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Eastonville Road – Londonderry Dr. to Rex Rd. Segment 2 Improvements Stationing 47+00.00 – 79+31.62

Final Drainage Report

March 2024 HR Green Project No: 201662.08

Prepared For:

D.R. Horton Contact: Riley Hillen, P.E. 9555 S. Kingston Ct. Englewood, CO 80112

Prepared By:

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> EDARP Filing No: CDR2321

> > See comment letter also.



Eastonville Road Final Drainage Report Project No.: 201662.08

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Colleen Monahan, P.E., LEED AP State of Colorado No. 56067 For and on behalf of HR Green Development, LLC

Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Authorized Signature Address: D.R. Horton

9555 S. Kingston Court Englewood, CO

El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

County Engineer/ECM Administrator

Conditions:



Date

Date



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Include reference material (see items mentioned throughout the report to include)



I. General Purpose, Location and Description

a. Purpose

The purpose of this Final Drainage Report (FDR) for Eastonville Road Segment 2 Improvements is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls. This drainage report will detail the improvements of Eastonville Road from Londonderry Dr. to Rex Road for Segment 2. Stations 47+00.00 to 79+32.00 contain the Segment 2 Improvements for the Eastonville Road from Londonderry Drive to Rex Road for the portion of the project north of Grandview Filing No. 1. The project is all one project, however, the planset has been broken into two segments to align with the Grandview Reserve Filings. A separate FDR describes Segment 2 of the project.

b. Location ____ gravel

Eastonville Road from Londonderry Dr. to Rex Road, referred to as 'the site' herein, is an existing 26' wide temporary pavement road in El Paso County, Colorado. Per field inspection the existing pavement is not full depth, and therefore described as 'temporary' for the purpose of this report. The site lies in the existing 60' wide El Paso County Right-of-Way within Sections 21 and 28, Township 12 South, Range 64 West of the 6th Principal Meridian, in El Paso County, State of Colorado.

The site is bound by undeveloped land to the east and west that has historically been used as ranching lands. Falcon Regional Park, which contains ballparks and parking, and Falcon High School also border the site to the west. All lands to the east and west of the site are unplatted. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 0.69 miles (2.17 acres) of existing temporary pavement roadway north of Londonderry Dr. and south of Rex Road. Per field inspection the existing pavement is not full depth, and therefore described as 'temporary' for the purpose of this report. The existing temporary pavement width for the length of the project is 26' wide. There are 4' wide gravel shoulders and native landscaped swales are located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts. See Appendix A for an existing conditions photo.

The existing roadway has slopes ranging from 0.3% up to about 4%. The general topography of the surrounding area is typical of high desert, short prairie grass with gently rolling hillside with slopes ranging from 2% to 4%. The project site drains generally from the west to the east and is tributary to Black Squirrel Creek.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam, Type A Blakeland loamy sand and Type B Stapleton sandy loam. The NRCS soil survey is presented in Appendix A.

Gieck Ranch Tributary #1 (Channel A) is the only drainageway that traverses the site in the west to east direction through an existing culvert under Eastonville Road. The channel is a mapped wetland and a wetland permit will be required for a part of this Eastonville Road improvement project. Channel A is not within a FEMA floodplain.

Gieck Ranch Tributary #2 is located on the north end of the project site and will not be impacted by this project. There are no known irrigation facilities in the area.



Existing utilities include an underground gas line that runs under Eastonville road through the Grandview reserve property south of the segment 2 improvements, an existing raw water line that follows the west side of Eastonville north of Falcon Regional Park, and an existing aboveground electrical line along the western side of Eastonville Road. An existing drainage map with these facilities is presented in Appendix F.

d. Floodplain Statement

Based on FEMA Firm map 08041C0552G December 7, 2018, the site is not located in any FEMA designated floodplain. See FEMA Firm Map in Appendix A. There is a Zone A floodplain north of the site and a Zone AE south of the site, both of which will not be altered with the associated Eastonville Road improvements.

II. Drainage Design Criteria

a. Drainage Criteria

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. The detention pond allowable release rate will be limited to less than historic rates.

Rainfall Depths per NOAA Atlas 14			
Return Period (yr) 5 100			
1-hr Rainfall Depth (in)	1.21	2.49	

Inlet sizing was performed per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

III. Drainage Basins and Subbasins

a. Major Basin Description

The site is located within the Gieck Ranch Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

- 1. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 2. "Master Development Drainage Plan Meridian Ranch" prepared by Tech Contractors, July 2021.
- 3. "Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch" by Tech Contractors, August 2022.

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and is rolling range land typical of Colorado's semi-arid climates. It should be noted that the Gieck Ranch DBPS has not been approved at the time of this report.



The Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch indicate that the Eastonville Road culvert crossing at the Gieck Ranch Tributary #1, within the project boundary, does not provide enough capacity for the historic flow rates. This culvert will be upgraded as part of this project.

Within the Gieck Ranch Drainage Basin, ranching has historically been the predominant land use, with rolling topography between 2%-4% slopes. Recently urbanization is occurring within the drainage basin, most notably for this project are Meridian Ranch and Latigo Trails Developments. Both are single family residential neighborhoods located upstream to the west and northwest of the Eastonville Segment 2 Improvements project site.

b. Existing Subbasin Description

Eastonville Road Segment 2 (the site) accepts flows from areas to the west and northwest of the site, including portions of Meridian Ranch and Latigo Trails Development. The flows and design points used in the following descriptions are taken from the approved Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch provides the detailed analysis of the pond releases and flows as they outfall from those developments upstream of this Eastonville Road site. For the purpose of this report, full buildout of the Meridian Ranch development was assumed; hence the developed peak flow rates from the "future buildout conditions" for the entirety of Meridian Ranch were used to evaluate the existing conditions below.

Basin EX1 (The Sanctuary Filing 1 FG-38) is 85.16 acres of undeveloped area and temporary pavement area to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 for a total area of 321.5 acres (The Sanctuary Filing 1 G18). Flows at DP1 ($Q_5 = 28.3$ cfs $Q_{100} = 365.2$ cfs) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Gieck Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin EX2 (The Sanctuary Filing 1 FG36) is 18.88 acres undeveloped area, parking lot, and temporary pavement to the crown of Eastonville Road roadway. Stormwater from this basin is conveyed overland to DP2 (The Sanctuary Filing 1 FG36). Flows at DP2 ($Q_5 = 1.7$ cfs $Q_{100} = 18.8$ cfs) are conveyed southerly across Rex Road in an existing 24" RCP culvert and discharges to Basin EX3.

Basin EX3 is 51.06 acres of undeveloped area and the Falcon Regional Park ball fields and temporary pavement to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G15 via an existing roadside swale where it then combines with DP2 flows. Flows travel to DP3 for a total area of 131.3 acres (The Sanctuary Filing 1 Design Point G16) where they are conveyed across Eastonville Road in an existing 24" CMP culvert ($Q_5 = 6.1 \text{ cfs } Q_{100} = 112.1 \text{ cfs}$).

Basin EX4 is 62.87 acres of undeveloped area and temporary pavement to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G12 (Meridian Ranch Pond G) to Gieck Ranch Tributary #1 and an existing roadside swale to DP 4 for a total area of 832.7 acres (The Sanctuary Filing 1 Design Point G06) ($Q_5 = 22.4$ cfs $Q_{100} = 491$ cfs). Flows at DP4 are conveyed across Eastonville Road in an existing 18" CMP culvert and discharges to Gieck Ranch Tributary #1 (Channel A).



c. Proposed Subbasin Description Description of Proposed Project

The proposed project includes improvements to Eastonville Road from Londonderry Drive to Rex Road. As described above, the current condition of the existing roadway in this area consists of 26' wide temporary pavement roadway with 4' wide sand shoulders and weedy swales located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts.

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). This includes Basins EA1-EA11.

Refer to the Eastonville Road Segment 1 improvements FDR for subbasin information and calculations south of subbasins EA10 & EA11.

Eastonville Road Basins

Unresolved: – Verify <u>all</u> basin flows with hydrology spreadsheet

Basin EA1 is 0.22 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.7$ cfs $Q_{100} = 1.3$ cfs) is conveyed in curb and gutter to DP2. Flows at DP2 are captured in a 5' Type R sump inlet (Public) and pped to Pond C, a private full spectrum sand filter basin. Basin EA1 will be detained by the Pond C Sand Filter.

Basin EA2 is 0.25 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.8 \text{ cfs } Q_{100} = 1.5 \text{ cfs}$) is conveyed in curb and gutter to DP3. Flows at DP3 are captured in a 5' Type R sump inlet (Public) and piped to Pond C. Basin EA2 will be detained by the Pond C Sand Filter.

Basin EA3 is 0.20 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.7$ cfs $Q_{100} = 1.4$ cfs) is conveyed in curb and gutter to DP5. Flows at DP5 are captured in

Unresolved: DP6.1? There is no DP9.1 shown on map or listed in hydrology spreadsheet
(Public) and piped to DP9.1. Basin EA3 will not be detained per the Meridian Ranch Unresolved: Include excerpt in append

Dasin EA4 is 0.17 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-SeMeridian Ranch MDDP ar Stormwater ($Q_5 = 0.5$ cfs $Q_{100} = 1.1$ cfs) is conveyed in curb and gutter to DP6. Flows at DP6 are captured in a 5' Type R sump inlet (Public) and piped to DP9.1. Basin EA4 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA5 is 0.16 acres of undeveloped area and includes the Pond C Sand Filter. Stormwater ($Q_5 = 0.1$ cfs $Q_{100} = 0.4$ cfs) is flows directly into the Pond C Sand Filter.

Basin EA6 is 0.70 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ($Q_5 = 3.1 \text{ cfs } Q_{100} = 5.5 \text{ cfs}$) is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA6. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA6 will be detained in TSB #1.

Basin EA7 is 0.65 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ($Q_5 = 2.5 \text{ cfs } Q_{100} = 4.7 \text{ cfs}$ is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA7. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA7 will be detained in TSB #1.



Basin EA8 is 2.08 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 5.0 \text{ cfs } Q_{100} = 9.0 \text{ cfs}$) is conveyed in curb and gutter to DP14. Flows at DP14 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA8 will be detained Pond B Full Spectrum Detention Basin.

Basin EA9 is 2.99 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 4.6 \text{ cfs } Q_{100} = 9.5 \text{ cfs}$) is conveyed in curb and gutter to DP15. Flows at DP15 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA9 will be detained Pond B Full Spectrum Detention Basin.

Basin EA10 is 0.12 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.6$ cfs $Q_{100} = 1.1$ cfs) is conveyed in curb and gutter to DP16.1 Flows from DP16.1 drain south and captured in a 10' Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Basin EA11 is 0.19 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.5$ cfs $Q_{100} = 1.0$ cfs) is conveyed in curb and gutter to DP17.1. Flows from DP17.1 drain south and captured in a 10' Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Offsite Basins

- Verify all basin flows with hydrology spreadsheet. Include all basins in spreadsheet and summary table on maps

Basin OS1 (EX1) is 85.16 acres of undeveloped area. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 (The Sanctuary Filing 1 G18). Flows at DP1 ($Q_5 = 28.3$ cfs $Q_{100} = 365.2$ cfs) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Gieck Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin OS2 is 15.03 acres of undeveloped land and parking area north of Rex Road and contains a portion of Rex Road ($Q_5 = 4.2 \text{ cfs } Q_{100} = 21.6 \text{ cfs}$). Stormwater is conveyed to DP7 and is captured in a proposed 24" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS2.

Basin OS3 is 1.00 acre of undeveloped land ($Q_5 = 0.2$ cfs $Q_{100} = 1.2$ cfs) along the western edge of Eastonville Road. Stormwater is conveyed to DP8 and is captured in a proposed 18" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS3.

Basin OS4 is 9.60 acres of undeveloped land ($Q_5 = 3.8 \text{ cfs } Q_{100} = 17.3 \text{ cfs}$) along the western edge of Eastonville Road. Stormwater is conveyed to DP11 in a roadside swale where it combines with Meridian Ranch DP G15 flows ($Q_5 = 8 \text{ cfs } Q_{100} = 54.0 \text{ cfs}$) before being captured in a proposed 30" RCP culvert and piped to Channel B. The combined flows as it reaches DP11 is $Q_5 = 10.5 \text{ cfs } Q_{100} = 144.5 \text{ cfs}$.

Basin OS5 is 40.26 acres of undeveloped land and Falcon Regional Park ($Q_5 = 13.3 \text{ cfs } Q_{100} = 64.0 \text{ cfs}$) along the western edge of Eastonville Road. Stormwater is conveyed to DP12 in a roadside swale and is captured in a proposed 48" RCP culvert and piped to Channel B.

Basin OS6 is 60.83 acres of undeveloped land ($Q_5 = 8.9$ cfs $Q_{100} = 60.6$ cfs) along the western edge of Eastonville Road. Basin OS6 flows are adapted directly from the approved The Sanctuary Filing 1 FDR.



Stormwater is conveyed to DP16 in a roadside swale where it combines with Meridian Ranch DP G12 flows before being conveyed across Eastonville Road in dual 10' x 3.5' RCBC to Channel A. The combined flows at DP16 (EX4) are $Q_5 = 22.4$ cfs $Q_{100} = 491$ cfs.

Basin OS7 is future outflow of 11.42 acres of a future stormwater detention pond outflow developed land that will be detained to meet existing conditions ($Q_5 = 3.4$ cfs $Q_{100} = 22.7$ cfs) in the southeast corner of Eastonville Road and Rex Road. From there, stormwater is piped to Channel B.

IV. Drainage Facility Design

a. General Concept

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). Inlets will be placed at low points and roundabout entrances. Stormwater from this roadway will be piped to either a full spectrum detention pond, sand filter or temporary sediment basin. All ponds and water quality features will discharge at less than historic rates.

b. Water Quality & Detention

Pond C (Sand Filter)

Water quality and stormwater detention for Basins EA1, 2, & 5 is provided in Sand Filter Basin C. SFB C is a private, full spectrum sand filter basin within the Grandview Reserve property to be developed in the future. In Pond C, a total of 0.63 from the proposed project acres at 54% composite imperviousness will be detained. The minimum required acreage of treatment is 0.63 acres. The WQCV is 0.009 ac-ft, the EURV is 0.037 ac-ft, and the 100-year detention volume is 0.062 ac-ft. The WQCV, EURV and 100-year storms are released in 12, 41 and 44 hours, respectively. A 10' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 12' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard south. SFB C outfalls towards the future Channel B improvements at historic runoff rates. Runoff from Pond C will follow historic drainage patterns and not exceed historic flow rates.

Pond B (Full Spectrum Detention Basin)

EDB B "Pond B" will provide detention and water quality treatment for subbasins EA8 & EA9 per this report. Refer to the Eastonville Road Segment 1 FDR for detention basin details.

c. Inspection and Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated that all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All private detention ponds are to be owned and maintained by the Grandview Reserve Metropolitan District NO. 2 (DISTRICT), once established, unless an agreement is reached stating otherwise. Maintenance access for all full spectrum detention facilities will be provided from public Right-of-Way. Maintenance access for the drainageways will be provided through the proposed tracts.



V. Wetlands Mitigation

There is an existing wetland in Gieck Ranch Tributary #1 (Channel A). The wetland is contained entirely within the channel and is classified as jurisdictional. A Nationwide Wetland Permit will be applied for due to the disturbed area at the Dawlish Roundabout. Wetlands maintenance will be the responsibility of the DISTRICT.

VI. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates. The Impervious Reduction Factor (IRF) method was used and is presented in Appendix D.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum detention pond provides water quality treatment for the site. The WQCV is released over a period of at least 12 hours for SFBs and 40 hours for EDBs while the EURV is released over a period of 40-44 hours for SFBs and 68 - 72 hours for EDBs as recommended by the MHFD.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

VIII. Opinion of Probable Cost

An engineer's opinion of probable cost has been provided below for public and private drainage infrastructure improvements. This includes cost estimates for the public full spectrum sand filter basin C. All required stormwater infrastructure will be installed per El Paso County Requirements.

	Public Infrastructure Cost Estimate	е		
	Line Item	Quantity	Unit Price	Cost
	15" Reinforced Concrete Pipe	128	\$45 LF	\$5,760
1	18" Reinforced Concrete Pipe	808	\$76 LF	\$61,408
/	24" Reinforced Concrete Pipe	161	\$114 LF	\$18,354
	48" Reinforced Concrete Pipe	1678	\$187 LF	\$313,786
7	15" CDOT FES	1	\$500 EA	\$500

Unresolved: Quantities and unit costs should match with FAE estimate



24" CDOT FES	2	\$684	EA	\$1,368
48" CDOT FES	2	\$912	EA	\$1,824
6' DIA Storm Manhole	12	\$7,734	EA	\$92,808
10' CDOT Type R Inlet	6	\$6,703	EA	\$40,218
Rip Rap, d50 size from 6"-24"	2	\$97	Tons	\$194
3' x 10' Concrete Box Culvert w/ Wingwalls	110	\$400	Tons	\$44,000
10% Contingency				\$58,022
TOTAL:				\$638,242

Public SFB C Cost Estimate				
Line Item	Quantity	Unit F	Price	Cost
Rip Rap, d50 size from 6"-24" (Inflow)	1.5	\$97	Tons	\$146
Sand Filter Media	44	\$100	/CY	\$4,400
4" Perforated PVC Underdrain	10	\$10	/LF	\$100
12" ABC Maintenance Access	19	\$40	/CY	\$760
Outlet Structure w/ Orifice Plate	1	\$5,000	EA	\$5,000
Rip Rap, d50 size from 6"-24" (Spillway)	19.5	\$97	Tons	\$1,892
12" RCP Outlet Pipe	150	\$60	/LF	\$9,000
12" RCP FES	1	\$350	EA	\$350
10% Contingency				\$2,165
TOTAL:				\$23,812

does not match what is shown in Section 1 of FAE

IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes have been sized and and calculations are provided in Appendix C. All proposed storm sewer will be designed in accordance with El Paso County Drainage Criteria Manuals.

X. Summary

Eastonville Road lies within the Gieck Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds, sand filters and temporary sediment basins. There is one major drainageway that traverses the site: Gieck Ranch Tributary 1. The water quality and detention features ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT). All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

The development of this project will not adversely affect downstream properties.

XI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.



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XII. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
- 4. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 5. "Master Development Drainage Plan Meridian Ranch" prepared by Tech Contractors, July 2021.
- 6. "The Sanctuary Filing 1 at Meridian Ranch" prepared by Tech Contactors, August 2022.



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APPENDIX A - VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP

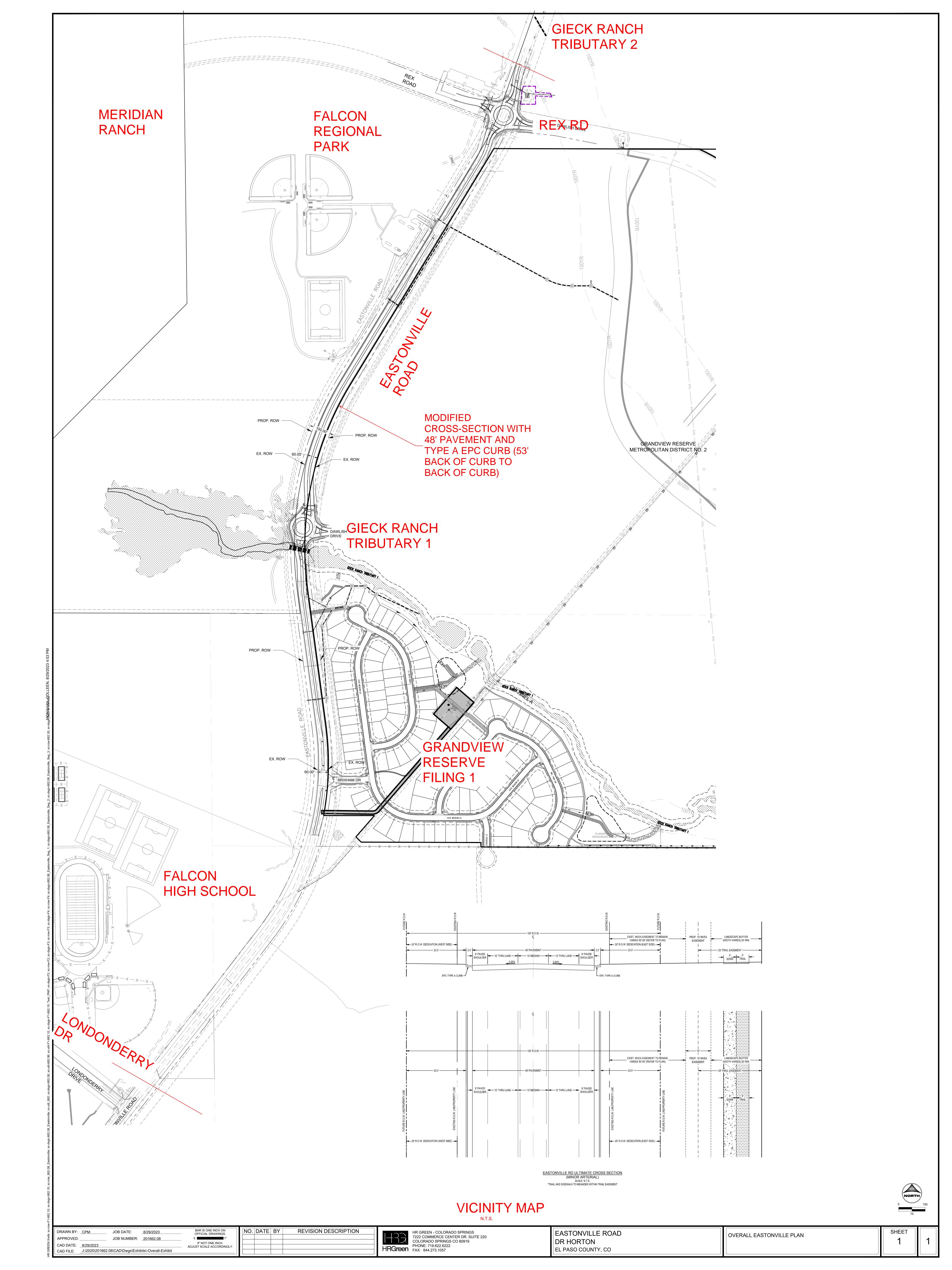
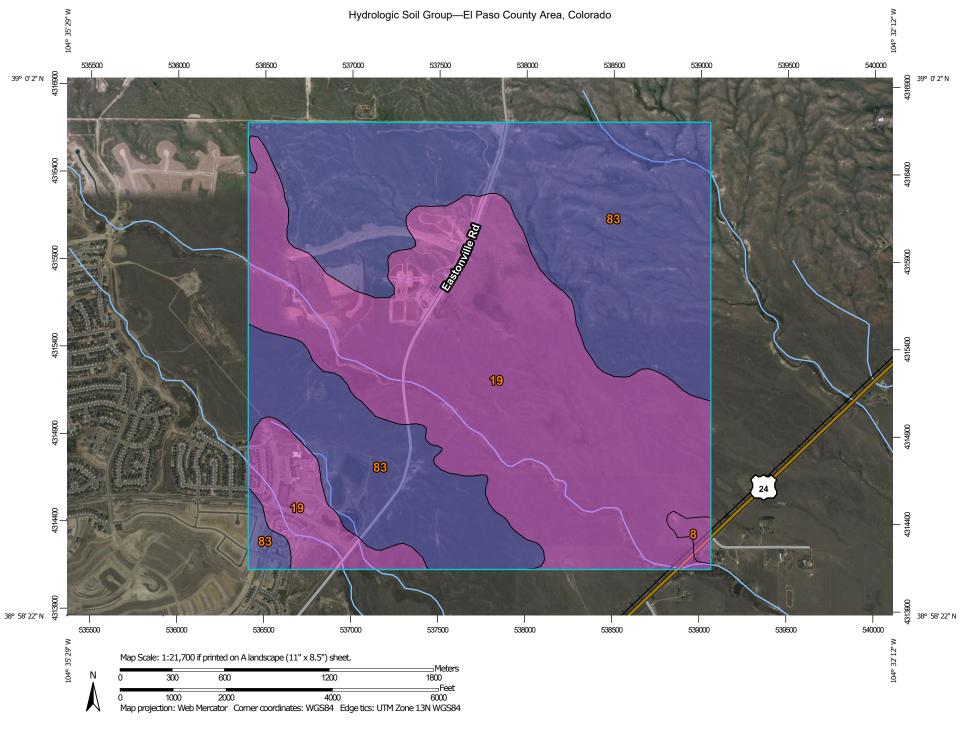


Photo - at Londonderry and Eastonville looking north

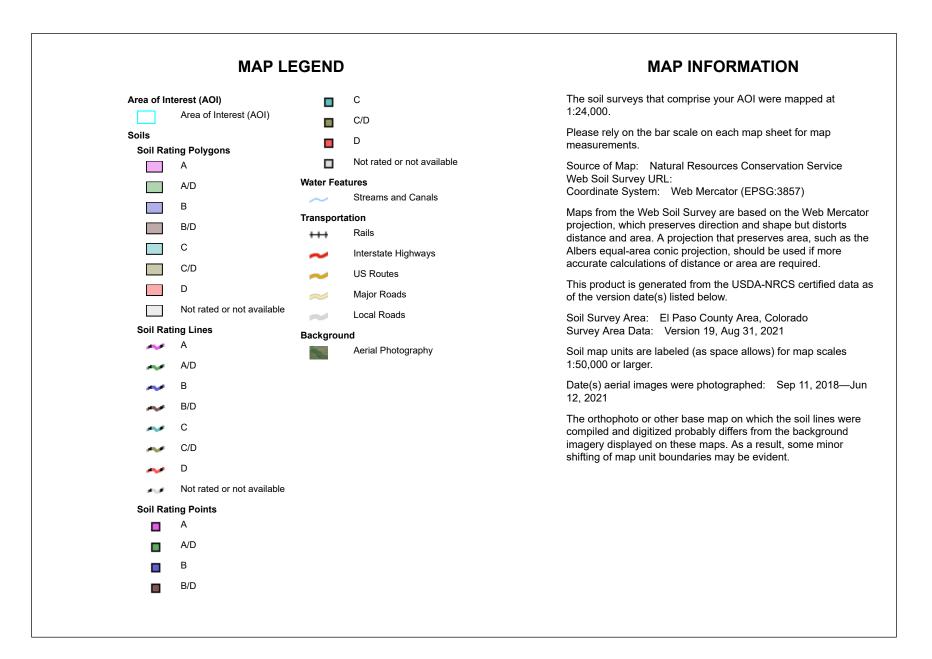




Natural Resources Conservation Service

USDA

Web Soil Survey National Cooperative Soil Survey



8

19

83

Totals for Area of Interest

	irguix		oup		
	Map unit symbol	Map unit name	Rating	Acres in AOI	
3		Blakeland loamy sand, 1 to 9 percent slopes	A	10.4	

