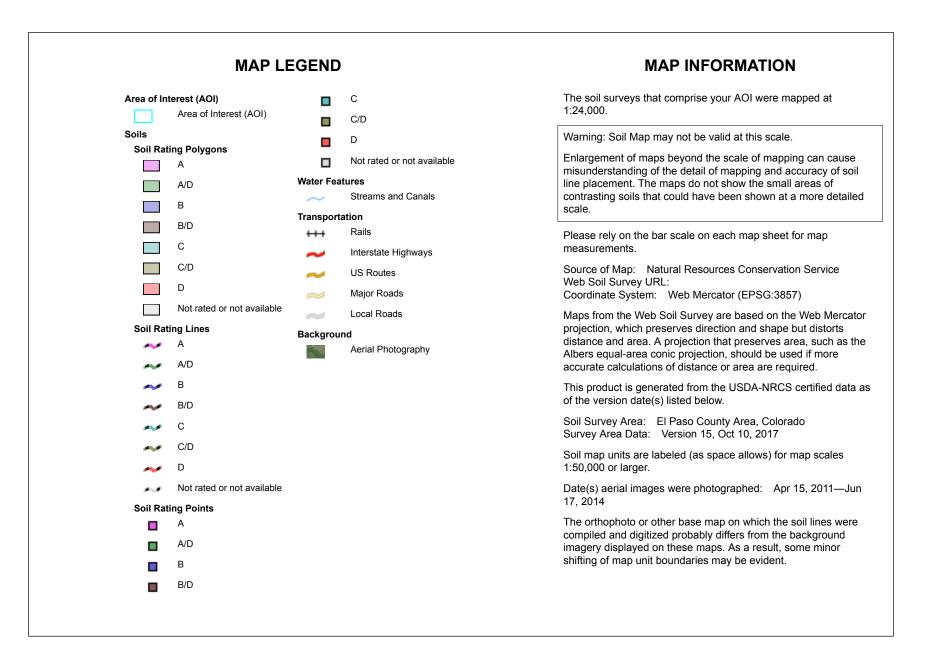
unmapped and unmodernized areas cannot be used for regulatory purposes.



Natural Resources Conservation Service

Web Soil Survey National Cooperative Soil Survey

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Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
97	Truckton sandy loam, 3 to 9 percent slopes	A	56.4	100.0%
Totals for Area of Intere	st		56.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

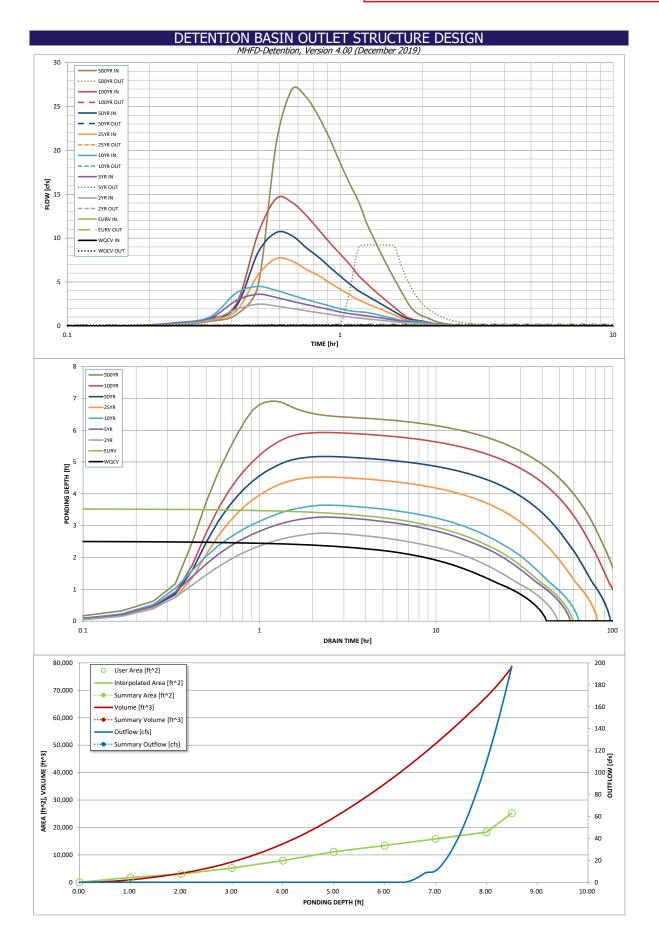
Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified APPROVED DRAINAGE REPORT EXCERPTS

WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND INTERIM DESIGN

	DETENTION BASIN OUTLET STRUCTURE DESIGN									
Project	Windermere Filing		HFD-Detention, Vo	ersion 4.03 (May	2020)					
-	South Pond - Inte									
ZONE 3	South Pond - Inte	rini condición		Estimated	Fatimated					
ZONE 2 ZONE 1				Estimated	Estimated	Outlat Turna				
100-YR VOLUME EURV WQCV			7 4 4 4 4 9 9 9	Stage (ft)	Volume (ac-ft)	Outlet Type	1			
			Zone 1 (WQCV)		0.118	Orifice Plate	-			
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)		0.124	Orifice Plate				
PERMANENT ORIFICES			Zone 3 (100-year)	4.82	0.253	Weir&Pipe (Restrict)				
Example Zone	Configuration (Re	etention Pond)		Total (all zones)	0.496		-			
User Input: Orifice at Underdrain Outlet (typical	ly used to drain W	OCV in a Filtration E	<u>3MP)</u>			-	Calculated Parame	eters for Underdrain	<u>1</u>	
Underdrain Orifice Invert Depth =		ft (distance below	the filtration media	surface)	Underd	Irain Orifice Area =		ft ²		
Underdrain Orifice Diameter =		inches			Underdrain	Orifice Centroid =		feet		
User Input: Orifice Plate with one or more orific	· · · · · · · · · · · · · · · · · · ·		-				Calculated Parame			
Invert of Lowest Orifice =		ft (relative to basin	n bottom at Stage =	= 0 ft)		ce Area per Row =	N/A	ft ²		
Depth at top of Zone using Orifice Plate =			n bottom at Stage =	= 0 ft)		ptical Half-Width =	N/A	feet		
Orifice Plate: Orifice Vertical Spacing =	25.40	inches				ical Slot Centroid =	N/A	feet		
Orifice Plate: Orifice Area per Row =	w = N/A inches Elliptical Slot Area = N/A ft ²									
User Input: Stage and Total Area of Each Orific								T	1	
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft)	0.00	1.18	2.35			-		l	-	
Orifice Area (sq. inches)	0.67	0.67	0.67					<u> </u>	1	
								T	1	
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	-	
Stage of Orifice Centroid (ft)									-	
Orifice Area (sq. inches)										
User Input: Vertical Orifice (Circular or Rectand	ular)						Calculated Param	eters for Vertical Or	rifico	
Oser Input. Verucal Office (Circular of Rectang	Not Selected	Not Selected	1				Not Selected	Not Selected		
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basir	bottom at Stage -	-0ft) Vor	tical Orifice Area =	N/A	N/A	ft ²	
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basir	-	•	I Orifice Centroid =	N/A N/A	N/A N/A	feet	
Vertical Orifice Diameter =	N/A	N/A	inches	i bolloin al Slaye -	= 0 it) vertical		IN/A	N/A	leet	
	N/A	N/A	inches							
User Input: Overflow Weir (Dropbox with Flat o	or Sloped Grate and	d Outlet Pipe OR Re	ctangular/Trapezoi	dal Weir (and No C	Outlet Pipe)		Calculated Parame	eters for Overflow \	Weir	
oser input. Overnow weir (propoox with hit e	Zone 3 Weir	Not Selected			<u>Judet ripej</u>		Zone 3 Weir	Not Selected		
Overflow Weir Front Edge Height, Ho =	6.40		ft (relative to basin b	hottom at Stage = 0	ft) Height of Grate	- Upper Edge, H. =	6.40	N/A	feet	
Overflow Weir Front Edge Length =	3.92	N/A	feet	bottom ut Stuge – o		eir Slope Length =	3.92	N/A	feet	
Overflow Weir Grate Slope =	0.00	N/A	H:V	Gra	ate Open Area / 10	• -	16.92	N/A		
Horiz. Length of Weir Sides =	3.92	N/A	feet		erflow Grate Open		10.76	N/A	ft ²	
Overflow Grate Open Area % =	70%	N/A	%, grate open are		verflow Grate Open		5.38	N/A	ft ²	
Debris Clogging % =	50%	N/A	%				5150		1.4	
		.,								
User Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice,	Restrictor Plate, or	Rectangular Orifice	:)	Cal	Iculated Parameters	s for Outlet Pipe w	/ Flow Restriction P	late	
	Zone 3 Restrictor	Not Selected		-			Zone 3 Restrictor	Not Selected	1	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below ba	asin bottom at Stage	= 0 ft) Ou	utlet Orifice Area =	0.64	N/A	ft ²	
Outlet Pipe Diameter =	18.00	N/A	inches		Outlet	Orifice Centroid =	0.34	N/A	feet	
Restrictor Plate Height Above Pipe Invert =	7.00		inches	Half-Cent	ral Angle of Restric	tor Plate on Pipe =	1.35	N/A	radians	
	•	•						•	•	
User Input: Emergency Spillway (Rectangular or	r Trapezoidal)	_					Calculated Parame	eters for Spillway		
Spillway Invert Stage=	6.94	ft (relative to basin	n bottom at Stage =	= 0 ft)	Spillway D	esign Flow Depth=	0.55	feet		
Spillway Crest Length =	27.00	feet			Stage at T	op of Freeboard =	8.49	feet		
Spillway End Slopes =	4.00	H:V			Basin Area at T	op of Freeboard =	0.58	acres		
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at T	op of Freeboard =	1.80	acre-ft		
Routed Hydrograph Results	The upor can ever	rida tha dafault (1)	UD hydrographs an	d runoff volumos h	w optoring now val	was in the Inflow H	hidrographs table (Columns W through	45)	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year	
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.49	
CUHP Runoff Volume (acre-ft) =	0.118	0.243	0.156	0.221	0.279	0.448	0.608	0.825	1.590	
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.156	0.221	0.279	0.448	0.608	0.825	1.590	
CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A N/A	N/A N/A	0.1	0.2	0.3	2.9	5.6	9.1	20.5	
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.03	0.27	0.52	0.84	1.89	
Peak Inflow Q (cfs) =	N/A	N/A	2.5	3.6	4.5	7.7	10.6	14.5	27.0	
Peak Outflow Q (cfs) =	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	9.2	
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.3	0.0	0.0	0.0	0.4	
Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	Plate N/A	Plate N/A	Plate N/A	Plate N/A	Plate N/A	Plate N/A	Plate N/A	Plate N/A	Outlet Plate 1 0.8	
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	0.8 N/A	
Time to Drain 97% of Inflow Volume (hours) =	38	53	44	51	57	71	83	99	103	
Time to Drain 99% of Inflow Volume (hours) =	40	57	47	55	61	77	91	108	116	
Maximum Ponding Depth (ft) =	2.51	3.53	2.76	3.27	3.64	4.53	5.17	5.93	6.91	
Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =	0.10 0.118	0.15 0.243	0.11 0.144	0.14 0.204	0.16 0.260	0.22 0.427	0.27 0.585	0.30	0.36	
- axinani volune Storeu (acrefit) =	3.110	0.2.13	0.1.1	0.201	0.200	0.12/	0.303	0.755	4.16/	

WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND INTERIM DESIGN



WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND INTERIM DESIGN

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

I	SOURCE	verride the calcu CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
ime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]		100 Year [cfs]	
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 11111	0:05:00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.18	0.30	0.37	0.00	0.02	0.30	0.10
ľ	0:20:00	0.00	0.00	0.66	0.86	1.01	0.64	0.75	0.80	1.28
	0:25:00	0.00	0.00	1.87	2.88	3.75	1.72	2.23	2.52	4.55
	0:30:00	0.00	0.00	2.47	3.59	4.48	5.79	8.34	10.48	20.89
	0:35:00	0.00	0.00	2.25	3.22	4.03	7.67	10.63	14.52	26.95
	0:40:00	0.00	0.00	1.98	2.79	3.48	7.36	10.26	14.06	26.08
	0:45:00	0.00	0.00	1.71	2.42	3.01	6.45	8.92	12.61	23.86
	0:50:00	0.00	0.00	1.50 1.31	2.13	2.62 2.26	5.72 4.89	7.82 6.68	10.97 9.47	21.29 18.56
	1:00:00	0.00	0.00	1.31	1.84 1.57	1.94	4.09	5.67	8.18	16.22
	1:05:00	0.00	0.00	1.00	1.37	1.72	3.54	4.78	7.01	14.18
·	1:10:00	0.00	0.00	0.89	1.26	1.61	2.96	3.99	5.75	11.72
	1:15:00	0.00	0.00	0.79	1.14	1.52	2.54	3.44	4.83	9.85
	1:20:00	0.00	0.00	0.71	1.01	1.35	2.18	2.93	4.04	8.14
ļ.	1:25:00	0.00	0.00	0.62	0.89	1.16	1.86	2.47	3.34	6.64
ļ	1:30:00	0.00	0.00	0.54	0.77	0.97	1.53	2.02	2.69	5.30
ļ	1:35:00	0.00	0.00	0.46	0.65	0.81	1.23	1.59	2.08	4.03
-	1:40:00	0.00	0.00	0.40	0.53	0.66	0.94	1.18	1.51	2.87
·	1:45:00	0.00	0.00	0.36	0.45	0.59	0.69	0.84	1.03 0.76	1.94
	1:55:00	0.00	0.00	0.33	0.39	0.52	0.49	0.58	0.70	1.13
	2:00:00	0.00	0.00	0.28	0.36	0.48	0.46	0.53	0.55	0.93
	2:05:00	0.00	0.00	0.20	0.29	0.38	0.36	0.33	0.35	0.68
	2:10:00	0.00	0.00	0.18	0.23	0.30	0.28	0.32	0.31	0.49
	2:15:00	0.00	0.00	0.14	0.18	0.23	0.21	0.24	0.23	0.34
	2:20:00	0.00	0.00	0.11	0.14	0.18	0.16	0.18	0.17	0.24
	2:25:00	0.00	0.00	0.08	0.11	0.14	0.13	0.14	0.13	0.18
	2:30:00	0.00	0.00	0.06	0.08	0.10	0.09	0.11	0.10	0.14
	2:35:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.07	0.10
-	2:40:00 2:45:00	0.00	0.00	0.04	0.05	0.06	0.05	0.06	0.06	0.08
·	2:45:00	0.00	0.00	0.03	0.03	0.04	0.04	0.04	0.04	0.06
	2:55:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
-	3:00:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
·	3:05:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
ľ	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:35:00 3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ł	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ł	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
]	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ł	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
į	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

