



**FINAL DRAINAGE REPORT FOR
SHILOH MESA RETAIL SOUTH FIL #1
COLORADO SPRINGS, COLORADO**

APRIL 2022

Prepared For:

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Job No. 2214.00

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**FINAL DRAINAGE REPORT FOR
SHILOH MESA RETAIL SOUTH FIL #1
COLORADO SPRINGS, COLORADO**

ENGINEER’S STATEMENT:

This report and plan for the drainage design of “SHILO MESA RETAIL SOUTH FIL #1” was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

L Ducett, P.E. 32339

Seal

DEVELOPER’S STATEMENT:

COLORADO COMMERCIAL BUILDERS hereby certifies that the drainage facilities for SHILOH MESA RETAIL SOUTH FIL #1 shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to section 7.7.906 of the City Code; and cannot, on behalf of SHILOH MESA RETAIL SOUTH FIL #1 guarantee that final drainage design review will absolve COLORADO COMMERCIAL BUILDERS and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer’s drainage design.

COLORADO COMMERCIAL BUILDERS

Authorized Signature

Date

Printed Name

Title

Address

City of Colorado Springs Statement:

Filed in accordance with Section 7-7-906 of the Code of the City of Colorado Springs, 2001, as amended.

For City Engineer
Conditions:

Date

FINAL DRAINAGE REPORT FOR SHILOH MESA RETAIL SOUTH FIL #1 COLORADO SPRINGS, COLORADO

PURPOSE AND JUSTIFICATION

The purpose of this Final Drainage Report is to identify and analyze the existing drainage patterns, determine existing runoff quantities, and analyze the proposed development of this site as a commercial site (small retail). This site is a single parcel that has not been previously platted. This site was previously studied in:

“Master Development Drainage Plan Amendment For Shiloh Mesa at Woodmen Heights and Final Drainage Report for Shiloh Mesa Commercial Filing No. 1” dated July 2019 by Matrix Design Group.

GENERAL DESCRIPTION

This Final Drainage Report for “SHILOH MESA RETAIL SOUTH FIL #1”, located northeast of the intersection of Marksheffel Road and Geraldine Point, is an analysis of an approximately 3.18 ac site. The site is currently a vacant parcel. The proposed development is a commercial retail complex, utility lines, storm water facilities, and the associated modifications to the site. The site it proposed to be subdivided into two lots, Lot 1 is x acres and Lot 2 is x acres.

The site is in the southwest quarter of Section 4, Township 13 South, Range 65 West of the 6th Principal Meridian within the City of Colorado Springs El Paso County, Colorado. The parcel is bounded to the west by N Marksheffel Road, to the north by Geraldine Point, a private ROW, to the north east by Carmella Grove a private ROW, to the east by an existing private detention facility Tract A Shiloh Mesa Commercial Filing No. 1 (see vicinity map in appendix).

The site lies within the Sand Creek Drainage Basin, with storm runoff draining to the west. The property is not in a streamside zone.

The site consists of 66.9% Blakeland loamy sand (8) and 33.1% Pring coarse sandy loam (71) per the USDA, NRCS web soil survey. The hydrologic group “B” was used to represent the soil types and determine the onsite basin overland flow. (see map in appendix)

The study area consists of undeveloped land, which is currently a vacant parcel, with mostly grass and dirt surfaces. Some earthwork appears to have been done on the site previously. The northly portion of the site has been improved with a private road (Geraldine Point) and the rest of the site is impervious. The site currently drains toward the west, with slopes ranging from 2% to 6%.

EXISTING DRAINAGE CONDITIONS

Existing runoff on the site, and adjacent areas to the east, flows west, before flowing into the Woodmen Road and Marksheffel Road gutters. The following is a description of the existing Basins, Design Points, and the overall existing drainage characteristics for the site. (see Existing Drainage Map in the appendix).

Basin EX-A’s 2.9 acres consists of undeveloped land and pavement on Geraldine Point. Runoff ($Q_5 = 0.1$ cfs, $Q_{100} = 0.7$ cfs) sheet flows west to design point A and into the Marksheffel Road right of way.

Basin EX-B’s 0.14 acres consists of undeveloped land. Runoff ($Q_5 = 0.1$ cfs, $Q_{100} = 0.4$ cfs) sheet flows east to design point EX2 and into the existing private extended detention pond to the east of the site in Tract A of the Shiloh Mesa Commercial Filing No. 1 site.

Basin EX-C’s 0.14 acres consists of undeveloped land. Runoff ($Q_5 = 0.1$ cfs, $Q_{100} = 0.4$ cfs) sheet flows south to design point EX3 and into the Woodmen Road Right of Way.

PROPOSED DRAINAGE CONDITIONS

In the proposed condition the overall drainage pattern for the site changes quite a bit, with runoff being collected and channeled along gutter and through storm sewers. Drainage will generally be to the southwest, with the site draining to the proposed private extended detention basin, before runoff leaves the site via storm sewer. The changes to the site include constructing the building,

utility lines, parking facilities, storm water facilities, grading, paving, and the associated modifications to the site.

Basin A (0.31 acres) is on the west side of the site and includes building, parking, and landscaping areas that sheet and channel flow south to a curb inlet at Design Point 4. Basin A flow is 0.9 cfs for the 5 year event and 2.0 cfs for the 100 year event.

Basin B (0.55 acres) is on the south side of the site and includes building, landscaping, and the EDB areas that sheet flows west to the EDB at Design Point 8. Basin B flow is 0.5 cfs for the 5 year event and 1.7 cfs for the 100 year event.

Basin C (1.60 acres) is on the bulk of the site and includes building, parking, landscaping areas that sheet flow north and west off the site to a curb inlet at Design Point 2. Basin C flow is 5.7 cfs for the 5 year event and 11.6 cfs for the 100 year event.

Basin D (0.08 acres) is on the east side of the site and includes landscaping area that sheet flows east off the site at Design Point 5. Basin D flow is 0.4 cfs for the 5 year event and 0.7 cfs for the 100 year event.

Basin E (0.20 acres) is on the west side of the site and includes landscaping area that sheet flows west off the site at Design Point 3. Basin E flow is 1.1 cfs for the 5 year event and 2.2 cfs for the 100 year event.

Basin F (0.08 acres) is on the south side of the site and includes landscaping area that sheet flows south off the site at Design Point 7. Basin F flow is 0.4 cfs for the 5 year event and 0.8 cfs for the 100 year event.

Basin G (0.18 acres) is north of the site and includes Geraldine Point and part of the property to the north that sheet and channel flows west to a curb inlet at Design Point 1. Basin G flow is 0.4 cfs for the 5 year event and 1.0 cfs for the 100 year event.

Basin H (0.23 acres) is on the west side of the site and includes building, parking, and landscaping areas that sheet and channel flow north and west to a curb inlet at Design Point 6. Basin H flow is 0.9 cfs for the 5 year event and 2.0 cfs for the 100 year event.

At Design Point 8 is the proposed private full spectrum extended detention basin that will provide full spectrum detention. Based upon the 3.18 acres of area tributary (Basins A,B,C,G,H) and consisting of 75% impervious area, the required volume is 0.396 ac-ft. The bottom of the EDB is set at 6902.0, while the top is at 6909.0. The pond design has a WQCV storage requirement of 0.079 ac-ft. The corresponding water surface elevation is 6904.36. The required EURV storage volume of 0.214 ac-ft on top of the WQCV gives an elevation of 6906.79. The required 100-year storage volume of 0.103 ac-ft for a total of 0.396 ac-ft gives a 100-year elevation of 6907.60. The proposed forebay is 96 cu-ft in volume and meet the required 2% of the WQCV (see appendix for calculations). A metal plate over the outlet with one column containing three rows of 7/8" diameter holes spaced 18.1" apart will act as a water quality and EURV outlet. The release of the EURV is 0.1 cfs and will take 70 hours. A 2.0' x 2.0' inlet riser acts as the outlet structure, it is set at a grate elevation of 6906.80 and will route allowable runoff for the 100 year event. The proposed 18" outlet has a restrictor plate 3.80" above the invert giving a release of $Q_{100} = 2.8$ cfs. This is in conformance with the allowable release rate of 2.8 cfs. A 3' emergency weir set at 6908.00 will also be installed per the city standards with d50 = 12" rip rap and will safely pass the 100-year developed flow downstream. The pond outlet drains to an existing public storm manhole that the site currently drains to. Flow in the emergency overflow situation will flow into the ROW of Woodmen Road with a 100 year runoff spillway flow depth of 0.72'.

In an effort to protect receiving water and as part of the "four step process to minimize adverse impacts of urbanization" this site was analyzed in the following manner:

1. Reduce Runoff- Runoff from some of the impervious areas on the site is directed to landscaping areas where a portion of the runoff can infiltrate. See the IRF spreadsheet in the appendix for areas.
2. Treat Slowly Release WQCV- The proposed private full spectrum EDB will provide the required WQCV and slowly release it, thereby allowing solids and contaminants to settle out.

3. Stabilize Stream Channel- Drainage fees will be paid when this site is platted, which can be used to stabilize the Sand Creek channels. Also, there is no channel adjacent to this property and flows are primarily conveyed offsite via storm pipes.
4. Source Controls- As no materials storage or industrial operations are proposed for the site, no source controls have been proposed.

Please see detailed calculations in the appendix.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the City of Colorado Springs Storm Drainage Design Criteria Manual Volumes 1 & 2 January 2021. The Rational Method was used to estimate storm water runoff anticipated from design storms with 5-year and 100-year recurrence intervals. The Rational Method was used because it is the simplest method, that is applicable to the site, and allowed by the Drainage Criteria Manual.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the City of Colorado Springs Storm Drainage Design Criteria Manual Volumes 1 and 2 January 2021 and the Urban Drainage and Flood Control District (UDFCD) Urban Storm Drainage Criteria Manual Volumes 1, 2, and 3. The hydraulic calculations include open channel flow (for gutter capacities), inlet sizing calculations, and storm sewer sizing calculations. The pertinent data sheets are included in the appendix of this report. It is requested that the HGL calculations and plots be provided in an addendum at the time of storm sewer plan submittal. The HGL calculations will be performed using the software UD-SEWER (or similar).

