Drainage Letter Report

#### PRELIMINARY DRAINAGE REPORT

for

#### WINDERMERE FILING NO. 2

Colorado Springs, CO

April 6, 2022

**Engineering Review** 

07/14/2022 11:54:52 AM

dsdrice

JeffRice@elpasoco.com

(719) 520-7877

EPC Planning & Community Development Department

#### Prepared for:

Colo Windermere #2, LLC

4164 Austin Bluffs Parkway, #361 Colorado Springs, CO 80918 Contact: James Todd Stephens

Prepared by:

Drexel, Barrell & Co.

3 South Seventh Street Colorado Springs, CO 80905 Contact: Tim McConnell, P.E. (719) 260-0887

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### PRELIMINARY DRAINAGE REPORT

for

#### WINDERMERE FILING NO. 2

Colorado Springs, Colorado

#### 1.0 CERTIFICATION STATEMENTS

#### **ENGINEER'S STATEMENT**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E.	Date
Colorado P.E. License No. 33797	
For and on Behalf of Drexel, Barrell & Co.	

#### **DEVELOPER'S STATEMENT**

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name:	Colo Windermere #2, LLC		
By:			
•	James Todd Stephens	Date	
Title:	Owner		
Address:	4164 Austin Bluffs Parkway, #361		
	Colorado Sprinas, CO 80918		

#### **EL PASO COUNTY**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.	County Engineer/ECM Administrator	Date
CONDITIONS	delete	

## PRELIMINARY DRAINAGE REPORT

for

### WINDERMERE FILING NO. 2

Colorado Springs, Colorado

#### 2.0 PURPOSE

This report is prepared by Drexel, Barrel & Co in support of the Windermere Filing No. 2 subdivision. The purpose of this report is to identify onsite and offsite drainage patterns, storm sewer, inlet locations, and areas tributary to the site, and to safely route developed storm water runoff to adequate outfall facilities.

#### 3.0 GENERAL SITE DESCRIPTION

#### Location

The site is located at the northwest corner of N. Carefree Cir. and Marksheffel Rd. - the E 1/2 of Section 29, Township 13 S, Range 65 W of the 6th P.M., El Paso County, Colorado.

The site is bound on the west by Antelope Ridge Dr., on the north by the Windermere Filing No. 1 subdivision (Mardale Lane), on the east by Marksheffel Rd., and on the south by N. Carefree Cir.

#### Site Conditions

The site is approximately 9.26 acres in size and is proposed as a multi-family home subdivision. The proposed site development includes approximately 200 multi-family units. The site has recently been overlot graded, seeded and mulched as part of the Windermere Filing No. 1 development to the north. The site is located within the Sand Creek Drainage Basin. Historically, this site drains to the southeast towards the intersection of N. Carefree Circle and Marksheffel Road.

This site was studied as part of the approved Preliminary Drainage Report for Windermere & Final Drainage Report for Windermere Filing No. 1, by Classic Consulting (October 2014) and the more recently approved Final Drainage Report for Windermere Filing No. 1, by Drexel, Barrell & Co. (April 2022).

#### <u>Soils</u>

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S. Department of Agriculture Soil Conservation Service, the site is underlain by Truckton sandy loam, a type 'A' hydrologic soil. See appendix for map.

#### Climate

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the

majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

#### Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel #08041C0543 G (December 7, 2018) the project site is within a designated Zone X area described as "area of minimal hazard". A firmette map is included in the appendix.

#### 4.0 HISTORIC HYDROLOGY

Refer to an excerpt in the appendix for historic condition drainage map.

Existing Design Point 6 (DP-6-EX) covers runoff from DP-4-EX, Basin EX-R, and Basin EX-A.

- Design Point DP-4-EX consists of runoff from off-site Basin D-16, that discharges onto the Windermere property in the southwest corner and travels via roadside ditch towards DP-6-EX with runoff rates of  $Q_5$ =4.9 cfs and  $Q_{100}$ =10.7 cfs.
- EX-R is 0.53 acres of existing Marksheffel Road and roadside ditch that drains to the existing grated area drain at DP-6. ( $Q_5=2.4$  cfs and  $Q_{100}=4.4$  cfs)
- Basin EX-A is 13.20 acres of Windermere property with historic runoff of  $Q_5$ =14.5 cfs and  $Q_{100}$ =34.2 cfs.

Runoff rates of  $Q_5$ =18.5 cfs and  $Q_{100}$ =41.8 cfs reach the existing area drain at DP-6-EX in the historic condition. As discussed in the Classic Consulting report referenced above, the existing 24" storm sewer that exits this area drain appears to have been undersized, as the capacity of the existing 24" RCP pipe at 0.5% grade is only 17.2 cfs.

Existing Design Point 19 (DP-19-EX) consists of runoff from off-site basin NC-2 ( $Q_5$ =6.5 cfs and  $Q_{100}$ =11.8 cfs). An existing 15' Type R at-grade curb inlet just west of the intersection of N. Carefree Circle and Marksheffel Road intercepts a portion of this runoff ( $Q_5$ =4.8 cfs and  $Q_{100}$ =8.1 cfs) and discharges to the east via public 18" RCP storm sewer. Bypass flows continue to the east towards DP-20-EX.

Existing Design Point 20 (DP-20-EX) consists of basin runoff from basin NC-1, flowby from the at-grade inlet at DP-19-EX and pipe flow from DP-6-EX. An existing 10' Type R sump inlet intercepts all the surface runoff and combines it with the upstream flows from DP-6-EX and DP-19-EX inlet capture. Total historic runoff at this location is  $Q_5$ =24.5 cfs and  $Q_{100}$ =52.6 cfs. This runoff is captured in its entirety and continues within the existing Marksheffel Road storm system to the south.

#### 5.0 EXISTING HYDROLOGY

As described above, the Windermere Filing No. 2 site was overlot graded as part of the Windermere Filing No. 1 development. A full-spectrum detention facility was designed as part of the Filing No.1 Final Drainage Report, and in order to minimize future grading within the detention facility area, the volume was based on assumed final build-out

watershed imperviousness of 68%. Comparison between the original design and this proposed condition is further described below.

#### 6.0 PROPOSED HYDROLOGY & HYDRAULIC SUMMARY

The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals. Mile High Flood District design software (MHFD-Detention v.4.03) and Flowmaster were used to identify pond and storm system sizing, and inlet capacity charts from the current drainage criteria manual used for inlet sizing (see appendix for calculations). See below for a summary runoff table and description of each design point.