А

в

Hydrologic Soil Group

Columbine gravelly

sandy loam, 0 to 3 percent slopes

Stapleton sandy loam, 3

to 8 percent slopes

Description	
Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when t soils are not protected by vegetation, are thoroughly wet, and receive	:he

precipitation from long-duration storms. The soils in the United States are assigned to four groups (A, B, C, and D) and

three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Percent of AOI

839.5

835.7

1,685.6

0.6%

49.8%

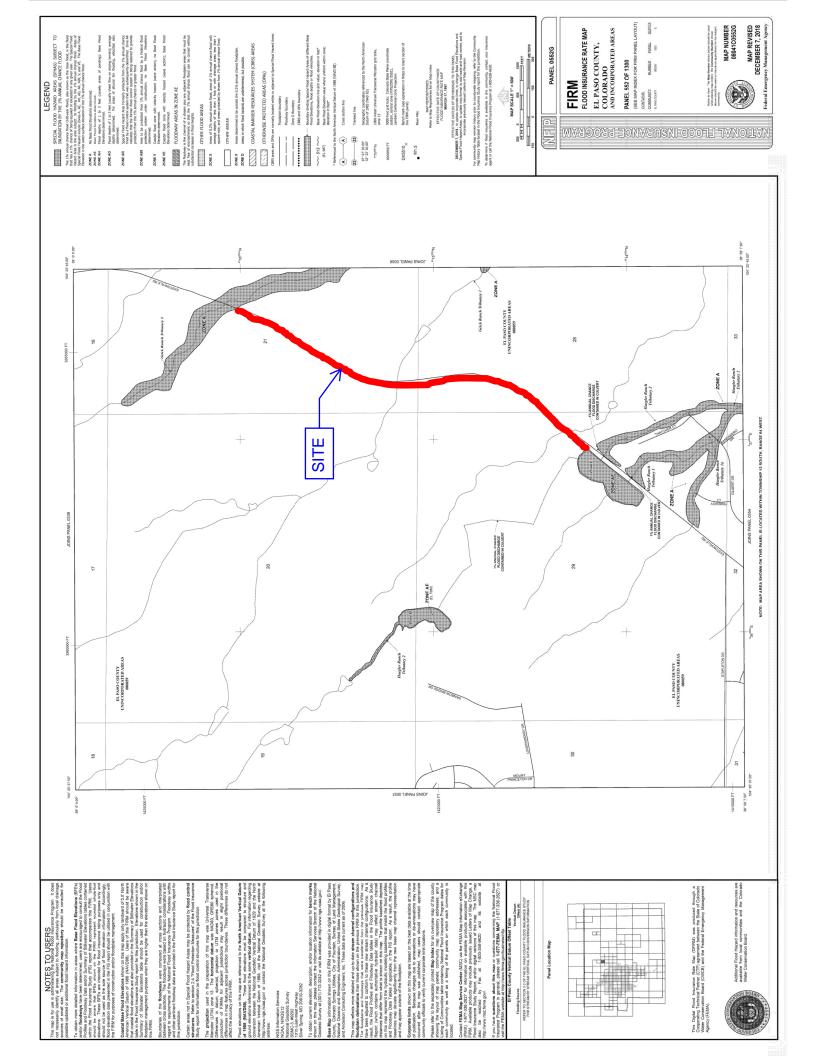
49.6%

100.0%

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





Precipitation Frequency Data Server

NOAA Atlas 14, Volume 8, Version 2 Location name: Elbert, Colorado, USA* Latitude: 38.9796°, Longitude: -104.5696° Elevation: 6996 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									
Duration				Average	recurrence	interval (ye	ars)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.239 (0.189-0.303)	0.291 (0.231-0.370)	0.381 (0.301-0.486)	0.461 (0.361-0.589)	0.576 (0.440-0.768)	0.671 (0.499-0.904)	0.770 (0.554-1.06)	0.875 (0.604-1.24)	1.02 (0.678-1.48)	1.14 (0.733-1.67)
10-min	0.350 (0.277-0.444)	0.426 (0.338-0.542)	0.558 (0.441-0.711)	0.674 (0.529-0.863)	0.844 (0.644-1.12)	0.982 (0.731-1.32)	1.13 (0.811-1.56)	1.28 (0.884-1.81)	1.49 (0.992-2.17)	1.66 (1.07-2.44)
15-min	0.426 (0.338-0.541)	0.520 (0.412-0.660)	0.681 (0.537-0.867)	0.823 (0.645-1.05)	1.03 (0.785-1.37)	1.20 (0.891-1.62)	1.37 (0.988-1.90)	1.56 (1.08-2.21)	1.82 (1.21-2.65)	2.03 (1.31-2.98)
30-min	0.608 (0.482-0.771)	0.740 (0.586-0.940)	0.968 (0.764-1.23)	1.17 (0.916-1.49)	1.46 (1.11-1.94)	1.70 (1.26-2.28)	1.94 (1.40-2.68)	2.20 (1.52-3.12)	2.57 (1.71-3.73)	2.86 (1.84-4.19)
60-min	0.775 (0.615-0.984)	0.933 (0.739-1.18)	1.21 (0.956-1.54)	1.46 (1.15-1.87)	1.84 (1.41-2.47)	2.16 (1.61-2.92)	2.49 (1.80-3.45)	2.85 (1.97-4.05)	3.37 (2.24-4.90)	3.78 (2.44-5.54)
2-hr	0.943 (0.754-1.19)	1.12 (0.898-1.42)	1.46 (1.16-1.84)	1.76 (1.39-2.23)	2.22 (1.72-2.97)	2.62 (1.97-3.52)	3.04 (2.21-4.19)	3.50 (2.45-4.95)	4.16 (2.80-6.03)	4.70 (3.06-6.85)
3-hr	1.03 (0.829-1.29)	1.22 (0.978-1.53)	1.57 (1.25-1.97)	1.90 (1.51-2.40)	2.41 (1.88-3.22)	2.86 (2.17-3.84)	3.34 (2.45-4.60)	3.88 (2.73-5.48)	4.66 (3.15-6.74)	5.29 (3.46-7.69)
6-hr	1.20 (0.968-1.48)	1.40 (1.13-1.74)	1.78 (1.44-2.22)	2.16 (1.73-2.70)	2.76 (2.18-3.66)	3.28 (2.52-4.39)	3.86 (2.86-5.29)	4.51 (3.20-6.34)	5.46 (3.73-7.86)	6.24 (4.12-9.01)
12-hr	1.38 (1.13-1.70)	1.61 (1.31-1.98)	2.05 (1.66-2.53)	2.48 (2.00-3.07)	3.15 (2.51-4.15)	3.74 (2.89-4.96)	4.39 (3.28-5.96)	5.12 (3.66-7.13)	6.17 (4.25-8.82)	7.04 (4.69-10.1)
24-hr	1.60 (1.31-1.95)	1.87 (1.54-2.28)	2.38 (1.94-2.91)	2.85 (2.32-3.51)	3.60 (2.88-4.67)	4.24 (3.29-5.56)	4.94 (3.71-6.63)	5.71 (4.12-7.87)	6.82 (4.73-9.66)	7.73 (5.20-11.0)
2-day	1.85 (1.54-2.24)	2.18 (1.80-2.63)	2.76 (2.28-3.34)	3.29 (2.70-4.01)	4.11 (3.30-5.27)	4.80 (3.76-6.22)	5.54 (4.19-7.36)	6.35 (4.62-8.68)	7.50 (5.25-10.5)	8.44 (5.73-11.9)
3-day	2.03 (1.69-2.44)	2.39 (1.98-2.87)	3.02 (2.50-3.64)	3.60 (2.97-4.36)	4.47 (3.60-5.69)	5.20 (4.08-6.70)	5.98 (4.55-7.90)	6.83 (4.99-9.28)	8.03 (5.65-11.2)	9.00 (6.15-12.7)
4-day	2.18 (1.82-2.61)	2.56 (2.13-3.06)	3.22 (2.68-3.87)	3.82 (3.16-4.62)	4.73 (3.83-6.00)	5.49 (4.33-7.04)	6.30 (4.81-8.30)	7.18 (5.26-9.72)	8.43 (5.94-11.7)	9.43 (6.46-13.3)
7-day	2.58 (2.17-3.07)	2.98 (2.50-3.54)	3.68 (3.08-4.39)	4.32 (3.60-5.18)	5.29 (4.30-6.65)	6.09 (4.84-7.76)	6.96 (5.34-9.09)	7.89 (5.82-10.6)	9.21 (6.55-12.8)	10.3 (7.10-14.4)
10-day	2.93 (2.48-3.47)	3.36 (2.84-3.98)	4.13 (3.47-4.90)	4.81 (4.02-5.74)	5.83 (4.76-7.28)	6.68 (5.32-8.45)	7.58 (5.85-9.86)	8.55 (6.34-11.4)	9.92 (7.08-13.7)	11.0 (7.65-15.4)
20-day	3.91 (3.33-4.58)	4.51 (3.84-5.29)	5.52 (4.68-6.50)	6.39 (5.39-7.55)	7.63 (6.25-9.37)	8.62 (6.90-10.8)	9.64 (7.47-12.4)	10.7 (7.98-14.1)	12.2 (8.74-16.6)	13.3 (9.31-18.4)
30-day	4.70 (4.02-5.47)	5.44 (4.65-6.34)	6.65 (5.66-7.78)	7.66 (6.49-9.00)	9.06 (7.44-11.0)	10.1 (8.15-12.5)	11.2 (8.74-14.3)	12.3 (9.24-16.2)	13.8 (9.98-18.7)	15.0 (10.5-20.6)
45-day	5.67 (4.88-6.57)	6.55 (5.63-7.60)	7.97 (6.82-9.27)	9.12 (7.77-10.7)	10.7 (8.79-12.9)	11.9 (9.56-14.5)	13.0 (10.2-16.4)	14.2 (10.6-18.4)	15.6 (11.3-21.0)	16.7 (11.9-23.0)
60-day	6.48 (5.60-7.48)	7.46 (6.43-8.62)	9.01 (7.74-10.4)	10.3 (8.77-11.9)	11.9 (9.82-14.3)	13.1 (10.6-16.0)	14.3 (11.2-18.0)	15.5 (11.7-20.0)	16.9 (12.3-22.6)	18.0 (12.8-24.6)

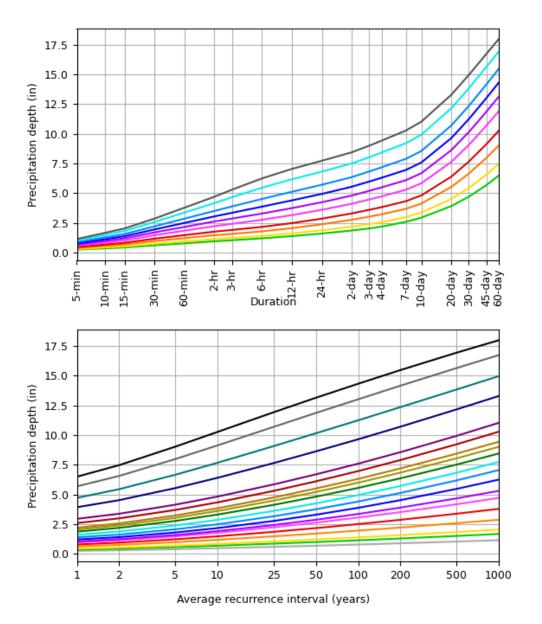
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

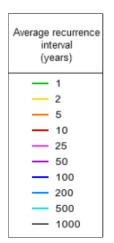
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical







Duration					
5-min	- 2-day				
10-min	- 3-day				
15-min	- 4-day				
- 30-min	- 7-day				
- 60-min	— 10-day				
2-hr	- 20-day				
— 3-hr	— 30-day				
— 6-hr	— 45-day				
- 12-hr	- 60-day				
— 24-hr					

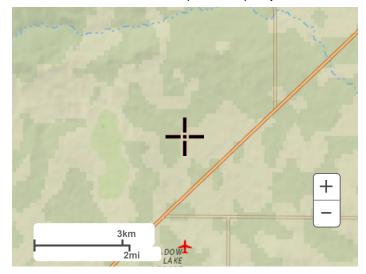
NOAA Atlas 14, Volume 8, Version 2

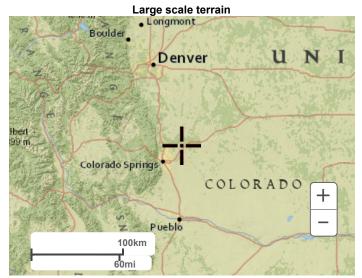
Created (GMT): Wed Nov 22 20:22:49 2023

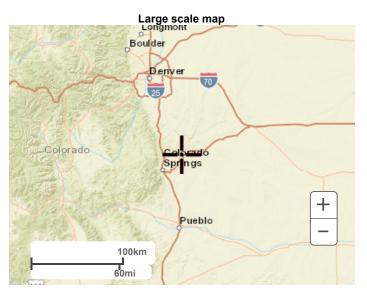
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Maps & aerials

Small scale terrain

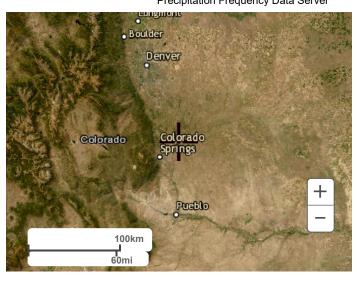






Large scale aerial

Precipitation Frequency Data Server



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer



Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX B – HYDROLOGIC CALCULATIONS

	EASTONVILLE ROAD	<u>Calc'd by:</u>	СМ
רד <u>ו</u>	EXISTING CONDITIONS	Checked by:	СМ
HRGreer	EL PASO COUNTY, CO	<u>Date:</u>	2/1/2024

SUMMARY RUNOFF TABLE						
BASIN AREA (ac) % IMPERVIOUS Q_5 (cfs) Q_{100} (cfs)						
G18*	321.53	-	28.3	365.2		
FG36*	18.88	-	1.7	18.8		
G16*	131.26	-	6.1	112.1		
G06* 832.70 - 22.4 491.0						
4	* AREA AND Q TAKEN FROM THE SANCTU					

DESIGN POINT SUMMARY TABLE							
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)				
1	G18*	28.3	365.2				
2	FG36*	1.7	18.8				
3	G16*	6.1	112.1				
4	4606* 22.4 491.0						

UARY FILING 1 FDR

Unresolved: Basin labels do not match basin labels on drainage map. Please revise to show same labels. Labels listed here are design points.

From map, need to list basins FG35, Ex1 thru Ex4

	EASTONVIL	LE ROAD)						<u>Calc'o</u>	d by:		C	M				
כרדו	EXISTING C		ONS						<u>Checl</u>	ked by:		C	M				
HRGreen	EL PASO COUNT	r y , co							Date:	-		2/1/	2024				
				CO	MPOSI	TE '(C' F.	ACTOR	S								
BASIN	UNDEVELOPED	WALKS & DRIVES	SINGLE Family	TOTAL	SOIL	UND	DEVE	LOPED	WAL	KS & DR	IVES	SINC	GLE FA	AMILY		MPOSI IOUSNE	
		ACRES			TYPE	%	C ₅	C ₁₀₀	%I	C 5	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀
EX1 - EX4*	/																
EAT - EA4																	

Provide excerpts from Sanctuary FDR for these calculations. Include them in "Excerpts from other reports" section.

1433	EAST	ONVILL	.E ROAD)				Calc'd b	y:		СМ
	EXIST	TING CO	ONDITIO	NS				Checked	by:		СМ
HRGreen	EL PAS	O COUNT	r y, co					Date:		2/1	/2024
				TIME O	F CONCE	NTRAT	ION				
BAS	IN DATA		OVER		E (T _i)		TRAV	EL TIME (T_t		TOTAL
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)
EX1-EX4*											
* FLOWS TO THE AREAS EX1 - EX4		N POINTS WE	RE TAKEN FR	OM "THE SA	NCTUARY FI	LING 1 FDR	" SO TC WAS N	IOT CALCUI	LATED FOR C	ONTRIBU	TING

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{v}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*}For buried riprap, select C_v value based on type of vegetative cover.



EASTONVILLE ROAD <u>Calc'd by:</u> **EXISTING CONDITIONS** Checked by: **DESIGN STORM: 5-YEAR** Date:

				DI	RECT	RUNO	FF		т	OTAL	RUN	OFF	S	TREE	T		PII	PE		TF	RAVEL	. TIME	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₅	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	G18*	321.53									28.3											
	2	FG36*	18.88									1.7											
	2	FG30	10.00									1.7											
	3	G16*	131.26									6.1											BASIN EX2, DP2 & D
	4	G06*	832.70									22.4											BASIN EX4 & DPG12 (SAN
		ľ,																					
																						1	

asin Labels need to natch with basin bels on map

СМ	
СМ	
2/1/2024	

REMARKS

DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)

DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3

& DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD

ANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR



EASTONVILLE ROAD Calc'd by: EXISTING CONDITIONS Checked by: DESIGN STORM: 100-YEAR Date:

				DI	RECT	RUNOF	F		тс	TAL I	RUNO	FF	S	TREE	ET		PII	PE		TR	AVEL [.]	TIME	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C100	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1	G18*	321.53									365.2											
	2	FG36*	18.88									18.8											
	3	G16*	131.26									112.1											BASIN EX2, DP2 &
	4	G06*	832.70									491.0											BASIN EX4 & DPG12 (SA

СМ	
СМ	
2/1/2024	

REMARKS

DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)

DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3

& DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD

SANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

HRGreen

EASTONVILLE ROAD SEG 2 PROPOSED CONDITIONS

EL PASO COUNTY, CO

 SEG 2
 Calc'd by:
 SPC

 ONS
 Checked by:
 CM

 Date:
 2/2/2024

Ś	SUMMAR	Y RUNOFF	TABLE	
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)
EA1	0.22	73	0.8	1.5
EA2	0.25	72	0.9	1.7
EA3	0.20	70	0.7	1.3
EA4	0.17	65	0.5	1.1
EA5	0.16	0	0.1	0.4
EA6	0.70	100	3.2	5.3
EA7	0.65	89	2.6	4.8
EA8	2.08	99	5.2	8.8
EA9	2.99	63	5.0	10.4
EA10	0.16	75	0.6	1.1
EA11	0.15	67	0.5	1.0
*G18	321.53	-	28.3	365.2
*FG36	18.88	-	1.7	18.8
OS3	1.00	2	0.3	2.2
OS4	9.60	9	4.8	21.6
*G16	131.26	-	6.1	112.1
*G06	832.70	-	22.4	491.0
OS7	11.42	2	3.6	24.4

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

DES	SIGN POINT SU	MMARY TA	BLE
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)
1	G18	28.3	365.2
2	FG36	1.7	18.8
2.1	EA1	0.8	1.5
3	G16, DP11	6.1	112.1
3.1	EA2, DP2.1	1.6	3.2
4	G06	22.4	491.0
4.1	EA5, DP3.1	1.7	3.4
5	EA3	0.7	1.3
6	DP5, EA4	1.2	2.4
6.1	DP6, DP8	2.9	22.4
7	OS3	0.3	2.2
8	DP2, DP7	2.0	21.0
9	DP6.1	2.9	22.4
10	EA6, EA7	5.6	9.9
11	OS4, DP9	7.5	44.0
12	OS7	3.6	24.4
13	DP3, DP12	26.0	136.4
14	EA8	5.2	8.8
15	EA9	5.0	10.4
15.1	DP14, DP15	10.2	19.1
16.1	EA10	0.6	1.1
17.1	EA11	0.5	1.0

Pr_Drainage_Calcs3

RBM 2/2/2024 10:36 AM

	EASTONVILLE ROAD SEG 2	<u>Calc'd by:</u>	SPC
	PROPOSED CONDITIONS	Checked by:	СМ
HRGreen	EL PASO COUNTY, CO	Date:	11/27/2023

SOIL TYPE: HSG A&B

COMPOSITE 'C' FACTORS																					
							LAN) USE	TYPE												
		Paved			c Flow Ar elts, Agr	-		Lawns	i	Land	Jse Und	defined	Land	Use Und	defined				MPOSITE OUSNESS & C		
	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀						
	100	0.90	0.96	2	0.09	0.36	0	0.08	0.35	0	0.00	0.00	0	0.00	0.00	TOTAL		FACTOR	-		
BASIN		ACRES			ACRES	•		ACRES	;		ACRES			ACRES	•	ACRES	%	C ₅	C ₁₀₀		
EA1		0.16						0.06								0.22	73	0.68	0.79		
EA2		0.18						0.07								0.25	72	0.67	0.79		
EA3		0.14						0.06								0.20	70	0.65	0.78		
EA4		0.11						0.06								0.17	65	0.61	0.74		
EA5		0.00						0.16								0.16	0	0.08	0.35		
EA6		0.70						0.00								0.70	100	0.90	0.96		
EA7		0.58						0.07								0.65	89	0.81	0.89		
EA8		2.06						0.02								2.08	99	0.89	0.95		
EA9		1.88						1.11								2.99	63	0.60	0.73		
EA10		0.12						0.04								0.16	75	0.70	0.81		
EA11		0.10						0.05								0.15	67	0.63	0.76		
G18																321.53					
FG36																18.88					
OS3	1				1.00								1			1.00	2	0.09	0.36		
OS4		0.70			8.90											9.60	9	0.15	0.40		
G16																131.26					
G06																832.70					
OS7					11.42											11.42	2	0.09	0.36		
Pond A	1	0.34			0.00			0.29					1			0.63	54	0.52	0.68		

	EAST	ONVILL	E ROAD	SEG 2				Calc'd b	y:	5	SPC		
14イブ			CONDITI	ONS				Checked	by:		СМ		
HRGreen	EL PAS		гч, со					Date:		2/2	2/2024		
BAS	SIN DATA		OVER		E (T _i)		TRAV	EL TIME (T_t		TOTAL		
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)		
EA1	0.68	0.22	34	2.0	3.6	20	137	1.4	2.4	1.0	5.0		
EA2	0.67	0.25	34	2.0	3.6	20	60	1.4	2.4	0.4	5.0		
EA3	0.65	0.20	34	2.0	3.8	20	126	1.4	2.4	0.9	5.0		
EA4	0.61	0.17	34	2.0	4.2	20	126	3.8	3.9	0.5	5.0		
EA5	0.08	0.16	20	2.0	6.6	20	20	33.0	11.5	0.0	6.7		
EA6	0.90	0.70	26	2.0	1.5	20	630	1.7	2.6	4.0	5.5		
EA7	0.81	0.65	24	2.0	2.1	20	630	1.7	2.6	4.0	6.1		
EA8	0.89	2.08	26	2.0	1.5	20	2500	0.7	1.7	24.9	26.4		
EA9	0.60	2.99	26	2.0	3.7	20	2500	0.7	1.7	24.9	28.6		
EA10	0.70	0.16	26	2.0	3.0	20	157	0.6	1.5	1.7	5.0		
EA11	0.63	0.15	26	2.0	3.5	20	157	0.6	1.5	1.7	5.2		
G18													
FG36													
OS3	0.09	1.00	220	2.1	21.4	10	345	2.3	1.5	3.8	25.2		
OS4	0.15	9.60	153	3.1	14.8	10	1124	2.5	1.6	11.8	26.6		
G16													
G06													
OS7	0.09	11.42	200	11.6	11.6	10	675	3.4	1.8	6.1	17.7		

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

* For buried riprap, select C_v value based on type of vegetative cover.



EASTONVILLE ROAD SEG 2 PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

<u>Calc'd by:</u>

Checked by:

Date:

				DI	RECT	RUNOF	F		Т	DTAL	RUNG	OFF	S	TREE	T		PIF	РЕ		TF	RAVEL	TIME	
	DESIGN POINT	BASIN ID	AREA (ac)	C5	<i>t_c (</i> min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	G18	321.53					28.3				28.3										-	
	2	FG36	18.88					1.7				1.7											
	2.1	EA1	0.22	0.68	5.0	0.15	E 47	0.8	5.0	0.15	5.17	0.8				0.8	0.15	1.0	1.5	56	5.9	0.16	
	3		0.22	0.00	5.0	0.15	5.17					6.1											
	3.1	G16						6.1	5.0	0.32	5.17	1.6				1.6	0.32	5.1	1.5	34	13.4	0.04	
	4	EA2	0.25	0.67	5.0	0.17	5.17	0.9				22.4											
	4.1	G06						22.4	6.7	0.33	5.17	1.7											
	5	EA5	0.16	0.08	6.7	0.01	4.74	0.1	5.0	0.13	5.17	0.7				0.7	0.13	0.5	1.3	48	3.7	0.21	
	6	EA3	0.20	0.65	5.0	0.13	5.17	0.7	5.2	0.23	5.11	1.2				1.2	0.23	2.4	1.3	43	8.1	0.09	
	6.1	EA4	0.17	0.61	5.0	0.10	5.17	0.5	13.2		3.71	2.9				2.9				61	7.2	0.14	
resolved:	7								13.1		3.72	0.3				0.3					6.4	0.11	
lete one of OS3 basins		OS3	> 1.00	0.09	13.1	0.09	3.72	0.3			3.72					2.0					6.4	0.10	
		OS3	1.00	0.09	13.1	0.09	3.72	0.3						0.00	0.1		0.09	1.5	1.5				
	9								13.2		3.71		2.9	0.32	2.1					615	2.9	3.56	
	10	EA6	0.70	0.90	5.5	0.63	5.02	3.2	6.1	1.16	4.88	5.6											
		EA7	0.65	0.81	6.1	0.53	4.88	2.6															
	11	OS4	9.60	0.15	17.1	1.43	3.32	4.8	17.1		3.32			1.76	0.5					530	1.4	6.25	BASIN OS4, D
	12	OS7	11.42	0.09	14.9	1.03	3.53	3.6	14.9	1.03	3.53	3.6				3.6	1.03	1.0	1.5	28	5.9	0.08	
	13								14.9	1.03	3.53	26.0											
	14	EA8	2.08	0.89	24.0	1.86	2.81	5.2	24.0	1.86	2.81	5.2				5.2	1.86	7.0	1.5	8	15.7	0.01	
	15	EA9	2.99				2.81		24.0	1.78	2.81	5.0				5.0	1.78	1.8	1.5	54	7.9	0.11	
	15.1		2.33	0.00	24.0	1.70	2.01	0.0	24.1	3.64	2.81	10.2											СОМВ
	16.1								5.0	0.11	5.17	0.6											BASIN EA10 CONVEYED
	47 4	EA10	0.16	0.70	5.0	0.11	5.17	0.6		0.00	E 44												BASIN EA11 CONVEYED
	17.1	EA11	0.15	0.63	5.2	0.09	5.11	0.5	5.2	0.09	5.11	0.5											

Unresolved: Missing Basins OS1, OS2, FG35 & OS6

SPC	
СМ	
2/2/2024	

REMARKS

BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1

BASIN EA2 CAPTURED IN 5' TYPE R INLET@ DP3, PIPE TO DP3.1

COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)

BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1

BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6, PIPE TO DP6.1

DP6 & DP8 FLOW @ DP6.1, PIPE TO DP9

BASIN OS3 CAPTURED IN 15" FES, PIPE TO DP8

DP2 & DP7 FLOW @ DP8, PIPE TO DP9

DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11

BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)

, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN 30" FES @ DP11, SWALE TO DP3

BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13

COMBINED DP3 & DP12, PIPE TO CHANNEL B

BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1

BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1

MBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR

D VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR

D VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR



1			EASTONVILLE ROAD SEG 2											G 2					Cal	Calc'd by: SPC						
	-23	à	PROPOSED CONDITIONS																Che	cked b	СМ					
L.				DESIGN STORM: 100-YEAR																	<u>Date:</u> 2/2/2024					
HR	Gree	n																								
				DIRECT RUNOFF TOTAL RUNOFF STREET PIPE T													PI	PE	TR	RAVEI	. TIME	REMARKS				
Ŀ	IN POINT	9	(ac)		Ē	l (ac)	hr.)	((u	l (ac)	/ (in./ hr.)	-	(cfs)	(ac)	% ⊒	(cfs)	l (ac)	% ⊒	SIZE (ft)	TH (ft)	(ft/s)	EL TIME (min)				
L REI	DESIGN	BASIN	AREA	00	(min)	C ₁₀₀ *A	(in./	(cfs)	(min)	C ₁₀₀ *A	(in./	(cfs)	street	C ₁₀₀ *A	SLOPE	QPIPE	C ₁₀₀ *A	SLOPE	PIPE (LENGTH	VEL. (TRAVEL				
S	1	B/	AF	C100	t_c	ပ်		Ø	t_c	ပ်		0 365.2	ď	ပ်	SL	Q	ပ်	SL	٩		>	۲,				
		G18						365.2																		
	2	FG36						18.8				18.8														
	2.1	EA1	0.22	0.70	5.0	0.17	0.00		5.0	0.17	8.68	1.5				1.5	0.17	1.0	1.5	56	5.9	0.16	BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1			
	3		0.22	0.79	5.0	0.17	8.68					112.1				112.1	0.00	5.1	1.5	34	13.4	0.04				
	3.1	G16						112.1		0.37	8.66	3.2											BASIN EA2 CAPTURED IN 5' TYPE R INLET@ DP3, PIPE TO DP3.1			
		EA2	0.25	0.79	5.0	0.20	8.68	1.7								404.0	0.00	0.5		10	0.7	0.04				
	4	G06						491.0				491.0				491.0	0.00	0.5	1.3	8 48	3.7	0.21				
	4.1	EA5	0.16	0.35	6.7	0.06	7.95	0.4		0.43	7.95	3.4				3.4	0.43	2.4	1.3	43	8.1	0.09	COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)			
	5								5.0	0.16	8.68	1.3				1.3	0.16	1.0	2.0	61	7.2	0.14	BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1			
	6	EA3	0.20	0.78	5.0	0.16	8.68	1.3		0.28	8.61	2.4				2.4	0.28	0.8	2.0	43	6.4	0.11	BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6, PIPE TO DP6.1			
	6.1	EA4	0.17	0.74	5.0	0.13	8.68	1.1				22.4				22.4	0.64	15	1 3	38	6.4	0.10	DP6 & DP8 FLOW @ DP6.1, PIPE TO DP9			
	0.1																									
	7	OS3	1.00	0.36	13.1	0.36	6.24	2.2		0.36	6.24	2.2				2.2	0.36	1.0	2.0	56	7.2	0.13	BASIN OS3 CAPTURED IN 15" FES, PIPE TO DP8			
	8								13.1	0.36	6.24	21.0	21.0	0.36	2.1					615	2.9	3.56	DP2 & DP7 FLOW @ DP8, PIPE TO DP9			
	9	OS3	1.00	0.36	13.1	0.36	6.24	2.2		0.64	5.63	22.4											DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11			
	10								6.1	1.21	8.19	9.9											BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)			
		EA6	0.70	0.90	5.5	0.63	8.43	5.3						0.00	0.5					500		0.05				
		EA7	0.65	0.89	6.1	0.58	8.19	4.8						0.00	0.5					530						
	11	OS4	9.60	0.40	17 1	3.88	5.58	21.6		4.52	5.58	44.0				44.0	4.52	1.0	4.0	1500	11.4	2.19	BASIN OS4, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN 30" FES @ DP11, SWALE TO DP3			
	12								14.9	4.11	5.93	24.4				24.4	4.11	1.0	1.5	5 28	5.9	0.08	BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13			
	13	OS7	11.42	0.36	14.9	4.11	5.93	24.4		4.11	5.92	136.4								$\left \right $			COMBINED DP3 & DP12, PIPE TO CHANNEL B			
	14								24.0	1.86	4 72	8.8				8.8	1.86	7.0	1 5	5 8	15.7	0.01	BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1			
		EA8	2.08	0.89	24.0	1.86	6 4.72	8.8																		
	15	EA9	2.99	0.73	24.0	2.19	4.72	10.4		2.19	4.72	10.4				10.4	2.19	1.8	1.5	54	7.9	0.11	BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1			
	15.1									4.05	4.71	19.1							_				COMBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR			
	16.1	EA40	0.40	0.04	E O	0.45	0.00			0.13	8.68	1.1											BASIN EA10 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR			
	17.1	EA10	0.16	0.81	5.0	0.13	8.68	1.1		0.11	8 58	1.0								$\left \right $			BASIN EA11 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD			
		EA11	0.15	0.76	5.2	0.11	8.58	1.0		0.11	0.00	1.0								1			SEGMENT 1 FDR			



Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX C – HYDRAULIC CALCULATIONS

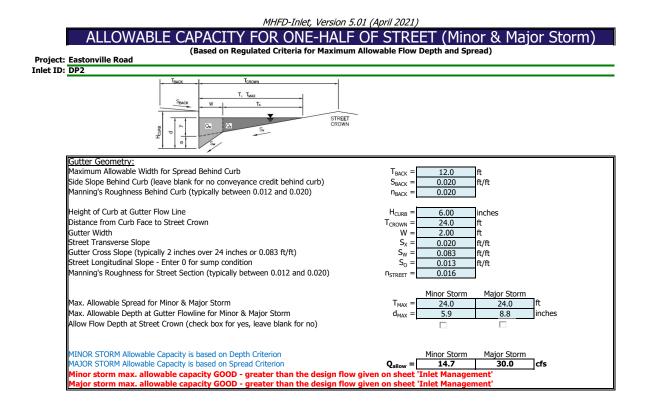
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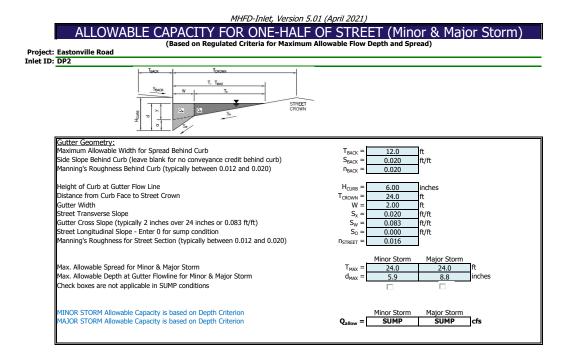
Provide design calculations for all proposed swales & ditches

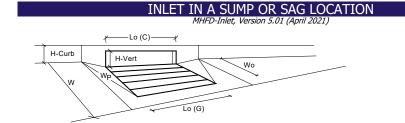
Unresolved: Provide design calculations for riprap outlet protection at end of all culverts

Unresolved: Provide analysis of any existing culverts that remain

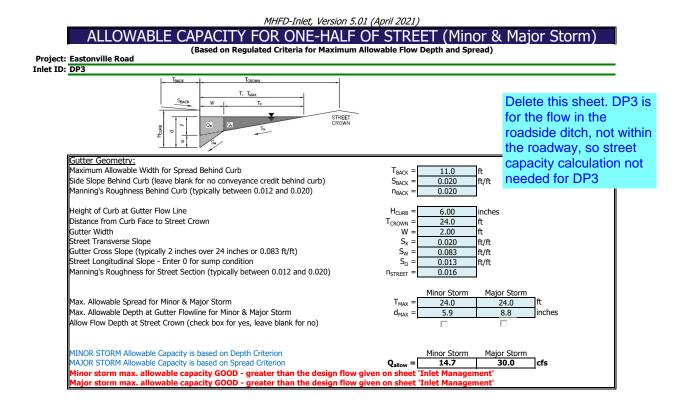
Unresolved: Include DP1 calculations for existing and needed culvert size

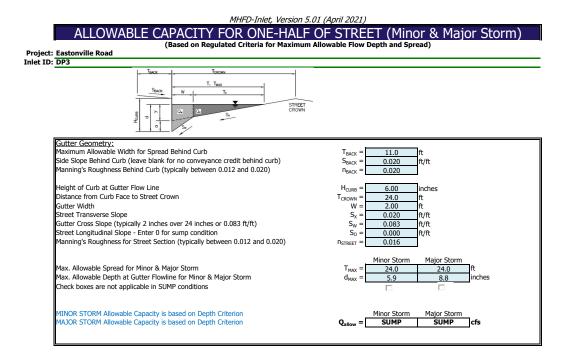






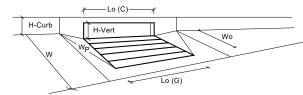
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.3	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.44	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.75	0.93	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.1	8.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>O PEAK)	Q PEAK REQUIRED =	0.8	1.5	cfs





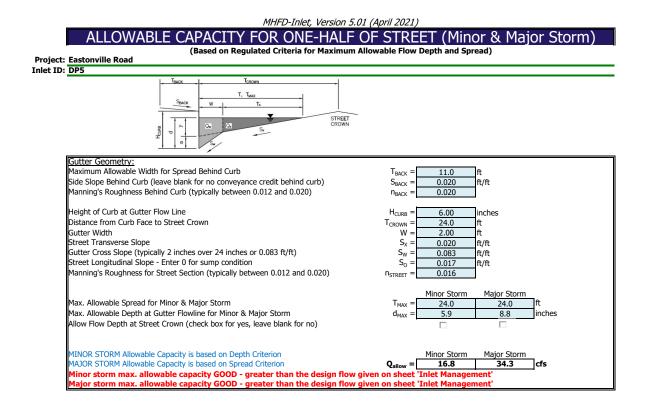
INLET IN A SUMP OR SAG LOCATION

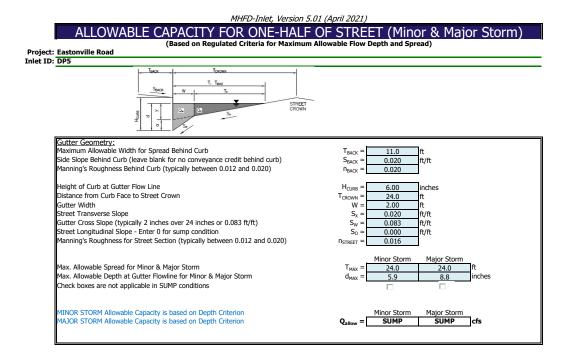
MHFD-Inlet, Version 5.01 (April 2021)

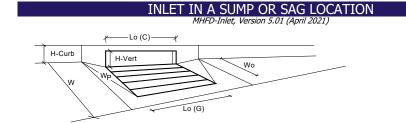


Delete this portion as DP 3 is within the roadside ditch at the culvert opening, not a curb inlet. Provide inlet design if an area inlet is being used at DP 3 and delete if not.

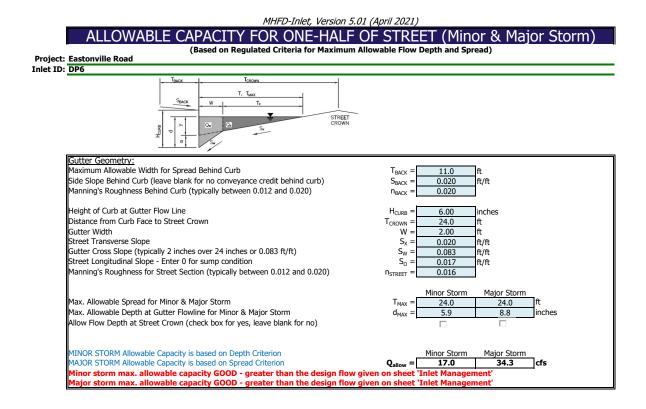
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =			inches
Number of Unit Inlets (Grate or Curb Opening)	No =			
Water Depth at Flowline (outside of local depression)	Ponding Depth =			inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$			feet
Width of a Unit Grate	W _o =			feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =			
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$			
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =			
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$			
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$			feet
Height of Vertical Curb Opening in Inches	H _{vert} =			inches
Height of Curb Orifice Throat in Inches	H _{throat} =			inches
Angle of Throat (see USDCM Figure ST-5)	Theta =			degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =			feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$			
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$			
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$			
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	-		cfs
	Q PEAK REQUIRED =			cfs

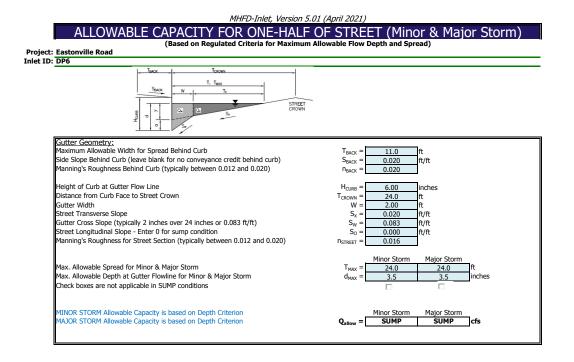


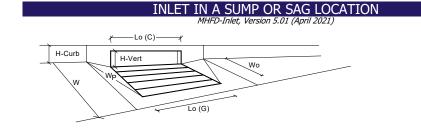




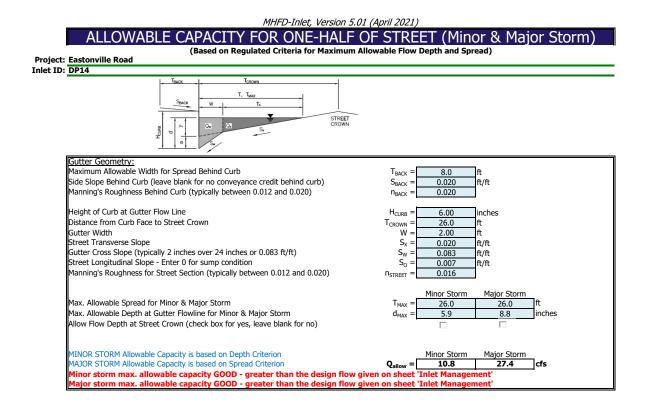
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.3	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.44	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.75	0.93	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q ₂ =	5.1	8.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>O PEAK)	Q PEAK REQUIRED =	0.7	1.4	cfs

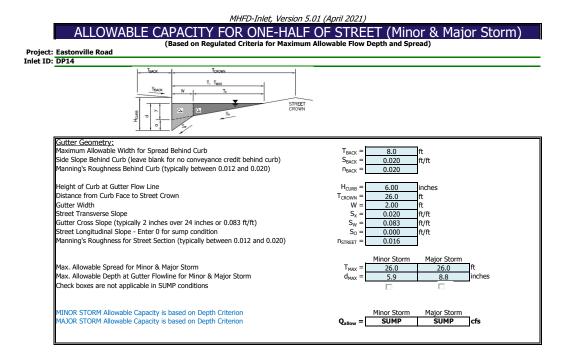


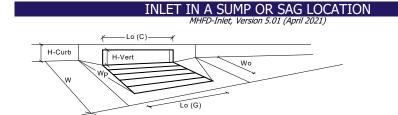




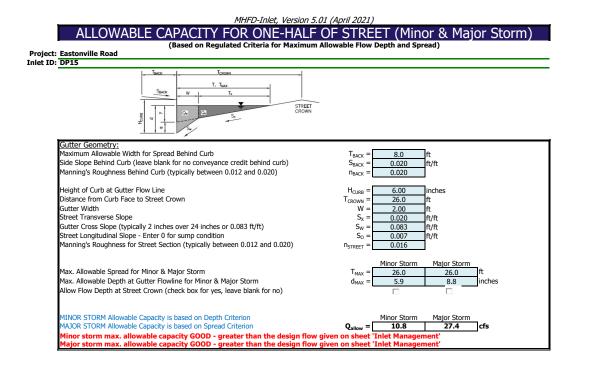
Design Information (Input)	CDOT Type R Curb Opening		MINOR	MAJOR		
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening		
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches	
Number of Unit Inlets (Grate or O	Curb Opening)	No =	1	1		
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	3.5	3.5	inches	
Grate Information		-	MINOR	MAJOR	Override Depths	
Length of a Unit Grate		$L_{o}(G) =$	N/A	N/A	feet	
Width of a Unit Grate		W _o =	N/A	N/A	feet	
Area Opening Ratio for a Grate (A _{ratio} =	N/A	N/A		
Clogging Factor for a Single Grate		$C_{f}(G) =$	N/A	N/A		
Grate Weir Coefficient (typical va		C_w (G) =	N/A	N/A		
Grate Orifice Coefficient (typical)	value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A		
Curb Opening Information		-	MINOR	MAJOR		
Length of a Unit Curb Opening		$L_{o}(C) =$	5.00	5.00	feet	
Height of Vertical Curb Opening i	in Inches	H _{vert} =	6.00	6.00	inches	
Height of Curb Orifice Throat in I	Inches	H _{throat} =	6.00	6.00	inches	
Angle of Throat (see USDCM Figu	ure ST-5)	Theta =	63.40	63.40	degrees	
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet	
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10		
Curb Opening Weir Coefficient (t		$C_{w}(C) =$	3.60	3.60		
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67]	
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR		
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft	
Depth for Curb Opening Weir Equ	uation	d _{Curb} =	0.13	0.13	ft	
Combination Inlet Performance R		RF _{Combination} =	0.45	0.45		
Curb Opening Performance Redu		RF _{Curb} =	0.99	0.99		
Grated Inlet Performance Reduct		RF _{Grate} =	N/A	N/A		
		Grate	.,,,,	.,,,	1	
		-	MINOR	MAJOR		n An an a tha an t
Total Inlet Interception Capacity		Q _a =	1.2		cfs Un	resolved:
Inlet Capacity IS GOOD for M	linor and Major Storms(>Q PEAK)	$Q_{PEAK REQUIRED} =$	0.5	1.1	cfs Do	r hydrology
				~ ~ ~		r hydrology
					sn sn	readsheet, DP6 has
					Q1	00 of 2.4 cfs.
					Int	erception capacity is not
					be	equate at this inlet
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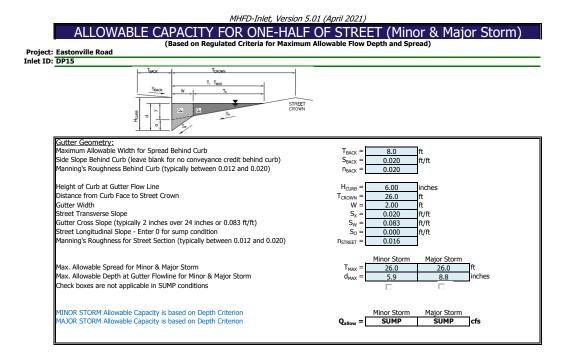


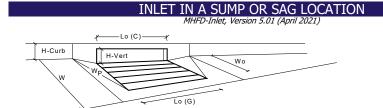




Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.55	0.73	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
	Gluce	•		-
	-	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	9.9	18.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	$Q_{PEAK REQUIRED} =$	5.0	9.0	cfs

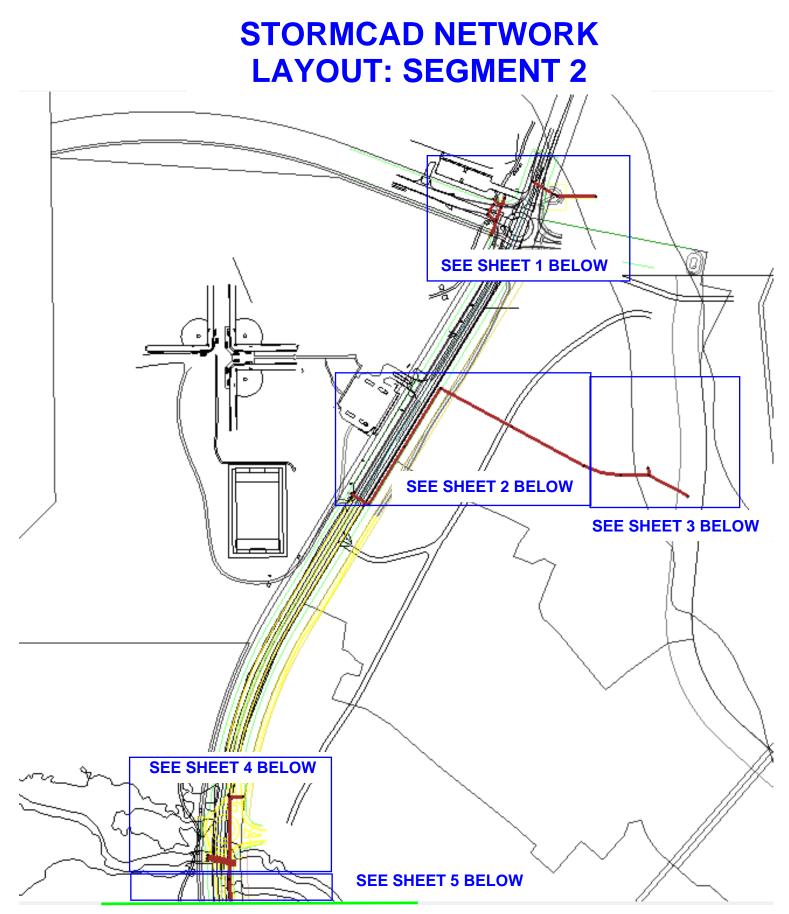




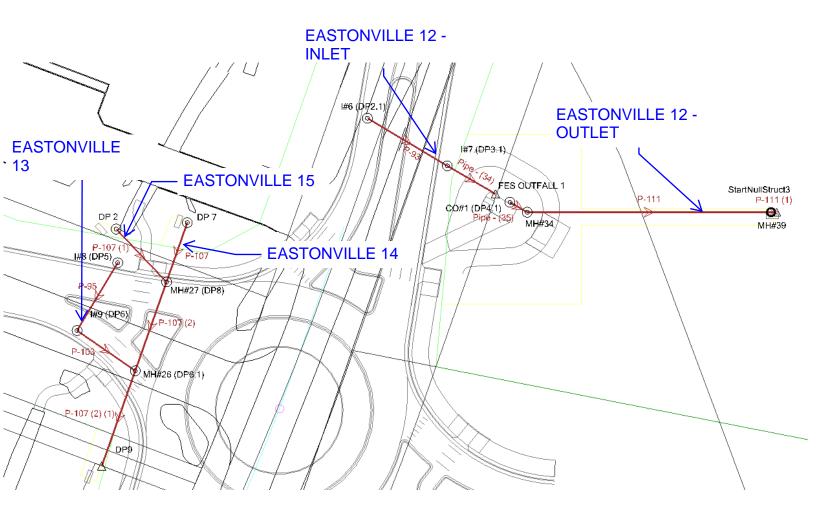


Design Information (Input) CDOT Type R Curb Opening	-	MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.55	0.73	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	9.9	18.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.6	<mark>9.5</mark>	cfs

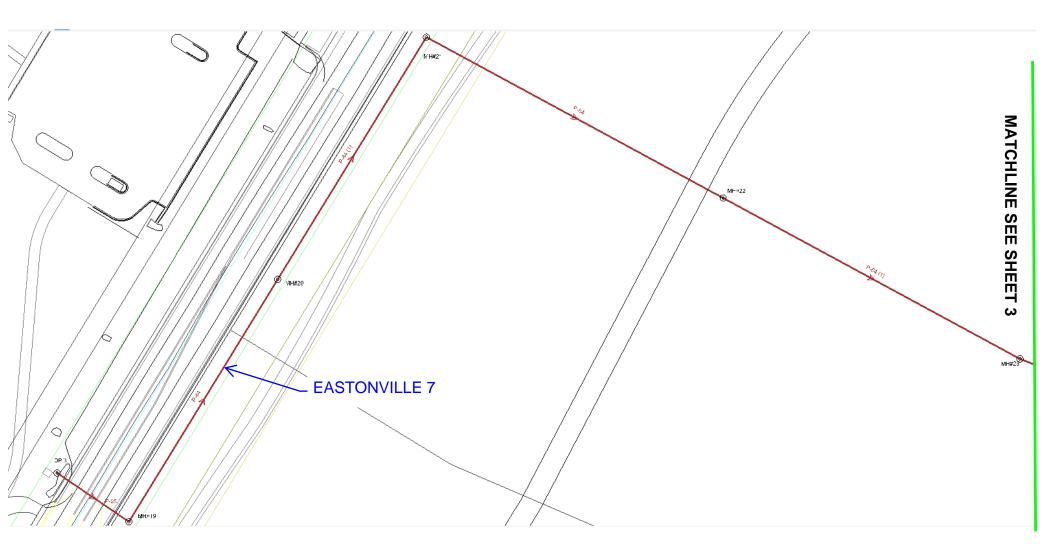
Verify correct design flows are being used at all inlets.