WATER QUALITY

Water quality for this development is being address by the proposed private full spectrum extended detention basin. Calculations can be found in the appendix.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain, as determined by Flood Insurance Rate Map No. 08041C0533 G dated December 7, 2018 (see appendix).

EROSION CONTROL

It is the policy of the City of Colorado Springs that we submit an erosion control plan with the drainage report. At this time, Terra Nova Engineering, Inc. respectfully requests that the erosion control plan be submitted in conjunction with the final grading plan. Rock socks, sediment control logs, silt fence, and inlet protection are currently proposed as erosion control measures.

CONSTRUCTION COST OPINION

Private Drainage Facilities Improvements (non Reimbursable)

	<u>Item</u>	<u>Quantity</u>	<u>Unit Cost</u>	<u>Cost</u>
1.	12" RCP Storm	30 LF	\$ 30	\$ 900
2.	12" HDPE Storm	181 LF	\$ 30	\$ 5,430
3.	24" HDPE Storm	330 LF	\$ 60	\$ 19,800
4.	4' Storm Manhole	4 EA	\$ 6,000	\$ 24,000
5.	Storm Inlet, 4' D-10-R	3 EA	\$ 6,000	\$ 18,000
6.	Storm Inlet, 8' D-10-R	1 EA	\$ 8,000	\$ 8,000
			Total	\$ 76,130

Public Drainage Facilities Improvements (non Reimbursable)

None.

Private Permanent BMPs (non-Reimbursable)

	<u>Description</u>	<u>Quantity</u>	<u>Unit Price</u>	<u>Cost</u>
1.	Extended Detention Basin			
	- Earthwork	1,300 CY	\$ 12	\$ 15,600
	- Forebays	1 EA	\$ 1,500	\$ 1,500
	- Trickle Channel	80 LF	\$ 32	\$ 2,560
	- Outlet Structures (2'x2')	1 EA	\$ 4,000	\$ 4,000

- Emergency Spillways	1 EA	\$ 2,000	\$ 2,000
- Access Roads	1 EA	\$ 1,000	\$ 1,000
- Stabilization	1 EA	\$ 5,000	<u>\$ 5,000</u>
		Subtotal	\$ 31,660
	10% Contingency		<u>\$ 3,166</u>
		Total	\$ 34,826

DRAINAGE FEES

The site is being platted as part of this development. The site is located in the Sand Creek Drainage Fee Basin. 2022 fees for this site will be calculated as follows and are due prior to plat recordation:

Sand Creek Drainage Fee Basin 2022

Drainage	\$20,160/acre	x	2.87 acres	=	<u>\$ 57,957.13</u>
					Total \$ 57,957.13

*Fees are due prior to plat recordation

MAINTENANCE

The proposed sand filter will be privately maintained. The proposed storm sewers that are private will be privately maintained.

SUMMARY

Development of this site will not adversely affect the downstream and surrounding developments. Proposed onsite collection and piping will drain into the proposed private full spectrum sand filter, before flowing offsite via storm sewer. Water quality and detention will be addressed by the proposed sand filter. This Final Drainage Report is in general conformance with the previously approved reports/studies for this site.

PREPARED BY:
TERRA NOVA ENGINEERING, INC.

L Ducett, P.E.
 President
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BIBLIOGRAPHY

“City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2”, January 2021

“NRCS Soil Map for El Paso County Area, Colorado”

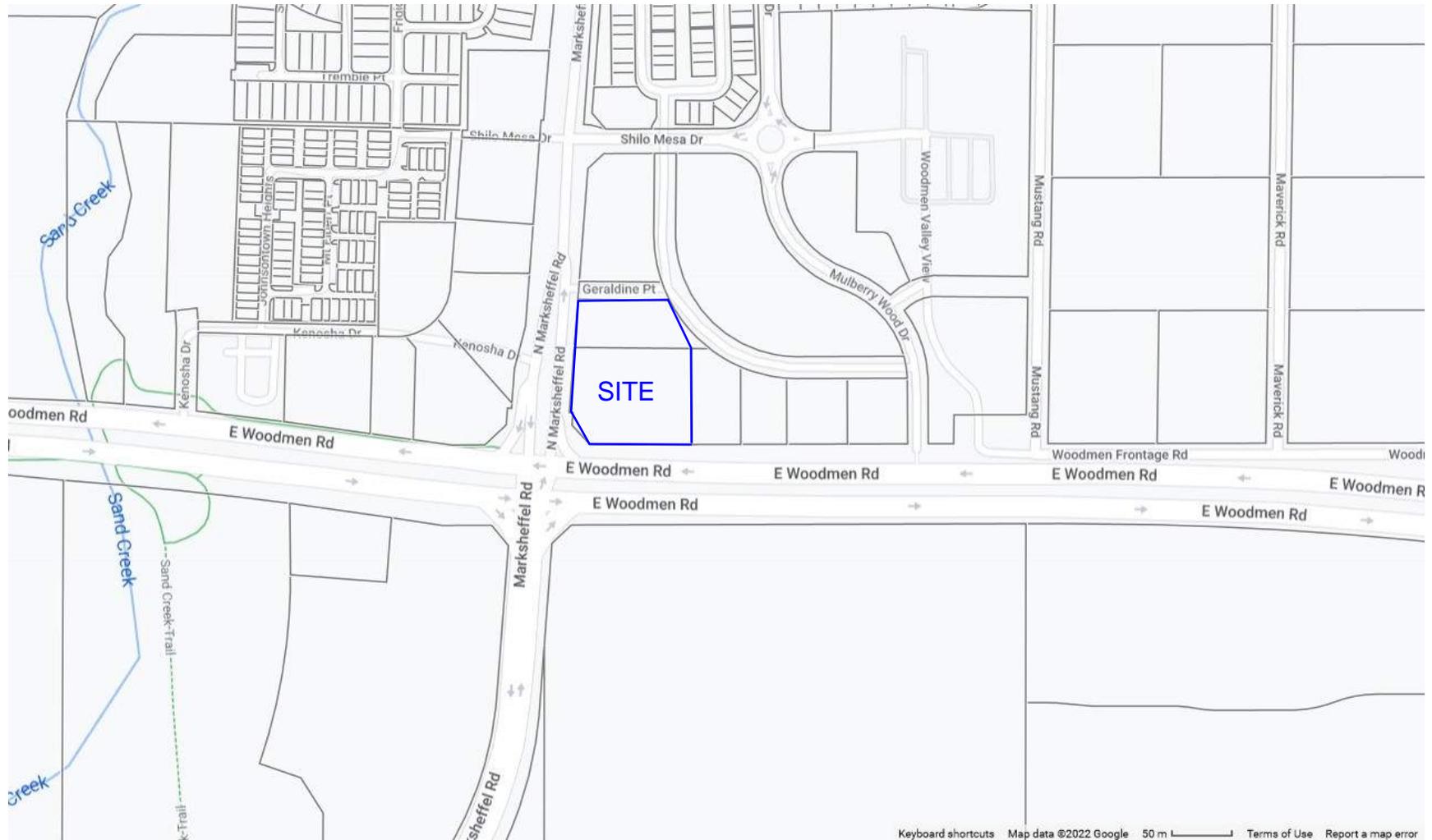
“FEMA Floodplain Map”

“Master Development Drainage Plan Amendment For Shiloh Mesa at Woodmen Heights and Final Drainage Report for Shiloh Mesa Commercial Filing No. 1” dated July 2019 by Matrix Design Group.