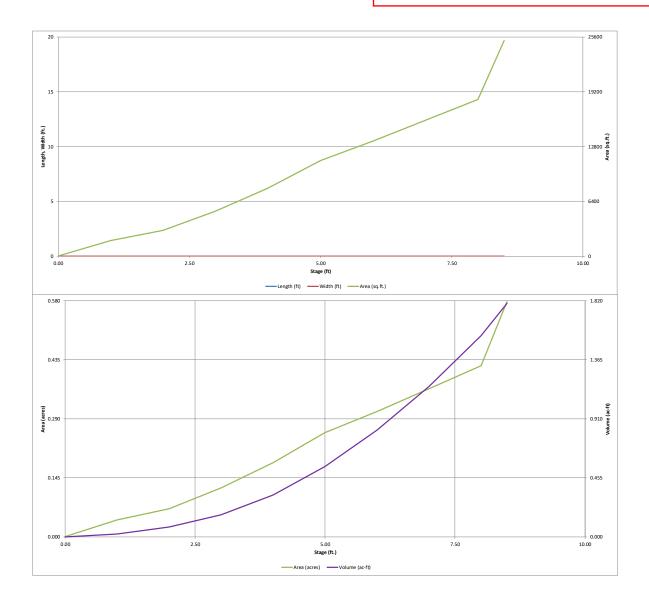
Project:	: Windermer	re South - F	INAL	MHFL	D-Detention, Versio	on 4.03 (Ma	ay 2020)								
Basin ID: ZONE 3 ZONE 3	E 2						1				CII I				R EXCERPT
		F						JUTF							
	E 1 AND 2	100-YE ORIFIC			Depth Increment =	Stage	Op		Width	Area	Override	Area	Volume	Volume	
Watershed Information	ie Configura	ation (Retei	ntion Pond)	Stage - Storage Description Top of Micropool	Stage (ft)	Override Stage (ft) 0.00		(ft)	(ft ²)	Area (ft ²) 40	(acre) 0.001	(ft ³)	(ac-ft)	
Selected BMP Type =					6574		1.00			-	1,801	0.041	920	0.021	
Watershed Area = Watershed Length =	10.89 700	acres ft			6575 6576		2.00				3,008 5,232	0.069	3,325 7,445	0.076	
Watershed Length to Centroid =	400	ft			6577		4.00		-		7,923	0.182	14,022	0.322	ļ
Watershed Slope = Watershed Imperviousness =	0.040 68.00%	ft/ft percent			6578 6579		5.00 6.00	-	-	-	11,161 13,425	0.256	23,564 35,857	0.541 0.823	
Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B =	100.0%	percent percent			6580 6581		7.00				15,853 18,293	0.364 0.420	50,496 67,569	1.159 1.551	
Percentage Hydrologic Soil Groups C/D =		percent			6581.5		8.50		-		25,208	0.579	78,445	1.801	
Target WQCV Drain Time = Location for 1-hr Rainfall Depths =		hours													
After providing required inputs above in	cluding 1-hour	r rainfall						-		-					
depths, click 'Run CUHP' to generate rur the embedded Colorado Urban Hydr			Optional U	ser Overrides				-							
Water Quality Capture Volume (WQCV) =		acre-feet	-	acre-feet				-		-					
Excess Urban Runoff Volume (EURV) = 2-yr Runoff Volume (P1 = 1.19 in.) =		acre-feet acre-feet	1.19	acre-feet inches											
5-yr Runoff Volume (P1 = 1.5 in.) =	0.838	acre-feet	1.50	inches											
10-yr Runoff Volume (P1 = 1.75 in.) = 25-yr Runoff Volume (P1 = 2 in.) =		acre-feet acre-feet	1.75 2.00	inches inches											
50-yr Runoff Volume (P1 = 2.25 in.) =	1.395	acre-feet	2.25	inches											
100-yr Runoff Volume (P1 = 2.52 in.) = 500-yr Runoff Volume (P1 = 3.49 in.) =		acre-feet acre-feet	2.52 3.49	inches inches				-	1 1	-			L	L	
Approximate 2-yr Detention Volume = Approximate 5-yr Detention Volume =		acre-feet acre-feet		-											
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	0.953	acre-feet						-	1	-					
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	1.143	acre-feet acre-feet													
Approximate 100-yr Detention Volume =		acre-feet							-	-					
Define Zones and Basin Geometry															
Zone 1 Volume (WQCV) =		acre-feet							-	-					
Zone 2 Volume (EURV - Zone 1) = Zone 3 Volume (100-year - Zones 1 & 2) =	-	acre-feet acre-feet													
Total Detention Basin Volume =	1.373	acre-feet													
Initial Surcharge Volume (ISV) = Initial Surcharge Depth (ISD) =	user user	ft 3						-							
Total Available Detention Depth (H _{total}) =	user	ft								-					1
Depth of Trickle Channel (H_{TC}) = Slope of Trickle Channel (S_{TC}) =	user user	ft ft/ft													
Slopes of Main Basin Sides (Smain) =		H:V						-		-					-
Basin Length-to-Width Ratio $(R_{L/W}) =$	user							-							
Initial Surcharge Area (A _{ISV}) =		ft ²							1 1						
Surcharge Volume Length $(L_{ISV}) =$ Surcharge Volume Width $(W_{ISV}) =$		ft ft						-	-	-					
Depth of Basin Floor (H _{FLOOR}) = Length of Basin Floor (L _{FLOOR}) =		ft ft													
Width of Basin Floor (W_{FLOOR}) =	user	ft						-	-	-					
Area of Basin Floor (A_{FLOOR}) = Volume of Basin Floor (V_{FLOOR}) =	user user	ft ² ft ³													
Depth of Main Basin (H_{MAIN}) =	user	ft													
Length of Main Basin (L _{MAIN}) = Width of Main Basin (W _{MAIN}) =		ft ft						-							
Area of Main Basin (A _{MAIN}) =	user	ft ²								-					1
Volume of Main Basin (V _{MAIN}) = Calculated Total Basin Volume (V _{total}) =	user user	ft ³ acre-feet													
, 2000)													L		
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

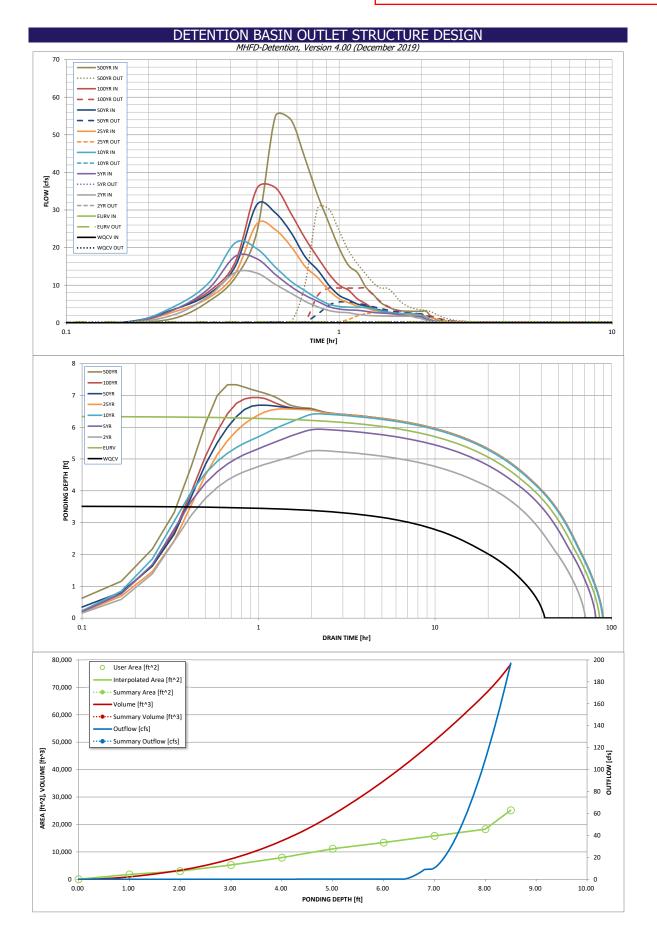
WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND FINAL DESIGN



WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND FINAL DESIGN

DETENTION BASIN OUTLET STRUCTURE DESIGN										
.			HFD-Detention, V	ersion 4.03 (May	2020)					
Project: Basin ID:	Windermere Sout	h - FINAL								
ZONE 3				Estimated	Estimated					
ZONE 2 ZONE 1				Stage (ft)	Volume (ac-ft)	Outlet Type				
100-YR VOLUME EURY WOCV			Zone 1 (WQCV)	3.52	0.242	Orifice Plate	1			
							-			
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	6.34	0.689	Orifice Plate	-			
PERMANENT ORIFICES	Configuration (R		Zone 3 (100-year)	7.57	0.442	Weir&Pipe (Restrict)				
	• ·			Total (all zones)	1.373					
User Input: Orifice at Underdrain Outlet (typical	ly used to drain WO	Ē.					Calculated Parame	eters for Underdrai	<u>n</u>	
Underdrain Orifice Invert Depth =		•	the filtration media	surface)		rain Orifice Area =		ft ²		
Underdrain Orifice Diameter =		inches			Underdrain	Orifice Centroid =		feet		
User Input: Orifice Plate with one or more orifi	coc or Elliptical Slot	Weir (typically use	d to drain WOCV a	nd/or ELIPV/ in a co	dimentation BMP)		Calculated Parame	tors for Plata		
Invert of Lowest Orifice =	0.00		n bottom at Stage =			ce Area per Row =	N/A	ft ²		
Depth at top of Zone using Orifice Plate =	6.34		n bottom at Stage =			ptical Half-Width =	N/A	feet		
Orifice Plate: Orifice Vertical Spacing =	25.40	inches		,		cal Slot Centroid =	N/A	feet		
Orifice Plate: Orifice Area per Row =	N/A	inches				lliptical Slot Area =	N/A	ft ²		
						•		_		
User Input: Stage and Total Area of Each Orific	e Row (numbered	from lowest to high	<u>nest)</u>						_	
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft)	0.00	2.11	4.23							
Orifice Area (sq. inches)	1.24	1.24	1.24							
	r		I		I	I	I	I	-	
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)		
Stage of Orifice Centroid (ft)									-	
Orifice Area (sq. inches)										
							Coloulated Deverse		: 6 :	
User Input: Vertical Orifice (Circular or Rectang	Not Selected	Net Colostad	1					eters for Vertical O	rifice	
Invert of Vertical Orifice =	N/A	Not Selected N/A	ft (relative to basir	bottom at Stago		tical Orifice Area =	Not Selected N/A	Not Selected N/A	ft ²	
Depth at top of Zone using Vertical Orifice =	N/A			-		Orifice Centroid =	N/A N/A	N/A N/A	feet	
Vertical Orifice Diameter =								N/A	licer	
	in the second se	N/N	inches							
User Input: Overflow Weir (Dropbox with Flat of	or Sloped Grate and	l Outlet Pipe OR Re	ctangular/Trapezoi	dal Weir (and No C	Dutlet Pipe)		Calculated Parame	eters for Overflow	Weir	
User Input: Overflow Weir (Dropbox with Flat o	zone 3 Weir	l Outlet Pipe OR Re Not Selected	ectangular/Trapezoi	dal Weir (and No C	Dutlet Pipe)		Calculated Parame Zone 3 Weir	Not Selected	<u>Weir</u>	
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho =					Dutlet Pipe) ft) Height of Grate	e Upper Edge, H _t =	Zone 3 Weir		<u>Weir</u> feet	
	Zone 3 Weir	Not Selected			ft) Height of Grate	e Upper Edge, H _t = eir Slope Length =	Zone 3 Weir	Not Selected]	
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 6.40 3.92 0.00	Not Selected N/A N/A N/A	ft (relative to basin I	pottom at Stage = 0	ft) Height of Grate	eir Slope Length =	Zone 3 Weir 6.40	Not Selected N/A	feet feet	
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WINDERMERE FILING NO. 1 FDR EXCERPT SOUTH POND FINAL DESIGN