#### **Rational Method Runoff Summary**

BASIN	AREA (AC)	Q5 (cfs)	Q100 (cfs)
A1	2.90	7.3	15.3
A2	3.29	6.4	13.4
B1	3.33	7.2	16.0
B2	0.49	1.0	2.3
B4	0.16	0.4	0.8
P1	1.00	0.5	2.7
D16	2.73	4.9	10.7
A3	1.61	1.4	6.1
NC2	1.61	6.3	12.1
EXR	0.53	2.4	4.4
C3	0.63	0.5	2.5
Pond Release	0.00	0.3	10.6
NC1	0.43	1.9	3.4

Design Point 1 represents the flows generated by basin A1 ( $Q_5$ =7.3 cfs and  $Q_{100}$ =15.3 cfs). These flows are captured by a proposed public 10' Type R sump inlet located at the low point of the proposed roadway.

Design Point 2 represents the surface flows generated by basin A2 ( $Q_5$ =6.4 cfs and  $Q_{100}$ =13.4 cfs), and the piped flows from DP1. The surface flows will be captured in their entirety by a proposed 10' Type R sump inlet located at the low point in the proposed roadway. These flows then combine with the piped flows from DP1, for a total flow of  $Q_5$ =12.1 cfs and  $Q_{100}$ =25.4 cfs, that will be discharged to the north via public 24" RCP storm sewer.

Design Point 3 covers flow from offsite basins B1 and B2, combined with onsite DP2. Flows of  $Q_5$ =18.2 cfs and  $Q_{100}$ =38.8 cfs travel via the existing private 24" RCP storm sewer to the east and discharge into the north end of the detention facility.

# Does this drain onto the property? If so, would it go to DP S, not into the pond?

Design Point 4 represents all flows reaching the existing detention facility (Basins B4, P1 and DP3) for a total flow of  $Q_5$ = 18.4cfs and  $Q_{100}$ =41.1cfs. The existing detention facility and modifications for this developed condition are described further below,

Design Point 5 is identical to DP-4-EX in the historic condition, and represents flows ( $Q_5$ = 4.9cfs and  $Q_{100}$ =10.7cfs) from offsite basin D16 that discharges on to the Windermere property. In the developed condition, it is proposed that the 24" RCP be extended to allow for the flow to be piped to the east and the roadside ditch removed.

Design Point 19 is equivalent to DP-19-EX, and consists of run off from off-site basin NC-2 and basin A3, for a total flow of  $Q_5$ = 6.7cfs and  $Q_{100}$ =16.3cfs) An existing 15' Type R atgrade curb inlet just west of the intersection of N. Carefree Circle and Marksheffel Road intercepts a portion of this runoff ( $Q_5$ =4.8 cfs and  $Q_{100}$ =8.1 cfs) and discharges to the east via public 18" RCP storm sewer.

Design Point S is located at the same existing areal/inlet as DP-6-EX. In the developed condition flows reaching this point, from basins EXR and C3, Design Point 6 and the pond release rate equate to  $Q_5$ = 7.1 cfs and  $Q_{100}$ =26.1 cfs. Far less than the  $Q_5$ =18.5 cfs and  $Q_{100}$ =41.8 cfs in the historic condition. As identified in the historic analysis of this design point, the existing 24" storm sewer exiting the area inlet is currently undersized. In this developed condition, the reduction in flows will allow for this existing pipe to function within capacity.

Design Point J1 is located at the existing manhole on the north side of N. Carefree Circle and represents the combining of flows from DP-19 and DP-S. Flows of  $Q_5$ = 12.9 cfs and  $Q_{100}$ =40.3 cfs continue to the south via 30" RCP towards DP-20.

Design Point 20 (equivalent to DP-EX-20) as in the existing condition consists of surface runoff from basin NC-1, flowby from the at-grade inlet at DP-19 and pipe flow from DP-J1. An existing 10' Type R sump inlet intercepts all the surface runoff and combines it with the upstream flows from DP-J1 and DP-19 existing at-grade inlet capture. Total developed runoff at this location is  $Q_5$ =14.3 cfs and  $Q_{100}$ =42.7 cfs, significantly less that the historic  $Q_5$ =24.5 cfs and  $Q_{100}$ =52.6 cfs. This runoff continues within the existing Marksheffel Road storm system to the south.

#### 7.0 EXISTING DETENTION/WATER QUALITY FACILITY

As part of the overlot design for Windermere Filing No. 1, the detention pond located in the southeast corner of the property was designed as a full-spectrum detention facility to capture flows from the Windermere Filing No. 2 basins.

In order to minimize future grading within the detention facility area, the volume was based on an assumed final build-out watershed imperviousness of 68.0%, which considered Windermere Filing No. 2 (Windermere Filing No. 1 – Tract B) as potentially higher density than single-family residential. As part of the Windermere Filing 1 overlot grading, the pond was excavated to full volume and the outlet structure and associated piping installed. An interim orifice plate (assuming full developed condition within the

street right-of-way, but no further development) was installed to allow for appropriate WQCV drain time. The orifice plate will need to be switched out to allow for discharge of the developed flows, and the restrictor plate raised to 7.80" above the invert of the 18" outfall pipe. No other portion of the detention facility will need to be modified.

Based on the analysis in this report, the developed condition encompasses a total of 12.79 acres that is tributary to this existing facility, with a composite imperviousness of 54.9% for the final fully developed condition. Required volumes are listed below.

		Required Volume						
	Imperviousness	WQCV EURV 100-YR						
FINAL	54.9%	0.24	0.83	1.29				

The actual pond volume at the proposed spillway stage is 1.15 acre-feet. A concrete forebay with an energy dissipater has been installed where the flows enter the pond. The volume of the forebay was designed for 3% of the WQCV volume for the pond, as is still within that limit for this final design condition. The flows exit the forebay through a notch, discharging into the concrete trickle channel at the bottom of the pond. The trickle channel conveys the flows to the micropool. The outlet structure then releases the flows at a reduced flow rate with the use of a plate with orifice holes, into a proposed 18" pipe with restrictor plate, discharging into an existing storm inlet at the corner of N. Carefree Circle and Marksheffel Rd, after which the flows continue to the south via the existing storm sewer system.

In accordance with El Paso County criteria, the modified Type C outlet structure with a permanent micropool will release the WQCV over a 40-hour period. Switching out of the orifice plate will ensure that the WQCV release rate remains within criteria for the final developed condition. The outlet structure will remain in place for the final condition and will result in release rates of  $Q_5$ =0.3 cfs and  $Q_{100}$ =10.6 cfs. For comparison, the existing basin EX-A released flow rates of  $Q_5$ =11.3 cfs and  $Q_{100}$ =28.2 cfs.

A 27-ft wide riprap emergency spillway is located on the south side of the pond. In the event that water overtops the spillway, flow will discharge into existing area inlet at the intersection of N. Carefree Cir and Marksheffel Rd, where it is then picked up by the existing storm system.

All detention facility calculations, including excerpts for forebay volumes, micropool surface areas, outlet structures, discharge pipes and spillway design are provided in the appendix.

The pond has a 15' wide maintenance access that provides access to the pond bottom, forebay and outlet structure per ECM 3.3.3.K. A private maintenance agreement and O&M manual has been established for this pond as required by the County.