VICINITY MAP

El Paso County - Community: Area Overview

Shilo Mesa South Vicinity Map



North is up ^^^

GENERAL LOCATION MAP

Shiloh Mesa South

Image Dated Oct 2019

Carmela Grove

Geraldine Pt

N Marksheffel Rd

SITE

E Woodmen Rd

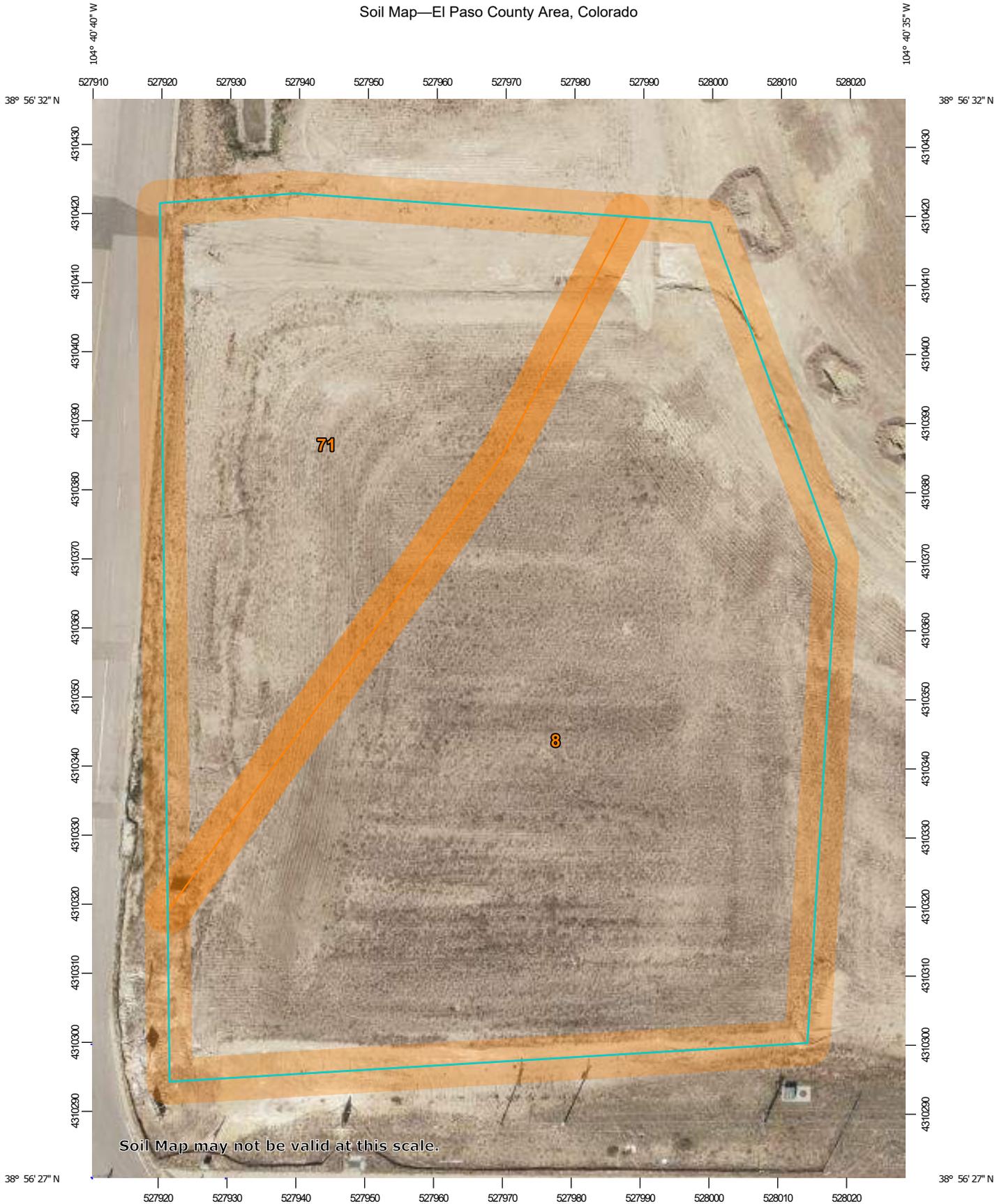
Google Earth

200 ft

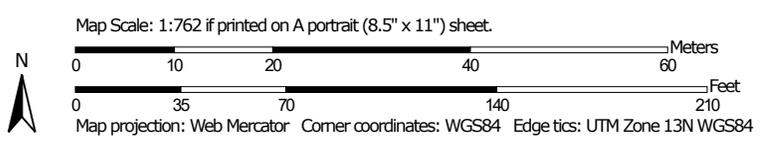


NRCS SOIL MAP

Soil Map—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	1.9	66.9%
71	Pring coarse sandy loam, 3 to 8 percent slopes	0.9	33.1%
Totals for Area of Interest		2.8	100.0%

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v

Elevation: 4,600 to 5,800 feet

Mean annual precipitation: 14 to 16 inches

Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent

Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand

AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent

Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XB210CO - Sandy Foothill

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent

Landform: Depressions

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 19, Aug 31, 2021

El Paso County Area, Colorado

71—Pring coarse sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 369k

Elevation: 6,800 to 7,600 feet

Farmland classification: Not prime farmland

Map Unit Composition

Pring and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pring

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Arkosic alluvium derived from sedimentary rock

Typical profile

A - 0 to 14 inches: coarse sandy loam

C - 14 to 60 inches: gravelly sandy loam

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High
(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 6.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: R048AY222CO - Loamy Park

Hydric soil rating: No

Minor Components

Pleasant

Percent of map unit:

Landform: Depressions

Hydric soil rating: Yes

Other soils

Percent of map unit:

Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 19, Aug 31, 2021

FEMA FIRM MAP

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **Floodways** have been determined, users are encouraged to consult the **Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations** tables contained within the **Flood Insurance Study (FIS)** report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, horizontal projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional inaccuracies in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
 NOAA, NNGS-12
 National Geodetic Survey
 SSMC-3, #9202
 1315 East-West Highway
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3422 or visit its website at <http://www.ngs.noaa.gov>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or dis-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

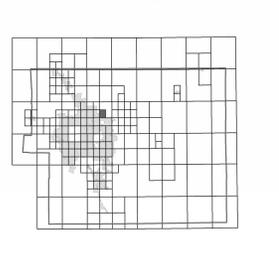
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/mfp>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM-BY-STREAM VERTICAL DATUM CONVERSION INFORMATION.	

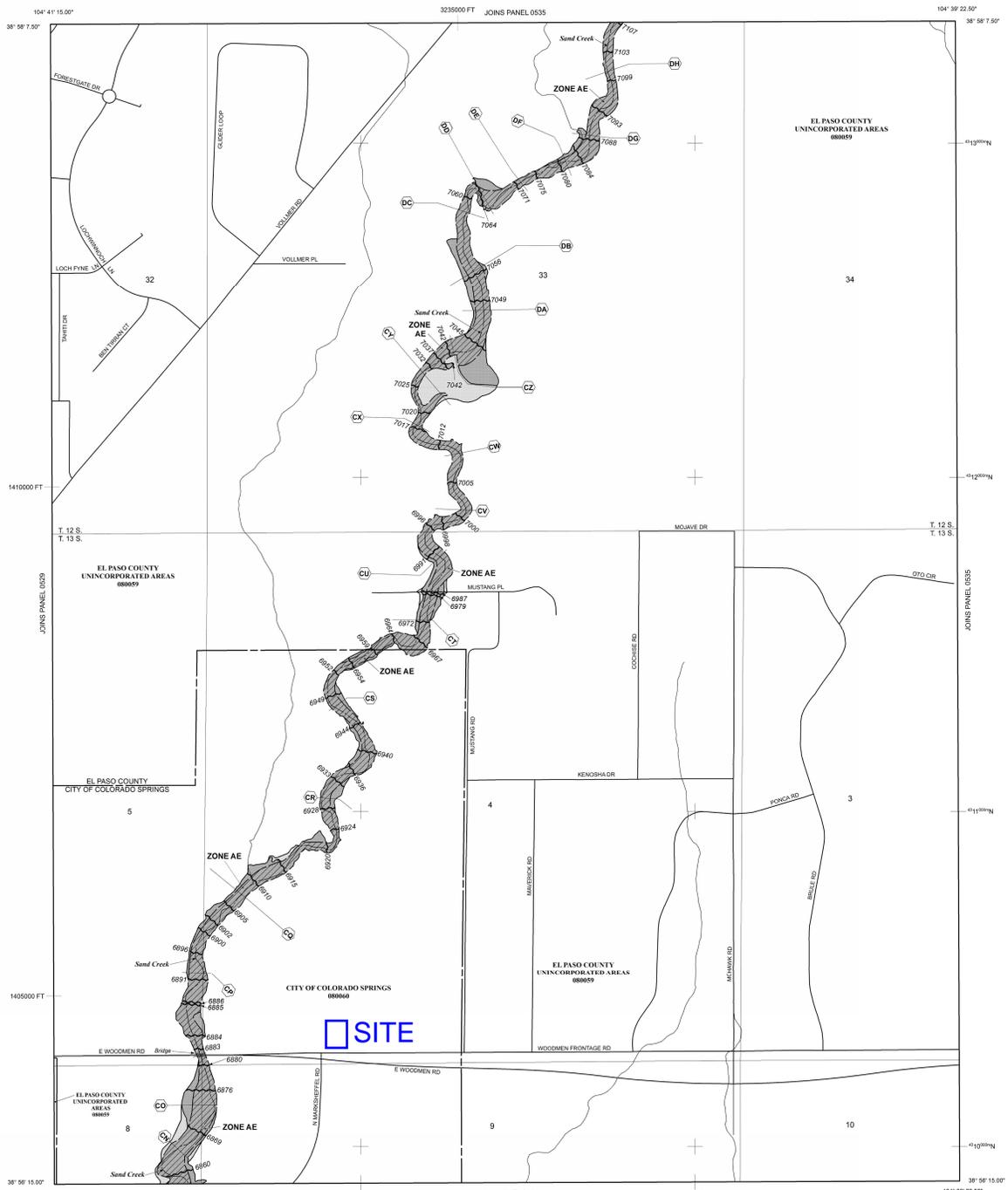
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently identified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazards (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood height.

OTHER FLOOD AREAS

- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot in any given area. This Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones AE, AH, AO, AV, A99, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**
- OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities
- Base Flood Elevation line and value; elevation in feet*
- Base Flood Elevation value where uniform within flood zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

- Cross section line
- Transsect line
- Geographic coordinates refer to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (EPSZONE 050).
- Lambert Conformal Conic Projection
- Bench mark (See explanation in Notes to Users section of this FIRM report)
- M1.5 River Mile

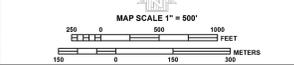
MAP REPOSITORIES: Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTRYWIDE FLOOD INSURANCE RATE MAP: MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL: DECEMBER 7, 2018. In order to comply with the National Flood Insurance Program and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Change.