DETENTION BASIN OUTLET ST WINDERMERE FILING NO. 1 FDR EXCERPT Outflow Hydrograph Workbook Filename: SOUTH POND FINAL DESIGN

	The user can ov		ated inflow hvdr	ographs from th	is workbook wit	n inflow hydrogra	aphs developed i	in a separate prog	aram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]		100 Year [cfs]	
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00 3.58	0.00	0.00	0.25	0.02	1.24 5.72
	0:20:00	0.00	0.00	7.15	9.15	10.68	6.68	7.69	8.35	12.02
	0:25:00	0.00	0.00	13.38	17.69	21.29	13.23	15.05	16.20	24.26
	0:30:00	0.00	0.00	13.20	16.99	19.67	26.35	31.45	35.75	54.89
	0:35:00	0.00	0.00	10.18	12.85	14.80	24.76	29.25	35.94	53.97
	0:40:00	0.00	0.00	7.86	9.61	11.02	20.31	24.00	29.05	43.65
	0:45:00 0:50:00	0.00	0.00	5.71 4.27	7.29 5.70	8.49 6.40	14.97 12.02	17.57 14.05	22.45 17.39	33.95
	0:55:00	0.00	0.00	3.25	4.28	4.93	8.64	9.99	17.39	26.56 19.85
	1:00:00	0.00	0.00	2.81	3.64	4.33	6.38	7.27	9.99	15.21
	1:05:00	0.00	0.00	2.65	3.41	4.15	5.32	6.06	8.64	13.31
	1:10:00	0.00	0.00	2.23	3.33	4.09	4.41	4.99	6.33	9.55
	1:15:00	0.00	0.00	2.01	3.06	4.06	3.95	4.46	5.08	7.52
	1:20:00	0.00	0.00	1.88	2.76	3.68	3.31	3.73	3.74	5.42
	1:25:00 1:30:00	0.00	0.00	1.80	2.60	3.14	3.00	3.37	3.03	4.32
	1:30:00	0.00	0.00	1.76 1.73	2.50	2.81 2.62	2.55 2.30	2.87	2.57	3.60 3.22
	1:40:00	0.00	0.00	1.73	2.44	2.62	2.30	2.58	2.32	3.10
	1:45:00	0.00	0.00	1.73	1.88	2.44	2.08	2.34	2.19	3.03
	1:50:00	0.00	0.00	1.73	1.76	2.41	2.05	2.30	2.19	3.03
	1:55:00	0.00	0.00	1.36	1.70	2.30	2.03	2.28	2.19	3.03
	2:00:00	0.00	0.00	1.15	1.57	2.02	2.03	2.28	2.19	3.03
	2:05:00 2:10:00	0.00	0.00	0.65	0.89	1.16	1.16	1.30	1.25	1.73
	2:10:00	0.00	0.00	0.36	0.50	0.65	0.66	0.74	0.71	0.98
	2:20:00	0.00	0.00	0.18	0.13	0.16	0.33	0.39	0.37	0.31
	2:25:00	0.00	0.00	0.03	0.05	0.05	0.06	0.07	0.07	0.09
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00 2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

5:55:00

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PAGE 21

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Inflow Hydrographs

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North Pond (North Forebay) FOREBAY VOLUME

Req'd V=3% x WQCV

Ex DP 24	Impervious 0.34	Area 79.05								
WQCV=			1.0826 ac-ft							
V=			0.0325 ac-ft							
Actual V			0.0409 ac-ft							
FOREBAY RELEASE NOTCH WIDTH										

5-YR NOTCH

Q=CLH^{3/2}

2% of Q= 2.23 cfs	5
C= 2.6	
H (height of forebay wall)= 1 ft	

L=

FOREBAY RELEASE NOTCH WIDTH

100-YR NOTCH

Q=CLH^{3/2}

Q ₁₀₀ =	199.7 0	cfs
2% of Q=	3.99 0	cfs
C=	2.6	
H (height of forebay wall)=	1 f	ft
0	2.0	ft

L=

18 in 3 in min.

10 in

3 in min.

North Pond (South Forebay) FOREBAY VOLUME

Req'd V=3% x WQCV

DPM1	Impervious 0.65	Area 40.15	
WQCV=			0.8503 ac-ft
V=			0.0255 ac-ft
Actual V			0.0310 ac-ft

FOREBAY RELEASE NOTCH WIDTH

5-YR NOTCH Q=CLH^{3/2}

Q₁₀₀= 54.8 cfs 2% of Q= 1.10 cfs C= 2.6 H (height of forebay wall)= 1 ft

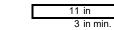
L=

FOREBAY RELEASE NOTCH WIDTH

100-YR NOTCH Q=CLH^{3/2}

L=

Q ₁₀₀ =	119.4 cfs
2% of Q=	2.39 cfs
C=	2.6
H (height of forebay wall)=	1 ft



5 in

3 in min.

WINDERMERE FILING NO. 1 FDR EXCERPT POND DESIGN

South Pond (Forebay) FOREBAY VOLUME

Req'd V=3% x WQCV

From Detention spreadsheet	
WQCV=	0.052 ac-ft
V=	0.0016 ac-ft
Actual V	0.0040 ac-ft

FOREBAY RELEASE NOTCH WIDTH

Q=CLH^{3/2}

Q ₁₀₀ =	17.9 cfs
2% of Q=	0.36 cfs
C=	2.6
H (height of forebay wall)=	1 ft
	-
L=	2 in

3 in min.

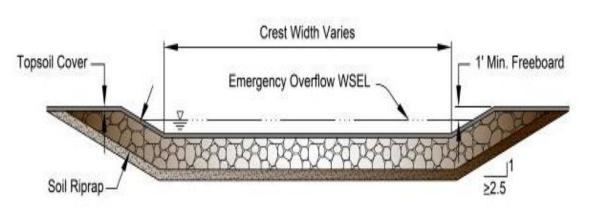
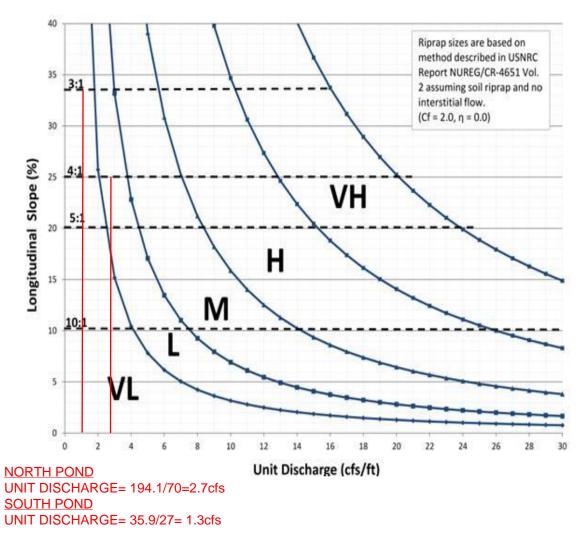


Figure 13-12c. Emergency Spillway Protection

Figure 13-12d. Riprap Types for Emergency Spillway Protection



HYDROLOGIC ANALYSIS

Review C3: Existing drainage map showing all the existing basins and DP is required. This calculation cannot be reviewed until the map is provided.

Review C4: Unresolved. Please provide hydrologic analysis of existing condition.