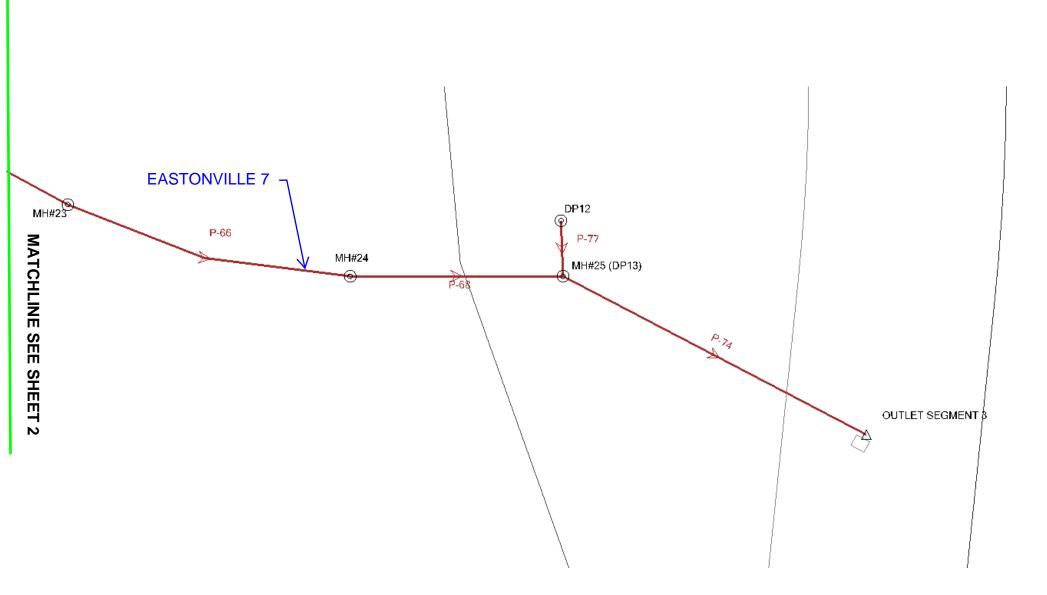
MATCHLINE REFER TO SEGMENT 2 FDR



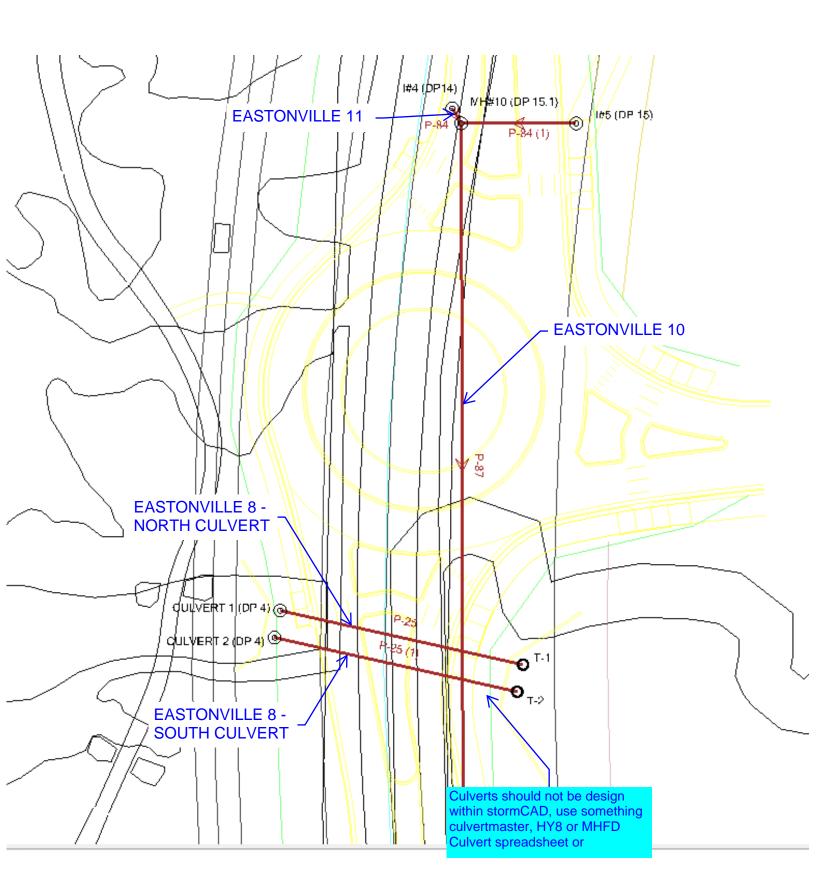




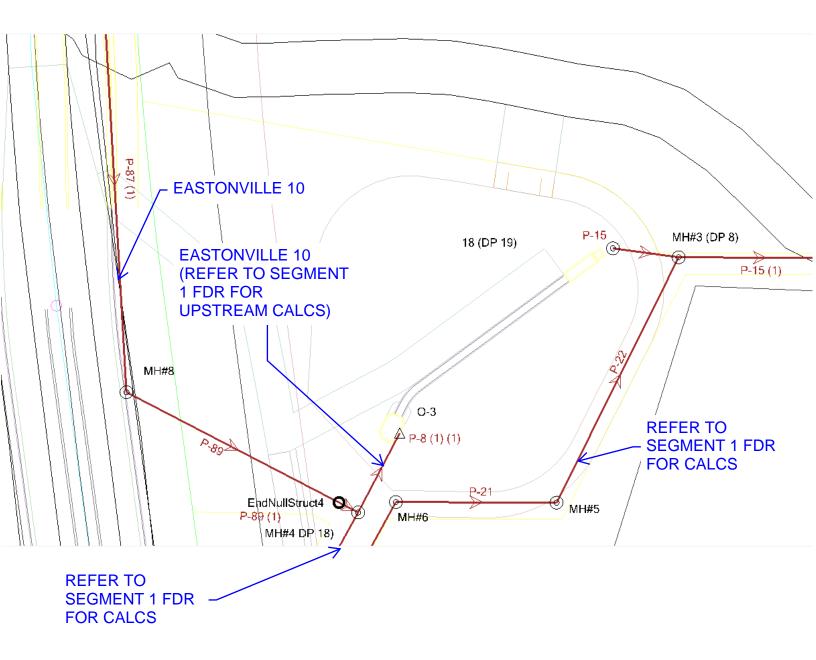








SHEET 4



SHEET 5

100 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

	Label	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Notes	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
66: P-8 (1) (1)	P-8 (1) (1)	MH#4 DP 18)	6,985.66	O-3	6,984.83	41.6	0.020	24.0	26.20	8.34	31.99	81.9	Concrete Pip	6,988.54	6,987.98
67: P-124	P-124	I#5 (DP 14)	6,981.25	O-5	6,981.08	34.3	0.005	18.0	6.50	4.74	7.43	87.5	Concrete Pip	6,982.33	6,982.10
68: P-121 (2)	P-121 (2)	44 (80)	6,970.65	O-6	6,970.61	9.0	0.005	24.0	9.00	2.86	15.95	56.4	Concrete Pip	6,972.88	6,972.87
69: P-18	P-18	I#3 (DP 7)	6,985.73	MH#7	6,985.38	71.3	0.005	42.0	53.30	8.11	71.14	74.9	Concrete Pip	6,988.48	6,988.38
70: P-20	P-20	MH#7	6,985.38	MH#6	6,984.50	175.6	0.005	42.0	53.30	8.11	71.14	74.9	Concrete Pip	6,987.84	6,987.61
71: P-5	P-5	I#2 (DP 17)	6,989.29	I#1 (DP 16)	6,989.74	52.0	-0.009	18.0	5.10	5.59	9.77	52.2	Concrete Pip	6,990.61	6,990.44
72: P-8 (1)	P-8 (1)	I#2 (DP 17)	6,988.79	MH#4 DP 18)	6,985.66	156.4	0.020	24.0	10.50	9.12	31.99	32.8	Concrete Pip	6,989.95	6,989.64
73: P-21	P-21	MH#6	6,984.50	MH#5	6,984.13	74.6	0.005	42.0	53.30	8.11	71.14	74.9	Concrete Pip	6,987.15	6,987.05
74: P-22	P-22	MH#5	6,984.13	MH#3 (DP 8)	6,980.80	127.1	0.026	42.0	53.30	15.14	162.72	32.8	Concrete Pip	6,986.41	6,983.39
75: P-15	P-15	18 (DP 19)	6,983.26	MH#3 (DP 8)	6,982.80	30.8	0.015	18.0	3.00	5.95	12.90	23.3	Concrete Pip	6,983.92	6,983.30
76: P-15 (1)	P-15 (1)	MH#3 (DP 8)	6,980.80	MH#2 (DP 8)	6,980.43	75.1	0.005	42.0	1.77	3.11	70.62	2.5	Concrete Pip	6,983.39	6,983.39
77: P-16	P-16	MH#2 (DP 8)	6,980.43	MH#1	6,980.05	78.1	0.005	42.0	54.30	8.06	70.19	77.4	Concrete Pir	6,982.74	6,982.46
78: P-123	P-123	I#4 (DP 13)	-	I#5 (DP 14)	6,981.25	52.0	0.005	18.0	3.40	4.11	7.43	45.8	Concrete Pir	6,982.73	6,982.69
79: P-17	P-17	MH#1	6,980.05		6,979.36	139.8	0.005	42.0	54.30	8.10	70.67		Concrete Pir	6,982.36	6,981.66
80: P-125	P-125	44 (69) (DP 15)	6,978.42		6,977.55	54.5	0.016	18.0	1.20	4.67	13.30		Concrete Pip	6,978.83	6,977.85
83: P-122	P-122	INLET (DP 3)	6,978.16		6,973.52	183.8	0.025	30.0	24.50	12.34	65.19		Concrete Pip	6,979.85	6,974.58
84: P-121	P-121	I#8 (DP 10)	6,971.18	44 (80)	6,970.65	105.1	0.005	24.0	9.00	5.26	16.06	56.0	Concrete Pip	6,973.05	6,972.89
85: P-130	P-130	I#6 (DP 1)	6,970.85	44 (81)	6,970.04	81.5	0.010	18.0	3.60	5.37	10.47	34.4	Concrete Pip	6,971.57	6,970.79
86: P-130 (1)	P-130 (1)	44 (81)	6,970.04	44 (77)	6,969.39	65.0	0.010	18.0	3.60	5.39	10.50	34.3	Concrete Pip	6,970.76	6,970.00
87: P-121 (1)	P-121 (1)	I#8 (DP 10)		I#7 (DP 9)	6,971.95	52.0	-0.005	18.0	4.10	4.37	7.57	54.2	Concrete Pip	6,973.24	6,973.18
88: P-131	P-131	44 (78) (DP 11)	6,968.42	44 (79)	6,967.50	62.5	0.015	18.0	1.40	4.75	12.77	11.0	Concrete Pip	6,968.87	6,967.84
126: P-111	P-111	MH#34	7,019.01	MH#39	7,017.01	146.6	0.014	18.0	3.40	5.94	12.28	27.7	Concrete Pip	7,019.72	7,017.55
127: P-89	P-89	MH#8	6,986.87	MH#4 DP 18)	6,985.66	111.1	0.011	24.0	19.10	6.08	23.64	80.8	Concrete Pip	6,990.43	6,989.64
、 、 、 、 、 、 、 、 、 、 、 、 、 、 、 、 、 、 、	P-25 (1)	CULVERT 2 (DP 4)	6,997.01		6,995.27	116.5	0.015		295.50	16.72	461.86	64.0	Concrete Bo	7,000.01	6,997.28
129: P-25	P-25	CULVERT 1 (DP 4)	6,997.01		6,995.27	116.6	0.015		245.50	15.71	461.72		Concrete Bo	6,999.67	6,997.02
131: P-107 (2)		MH#26 (DP6.1)	7,020.50		7,019.00	60.7	0.025	24.0	22.40	11.97	35.57	63.0	Concrete Pip	7,022.19	7,020.22
132: P-103	P-103	I#9 (DP6)		MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	2.40	6.54	16.08		Concrete Pip	7,023.89	7,023.91
		MH#27 (DP8)		MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	21.00	6.68	21.26	98.8	Concrete Pip	7,024.40	7,023.91
134: P-107	P-107	DP 7		MH#27 (DP8)	7,021.75	37.8	0.033	15.0	2.20	1.79	11.81		Concrete Pip	7,025.07	7,025.03
135: P-107 (1)		MH#27 (DP8)	7,021.00		7,021.26	43.9	-0.006	24.0	18.80	5.98	17.41	108.0	Concrete Pip	7,025.33	7,025.03
136: P-95	P-95	I#8 (DP5)		I#9 (DP6)	7,023.00	47.5	0.021	18.0	1.30	5.26	15.24		Concrete Pip	7,024.43	7,023.94
137: P-93	P-93	I#6 (DP2.1)		I#7 (DP3.1)	7,021.80	55.9	0.010	18.0	1.50	4.22	10.51	14.3	Concrete Pip	7,022.99	7,023.02
138: Pipe - (34		I#7 (DP3.1)		FES OUTFALL 1	7,021.01	33.5	0.023	18.0	3.20	7.09	16.07		Concrete Pip	7,023.01	7,023.00
	P-44 (1)	MH#20	7,001.18		6,998.52	266.5	0.010	48.0	112.10	8.92	143.63	78.0	Concrete Pip	7,005.57	7,003.94
141: P-64	P-64	MH#21	6,998.52		6,995.26	316.5	0.010	48.0	112.10	12.80	145.88		Concrete Pip	7,001.72	6,997.89
142: P-44	P-44	MH#19	7,003.94		7,001.28	266.5	0.010	48.0	112.10	12.64	143.63	78.0	Concrete Pip	7,007.14	7,005.63
143: P-26	P-26	DP 3	7,005.01		7,004.04	81.5	0.012	48.0	112.10	8.92	156.73		Concrete Pip	7,009.86	7,009.36
	P-64 (1)	MH#22	6,995.15		6,988.82	316.6	0.020	48.0	112.10	16.57	203.15	55.2	Concrete Pip	6,998.35	6,995.31
145: P-87	P-87	MH#10 (DP 15.1)	6,994.25		6,989.76	320.7	0.014	24.0	19.10	9.26	26.78		Concrete Pip	6,995.82	6,992.24
	P-87 (1)	MH#9	6,989.76		6,986.87	197.4	0.015	24.0	19.10	6.08	27.33	69.9	Concrete Pir	6,992.21	6,990.80
147: P-84	P-84	I#4 (DP14)	-	MH#10 (DP 1	6,994.25	8.1	0.179	18.0	8.80	4.98	44.40		Concrete Pip	6,997.31	6,997.25
	P-84 (1)	MH#10 (DP 15.1)		I#5 (DP 15)	6,995.50	53.9	-0.014	18.0	10.40	5.89	12.40	83.9	Concrete Pip	6,997.78	6,997.25
149: P-66	P-66	MH#23	6,988.82		6,988.00	149.0	0.006	48.0	112.10	8.92	106.64	105.1	Concrete Pip	6,995.25	6,994.34
150: P-68	P-68	MH#24	-	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	112.10	8.92	97.84	114.6	Concrete Pip	6,994.28	6,993.62
151: P-77	P-77	DP12		MH#25 (DP13)	6,989.50	28.1	0.029	24.0	24.40	7.77	38.62		Concrete Pir	6,993.95	6,993.62
152: P-74	P-74	MH#25 (DP13)	6,987.50	OUTLET SEG	6,986.67	173.3	0.005	48.0	136.40	10.85	99.34	137.3	Concrete Pip	6,991.97	6,990.15

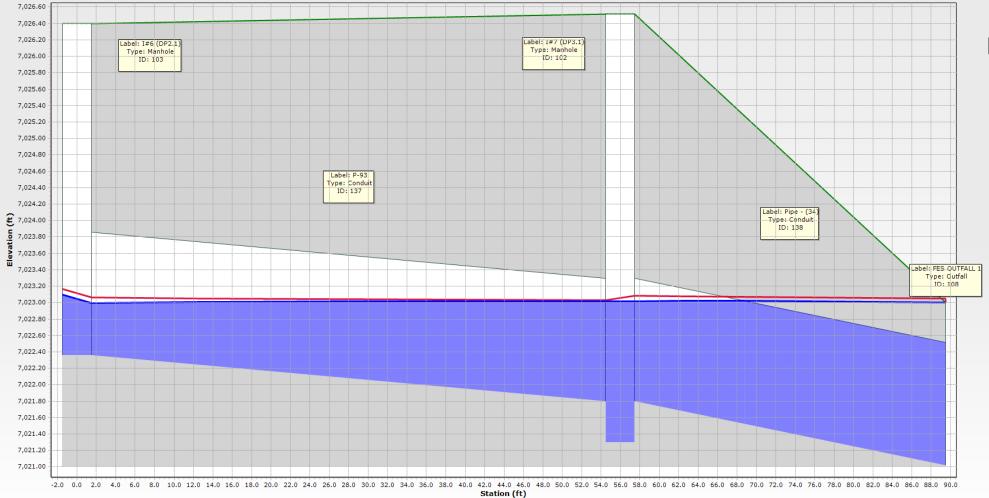
NOTE: SEGMENT 1 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

100 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

	Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Depth (Out) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss Method	Hydraulic Grade Line (In) (ft)	Notes	Headloss (ft)
35: MH#7	MH#7	6,993.52	6,993.52	53.30	2.47	6,987.84	Standard	6,988.38	STORM MH	0.54
36: I#1 (DP 16	I#1 (DP 16)	6,993.41	6,993.41	5.10	0.87	6,990.61	Standard	6,991.15	CDOT Type-	0.54
37: MH#4 DP	MH#4 DP 18)	6,993.40	6,993.40	26.20	2.88	6,988.54	Standard	6,989.64	STORM MH	1.10
38: I#2 (DP 17	I#2 (DP 17)	6,993.39	6,993.39	10.50	1.17	6,989.95	Standard	6,990.44	CDOT Type-	0.49
39: MH#6	MH#6	6,993.02	6,993.02	53.30	2.65	6,987.15	Standard	6,987.61		0.46
40: MH#5	MH#5	6,991.91	6,991.91	53.30	2.28	6,986.41	Standard	6,987.05	STORM MH	0.64
41: MH#3 (DP	MH#3 (DP 8)	6,991.13	6,991.13	1.77	2.28	6,983.39	Standard	6,983.39	STORM MH	0.00
42: I#3 (DP 7)	I#3 (DP 7)	6,990.73	6,990.73	53.30	2.83	6,988.48	Standard	6,989.49	CDOT Type-	1.01
43: 18 (DP 19)	18 (DP 19)	6,988.71	6,988.71	3.00	2.42	6,983.92	Standard	6,984.30	CDOT Type-	0.38
44: MH#2 (DP	MH#2 (DP 8)	6,985.74	6,985.74	54.30	2.31	6,982.74	Standard	6,983.39	STORM MH	0.65
45: I#4 (DP 13	I#4 (DP 13)	6,985.02	6,985.02	3.40	1.42	6,982.73	Standard	6,982.84	CDOT Type-	0.12
46: I#5 (DP 14	I#5 (DP 14)	6,985.02	6,985.02	6.50	1.28	6,982.33	Standard	6,982.69	CDOT Type-	0.36
47: MH#1	MH#1	6,984.95	6,984.95	54.30	2.31	6,982.36		6,982.46	STORM MH	0.10
49: 44 (69) (D	44 (69) (DP 15)	6,982.64	6,982.64	1.20	0.41	6,978.83		6,978.85	CDOT Type-	0.01
55: 44 (80)	44 (80)	6,975.21	6,975.21	9.00	2.13	6,972.88	Standard	6,972.89	Cylindrical S	0.01
56: 44 (81)	44 (81)	6,975.03	6,975.03	3.60	0.72	6,970.76	Standard	6,970.79	Cylindrical S	0.03
57: I#7 (DP 9)		6,974.64	6,974.64	4,10	1.29	6,973.24	Standard	6,973.39	CDOT Type-	0.15
58: I#8 (DP 10	` <i>`</i> /	6,974.64	6,974.64	9.00	1.87	6,973.05	Standard	6,973,18	CDOT Type-	0.14
59: I#6 (DP 1)	·	6,973.20	6,973.20	3.60	0.72	6,971.57	Standard	6,972.00	CDOT Type-	0.42
60: 44 (78) (D	44 (78) (DP 11)	6,973.16	6,973.16	1.40	0.44	6,968.87	Standard	6,969.03	CDOT Type-	0.16
98: MH#26 (D	MH#26 (DP6.1)	7,027.15	7,027.15	22.40	1.69	7,022.19	Standard	7,023.91	STORM MH	1.73
99: MH#27 (D	MH#27 (DP8)	7,027.09	7,027.09	21.00	3.40	7,024.40	Standard	7,025.03	STORM MH	0.62
100: I#9 (DP6)		7,027.04	7,027.04	2.40	0.89	7,023.89	Standard	7,023.94	CDOT Type-	0.05
101: I#8 (DP5)		7,026.63	7,026.63	1.30	0.43	7,024,43	Standard	7,024.66	CDOT Type-	0.23
102: I#7 (DP3.		7,026.51	7,026.51	3.20	1.71	7,023.01		7,023.02	CDOT Type-	0.00
103: I#6 (DP2.		7,026.40	7,026.40	1.50	0.63	7,022.99	Standard	7,023.10	CDOT Type-	0.10
106: MH#34	MH#34	7,023.51	7,023.51	3.40	0.70	7,019.72		7,019.84	CDOT Type-	0.13
111: MH#21	MH#21	7,014.03	7,014.03	112.10	3.20	7,001.72		7,003.94	STORM MH	2.22
112: MH#20	MH#20	7,012.41	7,012.41	112.10	4.38	7,005.57		7,005.63	STORM MH	0.06
113: MH#19	MH#19	7,010.85	7,010.85	112.10	3.20	7,007.14		7,009.36	STORM MH	2.22
115: MH#22	MH#22	7,005.85	7,005.85	112.10	3.20	6,998.35		6,998.44	STORM MH	0.08
116: MH#9	MH#9	7,003.03	7,003.03	19.10	2.45	6,992.21		6,992.24	STORM MH	0.03
117: I#4 (DP1	I#4 (DP14)	7,000.17	7,000.17	8.80	1.62	6,997.31		6,997.89	CDOT Type-	0.58
118: MH#10 (MH#10 (DP 1	7,000.01	7,000.01	19.10	1.57	6,995.82		6,997.25	STORM MH	1.43
119: I#5 (DP 1		6,999.67	6,999.67	10.40	1.88	6,997.78	Standard	6,998.59	CDOT Type-	0.81
120: MH#8	MH#8	6,996.13	6,996.13	10.40	3.77	6,990.43		6,990.80	STORM MH	0.31
120: MH#0 121: MH#23	MH#23	6,997.20	6,997.20	112.10	6.42	6,995.25		6,995.31	STORM MH	0.06
122: MH#24	MH#24	6,996.25	6,996.25	112.10	6.28	6,994.28	Standard	6,994.34	STORM MH	0.06
122: MH#24 123: DP12	DP12	6,996.40	6,996.40	24.40	3.63	6,993.95		6,995.35	CDOT Type-	1.41
123: DP12 124: MH#25 (MH#25 (DP13)	6,995.75	6,995.75	136.40	4.47	6,993.95	Standard	6,993.62	STORM MH	1.41
190: INLET (D	INLET (DP 3)	6,995.75	6,995.75	24.50	1.69	6,991.97	Standard	6,993.62	CDOT FES	1.05
190: INLET (D 192: DP 7	DP 7	7,024.45	7,024.45	24.50	1.69	7.024.45		7,024,52	CDOT FES	0.07
192: DP 7 193: DP 2	DP 7 DP 2	7,024.45	7,024.45	2.20	1.44	7,024.45	Standard	7,024.52	CDOT FES	0.07
193: DP 2 194: DP 3	DP 2 DP 3		7,024.26	18.80	4.42	7,024.26		7,025.10	CDOT FES	1.86
		7,009.43								
196: CULVERT	CULVERT 1 (7,000.01	7,000.01	245.50	2.66	6,999.67	Standard	7,001.66	Dummy Null	1.99
TAX: COLVERI	CULVERT 2 (7,000.01	7,000.01	295.50	3.00	7,000.01	Standard	7,002.27	Dummy Null	2.26

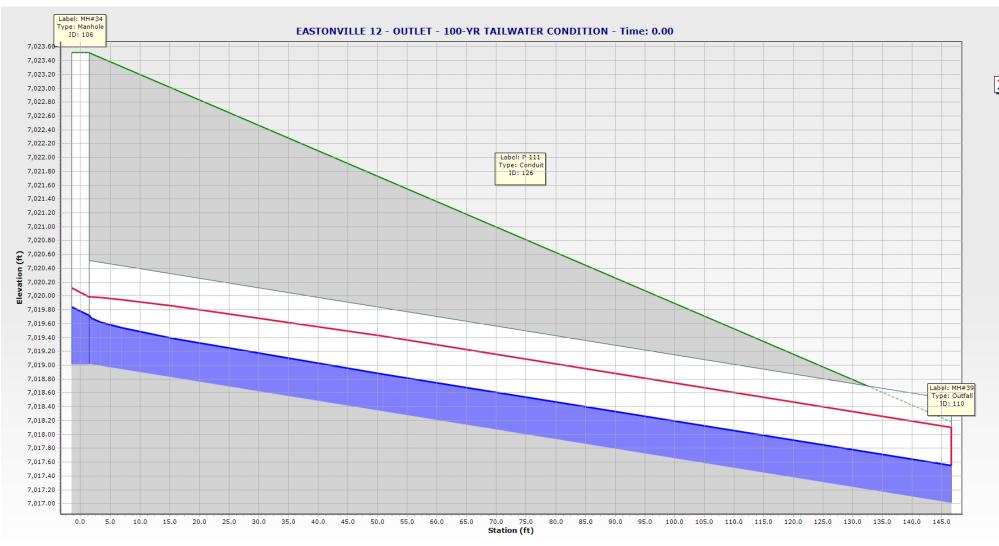
	Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
48: OUTFALL	OUTFALL	6,983.32	6,979.44		6,981.66	54.30	CDOT FES
53: 44 (70)	44 (70)	6,979.33	6,977.55		6,977.85	1.20	CDOT FES
54: 44 (65)	44 (65)	6,976.31	6,973.52		6,974.58	24.50	CDOT FES
61: 44 (77)	44 (77)	6,971.10	6,969.39		6,970.00	3.60	CDOT FES
64: 44 (79)	44 (79)	6,969.82	6,967.50		6,967.84	1.40	CDOT FES
107: DP9	DP9	7,022.74	7,019.00		7,020.22	22.40	CDOT FES
108: FES OUTF	FES OUTFALL 1	7,023.00	7,021.01	7,023.00	7,023.00	3.20	CDOT FES
110: MH#39	MH#39	7,018.18	7,017.01		7,017.55	3.40	CDOT FES
125: OUTLET S	OUTLET SEG	6,991.09	6,986.67	6,988.30	6,990.15	136.40	CDOT FES
162: 0-3	O-3	6,987.98	6,984.83	6,987.98	6,987.98	26.20	Dummy Null:
164: 0-5	O-5	6,982.10	6,981.08	6,982.10	6,982.10	6.50	Dummy Null:
165: 0-6	0-6	6,972.87	6,970.61	6,972.87	6,972.87	9.00	Dummy Null:
203: 0-7	0-7	6,998.27	6,995.27		6,997.02	245.50	Dummy Null:
207: 0-10	O-10	6,998.27	6,995.27		6,997.28	295.50	Dummy Null:

NOTE: SEGMENT 1 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

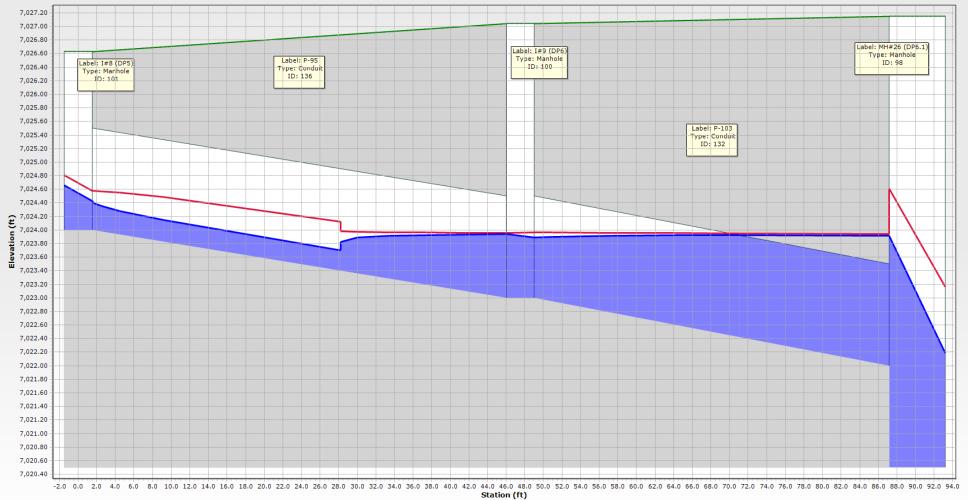


EASTONVILLE 12 - INLET - 100-YR TAILWATER CONDITION

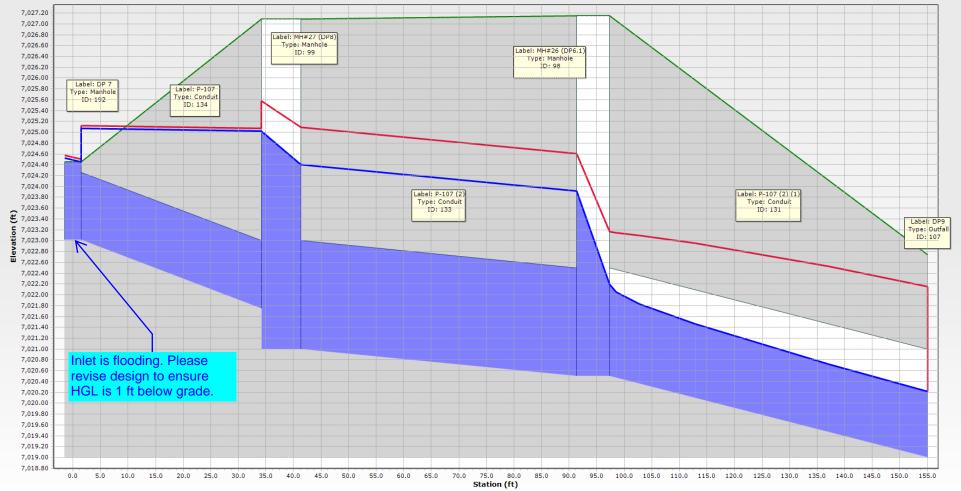
= EGL = HGL



= EGL = HGL

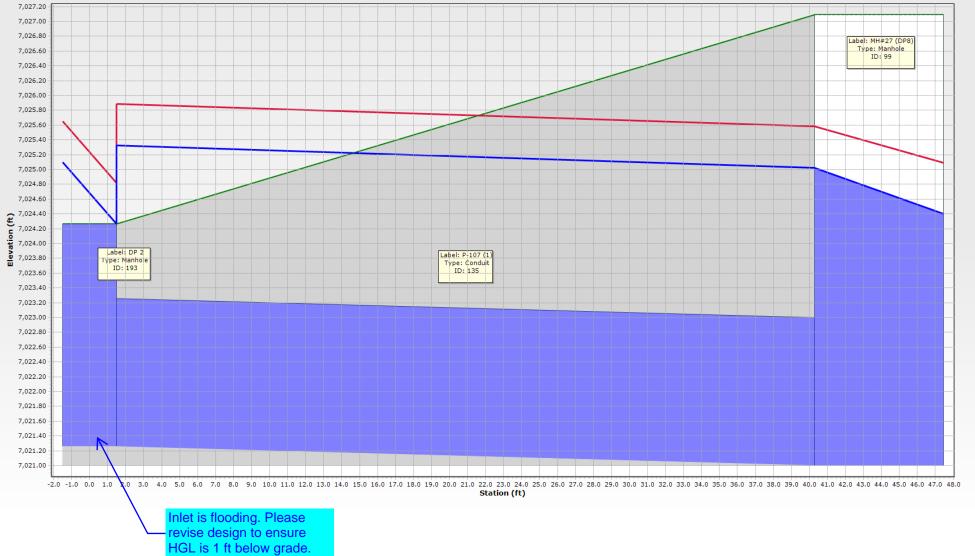


EASTONVILLE 13 - 100-YR TAILWATER CONDITION



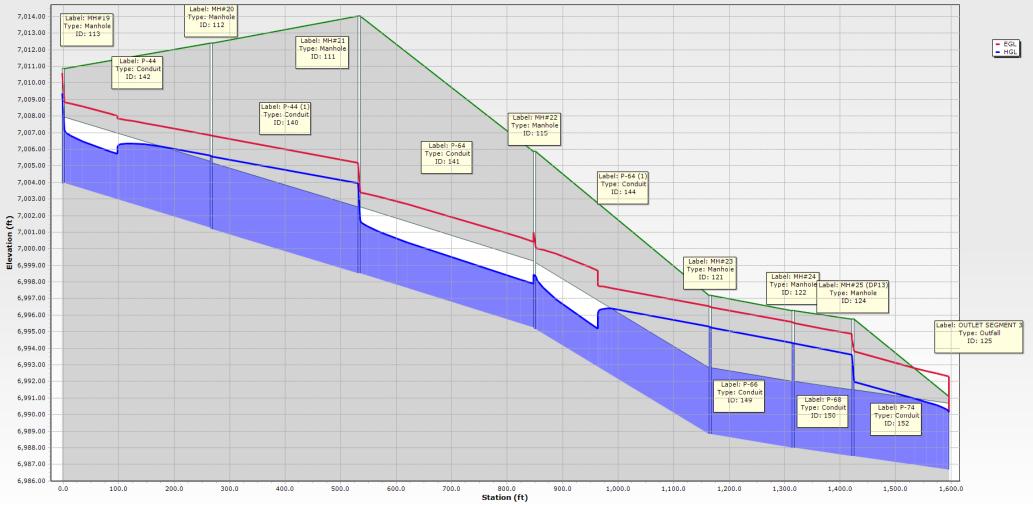
EASTONVILLE 14 - 100-YR TAILWATER CONDITION