For community map revision history prior to countrywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



PANEL 0533G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS

PANEL 533 OF 1300
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COUNTY	COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO	SPRING CITY	88000	003	G
EL PASO COUNTY		88000	003	G

Notice to User: The Map Number shown below should be used when showing your address. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0533G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

HYDROLOGIC CALCULATIONS

**SHILOH MESA RETAIL SOUTH FILING NO. 1
AREA RUNOFF AND COEFFICIENT (C) SUMMARY**

EXISTING

BASIN	DEVELOPED / IMPERVIOUS			UNDEVELOPED / NON-IMPERVIOUS			WEIGHTED		WEIGHTED CA		
	TOTAL AREA (Acres)	AREA (Acres)	C5	C100	AREA (Acres)	C5	C100	C5	C100	CA5	CA100
<i>A</i>	2.90	0.17	0.81	0.88	2.73	0.08	0.35	0.12	0.38	0.36	1.11
<i>B</i>	0.14	0.00	0.81	0.88	0.14	0.08	0.35	0.08	0.35	0.01	0.05
<i>C</i>	0.14	0.00	0.81	0.88	0.14	0.08	0.35	0.08	0.35	0.01	0.05

Total 3.18 0.17

Calculated by: LD

Date: 4/26/2022

Checked by: _____

DEVELOPED

BASIN	DEVELOPED / IMPERVIOUS			UNDEVELOPED / NON-IMPERVIOUS			WEIGHTED		WEIGHTED CA		
	TOTAL AREA (Acres)	AREA (Acres)	C5	C100	AREA (Acres)	C5	C100	C5	C100	CA5	CA100
<i>A</i>	0.31	0.20	0.81	0.88	0.11	0.08	0.35	0.55	0.69	0.17	0.21
<i>B</i>	0.55	0.13	0.81	0.88	0.42	0.08	0.35	0.25	0.48	0.14	0.26
<i>C</i>	1.60	1.45	0.81	0.88	0.15	0.08	0.35	0.74	0.83	1.19	1.33
<i>D</i>	0.08	0.08	0.81	0.88	0.00	0.08	0.35	0.81	0.88	0.06	0.07
<i>E</i>	0.20	0.20	0.81	0.88	0.00	0.08	0.35	0.81	0.88	0.16	0.18
<i>F</i>	0.08	0.08	0.81	0.88	0.00	0.08	0.35	0.81	0.88	0.06	0.07
<i>G</i>	0.18	0.09	0.81	0.88	0.09	0.08	0.35	0.45	0.62	0.08	0.11
<i>H</i>	0.23	0.15	0.81	0.88	0.08	0.08	0.35	0.56	0.70	0.13	0.16

Total 3.23 2.38

Calculated by: LD

Date: 4/26/2022

Checked by: _____

**SHILOH MESA RETAIL SOUTH FILING NO. 1
RUNOFF SUMMARY**

EXISTING

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _t (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		<small>* For Calcs See Runoff Summary</small>														
EXA	2.90	0.12	0.38	0.12	100	0.02	14.0	250	3.0%	4.0	1.0	15.1	3.5	5.9	1.2	6.5
EXB	0.14	0.08	0.35	0.08	20	0.02	6.6	0	2.0%	3.0	0.0	6.6	4.7	8.3	0.1	0.4
EXC	0.14	0.08	0.35	0.08	20	0.02	6.6	435	2.0%	3.0	2.4	9.0	4.2	7.4	0.0	0.4

Calculated by: LD
Date: 4/26/2022
Checked by: _____

DEVELOPED

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _t (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		<small>* For Calcs See Runoff Summary</small>														
A	0.31	0.55	0.69	0.55	20	0.02	3.5	180	3.0%	4.0	0.8	4.3	5.2	9.5	0.9	2.0
B	0.55	0.25	0.48	0.25	100	0.02	12.2	100	2.0%	3.0	0.6	12.7	3.7	6.4	0.5	1.7
C	1.60	0.74	0.83	0.74	40	0.02	3.3	435	2.0%	3.0	2.4	5.7	4.8	8.7	5.7	11.6
D	0.08	0.81	0.88	0.81	50	0.02	2.9	0	60.0%	10.0	0.0	2.9	5.6	10.4	0.4	0.7
E	0.20	0.81	0.88	0.81	20	0.33	0.7	0	20.0%	6.0	0.0	0.7	6.6	12.7	1.1	2.2
F	0.08	0.81	0.88	0.81	12	0.02	1.4	0	60.0%	10.0	0.0	1.4	6.2	11.8	0.4	0.8
G	0.18	0.45	0.62	0.45	12	0.02	3.3	0	60.0%	10.0	0.0	3.3	5.5	10.2	0.4	1.1
H	0.23	0.56	0.70	0.56	18	0.02	3.3	180	4.3%	6.0	0.5	3.8	5.3	9.8	0.7	1.6

Calculated by: LD
Date: 4/26/2022
Checked by: _____

**SHILOH MESA FILING NO. 2 LOT 1 SCHOOL
SURFACE ROUTING SUMMARY**

<i>Design Point(s)</i>	<i>Contributing Basins</i>	<i>Area (ac)</i>	<i>Flow (cfs)</i>	
			<i>Q₅</i>	<i>Q₁₀₀</i>
1	G	0.18	0.4	1.1
2	C	1.60	5.7	11.6
3	E	0.20	1.1	2.2
4	A	0.31	0.9	2.0
5	D	0.08	0.4	0.7
6	H	0.23	0.7	1.6
7	F	0.08	0.4	0.8
8	A,B,C,G,H	2.87	8.3	18.0

Calculated by: LD

Date: 4/26/2022

Checked by: _____

ST GABRIELS SCHOOL PIPE ROUTING SUMMARY

<i>Pipe Run #</i>	<i>Inlet #</i>	<i>Contributing Flow Sources</i>	<i>5 Year Flow (cfs)</i>	<i>100 Year Flow (cfs)</i>	<i>Slope</i>	<i>Pipe Size & Type</i>	<i>Owner</i>
<i>PR1</i>	<i>1</i>	G	0.4	1.1	1%	12" HDPE	Private
<i>PR2</i>	<i>2</i>	G,C	6.2	12.7	0.5%	24" HDPE	Private
<i>PR3</i>	<i>3</i>	G,C,H	6.9	14.3	0.5%	24" HDPE	Private
<i>PR4</i>	<i>-</i>	G,C,H	6.9	14.3	0.5%	24" HDPE	Private
<i>PR5</i>	<i>-</i>	G,C,H	6.9	14.3	0.5%	24" HDPE	Private
<i>PR6</i>	<i>-</i>	G,C,H	6.9	14.3	0.5%	24" HDPE	Private
<i>PR7</i>	<i>4</i>	A	0.9	2.0	10%	12" HDPE	Private
<i>PR8</i>	<i>-</i>	Pond Outlet	0.1	2.8	3%	12" HDPE	Private
<i>PR9</i>	<i>-</i>	Pond Outlet	0.1	2.8	3%	12" HDPE	Private

Calculated by: LD

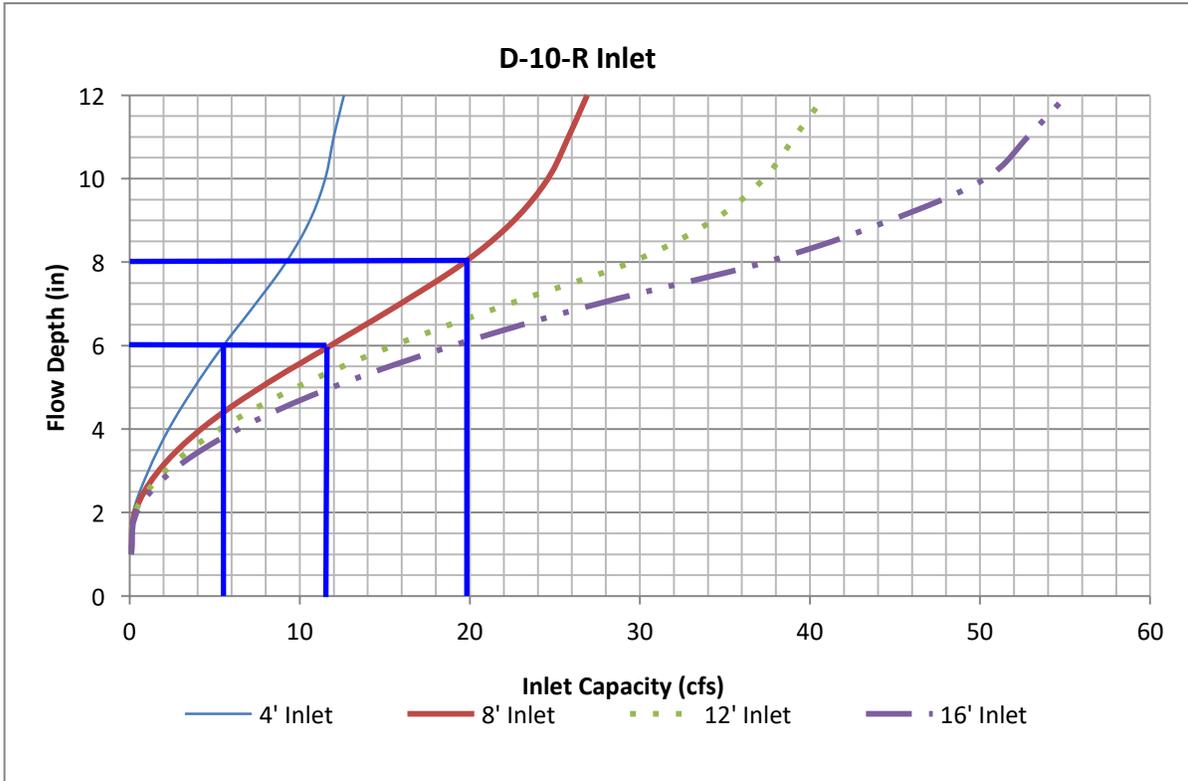
Date: 4/26/2022

Checked by: _____

HYDRAULIC CALCULATIONS

2214.00

Figure 8-12. Inlet Capacity Chart Sump Conditions, Curb Opening (D-10-R) Inlet



MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Shiloh Mesa Retail - South** Location: **Geraldine Point South Gutter - Capacity**
 By: **Dane Frank** Date: **4/27/2022**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