PROJECT IN	IFORMATION						
PROJECT:	Windermere 2						Ž
PROJECT NO:	21187-03						
DESIGN BY:	KGV					Drexe	, Barrell & Co.
REV. BY:	TDM						
AGENCY:	El Paso County						
REPORT TYPE:	Preliminary						
DATE:	6/5/2024						
Soil Type: A							
			C2*	C5*	C10*	C100*	% IMPERV
Landscape/Law	'n			0.15		0.50	0
Residential (<1/	8 acre)			0.45		0.59	65
Asphalt/Sidewa	lk			0.90		0.96	100
PROPOSED							
SUB-BASIN	SURFACE DESIGNATION	AREA		E RUNOFF CO		1	% IMPERV
		ACRE	C2	C5	C10	C100	
A1	Landscape/Lawn	0.06		0.15		0.50	0
	Residential (<1/8 acre)	6.69		0.45		0.59	65
	Asphalt/Sidewalk	0.04		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL A1		6.79					
A2	Landscape/Lawn	0.88		0.15		0.50	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.03		0.90		0.96	100
	WEIGHTED AVERAGE			0.18		0.52	4%
TOTAL A2		0.92					
			POND		-		
P1	Landscape/Lawn	1.00		0.15		0.50	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.15		0.50	0%
TOTAL P1		1.00					
			FFSITE	1	1		-
B1	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	3.33		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL B1		3.33					
B2	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	0.49		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL B2		0.49					
B4	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	0.16		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL B4		0.16					

ibutary to Pond	12.70					55.0%
Landscape/Lawn	0.00		0.15		0.50	0
Residential (<1/8 acre)	2.73		0.45		0.59	65
Asphalt/Sidewalk	0.00		0.90		0.96	100
WEIGHTED AVERAGE			0.45		0.59	65%
	2.73					
Landscape/Lawn	0.27		0.15		0.50	0
Residential (<1/8 acre)	0.00		0.45		0.59	65
Asphalt/Sidewalk	1.34		0.90		0.96	100
WEIGHTED AVERAGE			0.77		0.88	83%
	1.61					
Landscape/Lawn	0.00		0.15		0.50	0
Residential (<1/8 acre)	0.00		0.45		0.59	65
Asphalt/Sidewalk	0.53		0.90		0.96	100
WEIGHTED AVERAGE			0.90		0.96	100%
	0.53					
Landscape/Lawn	0.63		0.15		0.50	0
Residential (<1/8 acre)	0.00		0.45		0.59	65
Asphalt/Sidewalk	0.00		0.90		0.96	100
WEIGHTED AVERAGE			0.15		0.50	0%
	0.63					
Landscape/Lawn	0.03		0.15		0.50	0
Residential (<1/8 acre)	0.00		0.45		0.59	65
Asphalt/Sidewalk	0.40		0.90		0.96	100
WEIGHTED AVERAGE			0.85		0.93	93%
	0.43					
	Residential (<1/8 acre)	Residential (<1/8 acre)2.73Asphalt/Sidewalk0.00WEIGHTED AVERAGE2.73Landscape/Lawn0.27Residential (<1/8 acre)	Residential (<1/8 acre)	Residential (<1/8 acre) 2.73 0.45 Asphalt/Sidewalk 0.00 0.90 WEIGHTED AVERAGE 0.45 2.73 0.45 Landscape/Lawn 0.27 0.15 Residential (<1/8 acre)	Residential (<1/8 acre)	Residential (<1/8 acre) 2.73 0.45 0.59 Asphalt/Sidewalk 0.00 0.90 0.96 WEIGHTED AVERAGE 0.45 0.59 Landscape/Lawn 0.27 0.15 0.50 Residential (<1/8 acre)

PROJECT INFORMATION

PROJECT: PROJECT NO: DESIGN BY: REV. BY: AGENCY: REPORT TYPE: DATE: Windermere 2 21187-03 KGV TDM El Paso County Preliminary 6/5/2024



RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED TIME OF CONCENTRATION STANDARD FORM SF-2

		SUB-BASI	N			INITIAL/C	VERLAND)		TRAVEL	TIME				PIPE TR	AVEL TIME		TIME OF	CONC.	FINAL
		DATA				TIME (t _i)				(t _t)				(t _p)				t _c		t _c
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	LENGTH	HT	SLOPE	ti	LENGTH	HT	SLOPE	VEL.	t	LENGTH	SLOPE	VEL.	t	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	Ft	%	FPS	Min	tc	tc	Min
A1	1	0.45	0.59	6.79	100	2	3.0	8.4	855	21	3.7	10.1	1.4					9.8	5	9.8
B1		0.45	0.59	3.33	35	1	3.5	4.7	885	30	3.4	10.8	1.4					6.1	5	6.1
B2		0.45	0.59	0.49	50	2	4.0	5.4	725	20	2.8	9.8	1.2					6.6	5	6.6
B1+B2	2	0.45	0.59	3.82	F	rom Basin I	31	6.1						212	0.5	5.1	0.7	6.8	5	6.8
B4		0.45	0.59	0.16	50	17	33.3	2.7	185	3	1.5	4.0	0.8					3.4	5	5.0
P1		0.15	0.50	1.00	100	1	1.0	17.8	205	10	4.8	12.8	0.3					18.0	5	18.0
DP1+DP2+B4+P1	3	0.42	0.58	11.78	From	n Design Po	oint 1	9.8	250	2.5	1.0	4.0	1.0					10.9	5	10.9
D16	4	0.45	0.59	2.73	200	10	5.0	10.1	350	12	3.5	6.5	0.9					11.0	5	11.0
A2		0.18	0.52	0.92	50	10	5.9	6.7	992	25	3.3	8.5	1.9					8.7	5	8.7
NC2	19	0.77	0.88	1.61	50	2	4.0	2.7	1340	35	2.6	9.4	2.4					5.1	5	5.1
EXR		0.90	0.96	0.53	20	2	10.0	0.8	320	6	2.0	4.9	1.1					1.9	5	5.0
C3		0.15	0.50	0.63	60	12	20.0	5.1	455	15	3.3	5.6	1.4					6.4	5	6.4
EXR+C3+DP6+A2	S	0.41	0.61	4.81	From	n Design Po	pint 6	11.0						850	3.0	11.8	1.2	12.2	5	12.2
DP19+DPS	J1	0.50	0.67	6.42	Fron	n Design Po	pint S	12.2						100	1.0	5.9	0.3	12.4	5	12.4
NC1		0.85	0.93	0.43	45	1	2.2	2.4	185	4	2.2	8.7	0.4					2.8	5	5.0
DPJ1+NC1	20	0.52	0.69	6.85	From	Design Po	I	12.4					-	50	1.0	8.4	0.1	12.5	5	12.5

PROJECT INFORMATION	
PROJECT:	Windermere 2
PROJECT NO:	21187-03
DESIGN BY:	KGV
REV. BY:	TDM
AGENCY:	El Paso County
REPORT TYPE:	Preliminary
DATE:	6/5/2024



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RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED	RUNOFF	5	SYR STOR		P1=	1.50	
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
A1	1	6.79	0.45	9.8	3.06	4.13	12.6
B1		3.33	0.45	6.1	1.50	4.84	7.2
B2		0.49	0.45	6.6	0.22	4.72	1.0
B1+B2	2	3.82	0.45	6.8	1.72	4.68	8.1
B4		0.16	0.45	5.0	0.07	5.10	0.4
P1		1.00	0.15	18.0	0.15	3.17	0.5
DP1+DP2+B4+P1	3	11.78	0.42	10.9	5.00	3.97	19.8
D16	4	2.73	0.45	11.0	1.23	3.96	4.9
A2		0.92	0.18	8.7	0.16	4.32	0.7
NC2	19	1.61	0.77	5.1	1.25	5.08	6.3
EXR		0.53	0.90	5.0	0.48	5.10	2.4
C3		0.63	0.15	6.4	0.09	4.76	0.5
Pond Release	Р						0.3
EXR+C3+DP5+POND RELEASE	S	4.81	0.41	12.2	1.96	3.80	7.8
DP19+DPS	J1	6.42	0.50	12.4	3.21	3.76	12.4
NC1		0.43	0.85	5.0	0.36	5.10	1.9
DPJ1+NC1	20	6.85	0.52	12.5	3.57	3.75	13.7

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PROJECT INFORMATION

PROJECT: PROJECT NO: DESIGN BY: REV. BY: AGENCY: REPORT TYPE: DATE: Windermere 2 21187-03 KGV TDM El Paso County Preliminary 6/5/2024



Drexel, Barrell & Co.