- EGL - HGL

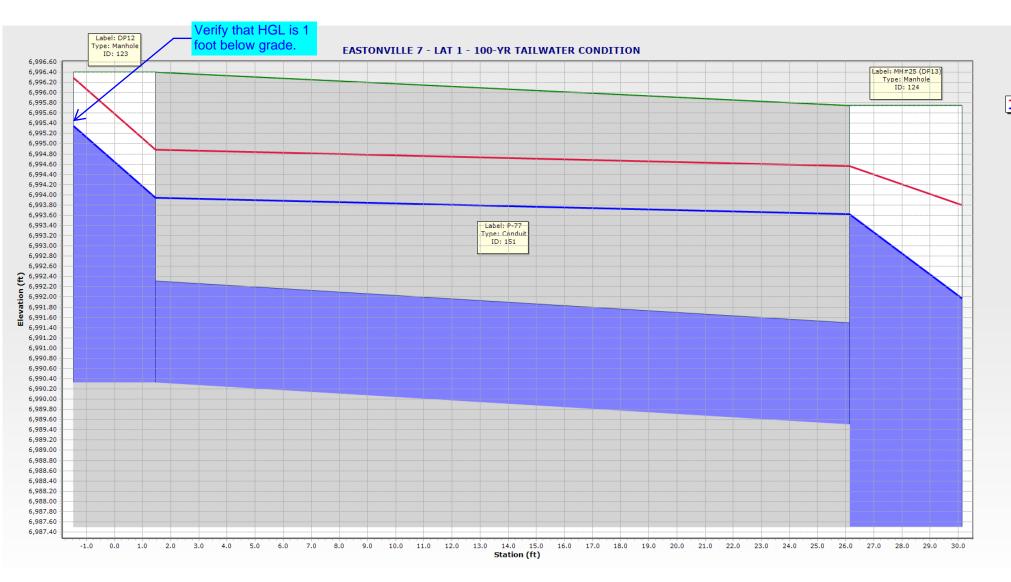


EASTONVILLE 15 - 100-YR TAILWATER CONDITION

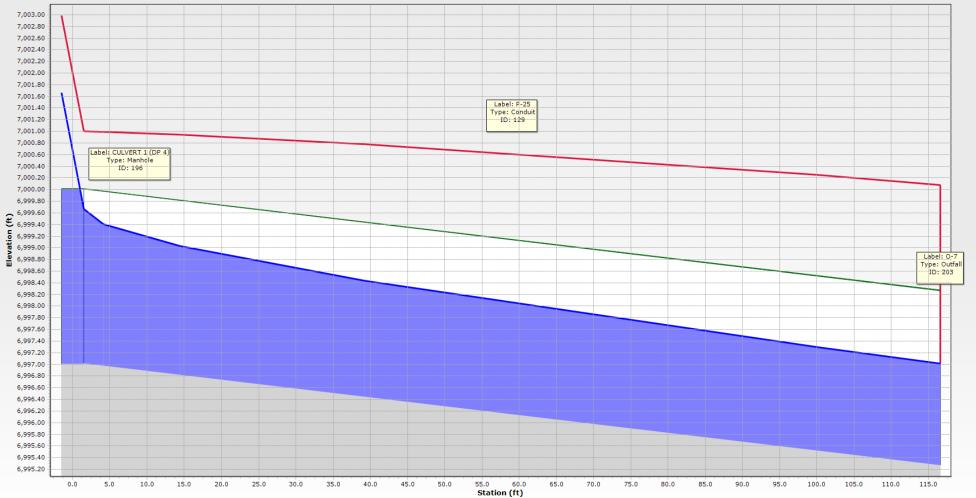
- EGL - HGL



EASTONVILLE 7 - 100-YR TAILWATER CONDITION - Time: 0.00

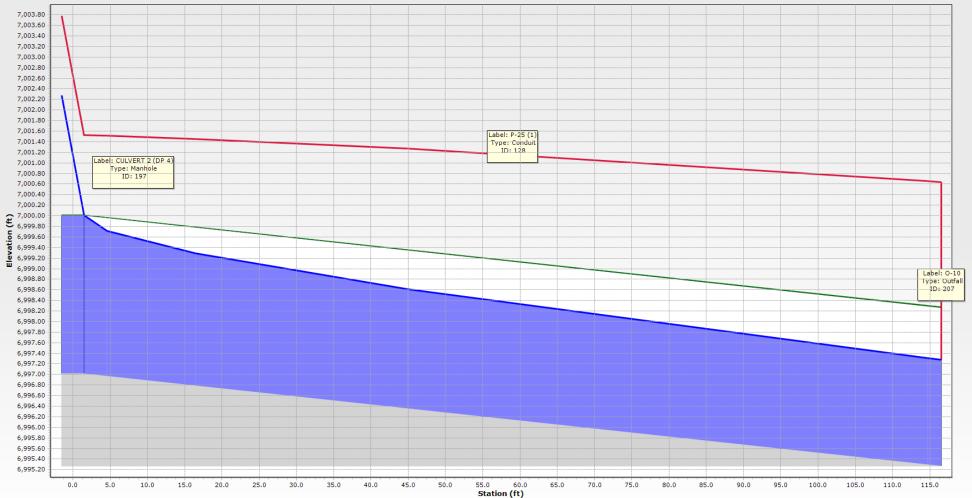


- EGL - HGL Use other format besides StormCAD to design culverts, to properly determine HW elevation, overtopping, etc

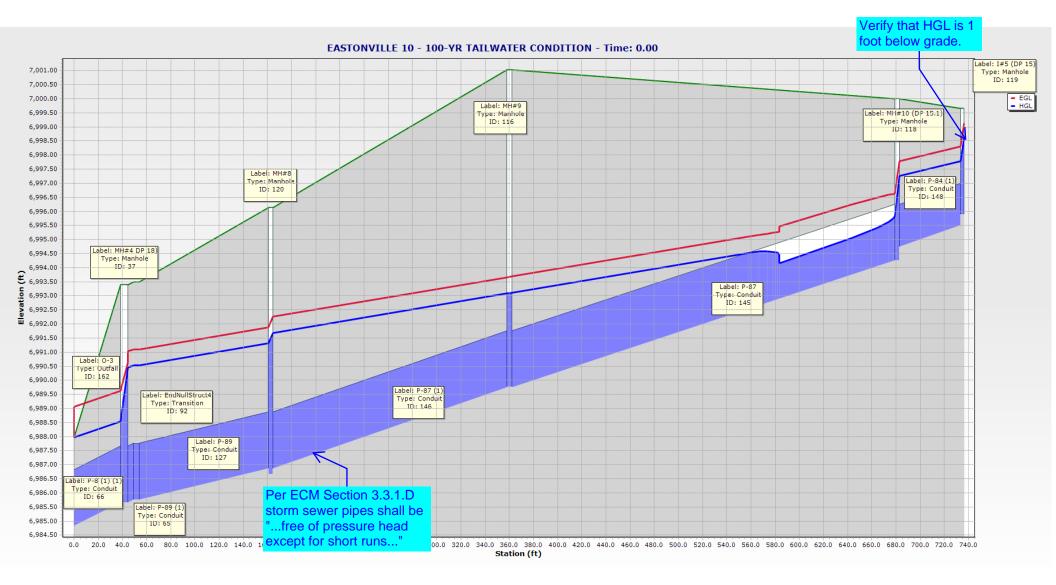


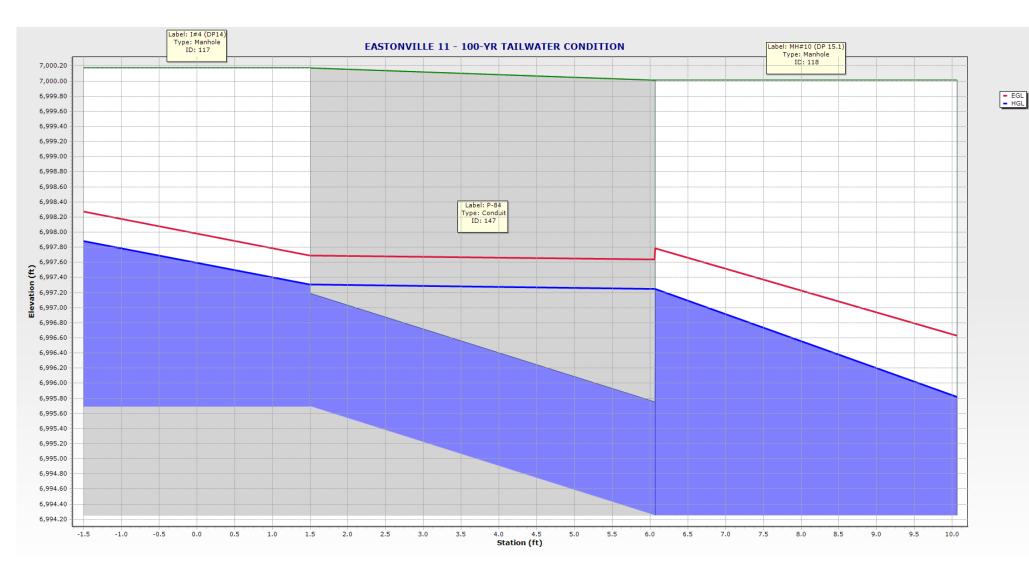
EASTONVILLE 8 - NORTH CULVERT - 100-YR TAILWATER CONDITION - Time: 0.00

= EGL = HGL



EASTONVILLE 8 - SOUTH CULVERT - 100-YR TAILWATER CONDITION





5 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

	Label	Start Node	Invert <mark>(</mark> Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Notes	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
66: P-8 (1) (1)	P-8 (1) (1)	MH#4 DP 18)	6,985.66	0-3	6,984.83	41.6	0.020	24.0	15.60	4.97	31.99		Concrete Pip	6,988.57	6,988.37
67: P-124	P-124	I#5 (DP 14)	6,981.25	O-5	6,981.08	34.3	0.005	18.0	3.90	4.25	7.43	52.5	Concrete Pip	6,982.28	6,982.25
68: P-121 (2)	P-121 (2)	44 (80)	6,970.65	O-6	6,970.61	9.0	0.005	24.0	4.20	1.34	15.95	26.3	Concrete Pip	6,973.23	6,973.23
69: P-18	P-18	I#3 (DP 7)	6,985.73	MH#7	6,985.38	71.3	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pip	6,986.58	6,986.42
70: P-20	P-20	MH#7	6,985.38	MH#6	6,984.50	175.6	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pir	6,986.22	6,985.54
71: P-5	P-5	I#2 (DP 17)	6,989.29	I#1 (DP 16)	6,989.74	52.0	-0.009	18.0	3.00	4.87	9.77	30.7	Concrete Pir	6,990.40	6,990.02
72: P-8 (1)	P-8 (1)	I#2 (DP 17)	6,988.79	MH#4 DP 18)	6,985.66	156.4	0.020	24.0	6.30	7.92	31.99	19.7	Concrete Pir	6,989.68	6,988.96
73: P-21	P-21	MH#6	6,984.50	MH#5	6,984.13	74.6	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pir	6,985.35	6,985.17
74: P-22	P-22	MH#5	6,984.13	MH#3 (DP 8)	6,980.80	127.1	0.026	42.0	7.90	8.74	162.72	4.9	Concrete Pip	6,984.97	6,981.95
75: P-15	P-15	18 (DP 19)	6,983.26	MH#3 (DP 8)	6,982.80	30.8	0.015	18.0	0.30	3.02	12.90	2.3	Concrete Pip	6,983.47	6,982.96
76: P-15 (1)	P-15 (1)	MH#3 (DP 8)	6,980.80	MH#2 (DP 8)	6,980.43	75.1	0.005	42.0	8.30	4.92	70.62	11.8	Concrete Pip	6,981.67	6,981.50
77: P-16	P-16	MH#2 (DP 8)	6,980.43	MH#1	6,980.05	78.1	0.005	42.0	8.30	4.90	70.19	11.8	Concrete Pip	6,981.30	6,980.95
78: P-123	P-123	I#4 (DP 13)	6,981.51	I#5 (DP 14)	6,981.25	52.0	0.005	18.0	2.10	3.61	7.43	28.3	Concrete Pip	6,982.43	6,982.42
79: P-17	P-17	MH#1	6,980.05	OUTFALL	6,979.36	139.8	0.005	42.0	8.30	4.92	70.67	11.7	Concrete Pip	6,980.92	6,980.17
80: P-125	P-125	44 (69) (DP 15)	6,978.42	44 (70)	6,977.55	54.5	0.016	18.0	0.30	3.09	13.30	2.3	Concrete Pip	6,978.63	6,977.71
83: P-122	P-122	INLET (DP 3)	6,978.16	44 (65)	6,973.52	183.8	0.025	30.0	3.70	7.19	65.19	5.7	Concrete Pip	6,978.80	6,973.93
84: P-121	P-121	I#8 (DP 10)	6,971.18	44 (80)	6,970.65	105.1	0.005	24.0	4.20	1.34	16.06	26.1	Concrete Pip	6,973.27	6,973.23
85: P-130	P-130	I#6 (DP 1)	6,970.85	44 (81)	6,970.04	81.5	0.010	18.0	0.50	3.05	10.47	4.8	Concrete Pip	6,971.11	6,970.31
86: P-130 (1)	P-130 (1)	44 (81)	6,970.04	44 (77)	6,969.39	65.0	0.010	18.0	0.50	3.05	10.50	4.8	Concrete Pip	6,970.30	6,969.61
87: P-121 (1)	P-121 (1)	I#8 (DP 10)	6,971.68	I#7 (DP 9)	6,971.95	52.0	-0.005	18.0	2.20	3.71	7.57	29.1	Concrete Pip	6,973.32	6,973.30
88: P-131	P-131	44 (78) (DP 11)	6,968.42	44 (79)	6,967.50	62.5	0.015	18.0	0.40	3.27	12.77	3.1	Concrete Pip	6,968.66	6,967.68
126: P-111	P-111	MH#34	7,019.01	MH#39	7,017.01	146.6	0.014	18.0	1.70	4.88	12.28	13.8	Concrete Pip	7,019.50	7,017.39
127: P-89	P-89	MH#8	6,986.87	MH#4 DP 18)	6,985.66	111.1	0.011	24.0	10.20	3.25	23.64	43.2	Concrete Pip	6,989.18	6,988.96
128: P-25 (1)	P-25 (1)	CULVERT 2 (DP 4)	6,997.01	O-10	6,995.27	116.5	0.015		11.20	5.01	461.86	2.4	Concrete Bo	6,997.35	6,995.49
129: P-25	P-25	CULVERT 1 (DP 4)	6,997.01	0-7	6,995.27	116.6	0.015		11.20	5.01	461.72	2.4	Concrete Bo	6,997.35	6,995.49
131: P-107 (2)	P-107 (2) (1)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	2.90	6.82	35.57	8.2	Concrete Pip	7,021.09	7,019.39
132: P-103	P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	1.20	5.34	16.08	7.5	Concrete Pip	7,023.41	7,022.28
133: P-107 (2)	P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	2.00	4.25	21.26	9.4	Concrete Pip	7,021.49	7,021.47
134: P-107	P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.30	4.09	11.81	2.5	Concrete Pip	7,023.22	7,021.89
135: P-107 (1)	P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	1.70	3.52	17.41	9.8	Concrete Pip	7,021.71	7,021.65
136: P-95	P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.70	4.38	15.24	4.6	Concrete Pip	7,024.31	7,023.50
137: P-93	P-93	I#6 (DP2.1)	7,022.36	I#7 (DP3.1)	7,021.80	55.9	0.010	18.0	0.80	3.51	10.51	7.6	Concrete Pip	7,023.00	7,023.00
138: Pipe - (34	Pipe - (34)	I#7 (DP3.1)	7,021.80	FES OUTFALL 1	7,021.01	33.5	0.023	18.0	1.60	5.81	16.07	10.0	Concrete Pip	7,023.00	7,023.00
140: P-44 (1)	P-44 (1)	MH#20	7,001.18	MH#21	6,998.52	266.5	0.010	48.0	6.10	5.68	143.63	4.2	Concrete Pip	7,001.90	6,999.57
141: P-64	P-64	MH#21	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	6.10	5.74	145.88	4.2	Concrete Pip	6,999.24	6,995.82
142: P-44	P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	6.10	5.68	143.63	4.2	Concrete Pip	7,004.66	7,001.84
143: P-26	P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	6.10	6.03	156.73	3.9	Concrete Pip	7,005.73	7,004.99
144: P-64 (1)	P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	6.10	7.23	203.15	3.0	Concrete Pip	6,995.87	6,989.55
145: P-87	P-87	MH#10 (DP 15.1)	6,994.25	MH#9	6,989.76	320.7	0.014	24.0	10.20	7.94	26.78	38.1	Concrete Pip	6,995.39	6,990.92
146: P-87 (1)	P-87 (1)	MH#9	6,989.76	MH#8	6,986.87	197.4	0.015	24.0	10.20	8.07	27.33	37.3	Concrete Pip	6,990.90	6,989.29
147: P-84	P-84	I#4 (DP14)	6,995.69	MH#10 (DP 1	6,994.25	8.1	0.179	18.0	5.20	16.82	44.40	11.7	Concrete Pip	6,996.57	6,995.64
148: P-84 (1)	P-84 (1)	MH#10 (DP 15.1)	6,994.75	I#5 (DP 15)	6,995.50	53.9	-0.014	18.0	5.00	6.64	12.40	40.3	Concrete Pip	6,996.36	6,995.64
149: P-66	P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	6.10	4.60	106.64	5.7	Concrete Pip	6,989.54	6,989.51
150: P-68	P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	6.10	4.33	97.84	6.2	Concrete Pip	6,989.51	6,989.51
151: P-77	P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	3.60	7.70	38.62	9.3	Concrete Pip	6,990.98	6,989.93
152: P-74	P-74	MH#25 (DP13)	6,987.50	OUTLET SEG	6,986.67	173.3	0.005	48.0	26.00	6.66	99.34	26.2	Concrete Pip	6,989.01	6,988.30

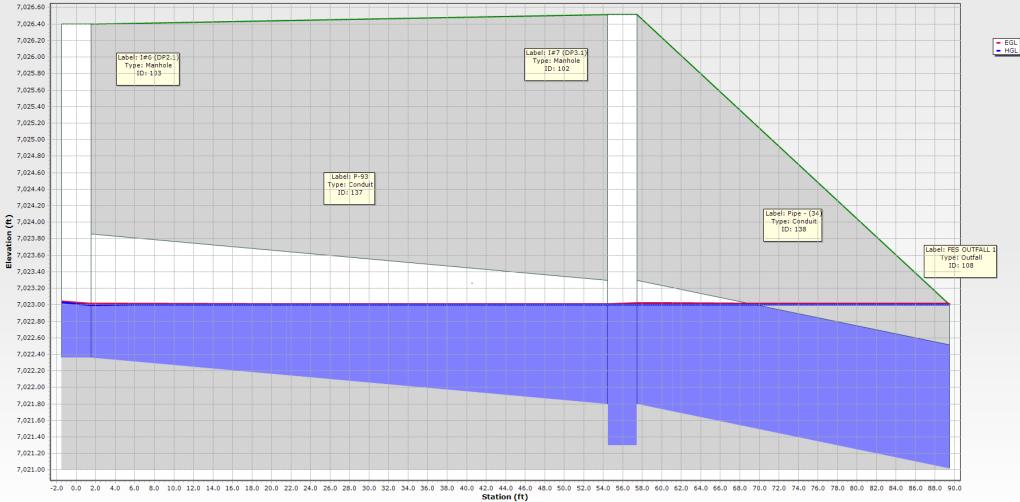
NOTE: EASTONVILLE 12 - INLET, EASTONVILLE 10, & EASTONVILLE 11 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

5 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

	Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Depth (Out) (ft)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Notes	Headloss (ft)
35: MH#7	MH#7	6,993.52	6,993.52	7.90	0.85	6,986.22	6,986.42	STORM MH	0.19
36: I#1 (DP 16	I#1 (DP 16)	6,993.41	6,993.41	3.00	0.66	6,990.40	6,990.77	CDOT Type-	0.38
37: MH#4 DP	MH#4 DP 18)	6,993.40	6,993.40	15.60	2.91	6,988.57	6,988.96	STORM MH	0.39
38: I#2 (DP 17	I#2 (DP 17)	6,993.39	6,993.39	6.30	0.90	6,989.68	6,990.02	CDOT Type-	0.35
39: MH#6	MH#6	6,993.02	6,993.02	7.90	0.85	6,985.35	6,985.54	STORM MH	0.19
40: MH#5	MH#5	6,991.91	6,991.91	7.90	0.85	6,984.97	6,985.17	STORM MH	0.19
41: MH#3 (DP	MH#3 (DP 8)	6,991.13	6,991.13	8.30	0.56	6,981.67	6,981.95	STORM MH	0.28
42: I#3 (DP 7)	I#3 (DP 7)	6,990.73	6,990,73	7.90	0.93	6,986.58	6,987.03	CDOT Type-	0.45
43: 18 (DP 19)	18 (DP 19)	6,988,71	6,988,71	0.30	1.96	6,983,47	6,983.57	CDOT Type-	0.10
44: MH#2 (DP		6,985,74	6,985,74	8.30	0.87	6,981.30	6,981,50	STORM MH	0.20
45: I#4 (DP 13		6,985.02	6,985.02	2,10	1.13	6,982.43	6,982,51	CDOT Type-	0.08
46: I#5 (DP 14		6,985.02	6,985.02	3.90	1.23	6,982,28	6,982,42	CDOT Type-	0.15
47: MH#1	MH#1	6,984.95	6,984.95	8.30	0.87	6,980.92	6,980.95	STORM MH	0.03
49: 44 (69) (D	44 (69) (DP 15)	6,982.64	6,982.64	0.30	0.20	6,978.63	6,978.63	CDOT Type-	0.01
55: 44 (80)	44 (80)	6,975.21	6,975,21	4.20	2,48	6,973,23	6,973,23	Cylindrical S	0.00
56: 44 (81)	44 (81)	6,975.03	6,975.03	0.50	0.26	6,970.30	6,970.31	Cylindrical S	0.01
57: I#7 (DP 9)		6,974.64	6,974.64	2.20	1.37	6,973.32	6,973.36	CDOT Type-	0.04
58: I#8 (DP 10		6,974.64	6,974.64	4.20	2.09	6,973.27	6,973.30	CDOT Type-	0.03
	I#6 (DP 1)	6,973.20	6,973.20	0,50	0.26	6,971.11	6,971.25	CDOT Type-	0.14
60: 44 (78) (D	44 (78) (DP 11)	6,973.16	6,973.16	0.40	0.23	6,968.66	6,968,74	CDOT Type-	0.08
98: MH#26 (D	MH#26 (DP6.1)	7,027.15	7,027.15	2,90	0.59	7,021.09	7,021.47	STORM MH	0.38
99: MH#27 (D	MH#27 (DP8)	7,027.09	7,027.09	2.00	0.49	7,021.49	7,021.65	STORM MH	0.16
100: I#9 (DP6)		7,027.04	7,027.04	1.20	0.41	7,023.41	7,023.50	CDOT Type-	0.09
101: I#8 (DP5)		7,026.63	7,026.63	0.70	0.31	7,024.31	7,024.47	CDOT Type-	0.15
102: I#7 (DP3.		7,026.51	7,026.51	1.60	1.70	7,023.00	7,023.00	CDOT Type-	0.00
102: I#7 (DF3: 103: I#6 (DP2.		7,026.40	7,026,40	0.80	0.64	7,023.00	7,023.03	CDOT Type-	0.03
105: I#0 (B12: 106: MH#34	MH#34	7,023.51	7,023.51	1.70	0.49	7,019.50	7,019.59	CDOT Type-	0.08
111: MH#21	MH#21	7,023.31	7,014.03	6.10	0.72	6,999.24	6,999.57	STORM MH	0.33
112: MH#20	MH#20	7,014.03	7,014.03	6.10	0.72	7,001.90	7,001.91	STORM MH	0.01
112: MH#19	MH#19	7,012.41	7,012.41	6.10	0.72	7,001.50	7,001.91	STORM MH	0.33
115: MH#22	MH#22	7,010.85	7,005.85	6.10	0.72	6,995.87	6,995.88	STORM MH	0.01
115: MH#22 116: MH#9	MH#9	7,003.83	7,003.83	10.20	1.14	6,990.90	6,990.92	STORM MH	0.01
117: I#4 (DP1	I#4 (DP14)	7,001.03	7,001.03	5.20	0.88	6,996.57	6,997.11	CDOT Type-	0.02
117: 1#4(DP1 118: MH#10(MH#10 (DP 1	7,000.17	7,000.17	10.20	1.14	6,995.39	6,995.64	STORM MH	0.33
119: I#5 (DP 1		6,999,67	6.999.67	5.00	0.46	6,996,36	6,996.89	CDOT Type-	0.24
120: MH#8	1#5 (DP 15) MH#8	6,999.67	6,999.67	10.20	2.52	6,996.36	6,989.29	STORM MH	0.55
				6,10					
121: MH#23	MH#23	6,997.20	6,997.20		0.72	6,989.54	6,989.55	STORM MH	0.01
122: MH#24	MH#24	6,996.25	6,996.25	6.10	1.51	6,989.51	6,989.51	STORM MH	0.00
123: DP12	DP12	6,996.40	6,996.40	3.60	0.67	6,990.98	6,991.35	CDOT Type-	0.36
124: MH#25 (MH#25 (DP13)	6,995.75	6,995.75	26.00	1.51	6,989.01	6,989.51	STORM MH	0.50
190: INLET (D	INLET (DP 3) DP 7	6,980.96	6,980.96	3.70	0.63	6,978.80	6,979.13	CDOT FES	0.34
192: DP 7		7,024.45	7,024.45	0.30	0.21	7,023.22	7,023.33	CDOT FES	0.11
193: DP 2	DP 2	7,024.26	7,024.26	1.70	0.45	7,021.71	7,021.95	CDOT FES	0.24
194: DP 3	DP 3	7,009.43	7,009.43	6.10	0.72	7,005.73	7,006.10	CDOT FES	0.37
196: CULVERT		7,000.01	7,000.01	11.20	0.34	6,997.35	6,997.61	Dummy Null	0.25
197: CULVERT	CULVERT 2 (7,000.01	7,000.01	11.20	0.34	6,997.35	6,997.61	Dummy Null	0.25