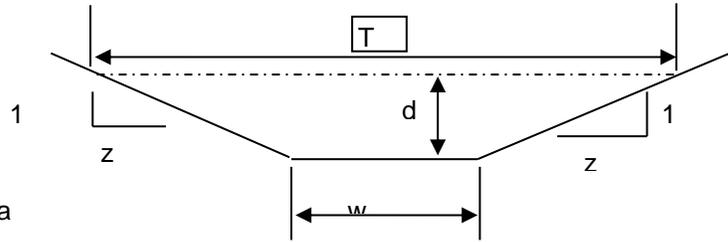
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 25
 b (btm width, ft)= 0
 d (depth, ft)= 0.5
 S (slope, ft/ft) 0.023
 n low = 0.013
 n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.5	3.13	13.01	0.24	6.69834173	20.9323	6.698342	20.9323	12.5	0.250

Sc low = 0.0041 Sc high = 0.0041

s_c = critical slope ft / ft

T = top width of the stream

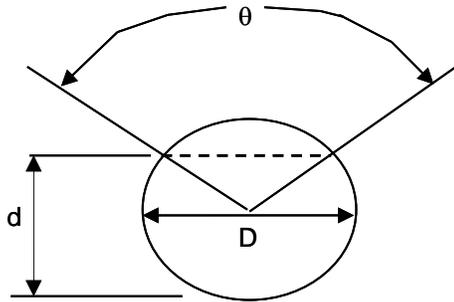
d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.0029	0.0054	0.0029	0.0054

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #1 (Q100=1.1 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

D= 12 inches
 d= 12 inches
 n= 0.013 mannings coeff
 theta= 0.0 degrees
 S= 0.01 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

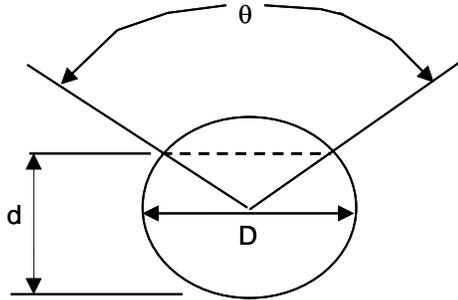
Solution to Mannings Equation					Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
0.79	3.14	0.25	4.54	3.56	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #2 (Q100=12.7 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.005 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

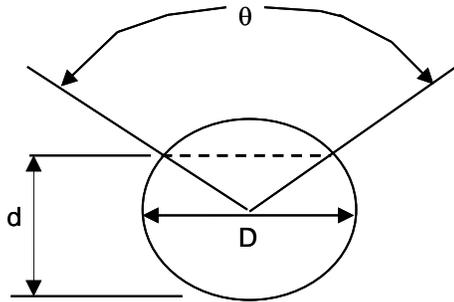
Solution to Mannings Equation					Manning's n-values	
Area, ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	5.52	17.33	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #3 (Q100=14.7 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.005 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

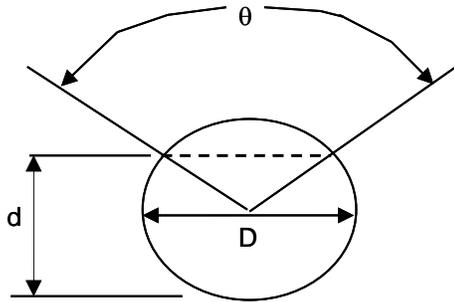
Solution to Mannings Equation					Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	5.52	17.33	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #4 (Q100=14.7 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.005 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

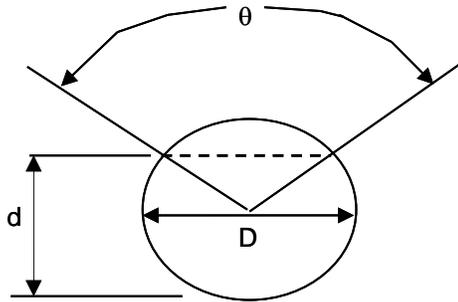
Solution to Mannings Equation					Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	5.52	17.33	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #5 (Q100=14.7 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data Entry Cells



INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 manning's coeff
 theta= 0.0 degrees
 S= 0.005 slope in/in

Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

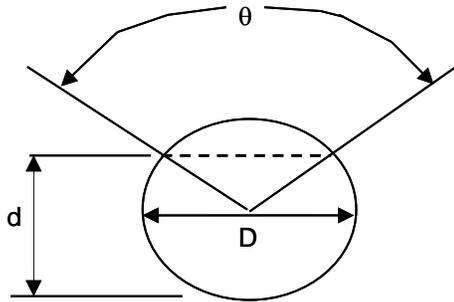
Solution to Mannings Equation					Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	5.52	17.33	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #6 (Q100=14.7 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

- R=A/P
- A=cross sectional area
- P=wetted perimeter
- S=slope of channel
- n=Manning's roughness coefficient

INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.005 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

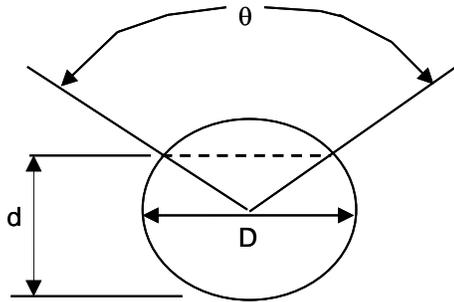
Solution to Mannings Equation					Manning's n-values	
Area, ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	5.52	17.33	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #7 (Q100=2.0 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

R=A/P
 A=cross sectional area
 P=wetted perimeter
 S=slope of channel
 n=Manning's roughness coefficient

INPUT

D= 12 inches
 d= 12 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.1 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

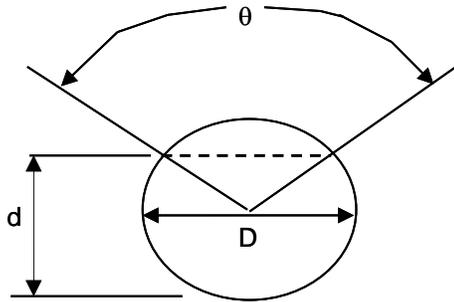
Solution to Mannings Equation					Manning's n-values	
Area, ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
0.79	3.14	0.25	15.54	12.20	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #8 (Q100=2.8 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

- R=A/P
- A=cross sectional area
- P=wetted perimeter
- S=slope of channel
- n=Manning's roughness coefficient

INPUT

D= 12 inches
 d= 12 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.03 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

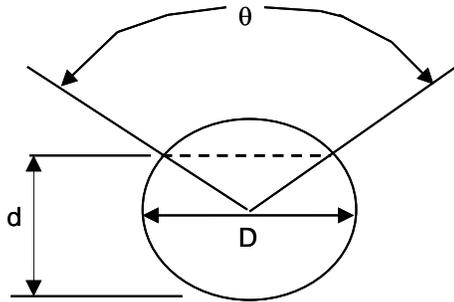
Solution to Mannings Equation					Manning's n-values	
Area, ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
0.79	3.14	0.25	8.51	6.68	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: Shilo Mesa Retail South Location: Pipe Run #9 (Q100=2.8 cfs)
 By: Dane Frank Date: 4/27/2022
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells



Mannings Formula

$$Q = (1.486/n) A R_h^{2/3} S^{1/2}$$

- R=A/P
- A=cross sectional area
- P=wetted perimeter
- S=slope of channel
- n=Manning's roughness coefficient

INPUT

D= 12 inches
 d= 12 inches
 n= 0.012 mannings coeff
 theta= 0.0 degrees
 S= 0.03 slope in/in

$$V = (1.49/n) R_h^{2/3} S^{1/2}$$

$$Q = V \times A$$

Solution to Mannings Equation					Manning's n-values	
Area, ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
0.79	3.14	0.25	8.51	6.68	PVC	0.01
					PE (<9" dia)	0.015
					PE (>12" dia)	0.02
					PE(9-12" dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

DETENTION BASIN DESIGN CALCULATIONS

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input

Calculated cells

***Design Storm: 1-Hour Rain Depth	2-Year Event	1.19	inches
***Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50	inches
***Major Storm: 1-Hour Rain Depth	100-Year Event	2.52	inches
Optional User Defined Storm	CUHP		
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event		

Designer: Dane Frank
Company: Terra Nova Engineering
Date: April 26, 2022
Project: Shilo Mesa North
Location: Sand Filter

Max Intensity for Optional User Defined Storm: 0

SITE INFORMATION (USER-INPUT)

Sub-basin Identifier	A	B	C	G	H										
Receiving Pervious Area Soil Type	Sandy Loam														
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	0.310	0.550	1.600	0.180	0.230										
Directly Connected Impervious Area (DCIA, acres)	0.200	0.130	1.450	0.090	0.150										
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000										
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000										
Separate Pervious Area (SPA, acres)	0.110	0.420	0.150	0.090	0.080										
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	C	C	C	C	C										

CALCULATED RESULTS (OUTPUT)

Total Calculated Area (ac, check against input)	0.310	0.550	1.600	0.180	0.230										
Directly Connected Impervious Area (DCIA, %)	64.5%	23.6%	90.6%	50.0%	65.2%										
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%										
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%										
Separate Pervious Area (SPA, %)	35.5%	76.4%	9.4%	50.0%	34.8%										
A _e (RPA / UIA)	0.000	0.000	0.000	0.000	0.000										
I _a Check	1.000	1.000	1.000	1.000	1.000										
f / I for 2-Year Event:	0.9	0.9	0.9	0.9	0.9										
f / I for 5-Year Event:	0.5	0.5	0.5	0.5	0.5										
f / I for 100-Year Event:	0.3	0.3	0.3	0.3	0.3										
f / I for Optional User Defined Storm CUHP:															
IRF for 2-Year Event:	1.00	1.00	1.00	1.00	1.00										
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00										
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00										
IRF for Optional User Defined Storm CUHP:															
Total Site Imperviousness: I _{total}	64.5%	23.6%	90.6%	50.0%	65.2%										
Effective Imperviousness for 2-Year Event:	64.5%	23.6%	90.6%	50.0%	65.2%										
Effective Imperviousness for 5-Year Event:	64.5%	23.6%	90.6%	50.0%	65.2%										
Effective Imperviousness for 100-Year Event:	64.5%	23.6%	90.6%	50.0%	65.2%										
Effective Imperviousness for Optional User Defined Storm CUHP:															