#### 8.0 FOUR-STEP PROCESS

This project conforms to the City of Colorado Springs/El Paso County Four Step Process. The process focuses on reducing runoff volumes, treating the water quality capture

volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

- 1. **Employ Runoff Reduction Practices:** Proposed impervious areas on this site (roofs, asphalt/sidewalk) will sheet flow across landscaped ground as much as possible to slow runoff and increase time of concentration prior to being conveyed to the proposed public streets and storm sewer system. This will minimize directly connected impervious areas within the project site.
- 2. Implement BMP's that provide a Water Quality Capture Volume with slow release: Runoff from this project will be treated through capture and slow release of the WQCV in apermanent Extended Detention Basin designed per current City of El Paso County drainage criteria.
- 3. **Stabilize Drainage Ways:** Flows from the detention facility are released directly into the existing storm sewer system and no stabilization will be necessary.
- 4. Implement Site Specific and Other Source Control BMP's: The site is proposed as a residential development, and as such standard household source control will be utilized in order to minimize potential pollutants entering the storm system. Example source control measures consist of: garages for storage of household chemicals, trash receptacles for individual households and in common areas for pet waste. The need for Industrial and Commercial BMP's was considered, however per ECM I.7.2.A the need for industrial and commercial BMPs are not applicable for this project.

#### 9.0 GEOTECHNICAL HAZARDS

In accordance with geotechnical recommendations, the project design is intended to direct runoff away from structures, and into the receiving storm sewer system and water quality/detention basins. This will be accomplished by a variety of means, i.e. curb and gutter and storm sewer. Per "Soils and Geology Study, Windermere Subdivision" by RMG, October 26, 2020 (Revised January 18, 2021), and updated with an addendum for Tract B (March 30, 2022)

#### 10.0 FACILITY MAINTENANCE

Ownership and maintenance of all public facilities, generally located within the public right-of-way will be by El Paso County. Ownership and maintenance of all tracts and private facilities will be by the Sands Metropolitan District #4.

#### 11.0 CONSTRUCTION COST ESTIMATE

Construction cost estimate will be provided with the Final Drainage Report.

#### 12.0 DRAINAGE/BRIDGE FEES

Drainage/Bridge fees will be provided with the Final Drainage Report.

Provide calculation - see comment letter

#### 13.0 CONCLUSIONS

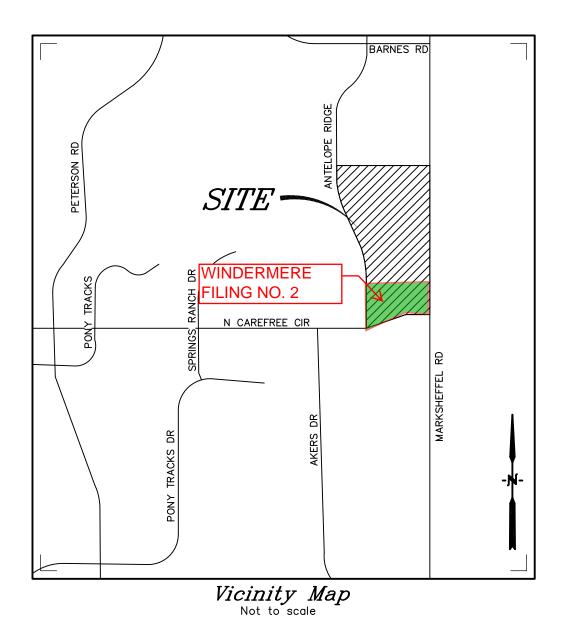
The Windermere Filing No. 2 project has been designed in accordance with El Paso County criteria. The detention facility has been designed to limit the release of storm runoff. This development will not negatively impact or increase flows in the downstream facilities.

#### 14.0 REFERENCES

The sources of information used in the development of this study are listed below:

- 1. City of Colorado Springs "Drainage Criteria Manual", 2016.
- 2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised October 2019.
- 3. Soil Survey for Colorado Springs and El Paso County, Colorado, U.S. Department of Agriculture, Soil Conservation Service, June 1980.
- 4. "Flood Insurance Studies for Colorado Springs and El Paso County, Colorado", prepared by the Federal Emergency Management Agency (FEMA), 2018.
- 5. "Soils and Geology Study, Windermere Subdivision", prepared by RMG, October 26, 2020, Revised January 18, 2021.
- 6. "Preliminary Drainage Report for Windermere & Final Drainage Report for Windermere Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, October 2014.
- 7. "Final Drainage Report Marksheffel Road from Constitution Ave. to Dublin Rd.," by CH2M Hill, dated May 2008 and Marksheffel Road Construction Drawings by Wilson & Company.
- 8. "Final Drainage Report for Windermere Filing No. 1" prepared by Drexel, Barrell & Co., March 8, 2022.







WINDERMERE COLORADO SPRINGS, CO VICINITY MAP Drexel, Barrell & Co.
Engineers • Surveyors

DATE:

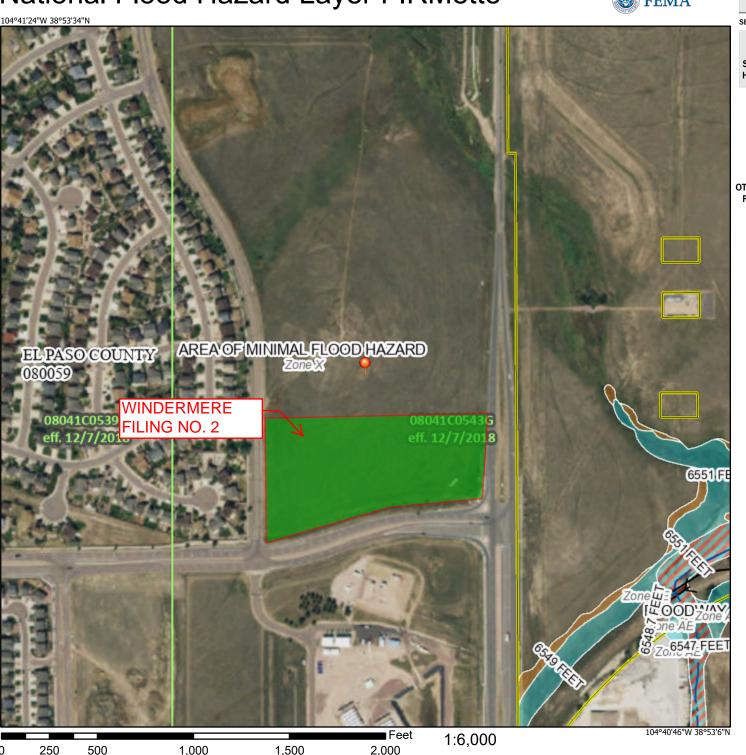
JOB NO: **21187-00CSCV** 



## National Flood Hazard Layer FIRMette

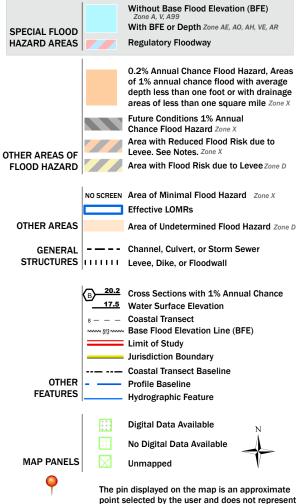


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 9/8/2021 at 3:46 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

an authoritative property location.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Date(s) aerial images were photographed: Apr 15, 2011—Jun Not rated or not available 17. 2014 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