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED	RUNOFF	10	0 YR STOF	RM		P1=	2.52
			DIRECT RUNC)FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
A1	1	6.79	0.59	9.8	4.02	6.93	27.9
B1		3.33	0.59	6.1	1.96	8.12	16.0
B2		0.49	0.59	6.6	0.29	7.92	2.3
B1+B2	2	3.82	0.59	6.8	2.25	7.87	17.7
B4		0.16	0.59	5.0	0.09	8.58	0.8
P1		1.00	0.50	18.0	0.50	5.33	2.7
DP1+DP2+B4+P1	3	11.78	0.58	10.9	6.87	6.67	45.8
D16	4	2.73	0.59	11.0	1.61	6.65	10.7
A2		0.92	0.52	8.7	0.48	7.26	3.4
NC2	19	1.61	0.88	5.1	1.42	8.54	12.1
EXR		0.53	0.96	5.0	0.51	8.58	4.4
C3		0.63	0.50	6.4	0.32	8.00	2.5
Pond Release	Р						10.6
EXR+C3+DP5+POND RELEASE	S	4.81	0.61	12.2	2.91	6.38	29.2
DP19+DPS	J1	6.42	0.67	12.4	4.33	6.32	38.0
NC1		0.43	0.93	5.0	0.40	8.58	3.4
DPJ1+NC1	20	6.85	0.69	12.5	4.73	6.29	40.4

HYDRAULIC ANALYSIS

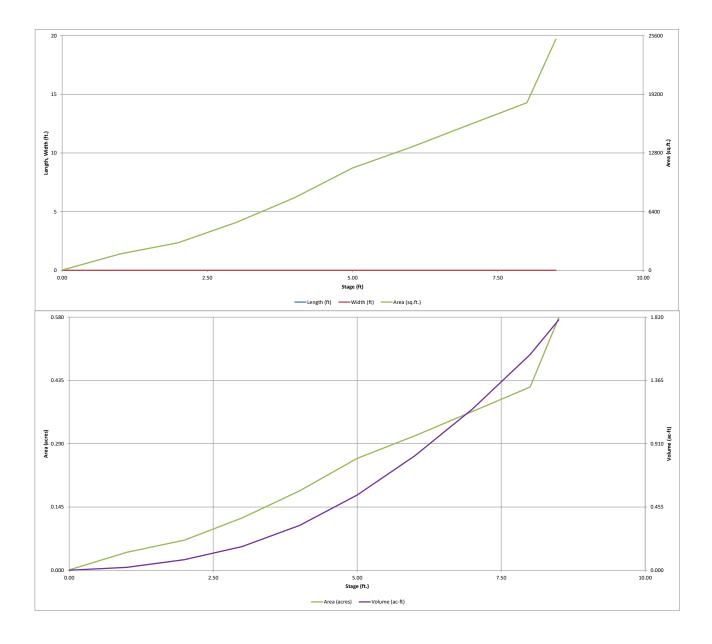
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

		DE	TENTIC		FD-Detention, Version			SLE BU.	ILDER					
Project:	Windermer	e Filing No.	1		D-Delention, versio	0.05 (110	·							
	Pond - Fina	I					_ WI	NDEF	RME	re fi	LING	NO.	. 2 SC	JUTI
	2 ONE 1			~			FIN	AL D	ESIG	N DI	EVEL	OPEI	D CO	NDI
e e e e e e e e e e e e e e e e e e e		100-YEA	AR		Donth Increment -].							
	1 AND 2	ORIFICE	E		Depth Increment =		Optional				Optional			
POOL Example Zone	Configurati	on (Retentio	on Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Watershed Information					Top of Micropool		0.00				40	0.001	(12)	(de le)
Selected BMP Type =	EDB	1			6574		1.00				1,801	0.041	920	0.021
Watershed Area =	12.79	acres			6575		2.00				3,008	0.069	3,325	0.076
Watershed Length =	1,000	ft			6576		3.00				5,232	0.120	7,445	0.171
Watershed Length to Centroid =	350	ft			6577		4.00				7,923	0.182	14,022	0.322
Watershed Slope =	0.040	ft/ft			6578		5.00				11,161	0.256	23,564	0.541
Watershed Imperviousness = Percentage Hydrologic Soil Group A =	54.90% 100.0%	percent percent			6579 6580		6.00 7.00				13,425 15,853	0.308	35,857 50,496	0.823
Percentage Hydrologic Soil Group B =	0.0%	percent			6581		8.00				18,293	0.420	67,569	1.551
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			6581.5		8.50				25,208	0.579	78,445	1.801
Target WQCV Drain Time =	40.0	hours												
Location for 1-hr Rainfall Depths =	User Input													
After providing required inputs above inc depths, click 'Run CUHP' to generate run														
the embedded Colorado Urban Hydro	graph Procedu	ure.	Optional Use	r Overrides										
Water Quality Capture Volume (WQCV) =	0.235	acre-feet		acre-feet										
Excess Urban Runoff Volume (EURV) =	0.831	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) =	0.593	acre-feet	1.19	inches										
5-yr Runoff Volume (P1 = 1.5 in.) =	0.785	acre-feet	1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	0.938	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) = 50-yr Runoff Volume (P1 = 2.25 in.) =	1.163	acre-feet acre-feet	2.00	inches inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	1.560	acre-feet	2.25	inches										
500-yr Runoff Volume (P1 = 3.49 in.) =	2.617	acre-feet	3.49	inches										
Approximate 2-yr Detention Volume =	0.537	acre-feet												
Approximate 5-yr Detention Volume =	0.705	acre-feet												
Approximate 10-yr Detention Volume =	0.856	acre-feet acre-feet												
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	1.157	acre-feet												
Approximate 100-yr Detention Volume =	1.289	acre-feet												
		-												
efine Zones and Basin Geometry		-												
Zone 1 Volume (WQCV) =	0.235	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	0.596	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	0.458	acre-feet acre-feet												
Initial Surcharge Volume (ISV) =	user	ft ³												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth (H _{total}) =	user	ft												
Depth of Trickle Channel (H_{TC}) =	user	ft												
Slope of Trickle Channel (S_{TC}) =	user	ft/ft												
Slopes of Main Basin Sides (S _{main}) =	user	H:V												
Basin Length-to-Width Ratio $(R_{L/W}) =$	user													
Initial Surcharge Area $(A_{ISV}) =$	user	ft 2												
Surcharge Volume Length $(L_{ISV}) =$	user	ft												
Surcharge Volume Width (W _{ISV}) =	user	ft												
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft												
Length of Basin Floor (L _{FLOOR}) =	user	ft												
Width of Basin Floor (W_{FLOOR}) = Area of Basin Floor (A_{FLOOR}) =	user	ft ft²												
Area of Basin Floor (A _{FLOOR}) = Volume of Basin Floor (V _{FLOOR}) =	user	ft ² ft ³											-	
Depth of Main Basin (H _{MAIN}) =	user	ft												
Length of Main Basin $(L_{MAIN}) =$	user	ft												
Width of Main Basin (W_{MAIN}) =	user	ft												
Area of Main Basin (A _{MAIN}) =	user	ft ²												
Volume of Main Basin (V _{MAIN}) = Calculated Total Basin Volume (V _{total}) =	user	ft ³ acre-feet												
conculated Total basin volume (v _{total}) =	user													
														<u> </u>
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													1	
												L		