LID / EFFECTIVE IMPERVIOUSNESS CREDITS

This line only for WQCV Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT** : Reduce Detention By:	0.0%	0.2%	0.0%	0.2%	0.1%	N/A									
User Defined CUHP CREDIT: Reduce Detention By:															

Total Site Imperviousness:	70.4%
Total Site Effective Imperviousness for 2-Year Event:	70.4%
Total Site Effective Imperviousness for 5-Year Event:	70.4%
Total Site Effective Imperviousness for 100-Year Event:	70.4%
Total Site Effective Imperviousness for Optional User Defined Storm CUHP:	

Notes:

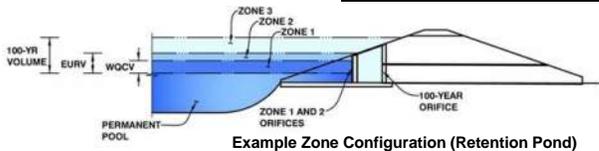
- * Use Green-Ampt average infiltration rate values from Table 3-3.
- ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.
- *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Shiloh Mesa Retail South Filing No. 1

Basin ID: Final detention and water quality



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.36	0.079	Orifice Plate
Zone 2 (EURV)	4.79	0.214	Orifice Plate
Zone 3 (100-year)	5.60	0.103	Weir&Pipe (Restrict)
Total (all zones)		0.396	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain		
Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	4.79	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	18.10	inches
Orifice Plate: Orifice Area per Row =	0.61	sq. inches (diameter = 7/8 inch)

Calculated Parameters for Plate		
WQ Orifice Area per Row =	4.236E-03	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.60	3.19					
Orifice Area (sq. inches)	0.61	0.61	0.61					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice		
Vertical Orifice Area =	N/A	ft ²
Vertical Orifice Centroid =	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.80	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	2.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	2.00	N/A	feet
Overflow Grate Type =	Close Mesh Grate	N/A	
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir		
Height of Grate Upper Edge, H _u =	4.80	N/A
Overflow Weir Slope Length =	2.00	N/A
Grate Open Area / 100-yr Orifice Area =	14.82	N/A
Overflow Grate Open Area w/o Debris =	3.16	N/A
Overflow Grate Open Area w/ Debris =	1.58	N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	12.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	3.80		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate		
Outlet Orifice Area =	0.21	ft ²
Outlet Orifice Centroid =	0.19	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.20	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	6.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	3.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway		
Spillway Design Flow Depth =	0.72	feet
Stage at Top of Freeboard =	7.72	feet
Basin Area at Top of Freeboard =	0.18	acres
Basin Volume at Top of Freeboard =	0.62	acre-ft

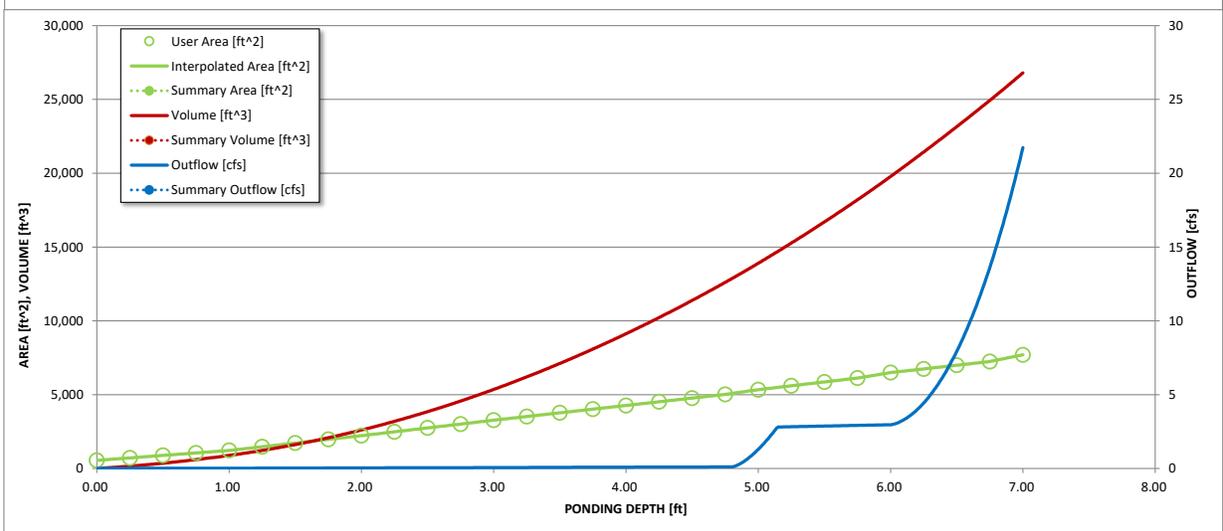
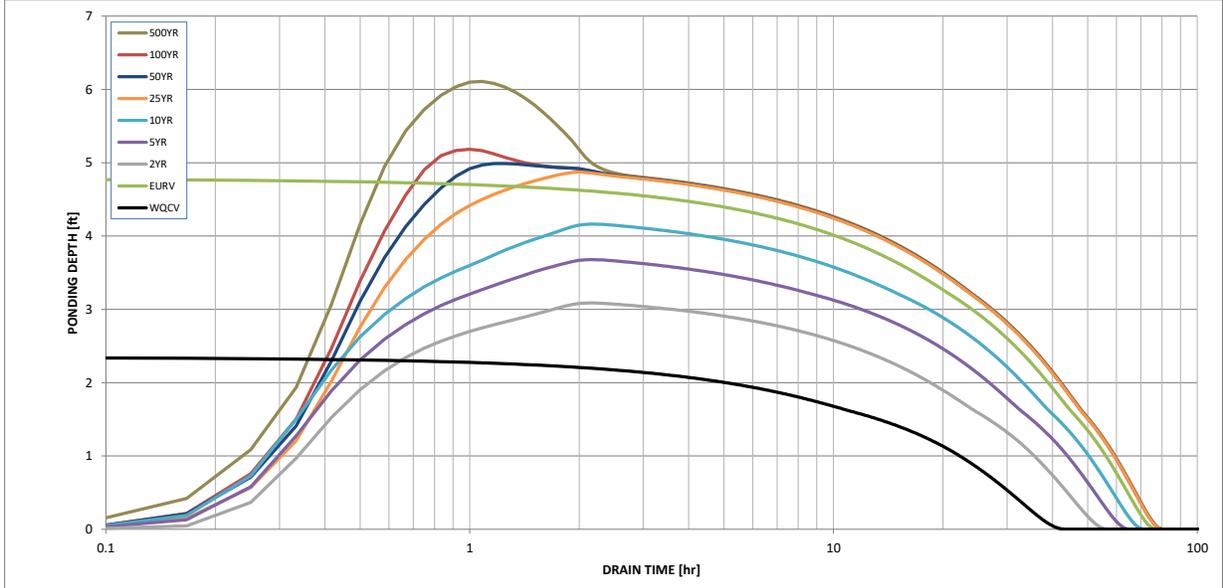
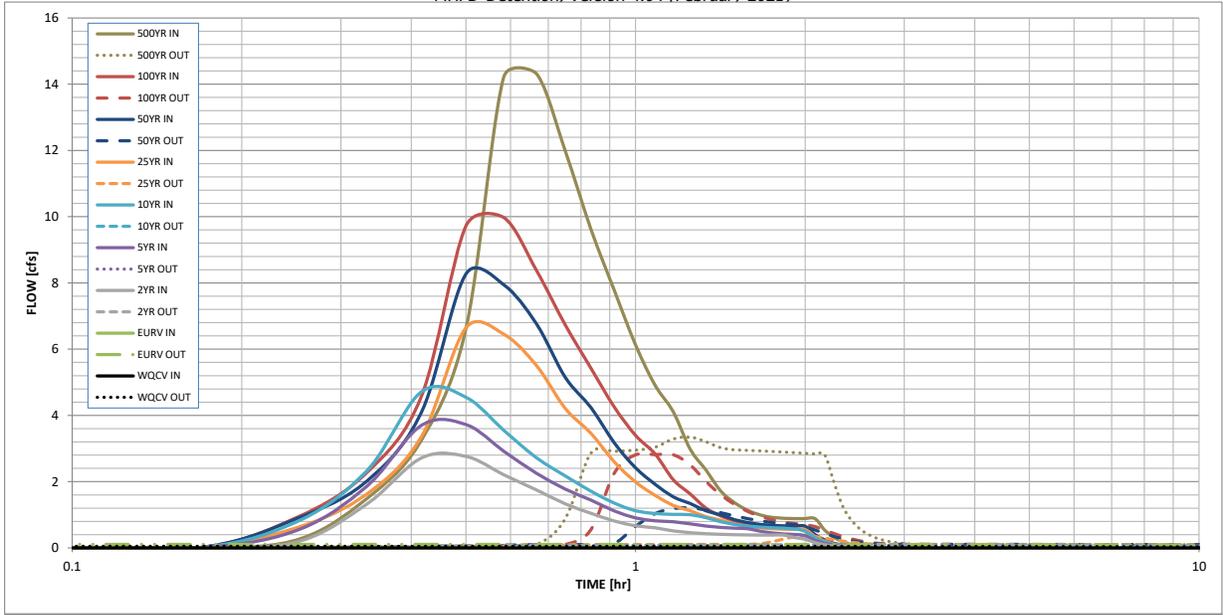
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	0.83	1.09	1.33	1.69	1.99	2.31	3.14
One-Hour Rainfall Depth (in) =	0.079	0.293	0.138	0.191	0.239	0.325	0.398	0.482	0.695
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.138	0.191	0.239	0.325	0.398	0.482	0.695
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.0	0.0	0.1	0.9	1.8	2.8	5.5
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.01	0.02	0.29	0.56	0.89	1.73
Peak Inflow Q (cfs) =	N/A	N/A	2.8	3.7	4.7	6.6	8.3	10.0	14.3
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.1	0.4	1.2	2.8	3.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.4	1.7	0.4	0.7	1.0	0.6
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.1	0.3	0.9	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	64	48	55	60	66	65	63	59
Time to Drain 99% of Inflow Volume (hours) =	40	70	52	59	65	72	72	71	69
Maximum Ponding Depth (ft) =	2.35	4.79	3.09	3.68	4.16	4.87	4.99	5.18	6.11
Area at Maximum Ponding Depth (acres) =	0.06	0.12	0.08	0.09	0.10	0.12	0.12	0.13	0.15
Maximum Volume Stored (acre-ft) =	0.079	0.294	0.129	0.178	0.225	0.304	0.317	0.342	0.469

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

FORBAY VOLUMES

FORBAY VOLUME

Required Forbay Volume = 2% of WQCV
 WQCV = 0.079 ac-ft
 WQCV = 3,441 cu-ft
 2% of WQCV = 34 cu-ft

<i>ELEV</i>	<i>AREA</i>	<i>AREA AVG.</i>	<i>DELTA ELEV.</i>	<i>VOLUME</i>	<i>VOLUME TOTAL</i>
6902.00	64	64	1.5	96	
6903.50	64				96

Design Volume: 96 C.F.
 0.002 A.F.