## **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
97	Truckton sandy loam, 3 to 9 percent slopes	А	56.4	100.0%
Totals for Area of Intere	st		56.4	100.0%

## **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

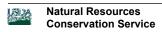
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified



DDO IECT IN	IFORMATION						
PROJECT:	Windermere 2						
PROJECT NO:	21187-03					D	al Parrell 8 Ca
DESIGN BY: REV. BY:	KGV					Drex	el, Barrell & Co.
	TDM						
AGENCY: REPORT TYPE:	El Paso County						
DATE:	Preliminary 4/7/2022						
Soil Type: A	4/1/2022						
Soli Type. A			C2*	C5*	C10*	C100*	% IMPERV
Landscape/Law	n		UZ.	0.25	010	0.35	0
Residential (<1/2				0.45		0.59	65
Asphalt/Sidewa				0.90		0.96	100
EXISTING							
SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSITE	RUNOFF CO	EFFICIENTS		% IMPERV
		ACRE	C2	C5	C10	C100	
EX-A	Landscape/Lawn	13.20		0.25		0.35	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.25		0.35	0%
TOTAL A1		13.20					
		0	FFSITE				
D16	Landscape/Lawn	0.00		0.25		0.35	0
	Residential (<1/8 acre)	2.73		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL D16		2.73					
EXR	Landscape/Lawn	0.00		0.25		0.35	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.53		0.90		0.96	100
	WEIGHTED AVERAGE			0.90		0.96	100%
TOTAL EXR		0.53					
NC2	Landscape/Lawn	0.27		0.25		0.35	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	1.34		0.90		0.96	100
	WEIGHTED AVERAGE			0.79		0.86	83%
TOTAL NC2		1.61	1				
NC1	Landscape/Lawn	0.03		0.25		0.35	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.40		0.90		0.96	100
	WEIGHTED AVERAGE	32		0.85		0.92	93%
TOTAL NC1		0.43		1.00			20,0

 PROJECT:
 Windermere 2

 PROJECT NO:
 21187-03

 DESIGN BY:
 KGV

 REV. BY:
 TDM

 AGENCY:
 EI Paso County

AGENCY: EI Paso Count
REPORT TYPE: Preliminary
DATE: 4/7/2022



#### RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

#### **EXISTING**

	;	SUB-BASII	١			INITIAL/C	VERLAND			TRAVEL	TIME				PIPE TR	AVEL TIME		TIME OF	CONC.	FINAL
		DATA				TIME (t <sub>i</sub> )				$(t_t)$			(t <sub>p</sub> )			t <sub>c</sub>		t <sub>c</sub>		
BASIN	DESIGN PT:	C <sub>5</sub>	C <sub>100</sub>	AREA	LENGTH	HT	SLOPE	t <sub>i</sub>	LENGTH	HT	SLOPE	VEL.	t <sub>t</sub>	LENGTH	SLOPE	VEL.	t <sub>t</sub>	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	Ft	%	FPS	Min	t <sub>c</sub>	t <sub>c</sub>	Min
EX-A		0.25	0.35	13.20	50	2	4.0	7.1	690	21	3.0	10.1	1.1					8.2	5	8.2
D16	DP-4-EX	0.45	0.59	2.73	200	10	5.0	10.1	350	12	3.5	6.5	0.9					11.0	5	11.0
EXR		0.90	0.96	0.53	20	2	10.0	0.8	320	6	2.0	4.9	1.1					1.9	5	5.0
DP4+EXA+EXR	DP-6-EX	0.30	0.41	16.46										850	3.0	7.0	2.0	13.0	5	13.0
NC2	DP-19-EX	0.79	0.86	1.61	50	2	4.0	2.6	1340	35	2.6	9.4	2.4					4.9	5	5.0
NC1		0.85	0.92	0.43	45	1	2.2	2.4	185	4	2.2	8.7	0.4					2.7	5	5.0
DP19+NC1+DP6	DP-20-EX	0.36	0.46	18.50		•				•				50	1.0	8.4	0.1	13.1	5	13.1

 PROJECT:
 Windermere 2

 PROJECT NO:
 21187-03

 DESIGN BY:
 KGV

 REV. BY:
 TDM



ounty

AGENCY: EI Paso County
REPORT TYPE: Preliminary
DATE: 4/7/2022

#### RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING	RUNOFF	5	YR STORI		P1=	1.50	
			DIRECT RUNC	FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t <sub>c</sub> (MIN)	C * A	I (IN/HR)	Q (CFS)
EX-A		13.20	0.25	8.2	3.30	4.40	14.5
D16	DP-4-EX	2.73	0.45	11.0	1.23	3.96	4.9
EXR		0.53	0.90	5.0	0.48	5.10	2.4
DP4+EXA+EXR	DP-6-EX	16.46	0.30	13.0	5.01	3.69	18.5
NC2	DP-19-EX	1.61	0.79	5.0	1.27	5.10	6.5
NC1		0.43	0.85	5.0	0.37	5.10	1.9
DP19+NC1+DP6	DP-20-EX	18.50	0.36	13.1	6.65	3.68	24.5

 PROJECT:
 Windermere 2

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 REV. BY:
 TDM



AGENCY: El Paso County
REPORT TYPE: Preliminary
DATE: 4/7/2022

### RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING		RUNOFF 100 YR STORM					P1=	2.52
				DIRECT RUNO	FF			
BASIN (S)	_	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t <sub>c</sub> (MIN)	C * A	I (IN/HR)	Q (CFS)
EX-A			13.20	0.35	8.2	4.62	7.40	34.2
D16	[	DP-4-EX	2.73	0.59	11.0	1.61	6.65	10.7
EXR			0.53	0.96	5.0	0.51	8.58	4.4
DP4+EXA+EXR		DP-6-EX	16.46	0.41	13.0	6.74	6.20	41.8
NC2	D	P-19-EX	1.61	0.86	5.0	1.38	8.58	11.8
NC1			0.43	0.92	5.0	0.39	8.58	3.4
DP19+NC1+DP6	D	P-20-EX	18.50	0.46	13.1	8.51	6.18	52.6