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

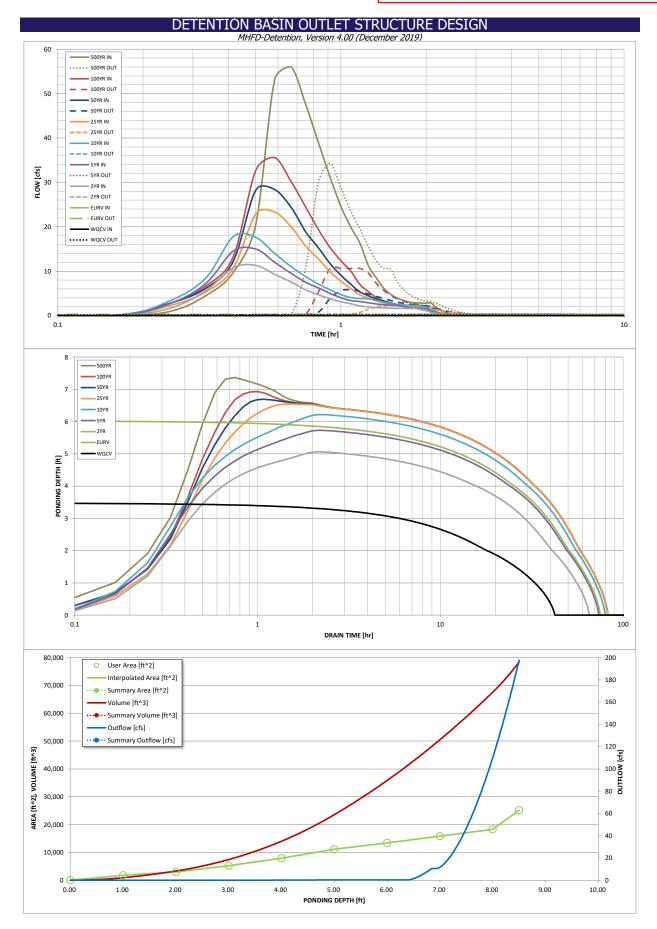
WINDERMERE FILING NO. 2 SOUTH POND FINAL DESIGN DEVELOPED CONDITION



WINDERMERE FILING NO. 2 SOUTH POND FINAL DESIGN DEVELOPED CONDITION

		:TENTION							
Project	Windermere Filing		IHFD-Detention, V	ersion 4.03 (May .	2020)				
	Pond - Final	NO. 1							
ZONE 3	Folia - Filiai								
ZONE 2 ZONE 1	\frown			Estimated	Estimated				
100-YR VOLUME EURY WOOL				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	3.48	0.235	Orifice Plate			
	100-YEAR		Zone 2 (EURV)	6.03	0.596	Orifice Plate			
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	7.35	0.458	Weir&Pipe (Restrict)			
T ETHIOTELT	Configuration (Re	tention Pond)	2011e 5 (100-year)			wend pe (Resulet)			
	•			Total (all zones)	1.289]			
User Input: Orifice at Underdrain Outlet (typical	<u>y used to drain WQ</u>			<i>.</i> .				ters for Underdrain	<u>l</u>
Underdrain Orifice Invert Depth =			the filtration media	surface)		Irain Orifice Area =		ft ²	
Underdrain Orifice Diameter =		inches			Underdrain	Orifice Centroid =		feet	
User Input: Orifice Plate with one or more orific							Calculated Parame		
Invert of Lowest Orifice =	0.00	ft (relative to basir	bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =	6.03	ft (relative to basir	bottom at Stage =	= 0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	24.10	inches			Ellipti	ical Slot Centroid =		feet	
Orifice Plate: Orifice Area per Row =	N/A	inches			E	lliptical Slot Area =	N/A	ft ²	
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to high	<u>est)</u>						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)]
Stage of Orifice Centroid (ft)		2.01	4.02						1
Orifice Area (sq. inches)	1.10	1.70	2.00						1
									-
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)			(optional)			now in (optional)	(optional)	now to (optional)	
Orifice Area (sq. inches)									1
Office Area (sq. incres)									1
User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Ori	fice
oser input. Vertical office (circular of freedally	Not Selected	Not Selected	1				Not Selected	Not Selected	1
			0 . (hattan at Chara	0.00	tiant Ouifing Aug			
Invert of Vertical Orifice =	N/A		ft (relative to basir	-	,	tical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A		ft (relative to basir	bottom at Stage =	= 0 π) Vertica	Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Tranezoid	al Mair (and No Ou			Coloulated Davama		
	· ·			ai weir (and No Ou	<u>itiet Pipe)</u>		Calculated Paralite	ters for Overflow W	<u>Veir</u>
	Zone 3 Weir	Not Selected			<u>itiet Pipe)</u>		Zone 3 Weir	Not Selected	<u>Veir</u>
Overflow Weir Front Edge Height, Ho =	· ·	Not Selected	ft (relative to basin b			e Upper Edge, H _t =			<u>Veir</u>]]feet
	Zone 3 Weir	Not Selected N/A			t) Height of Grate		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 6.40	Not Selected N/A N/A	ft (relative to basin t	pottom at Stage = 0 f	t) Height of Grate	e Upper Edge, H _t = /eir Slope Length =	Zone 3 Weir 6.40	Not Selected N/A	feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	Zone 3 Weir 6.40 3.92 0.00	Not Selected N/A N/A N/A	ft (relative to basin t feet H:V	oottom at Stage = 0 f Gr	t) Height of Grate Overflow W ate Open Area / 10	e Upper Edge, H _t = /eir Slope Length = 10-yr Orifice Area =	Zone 3 Weir 6.40 3.92 14.68	Not Selected N/A N/A N/A	feet feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 6.40 3.92 0.00 3.92	Not Selected N/A N/A N/A N/A	ft (relative to basin t feet H:V feet	oottom at Stage = 0 f Gr Ov	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open	e Upper Edge, H _t = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 6.40 3.92 14.68 10.78	Not Selected N/A N/A N/A N/A	feet feet ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 6.40 3.92 0.00 3.92 70%	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %, grate open are	oottom at Stage = 0 f Gr Ov	t) Height of Grate Overflow W ate Open Area / 10	e Upper Edge, H _t = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 6.40 3.92 14.68	Not Selected N/A N/A N/A	feet feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 6.40 3.92 0.00 3.92	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet	oottom at Stage = 0 f Gr Ov	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open	e Upper Edge, H _t = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 6.40 3.92 14.68 10.78	Not Selected N/A N/A N/A N/A	feet feet ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50%	Not Selected N/A N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %, grate open are %	oottom at Stage = 0 f Gr Ov	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	e Upper Edge, $H_t =$ leir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39	Not Selected N/A N/A N/A N/A N/A	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% • (Circular Orifice, R	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R	ft (relative to basin t feet H:V feet %, grate open are %	oottom at Stage = 0 f Gr Ov	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	e Upper Edge, H _t = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% <u>(Circular Orifice, R</u> Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected	ft (relative to basin t feet H:V feet %, grate open are % ectangular Orifice)	אסטנטש at Stage = 0 f Gr סע a/total area C	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open	e Upper Edge, H _t = leir Slope Length = l0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameters	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/ Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% 20% 20m 3 Restrictor 2.50	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba	אסטנטש at Stage = 0 f Gr סע a/total area C	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	e Upper Edge, H _t = (eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameters</u> utlet Orifice Area =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/ Zone 3 Restrictor 0.73	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A	feet feet ft ² ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% (<u>Circular Orifice, R</u> Zone 3 Restrictor 2.50 18.00	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba inches	bottom at Stage = 0 f Gr Ot a/total area C asin bottom at Stage	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Or Outlet	e Upper Edge, H _t = eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameters</u> utlet Orifice Area = t Orifice Centroid =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/ Zone 3 Restrictor 0.73 0.38	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A N/A	feet feet ft ² ft ² ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% <u>(Circular Orifice, R</u> Zone 3 Restrictor 2.50	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba	bottom at Stage = 0 f Gr Ot a/total area C asin bottom at Stage	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	e Upper Edge, H _t = eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameters</u> utlet Orifice Area = t Orifice Centroid =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/ Zone 3 Restrictor 0.73	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A	feet feet ft ² ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% C(Circular Orifice, R Zone 3 Restrictor 2.50 18.00 7.80	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba inches	bottom at Stage = 0 f Gr Ot a/total area C asin bottom at Stage	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Or Outlet	e Upper Edge, H _t = leir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = liculated Parameters utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 s for Outlet Pipe w/ Zone 3 Restrictor 0.73 0.38 1.44	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A N/A N/A	feet feet ft ² ft ² ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% Cicrcular Orifice, R Zone 3 Restrictor 2.50 18.00 7.80 Trapezoidal)	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba inches inches	oottom at Stage = 0 f Gr Ov a/total area C asin bottom at Stage Half-Cent	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open <u>Ca</u> = 0 ft) Or Outlet ral Angle of Restric	e Upper Edge, H _t = leir Slope Length = I0-yr Orlfice Area = Area w/o Debris = n Area w/ Debris = liculated Parameters utlet Orlfice Area = t Orlfice Centroid = tor Plate on Pipe =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 5.39 5 for Outlet Pipe w/ Zone 3 Restrictor 0.73 0.38 1.44 <u>Calculated Parame</u>	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A N/A N/A N/A	feet feet ft ² ft ² ft ² ft ²
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% Cicrcular Orifice, R Zone 3 Restrictor 2.50 18.00 7.80 Trapezoidal)	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ft (relative to basin t feet H:V feet %, grate open are % <u>ectangular Orifice)</u> ft (distance below ba inches inches	oottom at Stage = 0 f Gr Ov a/total area C asin bottom at Stage Half-Cent	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Nverflow Grate Open Dverflow Grate Open <u>Ca</u> = 0 ft) Oi Outlet ral Angle of Restric Spillway D	e Upper Edge, H _t = leir Slope Length = I0-yr Orlfice Area = Area w/o Debris = n Area w/ Debris = liculated Parameters utlet Orlfice Area = t Orlfice Centroid = tor Plate on Pipe =	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 5.39 5 for Outlet Pipe w/ Zone 3 Restrictor 0.73 0.38 1.44 Calculated Parame 0.55	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A N/A N/A N/A	feet feet ft ² ft ² ft ² ft ²
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = NeeHour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Plow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Zone 3 Weir 6.40 3.92 0.00 3.92 70% 50% C(ircular Orifice, R Zone 3 Restrictor 2.50 18.00 7.80 Trapezoidal) 6.94 27.00 4.00 1.00 The user can over: WQCV N/A 0.235 N/A N/A N/A N/A N/A Plate N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet ide the default CU/ EURV N/A 0.831 N/A	ft (relative to basin the feet H:V feet %, grate open are % ectangular Orifice) ft (distance below basin inches inches the bottom at Stage = het hydrographs and 2 Year 1.19 0.593 0.593 0.593 0.1 	xottom at Stage = 0 f Gr Ov a/total area C asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0.785 = 0.785 = 0.785 = 0.785 = 0.785 = 0.3 = 0.02 = 15.0 = 0.3 = 1.1 Plate N/A N/A 64	t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Neerflow Grate Open Diverflow Grate Open Call = 0 ft) Or Stage at T Basin Area at T Basin Area at T Basin Volume at T Contention Diversion Call Basin Volume at T Contention Diversion Call Call Call Call Call Call Call Cal	e Upper Edge, H _t = leir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth = rop of Freeboard = 0 of Freeboard = 2.00 1.1.63 1.163 3.3 0.7 0.26 2.3.3 2.3 0.7 Overflow Weir 1 0.2 N/A 69	Zone 3 Weir 6.40 3.92 14.68 10.78 5.39 5.39 5.39 5.07 0.73 0.38 1.44 Calculated Parame 0.55 8.49 0.58 1.80 Calculated Parame 0.55 0.58 1.80 Calculated Parame 0.55 0.73 0.58 1.80 Calculated Parame 0.55 0.73 0.58 1.80 Calculated Parame 0.55 0.58 0.58 0.9 Overflow Weir 1 0.5 N/A 67	Not Selected N/A N/A N/A N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft cumns W through . 100 Year 2.52 1.660 1.660 1.660 1.660 1.0.4 0.81 35.6 10.6 1.0 Outlet Plate 1 1.0 N/A 65	feet feet ft ² ft ² feet radians 500 Year 2.617 2.55 500 3.4.3 55.0 3.4.3 55.0 3.4.3 55.0 3.5 55.0 55 500 3.4.3 55.0 55 55 55 55 55 55 55 55 55 55 55 55 55