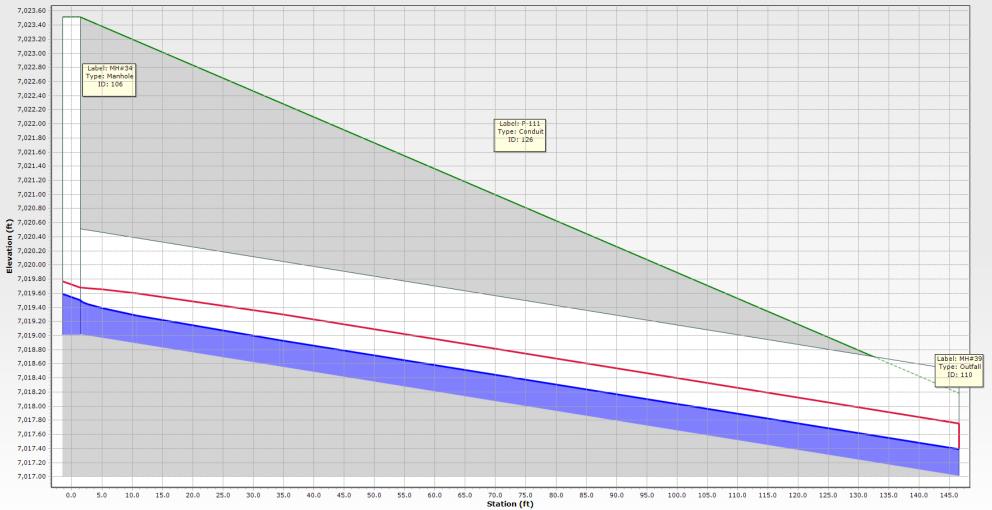
	Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
48: OUTFALL	OUTFALL	6,983.32	6,979.44		6,980.17	8.30	CDOT FES
53: 44 (70)	44 (70)	6,979.33	6,977.55		6,977.71	0.30	CDOT FES
54: 44 (65)	44 (65)	6,976.31	6,973.52		6,973.93	3.70	CDOT FES
61: 44 (77)	44 (77)	6,971.10	6,969.39		6,969.61	0.50	CDOT FES
64: 44 (79)	44 (79)	6,969.82	6,967.50		6,967.68	0.40	CDOT FES
107: DP9	DP9	7,022.74	7,019.00		7,019.39	2.90	CDOT FES
108: FES OUTF	FES OUTFALL 1	7,023.00	7,021.01	7,023.00	7,023.00	1.60	CDOT FES
110: MH#39	MH#39	7,018.18	7,017.01		7,017.39	1.70	CDOT FES
125: OUTLET S	OUTLET SEG	6,991.09	6,986.67	6,988.30	6,988.30	26.00	CDOT FES
162: 0-3	0-3	6,987.98	6,984.83	6,988.37	6,988.37	15.60	Dummy Null
164: 0-5	0-5	6,982.10	6,981.08	6,982.25	6,982.25	3.90	Dummy Null
165: 0-6	0-6	6,972.87	6,970.61	6,973.23	6,973.23	4.20	Dummy Null
203: 0-7	0-7	6,998.27	6,995.27		6,995.49	11.20	Dummy Null
207: 0-10	O-10	6,998.27	6,995.27		6,995.49	11.20	Dummy Null

NOTE: EASTONVILLE 12 - INLET, EASTONVILLE 10, & EASTONVILLE 11 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

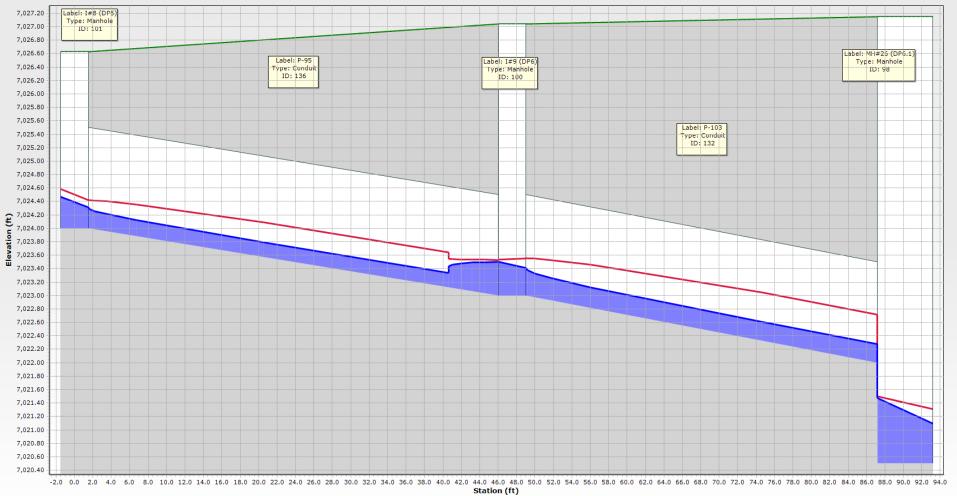


EASTONVILLE 12 - INLET - 5-YR TAILWATER CONDITION

NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE OUTFALL CONDITION BLEOW TO MEET CAPACITY & VELOCITY REQUIREMENTS

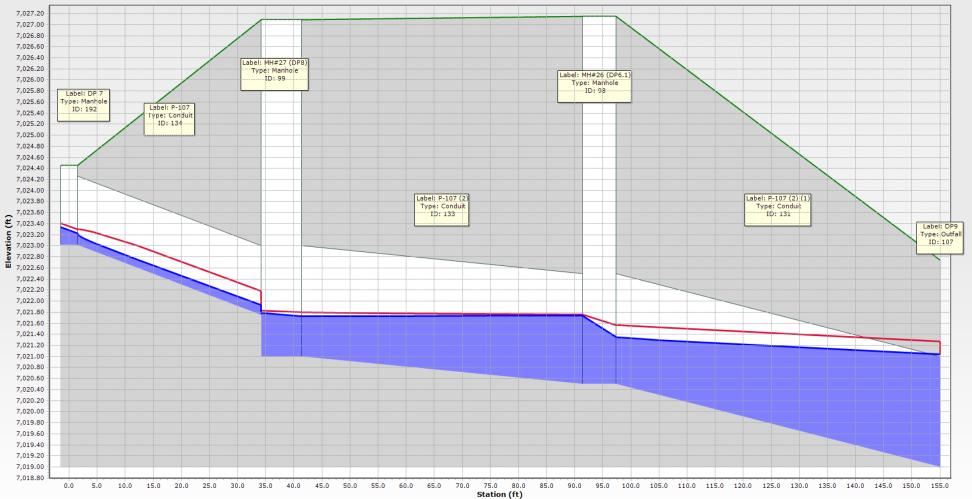


EASTONVILLE 12 - OUTLET - 5-YR TAILWATER CONDITION

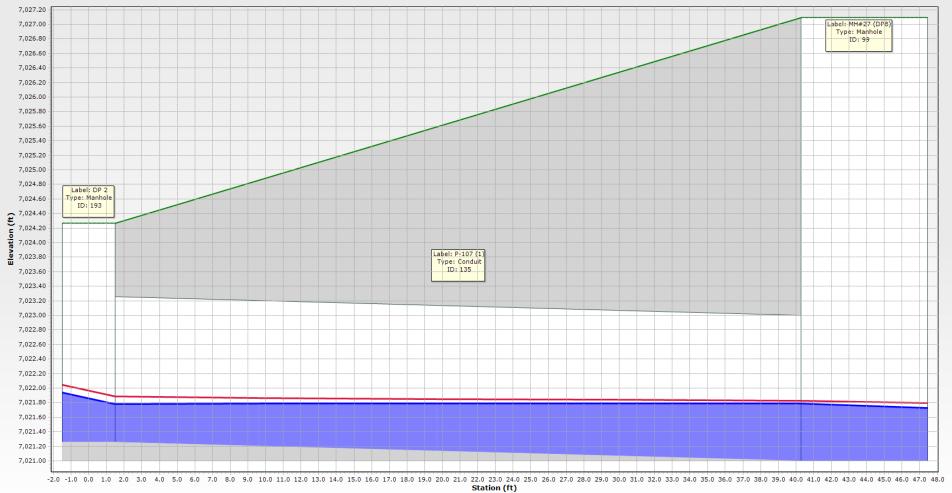


EASTONVILLE 13 - 5-YR TAILWATER CONDITION - Time: 0.00

= EGL = HGL



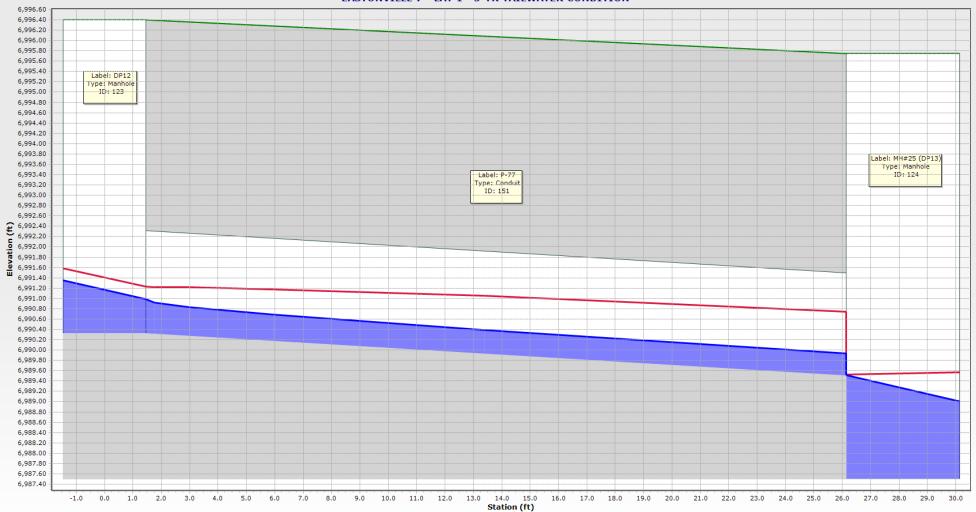
EASTONVILLE 14 - 5-YR TAILWATER CONDITION



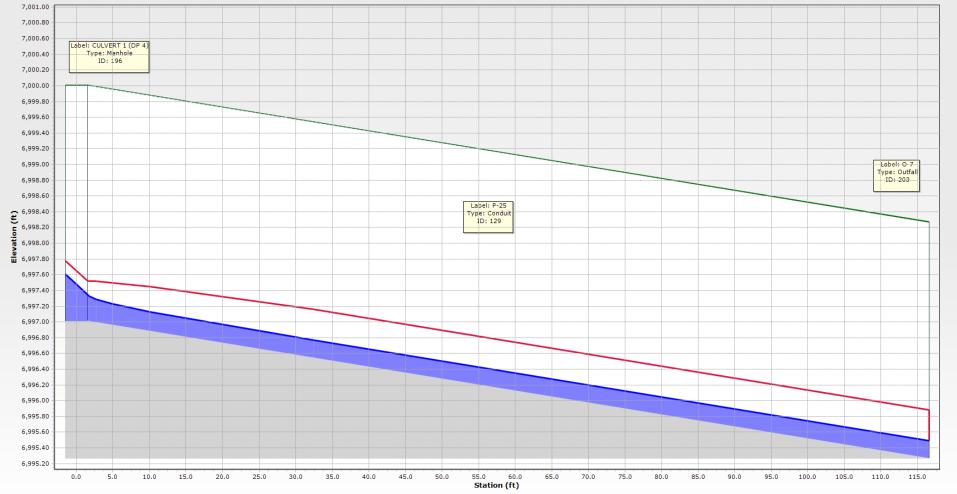
EASTONVILLE 15 - 5-YR TAILWATER CONDITION



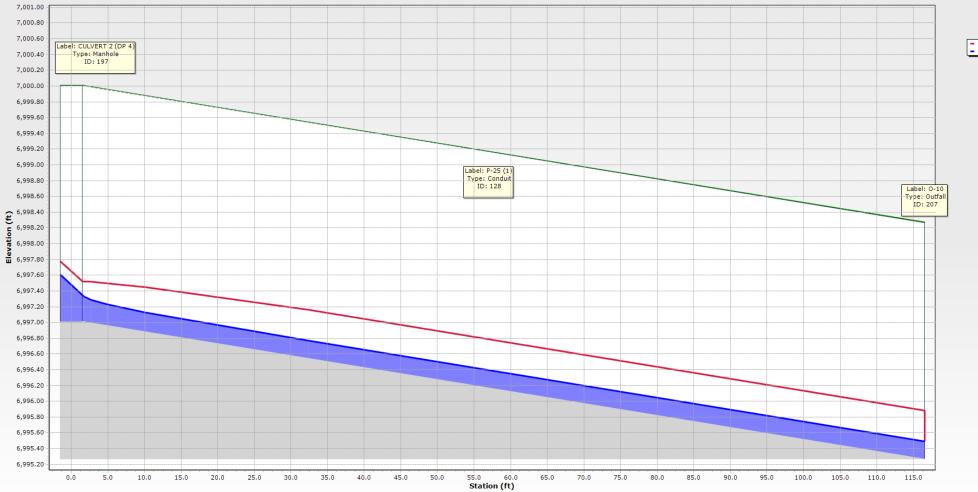
EASTONVILLE 7 - 5-YR TAILWATER CONDITION



EASTONVILLE 7 - LAT 1 - 5-YR TAILWATER CONDITION

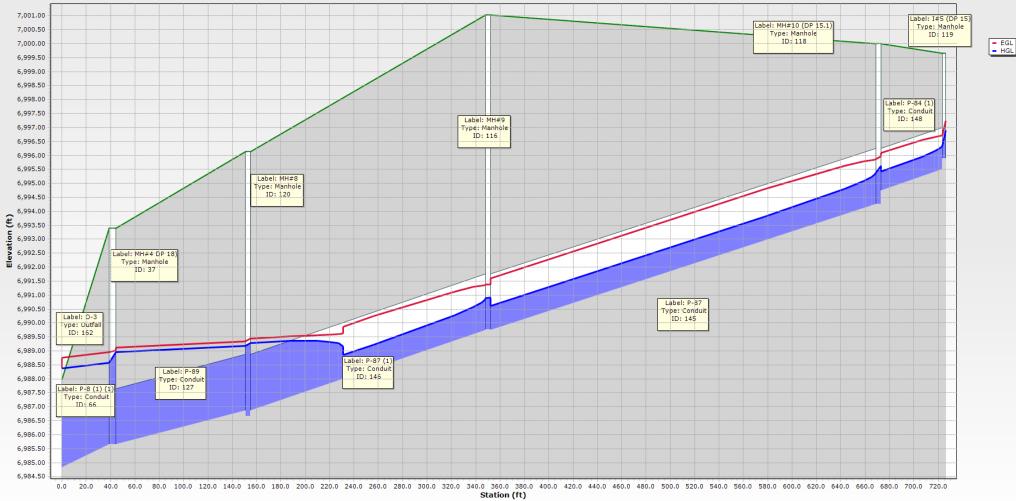


EASTONVILLE 8 - NORTH CULVERT - 5-YR TAILWATER CONDITION



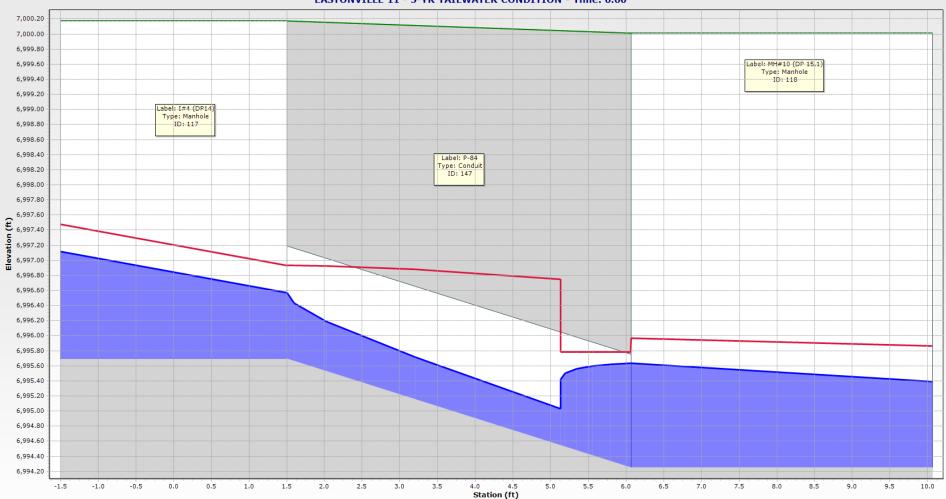
EASTONVILLE 8 - SOUTH CULVERT - 5-YR TAILWATER CONDITION

= EGL = HGL



EASTONVILLE 10 - 5-YR TAILWATER CONDITION - Time: 0.00

NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE OUTFALL CONDITION BLEOW TO MEET CAPACITY & VELOCITY REQUIREMENTS



EASTONVILLE 11 - 5-YR TAILWATER CONDITION - Time: 0.00

NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE OUTFALL CONDITION BLEOW TO MEET CAPACITY & VELOCITY REQUIREMENTS

= EGL = HGL

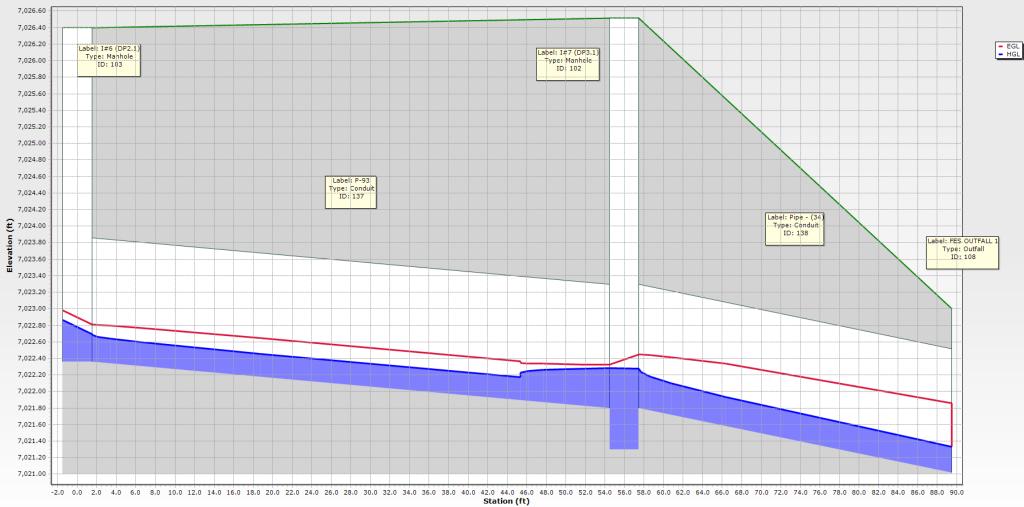
	Label	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Notes	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
66: P-8 (1) (1)	P-8 (1) (1)	MH#4 DP 18)	6,985.66	0-3	6,984.83	41.6	0.020	24.0	15.60	10.12	31.99		Concrete Pic	6,987.09	6,985.89
67: P-124	P-124	I#5 (DP 14)	6,981.25	O-5	6,981.08	34.3	0.005	18.0	3.90	4.25	7.43	52.5	Concrete Pip	6,982.13	6,982.10
68: P-121 (2)	P-121 (2)	44 (80)	6,970.65	0-6	6,970.61	9.0	0.005	24.0	4.20	4.28	15.95	26.3	Concrete Pip	6,971.37	6,971.31
69: P-18	P-18	I#3 (DP 7)	6,985.73	MH#7	6,985.38	71.3	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pip	6,986.58	6,986.42
70: P-20	P-20	MH#7	6,985.38	MH#6	6,984.50	175.6	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pip	6,986.22	6,985.54
71: P-5	P-5	I#2 (DP 17)	6,989.29	I#1 (DP 16)	6,989.74	52.0	-0.009	18.0	3.00	4.87	9.77	30.7	Concrete Pip	6,990.40	6,990.02
72: P-8 (1)	P-8 (1)	I#2 (DP 17)	6,988.79	MH#4 DP 18)	6,985.66	156.4	0.020	24.0	6.30	7.92	31.99	19.7	Concrete Pip	6,989.68	6,987.76
73: P-21	P-21	MH#6	6,984.50	MH#5	6,984.13	74.6	0.005	42.0	7.90	4.88	71.14	11.1	Concrete Pip	6,985.35	6,985.17
74: P-22	P-22	MH#5	6,984.13	MH#3 (DP 8)	6,980.80	127.1	0.026	42.0	7.90	8.74	162.72	4.9	Concrete Pir	6,984.97	6,981.95
75: P-15	P-15	18 (DP 19)	6,983.26	MH#3 (DP 8)	6,982.80	30.8	0.015	18.0	0.30	3.02	12.90	2.3	Concrete Pip	6,983.47	6,982.96
76: P-15 (1)	P-15 (1)	MH#3 (DP 8)	6,980.80	MH#2 (DP 8)	6,980.43	75.1	0.005	42.0	8.30	4.92	70.62	11.8	Concrete Pip	6,981.67	6,981.50
77: P-16	P-16	MH#2 (DP 8)	6,980.43	MH#1	6,980.05	78.1	0.005	42.0	8.30	4.90	70.19	11.8	Concrete Pip	6,981.30	6,980.95
78: P-123	P-123	I#4 (DP 13)	6,981.51	I#5 (DP 14)	6,981.25	52.0	0.005	18.0	2.10	3.61	7.43	28.3	Concrete Pip	6,982.35	6,982.34
79: P-17	P-17	MH#1	6,980.05	OUTFALL	6,979.36	139.8	0.005	42.0	8.30	4.92	70.67	11.7	Concrete Pip	6,980.92	6,980.17
80: P-125	P-125	44 (69) (DP 15)	6,978.42	44 (70)	6,977.55	54.5	0.016	18.0	0.30	3.09	13.30	2.3	Concrete Pip	6,978.63	6,977.71
83: P-122	P-122	INLET (DP 3)	6,978.16	44 (65)	6,973.52	183.8	0.025	30.0	3.70	7.19	65.19	5.7	Concrete Pip	6,978.80	6,973.93
84: P-121	P-121	I#8 (DP 10)	6,971.18	44 (80)	6,970.65	105.1	0.005	24.0	4.20	4.30	16.06	26.1	Concrete Pip	6,971.90	6,971.38
85: P-130	P-130	I#6 (DP 1)	6,970.85	44 (81)	6,970.04	81.5	0.010	18.0	0.50	3.05	10.47	4.8	Concrete Pip	6,971.11	6,970.31
86: P-130 (1)	P-130 (1)	44 (81)	6,970.04	44 (77)	6,969.39	65.0	0.010	18.0	0.50	3.05	10.50	4.8	Concrete Pip	6,970.30	6,969.61
87: P-121 (1)	P-121 (1)	I#8 (DP 10)	6,971.68	I#7 (DP 9)	6,971.95	52.0	-0.005	18.0	2.20	3.71	7.57	29.1	Concrete Pip	6,972.51	6,972.23
88: P-131	P-131	44 (78) (DP 11)	6,968.42	44 (79)	6,967.50	62.5	0.015	18.0	0.40	3.27	12.77	3.1	Concrete Pip	6,968.66	6,967.68
126: P-111	P-111	MH#34	7,019.01	MH#39	7,017.01	146.6	0.014	18.0	1.70	4.88	12.28	13.8	Concrete Pip	7,019.50	7,017.39
127: P-89	P-89	MH#8	6,986.87	MH#4 DP 18)	6,985.66	111.1	0.011	24.0	10.20	7.25	23.64	43.2	Concrete Pip	6,988.02	6,987.76
128: P-25 (1)	P-25 (1)	CULVERT 2 (DP 4)	6,997.01	O-10	6,995.27	116.5	0.015		11.20	5.01	461.86	2.4	Concrete Bo	6,997.35	6,995.49
129: P-25	P-25	CULVERT 1 (DP 4)	6,997.01	0-7	6,995.27	116.6	0.015		11.20	5.01	461.72	2.4	Concrete Bo	6,997.35	6,995.49
131: P-107 (2)	P-107 (2) (1)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	2.90	6.82	35.57	8.2	Concrete Pip	7,021.09	7,019.39
132: P-103	P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	1.20	5.34	16.08	7.5	Concrete Pip	7,023.41	7,022.28
133: P-107 (2)	P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	2.00	4.25	21.26	9.4	Concrete Pip	7,021.49	7,021.47
134: P-107	P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.30	4.09	11.81	2.5	Concrete Pip	7,023.22	7,021.89
135: P-107 (1)	P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	1.70	3.52	17.41	9.8	Concrete Pip	7,021.71	7,021.65
136: P-95	P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.70	4.38	15.24	4.6	Concrete Pip	7,024.31	7,023.50
137: P-93	P-93	I#6 (DP2.1)	7,022.36	I#7 (DP3.1)	7,021.80	55.9	0.010	18.0	0.80	3.51	10.51	7.6	Concrete Pip	7,022.69	7,022.28
138: Pipe - (34	Pipe - (34)	I#7 (DP3.1)	7,021.80	FES OUTFALL 1	7,021.01	33.5	0.023	18.0	1.60	5.81	16.07	10.0	Concrete Pip	7,022.27	7,021.33
140: P-44 (1)	P-44 (1)	MH#20	7,001.18	MH#21	6,998.52	266.5	0.010	48.0	6.10	5.68	143.63	4.2	Concrete Pip	7,001.90	6,999.57
141: P-64	P-64	MH#21	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	6.10	5.74	145.88	4.2	Concrete Pip	6,999.24	6,995.82
142: P-44	P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	6.10	5.68	143.63	4.2	Concrete Pip	7,004.66	7,001.84
143: P-26	P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	6.10	6.03	156.73	3.9	Concrete Pip	7,005.73	7,004.99
144: P-64 (1)	P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	6.10	7.23	203.15	3.0	Concrete Pip	6,995.87	6,989.55
145: P-87	P-87	MH#10 (DP 15.1)	6,994.25	MH#9	6,989.76	320.7	0.014	24.0	10.20	7.94	26.78	38.1	Concrete Pip	6,995.39	6,990.92
146: P-87 (1)	P-87 (1)	MH#9	6,989.76	MH#8	6,986.87	197.4	0.015	24.0	10.20	8.07	27.33	37.3	Concrete Pip	6,990.90	6,988.32
147: P-84	P-84	I#4 (DP14)	6,995.69	MH#10 (DP 1	6,994.25	8.1	0.179	18.0	5.20	16.82	44.40	11.7	Concrete Pip	6,996.57	6,995.64
148: P-84 (1)	P-84 (1)	MH#10 (DP 15.1)	6,994.75	I#5 (DP 15)	6,995.50	53.9	-0.014	18.0	5.00	6.64	12.40	40.3	Concrete Pip	6,996.36	6,995.64
149: P-66	P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	6.10	4.60	106.64	5.7	Concrete Pip	6,989.54	6,989.51
150: P-68	P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	6.10	4.33	97.84	6.2	Concrete Pip	6,989.51	6,989.51
151: P-77	P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	3.60	7.70	38.62	9.3	Concrete Pip	6,990.98	6,989.93
152: P-74	P-74	MH#25 (DP13)	6,987.50	OUTLET SEG	6,986.67	173.3	0.005	48.0	26.00	6.66	99.34	26.2	Concrete Pip	6,989.01	6,988.30