DRO IECT IN	NFORMATION						
PROJECT:	Windermere 2						
PROJECT: PROJECT NO:	21187-03						
DESIGN BY:	KGV					Drov	el, Barrell & Co.
REV. BY:	TDM					Diex	ei, Baireii & Co.
AGENCY:	El Paso County						
REPORT TYPE:	Preliminary						
DATE:	4/7/2022						
Soil Type: A	4/1/2022						
7 PO. 74			C2*	C5*	C10*	C100*	% IMPERV
Landscape/Law	vn			0.15	<b>U</b>	0.50	0
Residential (<1/				0.45		0.59	65
Asphalt/Sidewa	•			0.90		0.96	100
				0.00		0.00	100
PROPOSED							
SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSITE	E RUNOFF CO	EFFICIENTS		% IMPERV
		ACRE	C2	C5	C10	C100	
A1	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	2.45		0.45		0.59	65
	Asphalt/Sidewalk	0.44		0.90		0.96	100
	WEIGHTED AVERAGE			0.52		0.65	70%
TOTAL A1		2.90					
A2	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	2.85		0.45		0.59	65
	Asphalt/Sidewalk	0.44		0.90		0.96	100
	WEIGHTED AVERAGE			0.51		0.64	70%
TOTAL A2		3.29					
A3	Landscape/Lawn	1.51		0.15		0.50	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.10		0.90		0.96	100
	WEIGHTED AVERAGE			0.20		0.53	6%
TOTAL A3		1.61					
			POND	•	<u>.                                    </u>	•	
P1	Landscape/Lawn	1.00		0.15		0.50	0
	Residential (<1/8 acre)	0.00		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.15		0.50	0%
TOTAL P1		1.00					
_			FFSITE				
B1	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	3.33		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL B1		3.33					
B2	Landscape/Lawn	0.00		0.15		0.50	0
	Residential (<1/8 acre)	0.49		0.45		0.59	65
	Asphalt/Sidewalk	0.00		0.90		0.96	100
	WEIGHTED AVERAGE			0.45		0.59	65%
TOTAL B2		0.49					

B4	Landscape/Lawn	0.00	0.15	0.50	0
	Residential (<1/8 acre)	0.16	0.45	0.59	65
	Asphalt/Sidewalk	0.00	0.90	0.96	100
	WEIGHTED AVERAGE		0.45	0.59	65%
TOTAL B4		0.16			
Tr	ibutary to Pond	12.79			54.9%
D16	Landscape/Lawn	0.00	0.15	0.50	0
	Residential (<1/8 acre)	2.73	0.45	0.59	65
	Asphalt/Sidewalk	0.00	0.90	0.96	100
	WEIGHTED AVERAGE		0.45	0.59	65%
TOTAL D16		2.73			
NC2	Landscape/Lawn	0.27	0.15	0.50	0
	Residential (<1/8 acre)	0.00	0.45	0.59	65
	Asphalt/Sidewalk	1.34	0.90	0.96	100
	WEIGHTED AVERAGE		0.77	0.88	83%
TOTAL NC2		1.61			
EXR	Landscape/Lawn	0.00	0.15	0.50	0
	Residential (<1/8 acre)	0.00	0.45	0.59	65
	Asphalt/Sidewalk	0.53	0.90	0.96	100
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL EXR		0.53			
C3	Landscape/Lawn	0.63	0.15	0.50	0
	Residential (<1/8 acre)	0.00	0.45	0.59	65
	Asphalt/Sidewalk	0.00	0.90	0.96	100
	WEIGHTED AVERAGE		0.15	0.50	0%
TOTAL C3		0.63			
NC1	Landscape/Lawn	0.03	0.15	0.50	0
	Residential (<1/8 acre)	0.00	0.45	0.59	65
	Asphalt/Sidewalk	0.40	0.90	0.96	100
	WEIGHTED AVERAGE		0.85	0.93	93%
TOTAL NC1		0.43			

DATE:

 PROJECT:
 Windermere 2

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 TDM

 AGENCY:
 EI Paso County

 REPORT TYPE:
 Preliminary

Note: detailed review will be provided with the final plat/SDP.



## RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF PROPOSED TIME OF CONCENTRATION STANDARD FORM SF-2

4/7/2022

	;	SUB-BASI	N			INITIAL/O	VERLAND			TRAVEL	TIME				PIPE TR	AVEL TIME		TIME OF	CONC.	FINAL
		DATA				TIME (t <sub>i</sub> )				$(t_t)$					(t <sub>p</sub> )			t <sub>c</sub>	:	t <sub>c</sub>
BASIN	DESIGN PT:	C <sub>5</sub>	C <sub>100</sub>	AREA	LENGTH	HT	SLOPE	t <sub>i</sub>	LENGTH	HT	SLOPE	VEL.	t <sub>t</sub>	LENGTH	SLOPE	VEL.	t <sub>t</sub>	COMP.	MINIMUM	
				Ac	Ft	FT	%	Min	Ft	FT	%	FPS	Min	Ft	%	FPS	Min	t <sub>c</sub>	t <sub>c</sub>	Min
A1	1	0.52	0.65	2.90	50	2	4.0	4.8	690	21	3.0	10.1	1.1					6.0	5	6.0
A2		0.51	0.64	3.29	100	1	1.0	11.0	720	22	3.0	10.1	1.2					12.2	5	12.2
A1+A2	2	0.51	0.64	6.19														12.2	5	12.2
B1		0.45	0.59	3.33	35	1	3.5	4.7	885	30	3.4	10.8	1.4					6.1	5	6.1
B2		0.45	0.59	0.49	50	2	4.0	5.4	725	20	2.8	9.8	1.2					6.6	5	6.6
DP2+B1+B2	3	0.49	0.62	10.01										212	0.5	5.1	0.7	12.9	5	12.9
B4		0.45	0.59	0.16	50	17	33.3	2.7	185	3	1.5	4.0	0.8					3.4	5	5.0
P1		0.15	0.50	1.00	100	1	1.0	17.8	205	10	4.8	12.8	0.3					18.0	5	18.0
DP3+B4+P1	4	0.46	0.61	11.18					250	2.5	1.0	4.0	1.0					13.9	5	13.9
D16	5	0.45	0.59	2.73	200	10	5.0	10.1	350	12	3.5	6.5	0.9					11.0	5	11.0
A3		0.20	0.53	1.61	100	10	10.0	7.8	670	25	3.7	11.3	1.0					8.8	5	8.8
NC2		0.77	0.88	1.61	50	2	4.0	2.7	1340	35	2.6	9.4	2.4					5.1	5	5.1
A3+NC2	19	0.49	0.71	3.22					100	10	10.0	7.8	0.2					9.0	5	9.0
EXR		0.90	0.96	0.53	20	2	10.0	0.8	320	6	2.0	4.9	1.1					1.9	5	5.0
C3		0.15	0.50	0.63	60	12	20.0	5.1	455	15	3.3	5.6	1.4					6.4	5	6.4
EXR+C3+DP5	S	0.46	0.63	3.89										850	3.0	11.8	1.2	12.2	5	12.2
DP19+DPS	J1	0.47	0.66	7.11										100	1.0	5.9	0.3	12.4	5	12.4
NC1		0.85	0.93	0.43	45	1	2.2	2.4	185	4	2.2	8.7	0.4					2.8	5	5.0
DPJ1+NC1	20	0.49	0.68	7.54										50	1.0	8.4	0.1	12.5	5	12.5