WINDERMERE FILING NO. 2 SOUTH POND FINAL DESIGN DEVELOPED CONDITION



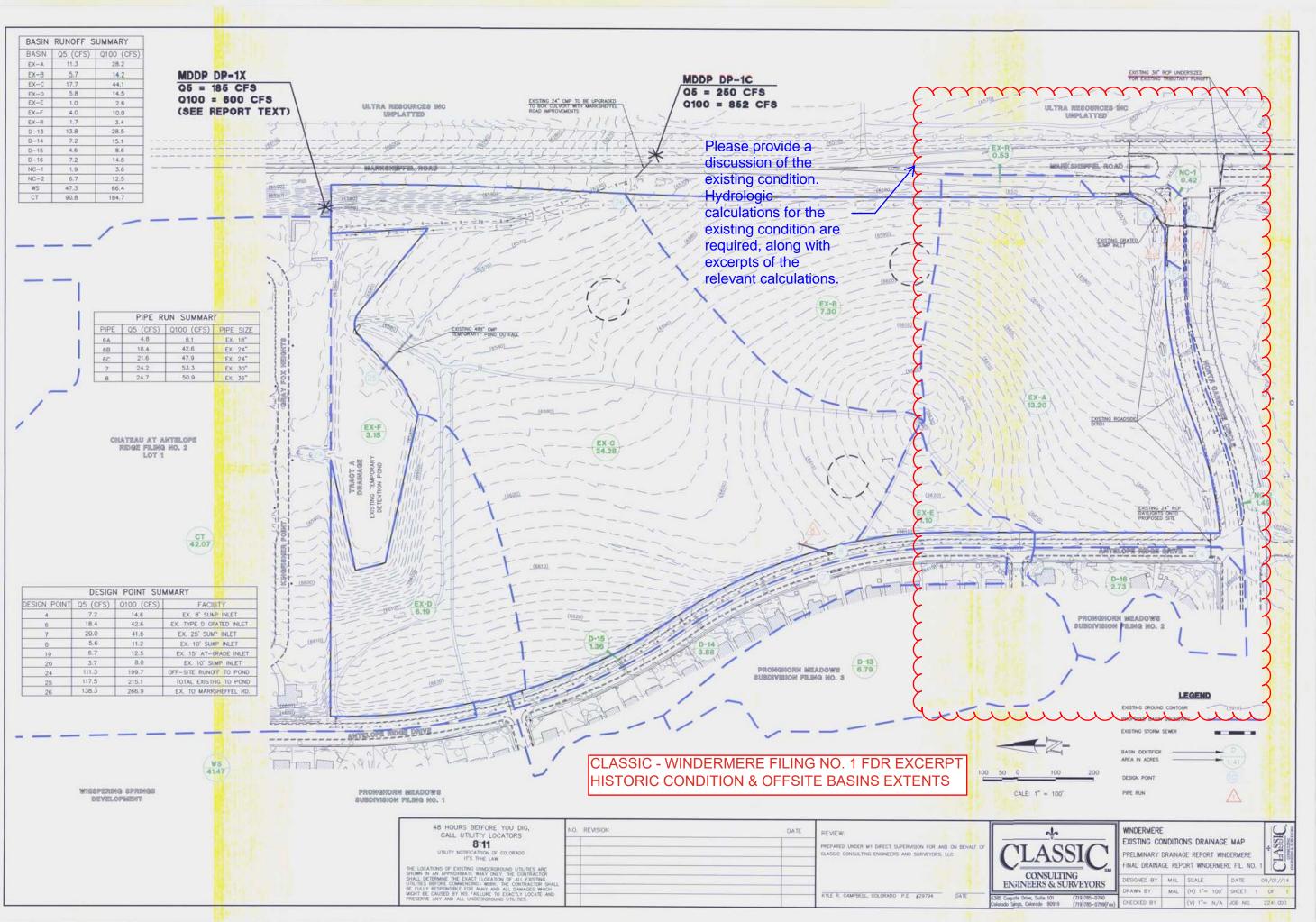
WINDERMERE FILING NO. 2 SOUTH POND FINAL DESIGN DEVELOPED CONDITION

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
ne Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cf
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.19	0.02	0.95
	0:15:00	0.00	0.00	1.68	2.73	3.39	2.28	2.81	2.79	4.49
	0:20:00	0.00	0.00	5.61	7.23	8.47	5.32	6.15	6.66	9.68
	0:25:00 0:30:00	0.00	0.00	10.75 11.32	14.52 14.97	17.75 17.61	10.67 22.87	12.20 28.23	13.26 32.69	20.56 53.10
	0:35:00	0.00	0.00	9.30	14.97	17.01	23.34	28.23	35.57	55.97
	0:40:00	0.00	0.00	7.55	9.51	11.03	20.01	24.38	30.21	47.63
	0:45:00	0.00	0.00	5.82	7.52	8.79	15.67	18.93	24.52	38.91
	0:50:00	0.00	0.00	4.67	6.22	7.11	12.74	15.26	19.35	31.09
	0:55:00	0.00	0.00	3.80	5.00	5.79	9.84	11.69	15.27	24.59
	1:00:00	0.00	0.00	3.09	4.02	4.72	7.73	9.07	12.35	19.94
	1:05:00	0.00	0.00	2.65 2.19	3.40 3.15	4.07	6.08 4.64	7.06	10.03 7.03	16.32 11.24
	1:15:00	0.00	0.00	1.94	2.90	3.85 3.78	3.95	4.48	5.42	8.50
	1:20:00	0.00	0.00	1.80	2.64	3.47	3.31	3.74	4.04	6.17
	1:25:00	0.00	0.00	1.71	2.47	3.02	2.93	3.30	3.20	4.77
	1:30:00	0.00	0.00	1.66	2.36	2.72	2.51	2.83	2.71	3.93
	1:35:00	0.00	0.00	1.63	2.30	2.53	2.25	2.54	2.38	3.37
	1:40:00	0.00	0.00	1.60	2.01	2.40	2.09	2.35	2.17	3.03
	1:45:00 1:50:00	0.00	0.00	1.59 1.59	1.81 1.69	2.32 2.26	1.99 1.93	2.23 2.17	2.07	2.87 2.82
	1:55:00	0.00	0.00	1.39	1.69	2.26	1.95	2.17	2.04	2.82
	2:00:00	0.00	0.00	1.13	1.50	1.92	1.88	2.13	2.02	2.80
	2:05:00	0.00	0.00	0.72	0.96	1.24	1.21	1.36	1.30	1.79
	2:10:00	0.00	0.00	0.45	0.60	0.78	0.77	0.86	0.82	1.13
	2:15:00	0.00	0.00	0.27	0.37	0.48	0.47	0.53	0.50	0.69
	2:20:00	0.00	0.00	0.15	0.22	0.28	0.28	0.31	0.30	0.41
	2:25:00	0.00	0.00	0.08	0.12	0.15	0.16	0.18	0.17	0.23
	2:30:00 2:35:00	0.00	0.00	0.03	0.06	0.06	0.07	0.08	0.07	0.10
	2:40:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00 3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00 3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DRAINAGE MAPS



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