PROPOSED MICROPOOL VOLUME

<i>ELEV</i>	<i>AREA</i>	<i>AREA AVG.</i>	<i>DELTA ELEV.</i>	<i>VOLUME</i>	<i>VOLUME TOTAL</i>
6898.50	24	24	3	72	
6901.50	24				72

End Area Method: 72 C.F.
 0.002 A.F.

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Shiloh Mesa Retail South** Location: **EDB Forebay Notch - Q=10.0 cfs * 2% = 0.20 cfs**
 By: **Dane Frank** Date: **4/28/2022**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

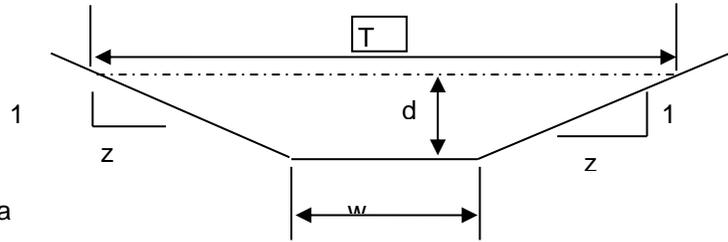
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 0
 b (btm width, ft)= 0.12
 d (depth, ft)= 1.5
 S (slope, ft/ft) 0.005
 n_{low} = 0.013
 n_{high} = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
1.5	0.18	3.12	0.06	1.20669572	0.21721	1.206696	0.21721	0.12	1.500

Sc low = 0.1656 Sc high = 0.1656

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.1159	0.2152	0.1159	0.2152

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Shiloh Mesa Retail South** Location: **EDB Trickle Channels (need Q= 0.2 cfs)**
 By: **Dane Frank** Date: **4/28/2022**
 Chk By: _____ Date: _____ version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

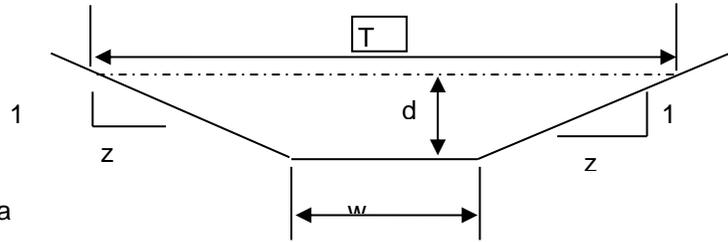
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 0
 b (btm width, ft)= 0.24
 d (depth, ft)= 0.5
 S (slope, ft/ft) 0.005
 n_{low} = 0.013
 n_{high} = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.5	0.12	1.24	0.10	1.70359501	0.20443	1.703595	0.20443	0.24	0.500

Sc low = 0.0277 Sc high = 0.0277

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

.7 Sc	1.3 Sc	.7 Sc	1.3 Sc
0.0194	0.0360	0.0194	0.0360

2214.00

Figure 13-12c. Emergency Spillway Protection

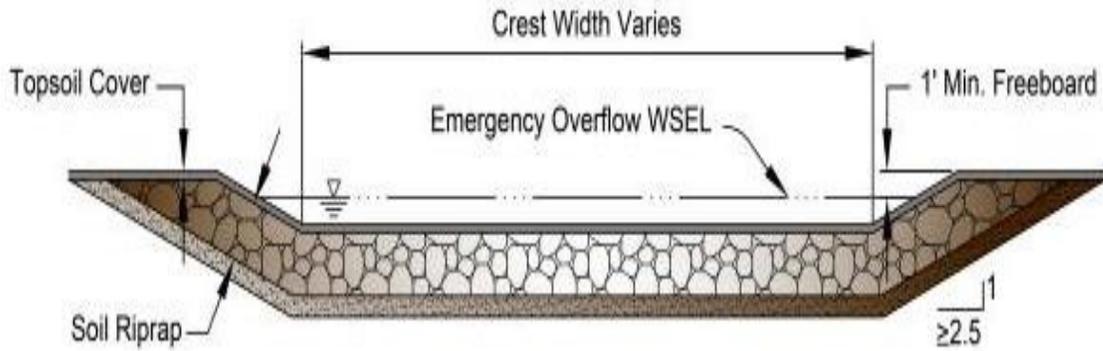
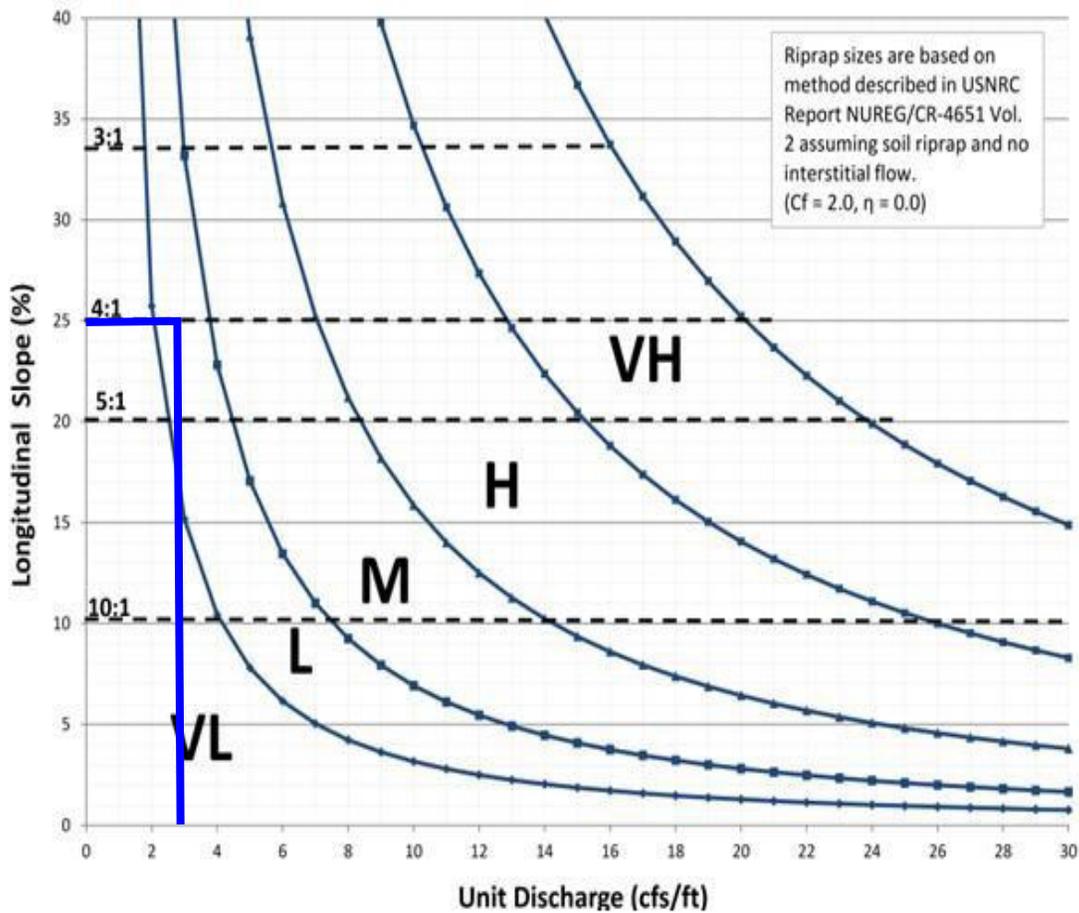
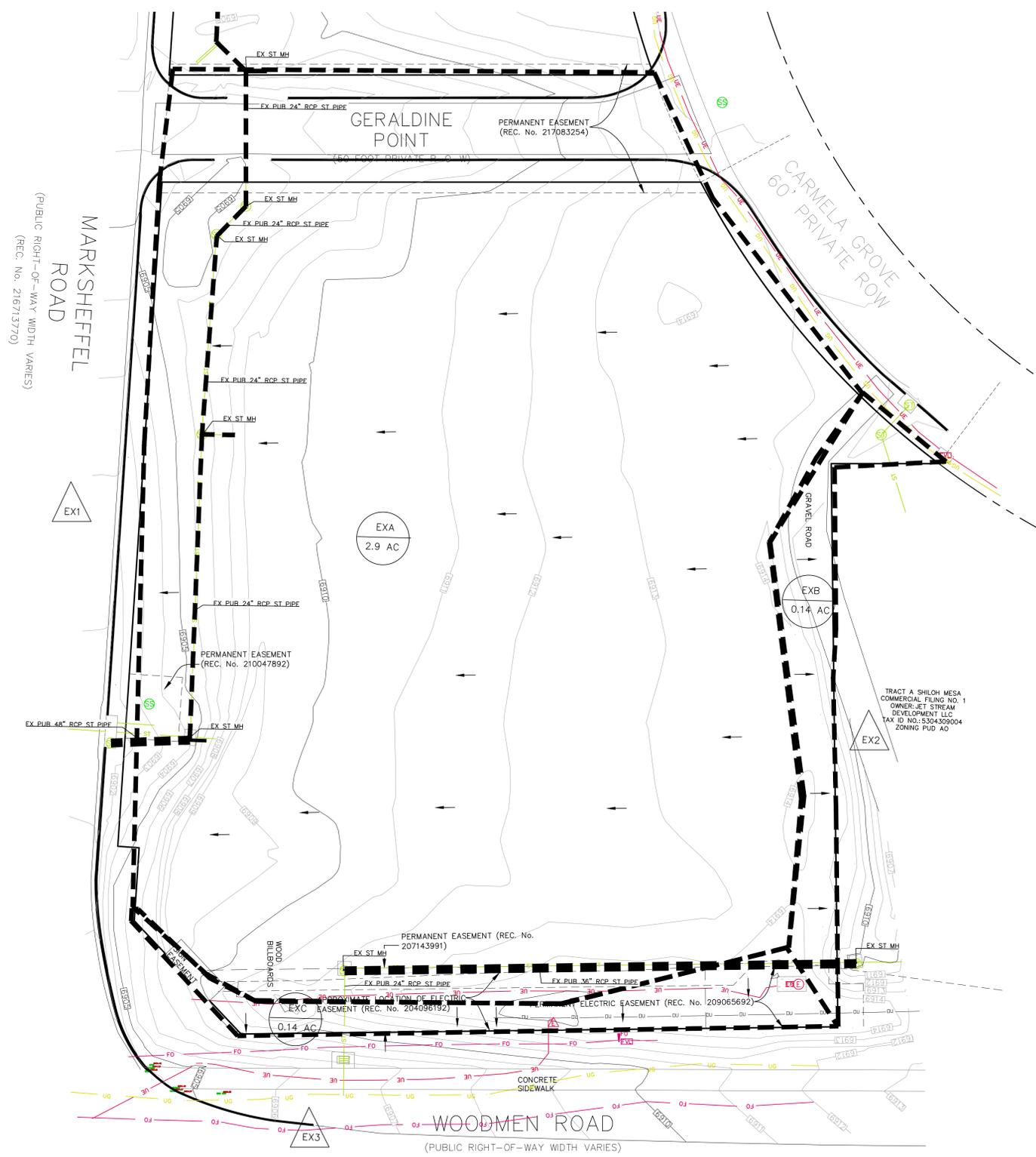