REPORT TYPE:

DATE:

 PROJECT:
 Windermere 2

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 21187-03

 DESIGN BY:
 KGV

 REV. BY:
 TDM

 AGENCY:
 EI Paso County



El Paso County
Preliminary

4/7/2022

#### RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED	RUNOFF	:	YR STORI	М		P1=	1.50
			DIRECT RUNC	FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t <sub>c</sub> (MIN)	C * A	I (IN/HR)	Q (CFS)
A1	1	2.90	0.52	6.0	1.50	4.87	7.3
A2		3.29	0.51	12.2	1.68	3.79	6.4
A1+A2	2	6.19	0.51	12.2	3.19	3.79	12.1
B1		3.33	0.45	6.1	1.50	4.84	7.2
B2		0.49	0.45	6.6	0.22	4.72	1.0
DP2+B1+B2	3	10.01	0.49	12.9	4.91	3.70	18.2
B4		0.16	0.45	5.0	0.07	5.10	0.4
P1		1.00	0.15	18.0	0.15	3.17	0.5
DP3+B4+P1	4	11.18	0.46	13.9	5.13	3.58	18.4
D16	5	2.73	0.45	11.0	1.23	3.96	4.9
A3		1.61	0.20	8.8	0.32	4.30	1.4
NC2		1.61	0.77	5.1	1.25	5.08	6.3
A3+NC2	19	3.22	0.49	9.0	1.56	4.26	6.7
EXR		0.53	0.90	5.0	0.48	5.10	2.4
C3		0.63	0.15	6.4	0.09	4.76	0.5
Pond Release							0.3
EXR+C3+DP5+POND RELEASE	S	3.89	0.46	12.2	1.80	3.80	7.1
DP19+DPS	J1	7.11	0.47	12.4	3.36	3.76	12.9
NC1		0.43	0.85	5.0	0.36	5.10	1.9
DPJ1+NC1	20	7.54	0.49	12.5	3.73	3.75	14.3

 PROJECT:
 Windermere 2

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AGENCY:

El Paso County Preliminary

REPORT TYPE: DATE:

4/7/2022

#### RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

PROPOSED	RUNOFF	10	00 YR STOF	RM		P1=	2.52
			DIRECT RUNC	)FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t <sub>c</sub> (MIN)	C * A	I (IN/HR)	Q (CFS)
A1	1	2.90	0.65	6.0	1.88	8.17	15.3
A2		3.29	0.64	12.2	2.11	6.36	13.4
A1+A2	2	6.19	0.64	12.2	3.98	6.36	25.4
B1		3.33	0.59	6.1	1.96	8.12	16.0
B2		0.49	0.59	6.6	0.29	7.92	2.3
DP2+B1+B2	3	10.01	0.62	12.9	6.24	6.22	38.8
B4		0.16	0.59	5.0	0.09	8.58	0.8
P1		1.00	0.50	18.0	0.50	5.33	2.7
DP3+B4+P1	4	11.18	0.61	13.9	6.83	6.01	41.1
D16	5	2.73	0.59	11.0	1.61	6.65	10.7
A3		1.61	0.53	8.8	0.85	7.22	6.1
NC2		1.61	0.88	5.1	1.42	8.54	12.1
A3+NC2	19	3.22	0.71	9.0	2.27	7.15	16.3
EXR		0.53	0.96	5.0	0.51	8.58	4.4
C3		0.63	0.50	6.4	0.32	8.00	2.5
Pond Release							10.6
EXR+C3+DP5+POND RELEASE	S	3.89	0.63	12.2	2.43	6.38	26.1
DP19+DPS	J1	7.11	0.66	12.4	4.71	6.32	40.3
NC1		0.43	0.93	5.0	0.40	8.58	3.4
DPJ1+NC1	20	7.54	0.68	12.5	5.10	6.29	42.7

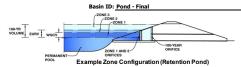
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

#### Project: Windermere Filing No. 2

acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches

2.25 inches 2.52 inches 3.49 inches



#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	12.79	acres
Watershed Length =	1,000	ft
Watershed Length to Centroid =	350	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	54.90%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Painfall Denths -	Hear Innut	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

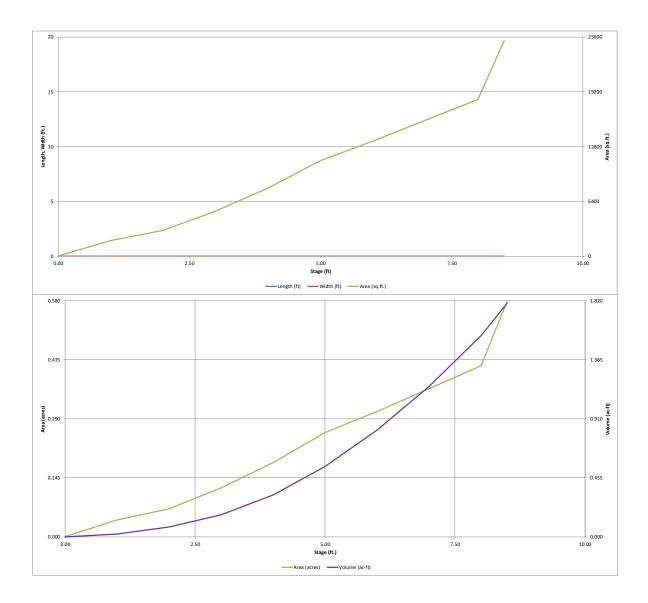
the embedded Colorado Urban Hydro		
Water Quality Capture Volume (WQCV) =	0.235	acre-feet
Excess Urban Runoff Volume (EURV) =	0.831	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.593	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.785	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.938	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.163	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	1.384	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.660	acre-feet
500-yr Runoff Volume (P1 = 3.49 in.) =	2.617	acre-feet
Approximate 2-yr Detention Volume =	0.537	acre-feet
Approximate 5-yr Detention Volume =	0.705	acre-feet
Approximate 10-yr Detention Volume =	0.856	acre-feet
Approximate 25-yr Detention Volume =	1.041	acre-feet
Approximate 50-yr Detention Volume =	1.157	acre-feet
Approximate 100-yr Detention Volume =	1.289	acre-feet
		-

#### Define Zones and Basin Geometry

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR})$ =	user	ft
Length of Basin Floor $(L_{FLOOR})$ =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin $(V_{MAIN}) =$	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-fee