5 YEAR FREE OUTFALL CONDITION: STRUCTURE SUMMARY TABLE

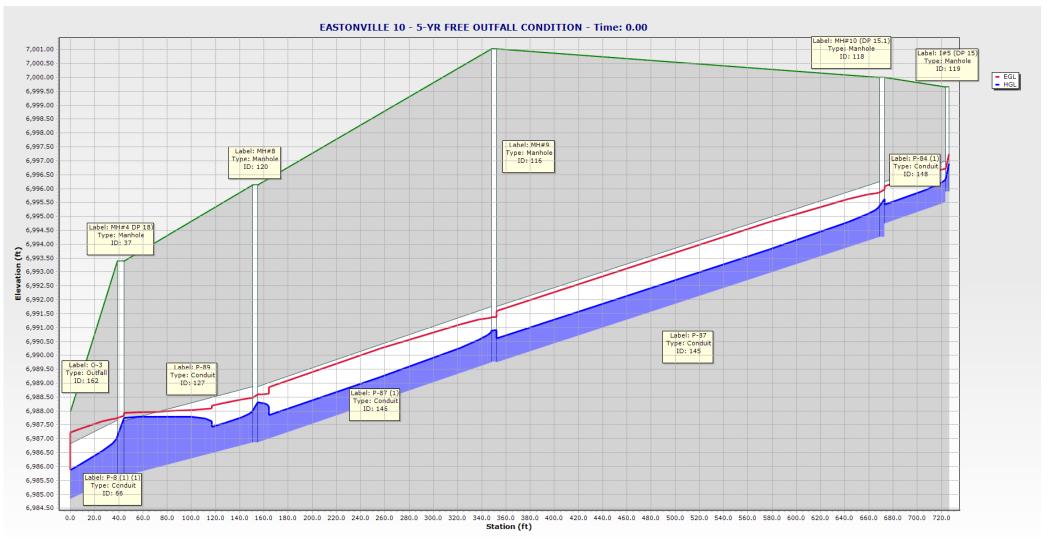
	Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Depth (Out) (ft)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Notes	Headloss (ft)
35: MH#7	MH#7	6,993.52	6,993.52	7.90	0.85	6,986.22	6,986.42	STORM MH	0.19
36: I#1 (DP 16	I#1 (DP 16)	6,993.41	6,993.41	3.00	0.66	6,990.40	6,990.77	CDOT Type-	0.38
37: MH#4 DP	MH#4 DP 18)	6,993.40	6,993.40	15.60	1.42	6,987.09	6,987.76	STORM MH	0.67
38: I#2 (DP 17	I#2 (DP 17)	6,993.39	6,993.39	6.30	0.90	6,989.68	6,990.02	CDOT Type-	0.35
39: MH#6	MH#6	6,993.02	6,993.02	7.90	0.85	6,985.35	6,985.54	STORM MH	0.19
40: MH#5	MH#5	6,991.91	6,991.91	7.90	0.85	6,984.97	6,985.17	STORM MH	0.19
41: MH#3 (DP	MH#3 (DP 8)	6,991.13	6,991.13	8.30	0.56	6,981.67	6,981.95	STORM MH	0.28
42: I#3 (DP 7)	I#3 (DP 7)	6,990.73	6,990.73	7.90	0.93	6,986.58	6,987.03	CDOT Type-	0.45
43: 18 (DP 19)	18 (DP 19)	6,988.71	6,988.71	0.30	1.96	6,983.47	6,983.57	CDOT Type-	0.10
44: MH#2 (DP	MH#2 (DP 8)	6,985.74	6,985.74	8.30	0.87	6,981.30	6,981.50	STORM MH	0.20
45: I#4 (DP 13		6,985.02	6,985.02	2.10	1.04	6,982.35	6,982.45	CDOT Type-	0.10
46: I#5 (DP 14	I#5 (DP 14)	6,985.02	6,985.02	3.90	1.09	6,982.13	6,982.34	CDOT Type-	0.21
47: MH#1	MH#1	6,984.95	6,984.95	8.30	0.87	6,980.92	6,980.95	STORM MH	0.03
49: 44 (69) (D	44 (69) (DP 15)	6,982.64	6,982.64	0.30	0.20	6,978.63	6,978.63	CDOT Type-	0.01
55: 44 (80)	44 (80)	6,975.21	6,975.21	4.20	0.62	6,971.37	6,971.38	Cylindrical S	0.01
56: 44 (81)	44 (81)	6,975.03	6,975.03	0.50	0.26	6,970.30	6,970.31	Cylindrical S	0.01
	I#7 (DP 9)	6,974.64	6,974.64	2.20	0.56	6,972.51	6,972.82	CDOT Type-	0.31
58: I#8 (DP 10		6,974.64	6,974.64	4.20	0.72	6,971.90	6,972.17	CDOT Type-	0.27
59: I#6 (DP 1)	I#6 (DP 1)	6,973.20	6,973.20	0.50	0.26	6,971.11	6,971.25	CDOT Type-	0.14
60: 44 (78) (D	44 (78) (DP 11)	6,973.16	6,973.16	0.40	0.23	6,968.66	6,968.74	CDOT Type-	0.08
98: MH#26 (D	MH#26 (DP6.1)	7,027.15	7,027.15	2.90	0.59	7,021.09	7,021.47	STORM MH	0.38
99: MH#27 (D	MH#27 (DP8)	7,027.09	7,027.09	2.00	0.49	7,021.49	7,021.65	STORM MH	0.16
100: I#9 (DP6)		7,027.04	7,027.04	1.20	0.41	7,023.41	7,023.50	CDOT Type-	0.09
101: I#8 (DP5)		7,026.63	7,026.63	0.70	0.31	7,024.31	7,024.47	CDOT Type-	0.16
	I#7 (DP3, 1)	7,026.51	7,026.51	1.60	0.97	7,022.27	7,022.28	CDOT Type-	0.01
102: I#6 (DP2.	·	7,026.40	7,026,40	0.80	0.33	7,022.69	7,022.87	CDOT Type-	0.18
106: MH#34	MH#34	7,023.51	7,023.51	1.70	0.49	7,019.50	7,019.59	CDOT Type-	0.08
111: MH#21	MH#21	7,014.03	7,014.03	6.10	0.72	6,999.24	6,999.57	STORM MH	0.33
112: MH#20	MH#20	7,011.03	7,012,41	6,10	0.72	7,001.90	7.001.91	STORM MH	0.01
112: MH#19	MH#19	7,012.41	7,012.41	6.10	0.72	7,001.50	7,001.91	STORM MH	0.33
115: MH#22	MH#22	7,010.85	7,010.85	6.10	0.72	6,995.87	6,995.88	STORM MH	0.01
115: MH#22 116: MH#9	MH#9	7,003.83	7,003.83	10.20	1.14	6,990.90	6,990.92	STORM MH	0.01
117: I#4 (DP1	I#4 (DP14)	7,001.03	7,001.03	5.20	0.88	6,996.57	6,997.11	CDOT Type-	0.55
117: 1#4 (DF1 118: MH#10 (MH#10 (DP 1	7,000.17	7,000.17	10.20	1.14	6,995.39	6,995.64	STORM MH	0.33
119: I#5 (DP 1		6,999.67	6,999.67	5.00	0.46	6,996.36	6,996.89	CDOT Type-	0.53
120: MH#8	1#5 (DP 15) MH#8	6,996.13	6,999.07	10.20	1.15	6,988.02	6,988.32	STORM MH	0.33
120: MH#0 121: MH#23	MH#23	6,996.13	6,996.13	6.10	0.72	6,989.54	6,989.55	STORM MH	0.30
121: MH#23 122: MH#24	MH#23 MH#24	6,997.20	6,997.20	6.10	1.51	6,989.54	6,989.55	STORM MH	0.01
122: MH#24 123: DP12	MH#24 DP12	6,996.25	6,996.25	3.60	0.67	6,989.51	6,989.51		0.00
123: DP12 124: MH#25 (26.00	1.51			CDOT Type-	0.36
	MH#25 (DP13)	6,995.75	6,995.75			6,989.01	6,989.51	STORM MH	0.50
190: INLET (D	INLET (DP 3)	6,980.96	6,980.96	3.70	0.63	6,978.80	6,979.13	CDOT FES	
192: DP 7	DP 7	7,024.45	7,024.45	0.30	0.21	7,023.22	7,023.33	CDOT FES	0.11
193: DP 2	DP 2	7,024.26	7,024.26	1.70	0.45	7,021.71	7,021.95	CDOT FES	0.24
194: DP 3	DP 3	7,009.43	7,009.43	6.10	0.72	7,005.73	7,006.10	CDOT FES	0.37
	CULVERT 1 (7,000.01	7,000.01	11.20	0.34	6,997.35	6,997.61	Dummy Null	0.25
197: CULVERT	CULVERT 2 (7,000.01	7,000.01	11.20	0.34	6,997.35	6,997.61	Dummy Null	0.25

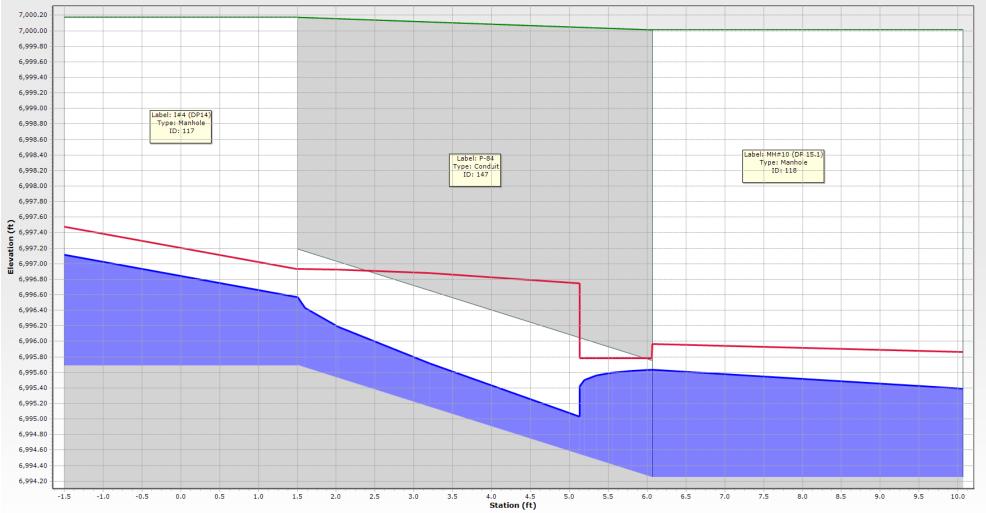
	Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
48: OUTFALL	OUTFALL	6,983.32	6,979.44		6,980.17	8.30	CDOT FES
53: 44 (70)	44 (70)	6,979.33	6,977.55		6,977.71	0.30	CDOT FES
54: 44 (65)	44 (65)	6,976.31	6,973.52		6,973.93	3.70	CDOT FES
61: 44 (77)	44 (77)	6,971.10	6,969.39		6,969.61	0.50	CDOT FES
64: 44 (79)	44 (79)	6,969.82	6,967.50		6,967.68	0.40	CDOT FES
107: DP9	DP9	7,022.74	7,019.00		7,019.39	2.90	CDOT FES
108: FES OUTF	FES OUTFALL 1	7,023.00	7,021.01		7,021.33	1.60	CDOT FES
110: MH#39	MH#39	7,018.18	7,017.01		7,017.39	1.70	CDOT FES
125: OUTLET S	OUTLET SEG	6,991.09	6,986.67	6,988.30	6,988.30	26.00	CDOT FES
162: 0-3	0-3	6,988.37	6,984.83		6,985.89	15.60	Dummy Null
164: 0-5	0-5	6,982.10	6,981.08	6,982.10	6,982.10	3.90	Dummy Null
165: 0-6	0-6	6,972.87	6,970.61		6,971.31	4.20	Dummy Null
203: 0-7	0-7	6,998.27	6,995.27		6,995.49	11.20	Dummy Null
207: 0-10	O-10	6,998.27	6,995.27		6,995.49	11.20	Dummy Null

NOTE: SEE PROFILES BELOW FOR PIPES STUDIED WITH THIS ANALYSIS



EASTONVILLE 12 - INLET - 5-YR FREE OUTFALL CONDITION





EASTONVILLE 11 - 5-YR FREE OUTFALL CONDITION - Time: 0.00



Eastonville Road Final Drainage Report Project No.: 201662.08

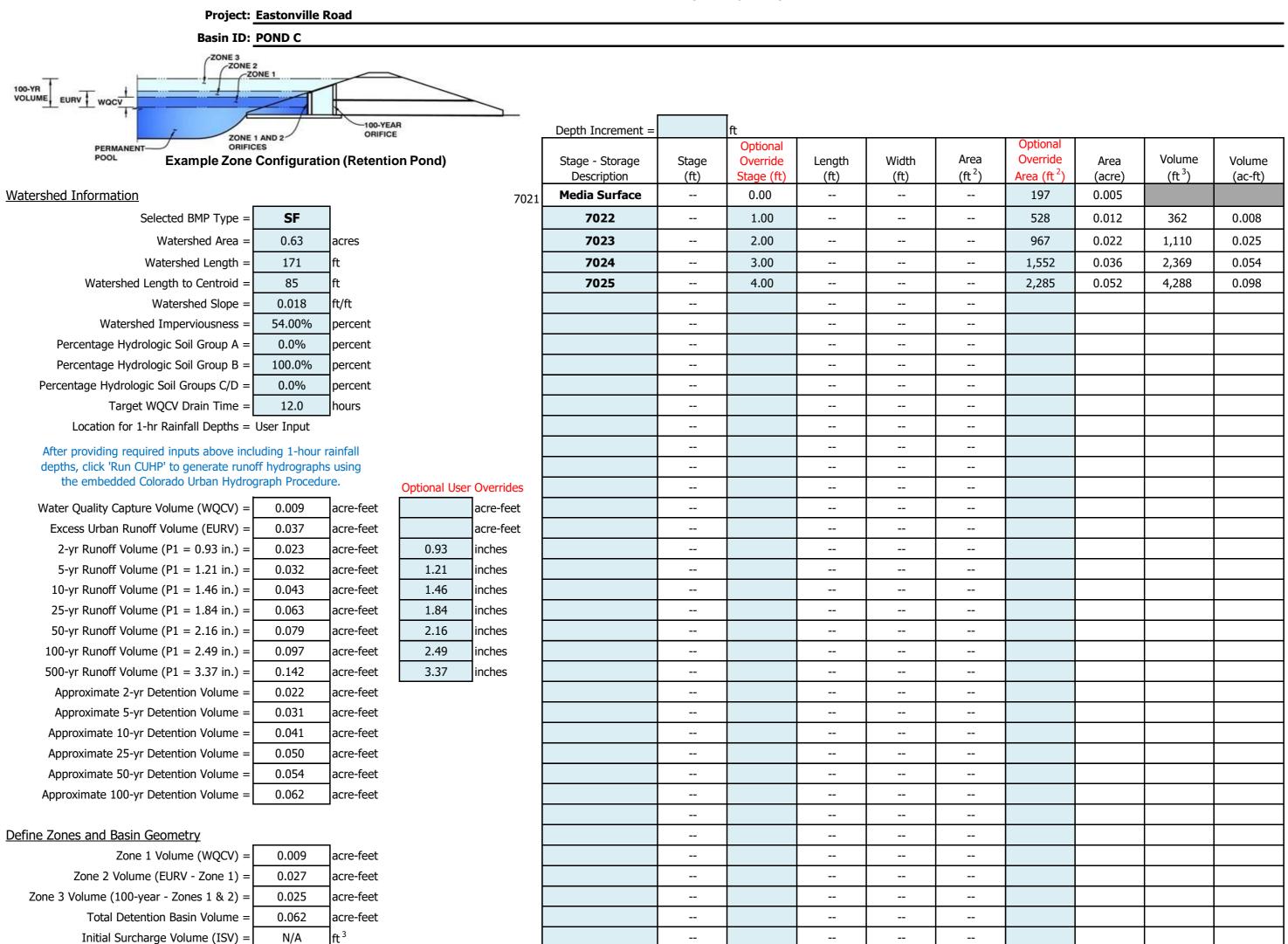
APPENDIX D – WATER QUALITY & DETENTION

	Design Procedure Forn	n: Sand Filter (SF)						
	UD-BMP (Version 3.07	, March 2018)	Sheet 1 of 2					
Designer:								
Company: Date:	HR Green January 30, 2024							
Project:	Eastonville Road - Segment 2 Improvements							
Location:	El Paso County, CO							
1. Basin Sto	rage Volume							
	ve Imperviousness of Tributary Area, ${\rm I_a}$, if all paved and roofed areas upstream of sand filter)	I _a = 54.0 %						
B) Tribut	ary Area's Imperviousness Ratio (i = $I_a/100$)	i = 0.540						
	r Quality Capture Volume (WQCV) Based on 12-hour Drain Time $CV=0.8 * (0.91* i^3 - 1.19 * i^2 + 0.78 * i)$	WQCV = 0.17 watershed inches						
D) Contr	ibuting Watershed Area (including sand filter area)	Area = 27,443 sq ft						
	Quality Capture Volume (WQCV) Design Volume	V _{WQCV} = <u>398</u> cu ft						
	atersheds Outside of the Denver Region, Depth of age Runoff Producing Storm	d ₆ = in						
	/atersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	V _{WQCV OTHER} =Cu ft						
	Input of Water Quality Capture Volume (WQCV) Design Volume if a different WQCV Design Volume is desired)	V _{WQCVUSER} =cu ft						
2. Basin Ge	ometry							
A) WQC\	/ Depth	$D_{WQCV} = 1.0$ ft						
	Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = 4.00 ft / ft						
C) Minimu	um Filter Area (Flat Surface Area)	A _{Min} = <u>185</u> sq ft						
D) Actual	Filter Area	A _{Actual} = 200 sq ft						
E) Volum	e Provided	$V_T = 4288$ cu ft						
3. Filter Mat	erial	Choose One 18" CDOT Class B or C Filter Material Other (Explain):						
4. Underdra	in System	Choose One						
A) Are un	derdrains provided?	YES						
B) Under	drain system orifice diameter for 12 hour drain time	O NO						
	i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice	y = 2.0 ft						
	ii) Volume to Drain in 12 Hours	Vol ₁₂ = <u>398</u> cu ft						
	iii) Orifice Diameter, 3/8" Minimum	D ₀ = 7/16 in						

	Design Procedure Forr	m: Sand Filter (SF)	
	000		Sheet 2 of 2
Designer:	SPC HR Green		
Company: Date:	January 30, 2024		
Project:	Eastonville Road - Segment 2 Improvements		
Location:	El Paso County, CO		
Location.			
A) Is an	able Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One	
	tlet Works ribe the type of energy dissipation at inlet points and means of eying flows in excess of the WQCV through the outlet	Engery dissapation at inlet points provide of conveying flows in excess of the WQC modified type 'C' inlet outlet structure gra	V through the outlet is via the
Notes:			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

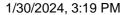


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Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H_{TC}) =	N/A	ft
Slope of Trickle Channel (S_{TC}) =	N/A	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
Initial Surcharge Area (A_{ISV}) =	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft

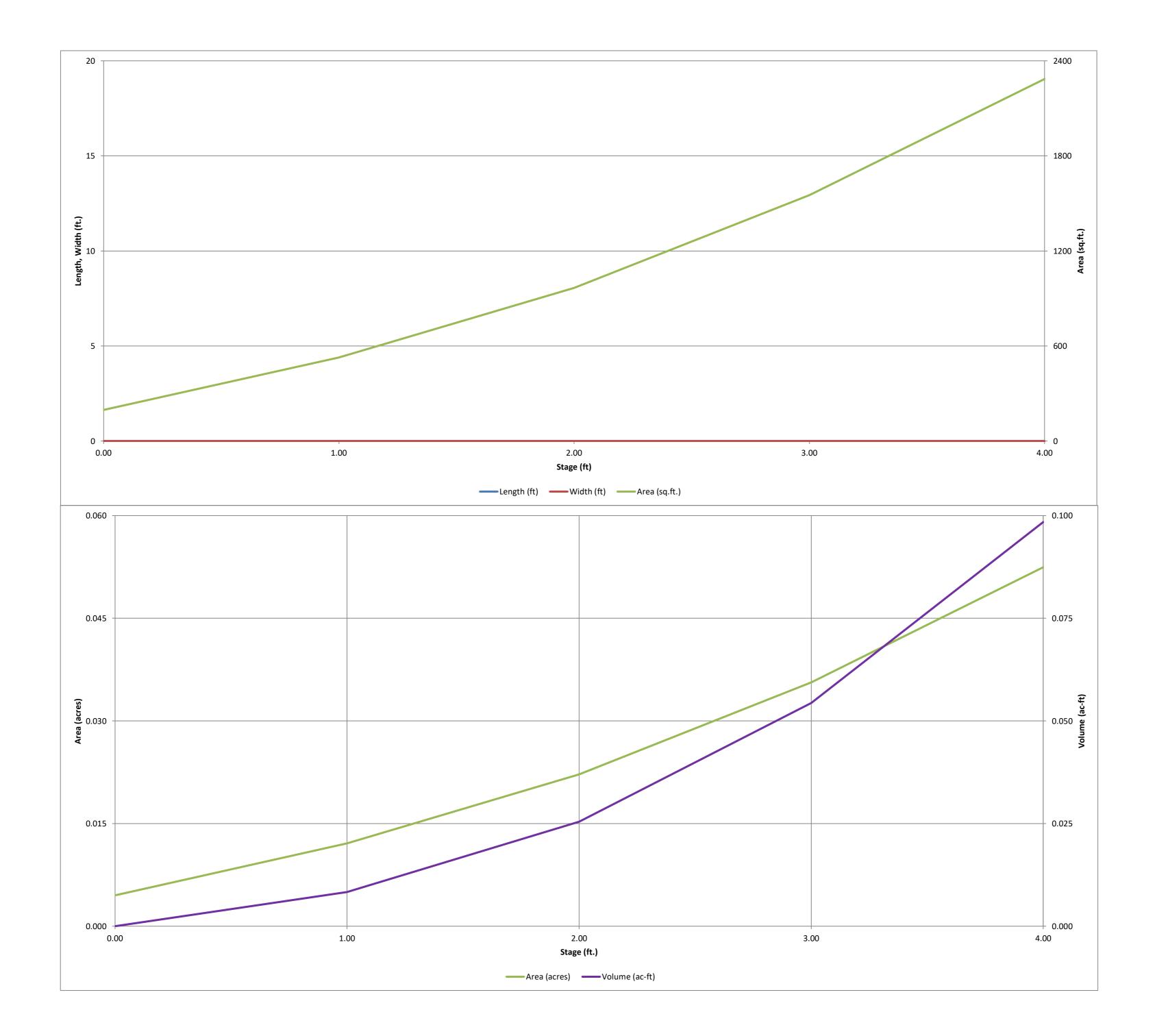
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet



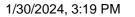


DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)







	DE			FLET STRU rsion 4.05 (Januar		SIGN			
Project:	Eastonville Road	ורזויז	-D-Delention, νει	SIULI 4.05 (Janual	y 2022)				
Basin ID:									
ZONE 3				Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)			Filtration Media			
	100-YEAR		Zone 2 (EURV)			Filtration Media			
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)			Weir&Pipe (Restrict)			
	Configuration (R			Total (all zones)		Weirdripe (Restrict)	J		
ser Input: Orifice at Underdrain Outlet (typical	vused to drain W(OCV in a Filtration F	RMD)		0.002	1	Calculated Parame	eters for Underdrai	'n
Underdrain Orifice Invert Depth =	-	ft (distance below	-	surface)	Underc	Irain Orifice Area =		ft ²	<u></u>
Underdrain Orifice Diameter =	0.47	inches				Orifice Centroid =		feet	
	-]	
ser Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically use	d to drain WQCV a	nd/or EURV in a se	dimentation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	N/A	ft (relative to basi	n bottom at Stage	= 0 ft)	WQ Orifi	ce Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basi	n bottom at Stage	= 0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A inches Elliptical Slot Centroid						N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	lliptical Slot Area =	N/A	ft ²	
ser Input: Stage and Total Area of Each Orific	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)]
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
			_		-				_
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
ser Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	eters for Vertical O	rifice
	Not Selected	Not Selected]				Not Selected	Not Selected	7
Invert of Vertical Orifice =	N/A		ft (relative to basi	n bottom at Stage =	= 0 ft) Ver	tical Orifice Area =		N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A		ft (relative to basi	n bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =		N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
			_						
ser Input: Overflow Weir (Dropbox with Flat o		d Outlat Dina OD Da	ctangular/Tranczo	idal Wair and Na O	utlat Dina)		Calculated Parame	tors for Overflow	Weir
• • •	r Sloped Grate and	<u>a Outlet Pipe OR Re</u>			<u>utiet Pipe)</u>				
	<u>r Sloped Grate and</u> Zone 3 Weir	Not Selected			<u>utiet Pipe)</u>		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	•	Not Selected				e Upper Edge, H _t =	Zone 3 Weir		feet
	Zone 3 Weir	Not Selected N/A			ft) Height of Grate	e Upper Edge, H _t = /eir Slope Length =	Zone 3 Weir 2.50	Not Selected	

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

0.00

3.00

Type C Grate

50%

N/A

N/A

N/A

N/A

H:V

feet

%

63.46

6.26

3.13

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.00	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.10	N/A	ft ²
Outlet Pipe Diameter =	12.00	N/A	inches	Outlet Orifice Centroid =	0.11	N/A	feet
Restrictor Plate Height Above Pipe Invert =	2.20		inches Half-Central Angle of	Restrictor Plate on Pipe =	0.88	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Overflow Weir Grate Slope =

Horiz. Length of Weir Sides =

Overflow Grate Type =

Debris Clogging % =

Spillway Invert Stage=	2.86	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	12.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

N/A

N/A

N/A

ft²

ft²

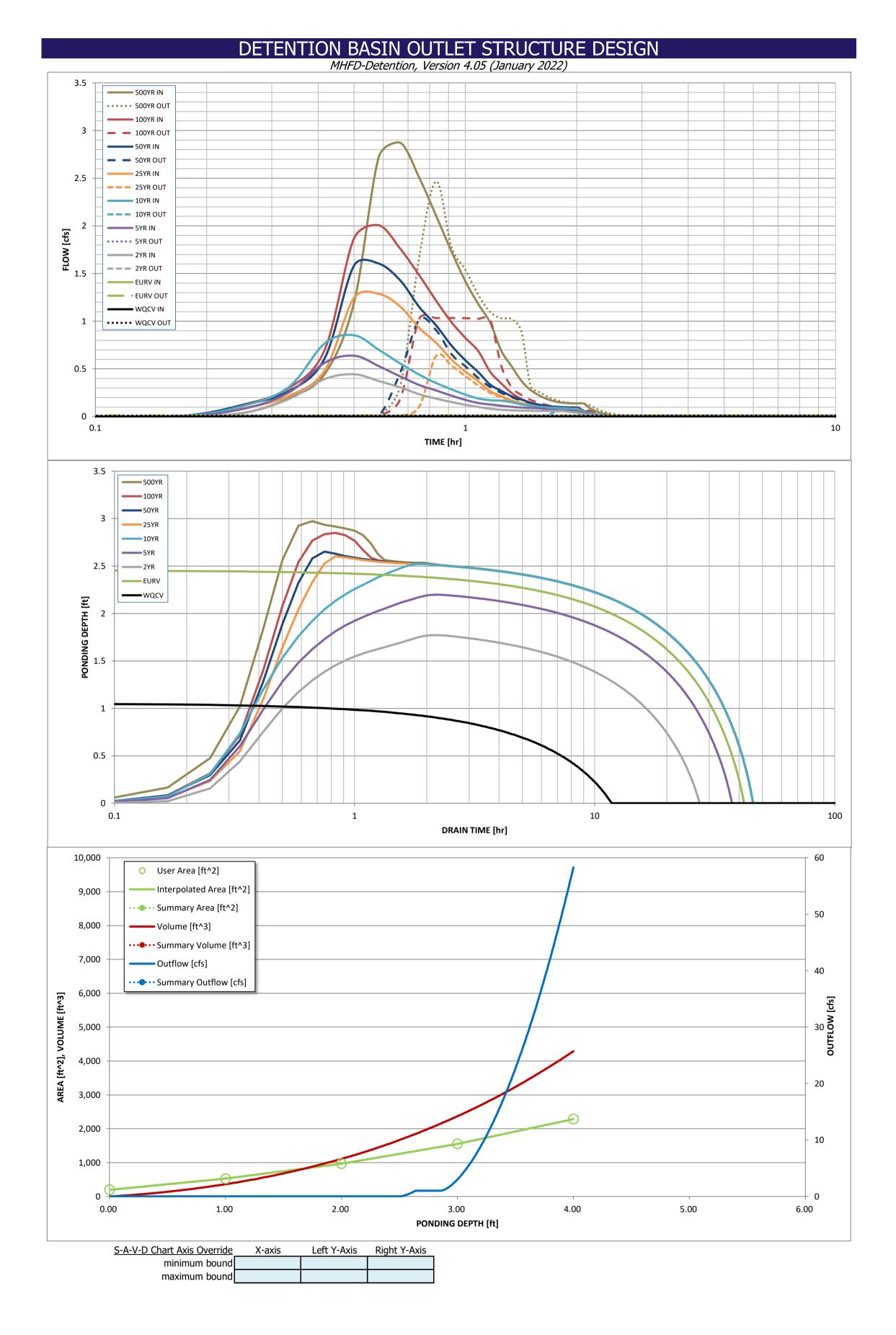
Spillway Design Flow Depth=	0.14	feet
Stage at Top of Freeboard =	4.00	feet
Basin Area at Top of Freeboard =	0.05	acres
Basin Volume at Top of Freeboard =	0.10	acre-ft