Figure 13-12d. Riprap Types for Emergency Spillway Protection



DRAINAGE MAP

N:\jobs\2214.00\DP\221400 DP.dwg, 4/28/2022 9:22:28 AM



EXISTING

BASIN	AREA TOTAL (Acres)	TOTAL FLOWS	
		Q _s (cfs)	Q _{in} (cfs)
EXA	2.90	1.2	6.5
EXB	0.14	0.1	0.4
EXC	0.14	0.1	0.4

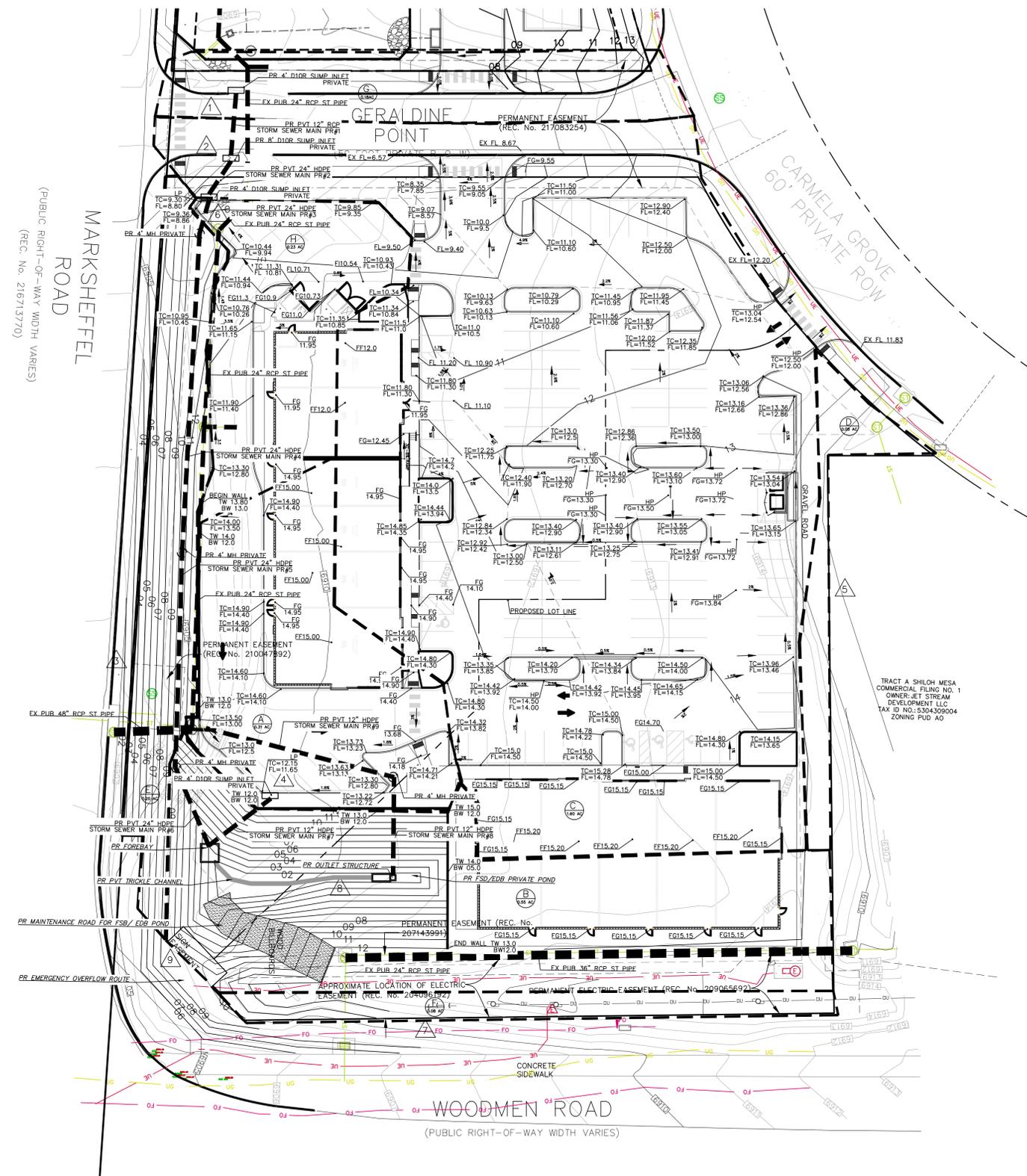
- LEGEND**
- P-7
12.22 BASIN DESIGNATION
 - 12.22 AREA IN BASIN (AC)
 - D DESIGN POINT
 - BASIN BOUNDARY
 - - - EXISTING 2' CONTOUR
 - - - EXISTING 10' CONTOUR
 - ← ROAD AND DITCH FLOW DIRECTION

- GRADING LEGEND**
- EXISTING CONTOURS - MAJOR --- 6130 ---
 - EXISTING CONTOURS - MINOR --- 6132 ---
 - PROPOSED CONTOURS - MAJOR **6130**
 - PROPOSED CONTOURS - MINOR **6132**
 - PROPERTY LINE - - - - -
 - FLOW DIRECTION → 3:1
 - TOP OF WALL TW
 - FINISHED GROUND FG
 - FLOWLINE FL
 - TOP OF STAIRS TS
 - BOTTOM OF STAIRS BS

- NOTE:**
- EXISTING VEGETATION CONSISTS OF NATIVE PRAIRIE GRASSES AND SHRUBS WITH GOOD TO EXCELLENT COVERAGE OF 75% TO 90%
 - AT THE TIME OF FINAL CONSTRUCTION EROSION CONTROL BLANKETS WILL NEED TO BE INSTALLED ON ALL 3:1 SLOPES

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DEVELOPED

BASIN	AREA TOTAL (Acres)	TOTAL FLOWS	
		Q _s (cfs)	Q ₁₀₀ (cfs)
A	0.31	0.9	2.0
B	0.55	0.5	1.7
C	1.60	5.7	11.6
D	0.08	0.4	0.7
E	0.20	1.1	2.2
F	0.08	0.4	0.8
G	0.18	0.4	1.1
H	0.23	0.9	2.0

LEGEND

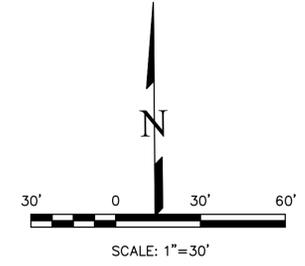
- P-7
12.22 BASIN DESIGNATION
- D DESIGN POINT
- BASIN BOUNDARY
- - - - EXISTING 2' CONTOUR
- - - - EXISTING 10' CONTOUR
- ROAD AND DITCH FLOW DIRECTION

GRADING LEGEND

- EXISTING CONTOURS - MAJOR 6130
- EXISTING CONTOURS - MINOR 6132
- PROPOSED CONTOURS - MAJOR 6130
- PROPOSED CONTOURS - MINOR 6132
- PROPERTY LINE
- FLOW DIRECTION 3:1
- TOP OF WALL TW
- FINISHED GROUND FG
- FLOWLINE FL
- TOP OF STAIRS TS
- BOTTOM OF STAIRS BS

NOTE:

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