Double Tourness		_							
Depth Increment =		ft Optional				Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool		0.00				40	0.001		
6574		1.00	-		-	1,801	0.041	920	0.021
6575		2.00	-		-	3,008	0.069	3,325	0.076
6576		3.00	-			5,232	0.120	7,445	0.171
6577		4.00	-		-	7,923	0.182	14,022	0.322
6578		5.00	-		-	11,161	0.256	23,564	0.541
6579		6.00	-		-	13,425	0.308	35,857	0.823
6580		7.00	-		-	15,853	0.364	50,496	1.159
6581		8.00	-		-	18,293	0.420	67,569	1.551
6581.5		8.50	-			25,208	0.579	78,445	1.801
0301.3		0.30				23,200	0.375	70,443	1.001
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M#FD-Detention\_v4.03-Windermere S.xism, Basin 4/7/2022, 2.04 PM

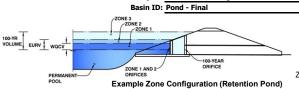


M#FD-Detention\_v4.03-Windermere S.xism, Basin 4/7/2022, 2.04 PM

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Windermere Filing No. 2



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.48	0.235	Orifice Plate
Zone 2 (EURV)	6.03	0.596	Orifice Plate
Zone 3 (100-year)	7.35	0.458	Weir&Pipe (Restrict)
-	Total (all zones)	1 289	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

	Calculated Parallie	ters for officerura
Underdrain Orifice Area =		ft²
Underdrain Orifice Centroid =		feet

Calculated Parameters for Vertical Orifice

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMI

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ O

Depth at top of Zone using Orifice Plate = 6.03 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 24.10 inches

Orifice Plate: Orifice Area per Row = N/A inches

on BMP)	Calculated Parame	ters for Plate
WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>
	•	

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)			
Stage of Orifice Centroid (ft)	0.00	2.01	4.02								
Orifice Area (sq. inches)	1.10	1.70	2.00								

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

ber Input. Vertical Office (circular of rectang	calculated Farameters for Vertical Office						
	Not Selected	Not Selected			Not Selected	Not Selected	İ
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches				•

User Input: Overflow Weir (Dropbox with Flat of	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.40	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, $H_t$ =	6.40	N/A	feet
Overflow Weir Front Edge Length =	3.92	N/A	feet Overflow Weir Slope Length =	3.92	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	14.68	N/A	
Horiz. Length of Weir Sides =	3.92	N/A	feet Overflow Grate Open Area w/o Debris =	10.78	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area	5.39	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor | Not Selected |

Zone 3 Restrictor | Not Selected |

Depth to Invert of Outlet Pipe = 2.50 N/A Outlet Orifice Area 0.73 ft (distance below basin bottom at Stage = 0 ft) N/A Outlet Pipe Diameter = 18.00 N/A inches Outlet Orifice Centroid = 0.38 N/A feet Restrictor Plate Height Above Pipe Invert = inches Half-Central Angle of Restrictor Plate on Pipe = radians 7.80 N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

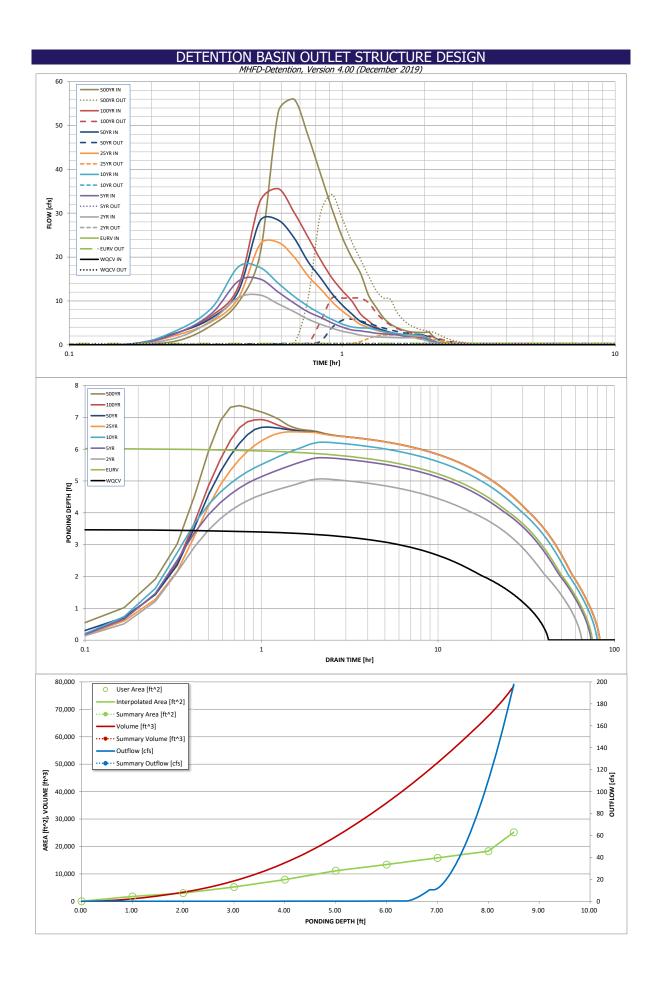
Debris Clogging % =

50%

N/A

<u>nput: Emergency Spillway (Rectangular or</u>	Trapezoidal)			Calculated Parame	ters for Spillway
Spillway Invert Stage=	6.94	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.55	feet
Spillway Crest Length =	27.00	feet	Stage at Top of Freeboard =	8.49	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.58	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	1.80	acre-ft

Routed Hydrograph Results	The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.49
CUHP Runoff Volume (acre-ft) =	0.235	0.831	0.593	0.785	0.938	1.163	1.384	1.660	2.617
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.593	0.785	0.938	1.163	1.384	1.660	2.617
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.3	0.4	3.3	6.4	10.4	23.5
OPTIONAL Override Predevelopment Peak Q (cfs) =		N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =		N/A	0.01	0.02	0.03	0.26	0.50	0.81	1.83
Peak Inflow Q (cfs) =	N/A	N/A	11.3	15.0	17.8	23.3	28.4	35.6	56.0
Peak Outflow Q (cfs) =		0.3	0.3	0.3	0.3	2.3	5.8	10.6	34.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.1	0.8	0.7	0.9	1.0	1.5
Structure Controlling Flow =		Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.2	0.5	1.0	1.0
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	64	57	64	68	69	67	65	58
Time to Drain 99% of Inflow Volume (hours) =	40	70	62	69	75	77	76	75	72
Maximum Ponding Depth (ft) =	3.48	6.03	5.06	5.73	6.22	6.54	6.69	6.93	7.37
Area at Maximum Ponding Depth (acres) =	0.15	0.31	0.26	0.29	0.32	0.34	0.35	0.36	0.38
Maximum Volume Stored (acre-ft) =	0.236	0.832	0.556	0.742	0.889	0.998	1.049	1.134	1.294