Grate Open Area / 100-yr Orifice Area =

Overflow Grate Open Area w/o Debris =

Overflow Grate Open Area w/ Debris =

Routed Hydrograph Results	The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	0.93	1.21	1.46	1.84	2.16	2.49	3.37
CUHP Runoff Volume (acre-ft) =	0.009	0.037	0.023	0.032	0.043	0.063	0.079	0.097	0.142
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.023	0.032	0.043	0.063	0.079	0.097	0.142
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.2	0.5	0.8	1.0	1.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.12	0.32	0.87	1.20	1.59	2.49
Peak Inflow Q (cfs) =	N/A	N/A	0.4	0.6	0.9	1.3	1.6	2.0	2.9
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.6	1.0	1.0	2.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.4	1.2	1.3	1.0	1.6
Structure Controlling Flow =	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.1	0.2	0.2	0.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	11	40	26	36	44	43	42	42	40
Time to Drain 99% of Inflow Volume (hours) =	12	41	27	37	45	45	45	44	44
Maximum Ponding Depth (ft) =	1.06	2.46	1.77	2.20	2.52	2.60	2.65	2.85	2.97
Area at Maximum Ponding Depth (acres) =	0.01	0.03	0.02	0.02	0.03	0.03	0.03	0.03	0.04
Maximum Volume Stored (acre-ft) =	0.009	0.037	0.021	0.030	0.039	0.041	0.043	0.049	0.053



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can o		lated inflow hyd	drographs from	this workbook v	with inflow hydro	ographs develop	ed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.04
	0:15:00	0.00	0.00	0.04	0.08	0.11	0.09	0.12	0.12	0.19
	0:20:00	0.00	0.00	0.18	0.25	0.31	0.22	0.27	0.30	0.45
	0:25:00	0.00	0.00	0.39	0.56	0.77	0.48	0.61	0.70	1.19
	0:30:00	0.00	0.00	0.44	0.64	0.85	1.25	1.58	1.87	2.72
	0:35:00	0.00	0.00	0.37	0.53	0.70	1.29	1.60	2.01	2.87
	0:40:00	0.00	0.00	0.31	0.42	0.56	1.15	1.43	1.76	2.51
	0:45:00	0.00	0.00	0.23	0.33	0.44	0.93	1.15	1.48	2.11
	0:50:00 0:55:00	0.00	0.00	0.19	0.27	0.35	0.77	0.96	1.22	1.73
	1:00:00	0.00	0.00	0.15	0.22 0.18	0.29 0.23	0.60 0.47	0.75	0.99 0.83	1.42 1.18
	1:05:00	0.00	0.00	0.12	0.18	0.23	0.47	0.39	0.69	0.99
	1:10:00	0.00	0.00	0.08	0.13	0.17	0.27	0.34	0.05	0.69
	1:15:00	0.00	0.00	0.07	0.11	0.17	0.22	0.27	0.35	0.53
	1:20:00	0.00	0.00	0.07	0.10	0.15	0.17	0.21	0.25	0.38
	1:25:00	0.00	0.00	0.06	0.10	0.13	0.14	0.18	0.19	0.28
	1:30:00	0.00	0.00	0.06	0.09	0.11	0.12	0.15	0.15	0.22
	1:35:00	0.00	0.00	0.06	0.09	0.10	0.10	0.12	0.12	0.18
	1:40:00	0.00	0.00	0.06	0.08	0.10	0.09	0.11	0.11	0.16
	1:45:00	0.00	0.00	0.06	0.07	0.09	0.09	0.10	0.10	0.14
	1:50:00	0.00	0.00	0.06	0.06	0.09	0.08	0.10	0.09	0.14
	1:55:00 2:00:00	0.00	0.00	0.05 0.04	0.06	0.08	0.08	0.10	0.09	0.14
	2:05:00	0.00	0.00	0.04	0.08	0.08	0.08	0.10	0.09	0.14
	2:10:00	0.00	0.00	0.03	0.04	0.03	0.03	0.00	0.00	0.06
	2:15:00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.02	0.04
	2:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	2:25:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00 2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00 3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

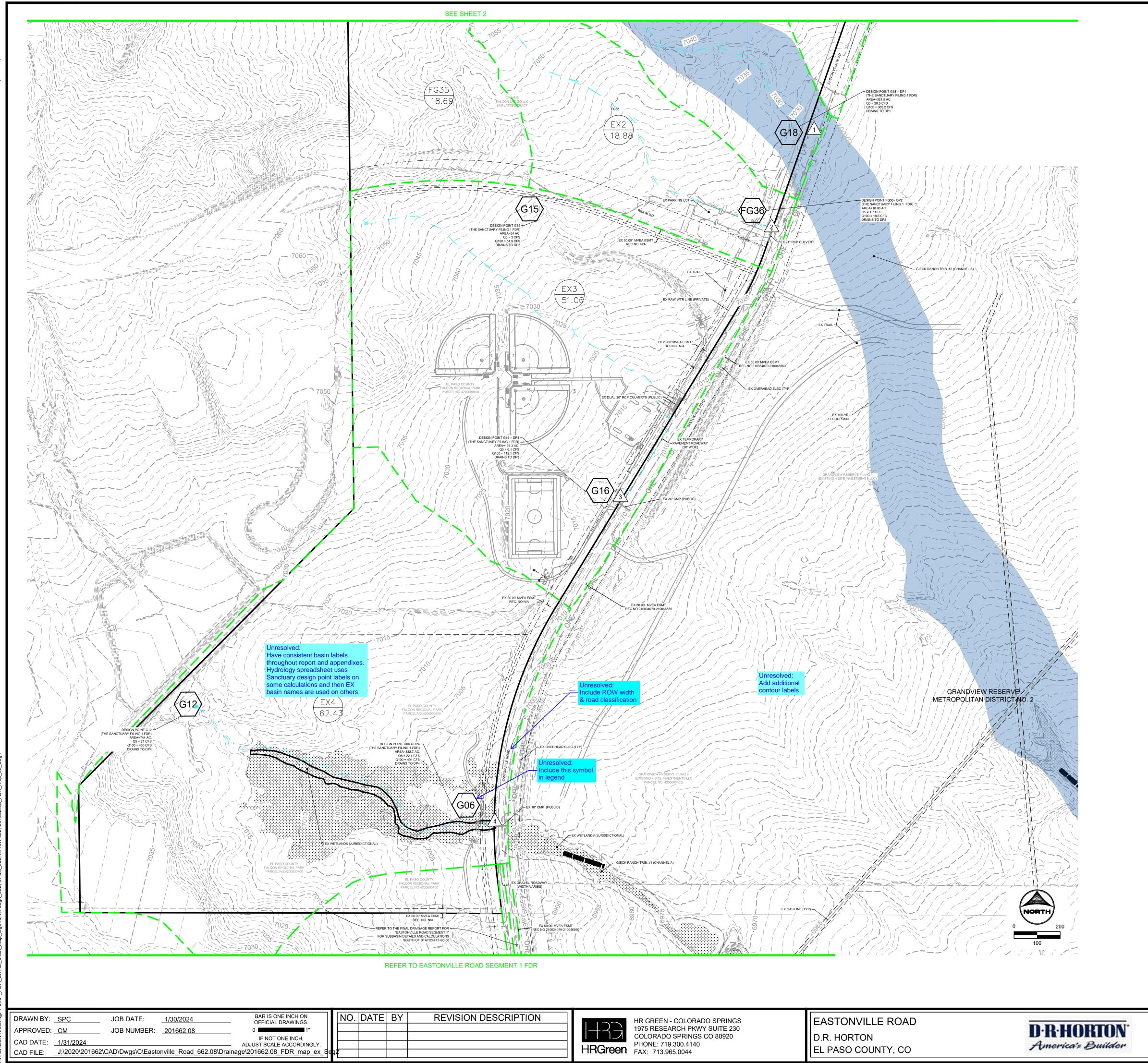
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor) from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of all
							outlets (e.g. vertical orifice,
							overflow grate, and spillway,
							where applicable).
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Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX E – DRAINAGE MAPS



LEGEND:

EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR EX STORM SEWER EX DRAINAGE SWALE EX PROPERTY LINE EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN — — — 5250 [·] — — _____

13

AREA

DESIGN POINT

nresolved:

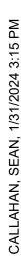
- Add Basin and Design Point Summary Tables

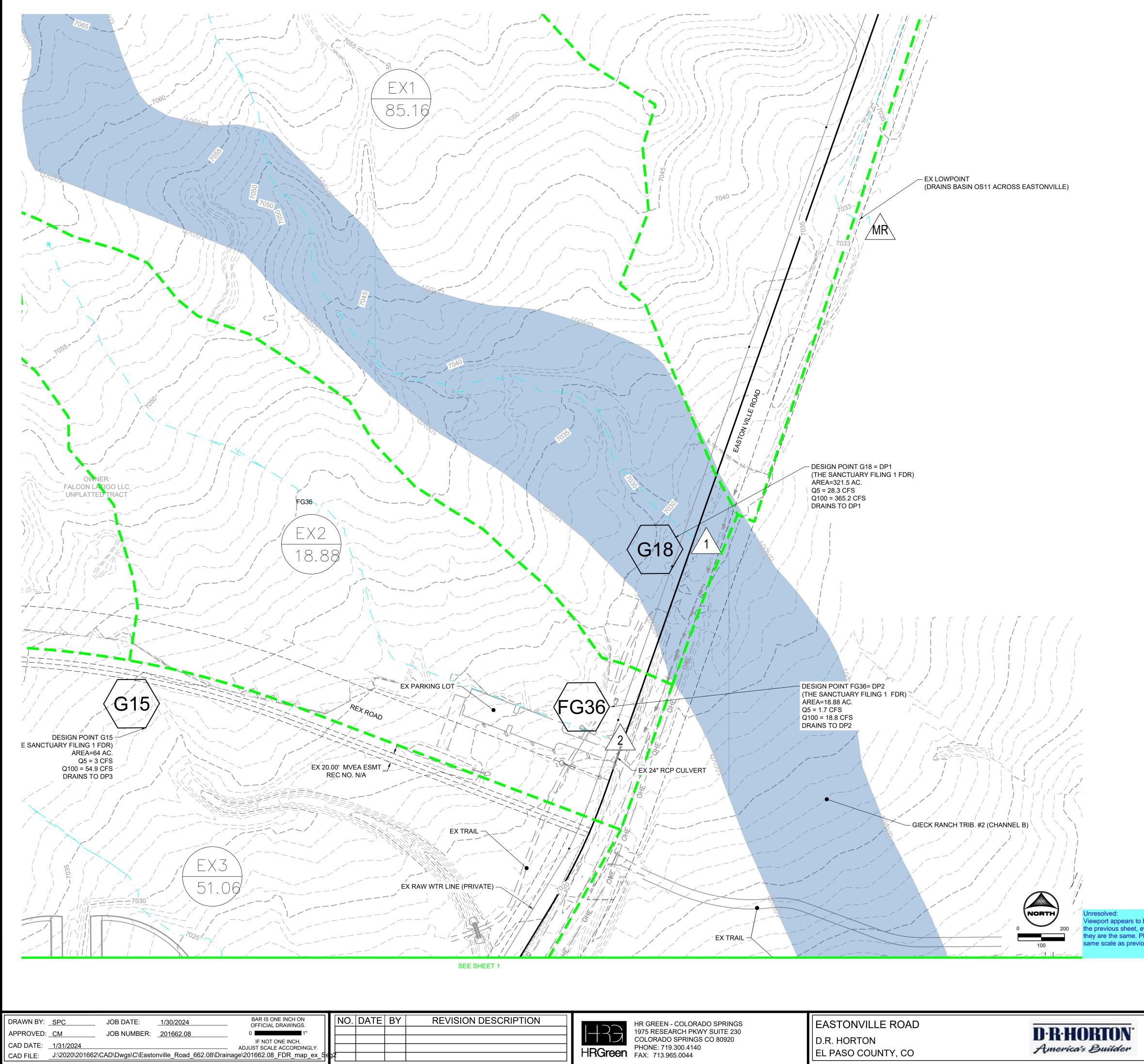
- Text is hard to read, suggest making it a little larger

-Could not find Design Points G15, G18, FG36, or G16 in the Sanctuary FDR for comparison. Recommended highlighting them in the reference section.

- Label all existing easements (all maps)

PROPOSED BASIN LABEL





|--|

EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR EX STORM SEWER EX DRAINAGE SWALE EX PROPERTY LINE EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN — — — 5250 [·] — — _____

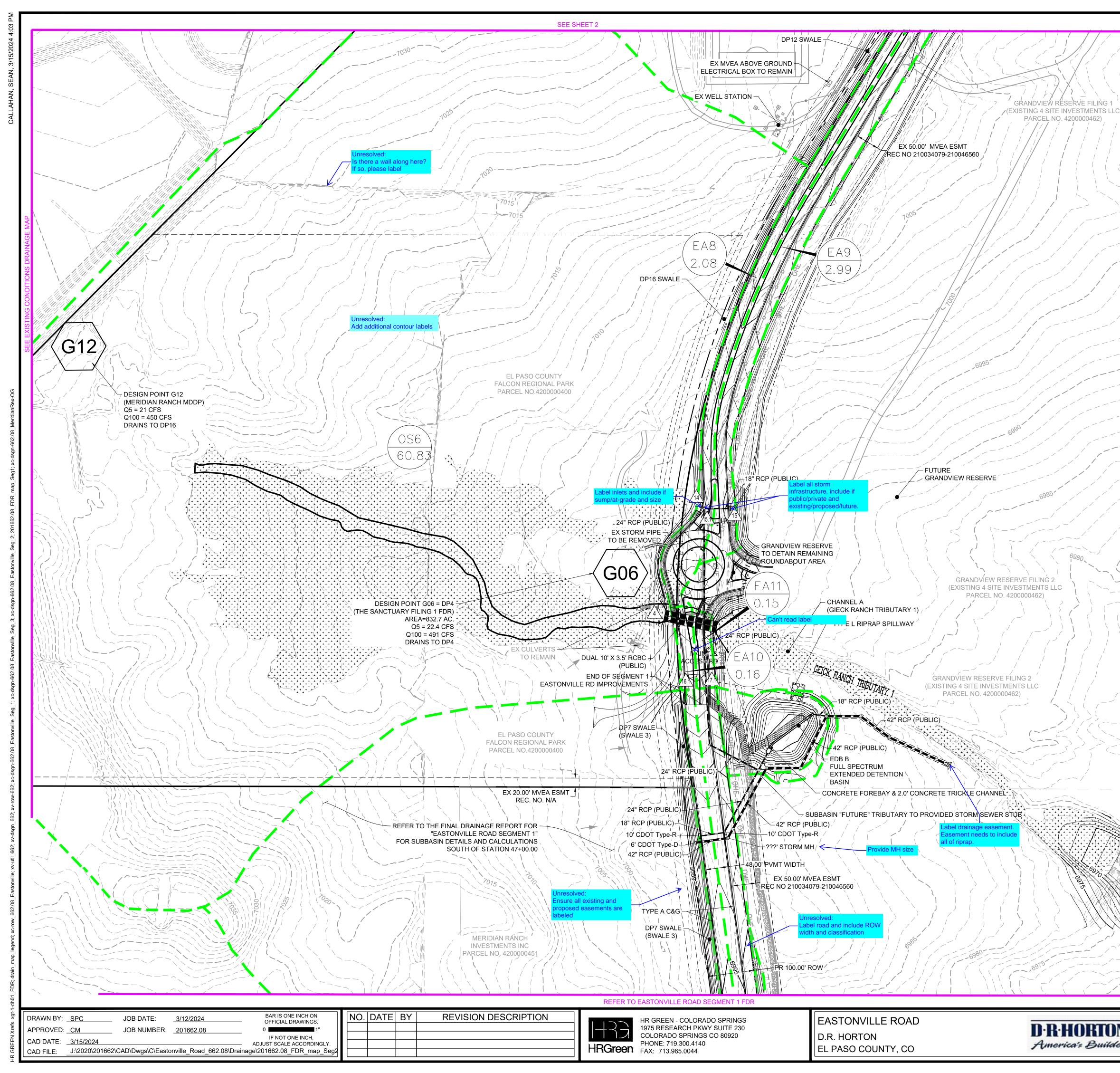
13

DESIGN POINT

PROPOSED BASIN LABEL



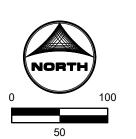
Viewport appears to be at a larger scale than the previous sheet, even though scales say they are the same. Please have viewport at same scale as previous sheet.











	3	G16	6.1	112.1
	3.1	EA2, DP2.1	1.6	3.2
	4	G06	22.4	491.0
	4.1	EA5, DP3.1	1.7	3.4
	5	EA3	0.7	1.3
	6	DP5, EA4	1.2	2.4
	6.1	DP6, DP8	2.9	22.4
	7 OS3 8 DP2, DP7 9 DP6.1 10 EA6, EA7		0.3	2.2
			2.0	21.0
			2.9	22.4
			5.6	9.9
	11 OS4, DP9		7.5	44.0
	12 OS7		3.6	24.4
	13 DP2, DP12		26.0	136.4
	14 EA8		5.2	8.8
	15 EA9 15.1 DP14, DP15		5.0	10.4
			10.2	19.1
	16.1	EA10	0.6	1.1
	17.1	EA11	0.5	1.0

DESIGN POINT SUMMARY TABLE								
ESIGN POINT	CONTRIBUTING BASINS	SQ5 (cfs)	SQ100 (c					

G18

FG36

EA1

1

2

2.1

AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

28.3

1.7

0.8

365.2

18.8

1.5

These are design point	7.7
labels. Please move to	
design point table and list corresponding basins in	

this table.

	SUMMARY RUNOFF TABLE								
	BASIN AREA (ac)		% IMPERVIOUS	Q5 (cfs)	Q100 (cfs)				
	EA1	0.22	73	0.8	1.5				
	EA2	0.25	72	0.9	1.7				
	EA3	0.20	70	0.7	1.3				
	EA4	0.17	65	0.5	1.1				
	EA5	0.16	0	0.1	0.4				
	EA6	0.70	100	3.2	5.3				
	EA7	0.65	89	2.6	4.8				
	EA8	2.08	99	5.2	8.8				
	EA9	2.99	63	5.0	10.4				
	EA10	0.16	75	0.6	1.1				
	EA11	0.15	67	0.5	1.0				
	<mark>∕</mark> *G18	321.53	-	28.3	365.2				
	*FG36	18.88	-	1.7	18.8				
	OS3	1.00	2	0.3	2.2				
	OS4	9.60	9	4.8	21.6				
$\overline{\ }$	*G16	131.26	-	6.1	112.1				
	* G06	832.70	-	22.4	491.0				
	OS7	11.42	2	3.6	24.4				

)S1, OS2, OS6 & FG35 in ummary table.

XX

DESIGN POINT PER MERIDIAN RANCH

LEGEND:

EXISTING MAJOR CONTOUR

EXISTING MINOR CONTOUR

PROPOSED STORM SEWER

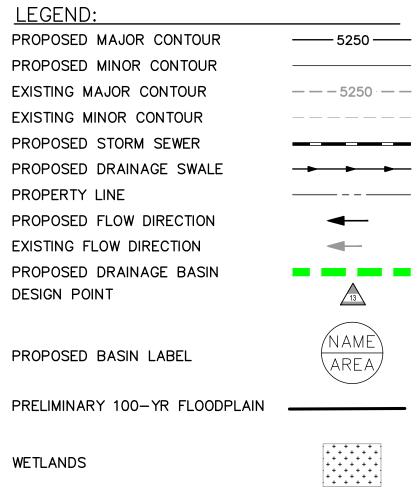
EXISTING FLOW DIRECTION

PROPOSED BASIN LABEL

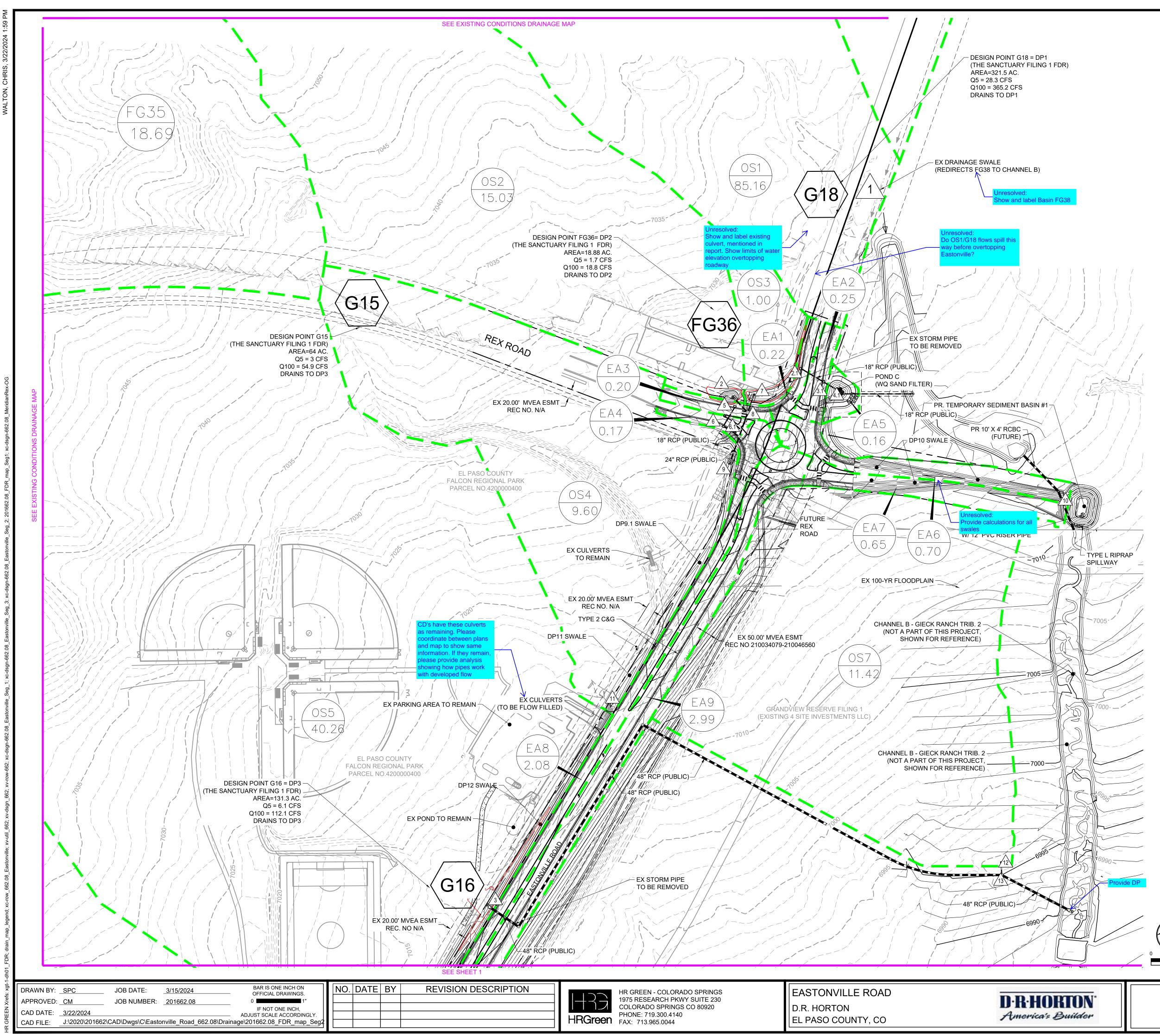
PROPERTY LINE

DESIGN POINT

WETLANDS







2.1

3

3.1

4

4.1

5

6

6.1

7

8

9

10

11

12

13

14

15

15.1

16.1

17.1

NORTH



365.2

18.8

1.5

112.1

3.2

491.0

3.4

1.3

2.4

22.4

2.2

21.0

22.4

9.9

44.0

24.4

136.4

8.8

10.4

19.1

1.1

1.0

2

LEGEND: PROPOSED MAJOR CONTOUR PROPOSED MINOR CONTOUR _____ EXISTING MAJOR CONTOUR — — — 5250 · — — EXISTING MINOR CONTOUR PROPOSED STORM SEWER PROPOSED DRAINAGE SWALE PROPERTY LINE _____ PROPOSED FLOW DIRECTION ◀--EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN DESIGN POINT 13 (NAME) PROPOSED BASIN LABEL AREA PRELIMINARY 100-YR FLOODPLAIN WETLANDS

DESIGN POINT PER MERIDIAN RANCH

XX

SUMMARY RUNOFF TABLE								
BASIN	AREA (ac)	% IMPERVIOUS	Q5 (cfs)	Q100 (cfs)				
EA1	0.22	73	0.8	1.5				
EA2	0.25	72	0.9	1.7				
EA3	0.20	70	0.7	1.3				
EA4	0.17	65	0.5	1.1				
EA5	0.16	0	0.1	0.4				
EA6	0.70	100	3.2	5.3				
EA7	0.65	89	2.6	4.8				
EA8	2.08	99	5.2	8.8				
EA9	2.99	63	5.0	10.4				
EA10	0.16	75	0.6	1.1				
EA11	0.15	67	0.5	1.0				
*G18	321.53	-	28.3	365.2				
*FG36	18.88	-	1.7	18.8				
OS3	1.00	2	0.3	2.2				
OS4	9.60	9	4.8	21.6				
*G16	131.26	-	6.1	112.1				
*G06	832.70	-	22.4	491.0				
OS7	11.42	2	3.6	24.4				

OS7 | 11.42 | 2 * AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR DESIGN POINT SUMMARY TABLE DESIGN CONTRIBUTING SQ5 (cfs) SQ100 (cfs) POINT BASINS G18 28.3 1 FG36 1.7 2

EA1

GP16, DP11

EA2, DP2.1

G06

EA5, DP3.1

EA3

DP5, EA4

DP6, DP8

OS3

DP2, DP7

DP6.1

EA6, EA7

OS4, DP9

OS7

EA8

EA9

DP14, DP15

EA10

EA11

DP3, DP12

0.8

6.1

1.6

22.4

1.7

0.7

1.2

2.9

0.3

2.0

2.9

5.6

7.5

3.6

26.0

5.2

5.0

10.2

0.6

0.5

SHEET