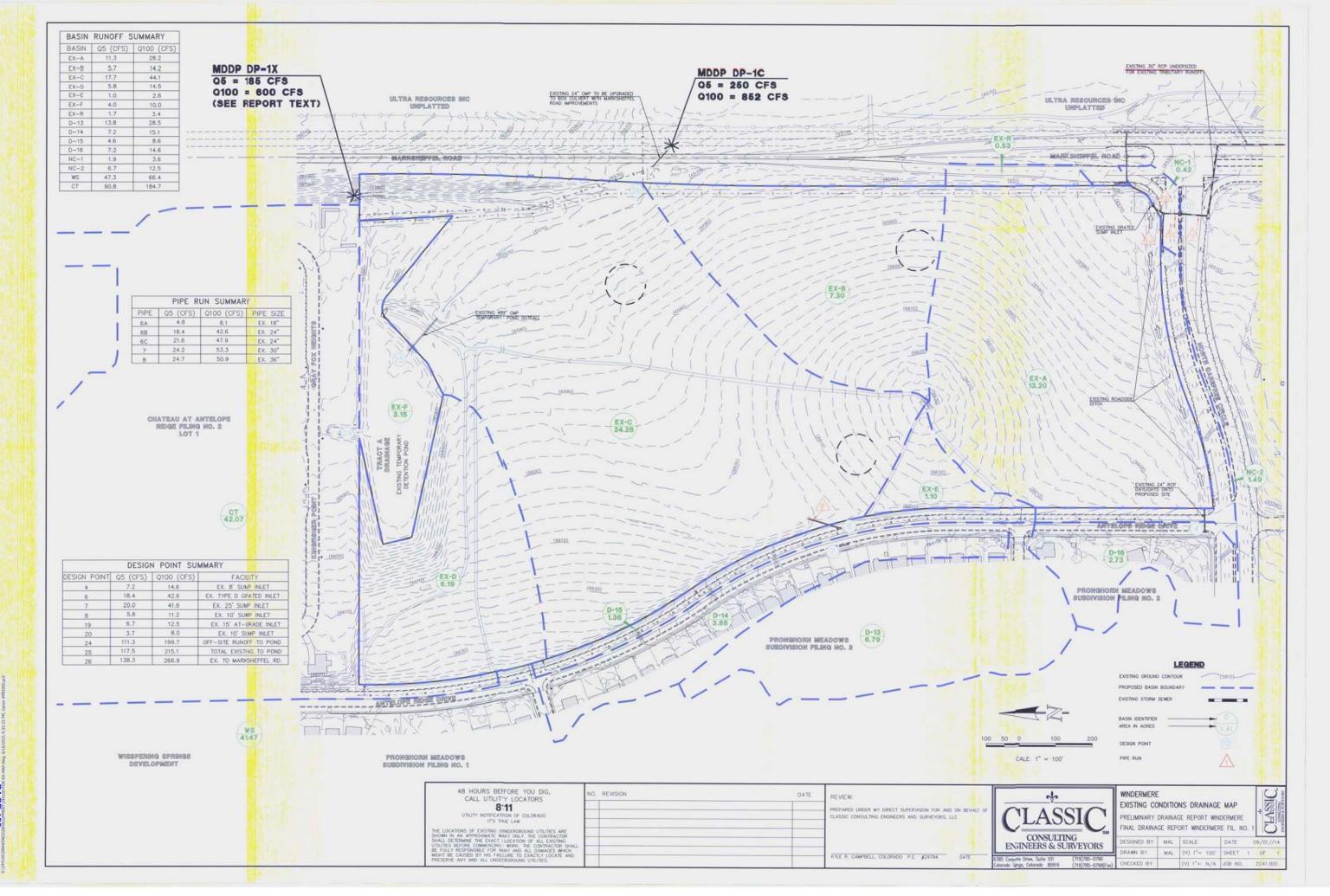


## DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

								culp		CLIND
T	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]			100 Year [cfs]	
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.19	0.02	0.95
	0:15:00 0:20:00	0.00	0.00	1.68	2.73	3.39 8.47	2.28	2.81	2.79	4.49
	0:25:00	0.00	0.00	5.61 10.75	7.23 14.52	17.75	5.32 10.67	6.15 12.20	6.66 13.26	9.68 20.56
	0:30:00	0.00	0.00	11.32	14.97	17.61	22.87	28.23	32.69	53.10
	0:35:00	0.00	0.00	9.30	12.01	14.00	23.34	28.40	35.57	55.97
	0:40:00	0.00	0.00	7.55	9.51	11.03	20.01	24.38	30.21	47.63
	0:45:00	0.00	0.00	5.82	7.52	8.79	15.67	18.93	24.52	38.91
	0:50:00	0.00	0.00	4.67	6.22	7.11	12.74	15.26	19.35	31.09
	0:55:00	0.00	0.00	3.80	5.00	5.79	9.84	11.69	15.27	24.59
	1:00:00	0.00	0.00	3.09	4.02	4.72	7.73	9.07	12.35	19.94
	1:05:00	0.00	0.00	2.65	3.40	4.07	6.08	7.06	10.03	16.32
	1:10:00 1:15:00	0.00	0.00	2.19 1.94	3.15 2.90	3.85 3.78	4.64 3.95	5.31 4.48	7.03 5.42	11.24 8.50
	1:20:00	0.00	0.00	1.80	2.64	3.47	3.31	3.74	4.04	6.17
	1:25:00	0.00	0.00	1.71	2.47	3.02	2.93	3.30	3.20	4.77
	1:30:00	0.00	0.00	1.66	2.36	2.72	2.51	2.83	2.71	3.93
	1:35:00	0.00	0.00	1.63	2.30	2.53	2.25	2.54	2.38	3.37
	1:40:00	0.00	0.00	1.60	2.01	2.40	2.09	2.35	2.17	3.03
	1:45:00	0.00	0.00	1.59	1.81	2.32	1.99	2.23	2.07	2.87
	1:50:00	0.00	0.00	1.59	1.69	2.26	1.93	2.17	2.04	2.82
	1:55:00 2:00:00	0.00	0.00	1.31	1.61	2.15	1.90	2.13	2.02	2.80
	2:00:00	0.00	0.00	1.13 0.72	1.50 0.96	1.92 1.24	1.88	2.11 1.36	1.30	2.80 1.79
	2:10:00	0.00	0.00	0.72	0.60	0.78	0.77	0.86	0.82	1.13
	2:15:00	0.00	0.00	0.27	0.37	0.48	0.47	0.53	0.50	0.69
	2:20:00	0.00	0.00	0.15	0.22	0.28	0.28	0.31	0.30	0.41
	2:25:00	0.00	0.00	0.08	0.12	0.15	0.16	0.18	0.17	0.23
	2:30:00	0.00	0.00	0.03	0.06	0.06	0.07	0.08	0.07	0.10
	2:35:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00 2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



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